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INTERVENTO

FONDO COMPLEMENTARE AL PIANO NAZIONALE DI RIPRESA E RESILIENZA
PROGRAMMA "SICURO, VERDE E SOCIALE: RIQUALIFICAZIONE DELL'EDILIZIA RESIDENZIALE PUBBLICA"

**PROGETTO DI MANUTENZIONE STRAORDINARIA PER IL RESTAURO E RISANAMENTO
CONSERVATIVO DI DUE CASAMENTI A CORTE SITI IN
COMUNE DI BOLOGNA LOCALITA' CIRENAICA.
VIA LIBIA CIV. 29÷51 PER COMPLESSIVI 70 ALLOGGI
DI ERP CON RELATIVE PERTINENZE E PARTI COMUNI**

LOTTO **3053/PN_2**

PROGETTO ESECUTIVO

TAV. TAB_15		OGGETTO TABULATI DI CALCOLO CIVICO 43-45 STATO DI FATTO			DATA Settembre 2022	
SCALA					N. DISEGNO	
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03						

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TABULATI DI CALCOLO
CIVICI 43-45
STATO DI FATTO



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1 Risultati numerici

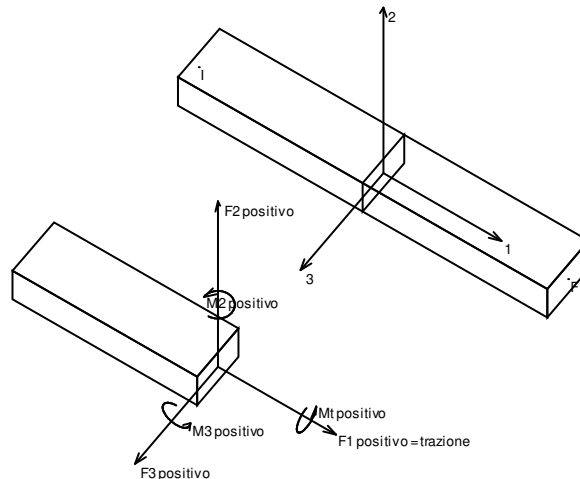
1.1 Sollecitazioni

1.1.1 Sollecitazioni aste

1.1.1.1 Convenzioni di segno aste

Le abbreviazioni relative alle sollecitazioni sugli elementi aste sono da intendersi:

- $F1$ (N): sforzo normale nell'asta;
- $F2$: sforzo di taglio agente nella direzione dell'asse locale 2;
- $F3$: sforzo di taglio agente nella direzione dell'asse locale 3;
- $M1$ (Mt): momento attorno all'asse locale 1; equivale al momento torcente;
- $M2$: momento attorno all'asse locale 2;
- $M3$: momento attorno all'asse locale 3.



La convenzione sui segni per i parametri di sollecitazione delle aste è la seguente:

presa un'asta con nodo iniziale i e nodo finale f , asse 1 che va da i a f , assi 2 e 3 presi secondo quanto indicato nei paragrafi successivi relativi al sistema locale delle aste sezionando l'asta in un punto e considerando la sezione sinistra del punto in cui si è effettuato il taglio (sezione da cui esce il versore asse 1) i parametri di sollecitazione sono positivi se hanno verso e direzione concordi con il sistema di riferimento locale dell'asta 1, 2, 3 (per i momenti si adotta la regola della mano destra).

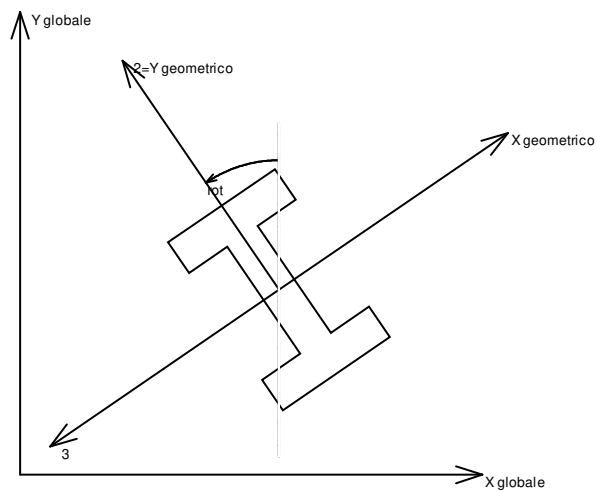
Il sistema è definito diversamente per tre categorie di aste, a seconda che siano originate da:

- aste verticali ad esempio pilastri e colonne;
- aste non verticali non di c.a., ad esempio travi di acciaio o legno;
- aste non verticali in c.a.: travi in c.a. di piano, falda o a quota generica.

Nel seguito si indica con 1, 2 e 3 il sistema locale dell'asta che non sempre coincide con gli assi principali della sezione. Si ricorda che per assi principali si intendono gli assi rispetto a cui si ha il raggio di inerzia minimo e massimo. Gli assi 1, 2 e 3 rispettano la regola della mano destra.

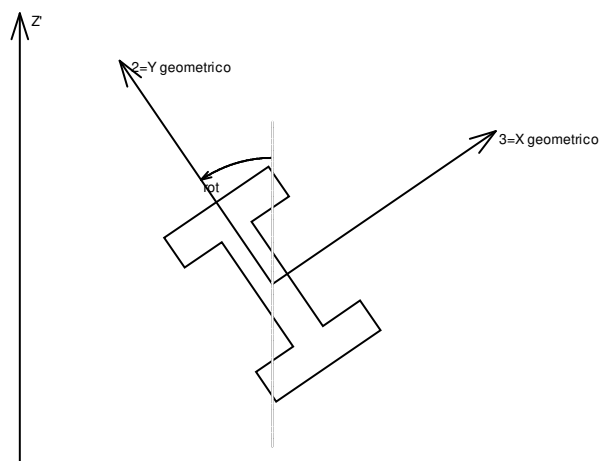


Sistema locale aste verticali



Nella figura si considera l'asse 1 uscente dal foglio (l'osservatore guarda in direzione opposta a quella dell'asse 1).

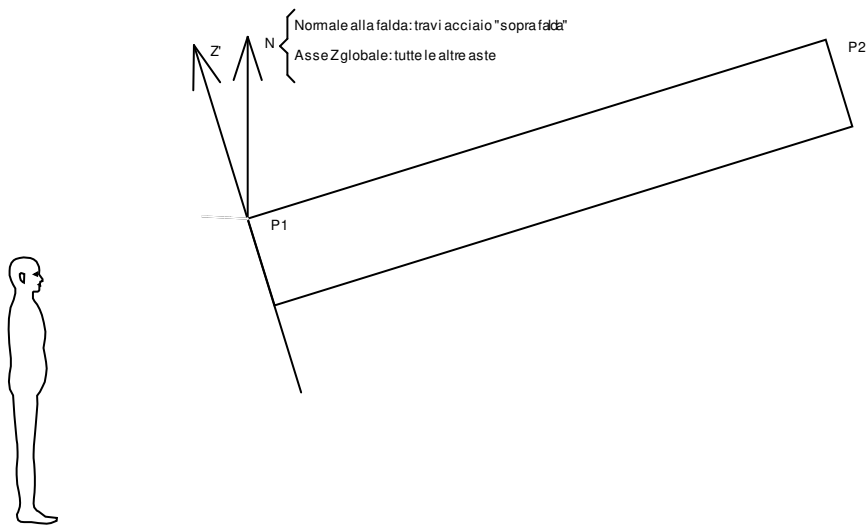
Sistema locale aste non verticali



Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1).

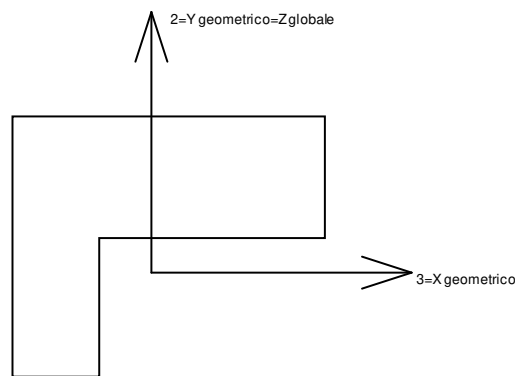
L'asse Z' è illustrato nella figura seguente dove:

- P1 è il punto di inserimento iniziale dell'asta;
- P2 è il punto di inserimento finale dell'asta;
- N è la normale al piano o falda di inserimento;



Z' è quindi l'intersezione tra il piano passante per $P1$, $P2$ contenente N e il piano della sezione iniziale dell'asta.

Sistema locale aste derivanti da travi in c.a.



Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1). L'asse 2 è sempre verticale e quindi coincidente con l'asse Z globale nonché con l'asse y geometrico. L'asse 3 coincide con l'asse x geometrico. Si sottolinea il fatto che gli assi 2 e 3 non corrispondono agli assi principali della sezione.

1.1.2 Sollecitazioni gusci

1.1.2.1 Convenzioni di segno gusci

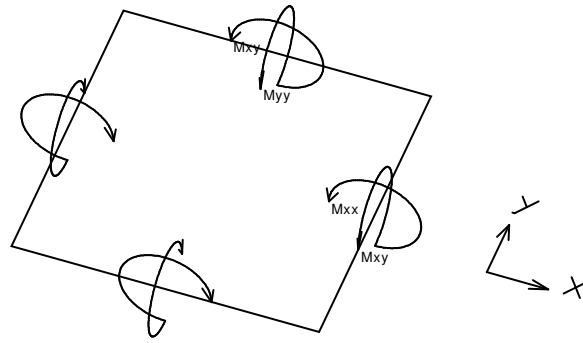
Sono individuate distinte convenzioni di segno in relazione al tipo di elemento strutturale a cui il guscio si riferisce:

- convenzione per gusci non verticali, originati ad esempio da piastre e platee;
- convenzione per gusci verticali, originati ad esempio da pareti e muri.

Convenzione di segno per gusci non verticali

Il sistema di riferimento nel quale sono espressi i parametri di sollecitazione è così definito: origine appartenente al piano dell'elemento, asse x e y contenuti nel piano dell'elemento e terzo asse (z) ortogonale al piano dell'elemento a formare una terna destrorsa. In particolare l'asse x ha proiezione in pianta parallela ed equivale all'asse globale X . Nel caso di piastre orizzontali (caso più comune) gli assi x , y e z locali all'elemento sono paralleli ed equivale agli assi X , Y e Z globali. Si sottolinea che non ha alcun interesse collocare esattamente nel piano dell'elemento la posizione dell'origine in quanto i parametri di sollecitazione sono invarianti rispetto a tale posizione.

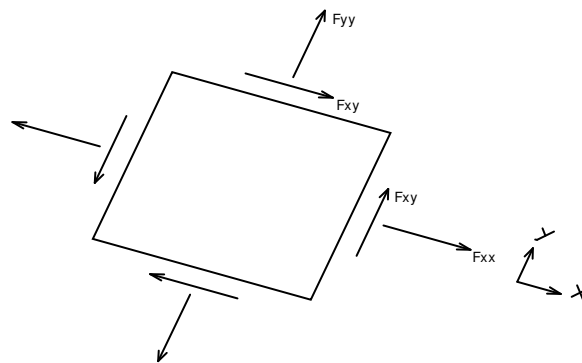
In figura è mostrato un elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione M_{xx} , M_{yy} , M_{xy} .



Si definiscono:

- M_{xx} : momento flettente [Forza*Lunghezza/Lunghezza] agente sul bordo di normale x (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- M_{yy} : momento flettente [Forza*Lunghezza/Lunghezza] agente sul bordo di normale y (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- M_{xy} : momento torcente [Forza*Lunghezza/Lunghezza] agente sui bordi (verso positivo indicato dalla freccia in figura).

Per quanto riguarda le sollecitazioni estensionali si faccia riferimento alla figura seguente dove per lo stesso elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione F_{xx} , F_{yy} , F_{xy} .



Si definiscono:

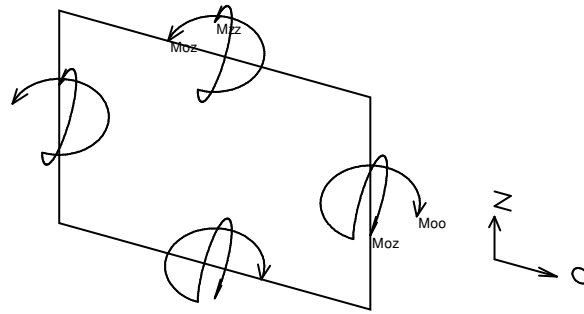
- F_{xx} : sforzo estensionale [Forza/Lunghezza] agente sul bordo di normale x (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- F_{yy} : sforzo estensionale [Forza/Lunghezza] agente sul bordo di normale all'asse y (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- F_{xy} : sforzo di taglio [Forza/Lunghezza] agente sui bordi (verso positivo indicato dalla freccia in figura).

Vengono riportati inoltre i tagli fuori dal piano dell'elemento guscio:

- V_x : taglio fuori piano [Forza/Lunghezza] applicato al bordo di normale parallela all'asse x ;
- V_y : taglio fuori piano [Forza/Lunghezza] applicato al bordo di normale parallela all'asse y .

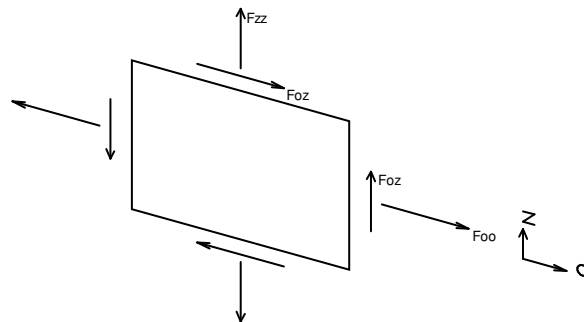
Convenzione di segno per gusci verticali

Il sistema di riferimento nel quale sono espressi i parametri di sollecitazione è così definito: origine appartenente al piano dell'elemento, asse O (ascisse) e z (ordinate) contenuti nel piano dell'elemento e terzo asse ortogonale al piano dell'elemento a formare una terna destrorsa. In particolare l'asse O è orizzontale e l'asse z parallelo ed equiverso con l'asse Z globale. Si sottolinea che non ha alcun interesse collocare esattamente nel piano dell'elemento la posizione dell'origine in quanto i parametri di sollecitazione sono invarianti rispetto a tale posizione. In figura è mostrato un elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione M_{xx} , M_{yy} , M_{xy} , F_{xx} , F_{yy} , F_{xy} .



- Moo: momento flettente distribuito $[Forza * Lunghezza / Lunghezza]$ applicato al bordo di normale parallela all'asse O (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- Mzz: momento flettente distribuito $[Forza * Lunghezza / Lunghezza]$ applicato al bordo di normale parallela all'asse z (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- Moz: momento 'torcente' distribuito $[Forza * Lunghezza / Lunghezza]$ applicato sui bordi (verso positivo indicato dalla freccia in figura).

Per quanto riguarda le sollecitazioni estensionali si faccia riferimento alla figura seguente dove per lo stesso elemento infinitesimo di shell con indicato il sistema di riferimento i parametri di sollecitazione Foo, Fzz, Foz sono rispettivamente:



- Fzz: sforzo tensionale distribuito $[Forza / Lunghezza]$ applicato al bordo di normale parallela all'asse z (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- Foo: sforzo tensionale distribuito $[Forza / Lunghezza]$ applicato al bordo di normale parallela all'asse O (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- Foz: sforzo tagliante distribuito $[Forza / Lunghezza]$ applicato sui bordi (verso positivo indicato dalla freccia in figura).

Vengono riportati inoltre i tagli fuori dal piano dell'elemento guscio:

- Vo: taglio fuori piano applicato al bordo di normale parallela all'asse O;
- Vz: taglio fuori piano applicato al bordo di normale parallela all'asse z.

1.1.2.2 Sollecitazioni estreme gusci

Shell: elemento guscio a cui si riferiscono le sollecitazioni.

Ind: indice del guscio.

Cont.: contesto a cui si riferiscono le sollecitazioni.

N.br.: nome breve della condizione o combinazione di carico.

Nodo: nodo su cui si basa il guscio a cui si riferisce la sollecitazione.

Ind: indice del nodo.

Sollecitazione: valori della sollecitazione.

M11: componente M11 della sollecitazione del guscio nel nodo indicato. $[daN * m / m]$

M12: componente M12 della sollecitazione del guscio nel nodo indicato. $[daN * m / m]$

M22: componente M22 della sollecitazione del guscio nel nodo indicato. $[daN * m / m]$

F11: componente F11 della sollecitazione del guscio nel nodo indicato. $[daN / m]$

F12: componente F12 della sollecitazione del guscio nel nodo indicato. $[daN / m]$

F22: componente F22 della sollecitazione del guscio nel nodo indicato. $[daN / m]$

V13: componente V13 della sollecitazione del guscio nel nodo indicato. $[daN / m]$

V23: componente V23 della sollecitazione del guscio nel nodo indicato. $[daN / m]$

Sollecitazioni con momento M11 minimo

Vengono mostrati i soli 5 gusci più sollecitati.



Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
90	SLV 7	1070	-1756	328	-3157	-1347	1610	-9546	-4869	7039
84	SLV 11	1070	-1754	-337	-3156	-1343	-1576	-9503	4745	7034
386	SLV 11	944	-1717	369	-3198	122	-1493	133	-5163	7198
380	SLV 7	944	-1717	-372	-3198	81	1448	191	5094	7198
634	SLV 11	1007	-1177	824	-3918	357	287	-7042	-5689	9282

Sollecitazioni con momento M11 massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
90	SLV 9	1070	1744	-327	3134	-17	-1529	29	4826	-6943
84	SLV 5	1070	1742	336	3133	-47	1510	-33	-4703	-6938
386	SLV 5	944	1731	-371	3223	-1668	1584	-9743	5214	-7301
380	SLV 9	944	1730	373	3223	-1619	-1615	-9784	-5144	-7300
634	SLV 5	1007	1176	-824	3918	-234	876	-7361	5689	-9282

Sollecitazioni con momento M22 minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
633	SLV 7	1007	-1164	-797	-3947	351	-270	-7052	5729	9520
634	SLV 11	1007	-1177	824	-3918	357	287	-7042	-5689	9282
386	SLV Y	944	-1701	351	-3204	829	-1272	4971	-5159	7232
380	SLV Y	944	-1698	-354	-3203	819	1262	4961	5080	7230
90	SLV 7	1070	-1756	328	-3157	-1347	1610	-9546	-4869	7039

Sollecitazioni con momento M22 massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
633	SLV 9	1007	1164	797	3947	-251	-858	-7378	-5729	-9520
634	SLV 5	1007	1176	-824	3918	-234	876	-7361	5689	-9282
380	SLV 9	944	1730	373	3223	-1619	-1615	-9784	-5144	-7300
386	SLV 5	944	1731	-371	3223	-1668	1584	-9743	5214	-7301
90	SLV 9	1070	1744	-327	3134	-17	-1529	29	4826	-6943

Sollecitazioni con sforzo F11 minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
1642	SLV 7	1053	-22	1	-3	-41644	38209	-33122	57	5
1412	SLV 5	960	-20	-6	-3	-39328	-36127	-31994	-58	8
1643	SLV 9	1137	23	-1	3	-21882	14676	-10495	-30	-6
1413	SLV Y	1162	4	3	1	-20888	-14032	-8634	12	-3
1772	SLV Y	1053	-4	0	-1	-20569	48	2233	11	2

Sollecitazioni con sforzo F11 massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
1642	SLV 9	1053	22	-1	3	40824	-37766	29042	-57	-5
1412	SLV Y	960	4	2	1	38898	35908	30024	14	-2
1643	SLV 7	1137	-23	1	-3	21991	-14826	6842	30	6
1413	SLV 5	1162	-20	-6	-4	20963	14075	6820	-53	6
1772	SLV 9	1053	22	0	4	20795	-48	-4286	-49	-10

Sollecitazioni con sforzo F22 minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
1642	SLV 7	1053	-22	1	-3	-41644	38209	-33122	57	5
1412	SLV 9	960	13	1	1	-39209	-36208	-32063	30	-5
615	SLU 81	618	1	-1	1	-640	-2399	-23611	-8	5
763	SLU 81	621	0	0	0	-730	2602	-22702	0	0
1632	SLV 7	1137	-23	1	-3	-12349	19690	-21544	44	5

Sollecitazioni con sforzo F22 massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
1412	SLV Y	960	4	2	1	38898	35908	30024	14	-2
1642	SLV 9	1053	22	-1	3	40824	-37766	29042	-57	-5
1422	SLV Y	1162	4	2	1	10952	18678	18882	9	-2
1632	SLV 9	1137	23	-1	3	11935	-19547	17504	-44	-5
1532	SLV Y	1024	3	-2	5	15842	15882	13374	-29	-13

1.1.2.3 Sollecitazioni estreme gusci non verticali

Shell: elemento guscio a cui si riferiscono le sollecitazioni.

Ind: indice del guscio.

Cont.: contesto a cui si riferiscono le sollecitazioni.

N.br.: nome breve della condizione o combinazione di carico.

Nodo: nodo su cui si basa il guscio a cui si riferisce la sollecitazione.



Ind: indice del nodo.

Sollecitazione: valori della sollecitazione.

Mxx: componente Mxx della sollecitazione del guscio nel nodo indicato. [daN*m/m]

Mxy: componente Mxy della sollecitazione del guscio nel nodo indicato. [daN*m/m]

Myy: componente Myy della sollecitazione del guscio nel nodo indicato. [daN*m/m]

Fxx: componente Fxx della sollecitazione del guscio nel nodo indicato. [daN/m]

Fxy: componente Fxy della sollecitazione del guscio nel nodo indicato. [daN/m]

Fyy: componente Fyy della sollecitazione del guscio nel nodo indicato. [daN/m]

Vx: componente Vo della sollecitazione del guscio nel nodo indicato. [daN/m]

Vy: componente Vz della sollecitazione del guscio nel nodo indicato. [daN/m]

Sollecitazioni con momento Mxx minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy

Sollecitazioni con momento Mxx massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy

Sollecitazioni con momento Myy minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy

Sollecitazioni con momento Myy massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy

Sollecitazioni con sforzo Fxx minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy

Sollecitazioni con sforzo Fxx massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy

Sollecitazioni con sforzo Fyy minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy

Sollecitazioni con sforzo Fyy massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy

1.1.2.4 Sollecitazioni estreme gusci verticali

Shell: elemento guscio a cui si riferiscono le sollecitazioni.

Ind: indice del guscio.

Cont.: contesto a cui si riferiscono le sollecitazioni.

N.br.: nome breve della condizione o combinazione di carico.

Nodo: nodo su cui si basa il guscio a cui si riferisce la sollecitazione.

Ind: indice del nodo.

Sollecitazione: valori della sollecitazione.

Moo: componente Moo della sollecitazione del guscio nel nodo indicato. [daN*m/m]

Moz: componente Moz della sollecitazione del guscio nel nodo indicato. [daN*m/m]

Mzz: componente Mzz della sollecitazione del guscio nel nodo indicato. [daN*m/m]

Foo: componente Foo della sollecitazione del guscio nel nodo indicato. [daN/m]

Foz: componente Foz della sollecitazione del guscio nel nodo indicato. [daN/m]

Fzz: componente Fzz della sollecitazione del guscio nel nodo indicato. [daN/m]

Vo: componente Vo della sollecitazione del guscio nel nodo indicato. [daN/m]

Vz: componente Vz della sollecitazione del guscio nel nodo indicato. [daN/m]

Sollecitazioni con momento Moo minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
90	SLV 9	1070	-1744	-327	-3134	-17	1529	29	4826	6943
84	SLV 5	1070	-1742	336	-3133	-47	-1510	-33	-4703	6938
386	SLV 5	944	-1731	-371	-3223	-1668	-1584	-9743	5214	7301
380	SLV 9	944	-1730	373	-3223	-1619	1615	-9784	-5144	7300



Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
634	SLV 5	1007	-1176	-824	-3918	-234	-876	-7361	5689	9282

Sollecitazioni con momento Moo massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
90	SLV 7	1070	1756	328	3157	-1347	-1610	-9546	-4869	-7039
84	SLV 11	1070	1754	-337	3156	-1343	1576	-9503	4745	-7034
386	SLV 11	944	1717	369	3198	122	1493	133	-5163	-7198
380	SLV 7	944	1717	-372	3198	81	-1448	191	5094	-7198
634	SLV 11	1007	1177	824	3918	357	-287	-7042	-5689	-9282

Sollecitazioni con momento Mzz minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
633	SLV 9	1007	-1164	797	-3947	-251	858	-7378	-5729	9520
634	SLV 5	1007	-1176	-824	-3918	-234	-876	-7361	5689	9282
380	SLV 9	944	-1730	373	-3223	-1619	1615	-9784	-5144	7300
386	SLV 5	944	-1731	-371	-3223	-1668	-1584	-9743	5214	7301
90	SLV 9	1070	-1744	-327	-3134	-17	1529	29	4826	6943

Sollecitazioni con momento Mzz massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
633	SLV 7	1007	1164	-797	3947	351	270	-7052	5729	-9520
634	SLV 11	1007	1177	824	3918	357	-287	-7042	-5689	-9282
386	SLV Y	944	1701	351	3204	829	1272	4971	-5159	-7232
380	SLV Y	944	1698	-354	3203	819	-1262	4961	5080	-7230
90	SLV 7	1070	1756	328	3157	-1347	-1610	-9546	-4869	-7039

Sollecitazioni con sforzo Foo minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
1642	SLV 7	1053	-22	1	-3	-41644	38209	-33122	57	5
1412	SLV 5	960	-20	-6	-3	-39328	-36127	-31994	-58	8
1643	SLV 9	1137	23	-1	3	-21882	14676	-10495	-30	-6
1413	SLV Y	1162	4	3	1	-20888	-14032	-8634	12	-3
1772	SLV Y	1053	-4	0	-1	-20569	48	2233	11	2

Sollecitazioni con sforzo Foo massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
1642	SLV 9	1053	22	-1	3	40824	-37766	29042	-57	-5
1412	SLV Y	960	4	2	1	38898	35908	30024	14	-2
1643	SLV 7	1137	-23	1	-3	21991	-14826	6842	30	6
1413	SLV 5	1162	-20	-6	-4	20963	14075	6820	-53	6
1772	SLV 9	1053	22	0	4	20795	-48	-4286	-49	-10

Sollecitazioni con sforzo Fzz minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
1642	SLV 7	1053	-22	1	-3	-41644	38209	-33122	57	5
1412	SLV 9	960	13	1	1	-39209	-36208	-32063	30	-5
615	SLU 81	618	-1	-1	-1	-640	2399	-23611	-8	-5
763	SLU 81	621	0	0	0	-730	-2602	-22702	0	0
1632	SLV 7	1137	-23	1	-3	-12349	19690	-21544	44	5

Sollecitazioni con sforzo Fzz massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
1412	SLV Y	960	4	2	1	38898	35908	30024	14	-2
1642	SLV 9	1053	22	-1	3	40824	-37766	29042	-57	-5
1422	SLV Y	1162	4	2	1	10952	18678	18882	9	-2
1632	SLV 9	1137	23	-1	3	11935	-19547	17504	-44	-5
1532	SLV Y	1024	3	-2	5	15842	15882	13374	-29	-13

1.1.3 Sollecitazioni gusci armati

1.1.3.1 Convenzioni di segno gusci

Sono individuate distinte convenzioni di segno in relazione al tipo di elemento strutturale a cui il guscio si riferisce:

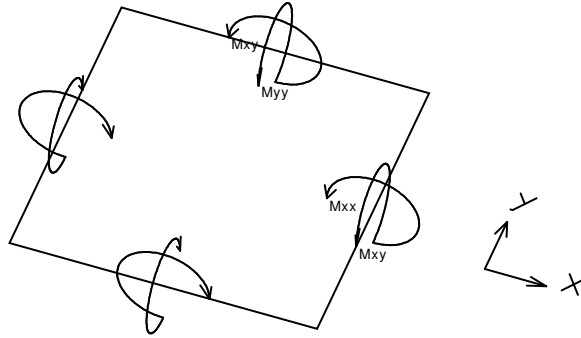
- convenzione per gusci non verticali, originati ad esempio da piastre e platee;
- convenzione per gusci verticali, originati ad esempio da pareti e muri.



Convenzione di segno per gusci non verticali

Il sistema di riferimento nel quale sono espressi i parametri di sollecitazione è così definito: origine appartenente al piano dell'elemento, asse x e y contenuti nel piano dell'elemento e terzo asse (z) ortogonale al piano dell'elemento a formare una terna destrorsa. In particolare l'asse x ha proiezione in pianta parallela ed equivale all'asse globale X . Nel caso di piastre orizzontali (caso più comune) gli assi x , y e z locali all'elemento sono paralleli ed equivale agli assi X , Y e Z globali. Si sottolinea che non ha alcun interesse collocare esattamente nel piano dell'elemento la posizione dell'origine in quanto i parametri di sollecitazione sono invarianti rispetto a tale posizione.

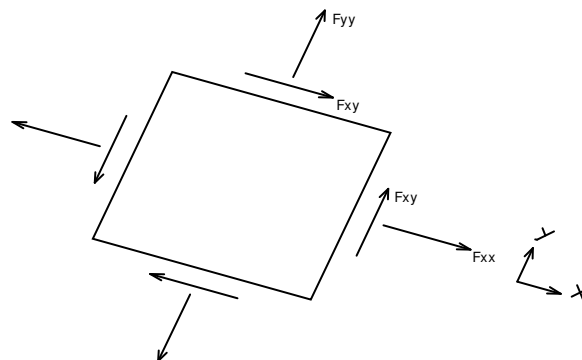
In figura è mostrato un elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione M_{xx} , M_{yy} , M_{xy} .



Si definiscono:

- M_{xx} : momento flettente [Forza*Lunghezza/Lunghezza] agente sul bordo di normale x (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- M_{yy} : momento flettente [Forza*Lunghezza/Lunghezza] agente sul bordo di normale y (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- M_{xy} : momento torcente [Forza*Lunghezza/Lunghezza] agente sui bordi (verso positivo indicato dalla freccia in figura).

Per quanto riguarda le sollecitazioni estensionali si faccia riferimento alla figura seguente dove per lo stesso elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione F_{xx} , F_{yy} , F_{xy} .



Si definiscono:

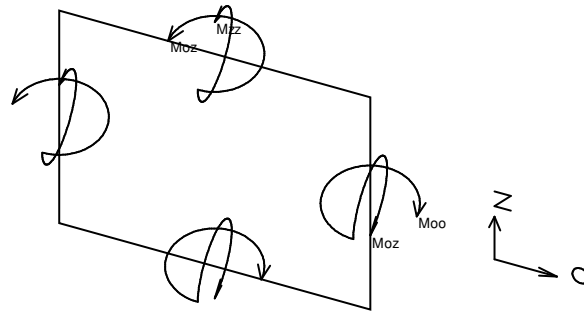
- F_{xx} : sforzo estensionale [Forza/Lunghezza] agente sul bordo di normale x (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- F_{yy} : sforzo estensionale [Forza/Lunghezza] agente sul bordo di normale all'asse y (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- F_{xy} : sforzo di taglio [Forza/Lunghezza] agente sui bordi (verso positivo indicato dalla freccia in figura).

Vengono riportati inoltre i tagli fuori dal piano dell'elemento guscio:

- V_x : taglio fuori piano [Forza/Lunghezza] applicato al bordo di normale parallela all'asse x ;
- V_y : taglio fuori piano [Forza/Lunghezza] applicato al bordo di normale parallela all'asse y .

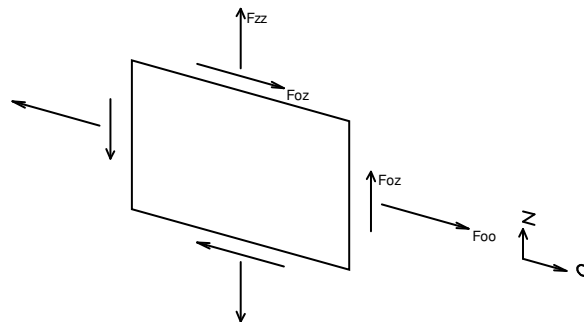
Convenzione di segno per gusci verticali

Il sistema di riferimento nel quale sono espressi i parametri di sollecitazione è così definito: origine appartenente al piano dell'elemento, asse O (ascisse) e z (ordinate) contenuti nel piano dell'elemento e terzo asse ortogonale al piano dell'elemento a formare una terna destrorsa. In particolare l'asse O è orizzontale e l'asse z parallelo ed equivale con l'asse Z globale. Si sottolinea che non ha alcun interesse collocare esattamente nel piano dell'elemento la posizione dell'origine in quanto i parametri di sollecitazione sono invarianti rispetto a tale posizione. In figura è mostrato un elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione M_{oo} , M_{zz} , M_{oz} .



- Moo: momento flettente distribuito $[Forza \cdot Lunghezza / Lunghezza]$ applicato al bordo di normale parallela all'asse O (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- Mzz: momento flettente distribuito $[Forza \cdot Lunghezza / Lunghezza]$ applicato al bordo di normale parallela all'asse z (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- Moz: momento 'torcente' distribuito $[Forza \cdot Lunghezza / Lunghezza]$ applicato sui bordi (verso positivo indicato dalla freccia in figura).

Per quanto riguarda le sollecitazioni estensionali si faccia riferimento alla figura seguente dove per lo stesso elemento infinitesimo di shell con indicato il sistema di riferimento i parametri di sollecitazione Foo, Fzz, Foz sono rispettivamente:



- Fzz: sforzo tensionale distribuito $[Forza / Lunghezza]$ applicato al bordo di normale parallela all'asse z (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- Foo: sforzo tensionale distribuito $[Forza / Lunghezza]$ applicato al bordo di normale parallela all'asse O (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- Foz: sforzo tagliante distribuito $[Forza / Lunghezza]$ applicato sui bordi (verso positivo indicato dalla freccia in figura).

Vengono riportati inoltre i tagli fuori dal piano dell'elemento guscio:

- Vo: taglio fuori piano applicato al bordo di normale parallela all'asse O;
- Vz: taglio fuori piano applicato al bordo di normale parallela all'asse z.

1.1.4 Sollecitazioni gusci muratura

1.1.4.1 Convenzioni di segno gusci muratura

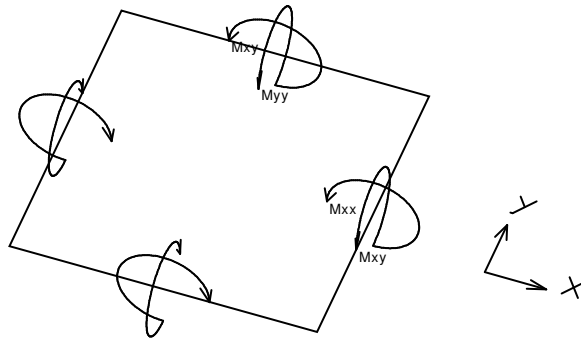
Sono individuate distinte convenzioni di segno in relazione al tipo di elemento strutturale a cui il guscio muratura si riferisce:

- convenzione per gusci non verticali, originati ad esempio da piastre e platee;
- convenzione per gusci verticali, originati ad esempio da pareti e muri.

Convenzione di segno per gusci non verticali

Il sistema di riferimento nel quale sono espressi i parametri di sollecitazione è così definito: origine appartenente al piano dell'elemento, asse x e y contenuti nel piano dell'elemento e terzo asse (z) ortogonale al piano dell'elemento a formare una terna destrorsa. In particolare l'asse x ha proiezione in pianta parallela ed equivale all'asse globale X. Nel caso di piastre orizzontali (caso più comune) gli assi x, y e z locali all'elemento sono paralleli ed equivale agli assi X, Y e Z globali. Si sottolinea che non ha alcun interesse collocare esattamente nel piano dell'elemento la posizione dell'origine in quanto i parametri di sollecitazione sono invarianti rispetto a tale posizione.

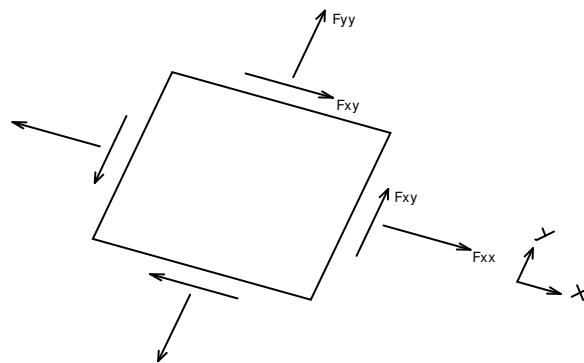
In figura è mostrato un elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione Mxx, Myy, Mxy.



Si definiscono:

- M_{xx} : momento flettente [Forza*Lunghezza/Lunghezza] agente sul bordo di normale x (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- M_{yy} : momento flettente [Forza*Lunghezza/Lunghezza] agente sul bordo di normale y (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- M_{xy} : momento torcente [Forza*Lunghezza/Lunghezza] agente sui bordi (verso positivo indicato dalla freccia in figura).

Per quanto riguarda le sollecitazioni estensionali si faccia riferimento alla figura seguente dove per lo stesso elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione F_{xx} , F_{yy} , F_{xy} .

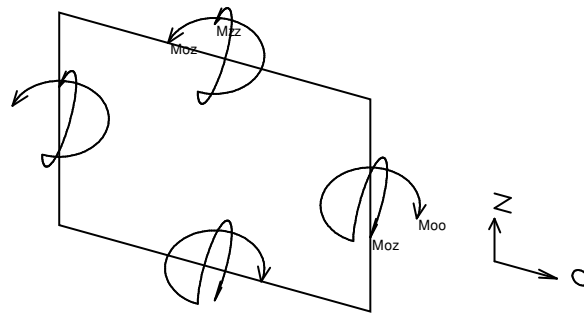


Si definiscono:

- F_{xx} : sforzo tensionale [Forza/Lunghezza] agente sul bordo di normale x (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- F_{yy} : sforzo tensionale [Forza/Lunghezza] agente sul bordo di normale all'asse y (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- F_{xy} : sforzo tagliante [Forza/Lunghezza] agente sui bordi (verso positivo indicato dalla freccia in figura).

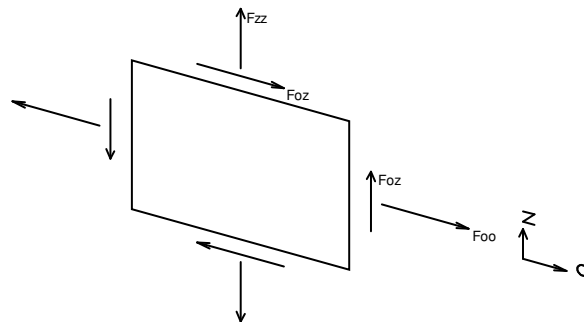
Convenzione di segno per gusci verticali

Il sistema di riferimento nel quale sono espressi i parametri di sollecitazione è così definito: origine appartenente al piano dell'elemento, asse O (ascisse) e z (ordinate) contenuti nel piano dell'elemento e terzo asse ortogonale al piano dell'elemento a formare una terna destrorsa. In particolare l'asse O è orizzontale e l'asse z parallelo ed equiverso con l'asse Z globale. Si sottolinea che non ha alcun interesse collocare esattamente nel piano dell'elemento la posizione dell'origine in quanto i parametri di sollecitazione sono invarianti rispetto a tale posizione. In figura è mostrato un elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione M_{oo} , M_{zz} , M_{oz} .



- Moo: momento flettente distribuito $[Forza * Lunghezza / Lunghezza]$ applicato al bordo di normale parallela all'asse O (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- Mzz: momento flettente distribuito $[Forza * Lunghezza / Lunghezza]$ applicato al bordo di normale parallela all'asse z (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- Moz: momento 'torcente' distribuito $[Forza * Lunghezza / Lunghezza]$ applicato sui bordi (verso positivo indicato dalla freccia in figura).

Per quanto riguarda le sollecitazioni estensionali si faccia riferimento alla figura seguente dove per lo stesso elemento infinitesimo di shell con indicato il sistema di riferimento i parametri di sollecitazione Foo, Fzz, Foz sono rispettivamente:



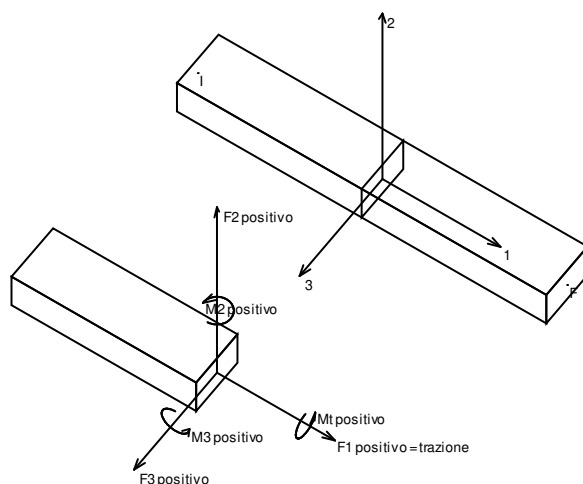
- Fzz: sforzo tensionale distribuito $[Forza / Lunghezza]$ applicato al bordo di normale parallela all'asse z (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- Foo: sforzo tensionale distribuito $[Forza / Lunghezza]$ applicato al bordo di normale parallela all'asse O (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- Foz: sforzo tagliante distribuito $[Forza / Lunghezza]$ applicato sui bordi (verso positivo indicato dalla freccia in figura).

1.1.5 Sollecitazioni aste in muratura

1.1.5.1 Convenzioni di segno aste

Le abbreviazioni relative alle sollecitazioni sugli elementi aste sono da intendersi:

- F1 (N): sforzo normale nell'asta;
- F2: sforzo di taglio agente nella direzione dell'asse locale 2;
- F3: sforzo di taglio agente nella direzione dell'asse locale 3;
- M1 (Mt): momento attorno all'asse locale 1; equivale al momento torcente;
- M2: momento attorno all'asse locale 2;
- M3: momento attorno all'asse locale 3.



La convenzione sui segni per i parametri di sollecitazione delle aste è la seguente:

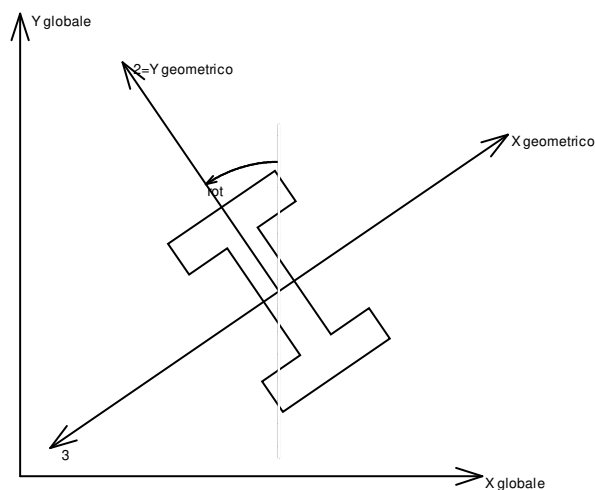
presa un'asta con nodo iniziale i e nodo finale f , asse 1 che va da i a f , assi 2 e 3 presi secondo quanto indicato nei paragrafi successivi relativi al sistema locale delle aste sezionando l'asta in un punto e considerando la sezione sinistra del punto in cui si è effettuato il taglio (sezione da cui esce il versore asse 1) i parametri di sollecitazione sono positivi se hanno verso e direzione concordi con il sistema di riferimento locale dell'asta 1, 2, 3 (per i momenti si adotta la regola della mano destra).

Il sistema è definito diversamente per tre categorie di aste, a seconda che siano originate da:

- aste verticali ad esempio pilastri e colonne;
- aste non verticali non di c.a., ad esempio travi di acciaio o legno;
- aste non verticali in c.a.: travi in c.a. di piano, falda o a quota generica.

Nel seguito si indica con 1, 2 e 3 il sistema locale dell'asta che non sempre coincide con gli assi principali della sezione. Si ricorda che per assi principali si intendono gli assi rispetto a cui si ha il raggio di inerzia minimo e massimo. Gli assi 1, 2 e 3 rispettano la regola della mano destra.

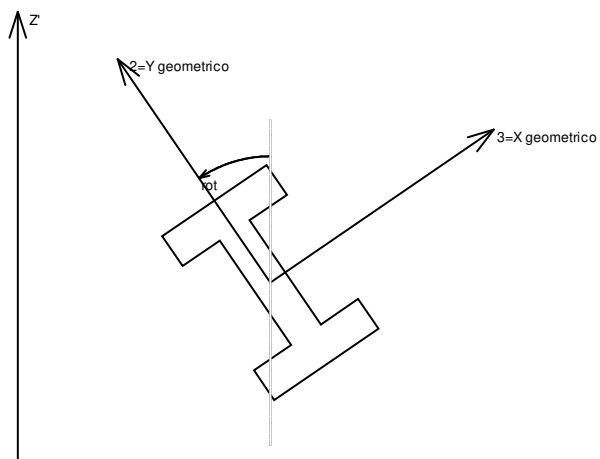
Sistema locale aste verticali



Nella figura si considera l'asse 1 uscente dal foglio (l'osservatore guarda in direzione opposta a quella dell'asse 1).



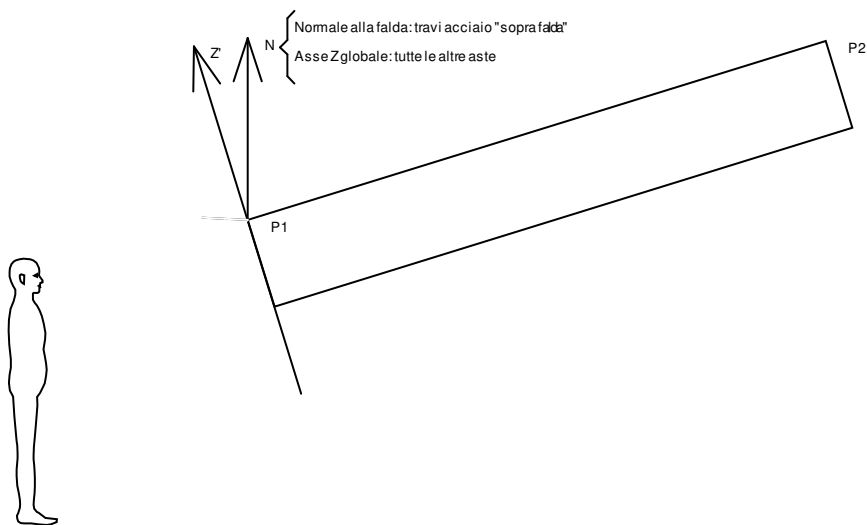
Sistema locale aste non verticali



Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1).

L'asse Z' è illustrato nella figura seguente dove:

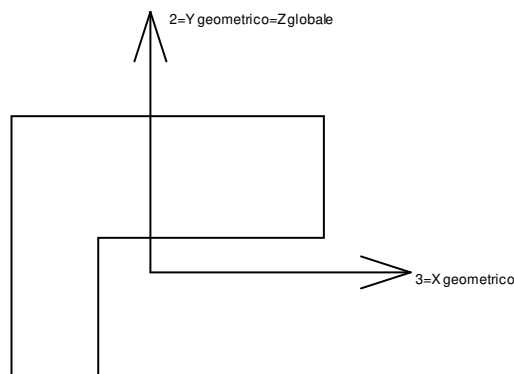
- $P1$ è il punto di inserimento iniziale dell'asta;
- $P2$ è il punto di inserimento finale dell'asta;
- N è la normale al piano o falda di inserimento;



Z' è quindi l'intersezione tra il piano passante per $P1, P2$ contenente N e il piano della sezione iniziale dell'asta.



Sistema locale aste derivanti da travi in c.a.



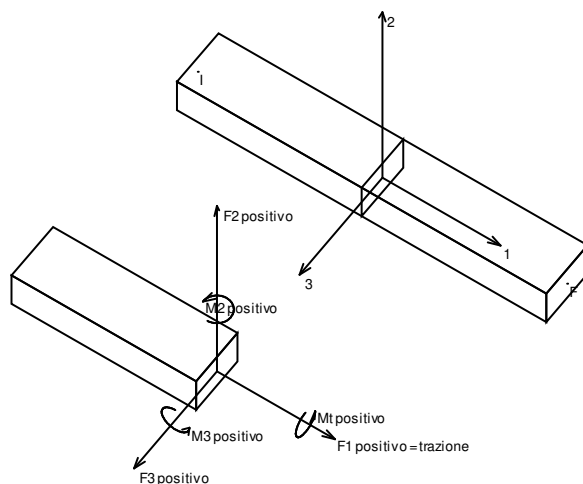
Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1). L'asse 2 è sempre verticale e quindi coincidente con l'asse Z globale nonché con l'asse y geometrico. L'asse 3 coincide con l'asse x geometrico. Si sottolinea il fatto che gli assi 2 e 3 non corrispondono agli assi principali della sezione.

1.1.6 Sollecitazioni aste in muratura FRCM

1.1.6.1 Convenzioni di segno aste

Le abbreviazioni relative alle sollecitazioni sugli elementi aste sono da intendersi:

- F1 (N): sforzo normale nell'asta;
- F2: sforzo di taglio agente nella direzione dell'asse locale 2;
- F3: sforzo di taglio agente nella direzione dell'asse locale 3;
- M1 (Mt): momento attorno all'asse locale 1; equivale al momento torcente;
- M2: momento attorno all'asse locale 2;
- M3: momento attorno all'asse locale 3.



La convenzione sui segni per i parametri di sollecitazione delle aste è la seguente:

presa un'asta con nodo iniziale i e nodo finale f, asse 1 che va da i a f, assi 2 e 3 presi secondo quanto indicato nei paragrafi successivi relativi al sistema locale delle aste sezionando l'asta in un punto e considerando la sezione sinistra del punto in cui si è effettuato il taglio (sezione da cui esce il versore asse 1) i parametri di sollecitazione sono positivi se hanno verso e direzione concordi con il sistema di riferimento locale dell'asta 1, 2, 3 (per i momenti si adotta la regola della mano destra).

Il sistema è definito diversamente per tre categorie di aste, a seconda che siano originate da:

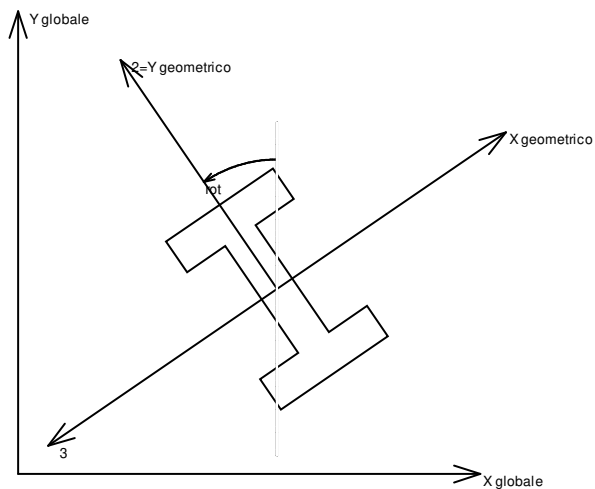
- aste verticali ad esempio pilastri e colonne;
- aste non verticali non di c.a., ad esempio travi di acciaio o legno;
- aste non verticali in c.a.: travi in c.a. di piano, falda o a quota generica.

Nel seguito si indica con 1, 2 e 3 il sistema locale dell'asta che non sempre coincide con gli assi principali della sezione. Si ricorda che per assi principali si intendono gli



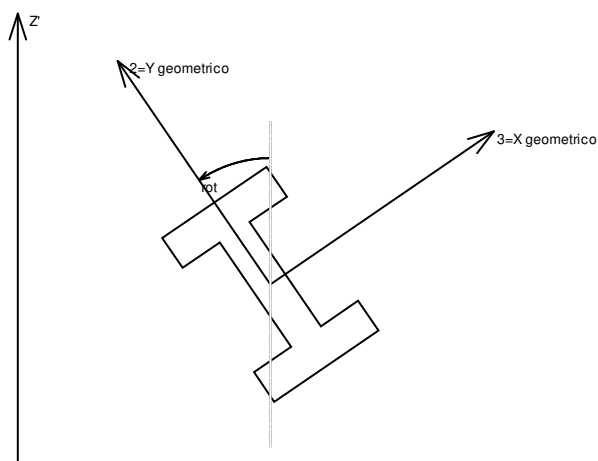
assi rispetto a cui si ha il raggio di inerzia minimo e massimo. Gli assi 1, 2 e 3 rispettano la regola della mano destra.

Sistema locale aste verticali



Nella figura si considera l'asse 1 uscente dal foglio (l'osservatore guarda in direzione opposta a quella dell'asse 1).

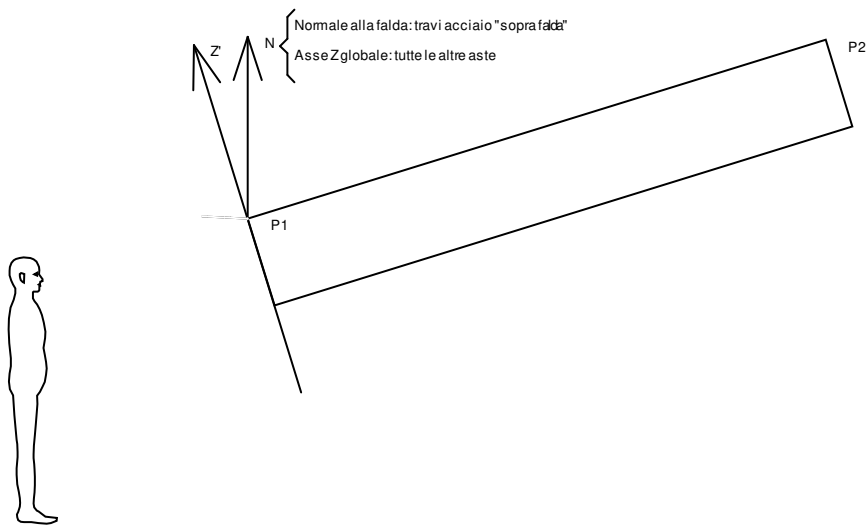
Sistema locale aste non verticali



Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1).

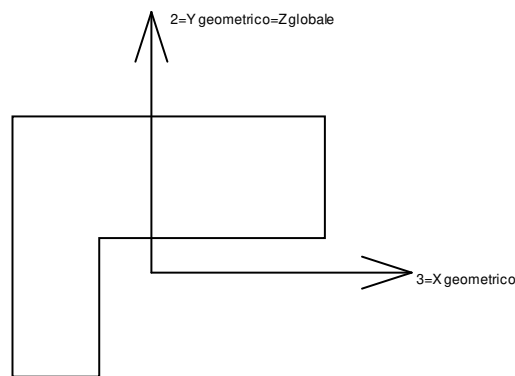
L'asse Z' è illustrato nella figura seguente dove:

- P1 è il punto di inserimento iniziale dell'asta;
- P2 è il punto di inserimento finale dell'asta;
- N è la normale al piano o falda di inserimento;



Z' è quindi l'intersezione tra il piano passante per P1, P2 contenente N e il piano della sezione iniziale dell'asta.

Sistema locale aste derivanti da travi in c.a.



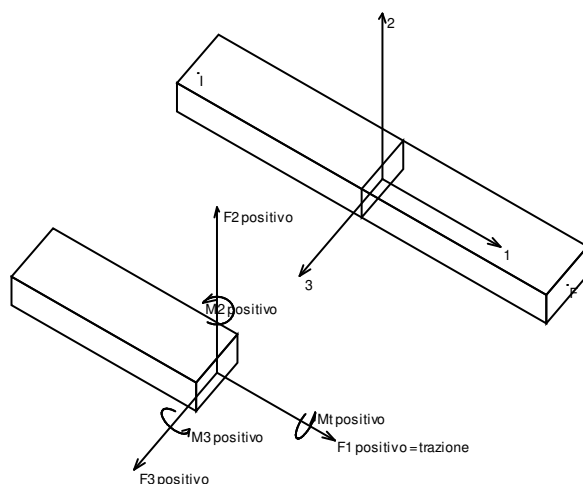
Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1). L'asse 2 è sempre verticale e quindi coincidente con l'asse Z globale nonché con l'asse y geometrico. L'asse 3 coincide con l'asse x geometrico. Si sottolinea il fatto che gli assi 2 e 3 non corrispondono agli assi principali della sezione.

1.1.7 Sollecitazioni aste in muratura armata

1.1.7.1 Convenzioni di segno aste

Le abbreviazioni relative alle sollecitazioni sugli elementi aste sono da intendersi:

- F1 (N): sforzo normale nell'asta;
- F2: sforzo di taglio agente nella direzione dell'asse locale 2;
- F3: sforzo di taglio agente nella direzione dell'asse locale 3;
- M1 (Mt): momento attorno all'asse locale 1; equivale al momento torcente;
- M2: momento attorno all'asse locale 2;
- M3: momento attorno all'asse locale 3.



La convenzione sui segni per i parametri di sollecitazione delle aste è la seguente:

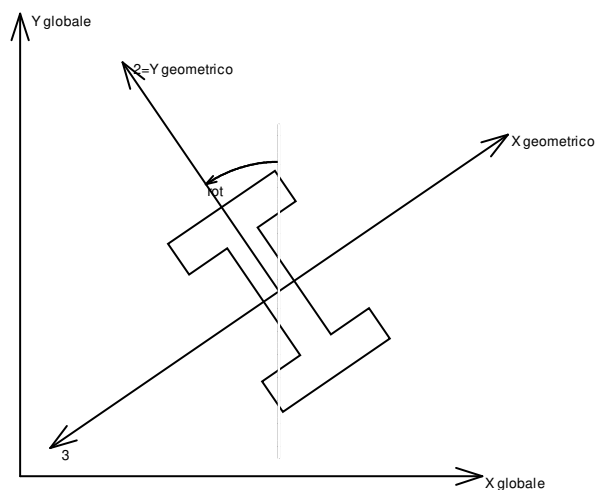
presa un'asta con nodo iniziale i e nodo finale f , asse 1 che va da i a f , assi 2 e 3 presi secondo quanto indicato nei paragrafi successivi relativi al sistema locale delle aste sezionando l'asta in un punto e considerando la sezione sinistra del punto in cui si è effettuato il taglio (sezione da cui esce il versore asse 1) i parametri di sollecitazione sono positivi se hanno verso e direzione concordi con il sistema di riferimento locale dell'asta 1, 2, 3 (per i momenti si adotta la regola della mano destra).

Il sistema è definito diversamente per tre categorie di aste, a seconda che siano originate da:

- aste verticali ad esempio pilastri e colonne;
- aste non verticali non di c.a., ad esempio travi di acciaio o legno;
- aste non verticali in c.a.: travi in c.a. di piano, falda o a quota generica.

Nel seguito si indica con 1, 2 e 3 il sistema locale dell'asta che non sempre coincide con gli assi principali della sezione. Si ricorda che per assi principali si intendono gli assi rispetto a cui si ha il raggio di inerzia minimo e massimo. Gli assi 1, 2 e 3 rispettano la regola della mano destra.

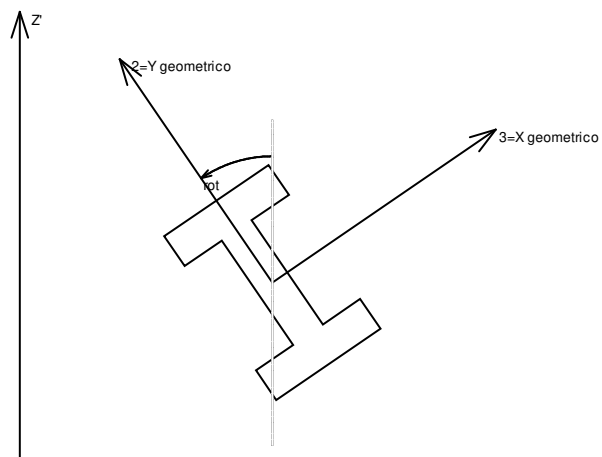
Sistema locale aste verticali



Nella figura si considera l'asse 1 uscente dal foglio (l'osservatore guarda in direzione opposta a quella dell'asse 1).



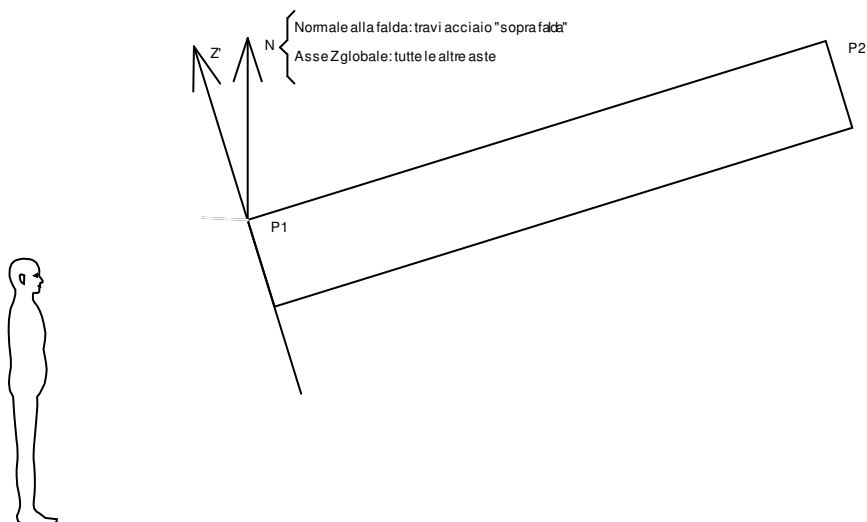
Sistema locale aste non verticali



Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1).

L'asse Z' è illustrato nella figura seguente dove:

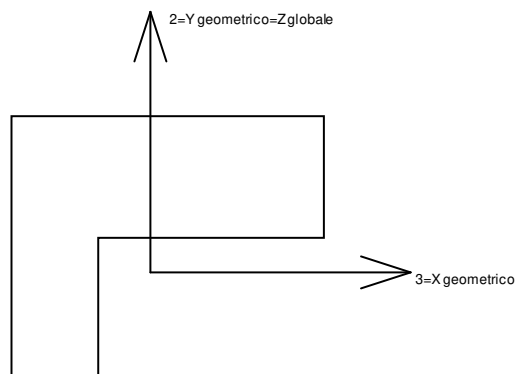
- $P1$ è il punto di inserimento iniziale dell'asta;
- $P2$ è il punto di inserimento finale dell'asta;
- N è la normale al piano o falda di inserimento;



Z' è quindi l'intersezione tra il piano passante per $P1, P2$ contenente N e il piano della sezione iniziale dell'asta.



Sistema locale aste derivanti da travi in c.a.



Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1). L'asse 2 è sempre verticale e quindi coincidente con l'asse Z globale nonché con l'asse y geometrico. L'asse 3 coincide con l'asse x geometrico. Si sottolinea il fatto che gli assi 2 e 3 non corrispondono agli assi principali della sezione.

1.2 Reazioni nodali

1.2.1 Reazioni nodali estreme

Nodo: Nodo sollecitato dalla reazione vincolare.

Ind.: indice del nodo.

Cont.: Contesto a cui si riferisce la reazione vincolare.

N.br.: nome breve della condizione o combinazione di carico.

Reazione a traslazione: reazione vincolare traslazionale del nodo.

x: componente X della reazione vincolare del nodo. [daN]

y: componente Y della reazione vincolare del nodo. [daN]

z: componente Z della reazione vincolare del nodo. [daN]

Reazione a rotazione: reazione vincolare rotazionale del nodo.

x: componente X della reazione a rotazione del nodo. [daN*m]

y: componente Y della reazione a rotazione del nodo. [daN*m]

z: componente Z della reazione a rotazione del nodo. [daN*m]

Reazioni Fx minime

Vengono mostrati i soli 5 nodi più sollecitati.

Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
67	SLV 15	-1163	78	3831	-11.52	-34.7	-1.94
80	SLV 15	-1128	-77	3010	110.4	-52.33	-0.12
79	SLV 15	-1094	-80	3990	106.17	-53.23	0.25
81	SLV 15	-1081	-66	3213	106.09	-49.67	-0.31
78	SLV 15	-1049	-73	2483	99.8	-49.95	0.22

Reazioni Fx massime

Vengono mostrati i soli 5 nodi più sollecitati.

Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
90	SLV 1	1189	-80	3959	7.49	37.69	-1.18
80	SLV 1	1112	77	2642	-110.39	52.12	0.12
79	SLV 1	1089	80	3959	-106.18	53.03	-0.25
81	SLV 1	1069	66	2542	-106.08	49.64	0.31
88	SLV 1	1066	42	4308	-51.72	55.46	-0.03

Reazioni Fy minime

Vengono mostrati i soli 5 nodi più sollecitati.

Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
121	SLV 11	27	-844	3509	46.35	13.83	0.08
118	SLV 11	44	-818	2943	40.56	22.91	-0.03
124	SLV 11	-652	-791	4650	28.07	-16.71	0.05
115	SLV 11	38	-772	2722	37.61	24.15	-0.03
112	SLV 11	27	-718	2579	35.01	21.09	-0.02

Reazioni Fy massime

Vengono mostrati i soli 5 nodi più sollecitati.



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
35	SLV 9	28	770	3338	-42.11	13.11	-0.07
2	SLV 9	-556	738	4270	-25.78	-13.51	-0.08
38	SLV 5	56	724	2559	-33.84	37.37	0.01
34	SLV 5	-25	700	3071	-39.24	-12.21	0.07
32	SLV 5	545	699	4040	-23.53	13.02	0.08

Reazioni Fz minime

Vengono mostrati i soli 5 nodi più sollecitati.

Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
89	SLV X	-516	-8	-1638	6.32	-30.89	0.02
90	SLV X	-497	6	-1478	2.81	-18.24	-0.44
2	SLV Y	66	-301	-1043	13.26	-2.28	0.12
154	SLV X	-269	87	-977	-2.87	-11.32	-0.1
32	SLV Y	-63	-264	-932	11.41	2.05	-0.11

Reazioni Fz massime

Vengono mostrati i soli 5 nodi più sollecitati.

Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
89	SLU 81	910	0	6545	0	50.63	0
79	SLU 81	-2	0	6397	0	-0.09	0
68	SLU 81	-883	0	6344	0.11	-51.34	0
65	SLU 81	-498	-229	6051	16.82	-21.35	0.09
88	SLU 81	732	0	5857	0	36.71	0

1.2.2 Reazioni nodali in combinazioni di carico

Nodo: Nodo sollecitato dalla reazione vincolare.

Ind.: indice del nodo.

Cont.: Contesto a cui si riferisce la reazione vincolare.

N.br.: nome breve della condizione o combinazione di carico.

Reazione a traslazione: reazione vincolare traslazionale del nodo.

x: componente X della reazione vincolare del nodo. [daN]

y: componente Y della reazione vincolare del nodo. [daN]

z: componente Z della reazione vincolare del nodo. [daN]

Reazione a rotazione: reazione vincolare rotazionale del nodo.

x: componente X della reazione a rotazione del nodo. [daN*m]

y: componente Y della reazione a rotazione del nodo. [daN*m]

z: componente Z della reazione a rotazione del nodo. [daN*m]

Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
2	SLU 1	-382	386	2743	-11.14	-11.41	0.01
2	SLU 2	-382	386	2743	-11.14	-11.41	0.01
2	SLU 3	-382	386	2743	-11.14	-11.41	0.01
2	SLU 4	-382	386	2743	-11.14	-11.41	0.01
2	SLU 5	-382	386	2743	-11.14	-11.41	0.01
2	SLU 6	-382	386	2743	-11.14	-11.41	0.01
2	SLU 7	-382	386	2743	-11.14	-11.41	0.01
2	SLU 8	-382	386	2743	-11.14	-11.41	0.01
2	SLU 9	-382	386	2743	-11.14	-11.41	0.01
2	SLU 10	-484	438	3272	-12.24	-15.05	0.03
2	SLU 11	-484	438	3272	-12.24	-15.05	0.03
2	SLU 12	-484	438	3272	-12.24	-15.05	0.03
2	SLU 13	-484	438	3272	-12.24	-15.05	0.03
2	SLU 14	-484	438	3272	-12.24	-15.05	0.03
2	SLU 15	-484	438	3272	-12.24	-15.05	0.03
2	SLU 16	-484	438	3272	-12.24	-15.05	0.03
2	SLU 17	-484	438	3272	-12.24	-15.05	0.03
2	SLU 18	-528	460	3499	-12.71	-16.6	0.04
2	SLU 19	-528	460	3499	-12.71	-16.6	0.04
2	SLU 20	-528	460	3499	-12.71	-16.6	0.04
2	SLU 21	-528	460	3499	-12.71	-16.6	0.04
2	SLU 22	-438	418	3050	-11.89	-13.36	0.02
2	SLU 23	-438	418	3050	-11.89	-13.36	0.02
2	SLU 24	-438	418	3050	-11.89	-13.36	0.02
2	SLU 25	-438	418	3050	-11.89	-13.36	0.02
2	SLU 26	-438	418	3050	-11.89	-13.36	0.02
2	SLU 27	-438	418	3050	-11.89	-13.36	0.02
2	SLU 28	-438	418	3050	-11.89	-13.36	0.02
2	SLU 29	-438	418	3050	-11.89	-13.36	0.02
2	SLU 30	-438	418	3050	-11.89	-13.36	0.02
2	SLU 31	-541	470	3579	-12.99	-17	0.04
2	SLU 32	-541	470	3579	-12.99	-17	0.04
2	SLU 33	-541	470	3579	-12.99	-17	0.04
2	SLU 34	-541	470	3579	-12.99	-17	0.04
2	SLU 35	-541	470	3579	-12.99	-17	0.04
2	SLU 36	-541	470	3579	-12.99	-17	0.04
2	SLU 37	-541	470	3579	-12.99	-17	0.04
2	SLU 38	-541	470	3579	-12.99	-17	0.04
2	SLU 39	-585	492	3806	-13.46	-18.56	0.05
2	SLU 40	-585	492	3806	-13.46	-18.56	0.05
2	SLU 41	-585	492	3806	-13.46	-18.56	0.05



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
2	SLU 42	-585	492	3806	-13.46	-18.56	0.05
2	SLU 43	-477	491	3461	-14.22	-14.16	0.01
2	SLU 44	-477	491	3461	-14.22	-14.16	0.01
2	SLU 45	-477	491	3461	-14.22	-14.16	0.01
2	SLU 46	-477	491	3461	-14.22	-14.16	0.01
2	SLU 47	-477	491	3461	-14.22	-14.16	0.01
2	SLU 48	-477	491	3461	-14.22	-14.16	0.01
2	SLU 49	-477	491	3461	-14.22	-14.16	0.01
2	SLU 50	-477	491	3461	-14.22	-14.16	0.01
2	SLU 51	-477	491	3461	-14.22	-14.16	0.01
2	SLU 52	-580	542	3990	-15.32	-17.8	0.03
2	SLU 53	-580	542	3990	-15.32	-17.8	0.03
2	SLU 54	-580	542	3990	-15.32	-17.8	0.03
2	SLU 55	-580	542	3990	-15.32	-17.8	0.03
2	SLU 56	-580	542	3990	-15.32	-17.8	0.03
2	SLU 57	-580	542	3990	-15.32	-17.8	0.03
2	SLU 58	-580	542	3990	-15.32	-17.8	0.03
2	SLU 59	-580	542	3990	-15.32	-17.8	0.03
2	SLU 60	-624	564	4217	-15.79	-19.36	0.04
2	SLU 61	-624	564	4217	-15.79	-19.36	0.04
2	SLU 62	-624	564	4217	-15.79	-19.36	0.04
2	SLU 63	-624	564	4217	-15.79	-19.36	0.04
2	SLU 64	-533	523	3767	-14.98	-16.11	0.02
2	SLU 65	-533	523	3767	-14.98	-16.11	0.02
2	SLU 66	-533	523	3767	-14.98	-16.11	0.02
2	SLU 67	-533	523	3767	-14.98	-16.11	0.02
2	SLU 68	-533	523	3767	-14.98	-16.11	0.02
2	SLU 69	-533	523	3767	-14.98	-16.11	0.02
2	SLU 70	-533	523	3767	-14.98	-16.11	0.02
2	SLU 71	-533	523	3767	-14.98	-16.11	0.02
2	SLU 72	-533	523	3767	-14.98	-16.11	0.02
2	SLU 73	-636	575	4297	-16.07	-19.75	0.04
2	SLU 74	-636	575	4297	-16.07	-19.75	0.04
2	SLU 75	-636	575	4297	-16.07	-19.75	0.04
2	SLU 76	-636	575	4297	-16.07	-19.75	0.04
2	SLU 77	-636	575	4297	-16.07	-19.75	0.04
2	SLU 78	-636	575	4297	-16.07	-19.75	0.04
2	SLU 79	-636	575	4297	-16.07	-19.75	0.04
2	SLU 80	-636	575	4297	-16.07	-19.75	0.04
2	SLU 81	-680	597	4524	-16.54	-21.31	0.05
2	SLU 82	-680	597	4524	-16.54	-21.31	0.05
2	SLU 83	-680	597	4524	-16.54	-21.31	0.05
2	SLU 84	-680	597	4524	-16.54	-21.31	0.05
2	SLE RA 1	-398	395	2831	-11.35	-11.97	0.01
2	SLE RA 2	-398	395	2831	-11.35	-11.97	0.01
2	SLE RA 3	-398	395	2831	-11.35	-11.97	0.01
2	SLE RA 4	-398	395	2831	-11.35	-11.97	0.01
2	SLE RA 5	-398	395	2831	-11.35	-11.97	0.01
2	SLE RA 6	-398	395	2831	-11.35	-11.97	0.01
2	SLE RA 7	-398	395	2831	-11.35	-11.97	0.01
2	SLE RA 8	-398	395	2831	-11.35	-11.97	0.01
2	SLE RA 9	-398	395	2831	-11.35	-11.97	0.01
2	SLE RA 10	-466	430	3184	-12.09	-14.39	0.03
2	SLE RA 11	-466	430	3184	-12.09	-14.39	0.03
2	SLE RA 12	-466	430	3184	-12.09	-14.39	0.03
2	SLE RA 13	-466	430	3184	-12.09	-14.39	0.03
2	SLE RA 14	-466	430	3184	-12.09	-14.39	0.03
2	SLE RA 15	-466	430	3184	-12.09	-14.39	0.03
2	SLE RA 16	-466	430	3184	-12.09	-14.39	0.03
2	SLE RA 17	-466	430	3184	-12.09	-14.39	0.03
2	SLE RA 18	-496	444	3335	-12.4	-15.43	0.03
2	SLE RA 19	-496	444	3335	-12.4	-15.43	0.03
2	SLE RA 20	-496	444	3335	-12.4	-15.43	0.03
2	SLE RA 21	-496	444	3335	-12.4	-15.43	0.03
2	SLE FR 1	-398	395	2831	-11.35	-11.97	0.01
2	SLE FR 2	-398	395	2831	-11.35	-11.97	0.01
2	SLE FR 3	-398	395	2831	-11.35	-11.97	0.01
2	SLE FR 4	-427	410	2982	-11.67	-13	0.02
2	SLE FR 5	-427	410	2982	-11.67	-13	0.02
2	SLE FR 6	-447	420	3083	-11.88	-13.7	0.02
2	SLE QP 1	-398	395	2831	-11.35	-11.97	0.01
2	SLE QP 2	-427	410	2982	-11.67	-13	0.02
2	SLD 1	-346	409	2763	-12.12	-8.79	-0.03
2	SLD 2	-346	409	2763	-12.12	-8.79	-0.03
2	SLD 3	-331	333	2503	-8.79	-9.34	0
2	SLD 4	-331	333	2503	-8.79	-9.34	0
2	SLD 5	-426	525	3311	-16.85	-10.9	-0.04
2	SLD 6	-426	525	3311	-16.85	-10.9	-0.04
2	SLD 7	-375	272	2443	-5.76	-12.74	0.06
2	SLD 8	-375	272	2443	-5.76	-12.74	0.06
2	SLD 9	-480	548	3520	-17.58	-13.27	-0.02
2	SLD 10	-480	548	3520	-17.58	-13.27	-0.02
2	SLD 11	-428	295	2653	-6.48	-15.11	0.08
2	SLD 12	-428	295	2653	-6.48	-15.11	0.08
2	SLD 13	-524	487	3461	-14.54	-16.67	0.04
2	SLD 14	-524	487	3461	-14.54	-16.67	0.04
2	SLD 15	-509	411	3201	-11.21	-17.22	0.07
2	SLD 16	-509	411	3201	-11.21	-17.22	0.07



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
2	SLV 1	-238	409	2477	-12.79	-3.04	-0.1
2	SLV 2	-238	409	2477	-12.79	-3.04	-0.1
2	SLV 3	-198	229	1851	-4.84	-4.4	-0.03
2	SLV 4	-198	229	1851	-4.84	-4.4	-0.03
2	SLV 5	-430	683	3780	-24.07	-7.94	-0.13
2	SLV 6	-430	683	3780	-24.07	-7.94	-0.13
2	SLV 7	-299	82	1693	2.44	-12.49	0.12
2	SLV 8	-299	82	1693	2.44	-12.49	0.12
2	SLV 9	-556	738	4270	-25.78	-13.51	-0.08
2	SLV 10	-556	738	4270	-25.78	-13.51	-0.08
2	SLV 11	-425	137	2184	0.73	-18.07	0.17
2	SLV 12	-425	137	2184	0.73	-18.07	0.17
2	SLV 13	-656	591	4113	-18.5	-21.61	0.07
2	SLV 14	-656	591	4113	-18.5	-21.61	0.07
2	SLV 15	-617	411	3487	-10.54	-22.97	0.14
2	SLV 16	-617	411	3487	-10.54	-22.97	0.14
3	SLU 1	-288	3	2118	-0.82	-18.75	0.01
3	SLU 2	-288	3	2118	-0.82	-18.75	0.01
3	SLU 3	-288	3	2118	-0.82	-18.75	0.01
3	SLU 4	-288	3	2118	-0.82	-18.75	0.01
3	SLU 5	-288	3	2118	-0.82	-18.75	0.01
3	SLU 6	-288	3	2118	-0.82	-18.75	0.01
3	SLU 7	-288	3	2118	-0.82	-18.75	0.01
3	SLU 8	-288	3	2118	-0.82	-18.75	0.01
3	SLU 9	-288	3	2118	-0.82	-18.75	0.01
3	SLU 10	-400	3	2523	-0.94	-25.44	0.01
3	SLU 11	-400	3	2523	-0.94	-25.44	0.01
3	SLU 12	-400	3	2523	-0.94	-25.44	0.01
3	SLU 13	-400	3	2523	-0.94	-25.44	0.01
3	SLU 14	-400	3	2523	-0.94	-25.44	0.01
3	SLU 15	-400	3	2523	-0.94	-25.44	0.01
3	SLU 16	-400	3	2523	-0.94	-25.44	0.01
3	SLU 17	-400	3	2523	-0.94	-25.44	0.01
3	SLU 18	-449	3	2697	-0.99	-28.31	0.01
3	SLU 19	-449	3	2697	-0.99	-28.31	0.01
3	SLU 20	-449	3	2697	-0.99	-28.31	0.01
3	SLU 21	-449	3	2697	-0.99	-28.31	0.01
3	SLU 22	-347	3	2353	-0.89	-22.29	0.01
3	SLU 23	-347	3	2353	-0.89	-22.29	0.01
3	SLU 24	-347	3	2353	-0.89	-22.29	0.01
3	SLU 25	-347	3	2353	-0.89	-22.29	0.01
3	SLU 26	-347	3	2353	-0.89	-22.29	0.01
3	SLU 27	-347	3	2353	-0.89	-22.29	0.01
3	SLU 28	-347	3	2353	-0.89	-22.29	0.01
3	SLU 29	-347	3	2353	-0.89	-22.29	0.01
3	SLU 30	-347	3	2353	-0.89	-22.29	0.01
3	SLU 31	-460	3	2758	-1.01	-28.98	0.01
3	SLU 32	-460	3	2758	-1.01	-28.98	0.01
3	SLU 33	-460	3	2758	-1.01	-28.98	0.01
3	SLU 34	-460	3	2758	-1.01	-28.98	0.01
3	SLU 35	-460	3	2758	-1.01	-28.98	0.01
3	SLU 36	-460	3	2758	-1.01	-28.98	0.01
3	SLU 37	-460	3	2758	-1.01	-28.98	0.01
3	SLU 38	-460	3	2758	-1.01	-28.98	0.01
3	SLU 39	-508	3	2932	-1.06	-31.85	0.02
3	SLU 40	-508	3	2932	-1.06	-31.85	0.02
3	SLU 41	-508	3	2932	-1.06	-31.85	0.02
3	SLU 42	-508	3	2932	-1.06	-31.85	0.02
3	SLU 43	-354	3	2673	-1.04	-23.17	0.01
3	SLU 44	-354	3	2673	-1.04	-23.17	0.01
3	SLU 45	-354	3	2673	-1.04	-23.17	0.01
3	SLU 46	-354	3	2673	-1.04	-23.17	0.01
3	SLU 47	-354	3	2673	-1.04	-23.17	0.01
3	SLU 48	-354	3	2673	-1.04	-23.17	0.01
3	SLU 49	-354	3	2673	-1.04	-23.17	0.01
3	SLU 50	-354	3	2673	-1.04	-23.17	0.01
3	SLU 51	-354	3	2673	-1.04	-23.17	0.01
3	SLU 52	-466	4	3078	-1.16	-29.85	0.02
3	SLU 53	-466	4	3078	-1.16	-29.85	0.02
3	SLU 54	-466	4	3078	-1.16	-29.85	0.02
3	SLU 55	-466	4	3078	-1.16	-29.85	0.02
3	SLU 56	-466	4	3078	-1.16	-29.85	0.02
3	SLU 57	-466	4	3078	-1.16	-29.85	0.02
3	SLU 58	-466	4	3078	-1.16	-29.85	0.02
3	SLU 59	-466	4	3078	-1.16	-29.85	0.02
3	SLU 60	-515	4	3252	-1.21	-32.72	0.02
3	SLU 61	-515	4	3252	-1.21	-32.72	0.02
3	SLU 62	-515	4	3252	-1.21	-32.72	0.02
3	SLU 63	-515	4	3252	-1.21	-32.72	0.02
3	SLU 64	-413	4	2908	-1.11	-26.71	0.02
3	SLU 65	-413	4	2908	-1.11	-26.71	0.02
3	SLU 66	-413	4	2908	-1.11	-26.71	0.02
3	SLU 67	-413	4	2908	-1.11	-26.71	0.02
3	SLU 68	-413	4	2908	-1.11	-26.71	0.02
3	SLU 69	-413	4	2908	-1.11	-26.71	0.02
3	SLU 70	-413	4	2908	-1.11	-26.71	0.02
3	SLU 71	-413	4	2908	-1.11	-26.71	0.02
3	SLU 72	-413	4	2908	-1.11	-26.71	0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
3	SLU 73	-526	4	3313	-1.23	-33.39	0.02
3	SLU 74	-526	4	3313	-1.23	-33.39	0.02
3	SLU 75	-526	4	3313	-1.23	-33.39	0.02
3	SLU 76	-526	4	3313	-1.23	-33.39	0.02
3	SLU 77	-526	4	3313	-1.23	-33.39	0.02
3	SLU 78	-526	4	3313	-1.23	-33.39	0.02
3	SLU 79	-526	4	3313	-1.23	-33.39	0.02
3	SLU 80	-526	4	3313	-1.23	-33.39	0.02
3	SLU 81	-574	4	3487	-1.28	-36.26	0.02
3	SLU 82	-574	4	3487	-1.28	-36.26	0.02
3	SLU 83	-574	4	3487	-1.28	-36.26	0.02
3	SLU 84	-574	4	3487	-1.28	-36.26	0.02
3	SLE RA 1	-304	3	2185	-0.84	-19.77	0.01
3	SLE RA 2	-304	3	2185	-0.84	-19.77	0.01
3	SLE RA 3	-304	3	2185	-0.84	-19.77	0.01
3	SLE RA 4	-304	3	2185	-0.84	-19.77	0.01
3	SLE RA 5	-304	3	2185	-0.84	-19.77	0.01
3	SLE RA 6	-304	3	2185	-0.84	-19.77	0.01
3	SLE RA 7	-304	3	2185	-0.84	-19.77	0.01
3	SLE RA 8	-304	3	2185	-0.84	-19.77	0.01
3	SLE RA 9	-304	3	2185	-0.84	-19.77	0.01
3	SLE RA 10	-380	3	2455	-0.92	-24.22	0.01
3	SLE RA 11	-380	3	2455	-0.92	-24.22	0.01
3	SLE RA 12	-380	3	2455	-0.92	-24.22	0.01
3	SLE RA 13	-380	3	2455	-0.92	-24.22	0.01
3	SLE RA 14	-380	3	2455	-0.92	-24.22	0.01
3	SLE RA 15	-380	3	2455	-0.92	-24.22	0.01
3	SLE RA 16	-380	3	2455	-0.92	-24.22	0.01
3	SLE RA 17	-380	3	2455	-0.92	-24.22	0.01
3	SLE RA 18	-412	3	2571	-0.95	-26.13	0.01
3	SLE RA 19	-412	3	2571	-0.95	-26.13	0.01
3	SLE RA 20	-412	3	2571	-0.95	-26.13	0.01
3	SLE RA 21	-412	3	2571	-0.95	-26.13	0.01
3	SLE FR 1	-304	3	2185	-0.84	-19.77	0.01
3	SLE FR 2	-304	3	2185	-0.84	-19.77	0.01
3	SLE FR 3	-304	3	2185	-0.84	-19.77	0.01
3	SLE FR 4	-337	3	2301	-0.87	-21.68	0.01
3	SLE FR 5	-337	3	2301	-0.87	-21.68	0.01
3	SLE FR 6	-358	3	2378	-0.9	-22.95	0.01
3	SLE QP 1	-304	3	2185	-0.84	-19.77	0.01
3	SLE QP 2	-337	3	2301	-0.87	-21.68	0.01
3	SLD 1	-192	10	2175	-7.34	-14.44	0
3	SLD 2	-192	10	2175	-7.34	-14.44	0
3	SLD 3	-219	13	2014	-3.01	-13.56	-0.02
3	SLD 4	-219	13	2014	-3.01	-13.56	-0.02
3	SLD 5	-251	0	2506	-9.38	-20.83	0.04
3	SLD 6	-251	0	2506	-9.38	-20.83	0.04
3	SLD 7	-343	11	1972	5.06	-17.92	-0.02
3	SLD 8	-343	11	1972	5.06	-17.92	-0.02
3	SLD 9	-330	-5	2630	-6.8	-25.43	0.05
3	SLD 10	-330	-5	2630	-6.8	-25.43	0.05
3	SLD 11	-422	5	2096	7.64	-22.52	-0.01
3	SLD 12	-422	5	2096	7.64	-22.52	-0.01
3	SLD 13	-454	-8	2588	1.26	-29.79	0.04
3	SLD 14	-454	-8	2588	1.26	-29.79	0.04
3	SLD 15	-482	-5	2427	5.59	-28.91	0.02
3	SLD 16	-482	-5	2427	5.59	-28.91	0.02
3	SLV 1	4	20	2010	-17.2	-4.65	-0.01
3	SLV 2	4	20	2010	-17.2	-4.65	-0.01
3	SLV 3	-61	29	1624	-6.06	-2.56	-0.06
3	SLV 4	-61	29	1624	-6.06	-2.56	-0.06
3	SLV 5	-136	-5	2798	-22.67	-19.74	0.08
3	SLV 6	-136	-5	2798	-22.67	-19.74	0.08
3	SLV 7	-353	23	1513	14.47	-12.77	-0.08
3	SLV 8	-353	23	1513	14.47	-12.77	-0.08
3	SLV 9	-321	-18	3089	-16.22	-30.58	0.11
3	SLV 10	-321	-18	3089	-16.22	-30.58	0.11
3	SLV 11	-538	10	1803	20.92	-23.61	-0.06
3	SLV 12	-538	10	1803	20.92	-23.61	-0.06
3	SLV 13	-613	-23	2977	4.31	-40.79	0.08
3	SLV 14	-613	-23	2977	4.31	-40.79	0.08
3	SLV 15	-678	-15	2592	15.46	-38.7	0.03
3	SLV 16	-678	-15	2592	15.46	-38.7	0.03
4	SLU 1	-242	0	1883	-0.37	-13.76	0
4	SLU 2	-242	0	1883	-0.37	-13.76	0
4	SLU 3	-242	0	1883	-0.37	-13.76	0
4	SLU 4	-242	0	1883	-0.37	-13.76	0
4	SLU 5	-242	0	1883	-0.37	-13.76	0
4	SLU 6	-242	0	1883	-0.37	-13.76	0
4	SLU 7	-242	0	1883	-0.37	-13.76	0
4	SLU 8	-242	0	1883	-0.37	-13.76	0
4	SLU 9	-242	0	1883	-0.37	-13.76	0
4	SLU 10	-350	0	2244	-0.43	-19.68	0
4	SLU 11	-350	0	2244	-0.43	-19.68	0
4	SLU 12	-350	0	2244	-0.43	-19.68	0
4	SLU 13	-350	0	2244	-0.43	-19.68	0
4	SLU 14	-350	0	2244	-0.43	-19.68	0
4	SLU 15	-350	0	2244	-0.43	-19.68	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
4	SLU 16	-350	0	2244	-0.43	-19.68	0
4	SLU 17	-350	0	2244	-0.43	-19.68	0
4	SLU 18	-397	0	2399	-0.46	-22.22	0
4	SLU 19	-397	0	2399	-0.46	-22.22	0
4	SLU 20	-397	0	2399	-0.46	-22.22	0
4	SLU 21	-397	0	2399	-0.46	-22.22	0
4	SLU 22	-298	0	2093	-0.41	-16.83	0
4	SLU 23	-298	0	2093	-0.41	-16.83	0
4	SLU 24	-298	0	2093	-0.41	-16.83	0
4	SLU 25	-298	0	2093	-0.41	-16.83	0
4	SLU 26	-298	0	2093	-0.41	-16.83	0
4	SLU 27	-298	0	2093	-0.41	-16.83	0
4	SLU 28	-298	0	2093	-0.41	-16.83	0
4	SLU 29	-298	0	2093	-0.41	-16.83	0
4	SLU 30	-298	0	2093	-0.41	-16.83	0
4	SLU 31	-407	0	2455	-0.47	-22.75	0
4	SLU 32	-407	0	2455	-0.47	-22.75	0
4	SLU 33	-407	0	2455	-0.47	-22.75	0
4	SLU 34	-407	0	2455	-0.47	-22.75	0
4	SLU 35	-407	0	2455	-0.47	-22.75	0
4	SLU 36	-407	0	2455	-0.47	-22.75	0
4	SLU 37	-407	0	2455	-0.47	-22.75	0
4	SLU 38	-407	0	2455	-0.47	-22.75	0
4	SLU 39	-453	1	2610	-0.49	-25.29	-0.01
4	SLU 40	-453	1	2610	-0.49	-25.29	-0.01
4	SLU 41	-453	1	2610	-0.49	-25.29	-0.01
4	SLU 42	-453	1	2610	-0.49	-25.29	-0.01
4	SLU 43	-295	0	2375	-0.47	-16.83	-0.01
4	SLU 44	-295	0	2375	-0.47	-16.83	-0.01
4	SLU 45	-295	0	2375	-0.47	-16.83	-0.01
4	SLU 46	-295	0	2375	-0.47	-16.83	-0.01
4	SLU 47	-295	0	2375	-0.47	-16.83	-0.01
4	SLU 48	-295	0	2375	-0.47	-16.83	-0.01
4	SLU 49	-295	0	2375	-0.47	-16.83	-0.01
4	SLU 50	-295	0	2375	-0.47	-16.83	-0.01
4	SLU 51	-295	0	2375	-0.47	-16.83	-0.01
4	SLU 52	-404	1	2737	-0.53	-22.76	-0.01
4	SLU 53	-404	1	2737	-0.53	-22.76	-0.01
4	SLU 54	-404	1	2737	-0.53	-22.76	-0.01
4	SLU 55	-404	1	2737	-0.53	-22.76	-0.01
4	SLU 56	-404	1	2737	-0.53	-22.76	-0.01
4	SLU 57	-404	1	2737	-0.53	-22.76	-0.01
4	SLU 58	-404	1	2737	-0.53	-22.76	-0.01
4	SLU 59	-404	1	2737	-0.53	-22.76	-0.01
4	SLU 60	-450	1	2892	-0.56	-25.3	-0.01
4	SLU 61	-450	1	2892	-0.56	-25.3	-0.01
4	SLU 62	-450	1	2892	-0.56	-25.3	-0.01
4	SLU 63	-450	1	2892	-0.56	-25.3	-0.01
4	SLU 64	-351	0	2586	-0.51	-19.9	-0.01
4	SLU 65	-351	0	2586	-0.51	-19.9	-0.01
4	SLU 66	-351	0	2586	-0.51	-19.9	-0.01
4	SLU 67	-351	0	2586	-0.51	-19.9	-0.01
4	SLU 68	-351	0	2586	-0.51	-19.9	-0.01
4	SLU 69	-351	0	2586	-0.51	-19.9	-0.01
4	SLU 70	-351	0	2586	-0.51	-19.9	-0.01
4	SLU 71	-351	0	2586	-0.51	-19.9	-0.01
4	SLU 72	-351	0	2586	-0.51	-19.9	-0.01
4	SLU 73	-460	1	2947	-0.57	-25.83	-0.01
4	SLU 74	-460	1	2947	-0.57	-25.83	-0.01
4	SLU 75	-460	1	2947	-0.57	-25.83	-0.01
4	SLU 76	-460	1	2947	-0.57	-25.83	-0.01
4	SLU 77	-460	1	2947	-0.57	-25.83	-0.01
4	SLU 78	-460	1	2947	-0.57	-25.83	-0.01
4	SLU 79	-460	1	2947	-0.57	-25.83	-0.01
4	SLU 80	-460	1	2947	-0.57	-25.83	-0.01
4	SLU 81	-507	1	3102	-0.59	-28.36	-0.01
4	SLU 82	-507	1	3102	-0.59	-28.36	-0.01
4	SLU 83	-507	1	3102	-0.59	-28.36	-0.01
4	SLU 84	-507	1	3102	-0.59	-28.36	-0.01
4	SLE RA 1	-258	0	1943	-0.38	-14.63	0
4	SLE RA 2	-258	0	1943	-0.38	-14.63	0
4	SLE RA 3	-258	0	1943	-0.38	-14.63	0
4	SLE RA 4	-258	0	1943	-0.38	-14.63	0
4	SLE RA 5	-258	0	1943	-0.38	-14.63	0
4	SLE RA 6	-258	0	1943	-0.38	-14.63	0
4	SLE RA 7	-258	0	1943	-0.38	-14.63	0
4	SLE RA 8	-258	0	1943	-0.38	-14.63	0
4	SLE RA 9	-258	0	1943	-0.38	-14.63	0
4	SLE RA 10	-330	0	2184	-0.42	-18.58	0
4	SLE RA 11	-330	0	2184	-0.42	-18.58	0
4	SLE RA 12	-330	0	2184	-0.42	-18.58	0
4	SLE RA 13	-330	0	2184	-0.42	-18.58	0
4	SLE RA 14	-330	0	2184	-0.42	-18.58	0
4	SLE RA 15	-330	0	2184	-0.42	-18.58	0
4	SLE RA 16	-330	0	2184	-0.42	-18.58	0
4	SLE RA 17	-330	0	2184	-0.42	-18.58	0
4	SLE RA 18	-361	0	2287	-0.44	-20.28	0
4	SLE RA 19	-361	0	2287	-0.44	-20.28	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
4	SLE RA 20	-361	0	2287	-0.44	-20.28	0
4	SLE RA 21	-361	0	2287	-0.44	-20.28	0
4	SLE FR 1	-258	0	1943	-0.38	-14.63	0
4	SLE FR 2	-258	0	1943	-0.38	-14.63	0
4	SLE FR 3	-258	0	1943	-0.38	-14.63	0
4	SLE FR 4	-289	0	2046	-0.4	-16.33	0
4	SLE FR 5	-289	0	2046	-0.4	-16.33	0
4	SLE FR 6	-310	0	2115	-0.41	-17.46	0
4	SLE QP 1	-258	0	1943	-0.38	-14.63	0
4	SLE QP 2	-289	0	2046	-0.4	-16.33	0
4	SLD 1	-131	9	1981	-12.56	-7.57	-0.03
4	SLD 2	-131	9	1981	-12.56	-7.57	-0.03
4	SLD 3	-154	15	1880	-3.45	-8.52	-0.08
4	SLD 4	-154	15	1880	-3.45	-8.52	-0.08
4	SLD 5	-208	-7	2180	-17.86	-12.26	0.05
4	SLD 6	-208	-7	2180	-17.86	-12.26	0.05
4	SLD 7	-282	14	1844	12.5	-15.42	-0.09
4	SLD 8	-282	14	1844	12.5	-15.42	-0.09
4	SLD 9	-296	-14	2249	-13.3	-17.23	0.08
4	SLD 10	-296	-14	2249	-13.3	-17.23	0.08
4	SLD 11	-370	7	1913	17.07	-20.39	-0.06
4	SLD 12	-370	7	1913	17.07	-20.39	-0.06
4	SLD 13	-424	-14	2212	2.65	-24.14	0.07
4	SLD 14	-424	-14	2212	2.65	-24.14	0.07
4	SLD 15	-446	-8	2111	11.76	-25.08	0.02
4	SLD 16	-446	-8	2111	11.76	-25.08	0.02
4	SLV 1	82	21	1898	-31.35	4.3	-0.07
4	SLV 2	82	21	1898	-31.35	4.3	-0.07
4	SLV 3	30	37	1655	-7.79	2.05	-0.18
4	SLV 4	30	37	1655	-7.79	2.05	-0.18
4	SLV 5	-98	-18	2371	-45.41	-6.74	0.14
4	SLV 6	-98	-18	2371	-45.41	-6.74	0.14
4	SLV 7	-273	36	1560	33.11	-14.21	-0.23
4	SLV 8	-273	36	1560	33.11	-14.21	-0.23
4	SLV 9	-305	-35	2533	-33.91	-18.44	0.22
4	SLV 10	-305	-35	2533	-33.91	-18.44	0.22
4	SLV 11	-480	19	1722	44.61	-25.91	-0.15
4	SLV 12	-480	19	1722	44.61	-25.91	-0.15
4	SLV 13	-607	-36	2438	6.99	-34.71	0.18
4	SLV 14	-607	-36	2438	6.99	-34.71	0.18
4	SLV 15	-660	-20	2194	30.55	-36.95	0.07
4	SLV 16	-660	-20	2194	30.55	-36.95	0.07
5	SLU 1	-227	0	1800	-0.19	-13.44	0
5	SLU 2	-227	0	1800	-0.19	-13.44	0
5	SLU 3	-227	0	1800	-0.19	-13.44	0
5	SLU 4	-227	0	1800	-0.19	-13.44	0
5	SLU 5	-227	0	1800	-0.19	-13.44	0
5	SLU 6	-227	0	1800	-0.19	-13.44	0
5	SLU 7	-227	0	1800	-0.19	-13.44	0
5	SLU 8	-227	0	1800	-0.19	-13.44	0
5	SLU 9	-227	0	1800	-0.19	-13.44	0
5	SLU 10	-338	0	2160	-0.22	-19.7	0
5	SLU 11	-338	0	2160	-0.22	-19.7	0
5	SLU 12	-338	0	2160	-0.22	-19.7	0
5	SLU 13	-338	0	2160	-0.22	-19.7	0
5	SLU 14	-338	0	2160	-0.22	-19.7	0
5	SLU 15	-338	0	2160	-0.22	-19.7	0
5	SLU 16	-338	0	2160	-0.22	-19.7	0
5	SLU 17	-338	0	2160	-0.22	-19.7	0
5	SLU 18	-386	0	2314	-0.23	-22.38	0
5	SLU 19	-386	0	2314	-0.23	-22.38	0
5	SLU 20	-386	0	2314	-0.23	-22.38	0
5	SLU 21	-386	0	2314	-0.23	-22.38	0
5	SLU 22	-284	0	2008	-0.21	-16.66	0
5	SLU 23	-284	0	2008	-0.21	-16.66	0
5	SLU 24	-284	0	2008	-0.21	-16.66	0
5	SLU 25	-284	0	2008	-0.21	-16.66	0
5	SLU 26	-284	0	2008	-0.21	-16.66	0
5	SLU 27	-284	0	2008	-0.21	-16.66	0
5	SLU 28	-284	0	2008	-0.21	-16.66	0
5	SLU 29	-284	0	2008	-0.21	-16.66	0
5	SLU 30	-284	0	2008	-0.21	-16.66	0
5	SLU 31	-395	0	2368	-0.24	-22.92	0
5	SLU 32	-395	0	2368	-0.24	-22.92	0
5	SLU 33	-395	0	2368	-0.24	-22.92	0
5	SLU 34	-395	0	2368	-0.24	-22.92	0
5	SLU 35	-395	0	2368	-0.24	-22.92	0
5	SLU 36	-395	0	2368	-0.24	-22.92	0
5	SLU 37	-395	0	2368	-0.24	-22.92	0
5	SLU 38	-395	0	2368	-0.24	-22.92	0
5	SLU 39	-443	0	2522	-0.25	-25.6	0
5	SLU 40	-443	0	2522	-0.25	-25.6	0
5	SLU 41	-443	0	2522	-0.25	-25.6	0
5	SLU 42	-443	0	2522	-0.25	-25.6	0
5	SLU 43	-275	0	2269	-0.24	-16.36	0
5	SLU 44	-275	0	2269	-0.24	-16.36	0
5	SLU 45	-275	0	2269	-0.24	-16.36	0
5	SLU 46	-275	0	2269	-0.24	-16.36	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
5	SLU 47	-275	0	2269	-0.24	-16.36	0
5	SLU 48	-275	0	2269	-0.24	-16.36	0
5	SLU 49	-275	0	2269	-0.24	-16.36	0
5	SLU 50	-275	0	2269	-0.24	-16.36	0
5	SLU 51	-275	0	2269	-0.24	-16.36	0
5	SLU 52	-387	0	2628	-0.27	-22.62	0
5	SLU 53	-387	0	2628	-0.27	-22.62	0
5	SLU 54	-387	0	2628	-0.27	-22.62	0
5	SLU 55	-387	0	2628	-0.27	-22.62	0
5	SLU 56	-387	0	2628	-0.27	-22.62	0
5	SLU 57	-387	0	2628	-0.27	-22.62	0
5	SLU 58	-387	0	2628	-0.27	-22.62	0
5	SLU 59	-387	0	2628	-0.27	-22.62	0
5	SLU 60	-434	0	2782	-0.28	-25.31	0
5	SLU 61	-434	0	2782	-0.28	-25.31	0
5	SLU 62	-434	0	2782	-0.28	-25.31	0
5	SLU 63	-434	0	2782	-0.28	-25.31	0
5	SLU 64	-332	0	2477	-0.26	-19.58	0
5	SLU 65	-332	0	2477	-0.26	-19.58	0
5	SLU 66	-332	0	2477	-0.26	-19.58	0
5	SLU 67	-332	0	2477	-0.26	-19.58	0
5	SLU 68	-332	0	2477	-0.26	-19.58	0
5	SLU 69	-332	0	2477	-0.26	-19.58	0
5	SLU 70	-332	0	2477	-0.26	-19.58	0
5	SLU 71	-332	0	2477	-0.26	-19.58	0
5	SLU 72	-332	0	2477	-0.26	-19.58	0
5	SLU 73	-444	0	2837	-0.29	-25.84	0
5	SLU 74	-444	0	2837	-0.29	-25.84	0
5	SLU 75	-444	0	2837	-0.29	-25.84	0
5	SLU 76	-444	0	2837	-0.29	-25.84	0
5	SLU 77	-444	0	2837	-0.29	-25.84	0
5	SLU 78	-444	0	2837	-0.29	-25.84	0
5	SLU 79	-444	0	2837	-0.29	-25.84	0
5	SLU 80	-444	0	2837	-0.29	-25.84	0
5	SLU 81	-492	0	2991	-0.3	-28.53	0
5	SLU 82	-492	0	2991	-0.3	-28.53	0
5	SLU 83	-492	0	2991	-0.3	-28.53	0
5	SLU 84	-492	0	2991	-0.3	-28.53	0
5	SLE RA 1	-243	0	1860	-0.2	-14.36	0
5	SLE RA 2	-243	0	1860	-0.2	-14.36	0
5	SLE RA 3	-243	0	1860	-0.2	-14.36	0
5	SLE RA 4	-243	0	1860	-0.2	-14.36	0
5	SLE RA 5	-243	0	1860	-0.2	-14.36	0
5	SLE RA 6	-243	0	1860	-0.2	-14.36	0
5	SLE RA 7	-243	0	1860	-0.2	-14.36	0
5	SLE RA 8	-243	0	1860	-0.2	-14.36	0
5	SLE RA 9	-243	0	1860	-0.2	-14.36	0
5	SLE RA 10	-317	0	2099	-0.22	-18.53	0
5	SLE RA 11	-317	0	2099	-0.22	-18.53	0
5	SLE RA 12	-317	0	2099	-0.22	-18.53	0
5	SLE RA 13	-317	0	2099	-0.22	-18.53	0
5	SLE RA 14	-317	0	2099	-0.22	-18.53	0
5	SLE RA 15	-317	0	2099	-0.22	-18.53	0
5	SLE RA 16	-317	0	2099	-0.22	-18.53	0
5	SLE RA 17	-317	0	2099	-0.22	-18.53	0
5	SLE RA 18	-349	0	2202	-0.23	-20.32	0
5	SLE RA 19	-349	0	2202	-0.23	-20.32	0
5	SLE RA 20	-349	0	2202	-0.23	-20.32	0
5	SLE RA 21	-349	0	2202	-0.23	-20.32	0
5	SLE FR 1	-243	0	1860	-0.2	-14.36	0
5	SLE FR 2	-243	0	1860	-0.2	-14.36	0
5	SLE FR 3	-243	0	1860	-0.2	-14.36	0
5	SLE FR 4	-275	0	1962	-0.2	-16.14	0
5	SLE FR 5	-275	0	1962	-0.2	-16.14	0
5	SLE FR 6	-296	0	2031	-0.21	-17.34	0
5	SLE QP 1	-243	0	1860	-0.2	-14.36	0
5	SLE QP 2	-275	0	1962	-0.2	-16.14	0
5	SLD 1	-106	6	1936	-17.6	-6.6	-0.03
5	SLD 2	-106	6	1936	-17.6	-6.6	-0.03
5	SLD 3	-125	17	1867	-3.27	-7.47	-0.08
5	SLD 4	-125	17	1867	-3.27	-7.47	-0.08
5	SLD 5	-197	-14	2059	-27.17	-11.96	0.07
5	SLD 6	-197	-14	2059	-27.17	-11.96	0.07
5	SLD 7	-258	21	1829	20.62	-14.86	-0.1
5	SLD 8	-258	21	1829	20.62	-14.86	-0.1
5	SLD 9	-292	-20	2095	-21.03	-17.43	0.1
5	SLD 10	-292	-20	2095	-21.03	-17.43	0.1
5	SLD 11	-353	14	1866	26.76	-20.33	-0.07
5	SLD 12	-353	14	1866	26.76	-20.33	-0.07
5	SLD 13	-425	-16	2058	2.86	-24.82	0.07
5	SLD 14	-425	-16	2058	2.86	-24.82	0.07
5	SLD 15	-444	-6	1989	17.19	-25.69	0.02
5	SLD 16	-444	-6	1989	17.19	-25.69	0.02
5	SLV 1	123	16	1904	-44.83	6.35	-0.06
5	SLV 2	123	16	1904	-44.83	6.35	-0.06
5	SLV 3	79	42	1737	-7.47	4.28	-0.19
5	SLV 4	79	42	1737	-7.47	4.28	-0.19
5	SLV 5	-90	-35	2197	-70.26	-6.26	0.17



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
5	SLV 6	-90	-35	2197	-70.26	-6.26	0.17
5	SLV 7	-234	52	1642	54.28	-13.15	-0.25
5	SLV 8	-234	52	1642	54.28	-13.15	-0.25
5	SLV 9	-316	-52	2282	-54.69	-19.14	0.25
5	SLV 10	-316	-52	2282	-54.69	-19.14	0.25
5	SLV 11	-460	35	1727	69.85	-26.03	-0.18
5	SLV 12	-460	35	1727	69.85	-26.03	-0.18
5	SLV 13	-629	-41	2188	7.06	-36.57	0.19
5	SLV 14	-629	-41	2188	7.06	-36.57	0.19
5	SLV 15	-673	-15	2021	44.42	-38.64	0.06
5	SLV 16	-673	-15	2021	44.42	-38.64	0.06
6	SLU 1	-214	0	1770	-0.12	-11.76	0
6	SLU 2	-214	0	1770	-0.12	-11.76	0
6	SLU 3	-214	0	1770	-0.12	-11.76	0
6	SLU 4	-214	0	1770	-0.12	-11.76	0
6	SLU 5	-214	0	1770	-0.12	-11.76	0
6	SLU 6	-214	0	1770	-0.12	-11.76	0
6	SLU 7	-214	0	1770	-0.12	-11.76	0
6	SLU 8	-214	0	1770	-0.12	-11.76	0
6	SLU 9	-214	0	1770	-0.12	-11.76	0
6	SLU 10	-323	0	2146	-0.14	-17.65	0
6	SLU 11	-323	0	2146	-0.14	-17.65	0
6	SLU 12	-323	0	2146	-0.14	-17.65	0
6	SLU 13	-323	0	2146	-0.14	-17.65	0
6	SLU 14	-323	0	2146	-0.14	-17.65	0
6	SLU 15	-323	0	2146	-0.14	-17.65	0
6	SLU 16	-323	0	2146	-0.14	-17.65	0
6	SLU 17	-323	0	2146	-0.14	-17.65	0
6	SLU 18	-370	0	2306	-0.14	-20.17	0
6	SLU 19	-370	0	2306	-0.14	-20.17	0
6	SLU 20	-370	0	2306	-0.14	-20.17	0
6	SLU 21	-370	0	2306	-0.14	-20.17	0
6	SLU 22	-270	0	1986	-0.13	-14.75	0
6	SLU 23	-270	0	1986	-0.13	-14.75	0
6	SLU 24	-270	0	1986	-0.13	-14.75	0
6	SLU 25	-270	0	1986	-0.13	-14.75	0
6	SLU 26	-270	0	1986	-0.13	-14.75	0
6	SLU 27	-270	0	1986	-0.13	-14.75	0
6	SLU 28	-270	0	1986	-0.13	-14.75	0
6	SLU 29	-270	0	1986	-0.13	-14.75	0
6	SLU 30	-270	0	1986	-0.13	-14.75	0
6	SLU 31	-378	0	2361	-0.15	-20.63	0
6	SLU 32	-378	0	2361	-0.15	-20.63	0
6	SLU 33	-378	0	2361	-0.15	-20.63	0
6	SLU 34	-378	0	2361	-0.15	-20.63	0
6	SLU 35	-378	0	2361	-0.15	-20.63	0
6	SLU 36	-378	0	2361	-0.15	-20.63	0
6	SLU 37	-378	0	2361	-0.15	-20.63	0
6	SLU 38	-378	0	2361	-0.15	-20.63	0
6	SLU 39	-425	0	2522	-0.16	-23.16	0
6	SLU 40	-425	0	2522	-0.16	-23.16	0
6	SLU 41	-425	0	2522	-0.16	-23.16	0
6	SLU 42	-425	0	2522	-0.16	-23.16	0
6	SLU 43	-260	0	2227	-0.15	-14.26	0
6	SLU 44	-260	0	2227	-0.15	-14.26	0
6	SLU 45	-260	0	2227	-0.15	-14.26	0
6	SLU 46	-260	0	2227	-0.15	-14.26	0
6	SLU 47	-260	0	2227	-0.15	-14.26	0
6	SLU 48	-260	0	2227	-0.15	-14.26	0
6	SLU 49	-260	0	2227	-0.15	-14.26	0
6	SLU 50	-260	0	2227	-0.15	-14.26	0
6	SLU 51	-260	0	2227	-0.15	-14.26	0
6	SLU 52	-368	0	2603	-0.17	-20.15	0
6	SLU 53	-368	0	2603	-0.17	-20.15	0
6	SLU 54	-368	0	2603	-0.17	-20.15	0
6	SLU 55	-368	0	2603	-0.17	-20.15	0
6	SLU 56	-368	0	2603	-0.17	-20.15	0
6	SLU 57	-368	0	2603	-0.17	-20.15	0
6	SLU 58	-368	0	2603	-0.17	-20.15	0
6	SLU 59	-368	0	2603	-0.17	-20.15	0
6	SLU 60	-415	0	2763	-0.18	-22.68	0
6	SLU 61	-415	0	2763	-0.18	-22.68	0
6	SLU 62	-415	0	2763	-0.18	-22.68	0
6	SLU 63	-415	0	2763	-0.18	-22.68	0
6	SLU 64	-315	0	2443	-0.16	-17.25	0
6	SLU 65	-315	0	2443	-0.16	-17.25	0
6	SLU 66	-315	0	2443	-0.16	-17.25	0
6	SLU 67	-315	0	2443	-0.16	-17.25	0
6	SLU 68	-315	0	2443	-0.16	-17.25	0
6	SLU 69	-315	0	2443	-0.16	-17.25	0
6	SLU 70	-315	0	2443	-0.16	-17.25	0
6	SLU 71	-315	0	2443	-0.16	-17.25	0
6	SLU 72	-315	0	2443	-0.16	-17.25	0
6	SLU 73	-424	0	2818	-0.18	-23.14	0
6	SLU 74	-424	0	2818	-0.18	-23.14	0
6	SLU 75	-424	0	2818	-0.18	-23.14	0
6	SLU 76	-424	0	2818	-0.18	-23.14	0
6	SLU 77	-424	0	2818	-0.18	-23.14	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
6	SLU 78	-424	0	2818	-0.18	-23.14	0
6	SLU 79	-424	0	2818	-0.18	-23.14	0
6	SLU 80	-424	0	2818	-0.18	-23.14	0
6	SLU 81	-470	0	2979	-0.19	-25.66	0
6	SLU 82	-470	0	2979	-0.19	-25.66	0
6	SLU 83	-470	0	2979	-0.19	-25.66	0
6	SLU 84	-470	0	2979	-0.19	-25.66	0
6	SLE RA 1	-230	0	1832	-0.12	-12.61	0
6	SLE RA 2	-230	0	1832	-0.12	-12.61	0
6	SLE RA 3	-230	0	1832	-0.12	-12.61	0
6	SLE RA 4	-230	0	1832	-0.12	-12.61	0
6	SLE RA 5	-230	0	1832	-0.12	-12.61	0
6	SLE RA 6	-230	0	1832	-0.12	-12.61	0
6	SLE RA 7	-230	0	1832	-0.12	-12.61	0
6	SLE RA 8	-230	0	1832	-0.12	-12.61	0
6	SLE RA 9	-230	0	1832	-0.12	-12.61	0
6	SLE RA 10	-303	0	2082	-0.13	-16.54	0
6	SLE RA 11	-303	0	2082	-0.13	-16.54	0
6	SLE RA 12	-303	0	2082	-0.13	-16.54	0
6	SLE RA 13	-303	0	2082	-0.13	-16.54	0
6	SLE RA 14	-303	0	2082	-0.13	-16.54	0
6	SLE RA 15	-303	0	2082	-0.13	-16.54	0
6	SLE RA 16	-303	0	2082	-0.13	-16.54	0
6	SLE RA 17	-303	0	2082	-0.13	-16.54	0
6	SLE RA 18	-334	0	2189	-0.14	-18.22	0
6	SLE RA 19	-334	0	2189	-0.14	-18.22	0
6	SLE RA 20	-334	0	2189	-0.14	-18.22	0
6	SLE RA 21	-334	0	2189	-0.14	-18.22	0
6	SLE FR 1	-230	0	1832	-0.12	-12.61	0
6	SLE FR 2	-230	0	1832	-0.12	-12.61	0
6	SLE FR 3	-230	0	1832	-0.12	-12.61	0
6	SLE FR 4	-261	0	1939	-0.13	-14.3	0
6	SLE FR 5	-261	0	1939	-0.13	-14.3	0
6	SLE FR 6	-282	0	2011	-0.13	-15.42	0
6	SLE QP 1	-230	0	1832	-0.12	-12.61	0
6	SLE QP 2	-261	0	1939	-0.13	-14.3	0
6	SLD 1	-83	19	1929	-22.41	-4.17	-0.02
6	SLD 2	-83	19	1929	-22.41	-4.17	-0.02
6	SLD 3	-97	5	1882	-2.87	-4.91	-0.08
6	SLD 4	-97	5	1882	-2.87	-4.91	-0.08
6	SLD 5	-185	27	2007	-36.45	-10.14	0.09
6	SLD 6	-185	27	2007	-36.45	-10.14	0.09
6	SLD 7	-235	-20	1851	28.69	-12.6	-0.12
6	SLD 8	-235	-20	1851	28.69	-12.6	-0.12
6	SLD 9	-288	20	2028	-28.94	-15.99	0.12
6	SLD 10	-288	20	2028	-28.94	-15.99	0.12
6	SLD 11	-337	-27	1871	36.2	-18.45	-0.09
6	SLD 12	-337	-27	1871	36.2	-18.45	-0.09
6	SLD 13	-425	-5	1996	2.62	-23.68	0.08
6	SLD 14	-425	-5	1996	2.62	-23.68	0.08
6	SLD 15	-440	-19	1949	22.16	-24.42	0.02
6	SLD 16	-440	-19	1949	22.16	-24.42	0.02
6	SLV 1	160	47	1916	-57.64	9.54	-0.05
6	SLV 2	160	47	1916	-57.64	9.54	-0.05
6	SLV 3	124	12	1803	-6.23	7.79	-0.21
6	SLV 4	124	12	1803	-6.23	7.79	-0.21
6	SLV 5	-82	68	2105	-95.36	-4.49	0.23
6	SLV 6	-82	68	2105	-95.36	-4.49	0.23
6	SLV 7	-199	-50	1725	76.02	-10.32	-0.31
6	SLV 8	-199	-50	1725	76.02	-10.32	-0.31
6	SLV 9	-323	50	2153	-76.27	-18.27	0.3
6	SLV 10	-323	50	2153	-76.27	-18.27	0.3
6	SLV 11	-441	-68	1773	95.11	-24.1	-0.23
6	SLV 12	-441	-68	1773	95.11	-24.1	-0.23
6	SLV 13	-647	-12	2076	5.98	-36.38	0.21
6	SLV 14	-647	-12	2076	5.98	-36.38	0.21
6	SLV 15	-682	-47	1962	57.39	-38.13	0.05
6	SLV 16	-682	-47	1962	57.39	-38.13	0.05
7	SLU 1	-219	0	1783	-0.08	-12.32	0
7	SLU 2	-219	0	1783	-0.08	-12.32	0
7	SLU 3	-219	0	1783	-0.08	-12.32	0
7	SLU 4	-219	0	1783	-0.08	-12.32	0
7	SLU 5	-219	0	1783	-0.08	-12.32	0
7	SLU 6	-219	0	1783	-0.08	-12.32	0
7	SLU 7	-219	0	1783	-0.08	-12.32	0
7	SLU 8	-219	0	1783	-0.08	-12.32	0
7	SLU 9	-219	0	1783	-0.08	-12.32	0
7	SLU 10	-324	0	2185	-0.09	-18	0
7	SLU 11	-324	0	2185	-0.09	-18	0
7	SLU 12	-324	0	2185	-0.09	-18	0
7	SLU 13	-324	0	2185	-0.09	-18	0
7	SLU 14	-324	0	2185	-0.09	-18	0
7	SLU 15	-324	0	2185	-0.09	-18	0
7	SLU 16	-324	0	2185	-0.09	-18	0
7	SLU 17	-324	0	2185	-0.09	-18	0
7	SLU 18	-369	0	2357	-0.1	-20.44	0
7	SLU 19	-369	0	2357	-0.1	-20.44	0
7	SLU 20	-369	0	2357	-0.1	-20.44	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
7	SLU 21	-369	0	2357	-0.1	-20.44	0
7	SLU 22	-273	0	2013	-0.09	-15.27	0
7	SLU 23	-273	0	2013	-0.09	-15.27	0
7	SLU 24	-273	0	2013	-0.09	-15.27	0
7	SLU 25	-273	0	2013	-0.09	-15.27	0
7	SLU 26	-273	0	2013	-0.09	-15.27	0
7	SLU 27	-273	0	2013	-0.09	-15.27	0
7	SLU 28	-273	0	2013	-0.09	-15.27	0
7	SLU 29	-273	0	2013	-0.09	-15.27	0
7	SLU 30	-273	0	2013	-0.09	-15.27	0
7	SLU 31	-379	0	2415	-0.1	-20.96	0
7	SLU 32	-379	0	2415	-0.1	-20.96	0
7	SLU 33	-379	0	2415	-0.1	-20.96	0
7	SLU 34	-379	0	2415	-0.1	-20.96	0
7	SLU 35	-379	0	2415	-0.1	-20.96	0
7	SLU 36	-379	0	2415	-0.1	-20.96	0
7	SLU 37	-379	0	2415	-0.1	-20.96	0
7	SLU 38	-379	0	2415	-0.1	-20.96	0
7	SLU 39	-424	0	2587	-0.11	-23.39	0
7	SLU 40	-424	0	2587	-0.11	-23.39	0
7	SLU 41	-424	0	2587	-0.11	-23.39	0
7	SLU 42	-424	0	2587	-0.11	-23.39	0
7	SLU 43	-266	0	2239	-0.1	-15	0
7	SLU 44	-266	0	2239	-0.1	-15	0
7	SLU 45	-266	0	2239	-0.1	-15	0
7	SLU 46	-266	0	2239	-0.1	-15	0
7	SLU 47	-266	0	2239	-0.1	-15	0
7	SLU 48	-266	0	2239	-0.1	-15	0
7	SLU 49	-266	0	2239	-0.1	-15	0
7	SLU 50	-266	0	2239	-0.1	-15	0
7	SLU 51	-266	0	2239	-0.1	-15	0
7	SLU 52	-371	0	2641	-0.11	-20.68	0
7	SLU 53	-371	0	2641	-0.11	-20.68	0
7	SLU 54	-371	0	2641	-0.11	-20.68	0
7	SLU 55	-371	0	2641	-0.11	-20.68	0
7	SLU 56	-371	0	2641	-0.11	-20.68	0
7	SLU 57	-371	0	2641	-0.11	-20.68	0
7	SLU 58	-371	0	2641	-0.11	-20.68	0
7	SLU 59	-371	0	2641	-0.11	-20.68	0
7	SLU 60	-416	0	2813	-0.12	-23.12	0
7	SLU 61	-416	0	2813	-0.12	-23.12	0
7	SLU 62	-416	0	2813	-0.12	-23.12	0
7	SLU 63	-416	0	2813	-0.12	-23.12	0
7	SLU 64	-320	0	2469	-0.11	-17.95	0
7	SLU 65	-320	0	2469	-0.11	-17.95	0
7	SLU 66	-320	0	2469	-0.11	-17.95	0
7	SLU 67	-320	0	2469	-0.11	-17.95	0
7	SLU 68	-320	0	2469	-0.11	-17.95	0
7	SLU 69	-320	0	2469	-0.11	-17.95	0
7	SLU 70	-320	0	2469	-0.11	-17.95	0
7	SLU 71	-320	0	2469	-0.11	-17.95	0
7	SLU 72	-320	0	2469	-0.11	-17.95	0
7	SLU 73	-426	0	2871	-0.12	-23.64	0
7	SLU 74	-426	0	2871	-0.12	-23.64	0
7	SLU 75	-426	0	2871	-0.12	-23.64	0
7	SLU 76	-426	0	2871	-0.12	-23.64	0
7	SLU 77	-426	0	2871	-0.12	-23.64	0
7	SLU 78	-426	0	2871	-0.12	-23.64	0
7	SLU 79	-426	0	2871	-0.12	-23.64	0
7	SLU 80	-426	0	2871	-0.12	-23.64	0
7	SLU 81	-471	0	3043	-0.13	-26.07	0
7	SLU 82	-471	0	3043	-0.13	-26.07	0
7	SLU 83	-471	0	3043	-0.13	-26.07	0
7	SLU 84	-471	0	3043	-0.13	-26.07	0
7	SLE RA 1	-235	0	1849	-0.08	-13.16	0
7	SLE RA 2	-235	0	1849	-0.08	-13.16	0
7	SLE RA 3	-235	0	1849	-0.08	-13.16	0
7	SLE RA 4	-235	0	1849	-0.08	-13.16	0
7	SLE RA 5	-235	0	1849	-0.08	-13.16	0
7	SLE RA 6	-235	0	1849	-0.08	-13.16	0
7	SLE RA 7	-235	0	1849	-0.08	-13.16	0
7	SLE RA 8	-235	0	1849	-0.08	-13.16	0
7	SLE RA 9	-235	0	1849	-0.08	-13.16	0
7	SLE RA 10	-305	0	2117	-0.09	-16.95	0
7	SLE RA 11	-305	0	2117	-0.09	-16.95	0
7	SLE RA 12	-305	0	2117	-0.09	-16.95	0
7	SLE RA 13	-305	0	2117	-0.09	-16.95	0
7	SLE RA 14	-305	0	2117	-0.09	-16.95	0
7	SLE RA 15	-305	0	2117	-0.09	-16.95	0
7	SLE RA 16	-305	0	2117	-0.09	-16.95	0
7	SLE RA 17	-305	0	2117	-0.09	-16.95	0
7	SLE RA 18	-335	0	2231	-0.1	-18.57	0
7	SLE RA 19	-335	0	2231	-0.1	-18.57	0
7	SLE RA 20	-335	0	2231	-0.1	-18.57	0
7	SLE RA 21	-335	0	2231	-0.1	-18.57	0
7	SLE FR 1	-235	0	1849	-0.08	-13.16	0
7	SLE FR 2	-235	0	1849	-0.08	-13.16	0
7	SLE FR 3	-235	0	1849	-0.08	-13.16	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
7	SLE FR 4	-265	0	1963	-0.09	-14.79	0
7	SLE FR 5	-265	0	1963	-0.09	-14.79	0
7	SLE FR 6	-285	0	2040	-0.09	-15.87	0
7	SLE QP 1	-235	0	1849	-0.08	-13.16	0
7	SLE QP 2	-265	0	1963	-0.09	-14.79	0
7	SLD 1	-94	21	1944	-26.77	-5.28	-0.07
7	SLD 2	-94	21	1944	-26.77	-5.28	-0.07
7	SLD 3	-82	4	1912	-2.3	-4.64	-0.01
7	SLD 4	-82	4	1912	-2.3	-4.64	-0.01
7	SLD 5	-232	32	2007	-45.2	-12.91	-0.11
7	SLD 6	-232	32	2007	-45.2	-12.91	-0.11
7	SLD 7	-191	-24	1899	36.36	-10.77	0.08
7	SLD 8	-191	-24	1899	36.36	-10.77	0.08
7	SLD 9	-338	24	2028	-36.53	-18.81	-0.09
7	SLD 10	-338	24	2028	-36.53	-18.81	-0.09
7	SLD 11	-297	-32	1920	45.02	-16.66	0.11
7	SLD 12	-297	-32	1920	45.02	-16.66	0.11
7	SLD 13	-448	-4	2015	2.13	-24.93	0.01
7	SLD 14	-448	-4	2015	2.13	-24.93	0.01
7	SLD 15	-435	-21	1983	26.59	-24.29	0.07
7	SLD 16	-435	-21	1983	26.59	-24.29	0.07
7	SLV 1	137	53	1920	-69.4	7.55	-0.19
7	SLV 2	137	53	1920	-69.4	7.55	-0.19
7	SLV 3	167	11	1841	-4.3	9.15	-0.04
7	SLV 4	167	11	1841	-4.3	9.15	-0.04
7	SLV 5	-189	81	2070	-119.62	-10.52	-0.28
7	SLV 6	-189	81	2070	-119.62	-10.52	-0.28
7	SLV 7	-90	-61	1808	97.39	-5.17	0.22
7	SLV 8	-90	-61	1808	97.39	-5.17	0.22
7	SLV 9	-439	62	2119	-97.56	-24.4	-0.22
7	SLV 10	-439	62	2119	-97.56	-24.4	-0.22
7	SLV 11	-340	-81	1857	119.45	-19.05	0.28
7	SLV 12	-340	-81	1857	119.45	-19.05	0.28
7	SLV 13	-696	-11	2086	4.12	-38.72	0.04
7	SLV 14	-696	-11	2086	4.12	-38.72	0.04
7	SLV 15	-667	-53	2007	69.23	-37.12	0.19
7	SLV 16	-667	-53	2007	69.23	-37.12	0.19
8	SLU 1	-194	0	1822	-0.06	-10.02	0
8	SLU 2	-194	0	1822	-0.06	-10.02	0
8	SLU 3	-194	0	1822	-0.06	-10.02	0
8	SLU 4	-194	0	1822	-0.06	-10.02	0
8	SLU 5	-194	0	1822	-0.06	-10.02	0
8	SLU 6	-194	0	1822	-0.06	-10.02	0
8	SLU 7	-194	0	1822	-0.06	-10.02	0
8	SLU 8	-194	0	1822	-0.06	-10.02	0
8	SLU 9	-194	0	1822	-0.06	-10.02	0
8	SLU 10	-284	0	2253	-0.07	-14.73	0
8	SLU 11	-284	0	2253	-0.07	-14.73	0
8	SLU 12	-284	0	2253	-0.07	-14.73	0
8	SLU 13	-284	0	2253	-0.07	-14.73	0
8	SLU 14	-284	0	2253	-0.07	-14.73	0
8	SLU 15	-284	0	2253	-0.07	-14.73	0
8	SLU 16	-284	0	2253	-0.07	-14.73	0
8	SLU 17	-284	0	2253	-0.07	-14.73	0
8	SLU 18	-323	0	2438	-0.07	-16.75	0
8	SLU 19	-323	0	2438	-0.07	-16.75	0
8	SLU 20	-323	0	2438	-0.07	-16.75	0
8	SLU 21	-323	0	2438	-0.07	-16.75	0
8	SLU 22	-241	0	2068	-0.06	-12.44	0
8	SLU 23	-241	0	2068	-0.06	-12.44	0
8	SLU 24	-241	0	2068	-0.06	-12.44	0
8	SLU 25	-241	0	2068	-0.06	-12.44	0
8	SLU 26	-241	0	2068	-0.06	-12.44	0
8	SLU 27	-241	0	2068	-0.06	-12.44	0
8	SLU 28	-241	0	2068	-0.06	-12.44	0
8	SLU 29	-241	0	2068	-0.06	-12.44	0
8	SLU 30	-241	0	2068	-0.06	-12.44	0
8	SLU 31	-331	0	2499	-0.07	-17.15	0
8	SLU 32	-331	0	2499	-0.07	-17.15	0
8	SLU 33	-331	0	2499	-0.07	-17.15	0
8	SLU 34	-331	0	2499	-0.07	-17.15	0
8	SLU 35	-331	0	2499	-0.07	-17.15	0
8	SLU 36	-331	0	2499	-0.07	-17.15	0
8	SLU 37	-331	0	2499	-0.07	-17.15	0
8	SLU 38	-331	0	2499	-0.07	-17.15	0
8	SLU 39	-370	0	2684	-0.08	-19.17	0
8	SLU 40	-370	0	2684	-0.08	-19.17	0
8	SLU 41	-370	0	2684	-0.08	-19.17	0
8	SLU 42	-370	0	2684	-0.08	-19.17	0
8	SLU 43	-236	0	2284	-0.07	-12.19	0
8	SLU 44	-236	0	2284	-0.07	-12.19	0
8	SLU 45	-236	0	2284	-0.07	-12.19	0
8	SLU 46	-236	0	2284	-0.07	-12.19	0
8	SLU 47	-236	0	2284	-0.07	-12.19	0
8	SLU 48	-236	0	2284	-0.07	-12.19	0
8	SLU 49	-236	0	2284	-0.07	-12.19	0
8	SLU 50	-236	0	2284	-0.07	-12.19	0
8	SLU 51	-236	0	2284	-0.07	-12.19	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
8	SLU 52	-327	0	2715	-0.08	-16.9	0
8	SLU 53	-327	0	2715	-0.08	-16.9	0
8	SLU 54	-327	0	2715	-0.08	-16.9	0
8	SLU 55	-327	0	2715	-0.08	-16.9	0
8	SLU 56	-327	0	2715	-0.08	-16.9	0
8	SLU 57	-327	0	2715	-0.08	-16.9	0
8	SLU 58	-327	0	2715	-0.08	-16.9	0
8	SLU 59	-327	0	2715	-0.08	-16.9	0
8	SLU 60	-365	0	2900	-0.09	-18.92	0
8	SLU 61	-365	0	2900	-0.09	-18.92	0
8	SLU 62	-365	0	2900	-0.09	-18.92	0
8	SLU 63	-365	0	2900	-0.09	-18.92	0
8	SLU 64	-283	0	2530	-0.08	-14.61	0
8	SLU 65	-283	0	2530	-0.08	-14.61	0
8	SLU 66	-283	0	2530	-0.08	-14.61	0
8	SLU 67	-283	0	2530	-0.08	-14.61	0
8	SLU 68	-283	0	2530	-0.08	-14.61	0
8	SLU 69	-283	0	2530	-0.08	-14.61	0
8	SLU 70	-283	0	2530	-0.08	-14.61	0
8	SLU 71	-283	0	2530	-0.08	-14.61	0
8	SLU 72	-283	0	2530	-0.08	-14.61	0
8	SLU 73	-374	0	2961	-0.09	-19.32	0
8	SLU 74	-374	0	2961	-0.09	-19.32	0
8	SLU 75	-374	0	2961	-0.09	-19.32	0
8	SLU 76	-374	0	2961	-0.09	-19.32	0
8	SLU 77	-374	0	2961	-0.09	-19.32	0
8	SLU 78	-374	0	2961	-0.09	-19.32	0
8	SLU 79	-374	0	2961	-0.09	-19.32	0
8	SLU 80	-374	0	2961	-0.09	-19.32	0
8	SLU 81	-412	0	3146	-0.09	-21.34	0
8	SLU 82	-412	0	3146	-0.09	-21.34	0
8	SLU 83	-412	0	3146	-0.09	-21.34	0
8	SLU 84	-412	0	3146	-0.09	-21.34	0
8	SLE RA 1	-208	0	1892	-0.06	-10.71	0
8	SLE RA 2	-208	0	1892	-0.06	-10.71	0
8	SLE RA 3	-208	0	1892	-0.06	-10.71	0
8	SLE RA 4	-208	0	1892	-0.06	-10.71	0
8	SLE RA 5	-208	0	1892	-0.06	-10.71	0
8	SLE RA 6	-208	0	1892	-0.06	-10.71	0
8	SLE RA 7	-208	0	1892	-0.06	-10.71	0
8	SLE RA 8	-208	0	1892	-0.06	-10.71	0
8	SLE RA 9	-208	0	1892	-0.06	-10.71	0
8	SLE RA 10	-268	0	2180	-0.07	-13.85	0
8	SLE RA 11	-268	0	2180	-0.07	-13.85	0
8	SLE RA 12	-268	0	2180	-0.07	-13.85	0
8	SLE RA 13	-268	0	2180	-0.07	-13.85	0
8	SLE RA 14	-268	0	2180	-0.07	-13.85	0
8	SLE RA 15	-268	0	2180	-0.07	-13.85	0
8	SLE RA 16	-268	0	2180	-0.07	-13.85	0
8	SLE RA 17	-268	0	2180	-0.07	-13.85	0
8	SLE RA 18	-294	0	2303	-0.07	-15.2	0
8	SLE RA 19	-294	0	2303	-0.07	-15.2	0
8	SLE RA 20	-294	0	2303	-0.07	-15.2	0
8	SLE RA 21	-294	0	2303	-0.07	-15.2	0
8	SLE FR 1	-208	0	1892	-0.06	-10.71	0
8	SLE FR 2	-208	0	1892	-0.06	-10.71	0
8	SLE FR 3	-208	0	1892	-0.06	-10.71	0
8	SLE FR 4	-233	0	2016	-0.06	-12.05	0
8	SLE FR 5	-233	0	2016	-0.06	-12.05	0
8	SLE FR 6	-251	0	2098	-0.06	-12.95	0
8	SLE QP 1	-208	0	1892	-0.06	-10.71	0
8	SLE QP 2	-233	0	2016	-0.06	-12.05	0
8	SLD 1	-56	23	1990	-30.59	-2.41	-0.12
8	SLD 2	-56	23	1990	-30.59	-2.41	-0.12
8	SLD 3	-45	4	1967	-1.4	-1.87	-0.02
8	SLD 4	-45	4	1967	-1.4	-1.87	-0.02
8	SLD 5	-197	35	2043	-53.49	-9.99	-0.19
8	SLD 6	-197	35	2043	-53.49	-9.99	-0.19
8	SLD 7	-160	-27	1966	43.8	-8.17	0.15
8	SLD 8	-160	-27	1966	43.8	-8.17	0.15
8	SLD 9	-306	27	2065	-43.93	-15.94	-0.15
8	SLD 10	-306	27	2065	-43.93	-15.94	-0.15
8	SLD 11	-270	-35	1988	53.36	-14.12	0.19
8	SLD 12	-270	-35	1988	53.36	-14.12	0.19
8	SLD 13	-421	-4	2064	1.28	-22.24	0.02
8	SLD 14	-421	-4	2064	1.28	-22.24	0.02
8	SLD 15	-410	-23	2041	30.46	-21.7	0.12
8	SLD 16	-410	-23	2041	30.46	-21.7	0.12
8	SLV 1	182	59	1956	-79.98	10.61	-0.32
8	SLV 2	182	59	1956	-79.98	10.61	-0.32
8	SLV 3	210	11	1899	-1.34	11.95	-0.06
8	SLV 4	210	11	1899	-1.34	11.95	-0.06
8	SLV 5	-150	90	2085	-143.31	-7.29	-0.49
8	SLV 6	-150	90	2085	-143.31	-7.29	-0.49
8	SLV 7	-59	-69	1893	118.83	-2.81	0.38
8	SLV 8	-59	-69	1893	118.83	-2.81	0.38
8	SLV 9	-408	69	2138	-118.95	-21.29	-0.38
8	SLV 10	-408	69	2138	-118.95	-21.29	-0.38



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
8	SLV 11	-317	-90	1946	143.19	-16.81	0.49
8	SLV 12	-317	-90	1946	143.19	-16.81	0.49
8	SLV 13	-677	-11	2132	1.21	-36.06	0.05
8	SLV 14	-677	-11	2132	1.21	-36.06	0.05
8	SLV 15	-649	-59	2075	79.86	-34.71	0.32
8	SLV 16	-649	-59	2075	79.86	-34.71	0.32
9	SLU 1	-167	0	1856	-0.04	-8.6	0
9	SLU 2	-167	0	1856	-0.04	-8.6	0
9	SLU 3	-167	0	1856	-0.04	-8.6	0
9	SLU 4	-167	0	1856	-0.04	-8.6	0
9	SLU 5	-167	0	1856	-0.04	-8.6	0
9	SLU 6	-167	0	1856	-0.04	-8.6	0
9	SLU 7	-167	0	1856	-0.04	-8.6	0
9	SLU 8	-167	0	1856	-0.04	-8.6	0
9	SLU 9	-167	0	1856	-0.04	-8.6	0
9	SLU 10	-238	0	2307	-0.05	-12.2	0
9	SLU 11	-238	0	2307	-0.05	-12.2	0
9	SLU 12	-238	0	2307	-0.05	-12.2	0
9	SLU 13	-238	0	2307	-0.05	-12.2	0
9	SLU 14	-238	0	2307	-0.05	-12.2	0
9	SLU 15	-238	0	2307	-0.05	-12.2	0
9	SLU 16	-238	0	2307	-0.05	-12.2	0
9	SLU 17	-238	0	2307	-0.05	-12.2	0
9	SLU 18	-268	0	2500	-0.05	-13.74	0
9	SLU 19	-268	0	2500	-0.05	-13.74	0
9	SLU 20	-268	0	2500	-0.05	-13.74	0
9	SLU 21	-268	0	2500	-0.05	-13.74	0
9	SLU 22	-204	0	2114	-0.05	-10.5	0
9	SLU 23	-204	0	2114	-0.05	-10.5	0
9	SLU 24	-204	0	2114	-0.05	-10.5	0
9	SLU 25	-204	0	2114	-0.05	-10.5	0
9	SLU 26	-204	0	2114	-0.05	-10.5	0
9	SLU 27	-204	0	2114	-0.05	-10.5	0
9	SLU 28	-204	0	2114	-0.05	-10.5	0
9	SLU 29	-204	0	2114	-0.05	-10.5	0
9	SLU 30	-204	0	2114	-0.05	-10.5	0
9	SLU 31	-275	0	2564	-0.06	-14.1	0
9	SLU 32	-275	0	2564	-0.06	-14.1	0
9	SLU 33	-275	0	2564	-0.06	-14.1	0
9	SLU 34	-275	0	2564	-0.06	-14.1	0
9	SLU 35	-275	0	2564	-0.06	-14.1	0
9	SLU 36	-275	0	2564	-0.06	-14.1	0
9	SLU 37	-275	0	2564	-0.06	-14.1	0
9	SLU 38	-275	0	2564	-0.06	-14.1	0
9	SLU 39	-306	0	2758	-0.06	-15.65	0
9	SLU 40	-306	0	2758	-0.06	-15.65	0
9	SLU 41	-306	0	2758	-0.06	-15.65	0
9	SLU 42	-306	0	2758	-0.06	-15.65	0
9	SLU 43	-204	0	2324	-0.06	-10.52	0
9	SLU 44	-204	0	2324	-0.06	-10.52	0
9	SLU 45	-204	0	2324	-0.06	-10.52	0
9	SLU 46	-204	0	2324	-0.06	-10.52	0
9	SLU 47	-204	0	2324	-0.06	-10.52	0
9	SLU 48	-204	0	2324	-0.06	-10.52	0
9	SLU 49	-204	0	2324	-0.06	-10.52	0
9	SLU 50	-204	0	2324	-0.06	-10.52	0
9	SLU 51	-204	0	2324	-0.06	-10.52	0
9	SLU 52	-275	0	2775	-0.06	-14.13	0
9	SLU 53	-275	0	2775	-0.06	-14.13	0
9	SLU 54	-275	0	2775	-0.06	-14.13	0
9	SLU 55	-275	0	2775	-0.06	-14.13	0
9	SLU 56	-275	0	2775	-0.06	-14.13	0
9	SLU 57	-275	0	2775	-0.06	-14.13	0
9	SLU 58	-275	0	2775	-0.06	-14.13	0
9	SLU 59	-275	0	2775	-0.06	-14.13	0
9	SLU 60	-306	0	2969	-0.07	-15.67	0
9	SLU 61	-306	0	2969	-0.07	-15.67	0
9	SLU 62	-306	0	2969	-0.07	-15.67	0
9	SLU 63	-306	0	2969	-0.07	-15.67	0
9	SLU 64	-241	0	2582	-0.06	-12.43	0
9	SLU 65	-241	0	2582	-0.06	-12.43	0
9	SLU 66	-241	0	2582	-0.06	-12.43	0
9	SLU 67	-241	0	2582	-0.06	-12.43	0
9	SLU 68	-241	0	2582	-0.06	-12.43	0
9	SLU 69	-241	0	2582	-0.06	-12.43	0
9	SLU 70	-241	0	2582	-0.06	-12.43	0
9	SLU 71	-241	0	2582	-0.06	-12.43	0
9	SLU 72	-241	0	2582	-0.06	-12.43	0
9	SLU 73	-313	0	3033	-0.07	-16.03	0
9	SLU 74	-313	0	3033	-0.07	-16.03	0
9	SLU 75	-313	0	3033	-0.07	-16.03	0
9	SLU 76	-313	0	3033	-0.07	-16.03	0
9	SLU 77	-313	0	3033	-0.07	-16.03	0
9	SLU 78	-313	0	3033	-0.07	-16.03	0
9	SLU 79	-313	0	3033	-0.07	-16.03	0
9	SLU 80	-313	0	3033	-0.07	-16.03	0
9	SLU 81	-343	0	3226	-0.07	-17.57	0
9	SLU 82	-343	0	3226	-0.07	-17.57	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
9	SLU 83	-343	0	3226	-0.07	-17.57	0
9	SLU 84	-343	0	3226	-0.07	-17.57	0
9	SLE RA 1	-177	0	1930	-0.05	-9.14	0
9	SLE RA 2	-177	0	1930	-0.05	-9.14	0
9	SLE RA 3	-177	0	1930	-0.05	-9.14	0
9	SLE RA 4	-177	0	1930	-0.05	-9.14	0
9	SLE RA 5	-177	0	1930	-0.05	-9.14	0
9	SLE RA 6	-177	0	1930	-0.05	-9.14	0
9	SLE RA 7	-177	0	1930	-0.05	-9.14	0
9	SLE RA 8	-177	0	1930	-0.05	-9.14	0
9	SLE RA 9	-177	0	1930	-0.05	-9.14	0
9	SLE RA 10	-225	0	2230	-0.05	-11.54	0
9	SLE RA 11	-225	0	2230	-0.05	-11.54	0
9	SLE RA 12	-225	0	2230	-0.05	-11.54	0
9	SLE RA 13	-225	0	2230	-0.05	-11.54	0
9	SLE RA 14	-225	0	2230	-0.05	-11.54	0
9	SLE RA 15	-225	0	2230	-0.05	-11.54	0
9	SLE RA 16	-225	0	2230	-0.05	-11.54	0
9	SLE RA 17	-225	0	2230	-0.05	-11.54	0
9	SLE RA 18	-245	0	2359	-0.05	-12.57	0
9	SLE RA 19	-245	0	2359	-0.05	-12.57	0
9	SLE RA 20	-245	0	2359	-0.05	-12.57	0
9	SLE RA 21	-245	0	2359	-0.05	-12.57	0
9	SLE FR 1	-177	0	1930	-0.05	-9.14	0
9	SLE FR 2	-177	0	1930	-0.05	-9.14	0
9	SLE FR 3	-177	0	1930	-0.05	-9.14	0
9	SLE FR 4	-198	0	2058	-0.05	-10.17	0
9	SLE FR 5	-198	0	2058	-0.05	-10.17	0
9	SLE FR 6	-211	0	2144	-0.05	-10.86	0
9	SLE QP 1	-177	0	1930	-0.05	-9.14	0
9	SLE QP 2	-198	0	2058	-0.05	-10.17	0
9	SLD 1	-16	24	2039	-33.92	-0.64	-0.14
9	SLD 2	-16	24	2039	-33.92	-0.64	-0.14
9	SLD 3	-4	5	2021	0.03	0.01	-0.02
9	SLD 4	-4	5	2021	0.03	0.01	-0.02
9	SLD 5	-161	38	2081	-61.7	-8.28	-0.22
9	SLD 6	-161	38	2081	-61.7	-8.28	-0.22
9	SLD 7	-122	-29	2019	51.47	-6.14	0.17
9	SLD 8	-122	-29	2019	51.47	-6.14	0.17
9	SLD 9	-274	29	2098	-51.56	-14.2	-0.17
9	SLD 10	-274	29	2098	-51.56	-14.2	-0.17
9	SLD 11	-234	-38	2036	61.61	-12.05	0.22
9	SLD 12	-234	-38	2036	61.61	-12.05	0.22
9	SLD 13	-391	-5	2096	-0.13	-20.34	0.02
9	SLD 14	-391	-5	2096	-0.13	-20.34	0.02
9	SLD 15	-379	-24	2077	33.83	-19.7	0.14
9	SLD 16	-379	-24	2077	33.83	-19.7	0.14
9	SLV 1	228	63	2016	-89.51	12.15	-0.37
9	SLV 2	228	63	2016	-89.51	12.15	-0.37
9	SLV 3	259	11	1968	3.15	13.87	-0.06
9	SLV 4	259	11	1968	3.15	13.87	-0.06
9	SLV 5	-117	98	2118	-167.43	-6.07	-0.58
9	SLV 6	-117	98	2118	-167.43	-6.07	-0.58
9	SLV 7	-13	-75	1959	141.45	-0.36	0.45
9	SLV 8	-13	-75	1959	141.45	-0.36	0.45
9	SLV 9	-382	75	2158	-141.55	-19.98	-0.45
9	SLV 10	-382	75	2158	-141.55	-19.98	-0.45
9	SLV 11	-278	-98	1999	167.33	-14.27	0.58
9	SLV 12	-278	-98	1999	167.33	-14.27	0.58
9	SLV 13	-655	-11	2149	-3.25	-34.2	0.06
9	SLV 14	-655	-11	2149	-3.25	-34.2	0.06
9	SLV 15	-624	-63	2101	89.41	-32.49	0.37
9	SLV 16	-624	-63	2101	89.41	-32.49	0.37
10	SLU 1	-140	0	1881	-0.03	-7.08	0
10	SLU 2	-140	0	1881	-0.03	-7.08	0
10	SLU 3	-140	0	1881	-0.03	-7.08	0
10	SLU 4	-140	0	1881	-0.03	-7.08	0
10	SLU 5	-140	0	1881	-0.03	-7.08	0
10	SLU 6	-140	0	1881	-0.03	-7.08	0
10	SLU 7	-140	0	1881	-0.03	-7.08	0
10	SLU 8	-140	0	1881	-0.03	-7.08	0
10	SLU 9	-140	0	1881	-0.03	-7.08	0
10	SLU 10	-196	0	2343	-0.04	-10.05	0
10	SLU 11	-196	0	2343	-0.04	-10.05	0
10	SLU 12	-196	0	2343	-0.04	-10.05	0
10	SLU 13	-196	0	2343	-0.04	-10.05	0
10	SLU 14	-196	0	2343	-0.04	-10.05	0
10	SLU 15	-196	0	2343	-0.04	-10.05	0
10	SLU 16	-196	0	2343	-0.04	-10.05	0
10	SLU 17	-196	0	2343	-0.04	-10.05	0
10	SLU 18	-221	0	2541	-0.04	-11.32	0
10	SLU 19	-221	0	2541	-0.04	-11.32	0
10	SLU 20	-221	0	2541	-0.04	-11.32	0
10	SLU 21	-221	0	2541	-0.04	-11.32	0
10	SLU 22	-169	0	2146	-0.04	-8.6	0
10	SLU 23	-169	0	2146	-0.04	-8.6	0
10	SLU 24	-169	0	2146	-0.04	-8.6	0
10	SLU 25	-169	0	2146	-0.04	-8.6	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
10	SLU 26	-169	0	2146	-0.04	-8.6	0
10	SLU 27	-169	0	2146	-0.04	-8.6	0
10	SLU 28	-169	0	2146	-0.04	-8.6	0
10	SLU 29	-169	0	2146	-0.04	-8.6	0
10	SLU 30	-169	0	2146	-0.04	-8.6	0
10	SLU 31	-226	0	2608	-0.04	-11.57	0
10	SLU 32	-226	0	2608	-0.04	-11.57	0
10	SLU 33	-226	0	2608	-0.04	-11.57	0
10	SLU 34	-226	0	2608	-0.04	-11.57	0
10	SLU 35	-226	0	2608	-0.04	-11.57	0
10	SLU 36	-226	0	2608	-0.04	-11.57	0
10	SLU 37	-226	0	2608	-0.04	-11.57	0
10	SLU 38	-226	0	2608	-0.04	-11.57	0
10	SLU 39	-250	0	2805	-0.04	-12.84	0
10	SLU 40	-250	0	2805	-0.04	-12.84	0
10	SLU 41	-250	0	2805	-0.04	-12.84	0
10	SLU 42	-250	0	2805	-0.04	-12.84	0
10	SLU 43	-171	0	2355	-0.04	-8.69	0
10	SLU 44	-171	0	2355	-0.04	-8.69	0
10	SLU 45	-171	0	2355	-0.04	-8.69	0
10	SLU 46	-171	0	2355	-0.04	-8.69	0
10	SLU 47	-171	0	2355	-0.04	-8.69	0
10	SLU 48	-171	0	2355	-0.04	-8.69	0
10	SLU 49	-171	0	2355	-0.04	-8.69	0
10	SLU 50	-171	0	2355	-0.04	-8.69	0
10	SLU 51	-171	0	2355	-0.04	-8.69	0
10	SLU 52	-228	0	2816	-0.05	-11.66	0
10	SLU 53	-228	0	2816	-0.05	-11.66	0
10	SLU 54	-228	0	2816	-0.05	-11.66	0
10	SLU 55	-228	0	2816	-0.05	-11.66	0
10	SLU 56	-228	0	2816	-0.05	-11.66	0
10	SLU 57	-228	0	2816	-0.05	-11.66	0
10	SLU 58	-228	0	2816	-0.05	-11.66	0
10	SLU 59	-228	0	2816	-0.05	-11.66	0
10	SLU 60	-252	0	3014	-0.05	-12.93	0
10	SLU 61	-252	0	3014	-0.05	-12.93	0
10	SLU 62	-252	0	3014	-0.05	-12.93	0
10	SLU 63	-252	0	3014	-0.05	-12.93	0
10	SLU 64	-201	0	2620	-0.04	-10.2	0
10	SLU 65	-201	0	2620	-0.04	-10.2	0
10	SLU 66	-201	0	2620	-0.04	-10.2	0
10	SLU 67	-201	0	2620	-0.04	-10.2	0
10	SLU 68	-201	0	2620	-0.04	-10.2	0
10	SLU 69	-201	0	2620	-0.04	-10.2	0
10	SLU 70	-201	0	2620	-0.04	-10.2	0
10	SLU 71	-201	0	2620	-0.04	-10.2	0
10	SLU 72	-201	0	2620	-0.04	-10.2	0
10	SLU 73	-258	0	3081	-0.05	-13.17	0
10	SLU 74	-258	0	3081	-0.05	-13.17	0
10	SLU 75	-258	0	3081	-0.05	-13.17	0
10	SLU 76	-258	0	3081	-0.05	-13.17	0
10	SLU 77	-258	0	3081	-0.05	-13.17	0
10	SLU 78	-258	0	3081	-0.05	-13.17	0
10	SLU 79	-258	0	3081	-0.05	-13.17	0
10	SLU 80	-258	0	3081	-0.05	-13.17	0
10	SLU 81	-282	0	3279	-0.05	-14.45	0
10	SLU 82	-282	0	3279	-0.05	-14.45	0
10	SLU 83	-282	0	3279	-0.05	-14.45	0
10	SLU 84	-282	0	3279	-0.05	-14.45	0
10	SLE RA 1	-148	0	1957	-0.03	-7.51	0
10	SLE RA 2	-148	0	1957	-0.03	-7.51	0
10	SLE RA 3	-148	0	1957	-0.03	-7.51	0
10	SLE RA 4	-148	0	1957	-0.03	-7.51	0
10	SLE RA 5	-148	0	1957	-0.03	-7.51	0
10	SLE RA 6	-148	0	1957	-0.03	-7.51	0
10	SLE RA 7	-148	0	1957	-0.03	-7.51	0
10	SLE RA 8	-148	0	1957	-0.03	-7.51	0
10	SLE RA 9	-148	0	1957	-0.03	-7.51	0
10	SLE RA 10	-186	0	2265	-0.04	-9.5	0
10	SLE RA 11	-186	0	2265	-0.04	-9.5	0
10	SLE RA 12	-186	0	2265	-0.04	-9.5	0
10	SLE RA 13	-186	0	2265	-0.04	-9.5	0
10	SLE RA 14	-186	0	2265	-0.04	-9.5	0
10	SLE RA 15	-186	0	2265	-0.04	-9.5	0
10	SLE RA 16	-186	0	2265	-0.04	-9.5	0
10	SLE RA 17	-186	0	2265	-0.04	-9.5	0
10	SLE RA 18	-202	0	2396	-0.04	-10.34	0
10	SLE RA 19	-202	0	2396	-0.04	-10.34	0
10	SLE RA 20	-202	0	2396	-0.04	-10.34	0
10	SLE RA 21	-202	0	2396	-0.04	-10.34	0
10	SLE FR 1	-148	0	1957	-0.03	-7.51	0
10	SLE FR 2	-148	0	1957	-0.03	-7.51	0
10	SLE FR 3	-148	0	1957	-0.03	-7.51	0
10	SLE FR 4	-164	0	2089	-0.04	-8.36	0
10	SLE FR 5	-164	0	2089	-0.04	-8.36	0
10	SLE FR 6	-175	0	2177	-0.04	-8.93	0
10	SLE QP 1	-148	0	1957	-0.03	-7.51	0
10	SLE QP 2	-164	0	2089	-0.04	-8.36	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
10	SLD 1	24	26	2076	-36.86	1.34	0.02
10	SLD 2	24	26	2076	-36.86	1.34	0.02
10	SLD 3	37	4	2058	2.21	1.92	0.14
10	SLD 4	37	4	2058	2.21	1.92	0.14
10	SLD 5	-127	40	2113	-70.35	-6.34	-0.18
10	SLD 6	-127	40	2113	-70.35	-6.34	-0.18
10	SLD 7	-85	-31	2051	59.91	-4.39	0.23
10	SLD 8	-85	-31	2051	59.91	-4.39	0.23
10	SLD 9	-244	31	2126	-59.98	-12.33	-0.23
10	SLD 10	-244	31	2126	-59.98	-12.33	-0.23
10	SLD 11	-201	-40	2065	70.28	-10.39	0.18
10	SLD 12	-201	-40	2065	70.28	-10.39	0.18
10	SLD 13	-365	-4	2120	-2.28	-18.65	-0.14
10	SLD 14	-365	-4	2120	-2.28	-18.65	-0.14
10	SLD 15	-352	-26	2102	36.79	-18.06	-0.02
10	SLD 16	-352	-26	2102	36.79	-18.06	-0.02
10	SLV 1	276	67	2062	-98.2	14.35	0.05
10	SLV 2	276	67	2062	-98.2	14.35	0.05
10	SLV 3	310	10	2012	9.75	15.9	0.37
10	SLV 4	310	10	2012	9.75	15.9	0.37
10	SLV 5	-84	106	2156	-193.2	-3.89	-0.49
10	SLV 6	-84	106	2156	-193.2	-3.89	-0.49
10	SLV 7	30	-83	1990	166.61	1.26	0.61
10	SLV 8	30	-83	1990	166.61	1.26	0.61
10	SLV 9	-358	83	2188	-166.68	-17.98	-0.61
10	SLV 10	-358	83	2188	-166.68	-17.98	-0.61
10	SLV 11	-244	-106	2022	193.13	-12.84	0.49
10	SLV 12	-244	-106	2022	193.13	-12.84	0.49
10	SLV 13	-639	-10	2166	-9.82	-32.63	-0.37
10	SLV 14	-639	-10	2166	-9.82	-32.63	-0.37
10	SLV 15	-604	-67	2116	98.13	-31.08	-0.05
10	SLV 16	-604	-67	2116	98.13	-31.08	-0.05
11	SLU 1	-120	0	1898	-0.02	-5.9	0
11	SLU 2	-120	0	1898	-0.02	-5.9	0
11	SLU 3	-120	0	1898	-0.02	-5.9	0
11	SLU 4	-120	0	1898	-0.02	-5.9	0
11	SLU 5	-120	0	1898	-0.02	-5.9	0
11	SLU 6	-120	0	1898	-0.02	-5.9	0
11	SLU 7	-120	0	1898	-0.02	-5.9	0
11	SLU 8	-120	0	1898	-0.02	-5.9	0
11	SLU 9	-120	0	1898	-0.02	-5.9	0
11	SLU 10	-164	0	2363	-0.03	-8.05	0
11	SLU 11	-164	0	2363	-0.03	-8.05	0
11	SLU 12	-164	0	2363	-0.03	-8.05	0
11	SLU 13	-164	0	2363	-0.03	-8.05	0
11	SLU 14	-164	0	2363	-0.03	-8.05	0
11	SLU 15	-164	0	2363	-0.03	-8.05	0
11	SLU 16	-164	0	2363	-0.03	-8.05	0
11	SLU 17	-164	0	2363	-0.03	-8.05	0
11	SLU 18	-183	0	2563	-0.03	-8.97	0
11	SLU 19	-183	0	2563	-0.03	-8.97	0
11	SLU 20	-183	0	2563	-0.03	-8.97	0
11	SLU 21	-183	0	2563	-0.03	-8.97	0
11	SLU 22	-143	0	2166	-0.02	-7	0
11	SLU 23	-143	0	2166	-0.02	-7	0
11	SLU 24	-143	0	2166	-0.02	-7	0
11	SLU 25	-143	0	2166	-0.02	-7	0
11	SLU 26	-143	0	2166	-0.02	-7	0
11	SLU 27	-143	0	2166	-0.02	-7	0
11	SLU 28	-143	0	2166	-0.02	-7	0
11	SLU 29	-143	0	2166	-0.02	-7	0
11	SLU 30	-143	0	2166	-0.02	-7	0
11	SLU 31	-187	0	2631	-0.03	-9.15	0
11	SLU 32	-187	0	2631	-0.03	-9.15	0
11	SLU 33	-187	0	2631	-0.03	-9.15	0
11	SLU 34	-187	0	2631	-0.03	-9.15	0
11	SLU 35	-187	0	2631	-0.03	-9.15	0
11	SLU 36	-187	0	2631	-0.03	-9.15	0
11	SLU 37	-187	0	2631	-0.03	-9.15	0
11	SLU 38	-187	0	2631	-0.03	-9.15	0
11	SLU 39	-206	0	2831	-0.03	-10.07	0
11	SLU 40	-206	0	2831	-0.03	-10.07	0
11	SLU 41	-206	0	2831	-0.03	-10.07	0
11	SLU 42	-206	0	2831	-0.03	-10.07	0
11	SLU 43	-148	0	2376	-0.03	-7.29	0
11	SLU 44	-148	0	2376	-0.03	-7.29	0
11	SLU 45	-148	0	2376	-0.03	-7.29	0
11	SLU 46	-148	0	2376	-0.03	-7.29	0
11	SLU 47	-148	0	2376	-0.03	-7.29	0
11	SLU 48	-148	0	2376	-0.03	-7.29	0
11	SLU 49	-148	0	2376	-0.03	-7.29	0
11	SLU 50	-148	0	2376	-0.03	-7.29	0
11	SLU 51	-148	0	2376	-0.03	-7.29	0
11	SLU 52	-193	0	2841	-0.03	-9.44	0
11	SLU 53	-193	0	2841	-0.03	-9.44	0
11	SLU 54	-193	0	2841	-0.03	-9.44	0
11	SLU 55	-193	0	2841	-0.03	-9.44	0
11	SLU 56	-193	0	2841	-0.03	-9.44	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
11	SLU 57	-193	0	2841	-0.03	-9.44	0
11	SLU 58	-193	0	2841	-0.03	-9.44	0
11	SLU 59	-193	0	2841	-0.03	-9.44	0
11	SLU 60	-212	0	3040	-0.03	-10.36	0
11	SLU 61	-212	0	3040	-0.03	-10.36	0
11	SLU 62	-212	0	3040	-0.03	-10.36	0
11	SLU 63	-212	0	3040	-0.03	-10.36	0
11	SLU 64	-171	0	2644	-0.03	-8.39	0
11	SLU 65	-171	0	2644	-0.03	-8.39	0
11	SLU 66	-171	0	2644	-0.03	-8.39	0
11	SLU 67	-171	0	2644	-0.03	-8.39	0
11	SLU 68	-171	0	2644	-0.03	-8.39	0
11	SLU 69	-171	0	2644	-0.03	-8.39	0
11	SLU 70	-171	0	2644	-0.03	-8.39	0
11	SLU 71	-171	0	2644	-0.03	-8.39	0
11	SLU 72	-171	0	2644	-0.03	-8.39	0
11	SLU 73	-215	0	3109	-0.03	-10.54	0
11	SLU 74	-215	0	3109	-0.03	-10.54	0
11	SLU 75	-215	0	3109	-0.03	-10.54	0
11	SLU 76	-215	0	3109	-0.03	-10.54	0
11	SLU 77	-215	0	3109	-0.03	-10.54	0
11	SLU 78	-215	0	3109	-0.03	-10.54	0
11	SLU 79	-215	0	3109	-0.03	-10.54	0
11	SLU 80	-215	0	3109	-0.03	-10.54	0
11	SLU 81	-234	0	3308	-0.03	-11.46	0
11	SLU 82	-234	0	3308	-0.03	-11.46	0
11	SLU 83	-234	0	3308	-0.03	-11.46	0
11	SLU 84	-234	0	3308	-0.03	-11.46	0
11	SLE RA 1	-126	0	1975	-0.02	-6.21	0
11	SLE RA 2	-126	0	1975	-0.02	-6.21	0
11	SLE RA 3	-126	0	1975	-0.02	-6.21	0
11	SLE RA 4	-126	0	1975	-0.02	-6.21	0
11	SLE RA 5	-126	0	1975	-0.02	-6.21	0
11	SLE RA 6	-126	0	1975	-0.02	-6.21	0
11	SLE RA 7	-126	0	1975	-0.02	-6.21	0
11	SLE RA 8	-126	0	1975	-0.02	-6.21	0
11	SLE RA 9	-126	0	1975	-0.02	-6.21	0
11	SLE RA 10	-156	0	2285	-0.02	-7.64	0
11	SLE RA 11	-156	0	2285	-0.02	-7.64	0
11	SLE RA 12	-156	0	2285	-0.02	-7.64	0
11	SLE RA 13	-156	0	2285	-0.02	-7.64	0
11	SLE RA 14	-156	0	2285	-0.02	-7.64	0
11	SLE RA 15	-156	0	2285	-0.02	-7.64	0
11	SLE RA 16	-156	0	2285	-0.02	-7.64	0
11	SLE RA 17	-156	0	2285	-0.02	-7.64	0
11	SLE RA 18	-169	0	2418	-0.03	-8.26	0
11	SLE RA 19	-169	0	2418	-0.03	-8.26	0
11	SLE RA 20	-169	0	2418	-0.03	-8.26	0
11	SLE RA 21	-169	0	2418	-0.03	-8.26	0
11	SLE FR 1	-126	0	1975	-0.02	-6.21	0
11	SLE FR 2	-126	0	1975	-0.02	-6.21	0
11	SLE FR 3	-126	0	1975	-0.02	-6.21	0
11	SLE FR 4	-139	0	2108	-0.02	-6.83	0
11	SLE FR 5	-139	0	2108	-0.02	-6.83	0
11	SLE FR 6	-148	0	2196	-0.02	-7.24	0
11	SLE QP 1	-126	0	1975	-0.02	-6.21	0
11	SLE QP 2	-139	0	2108	-0.02	-6.83	0
11	SLD 1	52	-3	2070	-39.56	2.79	0.01
11	SLD 2	52	-3	2070	-39.56	2.79	0.01
11	SLD 3	68	-27	2047	5.37	3.59	0.14
11	SLD 4	68	-27	2047	5.37	3.59	0.14
11	SLD 5	-105	35	2131	-80.03	-5.15	-0.19
11	SLD 6	-105	35	2131	-80.03	-5.15	-0.19
11	SLD 7	-54	-44	2055	69.74	-2.49	0.23
11	SLD 8	-54	-44	2055	69.74	-2.49	0.23
11	SLD 9	-225	44	2160	-69.79	-11.16	-0.23
11	SLD 10	-225	44	2160	-69.79	-11.16	-0.23
11	SLD 11	-173	-35	2085	79.99	-8.5	0.19
11	SLD 12	-173	-35	2085	79.99	-8.5	0.19
11	SLD 13	-346	27	2168	-5.42	-17.24	-0.14
11	SLD 14	-346	27	2168	-5.42	-17.24	-0.14
11	SLD 15	-330	3	2146	39.52	-16.44	-0.01
11	SLD 16	-330	3	2146	39.52	-16.44	-0.01
11	SLV 1	308	-7	2024	-106.34	15.62	0.02
11	SLV 2	308	-7	2024	-106.34	15.62	0.02
11	SLV 3	350	-72	1961	19.01	17.82	0.36
11	SLV 4	350	-72	1961	19.01	17.82	0.36
11	SLV 5	-69	97	2177	-222.04	-3.42	-0.51
11	SLV 6	-69	97	2177	-222.04	-3.42	-0.51
11	SLV 7	72	-120	1969	195.8	3.9	0.63
11	SLV 8	72	-120	1969	195.8	3.9	0.63
11	SLV 9	-350	120	2246	-195.85	-17.55	-0.63
11	SLV 10	-350	120	2246	-195.85	-17.55	-0.63
11	SLV 11	-209	-97	2038	221.99	-10.23	0.51
11	SLV 12	-209	-97	2038	221.99	-10.23	0.51
11	SLV 13	-628	72	2254	-19.06	-31.47	-0.36
11	SLV 14	-628	72	2254	-19.06	-31.47	-0.36
11	SLV 15	-586	7	2192	106.29	-29.27	-0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
11	SLV 16	-586	7	2192	106.29	-29.27	-0.02
12	SLU 1	-116	0	1919	-0.01	-5.73	0
12	SLU 2	-116	0	1919	-0.01	-5.73	0
12	SLU 3	-116	0	1919	-0.01	-5.73	0
12	SLU 4	-116	0	1919	-0.01	-5.73	0
12	SLU 5	-116	0	1919	-0.01	-5.73	0
12	SLU 6	-116	0	1919	-0.01	-5.73	0
12	SLU 7	-116	0	1919	-0.01	-5.73	0
12	SLU 8	-116	0	1919	-0.01	-5.73	0
12	SLU 9	-116	0	1919	-0.01	-5.73	0
12	SLU 10	-158	0	2388	-0.01	-7.9	0
12	SLU 11	-158	0	2388	-0.01	-7.9	0
12	SLU 12	-158	0	2388	-0.01	-7.9	0
12	SLU 13	-158	0	2388	-0.01	-7.9	0
12	SLU 14	-158	0	2388	-0.01	-7.9	0
12	SLU 15	-158	0	2388	-0.01	-7.9	0
12	SLU 16	-158	0	2388	-0.01	-7.9	0
12	SLU 17	-158	0	2388	-0.01	-7.9	0
12	SLU 18	-176	0	2589	-0.01	-8.84	0
12	SLU 19	-176	0	2589	-0.01	-8.84	0
12	SLU 20	-176	0	2589	-0.01	-8.84	0
12	SLU 21	-176	0	2589	-0.01	-8.84	0
12	SLU 22	-136	0	2189	-0.01	-6.77	0
12	SLU 23	-136	0	2189	-0.01	-6.77	0
12	SLU 24	-136	0	2189	-0.01	-6.77	0
12	SLU 25	-136	0	2189	-0.01	-6.77	0
12	SLU 26	-136	0	2189	-0.01	-6.77	0
12	SLU 27	-136	0	2189	-0.01	-6.77	0
12	SLU 28	-136	0	2189	-0.01	-6.77	0
12	SLU 29	-136	0	2189	-0.01	-6.77	0
12	SLU 30	-136	0	2189	-0.01	-6.77	0
12	SLU 31	-178	0	2658	-0.01	-8.95	0
12	SLU 32	-178	0	2658	-0.01	-8.95	0
12	SLU 33	-178	0	2658	-0.01	-8.95	0
12	SLU 34	-178	0	2658	-0.01	-8.95	0
12	SLU 35	-178	0	2658	-0.01	-8.95	0
12	SLU 36	-178	0	2658	-0.01	-8.95	0
12	SLU 37	-178	0	2658	-0.01	-8.95	0
12	SLU 38	-178	0	2658	-0.01	-8.95	0
12	SLU 39	-196	0	2859	-0.01	-9.88	0
12	SLU 40	-196	0	2859	-0.01	-9.88	0
12	SLU 41	-196	0	2859	-0.01	-9.88	0
12	SLU 42	-196	0	2859	-0.01	-9.88	0
12	SLU 43	-143	0	2403	-0.01	-7.09	0
12	SLU 44	-143	0	2403	-0.01	-7.09	0
12	SLU 45	-143	0	2403	-0.01	-7.09	0
12	SLU 46	-143	0	2403	-0.01	-7.09	0
12	SLU 47	-143	0	2403	-0.01	-7.09	0
12	SLU 48	-143	0	2403	-0.01	-7.09	0
12	SLU 49	-143	0	2403	-0.01	-7.09	0
12	SLU 50	-143	0	2403	-0.01	-7.09	0
12	SLU 51	-143	0	2403	-0.01	-7.09	0
12	SLU 52	-185	0	2871	-0.01	-9.26	0
12	SLU 53	-185	0	2871	-0.01	-9.26	0
12	SLU 54	-185	0	2871	-0.01	-9.26	0
12	SLU 55	-185	0	2871	-0.01	-9.26	0
12	SLU 56	-185	0	2871	-0.01	-9.26	0
12	SLU 57	-185	0	2871	-0.01	-9.26	0
12	SLU 58	-185	0	2871	-0.01	-9.26	0
12	SLU 59	-185	0	2871	-0.01	-9.26	0
12	SLU 60	-204	0	3072	-0.01	-10.2	0
12	SLU 61	-204	0	3072	-0.01	-10.2	0
12	SLU 62	-204	0	3072	-0.01	-10.2	0
12	SLU 63	-204	0	3072	-0.01	-10.2	0
12	SLU 64	-164	0	2673	-0.01	-8.13	0
12	SLU 65	-164	0	2673	-0.01	-8.13	0
12	SLU 66	-164	0	2673	-0.01	-8.13	0
12	SLU 67	-164	0	2673	-0.01	-8.13	0
12	SLU 68	-164	0	2673	-0.01	-8.13	0
12	SLU 69	-164	0	2673	-0.01	-8.13	0
12	SLU 70	-164	0	2673	-0.01	-8.13	0
12	SLU 71	-164	0	2673	-0.01	-8.13	0
12	SLU 72	-164	0	2673	-0.01	-8.13	0
12	SLU 73	-206	0	3141	-0.01	-10.31	0
12	SLU 74	-206	0	3141	-0.01	-10.31	0
12	SLU 75	-206	0	3141	-0.01	-10.31	0
12	SLU 76	-206	0	3141	-0.01	-10.31	0
12	SLU 77	-206	0	3141	-0.01	-10.31	0
12	SLU 78	-206	0	3141	-0.01	-10.31	0
12	SLU 79	-206	0	3141	-0.01	-10.31	0
12	SLU 80	-206	0	3141	-0.01	-10.31	0
12	SLU 81	-224	0	3342	-0.02	-11.24	0
12	SLU 82	-224	0	3342	-0.02	-11.24	0
12	SLU 83	-224	0	3342	-0.02	-11.24	0
12	SLU 84	-224	0	3342	-0.02	-11.24	0
12	SLE RA 1	-121	0	1997	-0.01	-6.02	0
12	SLE RA 2	-121	0	1997	-0.01	-6.02	0
12	SLE RA 3	-121	0	1997	-0.01	-6.02	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
12	SLE RA 4	-121	0	1997	-0.01	-6.02	0
12	SLE RA 5	-121	0	1997	-0.01	-6.02	0
12	SLE RA 6	-121	0	1997	-0.01	-6.02	0
12	SLE RA 7	-121	0	1997	-0.01	-6.02	0
12	SLE RA 8	-121	0	1997	-0.01	-6.02	0
12	SLE RA 9	-121	0	1997	-0.01	-6.02	0
12	SLE RA 10	-150	0	2309	-0.01	-7.48	0
12	SLE RA 11	-150	0	2309	-0.01	-7.48	0
12	SLE RA 12	-150	0	2309	-0.01	-7.48	0
12	SLE RA 13	-150	0	2309	-0.01	-7.48	0
12	SLE RA 14	-150	0	2309	-0.01	-7.48	0
12	SLE RA 15	-150	0	2309	-0.01	-7.48	0
12	SLE RA 16	-150	0	2309	-0.01	-7.48	0
12	SLE RA 17	-150	0	2309	-0.01	-7.48	0
12	SLE RA 18	-162	0	2443	-0.01	-8.1	0
12	SLE RA 19	-162	0	2443	-0.01	-8.1	0
12	SLE RA 20	-162	0	2443	-0.01	-8.1	0
12	SLE RA 21	-162	0	2443	-0.01	-8.1	0
12	SLE FR 1	-121	0	1997	-0.01	-6.02	0
12	SLE FR 2	-121	0	1997	-0.01	-6.02	0
12	SLE FR 3	-121	0	1997	-0.01	-6.02	0
12	SLE FR 4	-133	0	2130	-0.01	-6.65	0
12	SLE FR 5	-133	0	2130	-0.01	-6.65	0
12	SLE FR 6	-142	0	2220	-0.01	-7.06	0
12	SLE QP 1	-121	0	1997	-0.01	-6.02	0
12	SLE QP 2	-133	0	2130	-0.01	-6.65	0
12	SLD 1	56	-1	2060	-9.74	2.85	0
12	SLD 2	56	-1	2060	-9.74	2.85	0
12	SLD 3	72	-29	2031	42.12	3.54	0.13
12	SLD 4	72	-29	2031	42.12	3.54	0.13
12	SLD 5	-101	43	2154	-81.57	-4.85	-0.2
12	SLD 6	-101	43	2154	-81.57	-4.85	-0.2
12	SLD 7	-47	-52	2056	91.27	-2.54	0.23
12	SLD 8	-47	-52	2056	91.27	-2.54	0.23
12	SLD 9	-220	52	2205	-91.3	-10.75	-0.23
12	SLD 10	-220	52	2205	-91.3	-10.75	-0.23
12	SLD 11	-166	-43	2106	81.55	-8.44	0.2
12	SLD 12	-166	-43	2106	81.55	-8.44	0.2
12	SLD 13	-339	29	2230	-42.14	-16.84	-0.13
12	SLD 14	-339	29	2230	-42.14	-16.84	-0.13
12	SLD 15	-323	1	2200	9.72	-16.14	0
12	SLD 16	-323	1	2200	9.72	-16.14	0
12	SLV 1	310	1	1974	-31.5	15.56	-0.02
12	SLV 2	310	1	1974	-31.5	15.56	-0.02
12	SLV 3	354	-78	1891	114.16	17.44	0.34
12	SLV 4	354	-78	1891	114.16	17.44	0.34
12	SLV 5	-68	121	2209	-230.38	-2.84	-0.55
12	SLV 6	-68	121	2209	-230.38	-2.84	-0.55
12	SLV 7	80	-144	1933	255.16	3.44	0.65
12	SLV 8	80	-144	1933	255.16	3.44	0.65
12	SLV 9	-347	144	2328	-255.19	-16.73	-0.65
12	SLV 10	-347	144	2328	-255.19	-16.73	-0.65
12	SLV 11	-199	-121	2052	230.36	-10.45	0.55
12	SLV 12	-199	-121	2052	230.36	-10.45	0.55
12	SLV 13	-621	78	2370	-114.19	-30.74	-0.34
12	SLV 14	-621	78	2370	-114.19	-30.74	-0.34
12	SLV 15	-577	-1	2287	31.48	-28.85	0.02
12	SLV 16	-577	-1	2287	31.48	-28.85	0.02
13	SLU 1	-110	0	1954	0	-5.13	0
13	SLU 2	-110	0	1954	0	-5.13	0
13	SLU 3	-110	0	1954	0	-5.13	0
13	SLU 4	-110	0	1954	0	-5.13	0
13	SLU 5	-110	0	1954	0	-5.13	0
13	SLU 6	-110	0	1954	0	-5.13	0
13	SLU 7	-110	0	1954	0	-5.13	0
13	SLU 8	-110	0	1954	0	-5.13	0
13	SLU 9	-110	0	1954	0	-5.13	0
13	SLU 10	-149	0	2431	0	-6.88	0
13	SLU 11	-149	0	2431	0	-6.88	0
13	SLU 12	-149	0	2431	0	-6.88	0
13	SLU 13	-149	0	2431	0	-6.88	0
13	SLU 14	-149	0	2431	0	-6.88	0
13	SLU 15	-149	0	2431	0	-6.88	0
13	SLU 16	-149	0	2431	0	-6.88	0
13	SLU 17	-149	0	2431	0	-6.88	0
13	SLU 18	-165	0	2636	0	-7.63	0
13	SLU 19	-165	0	2636	0	-7.63	0
13	SLU 20	-165	0	2636	0	-7.63	0
13	SLU 21	-165	0	2636	0	-7.63	0
13	SLU 22	-128	0	2228	0	-5.97	0
13	SLU 23	-128	0	2228	0	-5.97	0
13	SLU 24	-128	0	2228	0	-5.97	0
13	SLU 25	-128	0	2228	0	-5.97	0
13	SLU 26	-128	0	2228	0	-5.97	0
13	SLU 27	-128	0	2228	0	-5.97	0
13	SLU 28	-128	0	2228	0	-5.97	0
13	SLU 29	-128	0	2228	0	-5.97	0
13	SLU 30	-128	0	2228	0	-5.97	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
13	SLU 31	-167	0	2705	0	-7.72	0
13	SLU 32	-167	0	2705	0	-7.72	0
13	SLU 33	-167	0	2705	0	-7.72	0
13	SLU 34	-167	0	2705	0	-7.72	0
13	SLU 35	-167	0	2705	0	-7.72	0
13	SLU 36	-167	0	2705	0	-7.72	0
13	SLU 37	-167	0	2705	0	-7.72	0
13	SLU 38	-167	0	2705	0	-7.72	0
13	SLU 39	-183	0	2910	0	-8.47	0
13	SLU 40	-183	0	2910	0	-8.47	0
13	SLU 41	-183	0	2910	0	-8.47	0
13	SLU 42	-183	0	2910	0	-8.47	0
13	SLU 43	-137	0	2446	0	-6.39	0
13	SLU 44	-137	0	2446	0	-6.39	0
13	SLU 45	-137	0	2446	0	-6.39	0
13	SLU 46	-137	0	2446	0	-6.39	0
13	SLU 47	-137	0	2446	0	-6.39	0
13	SLU 48	-137	0	2446	0	-6.39	0
13	SLU 49	-137	0	2446	0	-6.39	0
13	SLU 50	-137	0	2446	0	-6.39	0
13	SLU 51	-137	0	2446	0	-6.39	0
13	SLU 52	-176	0	2923	0	-8.14	0
13	SLU 53	-176	0	2923	0	-8.14	0
13	SLU 54	-176	0	2923	0	-8.14	0
13	SLU 55	-176	0	2923	0	-8.14	0
13	SLU 56	-176	0	2923	0	-8.14	0
13	SLU 57	-176	0	2923	0	-8.14	0
13	SLU 58	-176	0	2923	0	-8.14	0
13	SLU 59	-176	0	2923	0	-8.14	0
13	SLU 60	-192	0	3128	0	-8.89	0
13	SLU 61	-192	0	3128	0	-8.89	0
13	SLU 62	-192	0	3128	0	-8.89	0
13	SLU 63	-192	0	3128	0	-8.89	0
13	SLU 64	-155	0	2720	0	-7.22	0
13	SLU 65	-155	0	2720	0	-7.22	0
13	SLU 66	-155	0	2720	0	-7.22	0
13	SLU 67	-155	0	2720	0	-7.22	0
13	SLU 68	-155	0	2720	0	-7.22	0
13	SLU 69	-155	0	2720	0	-7.22	0
13	SLU 70	-155	0	2720	0	-7.22	0
13	SLU 71	-155	0	2720	0	-7.22	0
13	SLU 72	-155	0	2720	0	-7.22	0
13	SLU 73	-194	0	3197	0	-8.97	0
13	SLU 74	-194	0	3197	0	-8.97	0
13	SLU 75	-194	0	3197	0	-8.97	0
13	SLU 76	-194	0	3197	0	-8.97	0
13	SLU 77	-194	0	3197	0	-8.97	0
13	SLU 78	-194	0	3197	0	-8.97	0
13	SLU 79	-194	0	3197	0	-8.97	0
13	SLU 80	-194	0	3197	0	-8.97	0
13	SLU 81	-210	0	3402	0	-9.72	0
13	SLU 82	-210	0	3402	0	-9.72	0
13	SLU 83	-210	0	3402	0	-9.72	0
13	SLU 84	-210	0	3402	0	-9.72	0
13	SLE RA 1	-116	0	2032	0	-5.37	0
13	SLE RA 2	-116	0	2032	0	-5.37	0
13	SLE RA 3	-116	0	2032	0	-5.37	0
13	SLE RA 4	-116	0	2032	0	-5.37	0
13	SLE RA 5	-116	0	2032	0	-5.37	0
13	SLE RA 6	-116	0	2032	0	-5.37	0
13	SLE RA 7	-116	0	2032	0	-5.37	0
13	SLE RA 8	-116	0	2032	0	-5.37	0
13	SLE RA 9	-116	0	2032	0	-5.37	0
13	SLE RA 10	-141	0	2350	0	-6.54	0
13	SLE RA 11	-141	0	2350	0	-6.54	0
13	SLE RA 12	-141	0	2350	0	-6.54	0
13	SLE RA 13	-141	0	2350	0	-6.54	0
13	SLE RA 14	-141	0	2350	0	-6.54	0
13	SLE RA 15	-141	0	2350	0	-6.54	0
13	SLE RA 16	-141	0	2350	0	-6.54	0
13	SLE RA 17	-141	0	2350	0	-6.54	0
13	SLE RA 18	-152	0	2487	0	-7.04	0
13	SLE RA 19	-152	0	2487	0	-7.04	0
13	SLE RA 20	-152	0	2487	0	-7.04	0
13	SLE RA 21	-152	0	2487	0	-7.04	0
13	SLE FR 1	-116	0	2032	0	-5.37	0
13	SLE FR 2	-116	0	2032	0	-5.37	0
13	SLE FR 3	-116	0	2032	0	-5.37	0
13	SLE FR 4	-126	0	2168	0	-5.87	0
13	SLE FR 5	-126	0	2168	0	-5.87	0
13	SLE FR 6	-134	0	2259	0	-6.2	0
13	SLE QP 1	-116	0	2032	0	-5.37	0
13	SLE QP 2	-126	0	2168	0	-5.87	0
13	SLD 1	57	4	2078	-15.38	3.22	-0.02
13	SLD 2	57	4	2078	-15.38	3.22	-0.02
13	SLD 3	75	-33	2039	44.55	4.13	0.11
13	SLD 4	75	-33	2039	44.55	4.13	0.11
13	SLD 5	-99	57	2200	-95.51	-4.52	-0.21



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
13	SLD 6	-99	57	2200	-95.51	-4.52	-0.21
13	SLD 7	-39	-65	2070	104.27	-1.5	0.23
13	SLD 8	-39	-65	2070	104.27	-1.5	0.23
13	SLD 9	-214	65	2266	-104.26	-10.24	-0.23
13	SLD 10	-214	65	2266	-104.26	-10.24	-0.23
13	SLD 11	-154	-57	2136	95.52	-7.23	0.21
13	SLD 12	-154	-57	2136	95.52	-7.23	0.21
13	SLD 13	-328	33	2298	-44.54	-15.87	-0.11
13	SLD 14	-328	33	2298	-44.54	-15.87	-0.11
13	SLD 15	-310	-4	2259	15.39	-14.96	0.02
13	SLD 16	-310	-4	2259	15.39	-14.96	0.02
13	SLV 1	301	15	1966	-47.39	15.34	-0.07
13	SLV 2	301	15	1966	-47.39	15.34	-0.07
13	SLV 3	351	-88	1857	121.61	17.85	0.3
13	SLV 4	351	-88	1857	121.61	17.85	0.3
13	SLV 5	-74	161	2273	-270.54	-3.31	-0.59
13	SLV 6	-74	161	2273	-270.54	-3.31	-0.59
13	SLV 7	93	-183	1910	292.81	5.05	0.66
13	SLV 8	93	-183	1910	292.81	5.05	0.66
13	SLV 9	-346	183	2427	-292.8	-16.79	-0.66
13	SLV 10	-346	183	2427	-292.8	-16.79	-0.66
13	SLV 11	-179	-161	2064	270.54	-8.43	0.59
13	SLV 12	-179	-161	2064	270.54	-8.43	0.59
13	SLV 13	-604	88	2480	-121.61	-29.59	-0.3
13	SLV 14	-604	88	2480	-121.61	-29.59	-0.3
13	SLV 15	-554	-15	2371	47.4	-27.08	0.07
13	SLV 16	-554	-15	2371	47.4	-27.08	0.07
14	SLU 1	-101	0	1998	0.01	-4.81	0
14	SLU 2	-101	0	1998	0.01	-4.81	0
14	SLU 3	-101	0	1998	0.01	-4.81	0
14	SLU 4	-101	0	1998	0.01	-4.81	0
14	SLU 5	-101	0	1998	0.01	-4.81	0
14	SLU 6	-101	0	1998	0.01	-4.81	0
14	SLU 7	-101	0	1998	0.01	-4.81	0
14	SLU 8	-101	0	1998	0.01	-4.81	0
14	SLU 9	-101	0	1998	0.01	-4.81	0
14	SLU 10	-136	0	2488	0.01	-6.57	0
14	SLU 11	-136	0	2488	0.01	-6.57	0
14	SLU 12	-136	0	2488	0.01	-6.57	0
14	SLU 13	-136	0	2488	0.01	-6.57	0
14	SLU 14	-136	0	2488	0.01	-6.57	0
14	SLU 15	-136	0	2488	0.01	-6.57	0
14	SLU 16	-136	0	2488	0.01	-6.57	0
14	SLU 17	-136	0	2488	0.01	-6.57	0
14	SLU 18	-152	0	2698	0.01	-7.32	0
14	SLU 19	-152	0	2698	0.01	-7.32	0
14	SLU 20	-152	0	2698	0.01	-7.32	0
14	SLU 21	-152	0	2698	0.01	-7.32	0
14	SLU 22	-117	0	2278	0.01	-5.61	0
14	SLU 23	-117	0	2278	0.01	-5.61	0
14	SLU 24	-117	0	2278	0.01	-5.61	0
14	SLU 25	-117	0	2278	0.01	-5.61	0
14	SLU 26	-117	0	2278	0.01	-5.61	0
14	SLU 27	-117	0	2278	0.01	-5.61	0
14	SLU 28	-117	0	2278	0.01	-5.61	0
14	SLU 29	-117	0	2278	0.01	-5.61	0
14	SLU 30	-117	0	2278	0.01	-5.61	0
14	SLU 31	-153	0	2768	0.01	-7.37	0
14	SLU 32	-153	0	2768	0.01	-7.37	0
14	SLU 33	-153	0	2768	0.01	-7.37	0
14	SLU 34	-153	0	2768	0.01	-7.37	0
14	SLU 35	-153	0	2768	0.01	-7.37	0
14	SLU 36	-153	0	2768	0.01	-7.37	0
14	SLU 37	-153	0	2768	0.01	-7.37	0
14	SLU 38	-153	0	2768	0.01	-7.37	0
14	SLU 39	-168	0	2978	0.01	-8.12	0
14	SLU 40	-168	0	2978	0.01	-8.12	0
14	SLU 41	-168	0	2978	0.01	-8.12	0
14	SLU 42	-168	0	2978	0.01	-8.12	0
14	SLU 43	-126	0	2501	0.01	-5.98	0
14	SLU 44	-126	0	2501	0.01	-5.98	0
14	SLU 45	-126	0	2501	0.01	-5.98	0
14	SLU 46	-126	0	2501	0.01	-5.98	0
14	SLU 47	-126	0	2501	0.01	-5.98	0
14	SLU 48	-126	0	2501	0.01	-5.98	0
14	SLU 49	-126	0	2501	0.01	-5.98	0
14	SLU 50	-126	0	2501	0.01	-5.98	0
14	SLU 51	-126	0	2501	0.01	-5.98	0
14	SLU 52	-161	0	2992	0.01	-7.73	0
14	SLU 53	-161	0	2992	0.01	-7.73	0
14	SLU 54	-161	0	2992	0.01	-7.73	0
14	SLU 55	-161	0	2992	0.01	-7.73	0
14	SLU 56	-161	0	2992	0.01	-7.73	0
14	SLU 57	-161	0	2992	0.01	-7.73	0
14	SLU 58	-161	0	2992	0.01	-7.73	0
14	SLU 59	-161	0	2992	0.01	-7.73	0
14	SLU 60	-176	0	3202	0.02	-8.49	0
14	SLU 61	-176	0	3202	0.02	-8.49	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
14	SLU 62	-176	0	3202	0.02	-8.49	0
14	SLU 63	-176	0	3202	0.02	-8.49	0
14	SLU 64	-142	0	2781	0.01	-6.78	0
14	SLU 65	-142	0	2781	0.01	-6.78	0
14	SLU 66	-142	0	2781	0.01	-6.78	0
14	SLU 67	-142	0	2781	0.01	-6.78	0
14	SLU 68	-142	0	2781	0.01	-6.78	0
14	SLU 69	-142	0	2781	0.01	-6.78	0
14	SLU 70	-142	0	2781	0.01	-6.78	0
14	SLU 71	-142	0	2781	0.01	-6.78	0
14	SLU 72	-142	0	2781	0.01	-6.78	0
14	SLU 73	-177	0	3271	0.02	-8.54	0
14	SLU 74	-177	0	3271	0.02	-8.54	0
14	SLU 75	-177	0	3271	0.02	-8.54	0
14	SLU 76	-177	0	3271	0.02	-8.54	0
14	SLU 77	-177	0	3271	0.02	-8.54	0
14	SLU 78	-177	0	3271	0.02	-8.54	0
14	SLU 79	-177	0	3271	0.02	-8.54	0
14	SLU 80	-177	0	3271	0.02	-8.54	0
14	SLU 81	-193	0	3482	0.02	-9.29	0
14	SLU 82	-193	0	3482	0.02	-9.29	0
14	SLU 83	-193	0	3482	0.02	-9.29	0
14	SLU 84	-193	0	3482	0.02	-9.29	0
14	SLE RA 1	-106	0	2078	0.01	-5.04	0
14	SLE RA 2	-106	0	2078	0.01	-5.04	0
14	SLE RA 3	-106	0	2078	0.01	-5.04	0
14	SLE RA 4	-106	0	2078	0.01	-5.04	0
14	SLE RA 5	-106	0	2078	0.01	-5.04	0
14	SLE RA 6	-106	0	2078	0.01	-5.04	0
14	SLE RA 7	-106	0	2078	0.01	-5.04	0
14	SLE RA 8	-106	0	2078	0.01	-5.04	0
14	SLE RA 9	-106	0	2078	0.01	-5.04	0
14	SLE RA 10	-129	0	2405	0.01	-6.21	0
14	SLE RA 11	-129	0	2405	0.01	-6.21	0
14	SLE RA 12	-129	0	2405	0.01	-6.21	0
14	SLE RA 13	-129	0	2405	0.01	-6.21	0
14	SLE RA 14	-129	0	2405	0.01	-6.21	0
14	SLE RA 15	-129	0	2405	0.01	-6.21	0
14	SLE RA 16	-129	0	2405	0.01	-6.21	0
14	SLE RA 17	-129	0	2405	0.01	-6.21	0
14	SLE RA 18	-139	0	2545	0.01	-6.71	0
14	SLE RA 19	-139	0	2545	0.01	-6.71	0
14	SLE RA 20	-139	0	2545	0.01	-6.71	0
14	SLE RA 21	-139	0	2545	0.01	-6.71	0
14	SLE FR 1	-106	0	2078	0.01	-5.04	0
14	SLE FR 2	-106	0	2078	0.01	-5.04	0
14	SLE FR 3	-106	0	2078	0.01	-5.04	0
14	SLE FR 4	-116	0	2218	0.01	-5.54	0
14	SLE FR 5	-116	0	2218	0.01	-5.54	0
14	SLE FR 6	-122	0	2311	0.01	-5.88	0
14	SLE QP 1	-106	0	2078	0.01	-5.04	0
14	SLE QP 2	-116	0	2218	0.01	-5.54	0
14	SLD 1	62	11	2127	-22.26	3.32	-0.04
14	SLD 2	62	11	2127	-22.26	3.32	-0.04
14	SLD 3	78	-37	2078	46.51	3.99	0.09
14	SLD 4	78	-37	2078	46.51	3.99	0.09
14	SLD 5	-87	76	2265	-110.98	-3.9	-0.21
14	SLD 6	-87	76	2265	-110.98	-3.9	-0.21
14	SLD 7	-33	-84	2101	118.27	-1.66	0.22
14	SLD 8	-33	-84	2101	118.27	-1.66	0.22
14	SLD 9	-198	83	2335	-118.25	-9.42	-0.22
14	SLD 10	-198	83	2335	-118.25	-9.42	-0.22
14	SLD 11	-145	-76	2170	111	-7.18	0.21
14	SLD 12	-145	-76	2170	111	-7.18	0.21
14	SLD 13	-309	37	2358	-46.49	-15.07	-0.09
14	SLD 14	-309	37	2358	-46.49	-15.07	-0.09
14	SLD 15	-293	-11	2309	22.28	-14.4	0.04
14	SLD 16	-293	-11	2309	22.28	-14.4	0.04
14	SLV 1	299	35	2018	-66.34	15.2	-0.11
14	SLV 2	299	35	2018	-66.34	15.2	-0.11
14	SLV 3	343	-100	1880	127.87	17.03	0.26
14	SLV 4	343	-100	1880	127.87	17.03	0.26
14	SLV 5	-59	215	2368	-314.46	-2.09	-0.59
14	SLV 6	-59	215	2368	-314.46	-2.09	-0.59
14	SLV 7	89	-235	1907	332.93	4	0.63
14	SLV 8	89	-235	1907	332.93	4	0.63
14	SLV 9	-321	234	2529	-332.91	-15.08	-0.63
14	SLV 10	-321	234	2529	-332.91	-15.08	-0.63
14	SLV 11	-173	-215	2068	314.48	-8.99	0.59
14	SLV 12	-173	-215	2068	314.48	-8.99	0.59
14	SLV 13	-575	100	2556	-127.85	-28.11	-0.26
14	SLV 14	-575	100	2556	-127.85	-28.11	-0.26
14	SLV 15	-530	-35	2418	66.37	-26.28	0.11
14	SLV 16	-530	-35	2418	66.37	-26.28	0.11
15	SLU 1	-75	0	2042	0.01	-3.37	0
15	SLU 2	-75	0	2042	0.01	-3.37	0
15	SLU 3	-75	0	2042	0.01	-3.37	0
15	SLU 4	-75	0	2042	0.01	-3.37	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
15	SLU 5	-75	0	2042	0.01	-3.37	0
15	SLU 6	-75	0	2042	0.01	-3.37	0
15	SLU 7	-75	0	2042	0.01	-3.37	0
15	SLU 8	-75	0	2042	0.01	-3.37	0
15	SLU 9	-75	0	2042	0.01	-3.37	0
15	SLU 10	-101	0	2547	0.01	-4.49	0
15	SLU 11	-101	0	2547	0.01	-4.49	0
15	SLU 12	-101	0	2547	0.01	-4.49	0
15	SLU 13	-101	0	2547	0.01	-4.49	0
15	SLU 14	-101	0	2547	0.01	-4.49	0
15	SLU 15	-101	0	2547	0.01	-4.49	0
15	SLU 16	-101	0	2547	0.01	-4.49	0
15	SLU 17	-101	0	2547	0.01	-4.49	0
15	SLU 18	-112	0	2763	0.01	-4.97	0
15	SLU 19	-112	0	2763	0.01	-4.97	0
15	SLU 20	-112	0	2763	0.01	-4.97	0
15	SLU 21	-112	0	2763	0.01	-4.97	0
15	SLU 22	-87	0	2328	0.01	-3.88	0
15	SLU 23	-87	0	2328	0.01	-3.88	0
15	SLU 24	-87	0	2328	0.01	-3.88	0
15	SLU 25	-87	0	2328	0.01	-3.88	0
15	SLU 26	-87	0	2328	0.01	-3.88	0
15	SLU 27	-87	0	2328	0.01	-3.88	0
15	SLU 28	-87	0	2328	0.01	-3.88	0
15	SLU 29	-87	0	2328	0.01	-3.88	0
15	SLU 30	-87	0	2328	0.01	-3.88	0
15	SLU 31	-113	0	2832	0.01	-5	0
15	SLU 32	-113	0	2832	0.01	-5	0
15	SLU 33	-113	0	2832	0.01	-5	0
15	SLU 34	-113	0	2832	0.01	-5	0
15	SLU 35	-113	0	2832	0.01	-5	0
15	SLU 36	-113	0	2832	0.01	-5	0
15	SLU 37	-113	0	2832	0.01	-5	0
15	SLU 38	-113	0	2832	0.01	-5	0
15	SLU 39	-124	0	3048	0.01	-5.48	0
15	SLU 40	-124	0	3048	0.01	-5.48	0
15	SLU 41	-124	0	3048	0.01	-5.48	0
15	SLU 42	-124	0	3048	0.01	-5.48	0
15	SLU 43	-94	0	2557	0.01	-4.21	0
15	SLU 44	-94	0	2557	0.01	-4.21	0
15	SLU 45	-94	0	2557	0.01	-4.21	0
15	SLU 46	-94	0	2557	0.01	-4.21	0
15	SLU 47	-94	0	2557	0.01	-4.21	0
15	SLU 48	-94	0	2557	0.01	-4.21	0
15	SLU 49	-94	0	2557	0.01	-4.21	0
15	SLU 50	-94	0	2557	0.01	-4.21	0
15	SLU 51	-94	0	2557	0.01	-4.21	0
15	SLU 52	-120	0	3061	0.01	-5.32	0
15	SLU 53	-120	0	3061	0.01	-5.32	0
15	SLU 54	-120	0	3061	0.01	-5.32	0
15	SLU 55	-120	0	3061	0.01	-5.32	0
15	SLU 56	-120	0	3061	0.01	-5.32	0
15	SLU 57	-120	0	3061	0.01	-5.32	0
15	SLU 58	-120	0	3061	0.01	-5.32	0
15	SLU 59	-120	0	3061	0.01	-5.32	0
15	SLU 60	-131	0	3277	0.02	-5.84	0
15	SLU 61	-131	0	3277	0.02	-5.84	0
15	SLU 62	-131	0	3277	0.02	-5.84	0
15	SLU 63	-131	0	3277	0.02	-5.84	0
15	SLU 64	-106	0	2843	0.01	-4.72	0
15	SLU 65	-106	0	2843	0.01	-4.72	0
15	SLU 66	-106	0	2843	0.01	-4.72	0
15	SLU 67	-106	0	2843	0.01	-4.72	0
15	SLU 68	-106	0	2843	0.01	-4.72	0
15	SLU 69	-106	0	2843	0.01	-4.72	0
15	SLU 70	-106	0	2843	0.01	-4.72	0
15	SLU 71	-106	0	2843	0.01	-4.72	0
15	SLU 72	-106	0	2843	0.01	-4.72	0
15	SLU 73	-131	0	3347	0.02	-5.84	0
15	SLU 74	-131	0	3347	0.02	-5.84	0
15	SLU 75	-131	0	3347	0.02	-5.84	0
15	SLU 76	-131	0	3347	0.02	-5.84	0
15	SLU 77	-131	0	3347	0.02	-5.84	0
15	SLU 78	-131	0	3347	0.02	-5.84	0
15	SLU 79	-131	0	3347	0.02	-5.84	0
15	SLU 80	-131	0	3347	0.02	-5.84	0
15	SLU 81	-142	0	3563	0.02	-6.32	0
15	SLU 82	-142	0	3563	0.02	-6.32	0
15	SLU 83	-142	0	3563	0.02	-6.32	0
15	SLU 84	-142	0	3563	0.02	-6.32	0
15	SLE RA 1	-79	0	2124	0.01	-3.52	0
15	SLE RA 2	-79	0	2124	0.01	-3.52	0
15	SLE RA 3	-79	0	2124	0.01	-3.52	0
15	SLE RA 4	-79	0	2124	0.01	-3.52	0
15	SLE RA 5	-79	0	2124	0.01	-3.52	0
15	SLE RA 6	-79	0	2124	0.01	-3.52	0
15	SLE RA 7	-79	0	2124	0.01	-3.52	0
15	SLE RA 8	-79	0	2124	0.01	-3.52	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
15	SLE RA 9	-79	0	2124	0.01	-3.52	0
15	SLE RA 10	-96	0	2460	0.01	-4.26	0
15	SLE RA 11	-96	0	2460	0.01	-4.26	0
15	SLE RA 12	-96	0	2460	0.01	-4.26	0
15	SLE RA 13	-96	0	2460	0.01	-4.26	0
15	SLE RA 14	-96	0	2460	0.01	-4.26	0
15	SLE RA 15	-96	0	2460	0.01	-4.26	0
15	SLE RA 16	-96	0	2460	0.01	-4.26	0
15	SLE RA 17	-96	0	2460	0.01	-4.26	0
15	SLE RA 18	-103	0	2604	0.01	-4.58	0
15	SLE RA 19	-103	0	2604	0.01	-4.58	0
15	SLE RA 20	-103	0	2604	0.01	-4.58	0
15	SLE RA 21	-103	0	2604	0.01	-4.58	0
15	SLE FR 1	-79	0	2124	0.01	-3.52	0
15	SLE FR 2	-79	0	2124	0.01	-3.52	0
15	SLE FR 3	-79	0	2124	0.01	-3.52	0
15	SLE FR 4	-86	0	2268	0.01	-3.84	0
15	SLE FR 5	-86	0	2268	0.01	-3.84	0
15	SLE FR 6	-91	0	2364	0.01	-4.05	0
15	SLE QP 1	-79	0	2124	0.01	-3.52	0
15	SLE QP 2	-86	0	2268	0.01	-3.84	0
15	SLD 1	89	20	2203	-29.95	4.8	-0.04
15	SLD 2	89	20	2203	-29.95	4.8	-0.04
15	SLD 3	103	-41	2144	47.54	5.51	0.07
15	SLD 4	103	-41	2144	47.54	5.51	0.07
15	SLD 5	-56	99	2338	-126.5	-2.32	-0.18
15	SLD 6	-56	99	2338	-126.5	-2.32	-0.18
15	SLD 7	-7	-105	2141	131.79	0.04	0.19
15	SLD 8	-7	-105	2141	131.79	0.04	0.19
15	SLD 9	-165	105	2395	-131.77	-7.71	-0.19
15	SLD 10	-165	105	2395	-131.77	-7.71	-0.19
15	SLD 11	-117	-99	2198	126.53	-5.35	0.18
15	SLD 12	-117	-99	2198	126.53	-5.35	0.18
15	SLD 13	-276	41	2392	-47.52	-13.18	-0.07
15	SLD 14	-276	41	2392	-47.52	-13.18	-0.07
15	SLD 15	-261	-20	2333	29.97	-12.47	0.04
15	SLD 16	-261	-20	2333	29.97	-12.47	0.04
15	SLV 1	323	60	2130	-87.16	16.37	-0.12
15	SLV 2	323	60	2130	-87.16	16.37	-0.12
15	SLV 3	363	-112	1965	131.7	18.31	0.19
15	SLV 4	363	-112	1965	131.7	18.31	0.19
15	SLV 5	-24	280	2478	-358.08	-0.72	-0.5
15	SLV 6	-24	280	2478	-358.08	-0.72	-0.5
15	SLV 7	109	-295	1925	371.46	5.75	0.53
15	SLV 8	109	-295	1925	371.46	5.75	0.53
15	SLV 9	-281	295	2611	-371.44	-13.43	-0.53
15	SLV 10	-281	295	2611	-371.44	-13.43	-0.53
15	SLV 11	-148	-280	2058	358.1	-6.96	0.5
15	SLV 12	-148	-280	2058	358.1	-6.96	0.5
15	SLV 13	-535	112	2572	-131.68	-25.99	-0.19
15	SLV 14	-535	112	2572	-131.68	-25.99	-0.19
15	SLV 15	-496	-60	2406	87.18	-24.05	0.12
15	SLV 16	-496	-60	2406	87.18	-24.05	0.12
16	SLU 1	-42	0	2076	0	-1.97	0
16	SLU 2	-42	0	2076	0	-1.97	0
16	SLU 3	-42	0	2076	0	-1.97	0
16	SLU 4	-42	0	2076	0	-1.97	0
16	SLU 5	-42	0	2076	0	-1.97	0
16	SLU 6	-42	0	2076	0	-1.97	0
16	SLU 7	-42	0	2076	0	-1.97	0
16	SLU 8	-42	0	2076	0	-1.97	0
16	SLU 9	-42	0	2076	0	-1.97	0
16	SLU 10	-56	0	2591	0	-2.66	0
16	SLU 11	-56	0	2591	0	-2.66	0
16	SLU 12	-56	0	2591	0	-2.66	0
16	SLU 13	-56	0	2591	0	-2.66	0
16	SLU 14	-56	0	2591	0	-2.66	0
16	SLU 15	-56	0	2591	0	-2.66	0
16	SLU 16	-56	0	2591	0	-2.66	0
16	SLU 17	-56	0	2591	0	-2.66	0
16	SLU 18	-62	0	2811	0.01	-2.95	0
16	SLU 19	-62	0	2811	0.01	-2.95	0
16	SLU 20	-62	0	2811	0.01	-2.95	0
16	SLU 21	-62	0	2811	0.01	-2.95	0
16	SLU 22	-49	0	2367	0	-2.28	0
16	SLU 23	-49	0	2367	0	-2.28	0
16	SLU 24	-49	0	2367	0	-2.28	0
16	SLU 25	-49	0	2367	0	-2.28	0
16	SLU 26	-49	0	2367	0	-2.28	0
16	SLU 27	-49	0	2367	0	-2.28	0
16	SLU 28	-49	0	2367	0	-2.28	0
16	SLU 29	-49	0	2367	0	-2.28	0
16	SLU 30	-49	0	2367	0	-2.28	0
16	SLU 31	-63	0	2881	0.01	-2.97	0
16	SLU 32	-63	0	2881	0.01	-2.97	0
16	SLU 33	-63	0	2881	0.01	-2.97	0
16	SLU 34	-63	0	2881	0.01	-2.97	0
16	SLU 35	-63	0	2881	0.01	-2.97	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
16	SLU 36	-63	0	2881	0.01	-2.97	0
16	SLU 37	-63	0	2881	0.01	-2.97	0
16	SLU 38	-63	0	2881	0.01	-2.97	0
16	SLU 39	-69	0	3101	0.01	-3.26	0
16	SLU 40	-69	0	3101	0.01	-3.26	0
16	SLU 41	-69	0	3101	0.01	-3.26	0
16	SLU 42	-69	0	3101	0.01	-3.26	0
16	SLU 43	-53	0	2599	0.01	-2.46	0
16	SLU 44	-53	0	2599	0.01	-2.46	0
16	SLU 45	-53	0	2599	0.01	-2.46	0
16	SLU 46	-53	0	2599	0.01	-2.46	0
16	SLU 47	-53	0	2599	0.01	-2.46	0
16	SLU 48	-53	0	2599	0.01	-2.46	0
16	SLU 49	-53	0	2599	0.01	-2.46	0
16	SLU 50	-53	0	2599	0.01	-2.46	0
16	SLU 51	-53	0	2599	0.01	-2.46	0
16	SLU 52	-67	0	3114	0.01	-3.14	0
16	SLU 53	-67	0	3114	0.01	-3.14	0
16	SLU 54	-67	0	3114	0.01	-3.14	0
16	SLU 55	-67	0	3114	0.01	-3.14	0
16	SLU 56	-67	0	3114	0.01	-3.14	0
16	SLU 57	-67	0	3114	0.01	-3.14	0
16	SLU 58	-67	0	3114	0.01	-3.14	0
16	SLU 59	-67	0	3114	0.01	-3.14	0
16	SLU 60	-73	0	3334	0.01	-3.44	0
16	SLU 61	-73	0	3334	0.01	-3.44	0
16	SLU 62	-73	0	3334	0.01	-3.44	0
16	SLU 63	-73	0	3334	0.01	-3.44	0
16	SLU 64	-59	0	2890	0.01	-2.77	0
16	SLU 65	-59	0	2890	0.01	-2.77	0
16	SLU 66	-59	0	2890	0.01	-2.77	0
16	SLU 67	-59	0	2890	0.01	-2.77	0
16	SLU 68	-59	0	2890	0.01	-2.77	0
16	SLU 69	-59	0	2890	0.01	-2.77	0
16	SLU 70	-59	0	2890	0.01	-2.77	0
16	SLU 71	-59	0	2890	0.01	-2.77	0
16	SLU 72	-59	0	2890	0.01	-2.77	0
16	SLU 73	-73	0	3404	0.01	-3.46	0
16	SLU 74	-73	0	3404	0.01	-3.46	0
16	SLU 75	-73	0	3404	0.01	-3.46	0
16	SLU 76	-73	0	3404	0.01	-3.46	0
16	SLU 77	-73	0	3404	0.01	-3.46	0
16	SLU 78	-73	0	3404	0.01	-3.46	0
16	SLU 79	-73	0	3404	0.01	-3.46	0
16	SLU 80	-73	0	3404	0.01	-3.46	0
16	SLU 81	-79	0	3625	0.01	-3.75	0
16	SLU 82	-79	0	3625	0.01	-3.75	0
16	SLU 83	-79	0	3625	0.01	-3.75	0
16	SLU 84	-79	0	3625	0.01	-3.75	0
16	SLE RA 1	-44	0	2159	0	-2.06	0
16	SLE RA 2	-44	0	2159	0	-2.06	0
16	SLE RA 3	-44	0	2159	0	-2.06	0
16	SLE RA 4	-44	0	2159	0	-2.06	0
16	SLE RA 5	-44	0	2159	0	-2.06	0
16	SLE RA 6	-44	0	2159	0	-2.06	0
16	SLE RA 7	-44	0	2159	0	-2.06	0
16	SLE RA 8	-44	0	2159	0	-2.06	0
16	SLE RA 9	-44	0	2159	0	-2.06	0
16	SLE RA 10	-53	0	2502	0	-2.52	0
16	SLE RA 11	-53	0	2502	0	-2.52	0
16	SLE RA 12	-53	0	2502	0	-2.52	0
16	SLE RA 13	-53	0	2502	0	-2.52	0
16	SLE RA 14	-53	0	2502	0	-2.52	0
16	SLE RA 15	-53	0	2502	0	-2.52	0
16	SLE RA 16	-53	0	2502	0	-2.52	0
16	SLE RA 17	-53	0	2502	0	-2.52	0
16	SLE RA 18	-57	0	2649	0.01	-2.72	0
16	SLE RA 19	-57	0	2649	0.01	-2.72	0
16	SLE RA 20	-57	0	2649	0.01	-2.72	0
16	SLE RA 21	-57	0	2649	0.01	-2.72	0
16	SLE FR 1	-44	0	2159	0	-2.06	0
16	SLE FR 2	-44	0	2159	0	-2.06	0
16	SLE FR 3	-44	0	2159	0	-2.06	0
16	SLE FR 4	-48	0	2306	0	-2.26	0
16	SLE FR 5	-48	0	2306	0	-2.26	0
16	SLE FR 6	-51	0	2404	0	-2.39	0
16	SLE QP 1	-44	0	2159	0	-2.06	0
16	SLE QP 2	-48	0	2306	0	-2.26	0
16	SLD 1	130	33	2287	-37.73	6.48	-0.05
16	SLD 2	130	33	2287	-37.73	6.48	-0.05
16	SLD 3	139	-45	2220	47.09	6.9	0.06
16	SLD 4	139	-45	2220	47.09	6.9	0.06
16	SLD 5	-9	128	2403	-139.97	-0.27	-0.18
16	SLD 6	-9	128	2403	-139.97	-0.27	-0.18
16	SLD 7	23	-132	2178	142.78	1.12	0.18
16	SLD 8	23	-132	2178	142.78	1.12	0.18
16	SLD 9	-119	132	2434	-142.77	-5.63	-0.18
16	SLD 10	-119	132	2434	-142.77	-5.63	-0.18



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
16	SLD 11	-87	-128	2209	139.98	-4.25	0.18
16	SLD 12	-87	-128	2209	139.98	-4.25	0.18
16	SLD 13	-235	45	2393	-47.08	-11.41	-0.06
16	SLD 14	-235	45	2393	-47.08	-11.41	-0.06
16	SLD 15	-226	-33	2325	37.74	-11	0.05
16	SLD 16	-226	-33	2325	37.74	-11	0.05
16	SLV 1	369	94	2278	-107.9	18.29	-0.14
16	SLV 2	369	94	2278	-107.9	18.29	-0.14
16	SLV 3	394	-126	2088	131.59	19.36	0.16
16	SLV 4	394	-126	2088	131.59	19.36	0.16
16	SLV 5	39	362	2586	-395.6	2.28	-0.51
16	SLV 6	39	362	2586	-395.6	2.28	-0.51
16	SLV 7	123	-372	1953	402.71	5.85	0.52
16	SLV 8	123	-372	1953	402.71	5.85	0.52
16	SLV 9	-219	372	2659	-402.7	-10.37	-0.52
16	SLV 10	-219	372	2659	-402.7	-10.37	-0.52
16	SLV 11	-135	-362	2026	395.61	-6.8	0.51
16	SLV 12	-135	-362	2026	395.61	-6.8	0.51
16	SLV 13	-490	126	2524	-131.58	-23.88	-0.16
16	SLV 14	-490	126	2524	-131.58	-23.88	-0.16
16	SLV 15	-465	-94	2334	107.91	-22.8	0.14
16	SLV 16	-465	-94	2334	107.91	-22.8	0.14
17	SLU 1	2	0	2543	0	0.12	0
17	SLU 2	2	0	2543	0	0.12	0
17	SLU 3	2	0	2543	0	0.12	0
17	SLU 4	2	0	2543	0	0.12	0
17	SLU 5	2	0	2543	0	0.12	0
17	SLU 6	2	0	2543	0	0.12	0
17	SLU 7	2	0	2543	0	0.12	0
17	SLU 8	2	0	2543	0	0.12	0
17	SLU 9	2	0	2543	0	0.12	0
17	SLU 10	4	0	3172	0	0.22	0
17	SLU 11	4	0	3172	0	0.22	0
17	SLU 12	4	0	3172	0	0.22	0
17	SLU 13	4	0	3172	0	0.22	0
17	SLU 14	4	0	3172	0	0.22	0
17	SLU 15	4	0	3172	0	0.22	0
17	SLU 16	4	0	3172	0	0.22	0
17	SLU 17	4	0	3172	0	0.22	0
17	SLU 18	4	0	3441	0	0.27	0
17	SLU 19	4	0	3441	0	0.27	0
17	SLU 20	4	0	3441	0	0.27	0
17	SLU 21	4	0	3441	0	0.27	0
17	SLU 22	3	0	2898	0	0.16	0
17	SLU 23	3	0	2898	0	0.16	0
17	SLU 24	3	0	2898	0	0.16	0
17	SLU 25	3	0	2898	0	0.16	0
17	SLU 26	3	0	2898	0	0.16	0
17	SLU 27	3	0	2898	0	0.16	0
17	SLU 28	3	0	2898	0	0.16	0
17	SLU 29	3	0	2898	0	0.16	0
17	SLU 30	3	0	2898	0	0.16	0
17	SLU 31	4	0	3526	0	0.27	0
17	SLU 32	4	0	3526	0	0.27	0
17	SLU 33	4	0	3526	0	0.27	0
17	SLU 34	4	0	3526	0	0.27	0
17	SLU 35	4	0	3526	0	0.27	0
17	SLU 36	4	0	3526	0	0.27	0
17	SLU 37	4	0	3526	0	0.27	0
17	SLU 38	4	0	3526	0	0.27	0
17	SLU 39	5	0	3795	0	0.31	0
17	SLU 40	5	0	3795	0	0.31	0
17	SLU 41	5	0	3795	0	0.31	0
17	SLU 42	5	0	3795	0	0.31	0
17	SLU 43	2	0	3185	0	0.14	0
17	SLU 44	2	0	3185	0	0.14	0
17	SLU 45	2	0	3185	0	0.14	0
17	SLU 46	2	0	3185	0	0.14	0
17	SLU 47	2	0	3185	0	0.14	0
17	SLU 48	2	0	3185	0	0.14	0
17	SLU 49	2	0	3185	0	0.14	0
17	SLU 50	2	0	3185	0	0.14	0
17	SLU 51	2	0	3185	0	0.14	0
17	SLU 52	4	0	3813	0	0.24	0
17	SLU 53	4	0	3813	0	0.24	0
17	SLU 54	4	0	3813	0	0.24	0
17	SLU 55	4	0	3813	0	0.24	0
17	SLU 56	4	0	3813	0	0.24	0
17	SLU 57	4	0	3813	0	0.24	0
17	SLU 58	4	0	3813	0	0.24	0
17	SLU 59	4	0	3813	0	0.24	0
17	SLU 60	5	0	4082	0	0.29	0
17	SLU 61	5	0	4082	0	0.29	0
17	SLU 62	5	0	4082	0	0.29	0
17	SLU 63	5	0	4082	0	0.29	0
17	SLU 64	3	0	3540	0	0.18	0
17	SLU 65	3	0	3540	0	0.18	0
17	SLU 66	3	0	3540	0	0.18	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
17	SLU 67	3	0	3540	0	0.18	0
17	SLU 68	3	0	3540	0	0.18	0
17	SLU 69	3	0	3540	0	0.18	0
17	SLU 70	3	0	3540	0	0.18	0
17	SLU 71	3	0	3540	0	0.18	0
17	SLU 72	3	0	3540	0	0.18	0
17	SLU 73	5	0	4168	0	0.29	0
17	SLU 74	5	0	4168	0	0.29	0
17	SLU 75	5	0	4168	0	0.29	0
17	SLU 76	5	0	4168	0	0.29	0
17	SLU 77	5	0	4168	0	0.29	0
17	SLU 78	5	0	4168	0	0.29	0
17	SLU 79	5	0	4168	0	0.29	0
17	SLU 80	5	0	4168	0	0.29	0
17	SLU 81	5	0	4437	0	0.33	0
17	SLU 82	5	0	4437	0	0.33	0
17	SLU 83	5	0	4437	0	0.33	0
17	SLU 84	5	0	4437	0	0.33	0
17	SLE RA 1	2	0	2645	0	0.13	0
17	SLE RA 2	2	0	2645	0	0.13	0
17	SLE RA 3	2	0	2645	0	0.13	0
17	SLE RA 4	2	0	2645	0	0.13	0
17	SLE RA 5	2	0	2645	0	0.13	0
17	SLE RA 6	2	0	2645	0	0.13	0
17	SLE RA 7	2	0	2645	0	0.13	0
17	SLE RA 8	2	0	2645	0	0.13	0
17	SLE RA 9	2	0	2645	0	0.13	0
17	SLE RA 10	3	0	3064	0	0.2	0
17	SLE RA 11	3	0	3064	0	0.2	0
17	SLE RA 12	3	0	3064	0	0.2	0
17	SLE RA 13	3	0	3064	0	0.2	0
17	SLE RA 14	3	0	3064	0	0.2	0
17	SLE RA 15	3	0	3064	0	0.2	0
17	SLE RA 16	3	0	3064	0	0.2	0
17	SLE RA 17	3	0	3064	0	0.2	0
17	SLE RA 18	4	0	3243	0	0.23	0
17	SLE RA 19	4	0	3243	0	0.23	0
17	SLE RA 20	4	0	3243	0	0.23	0
17	SLE RA 21	4	0	3243	0	0.23	0
17	SLE FR 1	2	0	2645	0	0.13	0
17	SLE FR 2	2	0	2645	0	0.13	0
17	SLE FR 3	2	0	2645	0	0.13	0
17	SLE FR 4	3	0	2824	0	0.16	0
17	SLE FR 5	3	0	2824	0	0.16	0
17	SLE FR 6	3	0	2944	0	0.18	0
17	SLE QP 1	2	0	2645	0	0.13	0
17	SLE QP 2	3	0	2824	0	0.16	0
17	SLD 1	181	47	2856	-43.47	8.93	-0.02
17	SLD 2	181	47	2856	-43.47	8.93	-0.02
17	SLD 3	187	-48	2797	44.51	9.24	-0.02
17	SLD 4	187	-48	2797	44.51	9.24	-0.02
17	SLD 5	47	158	2924	-146.47	2.33	0
17	SLD 6	47	158	2924	-146.47	2.33	0
17	SLD 7	67	-158	2725	146.78	3.35	-0.01
17	SLD 8	67	-158	2725	146.78	3.35	-0.01
17	SLD 9	-62	158	2923	-146.78	-3.02	0.01
17	SLD 10	-62	158	2923	-146.78	-3.02	0.01
17	SLD 11	-42	-158	2724	146.47	-2.01	0
17	SLD 12	-42	-158	2724	146.47	-2.01	0
17	SLD 13	-182	48	2852	-44.51	-8.92	0.02
17	SLD 14	-182	48	2852	-44.51	-8.92	0.02
17	SLD 15	-176	-46	2792	43.47	-8.61	0.02
17	SLD 16	-176	-46	2792	43.47	-8.61	0.02
17	SLV 1	424	131	2914	-122.89	20.84	-0.05
17	SLV 2	424	131	2914	-122.89	20.84	-0.05
17	SLV 3	438	-136	2746	125.38	21.56	-0.05
17	SLV 4	438	-136	2746	125.38	21.56	-0.05
17	SLV 5	107	445	3105	-413.41	5.28	0
17	SLV 6	107	445	3105	-413.41	5.28	0
17	SLV 7	155	-446	2547	414.16	7.67	-0.03
17	SLV 8	155	-446	2547	414.16	7.67	-0.03
17	SLV 9	-150	446	3101	-414.16	-7.34	0.03
17	SLV 10	-150	446	3101	-414.16	-7.34	0.03
17	SLV 11	-102	-445	2544	413.41	-4.96	0
17	SLV 12	-102	-445	2544	413.41	-4.96	0
17	SLV 13	-433	136	2902	-125.38	-21.23	0.05
17	SLV 14	-433	136	2902	-125.38	-21.23	0.05
17	SLV 15	-419	-131	2735	122.89	-20.52	0.05
17	SLV 16	-419	-131	2735	122.89	-20.52	0.05
18	SLU 1	44	0	2042	0	2.04	0
18	SLU 2	44	0	2042	0	2.04	0
18	SLU 3	44	0	2042	0	2.04	0
18	SLU 4	44	0	2042	0	2.04	0
18	SLU 5	44	0	2042	0	2.04	0
18	SLU 6	44	0	2042	0	2.04	0
18	SLU 7	44	0	2042	0	2.04	0
18	SLU 8	44	0	2042	0	2.04	0
18	SLU 9	44	0	2042	0	2.04	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
18	SLU 10	61	0	2547	0	2.82	0
18	SLU 11	61	0	2547	0	2.82	0
18	SLU 12	61	0	2547	0	2.82	0
18	SLU 13	61	0	2547	0	2.82	0
18	SLU 14	61	0	2547	0	2.82	0
18	SLU 15	61	0	2547	0	2.82	0
18	SLU 16	61	0	2547	0	2.82	0
18	SLU 17	61	0	2547	0	2.82	0
18	SLU 18	68	0	2764	0.01	3.16	0
18	SLU 19	68	0	2764	0.01	3.16	0
18	SLU 20	68	0	2764	0.01	3.16	0
18	SLU 21	68	0	2764	0.01	3.16	0
18	SLU 22	52	0	2328	0	2.4	0
18	SLU 23	52	0	2328	0	2.4	0
18	SLU 24	52	0	2328	0	2.4	0
18	SLU 25	52	0	2328	0	2.4	0
18	SLU 26	52	0	2328	0	2.4	0
18	SLU 27	52	0	2328	0	2.4	0
18	SLU 28	52	0	2328	0	2.4	0
18	SLU 29	52	0	2328	0	2.4	0
18	SLU 30	52	0	2328	0	2.4	0
18	SLU 31	69	0	2833	0.01	3.18	0
18	SLU 32	69	0	2833	0.01	3.18	0
18	SLU 33	69	0	2833	0.01	3.18	0
18	SLU 34	69	0	2833	0.01	3.18	0
18	SLU 35	69	0	2833	0.01	3.18	0
18	SLU 36	69	0	2833	0.01	3.18	0
18	SLU 37	69	0	2833	0.01	3.18	0
18	SLU 38	69	0	2833	0.01	3.18	0
18	SLU 39	76	0	3049	0.01	3.52	0
18	SLU 40	76	0	3049	0.01	3.52	0
18	SLU 41	76	0	3049	0.01	3.52	0
18	SLU 42	76	0	3049	0.01	3.52	0
18	SLU 43	55	0	2557	0.01	2.53	0
18	SLU 44	55	0	2557	0.01	2.53	0
18	SLU 45	55	0	2557	0.01	2.53	0
18	SLU 46	55	0	2557	0.01	2.53	0
18	SLU 47	55	0	2557	0.01	2.53	0
18	SLU 48	55	0	2557	0.01	2.53	0
18	SLU 49	55	0	2557	0.01	2.53	0
18	SLU 50	55	0	2557	0.01	2.53	0
18	SLU 51	55	0	2557	0.01	2.53	0
18	SLU 52	72	0	3062	0.01	3.31	0
18	SLU 53	72	0	3062	0.01	3.31	0
18	SLU 54	72	0	3062	0.01	3.31	0
18	SLU 55	72	0	3062	0.01	3.31	0
18	SLU 56	72	0	3062	0.01	3.31	0
18	SLU 57	72	0	3062	0.01	3.31	0
18	SLU 58	72	0	3062	0.01	3.31	0
18	SLU 59	72	0	3062	0.01	3.31	0
18	SLU 60	79	0	3279	0.01	3.65	0
18	SLU 61	79	0	3279	0.01	3.65	0
18	SLU 62	79	0	3279	0.01	3.65	0
18	SLU 63	79	0	3279	0.01	3.65	0
18	SLU 64	63	0	2843	0.01	2.88	0
18	SLU 65	63	0	2843	0.01	2.88	0
18	SLU 66	63	0	2843	0.01	2.88	0
18	SLU 67	63	0	2843	0.01	2.88	0
18	SLU 68	63	0	2843	0.01	2.88	0
18	SLU 69	63	0	2843	0.01	2.88	0
18	SLU 70	63	0	2843	0.01	2.88	0
18	SLU 71	63	0	2843	0.01	2.88	0
18	SLU 72	63	0	2843	0.01	2.88	0
18	SLU 73	80	0	3348	0.01	3.67	0
18	SLU 74	80	0	3348	0.01	3.67	0
18	SLU 75	80	0	3348	0.01	3.67	0
18	SLU 76	80	0	3348	0.01	3.67	0
18	SLU 77	80	0	3348	0.01	3.67	0
18	SLU 78	80	0	3348	0.01	3.67	0
18	SLU 79	80	0	3348	0.01	3.67	0
18	SLU 80	80	0	3348	0.01	3.67	0
18	SLU 81	87	0	3564	0.01	4.01	0
18	SLU 82	87	0	3564	0.01	4.01	0
18	SLU 83	87	0	3564	0.01	4.01	0
18	SLU 84	87	0	3564	0.01	4.01	0
18	SLE RA 1	47	0	2124	0	2.14	0
18	SLE RA 2	47	0	2124	0	2.14	0
18	SLE RA 3	47	0	2124	0	2.14	0
18	SLE RA 4	47	0	2124	0	2.14	0
18	SLE RA 5	47	0	2124	0	2.14	0
18	SLE RA 6	47	0	2124	0	2.14	0
18	SLE RA 7	47	0	2124	0	2.14	0
18	SLE RA 8	47	0	2124	0	2.14	0
18	SLE RA 9	47	0	2124	0	2.14	0
18	SLE RA 10	58	0	2461	0	2.66	0
18	SLE RA 11	58	0	2461	0	2.66	0
18	SLE RA 12	58	0	2461	0	2.66	0
18	SLE RA 13	58	0	2461	0	2.66	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
18	SLE RA 14	58	0	2461	0	2.66	0
18	SLE RA 15	58	0	2461	0	2.66	0
18	SLE RA 16	58	0	2461	0	2.66	0
18	SLE RA 17	58	0	2461	0	2.66	0
18	SLE RA 18	63	0	2605	0	2.89	0
18	SLE RA 19	63	0	2605	0	2.89	0
18	SLE RA 20	63	0	2605	0	2.89	0
18	SLE RA 21	63	0	2605	0	2.89	0
18	SLE FR 1	47	0	2124	0	2.14	0
18	SLE FR 2	47	0	2124	0	2.14	0
18	SLE FR 3	47	0	2124	0	2.14	0
18	SLE FR 4	51	0	2268	0	2.36	0
18	SLE FR 5	51	0	2268	0	2.36	0
18	SLE FR 6	55	0	2364	0	2.51	0
18	SLE QP 1	47	0	2124	0	2.14	0
18	SLE QP 2	51	0	2268	0	2.36	0
18	SLD 1	236	45	2357	-46.28	11.42	0.06
18	SLD 2	236	45	2357	-46.28	11.42	0.06
18	SLD 3	226	-32	2290	37.08	11	-0.05
18	SLD 4	226	-32	2290	37.08	11	-0.05
18	SLD 5	121	130	2396	-140.31	5.71	0.17
18	SLD 6	121	130	2396	-140.31	5.71	0.17
18	SLD 7	90	-126	2174	137.56	4.33	-0.17
18	SLD 8	90	-126	2174	137.56	4.33	-0.17
18	SLD 9	13	126	2363	-137.55	0.4	0.17
18	SLD 10	13	126	2363	-137.55	0.4	0.17
18	SLD 11	-18	-130	2140	140.32	-0.98	-0.17
18	SLD 12	-18	-130	2140	140.32	-0.98	-0.17
18	SLD 13	-124	32	2246	-37.07	-6.27	0.05
18	SLD 14	-124	32	2246	-37.07	-6.27	0.05
18	SLD 15	-133	-45	2179	46.29	-6.69	-0.06
18	SLD 16	-133	-45	2179	46.29	-6.69	-0.06
18	SLV 1	487	125	2491	-129.25	23.74	0.16
18	SLV 2	487	125	2491	-129.25	23.74	0.16
18	SLV 3	462	-92	2304	105.88	22.67	-0.14
18	SLV 4	462	-92	2304	105.88	22.67	-0.14
18	SLV 5	219	366	2620	-395.39	10.4	0.49
18	SLV 6	219	366	2620	-395.39	10.4	0.49
18	SLV 7	138	-356	1994	388.39	6.83	-0.48
18	SLV 8	138	-356	1994	388.39	6.83	-0.48
18	SLV 9	-35	356	2542	-388.38	-2.1	0.48
18	SLV 10	-35	356	2542	-388.38	-2.1	0.48
18	SLV 11	-116	-366	1917	395.4	-5.67	-0.49
18	SLV 12	-116	-366	1917	395.4	-5.67	-0.49
18	SLV 13	-360	92	2233	-105.87	-17.94	0.14
18	SLV 14	-360	92	2233	-105.87	-17.94	0.14
18	SLV 15	-384	-125	2045	129.26	-19.01	-0.16
18	SLV 16	-384	-125	2045	129.26	-19.01	-0.16
19	SLU 1	78	0	2009	0.01	3.56	0
19	SLU 2	78	0	2009	0.01	3.56	0
19	SLU 3	78	0	2009	0.01	3.56	0
19	SLU 4	78	0	2009	0.01	3.56	0
19	SLU 5	78	0	2009	0.01	3.56	0
19	SLU 6	78	0	2009	0.01	3.56	0
19	SLU 7	78	0	2009	0.01	3.56	0
19	SLU 8	78	0	2009	0.01	3.56	0
19	SLU 9	78	0	2009	0.01	3.56	0
19	SLU 10	107	0	2503	0.01	4.86	0
19	SLU 11	107	0	2503	0.01	4.86	0
19	SLU 12	107	0	2503	0.01	4.86	0
19	SLU 13	107	0	2503	0.01	4.86	0
19	SLU 14	107	0	2503	0.01	4.86	0
19	SLU 15	107	0	2503	0.01	4.86	0
19	SLU 16	107	0	2503	0.01	4.86	0
19	SLU 17	107	0	2503	0.01	4.86	0
19	SLU 18	119	0	2715	0.01	5.41	0
19	SLU 19	119	0	2715	0.01	5.41	0
19	SLU 20	119	0	2715	0.01	5.41	0
19	SLU 21	119	0	2715	0.01	5.41	0
19	SLU 22	91	0	2290	0.01	4.15	0
19	SLU 23	91	0	2290	0.01	4.15	0
19	SLU 24	91	0	2290	0.01	4.15	0
19	SLU 25	91	0	2290	0.01	4.15	0
19	SLU 26	91	0	2290	0.01	4.15	0
19	SLU 27	91	0	2290	0.01	4.15	0
19	SLU 28	91	0	2290	0.01	4.15	0
19	SLU 29	91	0	2290	0.01	4.15	0
19	SLU 30	91	0	2290	0.01	4.15	0
19	SLU 31	120	0	2783	0.01	5.45	0
19	SLU 32	120	0	2783	0.01	5.45	0
19	SLU 33	120	0	2783	0.01	5.45	0
19	SLU 34	120	0	2783	0.01	5.45	0
19	SLU 35	120	0	2783	0.01	5.45	0
19	SLU 36	120	0	2783	0.01	5.45	0
19	SLU 37	120	0	2783	0.01	5.45	0
19	SLU 38	120	0	2783	0.01	5.45	0
19	SLU 39	132	0	2995	0.01	6.01	0
19	SLU 40	132	0	2995	0.01	6.01	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
19	SLU 41	132	0	2995	0.01	6.01	0
19	SLU 42	132	0	2995	0.01	6.01	0
19	SLU 43	97	0	2516	0.01	4.42	0
19	SLU 44	97	0	2516	0.01	4.42	0
19	SLU 45	97	0	2516	0.01	4.42	0
19	SLU 46	97	0	2516	0.01	4.42	0
19	SLU 47	97	0	2516	0.01	4.42	0
19	SLU 48	97	0	2516	0.01	4.42	0
19	SLU 49	97	0	2516	0.01	4.42	0
19	SLU 50	97	0	2516	0.01	4.42	0
19	SLU 51	97	0	2516	0.01	4.42	0
19	SLU 52	125	0	3010	0.01	5.72	0
19	SLU 53	125	0	3010	0.01	5.72	0
19	SLU 54	125	0	3010	0.01	5.72	0
19	SLU 55	125	0	3010	0.01	5.72	0
19	SLU 56	125	0	3010	0.01	5.72	0
19	SLU 57	125	0	3010	0.01	5.72	0
19	SLU 58	125	0	3010	0.01	5.72	0
19	SLU 59	125	0	3010	0.01	5.72	0
19	SLU 60	138	0	3221	0.01	6.28	0
19	SLU 61	138	0	3221	0.01	6.28	0
19	SLU 62	138	0	3221	0.01	6.28	0
19	SLU 63	138	0	3221	0.01	6.28	0
19	SLU 64	110	0	2796	0.01	5.01	0
19	SLU 65	110	0	2796	0.01	5.01	0
19	SLU 66	110	0	2796	0.01	5.01	0
19	SLU 67	110	0	2796	0.01	5.01	0
19	SLU 68	110	0	2796	0.01	5.01	0
19	SLU 69	110	0	2796	0.01	5.01	0
19	SLU 70	110	0	2796	0.01	5.01	0
19	SLU 71	110	0	2796	0.01	5.01	0
19	SLU 72	110	0	2796	0.01	5.01	0
19	SLU 73	138	0	3290	0.02	6.31	0
19	SLU 74	138	0	3290	0.02	6.31	0
19	SLU 75	138	0	3290	0.02	6.31	0
19	SLU 76	138	0	3290	0.02	6.31	0
19	SLU 77	138	0	3290	0.02	6.31	0
19	SLU 78	138	0	3290	0.02	6.31	0
19	SLU 79	138	0	3290	0.02	6.31	0
19	SLU 80	138	0	3290	0.02	6.31	0
19	SLU 81	151	0	3502	0.02	6.87	0
19	SLU 82	151	0	3502	0.02	6.87	0
19	SLU 83	151	0	3502	0.02	6.87	0
19	SLU 84	151	0	3502	0.02	6.87	0
19	SLE RA 1	82	0	2089	0.01	3.73	0
19	SLE RA 2	82	0	2089	0.01	3.73	0
19	SLE RA 3	82	0	2089	0.01	3.73	0
19	SLE RA 4	82	0	2089	0.01	3.73	0
19	SLE RA 5	82	0	2089	0.01	3.73	0
19	SLE RA 6	82	0	2089	0.01	3.73	0
19	SLE RA 7	82	0	2089	0.01	3.73	0
19	SLE RA 8	82	0	2089	0.01	3.73	0
19	SLE RA 9	82	0	2089	0.01	3.73	0
19	SLE RA 10	101	0	2419	0.01	4.59	0
19	SLE RA 11	101	0	2419	0.01	4.59	0
19	SLE RA 12	101	0	2419	0.01	4.59	0
19	SLE RA 13	101	0	2419	0.01	4.59	0
19	SLE RA 14	101	0	2419	0.01	4.59	0
19	SLE RA 15	101	0	2419	0.01	4.59	0
19	SLE RA 16	101	0	2419	0.01	4.59	0
19	SLE RA 17	101	0	2419	0.01	4.59	0
19	SLE RA 18	109	0	2560	0.01	4.96	0
19	SLE RA 19	109	0	2560	0.01	4.96	0
19	SLE RA 20	109	0	2560	0.01	4.96	0
19	SLE RA 21	109	0	2560	0.01	4.96	0
19	SLE FR 1	82	0	2089	0.01	3.73	0
19	SLE FR 2	82	0	2089	0.01	3.73	0
19	SLE FR 3	82	0	2089	0.01	3.73	0
19	SLE FR 4	90	0	2231	0.01	4.1	0
19	SLE FR 5	90	0	2231	0.01	4.1	0
19	SLE FR 6	95	0	2325	0.01	4.35	0
19	SLE QP 1	82	0	2089	0.01	3.73	0
19	SLE QP 2	90	0	2231	0.01	4.1	0
19	SLD 1	276	40	2356	-46.58	13.32	0.06
19	SLD 2	276	40	2356	-46.58	13.32	0.06
19	SLD 3	262	-20	2297	29.56	12.64	-0.04
19	SLD 4	262	-20	2297	29.56	12.64	-0.04
19	SLD 5	167	103	2357	-129.43	7.9	0.17
19	SLD 6	167	103	2357	-129.43	7.9	0.17
19	SLD 7	121	-97	2161	124.34	5.63	-0.17
19	SLD 8	121	-97	2161	124.34	5.63	-0.17
19	SLD 9	59	97	2300	-124.32	2.57	0.16
19	SLD 10	59	97	2300	-124.32	2.57	0.16
19	SLD 11	13	-104	2104	129.46	0.3	-0.17
19	SLD 12	13	-104	2104	129.46	0.3	-0.17
19	SLD 13	-83	20	2164	-29.54	-4.45	0.04
19	SLD 14	-83	20	2164	-29.54	-4.45	0.04
19	SLD 15	-97	-40	2105	46.6	-5.13	-0.06



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
19	SLD 16	-97	-40	2105	46.6	-5.13	-0.06
19	SLV 1	532	110	2537	-128.92	25.96	0.18
19	SLV 2	532	110	2537	-128.92	25.96	0.18
19	SLV 3	494	-59	2372	85.66	24.1	-0.11
19	SLV 4	494	-59	2372	85.66	24.1	-0.11
19	SLV 5	280	290	2573	-364.12	13.47	0.49
19	SLV 6	280	290	2573	-364.12	13.47	0.49
19	SLV 7	154	-275	2023	351.15	7.28	-0.47
19	SLV 8	154	-275	2023	351.15	7.28	-0.47
19	SLV 9	26	275	2438	-351.13	0.91	0.47
19	SLV 10	26	275	2438	-351.13	0.91	0.47
19	SLV 11	-100	-291	1888	364.14	-5.28	-0.49
19	SLV 12	-100	-291	1888	364.14	-5.28	-0.49
19	SLV 13	-314	59	2089	-85.64	-15.91	0.11
19	SLV 14	-314	59	2089	-85.64	-15.91	0.11
19	SLV 15	-352	-110	1924	128.94	-17.76	-0.18
19	SLV 16	-352	-110	1924	128.94	-17.76	-0.18
20	SLU 1	103	0	1966	0.01	4.88	0
20	SLU 2	103	0	1966	0.01	4.88	0
20	SLU 3	103	0	1966	0.01	4.88	0
20	SLU 4	103	0	1966	0.01	4.88	0
20	SLU 5	103	0	1966	0.01	4.88	0
20	SLU 6	103	0	1966	0.01	4.88	0
20	SLU 7	103	0	1966	0.01	4.88	0
20	SLU 8	103	0	1966	0.01	4.88	0
20	SLU 9	103	0	1966	0.01	4.88	0
20	SLU 10	141	0	2445	0.01	6.72	0
20	SLU 11	141	0	2445	0.01	6.72	0
20	SLU 12	141	0	2445	0.01	6.72	0
20	SLU 13	141	0	2445	0.01	6.72	0
20	SLU 14	141	0	2445	0.01	6.72	0
20	SLU 15	141	0	2445	0.01	6.72	0
20	SLU 16	141	0	2445	0.01	6.72	0
20	SLU 17	141	0	2445	0.01	6.72	0
20	SLU 18	157	0	2650	0.01	7.51	0
20	SLU 19	157	0	2650	0.01	7.51	0
20	SLU 20	157	0	2650	0.01	7.51	0
20	SLU 21	157	0	2650	0.01	7.51	0
20	SLU 22	120	0	2240	0.01	5.72	0
20	SLU 23	120	0	2240	0.01	5.72	0
20	SLU 24	120	0	2240	0.01	5.72	0
20	SLU 25	120	0	2240	0.01	5.72	0
20	SLU 26	120	0	2240	0.01	5.72	0
20	SLU 27	120	0	2240	0.01	5.72	0
20	SLU 28	120	0	2240	0.01	5.72	0
20	SLU 29	120	0	2240	0.01	5.72	0
20	SLU 30	120	0	2240	0.01	5.72	0
20	SLU 31	158	0	2719	0.01	7.57	0
20	SLU 32	158	0	2719	0.01	7.57	0
20	SLU 33	158	0	2719	0.01	7.57	0
20	SLU 34	158	0	2719	0.01	7.57	0
20	SLU 35	158	0	2719	0.01	7.57	0
20	SLU 36	158	0	2719	0.01	7.57	0
20	SLU 37	158	0	2719	0.01	7.57	0
20	SLU 38	158	0	2719	0.01	7.57	0
20	SLU 39	174	0	2924	0.01	8.36	0
20	SLU 40	174	0	2924	0.01	8.36	0
20	SLU 41	174	0	2924	0.01	8.36	0
20	SLU 42	174	0	2924	0.01	8.36	0
20	SLU 43	128	0	2461	0.01	6.05	0
20	SLU 44	128	0	2461	0.01	6.05	0
20	SLU 45	128	0	2461	0.01	6.05	0
20	SLU 46	128	0	2461	0.01	6.05	0
20	SLU 47	128	0	2461	0.01	6.05	0
20	SLU 48	128	0	2461	0.01	6.05	0
20	SLU 49	128	0	2461	0.01	6.05	0
20	SLU 50	128	0	2461	0.01	6.05	0
20	SLU 51	128	0	2461	0.01	6.05	0
20	SLU 52	166	0	2940	0.01	7.9	0
20	SLU 53	166	0	2940	0.01	7.9	0
20	SLU 54	166	0	2940	0.01	7.9	0
20	SLU 55	166	0	2940	0.01	7.9	0
20	SLU 56	166	0	2940	0.01	7.9	0
20	SLU 57	166	0	2940	0.01	7.9	0
20	SLU 58	166	0	2940	0.01	7.9	0
20	SLU 59	166	0	2940	0.01	7.9	0
20	SLU 60	182	0	3146	0.02	8.69	0
20	SLU 61	182	0	3146	0.02	8.69	0
20	SLU 62	182	0	3146	0.02	8.69	0
20	SLU 63	182	0	3146	0.02	8.69	0
20	SLU 64	145	0	2735	0.01	6.9	0
20	SLU 65	145	0	2735	0.01	6.9	0
20	SLU 66	145	0	2735	0.01	6.9	0
20	SLU 67	145	0	2735	0.01	6.9	0
20	SLU 68	145	0	2735	0.01	6.9	0
20	SLU 69	145	0	2735	0.01	6.9	0
20	SLU 70	145	0	2735	0.01	6.9	0
20	SLU 71	145	0	2735	0.01	6.9	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
20	SLU 72	145	0	2735	0.01	6.9	0
20	SLU 73	183	0	3214	0.02	8.74	0
20	SLU 74	183	0	3214	0.02	8.74	0
20	SLU 75	183	0	3214	0.02	8.74	0
20	SLU 76	183	0	3214	0.02	8.74	0
20	SLU 77	183	0	3214	0.02	8.74	0
20	SLU 78	183	0	3214	0.02	8.74	0
20	SLU 79	183	0	3214	0.02	8.74	0
20	SLU 80	183	0	3214	0.02	8.74	0
20	SLU 81	199	0	3420	0.02	9.53	0
20	SLU 82	199	0	3420	0.02	9.53	0
20	SLU 83	199	0	3420	0.02	9.53	0
20	SLU 84	199	0	3420	0.02	9.53	0
20	SLE RA 1	108	0	2044	0.01	5.12	0
20	SLE RA 2	108	0	2044	0.01	5.12	0
20	SLE RA 3	108	0	2044	0.01	5.12	0
20	SLE RA 4	108	0	2044	0.01	5.12	0
20	SLE RA 5	108	0	2044	0.01	5.12	0
20	SLE RA 6	108	0	2044	0.01	5.12	0
20	SLE RA 7	108	0	2044	0.01	5.12	0
20	SLE RA 8	108	0	2044	0.01	5.12	0
20	SLE RA 9	108	0	2044	0.01	5.12	0
20	SLE RA 10	133	0	2363	0.01	6.35	0
20	SLE RA 11	133	0	2363	0.01	6.35	0
20	SLE RA 12	133	0	2363	0.01	6.35	0
20	SLE RA 13	133	0	2363	0.01	6.35	0
20	SLE RA 14	133	0	2363	0.01	6.35	0
20	SLE RA 15	133	0	2363	0.01	6.35	0
20	SLE RA 16	133	0	2363	0.01	6.35	0
20	SLE RA 17	133	0	2363	0.01	6.35	0
20	SLE RA 18	144	0	2500	0.01	6.88	0
20	SLE RA 19	144	0	2500	0.01	6.88	0
20	SLE RA 20	144	0	2500	0.01	6.88	0
20	SLE RA 21	144	0	2500	0.01	6.88	0
20	SLE FR 1	108	0	2044	0.01	5.12	0
20	SLE FR 2	108	0	2044	0.01	5.12	0
20	SLE FR 3	108	0	2044	0.01	5.12	0
20	SLE FR 4	119	0	2181	0.01	5.65	0
20	SLE FR 5	119	0	2181	0.01	5.65	0
20	SLE FR 6	126	0	2272	0.01	6	0
20	SLE QP 1	108	0	2044	0.01	5.12	0
20	SLE QP 2	119	0	2181	0.01	5.65	0
20	SLD 1	309	36	2322	-45.45	15.06	0.09
20	SLD 2	309	36	2322	-45.45	15.06	0.09
20	SLD 3	293	-11	2273	22.17	14.39	-0.03
20	SLD 4	293	-11	2273	22.17	14.39	-0.03
20	SLD 5	199	82	2298	-116.19	9.48	0.2
20	SLD 6	199	82	2298	-116.19	9.48	0.2
20	SLD 7	147	-75	2133	109.22	7.26	-0.19
20	SLD 8	147	-75	2133	109.22	7.26	-0.19
20	SLD 9	90	75	2228	-109.2	4.04	0.19
20	SLD 10	90	75	2228	-109.2	4.04	0.19
20	SLD 11	38	-83	2063	116.21	1.81	-0.21
20	SLD 12	38	-83	2063	116.21	1.81	-0.21
20	SLD 13	-56	11	2089	-22.15	-3.09	0.03
20	SLD 14	-56	11	2089	-22.15	-3.09	0.03
20	SLD 15	-72	-36	2039	45.48	-3.76	-0.09
20	SLD 16	-72	-36	2039	45.48	-3.76	-0.09
20	SLV 1	569	98	2523	-124.79	27.92	0.23
20	SLV 2	569	98	2523	-124.79	27.92	0.23
20	SLV 3	527	-35	2384	65.5	26.11	-0.1
20	SLV 4	527	-35	2384	65.5	26.11	-0.1
20	SLV 5	319	231	2494	-326.04	15.09	0.58
20	SLV 6	319	231	2494	-326.04	15.09	0.58
20	SLV 7	176	-212	2032	308.26	9.03	-0.54
20	SLV 8	176	-212	2032	308.26	9.03	-0.54
20	SLV 9	61	212	2330	-308.24	2.26	0.54
20	SLV 10	61	212	2330	-308.24	2.26	0.54
20	SLV 11	-82	-231	1868	326.06	-3.79	-0.58
20	SLV 12	-82	-231	1868	326.06	-3.79	-0.58
20	SLV 13	-289	35	1977	-65.48	-14.81	0.1
20	SLV 14	-289	35	1977	-65.48	-14.81	0.1
20	SLV 15	-332	-98	1839	124.81	-16.63	-0.23
20	SLV 16	-332	-98	1839	124.81	-16.63	-0.23
21	SLU 1	114	0	1921	0	5.35	0
21	SLU 2	114	0	1921	0	5.35	0
21	SLU 3	114	0	1921	0	5.35	0
21	SLU 4	114	0	1921	0	5.35	0
21	SLU 5	114	0	1921	0	5.35	0
21	SLU 6	114	0	1921	0	5.35	0
21	SLU 7	114	0	1921	0	5.35	0
21	SLU 8	114	0	1921	0	5.35	0
21	SLU 9	114	0	1921	0	5.35	0
21	SLU 10	155	0	2387	0	7.26	0
21	SLU 11	155	0	2387	0	7.26	0
21	SLU 12	155	0	2387	0	7.26	0
21	SLU 13	155	0	2387	0	7.26	0
21	SLU 14	155	0	2387	0	7.26	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
21	SLU 15	155	0	2387	0	7.26	0
21	SLU 16	155	0	2387	0	7.26	0
21	SLU 17	155	0	2387	0	7.26	0
21	SLU 18	173	0	2586	0	8.08	0
21	SLU 19	173	0	2586	0	8.08	0
21	SLU 20	173	0	2586	0	8.08	0
21	SLU 21	173	0	2586	0	8.08	0
21	SLU 22	133	0	2189	0	6.25	0
21	SLU 23	133	0	2189	0	6.25	0
21	SLU 24	133	0	2189	0	6.25	0
21	SLU 25	133	0	2189	0	6.25	0
21	SLU 26	133	0	2189	0	6.25	0
21	SLU 27	133	0	2189	0	6.25	0
21	SLU 28	133	0	2189	0	6.25	0
21	SLU 29	133	0	2189	0	6.25	0
21	SLU 30	133	0	2189	0	6.25	0
21	SLU 31	174	0	2655	0	8.17	0
21	SLU 32	174	0	2655	0	8.17	0
21	SLU 33	174	0	2655	0	8.17	0
21	SLU 34	174	0	2655	0	8.17	0
21	SLU 35	174	0	2655	0	8.17	0
21	SLU 36	174	0	2655	0	8.17	0
21	SLU 37	174	0	2655	0	8.17	0
21	SLU 38	174	0	2655	0	8.17	0
21	SLU 39	192	0	2854	0	8.99	0
21	SLU 40	192	0	2854	0	8.99	0
21	SLU 41	192	0	2854	0	8.99	0
21	SLU 42	192	0	2854	0	8.99	0
21	SLU 43	141	0	2406	0	6.64	0
21	SLU 44	141	0	2406	0	6.64	0
21	SLU 45	141	0	2406	0	6.64	0
21	SLU 46	141	0	2406	0	6.64	0
21	SLU 47	141	0	2406	0	6.64	0
21	SLU 48	141	0	2406	0	6.64	0
21	SLU 49	141	0	2406	0	6.64	0
21	SLU 50	141	0	2406	0	6.64	0
21	SLU 51	141	0	2406	0	6.64	0
21	SLU 52	182	0	2872	0	8.55	0
21	SLU 53	182	0	2872	0	8.55	0
21	SLU 54	182	0	2872	0	8.55	0
21	SLU 55	182	0	2872	0	8.55	0
21	SLU 56	182	0	2872	0	8.55	0
21	SLU 57	182	0	2872	0	8.55	0
21	SLU 58	182	0	2872	0	8.55	0
21	SLU 59	182	0	2872	0	8.55	0
21	SLU 60	200	0	3071	0	9.37	0
21	SLU 61	200	0	3071	0	9.37	0
21	SLU 62	200	0	3071	0	9.37	0
21	SLU 63	200	0	3071	0	9.37	0
21	SLU 64	160	0	2674	0	7.55	0
21	SLU 65	160	0	2674	0	7.55	0
21	SLU 66	160	0	2674	0	7.55	0
21	SLU 67	160	0	2674	0	7.55	0
21	SLU 68	160	0	2674	0	7.55	0
21	SLU 69	160	0	2674	0	7.55	0
21	SLU 70	160	0	2674	0	7.55	0
21	SLU 71	160	0	2674	0	7.55	0
21	SLU 72	160	0	2674	0	7.55	0
21	SLU 73	202	0	3140	0	9.46	0
21	SLU 74	202	0	3140	0	9.46	0
21	SLU 75	202	0	3140	0	9.46	0
21	SLU 76	202	0	3140	0	9.46	0
21	SLU 77	202	0	3140	0	9.46	0
21	SLU 78	202	0	3140	0	9.46	0
21	SLU 79	202	0	3140	0	9.46	0
21	SLU 80	202	0	3140	0	9.46	0
21	SLU 81	219	0	3339	0	10.28	0
21	SLU 82	219	0	3339	0	10.28	0
21	SLU 83	219	0	3339	0	10.28	0
21	SLU 84	219	0	3339	0	10.28	0
21	SLE RA 1	119	0	1998	0	5.61	0
21	SLE RA 2	119	0	1998	0	5.61	0
21	SLE RA 3	119	0	1998	0	5.61	0
21	SLE RA 4	119	0	1998	0	5.61	0
21	SLE RA 5	119	0	1998	0	5.61	0
21	SLE RA 6	119	0	1998	0	5.61	0
21	SLE RA 7	119	0	1998	0	5.61	0
21	SLE RA 8	119	0	1998	0	5.61	0
21	SLE RA 9	119	0	1998	0	5.61	0
21	SLE RA 10	147	0	2308	0	6.88	0
21	SLE RA 11	147	0	2308	0	6.88	0
21	SLE RA 12	147	0	2308	0	6.88	0
21	SLE RA 13	147	0	2308	0	6.88	0
21	SLE RA 14	147	0	2308	0	6.88	0
21	SLE RA 15	147	0	2308	0	6.88	0
21	SLE RA 16	147	0	2308	0	6.88	0
21	SLE RA 17	147	0	2308	0	6.88	0
21	SLE RA 18	158	0	2441	0	7.43	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
21	SLE RA 19	158	0	2441	0	7.43	0
21	SLE RA 20	158	0	2441	0	7.43	0
21	SLE RA 21	158	0	2441	0	7.43	0
21	SLE FR 1	119	0	1998	0	5.61	0
21	SLE FR 2	119	0	1998	0	5.61	0
21	SLE FR 3	119	0	1998	0	5.61	0
21	SLE FR 4	131	0	2131	0	6.15	0
21	SLE FR 5	131	0	2131	0	6.15	0
21	SLE FR 6	139	0	2220	0	6.52	0
21	SLE QP 1	119	0	1998	0	5.61	0
21	SLE QP 2	131	0	2131	0	6.15	0
21	SLD 1	328	32	2264	-43.5	15.96	0.1
21	SLD 2	328	32	2264	-43.5	15.96	0.1
21	SLD 3	310	-4	2224	15.54	15.07	-0.02
21	SLD 4	310	-4	2224	15.54	15.07	-0.02
21	SLD 5	217	65	2231	-102.6	10.44	0.21
21	SLD 6	217	65	2231	-102.6	10.44	0.21
21	SLD 7	158	-57	2099	94.21	7.48	-0.19
21	SLD 8	158	-57	2099	94.21	7.48	-0.19
21	SLD 9	104	56	2163	-94.21	4.82	0.19
21	SLD 10	104	56	2163	-94.21	4.82	0.19
21	SLD 11	45	-65	2031	102.6	1.87	-0.21
21	SLD 12	45	-65	2031	102.6	1.87	-0.21
21	SLD 13	-48	4	2038	-15.54	-2.77	0.02
21	SLD 14	-48	4	2038	-15.54	-2.77	0.02
21	SLD 15	-66	-32	1998	43.51	-3.66	-0.1
21	SLD 16	-66	-32	1998	43.51	-3.66	-0.1
21	SLV 1	598	86	2450	-118.47	29.41	0.27
21	SLV 2	598	86	2450	-118.47	29.41	0.27
21	SLV 3	549	-16	2340	47.13	26.97	-0.07
21	SLV 4	549	-16	2340	47.13	26.97	-0.07
21	SLV 5	345	180	2394	-286.71	16.83	0.59
21	SLV 6	345	180	2394	-286.71	16.83	0.59
21	SLV 7	183	-159	2026	265.31	8.69	-0.53
21	SLV 8	183	-159	2026	265.31	8.69	-0.53
21	SLV 9	79	159	2236	-265.3	3.61	0.53
21	SLV 10	79	159	2236	-265.3	3.61	0.53
21	SLV 11	-83	-180	1868	286.71	-4.53	-0.59
21	SLV 12	-83	-180	1868	286.71	-4.53	-0.59
21	SLV 13	-287	16	1922	-47.13	-14.67	0.07
21	SLV 14	-287	16	1922	-47.13	-14.67	0.07
21	SLV 15	-336	-86	1812	118.48	-17.11	-0.27
21	SLV 16	-336	-86	1812	118.48	-17.11	-0.27
22	SLU 1	119	0	1886	-0.01	5.89	0
22	SLU 2	119	0	1886	-0.01	5.89	0
22	SLU 3	119	0	1886	-0.01	5.89	0
22	SLU 4	119	0	1886	-0.01	5.89	0
22	SLU 5	119	0	1886	-0.01	5.89	0
22	SLU 6	119	0	1886	-0.01	5.89	0
22	SLU 7	119	0	1886	-0.01	5.89	0
22	SLU 8	119	0	1886	-0.01	5.89	0
22	SLU 9	119	0	1886	-0.01	5.89	0
22	SLU 10	164	0	2342	-0.01	8.17	0
22	SLU 11	164	0	2342	-0.01	8.17	0
22	SLU 12	164	0	2342	-0.01	8.17	0
22	SLU 13	164	0	2342	-0.01	8.17	0
22	SLU 14	164	0	2342	-0.01	8.17	0
22	SLU 15	164	0	2342	-0.01	8.17	0
22	SLU 16	164	0	2342	-0.01	8.17	0
22	SLU 17	164	0	2342	-0.01	8.17	0
22	SLU 18	183	0	2537	-0.01	9.15	0
22	SLU 19	183	0	2537	-0.01	9.15	0
22	SLU 20	183	0	2537	-0.01	9.15	0
22	SLU 21	183	0	2537	-0.01	9.15	0
22	SLU 22	141	0	2150	-0.01	6.98	0
22	SLU 23	141	0	2150	-0.01	6.98	0
22	SLU 24	141	0	2150	-0.01	6.98	0
22	SLU 25	141	0	2150	-0.01	6.98	0
22	SLU 26	141	0	2150	-0.01	6.98	0
22	SLU 27	141	0	2150	-0.01	6.98	0
22	SLU 28	141	0	2150	-0.01	6.98	0
22	SLU 29	141	0	2150	-0.01	6.98	0
22	SLU 30	141	0	2150	-0.01	6.98	0
22	SLU 31	185	0	2606	-0.01	9.26	0
22	SLU 32	185	0	2606	-0.01	9.26	0
22	SLU 33	185	0	2606	-0.01	9.26	0
22	SLU 34	185	0	2606	-0.01	9.26	0
22	SLU 35	185	0	2606	-0.01	9.26	0
22	SLU 36	185	0	2606	-0.01	9.26	0
22	SLU 37	185	0	2606	-0.01	9.26	0
22	SLU 38	185	0	2606	-0.01	9.26	0
22	SLU 39	204	0	2801	-0.01	10.24	0
22	SLU 40	204	0	2801	-0.01	10.24	0
22	SLU 41	204	0	2801	-0.01	10.24	0
22	SLU 42	204	0	2801	-0.01	10.24	0
22	SLU 43	148	0	2362	-0.01	7.29	0
22	SLU 44	148	0	2362	-0.01	7.29	0
22	SLU 45	148	0	2362	-0.01	7.29	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
22	SLU 46	148	0	2362	-0.01	7.29	0
22	SLU 47	148	0	2362	-0.01	7.29	0
22	SLU 48	148	0	2362	-0.01	7.29	0
22	SLU 49	148	0	2362	-0.01	7.29	0
22	SLU 50	148	0	2362	-0.01	7.29	0
22	SLU 51	148	0	2362	-0.01	7.29	0
22	SLU 52	192	0	2818	-0.01	9.56	0
22	SLU 53	192	0	2818	-0.01	9.56	0
22	SLU 54	192	0	2818	-0.01	9.56	0
22	SLU 55	192	0	2818	-0.01	9.56	0
22	SLU 56	192	0	2818	-0.01	9.56	0
22	SLU 57	192	0	2818	-0.01	9.56	0
22	SLU 58	192	0	2818	-0.01	9.56	0
22	SLU 59	192	0	2818	-0.01	9.56	0
22	SLU 60	211	0	3013	-0.02	10.54	0
22	SLU 61	211	0	3013	-0.02	10.54	0
22	SLU 62	211	0	3013	-0.02	10.54	0
22	SLU 63	211	0	3013	-0.02	10.54	0
22	SLU 64	169	0	2626	-0.01	8.38	0
22	SLU 65	169	0	2626	-0.01	8.38	0
22	SLU 66	169	0	2626	-0.01	8.38	0
22	SLU 67	169	0	2626	-0.01	8.38	0
22	SLU 68	169	0	2626	-0.01	8.38	0
22	SLU 69	169	0	2626	-0.01	8.38	0
22	SLU 70	169	0	2626	-0.01	8.38	0
22	SLU 71	169	0	2626	-0.01	8.38	0
22	SLU 72	169	0	2626	-0.01	8.38	0
22	SLU 73	214	0	3081	-0.02	10.66	0
22	SLU 74	214	0	3081	-0.02	10.66	0
22	SLU 75	214	0	3081	-0.02	10.66	0
22	SLU 76	214	0	3081	-0.02	10.66	0
22	SLU 77	214	0	3081	-0.02	10.66	0
22	SLU 78	214	0	3081	-0.02	10.66	0
22	SLU 79	214	0	3081	-0.02	10.66	0
22	SLU 80	214	0	3081	-0.02	10.66	0
22	SLU 81	233	0	3277	-0.02	11.63	0
22	SLU 82	233	0	3277	-0.02	11.63	0
22	SLU 83	233	0	3277	-0.02	11.63	0
22	SLU 84	233	0	3277	-0.02	11.63	0
22	SLE RA 1	125	0	1962	-0.01	6.2	0
22	SLE RA 2	125	0	1962	-0.01	6.2	0
22	SLE RA 3	125	0	1962	-0.01	6.2	0
22	SLE RA 4	125	0	1962	-0.01	6.2	0
22	SLE RA 5	125	0	1962	-0.01	6.2	0
22	SLE RA 6	125	0	1962	-0.01	6.2	0
22	SLE RA 7	125	0	1962	-0.01	6.2	0
22	SLE RA 8	125	0	1962	-0.01	6.2	0
22	SLE RA 9	125	0	1962	-0.01	6.2	0
22	SLE RA 10	155	0	2266	-0.01	7.72	0
22	SLE RA 11	155	0	2266	-0.01	7.72	0
22	SLE RA 12	155	0	2266	-0.01	7.72	0
22	SLE RA 13	155	0	2266	-0.01	7.72	0
22	SLE RA 14	155	0	2266	-0.01	7.72	0
22	SLE RA 15	155	0	2266	-0.01	7.72	0
22	SLE RA 16	155	0	2266	-0.01	7.72	0
22	SLE RA 17	155	0	2266	-0.01	7.72	0
22	SLE RA 18	168	0	2396	-0.01	8.37	0
22	SLE RA 19	168	0	2396	-0.01	8.37	0
22	SLE RA 20	168	0	2396	-0.01	8.37	0
22	SLE RA 21	168	0	2396	-0.01	8.37	0
22	SLE FR 1	125	0	1962	-0.01	6.2	0
22	SLE FR 2	125	0	1962	-0.01	6.2	0
22	SLE FR 3	125	0	1962	-0.01	6.2	0
22	SLE FR 4	138	0	2092	-0.01	6.85	0
22	SLE FR 5	138	0	2092	-0.01	6.85	0
22	SLE FR 6	147	0	2179	-0.01	7.29	0
22	SLE QP 1	125	0	1962	-0.01	6.2	0
22	SLE QP 2	138	0	2092	-0.01	6.85	0
22	SLD 1	339	29	2198	-41.18	16.86	0.11
22	SLD 2	339	29	2198	-41.18	16.86	0.11
22	SLD 3	323	0	2167	10.07	16.16	-0.01
22	SLD 4	323	0	2167	10.07	16.16	-0.01
22	SLD 5	223	52	2170	-90.09	10.92	0.2
22	SLD 6	223	52	2170	-90.09	10.92	0.2
22	SLD 7	169	-44	2068	80.74	8.58	-0.17
22	SLD 8	169	-44	2068	80.74	8.58	-0.17
22	SLD 9	107	43	2116	-80.77	5.13	0.17
22	SLD 10	107	43	2116	-80.77	5.13	0.17
22	SLD 11	54	-52	2014	90.07	2.79	-0.2
22	SLD 12	54	-52	2014	90.07	2.79	-0.2
22	SLD 13	-47	0	2017	-10.09	-2.45	0.01
22	SLD 14	-47	0	2017	-10.09	-2.45	0.01
22	SLD 15	-63	-29	1986	41.16	-3.15	-0.11
22	SLD 16	-63	-29	1986	41.16	-3.15	-0.11
22	SLV 1	614	77	2345	-111.21	30.52	0.29
22	SLV 2	614	77	2345	-111.21	30.52	0.29
22	SLV 3	570	-3	2260	31.7	28.62	-0.03
22	SLV 4	570	-3	2260	31.7	28.62	-0.03



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
22	SLV 5	347	143	2297	-250.11	16.84	0.56
22	SLV 6	347	143	2297	-250.11	16.84	0.56
22	SLV 7	201	-121	2014	226.24	10.5	-0.48
22	SLV 8	201	-121	2014	226.24	10.5	-0.48
22	SLV 9	75	121	2170	-226.27	3.21	0.48
22	SLV 10	75	121	2170	-226.27	3.21	0.48
22	SLV 11	-71	-143	1887	250.09	-3.13	-0.56
22	SLV 12	-71	-143	1887	250.09	-3.13	-0.56
22	SLV 13	-294	3	1923	-31.72	-14.91	0.03
22	SLV 14	-294	3	1923	-31.72	-14.91	0.03
22	SLV 15	-338	-77	1839	111.18	-16.81	-0.29
22	SLV 16	-338	-77	1839	111.18	-16.81	-0.29
23	SLU 1	124	0	1864	-0.02	6.12	0
23	SLU 2	124	0	1864	-0.02	6.12	0
23	SLU 3	124	0	1864	-0.02	6.12	0
23	SLU 4	124	0	1864	-0.02	6.12	0
23	SLU 5	124	0	1864	-0.02	6.12	0
23	SLU 6	124	0	1864	-0.02	6.12	0
23	SLU 7	124	0	1864	-0.02	6.12	0
23	SLU 8	124	0	1864	-0.02	6.12	0
23	SLU 9	124	0	1864	-0.02	6.12	0
23	SLU 10	171	0	2315	-0.03	8.39	0
23	SLU 11	171	0	2315	-0.03	8.39	0
23	SLU 12	171	0	2315	-0.03	8.39	0
23	SLU 13	171	0	2315	-0.03	8.39	0
23	SLU 14	171	0	2315	-0.03	8.39	0
23	SLU 15	171	0	2315	-0.03	8.39	0
23	SLU 16	171	0	2315	-0.03	8.39	0
23	SLU 17	171	0	2315	-0.03	8.39	0
23	SLU 18	191	0	2508	-0.03	9.37	0
23	SLU 19	191	0	2508	-0.03	9.37	0
23	SLU 20	191	0	2508	-0.03	9.37	0
23	SLU 21	191	0	2508	-0.03	9.37	0
23	SLU 22	148	0	2125	-0.03	7.28	0
23	SLU 23	148	0	2125	-0.03	7.28	0
23	SLU 24	148	0	2125	-0.03	7.28	0
23	SLU 25	148	0	2125	-0.03	7.28	0
23	SLU 26	148	0	2125	-0.03	7.28	0
23	SLU 27	148	0	2125	-0.03	7.28	0
23	SLU 28	148	0	2125	-0.03	7.28	0
23	SLU 29	148	0	2125	-0.03	7.28	0
23	SLU 30	148	0	2125	-0.03	7.28	0
23	SLU 31	194	0	2576	-0.03	9.55	0
23	SLU 32	194	0	2576	-0.03	9.55	0
23	SLU 33	194	0	2576	-0.03	9.55	0
23	SLU 34	194	0	2576	-0.03	9.55	0
23	SLU 35	194	0	2576	-0.03	9.55	0
23	SLU 36	194	0	2576	-0.03	9.55	0
23	SLU 37	194	0	2576	-0.03	9.55	0
23	SLU 38	194	0	2576	-0.03	9.55	0
23	SLU 39	214	0	2769	-0.03	10.53	0
23	SLU 40	214	0	2769	-0.03	10.53	0
23	SLU 41	214	0	2769	-0.03	10.53	0
23	SLU 42	214	0	2769	-0.03	10.53	0
23	SLU 43	153	0	2334	-0.03	7.56	0
23	SLU 44	153	0	2334	-0.03	7.56	0
23	SLU 45	153	0	2334	-0.03	7.56	0
23	SLU 46	153	0	2334	-0.03	7.56	0
23	SLU 47	153	0	2334	-0.03	7.56	0
23	SLU 48	153	0	2334	-0.03	7.56	0
23	SLU 49	153	0	2334	-0.03	7.56	0
23	SLU 50	153	0	2334	-0.03	7.56	0
23	SLU 51	153	0	2334	-0.03	7.56	0
23	SLU 52	200	0	2785	-0.03	9.83	0
23	SLU 53	200	0	2785	-0.03	9.83	0
23	SLU 54	200	0	2785	-0.03	9.83	0
23	SLU 55	200	0	2785	-0.03	9.83	0
23	SLU 56	200	0	2785	-0.03	9.83	0
23	SLU 57	200	0	2785	-0.03	9.83	0
23	SLU 58	200	0	2785	-0.03	9.83	0
23	SLU 59	200	0	2785	-0.03	9.83	0
23	SLU 60	220	0	2978	-0.03	10.81	0
23	SLU 61	220	0	2978	-0.03	10.81	0
23	SLU 62	220	0	2978	-0.03	10.81	0
23	SLU 63	220	0	2978	-0.03	10.81	0
23	SLU 64	177	0	2595	-0.03	8.72	0
23	SLU 65	177	0	2595	-0.03	8.72	0
23	SLU 66	177	0	2595	-0.03	8.72	0
23	SLU 67	177	0	2595	-0.03	8.72	0
23	SLU 68	177	0	2595	-0.03	8.72	0
23	SLU 69	177	0	2595	-0.03	8.72	0
23	SLU 70	177	0	2595	-0.03	8.72	0
23	SLU 71	177	0	2595	-0.03	8.72	0
23	SLU 72	177	0	2595	-0.03	8.72	0
23	SLU 73	223	0	3046	-0.04	10.99	0
23	SLU 74	223	0	3046	-0.04	10.99	0
23	SLU 75	223	0	3046	-0.04	10.99	0
23	SLU 76	223	0	3046	-0.04	10.99	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
23	SLU 77	223	0	3046	-0.04	10.99	0
23	SLU 78	223	0	3046	-0.04	10.99	0
23	SLU 79	223	0	3046	-0.04	10.99	0
23	SLU 80	223	0	3046	-0.04	10.99	0
23	SLU 81	243	0	3239	-0.04	11.97	0
23	SLU 82	243	0	3239	-0.04	11.97	0
23	SLU 83	243	0	3239	-0.04	11.97	0
23	SLU 84	243	0	3239	-0.04	11.97	0
23	SLE RA 1	131	0	1939	-0.02	6.45	0
23	SLE RA 2	131	0	1939	-0.02	6.45	0
23	SLE RA 3	131	0	1939	-0.02	6.45	0
23	SLE RA 4	131	0	1939	-0.02	6.45	0
23	SLE RA 5	131	0	1939	-0.02	6.45	0
23	SLE RA 6	131	0	1939	-0.02	6.45	0
23	SLE RA 7	131	0	1939	-0.02	6.45	0
23	SLE RA 8	131	0	1939	-0.02	6.45	0
23	SLE RA 9	131	0	1939	-0.02	6.45	0
23	SLE RA 10	162	0	2239	-0.03	7.97	0
23	SLE RA 11	162	0	2239	-0.03	7.97	0
23	SLE RA 12	162	0	2239	-0.03	7.97	0
23	SLE RA 13	162	0	2239	-0.03	7.97	0
23	SLE RA 14	162	0	2239	-0.03	7.97	0
23	SLE RA 15	162	0	2239	-0.03	7.97	0
23	SLE RA 16	162	0	2239	-0.03	7.97	0
23	SLE RA 17	162	0	2239	-0.03	7.97	0
23	SLE RA 18	175	0	2368	-0.03	8.62	0
23	SLE RA 19	175	0	2368	-0.03	8.62	0
23	SLE RA 20	175	0	2368	-0.03	8.62	0
23	SLE RA 21	175	0	2368	-0.03	8.62	0
23	SLE FR 1	131	0	1939	-0.02	6.45	0
23	SLE FR 2	131	0	1939	-0.02	6.45	0
23	SLE FR 3	131	0	1939	-0.02	6.45	0
23	SLE FR 4	144	0	2067	-0.02	7.1	0
23	SLE FR 5	144	0	2067	-0.02	7.1	0
23	SLE FR 6	153	0	2153	-0.03	7.53	0
23	SLE QP 1	131	0	1939	-0.02	6.45	0
23	SLE QP 2	144	0	2067	-0.02	7.1	0
23	SLD 1	345	27	2137	-38.72	17.28	0.11
23	SLD 2	345	27	2137	-38.72	17.28	0.11
23	SLD 3	330	2	2113	5.89	16.48	0.01
23	SLD 4	330	2	2113	5.89	16.48	0.01
23	SLD 5	228	45	2124	-79.3	11.36	0.19
23	SLD 6	228	45	2124	-79.3	11.36	0.19
23	SLD 7	176	-36	2045	69.42	8.7	-0.16
23	SLD 8	176	-36	2045	69.42	8.7	-0.16
23	SLD 9	112	36	2090	-69.47	5.5	0.16
23	SLD 10	112	36	2090	-69.47	5.5	0.16
23	SLD 11	60	-45	2011	79.25	2.84	-0.19
23	SLD 12	60	-45	2011	79.25	2.84	-0.19
23	SLD 13	-42	-3	2022	-5.94	-2.28	-0.01
23	SLD 14	-42	-3	2022	-5.94	-2.28	-0.01
23	SLD 15	-57	-27	1998	38.67	-3.08	-0.11
23	SLD 16	-57	-27	1998	38.67	-3.08	-0.11
23	SLV 1	620	70	2234	-103.64	31.17	0.3
23	SLV 2	620	70	2234	-103.64	31.17	0.3
23	SLV 3	578	5	2169	19.68	29	0.01
23	SLV 4	578	5	2169	19.68	29	0.01
23	SLV 5	351	121	2216	-218.14	17.62	0.53
23	SLV 6	351	121	2216	-218.14	17.62	0.53
23	SLV 7	211	-98	2000	192.92	10.37	-0.44
23	SLV 8	211	-98	2000	192.92	10.37	-0.44
23	SLV 9	77	98	2135	-192.97	3.83	0.44
23	SLV 10	77	98	2135	-192.97	3.83	0.44
23	SLV 11	-63	-121	1919	218.09	-3.42	-0.53
23	SLV 12	-63	-121	1919	218.09	-3.42	-0.53
23	SLV 13	-290	-5	1966	-19.73	-14.8	-0.01
23	SLV 14	-290	-5	1966	-19.73	-14.8	-0.01
23	SLV 15	-332	-70	1901	103.59	-16.97	-0.3
23	SLV 16	-332	-70	1901	103.59	-16.97	-0.3
24	SLU 1	142	0	1846	-0.03	7.24	0
24	SLU 2	142	0	1846	-0.03	7.24	0
24	SLU 3	142	0	1846	-0.03	7.24	0
24	SLU 4	142	0	1846	-0.03	7.24	0
24	SLU 5	142	0	1846	-0.03	7.24	0
24	SLU 6	142	0	1846	-0.03	7.24	0
24	SLU 7	142	0	1846	-0.03	7.24	0
24	SLU 8	142	0	1846	-0.03	7.24	0
24	SLU 9	142	0	1846	-0.03	7.24	0
24	SLU 10	200	0	2293	-0.04	10.26	0
24	SLU 11	200	0	2293	-0.04	10.26	0
24	SLU 12	200	0	2293	-0.04	10.26	0
24	SLU 13	200	0	2293	-0.04	10.26	0
24	SLU 14	200	0	2293	-0.04	10.26	0
24	SLU 15	200	0	2293	-0.04	10.26	0
24	SLU 16	200	0	2293	-0.04	10.26	0
24	SLU 17	200	0	2293	-0.04	10.26	0
24	SLU 18	224	0	2485	-0.04	11.55	0
24	SLU 19	224	0	2485	-0.04	11.55	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
24	SLU 20	224	0	2485	-0.04	11.55	0
24	SLU 21	224	0	2485	-0.04	11.55	0
24	SLU 22	172	0	2104	-0.04	8.78	0
24	SLU 23	172	0	2104	-0.04	8.78	0
24	SLU 24	172	0	2104	-0.04	8.78	0
24	SLU 25	172	0	2104	-0.04	8.78	0
24	SLU 26	172	0	2104	-0.04	8.78	0
24	SLU 27	172	0	2104	-0.04	8.78	0
24	SLU 28	172	0	2104	-0.04	8.78	0
24	SLU 29	172	0	2104	-0.04	8.78	0
24	SLU 30	172	0	2104	-0.04	8.78	0
24	SLU 31	230	0	2551	-0.04	11.8	0
24	SLU 32	230	0	2551	-0.04	11.8	0
24	SLU 33	230	0	2551	-0.04	11.8	0
24	SLU 34	230	0	2551	-0.04	11.8	0
24	SLU 35	230	0	2551	-0.04	11.8	0
24	SLU 36	230	0	2551	-0.04	11.8	0
24	SLU 37	230	0	2551	-0.04	11.8	0
24	SLU 38	230	0	2551	-0.04	11.8	0
24	SLU 39	254	0	2742	-0.05	13.09	0
24	SLU 40	254	0	2742	-0.05	13.09	0
24	SLU 41	254	0	2742	-0.05	13.09	0
24	SLU 42	254	0	2742	-0.05	13.09	0
24	SLU 43	175	0	2312	-0.04	8.88	0
24	SLU 44	175	0	2312	-0.04	8.88	0
24	SLU 45	175	0	2312	-0.04	8.88	0
24	SLU 46	175	0	2312	-0.04	8.88	0
24	SLU 47	175	0	2312	-0.04	8.88	0
24	SLU 48	175	0	2312	-0.04	8.88	0
24	SLU 49	175	0	2312	-0.04	8.88	0
24	SLU 50	175	0	2312	-0.04	8.88	0
24	SLU 51	175	0	2312	-0.04	8.88	0
24	SLU 52	232	0	2759	-0.05	11.9	0
24	SLU 53	232	0	2759	-0.05	11.9	0
24	SLU 54	232	0	2759	-0.05	11.9	0
24	SLU 55	232	0	2759	-0.05	11.9	0
24	SLU 56	232	0	2759	-0.05	11.9	0
24	SLU 57	232	0	2759	-0.05	11.9	0
24	SLU 58	232	0	2759	-0.05	11.9	0
24	SLU 59	232	0	2759	-0.05	11.9	0
24	SLU 60	257	0	2950	-0.05	13.19	0
24	SLU 61	257	0	2950	-0.05	13.19	0
24	SLU 62	257	0	2950	-0.05	13.19	0
24	SLU 63	257	0	2950	-0.05	13.19	0
24	SLU 64	204	0	2570	-0.05	10.42	0
24	SLU 65	204	0	2570	-0.05	10.42	0
24	SLU 66	204	0	2570	-0.05	10.42	0
24	SLU 67	204	0	2570	-0.05	10.42	0
24	SLU 68	204	0	2570	-0.05	10.42	0
24	SLU 69	204	0	2570	-0.05	10.42	0
24	SLU 70	204	0	2570	-0.05	10.42	0
24	SLU 71	204	0	2570	-0.05	10.42	0
24	SLU 72	204	0	2570	-0.05	10.42	0
24	SLU 73	262	0	3016	-0.05	13.44	0
24	SLU 74	262	0	3016	-0.05	13.44	0
24	SLU 75	262	0	3016	-0.05	13.44	0
24	SLU 76	262	0	3016	-0.05	13.44	0
24	SLU 77	262	0	3016	-0.05	13.44	0
24	SLU 78	262	0	3016	-0.05	13.44	0
24	SLU 79	262	0	3016	-0.05	13.44	0
24	SLU 80	262	0	3016	-0.05	13.44	0
24	SLU 81	287	0	3208	-0.06	14.74	0
24	SLU 82	287	0	3208	-0.06	14.74	0
24	SLU 83	287	0	3208	-0.06	14.74	0
24	SLU 84	287	0	3208	-0.06	14.74	0
24	SLE RA 1	151	0	1920	-0.04	7.68	0
24	SLE RA 2	151	0	1920	-0.04	7.68	0
24	SLE RA 3	151	0	1920	-0.04	7.68	0
24	SLE RA 4	151	0	1920	-0.04	7.68	0
24	SLE RA 5	151	0	1920	-0.04	7.68	0
24	SLE RA 6	151	0	1920	-0.04	7.68	0
24	SLE RA 7	151	0	1920	-0.04	7.68	0
24	SLE RA 8	151	0	1920	-0.04	7.68	0
24	SLE RA 9	151	0	1920	-0.04	7.68	0
24	SLE RA 10	189	0	2218	-0.04	9.69	0
24	SLE RA 11	189	0	2218	-0.04	9.69	0
24	SLE RA 12	189	0	2218	-0.04	9.69	0
24	SLE RA 13	189	0	2218	-0.04	9.69	0
24	SLE RA 14	189	0	2218	-0.04	9.69	0
24	SLE RA 15	189	0	2218	-0.04	9.69	0
24	SLE RA 16	189	0	2218	-0.04	9.69	0
24	SLE RA 17	189	0	2218	-0.04	9.69	0
24	SLE RA 18	206	0	2345	-0.04	10.55	0
24	SLE RA 19	206	0	2345	-0.04	10.55	0
24	SLE RA 20	206	0	2345	-0.04	10.55	0
24	SLE RA 21	206	0	2345	-0.04	10.55	0
24	SLE FR 1	151	0	1920	-0.04	7.68	0
24	SLE FR 2	151	0	1920	-0.04	7.68	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
24	SLE FR 3	151	0	1920	-0.04	7.68	0
24	SLE FR 4	167	0	2048	-0.04	8.54	0
24	SLE FR 5	167	0	2048	-0.04	8.54	0
24	SLE FR 6	178	0	2133	-0.04	9.12	0
24	SLE QP 1	151	0	1920	-0.04	7.68	0
24	SLE QP 2	167	0	2048	-0.04	8.54	0
24	SLD 1	363	26	2086	-2.99	18.64	0.11
24	SLD 2	363	26	2086	-2.99	18.64	0.11
24	SLD 3	350	3	2067	36.03	18.03	0.01
24	SLD 4	350	3	2067	36.03	18.03	0.01
24	SLD 5	246	41	2089	-60.1	12.49	0.19
24	SLD 6	246	41	2089	-60.1	12.49	0.19
24	SLD 7	202	-33	2024	69.96	10.46	-0.15
24	SLD 8	202	-33	2024	69.96	10.46	-0.15
24	SLD 9	132	33	2071	-70.04	6.62	0.15
24	SLD 10	132	33	2071	-70.04	6.62	0.15
24	SLD 11	89	-41	2006	60.03	4.59	-0.19
24	SLD 12	89	-41	2006	60.03	4.59	-0.19
24	SLD 13	-16	-3	2028	-36.1	-0.95	-0.01
24	SLD 14	-16	-3	2028	-36.1	-0.95	-0.01
24	SLD 15	-29	-26	2009	2.92	-1.55	-0.11
24	SLD 16	-29	-26	2009	2.92	-1.55	-0.11
24	SLV 1	630	66	2141	-10.98	32.36	0.29
24	SLV 2	630	66	2141	-10.98	32.36	0.29
24	SLV 3	596	8	2089	95.67	30.76	0.03
24	SLV 4	596	8	2089	95.67	30.76	0.03
24	SLV 5	359	108	2155	-165.08	18.12	0.49
24	SLV 6	359	108	2155	-165.08	18.12	0.49
24	SLV 7	243	-86	1981	190.44	12.78	-0.4
24	SLV 8	243	-86	1981	190.44	12.78	-0.4
24	SLV 9	91	86	2114	-190.51	4.3	0.4
24	SLV 10	91	86	2114	-190.51	4.3	0.4
24	SLV 11	-25	-108	1940	165.01	-1.03	-0.49
24	SLV 12	-25	-108	1940	165.01	-1.03	-0.49
24	SLV 13	-261	-8	2006	-95.75	-13.68	-0.03
24	SLV 14	-261	-8	2006	-95.75	-13.68	-0.03
24	SLV 15	-296	-66	1954	10.91	-15.28	-0.29
24	SLV 16	-296	-66	1954	10.91	-15.28	-0.29
25	SLU 1	167	0	1822	-0.05	8.64	0
25	SLU 2	167	0	1822	-0.05	8.64	0
25	SLU 3	167	0	1822	-0.05	8.64	0
25	SLU 4	167	0	1822	-0.05	8.64	0
25	SLU 5	167	0	1822	-0.05	8.64	0
25	SLU 6	167	0	1822	-0.05	8.64	0
25	SLU 7	167	0	1822	-0.05	8.64	0
25	SLU 8	167	0	1822	-0.05	8.64	0
25	SLU 9	167	0	1822	-0.05	8.64	0
25	SLU 10	238	0	2259	-0.05	12.24	0
25	SLU 11	238	0	2259	-0.05	12.24	0
25	SLU 12	238	0	2259	-0.05	12.24	0
25	SLU 13	238	0	2259	-0.05	12.24	0
25	SLU 14	238	0	2259	-0.05	12.24	0
25	SLU 15	238	0	2259	-0.05	12.24	0
25	SLU 16	238	0	2259	-0.05	12.24	0
25	SLU 17	238	0	2259	-0.05	12.24	0
25	SLU 18	269	0	2447	-0.06	13.78	0
25	SLU 19	269	0	2447	-0.06	13.78	0
25	SLU 20	269	0	2447	-0.06	13.78	0
25	SLU 21	269	0	2447	-0.06	13.78	0
25	SLU 22	205	0	2073	-0.05	10.54	0
25	SLU 23	205	0	2073	-0.05	10.54	0
25	SLU 24	205	0	2073	-0.05	10.54	0
25	SLU 25	205	0	2073	-0.05	10.54	0
25	SLU 26	205	0	2073	-0.05	10.54	0
25	SLU 27	205	0	2073	-0.05	10.54	0
25	SLU 28	205	0	2073	-0.05	10.54	0
25	SLU 29	205	0	2073	-0.05	10.54	0
25	SLU 30	205	0	2073	-0.05	10.54	0
25	SLU 31	276	0	2511	-0.06	14.14	0
25	SLU 32	276	0	2511	-0.06	14.14	0
25	SLU 33	276	0	2511	-0.06	14.14	0
25	SLU 34	276	0	2511	-0.06	14.14	0
25	SLU 35	276	0	2511	-0.06	14.14	0
25	SLU 36	276	0	2511	-0.06	14.14	0
25	SLU 37	276	0	2511	-0.06	14.14	0
25	SLU 38	276	0	2511	-0.06	14.14	0
25	SLU 39	306	0	2698	-0.06	15.68	0
25	SLU 40	306	0	2698	-0.06	15.68	0
25	SLU 41	306	0	2698	-0.06	15.68	0
25	SLU 42	306	0	2698	-0.06	15.68	0
25	SLU 43	205	0	2283	-0.06	10.59	0
25	SLU 44	205	0	2283	-0.06	10.59	0
25	SLU 45	205	0	2283	-0.06	10.59	0
25	SLU 46	205	0	2283	-0.06	10.59	0
25	SLU 47	205	0	2283	-0.06	10.59	0
25	SLU 48	205	0	2283	-0.06	10.59	0
25	SLU 49	205	0	2283	-0.06	10.59	0
25	SLU 50	205	0	2283	-0.06	10.59	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
25	SLU 51	205	0	2283	-0.06	10.59	0
25	SLU 52	276	0	2720	-0.07	14.18	0
25	SLU 53	276	0	2720	-0.07	14.18	0
25	SLU 54	276	0	2720	-0.07	14.18	0
25	SLU 55	276	0	2720	-0.07	14.18	0
25	SLU 56	276	0	2720	-0.07	14.18	0
25	SLU 57	276	0	2720	-0.07	14.18	0
25	SLU 58	276	0	2720	-0.07	14.18	0
25	SLU 59	276	0	2720	-0.07	14.18	0
25	SLU 60	306	0	2907	-0.07	15.72	0
25	SLU 61	306	0	2907	-0.07	15.72	0
25	SLU 62	306	0	2907	-0.07	15.72	0
25	SLU 63	306	0	2907	-0.07	15.72	0
25	SLU 64	242	0	2534	-0.06	12.48	0
25	SLU 65	242	0	2534	-0.06	12.48	0
25	SLU 66	242	0	2534	-0.06	12.48	0
25	SLU 67	242	0	2534	-0.06	12.48	0
25	SLU 68	242	0	2534	-0.06	12.48	0
25	SLU 69	242	0	2534	-0.06	12.48	0
25	SLU 70	242	0	2534	-0.06	12.48	0
25	SLU 71	242	0	2534	-0.06	12.48	0
25	SLU 72	242	0	2534	-0.06	12.48	0
25	SLU 73	313	0	2971	-0.07	16.08	0
25	SLU 74	313	0	2971	-0.07	16.08	0
25	SLU 75	313	0	2971	-0.07	16.08	0
25	SLU 76	313	0	2971	-0.07	16.08	0
25	SLU 77	313	0	2971	-0.07	16.08	0
25	SLU 78	313	0	2971	-0.07	16.08	0
25	SLU 79	313	0	2971	-0.07	16.08	0
25	SLU 80	313	0	2971	-0.07	16.08	0
25	SLU 81	343	0	3158	-0.08	17.62	0
25	SLU 82	343	0	3158	-0.08	17.62	0
25	SLU 83	343	0	3158	-0.08	17.62	0
25	SLU 84	343	0	3158	-0.08	17.62	0
25	SLE RA 1	178	0	1894	-0.05	9.19	0
25	SLE RA 2	178	0	1894	-0.05	9.19	0
25	SLE RA 3	178	0	1894	-0.05	9.19	0
25	SLE RA 4	178	0	1894	-0.05	9.19	0
25	SLE RA 5	178	0	1894	-0.05	9.19	0
25	SLE RA 6	178	0	1894	-0.05	9.19	0
25	SLE RA 7	178	0	1894	-0.05	9.19	0
25	SLE RA 8	178	0	1894	-0.05	9.19	0
25	SLE RA 9	178	0	1894	-0.05	9.19	0
25	SLE RA 10	225	0	2185	-0.05	11.58	0
25	SLE RA 11	225	0	2185	-0.05	11.58	0
25	SLE RA 12	225	0	2185	-0.05	11.58	0
25	SLE RA 13	225	0	2185	-0.05	11.58	0
25	SLE RA 14	225	0	2185	-0.05	11.58	0
25	SLE RA 15	225	0	2185	-0.05	11.58	0
25	SLE RA 16	225	0	2185	-0.05	11.58	0
25	SLE RA 17	225	0	2185	-0.05	11.58	0
25	SLE RA 18	246	0	2310	-0.06	12.61	0
25	SLE RA 19	246	0	2310	-0.06	12.61	0
25	SLE RA 20	246	0	2310	-0.06	12.61	0
25	SLE RA 21	246	0	2310	-0.06	12.61	0
25	SLE FR 1	178	0	1894	-0.05	9.19	0
25	SLE FR 2	178	0	1894	-0.05	9.19	0
25	SLE FR 3	178	0	1894	-0.05	9.19	0
25	SLE FR 4	198	0	2019	-0.05	10.21	0
25	SLE FR 5	198	0	2019	-0.05	10.21	0
25	SLE FR 6	212	0	2102	-0.05	10.9	0
25	SLE QP 1	178	0	1894	-0.05	9.19	0
25	SLE QP 2	198	0	2019	-0.05	10.21	0
25	SLD 1	387	-3	2053	-1.02	20.18	-0.01
25	SLD 2	387	-3	2053	-1.02	20.18	-0.01
25	SLD 3	375	-24	2034	33.07	19.52	-0.1
25	SLD 4	375	-24	2034	33.07	19.52	-0.1
25	SLD 5	274	30	2058	-52.04	14.21	0.13
25	SLD 6	274	30	2058	-52.04	14.21	0.13
25	SLD 7	233	-39	1994	61.59	12	-0.17
25	SLD 8	233	-39	1994	61.59	12	-0.17
25	SLD 9	164	39	2043	-61.69	8.43	0.17
25	SLD 10	164	39	2043	-61.69	8.43	0.17
25	SLD 11	123	-30	1979	51.94	6.22	-0.13
25	SLD 12	123	-30	1979	51.94	6.22	-0.13
25	SLD 13	21	24	2004	-33.17	0.91	0.1
25	SLD 14	21	24	2004	-33.17	0.91	0.1
25	SLD 15	9	3	1984	0.92	0.24	0.01
25	SLD 16	9	3	1984	0.92	0.24	0.01
25	SLV 1	645	-8	2102	-4.96	33.76	-0.03
25	SLV 2	645	-8	2102	-4.96	33.76	-0.03
25	SLV 3	613	-62	2052	87.08	32.02	-0.27
25	SLV 4	613	-62	2052	87.08	32.02	-0.27
25	SLV 5	381	79	2118	-141.12	19.93	0.35
25	SLV 6	381	79	2118	-141.12	19.93	0.35
25	SLV 7	274	-100	1954	165.68	14.1	-0.44
25	SLV 8	274	-100	1954	165.68	14.1	-0.44
25	SLV 9	123	100	2084	-165.78	6.32	0.44



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
25	SLV 10	123	100	2084	-165.78	6.32	0.44
25	SLV 11	15	-79	1919	141.01	0.5	-0.35
25	SLV 12	15	-79	1919	141.01	0.5	-0.35
25	SLV 13	-216	62	1985	-87.18	-11.59	0.27
25	SLV 14	-216	62	1985	-87.18	-11.59	0.27
25	SLV 15	-248	8	1936	4.85	-13.34	0.03
25	SLV 16	-248	8	1936	4.85	-13.34	0.03
26	SLU 1	195	0	1790	-0.06	10.15	0
26	SLU 2	195	0	1790	-0.06	10.15	0
26	SLU 3	195	0	1790	-0.06	10.15	0
26	SLU 4	195	0	1790	-0.06	10.15	0
26	SLU 5	195	0	1790	-0.06	10.15	0
26	SLU 6	195	0	1790	-0.06	10.15	0
26	SLU 7	195	0	1790	-0.06	10.15	0
26	SLU 8	195	0	1790	-0.06	10.15	0
26	SLU 9	195	0	1790	-0.06	10.15	0
26	SLU 10	284	0	2209	-0.07	14.83	0
26	SLU 11	284	0	2209	-0.07	14.83	0
26	SLU 12	284	0	2209	-0.07	14.83	0
26	SLU 13	284	0	2209	-0.07	14.83	0
26	SLU 14	284	0	2209	-0.07	14.83	0
26	SLU 15	284	0	2209	-0.07	14.83	0
26	SLU 16	284	0	2209	-0.07	14.83	0
26	SLU 17	284	0	2209	-0.07	14.83	0
26	SLU 18	322	0	2389	-0.08	16.83	0
26	SLU 19	322	0	2389	-0.08	16.83	0
26	SLU 20	322	0	2389	-0.08	16.83	0
26	SLU 21	322	0	2389	-0.08	16.83	0
26	SLU 22	241	0	2030	-0.07	12.57	0
26	SLU 23	241	0	2030	-0.07	12.57	0
26	SLU 24	241	0	2030	-0.07	12.57	0
26	SLU 25	241	0	2030	-0.07	12.57	0
26	SLU 26	241	0	2030	-0.07	12.57	0
26	SLU 27	241	0	2030	-0.07	12.57	0
26	SLU 28	241	0	2030	-0.07	12.57	0
26	SLU 29	241	0	2030	-0.07	12.57	0
26	SLU 30	241	0	2030	-0.07	12.57	0
26	SLU 31	330	0	2449	-0.08	17.24	0
26	SLU 32	330	0	2449	-0.08	17.24	0
26	SLU 33	330	0	2449	-0.08	17.24	0
26	SLU 34	330	0	2449	-0.08	17.24	0
26	SLU 35	330	0	2449	-0.08	17.24	0
26	SLU 36	330	0	2449	-0.08	17.24	0
26	SLU 37	330	0	2449	-0.08	17.24	0
26	SLU 38	330	0	2449	-0.08	17.24	0
26	SLU 39	368	0	2629	-0.08	19.25	0
26	SLU 40	368	0	2629	-0.08	19.25	0
26	SLU 41	368	0	2629	-0.08	19.25	0
26	SLU 42	368	0	2629	-0.08	19.25	0
26	SLU 43	238	0	2245	-0.08	12.37	0
26	SLU 44	238	0	2245	-0.08	12.37	0
26	SLU 45	238	0	2245	-0.08	12.37	0
26	SLU 46	238	0	2245	-0.08	12.37	0
26	SLU 47	238	0	2245	-0.08	12.37	0
26	SLU 48	238	0	2245	-0.08	12.37	0
26	SLU 49	238	0	2245	-0.08	12.37	0
26	SLU 50	238	0	2245	-0.08	12.37	0
26	SLU 51	238	0	2245	-0.08	12.37	0
26	SLU 52	327	0	2664	-0.09	17.04	0
26	SLU 53	327	0	2664	-0.09	17.04	0
26	SLU 54	327	0	2664	-0.09	17.04	0
26	SLU 55	327	0	2664	-0.09	17.04	0
26	SLU 56	327	0	2664	-0.09	17.04	0
26	SLU 57	327	0	2664	-0.09	17.04	0
26	SLU 58	327	0	2664	-0.09	17.04	0
26	SLU 59	327	0	2664	-0.09	17.04	0
26	SLU 60	365	0	2844	-0.09	19.05	0
26	SLU 61	365	0	2844	-0.09	19.05	0
26	SLU 62	365	0	2844	-0.09	19.05	0
26	SLU 63	365	0	2844	-0.09	19.05	0
26	SLU 64	284	0	2485	-0.09	14.78	0
26	SLU 65	284	0	2485	-0.09	14.78	0
26	SLU 66	284	0	2485	-0.09	14.78	0
26	SLU 67	284	0	2485	-0.09	14.78	0
26	SLU 68	284	0	2485	-0.09	14.78	0
26	SLU 69	284	0	2485	-0.09	14.78	0
26	SLU 70	284	0	2485	-0.09	14.78	0
26	SLU 71	284	0	2485	-0.09	14.78	0
26	SLU 72	284	0	2485	-0.09	14.78	0
26	SLU 73	373	0	2904	-0.1	19.46	0
26	SLU 74	373	0	2904	-0.1	19.46	0
26	SLU 75	373	0	2904	-0.1	19.46	0
26	SLU 76	373	0	2904	-0.1	19.46	0
26	SLU 77	373	0	2904	-0.1	19.46	0
26	SLU 78	373	0	2904	-0.1	19.46	0
26	SLU 79	373	0	2904	-0.1	19.46	0
26	SLU 80	373	0	2904	-0.1	19.46	0
26	SLU 81	411	0	3084	-0.1	21.46	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
26	SLU 82	411	0	3084	-0.1	21.46	0
26	SLU 83	411	0	3084	-0.1	21.46	0
26	SLU 84	411	0	3084	-0.1	21.46	0
26	SLE RA 1	208	0	1859	-0.06	10.84	0
26	SLE RA 2	208	0	1859	-0.06	10.84	0
26	SLE RA 3	208	0	1859	-0.06	10.84	0
26	SLE RA 4	208	0	1859	-0.06	10.84	0
26	SLE RA 5	208	0	1859	-0.06	10.84	0
26	SLE RA 6	208	0	1859	-0.06	10.84	0
26	SLE RA 7	208	0	1859	-0.06	10.84	0
26	SLE RA 8	208	0	1859	-0.06	10.84	0
26	SLE RA 9	208	0	1859	-0.06	10.84	0
26	SLE RA 10	268	0	2138	-0.07	13.96	0
26	SLE RA 11	268	0	2138	-0.07	13.96	0
26	SLE RA 12	268	0	2138	-0.07	13.96	0
26	SLE RA 13	268	0	2138	-0.07	13.96	0
26	SLE RA 14	268	0	2138	-0.07	13.96	0
26	SLE RA 15	268	0	2138	-0.07	13.96	0
26	SLE RA 16	268	0	2138	-0.07	13.96	0
26	SLE RA 17	268	0	2138	-0.07	13.96	0
26	SLE RA 18	293	0	2258	-0.07	15.29	0
26	SLE RA 19	293	0	2258	-0.07	15.29	0
26	SLE RA 20	293	0	2258	-0.07	15.29	0
26	SLE RA 21	293	0	2258	-0.07	15.29	0
26	SLE FR 1	208	0	1859	-0.06	10.84	0
26	SLE FR 2	208	0	1859	-0.06	10.84	0
26	SLE FR 3	208	0	1859	-0.06	10.84	0
26	SLE FR 4	234	0	1978	-0.07	12.18	0
26	SLE FR 5	234	0	1978	-0.07	12.18	0
26	SLE FR 6	251	0	2058	-0.07	13.07	0
26	SLE QP 1	208	0	1859	-0.06	10.84	0
26	SLE QP 2	234	0	1978	-0.07	12.18	0
26	SLD 1	418	-3	2022	0.23	22.18	-0.01
26	SLD 2	418	-3	2022	0.23	22.18	-0.01
26	SLD 3	406	-22	1999	29.67	21.59	-0.08
26	SLD 4	406	-22	1999	29.67	21.59	-0.08
26	SLD 5	307	28	2027	-44.62	16.08	0.1
26	SLD 6	307	28	2027	-44.62	16.08	0.1
26	SLD 7	267	-36	1949	53.5	14.1	-0.13
26	SLD 8	267	-36	1949	53.5	14.1	-0.13
26	SLD 9	200	36	2007	-53.63	10.26	0.13
26	SLD 10	200	36	2007	-53.63	10.26	0.13
26	SLD 11	160	-28	1930	44.48	8.27	-0.1
26	SLD 12	160	-28	1930	44.48	8.27	-0.1
26	SLD 13	62	22	1958	-29.8	2.77	0.08
26	SLD 14	62	22	1958	-29.8	2.77	0.08
26	SLD 15	50	3	1935	-0.37	2.17	0.01
26	SLD 16	50	3	1935	-0.37	2.17	0.01
26	SLV 1	667	-8	2083	-0.96	35.75	-0.03
26	SLV 2	667	-8	2083	-0.96	35.75	-0.03
26	SLV 3	638	-57	2025	77.54	34.28	-0.2
26	SLV 4	638	-57	2025	77.54	34.28	-0.2
26	SLV 5	409	73	2097	-119.39	21.48	0.26
26	SLV 6	409	73	2097	-119.39	21.48	0.26
26	SLV 7	310	-92	1905	142.27	16.58	-0.32
26	SLV 8	310	-92	1905	142.27	16.58	-0.32
26	SLV 9	158	92	2052	-142.41	7.77	0.32
26	SLV 10	158	92	2052	-142.41	7.77	0.32
26	SLV 11	59	-73	1860	119.26	2.87	-0.25
26	SLV 12	59	-73	1860	119.26	2.87	-0.25
26	SLV 13	-170	57	1931	-77.67	-9.93	0.2
26	SLV 14	-170	57	1931	-77.67	-9.93	0.2
26	SLV 15	-200	8	1874	0.83	-11.4	0.03
26	SLV 16	-200	8	1874	0.83	-11.4	0.03
27	SLU 1	219	0	1753	-0.09	12.25	0
27	SLU 2	219	0	1753	-0.09	12.25	0
27	SLU 3	219	0	1753	-0.09	12.25	0
27	SLU 4	219	0	1753	-0.09	12.25	0
27	SLU 5	219	0	1753	-0.09	12.25	0
27	SLU 6	219	0	1753	-0.09	12.25	0
27	SLU 7	219	0	1753	-0.09	12.25	0
27	SLU 8	219	0	1753	-0.09	12.25	0
27	SLU 9	219	0	1753	-0.09	12.25	0
27	SLU 10	322	0	2146	-0.1	17.82	0
27	SLU 11	322	0	2146	-0.1	17.82	0
27	SLU 12	322	0	2146	-0.1	17.82	0
27	SLU 13	322	0	2146	-0.1	17.82	0
27	SLU 14	322	0	2146	-0.1	17.82	0
27	SLU 15	322	0	2146	-0.1	17.82	0
27	SLU 16	322	0	2146	-0.1	17.82	0
27	SLU 17	322	0	2146	-0.1	17.82	0
27	SLU 18	366	0	2314	-0.11	20.2	0
27	SLU 19	366	0	2314	-0.11	20.2	0
27	SLU 20	366	0	2314	-0.11	20.2	0
27	SLU 21	366	0	2314	-0.11	20.2	0
27	SLU 22	272	0	1978	-0.09	15.16	0
27	SLU 23	272	0	1978	-0.09	15.16	0
27	SLU 24	272	0	1978	-0.09	15.16	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
27	SLU 25	272	0	1978	-0.09	15.16	0
27	SLU 26	272	0	1978	-0.09	15.16	0
27	SLU 27	272	0	1978	-0.09	15.16	0
27	SLU 28	272	0	1978	-0.09	15.16	0
27	SLU 29	272	0	1978	-0.09	15.16	0
27	SLU 30	272	0	1978	-0.09	15.16	0
27	SLU 31	375	0	2371	-0.11	20.72	0
27	SLU 32	375	0	2371	-0.11	20.72	0
27	SLU 33	375	0	2371	-0.11	20.72	0
27	SLU 34	375	0	2371	-0.11	20.72	0
27	SLU 35	375	0	2371	-0.11	20.72	0
27	SLU 36	375	0	2371	-0.11	20.72	0
27	SLU 37	375	0	2371	-0.11	20.72	0
27	SLU 38	375	0	2371	-0.11	20.72	0
27	SLU 39	419	0	2539	-0.11	23.1	0
27	SLU 40	419	0	2539	-0.11	23.1	0
27	SLU 41	419	0	2539	-0.11	23.1	0
27	SLU 42	419	0	2539	-0.11	23.1	0
27	SLU 43	266	0	2201	-0.11	14.93	0
27	SLU 44	266	0	2201	-0.11	14.93	0
27	SLU 45	266	0	2201	-0.11	14.93	0
27	SLU 46	266	0	2201	-0.11	14.93	0
27	SLU 47	266	0	2201	-0.11	14.93	0
27	SLU 48	266	0	2201	-0.11	14.93	0
27	SLU 49	266	0	2201	-0.11	14.93	0
27	SLU 50	266	0	2201	-0.11	14.93	0
27	SLU 51	266	0	2201	-0.11	14.93	0
27	SLU 52	369	0	2594	-0.12	20.5	0
27	SLU 53	369	0	2594	-0.12	20.5	0
27	SLU 54	369	0	2594	-0.12	20.5	0
27	SLU 55	369	0	2594	-0.12	20.5	0
27	SLU 56	369	0	2594	-0.12	20.5	0
27	SLU 57	369	0	2594	-0.12	20.5	0
27	SLU 58	369	0	2594	-0.12	20.5	0
27	SLU 59	369	0	2594	-0.12	20.5	0
27	SLU 60	413	0	2763	-0.13	22.88	0
27	SLU 61	413	0	2763	-0.13	22.88	0
27	SLU 62	413	0	2763	-0.13	22.88	0
27	SLU 63	413	0	2763	-0.13	22.88	0
27	SLU 64	320	0	2427	-0.12	17.84	0
27	SLU 65	320	0	2427	-0.12	17.84	0
27	SLU 66	320	0	2427	-0.12	17.84	0
27	SLU 67	320	0	2427	-0.12	17.84	0
27	SLU 68	320	0	2427	-0.12	17.84	0
27	SLU 69	320	0	2427	-0.12	17.84	0
27	SLU 70	320	0	2427	-0.12	17.84	0
27	SLU 71	320	0	2427	-0.12	17.84	0
27	SLU 72	320	0	2427	-0.12	17.84	0
27	SLU 73	423	0	2819	-0.13	23.4	0
27	SLU 74	423	0	2819	-0.13	23.4	0
27	SLU 75	423	0	2819	-0.13	23.4	0
27	SLU 76	423	0	2819	-0.13	23.4	0
27	SLU 77	423	0	2819	-0.13	23.4	0
27	SLU 78	423	0	2819	-0.13	23.4	0
27	SLU 79	423	0	2819	-0.13	23.4	0
27	SLU 80	423	0	2819	-0.13	23.4	0
27	SLU 81	467	0	2988	-0.14	25.78	0
27	SLU 82	467	0	2988	-0.14	25.78	0
27	SLU 83	467	0	2988	-0.14	25.78	0
27	SLU 84	467	0	2988	-0.14	25.78	0
27	SLE RA 1	234	0	1817	-0.09	13.08	0
27	SLE RA 2	234	0	1817	-0.09	13.08	0
27	SLE RA 3	234	0	1817	-0.09	13.08	0
27	SLE RA 4	234	0	1817	-0.09	13.08	0
27	SLE RA 5	234	0	1817	-0.09	13.08	0
27	SLE RA 6	234	0	1817	-0.09	13.08	0
27	SLE RA 7	234	0	1817	-0.09	13.08	0
27	SLE RA 8	234	0	1817	-0.09	13.08	0
27	SLE RA 9	234	0	1817	-0.09	13.08	0
27	SLE RA 10	303	0	2079	-0.1	16.79	0
27	SLE RA 11	303	0	2079	-0.1	16.79	0
27	SLE RA 12	303	0	2079	-0.1	16.79	0
27	SLE RA 13	303	0	2079	-0.1	16.79	0
27	SLE RA 14	303	0	2079	-0.1	16.79	0
27	SLE RA 15	303	0	2079	-0.1	16.79	0
27	SLE RA 16	303	0	2079	-0.1	16.79	0
27	SLE RA 17	303	0	2079	-0.1	16.79	0
27	SLE RA 18	332	0	2191	-0.1	18.38	0
27	SLE RA 19	332	0	2191	-0.1	18.38	0
27	SLE RA 20	332	0	2191	-0.1	18.38	0
27	SLE RA 21	332	0	2191	-0.1	18.38	0
27	SLE FR 1	234	0	1817	-0.09	13.08	0
27	SLE FR 2	234	0	1817	-0.09	13.08	0
27	SLE FR 3	234	0	1817	-0.09	13.08	0
27	SLE FR 4	264	0	1929	-0.09	14.67	0
27	SLE FR 5	264	0	1929	-0.09	14.67	0
27	SLE FR 6	283	0	2004	-0.09	15.73	0
27	SLE QP 1	234	0	1817	-0.09	13.08	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
27	SLE QP 2	264	0	1929	-0.09	14.67	0
27	SLD 1	443	-3	1979	1.03	24.65	-0.01
27	SLD 2	443	-3	1979	1.03	24.65	-0.01
27	SLD 3	429	-20	1948	25.77	23.95	-0.03
27	SLD 4	429	-20	1948	25.77	23.95	-0.03
27	SLD 5	338	25	1992	-37.28	18.72	0.03
27	SLD 6	338	25	1992	-37.28	18.72	0.03
27	SLD 7	293	-32	1887	45.19	16.4	-0.04
27	SLD 8	293	-32	1887	45.19	16.4	-0.04
27	SLD 9	234	32	1972	-45.38	12.95	0.04
27	SLD 10	234	32	1972	-45.38	12.95	0.04
27	SLD 11	190	-25	1866	37.1	10.62	-0.03
27	SLD 12	190	-25	1866	37.1	10.62	-0.03
27	SLD 13	98	20	1911	-25.96	5.39	0.03
27	SLD 14	98	20	1911	-25.96	5.39	0.03
27	SLD 15	84	3	1879	-1.21	4.7	0.01
27	SLD 16	84	3	1879	-1.21	4.7	0.01
27	SLV 1	686	-7	2048	1.7	38.2	-0.01
27	SLV 2	686	-7	2048	1.7	38.2	-0.01
27	SLV 3	654	-52	1971	66.94	36.48	-0.07
27	SLV 4	654	-52	1971	66.94	36.48	-0.07
27	SLV 5	439	65	2082	-98.5	24.35	0.09
27	SLV 6	439	65	2082	-98.5	24.35	0.09
27	SLV 7	332	-82	1825	118.97	18.6	-0.11
27	SLV 8	332	-82	1825	118.97	18.6	-0.11
27	SLV 9	195	82	2034	-119.15	10.75	0.11
27	SLV 10	195	82	2034	-119.15	10.75	0.11
27	SLV 11	88	-65	1777	98.32	5	-0.09
27	SLV 12	88	-65	1777	98.32	5	-0.09
27	SLV 13	-127	52	1888	-67.13	-7.13	0.07
27	SLV 14	-127	52	1888	-67.13	-7.13	0.07
27	SLV 15	-159	7	1811	-1.89	-8.86	0.01
27	SLV 16	-159	7	1811	-1.89	-8.86	0.01
28	SLU 1	216	0	1739	-0.12	11.93	0
28	SLU 2	216	0	1739	-0.12	11.93	0
28	SLU 3	216	0	1739	-0.12	11.93	0
28	SLU 4	216	0	1739	-0.12	11.93	0
28	SLU 5	216	0	1739	-0.12	11.93	0
28	SLU 6	216	0	1739	-0.12	11.93	0
28	SLU 7	216	0	1739	-0.12	11.93	0
28	SLU 8	216	0	1739	-0.12	11.93	0
28	SLU 9	216	0	1739	-0.12	11.93	0
28	SLU 10	323	0	2108	-0.15	17.75	0
28	SLU 11	323	0	2108	-0.15	17.75	0
28	SLU 12	323	0	2108	-0.15	17.75	0
28	SLU 13	323	0	2108	-0.15	17.75	0
28	SLU 14	323	0	2108	-0.15	17.75	0
28	SLU 15	323	0	2108	-0.15	17.75	0
28	SLU 16	323	0	2108	-0.15	17.75	0
28	SLU 17	323	0	2108	-0.15	17.75	0
28	SLU 18	369	0	2266	-0.15	20.24	0
28	SLU 19	369	0	2266	-0.15	20.24	0
28	SLU 20	369	0	2266	-0.15	20.24	0
28	SLU 21	369	0	2266	-0.15	20.24	0
28	SLU 22	271	0	1951	-0.14	14.9	0
28	SLU 23	271	0	1951	-0.14	14.9	0
28	SLU 24	271	0	1951	-0.14	14.9	0
28	SLU 25	271	0	1951	-0.14	14.9	0
28	SLU 26	271	0	1951	-0.14	14.9	0
28	SLU 27	271	0	1951	-0.14	14.9	0
28	SLU 28	271	0	1951	-0.14	14.9	0
28	SLU 29	271	0	1951	-0.14	14.9	0
28	SLU 30	271	0	1951	-0.14	14.9	0
28	SLU 31	378	0	2320	-0.16	20.72	0
28	SLU 32	378	0	2320	-0.16	20.72	0
28	SLU 33	378	0	2320	-0.16	20.72	0
28	SLU 34	378	0	2320	-0.16	20.72	0
28	SLU 35	378	0	2320	-0.16	20.72	0
28	SLU 36	378	0	2320	-0.16	20.72	0
28	SLU 37	378	0	2320	-0.16	20.72	0
28	SLU 38	378	0	2320	-0.16	20.72	0
28	SLU 39	424	0	2478	-0.17	23.22	0
28	SLU 40	424	0	2478	-0.17	23.22	0
28	SLU 41	424	0	2478	-0.17	23.22	0
28	SLU 42	424	0	2478	-0.17	23.22	0
28	SLU 43	262	0	2188	-0.16	14.49	0
28	SLU 44	262	0	2188	-0.16	14.49	0
28	SLU 45	262	0	2188	-0.16	14.49	0
28	SLU 46	262	0	2188	-0.16	14.49	0
28	SLU 47	262	0	2188	-0.16	14.49	0
28	SLU 48	262	0	2188	-0.16	14.49	0
28	SLU 49	262	0	2188	-0.16	14.49	0
28	SLU 50	262	0	2188	-0.16	14.49	0
28	SLU 51	262	0	2188	-0.16	14.49	0
28	SLU 52	369	0	2556	-0.18	20.31	0
28	SLU 53	369	0	2556	-0.18	20.31	0
28	SLU 54	369	0	2556	-0.18	20.31	0
28	SLU 55	369	0	2556	-0.18	20.31	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
28	SLU 56	369	0	2556	-0.18	20.31	0
28	SLU 57	369	0	2556	-0.18	20.31	0
28	SLU 58	369	0	2556	-0.18	20.31	0
28	SLU 59	369	0	2556	-0.18	20.31	0
28	SLU 60	415	0	2714	-0.19	22.8	0
28	SLU 61	415	0	2714	-0.19	22.8	0
28	SLU 62	415	0	2714	-0.19	22.8	0
28	SLU 63	415	0	2714	-0.19	22.8	0
28	SLU 64	317	0	2400	-0.17	17.46	0
28	SLU 65	317	0	2400	-0.17	17.46	0
28	SLU 66	317	0	2400	-0.17	17.46	0
28	SLU 67	317	0	2400	-0.17	17.46	0
28	SLU 68	317	0	2400	-0.17	17.46	0
28	SLU 69	317	0	2400	-0.17	17.46	0
28	SLU 70	317	0	2400	-0.17	17.46	0
28	SLU 71	317	0	2400	-0.17	17.46	0
28	SLU 72	317	0	2400	-0.17	17.46	0
28	SLU 73	424	0	2769	-0.19	23.28	0
28	SLU 74	424	0	2769	-0.19	23.28	0
28	SLU 75	424	0	2769	-0.19	23.28	0
28	SLU 76	424	0	2769	-0.19	23.28	0
28	SLU 77	424	0	2769	-0.19	23.28	0
28	SLU 78	424	0	2769	-0.19	23.28	0
28	SLU 79	424	0	2769	-0.19	23.28	0
28	SLU 80	424	0	2769	-0.19	23.28	0
28	SLU 81	470	0	2927	-0.2	25.78	0
28	SLU 82	470	0	2927	-0.2	25.78	0
28	SLU 83	470	0	2927	-0.2	25.78	0
28	SLU 84	470	0	2927	-0.2	25.78	0
28	SLE RA 1	232	0	1800	-0.13	12.78	0
28	SLE RA 2	232	0	1800	-0.13	12.78	0
28	SLE RA 3	232	0	1800	-0.13	12.78	0
28	SLE RA 4	232	0	1800	-0.13	12.78	0
28	SLE RA 5	232	0	1800	-0.13	12.78	0
28	SLE RA 6	232	0	1800	-0.13	12.78	0
28	SLE RA 7	232	0	1800	-0.13	12.78	0
28	SLE RA 8	232	0	1800	-0.13	12.78	0
28	SLE RA 9	232	0	1800	-0.13	12.78	0
28	SLE RA 10	303	0	2045	-0.14	16.66	0
28	SLE RA 11	303	0	2045	-0.14	16.66	0
28	SLE RA 12	303	0	2045	-0.14	16.66	0
28	SLE RA 13	303	0	2045	-0.14	16.66	0
28	SLE RA 14	303	0	2045	-0.14	16.66	0
28	SLE RA 15	303	0	2045	-0.14	16.66	0
28	SLE RA 16	303	0	2045	-0.14	16.66	0
28	SLE RA 17	303	0	2045	-0.14	16.66	0
28	SLE RA 18	334	0	2151	-0.15	18.32	0
28	SLE RA 19	334	0	2151	-0.15	18.32	0
28	SLE RA 20	334	0	2151	-0.15	18.32	0
28	SLE RA 21	334	0	2151	-0.15	18.32	0
28	SLE FR 1	232	0	1800	-0.13	12.78	0
28	SLE FR 2	232	0	1800	-0.13	12.78	0
28	SLE FR 3	232	0	1800	-0.13	12.78	0
28	SLE FR 4	262	0	1905	-0.13	14.44	0
28	SLE FR 5	262	0	1905	-0.13	14.44	0
28	SLE FR 6	283	0	1975	-0.14	15.55	0
28	SLE QP 1	232	0	1800	-0.13	12.78	0
28	SLE QP 2	262	0	1905	-0.13	14.44	0
28	SLD 1	421	-18	1968	1.6	23.55	-0.03
28	SLD 2	421	-18	1968	1.6	23.55	-0.03
28	SLD 3	437	-4	1922	21.4	24.36	-0.01
28	SLD 4	437	-4	1922	21.4	24.36	-0.01
28	SLD 5	286	-27	1992	-29.64	15.94	-0.05
28	SLD 6	286	-27	1992	-29.64	15.94	-0.05
28	SLD 7	339	21	1841	36.35	18.65	0.04
28	SLD 8	339	21	1841	36.35	18.65	0.04
28	SLD 9	186	-21	1968	-36.62	10.23	-0.04
28	SLD 10	186	-21	1968	-36.62	10.23	-0.04
28	SLD 11	239	27	1817	29.37	12.94	0.05
28	SLD 12	239	27	1817	29.37	12.94	0.05
28	SLD 13	88	4	1888	-21.67	4.52	0.01
28	SLD 14	88	4	1888	-21.67	4.52	0.01
28	SLD 15	104	18	1842	-1.87	5.33	0.03
28	SLD 16	104	18	1842	-1.87	5.33	0.03
28	SLV 1	636	-46	2053	3.64	35.89	-0.08
28	SLV 2	636	-46	2053	3.64	35.89	-0.08
28	SLV 3	674	-9	1944	55.33	37.81	-0.01
28	SLV 4	674	-9	1944	55.33	37.81	-0.01
28	SLV 5	317	-69	2115	-77.4	17.96	-0.13
28	SLV 6	317	-69	2115	-77.4	17.96	-0.13
28	SLV 7	444	52	1751	94.9	24.37	0.1
28	SLV 8	444	52	1751	94.9	24.37	0.1
28	SLV 9	81	-52	2059	-95.17	4.51	-0.1
28	SLV 10	81	-52	2059	-95.17	4.51	-0.1
28	SLV 11	208	69	1694	77.13	10.92	0.13
28	SLV 12	208	69	1694	77.13	10.92	0.13
28	SLV 13	-149	9	1866	-55.6	-8.93	0.01
28	SLV 14	-149	9	1866	-55.6	-8.93	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
28	SLV 15	-111	46	1757	-3.91	-7.01	0.08
28	SLV 16	-111	46	1757	-3.91	-7.01	0.08
29	SLU 1	227	0	1766	-0.2	13.47	0
29	SLU 2	227	0	1766	-0.2	13.47	0
29	SLU 3	227	0	1766	-0.2	13.47	0
29	SLU 4	227	0	1766	-0.2	13.47	0
29	SLU 5	227	0	1766	-0.2	13.47	0
29	SLU 6	227	0	1766	-0.2	13.47	0
29	SLU 7	227	0	1766	-0.2	13.47	0
29	SLU 8	227	0	1766	-0.2	13.47	0
29	SLU 9	227	0	1766	-0.2	13.47	0
29	SLU 10	336	0	2121	-0.23	19.66	0
29	SLU 11	336	0	2121	-0.23	19.66	0
29	SLU 12	336	0	2121	-0.23	19.66	0
29	SLU 13	336	0	2121	-0.23	19.66	0
29	SLU 14	336	0	2121	-0.23	19.66	0
29	SLU 15	336	0	2121	-0.23	19.66	0
29	SLU 16	336	0	2121	-0.23	19.66	0
29	SLU 17	336	0	2121	-0.23	19.66	0
29	SLU 18	383	0	2272	-0.25	22.31	0
29	SLU 19	383	0	2272	-0.25	22.31	0
29	SLU 20	383	0	2272	-0.25	22.31	0
29	SLU 21	383	0	2272	-0.25	22.31	0
29	SLU 22	283	0	1972	-0.22	16.67	0
29	SLU 23	283	0	1972	-0.22	16.67	0
29	SLU 24	283	0	1972	-0.22	16.67	0
29	SLU 25	283	0	1972	-0.22	16.67	0
29	SLU 26	283	0	1972	-0.22	16.67	0
29	SLU 27	283	0	1972	-0.22	16.67	0
29	SLU 28	283	0	1972	-0.22	16.67	0
29	SLU 29	283	0	1972	-0.22	16.67	0
29	SLU 30	283	0	1972	-0.22	16.67	0
29	SLU 31	392	0	2326	-0.26	22.85	0
29	SLU 32	392	0	2326	-0.26	22.85	0
29	SLU 33	392	0	2326	-0.26	22.85	0
29	SLU 34	392	0	2326	-0.26	22.85	0
29	SLU 35	392	0	2326	-0.26	22.85	0
29	SLU 36	392	0	2326	-0.26	22.85	0
29	SLU 37	392	0	2326	-0.26	22.85	0
29	SLU 38	392	0	2326	-0.26	22.85	0
29	SLU 39	439	0	2477	-0.27	25.51	0
29	SLU 40	439	0	2477	-0.27	25.51	0
29	SLU 41	439	0	2477	-0.27	25.51	0
29	SLU 42	439	0	2477	-0.27	25.51	0
29	SLU 43	275	0	2226	-0.26	16.42	0
29	SLU 44	275	0	2226	-0.26	16.42	0
29	SLU 45	275	0	2226	-0.26	16.42	0
29	SLU 46	275	0	2226	-0.26	16.42	0
29	SLU 47	275	0	2226	-0.26	16.42	0
29	SLU 48	275	0	2226	-0.26	16.42	0
29	SLU 49	275	0	2226	-0.26	16.42	0
29	SLU 50	275	0	2226	-0.26	16.42	0
29	SLU 51	275	0	2226	-0.26	16.42	0
29	SLU 52	385	0	2580	-0.29	22.61	0
29	SLU 53	385	0	2580	-0.29	22.61	0
29	SLU 54	385	0	2580	-0.29	22.61	0
29	SLU 55	385	0	2580	-0.29	22.61	0
29	SLU 56	385	0	2580	-0.29	22.61	0
29	SLU 57	385	0	2580	-0.29	22.61	0
29	SLU 58	385	0	2580	-0.29	22.61	0
29	SLU 59	385	0	2580	-0.29	22.61	0
29	SLU 60	431	0	2732	-0.3	25.26	0
29	SLU 61	431	0	2732	-0.3	25.26	0
29	SLU 62	431	0	2732	-0.3	25.26	0
29	SLU 63	431	0	2732	-0.3	25.26	0
29	SLU 64	331	0	2431	-0.28	19.61	0
29	SLU 65	331	0	2431	-0.28	19.61	0
29	SLU 66	331	0	2431	-0.28	19.61	0
29	SLU 67	331	0	2431	-0.28	19.61	0
29	SLU 68	331	0	2431	-0.28	19.61	0
29	SLU 69	331	0	2431	-0.28	19.61	0
29	SLU 70	331	0	2431	-0.28	19.61	0
29	SLU 71	331	0	2431	-0.28	19.61	0
29	SLU 72	331	0	2431	-0.28	19.61	0
29	SLU 73	441	0	2785	-0.31	25.8	0
29	SLU 74	441	0	2785	-0.31	25.8	0
29	SLU 75	441	0	2785	-0.31	25.8	0
29	SLU 76	441	0	2785	-0.31	25.8	0
29	SLU 77	441	0	2785	-0.31	25.8	0
29	SLU 78	441	0	2785	-0.31	25.8	0
29	SLU 79	441	0	2785	-0.31	25.8	0
29	SLU 80	441	0	2785	-0.31	25.8	0
29	SLU 81	488	0	2937	-0.32	28.45	0
29	SLU 82	488	0	2937	-0.32	28.45	0
29	SLU 83	488	0	2937	-0.32	28.45	0
29	SLU 84	488	0	2937	-0.32	28.45	0
29	SLE RA 1	243	0	1825	-0.21	14.39	0
29	SLE RA 2	243	0	1825	-0.21	14.39	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
29	SLE RA 3	243	0	1825	-0.21	14.39	0
29	SLE RA 4	243	0	1825	-0.21	14.39	0
29	SLE RA 5	243	0	1825	-0.21	14.39	0
29	SLE RA 6	243	0	1825	-0.21	14.39	0
29	SLE RA 7	243	0	1825	-0.21	14.39	0
29	SLE RA 8	243	0	1825	-0.21	14.39	0
29	SLE RA 9	243	0	1825	-0.21	14.39	0
29	SLE RA 10	315	0	2061	-0.23	18.51	0
29	SLE RA 11	315	0	2061	-0.23	18.51	0
29	SLE RA 12	315	0	2061	-0.23	18.51	0
29	SLE RA 13	315	0	2061	-0.23	18.51	0
29	SLE RA 14	315	0	2061	-0.23	18.51	0
29	SLE RA 15	315	0	2061	-0.23	18.51	0
29	SLE RA 16	315	0	2061	-0.23	18.51	0
29	SLE RA 17	315	0	2061	-0.23	18.51	0
29	SLE RA 18	347	0	2162	-0.24	20.28	0
29	SLE RA 19	347	0	2162	-0.24	20.28	0
29	SLE RA 20	347	0	2162	-0.24	20.28	0
29	SLE RA 21	347	0	2162	-0.24	20.28	0
29	SLE FR 1	243	0	1825	-0.21	14.39	0
29	SLE FR 2	243	0	1825	-0.21	14.39	0
29	SLE FR 3	243	0	1825	-0.21	14.39	0
29	SLE FR 4	274	0	1926	-0.22	16.15	0
29	SLE FR 5	274	0	1926	-0.22	16.15	0
29	SLE FR 6	295	0	1994	-0.22	17.33	0
29	SLE QP 1	243	0	1825	-0.21	14.39	0
29	SLE QP 2	274	0	1926	-0.22	16.15	0
29	SLD 1	420	-16	2027	2.04	24.64	-0.03
29	SLD 2	420	-16	2027	2.04	24.64	-0.03
29	SLD 3	440	-5	1961	16.6	25.58	-0.01
29	SLD 4	440	-5	1961	16.6	25.58	-0.01
29	SLD 5	288	-21	2056	-21.63	17.28	-0.05
29	SLD 6	288	-21	2056	-21.63	17.28	-0.05
29	SLD 7	353	14	1837	26.91	20.4	0.04
29	SLD 8	353	14	1837	26.91	20.4	0.04
29	SLD 9	195	-14	2015	-27.35	11.9	-0.03
29	SLD 10	195	-14	2015	-27.35	11.9	-0.03
29	SLD 11	259	21	1796	21.19	15.03	0.05
29	SLD 12	259	21	1796	21.19	15.03	0.05
29	SLD 13	108	6	1891	-17.03	6.73	0.01
29	SLD 14	108	6	1891	-17.03	6.73	0.01
29	SLD 15	127	16	1826	-2.47	7.66	0.03
29	SLD 16	127	16	1826	-2.47	7.66	0.03
29	SLV 1	619	-40	2164	5.11	36.14	-0.08
29	SLV 2	619	-40	2164	5.11	36.14	-0.08
29	SLV 3	665	-14	2006	42.81	38.37	-0.02
29	SLV 4	665	-14	2006	42.81	38.37	-0.02
29	SLV 5	308	-53	2237	-55.81	18.77	-0.12
29	SLV 6	308	-53	2237	-55.81	18.77	-0.12
29	SLV 7	461	37	1710	69.88	26.2	0.09
29	SLV 8	461	37	1710	69.88	26.2	0.09
29	SLV 9	87	-37	2142	-70.32	6.11	-0.09
29	SLV 10	87	-37	2142	-70.32	6.11	-0.09
29	SLV 11	240	53	1615	55.38	13.53	0.12
29	SLV 12	240	53	1615	55.38	13.53	0.12
29	SLV 13	-117	14	1846	-43.25	-6.06	0.02
29	SLV 14	-117	14	1846	-43.25	-6.06	0.02
29	SLV 15	-71	40	1688	-5.54	-3.84	0.08
29	SLV 16	-71	40	1688	-5.54	-3.84	0.08
30	SLU 1	236	0	1849	-0.39	13.43	0
30	SLU 2	236	0	1849	-0.39	13.43	0
30	SLU 3	236	0	1849	-0.39	13.43	0
30	SLU 4	236	0	1849	-0.39	13.43	0
30	SLU 5	236	0	1849	-0.39	13.43	0
30	SLU 6	236	0	1849	-0.39	13.43	0
30	SLU 7	236	0	1849	-0.39	13.43	0
30	SLU 8	236	0	1849	-0.39	13.43	0
30	SLU 9	236	0	1849	-0.39	13.43	0
30	SLU 10	342	0	2207	-0.45	19.16	0
30	SLU 11	342	0	2207	-0.45	19.16	0
30	SLU 12	342	0	2207	-0.45	19.16	0
30	SLU 13	342	0	2207	-0.45	19.16	0
30	SLU 14	342	0	2207	-0.45	19.16	0
30	SLU 15	342	0	2207	-0.45	19.16	0
30	SLU 16	342	0	2207	-0.45	19.16	0
30	SLU 17	342	0	2207	-0.45	19.16	0
30	SLU 18	387	0	2360	-0.48	21.62	0
30	SLU 19	387	0	2360	-0.48	21.62	0
30	SLU 20	387	0	2360	-0.48	21.62	0
30	SLU 21	387	0	2360	-0.48	21.62	0
30	SLU 22	291	0	2057	-0.43	16.4	0
30	SLU 23	291	0	2057	-0.43	16.4	0
30	SLU 24	291	0	2057	-0.43	16.4	0
30	SLU 25	291	0	2057	-0.43	16.4	0
30	SLU 26	291	0	2057	-0.43	16.4	0
30	SLU 27	291	0	2057	-0.43	16.4	0
30	SLU 28	291	0	2057	-0.43	16.4	0
30	SLU 29	291	0	2057	-0.43	16.4	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
30	SLU 30	291	0	2057	-0.43	16.4	0
30	SLU 31	396	0	2414	-0.49	22.14	0
30	SLU 32	396	0	2414	-0.49	22.14	0
30	SLU 33	396	0	2414	-0.49	22.14	0
30	SLU 34	396	0	2414	-0.49	22.14	0
30	SLU 35	396	0	2414	-0.49	22.14	0
30	SLU 36	396	0	2414	-0.49	22.14	0
30	SLU 37	396	0	2414	-0.49	22.14	0
30	SLU 38	396	0	2414	-0.49	22.14	0
30	SLU 39	441	0	2568	-0.52	24.59	0
30	SLU 40	441	0	2568	-0.52	24.59	0
30	SLU 41	441	0	2568	-0.52	24.59	0
30	SLU 42	441	0	2568	-0.52	24.59	0
30	SLU 43	289	0	2332	-0.49	16.44	0
30	SLU 44	289	0	2332	-0.49	16.44	0
30	SLU 45	289	0	2332	-0.49	16.44	0
30	SLU 46	289	0	2332	-0.49	16.44	0
30	SLU 47	289	0	2332	-0.49	16.44	0
30	SLU 48	289	0	2332	-0.49	16.44	0
30	SLU 49	289	0	2332	-0.49	16.44	0
30	SLU 50	289	0	2332	-0.49	16.44	0
30	SLU 51	289	0	2332	-0.49	16.44	0
30	SLU 52	394	0	2690	-0.56	22.17	0
30	SLU 53	394	0	2690	-0.56	22.17	0
30	SLU 54	394	0	2690	-0.56	22.17	0
30	SLU 55	394	0	2690	-0.56	22.17	0
30	SLU 56	394	0	2690	-0.56	22.17	0
30	SLU 57	394	0	2690	-0.56	22.17	0
30	SLU 58	394	0	2690	-0.56	22.17	0
30	SLU 59	394	0	2690	-0.56	22.17	0
30	SLU 60	439	1	2843	-0.58	24.63	0
30	SLU 61	439	1	2843	-0.58	24.63	0
30	SLU 62	439	1	2843	-0.58	24.63	0
30	SLU 63	439	1	2843	-0.58	24.63	0
30	SLU 64	343	0	2540	-0.53	19.41	0
30	SLU 65	343	0	2540	-0.53	19.41	0
30	SLU 66	343	0	2540	-0.53	19.41	0
30	SLU 67	343	0	2540	-0.53	19.41	0
30	SLU 68	343	0	2540	-0.53	19.41	0
30	SLU 69	343	0	2540	-0.53	19.41	0
30	SLU 70	343	0	2540	-0.53	19.41	0
30	SLU 71	343	0	2540	-0.53	19.41	0
30	SLU 72	343	0	2540	-0.53	19.41	0
30	SLU 73	448	1	2898	-0.6	25.15	0
30	SLU 74	448	1	2898	-0.6	25.15	0
30	SLU 75	448	1	2898	-0.6	25.15	0
30	SLU 76	448	1	2898	-0.6	25.15	0
30	SLU 77	448	1	2898	-0.6	25.15	0
30	SLU 78	448	1	2898	-0.6	25.15	0
30	SLU 79	448	1	2898	-0.6	25.15	0
30	SLU 80	448	1	2898	-0.6	25.15	0
30	SLU 81	493	1	3051	-0.62	27.6	0
30	SLU 82	493	1	3051	-0.62	27.6	0
30	SLU 83	493	1	3051	-0.62	27.6	0
30	SLU 84	493	1	3051	-0.62	27.6	0
30	SLE RA 1	252	0	1908	-0.4	14.28	0
30	SLE RA 2	252	0	1908	-0.4	14.28	0
30	SLE RA 3	252	0	1908	-0.4	14.28	0
30	SLE RA 4	252	0	1908	-0.4	14.28	0
30	SLE RA 5	252	0	1908	-0.4	14.28	0
30	SLE RA 6	252	0	1908	-0.4	14.28	0
30	SLE RA 7	252	0	1908	-0.4	14.28	0
30	SLE RA 8	252	0	1908	-0.4	14.28	0
30	SLE RA 9	252	0	1908	-0.4	14.28	0
30	SLE RA 10	322	0	2147	-0.44	18.1	0
30	SLE RA 11	322	0	2147	-0.44	18.1	0
30	SLE RA 12	322	0	2147	-0.44	18.1	0
30	SLE RA 13	322	0	2147	-0.44	18.1	0
30	SLE RA 14	322	0	2147	-0.44	18.1	0
30	SLE RA 15	322	0	2147	-0.44	18.1	0
30	SLE RA 16	322	0	2147	-0.44	18.1	0
30	SLE RA 17	322	0	2147	-0.44	18.1	0
30	SLE RA 18	352	0	2249	-0.46	19.74	0
30	SLE RA 19	352	0	2249	-0.46	19.74	0
30	SLE RA 20	352	0	2249	-0.46	19.74	0
30	SLE RA 21	352	0	2249	-0.46	19.74	0
30	SLE FR 1	252	0	1908	-0.4	14.28	0
30	SLE FR 2	252	0	1908	-0.4	14.28	0
30	SLE FR 3	252	0	1908	-0.4	14.28	0
30	SLE FR 4	282	0	2010	-0.42	15.92	0
30	SLE FR 5	282	0	2010	-0.42	15.92	0
30	SLE FR 6	302	0	2079	-0.43	17.01	0
30	SLE QP 1	252	0	1908	-0.4	14.28	0
30	SLE QP 2	282	0	2010	-0.42	15.92	0
30	SLD 1	414	-14	2178	2.07	23.53	-0.04
30	SLD 2	414	-14	2178	2.07	23.53	-0.04
30	SLD 3	437	-7	2083	11.36	24.54	-0.01
30	SLD 4	437	-7	2083	11.36	24.54	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
30	SLD 5	287	-14	2205	-13.77	16.67	-0.06
30	SLD 6	287	-14	2205	-13.77	16.67	-0.06
30	SLD 7	363	8	1888	17.21	20.03	0.05
30	SLD 8	363	8	1888	17.21	20.03	0.05
30	SLD 9	201	-7	2133	-18.05	11.8	-0.04
30	SLD 10	201	-7	2133	-18.05	11.8	-0.04
30	SLD 11	277	14	1816	12.93	15.16	0.06
30	SLD 12	277	14	1816	12.93	15.16	0.06
30	SLD 13	127	8	1938	-12.2	7.29	0.02
30	SLD 14	127	8	1938	-12.2	7.29	0.02
30	SLD 15	150	15	1842	-2.91	8.3	0.05
30	SLD 16	150	15	1842	-2.91	8.3	0.05
30	SLV 1	593	-35	2406	5.59	33.84	-0.11
30	SLV 2	593	-35	2406	5.59	33.84	-0.11
30	SLV 3	646	-18	2178	29.5	36.22	-0.03
30	SLV 4	646	-18	2178	29.5	36.22	-0.03
30	SLV 5	294	-36	2476	-34.88	17.69	-0.16
30	SLV 6	294	-36	2476	-34.88	17.69	-0.16
30	SLV 7	473	20	1714	44.82	25.62	0.12
30	SLV 8	473	20	1714	44.82	25.62	0.12
30	SLV 9	91	-20	2307	-45.65	6.22	-0.11
30	SLV 10	91	-20	2307	-45.65	6.22	-0.11
30	SLV 11	270	37	1545	34.04	14.15	0.16
30	SLV 12	270	37	1545	34.04	14.15	0.16
30	SLV 13	-82	19	1843	-30.34	-4.39	0.04
30	SLV 14	-82	19	1843	-30.34	-4.39	0.04
30	SLV 15	-29	36	1614	-6.43	-2.01	0.12
30	SLV 16	-29	36	1614	-6.43	-2.01	0.12
31	SLU 1	275	3	2089	-0.84	18.27	-0.01
31	SLU 2	275	3	2089	-0.84	18.27	-0.01
31	SLU 3	275	3	2089	-0.84	18.27	-0.01
31	SLU 4	275	3	2089	-0.84	18.27	-0.01
31	SLU 5	275	3	2089	-0.84	18.27	-0.01
31	SLU 6	275	3	2089	-0.84	18.27	-0.01
31	SLU 7	275	3	2089	-0.84	18.27	-0.01
31	SLU 8	275	3	2089	-0.84	18.27	-0.01
31	SLU 9	275	3	2089	-0.84	18.27	-0.01
31	SLU 10	383	3	2494	-0.98	24.78	-0.02
31	SLU 11	383	3	2494	-0.98	24.78	-0.02
31	SLU 12	383	3	2494	-0.98	24.78	-0.02
31	SLU 13	383	3	2494	-0.98	24.78	-0.02
31	SLU 14	383	3	2494	-0.98	24.78	-0.02
31	SLU 15	383	3	2494	-0.98	24.78	-0.02
31	SLU 16	383	3	2494	-0.98	24.78	-0.02
31	SLU 17	383	3	2494	-0.98	24.78	-0.02
31	SLU 18	429	3	2667	-1.03	27.57	-0.02
31	SLU 19	429	3	2667	-1.03	27.57	-0.02
31	SLU 20	429	3	2667	-1.03	27.57	-0.02
31	SLU 21	429	3	2667	-1.03	27.57	-0.02
31	SLU 22	332	3	2323	-0.92	21.72	-0.02
31	SLU 23	332	3	2323	-0.92	21.72	-0.02
31	SLU 24	332	3	2323	-0.92	21.72	-0.02
31	SLU 25	332	3	2323	-0.92	21.72	-0.02
31	SLU 26	332	3	2323	-0.92	21.72	-0.02
31	SLU 27	332	3	2323	-0.92	21.72	-0.02
31	SLU 28	332	3	2323	-0.92	21.72	-0.02
31	SLU 29	332	3	2323	-0.92	21.72	-0.02
31	SLU 30	332	3	2323	-0.92	21.72	-0.02
31	SLU 31	440	3	2728	-1.06	28.22	-0.02
31	SLU 32	440	3	2728	-1.06	28.22	-0.02
31	SLU 33	440	3	2728	-1.06	28.22	-0.02
31	SLU 34	440	3	2728	-1.06	28.22	-0.02
31	SLU 35	440	3	2728	-1.06	28.22	-0.02
31	SLU 36	440	3	2728	-1.06	28.22	-0.02
31	SLU 37	440	3	2728	-1.06	28.22	-0.02
31	SLU 38	440	3	2728	-1.06	28.22	-0.02
31	SLU 39	486	4	2902	-1.11	31.01	-0.02
31	SLU 40	486	4	2902	-1.11	31.01	-0.02
31	SLU 41	486	4	2902	-1.11	31.01	-0.02
31	SLU 42	486	4	2902	-1.11	31.01	-0.02
31	SLU 43	338	3	2635	-1.07	22.57	-0.02
31	SLU 44	338	3	2635	-1.07	22.57	-0.02
31	SLU 45	338	3	2635	-1.07	22.57	-0.02
31	SLU 46	338	3	2635	-1.07	22.57	-0.02
31	SLU 47	338	3	2635	-1.07	22.57	-0.02
31	SLU 48	338	3	2635	-1.07	22.57	-0.02
31	SLU 49	338	3	2635	-1.07	22.57	-0.02
31	SLU 50	338	3	2635	-1.07	22.57	-0.02
31	SLU 51	338	3	2635	-1.07	22.57	-0.02
31	SLU 52	446	4	3040	-1.2	29.08	-0.02
31	SLU 53	446	4	3040	-1.2	29.08	-0.02
31	SLU 54	446	4	3040	-1.2	29.08	-0.02
31	SLU 55	446	4	3040	-1.2	29.08	-0.02
31	SLU 56	446	4	3040	-1.2	29.08	-0.02
31	SLU 57	446	4	3040	-1.2	29.08	-0.02
31	SLU 58	446	4	3040	-1.2	29.08	-0.02
31	SLU 59	446	4	3040	-1.2	29.08	-0.02
31	SLU 60	492	4	3213	-1.26	31.87	-0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
31	SLU 61	492	4	3213	-1.26	31.87	-0.02
31	SLU 62	492	4	3213	-1.26	31.87	-0.02
31	SLU 63	492	4	3213	-1.26	31.87	-0.02
31	SLU 64	395	4	2870	-1.15	26.02	-0.02
31	SLU 65	395	4	2870	-1.15	26.02	-0.02
31	SLU 66	395	4	2870	-1.15	26.02	-0.02
31	SLU 67	395	4	2870	-1.15	26.02	-0.02
31	SLU 68	395	4	2870	-1.15	26.02	-0.02
31	SLU 69	395	4	2870	-1.15	26.02	-0.02
31	SLU 70	395	4	2870	-1.15	26.02	-0.02
31	SLU 71	395	4	2870	-1.15	26.02	-0.02
31	SLU 72	395	4	2870	-1.15	26.02	-0.02
31	SLU 73	503	4	3275	-1.28	32.53	-0.02
31	SLU 74	503	4	3275	-1.28	32.53	-0.02
31	SLU 75	503	4	3275	-1.28	32.53	-0.02
31	SLU 76	503	4	3275	-1.28	32.53	-0.02
31	SLU 77	503	4	3275	-1.28	32.53	-0.02
31	SLU 78	503	4	3275	-1.28	32.53	-0.02
31	SLU 79	503	4	3275	-1.28	32.53	-0.02
31	SLU 80	503	4	3275	-1.28	32.53	-0.02
31	SLU 81	549	4	3448	-1.34	35.31	-0.02
31	SLU 82	549	4	3448	-1.34	35.31	-0.02
31	SLU 83	549	4	3448	-1.34	35.31	-0.02
31	SLU 84	549	4	3448	-1.34	35.31	-0.02
31	SLE RA 1	291	3	2156	-0.87	19.26	-0.01
31	SLE RA 2	291	3	2156	-0.87	19.26	-0.01
31	SLE RA 3	291	3	2156	-0.87	19.26	-0.01
31	SLE RA 4	291	3	2156	-0.87	19.26	-0.01
31	SLE RA 5	291	3	2156	-0.87	19.26	-0.01
31	SLE RA 6	291	3	2156	-0.87	19.26	-0.01
31	SLE RA 7	291	3	2156	-0.87	19.26	-0.01
31	SLE RA 8	291	3	2156	-0.87	19.26	-0.01
31	SLE RA 9	291	3	2156	-0.87	19.26	-0.01
31	SLE RA 10	363	3	2426	-0.95	23.6	-0.02
31	SLE RA 11	363	3	2426	-0.95	23.6	-0.02
31	SLE RA 12	363	3	2426	-0.95	23.6	-0.02
31	SLE RA 13	363	3	2426	-0.95	23.6	-0.02
31	SLE RA 14	363	3	2426	-0.95	23.6	-0.02
31	SLE RA 15	363	3	2426	-0.95	23.6	-0.02
31	SLE RA 16	363	3	2426	-0.95	23.6	-0.02
31	SLE RA 17	363	3	2426	-0.95	23.6	-0.02
31	SLE RA 18	394	3	2541	-0.99	25.45	-0.02
31	SLE RA 19	394	3	2541	-0.99	25.45	-0.02
31	SLE RA 20	394	3	2541	-0.99	25.45	-0.02
31	SLE RA 21	394	3	2541	-0.99	25.45	-0.02
31	SLE FR 1	291	3	2156	-0.87	19.26	-0.01
31	SLE FR 2	291	3	2156	-0.87	19.26	-0.01
31	SLE FR 3	291	3	2156	-0.87	19.26	-0.01
31	SLE FR 4	322	3	2272	-0.9	21.12	-0.02
31	SLE FR 5	322	3	2272	-0.9	21.12	-0.02
31	SLE FR 6	343	3	2349	-0.93	22.36	-0.02
31	SLE QP 1	291	3	2156	-0.87	19.26	-0.01
31	SLE QP 2	322	3	2272	-0.9	21.12	-0.02
31	SLD 1	436	-7	2557	0.93	29.14	-0.03
31	SLD 2	436	-7	2557	0.93	29.14	-0.03
31	SLD 3	464	-4	2408	5.37	28.21	-0.02
31	SLD 4	464	-4	2408	5.37	28.21	-0.02
31	SLD 5	314	-5	2584	-7.08	24.92	-0.05
31	SLD 6	314	-5	2584	-7.08	24.92	-0.05
31	SLD 7	407	6	2086	7.71	21.84	0.01
31	SLD 8	407	6	2086	7.71	21.84	0.01
31	SLD 9	237	0	2457	-9.52	20.39	-0.04
31	SLD 10	237	0	2457	-9.52	20.39	-0.04
31	SLD 11	330	11	1959	5.27	17.31	0.02
31	SLD 12	330	11	1959	5.27	17.31	0.02
31	SLD 13	180	10	2135	-7.18	14.02	-0.01
31	SLD 14	180	10	2135	-7.18	14.02	-0.01
31	SLD 15	208	13	1986	-2.74	13.1	0
31	SLD 16	208	13	1986	-2.74	13.1	0
31	SLV 1	591	-22	2946	3.53	40.01	-0.07
31	SLV 2	591	-22	2946	3.53	40.01	-0.07
31	SLV 3	657	-13	2587	14.9	37.81	-0.02
31	SLV 4	657	-13	2587	14.9	37.81	-0.02
31	SLV 5	303	-17	3017	-16.82	30.13	-0.1
31	SLV 6	303	-17	3017	-16.82	30.13	-0.1
31	SLV 7	522	11	1823	21.08	22.78	0.05
31	SLV 8	522	11	1823	21.08	22.78	0.05
31	SLV 9	122	-5	2721	-22.89	19.46	-0.08
31	SLV 10	122	-5	2721	-22.89	19.46	-0.08
31	SLV 11	341	23	1526	15.01	12.1	0.07
31	SLV 12	341	23	1526	15.01	12.1	0.07
31	SLV 13	-12	19	1956	-16.71	4.43	-0.01
31	SLV 14	-12	19	1956	-16.71	4.43	-0.01
31	SLV 15	53	28	1598	-5.34	2.22	0.04
31	SLV 16	53	28	1598	-5.34	2.22	0.04
32	SLU 1	375	380	2632	-10.68	10.85	0
32	SLU 2	375	380	2632	-10.68	10.85	0
32	SLU 3	375	380	2632	-10.68	10.85	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
32	SLU 4	375	380	2632	-10.68	10.85	0
32	SLU 5	375	380	2632	-10.68	10.85	0
32	SLU 6	375	380	2632	-10.68	10.85	0
32	SLU 7	375	380	2632	-10.68	10.85	0
32	SLU 8	375	380	2632	-10.68	10.85	0
32	SLU 9	375	380	2632	-10.68	10.85	0
32	SLU 10	475	436	3150	-11.89	14.33	-0.02
32	SLU 11	475	436	3150	-11.89	14.33	-0.02
32	SLU 12	475	436	3150	-11.89	14.33	-0.02
32	SLU 13	475	436	3150	-11.89	14.33	-0.02
32	SLU 14	475	436	3150	-11.89	14.33	-0.02
32	SLU 15	475	436	3150	-11.89	14.33	-0.02
32	SLU 16	475	436	3150	-11.89	14.33	-0.02
32	SLU 17	475	436	3150	-11.89	14.33	-0.02
32	SLU 18	518	460	3372	-12.41	15.81	-0.03
32	SLU 19	518	460	3372	-12.41	15.81	-0.03
32	SLU 20	518	460	3372	-12.41	15.81	-0.03
32	SLU 21	518	460	3372	-12.41	15.81	-0.03
32	SLU 22	430	415	2931	-11.49	12.71	-0.01
32	SLU 23	430	415	2931	-11.49	12.71	-0.01
32	SLU 24	430	415	2931	-11.49	12.71	-0.01
32	SLU 25	430	415	2931	-11.49	12.71	-0.01
32	SLU 26	430	415	2931	-11.49	12.71	-0.01
32	SLU 27	430	415	2931	-11.49	12.71	-0.01
32	SLU 28	430	415	2931	-11.49	12.71	-0.01
32	SLU 29	430	415	2931	-11.49	12.71	-0.01
32	SLU 30	430	415	2931	-11.49	12.71	-0.01
32	SLU 31	531	471	3449	-12.69	16.19	-0.03
32	SLU 32	531	471	3449	-12.69	16.19	-0.03
32	SLU 33	531	471	3449	-12.69	16.19	-0.03
32	SLU 34	531	471	3449	-12.69	16.19	-0.03
32	SLU 35	531	471	3449	-12.69	16.19	-0.03
32	SLU 36	531	471	3449	-12.69	16.19	-0.03
32	SLU 37	531	471	3449	-12.69	16.19	-0.03
32	SLU 38	531	471	3449	-12.69	16.19	-0.03
32	SLU 39	574	494	3671	-13.21	17.67	-0.04
32	SLU 40	574	494	3671	-13.21	17.67	-0.04
32	SLU 41	574	494	3671	-13.21	17.67	-0.04
32	SLU 42	574	494	3671	-13.21	17.67	-0.04
32	SLU 43	468	483	3319	-13.61	13.47	0
32	SLU 44	468	483	3319	-13.61	13.47	0
32	SLU 45	468	483	3319	-13.61	13.47	0
32	SLU 46	468	483	3319	-13.61	13.47	0
32	SLU 47	468	483	3319	-13.61	13.47	0
32	SLU 48	468	483	3319	-13.61	13.47	0
32	SLU 49	468	483	3319	-13.61	13.47	0
32	SLU 50	468	483	3319	-13.61	13.47	0
32	SLU 51	468	483	3319	-13.61	13.47	0
32	SLU 52	569	538	3837	-14.82	16.94	-0.02
32	SLU 53	569	538	3837	-14.82	16.94	-0.02
32	SLU 54	569	538	3837	-14.82	16.94	-0.02
32	SLU 55	569	538	3837	-14.82	16.94	-0.02
32	SLU 56	569	538	3837	-14.82	16.94	-0.02
32	SLU 57	569	538	3837	-14.82	16.94	-0.02
32	SLU 58	569	538	3837	-14.82	16.94	-0.02
32	SLU 59	569	538	3837	-14.82	16.94	-0.02
32	SLU 60	612	562	4058	-15.34	18.43	-0.03
32	SLU 61	612	562	4058	-15.34	18.43	-0.03
32	SLU 62	612	562	4058	-15.34	18.43	-0.03
32	SLU 63	612	562	4058	-15.34	18.43	-0.03
32	SLU 64	524	517	3618	-14.41	15.33	-0.01
32	SLU 65	524	517	3618	-14.41	15.33	-0.01
32	SLU 66	524	517	3618	-14.41	15.33	-0.01
32	SLU 67	524	517	3618	-14.41	15.33	-0.01
32	SLU 68	524	517	3618	-14.41	15.33	-0.01
32	SLU 69	524	517	3618	-14.41	15.33	-0.01
32	SLU 70	524	517	3618	-14.41	15.33	-0.01
32	SLU 71	524	517	3618	-14.41	15.33	-0.01
32	SLU 72	524	517	3618	-14.41	15.33	-0.01
32	SLU 73	624	573	4136	-15.62	18.8	-0.03
32	SLU 74	624	573	4136	-15.62	18.8	-0.03
32	SLU 75	624	573	4136	-15.62	18.8	-0.03
32	SLU 76	624	573	4136	-15.62	18.8	-0.03
32	SLU 77	624	573	4136	-15.62	18.8	-0.03
32	SLU 78	624	573	4136	-15.62	18.8	-0.03
32	SLU 79	624	573	4136	-15.62	18.8	-0.03
32	SLU 80	624	573	4136	-15.62	18.8	-0.03
32	SLU 81	667	597	4358	-16.14	20.29	-0.04
32	SLU 82	667	597	4358	-16.14	20.29	-0.04
32	SLU 83	667	597	4358	-16.14	20.29	-0.04
32	SLU 84	667	597	4358	-16.14	20.29	-0.04
32	SLE RA 1	391	390	2717	-10.91	11.38	-0.01
32	SLE RA 2	391	390	2717	-10.91	11.38	-0.01
32	SLE RA 3	391	390	2717	-10.91	11.38	-0.01
32	SLE RA 4	391	390	2717	-10.91	11.38	-0.01
32	SLE RA 5	391	390	2717	-10.91	11.38	-0.01
32	SLE RA 6	391	390	2717	-10.91	11.38	-0.01
32	SLE RA 7	391	390	2717	-10.91	11.38	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
32	SLE RA 8	391	390	2717	-10.91	11.38	-0.01
32	SLE RA 9	391	390	2717	-10.91	11.38	-0.01
32	SLE RA 10	458	427	3063	-11.72	13.7	-0.02
32	SLE RA 11	458	427	3063	-11.72	13.7	-0.02
32	SLE RA 12	458	427	3063	-11.72	13.7	-0.02
32	SLE RA 13	458	427	3063	-11.72	13.7	-0.02
32	SLE RA 14	458	427	3063	-11.72	13.7	-0.02
32	SLE RA 15	458	427	3063	-11.72	13.7	-0.02
32	SLE RA 16	458	427	3063	-11.72	13.7	-0.02
32	SLE RA 17	458	427	3063	-11.72	13.7	-0.02
32	SLE RA 18	486	443	3210	-12.06	14.69	-0.02
32	SLE RA 19	486	443	3210	-12.06	14.69	-0.02
32	SLE RA 20	486	443	3210	-12.06	14.69	-0.02
32	SLE RA 21	486	443	3210	-12.06	14.69	-0.02
32	SLE FR 1	391	390	2717	-10.91	11.38	-0.01
32	SLE FR 2	391	390	2717	-10.91	11.38	-0.01
32	SLE FR 3	391	390	2717	-10.91	11.38	-0.01
32	SLE FR 4	419	406	2865	-11.26	12.38	-0.01
32	SLE FR 5	419	406	2865	-11.26	12.38	-0.01
32	SLE FR 6	438	417	2964	-11.49	13.04	-0.02
32	SLE QP 1	391	390	2717	-10.91	11.38	-0.01
32	SLE QP 2	419	406	2865	-11.26	12.38	-0.01
32	SLD 1	515	481	3327	-13.93	15.94	-0.03
32	SLD 2	515	481	3327	-13.93	15.94	-0.03
32	SLD 3	500	414	3094	-11.05	16.44	-0.06
32	SLD 4	500	414	3094	-11.05	16.44	-0.06
32	SLD 5	471	530	3358	-16.42	12.68	0.02
32	SLD 6	471	530	3358	-16.42	12.68	0.02
32	SLD 7	421	307	2580	-6.83	14.36	-0.07
32	SLD 8	421	307	2580	-6.83	14.36	-0.07
32	SLD 9	418	505	3151	-15.68	10.39	0.05
32	SLD 10	418	505	3151	-15.68	10.39	0.05
32	SLD 11	368	282	2373	-6.09	12.07	-0.05
32	SLD 12	368	282	2373	-6.09	12.07	-0.05
32	SLD 13	338	398	2637	-11.46	8.31	0.04
32	SLD 14	338	398	2637	-11.46	8.31	0.04
32	SLD 15	324	331	2403	-8.58	8.82	0.01
32	SLD 16	324	331	2403	-8.58	8.82	0.01
32	SLV 1	646	582	3954	-17.58	20.75	-0.06
32	SLV 2	646	582	3954	-17.58	20.75	-0.06
32	SLV 3	608	424	3395	-10.74	21.97	-0.13
32	SLV 4	608	424	3395	-10.74	21.97	-0.13
32	SLV 5	545	699	4040	-23.53	13.02	0.08
32	SLV 6	545	699	4040	-23.53	13.02	0.08
32	SLV 7	418	172	2176	-0.72	17.12	-0.15
32	SLV 8	418	172	2176	-0.72	17.12	-0.15
32	SLV 9	420	641	3555	-21.79	7.63	0.13
32	SLV 10	420	641	3555	-21.79	7.63	0.13
32	SLV 11	294	113	1690	1.02	11.73	-0.1
32	SLV 12	294	113	1690	1.02	11.73	-0.1
32	SLV 13	231	388	2335	-11.78	2.78	0.11
32	SLV 14	231	388	2335	-11.78	2.78	0.11
32	SLV 15	193	230	1776	-4.93	4.01	0.04
32	SLV 16	193	230	1776	-4.93	4.01	0.04
33	SLU 1	0	0	1016	0	0	0
33	SLU 2	0	0	1016	0	0	0
33	SLU 3	0	0	1016	0	0	0
33	SLU 4	0	0	1016	0	0	0
33	SLU 5	0	0	1016	0	0	0
33	SLU 6	0	0	1016	0	0	0
33	SLU 7	0	0	1016	0	0	0
33	SLU 8	0	0	1016	0	0	0
33	SLU 9	0	0	1016	0	0	0
33	SLU 10	0	0	1249	0	0	0
33	SLU 11	0	0	1249	0	0	0
33	SLU 12	0	0	1249	0	0	0
33	SLU 13	0	0	1249	0	0	0
33	SLU 14	0	0	1249	0	0	0
33	SLU 15	0	0	1249	0	0	0
33	SLU 16	0	0	1249	0	0	0
33	SLU 17	0	0	1249	0	0	0
33	SLU 18	0	0	1350	0	0	0
33	SLU 19	0	0	1350	0	0	0
33	SLU 20	0	0	1350	0	0	0
33	SLU 21	0	0	1350	0	0	0
33	SLU 22	0	0	1150	0	0	0
33	SLU 23	0	0	1150	0	0	0
33	SLU 24	0	0	1150	0	0	0
33	SLU 25	0	0	1150	0	0	0
33	SLU 26	0	0	1150	0	0	0
33	SLU 27	0	0	1150	0	0	0
33	SLU 28	0	0	1150	0	0	0
33	SLU 29	0	0	1150	0	0	0
33	SLU 30	0	0	1150	0	0	0
33	SLU 31	0	0	1384	0	0	0
33	SLU 32	0	0	1384	0	0	0
33	SLU 33	0	0	1384	0	0	0
33	SLU 34	0	0	1384	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
33	SLU 35	0	0	1384	0	0	0
33	SLU 36	0	0	1384	0	0	0
33	SLU 37	0	0	1384	0	0	0
33	SLU 38	0	0	1384	0	0	0
33	SLU 39	0	0	1484	0	0	0
33	SLU 40	0	0	1484	0	0	0
33	SLU 41	0	0	1484	0	0	0
33	SLU 42	0	0	1484	0	0	0
33	SLU 43	0	0	1274	0	0	0
33	SLU 44	0	0	1274	0	0	0
33	SLU 45	0	0	1274	0	0	0
33	SLU 46	0	0	1274	0	0	0
33	SLU 47	0	0	1274	0	0	0
33	SLU 48	0	0	1274	0	0	0
33	SLU 49	0	0	1274	0	0	0
33	SLU 50	0	0	1274	0	0	0
33	SLU 51	0	0	1274	0	0	0
33	SLU 52	0	0	1508	0	0	0
33	SLU 53	0	0	1508	0	0	0
33	SLU 54	0	0	1508	0	0	0
33	SLU 55	0	0	1508	0	0	0
33	SLU 56	0	0	1508	0	0	0
33	SLU 57	0	0	1508	0	0	0
33	SLU 58	0	0	1508	0	0	0
33	SLU 59	0	0	1508	0	0	0
33	SLU 60	0	0	1608	0	0	0
33	SLU 61	0	0	1608	0	0	0
33	SLU 62	0	0	1608	0	0	0
33	SLU 63	0	0	1608	0	0	0
33	SLU 64	0	0	1409	0	0	0
33	SLU 65	0	0	1409	0	0	0
33	SLU 66	0	0	1409	0	0	0
33	SLU 67	0	0	1409	0	0	0
33	SLU 68	0	0	1409	0	0	0
33	SLU 69	0	0	1409	0	0	0
33	SLU 70	0	0	1409	0	0	0
33	SLU 71	0	0	1409	0	0	0
33	SLU 72	0	0	1409	0	0	0
33	SLU 73	0	0	1642	0	0	0
33	SLU 74	0	0	1642	0	0	0
33	SLU 75	0	0	1642	0	0	0
33	SLU 76	0	0	1642	0	0	0
33	SLU 77	0	0	1642	0	0	0
33	SLU 78	0	0	1642	0	0	0
33	SLU 79	0	0	1642	0	0	0
33	SLU 80	0	0	1642	0	0	0
33	SLU 81	0	0	1742	0	0	0
33	SLU 82	0	0	1742	0	0	0
33	SLU 83	0	0	1742	0	0	0
33	SLU 84	0	0	1742	0	0	0
33	SLE RA 1	0	0	1054	0	0	0
33	SLE RA 2	0	0	1054	0	0	0
33	SLE RA 3	0	0	1054	0	0	0
33	SLE RA 4	0	0	1054	0	0	0
33	SLE RA 5	0	0	1054	0	0	0
33	SLE RA 6	0	0	1054	0	0	0
33	SLE RA 7	0	0	1054	0	0	0
33	SLE RA 8	0	0	1054	0	0	0
33	SLE RA 9	0	0	1054	0	0	0
33	SLE RA 10	0	0	1210	0	0	0
33	SLE RA 11	0	0	1210	0	0	0
33	SLE RA 12	0	0	1210	0	0	0
33	SLE RA 13	0	0	1210	0	0	0
33	SLE RA 14	0	0	1210	0	0	0
33	SLE RA 15	0	0	1210	0	0	0
33	SLE RA 16	0	0	1210	0	0	0
33	SLE RA 17	0	0	1210	0	0	0
33	SLE RA 18	0	0	1277	0	0	0
33	SLE RA 19	0	0	1277	0	0	0
33	SLE RA 20	0	0	1277	0	0	0
33	SLE RA 21	0	0	1277	0	0	0
33	SLE FR 1	0	0	1054	0	0	0
33	SLE FR 2	0	0	1054	0	0	0
33	SLE FR 3	0	0	1054	0	0	0
33	SLE FR 4	0	0	1121	0	0	0
33	SLE FR 5	0	0	1121	0	0	0
33	SLE FR 6	0	0	1165	0	0	0
33	SLE QP 1	0	0	1054	0	0	0
33	SLE QP 2	0	0	1121	0	0	0
33	SLD 1	1	0	1074	0.19	0.92	0
33	SLD 2	1	0	1074	0.19	0.92	0
33	SLD 3	1	-1	1158	-0.19	0.86	0
33	SLD 4	1	-1	1158	-0.19	0.86	0
33	SLD 5	0	2	979	0.62	0.37	0
33	SLD 6	0	2	979	0.62	0.37	0
33	SLD 7	0	-2	1260	-0.62	0.17	0
33	SLD 8	0	-2	1260	-0.62	0.17	0
33	SLD 9	0	2	982	0.62	-0.17	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
33	SLD 10	0	2	982	0.62	-0.17	0
33	SLD 11	0	-2	1263	-0.62	-0.36	0
33	SLD 12	0	-2	1263	-0.62	-0.36	0
33	SLD 13	-1	1	1083	0.19	-0.86	0
33	SLD 14	-1	1	1083	0.19	-0.86	0
33	SLD 15	-1	0	1168	-0.18	-0.92	0
33	SLD 16	-1	0	1168	-0.18	-0.92	0
33	SLV 1	2	1	991	0.52	2.35	0
33	SLV 2	2	1	991	0.52	2.35	0
33	SLV 3	2	-3	1229	-0.53	2.19	0
33	SLV 4	2	-3	1229	-0.53	2.19	0
33	SLV 5	0	6	722	1.75	0.94	0
33	SLV 6	0	6	722	1.75	0.94	0
33	SLV 7	1	-7	1513	-1.75	0.42	0
33	SLV 8	1	-7	1513	-1.75	0.42	0
33	SLV 9	-1	7	728	1.75	-0.42	0
33	SLV 10	-1	7	728	1.75	-0.42	0
33	SLV 11	0	-6	1520	-1.74	-0.94	0
33	SLV 12	0	-6	1520	-1.74	-0.94	0
33	SLV 13	-2	3	1013	0.53	-2.19	0
33	SLV 14	-2	3	1013	0.53	-2.19	0
33	SLV 15	-2	-1	1250	-0.52	-2.35	0
33	SLV 16	-2	-1	1250	-0.52	-2.35	0
34	SLU 1	3	282	2116	-16.25	0.87	0.01
34	SLU 2	3	282	2116	-16.25	0.87	0.01
34	SLU 3	3	282	2116	-16.25	0.87	0.01
34	SLU 4	3	282	2116	-16.25	0.87	0.01
34	SLU 5	3	282	2116	-16.25	0.87	0.01
34	SLU 6	3	282	2116	-16.25	0.87	0.01
34	SLU 7	3	282	2116	-16.25	0.87	0.01
34	SLU 8	3	282	2116	-16.25	0.87	0.01
34	SLU 9	3	282	2116	-16.25	0.87	0.01
34	SLU 10	3	300	2502	-17.77	1.12	0.01
34	SLU 11	3	300	2502	-17.77	1.12	0.01
34	SLU 12	3	300	2502	-17.77	1.12	0.01
34	SLU 13	3	300	2502	-17.77	1.12	0.01
34	SLU 14	3	300	2502	-17.77	1.12	0.01
34	SLU 15	3	300	2502	-17.77	1.12	0.01
34	SLU 16	3	300	2502	-17.77	1.12	0.01
34	SLU 17	3	300	2502	-17.77	1.12	0.01
34	SLU 18	4	307	2667	-18.43	1.23	0.01
34	SLU 19	4	307	2667	-18.43	1.23	0.01
34	SLU 20	4	307	2667	-18.43	1.23	0.01
34	SLU 21	4	307	2667	-18.43	1.23	0.01
34	SLU 22	3	297	2342	-17.33	1.01	0.01
34	SLU 23	3	297	2342	-17.33	1.01	0.01
34	SLU 24	3	297	2342	-17.33	1.01	0.01
34	SLU 25	3	297	2342	-17.33	1.01	0.01
34	SLU 26	3	297	2342	-17.33	1.01	0.01
34	SLU 27	3	297	2342	-17.33	1.01	0.01
34	SLU 28	3	297	2342	-17.33	1.01	0.01
34	SLU 29	3	297	2342	-17.33	1.01	0.01
34	SLU 30	3	297	2342	-17.33	1.01	0.01
34	SLU 31	4	314	2728	-18.85	1.25	0.01
34	SLU 32	4	314	2728	-18.85	1.25	0.01
34	SLU 33	4	314	2728	-18.85	1.25	0.01
34	SLU 34	4	314	2728	-18.85	1.25	0.01
34	SLU 35	4	314	2728	-18.85	1.25	0.01
34	SLU 36	4	314	2728	-18.85	1.25	0.01
34	SLU 37	4	314	2728	-18.85	1.25	0.01
34	SLU 38	4	314	2728	-18.85	1.25	0.01
34	SLU 39	4	322	2893	-19.5	1.36	0.01
34	SLU 40	4	322	2893	-19.5	1.36	0.01
34	SLU 41	4	322	2893	-19.5	1.36	0.01
34	SLU 42	4	322	2893	-19.5	1.36	0.01
34	SLU 43	3	362	2673	-20.76	1.08	0.01
34	SLU 44	3	362	2673	-20.76	1.08	0.01
34	SLU 45	3	362	2673	-20.76	1.08	0.01
34	SLU 46	3	362	2673	-20.76	1.08	0.01
34	SLU 47	3	362	2673	-20.76	1.08	0.01
34	SLU 48	3	362	2673	-20.76	1.08	0.01
34	SLU 49	3	362	2673	-20.76	1.08	0.01
34	SLU 50	3	362	2673	-20.76	1.08	0.01
34	SLU 51	3	362	2673	-20.76	1.08	0.01
34	SLU 52	4	379	3059	-22.28	1.33	0.01
34	SLU 53	4	379	3059	-22.28	1.33	0.01
34	SLU 54	4	379	3059	-22.28	1.33	0.01
34	SLU 55	4	379	3059	-22.28	1.33	0.01
34	SLU 56	4	379	3059	-22.28	1.33	0.01
34	SLU 57	4	379	3059	-22.28	1.33	0.01
34	SLU 58	4	379	3059	-22.28	1.33	0.01
34	SLU 59	4	379	3059	-22.28	1.33	0.01
34	SLU 60	4	387	3225	-22.93	1.44	0.02
34	SLU 61	4	387	3225	-22.93	1.44	0.02
34	SLU 62	4	387	3225	-22.93	1.44	0.02
34	SLU 63	4	387	3225	-22.93	1.44	0.02
34	SLU 64	4	376	2899	-21.84	1.22	0.01
34	SLU 65	4	376	2899	-21.84	1.22	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
34	SLU 66	4	376	2899	-21.84	1.22	0.01
34	SLU 67	4	376	2899	-21.84	1.22	0.01
34	SLU 68	4	376	2899	-21.84	1.22	0.01
34	SLU 69	4	376	2899	-21.84	1.22	0.01
34	SLU 70	4	376	2899	-21.84	1.22	0.01
34	SLU 71	4	376	2899	-21.84	1.22	0.01
34	SLU 72	4	376	2899	-21.84	1.22	0.01
34	SLU 73	4	394	3285	-23.36	1.47	0.02
34	SLU 74	4	394	3285	-23.36	1.47	0.02
34	SLU 75	4	394	3285	-23.36	1.47	0.02
34	SLU 76	4	394	3285	-23.36	1.47	0.02
34	SLU 77	4	394	3285	-23.36	1.47	0.02
34	SLU 78	4	394	3285	-23.36	1.47	0.02
34	SLU 79	4	394	3285	-23.36	1.47	0.02
34	SLU 80	4	394	3285	-23.36	1.47	0.02
34	SLU 81	5	401	3451	-24.01	1.58	0.02
34	SLU 82	5	401	3451	-24.01	1.58	0.02
34	SLU 83	5	401	3451	-24.01	1.58	0.02
34	SLU 84	5	401	3451	-24.01	1.58	0.02
34	SLE RA 1	3	286	2181	-16.56	0.91	0.01
34	SLE RA 2	3	286	2181	-16.56	0.91	0.01
34	SLE RA 3	3	286	2181	-16.56	0.91	0.01
34	SLE RA 4	3	286	2181	-16.56	0.91	0.01
34	SLE RA 5	3	286	2181	-16.56	0.91	0.01
34	SLE RA 6	3	286	2181	-16.56	0.91	0.01
34	SLE RA 7	3	286	2181	-16.56	0.91	0.01
34	SLE RA 8	3	286	2181	-16.56	0.91	0.01
34	SLE RA 9	3	286	2181	-16.56	0.91	0.01
34	SLE RA 10	3	298	2438	-17.58	1.07	0.01
34	SLE RA 11	3	298	2438	-17.58	1.07	0.01
34	SLE RA 12	3	298	2438	-17.58	1.07	0.01
34	SLE RA 13	3	298	2438	-17.58	1.07	0.01
34	SLE RA 14	3	298	2438	-17.58	1.07	0.01
34	SLE RA 15	3	298	2438	-17.58	1.07	0.01
34	SLE RA 16	3	298	2438	-17.58	1.07	0.01
34	SLE RA 17	3	298	2438	-17.58	1.07	0.01
34	SLE RA 18	3	303	2548	-18.01	1.15	0.01
34	SLE RA 19	3	303	2548	-18.01	1.15	0.01
34	SLE RA 20	3	303	2548	-18.01	1.15	0.01
34	SLE RA 21	3	303	2548	-18.01	1.15	0.01
34	SLE FR 1	3	286	2181	-16.56	0.91	0.01
34	SLE FR 2	3	286	2181	-16.56	0.91	0.01
34	SLE FR 3	3	286	2181	-16.56	0.91	0.01
34	SLE FR 4	3	291	2291	-17	0.98	0.01
34	SLE FR 5	3	291	2291	-17	0.98	0.01
34	SLE FR 6	3	295	2364	-17.29	1.03	0.01
34	SLE QP 1	3	286	2181	-16.56	0.91	0.01
34	SLE QP 2	3	291	2291	-17	0.98	0.01
34	SLD 1	4	383	2619	-21.65	3.39	0.02
34	SLD 2	4	383	2619	-21.65	3.39	0.02
34	SLD 3	11	288	2469	-16.39	7.22	0.01
34	SLD 4	11	288	2469	-16.39	7.22	0.01
34	SLD 5	-8	464	2617	-26.37	-4.1	0.03
34	SLD 6	-8	464	2617	-26.37	-4.1	0.03
34	SLD 7	17	145	2117	-8.84	8.65	-0.01
34	SLD 8	17	145	2117	-8.84	8.65	-0.01
34	SLD 9	-11	437	2465	-25.15	-6.69	0.03
34	SLD 10	-11	437	2465	-25.15	-6.69	0.03
34	SLD 11	14	119	1965	-7.62	6.06	-0.01
34	SLD 12	14	119	1965	-7.62	6.06	-0.01
34	SLD 13	-5	295	2113	-17.6	-5.26	0.01
34	SLD 14	-5	295	2113	-17.6	-5.26	0.01
34	SLD 15	2	199	1963	-12.34	-1.43	0
34	SLD 16	2	199	1963	-12.34	-1.43	0
34	SLV 1	5	509	3064	-28	6.71	0.04
34	SLV 2	5	509	3064	-28	6.71	0.04
34	SLV 3	24	282	2703	-15.51	16.54	0.01
34	SLV 4	24	282	2703	-15.51	16.54	0.01
34	SLV 5	-25	700	3071	-39.24	-12.21	0.07
34	SLV 6	-25	700	3071	-39.24	-12.21	0.07
34	SLV 7	38	-55	1867	2.39	20.55	-0.04
34	SLV 8	38	-55	1867	2.39	20.55	-0.04
34	SLV 9	-32	638	2715	-36.39	-18.59	0.06
34	SLV 10	-32	638	2715	-36.39	-18.59	0.06
34	SLV 11	31	-117	1511	5.25	14.17	-0.05
34	SLV 12	31	-117	1511	5.25	14.17	-0.05
34	SLV 13	-18	300	1879	-18.48	-14.58	0.01
34	SLV 14	-18	300	1879	-18.48	-14.58	0.01
34	SLV 15	1	74	1517	-5.99	-4.75	-0.02
34	SLV 16	1	74	1517	-5.99	-4.75	-0.02
35	SLU 1	-3	286	2289	-16.2	-0.9	-0.01
35	SLU 2	-3	286	2289	-16.2	-0.9	-0.01
35	SLU 3	-3	286	2289	-16.2	-0.9	-0.01
35	SLU 4	-3	286	2289	-16.2	-0.9	-0.01
35	SLU 5	-3	286	2289	-16.2	-0.9	-0.01
35	SLU 6	-3	286	2289	-16.2	-0.9	-0.01
35	SLU 7	-3	286	2289	-16.2	-0.9	-0.01
35	SLU 8	-3	286	2289	-16.2	-0.9	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
35	SLU 9	-3	286	2289	-16.2	-0.9	-0.01
35	SLU 10	-3	297	2697	-17.38	-1.16	-0.01
35	SLU 11	-3	297	2697	-17.38	-1.16	-0.01
35	SLU 12	-3	297	2697	-17.38	-1.16	-0.01
35	SLU 13	-3	297	2697	-17.38	-1.16	-0.01
35	SLU 14	-3	297	2697	-17.38	-1.16	-0.01
35	SLU 15	-3	297	2697	-17.38	-1.16	-0.01
35	SLU 16	-3	297	2697	-17.38	-1.16	-0.01
35	SLU 17	-3	297	2697	-17.38	-1.16	-0.01
35	SLU 18	-3	301	2872	-17.88	-1.27	-0.01
35	SLU 19	-3	301	2872	-17.88	-1.27	-0.01
35	SLU 20	-3	301	2872	-17.88	-1.27	-0.01
35	SLU 21	-3	301	2872	-17.88	-1.27	-0.01
35	SLU 22	-3	297	2529	-17.1	-1.04	-0.01
35	SLU 23	-3	297	2529	-17.1	-1.04	-0.01
35	SLU 24	-3	297	2529	-17.1	-1.04	-0.01
35	SLU 25	-3	297	2529	-17.1	-1.04	-0.01
35	SLU 26	-3	297	2529	-17.1	-1.04	-0.01
35	SLU 27	-3	297	2529	-17.1	-1.04	-0.01
35	SLU 28	-3	297	2529	-17.1	-1.04	-0.01
35	SLU 29	-3	297	2529	-17.1	-1.04	-0.01
35	SLU 30	-3	297	2529	-17.1	-1.04	-0.01
35	SLU 31	-4	308	2937	-18.28	-1.3	-0.01
35	SLU 32	-4	308	2937	-18.28	-1.3	-0.01
35	SLU 33	-4	308	2937	-18.28	-1.3	-0.01
35	SLU 34	-4	308	2937	-18.28	-1.3	-0.01
35	SLU 35	-4	308	2937	-18.28	-1.3	-0.01
35	SLU 36	-4	308	2937	-18.28	-1.3	-0.01
35	SLU 37	-4	308	2937	-18.28	-1.3	-0.01
35	SLU 38	-4	308	2937	-18.28	-1.3	-0.01
35	SLU 39	-4	312	3112	-18.79	-1.41	-0.02
35	SLU 40	-4	312	3112	-18.79	-1.41	-0.02
35	SLU 41	-4	312	3112	-18.79	-1.41	-0.02
35	SLU 42	-4	312	3112	-18.79	-1.41	-0.02
35	SLU 43	-3	369	2894	-20.74	-1.12	-0.01
35	SLU 44	-3	369	2894	-20.74	-1.12	-0.01
35	SLU 45	-3	369	2894	-20.74	-1.12	-0.01
35	SLU 46	-3	369	2894	-20.74	-1.12	-0.01
35	SLU 47	-3	369	2894	-20.74	-1.12	-0.01
35	SLU 48	-3	369	2894	-20.74	-1.12	-0.01
35	SLU 49	-3	369	2894	-20.74	-1.12	-0.01
35	SLU 50	-3	369	2894	-20.74	-1.12	-0.01
35	SLU 51	-3	369	2894	-20.74	-1.12	-0.01
35	SLU 52	-4	379	3302	-21.93	-1.38	-0.02
35	SLU 53	-4	379	3302	-21.93	-1.38	-0.02
35	SLU 54	-4	379	3302	-21.93	-1.38	-0.02
35	SLU 55	-4	379	3302	-21.93	-1.38	-0.02
35	SLU 56	-4	379	3302	-21.93	-1.38	-0.02
35	SLU 57	-4	379	3302	-21.93	-1.38	-0.02
35	SLU 58	-4	379	3302	-21.93	-1.38	-0.02
35	SLU 59	-4	379	3302	-21.93	-1.38	-0.02
35	SLU 60	-4	383	3476	-22.43	-1.49	-0.02
35	SLU 61	-4	383	3476	-22.43	-1.49	-0.02
35	SLU 62	-4	383	3476	-22.43	-1.49	-0.02
35	SLU 63	-4	383	3476	-22.43	-1.49	-0.02
35	SLU 64	-4	380	3133	-21.65	-1.26	-0.01
35	SLU 65	-4	380	3133	-21.65	-1.26	-0.01
35	SLU 66	-4	380	3133	-21.65	-1.26	-0.01
35	SLU 67	-4	380	3133	-21.65	-1.26	-0.01
35	SLU 68	-4	380	3133	-21.65	-1.26	-0.01
35	SLU 69	-4	380	3133	-21.65	-1.26	-0.01
35	SLU 70	-4	380	3133	-21.65	-1.26	-0.01
35	SLU 71	-4	380	3133	-21.65	-1.26	-0.01
35	SLU 72	-4	380	3133	-21.65	-1.26	-0.01
35	SLU 73	-4	390	3541	-22.83	-1.52	-0.02
35	SLU 74	-4	390	3541	-22.83	-1.52	-0.02
35	SLU 75	-4	390	3541	-22.83	-1.52	-0.02
35	SLU 76	-4	390	3541	-22.83	-1.52	-0.02
35	SLU 77	-4	390	3541	-22.83	-1.52	-0.02
35	SLU 78	-4	390	3541	-22.83	-1.52	-0.02
35	SLU 79	-4	390	3541	-22.83	-1.52	-0.02
35	SLU 80	-4	390	3541	-22.83	-1.52	-0.02
35	SLU 81	-4	394	3716	-23.34	-1.63	-0.02
35	SLU 82	-4	394	3716	-23.34	-1.63	-0.02
35	SLU 83	-4	394	3716	-23.34	-1.63	-0.02
35	SLU 84	-4	394	3716	-23.34	-1.63	-0.02
35	SLE RA 1	-3	290	2357	-16.45	-0.94	-0.01
35	SLE RA 2	-3	290	2357	-16.45	-0.94	-0.01
35	SLE RA 3	-3	290	2357	-16.45	-0.94	-0.01
35	SLE RA 4	-3	290	2357	-16.45	-0.94	-0.01
35	SLE RA 5	-3	290	2357	-16.45	-0.94	-0.01
35	SLE RA 6	-3	290	2357	-16.45	-0.94	-0.01
35	SLE RA 7	-3	290	2357	-16.45	-0.94	-0.01
35	SLE RA 8	-3	290	2357	-16.45	-0.94	-0.01
35	SLE RA 9	-3	290	2357	-16.45	-0.94	-0.01
35	SLE RA 10	-3	297	2629	-17.24	-1.11	-0.01
35	SLE RA 11	-3	297	2629	-17.24	-1.11	-0.01
35	SLE RA 12	-3	297	2629	-17.24	-1.11	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
35	SLE RA 13	-3	297	2629	-17.24	-1.11	-0.01
35	SLE RA 14	-3	297	2629	-17.24	-1.11	-0.01
35	SLE RA 15	-3	297	2629	-17.24	-1.11	-0.01
35	SLE RA 16	-3	297	2629	-17.24	-1.11	-0.01
35	SLE RA 17	-3	297	2629	-17.24	-1.11	-0.01
35	SLE RA 18	-3	300	2746	-17.58	-1.19	-0.01
35	SLE RA 19	-3	300	2746	-17.58	-1.19	-0.01
35	SLE RA 20	-3	300	2746	-17.58	-1.19	-0.01
35	SLE RA 21	-3	300	2746	-17.58	-1.19	-0.01
35	SLE FR 1	-3	290	2357	-16.45	-0.94	-0.01
35	SLE FR 2	-3	290	2357	-16.45	-0.94	-0.01
35	SLE FR 3	-3	290	2357	-16.45	-0.94	-0.01
35	SLE FR 4	-3	293	2474	-16.79	-1.01	-0.01
35	SLE FR 5	-3	293	2474	-16.79	-1.01	-0.01
35	SLE FR 6	-3	295	2552	-17.02	-1.06	-0.01
35	SLE QP 1	-3	290	2357	-16.45	-0.94	-0.01
35	SLE QP 2	-3	293	2474	-16.79	-1.01	-0.01
35	SLD 1	7	303	2288	-17.86	6.38	-0.01
35	SLD 2	7	303	2288	-17.86	6.38	-0.01
35	SLD 3	-1	190	2121	-11.83	2.19	0
35	SLD 4	-1	190	2121	-11.83	2.19	0
35	SLD 5	12	466	2673	-26.26	7.56	-0.03
35	SLD 6	12	466	2673	-26.26	7.56	-0.03
35	SLD 7	-15	92	2114	-6.15	-6.41	0.01
35	SLD 8	-15	92	2114	-6.15	-6.41	0.01
35	SLD 9	9	493	2834	-27.43	4.38	-0.03
35	SLD 10	9	493	2834	-27.43	4.38	-0.03
35	SLD 11	-18	119	2275	-7.32	-9.59	0.01
35	SLD 12	-18	119	2275	-7.32	-9.59	0.01
35	SLD 13	-4	395	2827	-21.75	-4.22	-0.02
35	SLD 14	-4	395	2827	-21.75	-4.22	-0.02
35	SLD 15	-12	283	2660	-15.72	-8.41	-0.01
35	SLD 16	-12	283	2660	-15.72	-8.41	-0.01
35	SLV 1	21	317	2046	-19.39	17.46	-0.01
35	SLV 2	21	317	2046	-19.39	17.46	-0.01
35	SLV 3	0	50	1641	-5.03	6.64	0.02
35	SLV 4	0	50	1641	-5.03	6.64	0.02
35	SLV 5	36	704	2960	-39.36	20.95	-0.06
35	SLV 6	36	704	2960	-39.36	20.95	-0.06
35	SLV 7	-34	-185	1610	8.52	-15.14	0.05
35	SLV 8	-34	-185	1610	8.52	-15.14	0.05
35	SLV 9	28	770	3338	-42.11	13.11	-0.07
35	SLV 10	28	770	3338	-42.11	13.11	-0.07
35	SLV 11	-42	-119	1988	5.77	-22.98	0.04
35	SLV 12	-42	-119	1988	5.77	-22.98	0.04
35	SLV 13	-6	535	3307	-28.56	-8.66	-0.05
35	SLV 14	-6	535	3307	-28.56	-8.66	-0.05
35	SLV 15	-27	268	2902	-14.19	-19.49	-0.01
35	SLV 16	-27	268	2902	-14.19	-19.49	-0.01
36	SLU 1	0	0	1043	0	0	0
36	SLU 2	0	0	1043	0	0	0
36	SLU 3	0	0	1043	0	0	0
36	SLU 4	0	0	1043	0	0	0
36	SLU 5	0	0	1043	0	0	0
36	SLU 6	0	0	1043	0	0	0
36	SLU 7	0	0	1043	0	0	0
36	SLU 8	0	0	1043	0	0	0
36	SLU 9	0	0	1043	0	0	0
36	SLU 10	0	0	1268	0	0	0
36	SLU 11	0	0	1268	0	0	0
36	SLU 12	0	0	1268	0	0	0
36	SLU 13	0	0	1268	0	0	0
36	SLU 14	0	0	1268	0	0	0
36	SLU 15	0	0	1268	0	0	0
36	SLU 16	0	0	1268	0	0	0
36	SLU 17	0	0	1268	0	0	0
36	SLU 18	0	0	1365	0	0	0
36	SLU 19	0	0	1365	0	0	0
36	SLU 20	0	0	1365	0	0	0
36	SLU 21	0	0	1365	0	0	0
36	SLU 22	0	0	1174	0	0	0
36	SLU 23	0	0	1174	0	0	0
36	SLU 24	0	0	1174	0	0	0
36	SLU 25	0	0	1174	0	0	0
36	SLU 26	0	0	1174	0	0	0
36	SLU 27	0	0	1174	0	0	0
36	SLU 28	0	0	1174	0	0	0
36	SLU 29	0	0	1174	0	0	0
36	SLU 30	0	0	1174	0	0	0
36	SLU 31	0	0	1399	0	0	0
36	SLU 32	0	0	1399	0	0	0
36	SLU 33	0	0	1399	0	0	0
36	SLU 34	0	0	1399	0	0	0
36	SLU 35	0	0	1399	0	0	0
36	SLU 36	0	0	1399	0	0	0
36	SLU 37	0	0	1399	0	0	0
36	SLU 38	0	0	1399	0	0	0
36	SLU 39	0	0	1495	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
36	SLU 40	0	0	1495	0	0	0
36	SLU 41	0	0	1495	0	0	0
36	SLU 42	0	0	1495	0	0	0
36	SLU 43	0	0	1312	0	0	0
36	SLU 44	0	0	1312	0	0	0
36	SLU 45	0	0	1312	0	0	0
36	SLU 46	0	0	1312	0	0	0
36	SLU 47	0	0	1312	0	0	0
36	SLU 48	0	0	1312	0	0	0
36	SLU 49	0	0	1312	0	0	0
36	SLU 50	0	0	1312	0	0	0
36	SLU 51	0	0	1312	0	0	0
36	SLU 52	0	0	1536	0	0	0
36	SLU 53	0	0	1536	0	0	0
36	SLU 54	0	0	1536	0	0	0
36	SLU 55	0	0	1536	0	0	0
36	SLU 56	0	0	1536	0	0	0
36	SLU 57	0	0	1536	0	0	0
36	SLU 58	0	0	1536	0	0	0
36	SLU 59	0	0	1536	0	0	0
36	SLU 60	0	0	1633	0	0	0
36	SLU 61	0	0	1633	0	0	0
36	SLU 62	0	0	1633	0	0	0
36	SLU 63	0	0	1633	0	0	0
36	SLU 64	0	0	1442	0	0	0
36	SLU 65	0	0	1442	0	0	0
36	SLU 66	0	0	1442	0	0	0
36	SLU 67	0	0	1442	0	0	0
36	SLU 68	0	0	1442	0	0	0
36	SLU 69	0	0	1442	0	0	0
36	SLU 70	0	0	1442	0	0	0
36	SLU 71	0	0	1442	0	0	0
36	SLU 72	0	0	1442	0	0	0
36	SLU 73	0	0	1667	0	0	0
36	SLU 74	0	0	1667	0	0	0
36	SLU 75	0	0	1667	0	0	0
36	SLU 76	0	0	1667	0	0	0
36	SLU 77	0	0	1667	0	0	0
36	SLU 78	0	0	1667	0	0	0
36	SLU 79	0	0	1667	0	0	0
36	SLU 80	0	0	1667	0	0	0
36	SLU 81	0	0	1764	0	0	0
36	SLU 82	0	0	1764	0	0	0
36	SLU 83	0	0	1764	0	0	0
36	SLU 84	0	0	1764	0	0	0
36	SLE RA 1	0	0	1081	0	0	0
36	SLE RA 2	0	0	1081	0	0	0
36	SLE RA 3	0	0	1081	0	0	0
36	SLE RA 4	0	0	1081	0	0	0
36	SLE RA 5	0	0	1081	0	0	0
36	SLE RA 6	0	0	1081	0	0	0
36	SLE RA 7	0	0	1081	0	0	0
36	SLE RA 8	0	0	1081	0	0	0
36	SLE RA 9	0	0	1081	0	0	0
36	SLE RA 10	0	0	1231	0	0	0
36	SLE RA 11	0	0	1231	0	0	0
36	SLE RA 12	0	0	1231	0	0	0
36	SLE RA 13	0	0	1231	0	0	0
36	SLE RA 14	0	0	1231	0	0	0
36	SLE RA 15	0	0	1231	0	0	0
36	SLE RA 16	0	0	1231	0	0	0
36	SLE RA 17	0	0	1231	0	0	0
36	SLE RA 18	0	0	1295	0	0	0
36	SLE RA 19	0	0	1295	0	0	0
36	SLE RA 20	0	0	1295	0	0	0
36	SLE RA 21	0	0	1295	0	0	0
36	SLE FR 1	0	0	1081	0	0	0
36	SLE FR 2	0	0	1081	0	0	0
36	SLE FR 3	0	0	1081	0	0	0
36	SLE FR 4	0	0	1145	0	0	0
36	SLE FR 5	0	0	1145	0	0	0
36	SLE FR 6	0	0	1188	0	0	0
36	SLE QP 1	0	0	1081	0	0	0
36	SLE QP 2	0	0	1145	0	0	0
36	SLD 1	-2	1	1126	-0.06	2.34	0
36	SLD 2	-2	1	1126	-0.06	2.34	0
36	SLD 3	-1	0	1153	0.06	2.22	0
36	SLD 4	-1	0	1153	0.06	2.22	0
36	SLD 5	-1	2	1098	-0.2	0.89	0
36	SLD 6	-1	2	1098	-0.2	0.89	0
36	SLD 7	0	-2	1188	0.2	0.48	0
36	SLD 8	0	-2	1188	0.2	0.48	0
36	SLD 9	0	2	1102	-0.2	-0.48	0
36	SLD 10	0	2	1102	-0.2	-0.48	0
36	SLD 11	1	-2	1192	0.2	-0.89	0
36	SLD 12	1	-2	1192	0.2	-0.89	0
36	SLD 13	1	0	1137	-0.06	-2.22	0
36	SLD 14	1	0	1137	-0.06	-2.22	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
36	SLD 15	2	-1	1164	0.06	-2.34	0
36	SLD 16	2	-1	1164	0.06	-2.34	0
36	SLV 1	-4	3	1094	-0.17	5.97	0
36	SLV 2	-4	3	1094	-0.17	5.97	0
36	SLV 3	-4	0	1169	0.17	5.65	0
36	SLV 4	-4	0	1169	0.17	5.65	0
36	SLV 5	-2	6	1015	-0.57	2.27	0
36	SLV 6	-2	6	1015	-0.57	2.27	0
36	SLV 7	-1	-5	1266	0.56	1.22	0
36	SLV 8	-1	-5	1266	0.56	1.22	0
36	SLV 9	1	5	1024	-0.57	-1.22	0
36	SLV 10	1	5	1024	-0.57	-1.22	0
36	SLV 11	2	-6	1275	0.56	-2.27	0
36	SLV 12	2	-6	1275	0.56	-2.27	0
36	SLV 13	4	0	1121	-0.17	-5.65	0
36	SLV 14	4	0	1121	-0.17	-5.65	0
36	SLV 15	4	-3	1196	0.17	-5.97	0
36	SLV 16	4	-3	1196	0.17	-5.97	0
37	SLU 1	0	230	1948	-11.78	0.46	0
37	SLU 2	0	230	1948	-11.78	0.46	0
37	SLU 3	0	230	1948	-11.78	0.46	0
37	SLU 4	0	230	1948	-11.78	0.46	0
37	SLU 5	0	230	1948	-11.78	0.46	0
37	SLU 6	0	230	1948	-11.78	0.46	0
37	SLU 7	0	230	1948	-11.78	0.46	0
37	SLU 8	0	230	1948	-11.78	0.46	0
37	SLU 9	0	230	1948	-11.78	0.46	0
37	SLU 10	1	243	2274	-12.63	0.59	0
37	SLU 11	1	243	2274	-12.63	0.59	0
37	SLU 12	1	243	2274	-12.63	0.59	0
37	SLU 13	1	243	2274	-12.63	0.59	0
37	SLU 14	1	243	2274	-12.63	0.59	0
37	SLU 15	1	243	2274	-12.63	0.59	0
37	SLU 16	1	243	2274	-12.63	0.59	0
37	SLU 17	1	243	2274	-12.63	0.59	0
37	SLU 18	1	248	2413	-12.99	0.65	0
37	SLU 19	1	248	2413	-12.99	0.65	0
37	SLU 20	1	248	2413	-12.99	0.65	0
37	SLU 21	1	248	2413	-12.99	0.65	0
37	SLU 22	0	241	2142	-12.45	0.53	0
37	SLU 23	0	241	2142	-12.45	0.53	0
37	SLU 24	0	241	2142	-12.45	0.53	0
37	SLU 25	0	241	2142	-12.45	0.53	0
37	SLU 26	0	241	2142	-12.45	0.53	0
37	SLU 27	0	241	2142	-12.45	0.53	0
37	SLU 28	0	241	2142	-12.45	0.53	0
37	SLU 29	0	241	2142	-12.45	0.53	0
37	SLU 30	0	241	2142	-12.45	0.53	0
37	SLU 31	1	254	2467	-13.3	0.67	0
37	SLU 32	1	254	2467	-13.3	0.67	0
37	SLU 33	1	254	2467	-13.3	0.67	0
37	SLU 34	1	254	2467	-13.3	0.67	0
37	SLU 35	1	254	2467	-13.3	0.67	0
37	SLU 36	1	254	2467	-13.3	0.67	0
37	SLU 37	1	254	2467	-13.3	0.67	0
37	SLU 38	1	254	2467	-13.3	0.67	0
37	SLU 39	1	259	2607	-13.67	0.73	0
37	SLU 40	1	259	2607	-13.67	0.73	0
37	SLU 41	1	259	2607	-13.67	0.73	0
37	SLU 42	1	259	2607	-13.67	0.73	0
37	SLU 43	1	295	2466	-15.08	0.57	0
37	SLU 44	1	295	2466	-15.08	0.57	0
37	SLU 45	1	295	2466	-15.08	0.57	0
37	SLU 46	1	295	2466	-15.08	0.57	0
37	SLU 47	1	295	2466	-15.08	0.57	0
37	SLU 48	1	295	2466	-15.08	0.57	0
37	SLU 49	1	295	2466	-15.08	0.57	0
37	SLU 50	1	295	2466	-15.08	0.57	0
37	SLU 51	1	295	2466	-15.08	0.57	0
37	SLU 52	1	308	2792	-15.93	0.7	0
37	SLU 53	1	308	2792	-15.93	0.7	0
37	SLU 54	1	308	2792	-15.93	0.7	0
37	SLU 55	1	308	2792	-15.93	0.7	0
37	SLU 56	1	308	2792	-15.93	0.7	0
37	SLU 57	1	308	2792	-15.93	0.7	0
37	SLU 58	1	308	2792	-15.93	0.7	0
37	SLU 59	1	308	2792	-15.93	0.7	0
37	SLU 60	1	313	2931	-16.29	0.76	0
37	SLU 61	1	313	2931	-16.29	0.76	0
37	SLU 62	1	313	2931	-16.29	0.76	0
37	SLU 63	1	313	2931	-16.29	0.76	0
37	SLU 64	1	307	2660	-15.75	0.64	0
37	SLU 65	1	307	2660	-15.75	0.64	0
37	SLU 66	1	307	2660	-15.75	0.64	0
37	SLU 67	1	307	2660	-15.75	0.64	0
37	SLU 68	1	307	2660	-15.75	0.64	0
37	SLU 69	1	307	2660	-15.75	0.64	0
37	SLU 70	1	307	2660	-15.75	0.64	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
37	SLU 71	1	307	2660	-15.75	0.64	0
37	SLU 72	1	307	2660	-15.75	0.64	0
37	SLU 73	1	319	2985	-16.6	0.78	0
37	SLU 74	1	319	2985	-16.6	0.78	0
37	SLU 75	1	319	2985	-16.6	0.78	0
37	SLU 76	1	319	2985	-16.6	0.78	0
37	SLU 77	1	319	2985	-16.6	0.78	0
37	SLU 78	1	319	2985	-16.6	0.78	0
37	SLU 79	1	319	2985	-16.6	0.78	0
37	SLU 80	1	319	2985	-16.6	0.78	0
37	SLU 81	1	324	3125	-16.97	0.84	-0.01
37	SLU 82	1	324	3125	-16.97	0.84	-0.01
37	SLU 83	1	324	3125	-16.97	0.84	-0.01
37	SLU 84	1	324	3125	-16.97	0.84	-0.01
37	SLE RA 1	0	233	2003	-11.97	0.48	0
37	SLE RA 2	0	233	2003	-11.97	0.48	0
37	SLE RA 3	0	233	2003	-11.97	0.48	0
37	SLE RA 4	0	233	2003	-11.97	0.48	0
37	SLE RA 5	0	233	2003	-11.97	0.48	0
37	SLE RA 6	0	233	2003	-11.97	0.48	0
37	SLE RA 7	0	233	2003	-11.97	0.48	0
37	SLE RA 8	0	233	2003	-11.97	0.48	0
37	SLE RA 9	0	233	2003	-11.97	0.48	0
37	SLE RA 10	0	242	2220	-12.54	0.57	0
37	SLE RA 11	0	242	2220	-12.54	0.57	0
37	SLE RA 12	0	242	2220	-12.54	0.57	0
37	SLE RA 13	0	242	2220	-12.54	0.57	0
37	SLE RA 14	0	242	2220	-12.54	0.57	0
37	SLE RA 15	0	242	2220	-12.54	0.57	0
37	SLE RA 16	0	242	2220	-12.54	0.57	0
37	SLE RA 17	0	242	2220	-12.54	0.57	0
37	SLE RA 18	1	245	2314	-12.78	0.61	0
37	SLE RA 19	1	245	2314	-12.78	0.61	0
37	SLE RA 20	1	245	2314	-12.78	0.61	0
37	SLE RA 21	1	245	2314	-12.78	0.61	0
37	SLE FR 1	0	233	2003	-11.97	0.48	0
37	SLE FR 2	0	233	2003	-11.97	0.48	0
37	SLE FR 3	0	233	2003	-11.97	0.48	0
37	SLE FR 4	0	237	2096	-12.21	0.52	0
37	SLE FR 5	0	237	2096	-12.21	0.52	0
37	SLE FR 6	0	239	2158	-12.37	0.54	0
37	SLE QP 1	0	233	2003	-11.97	0.48	0
37	SLE QP 2	0	237	2096	-12.21	0.52	0
37	SLD 1	3	320	2357	-16.27	6.27	-0.02
37	SLD 2	3	320	2357	-16.27	6.27	-0.02
37	SLD 3	14	219	2257	-11.12	12.79	-0.01
37	SLD 4	14	219	2257	-11.12	12.79	-0.01
37	SLD 5	-15	415	2326	-21.25	-7.64	-0.01
37	SLD 6	-15	415	2326	-21.25	-7.64	-0.01
37	SLD 7	21	78	1993	-4.07	14.08	0
37	SLD 8	21	78	1993	-4.07	14.08	0
37	SLD 9	-20	396	2200	-20.36	-13.05	0
37	SLD 10	-20	396	2200	-20.36	-13.05	0
37	SLD 11	16	59	1866	-3.18	8.67	0
37	SLD 12	16	59	1866	-3.18	8.67	0
37	SLD 13	-13	255	1935	-13.31	-11.76	0.01
37	SLD 14	-13	255	1935	-13.31	-11.76	0.01
37	SLD 15	-2	154	1835	-8.15	-5.24	0.01
37	SLD 16	-2	154	1835	-8.15	-5.24	0.01
37	SLV 1	6	433	2711	-21.79	14.17	-0.04
37	SLV 2	6	433	2711	-21.79	14.17	-0.04
37	SLV 3	34	194	2469	-9.6	30.89	-0.03
37	SLV 4	34	194	2469	-9.6	30.89	-0.03
37	SLV 5	-40	659	2647	-33.57	-20.74	-0.02
37	SLV 6	-40	659	2647	-33.57	-20.74	-0.02
37	SLV 7	53	-139	1842	7.06	34.98	0
37	SLV 8	53	-139	1842	7.06	34.98	0
37	SLV 9	-52	613	2351	-31.48	-33.95	-0.01
37	SLV 10	-52	613	2351	-31.48	-33.95	-0.01
37	SLV 11	41	-185	1546	9.15	21.77	0.02
37	SLV 12	41	-185	1546	9.15	21.77	0.02
37	SLV 13	-33	280	1724	-14.82	-29.86	0.02
37	SLV 14	-33	280	1724	-14.82	-29.86	0.02
37	SLV 15	-5	41	1482	-2.64	-13.14	0.03
37	SLV 16	-5	41	1482	-2.64	-13.14	0.03
38	SLU 1	0	223	2126	-11.05	-0.44	0
38	SLU 2	0	223	2126	-11.05	-0.44	0
38	SLU 3	0	223	2126	-11.05	-0.44	0
38	SLU 4	0	223	2126	-11.05	-0.44	0
38	SLU 5	0	223	2126	-11.05	-0.44	0
38	SLU 6	0	223	2126	-11.05	-0.44	0
38	SLU 7	0	223	2126	-11.05	-0.44	0
38	SLU 8	0	223	2126	-11.05	-0.44	0
38	SLU 9	0	223	2126	-11.05	-0.44	0
38	SLU 10	0	228	2473	-11.45	-0.58	0
38	SLU 11	0	228	2473	-11.45	-0.58	0
38	SLU 12	0	228	2473	-11.45	-0.58	0
38	SLU 13	0	228	2473	-11.45	-0.58	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
38	SLU 14	0	228	2473	-11.45	-0.58	0
38	SLU 15	0	228	2473	-11.45	-0.58	0
38	SLU 16	0	228	2473	-11.45	-0.58	0
38	SLU 17	0	228	2473	-11.45	-0.58	0
38	SLU 18	0	229	2622	-11.62	-0.63	0.01
38	SLU 19	0	229	2622	-11.62	-0.63	0.01
38	SLU 20	0	229	2622	-11.62	-0.63	0.01
38	SLU 21	0	229	2622	-11.62	-0.63	0.01
38	SLU 22	0	230	2334	-11.48	-0.51	0
38	SLU 23	0	230	2334	-11.48	-0.51	0
38	SLU 24	0	230	2334	-11.48	-0.51	0
38	SLU 25	0	230	2334	-11.48	-0.51	0
38	SLU 26	0	230	2334	-11.48	-0.51	0
38	SLU 27	0	230	2334	-11.48	-0.51	0
38	SLU 28	0	230	2334	-11.48	-0.51	0
38	SLU 29	0	230	2334	-11.48	-0.51	0
38	SLU 30	0	230	2334	-11.48	-0.51	0
38	SLU 31	0	235	2680	-11.88	-0.65	0.01
38	SLU 32	0	235	2680	-11.88	-0.65	0.01
38	SLU 33	0	235	2680	-11.88	-0.65	0.01
38	SLU 34	0	235	2680	-11.88	-0.65	0.01
38	SLU 35	0	235	2680	-11.88	-0.65	0.01
38	SLU 36	0	235	2680	-11.88	-0.65	0.01
38	SLU 37	0	235	2680	-11.88	-0.65	0.01
38	SLU 38	0	235	2680	-11.88	-0.65	0.01
38	SLU 39	0	236	2829	-12.05	-0.71	0.01
38	SLU 40	0	236	2829	-12.05	-0.71	0.01
38	SLU 41	0	236	2829	-12.05	-0.71	0.01
38	SLU 42	0	236	2829	-12.05	-0.71	0.01
38	SLU 43	0	288	2693	-14.21	-0.55	0
38	SLU 44	0	288	2693	-14.21	-0.55	0
38	SLU 45	0	288	2693	-14.21	-0.55	0
38	SLU 46	0	288	2693	-14.21	-0.55	0
38	SLU 47	0	288	2693	-14.21	-0.55	0
38	SLU 48	0	288	2693	-14.21	-0.55	0
38	SLU 49	0	288	2693	-14.21	-0.55	0
38	SLU 50	0	288	2693	-14.21	-0.55	0
38	SLU 51	0	288	2693	-14.21	-0.55	0
38	SLU 52	0	292	3040	-14.61	-0.68	0.01
38	SLU 53	0	292	3040	-14.61	-0.68	0.01
38	SLU 54	0	292	3040	-14.61	-0.68	0.01
38	SLU 55	0	292	3040	-14.61	-0.68	0.01
38	SLU 56	0	292	3040	-14.61	-0.68	0.01
38	SLU 57	0	292	3040	-14.61	-0.68	0.01
38	SLU 58	0	292	3040	-14.61	-0.68	0.01
38	SLU 59	0	292	3040	-14.61	-0.68	0.01
38	SLU 60	0	294	3189	-14.78	-0.74	0.01
38	SLU 61	0	294	3189	-14.78	-0.74	0.01
38	SLU 62	0	294	3189	-14.78	-0.74	0.01
38	SLU 63	0	294	3189	-14.78	-0.74	0.01
38	SLU 64	0	295	2901	-14.65	-0.62	0.01
38	SLU 65	0	295	2901	-14.65	-0.62	0.01
38	SLU 66	0	295	2901	-14.65	-0.62	0.01
38	SLU 67	0	295	2901	-14.65	-0.62	0.01
38	SLU 68	0	295	2901	-14.65	-0.62	0.01
38	SLU 69	0	295	2901	-14.65	-0.62	0.01
38	SLU 70	0	295	2901	-14.65	-0.62	0.01
38	SLU 71	0	295	2901	-14.65	-0.62	0.01
38	SLU 72	0	295	2901	-14.65	-0.62	0.01
38	SLU 73	0	299	3247	-15.05	-0.76	0.01
38	SLU 74	0	299	3247	-15.05	-0.76	0.01
38	SLU 75	0	299	3247	-15.05	-0.76	0.01
38	SLU 76	0	299	3247	-15.05	-0.76	0.01
38	SLU 77	0	299	3247	-15.05	-0.76	0.01
38	SLU 78	0	299	3247	-15.05	-0.76	0.01
38	SLU 79	0	299	3247	-15.05	-0.76	0.01
38	SLU 80	0	299	3247	-15.05	-0.76	0.01
38	SLU 81	-1	301	3396	-15.22	-0.81	0.01
38	SLU 82	-1	301	3396	-15.22	-0.81	0.01
38	SLU 83	-1	301	3396	-15.22	-0.81	0.01
38	SLU 84	-1	301	3396	-15.22	-0.81	0.01
38	SLE RA 1	0	225	2186	-11.17	-0.46	0
38	SLE RA 2	0	225	2186	-11.17	-0.46	0
38	SLE RA 3	0	225	2186	-11.17	-0.46	0
38	SLE RA 4	0	225	2186	-11.17	-0.46	0
38	SLE RA 5	0	225	2186	-11.17	-0.46	0
38	SLE RA 6	0	225	2186	-11.17	-0.46	0
38	SLE RA 7	0	225	2186	-11.17	-0.46	0
38	SLE RA 8	0	225	2186	-11.17	-0.46	0
38	SLE RA 9	0	225	2186	-11.17	-0.46	0
38	SLE RA 10	0	228	2417	-11.44	-0.55	0
38	SLE RA 11	0	228	2417	-11.44	-0.55	0
38	SLE RA 12	0	228	2417	-11.44	-0.55	0
38	SLE RA 13	0	228	2417	-11.44	-0.55	0
38	SLE RA 14	0	228	2417	-11.44	-0.55	0
38	SLE RA 15	0	228	2417	-11.44	-0.55	0
38	SLE RA 16	0	228	2417	-11.44	-0.55	0
38	SLE RA 17	0	228	2417	-11.44	-0.55	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
38	SLE RA 18	0	229	2516	-11.55	-0.59	0
38	SLE RA 19	0	229	2516	-11.55	-0.59	0
38	SLE RA 20	0	229	2516	-11.55	-0.59	0
38	SLE RA 21	0	229	2516	-11.55	-0.59	0
38	SLE FR 1	0	225	2186	-11.17	-0.46	0
38	SLE FR 2	0	225	2186	-11.17	-0.46	0
38	SLE FR 3	0	225	2186	-11.17	-0.46	0
38	SLE FR 4	0	227	2285	-11.29	-0.5	0
38	SLE FR 5	0	227	2285	-11.29	-0.5	0
38	SLE FR 6	0	227	2351	-11.36	-0.53	0
38	SLE QP 1	0	225	2186	-11.17	-0.46	0
38	SLE QP 2	0	227	2285	-11.29	-0.5	0
38	SLD 1	15	320	2107	-12.8	14.05	-0.01
38	SLD 2	15	320	2107	-12.8	14.05	-0.01
38	SLD 3	3	200	1999	-6.85	7.13	-0.01
38	SLD 4	3	200	1999	-6.85	7.13	-0.01
38	SLD 5	22	436	2396	-20.78	14.37	0.01
38	SLD 6	22	436	2396	-20.78	14.37	0.01
38	SLD 7	-17	37	2035	-0.92	-8.71	-0.01
38	SLD 8	-17	37	2035	-0.92	-8.71	-0.01
38	SLD 9	16	416	2535	-21.65	7.71	0.02
38	SLD 10	16	416	2535	-21.65	7.71	0.02
38	SLD 11	-22	17	2174	-1.8	-15.37	0
38	SLD 12	-22	17	2174	-1.8	-15.37	0
38	SLD 13	-4	253	2570	-15.73	-8.13	0.02
38	SLD 14	-4	253	2570	-15.73	-8.13	0.02
38	SLD 15	-15	133	2462	-9.77	-15.05	0.02
38	SLD 16	-15	133	2462	-9.77	-15.05	0.02
38	SLV 1	38	448	1875	-14.91	35.54	-0.03
38	SLV 2	38	448	1875	-14.91	35.54	-0.03
38	SLV 3	8	164	1612	-0.75	17.69	-0.04
38	SLV 4	8	164	1612	-0.75	17.69	-0.04
38	SLV 5	56	724	2559	-33.84	37.37	0.01
38	SLV 6	56	724	2559	-33.84	37.37	0.01
38	SLV 7	-43	-223	1685	13.34	-22.1	-0.02
38	SLV 8	-43	-223	1685	13.34	-22.1	-0.02
38	SLV 9	42	676	2884	-35.92	21.1	0.03
38	SLV 10	42	676	2884	-35.92	21.1	0.03
38	SLV 11	-57	-271	2010	11.27	-38.37	0
38	SLV 12	-57	-271	2010	11.27	-38.37	0
38	SLV 13	-9	289	2957	-21.82	-18.7	0.05
38	SLV 14	-9	289	2957	-21.82	-18.7	0.05
38	SLV 15	-39	5	2695	-7.67	-36.54	0.04
38	SLV 16	-39	5	2695	-7.67	-36.54	0.04
39	SLU 1	0	0	1061	0	0	0
39	SLU 2	0	0	1061	0	0	0
39	SLU 3	0	0	1061	0	0	0
39	SLU 4	0	0	1061	0	0	0
39	SLU 5	0	0	1061	0	0	0
39	SLU 6	0	0	1061	0	0	0
39	SLU 7	0	0	1061	0	0	0
39	SLU 8	0	0	1061	0	0	0
39	SLU 9	0	0	1061	0	0	0
39	SLU 10	0	0	1280	0	0	0
39	SLU 11	0	0	1280	0	0	0
39	SLU 12	0	0	1280	0	0	0
39	SLU 13	0	0	1280	0	0	0
39	SLU 14	0	0	1280	0	0	0
39	SLU 15	0	0	1280	0	0	0
39	SLU 16	0	0	1280	0	0	0
39	SLU 17	0	0	1280	0	0	0
39	SLU 18	0	0	1373	0	0	0
39	SLU 19	0	0	1373	0	0	0
39	SLU 20	0	0	1373	0	0	0
39	SLU 21	0	0	1373	0	0	0
39	SLU 22	0	0	1190	0	0	0
39	SLU 23	0	0	1190	0	0	0
39	SLU 24	0	0	1190	0	0	0
39	SLU 25	0	0	1190	0	0	0
39	SLU 26	0	0	1190	0	0	0
39	SLU 27	0	0	1190	0	0	0
39	SLU 28	0	0	1190	0	0	0
39	SLU 29	0	0	1190	0	0	0
39	SLU 30	0	0	1190	0	0	0
39	SLU 31	0	0	1409	0	0	0
39	SLU 32	0	0	1409	0	0	0
39	SLU 33	0	0	1409	0	0	0
39	SLU 34	0	0	1409	0	0	0
39	SLU 35	0	0	1409	0	0	0
39	SLU 36	0	0	1409	0	0	0
39	SLU 37	0	0	1409	0	0	0
39	SLU 38	0	0	1409	0	0	0
39	SLU 39	0	0	1502	0	0	0
39	SLU 40	0	0	1502	0	0	0
39	SLU 41	0	0	1502	0	0	0
39	SLU 42	0	0	1502	0	0	0
39	SLU 43	0	0	1335	0	0	0
39	SLU 44	0	0	1335	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
39	SLU 45	0	0	1335	0	0	0
39	SLU 46	0	0	1335	0	0	0
39	SLU 47	0	0	1335	0	0	0
39	SLU 48	0	0	1335	0	0	0
39	SLU 49	0	0	1335	0	0	0
39	SLU 50	0	0	1335	0	0	0
39	SLU 51	0	0	1335	0	0	0
39	SLU 52	0	0	1554	0	0	0
39	SLU 53	0	0	1554	0	0	0
39	SLU 54	0	0	1554	0	0	0
39	SLU 55	0	0	1554	0	0	0
39	SLU 56	0	0	1554	0	0	0
39	SLU 57	0	0	1554	0	0	0
39	SLU 58	0	0	1554	0	0	0
39	SLU 59	0	0	1554	0	0	0
39	SLU 60	0	0	1647	0	0	0
39	SLU 61	0	0	1647	0	0	0
39	SLU 62	0	0	1647	0	0	0
39	SLU 63	0	0	1647	0	0	0
39	SLU 64	0	0	1465	0	0	0
39	SLU 65	0	0	1465	0	0	0
39	SLU 66	0	0	1465	0	0	0
39	SLU 67	0	0	1465	0	0	0
39	SLU 68	0	0	1465	0	0	0
39	SLU 69	0	0	1465	0	0	0
39	SLU 70	0	0	1465	0	0	0
39	SLU 71	0	0	1465	0	0	0
39	SLU 72	0	0	1465	0	0	0
39	SLU 73	0	0	1683	0	0	0
39	SLU 74	0	0	1683	0	0	0
39	SLU 75	0	0	1683	0	0	0
39	SLU 76	0	0	1683	0	0	0
39	SLU 77	0	0	1683	0	0	0
39	SLU 78	0	0	1683	0	0	0
39	SLU 79	0	0	1683	0	0	0
39	SLU 80	0	0	1683	0	0	0
39	SLU 81	0	0	1777	0	0	0
39	SLU 82	0	0	1777	0	0	0
39	SLU 83	0	0	1777	0	0	0
39	SLU 84	0	0	1777	0	0	0
39	SLE RA 1	0	0	1098	0	0	0
39	SLE RA 2	0	0	1098	0	0	0
39	SLE RA 3	0	0	1098	0	0	0
39	SLE RA 4	0	0	1098	0	0	0
39	SLE RA 5	0	0	1098	0	0	0
39	SLE RA 6	0	0	1098	0	0	0
39	SLE RA 7	0	0	1098	0	0	0
39	SLE RA 8	0	0	1098	0	0	0
39	SLE RA 9	0	0	1098	0	0	0
39	SLE RA 10	0	0	1244	0	0	0
39	SLE RA 11	0	0	1244	0	0	0
39	SLE RA 12	0	0	1244	0	0	0
39	SLE RA 13	0	0	1244	0	0	0
39	SLE RA 14	0	0	1244	0	0	0
39	SLE RA 15	0	0	1244	0	0	0
39	SLE RA 16	0	0	1244	0	0	0
39	SLE RA 17	0	0	1244	0	0	0
39	SLE RA 18	0	0	1306	0	0	0
39	SLE RA 19	0	0	1306	0	0	0
39	SLE RA 20	0	0	1306	0	0	0
39	SLE RA 21	0	0	1306	0	0	0
39	SLE FR 1	0	0	1098	0	0	0
39	SLE FR 2	0	0	1098	0	0	0
39	SLE FR 3	0	0	1098	0	0	0
39	SLE FR 4	0	0	1161	0	0	0
39	SLE FR 5	0	0	1161	0	0	0
39	SLE FR 6	0	0	1202	0	0	0
39	SLE QP 1	0	0	1098	0	0	0
39	SLE QP 2	0	0	1161	0	0	0
39	SLD 1	-3	1	1137	-0.01	4.05	0
39	SLD 2	-3	1	1137	-0.01	4.05	0
39	SLD 3	-2	0	1172	0.01	3.87	0
39	SLD 4	-2	0	1172	0.01	3.87	0
39	SLD 5	-1	2	1101	-0.05	1.5	0
39	SLD 6	-1	2	1101	-0.05	1.5	0
39	SLD 7	0	-2	1217	0.05	0.88	0
39	SLD 8	0	-2	1217	0.05	0.88	0
39	SLD 9	0	2	1104	-0.04	-0.88	0
39	SLD 10	0	2	1104	-0.04	-0.88	0
39	SLD 11	1	-2	1220	0.05	-1.5	0
39	SLD 12	1	-2	1220	0.05	-1.5	0
39	SLD 13	2	0	1149	-0.01	-3.87	0
39	SLD 14	2	0	1149	-0.01	-3.87	0
39	SLD 15	3	-1	1184	0.01	-4.05	0
39	SLD 16	3	-1	1184	0.01	-4.05	0
39	SLV 1	-6	3	1098	-0.04	10.33	0
39	SLV 2	-6	3	1098	-0.04	10.33	0
39	SLV 3	-6	-1	1196	0.04	9.85	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
39	SLV 4	-6	-1	1196	0.04	9.85	0
39	SLV 5	-2	6	994	-0.13	3.82	0
39	SLV 6	-2	6	994	-0.13	3.82	0
39	SLV 7	-1	-5	1319	0.13	2.23	0
39	SLV 8	-1	-5	1319	0.13	2.23	0
39	SLV 9	1	5	1002	-0.13	-2.23	0
39	SLV 10	1	5	1002	-0.13	-2.23	0
39	SLV 11	2	-6	1327	0.13	-3.82	0
39	SLV 12	2	-6	1327	0.13	-3.82	0
39	SLV 13	6	1	1125	-0.04	-9.85	0
39	SLV 14	6	1	1125	-0.04	-9.85	0
39	SLV 15	6	-3	1223	0.04	-10.33	0
39	SLV 16	6	-3	1223	0.04	-10.33	0
40	SLU 1	0	183	1899	-9.18	0.29	0
40	SLU 2	0	183	1899	-9.18	0.29	0
40	SLU 3	0	183	1899	-9.18	0.29	0
40	SLU 4	0	183	1899	-9.18	0.29	0
40	SLU 5	0	183	1899	-9.18	0.29	0
40	SLU 6	0	183	1899	-9.18	0.29	0
40	SLU 7	0	183	1899	-9.18	0.29	0
40	SLU 8	0	183	1899	-9.18	0.29	0
40	SLU 9	0	183	1899	-9.18	0.29	0
40	SLU 10	0	192	2196	-9.76	0.39	0
40	SLU 11	0	192	2196	-9.76	0.39	0
40	SLU 12	0	192	2196	-9.76	0.39	0
40	SLU 13	0	192	2196	-9.76	0.39	0
40	SLU 14	0	192	2196	-9.76	0.39	0
40	SLU 15	0	192	2196	-9.76	0.39	0
40	SLU 16	0	192	2196	-9.76	0.39	0
40	SLU 17	0	192	2196	-9.76	0.39	0
40	SLU 18	0	196	2323	-10	0.43	0
40	SLU 19	0	196	2323	-10	0.43	0
40	SLU 20	0	196	2323	-10	0.43	0
40	SLU 21	0	196	2323	-10	0.43	0
40	SLU 22	0	192	2078	-9.69	0.34	0
40	SLU 23	0	192	2078	-9.69	0.34	0
40	SLU 24	0	192	2078	-9.69	0.34	0
40	SLU 25	0	192	2078	-9.69	0.34	0
40	SLU 26	0	192	2078	-9.69	0.34	0
40	SLU 27	0	192	2078	-9.69	0.34	0
40	SLU 28	0	192	2078	-9.69	0.34	0
40	SLU 29	0	192	2078	-9.69	0.34	0
40	SLU 30	0	192	2078	-9.69	0.34	0
40	SLU 31	0	201	2374	-10.26	0.44	0
40	SLU 32	0	201	2374	-10.26	0.44	0
40	SLU 33	0	201	2374	-10.26	0.44	0
40	SLU 34	0	201	2374	-10.26	0.44	0
40	SLU 35	0	201	2374	-10.26	0.44	0
40	SLU 36	0	201	2374	-10.26	0.44	0
40	SLU 37	0	201	2374	-10.26	0.44	0
40	SLU 38	0	201	2374	-10.26	0.44	0
40	SLU 39	0	205	2502	-10.51	0.48	0
40	SLU 40	0	205	2502	-10.51	0.48	0
40	SLU 41	0	205	2502	-10.51	0.48	0
40	SLU 42	0	205	2502	-10.51	0.48	0
40	SLU 43	0	235	2408	-11.76	0.35	0
40	SLU 44	0	235	2408	-11.76	0.35	0
40	SLU 45	0	235	2408	-11.76	0.35	0
40	SLU 46	0	235	2408	-11.76	0.35	0
40	SLU 47	0	235	2408	-11.76	0.35	0
40	SLU 48	0	235	2408	-11.76	0.35	0
40	SLU 49	0	235	2408	-11.76	0.35	0
40	SLU 50	0	235	2408	-11.76	0.35	0
40	SLU 51	0	235	2408	-11.76	0.35	0
40	SLU 52	0	244	2704	-12.34	0.45	0
40	SLU 53	0	244	2704	-12.34	0.45	0
40	SLU 54	0	244	2704	-12.34	0.45	0
40	SLU 55	0	244	2704	-12.34	0.45	0
40	SLU 56	0	244	2704	-12.34	0.45	0
40	SLU 57	0	244	2704	-12.34	0.45	0
40	SLU 58	0	244	2704	-12.34	0.45	0
40	SLU 59	0	244	2704	-12.34	0.45	0
40	SLU 60	0	248	2832	-12.59	0.5	0
40	SLU 61	0	248	2832	-12.59	0.5	0
40	SLU 62	0	248	2832	-12.59	0.5	0
40	SLU 63	0	248	2832	-12.59	0.5	0
40	SLU 64	0	244	2587	-12.27	0.41	0
40	SLU 65	0	244	2587	-12.27	0.41	0
40	SLU 66	0	244	2587	-12.27	0.41	0
40	SLU 67	0	244	2587	-12.27	0.41	0
40	SLU 68	0	244	2587	-12.27	0.41	0
40	SLU 69	0	244	2587	-12.27	0.41	0
40	SLU 70	0	244	2587	-12.27	0.41	0
40	SLU 71	0	244	2587	-12.27	0.41	0
40	SLU 72	0	244	2587	-12.27	0.41	0
40	SLU 73	0	253	2883	-12.84	0.51	0
40	SLU 74	0	253	2883	-12.84	0.51	0
40	SLU 75	0	253	2883	-12.84	0.51	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
40	SLU 76	0	253	2883	-12.84	0.51	0
40	SLU 77	0	253	2883	-12.84	0.51	0
40	SLU 78	0	253	2883	-12.84	0.51	0
40	SLU 79	0	253	2883	-12.84	0.51	0
40	SLU 80	0	253	2883	-12.84	0.51	0
40	SLU 81	0	257	3010	-13.09	0.55	0
40	SLU 82	0	257	3010	-13.09	0.55	0
40	SLU 83	0	257	3010	-13.09	0.55	0
40	SLU 84	0	257	3010	-13.09	0.55	0
40	SLE RA 1	0	186	1950	-9.33	0.3	0
40	SLE RA 2	0	186	1950	-9.33	0.3	0
40	SLE RA 3	0	186	1950	-9.33	0.3	0
40	SLE RA 4	0	186	1950	-9.33	0.3	0
40	SLE RA 5	0	186	1950	-9.33	0.3	0
40	SLE RA 6	0	186	1950	-9.33	0.3	0
40	SLE RA 7	0	186	1950	-9.33	0.3	0
40	SLE RA 8	0	186	1950	-9.33	0.3	0
40	SLE RA 9	0	186	1950	-9.33	0.3	0
40	SLE RA 10	0	192	2148	-9.71	0.37	0
40	SLE RA 11	0	192	2148	-9.71	0.37	0
40	SLE RA 12	0	192	2148	-9.71	0.37	0
40	SLE RA 13	0	192	2148	-9.71	0.37	0
40	SLE RA 14	0	192	2148	-9.71	0.37	0
40	SLE RA 15	0	192	2148	-9.71	0.37	0
40	SLE RA 16	0	192	2148	-9.71	0.37	0
40	SLE RA 17	0	192	2148	-9.71	0.37	0
40	SLE RA 18	0	194	2233	-9.87	0.4	0
40	SLE RA 19	0	194	2233	-9.87	0.4	0
40	SLE RA 20	0	194	2233	-9.87	0.4	0
40	SLE RA 21	0	194	2233	-9.87	0.4	0
40	SLE FR 1	0	186	1950	-9.33	0.3	0
40	SLE FR 2	0	186	1950	-9.33	0.3	0
40	SLE FR 3	0	186	1950	-9.33	0.3	0
40	SLE FR 4	0	188	2035	-9.49	0.33	0
40	SLE FR 5	0	188	2035	-9.49	0.33	0
40	SLE FR 6	0	190	2092	-9.6	0.35	0
40	SLE QP 1	0	186	1950	-9.33	0.3	0
40	SLE QP 2	0	188	2035	-9.49	0.33	0
40	SLD 1	8	266	2267	-13.34	10.16	-0.01
40	SLD 2	8	266	2267	-13.34	10.16	-0.01
40	SLD 3	19	161	2193	-8.01	18.01	-0.01
40	SLD 4	19	161	2193	-8.01	18.01	-0.01
40	SLD 5	-14	371	2216	-18.73	-8.63	-0.01
40	SLD 6	-14	371	2216	-18.73	-8.63	-0.01
40	SLD 7	22	20	1971	-0.96	17.55	0
40	SLD 8	22	20	1971	-0.96	17.55	0
40	SLD 9	-22	356	2100	-18.02	-16.89	0
40	SLD 10	-22	356	2100	-18.02	-16.89	0
40	SLD 11	14	5	1854	-0.25	9.29	0.01
40	SLD 12	14	5	1854	-0.25	9.29	0.01
40	SLD 13	-18	216	1877	-10.97	-17.35	0.01
40	SLD 14	-18	216	1877	-10.97	-17.35	0.01
40	SLD 15	-8	111	1804	-5.64	-9.5	0.01
40	SLD 16	-8	111	1804	-5.64	-9.5	0.01
40	SLV 1	18	372	2579	-18.62	23.68	-0.03
40	SLV 2	18	372	2579	-18.62	23.68	-0.03
40	SLV 3	46	122	2401	-5.94	43.76	-0.02
40	SLV 4	46	122	2401	-5.94	43.76	-0.02
40	SLV 5	-37	622	2468	-31.46	-23.12	-0.02
40	SLV 6	-37	622	2468	-31.46	-23.12	-0.02
40	SLV 7	56	-211	1875	10.81	43.81	0
40	SLV 8	56	-211	1875	10.81	43.81	0
40	SLV 9	-56	587	2196	-29.79	-43.15	-0.01
40	SLV 10	-56	587	2196	-29.79	-43.15	-0.01
40	SLV 11	37	-246	1602	12.48	23.78	0.02
40	SLV 12	37	-246	1602	12.48	23.78	0.02
40	SLV 13	-46	255	1670	-13.04	-43.1	0.02
40	SLV 14	-46	255	1670	-13.04	-43.1	0.02
40	SLV 15	-18	5	1491	-0.36	-23.02	0.03
40	SLV 16	-18	5	1491	-0.36	-23.02	0.03
41	SLU 1	0	174	2091	-8.48	-0.27	0
41	SLU 2	0	174	2091	-8.48	-0.27	0
41	SLU 3	0	174	2091	-8.48	-0.27	0
41	SLU 4	0	174	2091	-8.48	-0.27	0
41	SLU 5	0	174	2091	-8.48	-0.27	0
41	SLU 6	0	174	2091	-8.48	-0.27	0
41	SLU 7	0	174	2091	-8.48	-0.27	0
41	SLU 8	0	174	2091	-8.48	-0.27	0
41	SLU 9	0	174	2091	-8.48	-0.27	0
41	SLU 10	0	176	2411	-8.73	-0.37	0
41	SLU 11	0	176	2411	-8.73	-0.37	0
41	SLU 12	0	176	2411	-8.73	-0.37	0
41	SLU 13	0	176	2411	-8.73	-0.37	0
41	SLU 14	0	176	2411	-8.73	-0.37	0
41	SLU 15	0	176	2411	-8.73	-0.37	0
41	SLU 16	0	176	2411	-8.73	-0.37	0
41	SLU 17	0	176	2411	-8.73	-0.37	0
41	SLU 18	0	177	2548	-8.83	-0.41	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
41	SLU 19	0	177	2548	-8.83	-0.41	0
41	SLU 20	0	177	2548	-8.83	-0.41	0
41	SLU 21	0	177	2548	-8.83	-0.41	0
41	SLU 22	0	179	2285	-8.81	-0.32	0
41	SLU 23	0	179	2285	-8.81	-0.32	0
41	SLU 24	0	179	2285	-8.81	-0.32	0
41	SLU 25	0	179	2285	-8.81	-0.32	0
41	SLU 26	0	179	2285	-8.81	-0.32	0
41	SLU 27	0	179	2285	-8.81	-0.32	0
41	SLU 28	0	179	2285	-8.81	-0.32	0
41	SLU 29	0	179	2285	-8.81	-0.32	0
41	SLU 30	0	179	2285	-8.81	-0.32	0
41	SLU 31	0	182	2604	-9.06	-0.42	0
41	SLU 32	0	182	2604	-9.06	-0.42	0
41	SLU 33	0	182	2604	-9.06	-0.42	0
41	SLU 34	0	182	2604	-9.06	-0.42	0
41	SLU 35	0	182	2604	-9.06	-0.42	0
41	SLU 36	0	182	2604	-9.06	-0.42	0
41	SLU 37	0	182	2604	-9.06	-0.42	0
41	SLU 38	0	182	2604	-9.06	-0.42	0
41	SLU 39	0	183	2741	-9.16	-0.46	0
41	SLU 40	0	183	2741	-9.16	-0.46	0
41	SLU 41	0	183	2741	-9.16	-0.46	0
41	SLU 42	0	183	2741	-9.16	-0.46	0
41	SLU 43	0	224	2652	-10.91	-0.34	0
41	SLU 44	0	224	2652	-10.91	-0.34	0
41	SLU 45	0	224	2652	-10.91	-0.34	0
41	SLU 46	0	224	2652	-10.91	-0.34	0
41	SLU 47	0	224	2652	-10.91	-0.34	0
41	SLU 48	0	224	2652	-10.91	-0.34	0
41	SLU 49	0	224	2652	-10.91	-0.34	0
41	SLU 50	0	224	2652	-10.91	-0.34	0
41	SLU 51	0	224	2652	-10.91	-0.34	0
41	SLU 52	0	226	2972	-11.16	-0.43	0
41	SLU 53	0	226	2972	-11.16	-0.43	0
41	SLU 54	0	226	2972	-11.16	-0.43	0
41	SLU 55	0	226	2972	-11.16	-0.43	0
41	SLU 56	0	226	2972	-11.16	-0.43	0
41	SLU 57	0	226	2972	-11.16	-0.43	0
41	SLU 58	0	226	2972	-11.16	-0.43	0
41	SLU 59	0	226	2972	-11.16	-0.43	0
41	SLU 60	0	227	3109	-11.26	-0.47	0
41	SLU 61	0	227	3109	-11.26	-0.47	0
41	SLU 62	0	227	3109	-11.26	-0.47	0
41	SLU 63	0	227	3109	-11.26	-0.47	0
41	SLU 64	0	230	2846	-11.24	-0.39	0
41	SLU 65	0	230	2846	-11.24	-0.39	0
41	SLU 66	0	230	2846	-11.24	-0.39	0
41	SLU 67	0	230	2846	-11.24	-0.39	0
41	SLU 68	0	230	2846	-11.24	-0.39	0
41	SLU 69	0	230	2846	-11.24	-0.39	0
41	SLU 70	0	230	2846	-11.24	-0.39	0
41	SLU 71	0	230	2846	-11.24	-0.39	0
41	SLU 72	0	230	2846	-11.24	-0.39	0
41	SLU 73	0	232	3165	-11.49	-0.48	0
41	SLU 74	0	232	3165	-11.49	-0.48	0
41	SLU 75	0	232	3165	-11.49	-0.48	0
41	SLU 76	0	232	3165	-11.49	-0.48	0
41	SLU 77	0	232	3165	-11.49	-0.48	0
41	SLU 78	0	232	3165	-11.49	-0.48	0
41	SLU 79	0	232	3165	-11.49	-0.48	0
41	SLU 80	0	232	3165	-11.49	-0.48	0
41	SLU 81	0	233	3302	-11.59	-0.52	0
41	SLU 82	0	233	3302	-11.59	-0.52	0
41	SLU 83	0	233	3302	-11.59	-0.52	0
41	SLU 84	0	233	3302	-11.59	-0.52	0
41	SLE RA 1	0	175	2147	-8.57	-0.29	0
41	SLE RA 2	0	175	2147	-8.57	-0.29	0
41	SLE RA 3	0	175	2147	-8.57	-0.29	0
41	SLE RA 4	0	175	2147	-8.57	-0.29	0
41	SLE RA 5	0	175	2147	-8.57	-0.29	0
41	SLE RA 6	0	175	2147	-8.57	-0.29	0
41	SLE RA 7	0	175	2147	-8.57	-0.29	0
41	SLE RA 8	0	175	2147	-8.57	-0.29	0
41	SLE RA 9	0	175	2147	-8.57	-0.29	0
41	SLE RA 10	0	177	2360	-8.74	-0.35	0
41	SLE RA 11	0	177	2360	-8.74	-0.35	0
41	SLE RA 12	0	177	2360	-8.74	-0.35	0
41	SLE RA 13	0	177	2360	-8.74	-0.35	0
41	SLE RA 14	0	177	2360	-8.74	-0.35	0
41	SLE RA 15	0	177	2360	-8.74	-0.35	0
41	SLE RA 16	0	177	2360	-8.74	-0.35	0
41	SLE RA 17	0	177	2360	-8.74	-0.35	0
41	SLE RA 18	0	178	2451	-8.81	-0.38	0
41	SLE RA 19	0	178	2451	-8.81	-0.38	0
41	SLE RA 20	0	178	2451	-8.81	-0.38	0
41	SLE RA 21	0	178	2451	-8.81	-0.38	0
41	SLE FR 1	0	175	2147	-8.57	-0.29	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
41	SLE FR 2	0	175	2147	-8.57	-0.29	0
41	SLE FR 3	0	175	2147	-8.57	-0.29	0
41	SLE FR 4	0	176	2238	-8.65	-0.31	0
41	SLE FR 5	0	176	2238	-8.65	-0.31	0
41	SLE FR 6	0	176	2299	-8.69	-0.33	0
41	SLE QP 1	0	175	2147	-8.57	-0.29	0
41	SLE QP 2	0	176	2238	-8.65	-0.31	0
41	SLD 1	22	265	2058	-10.53	20.54	-0.01
41	SLD 2	22	265	2058	-10.53	20.54	-0.01
41	SLD 3	11	140	1981	-4.36	12.51	-0.02
41	SLD 4	11	140	1981	-4.36	12.51	-0.02
41	SLD 5	23	392	2302	-18.57	18.12	0
41	SLD 6	23	392	2302	-18.57	18.12	0
41	SLD 7	-13	-25	2043	1.99	-8.64	-0.01
41	SLD 8	-13	-25	2043	1.99	-8.64	-0.01
41	SLD 9	13	377	2433	-19.28	8.02	0.01
41	SLD 10	13	377	2433	-19.28	8.02	0.01
41	SLD 11	-23	-41	2174	1.28	-18.75	0
41	SLD 12	-23	-41	2174	1.28	-18.75	0
41	SLD 13	-11	212	2495	-12.93	-13.13	0.02
41	SLD 14	-11	212	2495	-12.93	-13.13	0.02
41	SLD 15	-22	87	2417	-6.76	-21.16	0.01
41	SLD 16	-22	87	2417	-6.76	-21.16	0.01
41	SLV 1	53	387	1822	-13.17	50.87	-0.03
41	SLV 2	53	387	1822	-13.17	50.87	-0.03
41	SLV 3	25	89	1634	1.53	30.29	-0.04
41	SLV 4	25	89	1634	1.53	30.29	-0.04
41	SLV 5	59	691	2399	-32.31	46.25	0.01
41	SLV 6	59	691	2399	-32.31	46.25	0.01
41	SLV 7	-35	-302	1771	16.72	-22.34	-0.03
41	SLV 8	-35	-302	1771	16.72	-22.34	-0.03
41	SLV 9	35	654	2705	-34.01	21.71	0.03
41	SLV 10	35	654	2705	-34.01	21.71	0.03
41	SLV 11	-59	-339	2077	15.02	-46.88	-0.01
41	SLV 12	-59	-339	2077	15.02	-46.88	-0.01
41	SLV 13	-26	263	2842	-18.82	-30.92	0.04
41	SLV 14	-26	263	2842	-18.82	-30.92	0.04
41	SLV 15	-54	-35	2654	-4.12	-51.5	0.03
41	SLV 16	-54	-35	2654	-4.12	-51.5	0.03
42	SLU 1	0	0	1077	0	0	0
42	SLU 2	0	0	1077	0	0	0
42	SLU 3	0	0	1077	0	0	0
42	SLU 4	0	0	1077	0	0	0
42	SLU 5	0	0	1077	0	0	0
42	SLU 6	0	0	1077	0	0	0
42	SLU 7	0	0	1077	0	0	0
42	SLU 8	0	0	1077	0	0	0
42	SLU 9	0	0	1077	0	0	0
42	SLU 10	0	0	1292	0	0	0
42	SLU 11	0	0	1292	0	0	0
42	SLU 12	0	0	1292	0	0	0
42	SLU 13	0	0	1292	0	0	0
42	SLU 14	0	0	1292	0	0	0
42	SLU 15	0	0	1292	0	0	0
42	SLU 16	0	0	1292	0	0	0
42	SLU 17	0	0	1292	0	0	0
42	SLU 18	0	0	1384	0	0	0
42	SLU 19	0	0	1384	0	0	0
42	SLU 20	0	0	1384	0	0	0
42	SLU 21	0	0	1384	0	0	0
42	SLU 22	0	0	1206	0	0	0
42	SLU 23	0	0	1206	0	0	0
42	SLU 24	0	0	1206	0	0	0
42	SLU 25	0	0	1206	0	0	0
42	SLU 26	0	0	1206	0	0	0
42	SLU 27	0	0	1206	0	0	0
42	SLU 28	0	0	1206	0	0	0
42	SLU 29	0	0	1206	0	0	0
42	SLU 30	0	0	1206	0	0	0
42	SLU 31	0	0	1421	0	0	0
42	SLU 32	0	0	1421	0	0	0
42	SLU 33	0	0	1421	0	0	0
42	SLU 34	0	0	1421	0	0	0
42	SLU 35	0	0	1421	0	0	0
42	SLU 36	0	0	1421	0	0	0
42	SLU 37	0	0	1421	0	0	0
42	SLU 38	0	0	1421	0	0	0
42	SLU 39	0	0	1513	0	0	0
42	SLU 40	0	0	1513	0	0	0
42	SLU 41	0	0	1513	0	0	0
42	SLU 42	0	0	1513	0	0	0
42	SLU 43	0	0	1355	0	0	0
42	SLU 44	0	0	1355	0	0	0
42	SLU 45	0	0	1355	0	0	0
42	SLU 46	0	0	1355	0	0	0
42	SLU 47	0	0	1355	0	0	0
42	SLU 48	0	0	1355	0	0	0
42	SLU 49	0	0	1355	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
42	SLU 50	0	0	1355	0	0	0
42	SLU 51	0	0	1355	0	0	0
42	SLU 52	0	0	1571	0	0	0
42	SLU 53	0	0	1571	0	0	0
42	SLU 54	0	0	1571	0	0	0
42	SLU 55	0	0	1571	0	0	0
42	SLU 56	0	0	1571	0	0	0
42	SLU 57	0	0	1571	0	0	0
42	SLU 58	0	0	1571	0	0	0
42	SLU 59	0	0	1571	0	0	0
42	SLU 60	0	0	1663	0	0	0
42	SLU 61	0	0	1663	0	0	0
42	SLU 62	0	0	1663	0	0	0
42	SLU 63	0	0	1663	0	0	0
42	SLU 64	0	0	1484	0	0	0
42	SLU 65	0	0	1484	0	0	0
42	SLU 66	0	0	1484	0	0	0
42	SLU 67	0	0	1484	0	0	0
42	SLU 68	0	0	1484	0	0	0
42	SLU 69	0	0	1484	0	0	0
42	SLU 70	0	0	1484	0	0	0
42	SLU 71	0	0	1484	0	0	0
42	SLU 72	0	0	1484	0	0	0
42	SLU 73	0	0	1700	0	0	0
42	SLU 74	0	0	1700	0	0	0
42	SLU 75	0	0	1700	0	0	0
42	SLU 76	0	0	1700	0	0	0
42	SLU 77	0	0	1700	0	0	0
42	SLU 78	0	0	1700	0	0	0
42	SLU 79	0	0	1700	0	0	0
42	SLU 80	0	0	1700	0	0	0
42	SLU 81	0	0	1792	0	0	0
42	SLU 82	0	0	1792	0	0	0
42	SLU 83	0	0	1792	0	0	0
42	SLU 84	0	0	1792	0	0	0
42	SLE RA 1	0	0	1114	0	0	0
42	SLE RA 2	0	0	1114	0	0	0
42	SLE RA 3	0	0	1114	0	0	0
42	SLE RA 4	0	0	1114	0	0	0
42	SLE RA 5	0	0	1114	0	0	0
42	SLE RA 6	0	0	1114	0	0	0
42	SLE RA 7	0	0	1114	0	0	0
42	SLE RA 8	0	0	1114	0	0	0
42	SLE RA 9	0	0	1114	0	0	0
42	SLE RA 10	0	0	1257	0	0	0
42	SLE RA 11	0	0	1257	0	0	0
42	SLE RA 12	0	0	1257	0	0	0
42	SLE RA 13	0	0	1257	0	0	0
42	SLE RA 14	0	0	1257	0	0	0
42	SLE RA 15	0	0	1257	0	0	0
42	SLE RA 16	0	0	1257	0	0	0
42	SLE RA 17	0	0	1257	0	0	0
42	SLE RA 18	0	0	1319	0	0	0
42	SLE RA 19	0	0	1319	0	0	0
42	SLE RA 20	0	0	1319	0	0	0
42	SLE RA 21	0	0	1319	0	0	0
42	SLE FR 1	0	0	1114	0	0	0
42	SLE FR 2	0	0	1114	0	0	0
42	SLE FR 3	0	0	1114	0	0	0
42	SLE FR 4	0	0	1175	0	0	0
42	SLE FR 5	0	0	1175	0	0	0
42	SLE FR 6	0	0	1216	0	0	0
42	SLE QP 1	0	0	1114	0	0	0
42	SLE QP 2	0	0	1175	0	0	0
42	SLD 1	-3	1	1162	-0.05	5.64	0
42	SLD 2	-3	1	1162	-0.05	5.64	0
42	SLD 3	-3	0	1177	0.05	5.4	0
42	SLD 4	-3	0	1177	0.05	5.4	0
42	SLD 5	-1	2	1149	-0.16	2.06	0
42	SLD 6	-1	2	1149	-0.16	2.06	0
42	SLD 7	-1	-2	1198	0.16	1.25	0
42	SLD 8	-1	-2	1198	0.16	1.25	0
42	SLD 9	1	2	1152	-0.16	-1.25	0
42	SLD 10	1	2	1152	-0.16	-1.25	0
42	SLD 11	1	-2	1201	0.16	-2.06	0
42	SLD 12	1	-2	1201	0.16	-2.06	0
42	SLD 13	3	0	1173	-0.05	-5.4	0
42	SLD 14	3	0	1173	-0.05	-5.4	0
42	SLD 15	3	-1	1188	0.05	-5.64	0
42	SLD 16	3	-1	1188	0.05	-5.64	0
42	SLV 1	-9	2	1143	-0.14	14.36	0
42	SLV 2	-9	2	1143	-0.14	14.36	0
42	SLV 3	-8	-1	1183	0.14	13.74	0
42	SLV 4	-8	-1	1183	0.14	13.74	0
42	SLV 5	-3	5	1104	-0.46	5.25	0
42	SLV 6	-3	5	1104	-0.46	5.25	0
42	SLV 7	-2	-5	1239	0.46	3.18	0
42	SLV 8	-2	-5	1239	0.46	3.18	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
42	SLV 9	2	5	1111	-0.46	-3.18	0
42	SLV 10	2	5	1111	-0.46	-3.18	0
42	SLV 11	3	-5	1246	0.46	-5.25	0
42	SLV 12	3	-5	1246	0.46	-5.25	0
42	SLV 13	8	1	1167	-0.14	-13.73	0
42	SLV 14	8	1	1167	-0.14	-13.73	0
42	SLV 15	9	-2	1207	0.14	-14.36	0
42	SLV 16	9	-2	1207	0.14	-14.36	0
43	SLU 1	0	158	1873	-7.84	0.23	0
43	SLU 2	0	158	1873	-7.84	0.23	0
43	SLU 3	0	158	1873	-7.84	0.23	0
43	SLU 4	0	158	1873	-7.84	0.23	0
43	SLU 5	0	158	1873	-7.84	0.23	0
43	SLU 6	0	158	1873	-7.84	0.23	0
43	SLU 7	0	158	1873	-7.84	0.23	0
43	SLU 8	0	158	1873	-7.84	0.23	0
43	SLU 9	0	158	1873	-7.84	0.23	0
43	SLU 10	0	169	2150	-8.48	0.33	0
43	SLU 11	0	169	2150	-8.48	0.33	0
43	SLU 12	0	169	2150	-8.48	0.33	0
43	SLU 13	0	169	2150	-8.48	0.33	0
43	SLU 14	0	169	2150	-8.48	0.33	0
43	SLU 15	0	169	2150	-8.48	0.33	0
43	SLU 16	0	169	2150	-8.48	0.33	0
43	SLU 17	0	169	2150	-8.48	0.33	0
43	SLU 18	0	173	2269	-8.76	0.37	0
43	SLU 19	0	173	2269	-8.76	0.37	0
43	SLU 20	0	173	2269	-8.76	0.37	0
43	SLU 21	0	173	2269	-8.76	0.37	0
43	SLU 22	0	167	2042	-8.36	0.28	0
43	SLU 23	0	167	2042	-8.36	0.28	0
43	SLU 24	0	167	2042	-8.36	0.28	0
43	SLU 25	0	167	2042	-8.36	0.28	0
43	SLU 26	0	167	2042	-8.36	0.28	0
43	SLU 27	0	167	2042	-8.36	0.28	0
43	SLU 28	0	167	2042	-8.36	0.28	0
43	SLU 29	0	167	2042	-8.36	0.28	0
43	SLU 30	0	167	2042	-8.36	0.28	0
43	SLU 31	0	178	2319	-9.01	0.38	0
43	SLU 32	0	178	2319	-9.01	0.38	0
43	SLU 33	0	178	2319	-9.01	0.38	0
43	SLU 34	0	178	2319	-9.01	0.38	0
43	SLU 35	0	178	2319	-9.01	0.38	0
43	SLU 36	0	178	2319	-9.01	0.38	0
43	SLU 37	0	178	2319	-9.01	0.38	0
43	SLU 38	0	178	2319	-9.01	0.38	0
43	SLU 39	0	183	2438	-9.29	0.42	0
43	SLU 40	0	183	2438	-9.29	0.42	0
43	SLU 41	0	183	2438	-9.29	0.42	0
43	SLU 42	0	183	2438	-9.29	0.42	0
43	SLU 43	0	201	2377	-10.01	0.29	0
43	SLU 44	0	201	2377	-10.01	0.29	0
43	SLU 45	0	201	2377	-10.01	0.29	0
43	SLU 46	0	201	2377	-10.01	0.29	0
43	SLU 47	0	201	2377	-10.01	0.29	0
43	SLU 48	0	201	2377	-10.01	0.29	0
43	SLU 49	0	201	2377	-10.01	0.29	0
43	SLU 50	0	201	2377	-10.01	0.29	0
43	SLU 51	0	201	2377	-10.01	0.29	0
43	SLU 52	0	212	2654	-10.65	0.38	0
43	SLU 53	0	212	2654	-10.65	0.38	0
43	SLU 54	0	212	2654	-10.65	0.38	0
43	SLU 55	0	212	2654	-10.65	0.38	0
43	SLU 56	0	212	2654	-10.65	0.38	0
43	SLU 57	0	212	2654	-10.65	0.38	0
43	SLU 58	0	212	2654	-10.65	0.38	0
43	SLU 59	0	212	2654	-10.65	0.38	0
43	SLU 60	0	217	2773	-10.93	0.42	0
43	SLU 61	0	217	2773	-10.93	0.42	0
43	SLU 62	0	217	2773	-10.93	0.42	0
43	SLU 63	0	217	2773	-10.93	0.42	0
43	SLU 64	0	211	2546	-10.54	0.34	0
43	SLU 65	0	211	2546	-10.54	0.34	0
43	SLU 66	0	211	2546	-10.54	0.34	0
43	SLU 67	0	211	2546	-10.54	0.34	0
43	SLU 68	0	211	2546	-10.54	0.34	0
43	SLU 69	0	211	2546	-10.54	0.34	0
43	SLU 70	0	211	2546	-10.54	0.34	0
43	SLU 71	0	211	2546	-10.54	0.34	0
43	SLU 72	0	211	2546	-10.54	0.34	0
43	SLU 73	0	222	2823	-11.18	0.43	0
43	SLU 74	0	222	2823	-11.18	0.43	0
43	SLU 75	0	222	2823	-11.18	0.43	0
43	SLU 76	0	222	2823	-11.18	0.43	0
43	SLU 77	0	222	2823	-11.18	0.43	0
43	SLU 78	0	222	2823	-11.18	0.43	0
43	SLU 79	0	222	2823	-11.18	0.43	0
43	SLU 80	0	222	2823	-11.18	0.43	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
43	SLU 81	0	227	2942	-11.46	0.47	0
43	SLU 82	0	227	2942	-11.46	0.47	0
43	SLU 83	0	227	2942	-11.46	0.47	0
43	SLU 84	0	227	2942	-11.46	0.47	0
43	SLE RA 1	0	160	1921	-7.99	0.25	0
43	SLE RA 2	0	160	1921	-7.99	0.25	0
43	SLE RA 3	0	160	1921	-7.99	0.25	0
43	SLE RA 4	0	160	1921	-7.99	0.25	0
43	SLE RA 5	0	160	1921	-7.99	0.25	0
43	SLE RA 6	0	160	1921	-7.99	0.25	0
43	SLE RA 7	0	160	1921	-7.99	0.25	0
43	SLE RA 8	0	160	1921	-7.99	0.25	0
43	SLE RA 9	0	160	1921	-7.99	0.25	0
43	SLE RA 10	0	168	2106	-8.42	0.31	0
43	SLE RA 11	0	168	2106	-8.42	0.31	0
43	SLE RA 12	0	168	2106	-8.42	0.31	0
43	SLE RA 13	0	168	2106	-8.42	0.31	0
43	SLE RA 14	0	168	2106	-8.42	0.31	0
43	SLE RA 15	0	168	2106	-8.42	0.31	0
43	SLE RA 16	0	168	2106	-8.42	0.31	0
43	SLE RA 17	0	168	2106	-8.42	0.31	0
43	SLE RA 18	0	171	2185	-8.6	0.34	0
43	SLE RA 19	0	171	2185	-8.6	0.34	0
43	SLE RA 20	0	171	2185	-8.6	0.34	0
43	SLE RA 21	0	171	2185	-8.6	0.34	0
43	SLE FR 1	0	160	1921	-7.99	0.25	0
43	SLE FR 2	0	160	1921	-7.99	0.25	0
43	SLE FR 3	0	160	1921	-7.99	0.25	0
43	SLE FR 4	0	163	2000	-8.17	0.27	0
43	SLE FR 5	0	163	2000	-8.17	0.27	0
43	SLE FR 6	0	166	2053	-8.3	0.29	0
43	SLE QP 1	0	160	1921	-7.99	0.25	0
43	SLE QP 2	0	163	2000	-8.17	0.27	0
43	SLD 1	14	238	2213	-11.81	13.8	-0.01
43	SLD 2	14	238	2213	-11.81	13.8	-0.01
43	SLD 3	24	129	2157	-6.44	22.03	-0.01
43	SLD 4	24	129	2157	-6.44	22.03	-0.01
43	SLD 5	-10	350	2149	-17.4	-8.15	-0.01
43	SLD 6	-10	350	2149	-17.4	-8.15	-0.01
43	SLD 7	22	-11	1963	0.49	19.29	0
43	SLD 8	22	-11	1963	0.49	19.29	0
43	SLD 9	-22	338	2038	-16.83	-18.74	0
43	SLD 10	-22	338	2038	-16.83	-18.74	0
43	SLD 11	11	-23	1852	1.06	8.7	0.01
43	SLD 12	11	-23	1852	1.06	8.7	0.01
43	SLD 13	-23	198	1844	-9.9	-21.48	0.01
43	SLD 14	-23	198	1844	-9.9	-21.48	0.01
43	SLD 15	-14	89	1788	-4.54	-13.25	0.01
43	SLD 16	-14	89	1788	-4.54	-13.25	0.01
43	SLV 1	33	339	2500	-16.77	32.44	-0.02
43	SLV 2	33	339	2500	-16.77	32.44	-0.02
43	SLV 3	57	82	2365	-4.06	53.41	-0.02
43	SLV 4	57	82	2365	-4.06	53.41	-0.02
43	SLV 5	-27	606	2355	-30.03	-21.87	-0.02
43	SLV 6	-27	606	2355	-30.03	-21.87	-0.02
43	SLV 7	55	-251	1905	12.34	48.01	0
43	SLV 8	55	-251	1905	12.34	48.01	0
43	SLV 9	-54	578	2096	-28.68	-47.46	0
43	SLV 10	-54	578	2096	-28.68	-47.46	0
43	SLV 11	28	-279	1645	13.68	22.42	0.02
43	SLV 12	28	-279	1645	13.68	22.42	0.02
43	SLV 13	-57	245	1636	-12.29	-52.86	0.02
43	SLV 14	-57	245	1636	-12.29	-52.86	0.02
43	SLV 15	-33	-12	1501	0.42	-31.89	0.02
43	SLV 16	-33	-12	1501	0.42	-31.89	0.02
44	SLU 1	0	146	2083	-6.94	-0.22	0
44	SLU 2	0	146	2083	-6.94	-0.22	0
44	SLU 3	0	146	2083	-6.94	-0.22	0
44	SLU 4	0	146	2083	-6.94	-0.22	0
44	SLU 5	0	146	2083	-6.94	-0.22	0
44	SLU 6	0	146	2083	-6.94	-0.22	0
44	SLU 7	0	146	2083	-6.94	-0.22	0
44	SLU 8	0	146	2083	-6.94	-0.22	0
44	SLU 9	0	146	2083	-6.94	-0.22	0
44	SLU 10	0	151	2388	-7.25	-0.31	0
44	SLU 11	0	151	2388	-7.25	-0.31	0
44	SLU 12	0	151	2388	-7.25	-0.31	0
44	SLU 13	0	151	2388	-7.25	-0.31	0
44	SLU 14	0	151	2388	-7.25	-0.31	0
44	SLU 15	0	151	2388	-7.25	-0.31	0
44	SLU 16	0	151	2388	-7.25	-0.31	0
44	SLU 17	0	151	2388	-7.25	-0.31	0
44	SLU 18	0	154	2518	-7.37	-0.35	0
44	SLU 19	0	154	2518	-7.37	-0.35	0
44	SLU 20	0	154	2518	-7.37	-0.35	0
44	SLU 21	0	154	2518	-7.37	-0.35	0
44	SLU 22	0	153	2270	-7.28	-0.27	0
44	SLU 23	0	153	2270	-7.28	-0.27	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
44	SLU 24	0	153	2270	-7.28	-0.27	0
44	SLU 25	0	153	2270	-7.28	-0.27	0
44	SLU 26	0	153	2270	-7.28	-0.27	0
44	SLU 27	0	153	2270	-7.28	-0.27	0
44	SLU 28	0	153	2270	-7.28	-0.27	0
44	SLU 29	0	153	2270	-7.28	-0.27	0
44	SLU 30	0	153	2270	-7.28	-0.27	0
44	SLU 31	0	158	2574	-7.58	-0.36	0
44	SLU 32	0	158	2574	-7.58	-0.36	0
44	SLU 33	0	158	2574	-7.58	-0.36	0
44	SLU 34	0	158	2574	-7.58	-0.36	0
44	SLU 35	0	158	2574	-7.58	-0.36	0
44	SLU 36	0	158	2574	-7.58	-0.36	0
44	SLU 37	0	158	2574	-7.58	-0.36	0
44	SLU 38	0	158	2574	-7.58	-0.36	0
44	SLU 39	0	160	2705	-7.71	-0.4	0
44	SLU 40	0	160	2705	-7.71	-0.4	0
44	SLU 41	0	160	2705	-7.71	-0.4	0
44	SLU 42	0	160	2705	-7.71	-0.4	0
44	SLU 43	0	187	2644	-8.91	-0.27	0
44	SLU 44	0	187	2644	-8.91	-0.27	0
44	SLU 45	0	187	2644	-8.91	-0.27	0
44	SLU 46	0	187	2644	-8.91	-0.27	0
44	SLU 47	0	187	2644	-8.91	-0.27	0
44	SLU 48	0	187	2644	-8.91	-0.27	0
44	SLU 49	0	187	2644	-8.91	-0.27	0
44	SLU 50	0	187	2644	-8.91	-0.27	0
44	SLU 51	0	187	2644	-8.91	-0.27	0
44	SLU 52	0	193	2948	-9.21	-0.36	0
44	SLU 53	0	193	2948	-9.21	-0.36	0
44	SLU 54	0	193	2948	-9.21	-0.36	0
44	SLU 55	0	193	2948	-9.21	-0.36	0
44	SLU 56	0	193	2948	-9.21	-0.36	0
44	SLU 57	0	193	2948	-9.21	-0.36	0
44	SLU 58	0	193	2948	-9.21	-0.36	0
44	SLU 59	0	193	2948	-9.21	-0.36	0
44	SLU 60	0	195	3079	-9.34	-0.4	0
44	SLU 61	0	195	3079	-9.34	-0.4	0
44	SLU 62	0	195	3079	-9.34	-0.4	0
44	SLU 63	0	195	3079	-9.34	-0.4	0
44	SLU 64	0	194	2830	-9.25	-0.32	0
44	SLU 65	0	194	2830	-9.25	-0.32	0
44	SLU 66	0	194	2830	-9.25	-0.32	0
44	SLU 67	0	194	2830	-9.25	-0.32	0
44	SLU 68	0	194	2830	-9.25	-0.32	0
44	SLU 69	0	194	2830	-9.25	-0.32	0
44	SLU 70	0	194	2830	-9.25	-0.32	0
44	SLU 71	0	194	2830	-9.25	-0.32	0
44	SLU 72	0	194	2830	-9.25	-0.32	0
44	SLU 73	0	200	3135	-9.55	-0.41	0
44	SLU 74	0	200	3135	-9.55	-0.41	0
44	SLU 75	0	200	3135	-9.55	-0.41	0
44	SLU 76	0	200	3135	-9.55	-0.41	0
44	SLU 77	0	200	3135	-9.55	-0.41	0
44	SLU 78	0	200	3135	-9.55	-0.41	0
44	SLU 79	0	200	3135	-9.55	-0.41	0
44	SLU 80	0	200	3135	-9.55	-0.41	0
44	SLU 81	0	202	3266	-9.68	-0.45	0
44	SLU 82	0	202	3266	-9.68	-0.45	0
44	SLU 83	0	202	3266	-9.68	-0.45	0
44	SLU 84	0	202	3266	-9.68	-0.45	0
44	SLE RA 1	0	148	2136	-7.04	-0.23	0
44	SLE RA 2	0	148	2136	-7.04	-0.23	0
44	SLE RA 3	0	148	2136	-7.04	-0.23	0
44	SLE RA 4	0	148	2136	-7.04	-0.23	0
44	SLE RA 5	0	148	2136	-7.04	-0.23	0
44	SLE RA 6	0	148	2136	-7.04	-0.23	0
44	SLE RA 7	0	148	2136	-7.04	-0.23	0
44	SLE RA 8	0	148	2136	-7.04	-0.23	0
44	SLE RA 9	0	148	2136	-7.04	-0.23	0
44	SLE RA 10	0	151	2339	-7.24	-0.3	0
44	SLE RA 11	0	151	2339	-7.24	-0.3	0
44	SLE RA 12	0	151	2339	-7.24	-0.3	0
44	SLE RA 13	0	151	2339	-7.24	-0.3	0
44	SLE RA 14	0	151	2339	-7.24	-0.3	0
44	SLE RA 15	0	151	2339	-7.24	-0.3	0
44	SLE RA 16	0	151	2339	-7.24	-0.3	0
44	SLE RA 17	0	151	2339	-7.24	-0.3	0
44	SLE RA 18	0	153	2426	-7.33	-0.32	0
44	SLE RA 19	0	153	2426	-7.33	-0.32	0
44	SLE RA 20	0	153	2426	-7.33	-0.32	0
44	SLE RA 21	0	153	2426	-7.33	-0.32	0
44	SLE FR 1	0	148	2136	-7.04	-0.23	0
44	SLE FR 2	0	148	2136	-7.04	-0.23	0
44	SLE FR 3	0	148	2136	-7.04	-0.23	0
44	SLE FR 4	0	149	2223	-7.13	-0.26	0
44	SLE FR 5	0	149	2223	-7.13	-0.26	0
44	SLE FR 6	0	150	2281	-7.18	-0.28	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
44	SLE QP 1	0	148	2136	-7.04	-0.23	0
44	SLE QP 2	0	149	2223	-7.13	-0.26	0
44	SLD 1	27	236	2040	-11.27	25.02	-0.01
44	SLD 2	27	236	2040	-11.27	25.02	-0.01
44	SLD 3	18	106	1983	-4.99	16.94	-0.01
44	SLD 4	18	106	1983	-4.99	16.94	-0.01
44	SLD 5	22	372	2255	-17.89	19.58	0
44	SLD 6	22	372	2255	-17.89	19.58	0
44	SLD 7	-9	-60	2065	3.04	-7.36	-0.01
44	SLD 8	-9	-60	2065	3.04	-7.36	-0.01
44	SLD 9	8	359	2382	-17.29	6.84	0.01
44	SLD 10	8	359	2382	-17.29	6.84	0.01
44	SLD 11	-22	-73	2192	3.64	-20.11	0
44	SLD 12	-22	-73	2192	3.64	-20.11	0
44	SLD 13	-18	193	2464	-9.27	-17.46	0.01
44	SLD 14	-18	193	2464	-9.27	-17.46	0.01
44	SLD 15	-27	63	2407	-2.99	-25.54	0.01
44	SLD 16	-27	63	2407	-2.99	-25.54	0.01
44	SLV 1	66	354	1798	-16.97	61.41	-0.02
44	SLV 2	66	354	1798	-16.97	61.41	-0.02
44	SLV 3	42	46	1659	-2.02	40.83	-0.03
44	SLV 4	42	46	1659	-2.02	40.83	-0.03
44	SLV 5	55	679	2306	-32.76	49.45	0.01
44	SLV 6	55	679	2306	-32.76	49.45	0.01
44	SLV 7	-23	-350	1844	17.08	-19.15	-0.02
44	SLV 8	-23	-350	1844	17.08	-19.15	-0.02
44	SLV 9	23	648	2603	-31.34	18.63	0.02
44	SLV 10	23	648	2603	-31.34	18.63	0.02
44	SLV 11	-55	-380	2141	18.5	-49.98	-0.01
44	SLV 12	-55	-380	2141	18.5	-49.98	-0.01
44	SLV 13	-43	253	2787	-12.23	-41.35	0.03
44	SLV 14	-43	253	2787	-12.23	-41.35	0.03
44	SLV 15	-66	-56	2649	2.72	-61.93	0.02
44	SLV 16	-66	-56	2649	2.72	-61.93	0.02
45	SLU 1	0	0	1090	0	0	0
45	SLU 2	0	0	1090	0	0	0
45	SLU 3	0	0	1090	0	0	0
45	SLU 4	0	0	1090	0	0	0
45	SLU 5	0	0	1090	0	0	0
45	SLU 6	0	0	1090	0	0	0
45	SLU 7	0	0	1090	0	0	0
45	SLU 8	0	0	1090	0	0	0
45	SLU 9	0	0	1090	0	0	0
45	SLU 10	0	0	1307	0	0	0
45	SLU 11	0	0	1307	0	0	0
45	SLU 12	0	0	1307	0	0	0
45	SLU 13	0	0	1307	0	0	0
45	SLU 14	0	0	1307	0	0	0
45	SLU 15	0	0	1307	0	0	0
45	SLU 16	0	0	1307	0	0	0
45	SLU 17	0	0	1307	0	0	0
45	SLU 18	0	0	1400	0	0	0
45	SLU 19	0	0	1400	0	0	0
45	SLU 20	0	0	1400	0	0	0
45	SLU 21	0	0	1400	0	0	0
45	SLU 22	0	0	1221	0	0	0
45	SLU 23	0	0	1221	0	0	0
45	SLU 24	0	0	1221	0	0	0
45	SLU 25	0	0	1221	0	0	0
45	SLU 26	0	0	1221	0	0	0
45	SLU 27	0	0	1221	0	0	0
45	SLU 28	0	0	1221	0	0	0
45	SLU 29	0	0	1221	0	0	0
45	SLU 30	0	0	1221	0	0	0
45	SLU 31	0	0	1437	0	0	0
45	SLU 32	0	0	1437	0	0	0
45	SLU 33	0	0	1437	0	0	0
45	SLU 34	0	0	1437	0	0	0
45	SLU 35	0	0	1437	0	0	0
45	SLU 36	0	0	1437	0	0	0
45	SLU 37	0	0	1437	0	0	0
45	SLU 38	0	0	1437	0	0	0
45	SLU 39	0	0	1530	0	0	0
45	SLU 40	0	0	1530	0	0	0
45	SLU 41	0	0	1530	0	0	0
45	SLU 42	0	0	1530	0	0	0
45	SLU 43	0	0	1373	0	0	0
45	SLU 44	0	0	1373	0	0	0
45	SLU 45	0	0	1373	0	0	0
45	SLU 46	0	0	1373	0	0	0
45	SLU 47	0	0	1373	0	0	0
45	SLU 48	0	0	1373	0	0	0
45	SLU 49	0	0	1373	0	0	0
45	SLU 50	0	0	1373	0	0	0
45	SLU 51	0	0	1373	0	0	0
45	SLU 52	0	0	1589	0	0	0
45	SLU 53	0	0	1589	0	0	0
45	SLU 54	0	0	1589	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
45	SLU 55	0	0	1589	0	0	0
45	SLU 56	0	0	1589	0	0	0
45	SLU 57	0	0	1589	0	0	0
45	SLU 58	0	0	1589	0	0	0
45	SLU 59	0	0	1589	0	0	0
45	SLU 60	0	0	1682	0	0	0
45	SLU 61	0	0	1682	0	0	0
45	SLU 62	0	0	1682	0	0	0
45	SLU 63	0	0	1682	0	0	0
45	SLU 64	0	0	1503	0	0	0
45	SLU 65	0	0	1503	0	0	0
45	SLU 66	0	0	1503	0	0	0
45	SLU 67	0	0	1503	0	0	0
45	SLU 68	0	0	1503	0	0	0
45	SLU 69	0	0	1503	0	0	0
45	SLU 70	0	0	1503	0	0	0
45	SLU 71	0	0	1503	0	0	0
45	SLU 72	0	0	1503	0	0	0
45	SLU 73	0	0	1720	0	0	0
45	SLU 74	0	0	1720	0	0	0
45	SLU 75	0	0	1720	0	0	0
45	SLU 76	0	0	1720	0	0	0
45	SLU 77	0	0	1720	0	0	0
45	SLU 78	0	0	1720	0	0	0
45	SLU 79	0	0	1720	0	0	0
45	SLU 80	0	0	1720	0	0	0
45	SLU 81	0	0	1812	0	0	0
45	SLU 82	0	0	1812	0	0	0
45	SLU 83	0	0	1812	0	0	0
45	SLU 84	0	0	1812	0	0	0
45	SLE RA 1	0	0	1128	0	0	0
45	SLE RA 2	0	0	1128	0	0	0
45	SLE RA 3	0	0	1128	0	0	0
45	SLE RA 4	0	0	1128	0	0	0
45	SLE RA 5	0	0	1128	0	0	0
45	SLE RA 6	0	0	1128	0	0	0
45	SLE RA 7	0	0	1128	0	0	0
45	SLE RA 8	0	0	1128	0	0	0
45	SLE RA 9	0	0	1128	0	0	0
45	SLE RA 10	0	0	1272	0	0	0
45	SLE RA 11	0	0	1272	0	0	0
45	SLE RA 12	0	0	1272	0	0	0
45	SLE RA 13	0	0	1272	0	0	0
45	SLE RA 14	0	0	1272	0	0	0
45	SLE RA 15	0	0	1272	0	0	0
45	SLE RA 16	0	0	1272	0	0	0
45	SLE RA 17	0	0	1272	0	0	0
45	SLE RA 18	0	0	1334	0	0	0
45	SLE RA 19	0	0	1334	0	0	0
45	SLE RA 20	0	0	1334	0	0	0
45	SLE RA 21	0	0	1334	0	0	0
45	SLE FR 1	0	0	1128	0	0	0
45	SLE FR 2	0	0	1128	0	0	0
45	SLE FR 3	0	0	1128	0	0	0
45	SLE FR 4	0	0	1190	0	0	0
45	SLE FR 5	0	0	1190	0	0	0
45	SLE FR 6	0	0	1231	0	0	0
45	SLE QP 1	0	0	1128	0	0	0
45	SLE QP 2	0	0	1190	0	0	0
45	SLD 1	-4	1	1177	-0.02	6.77	0
45	SLD 2	-4	1	1177	-0.02	6.77	0
45	SLD 3	-4	0	1194	0.02	6.48	0
45	SLD 4	-4	0	1194	0.02	6.48	0
45	SLD 5	-2	2	1161	-0.06	2.47	0
45	SLD 6	-2	2	1161	-0.06	2.47	0
45	SLD 7	-1	-2	1216	0.07	1.51	0
45	SLD 8	-1	-2	1216	0.07	1.51	0
45	SLD 9	1	2	1163	-0.06	-1.51	0
45	SLD 10	1	2	1163	-0.06	-1.51	0
45	SLD 11	2	-2	1218	0.07	-2.47	0
45	SLD 12	2	-2	1218	0.07	-2.47	0
45	SLD 13	4	0	1186	-0.02	-6.48	0
45	SLD 14	4	0	1186	-0.02	-6.48	0
45	SLD 15	4	-1	1202	0.02	-6.77	0
45	SLD 16	4	-1	1202	0.02	-6.77	0
45	SLV 1	-10	2	1157	-0.06	17.22	0
45	SLV 2	-10	2	1157	-0.06	17.22	0
45	SLV 3	-10	-1	1202	0.05	16.49	0
45	SLV 4	-10	-1	1202	0.05	16.49	0
45	SLV 5	-4	6	1111	-0.18	6.27	0
45	SLV 6	-4	6	1111	-0.18	6.27	0
45	SLV 7	-2	-5	1262	0.18	3.84	0
45	SLV 8	-2	-5	1262	0.18	3.84	0
45	SLV 9	2	5	1117	-0.18	-3.84	0
45	SLV 10	2	5	1117	-0.18	-3.84	0
45	SLV 11	4	-6	1268	0.18	-6.27	0
45	SLV 12	4	-6	1268	0.18	-6.27	0
45	SLV 13	10	1	1177	-0.05	-16.49	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
45	SLV 14	10	1	1177	-0.05	-16.49	0
45	SLV 15	10	-2	1222	0.06	-17.22	0
45	SLV 16	10	-2	1222	0.06	-17.22	0
46	SLU 1	0	140	1864	-6.79	0.23	0
46	SLU 2	0	140	1864	-6.79	0.23	0
46	SLU 3	0	140	1864	-6.79	0.23	0
46	SLU 4	0	140	1864	-6.79	0.23	0
46	SLU 5	0	140	1864	-6.79	0.23	0
46	SLU 6	0	140	1864	-6.79	0.23	0
46	SLU 7	0	140	1864	-6.79	0.23	0
46	SLU 8	0	140	1864	-6.79	0.23	0
46	SLU 9	0	140	1864	-6.79	0.23	0
46	SLU 10	0	154	2131	-7.53	0.34	0
46	SLU 11	0	154	2131	-7.53	0.34	0
46	SLU 12	0	154	2131	-7.53	0.34	0
46	SLU 13	0	154	2131	-7.53	0.34	0
46	SLU 14	0	154	2131	-7.53	0.34	0
46	SLU 15	0	154	2131	-7.53	0.34	0
46	SLU 16	0	154	2131	-7.53	0.34	0
46	SLU 17	0	154	2131	-7.53	0.34	0
46	SLU 18	0	161	2245	-7.84	0.39	0
46	SLU 19	0	161	2245	-7.84	0.39	0
46	SLU 20	0	161	2245	-7.84	0.39	0
46	SLU 21	0	161	2245	-7.84	0.39	0
46	SLU 22	0	151	2028	-7.35	0.29	0
46	SLU 23	0	151	2028	-7.35	0.29	0
46	SLU 24	0	151	2028	-7.35	0.29	0
46	SLU 25	0	151	2028	-7.35	0.29	0
46	SLU 26	0	151	2028	-7.35	0.29	0
46	SLU 27	0	151	2028	-7.35	0.29	0
46	SLU 28	0	151	2028	-7.35	0.29	0
46	SLU 29	0	151	2028	-7.35	0.29	0
46	SLU 30	0	151	2028	-7.35	0.29	0
46	SLU 31	0	166	2295	-8.08	0.4	0
46	SLU 32	0	166	2295	-8.08	0.4	0
46	SLU 33	0	166	2295	-8.08	0.4	0
46	SLU 34	0	166	2295	-8.08	0.4	0
46	SLU 35	0	166	2295	-8.08	0.4	0
46	SLU 36	0	166	2295	-8.08	0.4	0
46	SLU 37	0	166	2295	-8.08	0.4	0
46	SLU 38	0	166	2295	-8.08	0.4	0
46	SLU 39	0	172	2410	-8.4	0.44	0
46	SLU 40	0	172	2410	-8.4	0.44	0
46	SLU 41	0	172	2410	-8.4	0.44	0
46	SLU 42	0	172	2410	-8.4	0.44	0
46	SLU 43	0	178	2367	-8.63	0.29	0
46	SLU 44	0	178	2367	-8.63	0.29	0
46	SLU 45	0	178	2367	-8.63	0.29	0
46	SLU 46	0	178	2367	-8.63	0.29	0
46	SLU 47	0	178	2367	-8.63	0.29	0
46	SLU 48	0	178	2367	-8.63	0.29	0
46	SLU 49	0	178	2367	-8.63	0.29	0
46	SLU 50	0	178	2367	-8.63	0.29	0
46	SLU 51	0	178	2367	-8.63	0.29	0
46	SLU 52	0	192	2634	-9.37	0.39	0
46	SLU 53	0	192	2634	-9.37	0.39	0
46	SLU 54	0	192	2634	-9.37	0.39	0
46	SLU 55	0	192	2634	-9.37	0.39	0
46	SLU 56	0	192	2634	-9.37	0.39	0
46	SLU 57	0	192	2634	-9.37	0.39	0
46	SLU 58	0	192	2634	-9.37	0.39	0
46	SLU 59	0	192	2634	-9.37	0.39	0
46	SLU 60	0	199	2748	-9.69	0.44	0
46	SLU 61	0	199	2748	-9.69	0.44	0
46	SLU 62	0	199	2748	-9.69	0.44	0
46	SLU 63	0	199	2748	-9.69	0.44	0
46	SLU 64	0	189	2531	-9.19	0.34	0
46	SLU 65	0	189	2531	-9.19	0.34	0
46	SLU 66	0	189	2531	-9.19	0.34	0
46	SLU 67	0	189	2531	-9.19	0.34	0
46	SLU 68	0	189	2531	-9.19	0.34	0
46	SLU 69	0	189	2531	-9.19	0.34	0
46	SLU 70	0	189	2531	-9.19	0.34	0
46	SLU 71	0	189	2531	-9.19	0.34	0
46	SLU 72	0	189	2531	-9.19	0.34	0
46	SLU 73	0	204	2798	-9.93	0.45	0
46	SLU 74	0	204	2798	-9.93	0.45	0
46	SLU 75	0	204	2798	-9.93	0.45	0
46	SLU 76	0	204	2798	-9.93	0.45	0
46	SLU 77	0	204	2798	-9.93	0.45	0
46	SLU 78	0	204	2798	-9.93	0.45	0
46	SLU 79	0	204	2798	-9.93	0.45	0
46	SLU 80	0	204	2798	-9.93	0.45	0
46	SLU 81	0	210	2913	-10.25	0.49	0
46	SLU 82	0	210	2913	-10.25	0.49	0
46	SLU 83	0	210	2913	-10.25	0.49	0
46	SLU 84	0	210	2913	-10.25	0.49	0
46	SLE RA 1	0	143	1911	-6.95	0.25	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
46	SLE RA 2	0	143	1911	-6.95	0.25	0
46	SLE RA 3	0	143	1911	-6.95	0.25	0
46	SLE RA 4	0	143	1911	-6.95	0.25	0
46	SLE RA 5	0	143	1911	-6.95	0.25	0
46	SLE RA 6	0	143	1911	-6.95	0.25	0
46	SLE RA 7	0	143	1911	-6.95	0.25	0
46	SLE RA 8	0	143	1911	-6.95	0.25	0
46	SLE RA 9	0	143	1911	-6.95	0.25	0
46	SLE RA 10	0	153	2089	-7.44	0.32	0
46	SLE RA 11	0	153	2089	-7.44	0.32	0
46	SLE RA 12	0	153	2089	-7.44	0.32	0
46	SLE RA 13	0	153	2089	-7.44	0.32	0
46	SLE RA 14	0	153	2089	-7.44	0.32	0
46	SLE RA 15	0	153	2089	-7.44	0.32	0
46	SLE RA 16	0	153	2089	-7.44	0.32	0
46	SLE RA 17	0	153	2089	-7.44	0.32	0
46	SLE RA 18	0	157	2165	-7.65	0.35	0
46	SLE RA 19	0	157	2165	-7.65	0.35	0
46	SLE RA 20	0	157	2165	-7.65	0.35	0
46	SLE RA 21	0	157	2165	-7.65	0.35	0
46	SLE FR 1	0	143	1911	-6.95	0.25	0
46	SLE FR 2	0	143	1911	-6.95	0.25	0
46	SLE FR 3	0	143	1911	-6.95	0.25	0
46	SLE FR 4	0	147	1987	-7.16	0.28	0
46	SLE FR 5	0	147	1987	-7.16	0.28	0
46	SLE FR 6	0	150	2038	-7.3	0.3	0
46	SLE QP 1	0	143	1911	-6.95	0.25	0
46	SLE QP 2	0	147	1987	-7.16	0.28	0
46	SLD 1	18	220	2189	-10.79	16.1	-0.01
46	SLD 2	18	220	2189	-10.79	16.1	-0.01
46	SLD 3	26	109	2146	-5.25	24.14	0
46	SLD 4	26	109	2146	-5.25	24.14	0
46	SLD 5	-7	339	2113	-16.65	-7.18	-0.01
46	SLD 6	-7	339	2113	-16.65	-7.18	-0.01
46	SLD 7	20	-34	1969	1.82	19.64	0
46	SLD 8	20	-34	1969	1.82	19.64	0
46	SLD 9	-20	328	2005	-16.13	-19.08	0
46	SLD 10	-20	328	2005	-16.13	-19.08	0
46	SLD 11	7	-44	1861	2.33	7.74	0.01
46	SLD 12	7	-44	1861	2.33	7.74	0.01
46	SLD 13	-26	185	1829	-9.07	-23.58	0
46	SLD 14	-26	185	1829	-9.07	-23.58	0
46	SLD 15	-18	74	1786	-3.53	-15.54	0.01
46	SLD 16	-18	74	1786	-3.53	-15.54	0.01
46	SLV 1	42	321	2460	-15.78	37.9	-0.02
46	SLV 2	42	321	2460	-15.78	37.9	-0.02
46	SLV 3	63	56	2356	-2.59	58.34	-0.01
46	SLV 4	63	56	2356	-2.59	58.34	-0.01
46	SLV 5	-19	602	2288	-29.74	-19.44	-0.01
46	SLV 6	-19	602	2288	-29.74	-19.44	-0.01
46	SLV 7	51	-283	1939	14.21	48.7	0
46	SLV 8	51	-283	1939	14.21	48.7	0
46	SLV 9	-50	577	2036	-28.53	-48.14	0
46	SLV 10	-50	577	2036	-28.53	-48.14	0
46	SLV 11	19	-308	1687	15.42	20	0.01
46	SLV 12	19	-308	1687	15.42	20	0.01
46	SLV 13	-63	239	1619	-11.72	-57.77	0.01
46	SLV 14	-63	239	1619	-11.72	-57.77	0.01
46	SLV 15	-42	-27	1514	1.46	-37.33	0.02
46	SLV 16	-42	-27	1514	1.46	-37.33	0.02
47	SLU 1	0	127	2099	-5.9	-0.23	0
47	SLU 2	0	127	2099	-5.9	-0.23	0
47	SLU 3	0	127	2099	-5.9	-0.23	0
47	SLU 4	0	127	2099	-5.9	-0.23	0
47	SLU 5	0	127	2099	-5.9	-0.23	0
47	SLU 6	0	127	2099	-5.9	-0.23	0
47	SLU 7	0	127	2099	-5.9	-0.23	0
47	SLU 8	0	127	2099	-5.9	-0.23	0
47	SLU 9	0	127	2099	-5.9	-0.23	0
47	SLU 10	0	138	2400	-6.44	-0.33	0
47	SLU 11	0	138	2400	-6.44	-0.33	0
47	SLU 12	0	138	2400	-6.44	-0.33	0
47	SLU 13	0	138	2400	-6.44	-0.33	0
47	SLU 14	0	138	2400	-6.44	-0.33	0
47	SLU 15	0	138	2400	-6.44	-0.33	0
47	SLU 16	0	138	2400	-6.44	-0.33	0
47	SLU 17	0	138	2400	-6.44	-0.33	0
47	SLU 18	0	143	2529	-6.68	-0.38	0
47	SLU 19	0	143	2529	-6.68	-0.38	0
47	SLU 20	0	143	2529	-6.68	-0.38	0
47	SLU 21	0	143	2529	-6.68	-0.38	0
47	SLU 22	0	136	2285	-6.35	-0.28	0
47	SLU 23	0	136	2285	-6.35	-0.28	0
47	SLU 24	0	136	2285	-6.35	-0.28	0
47	SLU 25	0	136	2285	-6.35	-0.28	0
47	SLU 26	0	136	2285	-6.35	-0.28	0
47	SLU 27	0	136	2285	-6.35	-0.28	0
47	SLU 28	0	136	2285	-6.35	-0.28	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
47	SLU 29	0	136	2285	-6.35	-0.28	0
47	SLU 30	0	136	2285	-6.35	-0.28	0
47	SLU 31	0	148	2586	-6.89	-0.39	0
47	SLU 32	0	148	2586	-6.89	-0.39	0
47	SLU 33	0	148	2586	-6.89	-0.39	0
47	SLU 34	0	148	2586	-6.89	-0.39	0
47	SLU 35	0	148	2586	-6.89	-0.39	0
47	SLU 36	0	148	2586	-6.89	-0.39	0
47	SLU 37	0	148	2586	-6.89	-0.39	0
47	SLU 38	0	148	2586	-6.89	-0.39	0
47	SLU 39	0	153	2715	-7.13	-0.43	0
47	SLU 40	0	153	2715	-7.13	-0.43	0
47	SLU 41	0	153	2715	-7.13	-0.43	0
47	SLU 42	0	153	2715	-7.13	-0.43	0
47	SLU 43	0	162	2664	-7.51	-0.27	0
47	SLU 44	0	162	2664	-7.51	-0.27	0
47	SLU 45	0	162	2664	-7.51	-0.27	0
47	SLU 46	0	162	2664	-7.51	-0.27	0
47	SLU 47	0	162	2664	-7.51	-0.27	0
47	SLU 48	0	162	2664	-7.51	-0.27	0
47	SLU 49	0	162	2664	-7.51	-0.27	0
47	SLU 50	0	162	2664	-7.51	-0.27	0
47	SLU 51	0	162	2664	-7.51	-0.27	0
47	SLU 52	0	173	2966	-8.06	-0.38	0
47	SLU 53	0	173	2966	-8.06	-0.38	0
47	SLU 54	0	173	2966	-8.06	-0.38	0
47	SLU 55	0	173	2966	-8.06	-0.38	0
47	SLU 56	0	173	2966	-8.06	-0.38	0
47	SLU 57	0	173	2966	-8.06	-0.38	0
47	SLU 58	0	173	2966	-8.06	-0.38	0
47	SLU 59	0	173	2966	-8.06	-0.38	0
47	SLU 60	0	178	3095	-8.29	-0.43	0
47	SLU 61	0	178	3095	-8.29	-0.43	0
47	SLU 62	0	178	3095	-8.29	-0.43	0
47	SLU 63	0	178	3095	-8.29	-0.43	0
47	SLU 64	0	171	2850	-7.96	-0.33	0
47	SLU 65	0	171	2850	-7.96	-0.33	0
47	SLU 66	0	171	2850	-7.96	-0.33	0
47	SLU 67	0	171	2850	-7.96	-0.33	0
47	SLU 68	0	171	2850	-7.96	-0.33	0
47	SLU 69	0	171	2850	-7.96	-0.33	0
47	SLU 70	0	171	2850	-7.96	-0.33	0
47	SLU 71	0	171	2850	-7.96	-0.33	0
47	SLU 72	0	171	2850	-7.96	-0.33	0
47	SLU 73	0	183	3152	-8.51	-0.44	0
47	SLU 74	0	183	3152	-8.51	-0.44	0
47	SLU 75	0	183	3152	-8.51	-0.44	0
47	SLU 76	0	183	3152	-8.51	-0.44	0
47	SLU 77	0	183	3152	-8.51	-0.44	0
47	SLU 78	0	183	3152	-8.51	-0.44	0
47	SLU 79	0	183	3152	-8.51	-0.44	0
47	SLU 80	0	183	3152	-8.51	-0.44	0
47	SLU 81	0	187	3281	-8.74	-0.48	0
47	SLU 82	0	187	3281	-8.74	-0.48	0
47	SLU 83	0	187	3281	-8.74	-0.48	0
47	SLU 84	0	187	3281	-8.74	-0.48	0
47	SLE RA 1	0	129	2152	-6.02	-0.24	0
47	SLE RA 2	0	129	2152	-6.02	-0.24	0
47	SLE RA 3	0	129	2152	-6.02	-0.24	0
47	SLE RA 4	0	129	2152	-6.02	-0.24	0
47	SLE RA 5	0	129	2152	-6.02	-0.24	0
47	SLE RA 6	0	129	2152	-6.02	-0.24	0
47	SLE RA 7	0	129	2152	-6.02	-0.24	0
47	SLE RA 8	0	129	2152	-6.02	-0.24	0
47	SLE RA 9	0	129	2152	-6.02	-0.24	0
47	SLE RA 10	0	137	2353	-6.39	-0.31	0
47	SLE RA 11	0	137	2353	-6.39	-0.31	0
47	SLE RA 12	0	137	2353	-6.39	-0.31	0
47	SLE RA 13	0	137	2353	-6.39	-0.31	0
47	SLE RA 14	0	137	2353	-6.39	-0.31	0
47	SLE RA 15	0	137	2353	-6.39	-0.31	0
47	SLE RA 16	0	137	2353	-6.39	-0.31	0
47	SLE RA 17	0	137	2353	-6.39	-0.31	0
47	SLE RA 18	0	140	2439	-6.54	-0.34	0
47	SLE RA 19	0	140	2439	-6.54	-0.34	0
47	SLE RA 20	0	140	2439	-6.54	-0.34	0
47	SLE RA 21	0	140	2439	-6.54	-0.34	0
47	SLE FR 1	0	129	2152	-6.02	-0.24	0
47	SLE FR 2	0	129	2152	-6.02	-0.24	0
47	SLE FR 3	0	129	2152	-6.02	-0.24	0
47	SLE FR 4	0	133	2238	-6.18	-0.27	0
47	SLE FR 5	0	133	2238	-6.18	-0.27	0
47	SLE FR 6	0	135	2295	-6.28	-0.29	0
47	SLE QP 1	0	129	2152	-6.02	-0.24	0
47	SLE QP 2	0	133	2238	-6.18	-0.27	0
47	SLD 1	29	181	2048	-8.52	26.79	0
47	SLD 2	29	181	2048	-8.52	26.79	0
47	SLD 3	22	48	2006	-2.08	19.16	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
47	SLD 4	22	48	2006	-2.08	19.16	-0.01
47	SLD 5	20	349	2244	-16.64	19.41	0
47	SLD 6	20	349	2244	-16.64	19.41	0
47	SLD 7	-5	-95	2105	4.81	-6.01	-0.01
47	SLD 8	-5	-95	2105	4.81	-6.01	-0.01
47	SLD 9	5	360	2371	-17.17	5.46	0.01
47	SLD 10	5	360	2371	-17.17	5.46	0.01
47	SLD 11	-20	-84	2232	4.28	-19.96	0
47	SLD 12	-20	-84	2232	4.28	-19.96	0
47	SLD 13	-22	218	2470	-10.28	-19.71	0.01
47	SLD 14	-22	218	2470	-10.28	-19.71	0.01
47	SLD 15	-29	84	2428	-3.84	-27.33	0
47	SLD 16	-29	84	2428	-3.84	-27.33	0
47	SLV 1	70	248	1795	-11.78	65.46	-0.01
47	SLV 2	70	248	1795	-11.78	65.46	-0.01
47	SLV 3	52	-69	1694	3.57	46.13	-0.02
47	SLV 4	52	-69	1694	3.57	46.13	-0.02
47	SLV 5	50	649	2259	-31.14	48.77	0.01
47	SLV 6	50	649	2259	-31.14	48.77	0.01
47	SLV 7	-13	-409	1921	20.02	-15.67	-0.01
47	SLV 8	-13	-409	1921	20.02	-15.67	-0.01
47	SLV 9	13	675	2555	-32.38	15.13	0.01
47	SLV 10	13	675	2555	-32.38	15.13	0.01
47	SLV 11	-50	-383	2217	18.78	-49.31	-0.01
47	SLV 12	-50	-383	2217	18.78	-49.31	-0.01
47	SLV 13	-52	335	2782	-15.93	-46.67	0.02
47	SLV 14	-52	335	2782	-15.93	-46.67	0.02
47	SLV 15	-70	17	2680	-0.58	-66	0.01
47	SLV 16	-70	17	2680	-0.58	-66	0.01
48	SLU 1	0	0	1105	0	0	0
48	SLU 2	0	0	1105	0	0	0
48	SLU 3	0	0	1105	0	0	0
48	SLU 4	0	0	1105	0	0	0
48	SLU 5	0	0	1105	0	0	0
48	SLU 6	0	0	1105	0	0	0
48	SLU 7	0	0	1105	0	0	0
48	SLU 8	0	0	1105	0	0	0
48	SLU 9	0	0	1105	0	0	0
48	SLU 10	0	0	1327	0	0	0
48	SLU 11	0	0	1327	0	0	0
48	SLU 12	0	0	1327	0	0	0
48	SLU 13	0	0	1327	0	0	0
48	SLU 14	0	0	1327	0	0	0
48	SLU 15	0	0	1327	0	0	0
48	SLU 16	0	0	1327	0	0	0
48	SLU 17	0	0	1327	0	0	0
48	SLU 18	0	0	1422	0	0	0
48	SLU 19	0	0	1422	0	0	0
48	SLU 20	0	0	1422	0	0	0
48	SLU 21	0	0	1422	0	0	0
48	SLU 22	0	0	1239	0	0	0
48	SLU 23	0	0	1239	0	0	0
48	SLU 24	0	0	1239	0	0	0
48	SLU 25	0	0	1239	0	0	0
48	SLU 26	0	0	1239	0	0	0
48	SLU 27	0	0	1239	0	0	0
48	SLU 28	0	0	1239	0	0	0
48	SLU 29	0	0	1239	0	0	0
48	SLU 30	0	0	1239	0	0	0
48	SLU 31	0	0	1461	0	0	0
48	SLU 32	0	0	1461	0	0	0
48	SLU 33	0	0	1461	0	0	0
48	SLU 34	0	0	1461	0	0	0
48	SLU 35	0	0	1461	0	0	0
48	SLU 36	0	0	1461	0	0	0
48	SLU 37	0	0	1461	0	0	0
48	SLU 38	0	0	1461	0	0	0
48	SLU 39	0	0	1556	0	0	0
48	SLU 40	0	0	1556	0	0	0
48	SLU 41	0	0	1556	0	0	0
48	SLU 42	0	0	1556	0	0	0
48	SLU 43	0	0	1390	0	0	0
48	SLU 44	0	0	1390	0	0	0
48	SLU 45	0	0	1390	0	0	0
48	SLU 46	0	0	1390	0	0	0
48	SLU 47	0	0	1390	0	0	0
48	SLU 48	0	0	1390	0	0	0
48	SLU 49	0	0	1390	0	0	0
48	SLU 50	0	0	1390	0	0	0
48	SLU 51	0	0	1390	0	0	0
48	SLU 52	0	0	1612	0	0	0
48	SLU 53	0	0	1612	0	0	0
48	SLU 54	0	0	1612	0	0	0
48	SLU 55	0	0	1612	0	0	0
48	SLU 56	0	0	1612	0	0	0
48	SLU 57	0	0	1612	0	0	0
48	SLU 58	0	0	1612	0	0	0
48	SLU 59	0	0	1612	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
48	SLU 60	0	0	1707	0	0	0
48	SLU 61	0	0	1707	0	0	0
48	SLU 62	0	0	1707	0	0	0
48	SLU 63	0	0	1707	0	0	0
48	SLU 64	0	0	1524	0	0	0
48	SLU 65	0	0	1524	0	0	0
48	SLU 66	0	0	1524	0	0	0
48	SLU 67	0	0	1524	0	0	0
48	SLU 68	0	0	1524	0	0	0
48	SLU 69	0	0	1524	0	0	0
48	SLU 70	0	0	1524	0	0	0
48	SLU 71	0	0	1524	0	0	0
48	SLU 72	0	0	1524	0	0	0
48	SLU 73	0	0	1746	0	0	0
48	SLU 74	0	0	1746	0	0	0
48	SLU 75	0	0	1746	0	0	0
48	SLU 76	0	0	1746	0	0	0
48	SLU 77	0	0	1746	0	0	0
48	SLU 78	0	0	1746	0	0	0
48	SLU 79	0	0	1746	0	0	0
48	SLU 80	0	0	1746	0	0	0
48	SLU 81	0	0	1841	0	0	0
48	SLU 82	0	0	1841	0	0	0
48	SLU 83	0	0	1841	0	0	0
48	SLU 84	0	0	1841	0	0	0
48	SLE RA 1	0	0	1143	0	0	0
48	SLE RA 2	0	0	1143	0	0	0
48	SLE RA 3	0	0	1143	0	0	0
48	SLE RA 4	0	0	1143	0	0	0
48	SLE RA 5	0	0	1143	0	0	0
48	SLE RA 6	0	0	1143	0	0	0
48	SLE RA 7	0	0	1143	0	0	0
48	SLE RA 8	0	0	1143	0	0	0
48	SLE RA 9	0	0	1143	0	0	0
48	SLE RA 10	0	0	1291	0	0	0
48	SLE RA 11	0	0	1291	0	0	0
48	SLE RA 12	0	0	1291	0	0	0
48	SLE RA 13	0	0	1291	0	0	0
48	SLE RA 14	0	0	1291	0	0	0
48	SLE RA 15	0	0	1291	0	0	0
48	SLE RA 16	0	0	1291	0	0	0
48	SLE RA 17	0	0	1291	0	0	0
48	SLE RA 18	0	0	1354	0	0	0
48	SLE RA 19	0	0	1354	0	0	0
48	SLE RA 20	0	0	1354	0	0	0
48	SLE RA 21	0	0	1354	0	0	0
48	SLE FR 1	0	0	1143	0	0	0
48	SLE FR 2	0	0	1143	0	0	0
48	SLE FR 3	0	0	1143	0	0	0
48	SLE FR 4	0	0	1206	0	0	0
48	SLE FR 5	0	0	1206	0	0	0
48	SLE FR 6	0	0	1249	0	0	0
48	SLE QP 1	0	0	1143	0	0	0
48	SLE QP 2	0	0	1206	0	0	0
48	SLD 1	-4	0	1199	-0.05	7.27	0
48	SLD 2	-4	0	1199	-0.05	7.27	0
48	SLD 3	-4	-1	1207	0.05	6.96	0
48	SLD 4	-4	-1	1207	0.05	6.96	0
48	SLD 5	-2	2	1191	-0.16	2.65	0
48	SLD 6	-2	2	1191	-0.16	2.65	0
48	SLD 7	-1	-2	1220	0.16	1.62	0
48	SLD 8	-1	-2	1220	0.16	1.62	0
48	SLD 9	1	2	1193	-0.16	-1.62	0
48	SLD 10	1	2	1193	-0.16	-1.62	0
48	SLD 11	2	-2	1222	0.16	-2.65	0
48	SLD 12	2	-2	1222	0.16	-2.65	0
48	SLD 13	4	1	1205	-0.05	-6.96	0
48	SLD 14	4	1	1205	-0.05	-6.96	0
48	SLD 15	4	0	1214	0.05	-7.27	0
48	SLD 16	4	0	1214	0.05	-7.27	0
48	SLV 1	-11	1	1187	-0.13	18.47	0
48	SLV 2	-11	1	1187	-0.13	18.47	0
48	SLV 3	-10	-2	1209	0.13	17.68	0
48	SLV 4	-10	-2	1209	0.13	17.68	0
48	SLV 5	-4	5	1167	-0.44	6.73	0
48	SLV 6	-4	5	1167	-0.44	6.73	0
48	SLV 7	-2	-5	1241	0.44	4.12	0
48	SLV 8	-2	-5	1241	0.44	4.12	0
48	SLV 9	2	5	1171	-0.44	-4.12	0
48	SLV 10	2	5	1171	-0.44	-4.12	0
48	SLV 11	4	-5	1246	0.44	-6.73	0
48	SLV 12	4	-5	1246	0.44	-6.73	0
48	SLV 13	10	2	1203	-0.13	-17.68	0
48	SLV 14	10	2	1203	-0.13	-17.68	0
48	SLV 15	11	-1	1226	0.13	-18.47	0
48	SLV 16	11	-1	1226	0.13	-18.47	0
49	SLU 1	0	128	1869	-6.19	0.27	0
49	SLU 2	0	128	1869	-6.19	0.27	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
49	SLU 3	0	128	1869	-6.19	0.27	0
49	SLU 4	0	128	1869	-6.19	0.27	0
49	SLU 5	0	128	1869	-6.19	0.27	0
49	SLU 6	0	128	1869	-6.19	0.27	0
49	SLU 7	0	128	1869	-6.19	0.27	0
49	SLU 8	0	128	1869	-6.19	0.27	0
49	SLU 9	0	128	1869	-6.19	0.27	0
49	SLU 10	0	148	2132	-7.17	0.41	0
49	SLU 11	0	148	2132	-7.17	0.41	0
49	SLU 12	0	148	2132	-7.17	0.41	0
49	SLU 13	0	148	2132	-7.17	0.41	0
49	SLU 14	0	148	2132	-7.17	0.41	0
49	SLU 15	0	148	2132	-7.17	0.41	0
49	SLU 16	0	148	2132	-7.17	0.41	0
49	SLU 17	0	148	2132	-7.17	0.41	0
49	SLU 18	0	156	2246	-7.59	0.47	0
49	SLU 19	0	156	2246	-7.59	0.47	0
49	SLU 20	0	156	2246	-7.59	0.47	0
49	SLU 21	0	156	2246	-7.59	0.47	0
49	SLU 22	0	142	2032	-6.87	0.35	0
49	SLU 23	0	142	2032	-6.87	0.35	0
49	SLU 24	0	142	2032	-6.87	0.35	0
49	SLU 25	0	142	2032	-6.87	0.35	0
49	SLU 26	0	142	2032	-6.87	0.35	0
49	SLU 27	0	142	2032	-6.87	0.35	0
49	SLU 28	0	142	2032	-6.87	0.35	0
49	SLU 29	0	142	2032	-6.87	0.35	0
49	SLU 30	0	142	2032	-6.87	0.35	0
49	SLU 31	0	162	2296	-7.84	0.48	0
49	SLU 32	0	162	2296	-7.84	0.48	0
49	SLU 33	0	162	2296	-7.84	0.48	0
49	SLU 34	0	162	2296	-7.84	0.48	0
49	SLU 35	0	162	2296	-7.84	0.48	0
49	SLU 36	0	162	2296	-7.84	0.48	0
49	SLU 37	0	162	2296	-7.84	0.48	0
49	SLU 38	0	162	2296	-7.84	0.48	0
49	SLU 39	0	170	2409	-8.26	0.54	0
49	SLU 40	0	170	2409	-8.26	0.54	0
49	SLU 41	0	170	2409	-8.26	0.54	0
49	SLU 42	0	170	2409	-8.26	0.54	0
49	SLU 43	0	162	2373	-7.82	0.33	0
49	SLU 44	0	162	2373	-7.82	0.33	0
49	SLU 45	0	162	2373	-7.82	0.33	0
49	SLU 46	0	162	2373	-7.82	0.33	0
49	SLU 47	0	162	2373	-7.82	0.33	0
49	SLU 48	0	162	2373	-7.82	0.33	0
49	SLU 49	0	162	2373	-7.82	0.33	0
49	SLU 50	0	162	2373	-7.82	0.33	0
49	SLU 51	0	162	2373	-7.82	0.33	0
49	SLU 52	0	182	2637	-8.8	0.47	0
49	SLU 53	0	182	2637	-8.8	0.47	0
49	SLU 54	0	182	2637	-8.8	0.47	0
49	SLU 55	0	182	2637	-8.8	0.47	0
49	SLU 56	0	182	2637	-8.8	0.47	0
49	SLU 57	0	182	2637	-8.8	0.47	0
49	SLU 58	0	182	2637	-8.8	0.47	0
49	SLU 59	0	182	2637	-8.8	0.47	0
49	SLU 60	0	190	2750	-9.22	0.53	0
49	SLU 61	0	190	2750	-9.22	0.53	0
49	SLU 62	0	190	2750	-9.22	0.53	0
49	SLU 63	0	190	2750	-9.22	0.53	0
49	SLU 64	0	176	2537	-8.49	0.4	0
49	SLU 65	0	176	2537	-8.49	0.4	0
49	SLU 66	0	176	2537	-8.49	0.4	0
49	SLU 67	0	176	2537	-8.49	0.4	0
49	SLU 68	0	176	2537	-8.49	0.4	0
49	SLU 69	0	176	2537	-8.49	0.4	0
49	SLU 70	0	176	2537	-8.49	0.4	0
49	SLU 71	0	176	2537	-8.49	0.4	0
49	SLU 72	0	176	2537	-8.49	0.4	0
49	SLU 73	0	195	2801	-9.47	0.54	0
49	SLU 74	0	195	2801	-9.47	0.54	0
49	SLU 75	0	195	2801	-9.47	0.54	0
49	SLU 76	0	195	2801	-9.47	0.54	0
49	SLU 77	0	195	2801	-9.47	0.54	0
49	SLU 78	0	195	2801	-9.47	0.54	0
49	SLU 79	0	195	2801	-9.47	0.54	0
49	SLU 80	0	195	2801	-9.47	0.54	0
49	SLU 81	0	204	2914	-9.89	0.6	0
49	SLU 82	0	204	2914	-9.89	0.6	0
49	SLU 83	0	204	2914	-9.89	0.6	0
49	SLU 84	0	204	2914	-9.89	0.6	0
49	SLE RA 1	0	132	1915	-6.39	0.29	0
49	SLE RA 2	0	132	1915	-6.39	0.29	0
49	SLE RA 3	0	132	1915	-6.39	0.29	0
49	SLE RA 4	0	132	1915	-6.39	0.29	0
49	SLE RA 5	0	132	1915	-6.39	0.29	0
49	SLE RA 6	0	132	1915	-6.39	0.29	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
49	SLE RA 7	0	132	1915	-6.39	0.29	0
49	SLE RA 8	0	132	1915	-6.39	0.29	0
49	SLE RA 9	0	132	1915	-6.39	0.29	0
49	SLE RA 10	0	145	2091	-7.04	0.39	0
49	SLE RA 11	0	145	2091	-7.04	0.39	0
49	SLE RA 12	0	145	2091	-7.04	0.39	0
49	SLE RA 13	0	145	2091	-7.04	0.39	0
49	SLE RA 14	0	145	2091	-7.04	0.39	0
49	SLE RA 15	0	145	2091	-7.04	0.39	0
49	SLE RA 16	0	145	2091	-7.04	0.39	0
49	SLE RA 17	0	145	2091	-7.04	0.39	0
49	SLE RA 18	0	151	2167	-7.32	0.42	0
49	SLE RA 19	0	151	2167	-7.32	0.42	0
49	SLE RA 20	0	151	2167	-7.32	0.42	0
49	SLE RA 21	0	151	2167	-7.32	0.42	0
49	SLE FR 1	0	132	1915	-6.39	0.29	0
49	SLE FR 2	0	132	1915	-6.39	0.29	0
49	SLE FR 3	0	132	1915	-6.39	0.29	0
49	SLE FR 4	0	138	1991	-6.67	0.33	0
49	SLE FR 5	0	138	1991	-6.67	0.33	0
49	SLE FR 6	0	141	2041	-6.85	0.36	0
49	SLE QP 1	0	132	1915	-6.39	0.29	0
49	SLE QP 2	0	138	1991	-6.67	0.33	0
49	SLD 1	19	212	2187	-10.27	16.42	0
49	SLD 2	19	212	2187	-10.27	16.42	0
49	SLD 3	26	98	2153	-4.74	23.98	0
49	SLD 4	26	98	2153	-4.74	23.98	0
49	SLD 5	-5	332	2101	-16.14	-6.31	0
49	SLD 6	-5	332	2101	-16.14	-6.31	0
49	SLD 7	18	-46	1988	2.3	18.9	0
49	SLD 8	18	-46	1988	2.3	18.9	0
49	SLD 9	-18	321	1993	-15.63	-18.23	0
49	SLD 10	-18	321	1993	-15.63	-18.23	0
49	SLD 11	5	-56	1881	2.81	6.98	0
49	SLD 12	5	-56	1881	2.81	6.98	0
49	SLD 13	-25	177	1828	-8.59	-23.31	0
49	SLD 14	-25	177	1828	-8.59	-23.31	0
49	SLD 15	-18	64	1794	-3.06	-15.75	0
49	SLD 16	-18	64	1794	-3.06	-15.75	0
49	SLV 1	44	313	2451	-15.18	38.51	0
49	SLV 2	44	313	2451	-15.18	38.51	0
49	SLV 3	62	44	2369	-2.07	57.74	0.01
49	SLV 4	62	44	2369	-2.07	57.74	0.01
49	SLV 5	-14	598	2253	-29.11	-17.37	-0.01
49	SLV 6	-14	598	2253	-29.11	-17.37	-0.01
49	SLV 7	46	-299	1980	14.6	46.72	0.01
49	SLV 8	46	-299	1980	14.6	46.72	0.01
49	SLV 9	-45	574	2001	-27.93	-46.05	-0.01
49	SLV 10	-45	574	2001	-27.93	-46.05	-0.01
49	SLV 11	14	-323	1729	15.78	18.04	0.01
49	SLV 12	14	-323	1729	15.78	18.04	0.01
49	SLV 13	-61	232	1613	-11.26	-57.07	-0.01
49	SLV 14	-61	232	1613	-11.26	-57.07	-0.01
49	SLV 15	-43	-37	1531	1.85	-37.85	0
49	SLV 16	-43	-37	1531	1.85	-37.85	0
50	SLU 1	0	111	2135	-5.01	-0.28	0
50	SLU 2	0	111	2135	-5.01	-0.28	0
50	SLU 3	0	111	2135	-5.01	-0.28	0
50	SLU 4	0	111	2135	-5.01	-0.28	0
50	SLU 5	0	111	2135	-5.01	-0.28	0
50	SLU 6	0	111	2135	-5.01	-0.28	0
50	SLU 7	0	111	2135	-5.01	-0.28	0
50	SLU 8	0	111	2135	-5.01	-0.28	0
50	SLU 9	0	111	2135	-5.01	-0.28	0
50	SLU 10	0	129	2445	-5.76	-0.42	0
50	SLU 11	0	129	2445	-5.76	-0.42	0
50	SLU 12	0	129	2445	-5.76	-0.42	0
50	SLU 13	0	129	2445	-5.76	-0.42	0
50	SLU 14	0	129	2445	-5.76	-0.42	0
50	SLU 15	0	129	2445	-5.76	-0.42	0
50	SLU 16	0	129	2445	-5.76	-0.42	0
50	SLU 17	0	129	2445	-5.76	-0.42	0
50	SLU 18	0	137	2577	-6.09	-0.48	0
50	SLU 19	0	137	2577	-6.09	-0.48	0
50	SLU 20	0	137	2577	-6.09	-0.48	0
50	SLU 21	0	137	2577	-6.09	-0.48	0
50	SLU 22	0	124	2327	-5.55	-0.35	0
50	SLU 23	0	124	2327	-5.55	-0.35	0
50	SLU 24	0	124	2327	-5.55	-0.35	0
50	SLU 25	0	124	2327	-5.55	-0.35	0
50	SLU 26	0	124	2327	-5.55	-0.35	0
50	SLU 27	0	124	2327	-5.55	-0.35	0
50	SLU 28	0	124	2327	-5.55	-0.35	0
50	SLU 29	0	124	2327	-5.55	-0.35	0
50	SLU 30	0	124	2327	-5.55	-0.35	0
50	SLU 31	0	142	2636	-6.3	-0.49	0
50	SLU 32	0	142	2636	-6.3	-0.49	0
50	SLU 33	0	142	2636	-6.3	-0.49	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
50	SLU 34	0	142	2636	-6.3	-0.49	0
50	SLU 35	0	142	2636	-6.3	-0.49	0
50	SLU 36	0	142	2636	-6.3	-0.49	0
50	SLU 37	0	142	2636	-6.3	-0.49	0
50	SLU 38	0	142	2636	-6.3	-0.49	0
50	SLU 39	0	149	2769	-6.62	-0.55	0
50	SLU 40	0	149	2769	-6.62	-0.55	0
50	SLU 41	0	149	2769	-6.62	-0.55	0
50	SLU 42	0	149	2769	-6.62	-0.55	0
50	SLU 43	0	140	2710	-6.33	-0.33	0
50	SLU 44	0	140	2710	-6.33	-0.33	0
50	SLU 45	0	140	2710	-6.33	-0.33	0
50	SLU 46	0	140	2710	-6.33	-0.33	0
50	SLU 47	0	140	2710	-6.33	-0.33	0
50	SLU 48	0	140	2710	-6.33	-0.33	0
50	SLU 49	0	140	2710	-6.33	-0.33	0
50	SLU 50	0	140	2710	-6.33	-0.33	0
50	SLU 51	0	140	2710	-6.33	-0.33	0
50	SLU 52	0	158	3019	-7.08	-0.48	0
50	SLU 53	0	158	3019	-7.08	-0.48	0
50	SLU 54	0	158	3019	-7.08	-0.48	0
50	SLU 55	0	158	3019	-7.08	-0.48	0
50	SLU 56	0	158	3019	-7.08	-0.48	0
50	SLU 57	0	158	3019	-7.08	-0.48	0
50	SLU 58	0	158	3019	-7.08	-0.48	0
50	SLU 59	0	158	3019	-7.08	-0.48	0
50	SLU 60	0	166	3152	-7.41	-0.54	0
50	SLU 61	0	166	3152	-7.41	-0.54	0
50	SLU 62	0	166	3152	-7.41	-0.54	0
50	SLU 63	0	166	3152	-7.41	-0.54	0
50	SLU 64	0	153	2902	-6.87	-0.41	0
50	SLU 65	0	153	2902	-6.87	-0.41	0
50	SLU 66	0	153	2902	-6.87	-0.41	0
50	SLU 67	0	153	2902	-6.87	-0.41	0
50	SLU 68	0	153	2902	-6.87	-0.41	0
50	SLU 69	0	153	2902	-6.87	-0.41	0
50	SLU 70	0	153	2902	-6.87	-0.41	0
50	SLU 71	0	153	2902	-6.87	-0.41	0
50	SLU 72	0	153	2902	-6.87	-0.41	0
50	SLU 73	0	171	3211	-7.62	-0.55	0
50	SLU 74	0	171	3211	-7.62	-0.55	0
50	SLU 75	0	171	3211	-7.62	-0.55	0
50	SLU 76	0	171	3211	-7.62	-0.55	0
50	SLU 77	0	171	3211	-7.62	-0.55	0
50	SLU 78	0	171	3211	-7.62	-0.55	0
50	SLU 79	0	171	3211	-7.62	-0.55	0
50	SLU 80	0	171	3211	-7.62	-0.55	0
50	SLU 81	0	178	3344	-7.94	-0.61	0
50	SLU 82	0	178	3344	-7.94	-0.61	0
50	SLU 83	0	178	3344	-7.94	-0.61	0
50	SLU 84	0	178	3344	-7.94	-0.61	0
50	SLE RA 1	0	115	2190	-5.16	-0.3	0
50	SLE RA 2	0	115	2190	-5.16	-0.3	0
50	SLE RA 3	0	115	2190	-5.16	-0.3	0
50	SLE RA 4	0	115	2190	-5.16	-0.3	0
50	SLE RA 5	0	115	2190	-5.16	-0.3	0
50	SLE RA 6	0	115	2190	-5.16	-0.3	0
50	SLE RA 7	0	115	2190	-5.16	-0.3	0
50	SLE RA 8	0	115	2190	-5.16	-0.3	0
50	SLE RA 9	0	115	2190	-5.16	-0.3	0
50	SLE RA 10	0	127	2396	-5.67	-0.39	0
50	SLE RA 11	0	127	2396	-5.67	-0.39	0
50	SLE RA 12	0	127	2396	-5.67	-0.39	0
50	SLE RA 13	0	127	2396	-5.67	-0.39	0
50	SLE RA 14	0	127	2396	-5.67	-0.39	0
50	SLE RA 15	0	127	2396	-5.67	-0.39	0
50	SLE RA 16	0	127	2396	-5.67	-0.39	0
50	SLE RA 17	0	127	2396	-5.67	-0.39	0
50	SLE RA 18	0	132	2485	-5.88	-0.43	0
50	SLE RA 19	0	132	2485	-5.88	-0.43	0
50	SLE RA 20	0	132	2485	-5.88	-0.43	0
50	SLE RA 21	0	132	2485	-5.88	-0.43	0
50	SLE FR 1	0	115	2190	-5.16	-0.3	0
50	SLE FR 2	0	115	2190	-5.16	-0.3	0
50	SLE FR 3	0	115	2190	-5.16	-0.3	0
50	SLE FR 4	0	120	2278	-5.38	-0.34	0
50	SLE FR 5	0	120	2278	-5.38	-0.34	0
50	SLE FR 6	0	123	2337	-5.52	-0.36	0
50	SLE QP 1	0	115	2190	-5.16	-0.3	0
50	SLE QP 2	0	120	2278	-5.38	-0.34	0
50	SLD 1	21	171	2076	-7.82	25.59	0
50	SLD 2	21	171	2076	-7.82	25.59	0
50	SLD 3	27	36	2047	-1.35	18.56	0
50	SLD 4	27	36	2047	-1.35	18.56	0
50	SLD 5	-4	340	2262	-15.93	18.1	0.01
50	SLD 6	-4	340	2262	-15.93	18.1	0.01
50	SLD 7	18	-110	2164	5.65	-5.33	0
50	SLD 8	18	-110	2164	5.65	-5.33	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
50	SLD 9	-18	350	2392	-16.41	4.65	0
50	SLD 10	-18	350	2392	-16.41	4.65	0
50	SLD 11	4	-100	2295	5.17	-18.78	-0.01
50	SLD 12	4	-100	2295	5.17	-18.78	-0.01
50	SLD 13	-27	204	2510	-9.41	-19.24	0
50	SLD 14	-27	204	2510	-9.41	-19.24	0
50	SLD 15	-21	69	2480	-2.94	-26.27	0
50	SLD 16	-21	69	2480	-2.94	-26.27	0
50	SLV 1	49	241	1807	-11.22	62.5	0.01
50	SLV 2	49	241	1807	-11.22	62.5	0.01
50	SLV 3	66	-80	1736	4.21	44.65	0
50	SLV 4	66	-80	1736	4.21	44.65	0
50	SLV 5	-10	644	2245	-30.54	45.58	0.01
50	SLV 6	-10	644	2245	-30.54	45.58	0.01
50	SLV 7	45	-428	2007	20.91	-13.91	-0.01
50	SLV 8	45	-428	2007	20.91	-13.91	-0.01
50	SLV 9	-45	668	2549	-31.66	13.23	0.01
50	SLV 10	-45	668	2549	-31.66	13.23	0.01
50	SLV 11	10	-404	2311	19.78	-46.26	-0.01
50	SLV 12	10	-404	2311	19.78	-46.26	-0.01
50	SLV 13	-66	320	2821	-14.97	-45.33	0
50	SLV 14	-66	320	2821	-14.97	-45.33	0
50	SLV 15	-49	-2	2749	0.46	-63.17	-0.01
50	SLV 16	-49	-2	2749	0.46	-63.17	-0.01
51	SLU 1	0	0	1119	0	0	0
51	SLU 2	0	0	1119	0	0	0
51	SLU 3	0	0	1119	0	0	0
51	SLU 4	0	0	1119	0	0	0
51	SLU 5	0	0	1119	0	0	0
51	SLU 6	0	0	1119	0	0	0
51	SLU 7	0	0	1119	0	0	0
51	SLU 8	0	0	1119	0	0	0
51	SLU 9	0	0	1119	0	0	0
51	SLU 10	0	0	1351	0	0	0
51	SLU 11	0	0	1351	0	0	0
51	SLU 12	0	0	1351	0	0	0
51	SLU 13	0	0	1351	0	0	0
51	SLU 14	0	0	1351	0	0	0
51	SLU 15	0	0	1351	0	0	0
51	SLU 16	0	0	1351	0	0	0
51	SLU 17	0	0	1351	0	0	0
51	SLU 18	0	0	1450	0	0	0
51	SLU 19	0	0	1450	0	0	0
51	SLU 20	0	0	1450	0	0	0
51	SLU 21	0	0	1450	0	0	0
51	SLU 22	0	0	1258	0	0	0
51	SLU 23	0	0	1258	0	0	0
51	SLU 24	0	0	1258	0	0	0
51	SLU 25	0	0	1258	0	0	0
51	SLU 26	0	0	1258	0	0	0
51	SLU 27	0	0	1258	0	0	0
51	SLU 28	0	0	1258	0	0	0
51	SLU 29	0	0	1258	0	0	0
51	SLU 30	0	0	1258	0	0	0
51	SLU 31	0	0	1490	0	0	0
51	SLU 32	0	0	1490	0	0	0
51	SLU 33	0	0	1490	0	0	0
51	SLU 34	0	0	1490	0	0	0
51	SLU 35	0	0	1490	0	0	0
51	SLU 36	0	0	1490	0	0	0
51	SLU 37	0	0	1490	0	0	0
51	SLU 38	0	0	1490	0	0	0
51	SLU 39	0	0	1590	0	0	0
51	SLU 40	0	0	1590	0	0	0
51	SLU 41	0	0	1590	0	0	0
51	SLU 42	0	0	1590	0	0	0
51	SLU 43	0	0	1407	0	0	0
51	SLU 44	0	0	1407	0	0	0
51	SLU 45	0	0	1407	0	0	0
51	SLU 46	0	0	1407	0	0	0
51	SLU 47	0	0	1407	0	0	0
51	SLU 48	0	0	1407	0	0	0
51	SLU 49	0	0	1407	0	0	0
51	SLU 50	0	0	1407	0	0	0
51	SLU 51	0	0	1407	0	0	0
51	SLU 52	0	0	1638	0	0	0
51	SLU 53	0	0	1638	0	0	0
51	SLU 54	0	0	1638	0	0	0
51	SLU 55	0	0	1638	0	0	0
51	SLU 56	0	0	1638	0	0	0
51	SLU 57	0	0	1638	0	0	0
51	SLU 58	0	0	1638	0	0	0
51	SLU 59	0	0	1638	0	0	0
51	SLU 60	0	0	1738	0	0	0
51	SLU 61	0	0	1738	0	0	0
51	SLU 62	0	0	1738	0	0	0
51	SLU 63	0	0	1738	0	0	0
51	SLU 64	0	0	1546	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
51	SLU 65	0	0	1546	0	0	0
51	SLU 66	0	0	1546	0	0	0
51	SLU 67	0	0	1546	0	0	0
51	SLU 68	0	0	1546	0	0	0
51	SLU 69	0	0	1546	0	0	0
51	SLU 70	0	0	1546	0	0	0
51	SLU 71	0	0	1546	0	0	0
51	SLU 72	0	0	1546	0	0	0
51	SLU 73	0	0	1778	0	0	0
51	SLU 74	0	0	1778	0	0	0
51	SLU 75	0	0	1778	0	0	0
51	SLU 76	0	0	1778	0	0	0
51	SLU 77	0	0	1778	0	0	0
51	SLU 78	0	0	1778	0	0	0
51	SLU 79	0	0	1778	0	0	0
51	SLU 80	0	0	1778	0	0	0
51	SLU 81	0	0	1877	0	0	0
51	SLU 82	0	0	1877	0	0	0
51	SLU 83	0	0	1877	0	0	0
51	SLU 84	0	0	1877	0	0	0
51	SLE RA 1	0	0	1159	0	0	0
51	SLE RA 2	0	0	1159	0	0	0
51	SLE RA 3	0	0	1159	0	0	0
51	SLE RA 4	0	0	1159	0	0	0
51	SLE RA 5	0	0	1159	0	0	0
51	SLE RA 6	0	0	1159	0	0	0
51	SLE RA 7	0	0	1159	0	0	0
51	SLE RA 8	0	0	1159	0	0	0
51	SLE RA 9	0	0	1159	0	0	0
51	SLE RA 10	0	0	1313	0	0	0
51	SLE RA 11	0	0	1313	0	0	0
51	SLE RA 12	0	0	1313	0	0	0
51	SLE RA 13	0	0	1313	0	0	0
51	SLE RA 14	0	0	1313	0	0	0
51	SLE RA 15	0	0	1313	0	0	0
51	SLE RA 16	0	0	1313	0	0	0
51	SLE RA 17	0	0	1313	0	0	0
51	SLE RA 18	0	0	1379	0	0	0
51	SLE RA 19	0	0	1379	0	0	0
51	SLE RA 20	0	0	1379	0	0	0
51	SLE RA 21	0	0	1379	0	0	0
51	SLE FR 1	0	0	1159	0	0	0
51	SLE FR 2	0	0	1159	0	0	0
51	SLE FR 3	0	0	1159	0	0	0
51	SLE FR 4	0	0	1225	0	0	0
51	SLE FR 5	0	0	1225	0	0	0
51	SLE FR 6	0	0	1269	0	0	0
51	SLE QP 1	0	0	1159	0	0	0
51	SLE QP 2	0	0	1225	0	0	0
51	SLD 1	-5	0	1219	-0.02	7.15	0
51	SLD 2	-5	0	1219	-0.02	7.15	0
51	SLD 3	-4	-1	1226	0.02	6.84	0
51	SLD 4	-4	-1	1226	0.02	6.84	0
51	SLD 5	-2	2	1212	-0.07	2.62	0
51	SLD 6	-2	2	1212	-0.07	2.62	0
51	SLD 7	-1	-2	1236	0.07	1.58	0
51	SLD 8	-1	-2	1236	0.07	1.58	0
51	SLD 9	1	2	1214	-0.07	-1.58	0
51	SLD 10	1	2	1214	-0.07	-1.58	0
51	SLD 11	2	-2	1238	0.07	-2.62	0
51	SLD 12	2	-2	1238	0.07	-2.62	0
51	SLD 13	4	1	1224	-0.02	-6.84	0
51	SLD 14	4	1	1224	-0.02	-6.84	0
51	SLD 15	5	0	1231	0.02	-7.15	0
51	SLD 16	5	0	1231	0.02	-7.15	0
51	SLV 1	-12	1	1209	-0.06	18.14	0
51	SLV 2	-12	1	1209	-0.06	18.14	0
51	SLV 3	-11	-2	1227	0.06	17.36	0
51	SLV 4	-11	-2	1227	0.06	17.36	0
51	SLV 5	-4	5	1193	-0.2	6.63	0
51	SLV 6	-4	5	1193	-0.2	6.63	0
51	SLV 7	-2	-6	1253	0.2	4.02	0
51	SLV 8	-2	-6	1253	0.2	4.02	0
51	SLV 9	2	6	1197	-0.2	-4.02	0
51	SLV 10	2	6	1197	-0.2	-4.02	0
51	SLV 11	4	-5	1257	0.2	-6.63	0
51	SLV 12	4	-5	1257	0.2	-6.63	0
51	SLV 13	11	2	1222	-0.06	-17.36	0
51	SLV 14	11	2	1222	-0.06	-17.36	0
51	SLV 15	12	-1	1240	0.06	-18.14	0
51	SLV 16	12	-1	1240	0.06	-18.14	0
52	SLU 1	0	119	1885	-5.57	0.36	0
52	SLU 2	0	119	1885	-5.57	0.36	0
52	SLU 3	0	119	1885	-5.57	0.36	0
52	SLU 4	0	119	1885	-5.57	0.36	0
52	SLU 5	0	119	1885	-5.57	0.36	0
52	SLU 6	0	119	1885	-5.57	0.36	0
52	SLU 7	0	119	1885	-5.57	0.36	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
52	SLU 8	0	119	1885	-5.57	0.36	0
52	SLU 9	0	119	1885	-5.57	0.36	0
52	SLU 10	0	143	2153	-6.7	0.55	0
52	SLU 11	0	143	2153	-6.7	0.55	0
52	SLU 12	0	143	2153	-6.7	0.55	0
52	SLU 13	0	143	2153	-6.7	0.55	0
52	SLU 14	0	143	2153	-6.7	0.55	0
52	SLU 15	0	143	2153	-6.7	0.55	0
52	SLU 16	0	143	2153	-6.7	0.55	0
52	SLU 17	0	143	2153	-6.7	0.55	0
52	SLU 18	0	154	2268	-7.18	0.63	0
52	SLU 19	0	154	2268	-7.18	0.63	0
52	SLU 20	0	154	2268	-7.18	0.63	0
52	SLU 21	0	154	2268	-7.18	0.63	0
52	SLU 22	0	135	2051	-6.3	0.46	0
52	SLU 23	0	135	2051	-6.3	0.46	0
52	SLU 24	0	135	2051	-6.3	0.46	0
52	SLU 25	0	135	2051	-6.3	0.46	0
52	SLU 26	0	135	2051	-6.3	0.46	0
52	SLU 27	0	135	2051	-6.3	0.46	0
52	SLU 28	0	135	2051	-6.3	0.46	0
52	SLU 29	0	135	2051	-6.3	0.46	0
52	SLU 30	0	135	2051	-6.3	0.46	0
52	SLU 31	0	159	2320	-7.43	0.64	0
52	SLU 32	0	159	2320	-7.43	0.64	0
52	SLU 33	0	159	2320	-7.43	0.64	0
52	SLU 34	0	159	2320	-7.43	0.64	0
52	SLU 35	0	159	2320	-7.43	0.64	0
52	SLU 36	0	159	2320	-7.43	0.64	0
52	SLU 37	0	159	2320	-7.43	0.64	0
52	SLU 38	0	159	2320	-7.43	0.64	0
52	SLU 39	0	170	2435	-7.92	0.72	0
52	SLU 40	0	170	2435	-7.92	0.72	0
52	SLU 41	0	170	2435	-7.92	0.72	0
52	SLU 42	0	170	2435	-7.92	0.72	0
52	SLU 43	0	149	2393	-6.99	0.43	0
52	SLU 44	0	149	2393	-6.99	0.43	0
52	SLU 45	0	149	2393	-6.99	0.43	0
52	SLU 46	0	149	2393	-6.99	0.43	0
52	SLU 47	0	149	2393	-6.99	0.43	0
52	SLU 48	0	149	2393	-6.99	0.43	0
52	SLU 49	0	149	2393	-6.99	0.43	0
52	SLU 50	0	149	2393	-6.99	0.43	0
52	SLU 51	0	149	2393	-6.99	0.43	0
52	SLU 52	0	173	2661	-8.12	0.62	0
52	SLU 53	0	173	2661	-8.12	0.62	0
52	SLU 54	0	173	2661	-8.12	0.62	0
52	SLU 55	0	173	2661	-8.12	0.62	0
52	SLU 56	0	173	2661	-8.12	0.62	0
52	SLU 57	0	173	2661	-8.12	0.62	0
52	SLU 58	0	173	2661	-8.12	0.62	0
52	SLU 59	0	173	2661	-8.12	0.62	0
52	SLU 60	0	184	2776	-8.6	0.7	0
52	SLU 61	0	184	2776	-8.6	0.7	0
52	SLU 62	0	184	2776	-8.6	0.7	0
52	SLU 63	0	184	2776	-8.6	0.7	0
52	SLU 64	0	165	2560	-7.72	0.53	0
52	SLU 65	0	165	2560	-7.72	0.53	0
52	SLU 66	0	165	2560	-7.72	0.53	0
52	SLU 67	0	165	2560	-7.72	0.53	0
52	SLU 68	0	165	2560	-7.72	0.53	0
52	SLU 69	0	165	2560	-7.72	0.53	0
52	SLU 70	0	165	2560	-7.72	0.53	0
52	SLU 71	0	165	2560	-7.72	0.53	0
52	SLU 72	0	165	2560	-7.72	0.53	0
52	SLU 73	0	189	2828	-8.85	0.72	0
52	SLU 74	0	189	2828	-8.85	0.72	0
52	SLU 75	0	189	2828	-8.85	0.72	0
52	SLU 76	0	189	2828	-8.85	0.72	0
52	SLU 77	0	189	2828	-8.85	0.72	0
52	SLU 78	0	189	2828	-8.85	0.72	0
52	SLU 79	0	189	2828	-8.85	0.72	0
52	SLU 80	0	189	2828	-8.85	0.72	0
52	SLU 81	0	200	2943	-9.34	0.8	0
52	SLU 82	0	200	2943	-9.34	0.8	0
52	SLU 83	0	200	2943	-9.34	0.8	0
52	SLU 84	0	200	2943	-9.34	0.8	0
52	SLE RA 1	0	123	1932	-5.78	0.39	0
52	SLE RA 2	0	123	1932	-5.78	0.39	0
52	SLE RA 3	0	123	1932	-5.78	0.39	0
52	SLE RA 4	0	123	1932	-5.78	0.39	0
52	SLE RA 5	0	123	1932	-5.78	0.39	0
52	SLE RA 6	0	123	1932	-5.78	0.39	0
52	SLE RA 7	0	123	1932	-5.78	0.39	0
52	SLE RA 8	0	123	1932	-5.78	0.39	0
52	SLE RA 9	0	123	1932	-5.78	0.39	0
52	SLE RA 10	0	140	2111	-6.53	0.51	0
52	SLE RA 11	0	140	2111	-6.53	0.51	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
52	SLE RA 12	0	140	2111	-6.53	0.51	0
52	SLE RA 13	0	140	2111	-6.53	0.51	0
52	SLE RA 14	0	140	2111	-6.53	0.51	0
52	SLE RA 15	0	140	2111	-6.53	0.51	0
52	SLE RA 16	0	140	2111	-6.53	0.51	0
52	SLE RA 17	0	140	2111	-6.53	0.51	0
52	SLE RA 18	0	147	2188	-6.86	0.57	0
52	SLE RA 19	0	147	2188	-6.86	0.57	0
52	SLE RA 20	0	147	2188	-6.86	0.57	0
52	SLE RA 21	0	147	2188	-6.86	0.57	0
52	SLE FR 1	0	123	1932	-5.78	0.39	0
52	SLE FR 2	0	123	1932	-5.78	0.39	0
52	SLE FR 3	0	123	1932	-5.78	0.39	0
52	SLE FR 4	0	130	2009	-6.1	0.44	0
52	SLE FR 5	0	130	2009	-6.1	0.44	0
52	SLE FR 6	0	135	2060	-6.32	0.48	0
52	SLE QP 1	0	123	1932	-5.78	0.39	0
52	SLE QP 2	0	130	2009	-6.1	0.44	0
52	SLD 1	22	207	2205	-9.84	21.57	0
52	SLD 2	22	207	2205	-9.84	21.57	0
52	SLD 3	16	92	2179	-4.18	14.63	0
52	SLD 4	16	92	2179	-4.18	14.63	0
52	SLD 5	16	328	2108	-15.8	17.3	0
52	SLD 6	16	328	2108	-15.8	17.3	0
52	SLD 7	-5	-57	2020	3.06	-5.82	0.01
52	SLD 8	-5	-57	2020	3.06	-5.82	0.01
52	SLD 9	5	317	1998	-15.26	6.71	0
52	SLD 10	5	317	1998	-15.26	6.71	0
52	SLD 11	-16	-68	1910	3.6	-16.42	0
52	SLD 12	-16	-68	1910	3.6	-16.42	0
52	SLD 13	-15	169	1839	-8.02	-13.75	0
52	SLD 14	-15	169	1839	-8.02	-13.75	0
52	SLD 15	-22	53	1813	-2.37	-20.69	0
52	SLD 16	-22	53	1813	-2.37	-20.69	0
52	SLV 1	53	312	2468	-14.96	51.7	0.01
52	SLV 2	53	312	2468	-14.96	51.7	0.01
52	SLV 3	36	38	2404	-1.5	33.97	0.01
52	SLV 4	36	38	2404	-1.5	33.97	0.01
52	SLV 5	41	601	2244	-29.19	42.7	-0.01
52	SLV 6	41	601	2244	-29.19	42.7	-0.01
52	SLV 7	-14	-314	2030	15.7	-16.38	0.01
52	SLV 8	-14	-314	2030	15.7	-16.38	0.01
52	SLV 9	14	574	1987	-27.91	17.26	-0.01
52	SLV 10	14	574	1987	-27.91	17.26	-0.01
52	SLV 11	-40	-340	1774	16.98	-41.82	0.01
52	SLV 12	-40	-340	1774	16.98	-41.82	0.01
52	SLV 13	-36	223	1614	-10.71	-33.09	-0.01
52	SLV 14	-36	223	1614	-10.71	-33.09	-0.01
52	SLV 15	-52	-52	1550	2.76	-50.82	-0.01
52	SLV 16	-52	-52	1550	2.76	-50.82	-0.01
53	SLU 1	0	96	2194	-4.09	-0.38	0
53	SLU 2	0	96	2194	-4.09	-0.38	0
53	SLU 3	0	96	2194	-4.09	-0.38	0
53	SLU 4	0	96	2194	-4.09	-0.38	0
53	SLU 5	0	96	2194	-4.09	-0.38	0
53	SLU 6	0	96	2194	-4.09	-0.38	0
53	SLU 7	0	96	2194	-4.09	-0.38	0
53	SLU 8	0	96	2194	-4.09	-0.38	0
53	SLU 9	0	96	2194	-4.09	-0.38	0
53	SLU 10	0	121	2524	-5.15	-0.58	0
53	SLU 11	0	121	2524	-5.15	-0.58	0
53	SLU 12	0	121	2524	-5.15	-0.58	0
53	SLU 13	0	121	2524	-5.15	-0.58	0
53	SLU 14	0	121	2524	-5.15	-0.58	0
53	SLU 15	0	121	2524	-5.15	-0.58	0
53	SLU 16	0	121	2524	-5.15	-0.58	0
53	SLU 17	0	121	2524	-5.15	-0.58	0
53	SLU 18	0	132	2666	-5.6	-0.67	0
53	SLU 19	0	132	2666	-5.6	-0.67	0
53	SLU 20	0	132	2666	-5.6	-0.67	0
53	SLU 21	0	132	2666	-5.6	-0.67	0
53	SLU 22	0	112	2398	-4.77	-0.48	0
53	SLU 23	0	112	2398	-4.77	-0.48	0
53	SLU 24	0	112	2398	-4.77	-0.48	0
53	SLU 25	0	112	2398	-4.77	-0.48	0
53	SLU 26	0	112	2398	-4.77	-0.48	0
53	SLU 27	0	112	2398	-4.77	-0.48	0
53	SLU 28	0	112	2398	-4.77	-0.48	0
53	SLU 29	0	112	2398	-4.77	-0.48	0
53	SLU 30	0	112	2398	-4.77	-0.48	0
53	SLU 31	0	137	2728	-5.83	-0.69	0
53	SLU 32	0	137	2728	-5.83	-0.69	0
53	SLU 33	0	137	2728	-5.83	-0.69	0
53	SLU 34	0	137	2728	-5.83	-0.69	0
53	SLU 35	0	137	2728	-5.83	-0.69	0
53	SLU 36	0	137	2728	-5.83	-0.69	0
53	SLU 37	0	137	2728	-5.83	-0.69	0
53	SLU 38	0	137	2728	-5.83	-0.69	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
53	SLU 39	0	148	2870	-6.28	-0.77	0
53	SLU 40	0	148	2870	-6.28	-0.77	0
53	SLU 41	0	148	2870	-6.28	-0.77	0
53	SLU 42	0	148	2870	-6.28	-0.77	0
53	SLU 43	0	119	2783	-5.08	-0.46	0
53	SLU 44	0	119	2783	-5.08	-0.46	0
53	SLU 45	0	119	2783	-5.08	-0.46	0
53	SLU 46	0	119	2783	-5.08	-0.46	0
53	SLU 47	0	119	2783	-5.08	-0.46	0
53	SLU 48	0	119	2783	-5.08	-0.46	0
53	SLU 49	0	119	2783	-5.08	-0.46	0
53	SLU 50	0	119	2783	-5.08	-0.46	0
53	SLU 51	0	119	2783	-5.08	-0.46	0
53	SLU 52	0	144	3113	-6.14	-0.66	0
53	SLU 53	0	144	3113	-6.14	-0.66	0
53	SLU 54	0	144	3113	-6.14	-0.66	0
53	SLU 55	0	144	3113	-6.14	-0.66	0
53	SLU 56	0	144	3113	-6.14	-0.66	0
53	SLU 57	0	144	3113	-6.14	-0.66	0
53	SLU 58	0	144	3113	-6.14	-0.66	0
53	SLU 59	0	144	3113	-6.14	-0.66	0
53	SLU 60	0	155	3254	-6.59	-0.75	0
53	SLU 61	0	155	3254	-6.59	-0.75	0
53	SLU 62	0	155	3254	-6.59	-0.75	0
53	SLU 63	0	155	3254	-6.59	-0.75	0
53	SLU 64	0	135	2987	-5.76	-0.56	0
53	SLU 65	0	135	2987	-5.76	-0.56	0
53	SLU 66	0	135	2987	-5.76	-0.56	0
53	SLU 67	0	135	2987	-5.76	-0.56	0
53	SLU 68	0	135	2987	-5.76	-0.56	0
53	SLU 69	0	135	2987	-5.76	-0.56	0
53	SLU 70	0	135	2987	-5.76	-0.56	0
53	SLU 71	0	135	2987	-5.76	-0.56	0
53	SLU 72	0	135	2987	-5.76	-0.56	0
53	SLU 73	0	160	3317	-6.82	-0.76	0
53	SLU 74	0	160	3317	-6.82	-0.76	0
53	SLU 75	0	160	3317	-6.82	-0.76	0
53	SLU 76	0	160	3317	-6.82	-0.76	0
53	SLU 77	0	160	3317	-6.82	-0.76	0
53	SLU 78	0	160	3317	-6.82	-0.76	0
53	SLU 79	0	160	3317	-6.82	-0.76	0
53	SLU 80	0	160	3317	-6.82	-0.76	0
53	SLU 81	0	171	3458	-7.27	-0.85	0
53	SLU 82	0	171	3458	-7.27	-0.85	0
53	SLU 83	0	171	3458	-7.27	-0.85	0
53	SLU 84	0	171	3458	-7.27	-0.85	0
53	SLE RA 1	0	100	2253	-4.28	-0.41	0
53	SLE RA 2	0	100	2253	-4.28	-0.41	0
53	SLE RA 3	0	100	2253	-4.28	-0.41	0
53	SLE RA 4	0	100	2253	-4.28	-0.41	0
53	SLE RA 5	0	100	2253	-4.28	-0.41	0
53	SLE RA 6	0	100	2253	-4.28	-0.41	0
53	SLE RA 7	0	100	2253	-4.28	-0.41	0
53	SLE RA 8	0	100	2253	-4.28	-0.41	0
53	SLE RA 9	0	100	2253	-4.28	-0.41	0
53	SLE RA 10	0	117	2473	-4.99	-0.54	0
53	SLE RA 11	0	117	2473	-4.99	-0.54	0
53	SLE RA 12	0	117	2473	-4.99	-0.54	0
53	SLE RA 13	0	117	2473	-4.99	-0.54	0
53	SLE RA 14	0	117	2473	-4.99	-0.54	0
53	SLE RA 15	0	117	2473	-4.99	-0.54	0
53	SLE RA 16	0	117	2473	-4.99	-0.54	0
53	SLE RA 17	0	117	2473	-4.99	-0.54	0
53	SLE RA 18	0	125	2567	-5.29	-0.6	0
53	SLE RA 19	0	125	2567	-5.29	-0.6	0
53	SLE RA 20	0	125	2567	-5.29	-0.6	0
53	SLE RA 21	0	125	2567	-5.29	-0.6	0
53	SLE FR 1	0	100	2253	-4.28	-0.41	0
53	SLE FR 2	0	100	2253	-4.28	-0.41	0
53	SLE FR 3	0	100	2253	-4.28	-0.41	0
53	SLE FR 4	0	108	2347	-4.58	-0.47	0
53	SLE FR 5	0	108	2347	-4.58	-0.47	0
53	SLE FR 6	0	112	2410	-4.79	-0.51	0
53	SLE QP 1	0	100	2253	-4.28	-0.41	0
53	SLE QP 2	0	108	2347	-4.58	-0.47	0
53	SLD 1	15	158	2125	-7.01	15.27	0.01
53	SLD 2	15	158	2125	-7.01	15.27	0.01
53	SLD 3	22	23	2108	-0.55	21.76	0.01
53	SLD 4	22	23	2108	-0.55	21.76	0.01
53	SLD 5	-6	327	2306	-15.11	-5.6	0.01
53	SLD 6	-6	327	2306	-15.11	-5.6	0.01
53	SLD 7	17	-122	2249	6.43	16.05	0
53	SLD 8	17	-122	2249	6.43	16.05	0
53	SLD 9	-17	337	2444	-15.59	-16.98	0
53	SLD 10	-17	337	2444	-15.59	-16.98	0
53	SLD 11	5	-112	2388	5.95	4.66	-0.01
53	SLD 12	5	-112	2388	5.95	4.66	-0.01
53	SLD 13	-22	192	2586	-8.62	-22.69	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
53	SLD 14	-22	192	2586	-8.62	-22.69	-0.01
53	SLD 15	-16	57	2569	-2.15	-16.2	-0.01
53	SLD 16	-16	57	2569	-2.15	-16.2	-0.01
53	SLV 1	36	228	1829	-10.4	36.76	0.02
53	SLV 2	36	228	1829	-10.4	36.76	0.02
53	SLV 3	53	-93	1787	5	53.4	0.01
53	SLV 4	53	-93	1787	5	53.4	0.01
53	SLV 5	-16	631	2254	-29.7	-14.53	0.02
53	SLV 6	-16	631	2254	-29.7	-14.53	0.02
53	SLV 7	42	-440	2116	21.66	40.93	-0.01
53	SLV 8	42	-440	2116	21.66	40.93	-0.01
53	SLV 9	-42	655	2578	-30.83	-41.86	0.01
53	SLV 10	-42	655	2578	-30.83	-41.86	0.01
53	SLV 11	15	-416	2439	20.53	13.6	-0.02
53	SLV 12	15	-416	2439	20.53	13.6	-0.02
53	SLV 13	-54	308	2906	-14.17	-54.33	-0.01
53	SLV 14	-54	308	2906	-14.17	-54.33	-0.01
53	SLV 15	-36	-13	2865	1.23	-37.69	-0.02
53	SLV 16	-36	-13	2865	1.23	-37.69	-0.02
54	SLU 1	0	0	1133	0	0	0
54	SLU 2	0	0	1133	0	0	0
54	SLU 3	0	0	1133	0	0	0
54	SLU 4	0	0	1133	0	0	0
54	SLU 5	0	0	1133	0	0	0
54	SLU 6	0	0	1133	0	0	0
54	SLU 7	0	0	1133	0	0	0
54	SLU 8	0	0	1133	0	0	0
54	SLU 9	0	0	1133	0	0	0
54	SLU 10	0	0	1378	0	0	0
54	SLU 11	0	0	1378	0	0	0
54	SLU 12	0	0	1378	0	0	0
54	SLU 13	0	0	1378	0	0	0
54	SLU 14	0	0	1378	0	0	0
54	SLU 15	0	0	1378	0	0	0
54	SLU 16	0	0	1378	0	0	0
54	SLU 17	0	0	1378	0	0	0
54	SLU 18	0	0	1484	0	0	0
54	SLU 19	0	0	1484	0	0	0
54	SLU 20	0	0	1484	0	0	0
54	SLU 21	0	0	1484	0	0	0
54	SLU 22	0	0	1279	0	0	0
54	SLU 23	0	0	1279	0	0	0
54	SLU 24	0	0	1279	0	0	0
54	SLU 25	0	0	1279	0	0	0
54	SLU 26	0	0	1279	0	0	0
54	SLU 27	0	0	1279	0	0	0
54	SLU 28	0	0	1279	0	0	0
54	SLU 29	0	0	1279	0	0	0
54	SLU 30	0	0	1279	0	0	0
54	SLU 31	0	0	1525	0	0	0
54	SLU 32	0	0	1525	0	0	0
54	SLU 33	0	0	1525	0	0	0
54	SLU 34	0	0	1525	0	0	0
54	SLU 35	0	0	1525	0	0	0
54	SLU 36	0	0	1525	0	0	0
54	SLU 37	0	0	1525	0	0	0
54	SLU 38	0	0	1525	0	0	0
54	SLU 39	0	0	1630	0	0	0
54	SLU 40	0	0	1630	0	0	0
54	SLU 41	0	0	1630	0	0	0
54	SLU 42	0	0	1630	0	0	0
54	SLU 43	0	0	1422	0	0	0
54	SLU 44	0	0	1422	0	0	0
54	SLU 45	0	0	1422	0	0	0
54	SLU 46	0	0	1422	0	0	0
54	SLU 47	0	0	1422	0	0	0
54	SLU 48	0	0	1422	0	0	0
54	SLU 49	0	0	1422	0	0	0
54	SLU 50	0	0	1422	0	0	0
54	SLU 51	0	0	1422	0	0	0
54	SLU 52	0	0	1668	0	0	0
54	SLU 53	0	0	1668	0	0	0
54	SLU 54	0	0	1668	0	0	0
54	SLU 55	0	0	1668	0	0	0
54	SLU 56	0	0	1668	0	0	0
54	SLU 57	0	0	1668	0	0	0
54	SLU 58	0	0	1668	0	0	0
54	SLU 59	0	0	1668	0	0	0
54	SLU 60	0	0	1773	0	0	0
54	SLU 61	0	0	1773	0	0	0
54	SLU 62	0	0	1773	0	0	0
54	SLU 63	0	0	1773	0	0	0
54	SLU 64	0	0	1569	0	0	0
54	SLU 65	0	0	1569	0	0	0
54	SLU 66	0	0	1569	0	0	0
54	SLU 67	0	0	1569	0	0	0
54	SLU 68	0	0	1569	0	0	0
54	SLU 69	0	0	1569	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
54	SLU 70	0	0	1569	0	0	0
54	SLU 71	0	0	1569	0	0	0
54	SLU 72	0	0	1569	0	0	0
54	SLU 73	0	0	1814	0	0	0
54	SLU 74	0	0	1814	0	0	0
54	SLU 75	0	0	1814	0	0	0
54	SLU 76	0	0	1814	0	0	0
54	SLU 77	0	0	1814	0	0	0
54	SLU 78	0	0	1814	0	0	0
54	SLU 79	0	0	1814	0	0	0
54	SLU 80	0	0	1814	0	0	0
54	SLU 81	0	0	1920	0	0	0
54	SLU 82	0	0	1920	0	0	0
54	SLU 83	0	0	1920	0	0	0
54	SLU 84	0	0	1920	0	0	0
54	SLE RA 1	0	0	1174	0	0	0
54	SLE RA 2	0	0	1174	0	0	0
54	SLE RA 3	0	0	1174	0	0	0
54	SLE RA 4	0	0	1174	0	0	0
54	SLE RA 5	0	0	1174	0	0	0
54	SLE RA 6	0	0	1174	0	0	0
54	SLE RA 7	0	0	1174	0	0	0
54	SLE RA 8	0	0	1174	0	0	0
54	SLE RA 9	0	0	1174	0	0	0
54	SLE RA 10	0	0	1338	0	0	0
54	SLE RA 11	0	0	1338	0	0	0
54	SLE RA 12	0	0	1338	0	0	0
54	SLE RA 13	0	0	1338	0	0	0
54	SLE RA 14	0	0	1338	0	0	0
54	SLE RA 15	0	0	1338	0	0	0
54	SLE RA 16	0	0	1338	0	0	0
54	SLE RA 17	0	0	1338	0	0	0
54	SLE RA 18	0	0	1408	0	0	0
54	SLE RA 19	0	0	1408	0	0	0
54	SLE RA 20	0	0	1408	0	0	0
54	SLE RA 21	0	0	1408	0	0	0
54	SLE FR 1	0	0	1174	0	0	0
54	SLE FR 2	0	0	1174	0	0	0
54	SLE FR 3	0	0	1174	0	0	0
54	SLE FR 4	0	0	1245	0	0	0
54	SLE FR 5	0	0	1245	0	0	0
54	SLE FR 6	0	0	1291	0	0	0
54	SLE QP 1	0	0	1174	0	0	0
54	SLE QP 2	0	0	1245	0	0	0
54	SLD 1	5	0	1246	-0.05	6.6	0
54	SLD 2	5	0	1246	-0.05	6.6	0
54	SLD 3	5	-1	1239	0.05	6.3	0
54	SLD 4	5	-1	1239	0.05	6.3	0
54	SLD 5	1	2	1254	-0.16	2.43	0
54	SLD 6	1	2	1254	-0.16	2.43	0
54	SLD 7	2	-2	1234	0.16	1.44	0
54	SLD 8	2	-2	1234	0.16	1.44	0
54	SLD 9	-2	2	1256	-0.16	-1.44	0
54	SLD 10	-2	2	1256	-0.16	-1.44	0
54	SLD 11	-1	-2	1235	0.16	-2.43	0
54	SLD 12	-1	-2	1235	0.16	-2.43	0
54	SLD 13	-5	1	1250	-0.05	-6.3	0
54	SLD 14	-5	1	1250	-0.05	-6.3	0
54	SLD 15	-5	0	1244	0.05	-6.6	0
54	SLD 16	-5	0	1244	0.05	-6.6	0
54	SLV 1	12	1	1247	-0.13	16.71	0
54	SLV 2	12	1	1247	-0.13	16.71	0
54	SLV 3	12	-2	1232	0.13	15.97	0
54	SLV 4	12	-2	1232	0.13	15.97	0
54	SLV 5	2	5	1269	-0.45	6.14	0
54	SLV 6	2	5	1269	-0.45	6.14	0
54	SLV 7	5	-5	1217	0.45	3.66	0
54	SLV 8	5	-5	1217	0.45	3.66	0
54	SLV 9	-5	6	1272	-0.45	-3.66	0
54	SLV 10	-5	6	1272	-0.45	-3.66	0
54	SLV 11	-2	-5	1220	0.45	-6.14	0
54	SLV 12	-2	-5	1220	0.45	-6.14	0
54	SLV 13	-12	2	1257	-0.14	-15.97	0
54	SLV 14	-12	2	1257	-0.14	-15.97	0
54	SLV 15	-12	-1	1242	0.13	-16.71	0
54	SLV 16	-12	-1	1242	0.13	-16.71	0
55	SLU 1	0	113	1914	-5.25	0.5	0
55	SLU 2	0	113	1914	-5.25	0.5	0
55	SLU 3	0	113	1914	-5.25	0.5	0
55	SLU 4	0	113	1914	-5.25	0.5	0
55	SLU 5	0	113	1914	-5.25	0.5	0
55	SLU 6	0	113	1914	-5.25	0.5	0
55	SLU 7	0	113	1914	-5.25	0.5	0
55	SLU 8	0	113	1914	-5.25	0.5	0
55	SLU 9	0	113	1914	-5.25	0.5	0
55	SLU 10	1	143	2194	-6.63	0.76	0
55	SLU 11	1	143	2194	-6.63	0.76	0
55	SLU 12	1	143	2194	-6.63	0.76	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
55	SLU 13	1	143	2194	-6.63	0.76	0
55	SLU 14	1	143	2194	-6.63	0.76	0
55	SLU 15	1	143	2194	-6.63	0.76	0
55	SLU 16	1	143	2194	-6.63	0.76	0
55	SLU 17	1	143	2194	-6.63	0.76	0
55	SLU 18	1	156	2314	-7.22	0.87	0
55	SLU 19	1	156	2314	-7.22	0.87	0
55	SLU 20	1	156	2314	-7.22	0.87	0
55	SLU 21	1	156	2314	-7.22	0.87	0
55	SLU 22	0	132	2088	-6.11	0.64	0
55	SLU 23	0	132	2088	-6.11	0.64	0
55	SLU 24	0	132	2088	-6.11	0.64	0
55	SLU 25	0	132	2088	-6.11	0.64	0
55	SLU 26	0	132	2088	-6.11	0.64	0
55	SLU 27	0	132	2088	-6.11	0.64	0
55	SLU 28	0	132	2088	-6.11	0.64	0
55	SLU 29	0	132	2088	-6.11	0.64	0
55	SLU 30	0	132	2088	-6.11	0.64	0
55	SLU 31	1	162	2368	-7.48	0.9	0
55	SLU 32	1	162	2368	-7.48	0.9	0
55	SLU 33	1	162	2368	-7.48	0.9	0
55	SLU 34	1	162	2368	-7.48	0.9	0
55	SLU 35	1	162	2368	-7.48	0.9	0
55	SLU 36	1	162	2368	-7.48	0.9	0
55	SLU 37	1	162	2368	-7.48	0.9	0
55	SLU 38	1	162	2368	-7.48	0.9	0
55	SLU 39	1	175	2488	-8.08	1.01	0
55	SLU 40	1	175	2488	-8.08	1.01	0
55	SLU 41	1	175	2488	-8.08	1.01	0
55	SLU 42	1	175	2488	-8.08	1.01	0
55	SLU 43	0	140	2428	-6.54	0.6	0
55	SLU 44	0	140	2428	-6.54	0.6	0
55	SLU 45	0	140	2428	-6.54	0.6	0
55	SLU 46	0	140	2428	-6.54	0.6	0
55	SLU 47	0	140	2428	-6.54	0.6	0
55	SLU 48	0	140	2428	-6.54	0.6	0
55	SLU 49	0	140	2428	-6.54	0.6	0
55	SLU 50	0	140	2428	-6.54	0.6	0
55	SLU 51	0	140	2428	-6.54	0.6	0
55	SLU 52	1	171	2708	-7.91	0.87	0
55	SLU 53	1	171	2708	-7.91	0.87	0
55	SLU 54	1	171	2708	-7.91	0.87	0
55	SLU 55	1	171	2708	-7.91	0.87	0
55	SLU 56	1	171	2708	-7.91	0.87	0
55	SLU 57	1	171	2708	-7.91	0.87	0
55	SLU 58	1	171	2708	-7.91	0.87	0
55	SLU 59	1	171	2708	-7.91	0.87	0
55	SLU 60	1	184	2829	-8.51	0.98	0
55	SLU 61	1	184	2829	-8.51	0.98	0
55	SLU 62	1	184	2829	-8.51	0.98	0
55	SLU 63	1	184	2829	-8.51	0.98	0
55	SLU 64	1	159	2602	-7.39	0.74	0
55	SLU 65	1	159	2602	-7.39	0.74	0
55	SLU 66	1	159	2602	-7.39	0.74	0
55	SLU 67	1	159	2602	-7.39	0.74	0
55	SLU 68	1	159	2602	-7.39	0.74	0
55	SLU 69	1	159	2602	-7.39	0.74	0
55	SLU 70	1	159	2602	-7.39	0.74	0
55	SLU 71	1	159	2602	-7.39	0.74	0
55	SLU 72	1	159	2602	-7.39	0.74	0
55	SLU 73	1	189	2883	-8.77	1	0
55	SLU 74	1	189	2883	-8.77	1	0
55	SLU 75	1	189	2883	-8.77	1	0
55	SLU 76	1	189	2883	-8.77	1	0
55	SLU 77	1	189	2883	-8.77	1	0
55	SLU 78	1	189	2883	-8.77	1	0
55	SLU 79	1	189	2883	-8.77	1	0
55	SLU 80	1	189	2883	-8.77	1	0
55	SLU 81	1	202	3003	-9.36	1.11	0
55	SLU 82	1	202	3003	-9.36	1.11	0
55	SLU 83	1	202	3003	-9.36	1.11	0
55	SLU 84	1	202	3003	-9.36	1.11	0
55	SLE RA 1	0	118	1963	-5.5	0.54	0
55	SLE RA 2	0	118	1963	-5.5	0.54	0
55	SLE RA 3	0	118	1963	-5.5	0.54	0
55	SLE RA 4	0	118	1963	-5.5	0.54	0
55	SLE RA 5	0	118	1963	-5.5	0.54	0
55	SLE RA 6	0	118	1963	-5.5	0.54	0
55	SLE RA 7	0	118	1963	-5.5	0.54	0
55	SLE RA 8	0	118	1963	-5.5	0.54	0
55	SLE RA 9	0	118	1963	-5.5	0.54	0
55	SLE RA 10	1	138	2150	-6.42	0.71	0
55	SLE RA 11	1	138	2150	-6.42	0.71	0
55	SLE RA 12	1	138	2150	-6.42	0.71	0
55	SLE RA 13	1	138	2150	-6.42	0.71	0
55	SLE RA 14	1	138	2150	-6.42	0.71	0
55	SLE RA 15	1	138	2150	-6.42	0.71	0
55	SLE RA 16	1	138	2150	-6.42	0.71	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
55	SLE RA 17	1	138	2150	-6.42	0.71	0
55	SLE RA 18	1	147	2230	-6.81	0.79	0
55	SLE RA 19	1	147	2230	-6.81	0.79	0
55	SLE RA 20	1	147	2230	-6.81	0.79	0
55	SLE RA 21	1	147	2230	-6.81	0.79	0
55	SLE FR 1	0	118	1963	-5.5	0.54	0
55	SLE FR 2	0	118	1963	-5.5	0.54	0
55	SLE FR 3	0	118	1963	-5.5	0.54	0
55	SLE FR 4	0	127	2044	-5.89	0.62	0
55	SLE FR 5	0	127	2044	-5.89	0.62	0
55	SLE FR 6	0	133	2097	-6.15	0.66	0
55	SLE QP 1	0	118	1963	-5.5	0.54	0
55	SLE QP 2	0	127	2044	-5.89	0.62	0
55	SLD 1	16	207	2246	-9.7	17.35	0.01
55	SLD 2	16	207	2246	-9.7	17.35	0.01
55	SLD 3	9	91	2225	-4.09	11.12	0.01
55	SLD 4	9	91	2225	-4.09	11.12	0.01
55	SLD 5	15	327	2135	-15.54	15.08	0
55	SLD 6	15	327	2135	-15.54	15.08	0
55	SLD 7	-6	-60	2067	3.16	-5.67	0.01
55	SLD 8	-6	-60	2067	3.16	-5.67	0.01
55	SLD 9	7	314	2020	-14.94	6.9	-0.01
55	SLD 10	7	314	2020	-14.94	6.9	-0.01
55	SLD 11	-14	-73	1952	3.76	-13.85	0
55	SLD 12	-14	-73	1952	3.76	-13.85	0
55	SLD 13	-9	163	1862	-7.69	-9.89	-0.01
55	SLD 14	-9	163	1862	-7.69	-9.89	-0.01
55	SLD 15	-15	47	1842	-2.08	-16.12	-0.01
55	SLD 16	-15	47	1842	-2.08	-16.12	-0.01
55	SLV 1	37	316	2516	-14.89	41.25	0.02
55	SLV 2	37	316	2516	-14.89	41.25	0.02
55	SLV 3	21	41	2467	-1.59	25.21	0.02
55	SLV 4	21	41	2467	-1.59	25.21	0.02
55	SLV 5	36	601	2260	-28.76	37.12	-0.01
55	SLV 6	36	601	2260	-28.76	37.12	-0.01
55	SLV 7	-18	-317	2096	15.57	-16.32	0.02
55	SLV 8	-18	-317	2096	15.57	-16.32	0.02
55	SLV 9	19	570	1992	-27.35	17.55	-0.02
55	SLV 10	19	570	1992	-27.35	17.55	-0.02
55	SLV 11	-36	-348	1827	16.98	-35.89	0.01
55	SLV 12	-36	-348	1827	16.98	-35.89	0.01
55	SLV 13	-20	213	1620	-10.19	-23.98	-0.02
55	SLV 14	-20	213	1620	-10.19	-23.98	-0.02
55	SLV 15	-37	-62	1571	3.11	-40.02	-0.02
55	SLV 16	-37	-62	1571	3.11	-40.02	-0.02
56	SLU 1	0	73	2281	-2.91	-0.55	0
56	SLU 2	0	73	2281	-2.91	-0.55	0
56	SLU 3	0	73	2281	-2.91	-0.55	0
56	SLU 4	0	73	2281	-2.91	-0.55	0
56	SLU 5	0	73	2281	-2.91	-0.55	0
56	SLU 6	0	73	2281	-2.91	-0.55	0
56	SLU 7	0	73	2281	-2.91	-0.55	0
56	SLU 8	0	73	2281	-2.91	-0.55	0
56	SLU 9	0	73	2281	-2.91	-0.55	0
56	SLU 10	-1	105	2647	-4.15	-0.84	0
56	SLU 11	-1	105	2647	-4.15	-0.84	0
56	SLU 12	-1	105	2647	-4.15	-0.84	0
56	SLU 13	-1	105	2647	-4.15	-0.84	0
56	SLU 14	-1	105	2647	-4.15	-0.84	0
56	SLU 15	-1	105	2647	-4.15	-0.84	0
56	SLU 16	-1	105	2647	-4.15	-0.84	0
56	SLU 17	-1	105	2647	-4.15	-0.84	0
56	SLU 18	-1	118	2804	-4.68	-0.97	0
56	SLU 19	-1	118	2804	-4.68	-0.97	0
56	SLU 20	-1	118	2804	-4.68	-0.97	0
56	SLU 21	-1	118	2804	-4.68	-0.97	0
56	SLU 22	0	92	2506	-3.65	-0.71	0
56	SLU 23	0	92	2506	-3.65	-0.71	0
56	SLU 24	0	92	2506	-3.65	-0.71	0
56	SLU 25	0	92	2506	-3.65	-0.71	0
56	SLU 26	0	92	2506	-3.65	-0.71	0
56	SLU 27	0	92	2506	-3.65	-0.71	0
56	SLU 28	0	92	2506	-3.65	-0.71	0
56	SLU 29	0	92	2506	-3.65	-0.71	0
56	SLU 30	0	92	2506	-3.65	-0.71	0
56	SLU 31	-1	124	2872	-4.89	-1	0
56	SLU 32	-1	124	2872	-4.89	-1	0
56	SLU 33	-1	124	2872	-4.89	-1	0
56	SLU 34	-1	124	2872	-4.89	-1	0
56	SLU 35	-1	124	2872	-4.89	-1	0
56	SLU 36	-1	124	2872	-4.89	-1	0
56	SLU 37	-1	124	2872	-4.89	-1	0
56	SLU 38	-1	124	2872	-4.89	-1	0
56	SLU 39	-1	137	3029	-5.43	-1.12	0
56	SLU 40	-1	137	3029	-5.43	-1.12	0
56	SLU 41	-1	137	3029	-5.43	-1.12	0
56	SLU 42	-1	137	3029	-5.43	-1.12	0
56	SLU 43	0	88	2889	-3.53	-0.66	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
56	SLU 44	0	88	2889	-3.53	-0.66	0
56	SLU 45	0	88	2889	-3.53	-0.66	0
56	SLU 46	0	88	2889	-3.53	-0.66	0
56	SLU 47	0	88	2889	-3.53	-0.66	0
56	SLU 48	0	88	2889	-3.53	-0.66	0
56	SLU 49	0	88	2889	-3.53	-0.66	0
56	SLU 50	0	88	2889	-3.53	-0.66	0
56	SLU 51	0	88	2889	-3.53	-0.66	0
56	SLU 52	-1	120	3255	-4.77	-0.96	0
56	SLU 53	-1	120	3255	-4.77	-0.96	0
56	SLU 54	-1	120	3255	-4.77	-0.96	0
56	SLU 55	-1	120	3255	-4.77	-0.96	0
56	SLU 56	-1	120	3255	-4.77	-0.96	0
56	SLU 57	-1	120	3255	-4.77	-0.96	0
56	SLU 58	-1	120	3255	-4.77	-0.96	0
56	SLU 59	-1	120	3255	-4.77	-0.96	0
56	SLU 60	-1	134	3412	-5.3	-1.08	0
56	SLU 61	-1	134	3412	-5.3	-1.08	0
56	SLU 62	-1	134	3412	-5.3	-1.08	0
56	SLU 63	-1	134	3412	-5.3	-1.08	0
56	SLU 64	-1	107	3113	-4.27	-0.82	0
56	SLU 65	-1	107	3113	-4.27	-0.82	0
56	SLU 66	-1	107	3113	-4.27	-0.82	0
56	SLU 67	-1	107	3113	-4.27	-0.82	0
56	SLU 68	-1	107	3113	-4.27	-0.82	0
56	SLU 69	-1	107	3113	-4.27	-0.82	0
56	SLU 70	-1	107	3113	-4.27	-0.82	0
56	SLU 71	-1	107	3113	-4.27	-0.82	0
56	SLU 72	-1	107	3113	-4.27	-0.82	0
56	SLU 73	-1	139	3479	-5.51	-1.11	0
56	SLU 74	-1	139	3479	-5.51	-1.11	0
56	SLU 75	-1	139	3479	-5.51	-1.11	0
56	SLU 76	-1	139	3479	-5.51	-1.11	0
56	SLU 77	-1	139	3479	-5.51	-1.11	0
56	SLU 78	-1	139	3479	-5.51	-1.11	0
56	SLU 79	-1	139	3479	-5.51	-1.11	0
56	SLU 80	-1	139	3479	-5.51	-1.11	0
56	SLU 81	-1	153	3636	-6.04	-1.23	0
56	SLU 82	-1	153	3636	-6.04	-1.23	0
56	SLU 83	-1	153	3636	-6.04	-1.23	0
56	SLU 84	-1	153	3636	-6.04	-1.23	0
56	SLE RA 1	0	78	2346	-3.12	-0.6	0
56	SLE RA 2	0	78	2346	-3.12	-0.6	0
56	SLE RA 3	0	78	2346	-3.12	-0.6	0
56	SLE RA 4	0	78	2346	-3.12	-0.6	0
56	SLE RA 5	0	78	2346	-3.12	-0.6	0
56	SLE RA 6	0	78	2346	-3.12	-0.6	0
56	SLE RA 7	0	78	2346	-3.12	-0.6	0
56	SLE RA 8	0	78	2346	-3.12	-0.6	0
56	SLE RA 9	0	78	2346	-3.12	-0.6	0
56	SLE RA 10	-1	100	2590	-3.95	-0.79	0
56	SLE RA 11	-1	100	2590	-3.95	-0.79	0
56	SLE RA 12	-1	100	2590	-3.95	-0.79	0
56	SLE RA 13	-1	100	2590	-3.95	-0.79	0
56	SLE RA 14	-1	100	2590	-3.95	-0.79	0
56	SLE RA 15	-1	100	2590	-3.95	-0.79	0
56	SLE RA 16	-1	100	2590	-3.95	-0.79	0
56	SLE RA 17	-1	100	2590	-3.95	-0.79	0
56	SLE RA 18	-1	109	2694	-4.3	-0.87	0
56	SLE RA 19	-1	109	2694	-4.3	-0.87	0
56	SLE RA 20	-1	109	2694	-4.3	-0.87	0
56	SLE RA 21	-1	109	2694	-4.3	-0.87	0
56	SLE FR 1	0	78	2346	-3.12	-0.6	0
56	SLE FR 2	0	78	2346	-3.12	-0.6	0
56	SLE FR 3	0	78	2346	-3.12	-0.6	0
56	SLE FR 4	0	88	2450	-3.48	-0.68	0
56	SLE FR 5	0	88	2450	-3.48	-0.68	0
56	SLE FR 6	0	94	2520	-3.71	-0.73	0
56	SLE QP 1	0	78	2346	-3.12	-0.6	0
56	SLE QP 2	0	88	2450	-3.48	-0.68	0
56	SLD 1	7	134	2197	-5.81	10.21	0.01
56	SLD 2	7	134	2197	-5.81	10.21	0.01
56	SLD 3	15	2	2190	0.52	16.19	0.01
56	SLD 4	15	2	2190	0.52	16.19	0.01
56	SLD 5	-10	301	2385	-13.77	-6.48	0.01
56	SLD 6	-10	301	2385	-13.77	-6.48	0.01
56	SLD 7	16	-137	2361	7.32	13.46	0
56	SLD 8	16	-137	2361	7.32	13.46	0
56	SLD 9	-17	312	2539	-14.27	-14.81	0
56	SLD 10	-17	312	2539	-14.27	-14.81	0
56	SLD 11	9	-126	2515	6.82	5.13	-0.01
56	SLD 12	9	-126	2515	6.82	5.13	-0.01
56	SLD 13	-16	173	2710	-7.47	-17.55	-0.01
56	SLD 14	-16	173	2710	-7.47	-17.55	-0.01
56	SLD 15	-8	41	2703	-1.14	-11.57	-0.01
56	SLD 16	-8	41	2703	-1.14	-11.57	-0.01
56	SLV 1	16	198	1859	-9.07	24.78	0.03
56	SLV 2	16	198	1859	-9.07	24.78	0.03



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
56	SLV 3	37	-115	1842	6.02	40.3	0.02
56	SLV 4	37	-115	1842	6.02	40.3	0.02
56	SLV 5	-26	596	2299	-28.04	-16.58	0.03
56	SLV 6	-26	596	2299	-28.04	-16.58	0.03
56	SLV 7	41	-448	2242	22.26	35.15	-0.01
56	SLV 8	41	-448	2242	22.26	35.15	-0.01
56	SLV 9	-42	623	2659	-29.21	-36.51	0.01
56	SLV 10	-42	623	2659	-29.21	-36.51	0.01
56	SLV 11	25	-421	2601	21.09	15.22	-0.03
56	SLV 12	25	-421	2601	21.09	15.22	-0.03
56	SLV 13	-37	290	3058	-12.97	-41.66	-0.02
56	SLV 14	-37	290	3058	-12.97	-41.66	-0.02
56	SLV 15	-17	-23	3041	2.12	-26.14	-0.03
56	SLV 16	-17	-23	3041	2.12	-26.14	-0.03
57	SLU 1	0	0	1144	0	0	0
57	SLU 2	0	0	1144	0	0	0
57	SLU 3	0	0	1144	0	0	0
57	SLU 4	0	0	1144	0	0	0
57	SLU 5	0	0	1144	0	0	0
57	SLU 6	0	0	1144	0	0	0
57	SLU 7	0	0	1144	0	0	0
57	SLU 8	0	0	1144	0	0	0
57	SLU 9	0	0	1144	0	0	0
57	SLU 10	0	0	1405	0	0	0
57	SLU 11	0	0	1405	0	0	0
57	SLU 12	0	0	1405	0	0	0
57	SLU 13	0	0	1405	0	0	0
57	SLU 14	0	0	1405	0	0	0
57	SLU 15	0	0	1405	0	0	0
57	SLU 16	0	0	1405	0	0	0
57	SLU 17	0	0	1405	0	0	0
57	SLU 18	0	0	1518	0	0	0
57	SLU 19	0	0	1518	0	0	0
57	SLU 20	0	0	1518	0	0	0
57	SLU 21	0	0	1518	0	0	0
57	SLU 22	0	0	1298	0	0	0
57	SLU 23	0	0	1298	0	0	0
57	SLU 24	0	0	1298	0	0	0
57	SLU 25	0	0	1298	0	0	0
57	SLU 26	0	0	1298	0	0	0
57	SLU 27	0	0	1298	0	0	0
57	SLU 28	0	0	1298	0	0	0
57	SLU 29	0	0	1298	0	0	0
57	SLU 30	0	0	1298	0	0	0
57	SLU 31	0	0	1560	0	0	0
57	SLU 32	0	0	1560	0	0	0
57	SLU 33	0	0	1560	0	0	0
57	SLU 34	0	0	1560	0	0	0
57	SLU 35	0	0	1560	0	0	0
57	SLU 36	0	0	1560	0	0	0
57	SLU 37	0	0	1560	0	0	0
57	SLU 38	0	0	1560	0	0	0
57	SLU 39	0	0	1672	0	0	0
57	SLU 40	0	0	1672	0	0	0
57	SLU 41	0	0	1672	0	0	0
57	SLU 42	0	0	1672	0	0	0
57	SLU 43	0	0	1434	0	0	0
57	SLU 44	0	0	1434	0	0	0
57	SLU 45	0	0	1434	0	0	0
57	SLU 46	0	0	1434	0	0	0
57	SLU 47	0	0	1434	0	0	0
57	SLU 48	0	0	1434	0	0	0
57	SLU 49	0	0	1434	0	0	0
57	SLU 50	0	0	1434	0	0	0
57	SLU 51	0	0	1434	0	0	0
57	SLU 52	0	0	1696	0	0	0
57	SLU 53	0	0	1696	0	0	0
57	SLU 54	0	0	1696	0	0	0
57	SLU 55	0	0	1696	0	0	0
57	SLU 56	0	0	1696	0	0	0
57	SLU 57	0	0	1696	0	0	0
57	SLU 58	0	0	1696	0	0	0
57	SLU 59	0	0	1696	0	0	0
57	SLU 60	0	0	1808	0	0	0
57	SLU 61	0	0	1808	0	0	0
57	SLU 62	0	0	1808	0	0	0
57	SLU 63	0	0	1808	0	0	0
57	SLU 64	0	0	1588	0	0	0
57	SLU 65	0	0	1588	0	0	0
57	SLU 66	0	0	1588	0	0	0
57	SLU 67	0	0	1588	0	0	0
57	SLU 68	0	0	1588	0	0	0
57	SLU 69	0	0	1588	0	0	0
57	SLU 70	0	0	1588	0	0	0
57	SLU 71	0	0	1588	0	0	0
57	SLU 72	0	0	1588	0	0	0
57	SLU 73	0	0	1850	0	0	0
57	SLU 74	0	0	1850	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
57	SLU 75	0	0	1850	0	0	0
57	SLU 76	0	0	1850	0	0	0
57	SLU 77	0	0	1850	0	0	0
57	SLU 78	0	0	1850	0	0	0
57	SLU 79	0	0	1850	0	0	0
57	SLU 80	0	0	1850	0	0	0
57	SLU 81	0	0	1962	0	0	0
57	SLU 82	0	0	1962	0	0	0
57	SLU 83	0	0	1962	0	0	0
57	SLU 84	0	0	1962	0	0	0
57	SLE RA 1	0	0	1188	0	0	0
57	SLE RA 2	0	0	1188	0	0	0
57	SLE RA 3	0	0	1188	0	0	0
57	SLE RA 4	0	0	1188	0	0	0
57	SLE RA 5	0	0	1188	0	0	0
57	SLE RA 6	0	0	1188	0	0	0
57	SLE RA 7	0	0	1188	0	0	0
57	SLE RA 8	0	0	1188	0	0	0
57	SLE RA 9	0	0	1188	0	0	0
57	SLE RA 10	0	0	1362	0	0	0
57	SLE RA 11	0	0	1362	0	0	0
57	SLE RA 12	0	0	1362	0	0	0
57	SLE RA 13	0	0	1362	0	0	0
57	SLE RA 14	0	0	1362	0	0	0
57	SLE RA 15	0	0	1362	0	0	0
57	SLE RA 16	0	0	1362	0	0	0
57	SLE RA 17	0	0	1362	0	0	0
57	SLE RA 18	0	0	1437	0	0	0
57	SLE RA 19	0	0	1437	0	0	0
57	SLE RA 20	0	0	1437	0	0	0
57	SLE RA 21	0	0	1437	0	0	0
57	SLE FR 1	0	0	1188	0	0	0
57	SLE FR 2	0	0	1188	0	0	0
57	SLE FR 3	0	0	1188	0	0	0
57	SLE FR 4	0	0	1263	0	0	0
57	SLE FR 5	0	0	1263	0	0	0
57	SLE FR 6	0	0	1313	0	0	0
57	SLE QP 1	0	0	1188	0	0	0
57	SLE QP 2	0	0	1263	0	0	0
57	SLD 1	5	0	1268	-0.02	5.87	0
57	SLD 2	5	0	1268	-0.02	5.87	0
57	SLD 3	5	-1	1254	0.02	5.59	0
57	SLD 4	5	-1	1254	0.02	5.59	0
57	SLD 5	1	2	1284	-0.06	2.19	0
57	SLD 6	1	2	1284	-0.06	2.19	0
57	SLD 7	2	-2	1240	0.06	1.25	0
57	SLD 8	2	-2	1240	0.06	1.25	0
57	SLD 9	-2	2	1285	-0.06	-1.25	0
57	SLD 10	-2	2	1285	-0.06	-1.25	0
57	SLD 11	-1	-2	1241	0.06	-2.19	0
57	SLD 12	-1	-2	1241	0.06	-2.19	0
57	SLD 13	-5	1	1271	-0.02	-5.59	0
57	SLD 14	-5	1	1271	-0.02	-5.59	0
57	SLD 15	-5	0	1258	0.02	-5.87	0
57	SLD 16	-5	0	1258	0.02	-5.87	0
57	SLV 1	13	1	1277	-0.05	14.83	0
57	SLV 2	13	1	1277	-0.05	14.83	0
57	SLV 3	13	-2	1240	0.06	14.14	0
57	SLV 4	13	-2	1240	0.06	14.14	0
57	SLV 5	3	5	1323	-0.18	5.5	0
57	SLV 6	3	5	1323	-0.18	5.5	0
57	SLV 7	5	-5	1200	0.18	3.19	0
57	SLV 8	5	-5	1200	0.18	3.19	0
57	SLV 9	-5	5	1325	-0.18	-3.19	0
57	SLV 10	-5	5	1325	-0.18	-3.19	0
57	SLV 11	-3	-5	1203	0.18	-5.5	0
57	SLV 12	-3	-5	1203	0.18	-5.5	0
57	SLV 13	-13	2	1285	-0.06	-14.14	0
57	SLV 14	-13	2	1285	-0.06	-14.14	0
57	SLV 15	-13	-1	1248	0.05	-14.83	0
57	SLV 16	-13	-1	1248	0.05	-14.83	0
58	SLU 1	1	107	1959	-4.79	0.71	0
58	SLU 2	1	107	1959	-4.79	0.71	0
58	SLU 3	1	107	1959	-4.79	0.71	0
58	SLU 4	1	107	1959	-4.79	0.71	0
58	SLU 5	1	107	1959	-4.79	0.71	0
58	SLU 6	1	107	1959	-4.79	0.71	0
58	SLU 7	1	107	1959	-4.79	0.71	0
58	SLU 8	1	107	1959	-4.79	0.71	0
58	SLU 9	1	107	1959	-4.79	0.71	0
58	SLU 10	1	141	2261	-6.31	1.08	0
58	SLU 11	1	141	2261	-6.31	1.08	0
58	SLU 12	1	141	2261	-6.31	1.08	0
58	SLU 13	1	141	2261	-6.31	1.08	0
58	SLU 14	1	141	2261	-6.31	1.08	0
58	SLU 15	1	141	2261	-6.31	1.08	0
58	SLU 16	1	141	2261	-6.31	1.08	0
58	SLU 17	1	141	2261	-6.31	1.08	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
58	SLU 18	1	156	2390	-6.95	1.23	0
58	SLU 19	1	156	2390	-6.95	1.23	0
58	SLU 20	1	156	2390	-6.95	1.23	0
58	SLU 21	1	156	2390	-6.95	1.23	0
58	SLU 22	1	127	2145	-5.7	0.91	0
58	SLU 23	1	127	2145	-5.7	0.91	0
58	SLU 24	1	127	2145	-5.7	0.91	0
58	SLU 25	1	127	2145	-5.7	0.91	0
58	SLU 26	1	127	2145	-5.7	0.91	0
58	SLU 27	1	127	2145	-5.7	0.91	0
58	SLU 28	1	127	2145	-5.7	0.91	0
58	SLU 29	1	127	2145	-5.7	0.91	0
58	SLU 30	1	127	2145	-5.7	0.91	0
58	SLU 31	1	162	2447	-7.21	1.27	0
58	SLU 32	1	162	2447	-7.21	1.27	0
58	SLU 33	1	162	2447	-7.21	1.27	0
58	SLU 34	1	162	2447	-7.21	1.27	0
58	SLU 35	1	162	2447	-7.21	1.27	0
58	SLU 36	1	162	2447	-7.21	1.27	0
58	SLU 37	1	162	2447	-7.21	1.27	0
58	SLU 38	1	162	2447	-7.21	1.27	0
58	SLU 39	1	177	2576	-7.85	1.43	0
58	SLU 40	1	177	2576	-7.85	1.43	0
58	SLU 41	1	177	2576	-7.85	1.43	0
58	SLU 42	1	177	2576	-7.85	1.43	0
58	SLU 43	1	131	2483	-5.92	0.86	0
58	SLU 44	1	131	2483	-5.92	0.86	0
58	SLU 45	1	131	2483	-5.92	0.86	0
58	SLU 46	1	131	2483	-5.92	0.86	0
58	SLU 47	1	131	2483	-5.92	0.86	0
58	SLU 48	1	131	2483	-5.92	0.86	0
58	SLU 49	1	131	2483	-5.92	0.86	0
58	SLU 50	1	131	2483	-5.92	0.86	0
58	SLU 51	1	131	2483	-5.92	0.86	0
58	SLU 52	1	166	2784	-7.43	1.22	0
58	SLU 53	1	166	2784	-7.43	1.22	0
58	SLU 54	1	166	2784	-7.43	1.22	0
58	SLU 55	1	166	2784	-7.43	1.22	0
58	SLU 56	1	166	2784	-7.43	1.22	0
58	SLU 57	1	166	2784	-7.43	1.22	0
58	SLU 58	1	166	2784	-7.43	1.22	0
58	SLU 59	1	166	2784	-7.43	1.22	0
58	SLU 60	1	181	2914	-8.08	1.38	0
58	SLU 61	1	181	2914	-8.08	1.38	0
58	SLU 62	1	181	2914	-8.08	1.38	0
58	SLU 63	1	181	2914	-8.08	1.38	0
58	SLU 64	1	152	2669	-6.83	1.05	0
58	SLU 65	1	152	2669	-6.83	1.05	0
58	SLU 66	1	152	2669	-6.83	1.05	0
58	SLU 67	1	152	2669	-6.83	1.05	0
58	SLU 68	1	152	2669	-6.83	1.05	0
58	SLU 69	1	152	2669	-6.83	1.05	0
58	SLU 70	1	152	2669	-6.83	1.05	0
58	SLU 71	1	152	2669	-6.83	1.05	0
58	SLU 72	1	152	2669	-6.83	1.05	0
58	SLU 73	1	187	2971	-8.34	1.42	0
58	SLU 74	1	187	2971	-8.34	1.42	0
58	SLU 75	1	187	2971	-8.34	1.42	0
58	SLU 76	1	187	2971	-8.34	1.42	0
58	SLU 77	1	187	2971	-8.34	1.42	0
58	SLU 78	1	187	2971	-8.34	1.42	0
58	SLU 79	1	187	2971	-8.34	1.42	0
58	SLU 80	1	187	2971	-8.34	1.42	0
58	SLU 81	2	202	3100	-8.98	1.57	0
58	SLU 82	2	202	3100	-8.98	1.57	0
58	SLU 83	2	202	3100	-8.98	1.57	0
58	SLU 84	2	202	3100	-8.98	1.57	0
58	SLE RA 1	1	112	2012	-5.05	0.77	0
58	SLE RA 2	1	112	2012	-5.05	0.77	0
58	SLE RA 3	1	112	2012	-5.05	0.77	0
58	SLE RA 4	1	112	2012	-5.05	0.77	0
58	SLE RA 5	1	112	2012	-5.05	0.77	0
58	SLE RA 6	1	112	2012	-5.05	0.77	0
58	SLE RA 7	1	112	2012	-5.05	0.77	0
58	SLE RA 8	1	112	2012	-5.05	0.77	0
58	SLE RA 9	1	112	2012	-5.05	0.77	0
58	SLE RA 10	1	136	2213	-6.06	1.01	0
58	SLE RA 11	1	136	2213	-6.06	1.01	0
58	SLE RA 12	1	136	2213	-6.06	1.01	0
58	SLE RA 13	1	136	2213	-6.06	1.01	0
58	SLE RA 14	1	136	2213	-6.06	1.01	0
58	SLE RA 15	1	136	2213	-6.06	1.01	0
58	SLE RA 16	1	136	2213	-6.06	1.01	0
58	SLE RA 17	1	136	2213	-6.06	1.01	0
58	SLE RA 18	1	145	2299	-6.49	1.11	0
58	SLE RA 19	1	145	2299	-6.49	1.11	0
58	SLE RA 20	1	145	2299	-6.49	1.11	0
58	SLE RA 21	1	145	2299	-6.49	1.11	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
58	SLE FR 1	1	112	2012	-5.05	0.77	0
58	SLE FR 2	1	112	2012	-5.05	0.77	0
58	SLE FR 3	1	112	2012	-5.05	0.77	0
58	SLE FR 4	1	122	2098	-5.48	0.87	0
58	SLE FR 5	1	122	2098	-5.48	0.87	0
58	SLE FR 6	1	129	2156	-5.77	0.94	0
58	SLE QP 1	1	112	2012	-5.05	0.77	0
58	SLE QP 2	1	122	2098	-5.48	0.87	0
58	SLD 1	-1	207	2314	-9.51	12.17	0.01
58	SLD 2	-1	207	2314	-9.51	12.17	0.01
58	SLD 3	-7	90	2299	-3.81	6.82	0.01
58	SLD 4	-7	90	2299	-3.81	6.82	0.01
58	SLD 5	10	326	2186	-15.34	12.39	0
58	SLD 6	10	326	2186	-15.34	12.39	0
58	SLD 7	-11	-65	2136	3.67	-5.47	0.01
58	SLD 8	-11	-65	2136	3.67	-5.47	0.01
58	SLD 9	13	310	2061	-14.64	7.21	-0.01
58	SLD 10	13	310	2061	-14.64	7.21	-0.01
58	SLD 11	-8	-81	2011	4.38	-10.64	0
58	SLD 12	-8	-81	2011	4.38	-10.64	0
58	SLD 13	9	155	1898	-7.16	-5.07	-0.01
58	SLD 14	9	155	1898	-7.16	-5.07	-0.01
58	SLD 15	2	37	1883	-1.45	-10.43	-0.01
58	SLD 16	2	37	1883	-1.45	-10.43	-0.01
58	SLV 1	-2	323	2603	-15.03	28.41	0.03
58	SLV 2	-2	323	2603	-15.03	28.41	0.03
58	SLV 3	-19	45	2566	-1.45	14.49	0.03
58	SLV 4	-19	45	2566	-1.45	14.49	0.03
58	SLV 5	26	605	2306	-28.94	30.24	0
58	SLV 6	26	605	2306	-28.94	30.24	0
58	SLV 7	-31	-324	2183	16.32	-16.15	0.02
58	SLV 8	-31	-324	2183	16.32	-16.15	0.02
58	SLV 9	32	568	2014	-27.28	17.89	-0.02
58	SLV 10	32	568	2014	-27.28	17.89	-0.02
58	SLV 11	-24	-361	1891	17.97	-28.5	0
58	SLV 12	-24	-361	1891	17.97	-28.5	0
58	SLV 13	21	200	1631	-9.51	-12.75	-0.03
58	SLV 14	21	200	1631	-9.51	-12.75	-0.03
58	SLV 15	4	-79	1594	4.06	-26.66	-0.03
58	SLV 16	4	-79	1594	4.06	-26.66	-0.03
59	SLU 1	-1	33	2405	-0.55	-0.83	0
59	SLU 2	-1	33	2405	-0.55	-0.83	0
59	SLU 3	-1	33	2405	-0.55	-0.83	0
59	SLU 4	-1	33	2405	-0.55	-0.83	0
59	SLU 5	-1	33	2405	-0.55	-0.83	0
59	SLU 6	-1	33	2405	-0.55	-0.83	0
59	SLU 7	-1	33	2405	-0.55	-0.83	0
59	SLU 8	-1	33	2405	-0.55	-0.83	0
59	SLU 9	-1	33	2405	-0.55	-0.83	0
59	SLU 10	-1	69	2828	-1.8	-1.26	0
59	SLU 11	-1	69	2828	-1.8	-1.26	0
59	SLU 12	-1	69	2828	-1.8	-1.26	0
59	SLU 13	-1	69	2828	-1.8	-1.26	0
59	SLU 14	-1	69	2828	-1.8	-1.26	0
59	SLU 15	-1	69	2828	-1.8	-1.26	0
59	SLU 16	-1	69	2828	-1.8	-1.26	0
59	SLU 17	-1	69	2828	-1.8	-1.26	0
59	SLU 18	-1	85	3009	-2.34	-1.44	0
59	SLU 19	-1	85	3009	-2.34	-1.44	0
59	SLU 20	-1	85	3009	-2.34	-1.44	0
59	SLU 21	-1	85	3009	-2.34	-1.44	0
59	SLU 22	-1	54	2661	-1.27	-1.06	0
59	SLU 23	-1	54	2661	-1.27	-1.06	0
59	SLU 24	-1	54	2661	-1.27	-1.06	0
59	SLU 25	-1	54	2661	-1.27	-1.06	0
59	SLU 26	-1	54	2661	-1.27	-1.06	0
59	SLU 27	-1	54	2661	-1.27	-1.06	0
59	SLU 28	-1	54	2661	-1.27	-1.06	0
59	SLU 29	-1	54	2661	-1.27	-1.06	0
59	SLU 30	-1	54	2661	-1.27	-1.06	0
59	SLU 31	-1	90	3084	-2.52	-1.49	0
59	SLU 32	-1	90	3084	-2.52	-1.49	0
59	SLU 33	-1	90	3084	-2.52	-1.49	0
59	SLU 34	-1	90	3084	-2.52	-1.49	0
59	SLU 35	-1	90	3084	-2.52	-1.49	0
59	SLU 36	-1	90	3084	-2.52	-1.49	0
59	SLU 37	-1	90	3084	-2.52	-1.49	0
59	SLU 38	-1	90	3084	-2.52	-1.49	0
59	SLU 39	-2	105	3266	-3.05	-1.67	0
59	SLU 40	-2	105	3266	-3.05	-1.67	0
59	SLU 41	-2	105	3266	-3.05	-1.67	0
59	SLU 42	-2	105	3266	-3.05	-1.67	0
59	SLU 43	-1	36	3038	-0.47	-1.01	0
59	SLU 44	-1	36	3038	-0.47	-1.01	0
59	SLU 45	-1	36	3038	-0.47	-1.01	0
59	SLU 46	-1	36	3038	-0.47	-1.01	0
59	SLU 47	-1	36	3038	-0.47	-1.01	0
59	SLU 48	-1	36	3038	-0.47	-1.01	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
59	SLU 49	-1	36	3038	-0.47	-1.01	0
59	SLU 50	-1	36	3038	-0.47	-1.01	0
59	SLU 51	-1	36	3038	-0.47	-1.01	0
59	SLU 52	-1	72	3461	-1.72	-1.43	0
59	SLU 53	-1	72	3461	-1.72	-1.43	0
59	SLU 54	-1	72	3461	-1.72	-1.43	0
59	SLU 55	-1	72	3461	-1.72	-1.43	0
59	SLU 56	-1	72	3461	-1.72	-1.43	0
59	SLU 57	-1	72	3461	-1.72	-1.43	0
59	SLU 58	-1	72	3461	-1.72	-1.43	0
59	SLU 59	-1	72	3461	-1.72	-1.43	0
59	SLU 60	-1	88	3642	-2.26	-1.61	0
59	SLU 61	-1	88	3642	-2.26	-1.61	0
59	SLU 62	-1	88	3642	-2.26	-1.61	0
59	SLU 63	-1	88	3642	-2.26	-1.61	0
59	SLU 64	-1	57	3295	-1.19	-1.23	0
59	SLU 65	-1	57	3295	-1.19	-1.23	0
59	SLU 66	-1	57	3295	-1.19	-1.23	0
59	SLU 67	-1	57	3295	-1.19	-1.23	0
59	SLU 68	-1	57	3295	-1.19	-1.23	0
59	SLU 69	-1	57	3295	-1.19	-1.23	0
59	SLU 70	-1	57	3295	-1.19	-1.23	0
59	SLU 71	-1	57	3295	-1.19	-1.23	0
59	SLU 72	-1	57	3295	-1.19	-1.23	0
59	SLU 73	-2	93	3718	-2.44	-1.66	0
59	SLU 74	-2	93	3718	-2.44	-1.66	0
59	SLU 75	-2	93	3718	-2.44	-1.66	0
59	SLU 76	-2	93	3718	-2.44	-1.66	0
59	SLU 77	-2	93	3718	-2.44	-1.66	0
59	SLU 78	-2	93	3718	-2.44	-1.66	0
59	SLU 79	-2	93	3718	-2.44	-1.66	0
59	SLU 80	-2	93	3718	-2.44	-1.66	0
59	SLU 81	-2	108	3899	-2.98	-1.84	0
59	SLU 82	-2	108	3899	-2.98	-1.84	0
59	SLU 83	-2	108	3899	-2.98	-1.84	0
59	SLU 84	-2	108	3899	-2.98	-1.84	0
59	SLE RA 1	-1	39	2478	-0.76	-0.9	0
59	SLE RA 2	-1	39	2478	-0.76	-0.9	0
59	SLE RA 3	-1	39	2478	-0.76	-0.9	0
59	SLE RA 4	-1	39	2478	-0.76	-0.9	0
59	SLE RA 5	-1	39	2478	-0.76	-0.9	0
59	SLE RA 6	-1	39	2478	-0.76	-0.9	0
59	SLE RA 7	-1	39	2478	-0.76	-0.9	0
59	SLE RA 8	-1	39	2478	-0.76	-0.9	0
59	SLE RA 9	-1	39	2478	-0.76	-0.9	0
59	SLE RA 10	-1	63	2760	-1.59	-1.18	0
59	SLE RA 11	-1	63	2760	-1.59	-1.18	0
59	SLE RA 12	-1	63	2760	-1.59	-1.18	0
59	SLE RA 13	-1	63	2760	-1.59	-1.18	0
59	SLE RA 14	-1	63	2760	-1.59	-1.18	0
59	SLE RA 15	-1	63	2760	-1.59	-1.18	0
59	SLE RA 16	-1	63	2760	-1.59	-1.18	0
59	SLE RA 17	-1	63	2760	-1.59	-1.18	0
59	SLE RA 18	-1	74	2881	-1.95	-1.3	0
59	SLE RA 19	-1	74	2881	-1.95	-1.3	0
59	SLE RA 20	-1	74	2881	-1.95	-1.3	0
59	SLE RA 21	-1	74	2881	-1.95	-1.3	0
59	SLE FR 1	-1	39	2478	-0.76	-0.9	0
59	SLE FR 2	-1	39	2478	-0.76	-0.9	0
59	SLE FR 3	-1	39	2478	-0.76	-0.9	0
59	SLE FR 4	-1	49	2599	-1.11	-1.02	0
59	SLE FR 5	-1	49	2599	-1.11	-1.02	0
59	SLE FR 6	-1	56	2679	-1.35	-1.1	0
59	SLE QP 1	-1	39	2478	-0.76	-0.9	0
59	SLE QP 2	-1	49	2599	-1.11	-1.02	0
59	SLD 1	0	86	2283	-3.2	4.93	0.01
59	SLD 2	0	86	2283	-3.2	4.93	0.01
59	SLD 3	9	-37	2311	2.77	10.1	0
59	SLD 4	9	-37	2311	2.77	10.1	0
59	SLD 5	-14	248	2461	-10.8	-7.07	0.01
59	SLD 6	-14	248	2461	-10.8	-7.07	0.01
59	SLD 7	15	-164	2556	9.11	10.15	-0.01
59	SLD 8	15	-164	2556	9.11	10.15	-0.01
59	SLD 9	-17	263	2642	-11.34	-12.2	0
59	SLD 10	-17	263	2642	-11.34	-12.2	0
59	SLD 11	12	-149	2737	8.57	5.03	-0.01
59	SLD 12	12	-149	2737	8.57	5.03	-0.01
59	SLD 13	-10	136	2886	-5	-12.14	-0.01
59	SLD 14	-10	136	2886	-5	-12.14	-0.01
59	SLD 15	-2	12	2915	0.97	-6.98	-0.01
59	SLD 16	-2	12	2915	0.97	-6.98	-0.01
59	SLV 1	0	139	1859	-6.11	12.58	0.02
59	SLV 2	0	139	1859	-6.11	12.58	0.02
59	SLV 3	23	-156	1927	8.11	26.12	0.01
59	SLV 4	23	-156	1927	8.11	26.12	0.01
59	SLV 5	-36	522	2274	-24.19	-17.47	0.03
59	SLV 6	-36	522	2274	-24.19	-17.47	0.03
59	SLV 7	41	-458	2500	23.23	27.65	-0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
59	SLV 8	41	-458	2500	23.23	27.65	-0.02
59	SLV 9	-43	557	2697	-25.45	-29.7	0.01
59	SLV 10	-43	557	2697	-25.45	-29.7	0.01
59	SLV 11	34	-424	2924	21.96	15.43	-0.03
59	SLV 12	34	-424	2924	21.96	15.43	-0.03
59	SLV 13	-25	254	3270	-10.34	-28.16	-0.01
59	SLV 14	-25	254	3270	-10.34	-28.16	-0.01
59	SLV 15	-1	-40	3338	3.89	-14.63	-0.03
59	SLV 16	-1	-40	3338	3.89	-14.63	-0.03
60	SLU 1	0	0	1149	0	0	0
60	SLU 2	0	0	1149	0	0	0
60	SLU 3	0	0	1149	0	0	0
60	SLU 4	0	0	1149	0	0	0
60	SLU 5	0	0	1149	0	0	0
60	SLU 6	0	0	1149	0	0	0
60	SLU 7	0	0	1149	0	0	0
60	SLU 8	0	0	1149	0	0	0
60	SLU 9	0	0	1149	0	0	0
60	SLU 10	0	0	1427	0	0	0
60	SLU 11	0	0	1427	0	0	0
60	SLU 12	0	0	1427	0	0	0
60	SLU 13	0	0	1427	0	0	0
60	SLU 14	0	0	1427	0	0	0
60	SLU 15	0	0	1427	0	0	0
60	SLU 16	0	0	1427	0	0	0
60	SLU 17	0	0	1427	0	0	0
60	SLU 18	0	0	1546	0	0	0
60	SLU 19	0	0	1546	0	0	0
60	SLU 20	0	0	1546	0	0	0
60	SLU 21	0	0	1546	0	0	0
60	SLU 22	0	0	1312	0	0	0
60	SLU 23	0	0	1312	0	0	0
60	SLU 24	0	0	1312	0	0	0
60	SLU 25	0	0	1312	0	0	0
60	SLU 26	0	0	1312	0	0	0
60	SLU 27	0	0	1312	0	0	0
60	SLU 28	0	0	1312	0	0	0
60	SLU 29	0	0	1312	0	0	0
60	SLU 30	0	0	1312	0	0	0
60	SLU 31	0	0	1590	0	0	0
60	SLU 32	0	0	1590	0	0	0
60	SLU 33	0	0	1590	0	0	0
60	SLU 34	0	0	1590	0	0	0
60	SLU 35	0	0	1590	0	0	0
60	SLU 36	0	0	1590	0	0	0
60	SLU 37	0	0	1590	0	0	0
60	SLU 38	0	0	1590	0	0	0
60	SLU 39	0	0	1709	0	0	0
60	SLU 40	0	0	1709	0	0	0
60	SLU 41	0	0	1709	0	0	0
60	SLU 42	0	0	1709	0	0	0
60	SLU 43	0	0	1438	0	0	0
60	SLU 44	0	0	1438	0	0	0
60	SLU 45	0	0	1438	0	0	0
60	SLU 46	0	0	1438	0	0	0
60	SLU 47	0	0	1438	0	0	0
60	SLU 48	0	0	1438	0	0	0
60	SLU 49	0	0	1438	0	0	0
60	SLU 50	0	0	1438	0	0	0
60	SLU 51	0	0	1438	0	0	0
60	SLU 52	0	0	1716	0	0	0
60	SLU 53	0	0	1716	0	0	0
60	SLU 54	0	0	1716	0	0	0
60	SLU 55	0	0	1716	0	0	0
60	SLU 56	0	0	1716	0	0	0
60	SLU 57	0	0	1716	0	0	0
60	SLU 58	0	0	1716	0	0	0
60	SLU 59	0	0	1716	0	0	0
60	SLU 60	0	0	1835	0	0	0
60	SLU 61	0	0	1835	0	0	0
60	SLU 62	0	0	1835	0	0	0
60	SLU 63	0	0	1835	0	0	0
60	SLU 64	0	0	1601	0	0	0
60	SLU 65	0	0	1601	0	0	0
60	SLU 66	0	0	1601	0	0	0
60	SLU 67	0	0	1601	0	0	0
60	SLU 68	0	0	1601	0	0	0
60	SLU 69	0	0	1601	0	0	0
60	SLU 70	0	0	1601	0	0	0
60	SLU 71	0	0	1601	0	0	0
60	SLU 72	0	0	1601	0	0	0
60	SLU 73	0	0	1879	0	0	0
60	SLU 74	0	0	1879	0	0	0
60	SLU 75	0	0	1879	0	0	0
60	SLU 76	0	0	1879	0	0	0
60	SLU 77	0	0	1879	0	0	0
60	SLU 78	0	0	1879	0	0	0
60	SLU 79	0	0	1879	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
60	SLU 80	0	0	1879	0	0	0
60	SLU 81	0	0	1998	0	0	0
60	SLU 82	0	0	1998	0	0	0
60	SLU 83	0	0	1998	0	0	0
60	SLU 84	0	0	1998	0	0	0
60	SLE RA 1	0	0	1196	0	0	0
60	SLE RA 2	0	0	1196	0	0	0
60	SLE RA 3	0	0	1196	0	0	0
60	SLE RA 4	0	0	1196	0	0	0
60	SLE RA 5	0	0	1196	0	0	0
60	SLE RA 6	0	0	1196	0	0	0
60	SLE RA 7	0	0	1196	0	0	0
60	SLE RA 8	0	0	1196	0	0	0
60	SLE RA 9	0	0	1196	0	0	0
60	SLE RA 10	0	0	1381	0	0	0
60	SLE RA 11	0	0	1381	0	0	0
60	SLE RA 12	0	0	1381	0	0	0
60	SLE RA 13	0	0	1381	0	0	0
60	SLE RA 14	0	0	1381	0	0	0
60	SLE RA 15	0	0	1381	0	0	0
60	SLE RA 16	0	0	1381	0	0	0
60	SLE RA 17	0	0	1381	0	0	0
60	SLE RA 18	0	0	1460	0	0	0
60	SLE RA 19	0	0	1460	0	0	0
60	SLE RA 20	0	0	1460	0	0	0
60	SLE RA 21	0	0	1460	0	0	0
60	SLE FR 1	0	0	1196	0	0	0
60	SLE FR 2	0	0	1196	0	0	0
60	SLE FR 3	0	0	1196	0	0	0
60	SLE FR 4	0	0	1275	0	0	0
60	SLE FR 5	0	0	1275	0	0	0
60	SLE FR 6	0	0	1328	0	0	0
60	SLE QP 1	0	0	1196	0	0	0
60	SLE QP 2	0	0	1275	0	0	0
60	SLD 1	6	0	1280	-0.05	5.24	0
60	SLD 2	6	0	1280	-0.05	5.24	0
60	SLD 3	6	-1	1268	0.05	4.96	0
60	SLD 4	6	-1	1268	0.05	4.96	0
60	SLD 5	2	2	1294	-0.18	1.99	0
60	SLD 6	2	2	1294	-0.18	1.99	0
60	SLD 7	1	-2	1255	0.18	1.07	0
60	SLD 8	1	-2	1255	0.18	1.07	0
60	SLD 9	-1	2	1295	-0.18	-1.07	0
60	SLD 10	-1	2	1295	-0.18	-1.07	0
60	SLD 11	-2	-2	1256	0.18	-1.99	0
60	SLD 12	-2	-2	1256	0.18	-1.99	0
60	SLD 13	-6	1	1282	-0.05	-4.96	0
60	SLD 14	-6	1	1282	-0.05	-4.96	0
60	SLD 15	-6	0	1271	0.05	-5.24	0
60	SLD 16	-6	0	1271	0.05	-5.24	0
60	SLV 1	15	1	1288	-0.15	13.16	0
60	SLV 2	15	1	1288	-0.15	13.16	0
60	SLV 3	14	-2	1255	0.15	12.49	0
60	SLV 4	14	-2	1255	0.15	12.49	0
60	SLV 5	5	5	1328	-0.5	4.95	0
60	SLV 6	5	5	1328	-0.5	4.95	0
60	SLV 7	3	-6	1220	0.5	2.75	0
60	SLV 8	3	-6	1220	0.5	2.75	0
60	SLV 9	-3	6	1330	-0.5	-2.74	0
60	SLV 10	-3	6	1330	-0.5	-2.74	0
60	SLV 11	-5	-5	1222	0.5	-4.95	0
60	SLV 12	-5	-5	1222	0.5	-4.95	0
60	SLV 13	-14	2	1295	-0.15	-12.49	0
60	SLV 14	-14	2	1295	-0.15	-12.49	0
60	SLV 15	-15	-1	1262	0.15	-13.16	0
60	SLV 16	-15	-1	1262	0.15	-13.16	0
61	SLU 1	1	103	2029	-4.28	1.01	0
61	SLU 2	1	103	2029	-4.28	1.01	0
61	SLU 3	1	103	2029	-4.28	1.01	0
61	SLU 4	1	103	2029	-4.28	1.01	0
61	SLU 5	1	103	2029	-4.28	1.01	0
61	SLU 6	1	103	2029	-4.28	1.01	0
61	SLU 7	1	103	2029	-4.28	1.01	0
61	SLU 8	1	103	2029	-4.28	1.01	0
61	SLU 9	1	103	2029	-4.28	1.01	0
61	SLU 10	2	142	2365	-5.83	1.51	0
61	SLU 11	2	142	2365	-5.83	1.51	0
61	SLU 12	2	142	2365	-5.83	1.51	0
61	SLU 13	2	142	2365	-5.83	1.51	0
61	SLU 14	2	142	2365	-5.83	1.51	0
61	SLU 15	2	142	2365	-5.83	1.51	0
61	SLU 16	2	142	2365	-5.83	1.51	0
61	SLU 17	2	142	2365	-5.83	1.51	0
61	SLU 18	2	159	2509	-6.5	1.73	0
61	SLU 19	2	159	2509	-6.5	1.73	0
61	SLU 20	2	159	2509	-6.5	1.73	0
61	SLU 21	2	159	2509	-6.5	1.73	0
61	SLU 22	2	126	2235	-5.19	1.28	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
61	SLU 23	2	126	2235	-5.19	1.28	0
61	SLU 24	2	126	2235	-5.19	1.28	0
61	SLU 25	2	126	2235	-5.19	1.28	0
61	SLU 26	2	126	2235	-5.19	1.28	0
61	SLU 27	2	126	2235	-5.19	1.28	0
61	SLU 28	2	126	2235	-5.19	1.28	0
61	SLU 29	2	126	2235	-5.19	1.28	0
61	SLU 30	2	126	2235	-5.19	1.28	0
61	SLU 31	2	165	2571	-6.74	1.78	0
61	SLU 32	2	165	2571	-6.74	1.78	0
61	SLU 33	2	165	2571	-6.74	1.78	0
61	SLU 34	2	165	2571	-6.74	1.78	0
61	SLU 35	2	165	2571	-6.74	1.78	0
61	SLU 36	2	165	2571	-6.74	1.78	0
61	SLU 37	2	165	2571	-6.74	1.78	0
61	SLU 38	2	165	2571	-6.74	1.78	0
61	SLU 39	3	182	2714	-7.41	2	0
61	SLU 40	3	182	2714	-7.41	2	0
61	SLU 41	3	182	2714	-7.41	2	0
61	SLU 42	3	182	2714	-7.41	2	0
61	SLU 43	2	126	2568	-5.25	1.22	0
61	SLU 44	2	126	2568	-5.25	1.22	0
61	SLU 45	2	126	2568	-5.25	1.22	0
61	SLU 46	2	126	2568	-5.25	1.22	0
61	SLU 47	2	126	2568	-5.25	1.22	0
61	SLU 48	2	126	2568	-5.25	1.22	0
61	SLU 49	2	126	2568	-5.25	1.22	0
61	SLU 50	2	126	2568	-5.25	1.22	0
61	SLU 51	2	126	2568	-5.25	1.22	0
61	SLU 52	2	165	2903	-6.8	1.72	0
61	SLU 53	2	165	2903	-6.8	1.72	0
61	SLU 54	2	165	2903	-6.8	1.72	0
61	SLU 55	2	165	2903	-6.8	1.72	0
61	SLU 56	2	165	2903	-6.8	1.72	0
61	SLU 57	2	165	2903	-6.8	1.72	0
61	SLU 58	2	165	2903	-6.8	1.72	0
61	SLU 59	2	165	2903	-6.8	1.72	0
61	SLU 60	2	182	3047	-7.47	1.94	0
61	SLU 61	2	182	3047	-7.47	1.94	0
61	SLU 62	2	182	3047	-7.47	1.94	0
61	SLU 63	2	182	3047	-7.47	1.94	0
61	SLU 64	2	149	2773	-6.16	1.49	0
61	SLU 65	2	149	2773	-6.16	1.49	0
61	SLU 66	2	149	2773	-6.16	1.49	0
61	SLU 67	2	149	2773	-6.16	1.49	0
61	SLU 68	2	149	2773	-6.16	1.49	0
61	SLU 69	2	149	2773	-6.16	1.49	0
61	SLU 70	2	149	2773	-6.16	1.49	0
61	SLU 71	2	149	2773	-6.16	1.49	0
61	SLU 72	2	149	2773	-6.16	1.49	0
61	SLU 73	3	188	3109	-7.71	1.99	0
61	SLU 74	3	188	3109	-7.71	1.99	0
61	SLU 75	3	188	3109	-7.71	1.99	0
61	SLU 76	3	188	3109	-7.71	1.99	0
61	SLU 77	3	188	3109	-7.71	1.99	0
61	SLU 78	3	188	3109	-7.71	1.99	0
61	SLU 79	3	188	3109	-7.71	1.99	0
61	SLU 80	3	188	3109	-7.71	1.99	0
61	SLU 81	3	205	3253	-8.38	2.21	0
61	SLU 82	3	205	3253	-8.38	2.21	0
61	SLU 83	3	205	3253	-8.38	2.21	0
61	SLU 84	3	205	3253	-8.38	2.21	0
61	SLE RA 1	1	110	2088	-4.54	1.09	0
61	SLE RA 2	1	110	2088	-4.54	1.09	0
61	SLE RA 3	1	110	2088	-4.54	1.09	0
61	SLE RA 4	1	110	2088	-4.54	1.09	0
61	SLE RA 5	1	110	2088	-4.54	1.09	0
61	SLE RA 6	1	110	2088	-4.54	1.09	0
61	SLE RA 7	1	110	2088	-4.54	1.09	0
61	SLE RA 8	1	110	2088	-4.54	1.09	0
61	SLE RA 9	1	110	2088	-4.54	1.09	0
61	SLE RA 10	2	136	2312	-5.57	1.42	0
61	SLE RA 11	2	136	2312	-5.57	1.42	0
61	SLE RA 12	2	136	2312	-5.57	1.42	0
61	SLE RA 13	2	136	2312	-5.57	1.42	0
61	SLE RA 14	2	136	2312	-5.57	1.42	0
61	SLE RA 15	2	136	2312	-5.57	1.42	0
61	SLE RA 16	2	136	2312	-5.57	1.42	0
61	SLE RA 17	2	136	2312	-5.57	1.42	0
61	SLE RA 18	2	147	2408	-6.02	1.57	0
61	SLE RA 19	2	147	2408	-6.02	1.57	0
61	SLE RA 20	2	147	2408	-6.02	1.57	0
61	SLE RA 21	2	147	2408	-6.02	1.57	0
61	SLE FR 1	1	110	2088	-4.54	1.09	0
61	SLE FR 2	1	110	2088	-4.54	1.09	0
61	SLE FR 3	1	110	2088	-4.54	1.09	0
61	SLE FR 4	2	121	2184	-4.98	1.23	0
61	SLE FR 5	2	121	2184	-4.98	1.23	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
61	SLE FR 6	2	128	2248	-5.28	1.33	0
61	SLE QP 1	1	110	2088	-4.54	1.09	0
61	SLE QP 2	2	121	2184	-4.98	1.23	0
61	SLD 1	-2	211	2427	-9.04	7.33	0.01
61	SLD 2	-2	211	2427	-9.04	7.33	0.01
61	SLD 3	-8	94	2416	-3.43	3.17	0.02
61	SLD 4	-8	94	2416	-3.43	3.17	0.02
61	SLD 5	10	326	2273	-14.71	9.38	0
61	SLD 6	10	326	2273	-14.71	9.38	0
61	SLD 7	-10	-65	2238	4	-4.5	0.01
61	SLD 8	-10	-65	2238	4	-4.5	0.01
61	SLD 9	14	306	2130	-13.96	6.97	-0.01
61	SLD 10	14	306	2130	-13.96	6.97	-0.01
61	SLD 11	-7	-84	2095	4.75	-6.91	0
61	SLD 12	-7	-84	2095	4.75	-6.91	0
61	SLD 13	11	147	1952	-6.53	-0.71	-0.01
61	SLD 14	11	147	1952	-6.53	-0.71	-0.01
61	SLD 15	5	30	1941	-0.92	-4.87	-0.01
61	SLD 16	5	30	1941	-0.92	-4.87	-0.01
61	SLV 1	-5	335	2751	-14.56	16.21	0.03
61	SLV 2	-5	335	2751	-14.56	16.21	0.03
61	SLV 3	-22	57	2726	-1.26	5.33	0.04
61	SLV 4	-22	57	2726	-1.26	5.33	0.04
61	SLV 5	24	606	2393	-28.04	22.23	0
61	SLV 6	24	606	2393	-28.04	22.23	0
61	SLV 7	-30	-320	2308	16.32	-14.05	0.02
61	SLV 8	-30	-320	2308	16.32	-14.05	0.02
61	SLV 9	33	561	2060	-26.28	16.51	-0.02
61	SLV 10	33	561	2060	-26.28	16.51	-0.02
61	SLV 11	-21	-365	1976	18.07	-19.77	0
61	SLV 12	-21	-365	1976	18.07	-19.77	0
61	SLV 13	25	184	1642	-8.7	-2.86	-0.04
61	SLV 14	25	184	1642	-8.7	-2.86	-0.04
61	SLV 15	9	-93	1617	4.6	-13.75	-0.03
61	SLV 16	9	-93	1617	4.6	-13.75	-0.03
62	SLU 1	-2	-32	2624	3.18	-1.33	0.01
62	SLU 2	-2	-32	2624	3.18	-1.33	0.01
62	SLU 3	-2	-32	2624	3.18	-1.33	0.01
62	SLU 4	-2	-32	2624	3.18	-1.33	0.01
62	SLU 5	-2	-32	2624	3.18	-1.33	0.01
62	SLU 6	-2	-32	2624	3.18	-1.33	0.01
62	SLU 7	-2	-32	2624	3.18	-1.33	0.01
62	SLU 8	-2	-32	2624	3.18	-1.33	0.01
62	SLU 9	-2	-32	2624	3.18	-1.33	0.01
62	SLU 10	-3	6	3156	2.28	-1.95	0.01
62	SLU 11	-3	6	3156	2.28	-1.95	0.01
62	SLU 12	-3	6	3156	2.28	-1.95	0.01
62	SLU 13	-3	6	3156	2.28	-1.95	0.01
62	SLU 14	-3	6	3156	2.28	-1.95	0.01
62	SLU 15	-3	6	3156	2.28	-1.95	0.01
62	SLU 16	-3	6	3156	2.28	-1.95	0.01
62	SLU 17	-3	6	3156	2.28	-1.95	0.01
62	SLU 18	-4	22	3384	1.89	-2.22	0.01
62	SLU 19	-4	22	3384	1.89	-2.22	0.01
62	SLU 20	-4	22	3384	1.89	-2.22	0.01
62	SLU 21	-4	22	3384	1.89	-2.22	0.01
62	SLU 22	-3	-12	2941	2.72	-1.67	0.01
62	SLU 23	-3	-12	2941	2.72	-1.67	0.01
62	SLU 24	-3	-12	2941	2.72	-1.67	0.01
62	SLU 25	-3	-12	2941	2.72	-1.67	0.01
62	SLU 26	-3	-12	2941	2.72	-1.67	0.01
62	SLU 27	-3	-12	2941	2.72	-1.67	0.01
62	SLU 28	-3	-12	2941	2.72	-1.67	0.01
62	SLU 29	-3	-12	2941	2.72	-1.67	0.01
62	SLU 30	-3	-12	2941	2.72	-1.67	0.01
62	SLU 31	-4	26	3473	1.82	-2.29	0.01
62	SLU 32	-4	26	3473	1.82	-2.29	0.01
62	SLU 33	-4	26	3473	1.82	-2.29	0.01
62	SLU 34	-4	26	3473	1.82	-2.29	0.01
62	SLU 35	-4	26	3473	1.82	-2.29	0.01
62	SLU 36	-4	26	3473	1.82	-2.29	0.01
62	SLU 37	-4	26	3473	1.82	-2.29	0.01
62	SLU 38	-4	26	3473	1.82	-2.29	0.01
62	SLU 39	-4	42	3701	1.44	-2.56	0.01
62	SLU 40	-4	42	3701	1.44	-2.56	0.01
62	SLU 41	-4	42	3701	1.44	-2.56	0.01
62	SLU 42	-4	42	3701	1.44	-2.56	0.01
62	SLU 43	-3	-48	3303	4.28	-1.61	0.01
62	SLU 44	-3	-48	3303	4.28	-1.61	0.01
62	SLU 45	-3	-48	3303	4.28	-1.61	0.01
62	SLU 46	-3	-48	3303	4.28	-1.61	0.01
62	SLU 47	-3	-48	3303	4.28	-1.61	0.01
62	SLU 48	-3	-48	3303	4.28	-1.61	0.01
62	SLU 49	-3	-48	3303	4.28	-1.61	0.01
62	SLU 50	-3	-48	3303	4.28	-1.61	0.01
62	SLU 51	-3	-48	3303	4.28	-1.61	0.01
62	SLU 52	-4	-11	3835	3.39	-2.23	0.01
62	SLU 53	-4	-11	3835	3.39	-2.23	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
62	SLU 54	-4	-11	3835	3.39	-2.23	0.01
62	SLU 55	-4	-11	3835	3.39	-2.23	0.01
62	SLU 56	-4	-11	3835	3.39	-2.23	0.01
62	SLU 57	-4	-11	3835	3.39	-2.23	0.01
62	SLU 58	-4	-11	3835	3.39	-2.23	0.01
62	SLU 59	-4	-11	3835	3.39	-2.23	0.01
62	SLU 60	-4	6	4063	3	-2.5	0.01
62	SLU 61	-4	6	4063	3	-2.5	0.01
62	SLU 62	-4	6	4063	3	-2.5	0.01
62	SLU 63	-4	6	4063	3	-2.5	0.01
62	SLU 64	-4	-28	3620	3.83	-1.95	0.01
62	SLU 65	-4	-28	3620	3.83	-1.95	0.01
62	SLU 66	-4	-28	3620	3.83	-1.95	0.01
62	SLU 67	-4	-28	3620	3.83	-1.95	0.01
62	SLU 68	-4	-28	3620	3.83	-1.95	0.01
62	SLU 69	-4	-28	3620	3.83	-1.95	0.01
62	SLU 70	-4	-28	3620	3.83	-1.95	0.01
62	SLU 71	-4	-28	3620	3.83	-1.95	0.01
62	SLU 72	-4	-28	3620	3.83	-1.95	0.01
62	SLU 73	-4	9	4152	2.93	-2.57	0.01
62	SLU 74	-4	9	4152	2.93	-2.57	0.01
62	SLU 75	-4	9	4152	2.93	-2.57	0.01
62	SLU 76	-4	9	4152	2.93	-2.57	0.01
62	SLU 77	-4	9	4152	2.93	-2.57	0.01
62	SLU 78	-4	9	4152	2.93	-2.57	0.01
62	SLU 79	-4	9	4152	2.93	-2.57	0.01
62	SLU 80	-4	9	4152	2.93	-2.57	0.01
62	SLU 81	-5	26	4380	2.55	-2.84	0.01
62	SLU 82	-5	26	4380	2.55	-2.84	0.01
62	SLU 83	-5	26	4380	2.55	-2.84	0.01
62	SLU 84	-5	26	4380	2.55	-2.84	0.01
62	SLE RA 1	-3	-26	2715	3.04	-1.42	0.01
62	SLE RA 2	-3	-26	2715	3.04	-1.42	0.01
62	SLE RA 3	-3	-26	2715	3.04	-1.42	0.01
62	SLE RA 4	-3	-26	2715	3.04	-1.42	0.01
62	SLE RA 5	-3	-26	2715	3.04	-1.42	0.01
62	SLE RA 6	-3	-26	2715	3.04	-1.42	0.01
62	SLE RA 7	-3	-26	2715	3.04	-1.42	0.01
62	SLE RA 8	-3	-26	2715	3.04	-1.42	0.01
62	SLE RA 9	-3	-26	2715	3.04	-1.42	0.01
62	SLE RA 10	-3	-1	3069	2.45	-1.84	0.01
62	SLE RA 11	-3	-1	3069	2.45	-1.84	0.01
62	SLE RA 12	-3	-1	3069	2.45	-1.84	0.01
62	SLE RA 13	-3	-1	3069	2.45	-1.84	0.01
62	SLE RA 14	-3	-1	3069	2.45	-1.84	0.01
62	SLE RA 15	-3	-1	3069	2.45	-1.84	0.01
62	SLE RA 16	-3	-1	3069	2.45	-1.84	0.01
62	SLE RA 17	-3	-1	3069	2.45	-1.84	0.01
62	SLE RA 18	-4	10	3221	2.19	-2.02	0.01
62	SLE RA 19	-4	10	3221	2.19	-2.02	0.01
62	SLE RA 20	-4	10	3221	2.19	-2.02	0.01
62	SLE RA 21	-4	10	3221	2.19	-2.02	0.01
62	SLE FR 1	-3	-26	2715	3.04	-1.42	0.01
62	SLE FR 2	-3	-26	2715	3.04	-1.42	0.01
62	SLE FR 3	-3	-26	2715	3.04	-1.42	0.01
62	SLE FR 4	-3	-15	2867	2.79	-1.6	0.01
62	SLE FR 5	-3	-15	2867	2.79	-1.6	0.01
62	SLE FR 6	-3	-8	2968	2.62	-1.72	0.01
62	SLE QP 1	-3	-26	2715	3.04	-1.42	0.01
62	SLE QP 2	-3	-15	2867	2.79	-1.6	0.01
62	SLD 1	-4	8	2430	0.88	0.83	-0.01
62	SLD 2	-4	8	2430	0.88	0.83	-0.01
62	SLD 3	5	-104	2504	6.52	4.22	-0.03
62	SLD 4	5	-104	2504	6.52	4.22	-0.03
62	SLD 5	-17	160	2623	-6.34	-6.01	0.03
62	SLD 6	-17	160	2623	-6.34	-6.01	0.03
62	SLD 7	13	-211	2871	12.47	5.29	-0.03
62	SLD 8	13	-211	2871	12.47	5.29	-0.03
62	SLD 9	-19	180	2863	-6.89	-8.49	0.05
62	SLD 10	-19	180	2863	-6.89	-8.49	0.05
62	SLD 11	11	-191	3111	11.92	2.81	-0.01
62	SLD 12	11	-191	3111	11.92	2.81	-0.01
62	SLD 13	-11	73	3229	-0.94	-7.43	0.05
62	SLD 14	-11	73	3229	-0.94	-7.43	0.05
62	SLD 15	-2	-38	3304	4.7	-4.03	0.03
62	SLD 16	-2	-38	3304	4.7	-4.03	0.03
62	SLV 1	-7	41	1844	-1.8	3.76	-0.04
62	SLV 2	-7	41	1844	-1.8	3.76	-0.04
62	SLV 3	17	-224	2022	11.65	12.69	-0.09
62	SLV 4	17	-224	2022	11.65	12.69	-0.09
62	SLV 5	-40	403	2290	-18.99	-13.53	0.07
62	SLV 6	-40	403	2290	-18.99	-13.53	0.07
62	SLV 7	39	-480	2884	25.85	16.22	-0.09
62	SLV 8	39	-480	2884	25.85	16.22	-0.09
62	SLV 9	-45	449	2850	-20.27	-19.43	0.11
62	SLV 10	-45	449	2850	-20.27	-19.43	0.11
62	SLV 11	35	-434	3444	24.56	10.33	-0.05
62	SLV 12	35	-434	3444	24.56	10.33	-0.05



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
62	SLV 13	-23	194	3712	-6.07	-15.89	0.1
62	SLV 14	-23	194	3712	-6.07	-15.89	0.1
62	SLV 15	1	-71	3890	7.38	-6.97	0.06
62	SLV 16	1	-71	3890	7.38	-6.97	0.06
63	SLU 1	0	0	1137	0	0	0
63	SLU 2	0	0	1137	0	0	0
63	SLU 3	0	0	1137	0	0	0
63	SLU 4	0	0	1137	0	0	0
63	SLU 5	0	0	1137	0	0	0
63	SLU 6	0	0	1137	0	0	0
63	SLU 7	0	0	1137	0	0	0
63	SLU 8	0	0	1137	0	0	0
63	SLU 9	0	0	1137	0	0	0
63	SLU 10	0	0	1428	0	0	0
63	SLU 11	0	0	1428	0	0	0
63	SLU 12	0	0	1428	0	0	0
63	SLU 13	0	0	1428	0	0	0
63	SLU 14	0	0	1428	0	0	0
63	SLU 15	0	0	1428	0	0	0
63	SLU 16	0	0	1428	0	0	0
63	SLU 17	0	0	1428	0	0	0
63	SLU 18	0	0	1552	0	0	0
63	SLU 19	0	0	1552	0	0	0
63	SLU 20	0	0	1552	0	0	0
63	SLU 21	0	0	1552	0	0	0
63	SLU 22	0	0	1309	0	0	0
63	SLU 23	0	0	1309	0	0	0
63	SLU 24	0	0	1309	0	0	0
63	SLU 25	0	0	1309	0	0	0
63	SLU 26	0	0	1309	0	0	0
63	SLU 27	0	0	1309	0	0	0
63	SLU 28	0	0	1309	0	0	0
63	SLU 29	0	0	1309	0	0	0
63	SLU 30	0	0	1309	0	0	0
63	SLU 31	0	0	1600	0	0	0
63	SLU 32	0	0	1600	0	0	0
63	SLU 33	0	0	1600	0	0	0
63	SLU 34	0	0	1600	0	0	0
63	SLU 35	0	0	1600	0	0	0
63	SLU 36	0	0	1600	0	0	0
63	SLU 37	0	0	1600	0	0	0
63	SLU 38	0	0	1600	0	0	0
63	SLU 39	0	0	1724	0	0	0
63	SLU 40	0	0	1724	0	0	0
63	SLU 41	0	0	1724	0	0	0
63	SLU 42	0	0	1724	0	0	0
63	SLU 43	0	0	1419	0.01	0	0
63	SLU 44	0	0	1419	0.01	0	0
63	SLU 45	0	0	1419	0.01	0	0
63	SLU 46	0	0	1419	0.01	0	0
63	SLU 47	0	0	1419	0.01	0	0
63	SLU 48	0	0	1419	0.01	0	0
63	SLU 49	0	0	1419	0.01	0	0
63	SLU 50	0	0	1419	0.01	0	0
63	SLU 51	0	0	1419	0.01	0	0
63	SLU 52	0	0	1710	0.01	0	0
63	SLU 53	0	0	1710	0.01	0	0
63	SLU 54	0	0	1710	0.01	0	0
63	SLU 55	0	0	1710	0.01	0	0
63	SLU 56	0	0	1710	0.01	0	0
63	SLU 57	0	0	1710	0.01	0	0
63	SLU 58	0	0	1710	0.01	0	0
63	SLU 59	0	0	1710	0.01	0	0
63	SLU 60	0	0	1835	0.01	0	0
63	SLU 61	0	0	1835	0.01	0	0
63	SLU 62	0	0	1835	0.01	0	0
63	SLU 63	0	0	1835	0.01	0	0
63	SLU 64	0	0	1591	0.01	0	0
63	SLU 65	0	0	1591	0.01	0	0
63	SLU 66	0	0	1591	0.01	0	0
63	SLU 67	0	0	1591	0.01	0	0
63	SLU 68	0	0	1591	0.01	0	0
63	SLU 69	0	0	1591	0.01	0	0
63	SLU 70	0	0	1591	0.01	0	0
63	SLU 71	0	0	1591	0.01	0	0
63	SLU 72	0	0	1591	0.01	0	0
63	SLU 73	0	0	1882	0.01	0	0
63	SLU 74	0	0	1882	0.01	0	0
63	SLU 75	0	0	1882	0.01	0	0
63	SLU 76	0	0	1882	0.01	0	0
63	SLU 77	0	0	1882	0.01	0	0
63	SLU 78	0	0	1882	0.01	0	0
63	SLU 79	0	0	1882	0.01	0	0
63	SLU 80	0	0	1882	0.01	0	0
63	SLU 81	0	0	2006	0.01	0	0
63	SLU 82	0	0	2006	0.01	0	0
63	SLU 83	0	0	2006	0.01	0	0
63	SLU 84	0	0	2006	0.01	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
63	SLE RA 1	0	0	1186	0	0	0
63	SLE RA 2	0	0	1186	0	0	0
63	SLE RA 3	0	0	1186	0	0	0
63	SLE RA 4	0	0	1186	0	0	0
63	SLE RA 5	0	0	1186	0	0	0
63	SLE RA 6	0	0	1186	0	0	0
63	SLE RA 7	0	0	1186	0	0	0
63	SLE RA 8	0	0	1186	0	0	0
63	SLE RA 9	0	0	1186	0	0	0
63	SLE RA 10	0	0	1380	0	0	0
63	SLE RA 11	0	0	1380	0	0	0
63	SLE RA 12	0	0	1380	0	0	0
63	SLE RA 13	0	0	1380	0	0	0
63	SLE RA 14	0	0	1380	0	0	0
63	SLE RA 15	0	0	1380	0	0	0
63	SLE RA 16	0	0	1380	0	0	0
63	SLE RA 17	0	0	1380	0	0	0
63	SLE RA 18	0	0	1463	0	0	0
63	SLE RA 19	0	0	1463	0	0	0
63	SLE RA 20	0	0	1463	0	0	0
63	SLE RA 21	0	0	1463	0	0	0
63	SLE FR 1	0	0	1186	0	0	0
63	SLE FR 2	0	0	1186	0	0	0
63	SLE FR 3	0	0	1186	0	0	0
63	SLE FR 4	0	0	1269	0	0	0
63	SLE FR 5	0	0	1269	0	0	0
63	SLE FR 6	0	0	1324	0	0	0
63	SLE QP 1	0	0	1186	0	0	0
63	SLE QP 2	0	0	1269	0	0	0
63	SLD 1	6	0	1291	0	4.86	0
63	SLD 2	6	0	1291	0	4.86	0
63	SLD 3	6	-1	1245	0.01	4.58	0
63	SLD 4	6	-1	1245	0.01	4.58	0
63	SLD 5	2	2	1346	-0.03	1.87	0
63	SLD 6	2	2	1346	-0.03	1.87	0
63	SLD 7	1	-2	1191	0.04	0.96	0
63	SLD 8	1	-2	1191	0.04	0.96	0
63	SLD 9	-1	2	1347	-0.03	-0.96	0
63	SLD 10	-1	2	1347	-0.03	-0.96	0
63	SLD 11	-2	-2	1192	0.04	-1.87	0
63	SLD 12	-2	-2	1192	0.04	-1.87	0
63	SLD 13	-6	1	1294	-0.01	-4.58	0
63	SLD 14	-6	1	1294	-0.01	-4.58	0
63	SLD 15	-6	0	1247	0.01	-4.86	0
63	SLD 16	-6	0	1247	0.01	-4.86	0
63	SLV 1	15	1	1331	-0.02	12.13	0
63	SLV 2	15	1	1331	-0.02	12.13	0
63	SLV 3	15	-3	1200	0.03	11.48	0
63	SLV 4	15	-3	1200	0.03	11.48	0
63	SLV 5	6	5	1486	-0.08	4.62	0
63	SLV 6	6	5	1486	-0.08	4.62	0
63	SLV 7	3	-5	1050	0.09	2.46	0
63	SLV 8	3	-5	1050	0.09	2.46	0
63	SLV 9	-3	5	1488	-0.08	-2.46	0
63	SLV 10	-3	5	1488	-0.08	-2.46	0
63	SLV 11	-6	-5	1052	0.09	-4.62	0
63	SLV 12	-6	-5	1052	0.09	-4.62	0
63	SLV 13	-15	3	1338	-0.02	-11.47	0
63	SLV 14	-15	3	1338	-0.02	-11.47	0
63	SLV 15	-15	-1	1207	0.03	-12.12	0
63	SLV 16	-15	-1	1207	0.03	-12.12	0
64	SLU 1	3	103	2172	-3.88	1.43	-0.01
64	SLU 2	3	103	2172	-3.88	1.43	-0.01
64	SLU 3	3	103	2172	-3.88	1.43	-0.01
64	SLU 4	3	103	2172	-3.88	1.43	-0.01
64	SLU 5	3	103	2172	-3.88	1.43	-0.01
64	SLU 6	3	103	2172	-3.88	1.43	-0.01
64	SLU 7	3	103	2172	-3.88	1.43	-0.01
64	SLU 8	3	103	2172	-3.88	1.43	-0.01
64	SLU 9	3	103	2172	-3.88	1.43	-0.01
64	SLU 10	4	149	2578	-5.53	2.09	-0.01
64	SLU 11	4	149	2578	-5.53	2.09	-0.01
64	SLU 12	4	149	2578	-5.53	2.09	-0.01
64	SLU 13	4	149	2578	-5.53	2.09	-0.01
64	SLU 14	4	149	2578	-5.53	2.09	-0.01
64	SLU 15	4	149	2578	-5.53	2.09	-0.01
64	SLU 16	4	149	2578	-5.53	2.09	-0.01
64	SLU 17	4	149	2578	-5.53	2.09	-0.01
64	SLU 18	5	168	2753	-6.23	2.38	-0.01
64	SLU 19	5	168	2753	-6.23	2.38	-0.01
64	SLU 20	5	168	2753	-6.23	2.38	-0.01
64	SLU 21	5	168	2753	-6.23	2.38	-0.01
64	SLU 22	4	129	2417	-4.81	1.79	-0.01
64	SLU 23	4	129	2417	-4.81	1.79	-0.01
64	SLU 24	4	129	2417	-4.81	1.79	-0.01
64	SLU 25	4	129	2417	-4.81	1.79	-0.01
64	SLU 26	4	129	2417	-4.81	1.79	-0.01
64	SLU 27	4	129	2417	-4.81	1.79	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
64	SLU 28	4	129	2417	-4.81	1.79	-0.01
64	SLU 29	4	129	2417	-4.81	1.79	-0.01
64	SLU 30	4	129	2417	-4.81	1.79	-0.01
64	SLU 31	5	174	2823	-6.46	2.46	-0.01
64	SLU 32	5	174	2823	-6.46	2.46	-0.01
64	SLU 33	5	174	2823	-6.46	2.46	-0.01
64	SLU 34	5	174	2823	-6.46	2.46	-0.01
64	SLU 35	5	174	2823	-6.46	2.46	-0.01
64	SLU 36	5	174	2823	-6.46	2.46	-0.01
64	SLU 37	5	174	2823	-6.46	2.46	-0.01
64	SLU 38	5	174	2823	-6.46	2.46	-0.01
64	SLU 39	5	194	2997	-7.17	2.74	-0.01
64	SLU 40	5	194	2997	-7.17	2.74	-0.01
64	SLU 41	5	194	2997	-7.17	2.74	-0.01
64	SLU 42	5	194	2997	-7.17	2.74	-0.01
64	SLU 43	4	125	2740	-4.72	1.73	-0.01
64	SLU 44	4	125	2740	-4.72	1.73	-0.01
64	SLU 45	4	125	2740	-4.72	1.73	-0.01
64	SLU 46	4	125	2740	-4.72	1.73	-0.01
64	SLU 47	4	125	2740	-4.72	1.73	-0.01
64	SLU 48	4	125	2740	-4.72	1.73	-0.01
64	SLU 49	4	125	2740	-4.72	1.73	-0.01
64	SLU 50	4	125	2740	-4.72	1.73	-0.01
64	SLU 51	4	125	2740	-4.72	1.73	-0.01
64	SLU 52	5	171	3146	-6.37	2.4	-0.01
64	SLU 53	5	171	3146	-6.37	2.4	-0.01
64	SLU 54	5	171	3146	-6.37	2.4	-0.01
64	SLU 55	5	171	3146	-6.37	2.4	-0.01
64	SLU 56	5	171	3146	-6.37	2.4	-0.01
64	SLU 57	5	171	3146	-6.37	2.4	-0.01
64	SLU 58	5	171	3146	-6.37	2.4	-0.01
64	SLU 59	5	171	3146	-6.37	2.4	-0.01
64	SLU 60	5	190	3320	-7.08	2.68	-0.01
64	SLU 61	5	190	3320	-7.08	2.68	-0.01
64	SLU 62	5	190	3320	-7.08	2.68	-0.01
64	SLU 63	5	190	3320	-7.08	2.68	-0.01
64	SLU 64	4	151	2985	-5.66	2.09	-0.01
64	SLU 65	4	151	2985	-5.66	2.09	-0.01
64	SLU 66	4	151	2985	-5.66	2.09	-0.01
64	SLU 67	4	151	2985	-5.66	2.09	-0.01
64	SLU 68	4	151	2985	-5.66	2.09	-0.01
64	SLU 69	4	151	2985	-5.66	2.09	-0.01
64	SLU 70	4	151	2985	-5.66	2.09	-0.01
64	SLU 71	4	151	2985	-5.66	2.09	-0.01
64	SLU 72	4	151	2985	-5.66	2.09	-0.01
64	SLU 73	6	197	3391	-7.31	2.76	-0.01
64	SLU 74	6	197	3391	-7.31	2.76	-0.01
64	SLU 75	6	197	3391	-7.31	2.76	-0.01
64	SLU 76	6	197	3391	-7.31	2.76	-0.01
64	SLU 77	6	197	3391	-7.31	2.76	-0.01
64	SLU 78	6	197	3391	-7.31	2.76	-0.01
64	SLU 79	6	197	3391	-7.31	2.76	-0.01
64	SLU 80	6	197	3391	-7.31	2.76	-0.01
64	SLU 81	6	216	3565	-8.01	3.04	-0.01
64	SLU 82	6	216	3565	-8.01	3.04	-0.01
64	SLU 83	6	216	3565	-8.01	3.04	-0.01
64	SLU 84	6	216	3565	-8.01	3.04	-0.01
64	SLE RA 1	3	111	2242	-4.15	1.53	-0.01
64	SLE RA 2	3	111	2242	-4.15	1.53	-0.01
64	SLE RA 3	3	111	2242	-4.15	1.53	-0.01
64	SLE RA 4	3	111	2242	-4.15	1.53	-0.01
64	SLE RA 5	3	111	2242	-4.15	1.53	-0.01
64	SLE RA 6	3	111	2242	-4.15	1.53	-0.01
64	SLE RA 7	3	111	2242	-4.15	1.53	-0.01
64	SLE RA 8	3	111	2242	-4.15	1.53	-0.01
64	SLE RA 9	3	111	2242	-4.15	1.53	-0.01
64	SLE RA 10	4	141	2513	-5.24	1.97	-0.01
64	SLE RA 11	4	141	2513	-5.24	1.97	-0.01
64	SLE RA 12	4	141	2513	-5.24	1.97	-0.01
64	SLE RA 13	4	141	2513	-5.24	1.97	-0.01
64	SLE RA 14	4	141	2513	-5.24	1.97	-0.01
64	SLE RA 15	4	141	2513	-5.24	1.97	-0.01
64	SLE RA 16	4	141	2513	-5.24	1.97	-0.01
64	SLE RA 17	4	141	2513	-5.24	1.97	-0.01
64	SLE RA 18	4	154	2629	-5.72	2.16	-0.01
64	SLE RA 19	4	154	2629	-5.72	2.16	-0.01
64	SLE RA 20	4	154	2629	-5.72	2.16	-0.01
64	SLE RA 21	4	154	2629	-5.72	2.16	-0.01
64	SLE FR 1	3	111	2242	-4.15	1.53	-0.01
64	SLE FR 2	3	111	2242	-4.15	1.53	-0.01
64	SLE FR 3	3	111	2242	-4.15	1.53	-0.01
64	SLE FR 4	4	124	2358	-4.62	1.72	-0.01
64	SLE FR 5	4	124	2358	-4.62	1.72	-0.01
64	SLE FR 6	4	132	2436	-4.93	1.85	-0.01
64	SLE QP 1	3	111	2242	-4.15	1.53	-0.01
64	SLE QP 2	4	124	2358	-4.62	1.72	-0.01
64	SLD 1	-2	225	2667	-9	4.33	-0.02
64	SLD 2	-2	225	2667	-9	4.33	-0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
64	SLD 3	-7	107	2661	-3.31	1.91	-0.02
64	SLD 4	-7	107	2661	-3.31	1.91	-0.02
64	SLD 5	9	332	2460	-14.57	6.18	-0.02
64	SLD 6	9	332	2460	-14.57	6.18	-0.02
64	SLD 7	-7	-60	2440	4.41	-1.9	0
64	SLD 8	-7	-60	2440	4.41	-1.9	0
64	SLD 9	14	307	2276	-13.65	5.34	-0.01
64	SLD 10	14	307	2276	-13.65	5.34	-0.01
64	SLD 11	-2	-85	2257	5.34	-2.73	0
64	SLD 12	-2	-85	2257	5.34	-2.73	0
64	SLD 13	14	140	2055	-5.93	1.54	0
64	SLD 14	14	140	2055	-5.93	1.54	0
64	SLD 15	9	22	2049	-0.23	-0.89	0.01
64	SLD 16	9	22	2049	-0.23	-0.89	0.01
64	SLV 1	-9	363	3080	-14.99	8.18	-0.04
64	SLV 2	-9	363	3080	-14.99	8.18	-0.04
64	SLV 3	-21	83	3065	-1.44	1.82	-0.03
64	SLV 4	-21	83	3065	-1.44	1.82	-0.03
64	SLV 5	19	619	2596	-28.28	13.29	-0.04
64	SLV 6	19	619	2596	-28.28	13.29	-0.04
64	SLV 7	-23	-313	2549	16.89	-7.89	0.01
64	SLV 8	-23	-313	2549	16.89	-7.89	0.01
64	SLV 9	30	560	2168	-26.13	11.33	-0.02
64	SLV 10	30	560	2168	-26.13	11.33	-0.02
64	SLV 11	-12	-372	2120	19.05	-9.85	0.02
64	SLV 12	-12	-372	2120	19.05	-9.85	0.02
64	SLV 13	28	164	1651	-7.8	1.62	0.01
64	SLV 14	28	164	1651	-7.8	1.62	0.01
64	SLV 15	16	-115	1637	5.76	-4.73	0.03
64	SLV 16	16	-115	1637	5.76	-4.73	0.03
65	SLU 1	-275	-162	3608	11	-9.71	0.06
65	SLU 2	-275	-162	3608	11	-9.71	0.06
65	SLU 3	-275	-162	3608	11	-9.71	0.06
65	SLU 4	-275	-162	3608	11	-9.71	0.06
65	SLU 5	-275	-162	3608	11	-9.71	0.06
65	SLU 6	-275	-162	3608	11	-9.71	0.06
65	SLU 7	-275	-162	3608	11	-9.71	0.06
65	SLU 8	-275	-162	3608	11	-9.71	0.06
65	SLU 9	-275	-162	3608	11	-9.71	0.06
65	SLU 10	-353	-171	4355	12.37	-14.59	0.07
65	SLU 11	-353	-171	4355	12.37	-14.59	0.07
65	SLU 12	-353	-171	4355	12.37	-14.59	0.07
65	SLU 13	-353	-171	4355	12.37	-14.59	0.07
65	SLU 14	-353	-171	4355	12.37	-14.59	0.07
65	SLU 15	-353	-171	4355	12.37	-14.59	0.07
65	SLU 16	-353	-171	4355	12.37	-14.59	0.07
65	SLU 17	-353	-171	4355	12.37	-14.59	0.07
65	SLU 18	-386	-176	4676	12.97	-16.69	0.07
65	SLU 19	-386	-176	4676	12.97	-16.69	0.07
65	SLU 20	-386	-176	4676	12.97	-16.69	0.07
65	SLU 21	-386	-176	4676	12.97	-16.69	0.07
65	SLU 22	-320	-169	4054	11.85	-12.37	0.06
65	SLU 23	-320	-169	4054	11.85	-12.37	0.06
65	SLU 24	-320	-169	4054	11.85	-12.37	0.06
65	SLU 25	-320	-169	4054	11.85	-12.37	0.06
65	SLU 26	-320	-169	4054	11.85	-12.37	0.06
65	SLU 27	-320	-169	4054	11.85	-12.37	0.06
65	SLU 28	-320	-169	4054	11.85	-12.37	0.06
65	SLU 29	-320	-169	4054	11.85	-12.37	0.06
65	SLU 30	-320	-169	4054	11.85	-12.37	0.06
65	SLU 31	-398	-179	4802	13.23	-17.25	0.07
65	SLU 32	-398	-179	4802	13.23	-17.25	0.07
65	SLU 33	-398	-179	4802	13.23	-17.25	0.07
65	SLU 34	-398	-179	4802	13.23	-17.25	0.07
65	SLU 35	-398	-179	4802	13.23	-17.25	0.07
65	SLU 36	-398	-179	4802	13.23	-17.25	0.07
65	SLU 37	-398	-179	4802	13.23	-17.25	0.07
65	SLU 38	-398	-179	4802	13.23	-17.25	0.07
65	SLU 39	-431	-183	5122	13.82	-19.35	0.08
65	SLU 40	-431	-183	5122	13.82	-19.35	0.08
65	SLU 41	-431	-183	5122	13.82	-19.35	0.08
65	SLU 42	-431	-183	5122	13.82	-19.35	0.08
65	SLU 43	-342	-208	4537	14	-11.71	0.07
65	SLU 44	-342	-208	4537	14	-11.71	0.07
65	SLU 45	-342	-208	4537	14	-11.71	0.07
65	SLU 46	-342	-208	4537	14	-11.71	0.07
65	SLU 47	-342	-208	4537	14	-11.71	0.07
65	SLU 48	-342	-208	4537	14	-11.71	0.07
65	SLU 49	-342	-208	4537	14	-11.71	0.07
65	SLU 50	-342	-208	4537	14	-11.71	0.07
65	SLU 51	-342	-208	4537	14	-11.71	0.07
65	SLU 52	-420	-218	5284	15.38	-16.59	0.08
65	SLU 53	-420	-218	5284	15.38	-16.59	0.08
65	SLU 54	-420	-218	5284	15.38	-16.59	0.08
65	SLU 55	-420	-218	5284	15.38	-16.59	0.08
65	SLU 56	-420	-218	5284	15.38	-16.59	0.08
65	SLU 57	-420	-218	5284	15.38	-16.59	0.08
65	SLU 58	-420	-218	5284	15.38	-16.59	0.08



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
65	SLU 59	-420	-218	5284	15.38	-16.59	0.08
65	SLU 60	-453	-222	5605	15.97	-18.69	0.09
65	SLU 61	-453	-222	5605	15.97	-18.69	0.09
65	SLU 62	-453	-222	5605	15.97	-18.69	0.09
65	SLU 63	-453	-222	5605	15.97	-18.69	0.09
65	SLU 64	-387	-215	4983	14.86	-14.37	0.08
65	SLU 65	-387	-215	4983	14.86	-14.37	0.08
65	SLU 66	-387	-215	4983	14.86	-14.37	0.08
65	SLU 67	-387	-215	4983	14.86	-14.37	0.08
65	SLU 68	-387	-215	4983	14.86	-14.37	0.08
65	SLU 69	-387	-215	4983	14.86	-14.37	0.08
65	SLU 70	-387	-215	4983	14.86	-14.37	0.08
65	SLU 71	-387	-215	4983	14.86	-14.37	0.08
65	SLU 72	-387	-215	4983	14.86	-14.37	0.08
65	SLU 73	-465	-225	5731	16.23	-19.25	0.09
65	SLU 74	-465	-225	5731	16.23	-19.25	0.09
65	SLU 75	-465	-225	5731	16.23	-19.25	0.09
65	SLU 76	-465	-225	5731	16.23	-19.25	0.09
65	SLU 77	-465	-225	5731	16.23	-19.25	0.09
65	SLU 78	-465	-225	5731	16.23	-19.25	0.09
65	SLU 79	-465	-225	5731	16.23	-19.25	0.09
65	SLU 80	-465	-225	5731	16.23	-19.25	0.09
65	SLU 81	-498	-229	6051	16.82	-21.35	0.09
65	SLU 82	-498	-229	6051	16.82	-21.35	0.09
65	SLU 83	-498	-229	6051	16.82	-21.35	0.09
65	SLU 84	-498	-229	6051	16.82	-21.35	0.09
65	SLE RA 1	-288	-164	3735	11.24	-10.47	0.06
65	SLE RA 2	-288	-164	3735	11.24	-10.47	0.06
65	SLE RA 3	-288	-164	3735	11.24	-10.47	0.06
65	SLE RA 4	-288	-164	3735	11.24	-10.47	0.06
65	SLE RA 5	-288	-164	3735	11.24	-10.47	0.06
65	SLE RA 6	-288	-164	3735	11.24	-10.47	0.06
65	SLE RA 7	-288	-164	3735	11.24	-10.47	0.06
65	SLE RA 8	-288	-164	3735	11.24	-10.47	0.06
65	SLE RA 9	-288	-164	3735	11.24	-10.47	0.06
65	SLE RA 10	-340	-170	4234	12.16	-13.73	0.07
65	SLE RA 11	-340	-170	4234	12.16	-13.73	0.07
65	SLE RA 12	-340	-170	4234	12.16	-13.73	0.07
65	SLE RA 13	-340	-170	4234	12.16	-13.73	0.07
65	SLE RA 14	-340	-170	4234	12.16	-13.73	0.07
65	SLE RA 15	-340	-170	4234	12.16	-13.73	0.07
65	SLE RA 16	-340	-170	4234	12.16	-13.73	0.07
65	SLE RA 17	-340	-170	4234	12.16	-13.73	0.07
65	SLE RA 18	-362	-173	4447	12.55	-15.12	0.07
65	SLE RA 19	-362	-173	4447	12.55	-15.12	0.07
65	SLE RA 20	-362	-173	4447	12.55	-15.12	0.07
65	SLE RA 21	-362	-173	4447	12.55	-15.12	0.07
65	SLE FR 1	-288	-164	3735	11.24	-10.47	0.06
65	SLE FR 2	-288	-164	3735	11.24	-10.47	0.06
65	SLE FR 3	-288	-164	3735	11.24	-10.47	0.06
65	SLE FR 4	-310	-166	3949	11.63	-11.86	0.06
65	SLE FR 5	-310	-166	3949	11.63	-11.86	0.06
65	SLE FR 6	-325	-168	4091	11.9	-12.8	0.06
65	SLE QP 1	-288	-164	3735	11.24	-10.47	0.06
65	SLE QP 2	-310	-166	3949	11.63	-11.86	0.06
65	SLD 1	-254	-117	3332	8.06	-6.7	0.07
65	SLD 2	-254	-117	3332	8.06	-6.7	0.07
65	SLD 3	-257	-186	3538	12.38	-6.28	0.1
65	SLD 4	-257	-186	3538	12.38	-6.28	0.1
65	SLD 5	-289	-47	3451	4	-10.96	0.01
65	SLD 6	-289	-47	3451	4	-10.96	0.01
65	SLD 7	-299	-276	4138	18.42	-9.54	0.13
65	SLD 8	-299	-276	4138	18.42	-9.54	0.13
65	SLD 9	-322	-56	3760	4.85	-14.19	-0.01
65	SLD 10	-322	-56	3760	4.85	-14.19	-0.01
65	SLD 11	-332	-286	4447	19.26	-12.77	0.12
65	SLD 12	-332	-286	4447	19.26	-12.77	0.12
65	SLD 13	-364	-147	4360	10.89	-17.45	0.02
65	SLD 14	-364	-147	4360	10.89	-17.45	0.02
65	SLD 15	-367	-216	4566	15.21	-17.03	0.06
65	SLD 16	-367	-216	4566	15.21	-17.03	0.06
65	SLV 1	-178	-49	2501	3.14	0.16	0.07
65	SLV 2	-178	-49	2501	3.14	0.16	0.07
65	SLV 3	-186	-212	2994	13.53	1.18	0.16
65	SLV 4	-186	-212	2994	13.53	1.18	0.16
65	SLV 5	-259	116	2767	-6.67	-9.81	-0.08
65	SLV 6	-259	116	2767	-6.67	-9.81	-0.08
65	SLV 7	-284	-428	4410	27.95	-6.4	0.24
65	SLV 8	-284	-428	4410	27.95	-6.4	0.24
65	SLV 9	-336	95	3488	-4.68	-17.33	-0.11
65	SLV 10	-336	95	3488	-4.68	-17.33	-0.11
65	SLV 11	-361	-449	5130	29.93	-13.92	0.21
65	SLV 12	-361	-449	5130	29.93	-13.92	0.21
65	SLV 13	-434	-121	4904	9.74	-24.91	-0.04
65	SLV 14	-434	-121	4904	9.74	-24.91	-0.04
65	SLV 15	-442	-284	5396	20.13	-23.89	0.06
65	SLV 16	-442	-284	5396	20.13	-23.89	0.06
66	SLU 1	12	-1	697	0.36	-8.82	-0.06



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
66	SLU 2	12	-1	697	0.36	-8.82	-0.06
66	SLU 3	12	-1	697	0.36	-8.82	-0.06
66	SLU 4	12	-1	697	0.36	-8.82	-0.06
66	SLU 5	12	-1	697	0.36	-8.82	-0.06
66	SLU 6	12	-1	697	0.36	-8.82	-0.06
66	SLU 7	12	-1	697	0.36	-8.82	-0.06
66	SLU 8	12	-1	697	0.36	-8.82	-0.06
66	SLU 9	12	-1	697	0.36	-8.82	-0.06
66	SLU 10	-46	-2	651	0.44	-13.59	-0.08
66	SLU 11	-46	-2	651	0.44	-13.59	-0.08
66	SLU 12	-46	-2	651	0.44	-13.59	-0.08
66	SLU 13	-46	-2	651	0.44	-13.59	-0.08
66	SLU 14	-46	-2	651	0.44	-13.59	-0.08
66	SLU 15	-46	-2	651	0.44	-13.59	-0.08
66	SLU 16	-46	-2	651	0.44	-13.59	-0.08
66	SLU 17	-46	-2	651	0.44	-13.59	-0.08
66	SLU 18	-71	-2	631	0.48	-15.63	-0.08
66	SLU 19	-71	-2	631	0.48	-15.63	-0.08
66	SLU 20	-71	-2	631	0.48	-15.63	-0.08
66	SLU 21	-71	-2	631	0.48	-15.63	-0.08
66	SLU 22	-17	-1	688	0.41	-11.41	-0.07
66	SLU 23	-17	-1	688	0.41	-11.41	-0.07
66	SLU 24	-17	-1	688	0.41	-11.41	-0.07
66	SLU 25	-17	-1	688	0.41	-11.41	-0.07
66	SLU 26	-17	-1	688	0.41	-11.41	-0.07
66	SLU 27	-17	-1	688	0.41	-11.41	-0.07
66	SLU 28	-17	-1	688	0.41	-11.41	-0.07
66	SLU 29	-17	-1	688	0.41	-11.41	-0.07
66	SLU 30	-17	-1	688	0.41	-11.41	-0.07
66	SLU 31	-75	-2	643	0.49	-16.18	-0.09
66	SLU 32	-75	-2	643	0.49	-16.18	-0.09
66	SLU 33	-75	-2	643	0.49	-16.18	-0.09
66	SLU 34	-75	-2	643	0.49	-16.18	-0.09
66	SLU 35	-75	-2	643	0.49	-16.18	-0.09
66	SLU 36	-75	-2	643	0.49	-16.18	-0.09
66	SLU 37	-75	-2	643	0.49	-16.18	-0.09
66	SLU 38	-75	-2	643	0.49	-16.18	-0.09
66	SLU 39	-100	-2	623	0.53	-18.23	-0.09
66	SLU 40	-100	-2	623	0.53	-18.23	-0.09
66	SLU 41	-100	-2	623	0.53	-18.23	-0.09
66	SLU 42	-100	-2	623	0.53	-18.23	-0.09
66	SLU 43	26	-2	909	0.45	-10.58	-0.07
66	SLU 44	26	-2	909	0.45	-10.58	-0.07
66	SLU 45	26	-2	909	0.45	-10.58	-0.07
66	SLU 46	26	-2	909	0.45	-10.58	-0.07
66	SLU 47	26	-2	909	0.45	-10.58	-0.07
66	SLU 48	26	-2	909	0.45	-10.58	-0.07
66	SLU 49	26	-2	909	0.45	-10.58	-0.07
66	SLU 50	26	-2	909	0.45	-10.58	-0.07
66	SLU 51	26	-2	909	0.45	-10.58	-0.07
66	SLU 52	-32	-2	863	0.53	-15.35	-0.09
66	SLU 53	-32	-2	863	0.53	-15.35	-0.09
66	SLU 54	-32	-2	863	0.53	-15.35	-0.09
66	SLU 55	-32	-2	863	0.53	-15.35	-0.09
66	SLU 56	-32	-2	863	0.53	-15.35	-0.09
66	SLU 57	-32	-2	863	0.53	-15.35	-0.09
66	SLU 58	-32	-2	863	0.53	-15.35	-0.09
66	SLU 59	-32	-2	863	0.53	-15.35	-0.09
66	SLU 60	-57	-2	843	0.57	-17.39	-0.1
66	SLU 61	-57	-2	843	0.57	-17.39	-0.1
66	SLU 62	-57	-2	843	0.57	-17.39	-0.1
66	SLU 63	-57	-2	843	0.57	-17.39	-0.1
66	SLU 64	-4	-2	900	0.5	-13.17	-0.08
66	SLU 65	-4	-2	900	0.5	-13.17	-0.08
66	SLU 66	-4	-2	900	0.5	-13.17	-0.08
66	SLU 67	-4	-2	900	0.5	-13.17	-0.08
66	SLU 68	-4	-2	900	0.5	-13.17	-0.08
66	SLU 69	-4	-2	900	0.5	-13.17	-0.08
66	SLU 70	-4	-2	900	0.5	-13.17	-0.08
66	SLU 71	-4	-2	900	0.5	-13.17	-0.08
66	SLU 72	-4	-2	900	0.5	-13.17	-0.08
66	SLU 73	-62	-2	855	0.58	-17.94	-0.1
66	SLU 74	-62	-2	855	0.58	-17.94	-0.1
66	SLU 75	-62	-2	855	0.58	-17.94	-0.1
66	SLU 76	-62	-2	855	0.58	-17.94	-0.1
66	SLU 77	-62	-2	855	0.58	-17.94	-0.1
66	SLU 78	-62	-2	855	0.58	-17.94	-0.1
66	SLU 79	-62	-2	855	0.58	-17.94	-0.1
66	SLU 80	-62	-2	855	0.58	-17.94	-0.1
66	SLU 81	-86	-2	835	0.62	-19.98	-0.11
66	SLU 82	-86	-2	835	0.62	-19.98	-0.11
66	SLU 83	-86	-2	835	0.62	-19.98	-0.11
66	SLU 84	-86	-2	835	0.62	-19.98	-0.11
66	SLE RA 1	4	-1	694	0.37	-9.56	-0.06
66	SLE RA 2	4	-1	694	0.37	-9.56	-0.06
66	SLE RA 3	4	-1	694	0.37	-9.56	-0.06
66	SLE RA 4	4	-1	694	0.37	-9.56	-0.06
66	SLE RA 5	4	-1	694	0.37	-9.56	-0.06



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione		
		x	y	z		x	y	z
66	SLE RA 6	4	-1	694		0.37	-9.56	-0.06
66	SLE RA 7	4	-1	694		0.37	-9.56	-0.06
66	SLE RA 8	4	-1	694		0.37	-9.56	-0.06
66	SLE RA 9	4	-1	694		0.37	-9.56	-0.06
66	SLE RA 10	-35	-2	664		0.43	-12.74	-0.07
66	SLE RA 11	-35	-2	664		0.43	-12.74	-0.07
66	SLE RA 12	-35	-2	664		0.43	-12.74	-0.07
66	SLE RA 13	-35	-2	664		0.43	-12.74	-0.07
66	SLE RA 14	-35	-2	664		0.43	-12.74	-0.07
66	SLE RA 15	-35	-2	664		0.43	-12.74	-0.07
66	SLE RA 16	-35	-2	664		0.43	-12.74	-0.07
66	SLE RA 17	-35	-2	664		0.43	-12.74	-0.07
66	SLE RA 18	-52	-2	651		0.45	-14.1	-0.08
66	SLE RA 19	-52	-2	651		0.45	-14.1	-0.08
66	SLE RA 20	-52	-2	651		0.45	-14.1	-0.08
66	SLE RA 21	-52	-2	651		0.45	-14.1	-0.08
66	SLE FR 1	4	-1	694		0.37	-9.56	-0.06
66	SLE FR 2	4	-1	694		0.37	-9.56	-0.06
66	SLE FR 3	4	-1	694		0.37	-9.56	-0.06
66	SLE FR 4	-13	-1	681		0.4	-10.92	-0.07
66	SLE FR 5	-13	-1	681		0.4	-10.92	-0.07
66	SLE FR 6	-24	-2	673		0.41	-11.83	-0.07
66	SLE QP 1	4	-1	694		0.37	-9.56	-0.06
66	SLE QP 2	-13	-1	681		0.4	-10.92	-0.07
66	SLD 1	60	-8	876		1.26	-6.04	-0.26
66	SLD 2	60	-8	876		1.26	-6.04	-0.26
66	SLD 3	80	-21	943		3.21	-5.47	-0.71
66	SLD 4	80	-21	943		3.21	-5.47	-0.71
66	SLD 5	-21	17	637		-2.31	-10.31	0.56
66	SLD 6	-21	17	637		-2.31	-10.31	0.56
66	SLD 7	45	-28	862		4.21	-8.43	-0.94
66	SLD 8	45	-28	862		4.21	-8.43	-0.94
66	SLD 9	-71	25	500		-3.42	-13.41	0.81
66	SLD 10	-71	25	500		-3.42	-13.41	0.81
66	SLD 11	-5	-20	725		3.1	-11.53	-0.69
66	SLD 12	-5	-20	725		3.1	-11.53	-0.69
66	SLD 13	-106	18	420		-2.42	-16.37	0.57
66	SLD 14	-106	18	420		-2.42	-16.37	0.57
66	SLD 15	-86	5	487		-0.47	-15.81	0.12
66	SLD 16	-86	5	487		-0.47	-15.81	0.12
66	SLV 1	158	-14	1134		2.21	0.46	-0.46
66	SLV 2	158	-14	1134		2.21	0.46	-0.46
66	SLV 3	205	-50	1295		7.37	1.84	-1.65
66	SLV 4	205	-50	1295		7.37	1.84	-1.65
66	SLV 5	-33	48	574		-6.89	-9.61	1.61
66	SLV 6	-33	48	574		-6.89	-9.61	1.61
66	SLV 7	124	-69	1108		10.32	-4.99	-2.34
66	SLV 8	124	-69	1108		10.32	-4.99	-2.34
66	SLV 9	-150	67	254		-9.53	-16.85	2.21
66	SLV 10	-150	67	254		-9.53	-16.85	2.21
66	SLV 11	8	-51	788		7.68	-12.24	-1.75
66	SLV 12	8	-51	788		7.68	-12.24	-1.75
66	SLV 13	-231	47	68		-6.58	-23.69	1.51
66	SLV 14	-231	47	68		-6.58	-23.69	1.51
66	SLV 15	-183	11	228		-1.42	-22.31	0.33
66	SLV 16	-183	11	228		-1.42	-22.31	0.33
67	SLU 1	-581	0	2061		0.03	-15.06	0.01
67	SLU 2	-581	0	2061		0.03	-15.06	0.01
67	SLU 3	-581	0	2061		0.03	-15.06	0.01
67	SLU 4	-581	0	2061		0.03	-15.06	0.01
67	SLU 5	-581	0	2061		0.03	-15.06	0.01
67	SLU 6	-581	0	2061		0.03	-15.06	0.01
67	SLU 7	-581	0	2061		0.03	-15.06	0.01
67	SLU 8	-581	0	2061		0.03	-15.06	0.01
67	SLU 9	-581	0	2061		0.03	-15.06	0.01
67	SLU 10	-804	0	2819		0.04	-21.29	0.01
67	SLU 11	-804	0	2819		0.04	-21.29	0.01
67	SLU 12	-804	0	2819		0.04	-21.29	0.01
67	SLU 13	-804	0	2819		0.04	-21.29	0.01
67	SLU 14	-804	0	2819		0.04	-21.29	0.01
67	SLU 15	-804	0	2819		0.04	-21.29	0.01
67	SLU 16	-804	0	2819		0.04	-21.29	0.01
67	SLU 17	-804	0	2819		0.04	-21.29	0.01
67	SLU 18	-900	0	3144		0.05	-23.95	0.01
67	SLU 19	-900	0	3144		0.05	-23.95	0.01
67	SLU 20	-900	0	3144		0.05	-23.95	0.01
67	SLU 21	-900	0	3144		0.05	-23.95	0.01
67	SLU 22	-704	0	2482		0.04	-18.43	0.01
67	SLU 23	-704	0	2482		0.04	-18.43	0.01
67	SLU 24	-704	0	2482		0.04	-18.43	0.01
67	SLU 25	-704	0	2482		0.04	-18.43	0.01
67	SLU 26	-704	0	2482		0.04	-18.43	0.01
67	SLU 27	-704	0	2482		0.04	-18.43	0.01
67	SLU 28	-704	0	2482		0.04	-18.43	0.01
67	SLU 29	-704	0	2482		0.04	-18.43	0.01
67	SLU 30	-704	0	2482		0.04	-18.43	0.01
67	SLU 31	-927	0	3240		0.05	-24.66	0.01
67	SLU 32	-927	0	3240		0.05	-24.66	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
67	SLU 33	-927	0	3240	0.05	-24.66	0.01
67	SLU 34	-927	0	3240	0.05	-24.66	0.01
67	SLU 35	-927	0	3240	0.05	-24.66	0.01
67	SLU 36	-927	0	3240	0.05	-24.66	0.01
67	SLU 37	-927	0	3240	0.05	-24.66	0.01
67	SLU 38	-927	0	3240	0.05	-24.66	0.01
67	SLU 39	-1023	0	3565	0.06	-27.33	0.01
67	SLU 40	-1023	0	3565	0.06	-27.33	0.01
67	SLU 41	-1023	0	3565	0.06	-27.33	0.01
67	SLU 42	-1023	0	3565	0.06	-27.33	0.01
67	SLU 43	-713	0	2535	0.03	-18.42	0.01
67	SLU 44	-713	0	2535	0.03	-18.42	0.01
67	SLU 45	-713	0	2535	0.03	-18.42	0.01
67	SLU 46	-713	0	2535	0.03	-18.42	0.01
67	SLU 47	-713	0	2535	0.03	-18.42	0.01
67	SLU 48	-713	0	2535	0.03	-18.42	0.01
67	SLU 49	-713	0	2535	0.03	-18.42	0.01
67	SLU 50	-713	0	2535	0.03	-18.42	0.01
67	SLU 51	-713	0	2535	0.03	-18.42	0.01
67	SLU 52	-936	0	3294	0.05	-24.65	0.01
67	SLU 53	-936	0	3294	0.05	-24.65	0.01
67	SLU 54	-936	0	3294	0.05	-24.65	0.01
67	SLU 55	-936	0	3294	0.05	-24.65	0.01
67	SLU 56	-936	0	3294	0.05	-24.65	0.01
67	SLU 57	-936	0	3294	0.05	-24.65	0.01
67	SLU 58	-936	0	3294	0.05	-24.65	0.01
67	SLU 59	-936	0	3294	0.05	-24.65	0.01
67	SLU 60	-1032	0	3618	0.06	-27.32	0.01
67	SLU 61	-1032	0	3618	0.06	-27.32	0.01
67	SLU 62	-1032	0	3618	0.06	-27.32	0.01
67	SLU 63	-1032	0	3618	0.06	-27.32	0.01
67	SLU 64	-836	0	2956	0.04	-21.79	0.01
67	SLU 65	-836	0	2956	0.04	-21.79	0.01
67	SLU 66	-836	0	2956	0.04	-21.79	0.01
67	SLU 67	-836	0	2956	0.04	-21.79	0.01
67	SLU 68	-836	0	2956	0.04	-21.79	0.01
67	SLU 69	-836	0	2956	0.04	-21.79	0.01
67	SLU 70	-836	0	2956	0.04	-21.79	0.01
67	SLU 71	-836	0	2956	0.04	-21.79	0.01
67	SLU 72	-836	0	2956	0.04	-21.79	0.01
67	SLU 73	-1059	0	3714	0.06	-28.02	0.01
67	SLU 74	-1059	0	3714	0.06	-28.02	0.01
67	SLU 75	-1059	0	3714	0.06	-28.02	0.01
67	SLU 76	-1059	0	3714	0.06	-28.02	0.01
67	SLU 77	-1059	0	3714	0.06	-28.02	0.01
67	SLU 78	-1059	0	3714	0.06	-28.02	0.01
67	SLU 79	-1059	0	3714	0.06	-28.02	0.01
67	SLU 80	-1059	0	3714	0.06	-28.02	0.01
67	SLU 81	-1155	0	4039	0.06	-30.69	0.01
67	SLU 82	-1155	0	4039	0.06	-30.69	0.01
67	SLU 83	-1155	0	4039	0.06	-30.69	0.01
67	SLU 84	-1155	0	4039	0.06	-30.69	0.01
67	SLE RA 1	-616	0	2181	0.03	-16.02	0.01
67	SLE RA 2	-616	0	2181	0.03	-16.02	0.01
67	SLE RA 3	-616	0	2181	0.03	-16.02	0.01
67	SLE RA 4	-616	0	2181	0.03	-16.02	0.01
67	SLE RA 5	-616	0	2181	0.03	-16.02	0.01
67	SLE RA 6	-616	0	2181	0.03	-16.02	0.01
67	SLE RA 7	-616	0	2181	0.03	-16.02	0.01
67	SLE RA 8	-616	0	2181	0.03	-16.02	0.01
67	SLE RA 9	-616	0	2181	0.03	-16.02	0.01
67	SLE RA 10	-765	0	2687	0.04	-20.17	0.01
67	SLE RA 11	-765	0	2687	0.04	-20.17	0.01
67	SLE RA 12	-765	0	2687	0.04	-20.17	0.01
67	SLE RA 13	-765	0	2687	0.04	-20.17	0.01
67	SLE RA 14	-765	0	2687	0.04	-20.17	0.01
67	SLE RA 15	-765	0	2687	0.04	-20.17	0.01
67	SLE RA 16	-765	0	2687	0.04	-20.17	0.01
67	SLE RA 17	-765	0	2687	0.04	-20.17	0.01
67	SLE RA 18	-829	0	2903	0.05	-21.95	0.01
67	SLE RA 19	-829	0	2903	0.05	-21.95	0.01
67	SLE RA 20	-829	0	2903	0.05	-21.95	0.01
67	SLE RA 21	-829	0	2903	0.05	-21.95	0.01
67	SLE FR 1	-616	0	2181	0.03	-16.02	0.01
67	SLE FR 2	-616	0	2181	0.03	-16.02	0.01
67	SLE FR 3	-616	0	2181	0.03	-16.02	0.01
67	SLE FR 4	-680	0	2398	0.04	-17.8	0.01
67	SLE FR 5	-680	0	2398	0.04	-17.8	0.01
67	SLE FR 6	-722	0	2542	0.04	-18.99	0.01
67	SLE QP 1	-616	0	2181	0.03	-16.02	0.01
67	SLE QP 2	-680	0	2398	0.04	-17.8	0.01
67	SLD 1	-474	-28	1786	4.73	-10.59	0.8
67	SLD 2	-474	-28	1786	4.73	-10.59	0.8
67	SLD 3	-476	23	1794	-2.79	-10.7	-0.46
67	SLD 4	-476	23	1794	-2.79	-10.7	-0.46
67	SLD 5	-614	-85	2202	12.85	-15.48	2.16
67	SLD 6	-614	-85	2202	12.85	-15.48	2.16
67	SLD 7	-623	84	2229	-12.22	-15.83	-2.05



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
67	SLD 8	-623	84	2229	-12.22	-15.83	-2.05
67	SLD 9	-736	-84	2567	12.29	-19.77	2.06
67	SLD 10	-736	-84	2567	12.29	-19.77	2.06
67	SLD 11	-746	85	2594	-12.78	-20.12	-2.14
67	SLD 12	-746	85	2594	-12.78	-20.12	-2.14
67	SLD 13	-883	-23	3002	2.86	-24.9	0.48
67	SLD 14	-883	-23	3002	2.86	-24.9	0.48
67	SLD 15	-886	28	3010	-4.66	-25.01	-0.78
67	SLD 16	-886	28	3010	-4.66	-25.01	-0.78
67	SLV 1	-197	-78	965	11.59	-0.9	1.96
67	SLV 2	-197	-78	965	11.59	-0.9	1.96
67	SLV 3	-204	65	984	-6.98	-1.15	-1.17
67	SLV 4	-204	65	984	-6.98	-1.15	-1.17
67	SLV 5	-525	-240	1939	31.68	-12.35	5.33
67	SLV 6	-525	-240	1939	31.68	-12.35	5.33
67	SLV 7	-547	236	2003	-30.25	-13.19	-5.09
67	SLV 8	-547	236	2003	-30.25	-13.19	-5.09
67	SLV 9	-812	-236	2793	30.32	-22.42	5.1
67	SLV 10	-812	-236	2793	30.32	-22.42	5.1
67	SLV 11	-835	240	2857	-31.61	-23.25	-5.32
67	SLV 12	-835	240	2857	-31.61	-23.25	-5.32
67	SLV 13	-1156	-65	3812	7.05	-34.45	1.18
67	SLV 14	-1156	-65	3812	7.05	-34.45	1.18
67	SLV 15	-1163	78	3831	-11.52	-34.7	-1.94
67	SLV 16	-1163	78	3831	-11.52	-34.7	-1.94
68	SLU 1	-433	0	3289	0.05	-25.09	0
68	SLU 2	-433	0	3289	0.05	-25.09	0
68	SLU 3	-433	0	3289	0.05	-25.09	0
68	SLU 4	-433	0	3289	0.05	-25.09	0
68	SLU 5	-433	0	3289	0.05	-25.09	0
68	SLU 6	-433	0	3289	0.05	-25.09	0
68	SLU 7	-433	0	3289	0.05	-25.09	0
68	SLU 8	-433	0	3289	0.05	-25.09	0
68	SLU 9	-433	0	3289	0.05	-25.09	0
68	SLU 10	-612	0	4440	0.08	-35.58	0
68	SLU 11	-612	0	4440	0.08	-35.58	0
68	SLU 12	-612	0	4440	0.08	-35.58	0
68	SLU 13	-612	0	4440	0.08	-35.58	0
68	SLU 14	-612	0	4440	0.08	-35.58	0
68	SLU 15	-612	0	4440	0.08	-35.58	0
68	SLU 16	-612	0	4440	0.08	-35.58	0
68	SLU 17	-612	0	4440	0.08	-35.58	0
68	SLU 18	-689	0	4933	0.09	-40.07	0
68	SLU 19	-689	0	4933	0.09	-40.07	0
68	SLU 20	-689	0	4933	0.09	-40.07	0
68	SLU 21	-689	0	4933	0.09	-40.07	0
68	SLU 22	-530	0	3935	0.06	-30.78	0
68	SLU 23	-530	0	3935	0.06	-30.78	0
68	SLU 24	-530	0	3935	0.06	-30.78	0
68	SLU 25	-530	0	3935	0.06	-30.78	0
68	SLU 26	-530	0	3935	0.06	-30.78	0
68	SLU 27	-530	0	3935	0.06	-30.78	0
68	SLU 28	-530	0	3935	0.06	-30.78	0
68	SLU 29	-530	0	3935	0.06	-30.78	0
68	SLU 30	-530	0	3935	0.06	-30.78	0
68	SLU 31	-710	0	5086	0.09	-41.27	0
68	SLU 32	-710	0	5086	0.09	-41.27	0
68	SLU 33	-710	0	5086	0.09	-41.27	0
68	SLU 34	-710	0	5086	0.09	-41.27	0
68	SLU 35	-710	0	5086	0.09	-41.27	0
68	SLU 36	-710	0	5086	0.09	-41.27	0
68	SLU 37	-710	0	5086	0.09	-41.27	0
68	SLU 38	-710	0	5086	0.09	-41.27	0
68	SLU 39	-786	0	5579	0.1	-45.76	0
68	SLU 40	-786	0	5579	0.1	-45.76	0
68	SLU 41	-786	0	5579	0.1	-45.76	0
68	SLU 42	-786	0	5579	0.1	-45.76	0
68	SLU 43	-529	0	4055	0.06	-30.67	0
68	SLU 44	-529	0	4055	0.06	-30.67	0
68	SLU 45	-529	0	4055	0.06	-30.67	0
68	SLU 46	-529	0	4055	0.06	-30.67	0
68	SLU 47	-529	0	4055	0.06	-30.67	0
68	SLU 48	-529	0	4055	0.06	-30.67	0
68	SLU 49	-529	0	4055	0.06	-30.67	0
68	SLU 50	-529	0	4055	0.06	-30.67	0
68	SLU 51	-529	0	4055	0.06	-30.67	0
68	SLU 52	-708	0	5205	0.09	-41.16	0
68	SLU 53	-708	0	5205	0.09	-41.16	0
68	SLU 54	-708	0	5205	0.09	-41.16	0
68	SLU 55	-708	0	5205	0.09	-41.16	0
68	SLU 56	-708	0	5205	0.09	-41.16	0
68	SLU 57	-708	0	5205	0.09	-41.16	0
68	SLU 58	-708	0	5205	0.09	-41.16	0
68	SLU 59	-708	0	5205	0.09	-41.16	0
68	SLU 60	-785	0	5698	0.1	-45.65	0
68	SLU 61	-785	0	5698	0.1	-45.65	0
68	SLU 62	-785	0	5698	0.1	-45.65	0
68	SLU 63	-785	0	5698	0.1	-45.65	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
68	SLU 64	-627	0	4701	0.08	-36.36	0
68	SLU 65	-627	0	4701	0.08	-36.36	0
68	SLU 66	-627	0	4701	0.08	-36.36	0
68	SLU 67	-627	0	4701	0.08	-36.36	0
68	SLU 68	-627	0	4701	0.08	-36.36	0
68	SLU 69	-627	0	4701	0.08	-36.36	0
68	SLU 70	-627	0	4701	0.08	-36.36	0
68	SLU 71	-627	0	4701	0.08	-36.36	0
68	SLU 72	-627	0	4701	0.08	-36.36	0
68	SLU 73	-806	0	5851	0.1	-46.84	0
68	SLU 74	-806	0	5851	0.1	-46.84	0
68	SLU 75	-806	0	5851	0.1	-46.84	0
68	SLU 76	-806	0	5851	0.1	-46.84	0
68	SLU 77	-806	0	5851	0.1	-46.84	0
68	SLU 78	-806	0	5851	0.1	-46.84	0
68	SLU 79	-806	0	5851	0.1	-46.84	0
68	SLU 80	-806	0	5851	0.1	-46.84	0
68	SLU 81	-883	0	6344	0.11	-51.34	0
68	SLU 82	-883	0	6344	0.11	-51.34	0
68	SLU 83	-883	0	6344	0.11	-51.34	0
68	SLU 84	-883	0	6344	0.11	-51.34	0
68	SLE RA 1	-461	0	3474	0.05	-26.72	0
68	SLE RA 2	-461	0	3474	0.05	-26.72	0
68	SLE RA 3	-461	0	3474	0.05	-26.72	0
68	SLE RA 4	-461	0	3474	0.05	-26.72	0
68	SLE RA 5	-461	0	3474	0.05	-26.72	0
68	SLE RA 6	-461	0	3474	0.05	-26.72	0
68	SLE RA 7	-461	0	3474	0.05	-26.72	0
68	SLE RA 8	-461	0	3474	0.05	-26.72	0
68	SLE RA 9	-461	0	3474	0.05	-26.72	0
68	SLE RA 10	-580	0	4241	0.07	-33.71	0
68	SLE RA 11	-580	0	4241	0.07	-33.71	0
68	SLE RA 12	-580	0	4241	0.07	-33.71	0
68	SLE RA 13	-580	0	4241	0.07	-33.71	0
68	SLE RA 14	-580	0	4241	0.07	-33.71	0
68	SLE RA 15	-580	0	4241	0.07	-33.71	0
68	SLE RA 16	-580	0	4241	0.07	-33.71	0
68	SLE RA 17	-580	0	4241	0.07	-33.71	0
68	SLE RA 18	-631	0	4570	0.08	-36.7	0
68	SLE RA 19	-631	0	4570	0.08	-36.7	0
68	SLE RA 20	-631	0	4570	0.08	-36.7	0
68	SLE RA 21	-631	0	4570	0.08	-36.7	0
68	SLE FR 1	-461	0	3474	0.05	-26.72	0
68	SLE FR 2	-461	0	3474	0.05	-26.72	0
68	SLE FR 3	-461	0	3474	0.05	-26.72	0
68	SLE FR 4	-512	0	3803	0.06	-29.71	0
68	SLE FR 5	-512	0	3803	0.06	-29.71	0
68	SLE FR 6	-546	0	4022	0.07	-31.71	0
68	SLE QP 1	-461	0	3474	0.05	-26.72	0
68	SLE QP 2	-512	0	3803	0.06	-29.71	0
68	SLD 1	-306	8	3103	-8.55	-17.06	0.03
68	SLD 2	-306	8	3103	-8.55	-17.06	0.03
68	SLD 3	-309	-13	3113	12.67	-17.25	-0.04
68	SLD 4	-309	-13	3113	12.67	-17.25	-0.04
68	SLD 5	-445	35	3578	-34.7	-25.63	0.11
68	SLD 6	-445	35	3578	-34.7	-25.63	0.11
68	SLD 7	-456	-36	3611	36.03	-26.26	-0.12
68	SLD 8	-456	-36	3611	36.03	-26.26	-0.12
68	SLD 9	-568	36	3995	-35.9	-33.16	0.12
68	SLD 10	-568	36	3995	-35.9	-33.16	0.12
68	SLD 11	-578	-35	4027	34.83	-33.8	-0.11
68	SLD 12	-578	-35	4027	34.83	-33.8	-0.11
68	SLD 13	-714	13	4492	-12.55	-42.17	0.04
68	SLD 14	-714	13	4492	-12.55	-42.17	0.04
68	SLD 15	-718	-8	4502	8.67	-42.36	-0.03
68	SLD 16	-718	-8	4502	8.67	-42.36	-0.03
68	SLV 1	-30	20	2166	-22.67	-0.09	0.07
68	SLV 2	-30	20	2166	-22.67	-0.09	0.07
68	SLV 3	-37	-33	2189	32.67	-0.53	-0.11
68	SLV 4	-37	-33	2189	32.67	-0.53	-0.11
68	SLV 5	-356	86	3276	-90.69	-20.15	0.3
68	SLV 6	-356	86	3276	-90.69	-20.15	0.3
68	SLV 7	-381	-90	3354	93.77	-21.64	-0.31
68	SLV 8	-381	-90	3354	93.77	-21.64	-0.31
68	SLV 9	-643	90	4251	-93.65	-37.79	0.31
68	SLV 10	-643	90	4251	-93.65	-37.79	0.31
68	SLV 11	-668	-87	4329	90.81	-39.28	-0.3
68	SLV 12	-668	-87	4329	90.81	-39.28	-0.3
68	SLV 13	-986	33	5416	-32.54	-58.89	0.11
68	SLV 14	-986	33	5416	-32.54	-58.89	0.11
68	SLV 15	-994	-20	5440	22.79	-59.34	-0.07
68	SLV 16	-994	-20	5440	22.79	-59.34	-0.07
69	SLU 1	-329	0	2980	0.04	-16.18	0
69	SLU 2	-329	0	2980	0.04	-16.18	0
69	SLU 3	-329	0	2980	0.04	-16.18	0
69	SLU 4	-329	0	2980	0.04	-16.18	0
69	SLU 5	-329	0	2980	0.04	-16.18	0
69	SLU 6	-329	0	2980	0.04	-16.18	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
69	SLU 7	-329	0	2980	0.04	-16.18	0
69	SLU 8	-329	0	2980	0.04	-16.18	0
69	SLU 9	-329	0	2980	0.04	-16.18	0
69	SLU 10	-485	0	3972	0.06	-24.04	0
69	SLU 11	-485	0	3972	0.06	-24.04	0
69	SLU 12	-485	0	3972	0.06	-24.04	0
69	SLU 13	-485	0	3972	0.06	-24.04	0
69	SLU 14	-485	0	3972	0.06	-24.04	0
69	SLU 15	-485	0	3972	0.06	-24.04	0
69	SLU 16	-485	0	3972	0.06	-24.04	0
69	SLU 17	-485	0	3972	0.06	-24.04	0
69	SLU 18	-552	0	4397	0.07	-27.41	0
69	SLU 19	-552	0	4397	0.07	-27.41	0
69	SLU 20	-552	0	4397	0.07	-27.41	0
69	SLU 21	-552	0	4397	0.07	-27.41	0
69	SLU 22	-411	0	3545	0.05	-20.31	0
69	SLU 23	-411	0	3545	0.05	-20.31	0
69	SLU 24	-411	0	3545	0.05	-20.31	0
69	SLU 25	-411	0	3545	0.05	-20.31	0
69	SLU 26	-411	0	3545	0.05	-20.31	0
69	SLU 27	-411	0	3545	0.05	-20.31	0
69	SLU 28	-411	0	3545	0.05	-20.31	0
69	SLU 29	-411	0	3545	0.05	-20.31	0
69	SLU 30	-411	0	3545	0.05	-20.31	0
69	SLU 31	-567	0	4536	0.07	-28.17	0
69	SLU 32	-567	0	4536	0.07	-28.17	0
69	SLU 33	-567	0	4536	0.07	-28.17	0
69	SLU 34	-567	0	4536	0.07	-28.17	0
69	SLU 35	-567	0	4536	0.07	-28.17	0
69	SLU 36	-567	0	4536	0.07	-28.17	0
69	SLU 37	-567	0	4536	0.07	-28.17	0
69	SLU 38	-567	0	4536	0.07	-28.17	0
69	SLU 39	-634	0	4961	0.08	-31.54	0
69	SLU 40	-634	0	4961	0.08	-31.54	0
69	SLU 41	-634	0	4961	0.08	-31.54	0
69	SLU 42	-634	0	4961	0.08	-31.54	0
69	SLU 43	-399	0	3681	0.05	-19.61	0
69	SLU 44	-399	0	3681	0.05	-19.61	0
69	SLU 45	-399	0	3681	0.05	-19.61	0
69	SLU 46	-399	0	3681	0.05	-19.61	0
69	SLU 47	-399	0	3681	0.05	-19.61	0
69	SLU 48	-399	0	3681	0.05	-19.61	0
69	SLU 49	-399	0	3681	0.05	-19.61	0
69	SLU 50	-399	0	3681	0.05	-19.61	0
69	SLU 51	-399	0	3681	0.05	-19.61	0
69	SLU 52	-555	0	4672	0.07	-27.48	0
69	SLU 53	-555	0	4672	0.07	-27.48	0
69	SLU 54	-555	0	4672	0.07	-27.48	0
69	SLU 55	-555	0	4672	0.07	-27.48	0
69	SLU 56	-555	0	4672	0.07	-27.48	0
69	SLU 57	-555	0	4672	0.07	-27.48	0
69	SLU 58	-555	0	4672	0.07	-27.48	0
69	SLU 59	-555	0	4672	0.07	-27.48	0
69	SLU 60	-622	0	5097	0.07	-30.85	0
69	SLU 61	-622	0	5097	0.07	-30.85	0
69	SLU 62	-622	0	5097	0.07	-30.85	0
69	SLU 63	-622	0	5097	0.07	-30.85	0
69	SLU 64	-482	0	4245	0.06	-23.74	0
69	SLU 65	-482	0	4245	0.06	-23.74	0
69	SLU 66	-482	0	4245	0.06	-23.74	0
69	SLU 67	-482	0	4245	0.06	-23.74	0
69	SLU 68	-482	0	4245	0.06	-23.74	0
69	SLU 69	-482	0	4245	0.06	-23.74	0
69	SLU 70	-482	0	4245	0.06	-23.74	0
69	SLU 71	-482	0	4245	0.06	-23.74	0
69	SLU 72	-482	0	4245	0.06	-23.74	0
69	SLU 73	-638	0	5237	0.08	-31.61	0
69	SLU 74	-638	0	5237	0.08	-31.61	0
69	SLU 75	-638	0	5237	0.08	-31.61	0
69	SLU 76	-638	0	5237	0.08	-31.61	0
69	SLU 77	-638	0	5237	0.08	-31.61	0
69	SLU 78	-638	0	5237	0.08	-31.61	0
69	SLU 79	-638	0	5237	0.08	-31.61	0
69	SLU 80	-638	0	5237	0.08	-31.61	0
69	SLU 81	-705	0	5662	0.08	-34.98	0
69	SLU 82	-705	0	5662	0.08	-34.98	0
69	SLU 83	-705	0	5662	0.08	-34.98	0
69	SLU 84	-705	0	5662	0.08	-34.98	0
69	SLE RA 1	-352	0	3141	0.04	-17.36	0
69	SLE RA 2	-352	0	3141	0.04	-17.36	0
69	SLE RA 3	-352	0	3141	0.04	-17.36	0
69	SLE RA 4	-352	0	3141	0.04	-17.36	0
69	SLE RA 5	-352	0	3141	0.04	-17.36	0
69	SLE RA 6	-352	0	3141	0.04	-17.36	0
69	SLE RA 7	-352	0	3141	0.04	-17.36	0
69	SLE RA 8	-352	0	3141	0.04	-17.36	0
69	SLE RA 9	-352	0	3141	0.04	-17.36	0
69	SLE RA 10	-456	0	3802	0.05	-22.6	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
69	SLE RA 11	-456	0	3802	0.05	-22.6	0
69	SLE RA 12	-456	0	3802	0.05	-22.6	0
69	SLE RA 13	-456	0	3802	0.05	-22.6	0
69	SLE RA 14	-456	0	3802	0.05	-22.6	0
69	SLE RA 15	-456	0	3802	0.05	-22.6	0
69	SLE RA 16	-456	0	3802	0.05	-22.6	0
69	SLE RA 17	-456	0	3802	0.05	-22.6	0
69	SLE RA 18	-501	0	4086	0.06	-24.85	0
69	SLE RA 19	-501	0	4086	0.06	-24.85	0
69	SLE RA 20	-501	0	4086	0.06	-24.85	0
69	SLE RA 21	-501	0	4086	0.06	-24.85	0
69	SLE FR 1	-352	0	3141	0.04	-17.36	0
69	SLE FR 2	-352	0	3141	0.04	-17.36	0
69	SLE FR 3	-352	0	3141	0.04	-17.36	0
69	SLE FR 4	-397	0	3425	0.05	-19.6	0
69	SLE FR 5	-397	0	3425	0.05	-19.6	0
69	SLE FR 6	-427	0	3614	0.05	-21.1	0
69	SLE QP 1	-352	0	3141	0.04	-17.36	0
69	SLE QP 2	-397	0	3425	0.05	-19.6	0
69	SLD 1	-140	9	3075	-12.45	-5.67	0.01
69	SLD 2	-140	9	3075	-12.45	-5.67	0.01
69	SLD 3	-144	-14	3081	16.79	-5.9	-0.01
69	SLD 4	-144	-14	3081	16.79	-5.9	-0.01
69	SLD 5	-313	39	3310	-48.05	-15.08	0.04
69	SLD 6	-313	39	3310	-48.05	-15.08	0.04
69	SLD 7	-328	-40	3332	49.42	-15.83	-0.04
69	SLD 8	-328	-40	3332	49.42	-15.83	-0.04
69	SLD 9	-466	40	3518	-49.33	-23.37	0.04
69	SLD 10	-466	40	3518	-49.33	-23.37	0.04
69	SLD 11	-480	-39	3539	48.15	-24.12	-0.04
69	SLD 12	-480	-39	3539	48.15	-24.12	-0.04
69	SLD 13	-649	14	3768	-16.7	-33.31	0.01
69	SLD 14	-649	14	3768	-16.7	-33.31	0.01
69	SLD 15	-654	-9	3774	12.54	-33.53	-0.01
69	SLD 16	-654	-9	3774	12.54	-33.53	-0.01
69	SLV 1	205	25	2606	-34.25	13.07	0.04
69	SLV 2	205	25	2606	-34.25	13.07	0.04
69	SLV 3	195	-37	2622	44.97	12.54	-0.03
69	SLV 4	195	-37	2622	44.97	12.54	-0.03
69	SLV 5	-201	102	3155	-130.4	-9	0.11
69	SLV 6	-201	102	3155	-130.4	-9	0.11
69	SLV 7	-235	-105	3208	133.69	-10.76	-0.11
69	SLV 8	-235	-105	3208	133.69	-10.76	-0.11
69	SLV 9	-559	105	3642	-133.59	-28.44	0.11
69	SLV 10	-559	105	3642	-133.59	-28.44	0.11
69	SLV 11	-593	-102	3694	130.5	-30.21	-0.11
69	SLV 12	-593	-102	3694	130.5	-30.21	-0.11
69	SLV 13	-989	37	4227	-44.88	-51.75	0.03
69	SLV 14	-989	37	4227	-44.88	-51.75	0.03
69	SLV 15	-999	-25	4243	34.35	-52.28	-0.04
69	SLV 16	-999	-25	4243	34.35	-52.28	-0.04
70	SLU 1	-243	0	2858	0.03	-12.56	0
70	SLU 2	-243	0	2858	0.03	-12.56	0
70	SLU 3	-243	0	2858	0.03	-12.56	0
70	SLU 4	-243	0	2858	0.03	-12.56	0
70	SLU 5	-243	0	2858	0.03	-12.56	0
70	SLU 6	-243	0	2858	0.03	-12.56	0
70	SLU 7	-243	0	2858	0.03	-12.56	0
70	SLU 8	-243	0	2858	0.03	-12.56	0
70	SLU 9	-243	0	2858	0.03	-12.56	0
70	SLU 10	-374	0	3787	0.04	-19.25	0
70	SLU 11	-374	0	3787	0.04	-19.25	0
70	SLU 12	-374	0	3787	0.04	-19.25	0
70	SLU 13	-374	0	3787	0.04	-19.25	0
70	SLU 14	-374	0	3787	0.04	-19.25	0
70	SLU 15	-374	0	3787	0.04	-19.25	0
70	SLU 16	-374	0	3787	0.04	-19.25	0
70	SLU 17	-374	0	3787	0.04	-19.25	0
70	SLU 18	-431	0	4185	0.05	-22.11	0
70	SLU 19	-431	0	4185	0.05	-22.11	0
70	SLU 20	-431	0	4185	0.05	-22.11	0
70	SLU 21	-431	0	4185	0.05	-22.11	0
70	SLU 22	-311	0	3391	0.04	-16.02	0
70	SLU 23	-311	0	3391	0.04	-16.02	0
70	SLU 24	-311	0	3391	0.04	-16.02	0
70	SLU 25	-311	0	3391	0.04	-16.02	0
70	SLU 26	-311	0	3391	0.04	-16.02	0
70	SLU 27	-311	0	3391	0.04	-16.02	0
70	SLU 28	-311	0	3391	0.04	-16.02	0
70	SLU 29	-311	0	3391	0.04	-16.02	0
70	SLU 30	-311	0	3391	0.04	-16.02	0
70	SLU 31	-442	0	4320	0.05	-22.71	0
70	SLU 32	-442	0	4320	0.05	-22.71	0
70	SLU 33	-442	0	4320	0.05	-22.71	0
70	SLU 34	-442	0	4320	0.05	-22.71	0
70	SLU 35	-442	0	4320	0.05	-22.71	0
70	SLU 36	-442	0	4320	0.05	-22.71	0
70	SLU 37	-442	0	4320	0.05	-22.71	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
70	SLU 38	-442	0	4320	0.05	-22.71	0
70	SLU 39	-499	0	4718	0.06	-25.57	0
70	SLU 40	-499	0	4718	0.06	-25.57	0
70	SLU 41	-499	0	4718	0.06	-25.57	0
70	SLU 42	-499	0	4718	0.06	-25.57	0
70	SLU 43	-292	0	3533	0.03	-15.14	0
70	SLU 44	-292	0	3533	0.03	-15.14	0
70	SLU 45	-292	0	3533	0.03	-15.14	0
70	SLU 46	-292	0	3533	0.03	-15.14	0
70	SLU 47	-292	0	3533	0.03	-15.14	0
70	SLU 48	-292	0	3533	0.03	-15.14	0
70	SLU 49	-292	0	3533	0.03	-15.14	0
70	SLU 50	-292	0	3533	0.03	-15.14	0
70	SLU 51	-292	0	3533	0.03	-15.14	0
70	SLU 52	-424	0	4461	0.05	-21.83	0
70	SLU 53	-424	0	4461	0.05	-21.83	0
70	SLU 54	-424	0	4461	0.05	-21.83	0
70	SLU 55	-424	0	4461	0.05	-21.83	0
70	SLU 56	-424	0	4461	0.05	-21.83	0
70	SLU 57	-424	0	4461	0.05	-21.83	0
70	SLU 58	-424	0	4461	0.05	-21.83	0
70	SLU 59	-424	0	4461	0.05	-21.83	0
70	SLU 60	-480	0	4859	0.05	-24.69	0
70	SLU 61	-480	0	4859	0.05	-24.69	0
70	SLU 62	-480	0	4859	0.05	-24.69	0
70	SLU 63	-480	0	4859	0.05	-24.69	0
70	SLU 64	-360	0	4066	0.04	-18.6	0
70	SLU 65	-360	0	4066	0.04	-18.6	0
70	SLU 66	-360	0	4066	0.04	-18.6	0
70	SLU 67	-360	0	4066	0.04	-18.6	0
70	SLU 68	-360	0	4066	0.04	-18.6	0
70	SLU 69	-360	0	4066	0.04	-18.6	0
70	SLU 70	-360	0	4066	0.04	-18.6	0
70	SLU 71	-360	0	4066	0.04	-18.6	0
70	SLU 72	-360	0	4066	0.04	-18.6	0
70	SLU 73	-492	0	4994	0.06	-25.29	0
70	SLU 74	-492	0	4994	0.06	-25.29	0
70	SLU 75	-492	0	4994	0.06	-25.29	0
70	SLU 76	-492	0	4994	0.06	-25.29	0
70	SLU 77	-492	0	4994	0.06	-25.29	0
70	SLU 78	-492	0	4994	0.06	-25.29	0
70	SLU 79	-492	0	4994	0.06	-25.29	0
70	SLU 80	-492	0	4994	0.06	-25.29	0
70	SLU 81	-548	0	5393	0.06	-28.15	0
70	SLU 82	-548	0	5393	0.06	-28.15	0
70	SLU 83	-548	0	5393	0.06	-28.15	0
70	SLU 84	-548	0	5393	0.06	-28.15	0
70	SLE RA 1	-262	0	3010	0.03	-13.55	0
70	SLE RA 2	-262	0	3010	0.03	-13.55	0
70	SLE RA 3	-262	0	3010	0.03	-13.55	0
70	SLE RA 4	-262	0	3010	0.03	-13.55	0
70	SLE RA 5	-262	0	3010	0.03	-13.55	0
70	SLE RA 6	-262	0	3010	0.03	-13.55	0
70	SLE RA 7	-262	0	3010	0.03	-13.55	0
70	SLE RA 8	-262	0	3010	0.03	-13.55	0
70	SLE RA 9	-262	0	3010	0.03	-13.55	0
70	SLE RA 10	-350	0	3629	0.04	-18.01	0
70	SLE RA 11	-350	0	3629	0.04	-18.01	0
70	SLE RA 12	-350	0	3629	0.04	-18.01	0
70	SLE RA 13	-350	0	3629	0.04	-18.01	0
70	SLE RA 14	-350	0	3629	0.04	-18.01	0
70	SLE RA 15	-350	0	3629	0.04	-18.01	0
70	SLE RA 16	-350	0	3629	0.04	-18.01	0
70	SLE RA 17	-350	0	3629	0.04	-18.01	0
70	SLE RA 18	-387	0	3895	0.04	-19.92	0
70	SLE RA 19	-387	0	3895	0.04	-19.92	0
70	SLE RA 20	-387	0	3895	0.04	-19.92	0
70	SLE RA 21	-387	0	3895	0.04	-19.92	0
70	SLE FR 1	-262	0	3010	0.03	-13.55	0
70	SLE FR 2	-262	0	3010	0.03	-13.55	0
70	SLE FR 3	-262	0	3010	0.03	-13.55	0
70	SLE FR 4	-300	0	3276	0.03	-15.46	0
70	SLE FR 5	-300	0	3276	0.03	-15.46	0
70	SLE FR 6	-325	0	3453	0.04	-16.73	0
70	SLE QP 1	-262	0	3010	0.03	-13.55	0
70	SLE QP 2	-300	0	3276	0.03	-15.46	0
70	SLD 1	-13	10	3111	-15.16	-1.27	-0.01
70	SLD 2	-13	10	3111	-15.16	-1.27	-0.01
70	SLD 3	-18	-14	3116	19.53	-1.03	0.01
70	SLD 4	-18	-14	3116	19.53	-1.03	0.01
70	SLD 5	-206	40	3219	-57.13	-11.56	-0.03
70	SLD 6	-206	40	3219	-57.13	-11.56	-0.03
70	SLD 7	-223	-41	3235	58.49	-10.77	0.03
70	SLD 8	-223	-41	3235	58.49	-10.77	0.03
70	SLD 9	-377	41	3316	-58.42	-20.15	-0.03
70	SLD 10	-377	41	3316	-58.42	-20.15	-0.03
70	SLD 11	-393	-40	3333	57.2	-19.36	0.03
70	SLD 12	-393	-40	3333	57.2	-19.36	0.03



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
70	SLD 13	-581	14	3435	-19.46	-29.89	-0.01
70	SLD 14	-581	14	3435	-19.46	-29.89	-0.01
70	SLD 15	-586	-10	3440	15.22	-29.65	0.01
70	SLD 16	-586	-10	3440	15.22	-29.65	0.01
70	SLV 1	372	27	2890	-42.25	17.79	-0.02
70	SLV 2	372	27	2890	-42.25	17.79	-0.02
70	SLV 3	360	-38	2902	53.18	18.34	0.03
70	SLV 4	360	-38	2902	53.18	18.34	0.03
70	SLV 5	-81	106	3141	-157.39	-6.33	-0.08
70	SLV 6	-81	106	3141	-157.39	-6.33	-0.08
70	SLV 7	-119	-110	3182	160.71	-4.48	0.08
70	SLV 8	-119	-110	3182	160.71	-4.48	0.08
70	SLV 9	-480	110	3369	-160.64	-26.44	-0.08
70	SLV 10	-480	110	3369	-160.64	-26.44	-0.08
70	SLV 11	-518	-106	3410	157.46	-24.59	0.08
70	SLV 12	-518	-106	3410	157.46	-24.59	0.08
70	SLV 13	-960	38	3649	-53.11	-49.26	-0.03
70	SLV 14	-960	38	3649	-53.11	-49.26	-0.03
70	SLV 15	-971	-27	3661	42.32	-48.71	0.02
70	SLV 16	-971	-27	3661	42.32	-48.71	0.02
71	SLU 1	-177	0	2763	0.02	-8.73	0
71	SLU 2	-177	0	2763	0.02	-8.73	0
71	SLU 3	-177	0	2763	0.02	-8.73	0
71	SLU 4	-177	0	2763	0.02	-8.73	0
71	SLU 5	-177	0	2763	0.02	-8.73	0
71	SLU 6	-177	0	2763	0.02	-8.73	0
71	SLU 7	-177	0	2763	0.02	-8.73	0
71	SLU 8	-177	0	2763	0.02	-8.73	0
71	SLU 9	-177	0	2763	0.02	-8.73	0
71	SLU 10	-285	0	3650	0.03	-14.03	0
71	SLU 11	-285	0	3650	0.03	-14.03	0
71	SLU 12	-285	0	3650	0.03	-14.03	0
71	SLU 13	-285	0	3650	0.03	-14.03	0
71	SLU 14	-285	0	3650	0.03	-14.03	0
71	SLU 15	-285	0	3650	0.03	-14.03	0
71	SLU 16	-285	0	3650	0.03	-14.03	0
71	SLU 17	-285	0	3650	0.03	-14.03	0
71	SLU 18	-332	0	4030	0.03	-16.3	0
71	SLU 19	-332	0	4030	0.03	-16.3	0
71	SLU 20	-332	0	4030	0.03	-16.3	0
71	SLU 21	-332	0	4030	0.03	-16.3	0
71	SLU 22	-232	0	3274	0.03	-11.42	0
71	SLU 23	-232	0	3274	0.03	-11.42	0
71	SLU 24	-232	0	3274	0.03	-11.42	0
71	SLU 25	-232	0	3274	0.03	-11.42	0
71	SLU 26	-232	0	3274	0.03	-11.42	0
71	SLU 27	-232	0	3274	0.03	-11.42	0
71	SLU 28	-232	0	3274	0.03	-11.42	0
71	SLU 29	-232	0	3274	0.03	-11.42	0
71	SLU 30	-232	0	3274	0.03	-11.42	0
71	SLU 31	-340	0	4162	0.04	-16.72	0
71	SLU 32	-340	0	4162	0.04	-16.72	0
71	SLU 33	-340	0	4162	0.04	-16.72	0
71	SLU 34	-340	0	4162	0.04	-16.72	0
71	SLU 35	-340	0	4162	0.04	-16.72	0
71	SLU 36	-340	0	4162	0.04	-16.72	0
71	SLU 37	-340	0	4162	0.04	-16.72	0
71	SLU 38	-340	0	4162	0.04	-16.72	0
71	SLU 39	-387	0	4542	0.04	-18.99	0
71	SLU 40	-387	0	4542	0.04	-18.99	0
71	SLU 41	-387	0	4542	0.04	-18.99	0
71	SLU 42	-387	0	4542	0.04	-18.99	0
71	SLU 43	-211	0	3416	0.02	-10.43	0
71	SLU 44	-211	0	3416	0.02	-10.43	0
71	SLU 45	-211	0	3416	0.02	-10.43	0
71	SLU 46	-211	0	3416	0.02	-10.43	0
71	SLU 47	-211	0	3416	0.02	-10.43	0
71	SLU 48	-211	0	3416	0.02	-10.43	0
71	SLU 49	-211	0	3416	0.02	-10.43	0
71	SLU 50	-211	0	3416	0.02	-10.43	0
71	SLU 51	-211	0	3416	0.02	-10.43	0
71	SLU 52	-320	0	4303	0.03	-15.73	0
71	SLU 53	-320	0	4303	0.03	-15.73	0
71	SLU 54	-320	0	4303	0.03	-15.73	0
71	SLU 55	-320	0	4303	0.03	-15.73	0
71	SLU 56	-320	0	4303	0.03	-15.73	0
71	SLU 57	-320	0	4303	0.03	-15.73	0
71	SLU 58	-320	0	4303	0.03	-15.73	0
71	SLU 59	-320	0	4303	0.03	-15.73	0
71	SLU 60	-366	0	4684	0.04	-18	0
71	SLU 61	-366	0	4684	0.04	-18	0
71	SLU 62	-366	0	4684	0.04	-18	0
71	SLU 63	-366	0	4684	0.04	-18	0
71	SLU 64	-266	0	3928	0.03	-13.12	0
71	SLU 65	-266	0	3928	0.03	-13.12	0
71	SLU 66	-266	0	3928	0.03	-13.12	0
71	SLU 67	-266	0	3928	0.03	-13.12	0
71	SLU 68	-266	0	3928	0.03	-13.12	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
71	SLU 69	-266	0	3928	0.03	-13.12	0
71	SLU 70	-266	0	3928	0.03	-13.12	0
71	SLU 71	-266	0	3928	0.03	-13.12	0
71	SLU 72	-266	0	3928	0.03	-13.12	0
71	SLU 73	-375	0	4815	0.04	-18.42	0
71	SLU 74	-375	0	4815	0.04	-18.42	0
71	SLU 75	-375	0	4815	0.04	-18.42	0
71	SLU 76	-375	0	4815	0.04	-18.42	0
71	SLU 77	-375	0	4815	0.04	-18.42	0
71	SLU 78	-375	0	4815	0.04	-18.42	0
71	SLU 79	-375	0	4815	0.04	-18.42	0
71	SLU 80	-375	0	4815	0.04	-18.42	0
71	SLU 81	-421	0	5195	0.04	-20.69	0
71	SLU 82	-421	0	5195	0.04	-20.69	0
71	SLU 83	-421	0	5195	0.04	-20.69	0
71	SLU 84	-421	0	5195	0.04	-20.69	0
71	SLE RA 1	-193	0	2909	0.02	-9.5	0
71	SLE RA 2	-193	0	2909	0.02	-9.5	0
71	SLE RA 3	-193	0	2909	0.02	-9.5	0
71	SLE RA 4	-193	0	2909	0.02	-9.5	0
71	SLE RA 5	-193	0	2909	0.02	-9.5	0
71	SLE RA 6	-193	0	2909	0.02	-9.5	0
71	SLE RA 7	-193	0	2909	0.02	-9.5	0
71	SLE RA 8	-193	0	2909	0.02	-9.5	0
71	SLE RA 9	-193	0	2909	0.02	-9.5	0
71	SLE RA 10	-265	0	3500	0.03	-13.03	0
71	SLE RA 11	-265	0	3500	0.03	-13.03	0
71	SLE RA 12	-265	0	3500	0.03	-13.03	0
71	SLE RA 13	-265	0	3500	0.03	-13.03	0
71	SLE RA 14	-265	0	3500	0.03	-13.03	0
71	SLE RA 15	-265	0	3500	0.03	-13.03	0
71	SLE RA 16	-265	0	3500	0.03	-13.03	0
71	SLE RA 17	-265	0	3500	0.03	-13.03	0
71	SLE RA 18	-296	0	3754	0.03	-14.55	0
71	SLE RA 19	-296	0	3754	0.03	-14.55	0
71	SLE RA 20	-296	0	3754	0.03	-14.55	0
71	SLE RA 21	-296	0	3754	0.03	-14.55	0
71	SLE FR 1	-193	0	2909	0.02	-9.5	0
71	SLE FR 2	-193	0	2909	0.02	-9.5	0
71	SLE FR 3	-193	0	2909	0.02	-9.5	0
71	SLE FR 4	-224	0	3162	0.03	-11.01	0
71	SLE FR 5	-224	0	3162	0.03	-11.01	0
71	SLE FR 6	-244	0	3331	0.03	-12.02	0
71	SLE QP 1	-193	0	2909	0.02	-9.5	0
71	SLE QP 2	-224	0	3162	0.03	-11.01	0
71	SLD 1	91	10	3099	-17.41	4.7	-0.01
71	SLD 2	91	10	3099	-17.41	4.7	-0.01
71	SLD 3	86	-15	3103	21.68	4.45	0.02
71	SLD 4	86	-15	3103	21.68	4.45	0.02
71	SLD 5	-121	41	3137	-64.49	-5.92	-0.05
71	SLD 6	-121	41	3137	-64.49	-5.92	-0.05
71	SLD 7	-139	-42	3151	65.81	-6.76	0.05
71	SLD 8	-139	-42	3151	65.81	-6.76	0.05
71	SLD 9	-309	42	3174	-65.76	-15.27	-0.05
71	SLD 10	-309	42	3174	-65.76	-15.27	-0.05
71	SLD 11	-326	-41	3188	64.54	-16.11	0.05
71	SLD 12	-326	-41	3188	64.54	-16.11	0.05
71	SLD 13	-533	15	3221	-21.63	-26.48	-0.02
71	SLD 14	-533	15	3221	-21.63	-26.48	-0.02
71	SLD 15	-538	-10	3225	17.46	-26.73	0.01
71	SLD 16	-538	-10	3225	17.46	-26.73	0.01
71	SLV 1	514	28	3014	-48.89	25.84	-0.03
71	SLV 2	514	28	3014	-48.89	25.84	-0.03
71	SLV 3	502	-39	3023	59.66	25.25	0.05
71	SLV 4	502	-39	3023	59.66	25.25	0.05
71	SLV 5	16	110	3103	-179.28	0.94	-0.13
71	SLV 6	16	110	3103	-179.28	0.94	-0.13
71	SLV 7	-25	-113	3136	182.55	-1.04	0.14
71	SLV 8	-25	-113	3136	182.55	-1.04	0.14
71	SLV 9	-423	113	3189	-182.5	-20.99	-0.14
71	SLV 10	-423	113	3189	-182.5	-20.99	-0.14
71	SLV 11	-464	-109	3222	179.33	-22.97	0.13
71	SLV 12	-464	-109	3222	179.33	-22.97	0.13
71	SLV 13	-949	39	3301	-59.61	-47.27	-0.05
71	SLV 14	-949	39	3301	-59.61	-47.27	-0.05
71	SLV 15	-961	-28	3311	48.94	-47.87	0.03
71	SLV 16	-961	-28	3311	48.94	-47.87	0.03
72	SLU 1	-131	0	2683	0.02	-6.94	0
72	SLU 2	-131	0	2683	0.02	-6.94	0
72	SLU 3	-131	0	2683	0.02	-6.94	0
72	SLU 4	-131	0	2683	0.02	-6.94	0
72	SLU 5	-131	0	2683	0.02	-6.94	0
72	SLU 6	-131	0	2683	0.02	-6.94	0
72	SLU 7	-131	0	2683	0.02	-6.94	0
72	SLU 8	-131	0	2683	0.02	-6.94	0
72	SLU 9	-131	0	2683	0.02	-6.94	0
72	SLU 10	-219	0	3540	0.02	-11.39	0
72	SLU 11	-219	0	3540	0.02	-11.39	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
72	SLU 12	-219	0	3540	0.02	-11.39	0
72	SLU 13	-219	0	3540	0.02	-11.39	0
72	SLU 14	-219	0	3540	0.02	-11.39	0
72	SLU 15	-219	0	3540	0.02	-11.39	0
72	SLU 16	-219	0	3540	0.02	-11.39	0
72	SLU 17	-219	0	3540	0.02	-11.39	0
72	SLU 18	-256	0	3908	0.03	-13.3	0
72	SLU 19	-256	0	3908	0.03	-13.3	0
72	SLU 20	-256	0	3908	0.03	-13.3	0
72	SLU 21	-256	0	3908	0.03	-13.3	0
72	SLU 22	-175	0	3179	0.02	-9.19	0
72	SLU 23	-175	0	3179	0.02	-9.19	0
72	SLU 24	-175	0	3179	0.02	-9.19	0
72	SLU 25	-175	0	3179	0.02	-9.19	0
72	SLU 26	-175	0	3179	0.02	-9.19	0
72	SLU 27	-175	0	3179	0.02	-9.19	0
72	SLU 28	-175	0	3179	0.02	-9.19	0
72	SLU 29	-175	0	3179	0.02	-9.19	0
72	SLU 30	-175	0	3179	0.02	-9.19	0
72	SLU 31	-263	0	4036	0.03	-13.64	0
72	SLU 32	-263	0	4036	0.03	-13.64	0
72	SLU 33	-263	0	4036	0.03	-13.64	0
72	SLU 34	-263	0	4036	0.03	-13.64	0
72	SLU 35	-263	0	4036	0.03	-13.64	0
72	SLU 36	-263	0	4036	0.03	-13.64	0
72	SLU 37	-263	0	4036	0.03	-13.64	0
72	SLU 38	-263	0	4036	0.03	-13.64	0
72	SLU 39	-300	0	4404	0.03	-15.55	0
72	SLU 40	-300	0	4404	0.03	-15.55	0
72	SLU 41	-300	0	4404	0.03	-15.55	0
72	SLU 42	-300	0	4404	0.03	-15.55	0
72	SLU 43	-155	0	3318	0.02	-8.25	0
72	SLU 44	-155	0	3318	0.02	-8.25	0
72	SLU 45	-155	0	3318	0.02	-8.25	0
72	SLU 46	-155	0	3318	0.02	-8.25	0
72	SLU 47	-155	0	3318	0.02	-8.25	0
72	SLU 48	-155	0	3318	0.02	-8.25	0
72	SLU 49	-155	0	3318	0.02	-8.25	0
72	SLU 50	-155	0	3318	0.02	-8.25	0
72	SLU 51	-155	0	3318	0.02	-8.25	0
72	SLU 52	-243	0	4175	0.03	-12.7	0
72	SLU 53	-243	0	4175	0.03	-12.7	0
72	SLU 54	-243	0	4175	0.03	-12.7	0
72	SLU 55	-243	0	4175	0.03	-12.7	0
72	SLU 56	-243	0	4175	0.03	-12.7	0
72	SLU 57	-243	0	4175	0.03	-12.7	0
72	SLU 58	-243	0	4175	0.03	-12.7	0
72	SLU 59	-243	0	4175	0.03	-12.7	0
72	SLU 60	-280	0	4542	0.03	-14.61	0
72	SLU 61	-280	0	4542	0.03	-14.61	0
72	SLU 62	-280	0	4542	0.03	-14.61	0
72	SLU 63	-280	0	4542	0.03	-14.61	0
72	SLU 64	-199	0	3814	0.02	-10.5	0
72	SLU 65	-199	0	3814	0.02	-10.5	0
72	SLU 66	-199	0	3814	0.02	-10.5	0
72	SLU 67	-199	0	3814	0.02	-10.5	0
72	SLU 68	-199	0	3814	0.02	-10.5	0
72	SLU 69	-199	0	3814	0.02	-10.5	0
72	SLU 70	-199	0	3814	0.02	-10.5	0
72	SLU 71	-199	0	3814	0.02	-10.5	0
72	SLU 72	-199	0	3814	0.02	-10.5	0
72	SLU 73	-287	0	4671	0.03	-14.95	0
72	SLU 74	-287	0	4671	0.03	-14.95	0
72	SLU 75	-287	0	4671	0.03	-14.95	0
72	SLU 76	-287	0	4671	0.03	-14.95	0
72	SLU 77	-287	0	4671	0.03	-14.95	0
72	SLU 78	-287	0	4671	0.03	-14.95	0
72	SLU 79	-287	0	4671	0.03	-14.95	0
72	SLU 80	-287	0	4671	0.03	-14.95	0
72	SLU 81	-325	0	5039	0.03	-16.86	0
72	SLU 82	-325	0	5039	0.03	-16.86	0
72	SLU 83	-325	0	5039	0.03	-16.86	0
72	SLU 84	-325	0	5039	0.03	-16.86	0
72	SLE RA 1	-144	0	2825	0.02	-7.58	0
72	SLE RA 2	-144	0	2825	0.02	-7.58	0
72	SLE RA 3	-144	0	2825	0.02	-7.58	0
72	SLE RA 4	-144	0	2825	0.02	-7.58	0
72	SLE RA 5	-144	0	2825	0.02	-7.58	0
72	SLE RA 6	-144	0	2825	0.02	-7.58	0
72	SLE RA 7	-144	0	2825	0.02	-7.58	0
72	SLE RA 8	-144	0	2825	0.02	-7.58	0
72	SLE RA 9	-144	0	2825	0.02	-7.58	0
72	SLE RA 10	-202	0	3396	0.02	-10.55	0
72	SLE RA 11	-202	0	3396	0.02	-10.55	0
72	SLE RA 12	-202	0	3396	0.02	-10.55	0
72	SLE RA 13	-202	0	3396	0.02	-10.55	0
72	SLE RA 14	-202	0	3396	0.02	-10.55	0
72	SLE RA 15	-202	0	3396	0.02	-10.55	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
72	SLE RA 16	-202	0	3396	0.02	-10.55	0
72	SLE RA 17	-202	0	3396	0.02	-10.55	0
72	SLE RA 18	-227	0	3641	0.02	-11.82	0
72	SLE RA 19	-227	0	3641	0.02	-11.82	0
72	SLE RA 20	-227	0	3641	0.02	-11.82	0
72	SLE RA 21	-227	0	3641	0.02	-11.82	0
72	SLE FR 1	-144	0	2825	0.02	-7.58	0
72	SLE FR 2	-144	0	2825	0.02	-7.58	0
72	SLE FR 3	-144	0	2825	0.02	-7.58	0
72	SLE FR 4	-169	0	3070	0.02	-8.85	0
72	SLE FR 5	-169	0	3070	0.02	-8.85	0
72	SLE FR 6	-185	0	3233	0.02	-9.7	0
72	SLE QP 1	-144	0	2825	0.02	-7.58	0
72	SLE QP 2	-169	0	3070	0.02	-8.85	0
72	SLD 1	167	11	3157	-19.57	7.55	-0.02
72	SLD 2	167	11	3157	-19.57	7.55	-0.02
72	SLD 3	161	-15	3160	23.65	7.29	0.02
72	SLD 4	161	-15	3160	23.65	7.29	0.02
72	SLD 5	-60	41	3091	-71.4	-3.54	-0.07
72	SLD 6	-60	41	3091	-71.4	-3.54	-0.07
72	SLD 7	-78	-43	3102	72.65	-4.41	0.07
72	SLD 8	-78	-43	3102	72.65	-4.41	0.07
72	SLD 9	-260	43	3037	-72.61	-13.3	-0.07
72	SLD 10	-260	43	3037	-72.61	-13.3	-0.07
72	SLD 11	-278	-41	3049	71.44	-14.17	0.07
72	SLD 12	-278	-41	3049	71.44	-14.17	0.07
72	SLD 13	-499	15	2979	-23.61	-24.99	-0.02
72	SLD 14	-499	15	2979	-23.61	-24.99	-0.02
72	SLD 15	-504	-11	2983	19.6	-25.25	0.02
72	SLD 16	-504	-11	2983	19.6	-25.25	0.02
72	SLV 1	618	29	3274	-55.22	29.59	-0.05
72	SLV 2	618	29	3274	-55.22	29.59	-0.05
72	SLV 3	605	-39	3283	65.58	28.97	0.06
72	SLV 4	605	-39	3283	65.58	28.97	0.06
72	SLV 5	86	113	3118	-199.76	3.61	-0.18
72	SLV 6	86	113	3118	-199.76	3.61	-0.18
72	SLV 7	44	-116	3147	202.89	1.56	0.19
72	SLV 8	44	-116	3147	202.89	1.56	0.19
72	SLV 9	-382	116	2993	-202.86	-19.27	-0.19
72	SLV 10	-382	116	2993	-202.86	-19.27	-0.19
72	SLV 11	-424	-113	3022	199.8	-21.31	0.18
72	SLV 12	-424	-113	3022	199.8	-21.31	0.18
72	SLV 13	-943	39	2857	-65.54	-46.68	-0.06
72	SLV 14	-943	39	2857	-65.54	-46.68	-0.06
72	SLV 15	-956	-29	2866	55.26	-47.29	0.05
72	SLV 16	-956	-29	2866	55.26	-47.29	0.05
73	SLU 1	-86	0	2612	0.01	-4.36	0
73	SLU 2	-86	0	2612	0.01	-4.36	0
73	SLU 3	-86	0	2612	0.01	-4.36	0
73	SLU 4	-86	0	2612	0.01	-4.36	0
73	SLU 5	-86	0	2612	0.01	-4.36	0
73	SLU 6	-86	0	2612	0.01	-4.36	0
73	SLU 7	-86	0	2612	0.01	-4.36	0
73	SLU 8	-86	0	2612	0.01	-4.36	0
73	SLU 9	-86	0	2612	0.01	-4.36	0
73	SLU 10	-148	0	3442	0.02	-7.41	0
73	SLU 11	-148	0	3442	0.02	-7.41	0
73	SLU 12	-148	0	3442	0.02	-7.41	0
73	SLU 13	-148	0	3442	0.02	-7.41	0
73	SLU 14	-148	0	3442	0.02	-7.41	0
73	SLU 15	-148	0	3442	0.02	-7.41	0
73	SLU 16	-148	0	3442	0.02	-7.41	0
73	SLU 17	-148	0	3442	0.02	-7.41	0
73	SLU 18	-175	0	3797	0.02	-8.72	0
73	SLU 19	-175	0	3797	0.02	-8.72	0
73	SLU 20	-175	0	3797	0.02	-8.72	0
73	SLU 21	-175	0	3797	0.02	-8.72	0
73	SLU 22	-118	0	3094	0.01	-5.9	0
73	SLU 23	-118	0	3094	0.01	-5.9	0
73	SLU 24	-118	0	3094	0.01	-5.9	0
73	SLU 25	-118	0	3094	0.01	-5.9	0
73	SLU 26	-118	0	3094	0.01	-5.9	0
73	SLU 27	-118	0	3094	0.01	-5.9	0
73	SLU 28	-118	0	3094	0.01	-5.9	0
73	SLU 29	-118	0	3094	0.01	-5.9	0
73	SLU 30	-118	0	3094	0.01	-5.9	0
73	SLU 31	-180	0	3924	0.02	-8.95	0
73	SLU 32	-180	0	3924	0.02	-8.95	0
73	SLU 33	-180	0	3924	0.02	-8.95	0
73	SLU 34	-180	0	3924	0.02	-8.95	0
73	SLU 35	-180	0	3924	0.02	-8.95	0
73	SLU 36	-180	0	3924	0.02	-8.95	0
73	SLU 37	-180	0	3924	0.02	-8.95	0
73	SLU 38	-180	0	3924	0.02	-8.95	0
73	SLU 39	-206	0	4279	0.02	-10.26	0
73	SLU 40	-206	0	4279	0.02	-10.26	0
73	SLU 41	-206	0	4279	0.02	-10.26	0
73	SLU 42	-206	0	4279	0.02	-10.26	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
73	SLU 43	-101	0	3230	0.01	-5.14	0
73	SLU 44	-101	0	3230	0.01	-5.14	0
73	SLU 45	-101	0	3230	0.01	-5.14	0
73	SLU 46	-101	0	3230	0.01	-5.14	0
73	SLU 47	-101	0	3230	0.01	-5.14	0
73	SLU 48	-101	0	3230	0.01	-5.14	0
73	SLU 49	-101	0	3230	0.01	-5.14	0
73	SLU 50	-101	0	3230	0.01	-5.14	0
73	SLU 51	-101	0	3230	0.01	-5.14	0
73	SLU 52	-163	0	4060	0.02	-8.19	0
73	SLU 53	-163	0	4060	0.02	-8.19	0
73	SLU 54	-163	0	4060	0.02	-8.19	0
73	SLU 55	-163	0	4060	0.02	-8.19	0
73	SLU 56	-163	0	4060	0.02	-8.19	0
73	SLU 57	-163	0	4060	0.02	-8.19	0
73	SLU 58	-163	0	4060	0.02	-8.19	0
73	SLU 59	-163	0	4060	0.02	-8.19	0
73	SLU 60	-190	0	4415	0.02	-9.5	0
73	SLU 61	-190	0	4415	0.02	-9.5	0
73	SLU 62	-190	0	4415	0.02	-9.5	0
73	SLU 63	-190	0	4415	0.02	-9.5	0
73	SLU 64	-133	0	3713	0.02	-6.68	0
73	SLU 65	-133	0	3713	0.02	-6.68	0
73	SLU 66	-133	0	3713	0.02	-6.68	0
73	SLU 67	-133	0	3713	0.02	-6.68	0
73	SLU 68	-133	0	3713	0.02	-6.68	0
73	SLU 69	-133	0	3713	0.02	-6.68	0
73	SLU 70	-133	0	3713	0.02	-6.68	0
73	SLU 71	-133	0	3713	0.02	-6.68	0
73	SLU 72	-133	0	3713	0.02	-6.68	0
73	SLU 73	-195	0	4542	0.02	-9.73	0
73	SLU 74	-195	0	4542	0.02	-9.73	0
73	SLU 75	-195	0	4542	0.02	-9.73	0
73	SLU 76	-195	0	4542	0.02	-9.73	0
73	SLU 77	-195	0	4542	0.02	-9.73	0
73	SLU 78	-195	0	4542	0.02	-9.73	0
73	SLU 79	-195	0	4542	0.02	-9.73	0
73	SLU 80	-195	0	4542	0.02	-9.73	0
73	SLU 81	-222	0	4898	0.02	-11.04	0
73	SLU 82	-222	0	4898	0.02	-11.04	0
73	SLU 83	-222	0	4898	0.02	-11.04	0
73	SLU 84	-222	0	4898	0.02	-11.04	0
73	SLE RA 1	-95	0	2750	0.01	-4.8	0
73	SLE RA 2	-95	0	2750	0.01	-4.8	0
73	SLE RA 3	-95	0	2750	0.01	-4.8	0
73	SLE RA 4	-95	0	2750	0.01	-4.8	0
73	SLE RA 5	-95	0	2750	0.01	-4.8	0
73	SLE RA 6	-95	0	2750	0.01	-4.8	0
73	SLE RA 7	-95	0	2750	0.01	-4.8	0
73	SLE RA 8	-95	0	2750	0.01	-4.8	0
73	SLE RA 9	-95	0	2750	0.01	-4.8	0
73	SLE RA 10	-137	0	3303	0.02	-6.84	0
73	SLE RA 11	-137	0	3303	0.02	-6.84	0
73	SLE RA 12	-137	0	3303	0.02	-6.84	0
73	SLE RA 13	-137	0	3303	0.02	-6.84	0
73	SLE RA 14	-137	0	3303	0.02	-6.84	0
73	SLE RA 15	-137	0	3303	0.02	-6.84	0
73	SLE RA 16	-137	0	3303	0.02	-6.84	0
73	SLE RA 17	-137	0	3303	0.02	-6.84	0
73	SLE RA 18	-154	0	3540	0.02	-7.71	0
73	SLE RA 19	-154	0	3540	0.02	-7.71	0
73	SLE RA 20	-154	0	3540	0.02	-7.71	0
73	SLE RA 21	-154	0	3540	0.02	-7.71	0
73	SLE FR 1	-95	0	2750	0.01	-4.8	0
73	SLE FR 2	-95	0	2750	0.01	-4.8	0
73	SLE FR 3	-95	0	2750	0.01	-4.8	0
73	SLE FR 4	-113	0	2987	0.01	-5.67	0
73	SLE FR 5	-113	0	2987	0.01	-5.67	0
73	SLE FR 6	-125	0	3145	0.01	-6.25	0
73	SLE QP 1	-95	0	2750	0.01	-4.8	0
73	SLE QP 2	-113	0	2987	0.01	-5.67	0
73	SLD 1	241	11	3126	-21.81	11.49	-0.02
73	SLD 2	241	11	3126	-21.81	11.49	-0.02
73	SLD 3	235	-15	3129	25.73	11.24	0.03
73	SLD 4	235	-15	3129	25.73	11.24	0.03
73	SLD 5	1	43	3024	-78.62	-0.13	-0.09
73	SLD 6	1	43	3024	-78.62	-0.13	-0.09
73	SLD 7	-17	-45	3034	79.82	-0.99	0.09
73	SLD 8	-17	-45	3034	79.82	-0.99	0.09
73	SLD 9	-209	45	2939	-79.79	-10.36	-0.09
73	SLD 10	-209	45	2939	-79.79	-10.36	-0.09
73	SLD 11	-227	-43	2950	78.65	-11.21	0.09
73	SLD 12	-227	-43	2950	78.65	-11.21	0.09
73	SLD 13	-461	15	2845	-25.7	-22.58	-0.03
73	SLD 14	-461	15	2845	-25.7	-22.58	-0.03
73	SLD 15	-467	-11	2848	21.83	-22.84	0.02
73	SLD 16	-467	-11	2848	21.83	-22.84	0.02
73	SLV 1	716	32	3312	-61.78	34.58	-0.06



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
73	SLV 2	716	32	3312	-61.78	34.58	-0.06
73	SLV 3	704	-41	3319	71.7	33.97	0.09
73	SLV 4	704	-41	3319	71.7	33.97	0.09
73	SLV 5	155	120	3073	-220.97	7.32	-0.25
73	SLV 6	155	120	3073	-220.97	7.32	-0.25
73	SLV 7	113	-123	3098	223.97	5.3	0.25
73	SLV 8	113	-123	3098	223.97	5.3	0.25
73	SLV 9	-339	123	2875	-223.94	-16.65	-0.25
73	SLV 10	-339	123	2875	-223.94	-16.65	-0.25
73	SLV 11	-381	-120	2901	221	-18.66	0.25
73	SLV 12	-381	-120	2901	221	-18.66	0.25
73	SLV 13	-929	41	2654	-71.68	-45.32	-0.09
73	SLV 14	-929	41	2654	-71.68	-45.32	-0.09
73	SLV 15	-942	-32	2662	61.81	-45.92	0.06
73	SLV 16	-942	-32	2662	61.81	-45.92	0.06
74	SLU 1	-53	0	2543	0.01	-3.12	0
74	SLU 2	-53	0	2543	0.01	-3.12	0
74	SLU 3	-53	0	2543	0.01	-3.12	0
74	SLU 4	-53	0	2543	0.01	-3.12	0
74	SLU 5	-53	0	2543	0.01	-3.12	0
74	SLU 6	-53	0	2543	0.01	-3.12	0
74	SLU 7	-53	0	2543	0.01	-3.12	0
74	SLU 8	-53	0	2543	0.01	-3.12	0
74	SLU 9	-53	0	2543	0.01	-3.12	0
74	SLU 10	-93	0	3344	0.01	-5.33	0
74	SLU 11	-93	0	3344	0.01	-5.33	0
74	SLU 12	-93	0	3344	0.01	-5.33	0
74	SLU 13	-93	0	3344	0.01	-5.33	0
74	SLU 14	-93	0	3344	0.01	-5.33	0
74	SLU 15	-93	0	3344	0.01	-5.33	0
74	SLU 16	-93	0	3344	0.01	-5.33	0
74	SLU 17	-93	0	3344	0.01	-5.33	0
74	SLU 18	-111	0	3687	0.01	-6.27	0
74	SLU 19	-111	0	3687	0.01	-6.27	0
74	SLU 20	-111	0	3687	0.01	-6.27	0
74	SLU 21	-111	0	3687	0.01	-6.27	0
74	SLU 22	-74	0	3011	0.01	-4.25	0
74	SLU 23	-74	0	3011	0.01	-4.25	0
74	SLU 24	-74	0	3011	0.01	-4.25	0
74	SLU 25	-74	0	3011	0.01	-4.25	0
74	SLU 26	-74	0	3011	0.01	-4.25	0
74	SLU 27	-74	0	3011	0.01	-4.25	0
74	SLU 28	-74	0	3011	0.01	-4.25	0
74	SLU 29	-74	0	3011	0.01	-4.25	0
74	SLU 30	-74	0	3011	0.01	-4.25	0
74	SLU 31	-114	0	3812	0.01	-6.46	0
74	SLU 32	-114	0	3812	0.01	-6.46	0
74	SLU 33	-114	0	3812	0.01	-6.46	0
74	SLU 34	-114	0	3812	0.01	-6.46	0
74	SLU 35	-114	0	3812	0.01	-6.46	0
74	SLU 36	-114	0	3812	0.01	-6.46	0
74	SLU 37	-114	0	3812	0.01	-6.46	0
74	SLU 38	-114	0	3812	0.01	-6.46	0
74	SLU 39	-131	0	4155	0.02	-7.4	0
74	SLU 40	-131	0	4155	0.02	-7.4	0
74	SLU 41	-131	0	4155	0.02	-7.4	0
74	SLU 42	-131	0	4155	0.02	-7.4	0
74	SLU 43	-62	0	3146	0.01	-3.67	0
74	SLU 44	-62	0	3146	0.01	-3.67	0
74	SLU 45	-62	0	3146	0.01	-3.67	0
74	SLU 46	-62	0	3146	0.01	-3.67	0
74	SLU 47	-62	0	3146	0.01	-3.67	0
74	SLU 48	-62	0	3146	0.01	-3.67	0
74	SLU 49	-62	0	3146	0.01	-3.67	0
74	SLU 50	-62	0	3146	0.01	-3.67	0
74	SLU 51	-62	0	3146	0.01	-3.67	0
74	SLU 52	-102	0	3947	0.01	-5.88	0
74	SLU 53	-102	0	3947	0.01	-5.88	0
74	SLU 54	-102	0	3947	0.01	-5.88	0
74	SLU 55	-102	0	3947	0.01	-5.88	0
74	SLU 56	-102	0	3947	0.01	-5.88	0
74	SLU 57	-102	0	3947	0.01	-5.88	0
74	SLU 58	-102	0	3947	0.01	-5.88	0
74	SLU 59	-102	0	3947	0.01	-5.88	0
74	SLU 60	-119	0	4290	0.02	-6.82	0
74	SLU 61	-119	0	4290	0.02	-6.82	0
74	SLU 62	-119	0	4290	0.02	-6.82	0
74	SLU 63	-119	0	4290	0.02	-6.82	0
74	SLU 64	-82	0	3614	0.01	-4.79	0
74	SLU 65	-82	0	3614	0.01	-4.79	0
74	SLU 66	-82	0	3614	0.01	-4.79	0
74	SLU 67	-82	0	3614	0.01	-4.79	0
74	SLU 68	-82	0	3614	0.01	-4.79	0
74	SLU 69	-82	0	3614	0.01	-4.79	0
74	SLU 70	-82	0	3614	0.01	-4.79	0
74	SLU 71	-82	0	3614	0.01	-4.79	0
74	SLU 72	-82	0	3614	0.01	-4.79	0
74	SLU 73	-123	0	4414	0.02	-7	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
74	SLU 74	-123	0	4414	0.02	-7	0
74	SLU 75	-123	0	4414	0.02	-7	0
74	SLU 76	-123	0	4414	0.02	-7	0
74	SLU 77	-123	0	4414	0.02	-7	0
74	SLU 78	-123	0	4414	0.02	-7	0
74	SLU 79	-123	0	4414	0.02	-7	0
74	SLU 80	-123	0	4414	0.02	-7	0
74	SLU 81	-140	0	4757	0.02	-7.95	0
74	SLU 82	-140	0	4757	0.02	-7.95	0
74	SLU 83	-140	0	4757	0.02	-7.95	0
74	SLU 84	-140	0	4757	0.02	-7.95	0
74	SLE RA 1	-59	0	2677	0.01	-3.44	0
74	SLE RA 2	-59	0	2677	0.01	-3.44	0
74	SLE RA 3	-59	0	2677	0.01	-3.44	0
74	SLE RA 4	-59	0	2677	0.01	-3.44	0
74	SLE RA 5	-59	0	2677	0.01	-3.44	0
74	SLE RA 6	-59	0	2677	0.01	-3.44	0
74	SLE RA 7	-59	0	2677	0.01	-3.44	0
74	SLE RA 8	-59	0	2677	0.01	-3.44	0
74	SLE RA 9	-59	0	2677	0.01	-3.44	0
74	SLE RA 10	-86	0	3211	0.01	-4.91	0
74	SLE RA 11	-86	0	3211	0.01	-4.91	0
74	SLE RA 12	-86	0	3211	0.01	-4.91	0
74	SLE RA 13	-86	0	3211	0.01	-4.91	0
74	SLE RA 14	-86	0	3211	0.01	-4.91	0
74	SLE RA 15	-86	0	3211	0.01	-4.91	0
74	SLE RA 16	-86	0	3211	0.01	-4.91	0
74	SLE RA 17	-86	0	3211	0.01	-4.91	0
74	SLE RA 18	-97	0	3439	0.01	-5.54	0
74	SLE RA 19	-97	0	3439	0.01	-5.54	0
74	SLE RA 20	-97	0	3439	0.01	-5.54	0
74	SLE RA 21	-97	0	3439	0.01	-5.54	0
74	SLE FR 1	-59	0	2677	0.01	-3.44	0
74	SLE FR 2	-59	0	2677	0.01	-3.44	0
74	SLE FR 3	-59	0	2677	0.01	-3.44	0
74	SLE FR 4	-70	0	2906	0.01	-4.07	0
74	SLE FR 5	-70	0	2906	0.01	-4.07	0
74	SLE FR 6	-78	0	3058	0.01	-4.49	0
74	SLE QP 1	-59	0	2677	0.01	-3.44	0
74	SLE QP 2	-70	0	2906	0.01	-4.07	0
74	SLD 1	302	13	3077	-24.28	13.87	-0.03
74	SLD 2	302	13	3077	-24.28	13.87	-0.03
74	SLD 3	297	-17	3080	28.06	13.61	0.04
74	SLD 4	297	-17	3080	28.06	13.61	0.04
74	SLD 5	50	48	2952	-86.66	1.71	-0.12
74	SLD 6	50	48	2952	-86.66	1.71	-0.12
74	SLD 7	32	-49	2963	87.81	0.83	0.12
74	SLD 8	32	-49	2963	87.81	0.83	0.12
74	SLD 9	-172	49	2849	-87.79	-8.98	-0.12
74	SLD 10	-172	49	2849	-87.79	-8.98	-0.12
74	SLD 11	-190	-48	2859	86.68	-9.85	0.12
74	SLD 12	-190	-48	2859	86.68	-9.85	0.12
74	SLD 13	-437	17	2731	-28.04	-21.75	-0.04
74	SLD 14	-437	17	2731	-28.04	-21.75	-0.04
74	SLD 15	-443	-13	2734	24.3	-22.01	0.03
74	SLD 16	-443	-13	2734	24.3	-22.01	0.03
74	SLV 1	802	36	3306	-68.96	37.96	-0.09
74	SLV 2	802	36	3306	-68.96	37.96	-0.09
74	SLV 3	789	-46	3314	78.45	37.35	0.11
74	SLV 4	789	-46	3314	78.45	37.35	0.11
74	SLV 5	211	134	3015	-244.26	9.47	-0.34
74	SLV 6	211	134	3015	-244.26	9.47	-0.34
74	SLV 7	168	-137	3039	247.12	7.42	0.35
74	SLV 8	168	-137	3039	247.12	7.42	0.35
74	SLV 9	-309	137	2772	-247.1	-15.56	-0.35
74	SLV 10	-309	137	2772	-247.1	-15.56	-0.35
74	SLV 11	-351	-134	2797	244.28	-17.62	0.34
74	SLV 12	-351	-134	2797	244.28	-17.62	0.34
74	SLV 13	-930	46	2498	-78.43	-45.49	-0.11
74	SLV 14	-930	46	2498	-78.43	-45.49	-0.11
74	SLV 15	-943	-36	2505	68.98	-46.1	0.09
74	SLV 16	-943	-36	2505	68.98	-46.1	0.09
75	SLU 1	-22	0	2477	0.01	-1.32	0
75	SLU 2	-22	0	2477	0.01	-1.32	0
75	SLU 3	-22	0	2477	0.01	-1.32	0
75	SLU 4	-22	0	2477	0.01	-1.32	0
75	SLU 5	-22	0	2477	0.01	-1.32	0
75	SLU 6	-22	0	2477	0.01	-1.32	0
75	SLU 7	-22	0	2477	0.01	-1.32	0
75	SLU 8	-22	0	2477	0.01	-1.32	0
75	SLU 9	-22	0	2477	0.01	-1.32	0
75	SLU 10	-41	0	3246	0.01	-2.33	0
75	SLU 11	-41	0	3246	0.01	-2.33	0
75	SLU 12	-41	0	3246	0.01	-2.33	0
75	SLU 13	-41	0	3246	0.01	-2.33	0
75	SLU 14	-41	0	3246	0.01	-2.33	0
75	SLU 15	-41	0	3246	0.01	-2.33	0
75	SLU 16	-41	0	3246	0.01	-2.33	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
75	SLU 17	-41	0	3246	0.01	-2.33	0
75	SLU 18	-49	0	3575	0.01	-2.76	0
75	SLU 19	-49	0	3575	0.01	-2.76	0
75	SLU 20	-49	0	3575	0.01	-2.76	0
75	SLU 21	-49	0	3575	0.01	-2.76	0
75	SLU 22	-32	0	2929	0.01	-1.85	0
75	SLU 23	-32	0	2929	0.01	-1.85	0
75	SLU 24	-32	0	2929	0.01	-1.85	0
75	SLU 25	-32	0	2929	0.01	-1.85	0
75	SLU 26	-32	0	2929	0.01	-1.85	0
75	SLU 27	-32	0	2929	0.01	-1.85	0
75	SLU 28	-32	0	2929	0.01	-1.85	0
75	SLU 29	-32	0	2929	0.01	-1.85	0
75	SLU 30	-32	0	2929	0.01	-1.85	0
75	SLU 31	-51	0	3698	0.01	-2.86	0
75	SLU 32	-51	0	3698	0.01	-2.86	0
75	SLU 33	-51	0	3698	0.01	-2.86	0
75	SLU 34	-51	0	3698	0.01	-2.86	0
75	SLU 35	-51	0	3698	0.01	-2.86	0
75	SLU 36	-51	0	3698	0.01	-2.86	0
75	SLU 37	-51	0	3698	0.01	-2.86	0
75	SLU 38	-51	0	3698	0.01	-2.86	0
75	SLU 39	-59	0	4027	0.01	-3.29	0
75	SLU 40	-59	0	4027	0.01	-3.29	0
75	SLU 41	-59	0	4027	0.01	-3.29	0
75	SLU 42	-59	0	4027	0.01	-3.29	0
75	SLU 43	-25	0	3065	0.01	-1.53	0
75	SLU 44	-25	0	3065	0.01	-1.53	0
75	SLU 45	-25	0	3065	0.01	-1.53	0
75	SLU 46	-25	0	3065	0.01	-1.53	0
75	SLU 47	-25	0	3065	0.01	-1.53	0
75	SLU 48	-25	0	3065	0.01	-1.53	0
75	SLU 49	-25	0	3065	0.01	-1.53	0
75	SLU 50	-25	0	3065	0.01	-1.53	0
75	SLU 51	-25	0	3065	0.01	-1.53	0
75	SLU 52	-44	0	3834	0.01	-2.54	0
75	SLU 53	-44	0	3834	0.01	-2.54	0
75	SLU 54	-44	0	3834	0.01	-2.54	0
75	SLU 55	-44	0	3834	0.01	-2.54	0
75	SLU 56	-44	0	3834	0.01	-2.54	0
75	SLU 57	-44	0	3834	0.01	-2.54	0
75	SLU 58	-44	0	3834	0.01	-2.54	0
75	SLU 59	-44	0	3834	0.01	-2.54	0
75	SLU 60	-52	0	4163	0.01	-2.97	0
75	SLU 61	-52	0	4163	0.01	-2.97	0
75	SLU 62	-52	0	4163	0.01	-2.97	0
75	SLU 63	-52	0	4163	0.01	-2.97	0
75	SLU 64	-35	0	3517	0.01	-2.06	0
75	SLU 65	-35	0	3517	0.01	-2.06	0
75	SLU 66	-35	0	3517	0.01	-2.06	0
75	SLU 67	-35	0	3517	0.01	-2.06	0
75	SLU 68	-35	0	3517	0.01	-2.06	0
75	SLU 69	-35	0	3517	0.01	-2.06	0
75	SLU 70	-35	0	3517	0.01	-2.06	0
75	SLU 71	-35	0	3517	0.01	-2.06	0
75	SLU 72	-35	0	3517	0.01	-2.06	0
75	SLU 73	-54	0	4286	0.01	-3.07	0
75	SLU 74	-54	0	4286	0.01	-3.07	0
75	SLU 75	-54	0	4286	0.01	-3.07	0
75	SLU 76	-54	0	4286	0.01	-3.07	0
75	SLU 77	-54	0	4286	0.01	-3.07	0
75	SLU 78	-54	0	4286	0.01	-3.07	0
75	SLU 79	-54	0	4286	0.01	-3.07	0
75	SLU 80	-54	0	4286	0.01	-3.07	0
75	SLU 81	-62	0	4615	0.01	-3.51	0
75	SLU 82	-62	0	4615	0.01	-3.51	0
75	SLU 83	-62	0	4615	0.01	-3.51	0
75	SLU 84	-62	0	4615	0.01	-3.51	0
75	SLE RA 1	-25	0	2606	0.01	-1.47	0
75	SLE RA 2	-25	0	2606	0.01	-1.47	0
75	SLE RA 3	-25	0	2606	0.01	-1.47	0
75	SLE RA 4	-25	0	2606	0.01	-1.47	0
75	SLE RA 5	-25	0	2606	0.01	-1.47	0
75	SLE RA 6	-25	0	2606	0.01	-1.47	0
75	SLE RA 7	-25	0	2606	0.01	-1.47	0
75	SLE RA 8	-25	0	2606	0.01	-1.47	0
75	SLE RA 9	-25	0	2606	0.01	-1.47	0
75	SLE RA 10	-37	0	3119	0.01	-2.14	0
75	SLE RA 11	-37	0	3119	0.01	-2.14	0
75	SLE RA 12	-37	0	3119	0.01	-2.14	0
75	SLE RA 13	-37	0	3119	0.01	-2.14	0
75	SLE RA 14	-37	0	3119	0.01	-2.14	0
75	SLE RA 15	-37	0	3119	0.01	-2.14	0
75	SLE RA 16	-37	0	3119	0.01	-2.14	0
75	SLE RA 17	-37	0	3119	0.01	-2.14	0
75	SLE RA 18	-43	0	3338	0.01	-2.43	0
75	SLE RA 19	-43	0	3338	0.01	-2.43	0
75	SLE RA 20	-43	0	3338	0.01	-2.43	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
75	SLE RA 21	-43	0	3338	0.01	-2.43	0
75	SLE FR 1	-25	0	2606	0.01	-1.47	0
75	SLE FR 2	-25	0	2606	0.01	-1.47	0
75	SLE FR 3	-25	0	2606	0.01	-1.47	0
75	SLE FR 4	-30	0	2826	0.01	-1.76	0
75	SLE FR 5	-30	0	2826	0.01	-1.76	0
75	SLE FR 6	-34	0	2972	0.01	-1.95	0
75	SLE QP 1	-25	0	2606	0.01	-1.47	0
75	SLE QP 2	-30	0	2826	0.01	-1.76	0
75	SLD 1	362	15	3007	-27.06	16.92	-0.04
75	SLD 2	362	15	3007	-27.06	16.92	-0.04
75	SLD 3	357	-19	3010	30.64	16.68	0.06
75	SLD 4	357	-19	3010	30.64	16.68	0.06
75	SLD 5	95	56	2876	-95.62	4.22	-0.17
75	SLD 6	95	56	2876	-95.62	4.22	-0.17
75	SLD 7	78	-57	2885	96.7	3.4	0.17
75	SLD 8	78	-57	2885	96.7	3.4	0.17
75	SLD 9	-138	57	2766	-96.69	-6.92	-0.17
75	SLD 10	-138	57	2766	-96.69	-6.92	-0.17
75	SLD 11	-156	-56	2776	95.63	-7.73	0.17
75	SLD 12	-156	-56	2776	95.63	-7.73	0.17
75	SLD 13	-417	19	2642	-30.62	-20.19	-0.06
75	SLD 14	-417	19	2642	-30.62	-20.19	-0.06
75	SLD 15	-422	-15	2645	27.07	-20.44	0.04
75	SLD 16	-422	-15	2645	27.07	-20.44	0.04
75	SLV 1	888	43	3249	-76.92	42.02	-0.13
75	SLV 2	888	43	3249	-76.92	42.02	-0.13
75	SLV 3	876	-53	3256	85.8	41.44	0.16
75	SLV 4	876	-53	3256	85.8	41.44	0.16
75	SLV 5	264	158	2942	-269.87	12.25	-0.47
75	SLV 6	264	158	2942	-269.87	12.25	-0.47
75	SLV 7	223	-161	2965	272.54	10.32	0.48
75	SLV 8	223	-161	2965	272.54	10.32	0.48
75	SLV 9	-284	161	2686	-272.53	-13.84	-0.48
75	SLV 10	-284	161	2686	-272.53	-13.84	-0.48
75	SLV 11	-325	-158	2709	269.88	-15.77	0.47
75	SLV 12	-325	-158	2709	269.88	-15.77	0.47
75	SLV 13	-937	53	2396	-85.78	-44.95	-0.16
75	SLV 14	-937	53	2396	-85.78	-44.95	-0.16
75	SLV 15	-949	-43	2402	76.94	-45.53	0.13
75	SLV 16	-949	-43	2402	76.94	-45.53	0.13
76	SLU 1	-6	0	2415	0.01	-0.74	0
76	SLU 2	-6	0	2415	0.01	-0.74	0
76	SLU 3	-6	0	2415	0.01	-0.74	0
76	SLU 4	-6	0	2415	0.01	-0.74	0
76	SLU 5	-6	0	2415	0.01	-0.74	0
76	SLU 6	-6	0	2415	0.01	-0.74	0
76	SLU 7	-6	0	2415	0.01	-0.74	0
76	SLU 8	-6	0	2415	0.01	-0.74	0
76	SLU 9	-6	0	2415	0.01	-0.74	0
76	SLU 10	-11	0	3151	0.01	-1.27	0
76	SLU 11	-11	0	3151	0.01	-1.27	0
76	SLU 12	-11	0	3151	0.01	-1.27	0
76	SLU 13	-11	0	3151	0.01	-1.27	0
76	SLU 14	-11	0	3151	0.01	-1.27	0
76	SLU 15	-11	0	3151	0.01	-1.27	0
76	SLU 16	-11	0	3151	0.01	-1.27	0
76	SLU 17	-11	0	3151	0.01	-1.27	0
76	SLU 18	-14	0	3466	0.01	-1.49	0
76	SLU 19	-14	0	3466	0.01	-1.49	0
76	SLU 20	-14	0	3466	0.01	-1.49	0
76	SLU 21	-14	0	3466	0.01	-1.49	0
76	SLU 22	-9	0	2851	0.01	-1.04	0
76	SLU 23	-9	0	2851	0.01	-1.04	0
76	SLU 24	-9	0	2851	0.01	-1.04	0
76	SLU 25	-9	0	2851	0.01	-1.04	0
76	SLU 26	-9	0	2851	0.01	-1.04	0
76	SLU 27	-9	0	2851	0.01	-1.04	0
76	SLU 28	-9	0	2851	0.01	-1.04	0
76	SLU 29	-9	0	2851	0.01	-1.04	0
76	SLU 30	-9	0	2851	0.01	-1.04	0
76	SLU 31	-15	0	3587	0.01	-1.57	0
76	SLU 32	-15	0	3587	0.01	-1.57	0
76	SLU 33	-15	0	3587	0.01	-1.57	0
76	SLU 34	-15	0	3587	0.01	-1.57	0
76	SLU 35	-15	0	3587	0.01	-1.57	0
76	SLU 36	-15	0	3587	0.01	-1.57	0
76	SLU 37	-15	0	3587	0.01	-1.57	0
76	SLU 38	-15	0	3587	0.01	-1.57	0
76	SLU 39	-17	0	3902	0.01	-1.79	0
76	SLU 40	-17	0	3902	0.01	-1.79	0
76	SLU 41	-17	0	3902	0.01	-1.79	0
76	SLU 42	-17	0	3902	0.01	-1.79	0
76	SLU 43	-6	0	2990	0.01	-0.86	0
76	SLU 44	-6	0	2990	0.01	-0.86	0
76	SLU 45	-6	0	2990	0.01	-0.86	0
76	SLU 46	-6	0	2990	0.01	-0.86	0
76	SLU 47	-6	0	2990	0.01	-0.86	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione		
		x	y	z		x	y	z
76	SLU 48	-6	0	2990		0.01	-0.86	0
76	SLU 49	-6	0	2990		0.01	-0.86	0
76	SLU 50	-6	0	2990		0.01	-0.86	0
76	SLU 51	-6	0	2990		0.01	-0.86	0
76	SLU 52	-12	0	3726		0.01	-1.38	0
76	SLU 53	-12	0	3726		0.01	-1.38	0
76	SLU 54	-12	0	3726		0.01	-1.38	0
76	SLU 55	-12	0	3726		0.01	-1.38	0
76	SLU 56	-12	0	3726		0.01	-1.38	0
76	SLU 57	-12	0	3726		0.01	-1.38	0
76	SLU 58	-12	0	3726		0.01	-1.38	0
76	SLU 59	-12	0	3726		0.01	-1.38	0
76	SLU 60	-14	0	4041		0.01	-1.61	0
76	SLU 61	-14	0	4041		0.01	-1.61	0
76	SLU 62	-14	0	4041		0.01	-1.61	0
76	SLU 63	-14	0	4041		0.01	-1.61	0
76	SLU 64	-10	0	3426		0.01	-1.16	0
76	SLU 65	-10	0	3426		0.01	-1.16	0
76	SLU 66	-10	0	3426		0.01	-1.16	0
76	SLU 67	-10	0	3426		0.01	-1.16	0
76	SLU 68	-10	0	3426		0.01	-1.16	0
76	SLU 69	-10	0	3426		0.01	-1.16	0
76	SLU 70	-10	0	3426		0.01	-1.16	0
76	SLU 71	-10	0	3426		0.01	-1.16	0
76	SLU 72	-10	0	3426		0.01	-1.16	0
76	SLU 73	-15	0	4162		0.01	-1.68	0
76	SLU 74	-15	0	4162		0.01	-1.68	0
76	SLU 75	-15	0	4162		0.01	-1.68	0
76	SLU 76	-15	0	4162		0.01	-1.68	0
76	SLU 77	-15	0	4162		0.01	-1.68	0
76	SLU 78	-15	0	4162		0.01	-1.68	0
76	SLU 79	-15	0	4162		0.01	-1.68	0
76	SLU 80	-15	0	4162		0.01	-1.68	0
76	SLU 81	-18	0	4477		0.01	-1.91	0
76	SLU 82	-18	0	4477		0.01	-1.91	0
76	SLU 83	-18	0	4477		0.01	-1.91	0
76	SLU 84	-18	0	4477		0.01	-1.91	0
76	SLE RA 1	-7	0	2540		0.01	-0.82	0
76	SLE RA 2	-7	0	2540		0.01	-0.82	0
76	SLE RA 3	-7	0	2540		0.01	-0.82	0
76	SLE RA 4	-7	0	2540		0.01	-0.82	0
76	SLE RA 5	-7	0	2540		0.01	-0.82	0
76	SLE RA 6	-7	0	2540		0.01	-0.82	0
76	SLE RA 7	-7	0	2540		0.01	-0.82	0
76	SLE RA 8	-7	0	2540		0.01	-0.82	0
76	SLE RA 9	-7	0	2540		0.01	-0.82	0
76	SLE RA 10	-10	0	3030		0.01	-1.18	0
76	SLE RA 11	-10	0	3030		0.01	-1.18	0
76	SLE RA 12	-10	0	3030		0.01	-1.18	0
76	SLE RA 13	-10	0	3030		0.01	-1.18	0
76	SLE RA 14	-10	0	3030		0.01	-1.18	0
76	SLE RA 15	-10	0	3030		0.01	-1.18	0
76	SLE RA 16	-10	0	3030		0.01	-1.18	0
76	SLE RA 17	-10	0	3030		0.01	-1.18	0
76	SLE RA 18	-12	0	3240		0.01	-1.33	0
76	SLE RA 19	-12	0	3240		0.01	-1.33	0
76	SLE RA 20	-12	0	3240		0.01	-1.33	0
76	SLE RA 21	-12	0	3240		0.01	-1.33	0
76	SLE FR 1	-7	0	2540		0.01	-0.82	0
76	SLE FR 2	-7	0	2540		0.01	-0.82	0
76	SLE FR 3	-7	0	2540		0.01	-0.82	0
76	SLE FR 4	-8	0	2750		0.01	-0.97	0
76	SLE FR 5	-8	0	2750		0.01	-0.97	0
76	SLE FR 6	-9	0	2890		0.01	-1.07	0
76	SLE QP 1	-7	0	2540		0.01	-0.82	0
76	SLE QP 2	-8	0	2750		0.01	-0.97	0
76	SLD 1	406	18	2918		-30.05	18.8	-0.07
76	SLD 2	406	18	2918		-30.05	18.8	-0.07
76	SLD 3	401	-22	2915		33.23	18.54	0.06
76	SLD 4	401	-22	2915		33.23	18.54	0.06
76	SLD 5	124	67	2804		-104.99	5.35	-0.22
76	SLD 6	124	67	2804		-104.99	5.35	-0.22
76	SLD 7	107	-69	2795		105.95	4.49	0.22
76	SLD 8	107	-69	2795		105.95	4.49	0.22
76	SLD 9	-123	69	2704		-105.94	-6.44	-0.22
76	SLD 10	-123	69	2704		-105.94	-6.44	-0.22
76	SLD 11	-141	-67	2696		105	-7.3	0.22
76	SLD 12	-141	-67	2696		105	-7.3	0.22
76	SLD 13	-418	22	2585		-33.21	-20.49	-0.06
76	SLD 14	-418	22	2585		-33.21	-20.49	-0.06
76	SLD 15	-423	-18	2582		30.07	-20.74	0.07
76	SLD 16	-423	-18	2582		30.07	-20.74	0.07
76	SLV 1	963	52	3142		-85.38	45.33	-0.2
76	SLV 2	963	52	3142		-85.38	45.33	-0.2
76	SLV 3	951	-62	3136		93.16	44.72	0.17
76	SLV 4	951	-62	3136		93.16	44.72	0.17
76	SLV 5	302	189	2877		-296.39	13.84	-0.62
76	SLV 6	302	189	2877		-296.39	13.84	-0.62



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
76	SLV 7	261	-192	2856	298.73	11.81	0.61
76	SLV 8	261	-192	2856	298.73	11.81	0.61
76	SLV 9	-278	192	2644	-298.72	-13.76	-0.61
76	SLV 10	-278	192	2644	-298.72	-13.76	-0.61
76	SLV 11	-318	-189	2622	296.4	-15.79	0.62
76	SLV 12	-318	-189	2622	296.4	-15.79	0.62
76	SLV 13	-968	62	2364	-93.15	-46.67	-0.17
76	SLV 14	-968	62	2364	-93.15	-46.67	-0.17
76	SLV 15	-980	-52	2358	85.39	-47.28	0.2
76	SLV 16	-980	-52	2358	85.39	-47.28	0.2
77	SLU 1	4	0	2364	0	0.01	0
77	SLU 2	4	0	2364	0	0.01	0
77	SLU 3	4	0	2364	0	0.01	0
77	SLU 4	4	0	2364	0	0.01	0
77	SLU 5	4	0	2364	0	0.01	0
77	SLU 6	4	0	2364	0	0.01	0
77	SLU 7	4	0	2364	0	0.01	0
77	SLU 8	4	0	2364	0	0.01	0
77	SLU 9	4	0	2364	0	0.01	0
77	SLU 10	7	0	3071	0.01	0.06	0
77	SLU 11	7	0	3071	0.01	0.06	0
77	SLU 12	7	0	3071	0.01	0.06	0
77	SLU 13	7	0	3071	0.01	0.06	0
77	SLU 14	7	0	3071	0.01	0.06	0
77	SLU 15	7	0	3071	0.01	0.06	0
77	SLU 16	7	0	3071	0.01	0.06	0
77	SLU 17	7	0	3071	0.01	0.06	0
77	SLU 18	8	0	3374	0.01	0.08	0
77	SLU 19	8	0	3374	0.01	0.08	0
77	SLU 20	8	0	3374	0.01	0.08	0
77	SLU 21	8	0	3374	0.01	0.08	0
77	SLU 22	5	0	2787	0.01	0.01	0
77	SLU 23	5	0	2787	0.01	0.01	0
77	SLU 24	5	0	2787	0.01	0.01	0
77	SLU 25	5	0	2787	0.01	0.01	0
77	SLU 26	5	0	2787	0.01	0.01	0
77	SLU 27	5	0	2787	0.01	0.01	0
77	SLU 28	5	0	2787	0.01	0.01	0
77	SLU 29	5	0	2787	0.01	0.01	0
77	SLU 30	5	0	2787	0.01	0.01	0
77	SLU 31	8	0	3493	0.01	0.06	0
77	SLU 32	8	0	3493	0.01	0.06	0
77	SLU 33	8	0	3493	0.01	0.06	0
77	SLU 34	8	0	3493	0.01	0.06	0
77	SLU 35	8	0	3493	0.01	0.06	0
77	SLU 36	8	0	3493	0.01	0.06	0
77	SLU 37	8	0	3493	0.01	0.06	0
77	SLU 38	8	0	3493	0.01	0.06	0
77	SLU 39	9	0	3796	0.01	0.08	0
77	SLU 40	9	0	3796	0.01	0.08	0
77	SLU 41	9	0	3796	0.01	0.08	0
77	SLU 42	9	0	3796	0.01	0.08	0
77	SLU 43	5	0	2929	0.01	0.01	0
77	SLU 44	5	0	2929	0.01	0.01	0
77	SLU 45	5	0	2929	0.01	0.01	0
77	SLU 46	5	0	2929	0.01	0.01	0
77	SLU 47	5	0	2929	0.01	0.01	0
77	SLU 48	5	0	2929	0.01	0.01	0
77	SLU 49	5	0	2929	0.01	0.01	0
77	SLU 50	5	0	2929	0.01	0.01	0
77	SLU 51	5	0	2929	0.01	0.01	0
77	SLU 52	8	0	3636	0.01	0.06	0
77	SLU 53	8	0	3636	0.01	0.06	0
77	SLU 54	8	0	3636	0.01	0.06	0
77	SLU 55	8	0	3636	0.01	0.06	0
77	SLU 56	8	0	3636	0.01	0.06	0
77	SLU 57	8	0	3636	0.01	0.06	0
77	SLU 58	8	0	3636	0.01	0.06	0
77	SLU 59	8	0	3636	0.01	0.06	0
77	SLU 60	9	0	3938	0.01	0.09	0
77	SLU 61	9	0	3938	0.01	0.09	0
77	SLU 62	9	0	3938	0.01	0.09	0
77	SLU 63	9	0	3938	0.01	0.09	0
77	SLU 64	6	0	3351	0.01	0.01	0
77	SLU 65	6	0	3351	0.01	0.01	0
77	SLU 66	6	0	3351	0.01	0.01	0
77	SLU 67	6	0	3351	0.01	0.01	0
77	SLU 68	6	0	3351	0.01	0.01	0
77	SLU 69	6	0	3351	0.01	0.01	0
77	SLU 70	6	0	3351	0.01	0.01	0
77	SLU 71	6	0	3351	0.01	0.01	0
77	SLU 72	6	0	3351	0.01	0.01	0
77	SLU 73	9	0	4058	0.01	0.06	0
77	SLU 74	9	0	4058	0.01	0.06	0
77	SLU 75	9	0	4058	0.01	0.06	0
77	SLU 76	9	0	4058	0.01	0.06	0
77	SLU 77	9	0	4058	0.01	0.06	0
77	SLU 78	9	0	4058	0.01	0.06	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
77	SLU 79	9	0	4058	0.01	0.06	0
77	SLU 80	9	0	4058	0.01	0.06	0
77	SLU 81	10	0	4361	0.01	0.08	0
77	SLU 82	10	0	4361	0.01	0.08	0
77	SLU 83	10	0	4361	0.01	0.08	0
77	SLU 84	10	0	4361	0.01	0.08	0
77	SLE RA 1	4	0	2485	0	0.01	0
77	SLE RA 2	4	0	2485	0	0.01	0
77	SLE RA 3	4	0	2485	0	0.01	0
77	SLE RA 4	4	0	2485	0	0.01	0
77	SLE RA 5	4	0	2485	0	0.01	0
77	SLE RA 6	4	0	2485	0	0.01	0
77	SLE RA 7	4	0	2485	0	0.01	0
77	SLE RA 8	4	0	2485	0	0.01	0
77	SLE RA 9	4	0	2485	0	0.01	0
77	SLE RA 10	6	0	2956	0.01	0.04	0
77	SLE RA 11	6	0	2956	0.01	0.04	0
77	SLE RA 12	6	0	2956	0.01	0.04	0
77	SLE RA 13	6	0	2956	0.01	0.04	0
77	SLE RA 14	6	0	2956	0.01	0.04	0
77	SLE RA 15	6	0	2956	0.01	0.04	0
77	SLE RA 16	6	0	2956	0.01	0.04	0
77	SLE RA 17	6	0	2956	0.01	0.04	0
77	SLE RA 18	7	0	3158	0.01	0.06	0
77	SLE RA 19	7	0	3158	0.01	0.06	0
77	SLE RA 20	7	0	3158	0.01	0.06	0
77	SLE RA 21	7	0	3158	0.01	0.06	0
77	SLE FR 1	4	0	2485	0	0.01	0
77	SLE FR 2	4	0	2485	0	0.01	0
77	SLE FR 3	4	0	2485	0	0.01	0
77	SLE FR 4	5	0	2687	0.01	0.02	0
77	SLE FR 5	5	0	2687	0.01	0.02	0
77	SLE FR 6	6	0	2822	0.01	0.03	0
77	SLE QP 1	4	0	2485	0	0.01	0
77	SLE QP 2	5	0	2687	0.01	0.02	0
77	SLD 1	437	22	2815	-32.96	20.3	-0.08
77	SLD 2	437	22	2815	-32.96	20.3	-0.08
77	SLD 3	432	-26	2813	35.43	20.06	0.07
77	SLD 4	432	-26	2813	35.43	20.06	0.07
77	SLD 5	142	80	2729	-113.6	6.46	-0.25
77	SLD 6	142	80	2729	-113.6	6.46	-0.25
77	SLD 7	126	-81	2721	114.35	5.68	0.25
77	SLD 8	126	-81	2721	114.35	5.68	0.25
77	SLD 9	-115	81	2653	-114.34	-5.63	-0.25
77	SLD 10	-115	81	2653	-114.34	-5.63	-0.25
77	SLD 11	-132	-80	2645	113.61	-6.42	0.25
77	SLD 12	-132	-80	2645	113.61	-6.42	0.25
77	SLD 13	-422	26	2561	-35.42	-20.01	-0.07
77	SLD 14	-422	26	2561	-35.42	-20.01	-0.07
77	SLD 15	-427	-22	2558	32.97	-20.25	0.08
77	SLD 16	-427	-22	2558	32.97	-20.25	0.08
77	SLV 1	1018	63	2987	-93.45	47.51	-0.22
77	SLV 2	1018	63	2987	-93.45	47.51	-0.22
77	SLV 3	1006	-71	2982	99.46	46.95	0.2
77	SLV 4	1006	-71	2982	99.46	46.95	0.2
77	SLV 5	327	223	2786	-320.6	15.11	-0.71
77	SLV 6	327	223	2786	-320.6	15.11	-0.71
77	SLV 7	287	-226	2767	322.41	13.26	0.7
77	SLV 8	287	-226	2767	322.41	13.26	0.7
77	SLV 9	-277	226	2607	-322.4	-13.21	-0.7
77	SLV 10	-277	226	2607	-322.4	-13.21	-0.7
77	SLV 11	-317	-223	2588	320.61	-15.07	0.71
77	SLV 12	-317	-223	2588	320.61	-15.07	0.71
77	SLV 13	-995	71	2392	-99.45	-46.91	-0.2
77	SLV 14	-995	71	2392	-99.45	-46.91	-0.2
77	SLV 15	-1007	-63	2387	93.46	-47.46	0.22
77	SLV 16	-1007	-63	2387	93.46	-47.46	0.22
78	SLU 1	2	0	2330	0	-0.11	0
78	SLU 2	2	0	2330	0	-0.11	0
78	SLU 3	2	0	2330	0	-0.11	0
78	SLU 4	2	0	2330	0	-0.11	0
78	SLU 5	2	0	2330	0	-0.11	0
78	SLU 6	2	0	2330	0	-0.11	0
78	SLU 7	2	0	2330	0	-0.11	0
78	SLU 8	2	0	2330	0	-0.11	0
78	SLU 9	2	0	2330	0	-0.11	0
78	SLU 10	5	0	3016	0.01	-0.09	0
78	SLU 11	5	0	3016	0.01	-0.09	0
78	SLU 12	5	0	3016	0.01	-0.09	0
78	SLU 13	5	0	3016	0.01	-0.09	0
78	SLU 14	5	0	3016	0.01	-0.09	0
78	SLU 15	5	0	3016	0.01	-0.09	0
78	SLU 16	5	0	3016	0.01	-0.09	0
78	SLU 17	5	0	3016	0.01	-0.09	0
78	SLU 18	7	0	3310	0.01	-0.08	0
78	SLU 19	7	0	3310	0.01	-0.08	0
78	SLU 20	7	0	3310	0.01	-0.08	0
78	SLU 21	7	0	3310	0.01	-0.08	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
78	SLU 22	3	0	2743	0	-0.12	0
78	SLU 23	3	0	2743	0	-0.12	0
78	SLU 24	3	0	2743	0	-0.12	0
78	SLU 25	3	0	2743	0	-0.12	0
78	SLU 26	3	0	2743	0	-0.12	0
78	SLU 27	3	0	2743	0	-0.12	0
78	SLU 28	3	0	2743	0	-0.12	0
78	SLU 29	3	0	2743	0	-0.12	0
78	SLU 30	3	0	2743	0	-0.12	0
78	SLU 31	6	0	3429	0.01	-0.1	0
78	SLU 32	6	0	3429	0.01	-0.1	0
78	SLU 33	6	0	3429	0.01	-0.1	0
78	SLU 34	6	0	3429	0.01	-0.1	0
78	SLU 35	6	0	3429	0.01	-0.1	0
78	SLU 36	6	0	3429	0.01	-0.1	0
78	SLU 37	6	0	3429	0.01	-0.1	0
78	SLU 38	6	0	3429	0.01	-0.1	0
78	SLU 39	8	0	3723	0.01	-0.09	0
78	SLU 40	8	0	3723	0.01	-0.09	0
78	SLU 41	8	0	3723	0.01	-0.09	0
78	SLU 42	8	0	3723	0.01	-0.09	0
78	SLU 43	2	0	2888	0	-0.14	0
78	SLU 44	2	0	2888	0	-0.14	0
78	SLU 45	2	0	2888	0	-0.14	0
78	SLU 46	2	0	2888	0	-0.14	0
78	SLU 47	2	0	2888	0	-0.14	0
78	SLU 48	2	0	2888	0	-0.14	0
78	SLU 49	2	0	2888	0	-0.14	0
78	SLU 50	2	0	2888	0	-0.14	0
78	SLU 51	2	0	2888	0	-0.14	0
78	SLU 52	6	0	3574	0.01	-0.11	0
78	SLU 53	6	0	3574	0.01	-0.11	0
78	SLU 54	6	0	3574	0.01	-0.11	0
78	SLU 55	6	0	3574	0.01	-0.11	0
78	SLU 56	6	0	3574	0.01	-0.11	0
78	SLU 57	6	0	3574	0.01	-0.11	0
78	SLU 58	6	0	3574	0.01	-0.11	0
78	SLU 59	6	0	3574	0.01	-0.11	0
78	SLU 60	7	0	3868	0.01	-0.1	0
78	SLU 61	7	0	3868	0.01	-0.1	0
78	SLU 62	7	0	3868	0.01	-0.1	0
78	SLU 63	7	0	3868	0.01	-0.1	0
78	SLU 64	3	0	3300	0.01	-0.15	0
78	SLU 65	3	0	3300	0.01	-0.15	0
78	SLU 66	3	0	3300	0.01	-0.15	0
78	SLU 67	3	0	3300	0.01	-0.15	0
78	SLU 68	3	0	3300	0.01	-0.15	0
78	SLU 69	3	0	3300	0.01	-0.15	0
78	SLU 70	3	0	3300	0.01	-0.15	0
78	SLU 71	3	0	3300	0.01	-0.15	0
78	SLU 72	3	0	3300	0.01	-0.15	0
78	SLU 73	7	0	3986	0.01	-0.13	0
78	SLU 74	7	0	3986	0.01	-0.13	0
78	SLU 75	7	0	3986	0.01	-0.13	0
78	SLU 76	7	0	3986	0.01	-0.13	0
78	SLU 77	7	0	3986	0.01	-0.13	0
78	SLU 78	7	0	3986	0.01	-0.13	0
78	SLU 79	7	0	3986	0.01	-0.13	0
78	SLU 80	7	0	3986	0.01	-0.13	0
78	SLU 81	8	0	4280	0.01	-0.12	0
78	SLU 82	8	0	4280	0.01	-0.12	0
78	SLU 83	8	0	4280	0.01	-0.12	0
78	SLU 84	8	0	4280	0.01	-0.12	0
78	SLE RA 1	2	0	2448	0	-0.11	0
78	SLE RA 2	2	0	2448	0	-0.11	0
78	SLE RA 3	2	0	2448	0	-0.11	0
78	SLE RA 4	2	0	2448	0	-0.11	0
78	SLE RA 5	2	0	2448	0	-0.11	0
78	SLE RA 6	2	0	2448	0	-0.11	0
78	SLE RA 7	2	0	2448	0	-0.11	0
78	SLE RA 8	2	0	2448	0	-0.11	0
78	SLE RA 9	2	0	2448	0	-0.11	0
78	SLE RA 10	5	0	2906	0.01	-0.1	0
78	SLE RA 11	5	0	2906	0.01	-0.1	0
78	SLE RA 12	5	0	2906	0.01	-0.1	0
78	SLE RA 13	5	0	2906	0.01	-0.1	0
78	SLE RA 14	5	0	2906	0.01	-0.1	0
78	SLE RA 15	5	0	2906	0.01	-0.1	0
78	SLE RA 16	5	0	2906	0.01	-0.1	0
78	SLE RA 17	5	0	2906	0.01	-0.1	0
78	SLE RA 18	6	0	3102	0.01	-0.09	0
78	SLE RA 19	6	0	3102	0.01	-0.09	0
78	SLE RA 20	6	0	3102	0.01	-0.09	0
78	SLE RA 21	6	0	3102	0.01	-0.09	0
78	SLE FR 1	2	0	2448	0	-0.11	0
78	SLE FR 2	2	0	2448	0	-0.11	0
78	SLE FR 3	2	0	2448	0	-0.11	0
78	SLE FR 4	3	0	2644	0	-0.11	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
78	SLE FR 5	3	0	2644	0	-0.11	0
78	SLE FR 6	4	0	2775	0	-0.1	0
78	SLE QP 1	2	0	2448	0	-0.11	0
78	SLE QP 2	3	0	2644	0	-0.11	0
78	SLD 1	453	26	2713	-35.28	21.18	-0.08
78	SLD 2	453	26	2713	-35.28	21.18	-0.08
78	SLD 3	448	-28	2711	36.79	20.92	0.07
78	SLD 4	448	-28	2711	36.79	20.92	0.07
78	SLD 5	146	89	2668	-119.89	6.67	-0.26
78	SLD 6	146	89	2668	-119.89	6.67	-0.26
78	SLD 7	129	-90	2661	120.34	5.81	0.26
78	SLD 8	129	-90	2661	120.34	5.81	0.26
78	SLD 9	-122	90	2627	-120.33	-6.02	-0.26
78	SLD 10	-122	90	2627	-120.33	-6.02	-0.26
78	SLD 11	-139	-89	2620	119.89	-6.88	0.26
78	SLD 12	-139	-89	2620	119.89	-6.88	0.26
78	SLD 13	-441	28	2577	-36.78	-21.14	-0.07
78	SLD 14	-441	28	2577	-36.78	-21.14	-0.07
78	SLD 15	-446	-26	2575	35.29	-21.39	0.08
78	SLD 16	-446	-26	2575	35.29	-21.39	0.08
78	SLV 1	1055	73	2805	-99.79	49.74	-0.22
78	SLV 2	1055	73	2805	-99.79	49.74	-0.22
78	SLV 3	1043	-78	2800	103.43	49.13	0.21
78	SLV 4	1043	-78	2800	103.43	49.13	0.21
78	SLV 5	337	250	2700	-338.15	15.77	-0.72
78	SLV 6	337	250	2700	-338.15	15.77	-0.72
78	SLV 7	297	-252	2683	339.25	13.75	0.72
78	SLV 8	297	-252	2683	339.25	13.75	0.72
78	SLV 9	-291	252	2605	-339.24	-13.96	-0.72
78	SLV 10	-291	252	2605	-339.24	-13.96	-0.72
78	SLV 11	-330	-250	2588	338.16	-15.98	0.72
78	SLV 12	-330	-250	2588	338.16	-15.98	0.72
78	SLV 13	-1037	78	2488	-103.42	-49.35	-0.21
78	SLV 14	-1037	78	2488	-103.42	-49.35	-0.21
78	SLV 15	-1049	-73	2483	99.8	-49.95	0.22
78	SLV 16	-1049	-73	2483	99.8	-49.95	0.22
79	SLU 1	-3	0	3516	-0.01	-0.12	0
79	SLU 2	-3	0	3516	-0.01	-0.12	0
79	SLU 3	-3	0	3516	-0.01	-0.12	0
79	SLU 4	-3	0	3516	-0.01	-0.12	0
79	SLU 5	-3	0	3516	-0.01	-0.12	0
79	SLU 6	-3	0	3516	-0.01	-0.12	0
79	SLU 7	-3	0	3516	-0.01	-0.12	0
79	SLU 8	-3	0	3516	-0.01	-0.12	0
79	SLU 9	-3	0	3516	-0.01	-0.12	0
79	SLU 10	-2	0	4517	0	-0.08	0
79	SLU 11	-2	0	4517	0	-0.08	0
79	SLU 12	-2	0	4517	0	-0.08	0
79	SLU 13	-2	0	4517	0	-0.08	0
79	SLU 14	-2	0	4517	0	-0.08	0
79	SLU 15	-2	0	4517	0	-0.08	0
79	SLU 16	-2	0	4517	0	-0.08	0
79	SLU 17	-2	0	4517	0	-0.08	0
79	SLU 18	-2	0	4946	0	-0.06	0
79	SLU 19	-2	0	4946	0	-0.06	0
79	SLU 20	-2	0	4946	0	-0.06	0
79	SLU 21	-2	0	4946	0	-0.06	0
79	SLU 22	-3	0	4119	0	-0.1	0
79	SLU 23	-3	0	4119	0	-0.1	0
79	SLU 24	-3	0	4119	0	-0.1	0
79	SLU 25	-3	0	4119	0	-0.1	0
79	SLU 26	-3	0	4119	0	-0.1	0
79	SLU 27	-3	0	4119	0	-0.1	0
79	SLU 28	-3	0	4119	0	-0.1	0
79	SLU 29	-3	0	4119	0	-0.1	0
79	SLU 30	-3	0	4119	0	-0.1	0
79	SLU 31	-2	0	5119	0	-0.07	0
79	SLU 32	-2	0	5119	0	-0.07	0
79	SLU 33	-2	0	5119	0	-0.07	0
79	SLU 34	-2	0	5119	0	-0.07	0
79	SLU 35	-2	0	5119	0	-0.07	0
79	SLU 36	-2	0	5119	0	-0.07	0
79	SLU 37	-2	0	5119	0	-0.07	0
79	SLU 38	-2	0	5119	0	-0.07	0
79	SLU 39	-1	0	5548	0	-0.05	0
79	SLU 40	-1	0	5548	0	-0.05	0
79	SLU 41	-1	0	5548	0	-0.05	0
79	SLU 42	-1	0	5548	0	-0.05	0
79	SLU 43	-4	0	4365	-0.01	-0.15	0
79	SLU 44	-4	0	4365	-0.01	-0.15	0
79	SLU 45	-4	0	4365	-0.01	-0.15	0
79	SLU 46	-4	0	4365	-0.01	-0.15	0
79	SLU 47	-4	0	4365	-0.01	-0.15	0
79	SLU 48	-4	0	4365	-0.01	-0.15	0
79	SLU 49	-4	0	4365	-0.01	-0.15	0
79	SLU 50	-4	0	4365	-0.01	-0.15	0
79	SLU 51	-4	0	4365	-0.01	-0.15	0
79	SLU 52	-3	0	5365	-0.01	-0.11	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
79	SLU 53	-3	0	5365	-0.01	-0.11	0
79	SLU 54	-3	0	5365	-0.01	-0.11	0
79	SLU 55	-3	0	5365	-0.01	-0.11	0
79	SLU 56	-3	0	5365	-0.01	-0.11	0
79	SLU 57	-3	0	5365	-0.01	-0.11	0
79	SLU 58	-3	0	5365	-0.01	-0.11	0
79	SLU 59	-3	0	5365	-0.01	-0.11	0
79	SLU 60	-3	0	5794	0	-0.1	0
79	SLU 61	-3	0	5794	0	-0.1	0
79	SLU 62	-3	0	5794	0	-0.1	0
79	SLU 63	-3	0	5794	0	-0.1	0
79	SLU 64	-4	0	4967	-0.01	-0.14	0
79	SLU 65	-4	0	4967	-0.01	-0.14	0
79	SLU 66	-4	0	4967	-0.01	-0.14	0
79	SLU 67	-4	0	4967	-0.01	-0.14	0
79	SLU 68	-4	0	4967	-0.01	-0.14	0
79	SLU 69	-4	0	4967	-0.01	-0.14	0
79	SLU 70	-4	0	4967	-0.01	-0.14	0
79	SLU 71	-4	0	4967	-0.01	-0.14	0
79	SLU 72	-4	0	4967	-0.01	-0.14	0
79	SLU 73	-3	0	5968	0	-0.1	0
79	SLU 74	-3	0	5968	0	-0.1	0
79	SLU 75	-3	0	5968	0	-0.1	0
79	SLU 76	-3	0	5968	0	-0.1	0
79	SLU 77	-3	0	5968	0	-0.1	0
79	SLU 78	-3	0	5968	0	-0.1	0
79	SLU 79	-3	0	5968	0	-0.1	0
79	SLU 80	-3	0	5968	0	-0.1	0
79	SLU 81	-2	0	6397	0	-0.09	0
79	SLU 82	-2	0	6397	0	-0.09	0
79	SLU 83	-2	0	6397	0	-0.09	0
79	SLU 84	-2	0	6397	0	-0.09	0
79	SLE RA 1	-3	0	3688	-0.01	-0.11	0
79	SLE RA 2	-3	0	3688	-0.01	-0.11	0
79	SLE RA 3	-3	0	3688	-0.01	-0.11	0
79	SLE RA 4	-3	0	3688	-0.01	-0.11	0
79	SLE RA 5	-3	0	3688	-0.01	-0.11	0
79	SLE RA 6	-3	0	3688	-0.01	-0.11	0
79	SLE RA 7	-3	0	3688	-0.01	-0.11	0
79	SLE RA 8	-3	0	3688	-0.01	-0.11	0
79	SLE RA 9	-3	0	3688	-0.01	-0.11	0
79	SLE RA 10	-2	0	4355	0	-0.09	0
79	SLE RA 11	-2	0	4355	0	-0.09	0
79	SLE RA 12	-2	0	4355	0	-0.09	0
79	SLE RA 13	-2	0	4355	0	-0.09	0
79	SLE RA 14	-2	0	4355	0	-0.09	0
79	SLE RA 15	-2	0	4355	0	-0.09	0
79	SLE RA 16	-2	0	4355	0	-0.09	0
79	SLE RA 17	-2	0	4355	0	-0.09	0
79	SLE RA 18	-2	0	4641	0	-0.07	0
79	SLE RA 19	-2	0	4641	0	-0.07	0
79	SLE RA 20	-2	0	4641	0	-0.07	0
79	SLE RA 21	-2	0	4641	0	-0.07	0
79	SLE FR 1	-3	0	3688	-0.01	-0.11	0
79	SLE FR 2	-3	0	3688	-0.01	-0.11	0
79	SLE FR 3	-3	0	3688	-0.01	-0.11	0
79	SLE FR 4	-3	0	3974	0	-0.1	0
79	SLE FR 5	-3	0	3974	0	-0.1	0
79	SLE FR 6	-2	0	4165	0	-0.09	0
79	SLE QP 1	-3	0	3688	-0.01	-0.11	0
79	SLE QP 2	-3	0	3974	0	-0.1	0
79	SLD 1	464	28	3968	-37.61	22.46	-0.09
79	SLD 2	464	28	3968	-37.61	22.46	-0.09
79	SLD 3	459	-30	3972	38.39	22.07	0.08
79	SLD 4	459	-30	3972	38.39	22.07	0.08
79	SLD 5	145	97	3966	-126.54	7.27	-0.29
79	SLD 6	145	97	3966	-126.54	7.27	-0.29
79	SLD 7	128	-98	3980	126.77	5.95	0.29
79	SLD 8	128	-98	3980	126.77	5.95	0.29
79	SLD 9	-133	98	3969	-126.78	-6.15	-0.29
79	SLD 10	-133	98	3969	-126.78	-6.15	-0.29
79	SLD 11	-150	-97	3982	126.53	-7.47	0.29
79	SLD 12	-150	-97	3982	126.53	-7.47	0.29
79	SLD 13	-464	30	3976	-38.4	-22.27	-0.08
79	SLD 14	-464	30	3976	-38.4	-22.27	-0.08
79	SLD 15	-469	-28	3981	37.6	-22.67	0.09
79	SLD 16	-469	-28	3981	37.6	-22.67	0.09
79	SLV 1	1089	80	3959	-106.18	53.03	-0.25
79	SLV 2	1089	80	3959	-106.18	53.03	-0.25
79	SLV 3	1077	-84	3970	108.07	52.1	0.23
79	SLV 4	1077	-84	3970	108.07	52.1	0.23
79	SLV 5	344	272	3953	-356.79	17.25	-0.81
79	SLV 6	344	272	3953	-356.79	17.25	-0.81
79	SLV 7	303	-273	3989	357.35	14.15	0.8
79	SLV 8	303	-273	3989	357.35	14.15	0.8
79	SLV 9	-308	273	3959	-357.36	-14.35	-0.8
79	SLV 10	-308	273	3959	-357.36	-14.35	-0.8
79	SLV 11	-349	-272	3995	356.78	-17.45	0.81



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
79	SLV 12	-349	-272	3995	356.78	-17.45	0.81
79	SLV 13	-1082	84	3979	-108.07	-52.3	-0.23
79	SLV 14	-1082	84	3979	-108.07	-52.3	-0.23
79	SLV 15	-1094	-80	3990	106.17	-53.23	0.25
79	SLV 16	-1094	-80	3990	106.17	-53.23	0.25
80	SLU 1	-7	0	2490	0	-0.14	0
80	SLU 2	-7	0	2490	0	-0.14	0
80	SLU 3	-7	0	2490	0	-0.14	0
80	SLU 4	-7	0	2490	0	-0.14	0
80	SLU 5	-7	0	2490	0	-0.14	0
80	SLU 6	-7	0	2490	0	-0.14	0
80	SLU 7	-7	0	2490	0	-0.14	0
80	SLU 8	-7	0	2490	0	-0.14	0
80	SLU 9	-7	0	2490	0	-0.14	0
80	SLU 10	-9	0	3224	0	-0.07	0
80	SLU 11	-9	0	3224	0	-0.07	0
80	SLU 12	-9	0	3224	0	-0.07	0
80	SLU 13	-9	0	3224	0	-0.07	0
80	SLU 14	-9	0	3224	0	-0.07	0
80	SLU 15	-9	0	3224	0	-0.07	0
80	SLU 16	-9	0	3224	0	-0.07	0
80	SLU 17	-9	0	3224	0	-0.07	0
80	SLU 18	-10	0	3538	0.01	-0.04	0
80	SLU 19	-10	0	3538	0.01	-0.04	0
80	SLU 20	-10	0	3538	0.01	-0.04	0
80	SLU 21	-10	0	3538	0.01	-0.04	0
80	SLU 22	-8	0	2931	0	-0.1	0
80	SLU 23	-8	0	2931	0	-0.1	0
80	SLU 24	-8	0	2931	0	-0.1	0
80	SLU 25	-8	0	2931	0	-0.1	0
80	SLU 26	-8	0	2931	0	-0.1	0
80	SLU 27	-8	0	2931	0	-0.1	0
80	SLU 28	-8	0	2931	0	-0.1	0
80	SLU 29	-8	0	2931	0	-0.1	0
80	SLU 30	-8	0	2931	0	-0.1	0
80	SLU 31	-10	0	3664	0.01	-0.03	0
80	SLU 32	-10	0	3664	0.01	-0.03	0
80	SLU 33	-10	0	3664	0.01	-0.03	0
80	SLU 34	-10	0	3664	0.01	-0.03	0
80	SLU 35	-10	0	3664	0.01	-0.03	0
80	SLU 36	-10	0	3664	0.01	-0.03	0
80	SLU 37	-10	0	3664	0.01	-0.03	0
80	SLU 38	-10	0	3664	0.01	-0.03	0
80	SLU 39	-10	0	3978	0.01	0	0
80	SLU 40	-10	0	3978	0.01	0	0
80	SLU 41	-10	0	3978	0.01	0	0
80	SLU 42	-10	0	3978	0.01	0	0
80	SLU 43	-9	0	3087	0	-0.19	0
80	SLU 44	-9	0	3087	0	-0.19	0
80	SLU 45	-9	0	3087	0	-0.19	0
80	SLU 46	-9	0	3087	0	-0.19	0
80	SLU 47	-9	0	3087	0	-0.19	0
80	SLU 48	-9	0	3087	0	-0.19	0
80	SLU 49	-9	0	3087	0	-0.19	0
80	SLU 50	-9	0	3087	0	-0.19	0
80	SLU 51	-9	0	3087	0	-0.19	0
80	SLU 52	-11	0	3820	0.01	-0.12	0
80	SLU 53	-11	0	3820	0.01	-0.12	0
80	SLU 54	-11	0	3820	0.01	-0.12	0
80	SLU 55	-11	0	3820	0.01	-0.12	0
80	SLU 56	-11	0	3820	0.01	-0.12	0
80	SLU 57	-11	0	3820	0.01	-0.12	0
80	SLU 58	-11	0	3820	0.01	-0.12	0
80	SLU 59	-11	0	3820	0.01	-0.12	0
80	SLU 60	-12	0	4134	0.01	-0.1	0
80	SLU 61	-12	0	4134	0.01	-0.1	0
80	SLU 62	-12	0	4134	0.01	-0.1	0
80	SLU 63	-12	0	4134	0.01	-0.1	0
80	SLU 64	-10	0	3527	0	-0.15	0
80	SLU 65	-10	0	3527	0	-0.15	0
80	SLU 66	-10	0	3527	0	-0.15	0
80	SLU 67	-10	0	3527	0	-0.15	0
80	SLU 68	-10	0	3527	0	-0.15	0
80	SLU 69	-10	0	3527	0	-0.15	0
80	SLU 70	-10	0	3527	0	-0.15	0
80	SLU 71	-10	0	3527	0	-0.15	0
80	SLU 72	-10	0	3527	0	-0.15	0
80	SLU 73	-12	0	4260	0.01	-0.08	0
80	SLU 74	-12	0	4260	0.01	-0.08	0
80	SLU 75	-12	0	4260	0.01	-0.08	0
80	SLU 76	-12	0	4260	0.01	-0.08	0
80	SLU 77	-12	0	4260	0.01	-0.08	0
80	SLU 78	-12	0	4260	0.01	-0.08	0
80	SLU 79	-12	0	4260	0.01	-0.08	0
80	SLU 80	-12	0	4260	0.01	-0.08	0
80	SLU 81	-12	0	4574	0.01	-0.06	0
80	SLU 82	-12	0	4574	0.01	-0.06	0
80	SLU 83	-12	0	4574	0.01	-0.06	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
80	SLU 84	-12	0	4574	0.01	-0.06	0
80	SLE RA 1	-8	0	2616	0	-0.12	0
80	SLE RA 2	-8	0	2616	0	-0.12	0
80	SLE RA 3	-8	0	2616	0	-0.12	0
80	SLE RA 4	-8	0	2616	0	-0.12	0
80	SLE RA 5	-8	0	2616	0	-0.12	0
80	SLE RA 6	-8	0	2616	0	-0.12	0
80	SLE RA 7	-8	0	2616	0	-0.12	0
80	SLE RA 8	-8	0	2616	0	-0.12	0
80	SLE RA 9	-8	0	2616	0	-0.12	0
80	SLE RA 10	-9	0	3105	0	-0.08	0
80	SLE RA 11	-9	0	3105	0	-0.08	0
80	SLE RA 12	-9	0	3105	0	-0.08	0
80	SLE RA 13	-9	0	3105	0	-0.08	0
80	SLE RA 14	-9	0	3105	0	-0.08	0
80	SLE RA 15	-9	0	3105	0	-0.08	0
80	SLE RA 16	-9	0	3105	0	-0.08	0
80	SLE RA 17	-9	0	3105	0	-0.08	0
80	SLE RA 18	-9	0	3314	0	-0.06	0
80	SLE RA 19	-9	0	3314	0	-0.06	0
80	SLE RA 20	-9	0	3314	0	-0.06	0
80	SLE RA 21	-9	0	3314	0	-0.06	0
80	SLE FR 1	-8	0	2616	0	-0.12	0
80	SLE FR 2	-8	0	2616	0	-0.12	0
80	SLE FR 3	-8	0	2616	0	-0.12	0
80	SLE FR 4	-8	0	2826	0	-0.11	0
80	SLE FR 5	-8	0	2826	0	-0.11	0
80	SLE FR 6	-8	0	2965	0	-0.09	0
80	SLE QP 1	-8	0	2616	0	-0.12	0
80	SLE QP 2	-8	0	2826	0	-0.11	0
80	SLD 1	470	27	2747	-39.29	22.2	0.04
80	SLD 2	470	27	2747	-39.29	22.2	0.04
80	SLD 3	465	-29	2745	37.51	21.94	-0.04
80	SLD 4	465	-29	2745	37.51	21.94	-0.04
80	SLD 5	144	94	2805	-128.26	6.99	0.13
80	SLD 6	144	94	2805	-128.26	6.99	0.13
80	SLD 7	126	-95	2798	127.73	6.11	-0.13
80	SLD 8	126	-95	2798	127.73	6.11	-0.13
80	SLD 9	-142	95	2853	-127.72	-6.32	0.13
80	SLD 10	-142	95	2853	-127.72	-6.32	0.13
80	SLD 11	-160	-94	2846	128.27	-7.2	-0.13
80	SLD 12	-160	-94	2846	128.27	-7.2	-0.13
80	SLD 13	-481	29	2907	-37.5	-22.15	0.04
80	SLD 14	-481	29	2907	-37.5	-22.15	0.04
80	SLD 15	-487	-27	2905	39.29	-22.41	-0.04
80	SLD 16	-487	-27	2905	39.29	-22.41	-0.04
80	SLV 1	1112	77	2642	-110.39	52.12	0.12
80	SLV 2	1112	77	2642	-110.39	52.12	0.12
80	SLV 3	1100	-82	2637	106.13	51.5	-0.11
80	SLV 4	1100	-82	2637	106.13	51.5	-0.11
80	SLV 5	347	264	2778	-361.5	16.5	0.37
80	SLV 6	347	264	2778	-361.5	16.5	0.37
80	SLV 7	305	-266	2761	360.23	14.44	-0.37
80	SLV 8	305	-266	2761	360.23	14.44	-0.37
80	SLV 9	-321	266	2890	-360.22	-14.65	0.37
80	SLV 10	-321	266	2890	-360.22	-14.65	0.37
80	SLV 11	-363	-264	2873	361.51	-16.71	-0.37
80	SLV 12	-363	-264	2873	361.51	-16.71	-0.37
80	SLV 13	-1116	82	3015	-106.12	-51.71	0.11
80	SLV 14	-1116	82	3015	-106.12	-51.71	0.11
80	SLV 15	-1128	-77	3010	110.4	-52.33	-0.12
80	SLV 16	-1128	-77	3010	110.4	-52.33	-0.12
81	SLU 1	-6	0	2532	0	-0.06	0
81	SLU 2	-6	0	2532	0	-0.06	0
81	SLU 3	-6	0	2532	0	-0.06	0
81	SLU 4	-6	0	2532	0	-0.06	0
81	SLU 5	-6	0	2532	0	-0.06	0
81	SLU 6	-6	0	2532	0	-0.06	0
81	SLU 7	-6	0	2532	0	-0.06	0
81	SLU 8	-6	0	2532	0	-0.06	0
81	SLU 9	-6	0	2532	0	-0.06	0
81	SLU 10	-6	0	3289	0	0.04	0
81	SLU 11	-6	0	3289	0	0.04	0
81	SLU 12	-6	0	3289	0	0.04	0
81	SLU 13	-6	0	3289	0	0.04	0
81	SLU 14	-6	0	3289	0	0.04	0
81	SLU 15	-6	0	3289	0	0.04	0
81	SLU 16	-6	0	3289	0	0.04	0
81	SLU 17	-6	0	3289	0	0.04	0
81	SLU 18	-6	0	3613	0	0.08	0
81	SLU 19	-6	0	3613	0	0.08	0
81	SLU 20	-6	0	3613	0	0.08	0
81	SLU 21	-6	0	3613	0	0.08	0
81	SLU 22	-6	0	2984	0	0	0
81	SLU 23	-6	0	2984	0	0	0
81	SLU 24	-6	0	2984	0	0	0
81	SLU 25	-6	0	2984	0	0	0
81	SLU 26	-6	0	2984	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
81	SLU 27	-6	0	2984	0	0	0
81	SLU 28	-6	0	2984	0	0	0
81	SLU 29	-6	0	2984	0	0	0
81	SLU 30	-6	0	2984	0	0	0
81	SLU 31	-6	0	3741	0	0.1	0
81	SLU 32	-6	0	3741	0	0.1	0
81	SLU 33	-6	0	3741	0	0.1	0
81	SLU 34	-6	0	3741	0	0.1	0
81	SLU 35	-6	0	3741	0	0.1	0
81	SLU 36	-6	0	3741	0	0.1	0
81	SLU 37	-6	0	3741	0	0.1	0
81	SLU 38	-6	0	3741	0	0.1	0
81	SLU 39	-6	0	4065	0	0.15	0
81	SLU 40	-6	0	4065	0	0.15	0
81	SLU 41	-6	0	4065	0	0.15	0
81	SLU 42	-6	0	4065	0	0.15	0
81	SLU 43	-8	0	3136	0	-0.11	0
81	SLU 44	-8	0	3136	0	-0.11	0
81	SLU 45	-8	0	3136	0	-0.11	0
81	SLU 46	-8	0	3136	0	-0.11	0
81	SLU 47	-8	0	3136	0	-0.11	0
81	SLU 48	-8	0	3136	0	-0.11	0
81	SLU 49	-8	0	3136	0	-0.11	0
81	SLU 50	-8	0	3136	0	-0.11	0
81	SLU 51	-8	0	3136	0	-0.11	0
81	SLU 52	-8	0	3893	0	-0.01	0
81	SLU 53	-8	0	3893	0	-0.01	0
81	SLU 54	-8	0	3893	0	-0.01	0
81	SLU 55	-8	0	3893	0	-0.01	0
81	SLU 56	-8	0	3893	0	-0.01	0
81	SLU 57	-8	0	3893	0	-0.01	0
81	SLU 58	-8	0	3893	0	-0.01	0
81	SLU 59	-8	0	3893	0	-0.01	0
81	SLU 60	-8	0	4218	0	0.04	0
81	SLU 61	-8	0	4218	0	0.04	0
81	SLU 62	-8	0	4218	0	0.04	0
81	SLU 63	-8	0	4218	0	0.04	0
81	SLU 64	-8	0	3588	0	-0.04	0
81	SLU 65	-8	0	3588	0	-0.04	0
81	SLU 66	-8	0	3588	0	-0.04	0
81	SLU 67	-8	0	3588	0	-0.04	0
81	SLU 68	-8	0	3588	0	-0.04	0
81	SLU 69	-8	0	3588	0	-0.04	0
81	SLU 70	-8	0	3588	0	-0.04	0
81	SLU 71	-8	0	3588	0	-0.04	0
81	SLU 72	-8	0	3588	0	-0.04	0
81	SLU 73	-8	0	4345	0	0.06	0
81	SLU 74	-8	0	4345	0	0.06	0
81	SLU 75	-8	0	4345	0	0.06	0
81	SLU 76	-8	0	4345	0	0.06	0
81	SLU 77	-8	0	4345	0	0.06	0
81	SLU 78	-8	0	4345	0	0.06	0
81	SLU 79	-8	0	4345	0	0.06	0
81	SLU 80	-8	0	4345	0	0.06	0
81	SLU 81	-8	0	4670	0.01	0.1	0
81	SLU 82	-8	0	4670	0.01	0.1	0
81	SLU 83	-8	0	4670	0.01	0.1	0
81	SLU 84	-8	0	4670	0.01	0.1	0
81	SLE RA 1	-6	0	2661	0	-0.04	0
81	SLE RA 2	-6	0	2661	0	-0.04	0
81	SLE RA 3	-6	0	2661	0	-0.04	0
81	SLE RA 4	-6	0	2661	0	-0.04	0
81	SLE RA 5	-6	0	2661	0	-0.04	0
81	SLE RA 6	-6	0	2661	0	-0.04	0
81	SLE RA 7	-6	0	2661	0	-0.04	0
81	SLE RA 8	-6	0	2661	0	-0.04	0
81	SLE RA 9	-6	0	2661	0	-0.04	0
81	SLE RA 10	-6	0	3166	0	0.02	0
81	SLE RA 11	-6	0	3166	0	0.02	0
81	SLE RA 12	-6	0	3166	0	0.02	0
81	SLE RA 13	-6	0	3166	0	0.02	0
81	SLE RA 14	-6	0	3166	0	0.02	0
81	SLE RA 15	-6	0	3166	0	0.02	0
81	SLE RA 16	-6	0	3166	0	0.02	0
81	SLE RA 17	-6	0	3166	0	0.02	0
81	SLE RA 18	-6	0	3382	0	0.05	0
81	SLE RA 19	-6	0	3382	0	0.05	0
81	SLE RA 20	-6	0	3382	0	0.05	0
81	SLE RA 21	-6	0	3382	0	0.05	0
81	SLE FR 1	-6	0	2661	0	-0.04	0
81	SLE FR 2	-6	0	2661	0	-0.04	0
81	SLE FR 3	-6	0	2661	0	-0.04	0
81	SLE FR 4	-6	0	2877	0	-0.02	0
81	SLE FR 5	-6	0	2877	0	-0.02	0
81	SLE FR 6	-6	0	3021	0	0	0
81	SLE QP 1	-6	0	2661	0	-0.04	0
81	SLE QP 2	-6	0	2877	0	-0.02	0
81	SLD 1	453	23	2734	-37.85	21.18	0.11



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
81	SLD 2	453	23	2734	-37.85	21.18	0.11
81	SLD 3	448	-27	2731	34.75	20.94	-0.1
81	SLD 4	448	-27	2731	34.75	20.94	-0.1
81	SLD 5	140	83	2838	-121.46	6.71	0.35
81	SLD 6	140	83	2838	-121.46	6.71	0.35
81	SLD 7	122	-84	2830	120.53	5.91	-0.34
81	SLD 8	122	-84	2830	120.53	5.91	-0.34
81	SLD 9	-134	84	2924	-120.53	-5.94	0.34
81	SLD 10	-134	84	2924	-120.53	-5.94	0.34
81	SLD 11	-152	-83	2917	121.46	-6.74	-0.35
81	SLD 12	-152	-83	2917	121.46	-6.74	-0.35
81	SLD 13	-460	27	3023	-34.74	-20.97	0.1
81	SLD 14	-460	27	3023	-34.74	-20.97	0.1
81	SLD 15	-465	-23	3021	37.85	-21.21	-0.11
81	SLD 16	-465	-23	3021	37.85	-21.21	-0.11
81	SLV 1	1069	66	2542	-106.08	49.64	0.31
81	SLV 2	1069	66	2542	-106.08	49.64	0.31
81	SLV 3	1057	-75	2536	98.61	49.07	-0.28
81	SLV 4	1057	-75	2536	98.61	49.07	-0.28
81	SLV 5	335	234	2785	-342.28	15.74	0.98
81	SLV 6	335	234	2785	-342.28	15.74	0.98
81	SLV 7	294	-236	2766	340.04	13.85	-0.97
81	SLV 8	294	-236	2766	340.04	13.85	-0.97
81	SLV 9	-306	236	2988	-340.04	-13.88	0.97
81	SLV 10	-306	236	2988	-340.04	-13.88	0.97
81	SLV 11	-347	-234	2969	342.28	-15.77	-0.98
81	SLV 12	-347	-234	2969	342.28	-15.77	-0.98
81	SLV 13	-1069	75	3218	-98.61	-49.1	0.28
81	SLV 14	-1069	75	3218	-98.61	-49.1	0.28
81	SLV 15	-1081	-66	3213	106.09	-49.67	-0.31
81	SLV 16	-1081	-66	3213	106.09	-49.67	-0.31
82	SLU 1	10	0	2590	0	0.94	0
82	SLU 2	10	0	2590	0	0.94	0
82	SLU 3	10	0	2590	0	0.94	0
82	SLU 4	10	0	2590	0	0.94	0
82	SLU 5	10	0	2590	0	0.94	0
82	SLU 6	10	0	2590	0	0.94	0
82	SLU 7	10	0	2590	0	0.94	0
82	SLU 8	10	0	2590	0	0.94	0
82	SLU 9	10	0	2590	0	0.94	0
82	SLU 10	21	0	3380	0	1.78	0
82	SLU 11	21	0	3380	0	1.78	0
82	SLU 12	21	0	3380	0	1.78	0
82	SLU 13	21	0	3380	0	1.78	0
82	SLU 14	21	0	3380	0	1.78	0
82	SLU 15	21	0	3380	0	1.78	0
82	SLU 16	21	0	3380	0	1.78	0
82	SLU 17	21	0	3380	0	1.78	0
82	SLU 18	26	0	3719	0	2.14	0
82	SLU 19	26	0	3719	0	2.14	0
82	SLU 20	26	0	3719	0	2.14	0
82	SLU 21	26	0	3719	0	2.14	0
82	SLU 22	16	0	3058	0	1.38	0
82	SLU 23	16	0	3058	0	1.38	0
82	SLU 24	16	0	3058	0	1.38	0
82	SLU 25	16	0	3058	0	1.38	0
82	SLU 26	16	0	3058	0	1.38	0
82	SLU 27	16	0	3058	0	1.38	0
82	SLU 28	16	0	3058	0	1.38	0
82	SLU 29	16	0	3058	0	1.38	0
82	SLU 30	16	0	3058	0	1.38	0
82	SLU 31	28	0	3848	0	2.22	0
82	SLU 32	28	0	3848	0	2.22	0
82	SLU 33	28	0	3848	0	2.22	0
82	SLU 34	28	0	3848	0	2.22	0
82	SLU 35	28	0	3848	0	2.22	0
82	SLU 36	28	0	3848	0	2.22	0
82	SLU 37	28	0	3848	0	2.22	0
82	SLU 38	28	0	3848	0	2.22	0
82	SLU 39	33	0	4187	0	2.58	0
82	SLU 40	33	0	4187	0	2.58	0
82	SLU 41	33	0	4187	0	2.58	0
82	SLU 42	33	0	4187	0	2.58	0
82	SLU 43	10	0	3207	0	1.06	0
82	SLU 44	10	0	3207	0	1.06	0
82	SLU 45	10	0	3207	0	1.06	0
82	SLU 46	10	0	3207	0	1.06	0
82	SLU 47	10	0	3207	0	1.06	0
82	SLU 48	10	0	3207	0	1.06	0
82	SLU 49	10	0	3207	0	1.06	0
82	SLU 50	10	0	3207	0	1.06	0
82	SLU 51	10	0	3207	0	1.06	0
82	SLU 52	22	0	3997	0	1.9	0
82	SLU 53	22	0	3997	0	1.9	0
82	SLU 54	22	0	3997	0	1.9	0
82	SLU 55	22	0	3997	0	1.9	0
82	SLU 56	22	0	3997	0	1.9	0
82	SLU 57	22	0	3997	0	1.9	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
82	SLU 58	22	0	3997	0	1.9	0
82	SLU 59	22	0	3997	0	1.9	0
82	SLU 60	27	0	4335	0	2.26	0
82	SLU 61	27	0	4335	0	2.26	0
82	SLU 62	27	0	4335	0	2.26	0
82	SLU 63	27	0	4335	0	2.26	0
82	SLU 64	17	0	3675	0	1.51	0
82	SLU 65	17	0	3675	0	1.51	0
82	SLU 66	17	0	3675	0	1.51	0
82	SLU 67	17	0	3675	0	1.51	0
82	SLU 68	17	0	3675	0	1.51	0
82	SLU 69	17	0	3675	0	1.51	0
82	SLU 70	17	0	3675	0	1.51	0
82	SLU 71	17	0	3675	0	1.51	0
82	SLU 72	17	0	3675	0	1.51	0
82	SLU 73	29	0	4465	0	2.35	0
82	SLU 74	29	0	4465	0	2.35	0
82	SLU 75	29	0	4465	0	2.35	0
82	SLU 76	29	0	4465	0	2.35	0
82	SLU 77	29	0	4465	0	2.35	0
82	SLU 78	29	0	4465	0	2.35	0
82	SLU 79	29	0	4465	0	2.35	0
82	SLU 80	29	0	4465	0	2.35	0
82	SLU 81	34	0	4803	0	2.71	0
82	SLU 82	34	0	4803	0	2.71	0
82	SLU 83	34	0	4803	0	2.71	0
82	SLU 84	34	0	4803	0	2.71	0
82	SLE RA 1	12	0	2724	0	1.06	0
82	SLE RA 2	12	0	2724	0	1.06	0
82	SLE RA 3	12	0	2724	0	1.06	0
82	SLE RA 4	12	0	2724	0	1.06	0
82	SLE RA 5	12	0	2724	0	1.06	0
82	SLE RA 6	12	0	2724	0	1.06	0
82	SLE RA 7	12	0	2724	0	1.06	0
82	SLE RA 8	12	0	2724	0	1.06	0
82	SLE RA 9	12	0	2724	0	1.06	0
82	SLE RA 10	19	0	3250	0	1.62	0
82	SLE RA 11	19	0	3250	0	1.62	0
82	SLE RA 12	19	0	3250	0	1.62	0
82	SLE RA 13	19	0	3250	0	1.62	0
82	SLE RA 14	19	0	3250	0	1.62	0
82	SLE RA 15	19	0	3250	0	1.62	0
82	SLE RA 16	19	0	3250	0	1.62	0
82	SLE RA 17	19	0	3250	0	1.62	0
82	SLE RA 18	23	0	3476	0	1.86	0
82	SLE RA 19	23	0	3476	0	1.86	0
82	SLE RA 20	23	0	3476	0	1.86	0
82	SLE RA 21	23	0	3476	0	1.86	0
82	SLE FR 1	12	0	2724	0	1.06	0
82	SLE FR 2	12	0	2724	0	1.06	0
82	SLE FR 3	12	0	2724	0	1.06	0
82	SLE FR 4	15	0	2950	0	1.3	0
82	SLE FR 5	15	0	2950	0	1.3	0
82	SLE FR 6	17	0	3100	0	1.46	0
82	SLE QP 1	12	0	2724	0	1.06	0
82	SLE QP 2	15	0	2950	0	1.3	0
82	SLD 1	454	19	2764	-35.45	21.97	0.13
82	SLD 2	454	19	2764	-35.45	21.97	0.13
82	SLD 3	448	-24	2767	31.36	21.7	-0.1
82	SLD 4	448	-24	2767	31.36	21.7	-0.1
82	SLD 5	155	70	2890	-111.95	7.9	0.38
82	SLD 6	155	70	2890	-111.95	7.9	0.38
82	SLD 7	137	-71	2899	110.73	7.03	-0.38
82	SLD 8	137	-71	2899	110.73	7.03	-0.38
82	SLD 9	-107	71	3001	-110.72	-4.42	0.38
82	SLD 10	-107	71	3001	-110.72	-4.42	0.38
82	SLD 11	-125	-70	3009	111.96	-5.29	-0.38
82	SLD 12	-125	-70	3009	111.96	-5.29	-0.38
82	SLD 13	-419	24	3132	-31.35	-19.1	0.1
82	SLD 14	-419	24	3132	-31.35	-19.1	0.1
82	SLD 15	-424	-19	3135	35.45	-19.36	-0.13
82	SLD 16	-424	-19	3135	35.45	-19.36	-0.13
82	SLV 1	1043	53	2516	-99.12	49.7	0.35
82	SLV 2	1043	53	2516	-99.12	49.7	0.35
82	SLV 3	1030	-66	2522	89.18	49.08	-0.29
82	SLV 4	1030	-66	2522	89.18	49.08	-0.29
82	SLV 5	342	196	2810	-315.33	16.75	1.07
82	SLV 6	342	196	2810	-315.33	16.75	1.07
82	SLV 7	300	-200	2831	312.35	14.7	-1.06
82	SLV 8	300	-200	2831	312.35	14.7	-1.06
82	SLV 9	-271	200	3068	-312.35	-12.1	1.06
82	SLV 10	-271	200	3068	-312.35	-12.1	1.06
82	SLV 11	-313	-196	3089	315.34	-14.15	-1.07
82	SLV 12	-313	-196	3089	315.34	-14.15	-1.07
82	SLV 13	-1001	66	3377	-89.18	-46.48	0.29
82	SLV 14	-1001	66	3377	-89.18	-46.48	0.29
82	SLV 15	-1013	-53	3383	99.13	-47.09	-0.35
82	SLV 16	-1013	-53	3383	99.13	-47.09	-0.35



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
83	SLU 1	35	0	2658	0	1.94	0
83	SLU 2	35	0	2658	0	1.94	0
83	SLU 3	35	0	2658	0	1.94	0
83	SLU 4	35	0	2658	0	1.94	0
83	SLU 5	35	0	2658	0	1.94	0
83	SLU 6	35	0	2658	0	1.94	0
83	SLU 7	35	0	2658	0	1.94	0
83	SLU 8	35	0	2658	0	1.94	0
83	SLU 9	35	0	2658	0	1.94	0
83	SLU 10	64	0	3484	0	3.43	0
83	SLU 11	64	0	3484	0	3.43	0
83	SLU 12	64	0	3484	0	3.43	0
83	SLU 13	64	0	3484	0	3.43	0
83	SLU 14	64	0	3484	0	3.43	0
83	SLU 15	64	0	3484	0	3.43	0
83	SLU 16	64	0	3484	0	3.43	0
83	SLU 17	64	0	3484	0	3.43	0
83	SLU 18	76	0	3838	0	4.06	0
83	SLU 19	76	0	3838	0	4.06	0
83	SLU 20	76	0	3838	0	4.06	0
83	SLU 21	76	0	3838	0	4.06	0
83	SLU 22	50	0	3144	0	2.71	0
83	SLU 23	50	0	3144	0	2.71	0
83	SLU 24	50	0	3144	0	2.71	0
83	SLU 25	50	0	3144	0	2.71	0
83	SLU 26	50	0	3144	0	2.71	0
83	SLU 27	50	0	3144	0	2.71	0
83	SLU 28	50	0	3144	0	2.71	0
83	SLU 29	50	0	3144	0	2.71	0
83	SLU 30	50	0	3144	0	2.71	0
83	SLU 31	79	0	3970	0	4.19	0
83	SLU 32	79	0	3970	0	4.19	0
83	SLU 33	79	0	3970	0	4.19	0
83	SLU 34	79	0	3970	0	4.19	0
83	SLU 35	79	0	3970	0	4.19	0
83	SLU 36	79	0	3970	0	4.19	0
83	SLU 37	79	0	3970	0	4.19	0
83	SLU 38	79	0	3970	0	4.19	0
83	SLU 39	91	0	4324	0	4.83	0
83	SLU 40	91	0	4324	0	4.83	0
83	SLU 41	91	0	4324	0	4.83	0
83	SLU 42	91	0	4324	0	4.83	0
83	SLU 43	40	0	3290	0	2.26	0
83	SLU 44	40	0	3290	0	2.26	0
83	SLU 45	40	0	3290	0	2.26	0
83	SLU 46	40	0	3290	0	2.26	0
83	SLU 47	40	0	3290	0	2.26	0
83	SLU 48	40	0	3290	0	2.26	0
83	SLU 49	40	0	3290	0	2.26	0
83	SLU 50	40	0	3290	0	2.26	0
83	SLU 51	40	0	3290	0	2.26	0
83	SLU 52	69	0	4115	0	3.75	0
83	SLU 53	69	0	4115	0	3.75	0
83	SLU 54	69	0	4115	0	3.75	0
83	SLU 55	69	0	4115	0	3.75	0
83	SLU 56	69	0	4115	0	3.75	0
83	SLU 57	69	0	4115	0	3.75	0
83	SLU 58	69	0	4115	0	3.75	0
83	SLU 59	69	0	4115	0	3.75	0
83	SLU 60	82	0	4469	0	4.38	0
83	SLU 61	82	0	4469	0	4.38	0
83	SLU 62	82	0	4469	0	4.38	0
83	SLU 63	82	0	4469	0	4.38	0
83	SLU 64	55	0	3775	0	3.03	0
83	SLU 65	55	0	3775	0	3.03	0
83	SLU 66	55	0	3775	0	3.03	0
83	SLU 67	55	0	3775	0	3.03	0
83	SLU 68	55	0	3775	0	3.03	0
83	SLU 69	55	0	3775	0	3.03	0
83	SLU 70	55	0	3775	0	3.03	0
83	SLU 71	55	0	3775	0	3.03	0
83	SLU 72	55	0	3775	0	3.03	0
83	SLU 73	84	0	4601	0	4.51	0
83	SLU 74	84	0	4601	0	4.51	0
83	SLU 75	84	0	4601	0	4.51	0
83	SLU 76	84	0	4601	0	4.51	0
83	SLU 77	84	0	4601	0	4.51	0
83	SLU 78	84	0	4601	0	4.51	0
83	SLU 79	84	0	4601	0	4.51	0
83	SLU 80	84	0	4601	0	4.51	0
83	SLU 81	97	0	4955	0	5.15	0
83	SLU 82	97	0	4955	0	5.15	0
83	SLU 83	97	0	4955	0	5.15	0
83	SLU 84	97	0	4955	0	5.15	0
83	SLE RA 1	39	0	2797	0	2.16	0
83	SLE RA 2	39	0	2797	0	2.16	0
83	SLE RA 3	39	0	2797	0	2.16	0
83	SLE RA 4	39	0	2797	0	2.16	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
83	SLE RA 5	39	0	2797	0	2.16	0
83	SLE RA 6	39	0	2797	0	2.16	0
83	SLE RA 7	39	0	2797	0	2.16	0
83	SLE RA 8	39	0	2797	0	2.16	0
83	SLE RA 9	39	0	2797	0	2.16	0
83	SLE RA 10	59	0	3348	0	3.15	0
83	SLE RA 11	59	0	3348	0	3.15	0
83	SLE RA 12	59	0	3348	0	3.15	0
83	SLE RA 13	59	0	3348	0	3.15	0
83	SLE RA 14	59	0	3348	0	3.15	0
83	SLE RA 15	59	0	3348	0	3.15	0
83	SLE RA 16	59	0	3348	0	3.15	0
83	SLE RA 17	59	0	3348	0	3.15	0
83	SLE RA 18	67	0	3584	0	3.57	0
83	SLE RA 19	67	0	3584	0	3.57	0
83	SLE RA 20	67	0	3584	0	3.57	0
83	SLE RA 21	67	0	3584	0	3.57	0
83	SLE FR 1	39	0	2797	0	2.16	0
83	SLE FR 2	39	0	2797	0	2.16	0
83	SLE FR 3	39	0	2797	0	2.16	0
83	SLE FR 4	48	0	3033	0	2.58	0
83	SLE FR 5	48	0	3033	0	2.58	0
83	SLE FR 6	53	0	3190	0	2.87	0
83	SLE QP 1	39	0	2797	0	2.16	0
83	SLE QP 2	48	0	3033	0	2.58	0
83	SLD 1	460	15	2838	-32.61	21.99	0.11
83	SLD 2	460	15	2838	-32.61	21.99	0.11
83	SLD 3	455	-21	2840	28	21.75	-0.08
83	SLD 4	455	-21	2840	28	21.75	-0.08
83	SLD 5	179	58	2970	-101.7	8.77	0.33
83	SLD 6	179	58	2970	-101.7	8.77	0.33
83	SLD 7	162	-60	2979	100.32	7.97	-0.32
83	SLD 8	162	-60	2979	100.32	7.97	-0.32
83	SLD 9	-67	60	3087	-100.31	-2.8	0.32
83	SLD 10	-67	60	3087	-100.31	-2.8	0.32
83	SLD 11	-84	-58	3096	101.7	-3.6	-0.33
83	SLD 12	-84	-58	3096	101.7	-3.6	-0.33
83	SLD 13	-360	21	3226	-27.99	-16.58	0.08
83	SLD 14	-360	21	3226	-27.99	-16.58	0.08
83	SLD 15	-365	-15	3229	32.61	-16.82	-0.11
83	SLD 16	-365	-15	3229	32.61	-16.82	-0.11
83	SLV 1	1015	43	2576	-90.99	48.07	0.3
83	SLV 2	1015	43	2576	-90.99	48.07	0.3
83	SLV 3	1003	-56	2582	79.64	47.49	-0.24
83	SLV 4	1003	-56	2582	79.64	47.49	-0.24
83	SLV 5	357	163	2886	-286.08	17.1	0.91
83	SLV 6	357	163	2886	-286.08	17.1	0.91
83	SLV 7	315	-167	2907	282.68	15.19	-0.89
83	SLV 8	315	-167	2907	282.68	15.19	-0.89
83	SLV 9	-220	167	3159	-282.67	-10.02	0.89
83	SLV 10	-220	167	3159	-282.67	-10.02	0.89
83	SLV 11	-261	-163	3180	286.08	-11.93	-0.91
83	SLV 12	-261	-163	3180	286.08	-11.93	-0.91
83	SLV 13	-908	56	3484	-79.64	-42.32	0.24
83	SLV 14	-908	56	3484	-79.64	-42.32	0.24
83	SLV 15	-920	-43	3491	90.99	-42.9	-0.3
83	SLV 16	-920	-43	3491	90.99	-42.9	-0.3
84	SLU 1	76	0	2729	0	4.14	0
84	SLU 2	76	0	2729	0	4.14	0
84	SLU 3	76	0	2729	0	4.14	0
84	SLU 4	76	0	2729	0	4.14	0
84	SLU 5	76	0	2729	0	4.14	0
84	SLU 6	76	0	2729	0	4.14	0
84	SLU 7	76	0	2729	0	4.14	0
84	SLU 8	76	0	2729	0	4.14	0
84	SLU 9	76	0	2729	0	4.14	0
84	SLU 10	132	0	3588	0	7.06	0
84	SLU 11	132	0	3588	0	7.06	0
84	SLU 12	132	0	3588	0	7.06	0
84	SLU 13	132	0	3588	0	7.06	0
84	SLU 14	132	0	3588	0	7.06	0
84	SLU 15	132	0	3588	0	7.06	0
84	SLU 16	132	0	3588	0	7.06	0
84	SLU 17	132	0	3588	0	7.06	0
84	SLU 18	155	0	3956	0	8.32	0
84	SLU 19	155	0	3956	0	8.32	0
84	SLU 20	155	0	3956	0	8.32	0
84	SLU 21	155	0	3956	0	8.32	0
84	SLU 22	104	0	3231	0	5.62	0
84	SLU 23	104	0	3231	0	5.62	0
84	SLU 24	104	0	3231	0	5.62	0
84	SLU 25	104	0	3231	0	5.62	0
84	SLU 26	104	0	3231	0	5.62	0
84	SLU 27	104	0	3231	0	5.62	0
84	SLU 28	104	0	3231	0	5.62	0
84	SLU 29	104	0	3231	0	5.62	0
84	SLU 30	104	0	3231	0	5.62	0
84	SLU 31	160	0	4090	0	8.54	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
84	SLU 32	160	0	4090	0	8.54	0
84	SLU 33	160	0	4090	0	8.54	0
84	SLU 34	160	0	4090	0	8.54	0
84	SLU 35	160	0	4090	0	8.54	0
84	SLU 36	160	0	4090	0	8.54	0
84	SLU 37	160	0	4090	0	8.54	0
84	SLU 38	160	0	4090	0	8.54	0
84	SLU 39	184	0	4458	0	9.79	0
84	SLU 40	184	0	4458	0	9.79	0
84	SLU 41	184	0	4458	0	9.79	0
84	SLU 42	184	0	4458	0	9.79	0
84	SLU 43	89	0	3375	0	4.88	0
84	SLU 44	89	0	3375	0	4.88	0
84	SLU 45	89	0	3375	0	4.88	0
84	SLU 46	89	0	3375	0	4.88	0
84	SLU 47	89	0	3375	0	4.88	0
84	SLU 48	89	0	3375	0	4.88	0
84	SLU 49	89	0	3375	0	4.88	0
84	SLU 50	89	0	3375	0	4.88	0
84	SLU 51	89	0	3375	0	4.88	0
84	SLU 52	145	0	4235	0	7.8	0
84	SLU 53	145	0	4235	0	7.8	0
84	SLU 54	145	0	4235	0	7.8	0
84	SLU 55	145	0	4235	0	7.8	0
84	SLU 56	145	0	4235	0	7.8	0
84	SLU 57	145	0	4235	0	7.8	0
84	SLU 58	145	0	4235	0	7.8	0
84	SLU 59	145	0	4235	0	7.8	0
84	SLU 60	169	0	4603	0	9.05	0
84	SLU 61	169	0	4603	0	9.05	0
84	SLU 62	169	0	4603	0	9.05	0
84	SLU 63	169	0	4603	0	9.05	0
84	SLU 64	117	0	3877	0	6.36	0
84	SLU 65	117	0	3877	0	6.36	0
84	SLU 66	117	0	3877	0	6.36	0
84	SLU 67	117	0	3877	0	6.36	0
84	SLU 68	117	0	3877	0	6.36	0
84	SLU 69	117	0	3877	0	6.36	0
84	SLU 70	117	0	3877	0	6.36	0
84	SLU 71	117	0	3877	0	6.36	0
84	SLU 72	117	0	3877	0	6.36	0
84	SLU 73	173	0	4737	0	9.28	0
84	SLU 74	173	0	4737	0	9.28	0
84	SLU 75	173	0	4737	0	9.28	0
84	SLU 76	173	0	4737	0	9.28	0
84	SLU 77	173	0	4737	0	9.28	0
84	SLU 78	173	0	4737	0	9.28	0
84	SLU 79	173	0	4737	0	9.28	0
84	SLU 80	173	0	4737	0	9.28	0
84	SLU 81	197	0	5105	0	10.53	0
84	SLU 82	197	0	5105	0	10.53	0
84	SLU 83	197	0	5105	0	10.53	0
84	SLU 84	197	0	5105	0	10.53	0
84	SLE RA 1	84	0	2872	0	4.57	0
84	SLE RA 2	84	0	2872	0	4.57	0
84	SLE RA 3	84	0	2872	0	4.57	0
84	SLE RA 4	84	0	2872	0	4.57	0
84	SLE RA 5	84	0	2872	0	4.57	0
84	SLE RA 6	84	0	2872	0	4.57	0
84	SLE RA 7	84	0	2872	0	4.57	0
84	SLE RA 8	84	0	2872	0	4.57	0
84	SLE RA 9	84	0	2872	0	4.57	0
84	SLE RA 10	121	0	3445	0	6.51	0
84	SLE RA 11	121	0	3445	0	6.51	0
84	SLE RA 12	121	0	3445	0	6.51	0
84	SLE RA 13	121	0	3445	0	6.51	0
84	SLE RA 14	121	0	3445	0	6.51	0
84	SLE RA 15	121	0	3445	0	6.51	0
84	SLE RA 16	121	0	3445	0	6.51	0
84	SLE RA 17	121	0	3445	0	6.51	0
84	SLE RA 18	137	0	3691	0	7.35	0
84	SLE RA 19	137	0	3691	0	7.35	0
84	SLE RA 20	137	0	3691	0	7.35	0
84	SLE RA 21	137	0	3691	0	7.35	0
84	SLE FR 1	84	0	2872	0	4.57	0
84	SLE FR 2	84	0	2872	0	4.57	0
84	SLE FR 3	84	0	2872	0	4.57	0
84	SLE FR 4	100	0	3118	0	5.4	0
84	SLE FR 5	100	0	3118	0	5.4	0
84	SLE FR 6	111	0	3281	0	5.96	0
84	SLE QP 1	84	0	2872	0	4.57	0
84	SLE QP 2	100	0	3118	0	5.4	0
84	SLD 1	491	13	2943	-29.75	24.11	0.09
84	SLD 2	491	13	2943	-29.75	24.11	0.09
84	SLD 3	486	-18	2945	25.01	23.85	-0.06
84	SLD 4	486	-18	2945	25.01	23.85	-0.06
84	SLD 5	225	51	3061	-91.98	11.4	0.26
84	SLD 6	225	51	3061	-91.98	11.4	0.26



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
84	SLD 7	208	-52	3070	90.56	10.55	-0.25
84	SLD 8	208	-52	3070	90.56	10.55	-0.25
84	SLD 9	-8	52	3165	-90.56	0.25	0.25
84	SLD 10	-8	52	3165	-90.56	0.25	0.25
84	SLD 11	-26	-51	3174	91.99	-0.6	-0.26
84	SLD 12	-26	-51	3174	91.99	-0.6	-0.26
84	SLD 13	-286	18	3290	-25.01	-13.05	0.06
84	SLD 14	-286	18	3290	-25.01	-13.05	0.06
84	SLD 15	-291	-13	3292	29.76	-13.31	-0.09
84	SLD 16	-291	-13	3292	29.76	-13.31	-0.09
84	SLV 1	1017	36	2709	-82.83	49.23	0.24
84	SLV 2	1017	36	2709	-82.83	49.23	0.24
84	SLV 3	1004	-49	2715	70.95	48.63	-0.18
84	SLV 4	1004	-49	2715	70.95	48.63	-0.18
84	SLV 5	394	141	2986	-258.08	19.46	0.71
84	SLV 6	394	141	2986	-258.08	19.46	0.71
84	SLV 7	352	-145	3006	254.52	17.46	-0.69
84	SLV 8	352	-145	3006	254.52	17.46	-0.69
84	SLV 9	-152	145	3229	-254.52	-6.66	0.69
84	SLV 10	-152	145	3229	-254.52	-6.66	0.69
84	SLV 11	-194	-141	3250	258.09	-8.66	-0.71
84	SLV 12	-194	-141	3250	258.09	-8.66	-0.71
84	SLV 13	-804	49	3520	-70.95	-37.83	0.18
84	SLV 14	-804	49	3520	-70.95	-37.83	0.18
84	SLV 15	-817	-36	3527	82.83	-38.43	-0.24
84	SLV 16	-817	-36	3527	82.83	-38.43	-0.24
85	SLU 1	120	0	2800	0	5.98	0
85	SLU 2	120	0	2800	0	5.98	0
85	SLU 3	120	0	2800	0	5.98	0
85	SLU 4	120	0	2800	0	5.98	0
85	SLU 5	120	0	2800	0	5.98	0
85	SLU 6	120	0	2800	0	5.98	0
85	SLU 7	120	0	2800	0	5.98	0
85	SLU 8	120	0	2800	0	5.98	0
85	SLU 9	120	0	2800	0	5.98	0
85	SLU 10	201	0	3690	0	9.86	0
85	SLU 11	201	0	3690	0	9.86	0
85	SLU 12	201	0	3690	0	9.86	0
85	SLU 13	201	0	3690	0	9.86	0
85	SLU 14	201	0	3690	0	9.86	0
85	SLU 15	201	0	3690	0	9.86	0
85	SLU 16	201	0	3690	0	9.86	0
85	SLU 17	201	0	3690	0	9.86	0
85	SLU 18	236	0	4072	0	11.52	0
85	SLU 19	236	0	4072	0	11.52	0
85	SLU 20	236	0	4072	0	11.52	0
85	SLU 21	236	0	4072	0	11.52	0
85	SLU 22	161	0	3317	0	7.94	0
85	SLU 23	161	0	3317	0	7.94	0
85	SLU 24	161	0	3317	0	7.94	0
85	SLU 25	161	0	3317	0	7.94	0
85	SLU 26	161	0	3317	0	7.94	0
85	SLU 27	161	0	3317	0	7.94	0
85	SLU 28	161	0	3317	0	7.94	0
85	SLU 29	161	0	3317	0	7.94	0
85	SLU 30	161	0	3317	0	7.94	0
85	SLU 31	242	0	4207	0	11.82	0
85	SLU 32	242	0	4207	0	11.82	0
85	SLU 33	242	0	4207	0	11.82	0
85	SLU 34	242	0	4207	0	11.82	0
85	SLU 35	242	0	4207	0	11.82	0
85	SLU 36	242	0	4207	0	11.82	0
85	SLU 37	242	0	4207	0	11.82	0
85	SLU 38	242	0	4207	0	11.82	0
85	SLU 39	277	0	4589	0	13.48	0
85	SLU 40	277	0	4589	0	13.48	0
85	SLU 41	277	0	4589	0	13.48	0
85	SLU 42	277	0	4589	0	13.48	0
85	SLU 43	143	0	3463	0	7.1	0
85	SLU 44	143	0	3463	0	7.1	0
85	SLU 45	143	0	3463	0	7.1	0
85	SLU 46	143	0	3463	0	7.1	0
85	SLU 47	143	0	3463	0	7.1	0
85	SLU 48	143	0	3463	0	7.1	0
85	SLU 49	143	0	3463	0	7.1	0
85	SLU 50	143	0	3463	0	7.1	0
85	SLU 51	143	0	3463	0	7.1	0
85	SLU 52	224	0	4353	0	10.97	0
85	SLU 53	224	0	4353	0	10.97	0
85	SLU 54	224	0	4353	0	10.97	0
85	SLU 55	224	0	4353	0	10.97	0
85	SLU 56	224	0	4353	0	10.97	0
85	SLU 57	224	0	4353	0	10.97	0
85	SLU 58	224	0	4353	0	10.97	0
85	SLU 59	224	0	4353	0	10.97	0
85	SLU 60	258	0	4735	0	12.64	0
85	SLU 61	258	0	4735	0	12.64	0
85	SLU 62	258	0	4735	0	12.64	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
85	SLU 63	258	0	4735	0	12.64	0
85	SLU 64	184	0	3980	0	9.06	0
85	SLU 65	184	0	3980	0	9.06	0
85	SLU 66	184	0	3980	0	9.06	0
85	SLU 67	184	0	3980	0	9.06	0
85	SLU 68	184	0	3980	0	9.06	0
85	SLU 69	184	0	3980	0	9.06	0
85	SLU 70	184	0	3980	0	9.06	0
85	SLU 71	184	0	3980	0	9.06	0
85	SLU 72	184	0	3980	0	9.06	0
85	SLU 73	265	0	4870	0	12.94	0
85	SLU 74	265	0	4870	0	12.94	0
85	SLU 75	265	0	4870	0	12.94	0
85	SLU 76	265	0	4870	0	12.94	0
85	SLU 77	265	0	4870	0	12.94	0
85	SLU 78	265	0	4870	0	12.94	0
85	SLU 79	265	0	4870	0	12.94	0
85	SLU 80	265	0	4870	0	12.94	0
85	SLU 81	299	0	5252	0	14.6	0
85	SLU 82	299	0	5252	0	14.6	0
85	SLU 83	299	0	5252	0	14.6	0
85	SLU 84	299	0	5252	0	14.6	0
85	SLE RA 1	132	0	2948	0	6.54	0
85	SLE RA 2	132	0	2948	0	6.54	0
85	SLE RA 3	132	0	2948	0	6.54	0
85	SLE RA 4	132	0	2948	0	6.54	0
85	SLE RA 5	132	0	2948	0	6.54	0
85	SLE RA 6	132	0	2948	0	6.54	0
85	SLE RA 7	132	0	2948	0	6.54	0
85	SLE RA 8	132	0	2948	0	6.54	0
85	SLE RA 9	132	0	2948	0	6.54	0
85	SLE RA 10	186	0	3541	0	9.12	0
85	SLE RA 11	186	0	3541	0	9.12	0
85	SLE RA 12	186	0	3541	0	9.12	0
85	SLE RA 13	186	0	3541	0	9.12	0
85	SLE RA 14	186	0	3541	0	9.12	0
85	SLE RA 15	186	0	3541	0	9.12	0
85	SLE RA 16	186	0	3541	0	9.12	0
85	SLE RA 17	186	0	3541	0	9.12	0
85	SLE RA 18	209	0	3796	0	10.23	0
85	SLE RA 19	209	0	3796	0	10.23	0
85	SLE RA 20	209	0	3796	0	10.23	0
85	SLE RA 21	209	0	3796	0	10.23	0
85	SLE FR 1	132	0	2948	0	6.54	0
85	SLE FR 2	132	0	2948	0	6.54	0
85	SLE FR 3	132	0	2948	0	6.54	0
85	SLE FR 4	155	0	3202	0	7.65	0
85	SLE FR 5	155	0	3202	0	7.65	0
85	SLE FR 6	171	0	3372	0	8.39	0
85	SLE QP 1	132	0	2948	0	6.54	0
85	SLE QP 2	155	0	3202	0	7.65	0
85	SLD 1	524	12	3078	-27.12	25.27	0.07
85	SLD 2	524	12	3078	-27.12	25.27	0.07
85	SLD 3	519	-17	3076	22.38	25.03	-0.05
85	SLD 4	519	-17	3076	22.38	25.03	-0.05
85	SLD 5	274	47	3169	-83.21	13.3	0.2
85	SLD 6	274	47	3169	-83.21	13.3	0.2
85	SLD 7	256	-48	3161	81.78	12.49	-0.19
85	SLD 8	256	-48	3161	81.78	12.49	-0.19
85	SLD 9	54	48	3244	-81.78	2.8	0.19
85	SLD 10	54	48	3244	-81.78	2.8	0.19
85	SLD 11	37	-47	3236	83.21	1.99	-0.2
85	SLD 12	37	-47	3236	83.21	1.99	-0.2
85	SLD 13	-208	17	3329	-22.38	-9.74	0.05
85	SLD 14	-208	17	3329	-22.38	-9.74	0.05
85	SLD 15	-213	-12	3326	27.12	-9.98	-0.07
85	SLD 16	-213	-12	3326	27.12	-9.98	-0.07
85	SLV 1	1019	33	2912	-75.23	48.98	0.18
85	SLV 2	1019	33	2912	-75.23	48.98	0.18
85	SLV 3	1007	-45	2906	63.16	48.41	-0.14
85	SLV 4	1007	-45	2906	63.16	48.41	-0.14
85	SLV 5	433	129	3124	-232.46	20.92	0.54
85	SLV 6	433	129	3124	-232.46	20.92	0.54
85	SLV 7	392	-133	3105	228.84	19.01	-0.52
85	SLV 8	392	-133	3105	228.84	19.01	-0.52
85	SLV 9	-82	133	3300	-228.84	-3.71	0.52
85	SLV 10	-82	133	3300	-228.84	-3.71	0.52
85	SLV 11	-122	-129	3281	232.46	-5.62	-0.54
85	SLV 12	-122	-129	3281	232.46	-5.62	-0.54
85	SLV 13	-696	45	3499	-63.16	-33.11	0.14
85	SLV 14	-696	45	3499	-63.16	-33.11	0.14
85	SLV 15	-709	-33	3493	75.23	-33.69	-0.18
85	SLV 16	-709	-33	3493	75.23	-33.69	-0.18
86	SLU 1	178	0	2877	0	9	0
86	SLU 2	178	0	2877	0	9	0
86	SLU 3	178	0	2877	0	9	0
86	SLU 4	178	0	2877	0	9	0
86	SLU 5	178	0	2877	0	9	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
86	SLU 6	178	0	2877	0	9	0
86	SLU 7	178	0	2877	0	9	0
86	SLU 8	178	0	2877	0	9	0
86	SLU 9	178	0	2877	0	9	0
86	SLU 10	287	0	3798	0	14.48	0
86	SLU 11	287	0	3798	0	14.48	0
86	SLU 12	287	0	3798	0	14.48	0
86	SLU 13	287	0	3798	0	14.48	0
86	SLU 14	287	0	3798	0	14.48	0
86	SLU 15	287	0	3798	0	14.48	0
86	SLU 16	287	0	3798	0	14.48	0
86	SLU 17	287	0	3798	0	14.48	0
86	SLU 18	334	0	4192	0	16.84	0
86	SLU 19	334	0	4192	0	16.84	0
86	SLU 20	334	0	4192	0	16.84	0
86	SLU 21	334	0	4192	0	16.84	0
86	SLU 22	233	0	3409	0	11.78	0
86	SLU 23	233	0	3409	0	11.78	0
86	SLU 24	233	0	3409	0	11.78	0
86	SLU 25	233	0	3409	0	11.78	0
86	SLU 26	233	0	3409	0	11.78	0
86	SLU 27	233	0	3409	0	11.78	0
86	SLU 28	233	0	3409	0	11.78	0
86	SLU 29	233	0	3409	0	11.78	0
86	SLU 30	233	0	3409	0	11.78	0
86	SLU 31	343	0	4330	0	17.27	0
86	SLU 32	343	0	4330	0	17.27	0
86	SLU 33	343	0	4330	0	17.27	0
86	SLU 34	343	0	4330	0	17.27	0
86	SLU 35	343	0	4330	0	17.27	0
86	SLU 36	343	0	4330	0	17.27	0
86	SLU 37	343	0	4330	0	17.27	0
86	SLU 38	343	0	4330	0	17.27	0
86	SLU 39	390	0	4725	0	19.62	0
86	SLU 40	390	0	4725	0	19.62	0
86	SLU 41	390	0	4725	0	19.62	0
86	SLU 42	390	0	4725	0	19.62	0
86	SLU 43	212	0	3557	0	10.74	0
86	SLU 44	212	0	3557	0	10.74	0
86	SLU 45	212	0	3557	0	10.74	0
86	SLU 46	212	0	3557	0	10.74	0
86	SLU 47	212	0	3557	0	10.74	0
86	SLU 48	212	0	3557	0	10.74	0
86	SLU 49	212	0	3557	0	10.74	0
86	SLU 50	212	0	3557	0	10.74	0
86	SLU 51	212	0	3557	0	10.74	0
86	SLU 52	322	0	4478	0	16.23	0
86	SLU 53	322	0	4478	0	16.23	0
86	SLU 54	322	0	4478	0	16.23	0
86	SLU 55	322	0	4478	0	16.23	0
86	SLU 56	322	0	4478	0	16.23	0
86	SLU 57	322	0	4478	0	16.23	0
86	SLU 58	322	0	4478	0	16.23	0
86	SLU 59	322	0	4478	0	16.23	0
86	SLU 60	368	0	4873	0	18.58	0
86	SLU 61	368	0	4873	0	18.58	0
86	SLU 62	368	0	4873	0	18.58	0
86	SLU 63	368	0	4873	0	18.58	0
86	SLU 64	268	0	4090	0	13.52	0
86	SLU 65	268	0	4090	0	13.52	0
86	SLU 66	268	0	4090	0	13.52	0
86	SLU 67	268	0	4090	0	13.52	0
86	SLU 68	268	0	4090	0	13.52	0
86	SLU 69	268	0	4090	0	13.52	0
86	SLU 70	268	0	4090	0	13.52	0
86	SLU 71	268	0	4090	0	13.52	0
86	SLU 72	268	0	4090	0	13.52	0
86	SLU 73	377	0	5011	0	19.01	0
86	SLU 74	377	0	5011	0	19.01	0
86	SLU 75	377	0	5011	0	19.01	0
86	SLU 76	377	0	5011	0	19.01	0
86	SLU 77	377	0	5011	0	19.01	0
86	SLU 78	377	0	5011	0	19.01	0
86	SLU 79	377	0	5011	0	19.01	0
86	SLU 80	377	0	5011	0	19.01	0
86	SLU 81	424	0	5405	0	21.36	0
86	SLU 82	424	0	5405	0	21.36	0
86	SLU 83	424	0	5405	0	21.36	0
86	SLU 84	424	0	5405	0	21.36	0
86	SLE RA 1	194	0	3029	0	9.79	0
86	SLE RA 2	194	0	3029	0	9.79	0
86	SLE RA 3	194	0	3029	0	9.79	0
86	SLE RA 4	194	0	3029	0	9.79	0
86	SLE RA 5	194	0	3029	0	9.79	0
86	SLE RA 6	194	0	3029	0	9.79	0
86	SLE RA 7	194	0	3029	0	9.79	0
86	SLE RA 8	194	0	3029	0	9.79	0
86	SLE RA 9	194	0	3029	0	9.79	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
86	SLE RA 10	267	0	3643	0	13.45	0
86	SLE RA 11	267	0	3643	0	13.45	0
86	SLE RA 12	267	0	3643	0	13.45	0
86	SLE RA 13	267	0	3643	0	13.45	0
86	SLE RA 14	267	0	3643	0	13.45	0
86	SLE RA 15	267	0	3643	0	13.45	0
86	SLE RA 16	267	0	3643	0	13.45	0
86	SLE RA 17	267	0	3643	0	13.45	0
86	SLE RA 18	298	0	3906	0	15.02	0
86	SLE RA 19	298	0	3906	0	15.02	0
86	SLE RA 20	298	0	3906	0	15.02	0
86	SLE RA 21	298	0	3906	0	15.02	0
86	SLE FR 1	194	0	3029	0	9.79	0
86	SLE FR 2	194	0	3029	0	9.79	0
86	SLE FR 3	194	0	3029	0	9.79	0
86	SLE FR 4	225	0	3292	0	11.36	0
86	SLE FR 5	225	0	3292	0	11.36	0
86	SLE FR 6	246	0	3467	0	12.4	0
86	SLE QP 1	194	0	3029	0	9.79	0
86	SLE QP 2	225	0	3292	0	11.36	0
86	SLD 1	570	11	3226	-24.71	28.32	0.05
86	SLD 2	570	11	3226	-24.71	28.32	0.05
86	SLD 3	565	-16	3224	19.86	28.08	-0.04
86	SLD 4	565	-16	3224	19.86	28.08	-0.04
86	SLD 5	336	45	3276	-75.02	16.82	0.15
86	SLD 6	336	45	3276	-75.02	16.82	0.15
86	SLD 7	319	-47	3268	73.57	16	-0.14
86	SLD 8	319	-47	3268	73.57	16	-0.14
86	SLD 9	131	47	3316	-73.57	6.71	0.14
86	SLD 10	131	47	3316	-73.57	6.71	0.14
86	SLD 11	114	-45	3308	75.02	5.9	-0.15
86	SLD 12	114	-45	3308	75.02	5.9	-0.15
86	SLD 13	-115	16	3360	-19.86	-5.36	0.04
86	SLD 14	-115	16	3360	-19.86	-5.36	0.04
86	SLD 15	-120	-12	3358	24.71	-5.6	-0.05
86	SLD 16	-120	-12	3358	24.71	-5.6	-0.05
86	SLV 1	1034	31	3137	-68.13	51.11	0.14
86	SLV 2	1034	31	3137	-68.13	51.11	0.14
86	SLV 3	1022	-43	3132	55.72	50.54	-0.1
86	SLV 4	1022	-43	3132	55.72	50.54	-0.1
86	SLV 5	486	123	3254	-208.27	24.16	0.4
86	SLV 6	486	123	3254	-208.27	24.16	0.4
86	SLV 7	446	-127	3236	204.54	22.24	-0.39
86	SLV 8	446	-127	3236	204.54	22.24	-0.39
86	SLV 9	4	127	3348	-204.54	0.48	0.39
86	SLV 10	4	127	3348	-204.54	0.48	0.39
86	SLV 11	-36	-123	3330	208.27	-1.44	-0.4
86	SLV 12	-36	-123	3330	208.27	-1.44	-0.4
86	SLV 13	-572	43	3452	-55.72	-27.82	0.1
86	SLV 14	-572	43	3452	-55.72	-27.82	0.1
86	SLV 15	-584	-32	3447	68.13	-28.39	-0.14
86	SLV 16	-584	-32	3447	68.13	-28.39	-0.14
87	SLU 1	242	0	2968	0	11.88	0
87	SLU 2	242	0	2968	0	11.88	0
87	SLU 3	242	0	2968	0	11.88	0
87	SLU 4	242	0	2968	0	11.88	0
87	SLU 5	242	0	2968	0	11.88	0
87	SLU 6	242	0	2968	0	11.88	0
87	SLU 7	242	0	2968	0	11.88	0
87	SLU 8	242	0	2968	0	11.88	0
87	SLU 9	242	0	2968	0	11.88	0
87	SLU 10	374	0	3930	0	18.23	0
87	SLU 11	374	0	3930	0	18.23	0
87	SLU 12	374	0	3930	0	18.23	0
87	SLU 13	374	0	3930	0	18.23	0
87	SLU 14	374	0	3930	0	18.23	0
87	SLU 15	374	0	3930	0	18.23	0
87	SLU 16	374	0	3930	0	18.23	0
87	SLU 17	374	0	3930	0	18.23	0
87	SLU 18	431	0	4343	0	20.96	0
87	SLU 19	431	0	4343	0	20.96	0
87	SLU 20	431	0	4343	0	20.96	0
87	SLU 21	431	0	4343	0	20.96	0
87	SLU 22	310	0	3521	0	15.17	0
87	SLU 23	310	0	3521	0	15.17	0
87	SLU 24	310	0	3521	0	15.17	0
87	SLU 25	310	0	3521	0	15.17	0
87	SLU 26	310	0	3521	0	15.17	0
87	SLU 27	310	0	3521	0	15.17	0
87	SLU 28	310	0	3521	0	15.17	0
87	SLU 29	310	0	3521	0	15.17	0
87	SLU 30	310	0	3521	0	15.17	0
87	SLU 31	442	0	4484	0	21.52	0
87	SLU 32	442	0	4484	0	21.52	0
87	SLU 33	442	0	4484	0	21.52	0
87	SLU 34	442	0	4484	0	21.52	0
87	SLU 35	442	0	4484	0	21.52	0
87	SLU 36	442	0	4484	0	21.52	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
87	SLU 37	442	0	4484	0	21.52	0
87	SLU 38	442	0	4484	0	21.52	0
87	SLU 39	499	0	4896	0	24.24	0
87	SLU 40	499	0	4896	0	24.24	0
87	SLU 41	499	0	4896	0	24.24	0
87	SLU 42	499	0	4896	0	24.24	0
87	SLU 43	291	0	3668	0	14.32	0
87	SLU 44	291	0	3668	0	14.32	0
87	SLU 45	291	0	3668	0	14.32	0
87	SLU 46	291	0	3668	0	14.32	0
87	SLU 47	291	0	3668	0	14.32	0
87	SLU 48	291	0	3668	0	14.32	0
87	SLU 49	291	0	3668	0	14.32	0
87	SLU 50	291	0	3668	0	14.32	0
87	SLU 51	291	0	3668	0	14.32	0
87	SLU 52	423	0	4631	0	20.67	0
87	SLU 53	423	0	4631	0	20.67	0
87	SLU 54	423	0	4631	0	20.67	0
87	SLU 55	423	0	4631	0	20.67	0
87	SLU 56	423	0	4631	0	20.67	0
87	SLU 57	423	0	4631	0	20.67	0
87	SLU 58	423	0	4631	0	20.67	0
87	SLU 59	423	0	4631	0	20.67	0
87	SLU 60	480	0	5043	0	23.39	0
87	SLU 61	480	0	5043	0	23.39	0
87	SLU 62	480	0	5043	0	23.39	0
87	SLU 63	480	0	5043	0	23.39	0
87	SLU 64	359	0	4222	0	17.61	0
87	SLU 65	359	0	4222	0	17.61	0
87	SLU 66	359	0	4222	0	17.61	0
87	SLU 67	359	0	4222	0	17.61	0
87	SLU 68	359	0	4222	0	17.61	0
87	SLU 69	359	0	4222	0	17.61	0
87	SLU 70	359	0	4222	0	17.61	0
87	SLU 71	359	0	4222	0	17.61	0
87	SLU 72	359	0	4222	0	17.61	0
87	SLU 73	491	0	5185	0	23.96	0
87	SLU 74	491	0	5185	0	23.96	0
87	SLU 75	491	0	5185	0	23.96	0
87	SLU 76	491	0	5185	0	23.96	0
87	SLU 77	491	0	5185	0	23.96	0
87	SLU 78	491	0	5185	0	23.96	0
87	SLU 79	491	0	5185	0	23.96	0
87	SLU 80	491	0	5185	0	23.96	0
87	SLU 81	548	0	5597	0	26.68	0
87	SLU 82	548	0	5597	0	26.68	0
87	SLU 83	548	0	5597	0	26.68	0
87	SLU 84	548	0	5597	0	26.68	0
87	SLE RA 1	262	0	3126	0	12.82	0
87	SLE RA 2	262	0	3126	0	12.82	0
87	SLE RA 3	262	0	3126	0	12.82	0
87	SLE RA 4	262	0	3126	0	12.82	0
87	SLE RA 5	262	0	3126	0	12.82	0
87	SLE RA 6	262	0	3126	0	12.82	0
87	SLE RA 7	262	0	3126	0	12.82	0
87	SLE RA 8	262	0	3126	0	12.82	0
87	SLE RA 9	262	0	3126	0	12.82	0
87	SLE RA 10	350	0	3768	0	17.06	0
87	SLE RA 11	350	0	3768	0	17.06	0
87	SLE RA 12	350	0	3768	0	17.06	0
87	SLE RA 13	350	0	3768	0	17.06	0
87	SLE RA 14	350	0	3768	0	17.06	0
87	SLE RA 15	350	0	3768	0	17.06	0
87	SLE RA 16	350	0	3768	0	17.06	0
87	SLE RA 17	350	0	3768	0	17.06	0
87	SLE RA 18	387	0	4043	0	18.87	0
87	SLE RA 19	387	0	4043	0	18.87	0
87	SLE RA 20	387	0	4043	0	18.87	0
87	SLE RA 21	387	0	4043	0	18.87	0
87	SLE FR 1	262	0	3126	0	12.82	0
87	SLE FR 2	262	0	3126	0	12.82	0
87	SLE FR 3	262	0	3126	0	12.82	0
87	SLE FR 4	299	0	3401	0	14.64	0
87	SLE FR 5	299	0	3401	0	14.64	0
87	SLE FR 6	324	0	3584	0	15.85	0
87	SLE QP 1	262	0	3126	0	12.82	0
87	SLE QP 2	299	0	3401	0	14.64	0
87	SLD 1	612	16	3535	-22.28	30.02	0.04
87	SLD 2	612	16	3535	-22.28	30.02	0.04
87	SLD 3	607	-11	3532	17.19	29.8	-0.02
87	SLD 4	607	-11	3532	17.19	29.8	-0.02
87	SLD 5	400	46	3445	-66.55	19.59	0.1
87	SLD 6	400	46	3445	-66.55	19.59	0.1
87	SLD 7	384	-44	3436	65.02	18.85	-0.1
87	SLD 8	384	-44	3436	65.02	18.85	-0.1
87	SLD 9	214	44	3366	-65.02	10.43	0.1
87	SLD 10	214	44	3366	-65.02	10.43	0.1
87	SLD 11	198	-46	3357	66.55	9.69	-0.1



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
87	SLD 12	198	-46	3357	66.55	9.69	-0.1
87	SLD 13	-8	11	3270	-17.19	-0.52	0.02
87	SLD 14	-8	11	3270	-17.19	-0.52	0.02
87	SLD 15	-13	-16	3267	22.28	-0.74	-0.04
87	SLD 16	-13	-16	3267	22.28	-0.74	-0.04
87	SLV 1	1032	43	3715	-60.79	50.71	0.09
87	SLV 2	1032	43	3715	-60.79	50.71	0.09
87	SLV 3	1020	-30	3708	47.87	50.19	-0.06
87	SLV 4	1020	-30	3708	47.87	50.19	-0.06
87	SLV 5	536	123	3504	-183.04	26.26	0.26
87	SLV 6	536	123	3504	-183.04	26.26	0.26
87	SLV 7	499	-119	3484	179.16	24.5	-0.26
87	SLV 8	499	-119	3484	179.16	24.5	-0.26
87	SLV 9	100	119	3318	-179.16	4.78	0.26
87	SLV 10	100	119	3318	-179.16	4.78	0.26
87	SLV 11	63	-123	3298	183.04	3.01	-0.26
87	SLV 12	63	-123	3298	183.04	3.01	-0.26
87	SLV 13	-422	30	3094	-47.87	-20.91	0.06
87	SLV 14	-422	30	3094	-47.87	-20.91	0.06
87	SLV 15	-433	-43	3087	60.79	-21.44	-0.09
87	SLV 16	-433	-43	3087	60.79	-21.44	-0.09
88	SLU 1	340	0	3084	0	16.87	0
88	SLU 2	340	0	3084	0	16.87	0
88	SLU 3	340	0	3084	0	16.87	0
88	SLU 4	340	0	3084	0	16.87	0
88	SLU 5	340	0	3084	0	16.87	0
88	SLU 6	340	0	3084	0	16.87	0
88	SLU 7	340	0	3084	0	16.87	0
88	SLU 8	340	0	3084	0	16.87	0
88	SLU 9	340	0	3084	0	16.87	0
88	SLU 10	503	0	4109	0	25.2	0
88	SLU 11	503	0	4109	0	25.2	0
88	SLU 12	503	0	4109	0	25.2	0
88	SLU 13	503	0	4109	0	25.2	0
88	SLU 14	503	0	4109	0	25.2	0
88	SLU 15	503	0	4109	0	25.2	0
88	SLU 16	503	0	4109	0	25.2	0
88	SLU 17	503	0	4109	0	25.2	0
88	SLU 18	573	0	4548	0	28.78	0
88	SLU 19	573	0	4548	0	28.78	0
88	SLU 20	573	0	4548	0	28.78	0
88	SLU 21	573	0	4548	0	28.78	0
88	SLU 22	426	0	3669	0	21.24	0
88	SLU 23	426	0	3669	0	21.24	0
88	SLU 24	426	0	3669	0	21.24	0
88	SLU 25	426	0	3669	0	21.24	0
88	SLU 26	426	0	3669	0	21.24	0
88	SLU 27	426	0	3669	0	21.24	0
88	SLU 28	426	0	3669	0	21.24	0
88	SLU 29	426	0	3669	0	21.24	0
88	SLU 30	426	0	3669	0	21.24	0
88	SLU 31	589	0	4693	0	29.57	0
88	SLU 32	589	0	4693	0	29.57	0
88	SLU 33	589	0	4693	0	29.57	0
88	SLU 34	589	0	4693	0	29.57	0
88	SLU 35	589	0	4693	0	29.57	0
88	SLU 36	589	0	4693	0	29.57	0
88	SLU 37	589	0	4693	0	29.57	0
88	SLU 38	589	0	4693	0	29.57	0
88	SLU 39	659	0	5132	0	33.15	0
88	SLU 40	659	0	5132	0	33.15	0
88	SLU 41	659	0	5132	0	33.15	0
88	SLU 42	659	0	5132	0	33.15	0
88	SLU 43	412	0	3809	0	20.43	0
88	SLU 44	412	0	3809	0	20.43	0
88	SLU 45	412	0	3809	0	20.43	0
88	SLU 46	412	0	3809	0	20.43	0
88	SLU 47	412	0	3809	0	20.43	0
88	SLU 48	412	0	3809	0	20.43	0
88	SLU 49	412	0	3809	0	20.43	0
88	SLU 50	412	0	3809	0	20.43	0
88	SLU 51	412	0	3809	0	20.43	0
88	SLU 52	575	0	4834	0	28.76	0
88	SLU 53	575	0	4834	0	28.76	0
88	SLU 54	575	0	4834	0	28.76	0
88	SLU 55	575	0	4834	0	28.76	0
88	SLU 56	575	0	4834	0	28.76	0
88	SLU 57	575	0	4834	0	28.76	0
88	SLU 58	575	0	4834	0	28.76	0
88	SLU 59	575	0	4834	0	28.76	0
88	SLU 60	645	0	5273	0	32.34	0
88	SLU 61	645	0	5273	0	32.34	0
88	SLU 62	645	0	5273	0	32.34	0
88	SLU 63	645	0	5273	0	32.34	0
88	SLU 64	498	0	4393	0	24.8	0
88	SLU 65	498	0	4393	0	24.8	0
88	SLU 66	498	0	4393	0	24.8	0
88	SLU 67	498	0	4393	0	24.8	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
88	SLU 68	498	0	4393	0	24.8	0
88	SLU 69	498	0	4393	0	24.8	0
88	SLU 70	498	0	4393	0	24.8	0
88	SLU 71	498	0	4393	0	24.8	0
88	SLU 72	498	0	4393	0	24.8	0
88	SLU 73	662	0	5418	0	33.13	0
88	SLU 74	662	0	5418	0	33.13	0
88	SLU 75	662	0	5418	0	33.13	0
88	SLU 76	662	0	5418	0	33.13	0
88	SLU 77	662	0	5418	0	33.13	0
88	SLU 78	662	0	5418	0	33.13	0
88	SLU 79	662	0	5418	0	33.13	0
88	SLU 80	662	0	5418	0	33.13	0
88	SLU 81	732	0	5857	0	36.71	0
88	SLU 82	732	0	5857	0	36.71	0
88	SLU 83	732	0	5857	0	36.71	0
88	SLU 84	732	0	5857	0	36.71	0
88	SLE RA 1	364	0	3251	0	18.11	0
88	SLE RA 2	364	0	3251	0	18.11	0
88	SLE RA 3	364	0	3251	0	18.11	0
88	SLE RA 4	364	0	3251	0	18.11	0
88	SLE RA 5	364	0	3251	0	18.11	0
88	SLE RA 6	364	0	3251	0	18.11	0
88	SLE RA 7	364	0	3251	0	18.11	0
88	SLE RA 8	364	0	3251	0	18.11	0
88	SLE RA 9	364	0	3251	0	18.11	0
88	SLE RA 10	473	0	3934	0	23.67	0
88	SLE RA 11	473	0	3934	0	23.67	0
88	SLE RA 12	473	0	3934	0	23.67	0
88	SLE RA 13	473	0	3934	0	23.67	0
88	SLE RA 14	473	0	3934	0	23.67	0
88	SLE RA 15	473	0	3934	0	23.67	0
88	SLE RA 16	473	0	3934	0	23.67	0
88	SLE RA 17	473	0	3934	0	23.67	0
88	SLE RA 18	520	0	4227	0	26.05	0
88	SLE RA 19	520	0	4227	0	26.05	0
88	SLE RA 20	520	0	4227	0	26.05	0
88	SLE RA 21	520	0	4227	0	26.05	0
88	SLE FR 1	364	0	3251	0	18.11	0
88	SLE FR 2	364	0	3251	0	18.11	0
88	SLE FR 3	364	0	3251	0	18.11	0
88	SLE FR 4	411	0	3544	0	20.5	0
88	SLE FR 5	411	0	3544	0	20.5	0
88	SLE FR 6	442	0	3739	0	22.08	0
88	SLE QP 1	364	0	3251	0	18.11	0
88	SLE QP 2	411	0	3544	0	20.5	0
88	SLD 1	690	16	3870	-19.28	35.42	-0.01
88	SLD 2	690	16	3870	-19.28	35.42	-0.01
88	SLD 3	686	-10	3867	13.99	35.2	0.02
88	SLD 4	686	-10	3867	13.99	35.2	0.02
88	SLD 5	501	45	3648	-56.24	25.3	-0.05
88	SLD 6	501	45	3648	-56.24	25.3	-0.05
88	SLD 7	487	-43	3635	54.65	24.58	0.05
88	SLD 8	487	-43	3635	54.65	24.58	0.05
88	SLD 9	335	43	3453	-54.65	16.41	-0.05
88	SLD 10	335	43	3453	-54.65	16.41	-0.05
88	SLD 11	321	-45	3440	56.24	15.69	0.05
88	SLD 12	321	-45	3440	56.24	15.69	0.05
88	SLD 13	136	10	3221	-13.99	5.79	-0.02
88	SLD 14	136	10	3221	-13.99	5.79	-0.02
88	SLD 15	132	-16	3217	19.28	5.57	0.01
88	SLD 16	132	-16	3217	19.28	5.57	0.01
88	SLV 1	1066	42	4308	-51.72	55.46	-0.03
88	SLV 2	1066	42	4308	-51.72	55.46	-0.03
88	SLV 3	1056	-28	4299	38.5	54.95	0.05
88	SLV 4	1056	-28	4299	38.5	54.95	0.05
88	SLV 5	623	118	3787	-152.35	31.76	-0.12
88	SLV 6	623	118	3787	-152.35	31.76	-0.12
88	SLV 7	589	-114	3756	148.38	30.06	0.13
88	SLV 8	589	-114	3756	148.38	30.06	0.13
88	SLV 9	233	114	3332	-148.38	10.94	-0.13
88	SLV 10	233	114	3332	-148.38	10.94	-0.13
88	SLV 11	199	-118	3300	152.35	9.23	0.12
88	SLV 12	199	-118	3300	152.35	9.23	0.12
88	SLV 13	-234	28	2789	-38.5	-13.96	-0.05
88	SLV 14	-234	28	2789	-38.5	-13.96	-0.05
88	SLV 15	-244	-42	2779	51.72	-14.47	0.03
88	SLV 16	-244	-42	2779	51.72	-14.47	0.03
89	SLU 1	446	0	3393	0	24.77	0
89	SLU 2	446	0	3393	0	24.77	0
89	SLU 3	446	0	3393	0	24.77	0
89	SLU 4	446	0	3393	0	24.77	0
89	SLU 5	446	0	3393	0	24.77	0
89	SLU 6	446	0	3393	0	24.77	0
89	SLU 7	446	0	3393	0	24.77	0
89	SLU 8	446	0	3393	0	24.77	0
89	SLU 9	446	0	3393	0	24.77	0
89	SLU 10	631	0	4580	0	35.09	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
89	SLU 11	631	0	4580	0	35.09	0
89	SLU 12	631	0	4580	0	35.09	0
89	SLU 13	631	0	4580	0	35.09	0
89	SLU 14	631	0	4580	0	35.09	0
89	SLU 15	631	0	4580	0	35.09	0
89	SLU 16	631	0	4580	0	35.09	0
89	SLU 17	631	0	4580	0	35.09	0
89	SLU 18	710	0	5089	0	39.52	0
89	SLU 19	710	0	5089	0	39.52	0
89	SLU 20	710	0	5089	0	39.52	0
89	SLU 21	710	0	5089	0	39.52	0
89	SLU 22	547	0	4060	0	30.38	0
89	SLU 23	547	0	4060	0	30.38	0
89	SLU 24	547	0	4060	0	30.38	0
89	SLU 25	547	0	4060	0	30.38	0
89	SLU 26	547	0	4060	0	30.38	0
89	SLU 27	547	0	4060	0	30.38	0
89	SLU 28	547	0	4060	0	30.38	0
89	SLU 29	547	0	4060	0	30.38	0
89	SLU 30	547	0	4060	0	30.38	0
89	SLU 31	732	0	5247	0	40.7	0
89	SLU 32	732	0	5247	0	40.7	0
89	SLU 33	732	0	5247	0	40.7	0
89	SLU 34	732	0	5247	0	40.7	0
89	SLU 35	732	0	5247	0	40.7	0
89	SLU 36	732	0	5247	0	40.7	0
89	SLU 37	732	0	5247	0	40.7	0
89	SLU 38	732	0	5247	0	40.7	0
89	SLU 39	811	0	5756	0	45.12	0
89	SLU 40	811	0	5756	0	45.12	0
89	SLU 41	811	0	5756	0	45.12	0
89	SLU 42	811	0	5756	0	45.12	0
89	SLU 43	545	0	4182	0	30.28	0
89	SLU 44	545	0	4182	0	30.28	0
89	SLU 45	545	0	4182	0	30.28	0
89	SLU 46	545	0	4182	0	30.28	0
89	SLU 47	545	0	4182	0	30.28	0
89	SLU 48	545	0	4182	0	30.28	0
89	SLU 49	545	0	4182	0	30.28	0
89	SLU 50	545	0	4182	0	30.28	0
89	SLU 51	545	0	4182	0	30.28	0
89	SLU 52	730	0	5369	0	40.6	0
89	SLU 53	730	0	5369	0	40.6	0
89	SLU 54	730	0	5369	0	40.6	0
89	SLU 55	730	0	5369	0	40.6	0
89	SLU 56	730	0	5369	0	40.6	0
89	SLU 57	730	0	5369	0	40.6	0
89	SLU 58	730	0	5369	0	40.6	0
89	SLU 59	730	0	5369	0	40.6	0
89	SLU 60	809	0	5878	0	45.03	0
89	SLU 61	809	0	5878	0	45.03	0
89	SLU 62	809	0	5878	0	45.03	0
89	SLU 63	809	0	5878	0	45.03	0
89	SLU 64	646	0	4849	0	35.89	0
89	SLU 65	646	0	4849	0	35.89	0
89	SLU 66	646	0	4849	0	35.89	0
89	SLU 67	646	0	4849	0	35.89	0
89	SLU 68	646	0	4849	0	35.89	0
89	SLU 69	646	0	4849	0	35.89	0
89	SLU 70	646	0	4849	0	35.89	0
89	SLU 71	646	0	4849	0	35.89	0
89	SLU 72	646	0	4849	0	35.89	0
89	SLU 73	831	0	6036	0	46.21	0
89	SLU 74	831	0	6036	0	46.21	0
89	SLU 75	831	0	6036	0	46.21	0
89	SLU 76	831	0	6036	0	46.21	0
89	SLU 77	831	0	6036	0	46.21	0
89	SLU 78	831	0	6036	0	46.21	0
89	SLU 79	831	0	6036	0	46.21	0
89	SLU 80	831	0	6036	0	46.21	0
89	SLU 81	910	0	6545	0	50.63	0
89	SLU 82	910	0	6545	0	50.63	0
89	SLU 83	910	0	6545	0	50.63	0
89	SLU 84	910	0	6545	0	50.63	0
89	SLE RA 1	475	0	3583	0	26.37	0
89	SLE RA 2	475	0	3583	0	26.37	0
89	SLE RA 3	475	0	3583	0	26.37	0
89	SLE RA 4	475	0	3583	0	26.37	0
89	SLE RA 5	475	0	3583	0	26.37	0
89	SLE RA 6	475	0	3583	0	26.37	0
89	SLE RA 7	475	0	3583	0	26.37	0
89	SLE RA 8	475	0	3583	0	26.37	0
89	SLE RA 9	475	0	3583	0	26.37	0
89	SLE RA 10	598	0	4375	0	33.25	0
89	SLE RA 11	598	0	4375	0	33.25	0
89	SLE RA 12	598	0	4375	0	33.25	0
89	SLE RA 13	598	0	4375	0	33.25	0
89	SLE RA 14	598	0	4375	0	33.25	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
89	SLE RA 15	598	0	4375	0	33.25	0
89	SLE RA 16	598	0	4375	0	33.25	0
89	SLE RA 17	598	0	4375	0	33.25	0
89	SLE RA 18	651	0	4714	0	36.2	0
89	SLE RA 19	651	0	4714	0	36.2	0
89	SLE RA 20	651	0	4714	0	36.2	0
89	SLE RA 21	651	0	4714	0	36.2	0
89	SLE FR 1	475	0	3583	0	26.37	0
89	SLE FR 2	475	0	3583	0	26.37	0
89	SLE FR 3	475	0	3583	0	26.37	0
89	SLE FR 4	528	0	3923	0	29.32	0
89	SLE FR 5	528	0	3923	0	29.32	0
89	SLE FR 6	563	0	4149	0	31.29	0
89	SLE QP 1	475	0	3583	0	26.37	0
89	SLE QP 2	528	0	3923	0	29.32	0
89	SLD 1	749	15	4626	-14.6	42.59	-0.04
89	SLD 2	749	15	4626	-14.6	42.59	-0.04
89	SLD 3	746	-9	4619	9.44	42.4	0.03
89	SLD 4	746	-9	4619	9.44	42.4	0.03
89	SLD 5	599	40	4146	-40.85	33.59	-0.13
89	SLD 6	599	40	4146	-40.85	33.59	-0.13
89	SLD 7	588	-38	4120	39.3	32.96	0.12
89	SLD 8	588	-38	4120	39.3	32.96	0.12
89	SLD 9	467	38	3726	-39.3	25.69	-0.12
89	SLD 10	467	38	3726	-39.3	25.69	-0.12
89	SLD 11	456	-40	3700	40.85	25.06	0.13
89	SLD 12	456	-40	3700	40.85	25.06	0.13
89	SLD 13	309	8	3226	-9.44	16.24	-0.03
89	SLD 14	309	8	3226	-9.44	16.24	-0.03
89	SLD 15	306	-15	3219	14.6	16.06	0.04
89	SLD 16	306	-15	3219	14.6	16.06	0.04
89	SLV 1	1048	37	5570	-37.7	60.44	-0.12
89	SLV 2	1048	37	5570	-37.7	60.44	-0.12
89	SLV 3	1040	-21	5552	25.07	59.99	0.08
89	SLV 4	1040	-21	5552	25.07	59.99	0.08
89	SLV 5	696	99	4445	-106.51	39.34	-0.33
89	SLV 6	696	99	4445	-106.51	39.34	-0.33
89	SLV 7	669	-95	4383	102.72	37.84	0.32
89	SLV 8	669	-95	4383	102.72	37.84	0.32
89	SLV 9	386	95	3462	-102.72	20.8	-0.32
89	SLV 10	386	95	3462	-102.72	20.8	-0.32
89	SLV 11	359	-99	3400	106.51	19.31	0.33
89	SLV 12	359	-99	3400	106.51	19.31	0.33
89	SLV 13	15	21	2293	-25.07	-1.35	-0.08
89	SLV 14	15	21	2293	-25.07	-1.35	-0.08
89	SLV 15	7	-37	2275	37.7	-1.79	0.12
89	SLV 16	7	-37	2275	37.7	-1.79	0.12
90	SLU 1	588	0	2125	0	16.32	0
90	SLU 2	588	0	2125	0	16.32	0
90	SLU 3	588	0	2125	0	16.32	0
90	SLU 4	588	0	2125	0	16.32	0
90	SLU 5	588	0	2125	0	16.32	0
90	SLU 6	588	0	2125	0	16.32	0
90	SLU 7	588	0	2125	0	16.32	0
90	SLU 8	588	0	2125	0	16.32	0
90	SLU 9	588	0	2125	0	16.32	0
90	SLU 10	816	0	2908	0	23.15	0
90	SLU 11	816	0	2908	0	23.15	0
90	SLU 12	816	0	2908	0	23.15	0
90	SLU 13	816	0	2908	0	23.15	0
90	SLU 14	816	0	2908	0	23.15	0
90	SLU 15	816	0	2908	0	23.15	0
90	SLU 16	816	0	2908	0	23.15	0
90	SLU 17	816	0	2908	0	23.15	0
90	SLU 18	913	0	3244	0	26.07	0
90	SLU 19	913	0	3244	0	26.07	0
90	SLU 20	913	0	3244	0	26.07	0
90	SLU 21	913	0	3244	0	26.07	0
90	SLU 22	713	0	2560	0	20.02	0
90	SLU 23	713	0	2560	0	20.02	0
90	SLU 24	713	0	2560	0	20.02	0
90	SLU 25	713	0	2560	0	20.02	0
90	SLU 26	713	0	2560	0	20.02	0
90	SLU 27	713	0	2560	0	20.02	0
90	SLU 28	713	0	2560	0	20.02	0
90	SLU 29	713	0	2560	0	20.02	0
90	SLU 30	713	0	2560	0	20.02	0
90	SLU 31	941	0	3343	0	26.84	0
90	SLU 32	941	0	3343	0	26.84	0
90	SLU 33	941	0	3343	0	26.84	0
90	SLU 34	941	0	3343	0	26.84	0
90	SLU 35	941	0	3343	0	26.84	0
90	SLU 36	941	0	3343	0	26.84	0
90	SLU 37	941	0	3343	0	26.84	0
90	SLU 38	941	0	3343	0	26.84	0
90	SLU 39	1039	0	3679	0	29.77	0
90	SLU 40	1039	0	3679	0	29.77	0
90	SLU 41	1039	0	3679	0	29.77	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
90	SLU 42	1039	0	3679	0	29.77	0
90	SLU 43	721	0	2613	0	19.95	0
90	SLU 44	721	0	2613	0	19.95	0
90	SLU 45	721	0	2613	0	19.95	0
90	SLU 46	721	0	2613	0	19.95	0
90	SLU 47	721	0	2613	0	19.95	0
90	SLU 48	721	0	2613	0	19.95	0
90	SLU 49	721	0	2613	0	19.95	0
90	SLU 50	721	0	2613	0	19.95	0
90	SLU 51	721	0	2613	0	19.95	0
90	SLU 52	949	0	3397	0	26.78	0
90	SLU 53	949	0	3397	0	26.78	0
90	SLU 54	949	0	3397	0	26.78	0
90	SLU 55	949	0	3397	0	26.78	0
90	SLU 56	949	0	3397	0	26.78	0
90	SLU 57	949	0	3397	0	26.78	0
90	SLU 58	949	0	3397	0	26.78	0
90	SLU 59	949	0	3397	0	26.78	0
90	SLU 60	1047	0	3732	0	29.7	0
90	SLU 61	1047	0	3732	0	29.7	0
90	SLU 62	1047	0	3732	0	29.7	0
90	SLU 63	1047	0	3732	0	29.7	0
90	SLU 64	846	0	3048	0	23.65	0
90	SLU 65	846	0	3048	0	23.65	0
90	SLU 66	846	0	3048	0	23.65	0
90	SLU 67	846	0	3048	0	23.65	0
90	SLU 68	846	0	3048	0	23.65	0
90	SLU 69	846	0	3048	0	23.65	0
90	SLU 70	846	0	3048	0	23.65	0
90	SLU 71	846	0	3048	0	23.65	0
90	SLU 72	846	0	3048	0	23.65	0
90	SLU 73	1074	0	3831	0	30.47	0
90	SLU 74	1074	0	3831	0	30.47	0
90	SLU 75	1074	0	3831	0	30.47	0
90	SLU 76	1074	0	3831	0	30.47	0
90	SLU 77	1074	0	3831	0	30.47	0
90	SLU 78	1074	0	3831	0	30.47	0
90	SLU 79	1074	0	3831	0	30.47	0
90	SLU 80	1074	0	3831	0	30.47	0
90	SLU 81	1172	0	4167	0	33.4	0
90	SLU 82	1172	0	4167	0	33.4	0
90	SLU 83	1172	0	4167	0	33.4	0
90	SLU 84	1172	0	4167	0	33.4	0
90	SLE RA 1	624	0	2249	0	17.38	0
90	SLE RA 2	624	0	2249	0	17.38	0
90	SLE RA 3	624	0	2249	0	17.38	0
90	SLE RA 4	624	0	2249	0	17.38	0
90	SLE RA 5	624	0	2249	0	17.38	0
90	SLE RA 6	624	0	2249	0	17.38	0
90	SLE RA 7	624	0	2249	0	17.38	0
90	SLE RA 8	624	0	2249	0	17.38	0
90	SLE RA 9	624	0	2249	0	17.38	0
90	SLE RA 10	776	0	2771	0	21.93	0
90	SLE RA 11	776	0	2771	0	21.93	0
90	SLE RA 12	776	0	2771	0	21.93	0
90	SLE RA 13	776	0	2771	0	21.93	0
90	SLE RA 14	776	0	2771	0	21.93	0
90	SLE RA 15	776	0	2771	0	21.93	0
90	SLE RA 16	776	0	2771	0	21.93	0
90	SLE RA 17	776	0	2771	0	21.93	0
90	SLE RA 18	841	0	2995	0	23.88	0
90	SLE RA 19	841	0	2995	0	23.88	0
90	SLE RA 20	841	0	2995	0	23.88	0
90	SLE RA 21	841	0	2995	0	23.88	0
90	SLE FR 1	624	0	2249	0	17.38	0
90	SLE FR 2	624	0	2249	0	17.38	0
90	SLE FR 3	624	0	2249	0	17.38	0
90	SLE FR 4	689	0	2473	0	19.33	0
90	SLE FR 5	689	0	2473	0	19.33	0
90	SLE FR 6	732	0	2622	0	20.63	0
90	SLE QP 1	624	0	2249	0	17.38	0
90	SLE QP 2	689	0	2473	0	19.33	0
90	SLD 1	902	-29	3108	3.03	27.17	-0.48
90	SLD 2	902	-29	3108	3.03	27.17	-0.48
90	SLD 3	899	24	3100	-5.36	27.07	0.85
90	SLD 4	899	24	3100	-5.36	27.07	0.85
90	SLD 5	757	-89	2674	13.63	21.84	-2.15
90	SLD 6	757	-89	2674	13.63	21.84	-2.15
90	SLD 7	748	87	2650	-14.33	21.49	2.26
90	SLD 8	748	87	2650	-14.33	21.49	2.26
90	SLD 9	630	-87	2296	14.33	17.16	-2.26
90	SLD 10	630	-87	2296	14.33	17.16	-2.26
90	SLD 11	621	89	2271	-13.63	16.82	2.15
90	SLD 12	621	89	2271	-13.63	16.82	2.15
90	SLD 13	478	-24	1845	5.36	11.59	-0.85
90	SLD 14	478	-24	1845	5.36	11.59	-0.85
90	SLD 15	475	29	1838	-3.03	11.49	0.48
90	SLD 16	475	29	1838	-3.03	11.49	0.48



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
90	SLV 1	1189	-80	3959	7.49	37.69	-1.18
90	SLV 2	1189	-80	3959	7.49	37.69	-1.18
90	SLV 3	1182	68	3942	-13.1	37.45	2.07
90	SLV 4	1182	68	3942	-13.1	37.45	2.07
90	SLV 5	848	-249	2945	33.47	25.21	-5.29
90	SLV 6	848	-249	2945	33.47	25.21	-5.29
90	SLV 7	827	246	2887	-35.15	24.4	5.55
90	SLV 8	827	246	2887	-35.15	24.4	5.55
90	SLV 9	550	-246	2058	35.15	14.26	-5.55
90	SLV 10	550	-246	2058	35.15	14.26	-5.55
90	SLV 11	529	249	2001	-33.47	13.45	5.29
90	SLV 12	529	249	2001	-33.47	13.45	5.29
90	SLV 13	195	-68	1003	13.1	1.21	-2.07
90	SLV 14	195	-68	1003	13.1	1.21	-2.07
90	SLV 15	189	80	986	-7.49	0.96	1.19
90	SLV 16	189	80	986	-7.49	0.96	1.19
91	SLU 1	41	0	443	0	9.66	0
91	SLU 2	41	0	443	0	9.66	0
91	SLU 3	41	0	443	0	9.66	0
91	SLU 4	41	0	443	0	9.66	0
91	SLU 5	41	0	443	0	9.66	0
91	SLU 6	41	0	443	0	9.66	0
91	SLU 7	41	0	443	0	9.66	0
91	SLU 8	41	0	443	0	9.66	0
91	SLU 9	41	0	443	0	9.66	0
91	SLU 10	116	0	320	0	14.77	0
91	SLU 11	116	0	320	0	14.77	0
91	SLU 12	116	0	320	0	14.77	0
91	SLU 13	116	0	320	0	14.77	0
91	SLU 14	116	0	320	0	14.77	0
91	SLU 15	116	0	320	0	14.77	0
91	SLU 16	116	0	320	0	14.77	0
91	SLU 17	116	0	320	0	14.77	0
91	SLU 18	149	0	268	0	16.96	0
91	SLU 19	149	0	268	0	16.96	0
91	SLU 20	149	0	268	0	16.96	0
91	SLU 21	149	0	268	0	16.96	0
91	SLU 22	80	0	391	0	12.43	0
91	SLU 23	80	0	391	0	12.43	0
91	SLU 24	80	0	391	0	12.43	0
91	SLU 25	80	0	391	0	12.43	0
91	SLU 26	80	0	391	0	12.43	0
91	SLU 27	80	0	391	0	12.43	0
91	SLU 28	80	0	391	0	12.43	0
91	SLU 29	80	0	391	0	12.43	0
91	SLU 30	80	0	391	0	12.43	0
91	SLU 31	155	0	268	0	17.54	0
91	SLU 32	155	0	268	0	17.54	0
91	SLU 33	155	0	268	0	17.54	0
91	SLU 34	155	0	268	0	17.54	0
91	SLU 35	155	0	268	0	17.54	0
91	SLU 36	155	0	268	0	17.54	0
91	SLU 37	155	0	268	0	17.54	0
91	SLU 38	155	0	268	0	17.54	0
91	SLU 39	188	0	215	0	19.73	0
91	SLU 40	188	0	215	0	19.73	0
91	SLU 41	188	0	215	0	19.73	0
91	SLU 42	188	0	215	0	19.73	0
91	SLU 43	40	0	594	0	11.61	0
91	SLU 44	40	0	594	0	11.61	0
91	SLU 45	40	0	594	0	11.61	0
91	SLU 46	40	0	594	0	11.61	0
91	SLU 47	40	0	594	0	11.61	0
91	SLU 48	40	0	594	0	11.61	0
91	SLU 49	40	0	594	0	11.61	0
91	SLU 50	40	0	594	0	11.61	0
91	SLU 51	40	0	594	0	11.61	0
91	SLU 52	115	0	471	0	16.72	0
91	SLU 53	115	0	471	0	16.72	0
91	SLU 54	115	0	471	0	16.72	0
91	SLU 55	115	0	471	0	16.72	0
91	SLU 56	115	0	471	0	16.72	0
91	SLU 57	115	0	471	0	16.72	0
91	SLU 58	115	0	471	0	16.72	0
91	SLU 59	115	0	471	0	16.72	0
91	SLU 60	148	0	418	0	18.91	0
91	SLU 61	148	0	418	0	18.91	0
91	SLU 62	148	0	418	0	18.91	0
91	SLU 63	148	0	418	0	18.91	0
91	SLU 64	79	0	542	0	14.38	0
91	SLU 65	79	0	542	0	14.38	0
91	SLU 66	79	0	542	0	14.38	0
91	SLU 67	79	0	542	0	14.38	0
91	SLU 68	79	0	542	0	14.38	0
91	SLU 69	79	0	542	0	14.38	0
91	SLU 70	79	0	542	0	14.38	0
91	SLU 71	79	0	542	0	14.38	0
91	SLU 72	79	0	542	0	14.38	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
91	SLU 73	154	0	419	0	19.49	0
91	SLU 74	154	0	419	0	19.49	0
91	SLU 75	154	0	419	0	19.49	0
91	SLU 76	154	0	419	0	19.49	0
91	SLU 77	154	0	419	0	19.49	0
91	SLU 78	154	0	419	0	19.49	0
91	SLU 79	154	0	419	0	19.49	0
91	SLU 80	154	0	419	0	19.49	0
91	SLU 81	187	0	366	0	21.68	0
91	SLU 82	187	0	366	0	21.68	0
91	SLU 83	187	0	366	0	21.68	0
91	SLU 84	187	0	366	0	21.68	0
91	SLE RA 1	52	0	428	0	10.45	0
91	SLE RA 2	52	0	428	0	10.45	0
91	SLE RA 3	52	0	428	0	10.45	0
91	SLE RA 4	52	0	428	0	10.45	0
91	SLE RA 5	52	0	428	0	10.45	0
91	SLE RA 6	52	0	428	0	10.45	0
91	SLE RA 7	52	0	428	0	10.45	0
91	SLE RA 8	52	0	428	0	10.45	0
91	SLE RA 9	52	0	428	0	10.45	0
91	SLE RA 10	102	0	346	0	13.86	0
91	SLE RA 11	102	0	346	0	13.86	0
91	SLE RA 12	102	0	346	0	13.86	0
91	SLE RA 13	102	0	346	0	13.86	0
91	SLE RA 14	102	0	346	0	13.86	0
91	SLE RA 15	102	0	346	0	13.86	0
91	SLE RA 16	102	0	346	0	13.86	0
91	SLE RA 17	102	0	346	0	13.86	0
91	SLE RA 18	124	0	311	0	15.32	0
91	SLE RA 19	124	0	311	0	15.32	0
91	SLE RA 20	124	0	311	0	15.32	0
91	SLE RA 21	124	0	311	0	15.32	0
91	SLE FR 1	52	0	428	0	10.45	0
91	SLE FR 2	52	0	428	0	10.45	0
91	SLE FR 3	52	0	428	0	10.45	0
91	SLE FR 4	73	0	393	0	11.91	0
91	SLE FR 5	73	0	393	0	11.91	0
91	SLE FR 6	88	0	370	0	12.89	0
91	SLE QP 1	52	0	428	0	10.45	0
91	SLE QP 2	73	0	393	0	11.91	0
91	SLD 1	179	7	87	-1.13	18.06	-0.25
91	SLD 2	179	7	87	-1.13	18.06	-0.25
91	SLD 3	180	-2	91	0.37	18	0.09
91	SLD 4	180	-2	91	0.37	18	0.09
91	SLD 5	103	17	295	-2.62	13.84	-0.59
91	SLD 6	103	17	295	-2.62	13.84	-0.59
91	SLD 7	107	-16	309	2.4	13.65	0.54
91	SLD 8	107	-16	309	2.4	13.65	0.54
91	SLD 9	40	16	478	-2.39	10.17	-0.54
91	SLD 10	40	16	478	-2.39	10.17	-0.54
91	SLD 11	44	-17	491	2.63	9.98	0.59
91	SLD 12	44	-17	491	2.63	9.98	0.59
91	SLD 13	-33	2	696	-0.37	5.82	-0.09
91	SLD 14	-33	2	696	-0.37	5.82	-0.09
91	SLD 15	-32	-8	700	1.14	5.77	0.25
91	SLD 16	-32	-8	700	1.14	5.77	0.25
91	SLV 1	319	19	-323	-2.89	26.27	-0.64
91	SLV 2	319	19	-323	-2.89	26.27	-0.64
91	SLV 3	322	-7	-314	1.07	26.14	0.25
91	SLV 4	322	-7	-314	1.07	26.14	0.25
91	SLV 5	143	45	164	-6.87	16.42	-1.55
91	SLV 6	143	45	164	-6.87	16.42	-1.55
91	SLV 7	152	-42	195	6.33	15.98	1.43
91	SLV 8	152	-42	195	6.33	15.98	1.43
91	SLV 9	-5	42	591	-6.32	7.84	-1.43
91	SLV 10	-5	42	591	-6.32	7.84	-1.43
91	SLV 11	4	-45	622	6.88	7.4	1.55
91	SLV 12	4	-45	622	6.88	7.4	1.55
91	SLV 13	-175	7	1100	-1.07	-2.32	-0.25
91	SLV 14	-175	7	1100	-1.07	-2.32	-0.25
91	SLV 15	-172	-19	1109	2.89	-2.45	0.64
91	SLV 16	-172	-19	1109	2.89	-2.45	0.64
92	SLU 1	253	-2	3222	0.07	10.84	0
92	SLU 2	253	-2	3222	0.07	10.84	0
92	SLU 3	253	-2	3222	0.07	10.84	0
92	SLU 4	253	-2	3222	0.07	10.84	0
92	SLU 5	253	-2	3222	0.07	10.84	0
92	SLU 6	253	-2	3222	0.07	10.84	0
92	SLU 7	253	-2	3222	0.07	10.84	0
92	SLU 8	253	-2	3222	0.07	10.84	0
92	SLU 9	253	-2	3222	0.07	10.84	0
92	SLU 10	324	-4	3811	0.13	15.99	0
92	SLU 11	324	-4	3811	0.13	15.99	0
92	SLU 12	324	-4	3811	0.13	15.99	0
92	SLU 13	324	-4	3811	0.13	15.99	0
92	SLU 14	324	-4	3811	0.13	15.99	0
92	SLU 15	324	-4	3811	0.13	15.99	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
92	SLU 16	324	-4	3811	0.13	15.99	0
92	SLU 17	324	-4	3811	0.13	15.99	0
92	SLU 18	354	-4	4064	0.16	18.2	0
92	SLU 19	354	-4	4064	0.16	18.2	0
92	SLU 20	354	-4	4064	0.16	18.2	0
92	SLU 21	354	-4	4064	0.16	18.2	0
92	SLU 22	294	-3	3581	0.09	13.67	0
92	SLU 23	294	-3	3581	0.09	13.67	0
92	SLU 24	294	-3	3581	0.09	13.67	0
92	SLU 25	294	-3	3581	0.09	13.67	0
92	SLU 26	294	-3	3581	0.09	13.67	0
92	SLU 27	294	-3	3581	0.09	13.67	0
92	SLU 28	294	-3	3581	0.09	13.67	0
92	SLU 29	294	-3	3581	0.09	13.67	0
92	SLU 30	294	-3	3581	0.09	13.67	0
92	SLU 31	365	-4	4170	0.15	18.82	0
92	SLU 32	365	-4	4170	0.15	18.82	0
92	SLU 33	365	-4	4170	0.15	18.82	0
92	SLU 34	365	-4	4170	0.15	18.82	0
92	SLU 35	365	-4	4170	0.15	18.82	0
92	SLU 36	365	-4	4170	0.15	18.82	0
92	SLU 37	365	-4	4170	0.15	18.82	0
92	SLU 38	365	-4	4170	0.15	18.82	0
92	SLU 39	396	-5	4422	0.18	21.03	0
92	SLU 40	396	-5	4422	0.18	21.03	0
92	SLU 41	396	-5	4422	0.18	21.03	0
92	SLU 42	396	-5	4422	0.18	21.03	0
92	SLU 43	315	-3	4066	0.08	13.12	0
92	SLU 44	315	-3	4066	0.08	13.12	0
92	SLU 45	315	-3	4066	0.08	13.12	0
92	SLU 46	315	-3	4066	0.08	13.12	0
92	SLU 47	315	-3	4066	0.08	13.12	0
92	SLU 48	315	-3	4066	0.08	13.12	0
92	SLU 49	315	-3	4066	0.08	13.12	0
92	SLU 50	315	-3	4066	0.08	13.12	0
92	SLU 51	315	-3	4066	0.08	13.12	0
92	SLU 52	386	-4	4655	0.14	18.28	0
92	SLU 53	386	-4	4655	0.14	18.28	0
92	SLU 54	386	-4	4655	0.14	18.28	0
92	SLU 55	386	-4	4655	0.14	18.28	0
92	SLU 56	386	-4	4655	0.14	18.28	0
92	SLU 57	386	-4	4655	0.14	18.28	0
92	SLU 58	386	-4	4655	0.14	18.28	0
92	SLU 59	386	-4	4655	0.14	18.28	0
92	SLU 60	416	-5	4908	0.17	20.48	0
92	SLU 61	416	-5	4908	0.17	20.48	0
92	SLU 62	416	-5	4908	0.17	20.48	0
92	SLU 63	416	-5	4908	0.17	20.48	0
92	SLU 64	356	-3	4425	0.11	15.95	0
92	SLU 65	356	-3	4425	0.11	15.95	0
92	SLU 66	356	-3	4425	0.11	15.95	0
92	SLU 67	356	-3	4425	0.11	15.95	0
92	SLU 68	356	-3	4425	0.11	15.95	0
92	SLU 69	356	-3	4425	0.11	15.95	0
92	SLU 70	356	-3	4425	0.11	15.95	0
92	SLU 71	356	-3	4425	0.11	15.95	0
92	SLU 72	356	-3	4425	0.11	15.95	0
92	SLU 73	427	-5	5014	0.17	21.1	0
92	SLU 74	427	-5	5014	0.17	21.1	0
92	SLU 75	427	-5	5014	0.17	21.1	0
92	SLU 76	427	-5	5014	0.17	21.1	0
92	SLU 77	427	-5	5014	0.17	21.1	0
92	SLU 78	427	-5	5014	0.17	21.1	0
92	SLU 79	427	-5	5014	0.17	21.1	0
92	SLU 80	427	-5	5014	0.17	21.1	0
92	SLU 81	458	-6	5266	0.19	23.31	0
92	SLU 82	458	-6	5266	0.19	23.31	0
92	SLU 83	458	-6	5266	0.19	23.31	0
92	SLU 84	458	-6	5266	0.19	23.31	0
92	SLE RA 1	265	-2	3325	0.08	11.65	0
92	SLE RA 2	265	-2	3325	0.08	11.65	0
92	SLE RA 3	265	-2	3325	0.08	11.65	0
92	SLE RA 4	265	-2	3325	0.08	11.65	0
92	SLE RA 5	265	-2	3325	0.08	11.65	0
92	SLE RA 6	265	-2	3325	0.08	11.65	0
92	SLE RA 7	265	-2	3325	0.08	11.65	0
92	SLE RA 8	265	-2	3325	0.08	11.65	0
92	SLE RA 9	265	-2	3325	0.08	11.65	0
92	SLE RA 10	312	-3	3717	0.12	15.08	0
92	SLE RA 11	312	-3	3717	0.12	15.08	0
92	SLE RA 12	312	-3	3717	0.12	15.08	0
92	SLE RA 13	312	-3	3717	0.12	15.08	0
92	SLE RA 14	312	-3	3717	0.12	15.08	0
92	SLE RA 15	312	-3	3717	0.12	15.08	0
92	SLE RA 16	312	-3	3717	0.12	15.08	0
92	SLE RA 17	312	-3	3717	0.12	15.08	0
92	SLE RA 18	332	-4	3886	0.13	16.56	0
92	SLE RA 19	332	-4	3886	0.13	16.56	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
92	SLE RA 20	332	-4	3886	0.13	16.56	0
92	SLE RA 21	332	-4	3886	0.13	16.56	0
92	SLE FR 1	265	-2	3325	0.08	11.65	0
92	SLE FR 2	265	-2	3325	0.08	11.65	0
92	SLE FR 3	265	-2	3325	0.08	11.65	0
92	SLE FR 4	285	-3	3493	0.09	13.12	0
92	SLE FR 5	285	-3	3493	0.09	13.12	0
92	SLE FR 6	299	-3	3605	0.11	14.1	0
92	SLE QP 1	265	-2	3325	0.08	11.65	0
92	SLE QP 2	285	-3	3493	0.09	13.12	0
92	SLD 1	336	40	3875	-1.99	18.76	0.01
92	SLD 2	336	40	3875	-1.99	18.76	0.01
92	SLD 3	337	-79	3873	3.79	18.82	-0.02
92	SLD 4	337	-79	3873	3.79	18.82	-0.02
92	SLD 5	299	189	3612	-9.3	14.72	0.05
92	SLD 6	299	189	3612	-9.3	14.72	0.05
92	SLD 7	302	-205	3602	9.97	14.93	-0.05
92	SLD 8	302	-205	3602	9.97	14.93	-0.05
92	SLD 9	268	199	3384	-9.78	11.31	0.05
92	SLD 10	268	199	3384	-9.78	11.31	0.05
92	SLD 11	271	-195	3374	9.49	11.52	-0.05
92	SLD 12	271	-195	3374	9.49	11.52	-0.05
92	SLD 13	234	73	3114	-3.6	7.42	0.02
92	SLD 14	234	73	3114	-3.6	7.42	0.02
92	SLD 15	234	-45	3111	2.18	7.48	-0.01
92	SLD 16	234	-45	3111	2.18	7.48	-0.01
92	SLV 1	404	98	4386	-4.89	26.27	0.02
92	SLV 2	404	98	4386	-4.89	26.27	0.02
92	SLV 3	406	-182	4379	8.86	26.42	-0.05
92	SLV 4	406	-182	4379	8.86	26.42	-0.05
92	SLV 5	318	453	3772	-22.27	16.83	0.11
92	SLV 6	318	453	3772	-22.27	16.83	0.11
92	SLV 7	324	-482	3748	23.59	17.34	-0.12
92	SLV 8	324	-482	3748	23.59	17.34	-0.12
92	SLV 9	246	476	3238	-23.4	8.9	0.12
92	SLV 10	246	476	3238	-23.4	8.9	0.12
92	SLV 11	253	-458	3214	22.45	9.41	-0.11
92	SLV 12	253	-458	3214	22.45	9.41	-0.11
92	SLV 13	165	176	2607	-8.67	-0.18	0.05
92	SLV 14	165	176	2607	-8.67	-0.18	0.05
92	SLV 15	167	-104	2600	5.08	-0.03	-0.02
92	SLV 16	167	-104	2600	5.08	-0.03	-0.02
93	SLU 1	-1	-369	1190	6.79	-0.65	-0.15
93	SLU 2	-1	-369	1190	6.79	-0.65	-0.15
93	SLU 3	-1	-369	1190	6.79	-0.65	-0.15
93	SLU 4	-1	-369	1190	6.79	-0.65	-0.15
93	SLU 5	-1	-369	1190	6.79	-0.65	-0.15
93	SLU 6	-1	-369	1190	6.79	-0.65	-0.15
93	SLU 7	-1	-369	1190	6.79	-0.65	-0.15
93	SLU 8	-1	-369	1190	6.79	-0.65	-0.15
93	SLU 9	-1	-369	1190	6.79	-0.65	-0.15
93	SLU 10	-2	-452	1459	8.26	-0.95	-0.21
93	SLU 11	-2	-452	1459	8.26	-0.95	-0.21
93	SLU 12	-2	-452	1459	8.26	-0.95	-0.21
93	SLU 13	-2	-452	1459	8.26	-0.95	-0.21
93	SLU 14	-2	-452	1459	8.26	-0.95	-0.21
93	SLU 15	-2	-452	1459	8.26	-0.95	-0.21
93	SLU 16	-2	-452	1459	8.26	-0.95	-0.21
93	SLU 17	-2	-452	1459	8.26	-0.95	-0.21
93	SLU 18	-2	-488	1574	8.89	-1.08	-0.24
93	SLU 19	-2	-488	1574	8.89	-1.08	-0.24
93	SLU 20	-2	-488	1574	8.89	-1.08	-0.24
93	SLU 21	-2	-488	1574	8.89	-1.08	-0.24
93	SLU 22	-2	-418	1348	7.65	-0.81	-0.18
93	SLU 23	-2	-418	1348	7.65	-0.81	-0.18
93	SLU 24	-2	-418	1348	7.65	-0.81	-0.18
93	SLU 25	-2	-418	1348	7.65	-0.81	-0.18
93	SLU 26	-2	-418	1348	7.65	-0.81	-0.18
93	SLU 27	-2	-418	1348	7.65	-0.81	-0.18
93	SLU 28	-2	-418	1348	7.65	-0.81	-0.18
93	SLU 29	-2	-418	1348	7.65	-0.81	-0.18
93	SLU 30	-2	-418	1348	7.65	-0.81	-0.18
93	SLU 31	-2	-501	1617	9.12	-1.11	-0.25
93	SLU 32	-2	-501	1617	9.12	-1.11	-0.25
93	SLU 33	-2	-501	1617	9.12	-1.11	-0.25
93	SLU 34	-2	-501	1617	9.12	-1.11	-0.25
93	SLU 35	-2	-501	1617	9.12	-1.11	-0.25
93	SLU 36	-2	-501	1617	9.12	-1.11	-0.25
93	SLU 37	-2	-501	1617	9.12	-1.11	-0.25
93	SLU 38	-2	-501	1617	9.12	-1.11	-0.25
93	SLU 39	-3	-536	1732	9.75	-1.24	-0.28
93	SLU 40	-3	-536	1732	9.75	-1.24	-0.28
93	SLU 41	-3	-536	1732	9.75	-1.24	-0.28
93	SLU 42	-3	-536	1732	9.75	-1.24	-0.28
93	SLU 43	-2	-463	1493	8.53	-0.79	-0.18
93	SLU 44	-2	-463	1493	8.53	-0.79	-0.18
93	SLU 45	-2	-463	1493	8.53	-0.79	-0.18
93	SLU 46	-2	-463	1493	8.53	-0.79	-0.18



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
93	SLU 47	-2	-463	1493	8.53	-0.79	-0.18
93	SLU 48	-2	-463	1493	8.53	-0.79	-0.18
93	SLU 49	-2	-463	1493	8.53	-0.79	-0.18
93	SLU 50	-2	-463	1493	8.53	-0.79	-0.18
93	SLU 51	-2	-463	1493	8.53	-0.79	-0.18
93	SLU 52	-2	-546	1762	10	-1.09	-0.24
93	SLU 53	-2	-546	1762	10	-1.09	-0.24
93	SLU 54	-2	-546	1762	10	-1.09	-0.24
93	SLU 55	-2	-546	1762	10	-1.09	-0.24
93	SLU 56	-2	-546	1762	10	-1.09	-0.24
93	SLU 57	-2	-546	1762	10	-1.09	-0.24
93	SLU 58	-2	-546	1762	10	-1.09	-0.24
93	SLU 59	-2	-546	1762	10	-1.09	-0.24
93	SLU 60	-3	-582	1877	10.63	-1.22	-0.27
93	SLU 61	-3	-582	1877	10.63	-1.22	-0.27
93	SLU 62	-3	-582	1877	10.63	-1.22	-0.27
93	SLU 63	-3	-582	1877	10.63	-1.22	-0.27
93	SLU 64	-2	-512	1651	9.39	-0.95	-0.21
93	SLU 65	-2	-512	1651	9.39	-0.95	-0.21
93	SLU 66	-2	-512	1651	9.39	-0.95	-0.21
93	SLU 67	-2	-512	1651	9.39	-0.95	-0.21
93	SLU 68	-2	-512	1651	9.39	-0.95	-0.21
93	SLU 69	-2	-512	1651	9.39	-0.95	-0.21
93	SLU 70	-2	-512	1651	9.39	-0.95	-0.21
93	SLU 71	-2	-512	1651	9.39	-0.95	-0.21
93	SLU 72	-2	-512	1651	9.39	-0.95	-0.21
93	SLU 73	-3	-595	1920	10.86	-1.25	-0.28
93	SLU 74	-3	-595	1920	10.86	-1.25	-0.28
93	SLU 75	-3	-595	1920	10.86	-1.25	-0.28
93	SLU 76	-3	-595	1920	10.86	-1.25	-0.28
93	SLU 77	-3	-595	1920	10.86	-1.25	-0.28
93	SLU 78	-3	-595	1920	10.86	-1.25	-0.28
93	SLU 79	-3	-595	1920	10.86	-1.25	-0.28
93	SLU 80	-3	-595	1920	10.86	-1.25	-0.28
93	SLU 81	-3	-630	2035	11.49	-1.38	-0.31
93	SLU 82	-3	-630	2035	11.49	-1.38	-0.31
93	SLU 83	-3	-630	2035	11.49	-1.38	-0.31
93	SLU 84	-3	-630	2035	11.49	-1.38	-0.31
93	SLE RA 1	-2	-383	1235	7.04	-0.7	-0.16
93	SLE RA 2	-2	-383	1235	7.04	-0.7	-0.16
93	SLE RA 3	-2	-383	1235	7.04	-0.7	-0.16
93	SLE RA 4	-2	-383	1235	7.04	-0.7	-0.16
93	SLE RA 5	-2	-383	1235	7.04	-0.7	-0.16
93	SLE RA 6	-2	-383	1235	7.04	-0.7	-0.16
93	SLE RA 7	-2	-383	1235	7.04	-0.7	-0.16
93	SLE RA 8	-2	-383	1235	7.04	-0.7	-0.16
93	SLE RA 9	-2	-383	1235	7.04	-0.7	-0.16
93	SLE RA 10	-2	-438	1415	8.01	-0.9	-0.2
93	SLE RA 11	-2	-438	1415	8.01	-0.9	-0.2
93	SLE RA 12	-2	-438	1415	8.01	-0.9	-0.2
93	SLE RA 13	-2	-438	1415	8.01	-0.9	-0.2
93	SLE RA 14	-2	-438	1415	8.01	-0.9	-0.2
93	SLE RA 15	-2	-438	1415	8.01	-0.9	-0.2
93	SLE RA 16	-2	-438	1415	8.01	-0.9	-0.2
93	SLE RA 17	-2	-438	1415	8.01	-0.9	-0.2
93	SLE RA 18	-2	-462	1491	8.43	-0.98	-0.22
93	SLE RA 19	-2	-462	1491	8.43	-0.98	-0.22
93	SLE RA 20	-2	-462	1491	8.43	-0.98	-0.22
93	SLE RA 21	-2	-462	1491	8.43	-0.98	-0.22
93	SLE FR 1	-2	-383	1235	7.04	-0.7	-0.16
93	SLE FR 2	-2	-383	1235	7.04	-0.7	-0.16
93	SLE FR 3	-2	-383	1235	7.04	-0.7	-0.16
93	SLE FR 4	-2	-407	1312	7.46	-0.78	-0.18
93	SLE FR 5	-2	-407	1312	7.46	-0.78	-0.18
93	SLE FR 6	-2	-422	1363	7.73	-0.84	-0.19
93	SLE QP 1	-2	-383	1235	7.04	-0.7	-0.16
93	SLE QP 2	-2	-407	1312	7.46	-0.78	-0.18
93	SLD 1	-7	-314	1035	5.4	-1.29	-0.3
93	SLD 2	-7	-314	1035	5.4	-1.29	-0.3
93	SLD 3	-19	-361	1155	6.89	-2.45	-0.63
93	SLD 4	-19	-361	1155	6.89	-2.45	-0.63
93	SLD 5	14	-307	1047	4.58	0.82	0.28
93	SLD 6	14	-307	1047	4.58	0.82	0.28
93	SLD 7	-24	-465	1447	9.54	-3.04	-0.8
93	SLD 8	-24	-465	1447	9.54	-3.04	-0.8
93	SLD 9	21	-348	1177	5.37	1.47	0.45
93	SLD 10	21	-348	1177	5.37	1.47	0.45
93	SLD 11	-18	-507	1577	10.33	-2.38	-0.63
93	SLD 12	-18	-507	1577	10.33	-2.38	-0.63
93	SLD 13	15	-452	1470	8.02	0.88	0.28
93	SLD 14	15	-452	1470	8.02	0.88	0.28
93	SLD 15	4	-499	1590	9.51	-0.27	-0.05
93	SLD 16	4	-499	1590	9.51	-0.27	-0.05
93	SLV 1	-13	-189	661	2.62	-1.85	-0.43
93	SLV 2	-13	-189	661	2.62	-1.85	-0.43
93	SLV 3	-43	-302	947	6.17	-4.9	-1.29
93	SLV 4	-43	-302	947	6.17	-4.9	-1.29
93	SLV 5	41	-170	682	0.62	3.52	1.05



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
93	SLV 6	41	-170	682	0.62	3.52	1.05
93	SLV 7	-61	-547	1637	12.45	-6.64	-1.81
93	SLV 8	-61	-547	1637	12.45	-6.64	-1.81
93	SLV 9	57	-266	987	2.46	5.08	1.46
93	SLV 10	57	-266	987	2.46	5.08	1.46
93	SLV 11	-45	-644	1942	14.29	-5.08	-1.4
93	SLV 12	-45	-644	1942	14.29	-5.08	-1.4
93	SLV 13	40	-511	1677	8.74	3.34	0.94
93	SLV 14	40	-511	1677	8.74	3.34	0.94
93	SLV 15	9	-624	1964	12.29	0.29	0.08
93	SLV 16	9	-624	1964	12.29	0.29	0.08
94	SLU 1	0	0	1150	0.01	0	0
94	SLU 2	0	0	1150	0.01	0	0
94	SLU 3	0	0	1150	0.01	0	0
94	SLU 4	0	0	1150	0.01	0	0
94	SLU 5	0	0	1150	0.01	0	0
94	SLU 6	0	0	1150	0.01	0	0
94	SLU 7	0	0	1150	0.01	0	0
94	SLU 8	0	0	1150	0.01	0	0
94	SLU 9	0	0	1150	0.01	0	0
94	SLU 10	0	0	1443	0.01	0	0
94	SLU 11	0	0	1443	0.01	0	0
94	SLU 12	0	0	1443	0.01	0	0
94	SLU 13	0	0	1443	0.01	0	0
94	SLU 14	0	0	1443	0.01	0	0
94	SLU 15	0	0	1443	0.01	0	0
94	SLU 16	0	0	1443	0.01	0	0
94	SLU 17	0	0	1443	0.01	0	0
94	SLU 18	0	0	1568	0	0	0
94	SLU 19	0	0	1568	0	0	0
94	SLU 20	0	0	1568	0	0	0
94	SLU 21	0	0	1568	0	0	0
94	SLU 22	0	0	1323	0	0	0
94	SLU 23	0	0	1323	0	0	0
94	SLU 24	0	0	1323	0	0	0
94	SLU 25	0	0	1323	0	0	0
94	SLU 26	0	0	1323	0	0	0
94	SLU 27	0	0	1323	0	0	0
94	SLU 28	0	0	1323	0	0	0
94	SLU 29	0	0	1323	0	0	0
94	SLU 30	0	0	1323	0	0	0
94	SLU 31	0	0	1616	0	0	0
94	SLU 32	0	0	1616	0	0	0
94	SLU 33	0	0	1616	0	0	0
94	SLU 34	0	0	1616	0	0	0
94	SLU 35	0	0	1616	0	0	0
94	SLU 36	0	0	1616	0	0	0
94	SLU 37	0	0	1616	0	0	0
94	SLU 38	0	0	1616	0	0	0
94	SLU 39	0	0	1741	0	0	0
94	SLU 40	0	0	1741	0	0	0
94	SLU 41	0	0	1741	0	0	0
94	SLU 42	0	0	1741	0	0	0
94	SLU 43	0	0	1435	0.01	0	0
94	SLU 44	0	0	1435	0.01	0	0
94	SLU 45	0	0	1435	0.01	0	0
94	SLU 46	0	0	1435	0.01	0	0
94	SLU 47	0	0	1435	0.01	0	0
94	SLU 48	0	0	1435	0.01	0	0
94	SLU 49	0	0	1435	0.01	0	0
94	SLU 50	0	0	1435	0.01	0	0
94	SLU 51	0	0	1435	0.01	0	0
94	SLU 52	0	0	1728	0.01	0	0
94	SLU 53	0	0	1728	0.01	0	0
94	SLU 54	0	0	1728	0.01	0	0
94	SLU 55	0	0	1728	0.01	0	0
94	SLU 56	0	0	1728	0.01	0	0
94	SLU 57	0	0	1728	0.01	0	0
94	SLU 58	0	0	1728	0.01	0	0
94	SLU 59	0	0	1728	0.01	0	0
94	SLU 60	0	0	1854	0.01	0	0
94	SLU 61	0	0	1854	0.01	0	0
94	SLU 62	0	0	1854	0.01	0	0
94	SLU 63	0	0	1854	0.01	0	0
94	SLU 64	0	0	1609	0.01	0	0
94	SLU 65	0	0	1609	0.01	0	0
94	SLU 66	0	0	1609	0.01	0	0
94	SLU 67	0	0	1609	0.01	0	0
94	SLU 68	0	0	1609	0.01	0	0
94	SLU 69	0	0	1609	0.01	0	0
94	SLU 70	0	0	1609	0.01	0	0
94	SLU 71	0	0	1609	0.01	0	0
94	SLU 72	0	0	1609	0.01	0	0
94	SLU 73	0	0	1901	0.01	0	0
94	SLU 74	0	0	1901	0.01	0	0
94	SLU 75	0	0	1901	0.01	0	0
94	SLU 76	0	0	1901	0.01	0	0
94	SLU 77	0	0	1901	0.01	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
94	SLU 78	0	0	1901	0.01	0	0
94	SLU 79	0	0	1901	0.01	0	0
94	SLU 80	0	0	1901	0.01	0	0
94	SLU 81	0	0	2027	0.01	0	0
94	SLU 82	0	0	2027	0.01	0	0
94	SLU 83	0	0	2027	0.01	0	0
94	SLU 84	0	0	2027	0.01	0	0
94	SLE RA 1	0	0	1199	0.01	0	0
94	SLE RA 2	0	0	1199	0.01	0	0
94	SLE RA 3	0	0	1199	0.01	0	0
94	SLE RA 4	0	0	1199	0.01	0	0
94	SLE RA 5	0	0	1199	0.01	0	0
94	SLE RA 6	0	0	1199	0.01	0	0
94	SLE RA 7	0	0	1199	0.01	0	0
94	SLE RA 8	0	0	1199	0.01	0	0
94	SLE RA 9	0	0	1199	0.01	0	0
94	SLE RA 10	0	0	1394	0	0	0
94	SLE RA 11	0	0	1394	0	0	0
94	SLE RA 12	0	0	1394	0	0	0
94	SLE RA 13	0	0	1394	0	0	0
94	SLE RA 14	0	0	1394	0	0	0
94	SLE RA 15	0	0	1394	0	0	0
94	SLE RA 16	0	0	1394	0	0	0
94	SLE RA 17	0	0	1394	0	0	0
94	SLE RA 18	0	0	1478	0	0	0
94	SLE RA 19	0	0	1478	0	0	0
94	SLE RA 20	0	0	1478	0	0	0
94	SLE RA 21	0	0	1478	0	0	0
94	SLE FR 1	0	0	1199	0.01	0	0
94	SLE FR 2	0	0	1199	0.01	0	0
94	SLE FR 3	0	0	1199	0.01	0	0
94	SLE FR 4	0	0	1283	0.01	0	0
94	SLE FR 5	0	0	1283	0.01	0	0
94	SLE FR 6	0	0	1339	0.01	0	0
94	SLE QP 1	0	0	1199	0.01	0	0
94	SLE QP 2	0	0	1283	0.01	0	0
94	SLD 1	6	1	1263	-0.01	4.92	0
94	SLD 2	6	1	1263	-0.01	4.92	0
94	SLD 3	6	-1	1306	0.02	4.66	0
94	SLD 4	6	-1	1306	0.02	4.66	0
94	SLD 5	2	2	1213	-0.06	1.87	0
94	SLD 6	2	2	1213	-0.06	1.87	0
94	SLD 7	1	-2	1354	0.07	1.01	0
94	SLD 8	1	-2	1354	0.07	1.01	0
94	SLD 9	-1	2	1212	-0.06	-1.01	0
94	SLD 10	-1	2	1212	-0.06	-1.01	0
94	SLD 11	-2	-2	1353	0.07	-1.87	0
94	SLD 12	-2	-2	1353	0.07	-1.87	0
94	SLD 13	-6	1	1260	-0.01	-4.66	0
94	SLD 14	-6	1	1260	-0.01	-4.66	0
94	SLD 15	-6	-1	1303	0.02	-4.92	0
94	SLD 16	-6	-1	1303	0.02	-4.92	0
94	SLV 1	16	2	1227	-0.05	12.31	0
94	SLV 2	16	2	1227	-0.05	12.31	0
94	SLV 3	15	-2	1346	0.06	11.69	0
94	SLV 4	15	-2	1346	0.06	11.69	0
94	SLV 5	6	6	1085	-0.17	4.62	0
94	SLV 6	6	6	1085	-0.17	4.62	0
94	SLV 7	3	-6	1483	0.18	2.58	0
94	SLV 8	3	-6	1483	0.18	2.58	0
94	SLV 9	-3	7	1083	-0.17	-2.58	0
94	SLV 10	-3	7	1083	-0.17	-2.58	0
94	SLV 11	-6	-6	1481	0.18	-4.62	0
94	SLV 12	-6	-6	1481	0.18	-4.62	0
94	SLV 13	-15	2	1220	-0.05	-11.69	0
94	SLV 14	-15	2	1220	-0.05	-11.69	0
94	SLV 15	-16	-2	1339	0.06	-12.31	0
94	SLV 16	-16	-2	1339	0.06	-12.31	0
95	SLU 1	3	-108	2192	4.05	1.44	0.01
95	SLU 2	3	-108	2192	4.05	1.44	0.01
95	SLU 3	3	-108	2192	4.05	1.44	0.01
95	SLU 4	3	-108	2192	4.05	1.44	0.01
95	SLU 5	3	-108	2192	4.05	1.44	0.01
95	SLU 6	3	-108	2192	4.05	1.44	0.01
95	SLU 7	3	-108	2192	4.05	1.44	0.01
95	SLU 8	3	-108	2192	4.05	1.44	0.01
95	SLU 9	3	-108	2192	4.05	1.44	0.01
95	SLU 10	4	-156	2600	5.83	2.11	0.01
95	SLU 11	4	-156	2600	5.83	2.11	0.01
95	SLU 12	4	-156	2600	5.83	2.11	0.01
95	SLU 13	4	-156	2600	5.83	2.11	0.01
95	SLU 14	4	-156	2600	5.83	2.11	0.01
95	SLU 15	4	-156	2600	5.83	2.11	0.01
95	SLU 16	4	-156	2600	5.83	2.11	0.01
95	SLU 17	4	-156	2600	5.83	2.11	0.01
95	SLU 18	5	-177	2775	6.59	2.39	0.01
95	SLU 19	5	-177	2775	6.59	2.39	0.01
95	SLU 20	5	-177	2775	6.59	2.39	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
95	SLU 21	5	-177	2775	6.59	2.39	0.01
95	SLU 22	4	-135	2438	5.04	1.8	0.01
95	SLU 23	4	-135	2438	5.04	1.8	0.01
95	SLU 24	4	-135	2438	5.04	1.8	0.01
95	SLU 25	4	-135	2438	5.04	1.8	0.01
95	SLU 26	4	-135	2438	5.04	1.8	0.01
95	SLU 27	4	-135	2438	5.04	1.8	0.01
95	SLU 28	4	-135	2438	5.04	1.8	0.01
95	SLU 29	4	-135	2438	5.04	1.8	0.01
95	SLU 30	4	-135	2438	5.04	1.8	0.01
95	SLU 31	5	-183	2846	6.82	2.47	0.01
95	SLU 32	5	-183	2846	6.82	2.47	0.01
95	SLU 33	5	-183	2846	6.82	2.47	0.01
95	SLU 34	5	-183	2846	6.82	2.47	0.01
95	SLU 35	5	-183	2846	6.82	2.47	0.01
95	SLU 36	5	-183	2846	6.82	2.47	0.01
95	SLU 37	5	-183	2846	6.82	2.47	0.01
95	SLU 38	5	-183	2846	6.82	2.47	0.01
95	SLU 39	5	-204	3021	7.58	2.76	0.01
95	SLU 40	5	-204	3021	7.58	2.76	0.01
95	SLU 41	5	-204	3021	7.58	2.76	0.01
95	SLU 42	5	-204	3021	7.58	2.76	0.01
95	SLU 43	4	-131	2765	4.93	1.74	0.01
95	SLU 44	4	-131	2765	4.93	1.74	0.01
95	SLU 45	4	-131	2765	4.93	1.74	0.01
95	SLU 46	4	-131	2765	4.93	1.74	0.01
95	SLU 47	4	-131	2765	4.93	1.74	0.01
95	SLU 48	4	-131	2765	4.93	1.74	0.01
95	SLU 49	4	-131	2765	4.93	1.74	0.01
95	SLU 50	4	-131	2765	4.93	1.74	0.01
95	SLU 51	4	-131	2765	4.93	1.74	0.01
95	SLU 52	5	-179	3174	6.71	2.41	0.01
95	SLU 53	5	-179	3174	6.71	2.41	0.01
95	SLU 54	5	-179	3174	6.71	2.41	0.01
95	SLU 55	5	-179	3174	6.71	2.41	0.01
95	SLU 56	5	-179	3174	6.71	2.41	0.01
95	SLU 57	5	-179	3174	6.71	2.41	0.01
95	SLU 58	5	-179	3174	6.71	2.41	0.01
95	SLU 59	5	-179	3174	6.71	2.41	0.01
95	SLU 60	5	-200	3349	7.47	2.7	0.01
95	SLU 61	5	-200	3349	7.47	2.7	0.01
95	SLU 62	5	-200	3349	7.47	2.7	0.01
95	SLU 63	5	-200	3349	7.47	2.7	0.01
95	SLU 64	4	-158	3012	5.92	2.11	0.01
95	SLU 65	4	-158	3012	5.92	2.11	0.01
95	SLU 66	4	-158	3012	5.92	2.11	0.01
95	SLU 67	4	-158	3012	5.92	2.11	0.01
95	SLU 68	4	-158	3012	5.92	2.11	0.01
95	SLU 69	4	-158	3012	5.92	2.11	0.01
95	SLU 70	4	-158	3012	5.92	2.11	0.01
95	SLU 71	4	-158	3012	5.92	2.11	0.01
95	SLU 72	4	-158	3012	5.92	2.11	0.01
95	SLU 73	6	-206	3420	7.7	2.78	0.01
95	SLU 74	6	-206	3420	7.7	2.78	0.01
95	SLU 75	6	-206	3420	7.7	2.78	0.01
95	SLU 76	6	-206	3420	7.7	2.78	0.01
95	SLU 77	6	-206	3420	7.7	2.78	0.01
95	SLU 78	6	-206	3420	7.7	2.78	0.01
95	SLU 79	6	-206	3420	7.7	2.78	0.01
95	SLU 80	6	-206	3420	7.7	2.78	0.01
95	SLU 81	6	-227	3595	8.46	3.06	0.01
95	SLU 82	6	-227	3595	8.46	3.06	0.01
95	SLU 83	6	-227	3595	8.46	3.06	0.01
95	SLU 84	6	-227	3595	8.46	3.06	0.01
95	SLE RA 1	3	-115	2262	4.34	1.54	0.01
95	SLE RA 2	3	-115	2262	4.34	1.54	0.01
95	SLE RA 3	3	-115	2262	4.34	1.54	0.01
95	SLE RA 4	3	-115	2262	4.34	1.54	0.01
95	SLE RA 5	3	-115	2262	4.34	1.54	0.01
95	SLE RA 6	3	-115	2262	4.34	1.54	0.01
95	SLE RA 7	3	-115	2262	4.34	1.54	0.01
95	SLE RA 8	3	-115	2262	4.34	1.54	0.01
95	SLE RA 9	3	-115	2262	4.34	1.54	0.01
95	SLE RA 10	4	-148	2535	5.52	1.99	0.01
95	SLE RA 11	4	-148	2535	5.52	1.99	0.01
95	SLE RA 12	4	-148	2535	5.52	1.99	0.01
95	SLE RA 13	4	-148	2535	5.52	1.99	0.01
95	SLE RA 14	4	-148	2535	5.52	1.99	0.01
95	SLE RA 15	4	-148	2535	5.52	1.99	0.01
95	SLE RA 16	4	-148	2535	5.52	1.99	0.01
95	SLE RA 17	4	-148	2535	5.52	1.99	0.01
95	SLE RA 18	4	-162	2651	6.03	2.18	0.01
95	SLE RA 19	4	-162	2651	6.03	2.18	0.01
95	SLE RA 20	4	-162	2651	6.03	2.18	0.01
95	SLE RA 21	4	-162	2651	6.03	2.18	0.01
95	SLE FR 1	3	-115	2262	4.34	1.54	0.01
95	SLE FR 2	3	-115	2262	4.34	1.54	0.01
95	SLE FR 3	3	-115	2262	4.34	1.54	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
95	SLE FR 4	4	-129	2379	4.84	1.73	0.01
95	SLE FR 5	4	-129	2379	4.84	1.73	0.01
95	SLE FR 6	4	-139	2457	5.18	1.86	0.01
95	SLE QP 1	3	-115	2262	4.34	1.54	0.01
95	SLE QP 2	4	-129	2379	4.84	1.73	0.01
95	SLD 1	-7	-124	2681	4.03	1.86	0.02
95	SLD 2	-7	-124	2681	4.03	1.86	0.02
95	SLD 3	-2	-243	2685	9.79	4.33	0.02
95	SLD 4	-2	-243	2685	9.79	4.33	0.02
95	SLD 5	-7	53	2463	-4.14	-1.97	0.02
95	SLD 6	-7	53	2463	-4.14	-1.97	0.02
95	SLD 7	9	-345	2477	15.06	6.25	0
95	SLD 8	9	-345	2477	15.06	6.25	0
95	SLD 9	-2	86	2281	-5.38	-2.79	0.01
95	SLD 10	-2	86	2281	-5.38	-2.79	0.01
95	SLD 11	14	-312	2295	13.83	5.43	0
95	SLD 12	14	-312	2295	13.83	5.43	0
95	SLD 13	9	-15	2073	-0.1	-0.87	0
95	SLD 14	9	-15	2073	-0.1	-0.87	0
95	SLD 15	14	-135	2078	5.66	1.6	-0.01
95	SLD 16	14	-135	2078	5.66	1.6	-0.01
95	SLV 1	-22	-114	3083	2.82	1.71	0.04
95	SLV 2	-22	-114	3083	2.82	1.71	0.04
95	SLV 3	-9	-398	3094	16.53	8.18	0.03
95	SLV 4	-9	-398	3094	16.53	8.18	0.03
95	SLV 5	-24	305	2575	-16.55	-8.09	0.04
95	SLV 6	-24	305	2575	-16.55	-8.09	0.04
95	SLV 7	20	-640	2609	29.14	13.48	-0.01
95	SLV 8	20	-640	2609	29.14	13.48	-0.01
95	SLV 9	-13	382	2149	-19.45	-10.02	0.02
95	SLV 10	-13	382	2149	-19.45	-10.02	0.02
95	SLV 11	31	-564	2183	26.24	11.55	-0.02
95	SLV 12	31	-564	2183	26.24	11.55	-0.02
95	SLV 13	16	139	1665	-6.84	-4.72	-0.01
95	SLV 14	16	139	1665	-6.84	-4.72	-0.01
95	SLV 15	29	-144	1675	6.87	1.75	-0.03
95	SLV 16	29	-144	1675	6.87	1.75	-0.03
96	SLU 1	0	0	1162	0	0	0
96	SLU 2	0	0	1162	0	0	0
96	SLU 3	0	0	1162	0	0	0
96	SLU 4	0	0	1162	0	0	0
96	SLU 5	0	0	1162	0	0	0
96	SLU 6	0	0	1162	0	0	0
96	SLU 7	0	0	1162	0	0	0
96	SLU 8	0	0	1162	0	0	0
96	SLU 9	0	0	1162	0	0	0
96	SLU 10	0	0	1440	0	0	0
96	SLU 11	0	0	1440	0	0	0
96	SLU 12	0	0	1440	0	0	0
96	SLU 13	0	0	1440	0	0	0
96	SLU 14	0	0	1440	0	0	0
96	SLU 15	0	0	1440	0	0	0
96	SLU 16	0	0	1440	0	0	0
96	SLU 17	0	0	1440	0	0	0
96	SLU 18	0	0	1559	0	0	0
96	SLU 19	0	0	1559	0	0	0
96	SLU 20	0	0	1559	0	0	0
96	SLU 21	0	0	1559	0	0	0
96	SLU 22	0	0	1326	0	0	0
96	SLU 23	0	0	1326	0	0	0
96	SLU 24	0	0	1326	0	0	0
96	SLU 25	0	0	1326	0	0	0
96	SLU 26	0	0	1326	0	0	0
96	SLU 27	0	0	1326	0	0	0
96	SLU 28	0	0	1326	0	0	0
96	SLU 29	0	0	1326	0	0	0
96	SLU 30	0	0	1326	0	0	0
96	SLU 31	0	0	1604	0	0	0
96	SLU 32	0	0	1604	0	0	0
96	SLU 33	0	0	1604	0	0	0
96	SLU 34	0	0	1604	0	0	0
96	SLU 35	0	0	1604	0	0	0
96	SLU 36	0	0	1604	0	0	0
96	SLU 37	0	0	1604	0	0	0
96	SLU 38	0	0	1604	0	0	0
96	SLU 39	0	0	1723	0	0	0
96	SLU 40	0	0	1723	0	0	0
96	SLU 41	0	0	1723	0	0	0
96	SLU 42	0	0	1723	0	0	0
96	SLU 43	0	0	1455	0	0	0
96	SLU 44	0	0	1455	0	0	0
96	SLU 45	0	0	1455	0	0	0
96	SLU 46	0	0	1455	0	0	0
96	SLU 47	0	0	1455	0	0	0
96	SLU 48	0	0	1455	0	0	0
96	SLU 49	0	0	1455	0	0	0
96	SLU 50	0	0	1455	0	0	0
96	SLU 51	0	0	1455	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
96	SLU 52	0	0	1732	0	0	0
96	SLU 53	0	0	1732	0	0	0
96	SLU 54	0	0	1732	0	0	0
96	SLU 55	0	0	1732	0	0	0
96	SLU 56	0	0	1732	0	0	0
96	SLU 57	0	0	1732	0	0	0
96	SLU 58	0	0	1732	0	0	0
96	SLU 59	0	0	1732	0	0	0
96	SLU 60	0	0	1851	0	0	0
96	SLU 61	0	0	1851	0	0	0
96	SLU 62	0	0	1851	0	0	0
96	SLU 63	0	0	1851	0	0	0
96	SLU 64	0	0	1618	0	0	0
96	SLU 65	0	0	1618	0	0	0
96	SLU 66	0	0	1618	0	0	0
96	SLU 67	0	0	1618	0	0	0
96	SLU 68	0	0	1618	0	0	0
96	SLU 69	0	0	1618	0	0	0
96	SLU 70	0	0	1618	0	0	0
96	SLU 71	0	0	1618	0	0	0
96	SLU 72	0	0	1618	0	0	0
96	SLU 73	0	0	1896	0	0	0
96	SLU 74	0	0	1896	0	0	0
96	SLU 75	0	0	1896	0	0	0
96	SLU 76	0	0	1896	0	0	0
96	SLU 77	0	0	1896	0	0	0
96	SLU 78	0	0	1896	0	0	0
96	SLU 79	0	0	1896	0	0	0
96	SLU 80	0	0	1896	0	0	0
96	SLU 81	0	0	2015	0	0	0
96	SLU 82	0	0	2015	0	0	0
96	SLU 83	0	0	2015	0	0	0
96	SLU 84	0	0	2015	0	0	0
96	SLE RA 1	0	0	1209	0	0	0
96	SLE RA 2	0	0	1209	0	0	0
96	SLE RA 3	0	0	1209	0	0	0
96	SLE RA 4	0	0	1209	0	0	0
96	SLE RA 5	0	0	1209	0	0	0
96	SLE RA 6	0	0	1209	0	0	0
96	SLE RA 7	0	0	1209	0	0	0
96	SLE RA 8	0	0	1209	0	0	0
96	SLE RA 9	0	0	1209	0	0	0
96	SLE RA 10	0	0	1394	0	0	0
96	SLE RA 11	0	0	1394	0	0	0
96	SLE RA 12	0	0	1394	0	0	0
96	SLE RA 13	0	0	1394	0	0	0
96	SLE RA 14	0	0	1394	0	0	0
96	SLE RA 15	0	0	1394	0	0	0
96	SLE RA 16	0	0	1394	0	0	0
96	SLE RA 17	0	0	1394	0	0	0
96	SLE RA 18	0	0	1473	0	0	0
96	SLE RA 19	0	0	1473	0	0	0
96	SLE RA 20	0	0	1473	0	0	0
96	SLE RA 21	0	0	1473	0	0	0
96	SLE FR 1	0	0	1209	0	0	0
96	SLE FR 2	0	0	1209	0	0	0
96	SLE FR 3	0	0	1209	0	0	0
96	SLE FR 4	0	0	1288	0	0	0
96	SLE FR 5	0	0	1288	0	0	0
96	SLE FR 6	0	0	1341	0	0	0
96	SLE QP 1	0	0	1209	0	0	0
96	SLE QP 2	0	0	1288	0	0	0
96	SLD 1	6	0	1283	-0.05	5.09	0
96	SLD 2	6	0	1283	-0.05	5.09	0
96	SLD 3	6	-1	1296	0.05	5.33	0
96	SLD 4	6	-1	1296	0.05	5.33	0
96	SLD 5	2	2	1267	-0.17	1.15	0
96	SLD 6	2	2	1267	-0.17	1.15	0
96	SLD 7	1	-2	1310	0.17	1.97	0
96	SLD 8	1	-2	1310	0.17	1.97	0
96	SLD 9	-1	2	1266	-0.17	-1.97	0
96	SLD 10	-1	2	1266	-0.17	-1.97	0
96	SLD 11	-2	-2	1309	0.17	-1.15	0
96	SLD 12	-2	-2	1309	0.17	-1.15	0
96	SLD 13	-6	1	1280	-0.05	-5.33	0
96	SLD 14	-6	1	1280	-0.05	-5.33	0
96	SLD 15	-6	0	1293	0.05	-5.08	0
96	SLD 16	-6	0	1293	0.05	-5.08	0
96	SLV 1	15	1	1274	-0.14	12.83	0
96	SLV 2	15	1	1274	-0.14	12.83	0
96	SLV 3	14	-2	1310	0.14	13.43	0
96	SLV 4	14	-2	1310	0.14	13.43	0
96	SLV 5	5	5	1230	-0.47	2.94	0
96	SLV 6	5	5	1230	-0.47	2.94	0
96	SLV 7	3	-5	1349	0.47	4.94	0
96	SLV 8	3	-5	1349	0.47	4.94	0
96	SLV 9	-3	5	1228	-0.47	-4.94	0
96	SLV 10	-3	5	1228	-0.47	-4.94	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
96	SLV 11	-5	-5	1346	0.47	-2.94	0
96	SLV 12	-5	-5	1346	0.47	-2.94	0
96	SLV 13	-14	2	1267	-0.14	-13.43	0
96	SLV 14	-14	2	1267	-0.14	-13.43	0
96	SLV 15	-15	-1	1302	0.14	-12.83	0
96	SLV 16	-15	-1	1302	0.14	-12.83	0
97	SLU 1	1	-108	2045	4.46	1.01	0
97	SLU 2	1	-108	2045	4.46	1.01	0
97	SLU 3	1	-108	2045	4.46	1.01	0
97	SLU 4	1	-108	2045	4.46	1.01	0
97	SLU 5	1	-108	2045	4.46	1.01	0
97	SLU 6	1	-108	2045	4.46	1.01	0
97	SLU 7	1	-108	2045	4.46	1.01	0
97	SLU 8	1	-108	2045	4.46	1.01	0
97	SLU 9	1	-108	2045	4.46	1.01	0
97	SLU 10	2	-150	2380	6.15	1.51	0
97	SLU 11	2	-150	2380	6.15	1.51	0
97	SLU 12	2	-150	2380	6.15	1.51	0
97	SLU 13	2	-150	2380	6.15	1.51	0
97	SLU 14	2	-150	2380	6.15	1.51	0
97	SLU 15	2	-150	2380	6.15	1.51	0
97	SLU 16	2	-150	2380	6.15	1.51	0
97	SLU 17	2	-150	2380	6.15	1.51	0
97	SLU 18	2	-168	2523	6.87	1.73	0
97	SLU 19	2	-168	2523	6.87	1.73	0
97	SLU 20	2	-168	2523	6.87	1.73	0
97	SLU 21	2	-168	2523	6.87	1.73	0
97	SLU 22	2	-132	2251	5.42	1.28	0
97	SLU 23	2	-132	2251	5.42	1.28	0
97	SLU 24	2	-132	2251	5.42	1.28	0
97	SLU 25	2	-132	2251	5.42	1.28	0
97	SLU 26	2	-132	2251	5.42	1.28	0
97	SLU 27	2	-132	2251	5.42	1.28	0
97	SLU 28	2	-132	2251	5.42	1.28	0
97	SLU 29	2	-132	2251	5.42	1.28	0
97	SLU 30	2	-132	2251	5.42	1.28	0
97	SLU 31	2	-174	2585	7.11	1.79	0
97	SLU 32	2	-174	2585	7.11	1.79	0
97	SLU 33	2	-174	2585	7.11	1.79	0
97	SLU 34	2	-174	2585	7.11	1.79	0
97	SLU 35	2	-174	2585	7.11	1.79	0
97	SLU 36	2	-174	2585	7.11	1.79	0
97	SLU 37	2	-174	2585	7.11	1.79	0
97	SLU 38	2	-174	2585	7.11	1.79	0
97	SLU 39	2	-192	2729	7.83	2	0
97	SLU 40	2	-192	2729	7.83	2	0
97	SLU 41	2	-192	2729	7.83	2	0
97	SLU 42	2	-192	2729	7.83	2	0
97	SLU 43	1	-132	2588	5.47	1.22	0
97	SLU 44	1	-132	2588	5.47	1.22	0
97	SLU 45	1	-132	2588	5.47	1.22	0
97	SLU 46	1	-132	2588	5.47	1.22	0
97	SLU 47	1	-132	2588	5.47	1.22	0
97	SLU 48	1	-132	2588	5.47	1.22	0
97	SLU 49	1	-132	2588	5.47	1.22	0
97	SLU 50	1	-132	2588	5.47	1.22	0
97	SLU 51	1	-132	2588	5.47	1.22	0
97	SLU 52	2	-174	2923	7.16	1.72	0
97	SLU 53	2	-174	2923	7.16	1.72	0
97	SLU 54	2	-174	2923	7.16	1.72	0
97	SLU 55	2	-174	2923	7.16	1.72	0
97	SLU 56	2	-174	2923	7.16	1.72	0
97	SLU 57	2	-174	2923	7.16	1.72	0
97	SLU 58	2	-174	2923	7.16	1.72	0
97	SLU 59	2	-174	2923	7.16	1.72	0
97	SLU 60	2	-192	3066	7.88	1.94	0
97	SLU 61	2	-192	3066	7.88	1.94	0
97	SLU 62	2	-192	3066	7.88	1.94	0
97	SLU 63	2	-192	3066	7.88	1.94	0
97	SLU 64	2	-156	2794	6.43	1.49	0
97	SLU 65	2	-156	2794	6.43	1.49	0
97	SLU 66	2	-156	2794	6.43	1.49	0
97	SLU 67	2	-156	2794	6.43	1.49	0
97	SLU 68	2	-156	2794	6.43	1.49	0
97	SLU 69	2	-156	2794	6.43	1.49	0
97	SLU 70	2	-156	2794	6.43	1.49	0
97	SLU 71	2	-156	2794	6.43	1.49	0
97	SLU 72	2	-156	2794	6.43	1.49	0
97	SLU 73	2	-198	3128	8.12	2	0
97	SLU 74	2	-198	3128	8.12	2	0
97	SLU 75	2	-198	3128	8.12	2	0
97	SLU 76	2	-198	3128	8.12	2	0
97	SLU 77	2	-198	3128	8.12	2	0
97	SLU 78	2	-198	3128	8.12	2	0
97	SLU 79	2	-198	3128	8.12	2	0
97	SLU 80	2	-198	3128	8.12	2	0
97	SLU 81	3	-216	3272	8.84	2.21	0
97	SLU 82	3	-216	3272	8.84	2.21	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
97	SLU 83	3	-216	3272	8.84	2.21	0
97	SLU 84	3	-216	3272	8.84	2.21	0
97	SLE RA 1	1	-114	2104	4.74	1.09	0
97	SLE RA 2	1	-114	2104	4.74	1.09	0
97	SLE RA 3	1	-114	2104	4.74	1.09	0
97	SLE RA 4	1	-114	2104	4.74	1.09	0
97	SLE RA 5	1	-114	2104	4.74	1.09	0
97	SLE RA 6	1	-114	2104	4.74	1.09	0
97	SLE RA 7	1	-114	2104	4.74	1.09	0
97	SLE RA 8	1	-114	2104	4.74	1.09	0
97	SLE RA 9	1	-114	2104	4.74	1.09	0
97	SLE RA 10	2	-143	2327	5.86	1.42	0
97	SLE RA 11	2	-143	2327	5.86	1.42	0
97	SLE RA 12	2	-143	2327	5.86	1.42	0
97	SLE RA 13	2	-143	2327	5.86	1.42	0
97	SLE RA 14	2	-143	2327	5.86	1.42	0
97	SLE RA 15	2	-143	2327	5.86	1.42	0
97	SLE RA 16	2	-143	2327	5.86	1.42	0
97	SLE RA 17	2	-143	2327	5.86	1.42	0
97	SLE RA 18	2	-155	2423	6.34	1.57	0
97	SLE RA 19	2	-155	2423	6.34	1.57	0
97	SLE RA 20	2	-155	2423	6.34	1.57	0
97	SLE RA 21	2	-155	2423	6.34	1.57	0
97	SLE FR 1	1	-114	2104	4.74	1.09	0
97	SLE FR 2	1	-114	2104	4.74	1.09	0
97	SLE FR 3	1	-114	2104	4.74	1.09	0
97	SLE FR 4	2	-126	2200	5.22	1.23	0
97	SLE FR 5	2	-126	2200	5.22	1.23	0
97	SLE FR 6	2	-135	2263	5.54	1.33	0
97	SLE QP 1	1	-114	2104	4.74	1.09	0
97	SLE QP 2	2	-126	2200	5.22	1.23	0
97	SLD 1	-7	-112	2425	4.22	3.19	-0.02
97	SLD 2	-7	-112	2425	4.22	3.19	-0.02
97	SLD 3	-1	-231	2433	9.91	7.42	-0.01
97	SLD 4	-1	-231	2433	9.91	7.42	-0.01
97	SLD 5	-11	58	2254	-3.7	-4.59	-0.01
97	SLD 6	-11	58	2254	-3.7	-4.59	-0.01
97	SLD 7	10	-338	2282	15.25	9.5	0
97	SLD 8	10	-338	2282	15.25	9.5	0
97	SLD 9	-7	85	2117	-4.81	-7.03	0
97	SLD 10	-7	85	2117	-4.81	-7.03	0
97	SLD 11	14	-311	2145	14.14	7.05	0.01
97	SLD 12	14	-311	2145	14.14	7.05	0.01
97	SLD 13	4	-22	1966	0.53	-4.95	0.01
97	SLD 14	4	-22	1966	0.53	-4.95	0.01
97	SLD 15	10	-141	1974	6.21	-0.73	0.01
97	SLD 16	10	-141	1974	6.21	-0.73	0.01
97	SLV 1	-21	-92	2725	2.8	5.41	-0.04
97	SLV 2	-21	-92	2725	2.8	5.41	-0.04
97	SLV 3	-5	-374	2745	16.28	16.46	-0.03
97	SLV 4	-5	-374	2745	16.28	16.46	-0.03
97	SLV 5	-30	312	2326	-15.95	-14.27	-0.02
97	SLV 6	-30	312	2326	-15.95	-14.27	-0.02
97	SLV 7	24	-629	2394	28.98	22.56	0
97	SLV 8	24	-629	2394	28.98	22.56	0
97	SLV 9	-21	376	2005	-18.54	-20.09	0
97	SLV 10	-21	376	2005	-18.54	-20.09	0
97	SLV 11	33	-565	2073	26.39	16.74	0.02
97	SLV 12	33	-565	2073	26.39	16.74	0.02
97	SLV 13	8	121	1654	-5.84	-13.99	0.03
97	SLV 14	8	121	1654	-5.84	-13.99	0.03
97	SLV 15	24	-161	1674	7.64	-2.94	0.04
97	SLV 16	24	-161	1674	7.64	-2.94	0.04
98	SLU 1	0	0	1157	0	0	0
98	SLU 2	0	0	1157	0	0	0
98	SLU 3	0	0	1157	0	0	0
98	SLU 4	0	0	1157	0	0	0
98	SLU 5	0	0	1157	0	0	0
98	SLU 6	0	0	1157	0	0	0
98	SLU 7	0	0	1157	0	0	0
98	SLU 8	0	0	1157	0	0	0
98	SLU 9	0	0	1157	0	0	0
98	SLU 10	0	0	1416	0	0	0
98	SLU 11	0	0	1416	0	0	0
98	SLU 12	0	0	1416	0	0	0
98	SLU 13	0	0	1416	0	0	0
98	SLU 14	0	0	1416	0	0	0
98	SLU 15	0	0	1416	0	0	0
98	SLU 16	0	0	1416	0	0	0
98	SLU 17	0	0	1416	0	0	0
98	SLU 18	0	0	1528	0	0	0
98	SLU 19	0	0	1528	0	0	0
98	SLU 20	0	0	1528	0	0	0
98	SLU 21	0	0	1528	0	0	0
98	SLU 22	0	0	1311	0	0	0
98	SLU 23	0	0	1311	0	0	0
98	SLU 24	0	0	1311	0	0	0
98	SLU 25	0	0	1311	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
98	SLU 26	0	0	1311	0	0	0
98	SLU 27	0	0	1311	0	0	0
98	SLU 28	0	0	1311	0	0	0
98	SLU 29	0	0	1311	0	0	0
98	SLU 30	0	0	1311	0	0	0
98	SLU 31	0	0	1571	0	0	0
98	SLU 32	0	0	1571	0	0	0
98	SLU 33	0	0	1571	0	0	0
98	SLU 34	0	0	1571	0	0	0
98	SLU 35	0	0	1571	0	0	0
98	SLU 36	0	0	1571	0	0	0
98	SLU 37	0	0	1571	0	0	0
98	SLU 38	0	0	1571	0	0	0
98	SLU 39	0	0	1682	0	0	0
98	SLU 40	0	0	1682	0	0	0
98	SLU 41	0	0	1682	0	0	0
98	SLU 42	0	0	1682	0	0	0
98	SLU 43	0	0	1451	0	0	0
98	SLU 44	0	0	1451	0	0	0
98	SLU 45	0	0	1451	0	0	0
98	SLU 46	0	0	1451	0	0	0
98	SLU 47	0	0	1451	0	0	0
98	SLU 48	0	0	1451	0	0	0
98	SLU 49	0	0	1451	0	0	0
98	SLU 50	0	0	1451	0	0	0
98	SLU 51	0	0	1451	0	0	0
98	SLU 52	0	0	1710	0	0	0
98	SLU 53	0	0	1710	0	0	0
98	SLU 54	0	0	1710	0	0	0
98	SLU 55	0	0	1710	0	0	0
98	SLU 56	0	0	1710	0	0	0
98	SLU 57	0	0	1710	0	0	0
98	SLU 58	0	0	1710	0	0	0
98	SLU 59	0	0	1710	0	0	0
98	SLU 60	0	0	1822	0	0	0
98	SLU 61	0	0	1822	0	0	0
98	SLU 62	0	0	1822	0	0	0
98	SLU 63	0	0	1822	0	0	0
98	SLU 64	0	0	1605	0	0	0
98	SLU 65	0	0	1605	0	0	0
98	SLU 66	0	0	1605	0	0	0
98	SLU 67	0	0	1605	0	0	0
98	SLU 68	0	0	1605	0	0	0
98	SLU 69	0	0	1605	0	0	0
98	SLU 70	0	0	1605	0	0	0
98	SLU 71	0	0	1605	0	0	0
98	SLU 72	0	0	1605	0	0	0
98	SLU 73	0	0	1865	0	0	0
98	SLU 74	0	0	1865	0	0	0
98	SLU 75	0	0	1865	0	0	0
98	SLU 76	0	0	1865	0	0	0
98	SLU 77	0	0	1865	0	0	0
98	SLU 78	0	0	1865	0	0	0
98	SLU 79	0	0	1865	0	0	0
98	SLU 80	0	0	1865	0	0	0
98	SLU 81	0	0	1976	0	0	0
98	SLU 82	0	0	1976	0	0	0
98	SLU 83	0	0	1976	0	0	0
98	SLU 84	0	0	1976	0	0	0
98	SLE RA 1	0	0	1201	0	0	0
98	SLE RA 2	0	0	1201	0	0	0
98	SLE RA 3	0	0	1201	0	0	0
98	SLE RA 4	0	0	1201	0	0	0
98	SLE RA 5	0	0	1201	0	0	0
98	SLE RA 6	0	0	1201	0	0	0
98	SLE RA 7	0	0	1201	0	0	0
98	SLE RA 8	0	0	1201	0	0	0
98	SLE RA 9	0	0	1201	0	0	0
98	SLE RA 10	0	0	1374	0	0	0
98	SLE RA 11	0	0	1374	0	0	0
98	SLE RA 12	0	0	1374	0	0	0
98	SLE RA 13	0	0	1374	0	0	0
98	SLE RA 14	0	0	1374	0	0	0
98	SLE RA 15	0	0	1374	0	0	0
98	SLE RA 16	0	0	1374	0	0	0
98	SLE RA 17	0	0	1374	0	0	0
98	SLE RA 18	0	0	1448	0	0	0
98	SLE RA 19	0	0	1448	0	0	0
98	SLE RA 20	0	0	1448	0	0	0
98	SLE RA 21	0	0	1448	0	0	0
98	SLE FR 1	0	0	1201	0	0	0
98	SLE FR 2	0	0	1201	0	0	0
98	SLE FR 3	0	0	1201	0	0	0
98	SLE FR 4	0	0	1275	0	0	0
98	SLE FR 5	0	0	1275	0	0	0
98	SLE FR 6	0	0	1324	0	0	0
98	SLE QP 1	0	0	1201	0	0	0
98	SLE QP 2	0	0	1275	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
98	SLD 1	5	0	1270	-0.02	5.76	0
98	SLD 2	5	0	1270	-0.02	5.76	0
98	SLD 3	5	-1	1283	0.02	6.01	0
98	SLD 4	5	-1	1283	0.02	6.01	0
98	SLD 5	2	2	1255	-0.07	1.35	0
98	SLD 6	2	2	1255	-0.07	1.35	0
98	SLD 7	1	-2	1296	0.07	2.18	0
98	SLD 8	1	-2	1296	0.07	2.18	0
98	SLD 9	-1	2	1254	-0.07	-2.18	0
98	SLD 10	-1	2	1254	-0.07	-2.18	0
98	SLD 11	-2	-2	1295	0.07	-1.35	0
98	SLD 12	-2	-2	1295	0.07	-1.35	0
98	SLD 13	-5	1	1267	-0.02	-6.01	0
98	SLD 14	-5	1	1267	-0.02	-6.01	0
98	SLD 15	-5	0	1280	0.02	-5.76	0
98	SLD 16	-5	0	1280	0.02	-5.76	0
98	SLV 1	13	1	1262	-0.06	14.59	0
98	SLV 2	13	1	1262	-0.06	14.59	0
98	SLV 3	13	-3	1296	0.06	15.22	0
98	SLV 4	13	-3	1296	0.06	15.22	0
98	SLV 5	5	5	1220	-0.19	3.42	0
98	SLV 6	5	5	1220	-0.19	3.42	0
98	SLV 7	3	-6	1333	0.19	5.53	0
98	SLV 8	3	-6	1333	0.19	5.53	0
98	SLV 9	-3	6	1217	-0.19	-5.52	0
98	SLV 10	-3	6	1217	-0.19	-5.52	0
98	SLV 11	-5	-5	1330	0.19	-3.42	0
98	SLV 12	-5	-5	1330	0.19	-3.42	0
98	SLV 13	-13	3	1254	-0.06	-15.22	0
98	SLV 14	-13	3	1254	-0.06	-15.22	0
98	SLV 15	-13	-1	1288	0.06	-14.59	0
98	SLV 16	-13	-1	1288	0.06	-14.59	0
99	SLU 1	1	-111	1972	4.99	0.71	0
99	SLU 2	1	-111	1972	4.99	0.71	0
99	SLU 3	1	-111	1972	4.99	0.71	0
99	SLU 4	1	-111	1972	4.99	0.71	0
99	SLU 5	1	-111	1972	4.99	0.71	0
99	SLU 6	1	-111	1972	4.99	0.71	0
99	SLU 7	1	-111	1972	4.99	0.71	0
99	SLU 8	1	-111	1972	4.99	0.71	0
99	SLU 9	1	-111	1972	4.99	0.71	0
99	SLU 10	1	-149	2270	6.62	1.07	0
99	SLU 11	1	-149	2270	6.62	1.07	0
99	SLU 12	1	-149	2270	6.62	1.07	0
99	SLU 13	1	-149	2270	6.62	1.07	0
99	SLU 14	1	-149	2270	6.62	1.07	0
99	SLU 15	1	-149	2270	6.62	1.07	0
99	SLU 16	1	-149	2270	6.62	1.07	0
99	SLU 17	1	-149	2270	6.62	1.07	0
99	SLU 18	1	-165	2398	7.32	1.22	0
99	SLU 19	1	-165	2398	7.32	1.22	0
99	SLU 20	1	-165	2398	7.32	1.22	0
99	SLU 21	1	-165	2398	7.32	1.22	0
99	SLU 22	1	-133	2157	5.94	0.9	0
99	SLU 23	1	-133	2157	5.94	0.9	0
99	SLU 24	1	-133	2157	5.94	0.9	0
99	SLU 25	1	-133	2157	5.94	0.9	0
99	SLU 26	1	-133	2157	5.94	0.9	0
99	SLU 27	1	-133	2157	5.94	0.9	0
99	SLU 28	1	-133	2157	5.94	0.9	0
99	SLU 29	1	-133	2157	5.94	0.9	0
99	SLU 30	1	-133	2157	5.94	0.9	0
99	SLU 31	1	-170	2455	7.57	1.26	0
99	SLU 32	1	-170	2455	7.57	1.26	0
99	SLU 33	1	-170	2455	7.57	1.26	0
99	SLU 34	1	-170	2455	7.57	1.26	0
99	SLU 35	1	-170	2455	7.57	1.26	0
99	SLU 36	1	-170	2455	7.57	1.26	0
99	SLU 37	1	-170	2455	7.57	1.26	0
99	SLU 38	1	-170	2455	7.57	1.26	0
99	SLU 39	1	-186	2583	8.27	1.42	0
99	SLU 40	1	-186	2583	8.27	1.42	0
99	SLU 41	1	-186	2583	8.27	1.42	0
99	SLU 42	1	-186	2583	8.27	1.42	0
99	SLU 43	1	-137	2500	6.15	0.85	0
99	SLU 44	1	-137	2500	6.15	0.85	0
99	SLU 45	1	-137	2500	6.15	0.85	0
99	SLU 46	1	-137	2500	6.15	0.85	0
99	SLU 47	1	-137	2500	6.15	0.85	0
99	SLU 48	1	-137	2500	6.15	0.85	0
99	SLU 49	1	-137	2500	6.15	0.85	0
99	SLU 50	1	-137	2500	6.15	0.85	0
99	SLU 51	1	-137	2500	6.15	0.85	0
99	SLU 52	1	-174	2798	7.79	1.21	0
99	SLU 53	1	-174	2798	7.79	1.21	0
99	SLU 54	1	-174	2798	7.79	1.21	0
99	SLU 55	1	-174	2798	7.79	1.21	0
99	SLU 56	1	-174	2798	7.79	1.21	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
99	SLU 57	1	-174	2798	7.79	1.21	0
99	SLU 58	1	-174	2798	7.79	1.21	0
99	SLU 59	1	-174	2798	7.79	1.21	0
99	SLU 60	1	-190	2926	8.49	1.37	0
99	SLU 61	1	-190	2926	8.49	1.37	0
99	SLU 62	1	-190	2926	8.49	1.37	0
99	SLU 63	1	-190	2926	8.49	1.37	0
99	SLU 64	1	-159	2685	7.11	1.04	0
99	SLU 65	1	-159	2685	7.11	1.04	0
99	SLU 66	1	-159	2685	7.11	1.04	0
99	SLU 67	1	-159	2685	7.11	1.04	0
99	SLU 68	1	-159	2685	7.11	1.04	0
99	SLU 69	1	-159	2685	7.11	1.04	0
99	SLU 70	1	-159	2685	7.11	1.04	0
99	SLU 71	1	-159	2685	7.11	1.04	0
99	SLU 72	1	-159	2685	7.11	1.04	0
99	SLU 73	1	-196	2983	8.74	1.41	0
99	SLU 74	1	-196	2983	8.74	1.41	0
99	SLU 75	1	-196	2983	8.74	1.41	0
99	SLU 76	1	-196	2983	8.74	1.41	0
99	SLU 77	1	-196	2983	8.74	1.41	0
99	SLU 78	1	-196	2983	8.74	1.41	0
99	SLU 79	1	-196	2983	8.74	1.41	0
99	SLU 80	1	-196	2983	8.74	1.41	0
99	SLU 81	1	-212	3111	9.44	1.56	0
99	SLU 82	1	-212	3111	9.44	1.56	0
99	SLU 83	1	-212	3111	9.44	1.56	0
99	SLU 84	1	-212	3111	9.44	1.56	0
99	SLE RA 1	1	-117	2025	5.26	0.76	0
99	SLE RA 2	1	-117	2025	5.26	0.76	0
99	SLE RA 3	1	-117	2025	5.26	0.76	0
99	SLE RA 4	1	-117	2025	5.26	0.76	0
99	SLE RA 5	1	-117	2025	5.26	0.76	0
99	SLE RA 6	1	-117	2025	5.26	0.76	0
99	SLE RA 7	1	-117	2025	5.26	0.76	0
99	SLE RA 8	1	-117	2025	5.26	0.76	0
99	SLE RA 9	1	-117	2025	5.26	0.76	0
99	SLE RA 10	1	-142	2224	6.35	1	0
99	SLE RA 11	1	-142	2224	6.35	1	0
99	SLE RA 12	1	-142	2224	6.35	1	0
99	SLE RA 13	1	-142	2224	6.35	1	0
99	SLE RA 14	1	-142	2224	6.35	1	0
99	SLE RA 15	1	-142	2224	6.35	1	0
99	SLE RA 16	1	-142	2224	6.35	1	0
99	SLE RA 17	1	-142	2224	6.35	1	0
99	SLE RA 18	1	-153	2309	6.81	1.11	0
99	SLE RA 19	1	-153	2309	6.81	1.11	0
99	SLE RA 20	1	-153	2309	6.81	1.11	0
99	SLE RA 21	1	-153	2309	6.81	1.11	0
99	SLE FR 1	1	-117	2025	5.26	0.76	0
99	SLE FR 2	1	-117	2025	5.26	0.76	0
99	SLE FR 3	1	-117	2025	5.26	0.76	0
99	SLE FR 4	1	-128	2110	5.72	0.86	0
99	SLE FR 5	1	-128	2110	5.72	0.86	0
99	SLE FR 6	1	-135	2167	6.04	0.93	0
99	SLE QP 1	1	-117	2025	5.26	0.76	0
99	SLE QP 2	1	-128	2110	5.72	0.86	0
99	SLD 1	-7	-109	2298	4.67	6.94	-0.01
99	SLD 2	-7	-109	2298	4.67	6.94	-0.01
99	SLD 3	-1	-228	2311	10.45	12.36	-0.01
99	SLD 4	-1	-228	2311	10.45	12.36	-0.01
99	SLD 5	-11	59	2147	-3.37	-5.52	-0.01
99	SLD 6	-11	59	2147	-3.37	-5.52	-0.01
99	SLD 7	10	-339	2190	15.92	12.52	0
99	SLD 8	10	-339	2190	15.92	12.52	0
99	SLD 9	-9	83	2030	-4.47	-10.79	0
99	SLD 10	-9	83	2030	-4.47	-10.79	0
99	SLD 11	13	-315	2073	14.82	7.25	0.01
99	SLD 12	13	-315	2073	14.82	7.25	0.01
99	SLD 13	2	-28	1909	1	-10.63	0.01
99	SLD 14	2	-28	1909	1	-10.63	0.01
99	SLD 15	9	-147	1922	6.78	-5.21	0.01
99	SLD 16	9	-147	1922	6.78	-5.21	0.01
99	SLV 1	-19	-82	2549	3.14	14.85	-0.03
99	SLV 2	-19	-82	2549	3.14	14.85	-0.03
99	SLV 3	-2	-365	2581	16.91	28.92	-0.03
99	SLV 4	-2	-365	2581	16.91	28.92	-0.03
99	SLV 5	-31	316	2194	-15.93	-16.27	-0.02
99	SLV 6	-31	316	2194	-15.93	-16.27	-0.02
99	SLV 7	26	-629	2298	29.96	30.61	0
99	SLV 8	26	-629	2298	29.96	30.61	0
99	SLV 9	-24	373	1921	-18.51	-28.88	0
99	SLV 10	-24	373	1921	-18.51	-28.88	0
99	SLV 11	33	-572	2025	27.38	18	0.02
99	SLV 12	33	-572	2025	27.38	18	0.02
99	SLV 13	3	109	1639	-5.46	-27.19	0.03
99	SLV 14	3	109	1639	-5.46	-27.19	0.03
99	SLV 15	20	-174	1670	8.31	-13.12	0.03



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
99	SLV 16	20	-174	1670	8.31	-13.12	0.03
100	SLU 1	0	273	1182	-5.66	-0.19	0.03
100	SLU 2	0	273	1182	-5.66	-0.19	0.03
100	SLU 3	0	273	1182	-5.66	-0.19	0.03
100	SLU 4	0	273	1182	-5.66	-0.19	0.03
100	SLU 5	0	273	1182	-5.66	-0.19	0.03
100	SLU 6	0	273	1182	-5.66	-0.19	0.03
100	SLU 7	0	273	1182	-5.66	-0.19	0.03
100	SLU 8	0	273	1182	-5.66	-0.19	0.03
100	SLU 9	0	273	1182	-5.66	-0.19	0.03
100	SLU 10	0	305	1323	-6.19	-0.3	0.05
100	SLU 11	0	305	1323	-6.19	-0.3	0.05
100	SLU 12	0	305	1323	-6.19	-0.3	0.05
100	SLU 13	0	305	1323	-6.19	-0.3	0.05
100	SLU 14	0	305	1323	-6.19	-0.3	0.05
100	SLU 15	0	305	1323	-6.19	-0.3	0.05
100	SLU 16	0	305	1323	-6.19	-0.3	0.05
100	SLU 17	0	305	1323	-6.19	-0.3	0.05
100	SLU 18	0	319	1384	-6.41	-0.35	0.06
100	SLU 19	0	319	1384	-6.41	-0.35	0.06
100	SLU 20	0	319	1384	-6.41	-0.35	0.06
100	SLU 21	0	319	1384	-6.41	-0.35	0.06
100	SLU 22	0	293	1271	-5.99	-0.25	0.04
100	SLU 23	0	293	1271	-5.99	-0.25	0.04
100	SLU 24	0	293	1271	-5.99	-0.25	0.04
100	SLU 25	0	293	1271	-5.99	-0.25	0.04
100	SLU 26	0	293	1271	-5.99	-0.25	0.04
100	SLU 27	0	293	1271	-5.99	-0.25	0.04
100	SLU 28	0	293	1271	-5.99	-0.25	0.04
100	SLU 29	0	293	1271	-5.99	-0.25	0.04
100	SLU 30	0	293	1271	-5.99	-0.25	0.04
100	SLU 31	0	325	1413	-6.52	-0.36	0.06
100	SLU 32	0	325	1413	-6.52	-0.36	0.06
100	SLU 33	0	325	1413	-6.52	-0.36	0.06
100	SLU 34	0	325	1413	-6.52	-0.36	0.06
100	SLU 35	0	325	1413	-6.52	-0.36	0.06
100	SLU 36	0	325	1413	-6.52	-0.36	0.06
100	SLU 37	0	325	1413	-6.52	-0.36	0.06
100	SLU 38	0	325	1413	-6.52	-0.36	0.06
100	SLU 39	-1	339	1473	-6.74	-0.4	0.07
100	SLU 40	-1	339	1473	-6.74	-0.4	0.07
100	SLU 41	-1	339	1473	-6.74	-0.4	0.07
100	SLU 42	-1	339	1473	-6.74	-0.4	0.07
100	SLU 43	0	349	1506	-7.24	-0.23	0.04
100	SLU 44	0	349	1506	-7.24	-0.23	0.04
100	SLU 45	0	349	1506	-7.24	-0.23	0.04
100	SLU 46	0	349	1506	-7.24	-0.23	0.04
100	SLU 47	0	349	1506	-7.24	-0.23	0.04
100	SLU 48	0	349	1506	-7.24	-0.23	0.04
100	SLU 49	0	349	1506	-7.24	-0.23	0.04
100	SLU 50	0	349	1506	-7.24	-0.23	0.04
100	SLU 51	0	349	1506	-7.24	-0.23	0.04
100	SLU 52	0	380	1647	-7.77	-0.34	0.06
100	SLU 53	0	380	1647	-7.77	-0.34	0.06
100	SLU 54	0	380	1647	-7.77	-0.34	0.06
100	SLU 55	0	380	1647	-7.77	-0.34	0.06
100	SLU 56	0	380	1647	-7.77	-0.34	0.06
100	SLU 57	0	380	1647	-7.77	-0.34	0.06
100	SLU 58	0	380	1647	-7.77	-0.34	0.06
100	SLU 59	0	380	1647	-7.77	-0.34	0.06
100	SLU 60	0	394	1707	-8	-0.39	0.06
100	SLU 61	0	394	1707	-8	-0.39	0.06
100	SLU 62	0	394	1707	-8	-0.39	0.06
100	SLU 63	0	394	1707	-8	-0.39	0.06
100	SLU 64	0	368	1595	-7.57	-0.29	0.05
100	SLU 65	0	368	1595	-7.57	-0.29	0.05
100	SLU 66	0	368	1595	-7.57	-0.29	0.05
100	SLU 67	0	368	1595	-7.57	-0.29	0.05
100	SLU 68	0	368	1595	-7.57	-0.29	0.05
100	SLU 69	0	368	1595	-7.57	-0.29	0.05
100	SLU 70	0	368	1595	-7.57	-0.29	0.05
100	SLU 71	0	368	1595	-7.57	-0.29	0.05
100	SLU 72	0	368	1595	-7.57	-0.29	0.05
100	SLU 73	0	400	1736	-8.1	-0.4	0.06
100	SLU 74	0	400	1736	-8.1	-0.4	0.06
100	SLU 75	0	400	1736	-8.1	-0.4	0.06
100	SLU 76	0	400	1736	-8.1	-0.4	0.06
100	SLU 77	0	400	1736	-8.1	-0.4	0.06
100	SLU 78	0	400	1736	-8.1	-0.4	0.06
100	SLU 79	0	400	1736	-8.1	-0.4	0.06
100	SLU 80	0	400	1736	-8.1	-0.4	0.06
100	SLU 81	-1	414	1797	-8.33	-0.44	0.07
100	SLU 82	-1	414	1797	-8.33	-0.44	0.07
100	SLU 83	-1	414	1797	-8.33	-0.44	0.07
100	SLU 84	-1	414	1797	-8.33	-0.44	0.07
100	SLE RA 1	0	279	1207	-5.75	-0.21	0.03
100	SLE RA 2	0	279	1207	-5.75	-0.21	0.03
100	SLE RA 3	0	279	1207	-5.75	-0.21	0.03



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
100	SLE RA 4	0	279	1207	-5.75	-0.21	0.03
100	SLE RA 5	0	279	1207	-5.75	-0.21	0.03
100	SLE RA 6	0	279	1207	-5.75	-0.21	0.03
100	SLE RA 7	0	279	1207	-5.75	-0.21	0.03
100	SLE RA 8	0	279	1207	-5.75	-0.21	0.03
100	SLE RA 9	0	279	1207	-5.75	-0.21	0.03
100	SLE RA 10	0	300	1302	-6.1	-0.28	0.05
100	SLE RA 11	0	300	1302	-6.1	-0.28	0.05
100	SLE RA 12	0	300	1302	-6.1	-0.28	0.05
100	SLE RA 13	0	300	1302	-6.1	-0.28	0.05
100	SLE RA 14	0	300	1302	-6.1	-0.28	0.05
100	SLE RA 15	0	300	1302	-6.1	-0.28	0.05
100	SLE RA 16	0	300	1302	-6.1	-0.28	0.05
100	SLE RA 17	0	300	1302	-6.1	-0.28	0.05
100	SLE RA 18	0	309	1342	-6.26	-0.31	0.05
100	SLE RA 19	0	309	1342	-6.26	-0.31	0.05
100	SLE RA 20	0	309	1342	-6.26	-0.31	0.05
100	SLE RA 21	0	309	1342	-6.26	-0.31	0.05
100	SLE FR 1	0	279	1207	-5.75	-0.21	0.03
100	SLE FR 2	0	279	1207	-5.75	-0.21	0.03
100	SLE FR 3	0	279	1207	-5.75	-0.21	0.03
100	SLE FR 4	0	288	1248	-5.9	-0.24	0.04
100	SLE FR 5	0	288	1248	-5.9	-0.24	0.04
100	SLE FR 6	0	294	1275	-6	-0.26	0.04
100	SLE QP 1	0	279	1207	-5.75	-0.21	0.03
100	SLE QP 2	0	288	1248	-5.9	-0.24	0.04
100	SLD 1	-17	307	1269	-6.77	8.02	-1.1
100	SLD 2	-17	307	1269	-6.77	8.02	-1.1
100	SLD 3	-27	239	1088	-4.15	5.13	-0.64
100	SLD 4	-27	239	1088	-4.15	5.13	-0.64
100	SLD 5	10	396	1529	-10.14	6.63	-1
100	SLD 6	10	396	1529	-10.14	6.63	-1
100	SLD 7	-23	171	925	-1.4	-3.02	0.53
100	SLD 8	-23	171	925	-1.4	-3.02	0.53
100	SLD 9	23	405	1570	-10.41	2.54	-0.46
100	SLD 10	23	405	1570	-10.41	2.54	-0.46
100	SLD 11	-10	180	967	-1.67	-7.1	1.08
100	SLD 12	-10	180	967	-1.67	-7.1	1.08
100	SLD 13	26	337	1407	-7.66	-5.61	0.72
100	SLD 14	26	337	1407	-7.66	-5.61	0.72
100	SLD 15	16	269	1226	-5.04	-8.5	1.18
100	SLD 16	16	269	1226	-5.04	-8.5	1.18
100	SLV 1	-41	333	1302	-7.98	19.69	-2.71
100	SLV 2	-41	333	1302	-7.98	19.69	-2.71
100	SLV 3	-67	172	870	-1.72	12.13	-1.49
100	SLV 4	-67	172	870	-1.72	12.13	-1.49
100	SLV 5	27	547	1920	-16.01	17.22	-2.62
100	SLV 6	27	547	1920	-16.01	17.22	-2.62
100	SLV 7	-59	8	479	4.84	-8.01	1.42
100	SLV 8	-59	8	479	4.84	-8.01	1.42
100	SLV 9	59	568	2017	-16.65	7.53	-1.34
100	SLV 10	59	568	2017	-16.65	7.53	-1.34
100	SLV 11	-27	29	576	4.21	-17.7	2.7
100	SLV 12	-27	29	576	4.21	-17.7	2.7
100	SLV 13	66	404	1626	-10.09	-12.61	1.57
100	SLV 14	66	404	1626	-10.09	-12.61	1.57
100	SLV 15	40	243	1193	-3.83	-20.17	2.79
100	SLV 16	40	243	1193	-3.83	-20.17	2.79
101	SLU 1	0	0	1145	0	0	0
101	SLU 2	0	0	1145	0	0	0
101	SLU 3	0	0	1145	0	0	0
101	SLU 4	0	0	1145	0	0	0
101	SLU 5	0	0	1145	0	0	0
101	SLU 6	0	0	1145	0	0	0
101	SLU 7	0	0	1145	0	0	0
101	SLU 8	0	0	1145	0	0	0
101	SLU 9	0	0	1145	0	0	0
101	SLU 10	0	0	1387	0	0	0
101	SLU 11	0	0	1387	0	0	0
101	SLU 12	0	0	1387	0	0	0
101	SLU 13	0	0	1387	0	0	0
101	SLU 14	0	0	1387	0	0	0
101	SLU 15	0	0	1387	0	0	0
101	SLU 16	0	0	1387	0	0	0
101	SLU 17	0	0	1387	0	0	0
101	SLU 18	0	0	1491	0	0	0
101	SLU 19	0	0	1491	0	0	0
101	SLU 20	0	0	1491	0	0	0
101	SLU 21	0	0	1491	0	0	0
101	SLU 22	0	0	1291	0	0	0
101	SLU 23	0	0	1291	0	0	0
101	SLU 24	0	0	1291	0	0	0
101	SLU 25	0	0	1291	0	0	0
101	SLU 26	0	0	1291	0	0	0
101	SLU 27	0	0	1291	0	0	0
101	SLU 28	0	0	1291	0	0	0
101	SLU 29	0	0	1291	0	0	0
101	SLU 30	0	0	1291	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
101	SLU 31	0	0	1533	0	0	0
101	SLU 32	0	0	1533	0	0	0
101	SLU 33	0	0	1533	0	0	0
101	SLU 34	0	0	1533	0	0	0
101	SLU 35	0	0	1533	0	0	0
101	SLU 36	0	0	1533	0	0	0
101	SLU 37	0	0	1533	0	0	0
101	SLU 38	0	0	1533	0	0	0
101	SLU 39	0	0	1636	0	0	0
101	SLU 40	0	0	1636	0	0	0
101	SLU 41	0	0	1636	0	0	0
101	SLU 42	0	0	1636	0	0	0
101	SLU 43	0	0	1439	0	0	0
101	SLU 44	0	0	1439	0	0	0
101	SLU 45	0	0	1439	0	0	0
101	SLU 46	0	0	1439	0	0	0
101	SLU 47	0	0	1439	0	0	0
101	SLU 48	0	0	1439	0	0	0
101	SLU 49	0	0	1439	0	0	0
101	SLU 50	0	0	1439	0	0	0
101	SLU 51	0	0	1439	0	0	0
101	SLU 52	0	0	1681	0	0	0
101	SLU 53	0	0	1681	0	0	0
101	SLU 54	0	0	1681	0	0	0
101	SLU 55	0	0	1681	0	0	0
101	SLU 56	0	0	1681	0	0	0
101	SLU 57	0	0	1681	0	0	0
101	SLU 58	0	0	1681	0	0	0
101	SLU 59	0	0	1681	0	0	0
101	SLU 60	0	0	1784	0	0	0
101	SLU 61	0	0	1784	0	0	0
101	SLU 62	0	0	1784	0	0	0
101	SLU 63	0	0	1784	0	0	0
101	SLU 64	0	0	1584	0	0	0
101	SLU 65	0	0	1584	0	0	0
101	SLU 66	0	0	1584	0	0	0
101	SLU 67	0	0	1584	0	0	0
101	SLU 68	0	0	1584	0	0	0
101	SLU 69	0	0	1584	0	0	0
101	SLU 70	0	0	1584	0	0	0
101	SLU 71	0	0	1584	0	0	0
101	SLU 72	0	0	1584	0	0	0
101	SLU 73	0	0	1826	0	0	0
101	SLU 74	0	0	1826	0	0	0
101	SLU 75	0	0	1826	0	0	0
101	SLU 76	0	0	1826	0	0	0
101	SLU 77	0	0	1826	0	0	0
101	SLU 78	0	0	1826	0	0	0
101	SLU 79	0	0	1826	0	0	0
101	SLU 80	0	0	1826	0	0	0
101	SLU 81	0	0	1930	0	0	0
101	SLU 82	0	0	1930	0	0	0
101	SLU 83	0	0	1930	0	0	0
101	SLU 84	0	0	1930	0	0	0
101	SLE RA 1	0	0	1187	0	0	0
101	SLE RA 2	0	0	1187	0	0	0
101	SLE RA 3	0	0	1187	0	0	0
101	SLE RA 4	0	0	1187	0	0	0
101	SLE RA 5	0	0	1187	0	0	0
101	SLE RA 6	0	0	1187	0	0	0
101	SLE RA 7	0	0	1187	0	0	0
101	SLE RA 8	0	0	1187	0	0	0
101	SLE RA 9	0	0	1187	0	0	0
101	SLE RA 10	0	0	1348	0	0	0
101	SLE RA 11	0	0	1348	0	0	0
101	SLE RA 12	0	0	1348	0	0	0
101	SLE RA 13	0	0	1348	0	0	0
101	SLE RA 14	0	0	1348	0	0	0
101	SLE RA 15	0	0	1348	0	0	0
101	SLE RA 16	0	0	1348	0	0	0
101	SLE RA 17	0	0	1348	0	0	0
101	SLE RA 18	0	0	1417	0	0	0
101	SLE RA 19	0	0	1417	0	0	0
101	SLE RA 20	0	0	1417	0	0	0
101	SLE RA 21	0	0	1417	0	0	0
101	SLE FR 1	0	0	1187	0	0	0
101	SLE FR 2	0	0	1187	0	0	0
101	SLE FR 3	0	0	1187	0	0	0
101	SLE FR 4	0	0	1256	0	0	0
101	SLE FR 5	0	0	1256	0	0	0
101	SLE FR 6	0	0	1302	0	0	0
101	SLE QP 1	0	0	1187	0	0	0
101	SLE QP 2	0	0	1256	0	0	0
101	SLD 1	5	0	1254	-0.05	6.51	0
101	SLD 2	5	0	1254	-0.05	6.51	0
101	SLD 3	5	-1	1261	0.05	6.78	0
101	SLD 4	5	-1	1261	0.05	6.78	0
101	SLD 5	2	2	1245	-0.16	1.55	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
101	SLD 6	2	2	1245	-0.16	1.55	0
101	SLD 7	1	-2	1268	0.16	2.44	0
101	SLD 8	1	-2	1268	0.16	2.44	0
101	SLD 9	-1	2	1244	-0.16	-2.44	0
101	SLD 10	-1	2	1244	-0.16	-2.44	0
101	SLD 11	-2	-2	1267	0.16	-1.55	0
101	SLD 12	-2	-2	1267	0.16	-1.55	0
101	SLD 13	-5	1	1251	-0.05	-6.77	0
101	SLD 14	-5	1	1251	-0.05	-6.77	0
101	SLD 15	-5	0	1258	0.05	-6.51	0
101	SLD 16	-5	0	1258	0.05	-6.51	0
101	SLV 1	12	1	1252	-0.13	16.54	0
101	SLV 2	12	1	1252	-0.13	16.54	0
101	SLV 3	12	-2	1268	0.14	17.23	0
101	SLV 4	12	-2	1268	0.14	17.23	0
101	SLV 5	5	5	1230	-0.45	3.92	0
101	SLV 6	5	5	1230	-0.45	3.92	0
101	SLV 7	3	-5	1285	0.45	6.21	0
101	SLV 8	3	-5	1285	0.45	6.21	0
101	SLV 9	-3	5	1227	-0.45	-6.21	0
101	SLV 10	-3	5	1227	-0.45	-6.21	0
101	SLV 11	-5	-5	1282	0.45	-3.92	0
101	SLV 12	-5	-5	1282	0.45	-3.92	0
101	SLV 13	-12	2	1244	-0.14	-17.22	0
101	SLV 14	-12	2	1244	-0.14	-17.22	0
101	SLV 15	-12	-1	1260	0.13	-16.54	0
101	SLV 16	-12	-1	1260	0.13	-16.54	0
102	SLU 1	0	-117	1924	5.43	0.49	0
102	SLU 2	0	-117	1924	5.43	0.49	0
102	SLU 3	0	-117	1924	5.43	0.49	0
102	SLU 4	0	-117	1924	5.43	0.49	0
102	SLU 5	0	-117	1924	5.43	0.49	0
102	SLU 6	0	-117	1924	5.43	0.49	0
102	SLU 7	0	-117	1924	5.43	0.49	0
102	SLU 8	0	-117	1924	5.43	0.49	0
102	SLU 9	0	-117	1924	5.43	0.49	0
102	SLU 10	1	-150	2199	6.92	0.75	0
102	SLU 11	1	-150	2199	6.92	0.75	0
102	SLU 12	1	-150	2199	6.92	0.75	0
102	SLU 13	1	-150	2199	6.92	0.75	0
102	SLU 14	1	-150	2199	6.92	0.75	0
102	SLU 15	1	-150	2199	6.92	0.75	0
102	SLU 16	1	-150	2199	6.92	0.75	0
102	SLU 17	1	-150	2199	6.92	0.75	0
102	SLU 18	1	-164	2317	7.56	0.86	0
102	SLU 19	1	-164	2317	7.56	0.86	0
102	SLU 20	1	-164	2317	7.56	0.86	0
102	SLU 21	1	-164	2317	7.56	0.86	0
102	SLU 22	0	-137	2096	6.33	0.63	0
102	SLU 23	0	-137	2096	6.33	0.63	0
102	SLU 24	0	-137	2096	6.33	0.63	0
102	SLU 25	0	-137	2096	6.33	0.63	0
102	SLU 26	0	-137	2096	6.33	0.63	0
102	SLU 27	0	-137	2096	6.33	0.63	0
102	SLU 28	0	-137	2096	6.33	0.63	0
102	SLU 29	0	-137	2096	6.33	0.63	0
102	SLU 30	0	-137	2096	6.33	0.63	0
102	SLU 31	1	-170	2371	7.82	0.89	0
102	SLU 32	1	-170	2371	7.82	0.89	0
102	SLU 33	1	-170	2371	7.82	0.89	0
102	SLU 34	1	-170	2371	7.82	0.89	0
102	SLU 35	1	-170	2371	7.82	0.89	0
102	SLU 36	1	-170	2371	7.82	0.89	0
102	SLU 37	1	-170	2371	7.82	0.89	0
102	SLU 38	1	-170	2371	7.82	0.89	0
102	SLU 39	1	-184	2489	8.46	1	0
102	SLU 40	1	-184	2489	8.46	1	0
102	SLU 41	1	-184	2489	8.46	1	0
102	SLU 42	1	-184	2489	8.46	1	0
102	SLU 43	0	-146	2442	6.76	0.59	0
102	SLU 44	0	-146	2442	6.76	0.59	0
102	SLU 45	0	-146	2442	6.76	0.59	0
102	SLU 46	0	-146	2442	6.76	0.59	0
102	SLU 47	0	-146	2442	6.76	0.59	0
102	SLU 48	0	-146	2442	6.76	0.59	0
102	SLU 49	0	-146	2442	6.76	0.59	0
102	SLU 50	0	-146	2442	6.76	0.59	0
102	SLU 51	0	-146	2442	6.76	0.59	0
102	SLU 52	1	-179	2717	8.24	0.85	0
102	SLU 53	1	-179	2717	8.24	0.85	0
102	SLU 54	1	-179	2717	8.24	0.85	0
102	SLU 55	1	-179	2717	8.24	0.85	0
102	SLU 56	1	-179	2717	8.24	0.85	0
102	SLU 57	1	-179	2717	8.24	0.85	0
102	SLU 58	1	-179	2717	8.24	0.85	0
102	SLU 59	1	-179	2717	8.24	0.85	0
102	SLU 60	1	-193	2835	8.88	0.96	0
102	SLU 61	1	-193	2835	8.88	0.96	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
102	SLU 62	1	-193	2835	8.88	0.96	0
102	SLU 63	1	-193	2835	8.88	0.96	0
102	SLU 64	0	-165	2614	7.66	0.73	0
102	SLU 65	0	-165	2614	7.66	0.73	0
102	SLU 66	0	-165	2614	7.66	0.73	0
102	SLU 67	0	-165	2614	7.66	0.73	0
102	SLU 68	0	-165	2614	7.66	0.73	0
102	SLU 69	0	-165	2614	7.66	0.73	0
102	SLU 70	0	-165	2614	7.66	0.73	0
102	SLU 71	0	-165	2614	7.66	0.73	0
102	SLU 72	0	-165	2614	7.66	0.73	0
102	SLU 73	1	-198	2889	9.14	0.99	0
102	SLU 74	1	-198	2889	9.14	0.99	0
102	SLU 75	1	-198	2889	9.14	0.99	0
102	SLU 76	1	-198	2889	9.14	0.99	0
102	SLU 77	1	-198	2889	9.14	0.99	0
102	SLU 78	1	-198	2889	9.14	0.99	0
102	SLU 79	1	-198	2889	9.14	0.99	0
102	SLU 80	1	-198	2889	9.14	0.99	0
102	SLU 81	1	-213	3007	9.78	1.1	0
102	SLU 82	1	-213	3007	9.78	1.1	0
102	SLU 83	1	-213	3007	9.78	1.1	0
102	SLU 84	1	-213	3007	9.78	1.1	0
102	SLE RA 1	0	-123	1973	5.69	0.53	0
102	SLE RA 2	0	-123	1973	5.69	0.53	0
102	SLE RA 3	0	-123	1973	5.69	0.53	0
102	SLE RA 4	0	-123	1973	5.69	0.53	0
102	SLE RA 5	0	-123	1973	5.69	0.53	0
102	SLE RA 6	0	-123	1973	5.69	0.53	0
102	SLE RA 7	0	-123	1973	5.69	0.53	0
102	SLE RA 8	0	-123	1973	5.69	0.53	0
102	SLE RA 9	0	-123	1973	5.69	0.53	0
102	SLE RA 10	0	-145	2156	6.68	0.7	0
102	SLE RA 11	0	-145	2156	6.68	0.7	0
102	SLE RA 12	0	-145	2156	6.68	0.7	0
102	SLE RA 13	0	-145	2156	6.68	0.7	0
102	SLE RA 14	0	-145	2156	6.68	0.7	0
102	SLE RA 15	0	-145	2156	6.68	0.7	0
102	SLE RA 16	0	-145	2156	6.68	0.7	0
102	SLE RA 17	0	-145	2156	6.68	0.7	0
102	SLE RA 18	1	-154	2235	7.11	0.78	0
102	SLE RA 19	1	-154	2235	7.11	0.78	0
102	SLE RA 20	1	-154	2235	7.11	0.78	0
102	SLE RA 21	1	-154	2235	7.11	0.78	0
102	SLE FR 1	0	-123	1973	5.69	0.53	0
102	SLE FR 2	0	-123	1973	5.69	0.53	0
102	SLE FR 3	0	-123	1973	5.69	0.53	0
102	SLE FR 4	0	-132	2051	6.12	0.6	0
102	SLE FR 5	0	-132	2051	6.12	0.6	0
102	SLE FR 6	0	-139	2104	6.4	0.65	0
102	SLE QP 1	0	-123	1973	5.69	0.53	0
102	SLE QP 2	0	-132	2051	6.12	0.6	0
102	SLD 1	10	-111	2216	4.97	11.31	-0.01
102	SLD 2	10	-111	2216	4.97	11.31	-0.01
102	SLD 3	16	-229	2234	10.67	17.58	-0.01
102	SLD 4	16	-229	2234	10.67	17.58	-0.01
102	SLD 5	-6	53	2074	-2.87	-5.69	-0.01
102	SLD 6	-6	53	2074	-2.87	-5.69	-0.01
102	SLD 7	15	-341	2133	16.13	15.2	0
102	SLD 8	15	-341	2133	16.13	15.2	0
102	SLD 9	-14	76	1970	-3.89	-13.99	0
102	SLD 10	-14	76	1970	-3.89	-13.99	0
102	SLD 11	7	-318	2029	15.11	6.9	0.01
102	SLD 12	7	-318	2029	15.11	6.9	0.01
102	SLD 13	-15	-36	1869	1.57	-16.37	0.01
102	SLD 14	-15	-36	1869	1.57	-16.37	0.01
102	SLD 15	-9	-154	1887	7.27	-10.1	0.01
102	SLD 16	-9	-154	1887	7.27	-10.1	0.01
102	SLV 1	21	-80	2435	3.34	25.76	-0.02
102	SLV 2	21	-80	2435	3.34	25.76	-0.02
102	SLV 3	38	-361	2478	16.86	41.9	-0.02
102	SLV 4	38	-361	2478	16.86	41.9	-0.02
102	SLV 5	-18	309	2101	-15.21	-16.33	-0.02
102	SLV 6	-18	309	2101	-15.21	-16.33	-0.02
102	SLV 7	37	-627	2245	29.84	37.47	0.01
102	SLV 8	37	-627	2245	29.84	37.47	0.01
102	SLV 9	-36	362	1858	-17.6	-36.26	-0.01
102	SLV 10	-36	362	1858	-17.6	-36.26	-0.01
102	SLV 11	19	-574	2001	27.45	17.54	0.02
102	SLV 12	19	-574	2001	27.45	17.54	0.02
102	SLV 13	-37	96	1624	-4.62	-40.69	0.02
102	SLV 14	-37	96	1624	-4.62	-40.69	0.02
102	SLV 15	-21	-184	1667	8.89	-24.55	0.02
102	SLV 16	-21	-184	1667	8.89	-24.55	0.02
103	SLU 1	0	138	2147	-7.65	-0.35	0
103	SLU 2	0	138	2147	-7.65	-0.35	0
103	SLU 3	0	138	2147	-7.65	-0.35	0
103	SLU 4	0	138	2147	-7.65	-0.35	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
103	SLU 5	0	138	2147	-7.65	-0.35	0
103	SLU 6	0	138	2147	-7.65	-0.35	0
103	SLU 7	0	138	2147	-7.65	-0.35	0
103	SLU 8	0	138	2147	-7.65	-0.35	0
103	SLU 9	0	138	2147	-7.65	-0.35	0
103	SLU 10	-1	152	2417	-8.45	-0.54	0
103	SLU 11	-1	152	2417	-8.45	-0.54	0
103	SLU 12	-1	152	2417	-8.45	-0.54	0
103	SLU 13	-1	152	2417	-8.45	-0.54	0
103	SLU 14	-1	152	2417	-8.45	-0.54	0
103	SLU 15	-1	152	2417	-8.45	-0.54	0
103	SLU 16	-1	152	2417	-8.45	-0.54	0
103	SLU 17	-1	152	2417	-8.45	-0.54	0
103	SLU 18	-1	158	2533	-8.79	-0.62	0
103	SLU 19	-1	158	2533	-8.79	-0.62	0
103	SLU 20	-1	158	2533	-8.79	-0.62	0
103	SLU 21	-1	158	2533	-8.79	-0.62	0
103	SLU 22	0	146	2318	-8.1	-0.44	0
103	SLU 23	0	146	2318	-8.1	-0.44	0
103	SLU 24	0	146	2318	-8.1	-0.44	0
103	SLU 25	0	146	2318	-8.1	-0.44	0
103	SLU 26	0	146	2318	-8.1	-0.44	0
103	SLU 27	0	146	2318	-8.1	-0.44	0
103	SLU 28	0	146	2318	-8.1	-0.44	0
103	SLU 29	0	146	2318	-8.1	-0.44	0
103	SLU 30	0	146	2318	-8.1	-0.44	0
103	SLU 31	-1	160	2588	-8.9	-0.63	0
103	SLU 32	-1	160	2588	-8.9	-0.63	0
103	SLU 33	-1	160	2588	-8.9	-0.63	0
103	SLU 34	-1	160	2588	-8.9	-0.63	0
103	SLU 35	-1	160	2588	-8.9	-0.63	0
103	SLU 36	-1	160	2588	-8.9	-0.63	0
103	SLU 37	-1	160	2588	-8.9	-0.63	0
103	SLU 38	-1	160	2588	-8.9	-0.63	0
103	SLU 39	-1	167	2704	-9.25	-0.72	0
103	SLU 40	-1	167	2704	-9.25	-0.72	0
103	SLU 41	-1	167	2704	-9.25	-0.72	0
103	SLU 42	-1	167	2704	-9.25	-0.72	0
103	SLU 43	0	176	2732	-9.79	-0.42	0
103	SLU 44	0	176	2732	-9.79	-0.42	0
103	SLU 45	0	176	2732	-9.79	-0.42	0
103	SLU 46	0	176	2732	-9.79	-0.42	0
103	SLU 47	0	176	2732	-9.79	-0.42	0
103	SLU 48	0	176	2732	-9.79	-0.42	0
103	SLU 49	0	176	2732	-9.79	-0.42	0
103	SLU 50	0	176	2732	-9.79	-0.42	0
103	SLU 51	0	176	2732	-9.79	-0.42	0
103	SLU 52	-1	191	3002	-10.59	-0.61	0
103	SLU 53	-1	191	3002	-10.59	-0.61	0
103	SLU 54	-1	191	3002	-10.59	-0.61	0
103	SLU 55	-1	191	3002	-10.59	-0.61	0
103	SLU 56	-1	191	3002	-10.59	-0.61	0
103	SLU 57	-1	191	3002	-10.59	-0.61	0
103	SLU 58	-1	191	3002	-10.59	-0.61	0
103	SLU 59	-1	191	3002	-10.59	-0.61	0
103	SLU 60	-1	197	3118	-10.94	-0.69	0
103	SLU 61	-1	197	3118	-10.94	-0.69	0
103	SLU 62	-1	197	3118	-10.94	-0.69	0
103	SLU 63	-1	197	3118	-10.94	-0.69	0
103	SLU 64	-1	184	2903	-10.24	-0.51	0
103	SLU 65	-1	184	2903	-10.24	-0.51	0
103	SLU 66	-1	184	2903	-10.24	-0.51	0
103	SLU 67	-1	184	2903	-10.24	-0.51	0
103	SLU 68	-1	184	2903	-10.24	-0.51	0
103	SLU 69	-1	184	2903	-10.24	-0.51	0
103	SLU 70	-1	184	2903	-10.24	-0.51	0
103	SLU 71	-1	184	2903	-10.24	-0.51	0
103	SLU 72	-1	184	2903	-10.24	-0.51	0
103	SLU 73	-1	199	3174	-11.04	-0.7	0
103	SLU 74	-1	199	3174	-11.04	-0.7	0
103	SLU 75	-1	199	3174	-11.04	-0.7	0
103	SLU 76	-1	199	3174	-11.04	-0.7	0
103	SLU 77	-1	199	3174	-11.04	-0.7	0
103	SLU 78	-1	199	3174	-11.04	-0.7	0
103	SLU 79	-1	199	3174	-11.04	-0.7	0
103	SLU 80	-1	199	3174	-11.04	-0.7	0
103	SLU 81	-1	205	3289	-11.39	-0.79	0
103	SLU 82	-1	205	3289	-11.39	-0.79	0
103	SLU 83	-1	205	3289	-11.39	-0.79	0
103	SLU 84	-1	205	3289	-11.39	-0.79	0
103	SLE RA 1	0	140	2196	-7.78	-0.37	0
103	SLE RA 2	0	140	2196	-7.78	-0.37	0
103	SLE RA 3	0	140	2196	-7.78	-0.37	0
103	SLE RA 4	0	140	2196	-7.78	-0.37	0
103	SLE RA 5	0	140	2196	-7.78	-0.37	0
103	SLE RA 6	0	140	2196	-7.78	-0.37	0
103	SLE RA 7	0	140	2196	-7.78	-0.37	0
103	SLE RA 8	0	140	2196	-7.78	-0.37	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
103	SLE RA 9	0	140	2196	-7.78	-0.37	0
103	SLE RA 10	-1	150	2376	-8.31	-0.5	0
103	SLE RA 11	-1	150	2376	-8.31	-0.5	0
103	SLE RA 12	-1	150	2376	-8.31	-0.5	0
103	SLE RA 13	-1	150	2376	-8.31	-0.5	0
103	SLE RA 14	-1	150	2376	-8.31	-0.5	0
103	SLE RA 15	-1	150	2376	-8.31	-0.5	0
103	SLE RA 16	-1	150	2376	-8.31	-0.5	0
103	SLE RA 17	-1	150	2376	-8.31	-0.5	0
103	SLE RA 18	-1	154	2453	-8.54	-0.56	0
103	SLE RA 19	-1	154	2453	-8.54	-0.56	0
103	SLE RA 20	-1	154	2453	-8.54	-0.56	0
103	SLE RA 21	-1	154	2453	-8.54	-0.56	0
103	SLE FR 1	0	140	2196	-7.78	-0.37	0
103	SLE FR 2	0	140	2196	-7.78	-0.37	0
103	SLE FR 3	0	140	2196	-7.78	-0.37	0
103	SLE FR 4	0	144	2273	-8.01	-0.43	0
103	SLE FR 5	0	144	2273	-8.01	-0.43	0
103	SLE FR 6	-1	147	2324	-8.16	-0.46	0
103	SLE QP 1	0	140	2196	-7.78	-0.37	0
103	SLE QP 2	0	144	2273	-8.01	-0.43	0
103	SLD 1	27	168	2217	-9.5	23.02	0.08
103	SLD 2	27	168	2217	-9.5	23.02	0.08
103	SLD 3	20	84	2040	-4.6	16.58	0.06
103	SLD 4	20	84	2040	-4.6	16.58	0.06
103	SLD 5	18	279	2524	-15.89	16.37	0.07
103	SLD 6	18	279	2524	-15.89	16.37	0.07
103	SLD 7	-5	-2	1935	0.44	-5.09	-0.03
103	SLD 8	-5	-2	1935	0.44	-5.09	-0.03
103	SLD 9	4	290	2611	-16.46	4.24	0.02
103	SLD 10	4	290	2611	-16.46	4.24	0.02
103	SLD 11	-19	9	2022	-0.13	-17.23	-0.07
103	SLD 12	-19	9	2022	-0.13	-17.23	-0.07
103	SLD 13	-20	204	2506	-11.42	-17.44	-0.06
103	SLD 14	-20	204	2506	-11.42	-17.44	-0.06
103	SLD 15	-27	120	2329	-6.52	-23.88	-0.09
103	SLD 16	-27	120	2329	-6.52	-23.88	-0.09
103	SLV 1	65	202	2146	-11.58	56.42	0.21
103	SLV 2	65	202	2146	-11.58	56.42	0.21
103	SLV 3	47	1	1725	0.1	39.92	0.13
103	SLV 4	47	1	1725	0.1	39.92	0.13
103	SLV 5	46	466	2874	-26.8	41.65	0.17
103	SLV 6	46	466	2874	-26.8	41.65	0.17
103	SLV 7	-14	-204	1470	12.15	-13.35	-0.07
103	SLV 8	-14	-204	1470	12.15	-13.35	-0.07
103	SLV 9	13	492	3076	-28.17	12.49	0.07
103	SLV 10	13	492	3076	-28.17	12.49	0.07
103	SLV 11	-47	-178	1672	10.79	-42.5	-0.17
103	SLV 12	-47	-178	1672	10.79	-42.5	-0.17
103	SLV 13	-47	287	2821	-16.12	-40.77	-0.14
103	SLV 14	-47	287	2821	-16.12	-40.77	-0.14
103	SLV 15	-65	86	2400	-4.44	-57.27	-0.21
103	SLV 16	-65	86	2400	-4.44	-57.27	-0.21
104	SLU 1	0	0	1131	0	0	0
104	SLU 2	0	0	1131	0	0	0
104	SLU 3	0	0	1131	0	0	0
104	SLU 4	0	0	1131	0	0	0
104	SLU 5	0	0	1131	0	0	0
104	SLU 6	0	0	1131	0	0	0
104	SLU 7	0	0	1131	0	0	0
104	SLU 8	0	0	1131	0	0	0
104	SLU 9	0	0	1131	0	0	0
104	SLU 10	0	0	1357	0	0	0
104	SLU 11	0	0	1357	0	0	0
104	SLU 12	0	0	1357	0	0	0
104	SLU 13	0	0	1357	0	0	0
104	SLU 14	0	0	1357	0	0	0
104	SLU 15	0	0	1357	0	0	0
104	SLU 16	0	0	1357	0	0	0
104	SLU 17	0	0	1357	0	0	0
104	SLU 18	0	0	1454	0	0	0
104	SLU 19	0	0	1454	0	0	0
104	SLU 20	0	0	1454	0	0	0
104	SLU 21	0	0	1454	0	0	0
104	SLU 22	0	0	1269	0	0	0
104	SLU 23	0	0	1269	0	0	0
104	SLU 24	0	0	1269	0	0	0
104	SLU 25	0	0	1269	0	0	0
104	SLU 26	0	0	1269	0	0	0
104	SLU 27	0	0	1269	0	0	0
104	SLU 28	0	0	1269	0	0	0
104	SLU 29	0	0	1269	0	0	0
104	SLU 30	0	0	1269	0	0	0
104	SLU 31	0	0	1496	0	0	0
104	SLU 32	0	0	1496	0	0	0
104	SLU 33	0	0	1496	0	0	0
104	SLU 34	0	0	1496	0	0	0
104	SLU 35	0	0	1496	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
104	SLU 36	0	0	1496	0	0	0
104	SLU 37	0	0	1496	0	0	0
104	SLU 38	0	0	1496	0	0	0
104	SLU 39	0	0	1593	0	0	0
104	SLU 40	0	0	1593	0	0	0
104	SLU 41	0	0	1593	0	0	0
104	SLU 42	0	0	1593	0	0	0
104	SLU 43	0	0	1423	0	0	0
104	SLU 44	0	0	1423	0	0	0
104	SLU 45	0	0	1423	0	0	0
104	SLU 46	0	0	1423	0	0	0
104	SLU 47	0	0	1423	0	0	0
104	SLU 48	0	0	1423	0	0	0
104	SLU 49	0	0	1423	0	0	0
104	SLU 50	0	0	1423	0	0	0
104	SLU 51	0	0	1423	0	0	0
104	SLU 52	0	0	1650	0	0	0
104	SLU 53	0	0	1650	0	0	0
104	SLU 54	0	0	1650	0	0	0
104	SLU 55	0	0	1650	0	0	0
104	SLU 56	0	0	1650	0	0	0
104	SLU 57	0	0	1650	0	0	0
104	SLU 58	0	0	1650	0	0	0
104	SLU 59	0	0	1650	0	0	0
104	SLU 60	0	0	1746	0	0	0
104	SLU 61	0	0	1746	0	0	0
104	SLU 62	0	0	1746	0	0	0
104	SLU 63	0	0	1746	0	0	0
104	SLU 64	0	0	1561	0	0	0
104	SLU 65	0	0	1561	0	0	0
104	SLU 66	0	0	1561	0	0	0
104	SLU 67	0	0	1561	0	0	0
104	SLU 68	0	0	1561	0	0	0
104	SLU 69	0	0	1561	0	0	0
104	SLU 70	0	0	1561	0	0	0
104	SLU 71	0	0	1561	0	0	0
104	SLU 72	0	0	1561	0	0	0
104	SLU 73	0	0	1788	0	0	0
104	SLU 74	0	0	1788	0	0	0
104	SLU 75	0	0	1788	0	0	0
104	SLU 76	0	0	1788	0	0	0
104	SLU 77	0	0	1788	0	0	0
104	SLU 78	0	0	1788	0	0	0
104	SLU 79	0	0	1788	0	0	0
104	SLU 80	0	0	1788	0	0	0
104	SLU 81	0	0	1885	0	0	0
104	SLU 82	0	0	1885	0	0	0
104	SLU 83	0	0	1885	0	0	0
104	SLU 84	0	0	1885	0	0	0
104	SLE RA 1	0	0	1171	0	0	0
104	SLE RA 2	0	0	1171	0	0	0
104	SLE RA 3	0	0	1171	0	0	0
104	SLE RA 4	0	0	1171	0	0	0
104	SLE RA 5	0	0	1171	0	0	0
104	SLE RA 6	0	0	1171	0	0	0
104	SLE RA 7	0	0	1171	0	0	0
104	SLE RA 8	0	0	1171	0	0	0
104	SLE RA 9	0	0	1171	0	0	0
104	SLE RA 10	0	0	1322	0	0	0
104	SLE RA 11	0	0	1322	0	0	0
104	SLE RA 12	0	0	1322	0	0	0
104	SLE RA 13	0	0	1322	0	0	0
104	SLE RA 14	0	0	1322	0	0	0
104	SLE RA 15	0	0	1322	0	0	0
104	SLE RA 16	0	0	1322	0	0	0
104	SLE RA 17	0	0	1322	0	0	0
104	SLE RA 18	0	0	1386	0	0	0
104	SLE RA 19	0	0	1386	0	0	0
104	SLE RA 20	0	0	1386	0	0	0
104	SLE RA 21	0	0	1386	0	0	0
104	SLE FR 1	0	0	1171	0	0	0
104	SLE FR 2	0	0	1171	0	0	0
104	SLE FR 3	0	0	1171	0	0	0
104	SLE FR 4	0	0	1235	0	0	0
104	SLE FR 5	0	0	1235	0	0	0
104	SLE FR 6	0	0	1278	0	0	0
104	SLE QP 1	0	0	1171	0	0	0
104	SLE QP 2	0	0	1235	0	0	0
104	SLD 1	-4	0	1241	-0.02	7.08	0
104	SLD 2	-4	0	1241	-0.02	7.08	0
104	SLD 3	-5	-1	1233	0.02	7.36	0
104	SLD 4	-5	-1	1233	0.02	7.36	0
104	SLD 5	-1	2	1250	-0.07	1.7	0
104	SLD 6	-1	2	1250	-0.07	1.7	0
104	SLD 7	-2	-2	1222	0.07	2.63	0
104	SLD 8	-2	-2	1222	0.07	2.63	0
104	SLD 9	2	2	1249	-0.07	-2.63	0
104	SLD 10	2	2	1249	-0.07	-2.63	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
104	SLD 11	1	-2	1221	0.07	-1.7	0
104	SLD 12	1	-2	1221	0.07	-1.7	0
104	SLD 13	5	1	1238	-0.02	-7.36	0
104	SLD 14	5	1	1238	-0.02	-7.36	0
104	SLD 15	4	0	1229	0.02	-7.08	0
104	SLD 16	4	0	1229	0.02	-7.08	0
104	SLV 1	-11	1	1250	-0.06	18.02	0
104	SLV 2	-11	1	1250	-0.06	18.02	0
104	SLV 3	-12	-2	1229	0.06	18.74	0
104	SLV 4	-12	-2	1229	0.06	18.74	0
104	SLV 5	-3	5	1272	-0.2	4.31	0
104	SLV 6	-3	5	1272	-0.2	4.31	0
104	SLV 7	-4	-6	1201	0.2	6.72	0
104	SLV 8	-4	-6	1201	0.2	6.72	0
104	SLV 9	4	6	1270	-0.2	-6.72	0
104	SLV 10	4	6	1270	-0.2	-6.72	0
104	SLV 11	3	-5	1198	0.2	-4.31	0
104	SLV 12	3	-5	1198	0.2	-4.31	0
104	SLV 13	12	2	1242	-0.06	-18.74	0
104	SLV 14	12	2	1242	-0.06	-18.74	0
104	SLV 15	11	-1	1221	0.06	-18.01	0
104	SLV 16	11	-1	1221	0.06	-18.01	0
105	SLU 1	0	-123	1892	5.75	0.35	0
105	SLU 2	0	-123	1892	5.75	0.35	0
105	SLU 3	0	-123	1892	5.75	0.35	0
105	SLU 4	0	-123	1892	5.75	0.35	0
105	SLU 5	0	-123	1892	5.75	0.35	0
105	SLU 6	0	-123	1892	5.75	0.35	0
105	SLU 7	0	-123	1892	5.75	0.35	0
105	SLU 8	0	-123	1892	5.75	0.35	0
105	SLU 9	0	-123	1892	5.75	0.35	0
105	SLU 10	0	-150	2154	6.98	0.53	0
105	SLU 11	0	-150	2154	6.98	0.53	0
105	SLU 12	0	-150	2154	6.98	0.53	0
105	SLU 13	0	-150	2154	6.98	0.53	0
105	SLU 14	0	-150	2154	6.98	0.53	0
105	SLU 15	0	-150	2154	6.98	0.53	0
105	SLU 16	0	-150	2154	6.98	0.53	0
105	SLU 17	0	-150	2154	6.98	0.53	0
105	SLU 18	0	-161	2266	7.5	0.61	0
105	SLU 19	0	-161	2266	7.5	0.61	0
105	SLU 20	0	-161	2266	7.5	0.61	0
105	SLU 21	0	-161	2266	7.5	0.61	0
105	SLU 22	0	-140	2056	6.53	0.44	0
105	SLU 23	0	-140	2056	6.53	0.44	0
105	SLU 24	0	-140	2056	6.53	0.44	0
105	SLU 25	0	-140	2056	6.53	0.44	0
105	SLU 26	0	-140	2056	6.53	0.44	0
105	SLU 27	0	-140	2056	6.53	0.44	0
105	SLU 28	0	-140	2056	6.53	0.44	0
105	SLU 29	0	-140	2056	6.53	0.44	0
105	SLU 30	0	-140	2056	6.53	0.44	0
105	SLU 31	0	-167	2318	7.75	0.63	0
105	SLU 32	0	-167	2318	7.75	0.63	0
105	SLU 33	0	-167	2318	7.75	0.63	0
105	SLU 34	0	-167	2318	7.75	0.63	0
105	SLU 35	0	-167	2318	7.75	0.63	0
105	SLU 36	0	-167	2318	7.75	0.63	0
105	SLU 37	0	-167	2318	7.75	0.63	0
105	SLU 38	0	-167	2318	7.75	0.63	0
105	SLU 39	0	-178	2430	8.28	0.7	0
105	SLU 40	0	-178	2430	8.28	0.7	0
105	SLU 41	0	-178	2430	8.28	0.7	0
105	SLU 42	0	-178	2430	8.28	0.7	0
105	SLU 43	0	-154	2403	7.21	0.42	0
105	SLU 44	0	-154	2403	7.21	0.42	0
105	SLU 45	0	-154	2403	7.21	0.42	0
105	SLU 46	0	-154	2403	7.21	0.42	0
105	SLU 47	0	-154	2403	7.21	0.42	0
105	SLU 48	0	-154	2403	7.21	0.42	0
105	SLU 49	0	-154	2403	7.21	0.42	0
105	SLU 50	0	-154	2403	7.21	0.42	0
105	SLU 51	0	-154	2403	7.21	0.42	0
105	SLU 52	0	-181	2665	8.44	0.6	0
105	SLU 53	0	-181	2665	8.44	0.6	0
105	SLU 54	0	-181	2665	8.44	0.6	0
105	SLU 55	0	-181	2665	8.44	0.6	0
105	SLU 56	0	-181	2665	8.44	0.6	0
105	SLU 57	0	-181	2665	8.44	0.6	0
105	SLU 58	0	-181	2665	8.44	0.6	0
105	SLU 59	0	-181	2665	8.44	0.6	0
105	SLU 60	0	-192	2777	8.96	0.68	0
105	SLU 61	0	-192	2777	8.96	0.68	0
105	SLU 62	0	-192	2777	8.96	0.68	0
105	SLU 63	0	-192	2777	8.96	0.68	0
105	SLU 64	0	-171	2567	7.99	0.52	0
105	SLU 65	0	-171	2567	7.99	0.52	0
105	SLU 66	0	-171	2567	7.99	0.52	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
105	SLU 67	0	-171	2567	7.99	0.52	0
105	SLU 68	0	-171	2567	7.99	0.52	0
105	SLU 69	0	-171	2567	7.99	0.52	0
105	SLU 70	0	-171	2567	7.99	0.52	0
105	SLU 71	0	-171	2567	7.99	0.52	0
105	SLU 72	0	-171	2567	7.99	0.52	0
105	SLU 73	0	-198	2829	9.21	0.7	0
105	SLU 74	0	-198	2829	9.21	0.7	0
105	SLU 75	0	-198	2829	9.21	0.7	0
105	SLU 76	0	-198	2829	9.21	0.7	0
105	SLU 77	0	-198	2829	9.21	0.7	0
105	SLU 78	0	-198	2829	9.21	0.7	0
105	SLU 79	0	-198	2829	9.21	0.7	0
105	SLU 80	0	-198	2829	9.21	0.7	0
105	SLU 81	0	-209	2941	9.74	0.78	0
105	SLU 82	0	-209	2941	9.74	0.78	0
105	SLU 83	0	-209	2941	9.74	0.78	0
105	SLU 84	0	-209	2941	9.74	0.78	0
105	SLE RA 1	0	-128	1939	5.97	0.38	0
105	SLE RA 2	0	-128	1939	5.97	0.38	0
105	SLE RA 3	0	-128	1939	5.97	0.38	0
105	SLE RA 4	0	-128	1939	5.97	0.38	0
105	SLE RA 5	0	-128	1939	5.97	0.38	0
105	SLE RA 6	0	-128	1939	5.97	0.38	0
105	SLE RA 7	0	-128	1939	5.97	0.38	0
105	SLE RA 8	0	-128	1939	5.97	0.38	0
105	SLE RA 9	0	-128	1939	5.97	0.38	0
105	SLE RA 10	0	-146	2113	6.79	0.5	0
105	SLE RA 11	0	-146	2113	6.79	0.5	0
105	SLE RA 12	0	-146	2113	6.79	0.5	0
105	SLE RA 13	0	-146	2113	6.79	0.5	0
105	SLE RA 14	0	-146	2113	6.79	0.5	0
105	SLE RA 15	0	-146	2113	6.79	0.5	0
105	SLE RA 16	0	-146	2113	6.79	0.5	0
105	SLE RA 17	0	-146	2113	6.79	0.5	0
105	SLE RA 18	0	-153	2188	7.14	0.55	0
105	SLE RA 19	0	-153	2188	7.14	0.55	0
105	SLE RA 20	0	-153	2188	7.14	0.55	0
105	SLE RA 21	0	-153	2188	7.14	0.55	0
105	SLE FR 1	0	-128	1939	5.97	0.38	0
105	SLE FR 2	0	-128	1939	5.97	0.38	0
105	SLE FR 3	0	-128	1939	5.97	0.38	0
105	SLE FR 4	0	-135	2014	6.32	0.43	0
105	SLE FR 5	0	-135	2014	6.32	0.43	0
105	SLE FR 6	0	-140	2063	6.56	0.46	0
105	SLE QP 1	0	-128	1939	5.97	0.38	0
105	SLE QP 2	0	-135	2014	6.32	0.43	0
105	SLD 1	16	-112	2162	5.1	21.78	0
105	SLD 2	16	-112	2162	5.1	21.78	0
105	SLD 3	22	-230	2186	10.85	14.81	0
105	SLD 4	22	-230	2186	10.85	14.81	0
105	SLD 5	-5	50	2023	-2.77	17.4	-0.01
105	SLD 6	-5	50	2023	-2.77	17.4	-0.01
105	SLD 7	16	-342	2100	16.41	-5.83	0
105	SLD 8	16	-342	2100	16.41	-5.83	0
105	SLD 9	-16	71	1927	-3.76	6.69	0
105	SLD 10	-16	71	1927	-3.76	6.69	0
105	SLD 11	5	-321	2004	15.41	-16.55	0.01
105	SLD 12	5	-321	2004	15.41	-16.55	0.01
105	SLD 13	-22	-41	1842	1.79	-13.95	0
105	SLD 14	-22	-41	1842	1.79	-13.95	0
105	SLD 15	-15	-159	1865	7.54	-20.92	0
105	SLD 16	-15	-159	1865	7.54	-20.92	0
105	SLV 1	37	-79	2360	3.36	52.3	-0.01
105	SLV 2	37	-79	2360	3.36	52.3	-0.01
105	SLV 3	53	-358	2417	17.05	34.49	0
105	SLV 4	53	-358	2417	17.05	34.49	0
105	SLV 5	-14	306	2032	-15.33	43.01	-0.01
105	SLV 6	-14	306	2032	-15.33	43.01	-0.01
105	SLV 7	41	-626	2220	30.31	-16.37	0.01
105	SLV 8	41	-626	2220	30.31	-16.37	0.01
105	SLV 9	-40	356	1807	-17.66	17.23	-0.01
105	SLV 10	-40	356	1807	-17.66	17.23	-0.01
105	SLV 11	14	-577	1995	27.97	-42.15	0.01
105	SLV 12	14	-577	1995	27.97	-42.15	0.01
105	SLV 13	-53	88	1610	-4.41	-33.63	0
105	SLV 14	-53	88	1610	-4.41	-33.63	0
105	SLV 15	-36	-192	1667	9.28	-51.44	0.01
105	SLV 16	-36	-192	1667	9.28	-51.44	0.01
106	SLU 1	0	-9	2165	1.19	-0.28	0
106	SLU 2	0	-9	2165	1.19	-0.28	0
106	SLU 3	0	-9	2165	1.19	-0.28	0
106	SLU 4	0	-9	2165	1.19	-0.28	0
106	SLU 5	0	-9	2165	1.19	-0.28	0
106	SLU 6	0	-9	2165	1.19	-0.28	0
106	SLU 7	0	-9	2165	1.19	-0.28	0
106	SLU 8	0	-9	2165	1.19	-0.28	0
106	SLU 9	0	-9	2165	1.19	-0.28	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
106	SLU 10	0	-16	2453	1.74	-0.42	0
106	SLU 11	0	-16	2453	1.74	-0.42	0
106	SLU 12	0	-16	2453	1.74	-0.42	0
106	SLU 13	0	-16	2453	1.74	-0.42	0
106	SLU 14	0	-16	2453	1.74	-0.42	0
106	SLU 15	0	-16	2453	1.74	-0.42	0
106	SLU 16	0	-16	2453	1.74	-0.42	0
106	SLU 17	0	-16	2453	1.74	-0.42	0
106	SLU 18	0	-20	2576	1.97	-0.48	0
106	SLU 19	0	-20	2576	1.97	-0.48	0
106	SLU 20	0	-20	2576	1.97	-0.48	0
106	SLU 21	0	-20	2576	1.97	-0.48	0
106	SLU 22	0	-15	2346	1.57	-0.35	0
106	SLU 23	0	-15	2346	1.57	-0.35	0
106	SLU 24	0	-15	2346	1.57	-0.35	0
106	SLU 25	0	-15	2346	1.57	-0.35	0
106	SLU 26	0	-15	2346	1.57	-0.35	0
106	SLU 27	0	-15	2346	1.57	-0.35	0
106	SLU 28	0	-15	2346	1.57	-0.35	0
106	SLU 29	0	-15	2346	1.57	-0.35	0
106	SLU 30	0	-15	2346	1.57	-0.35	0
106	SLU 31	0	-22	2633	2.12	-0.49	0
106	SLU 32	0	-22	2633	2.12	-0.49	0
106	SLU 33	0	-22	2633	2.12	-0.49	0
106	SLU 34	0	-22	2633	2.12	-0.49	0
106	SLU 35	0	-22	2633	2.12	-0.49	0
106	SLU 36	0	-22	2633	2.12	-0.49	0
106	SLU 37	0	-22	2633	2.12	-0.49	0
106	SLU 38	0	-22	2633	2.12	-0.49	0
106	SLU 39	0	-25	2757	2.35	-0.56	0
106	SLU 40	0	-25	2757	2.35	-0.56	0
106	SLU 41	0	-25	2757	2.35	-0.56	0
106	SLU 42	0	-25	2757	2.35	-0.56	0
106	SLU 43	0	-10	2753	1.42	-0.33	0
106	SLU 44	0	-10	2753	1.42	-0.33	0
106	SLU 45	0	-10	2753	1.42	-0.33	0
106	SLU 46	0	-10	2753	1.42	-0.33	0
106	SLU 47	0	-10	2753	1.42	-0.33	0
106	SLU 48	0	-10	2753	1.42	-0.33	0
106	SLU 49	0	-10	2753	1.42	-0.33	0
106	SLU 50	0	-10	2753	1.42	-0.33	0
106	SLU 51	0	-10	2753	1.42	-0.33	0
106	SLU 52	0	-17	3041	1.97	-0.48	0
106	SLU 53	0	-17	3041	1.97	-0.48	0
106	SLU 54	0	-17	3041	1.97	-0.48	0
106	SLU 55	0	-17	3041	1.97	-0.48	0
106	SLU 56	0	-17	3041	1.97	-0.48	0
106	SLU 57	0	-17	3041	1.97	-0.48	0
106	SLU 58	0	-17	3041	1.97	-0.48	0
106	SLU 59	0	-17	3041	1.97	-0.48	0
106	SLU 60	0	-20	3164	2.2	-0.54	0
106	SLU 61	0	-20	3164	2.2	-0.54	0
106	SLU 62	0	-20	3164	2.2	-0.54	0
106	SLU 63	0	-20	3164	2.2	-0.54	0
106	SLU 64	0	-16	2934	1.8	-0.41	0
106	SLU 65	0	-16	2934	1.8	-0.41	0
106	SLU 66	0	-16	2934	1.8	-0.41	0
106	SLU 67	0	-16	2934	1.8	-0.41	0
106	SLU 68	0	-16	2934	1.8	-0.41	0
106	SLU 69	0	-16	2934	1.8	-0.41	0
106	SLU 70	0	-16	2934	1.8	-0.41	0
106	SLU 71	0	-16	2934	1.8	-0.41	0
106	SLU 72	0	-16	2934	1.8	-0.41	0
106	SLU 73	0	-23	3221	2.35	-0.55	0
106	SLU 74	0	-23	3221	2.35	-0.55	0
106	SLU 75	0	-23	3221	2.35	-0.55	0
106	SLU 76	0	-23	3221	2.35	-0.55	0
106	SLU 77	0	-23	3221	2.35	-0.55	0
106	SLU 78	0	-23	3221	2.35	-0.55	0
106	SLU 79	0	-23	3221	2.35	-0.55	0
106	SLU 80	0	-23	3221	2.35	-0.55	0
106	SLU 81	0	-26	3344	2.58	-0.61	0
106	SLU 82	0	-26	3344	2.58	-0.61	0
106	SLU 83	0	-26	3344	2.58	-0.61	0
106	SLU 84	0	-26	3344	2.58	-0.61	0
106	SLE RA 1	0	-11	2217	1.3	-0.3	0
106	SLE RA 2	0	-11	2217	1.3	-0.3	0
106	SLE RA 3	0	-11	2217	1.3	-0.3	0
106	SLE RA 4	0	-11	2217	1.3	-0.3	0
106	SLE RA 5	0	-11	2217	1.3	-0.3	0
106	SLE RA 6	0	-11	2217	1.3	-0.3	0
106	SLE RA 7	0	-11	2217	1.3	-0.3	0
106	SLE RA 8	0	-11	2217	1.3	-0.3	0
106	SLE RA 9	0	-11	2217	1.3	-0.3	0
106	SLE RA 10	0	-16	2409	1.67	-0.39	0
106	SLE RA 11	0	-16	2409	1.67	-0.39	0
106	SLE RA 12	0	-16	2409	1.67	-0.39	0
106	SLE RA 13	0	-16	2409	1.67	-0.39	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
106	SLE RA 14	0	-16	2409	1.67	-0.39	0
106	SLE RA 15	0	-16	2409	1.67	-0.39	0
106	SLE RA 16	0	-16	2409	1.67	-0.39	0
106	SLE RA 17	0	-16	2409	1.67	-0.39	0
106	SLE RA 18	0	-18	2491	1.82	-0.43	0
106	SLE RA 19	0	-18	2491	1.82	-0.43	0
106	SLE RA 20	0	-18	2491	1.82	-0.43	0
106	SLE RA 21	0	-18	2491	1.82	-0.43	0
106	SLE FR 1	0	-11	2217	1.3	-0.3	0
106	SLE FR 2	0	-11	2217	1.3	-0.3	0
106	SLE FR 3	0	-11	2217	1.3	-0.3	0
106	SLE FR 4	0	-13	2299	1.46	-0.34	0
106	SLE FR 5	0	-13	2299	1.46	-0.34	0
106	SLE FR 6	0	-14	2354	1.56	-0.37	0
106	SLE QP 1	0	-11	2217	1.3	-0.3	0
106	SLE QP 2	0	-13	2299	1.46	-0.34	0
106	SLD 1	24	73	2168	-2.92	20.51	0.01
106	SLD 2	24	73	2168	-2.92	20.51	0.01
106	SLD 3	31	-35	2105	2.64	28.01	0.02
106	SLD 4	31	-35	2105	2.64	28.01	0.02
106	SLD 5	-4	177	2356	-8.29	-5.45	-0.01
106	SLD 6	-4	177	2356	-8.29	-5.45	-0.01
106	SLD 7	20	-184	2144	10.24	19.54	0.02
106	SLD 8	20	-184	2144	10.24	19.54	0.02
106	SLD 9	-21	158	2454	-7.33	-20.21	-0.02
106	SLD 10	-21	158	2454	-7.33	-20.21	-0.02
106	SLD 11	4	-203	2242	11.2	4.78	0.01
106	SLD 12	4	-203	2242	11.2	4.78	0.01
106	SLD 13	-31	9	2494	0.27	-28.69	-0.02
106	SLD 14	-31	9	2494	0.27	-28.69	-0.02
106	SLD 15	-24	-99	2430	5.83	-21.19	-0.01
106	SLD 16	-24	-99	2430	5.83	-21.19	-0.01
106	SLV 1	57	191	1994	-8.92	49.67	0.03
106	SLV 2	57	191	1994	-8.92	49.67	0.03
106	SLV 3	75	-67	1843	4.34	68.74	0.05
106	SLV 4	75	-67	1843	4.34	68.74	0.05
106	SLV 5	-11	441	2437	-21.78	-14.26	-0.02
106	SLV 6	-11	441	2437	-21.78	-14.26	-0.02
106	SLV 7	51	-422	1933	22.44	49.31	0.04
106	SLV 8	51	-422	1933	22.44	49.31	0.04
106	SLV 9	-51	396	2665	-19.53	-49.98	-0.04
106	SLV 10	-51	396	2665	-19.53	-49.98	-0.04
106	SLV 11	11	-467	2161	24.69	13.58	0.02
106	SLV 12	11	-467	2161	24.69	13.58	0.02
106	SLV 13	-75	42	2755	-1.43	-69.42	-0.05
106	SLV 14	-75	42	2755	-1.43	-69.42	-0.05
106	SLV 15	-57	-217	2604	11.84	-50.35	-0.03
106	SLV 16	-57	-217	2604	11.84	-50.35	-0.03
107	SLU 1	0	0	1117	0	0	0
107	SLU 2	0	0	1117	0	0	0
107	SLU 3	0	0	1117	0	0	0
107	SLU 4	0	0	1117	0	0	0
107	SLU 5	0	0	1117	0	0	0
107	SLU 6	0	0	1117	0	0	0
107	SLU 7	0	0	1117	0	0	0
107	SLU 8	0	0	1117	0	0	0
107	SLU 9	0	0	1117	0	0	0
107	SLU 10	0	0	1332	0	0	0
107	SLU 11	0	0	1332	0	0	0
107	SLU 12	0	0	1332	0	0	0
107	SLU 13	0	0	1332	0	0	0
107	SLU 14	0	0	1332	0	0	0
107	SLU 15	0	0	1332	0	0	0
107	SLU 16	0	0	1332	0	0	0
107	SLU 17	0	0	1332	0	0	0
107	SLU 18	0	0	1424	0	0	0
107	SLU 19	0	0	1424	0	0	0
107	SLU 20	0	0	1424	0	0	0
107	SLU 21	0	0	1424	0	0	0
107	SLU 22	0	0	1249	0	0	0
107	SLU 23	0	0	1249	0	0	0
107	SLU 24	0	0	1249	0	0	0
107	SLU 25	0	0	1249	0	0	0
107	SLU 26	0	0	1249	0	0	0
107	SLU 27	0	0	1249	0	0	0
107	SLU 28	0	0	1249	0	0	0
107	SLU 29	0	0	1249	0	0	0
107	SLU 30	0	0	1249	0	0	0
107	SLU 31	0	0	1464	0	0	0
107	SLU 32	0	0	1464	0	0	0
107	SLU 33	0	0	1464	0	0	0
107	SLU 34	0	0	1464	0	0	0
107	SLU 35	0	0	1464	0	0	0
107	SLU 36	0	0	1464	0	0	0
107	SLU 37	0	0	1464	0	0	0
107	SLU 38	0	0	1464	0	0	0
107	SLU 39	0	0	1556	0	0	0
107	SLU 40	0	0	1556	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
107	SLU 41	0	0	1556	0	0	0
107	SLU 42	0	0	1556	0	0	0
107	SLU 43	0	0	1407	0	0	0
107	SLU 44	0	0	1407	0	0	0
107	SLU 45	0	0	1407	0	0	0
107	SLU 46	0	0	1407	0	0	0
107	SLU 47	0	0	1407	0	0	0
107	SLU 48	0	0	1407	0	0	0
107	SLU 49	0	0	1407	0	0	0
107	SLU 50	0	0	1407	0	0	0
107	SLU 51	0	0	1407	0	0	0
107	SLU 52	0	0	1622	0	0	0
107	SLU 53	0	0	1622	0	0	0
107	SLU 54	0	0	1622	0	0	0
107	SLU 55	0	0	1622	0	0	0
107	SLU 56	0	0	1622	0	0	0
107	SLU 57	0	0	1622	0	0	0
107	SLU 58	0	0	1622	0	0	0
107	SLU 59	0	0	1622	0	0	0
107	SLU 60	0	0	1714	0	0	0
107	SLU 61	0	0	1714	0	0	0
107	SLU 62	0	0	1714	0	0	0
107	SLU 63	0	0	1714	0	0	0
107	SLU 64	0	0	1539	0	0	0
107	SLU 65	0	0	1539	0	0	0
107	SLU 66	0	0	1539	0	0	0
107	SLU 67	0	0	1539	0	0	0
107	SLU 68	0	0	1539	0	0	0
107	SLU 69	0	0	1539	0	0	0
107	SLU 70	0	0	1539	0	0	0
107	SLU 71	0	0	1539	0	0	0
107	SLU 72	0	0	1539	0	0	0
107	SLU 73	0	0	1754	0	0	0
107	SLU 74	0	0	1754	0	0	0
107	SLU 75	0	0	1754	0	0	0
107	SLU 76	0	0	1754	0	0	0
107	SLU 77	0	0	1754	0	0	0
107	SLU 78	0	0	1754	0	0	0
107	SLU 79	0	0	1754	0	0	0
107	SLU 80	0	0	1754	0	0	0
107	SLU 81	0	0	1846	0	0	0
107	SLU 82	0	0	1846	0	0	0
107	SLU 83	0	0	1846	0	0	0
107	SLU 84	0	0	1846	0	0	0
107	SLE RA 1	0	0	1155	0	0	0
107	SLE RA 2	0	0	1155	0	0	0
107	SLE RA 3	0	0	1155	0	0	0
107	SLE RA 4	0	0	1155	0	0	0
107	SLE RA 5	0	0	1155	0	0	0
107	SLE RA 6	0	0	1155	0	0	0
107	SLE RA 7	0	0	1155	0	0	0
107	SLE RA 8	0	0	1155	0	0	0
107	SLE RA 9	0	0	1155	0	0	0
107	SLE RA 10	0	0	1298	0	0	0
107	SLE RA 11	0	0	1298	0	0	0
107	SLE RA 12	0	0	1298	0	0	0
107	SLE RA 13	0	0	1298	0	0	0
107	SLE RA 14	0	0	1298	0	0	0
107	SLE RA 15	0	0	1298	0	0	0
107	SLE RA 16	0	0	1298	0	0	0
107	SLE RA 17	0	0	1298	0	0	0
107	SLE RA 18	0	0	1359	0	0	0
107	SLE RA 19	0	0	1359	0	0	0
107	SLE RA 20	0	0	1359	0	0	0
107	SLE RA 21	0	0	1359	0	0	0
107	SLE FR 1	0	0	1155	0	0	0
107	SLE FR 2	0	0	1155	0	0	0
107	SLE FR 3	0	0	1155	0	0	0
107	SLE FR 4	0	0	1216	0	0	0
107	SLE FR 5	0	0	1216	0	0	0
107	SLE FR 6	0	0	1257	0	0	0
107	SLE QP 1	0	0	1155	0	0	0
107	SLE QP 2	0	0	1216	0	0	0
107	SLD 1	-4	0	1223	-0.05	7.49	0
107	SLD 2	-4	0	1223	-0.05	7.49	0
107	SLD 3	-4	-1	1213	0.05	7.21	0
107	SLD 4	-4	-1	1213	0.05	7.21	0
107	SLD 5	-1	2	1234	-0.16	2.67	0
107	SLD 6	-1	2	1234	-0.16	2.67	0
107	SLD 7	-2	-2	1200	0.16	1.75	0
107	SLD 8	-2	-2	1200	0.16	1.75	0
107	SLD 9	2	2	1233	-0.16	-1.74	0
107	SLD 10	2	2	1233	-0.16	-1.74	0
107	SLD 11	1	-2	1199	0.16	-2.66	0
107	SLD 12	1	-2	1199	0.16	-2.66	0
107	SLD 13	4	1	1220	-0.05	-7.21	0
107	SLD 14	4	1	1220	-0.05	-7.21	0
107	SLD 15	4	0	1210	0.05	-7.49	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
107	SLD 16	4	0	1210	0.05	-7.49	0
107	SLV 1	-10	1	1234	-0.13	19.08	0
107	SLV 2	-10	1	1234	-0.13	19.08	0
107	SLV 3	-11	-2	1207	0.14	18.37	0
107	SLV 4	-11	-2	1207	0.14	18.37	0
107	SLV 5	-2	5	1262	-0.45	6.81	0
107	SLV 6	-2	5	1262	-0.45	6.81	0
107	SLV 7	-4	-6	1173	0.45	4.43	0
107	SLV 8	-4	-6	1173	0.45	4.43	0
107	SLV 9	4	6	1260	-0.45	-4.43	0
107	SLV 10	4	6	1260	-0.45	-4.43	0
107	SLV 11	2	-5	1170	0.45	-6.81	0
107	SLV 12	2	-5	1170	0.45	-6.81	0
107	SLV 13	11	2	1226	-0.14	-18.37	0
107	SLV 14	11	2	1226	-0.14	-18.37	0
107	SLV 15	10	-1	1199	0.13	-19.08	0
107	SLV 16	10	-1	1199	0.13	-19.08	0
108	SLU 1	0	-132	1874	6.34	0.26	0
108	SLU 2	0	-132	1874	6.34	0.26	0
108	SLU 3	0	-132	1874	6.34	0.26	0
108	SLU 4	0	-132	1874	6.34	0.26	0
108	SLU 5	0	-132	1874	6.34	0.26	0
108	SLU 6	0	-132	1874	6.34	0.26	0
108	SLU 7	0	-132	1874	6.34	0.26	0
108	SLU 8	0	-132	1874	6.34	0.26	0
108	SLU 9	0	-132	1874	6.34	0.26	0
108	SLU 10	0	-153	2130	7.39	0.4	0
108	SLU 11	0	-153	2130	7.39	0.4	0
108	SLU 12	0	-153	2130	7.39	0.4	0
108	SLU 13	0	-153	2130	7.39	0.4	0
108	SLU 14	0	-153	2130	7.39	0.4	0
108	SLU 15	0	-153	2130	7.39	0.4	0
108	SLU 16	0	-153	2130	7.39	0.4	0
108	SLU 17	0	-153	2130	7.39	0.4	0
108	SLU 18	0	-162	2240	7.84	0.45	0
108	SLU 19	0	-162	2240	7.84	0.45	0
108	SLU 20	0	-162	2240	7.84	0.45	0
108	SLU 21	0	-162	2240	7.84	0.45	0
108	SLU 22	0	-146	2034	7.05	0.33	0
108	SLU 23	0	-146	2034	7.05	0.33	0
108	SLU 24	0	-146	2034	7.05	0.33	0
108	SLU 25	0	-146	2034	7.05	0.33	0
108	SLU 26	0	-146	2034	7.05	0.33	0
108	SLU 27	0	-146	2034	7.05	0.33	0
108	SLU 28	0	-146	2034	7.05	0.33	0
108	SLU 29	0	-146	2034	7.05	0.33	0
108	SLU 30	0	-146	2034	7.05	0.33	0
108	SLU 31	0	-168	2290	8.09	0.46	0
108	SLU 32	0	-168	2290	8.09	0.46	0
108	SLU 33	0	-168	2290	8.09	0.46	0
108	SLU 34	0	-168	2290	8.09	0.46	0
108	SLU 35	0	-168	2290	8.09	0.46	0
108	SLU 36	0	-168	2290	8.09	0.46	0
108	SLU 37	0	-168	2290	8.09	0.46	0
108	SLU 38	0	-168	2290	8.09	0.46	0
108	SLU 39	0	-177	2400	8.54	0.52	0
108	SLU 40	0	-177	2400	8.54	0.52	0
108	SLU 41	0	-177	2400	8.54	0.52	0
108	SLU 42	0	-177	2400	8.54	0.52	0
108	SLU 43	0	-166	2381	8	0.32	0
108	SLU 44	0	-166	2381	8	0.32	0
108	SLU 45	0	-166	2381	8	0.32	0
108	SLU 46	0	-166	2381	8	0.32	0
108	SLU 47	0	-166	2381	8	0.32	0
108	SLU 48	0	-166	2381	8	0.32	0
108	SLU 49	0	-166	2381	8	0.32	0
108	SLU 50	0	-166	2381	8	0.32	0
108	SLU 51	0	-166	2381	8	0.32	0
108	SLU 52	0	-188	2637	9.05	0.45	0
108	SLU 53	0	-188	2637	9.05	0.45	0
108	SLU 54	0	-188	2637	9.05	0.45	0
108	SLU 55	0	-188	2637	9.05	0.45	0
108	SLU 56	0	-188	2637	9.05	0.45	0
108	SLU 57	0	-188	2637	9.05	0.45	0
108	SLU 58	0	-188	2637	9.05	0.45	0
108	SLU 59	0	-188	2637	9.05	0.45	0
108	SLU 60	0	-197	2747	9.5	0.51	0
108	SLU 61	0	-197	2747	9.5	0.51	0
108	SLU 62	0	-197	2747	9.5	0.51	0
108	SLU 63	0	-197	2747	9.5	0.51	0
108	SLU 64	0	-181	2541	8.71	0.39	0
108	SLU 65	0	-181	2541	8.71	0.39	0
108	SLU 66	0	-181	2541	8.71	0.39	0
108	SLU 67	0	-181	2541	8.71	0.39	0
108	SLU 68	0	-181	2541	8.71	0.39	0
108	SLU 69	0	-181	2541	8.71	0.39	0
108	SLU 70	0	-181	2541	8.71	0.39	0
108	SLU 71	0	-181	2541	8.71	0.39	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
108	SLU 72	0	-181	2541	8.71	0.39	0
108	SLU 73	0	-202	2797	9.75	0.52	0
108	SLU 74	0	-202	2797	9.75	0.52	0
108	SLU 75	0	-202	2797	9.75	0.52	0
108	SLU 76	0	-202	2797	9.75	0.52	0
108	SLU 77	0	-202	2797	9.75	0.52	0
108	SLU 78	0	-202	2797	9.75	0.52	0
108	SLU 79	0	-202	2797	9.75	0.52	0
108	SLU 80	0	-202	2797	9.75	0.52	0
108	SLU 81	0	-212	2907	10.2	0.58	0
108	SLU 82	0	-212	2907	10.2	0.58	0
108	SLU 83	0	-212	2907	10.2	0.58	0
108	SLU 84	0	-212	2907	10.2	0.58	0
108	SLE RA 1	0	-136	1920	6.54	0.28	0
108	SLE RA 2	0	-136	1920	6.54	0.28	0
108	SLE RA 3	0	-136	1920	6.54	0.28	0
108	SLE RA 4	0	-136	1920	6.54	0.28	0
108	SLE RA 5	0	-136	1920	6.54	0.28	0
108	SLE RA 6	0	-136	1920	6.54	0.28	0
108	SLE RA 7	0	-136	1920	6.54	0.28	0
108	SLE RA 8	0	-136	1920	6.54	0.28	0
108	SLE RA 9	0	-136	1920	6.54	0.28	0
108	SLE RA 10	0	-150	2090	7.24	0.37	0
108	SLE RA 11	0	-150	2090	7.24	0.37	0
108	SLE RA 12	0	-150	2090	7.24	0.37	0
108	SLE RA 13	0	-150	2090	7.24	0.37	0
108	SLE RA 14	0	-150	2090	7.24	0.37	0
108	SLE RA 15	0	-150	2090	7.24	0.37	0
108	SLE RA 16	0	-150	2090	7.24	0.37	0
108	SLE RA 17	0	-150	2090	7.24	0.37	0
108	SLE RA 18	0	-156	2163	7.54	0.41	0
108	SLE RA 19	0	-156	2163	7.54	0.41	0
108	SLE RA 20	0	-156	2163	7.54	0.41	0
108	SLE RA 21	0	-156	2163	7.54	0.41	0
108	SLE FR 1	0	-136	1920	6.54	0.28	0
108	SLE FR 2	0	-136	1920	6.54	0.28	0
108	SLE FR 3	0	-136	1920	6.54	0.28	0
108	SLE FR 4	0	-142	1993	6.84	0.32	0
108	SLE FR 5	0	-142	1993	6.84	0.32	0
108	SLE FR 6	0	-146	2042	7.04	0.35	0
108	SLE QP 1	0	-136	1920	6.54	0.28	0
108	SLE QP 2	0	-142	1993	6.84	0.32	0
108	SLD 1	26	-119	2132	5.62	24.09	0
108	SLD 2	26	-119	2132	5.62	24.09	0
108	SLD 3	19	-234	2162	11.25	16.49	0
108	SLD 4	19	-234	2162	11.25	16.49	0
108	SLD 5	18	41	1989	-2.06	18.98	0
108	SLD 6	18	41	1989	-2.06	18.98	0
108	SLD 7	-5	-345	2089	16.7	-6.36	0
108	SLD 8	-5	-345	2089	16.7	-6.36	0
108	SLD 9	5	61	1897	-3.02	7	0
108	SLD 10	5	61	1897	-3.02	7	0
108	SLD 11	-18	-325	1997	15.74	-18.34	0
108	SLD 12	-18	-325	1997	15.74	-18.34	0
108	SLD 13	-18	-50	1824	2.43	-15.84	0
108	SLD 14	-18	-50	1824	2.43	-15.84	0
108	SLD 15	-25	-166	1854	8.06	-23.45	0
108	SLD 16	-25	-166	1854	8.06	-23.45	0
108	SLV 1	61	-85	2316	3.91	58.12	0
108	SLV 2	61	-85	2316	3.91	58.12	0
108	SLV 3	44	-360	2389	17.25	38.78	0.01
108	SLV 4	44	-360	2389	17.25	38.78	0.01
108	SLV 5	45	292	1979	-14.28	47	-0.01
108	SLV 6	45	292	1979	-14.28	47	-0.01
108	SLV 7	-14	-624	2222	30.21	-17.48	0.01
108	SLV 8	-14	-624	2222	30.21	-17.48	0.01
108	SLV 9	14	340	1763	-16.52	18.13	-0.01
108	SLV 10	14	340	1763	-16.52	18.13	-0.01
108	SLV 11	-45	-576	2007	27.96	-46.36	0.01
108	SLV 12	-45	-576	2007	27.96	-46.36	0.01
108	SLV 13	-44	76	1597	-3.57	-38.13	-0.01
108	SLV 14	-44	76	1597	-3.57	-38.13	-0.01
108	SLV 15	-61	-199	1670	9.78	-57.48	0
108	SLV 16	-61	-199	1670	9.78	-57.48	0
109	SLU 1	0	-102	2180	4.51	-0.23	0
109	SLU 2	0	-102	2180	4.51	-0.23	0
109	SLU 3	0	-102	2180	4.51	-0.23	0
109	SLU 4	0	-102	2180	4.51	-0.23	0
109	SLU 5	0	-102	2180	4.51	-0.23	0
109	SLU 6	0	-102	2180	4.51	-0.23	0
109	SLU 7	0	-102	2180	4.51	-0.23	0
109	SLU 8	0	-102	2180	4.51	-0.23	0
109	SLU 9	0	-102	2180	4.51	-0.23	0
109	SLU 10	0	-120	2480	5.37	-0.35	0
109	SLU 11	0	-120	2480	5.37	-0.35	0
109	SLU 12	0	-120	2480	5.37	-0.35	0
109	SLU 13	0	-120	2480	5.37	-0.35	0
109	SLU 14	0	-120	2480	5.37	-0.35	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
109	SLU 15	0	-120	2480	5.37	-0.35	0
109	SLU 16	0	-120	2480	5.37	-0.35	0
109	SLU 17	0	-120	2480	5.37	-0.35	0
109	SLU 18	0	-128	2608	5.74	-0.39	0
109	SLU 19	0	-128	2608	5.74	-0.39	0
109	SLU 20	0	-128	2608	5.74	-0.39	0
109	SLU 21	0	-128	2608	5.74	-0.39	0
109	SLU 22	0	-115	2366	5.12	-0.29	0
109	SLU 23	0	-115	2366	5.12	-0.29	0
109	SLU 24	0	-115	2366	5.12	-0.29	0
109	SLU 25	0	-115	2366	5.12	-0.29	0
109	SLU 26	0	-115	2366	5.12	-0.29	0
109	SLU 27	0	-115	2366	5.12	-0.29	0
109	SLU 28	0	-115	2366	5.12	-0.29	0
109	SLU 29	0	-115	2366	5.12	-0.29	0
109	SLU 30	0	-115	2366	5.12	-0.29	0
109	SLU 31	0	-133	2666	5.98	-0.4	0
109	SLU 32	0	-133	2666	5.98	-0.4	0
109	SLU 33	0	-133	2666	5.98	-0.4	0
109	SLU 34	0	-133	2666	5.98	-0.4	0
109	SLU 35	0	-133	2666	5.98	-0.4	0
109	SLU 36	0	-133	2666	5.98	-0.4	0
109	SLU 37	0	-133	2666	5.98	-0.4	0
109	SLU 38	0	-133	2666	5.98	-0.4	0
109	SLU 39	0	-141	2795	6.34	-0.45	0
109	SLU 40	0	-141	2795	6.34	-0.45	0
109	SLU 41	0	-141	2795	6.34	-0.45	0
109	SLU 42	0	-141	2795	6.34	-0.45	0
109	SLU 43	0	-128	2769	5.65	-0.29	0
109	SLU 44	0	-128	2769	5.65	-0.29	0
109	SLU 45	0	-128	2769	5.65	-0.29	0
109	SLU 46	0	-128	2769	5.65	-0.29	0
109	SLU 47	0	-128	2769	5.65	-0.29	0
109	SLU 48	0	-128	2769	5.65	-0.29	0
109	SLU 49	0	-128	2769	5.65	-0.29	0
109	SLU 50	0	-128	2769	5.65	-0.29	0
109	SLU 51	0	-128	2769	5.65	-0.29	0
109	SLU 52	0	-146	3070	6.51	-0.4	0
109	SLU 53	0	-146	3070	6.51	-0.4	0
109	SLU 54	0	-146	3070	6.51	-0.4	0
109	SLU 55	0	-146	3070	6.51	-0.4	0
109	SLU 56	0	-146	3070	6.51	-0.4	0
109	SLU 57	0	-146	3070	6.51	-0.4	0
109	SLU 58	0	-146	3070	6.51	-0.4	0
109	SLU 59	0	-146	3070	6.51	-0.4	0
109	SLU 60	0	-154	3198	6.88	-0.44	0
109	SLU 61	0	-154	3198	6.88	-0.44	0
109	SLU 62	0	-154	3198	6.88	-0.44	0
109	SLU 63	0	-154	3198	6.88	-0.44	0
109	SLU 64	0	-141	2956	6.26	-0.34	0
109	SLU 65	0	-141	2956	6.26	-0.34	0
109	SLU 66	0	-141	2956	6.26	-0.34	0
109	SLU 67	0	-141	2956	6.26	-0.34	0
109	SLU 68	0	-141	2956	6.26	-0.34	0
109	SLU 69	0	-141	2956	6.26	-0.34	0
109	SLU 70	0	-141	2956	6.26	-0.34	0
109	SLU 71	0	-141	2956	6.26	-0.34	0
109	SLU 72	0	-141	2956	6.26	-0.34	0
109	SLU 73	0	-159	3256	7.12	-0.45	0
109	SLU 74	0	-159	3256	7.12	-0.45	0
109	SLU 75	0	-159	3256	7.12	-0.45	0
109	SLU 76	0	-159	3256	7.12	-0.45	0
109	SLU 77	0	-159	3256	7.12	-0.45	0
109	SLU 78	0	-159	3256	7.12	-0.45	0
109	SLU 79	0	-159	3256	7.12	-0.45	0
109	SLU 80	0	-159	3256	7.12	-0.45	0
109	SLU 81	0	-167	3385	7.49	-0.5	0
109	SLU 82	0	-167	3385	7.49	-0.5	0
109	SLU 83	0	-167	3385	7.49	-0.5	0
109	SLU 84	0	-167	3385	7.49	-0.5	0
109	SLE RA 1	0	-106	2233	4.68	-0.25	0
109	SLE RA 2	0	-106	2233	4.68	-0.25	0
109	SLE RA 3	0	-106	2233	4.68	-0.25	0
109	SLE RA 4	0	-106	2233	4.68	-0.25	0
109	SLE RA 5	0	-106	2233	4.68	-0.25	0
109	SLE RA 6	0	-106	2233	4.68	-0.25	0
109	SLE RA 7	0	-106	2233	4.68	-0.25	0
109	SLE RA 8	0	-106	2233	4.68	-0.25	0
109	SLE RA 9	0	-106	2233	4.68	-0.25	0
109	SLE RA 10	0	-118	2433	5.26	-0.33	0
109	SLE RA 11	0	-118	2433	5.26	-0.33	0
109	SLE RA 12	0	-118	2433	5.26	-0.33	0
109	SLE RA 13	0	-118	2433	5.26	-0.33	0
109	SLE RA 14	0	-118	2433	5.26	-0.33	0
109	SLE RA 15	0	-118	2433	5.26	-0.33	0
109	SLE RA 16	0	-118	2433	5.26	-0.33	0
109	SLE RA 17	0	-118	2433	5.26	-0.33	0
109	SLE RA 18	0	-123	2519	5.5	-0.36	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
109	SLE RA 19	0	-123	2519	5.5	-0.36	0
109	SLE RA 20	0	-123	2519	5.5	-0.36	0
109	SLE RA 21	0	-123	2519	5.5	-0.36	0
109	SLE FR 1	0	-106	2233	4.68	-0.25	0
109	SLE FR 2	0	-106	2233	4.68	-0.25	0
109	SLE FR 3	0	-106	2233	4.68	-0.25	0
109	SLE FR 4	0	-111	2319	4.93	-0.28	0
109	SLE FR 5	0	-111	2319	4.93	-0.28	0
109	SLE FR 6	0	-114	2376	5.09	-0.3	0
109	SLE QP 1	0	-106	2233	4.68	-0.25	0
109	SLE QP 2	0	-111	2319	4.93	-0.28	0
109	SLD 1	22	-10	2137	0.07	20.46	0.01
109	SLD 2	22	-10	2137	0.07	20.46	0.01
109	SLD 3	31	-130	2156	5.97	28.77	0.01
109	SLD 4	31	-130	2156	5.97	28.77	0.01
109	SLD 5	-6	102	2237	-5.48	-6.66	0
109	SLD 6	-6	102	2237	-5.48	-6.66	0
109	SLD 7	22	-300	2297	14.19	21.03	0.01
109	SLD 8	22	-300	2297	14.19	21.03	0.01
109	SLD 9	-22	78	2340	-4.33	-21.6	-0.01
109	SLD 10	-22	78	2340	-4.33	-21.6	-0.01
109	SLD 11	6	-324	2401	15.33	6.1	0
109	SLD 12	6	-324	2401	15.33	6.1	0
109	SLD 13	-31	-92	2482	3.89	-29.33	-0.01
109	SLD 14	-31	-92	2482	3.89	-29.33	-0.01
109	SLD 15	-23	-212	2500	9.79	-21.03	-0.01
109	SLD 16	-23	-212	2500	9.79	-21.03	-0.01
109	SLV 1	54	129	1894	-6.6	49.62	0.02
109	SLV 2	54	129	1894	-6.6	49.62	0.02
109	SLV 3	75	-158	1938	7.48	70.83	0.02
109	SLV 4	75	-158	1938	7.48	70.83	0.02
109	SLV 5	-17	397	2126	-19.88	-17.48	0
109	SLV 6	-17	397	2126	-19.88	-17.48	0
109	SLV 7	55	-561	2270	27.04	53.22	0.01
109	SLV 8	55	-561	2270	27.04	53.22	0.01
109	SLV 9	-56	339	2367	-17.19	-53.79	-0.01
109	SLV 10	-56	339	2367	-17.19	-53.79	-0.01
109	SLV 11	17	-619	2512	29.74	16.91	0
109	SLV 12	17	-619	2512	29.74	16.91	0
109	SLV 13	-76	-64	2700	2.38	-71.4	-0.02
109	SLV 14	-76	-64	2700	2.38	-71.4	-0.02
109	SLV 15	-54	-351	2743	16.46	-50.19	-0.02
109	SLV 16	-54	-351	2743	16.46	-50.19	-0.02
110	SLU 1	0	0	1104	0	0	0
110	SLU 2	0	0	1104	0	0	0
110	SLU 3	0	0	1104	0	0	0
110	SLU 4	0	0	1104	0	0	0
110	SLU 5	0	0	1104	0	0	0
110	SLU 6	0	0	1104	0	0	0
110	SLU 7	0	0	1104	0	0	0
110	SLU 8	0	0	1104	0	0	0
110	SLU 9	0	0	1104	0	0	0
110	SLU 10	0	0	1311	0	0	0
110	SLU 11	0	0	1311	0	0	0
110	SLU 12	0	0	1311	0	0	0
110	SLU 13	0	0	1311	0	0	0
110	SLU 14	0	0	1311	0	0	0
110	SLU 15	0	0	1311	0	0	0
110	SLU 16	0	0	1311	0	0	0
110	SLU 17	0	0	1311	0	0	0
110	SLU 18	0	0	1400	0	0	0
110	SLU 19	0	0	1400	0	0	0
110	SLU 20	0	0	1400	0	0	0
110	SLU 21	0	0	1400	0	0	0
110	SLU 22	0	0	1232	0	0	0
110	SLU 23	0	0	1232	0	0	0
110	SLU 24	0	0	1232	0	0	0
110	SLU 25	0	0	1232	0	0	0
110	SLU 26	0	0	1232	0	0	0
110	SLU 27	0	0	1232	0	0	0
110	SLU 28	0	0	1232	0	0	0
110	SLU 29	0	0	1232	0	0	0
110	SLU 30	0	0	1232	0	0	0
110	SLU 31	0	0	1439	0	0	0
110	SLU 32	0	0	1439	0	0	0
110	SLU 33	0	0	1439	0	0	0
110	SLU 34	0	0	1439	0	0	0
110	SLU 35	0	0	1439	0	0	0
110	SLU 36	0	0	1439	0	0	0
110	SLU 37	0	0	1439	0	0	0
110	SLU 38	0	0	1439	0	0	0
110	SLU 39	0	0	1528	0	0	0
110	SLU 40	0	0	1528	0	0	0
110	SLU 41	0	0	1528	0	0	0
110	SLU 42	0	0	1528	0	0	0
110	SLU 43	0	0	1391	0	0	0
110	SLU 44	0	0	1391	0	0	0
110	SLU 45	0	0	1391	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
110	SLU 46	0	0	1391	0	0	0
110	SLU 47	0	0	1391	0	0	0
110	SLU 48	0	0	1391	0	0	0
110	SLU 49	0	0	1391	0	0	0
110	SLU 50	0	0	1391	0	0	0
110	SLU 51	0	0	1391	0	0	0
110	SLU 52	0	0	1598	0	0	0
110	SLU 53	0	0	1598	0	0	0
110	SLU 54	0	0	1598	0	0	0
110	SLU 55	0	0	1598	0	0	0
110	SLU 56	0	0	1598	0	0	0
110	SLU 57	0	0	1598	0	0	0
110	SLU 58	0	0	1598	0	0	0
110	SLU 59	0	0	1598	0	0	0
110	SLU 60	0	0	1687	0	0	0
110	SLU 61	0	0	1687	0	0	0
110	SLU 62	0	0	1687	0	0	0
110	SLU 63	0	0	1687	0	0	0
110	SLU 64	0	0	1519	0	0	0
110	SLU 65	0	0	1519	0	0	0
110	SLU 66	0	0	1519	0	0	0
110	SLU 67	0	0	1519	0	0	0
110	SLU 68	0	0	1519	0	0	0
110	SLU 69	0	0	1519	0	0	0
110	SLU 70	0	0	1519	0	0	0
110	SLU 71	0	0	1519	0	0	0
110	SLU 72	0	0	1519	0	0	0
110	SLU 73	0	0	1726	0	0	0
110	SLU 74	0	0	1726	0	0	0
110	SLU 75	0	0	1726	0	0	0
110	SLU 76	0	0	1726	0	0	0
110	SLU 77	0	0	1726	0	0	0
110	SLU 78	0	0	1726	0	0	0
110	SLU 79	0	0	1726	0	0	0
110	SLU 80	0	0	1726	0	0	0
110	SLU 81	0	0	1815	0	0	0
110	SLU 82	0	0	1815	0	0	0
110	SLU 83	0	0	1815	0	0	0
110	SLU 84	0	0	1815	0	0	0
110	SLE RA 1	0	0	1141	0	0	0
110	SLE RA 2	0	0	1141	0	0	0
110	SLE RA 3	0	0	1141	0	0	0
110	SLE RA 4	0	0	1141	0	0	0
110	SLE RA 5	0	0	1141	0	0	0
110	SLE RA 6	0	0	1141	0	0	0
110	SLE RA 7	0	0	1141	0	0	0
110	SLE RA 8	0	0	1141	0	0	0
110	SLE RA 9	0	0	1141	0	0	0
110	SLE RA 10	0	0	1279	0	0	0
110	SLE RA 11	0	0	1279	0	0	0
110	SLE RA 12	0	0	1279	0	0	0
110	SLE RA 13	0	0	1279	0	0	0
110	SLE RA 14	0	0	1279	0	0	0
110	SLE RA 15	0	0	1279	0	0	0
110	SLE RA 16	0	0	1279	0	0	0
110	SLE RA 17	0	0	1279	0	0	0
110	SLE RA 18	0	0	1338	0	0	0
110	SLE RA 19	0	0	1338	0	0	0
110	SLE RA 20	0	0	1338	0	0	0
110	SLE RA 21	0	0	1338	0	0	0
110	SLE FR 1	0	0	1141	0	0	0
110	SLE FR 2	0	0	1141	0	0	0
110	SLE FR 3	0	0	1141	0	0	0
110	SLE FR 4	0	0	1200	0	0	0
110	SLE FR 5	0	0	1200	0	0	0
110	SLE FR 6	0	0	1239	0	0	0
110	SLE QP 1	0	0	1141	0	0	0
110	SLE QP 2	0	0	1200	0	0	0
110	SLD 1	-4	0	1211	-0.02	6.97	0
110	SLD 2	-4	0	1211	-0.02	6.97	0
110	SLD 3	-4	-1	1192	0.02	6.72	0
110	SLD 4	-4	-1	1192	0.02	6.72	0
110	SLD 5	-1	2	1232	-0.07	2.47	0
110	SLD 6	-1	2	1232	-0.07	2.47	0
110	SLD 7	-1	-2	1168	0.06	1.64	0
110	SLD 8	-1	-2	1168	0.06	1.64	0
110	SLD 9	1	2	1231	-0.07	-1.63	0
110	SLD 10	1	2	1231	-0.07	-1.63	0
110	SLD 11	1	-2	1167	0.06	-2.47	0
110	SLD 12	1	-2	1167	0.06	-2.47	0
110	SLD 13	4	1	1208	-0.02	-6.72	0
110	SLD 14	4	1	1208	-0.02	-6.72	0
110	SLD 15	4	0	1189	0.02	-6.97	0
110	SLD 16	4	0	1189	0.02	-6.97	0
110	SLV 1	-10	1	1229	-0.05	17.78	0
110	SLV 2	-10	1	1229	-0.05	17.78	0
110	SLV 3	-10	-3	1177	0.06	17.13	0
110	SLV 4	-10	-3	1177	0.06	17.13	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
110	SLV 5	-2	5	1288	-0.18	6.33	0
110	SLV 6	-2	5	1288	-0.18	6.33	0
110	SLV 7	-4	-6	1113	0.18	4.15	0
110	SLV 8	-4	-6	1113	0.18	4.15	0
110	SLV 9	4	6	1286	-0.18	-4.15	0
110	SLV 10	4	6	1286	-0.18	-4.15	0
110	SLV 11	2	-5	1111	0.18	-6.32	0
110	SLV 12	2	-5	1111	0.18	-6.32	0
110	SLV 13	10	3	1223	-0.06	-17.13	0
110	SLV 14	10	3	1223	-0.06	-17.13	0
110	SLV 15	10	-1	1170	0.05	-17.78	0
110	SLV 16	10	-1	1170	0.05	-17.78	0
111	SLU 1	0	-143	1868	6.92	0.23	0
111	SLU 2	0	-143	1868	6.92	0.23	0
111	SLU 3	0	-143	1868	6.92	0.23	0
111	SLU 4	0	-143	1868	6.92	0.23	0
111	SLU 5	0	-143	1868	6.92	0.23	0
111	SLU 6	0	-143	1868	6.92	0.23	0
111	SLU 7	0	-143	1868	6.92	0.23	0
111	SLU 8	0	-143	1868	6.92	0.23	0
111	SLU 9	0	-143	1868	6.92	0.23	0
111	SLU 10	0	-158	2126	7.7	0.33	0
111	SLU 11	0	-158	2126	7.7	0.33	0
111	SLU 12	0	-158	2126	7.7	0.33	0
111	SLU 13	0	-158	2126	7.7	0.33	0
111	SLU 14	0	-158	2126	7.7	0.33	0
111	SLU 15	0	-158	2126	7.7	0.33	0
111	SLU 16	0	-158	2126	7.7	0.33	0
111	SLU 17	0	-158	2126	7.7	0.33	0
111	SLU 18	0	-165	2237	8.03	0.37	0
111	SLU 19	0	-165	2237	8.03	0.37	0
111	SLU 20	0	-165	2237	8.03	0.37	0
111	SLU 21	0	-165	2237	8.03	0.37	0
111	SLU 22	0	-155	2029	7.5	0.28	0
111	SLU 23	0	-155	2029	7.5	0.28	0
111	SLU 24	0	-155	2029	7.5	0.28	0
111	SLU 25	0	-155	2029	7.5	0.28	0
111	SLU 26	0	-155	2029	7.5	0.28	0
111	SLU 27	0	-155	2029	7.5	0.28	0
111	SLU 28	0	-155	2029	7.5	0.28	0
111	SLU 29	0	-155	2029	7.5	0.28	0
111	SLU 30	0	-155	2029	7.5	0.28	0
111	SLU 31	0	-170	2286	8.28	0.38	0
111	SLU 32	0	-170	2286	8.28	0.38	0
111	SLU 33	0	-170	2286	8.28	0.38	0
111	SLU 34	0	-170	2286	8.28	0.38	0
111	SLU 35	0	-170	2286	8.28	0.38	0
111	SLU 36	0	-170	2286	8.28	0.38	0
111	SLU 37	0	-170	2286	8.28	0.38	0
111	SLU 38	0	-170	2286	8.28	0.38	0
111	SLU 39	0	-177	2397	8.61	0.43	0
111	SLU 40	0	-177	2397	8.61	0.43	0
111	SLU 41	0	-177	2397	8.61	0.43	0
111	SLU 42	0	-177	2397	8.61	0.43	0
111	SLU 43	0	-181	2374	8.8	0.27	0
111	SLU 44	0	-181	2374	8.8	0.27	0
111	SLU 45	0	-181	2374	8.8	0.27	0
111	SLU 46	0	-181	2374	8.8	0.27	0
111	SLU 47	0	-181	2374	8.8	0.27	0
111	SLU 48	0	-181	2374	8.8	0.27	0
111	SLU 49	0	-181	2374	8.8	0.27	0
111	SLU 50	0	-181	2374	8.8	0.27	0
111	SLU 51	0	-181	2374	8.8	0.27	0
111	SLU 52	0	-197	2632	9.58	0.38	0
111	SLU 53	0	-197	2632	9.58	0.38	0
111	SLU 54	0	-197	2632	9.58	0.38	0
111	SLU 55	0	-197	2632	9.58	0.38	0
111	SLU 56	0	-197	2632	9.58	0.38	0
111	SLU 57	0	-197	2632	9.58	0.38	0
111	SLU 58	0	-197	2632	9.58	0.38	0
111	SLU 59	0	-197	2632	9.58	0.38	0
111	SLU 60	0	-204	2743	9.91	0.42	0
111	SLU 61	0	-204	2743	9.91	0.42	0
111	SLU 62	0	-204	2743	9.91	0.42	0
111	SLU 63	0	-204	2743	9.91	0.42	0
111	SLU 64	0	-193	2534	9.38	0.33	0
111	SLU 65	0	-193	2534	9.38	0.33	0
111	SLU 66	0	-193	2534	9.38	0.33	0
111	SLU 67	0	-193	2534	9.38	0.33	0
111	SLU 68	0	-193	2534	9.38	0.33	0
111	SLU 69	0	-193	2534	9.38	0.33	0
111	SLU 70	0	-193	2534	9.38	0.33	0
111	SLU 71	0	-193	2534	9.38	0.33	0
111	SLU 72	0	-193	2534	9.38	0.33	0
111	SLU 73	0	-209	2792	10.16	0.43	0
111	SLU 74	0	-209	2792	10.16	0.43	0
111	SLU 75	0	-209	2792	10.16	0.43	0
111	SLU 76	0	-209	2792	10.16	0.43	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
111	SLU 77	0	-209	2792	10.16	0.43	0
111	SLU 78	0	-209	2792	10.16	0.43	0
111	SLU 79	0	-209	2792	10.16	0.43	0
111	SLU 80	0	-209	2792	10.16	0.43	0
111	SLU 81	0	-216	2903	10.49	0.48	0
111	SLU 82	0	-216	2903	10.49	0.48	0
111	SLU 83	0	-216	2903	10.49	0.48	0
111	SLU 84	0	-216	2903	10.49	0.48	0
111	SLE RA 1	0	-146	1914	7.09	0.24	0
111	SLE RA 2	0	-146	1914	7.09	0.24	0
111	SLE RA 3	0	-146	1914	7.09	0.24	0
111	SLE RA 4	0	-146	1914	7.09	0.24	0
111	SLE RA 5	0	-146	1914	7.09	0.24	0
111	SLE RA 6	0	-146	1914	7.09	0.24	0
111	SLE RA 7	0	-146	1914	7.09	0.24	0
111	SLE RA 8	0	-146	1914	7.09	0.24	0
111	SLE RA 9	0	-146	1914	7.09	0.24	0
111	SLE RA 10	0	-156	2086	7.61	0.31	0
111	SLE RA 11	0	-156	2086	7.61	0.31	0
111	SLE RA 12	0	-156	2086	7.61	0.31	0
111	SLE RA 13	0	-156	2086	7.61	0.31	0
111	SLE RA 14	0	-156	2086	7.61	0.31	0
111	SLE RA 15	0	-156	2086	7.61	0.31	0
111	SLE RA 16	0	-156	2086	7.61	0.31	0
111	SLE RA 17	0	-156	2086	7.61	0.31	0
111	SLE RA 18	0	-161	2160	7.83	0.34	0
111	SLE RA 19	0	-161	2160	7.83	0.34	0
111	SLE RA 20	0	-161	2160	7.83	0.34	0
111	SLE RA 21	0	-161	2160	7.83	0.34	0
111	SLE FR 1	0	-146	1914	7.09	0.24	0
111	SLE FR 2	0	-146	1914	7.09	0.24	0
111	SLE FR 3	0	-146	1914	7.09	0.24	0
111	SLE FR 4	0	-151	1988	7.31	0.27	0
111	SLE FR 5	0	-151	1988	7.31	0.27	0
111	SLE FR 6	0	-154	2037	7.46	0.29	0
111	SLE QP 1	0	-146	1914	7.09	0.24	0
111	SLE QP 2	0	-151	1988	7.31	0.27	0
111	SLD 1	26	-128	2122	6.14	24.1	0.01
111	SLD 2	26	-128	2122	6.14	24.1	0.01
111	SLD 3	18	-242	2161	11.77	16	0.01
111	SLD 4	18	-242	2161	11.77	16	0.01
111	SLD 5	20	29	1969	-1.58	19.71	0
111	SLD 6	20	29	1969	-1.58	19.71	0
111	SLD 7	-7	-351	2099	17.19	-7.3	0.01
111	SLD 8	-7	-351	2099	17.19	-7.3	0.01
111	SLD 9	7	50	1877	-2.57	7.84	-0.01
111	SLD 10	7	50	1877	-2.57	7.84	-0.01
111	SLD 11	-20	-330	2007	16.2	-19.17	0
111	SLD 12	-20	-330	2007	16.2	-19.17	0
111	SLD 13	-17	-59	1815	2.85	-15.46	-0.01
111	SLD 14	-17	-59	1815	2.85	-15.46	-0.01
111	SLD 15	-26	-173	1854	8.48	-23.56	-0.01
111	SLD 16	-26	-173	1854	8.48	-23.56	-0.01
111	SLV 1	62	-96	2299	4.48	58.37	0.01
111	SLV 2	62	-96	2299	4.48	58.37	0.01
111	SLV 3	41	-367	2394	17.88	37.74	0.02
111	SLV 4	41	-367	2394	17.88	37.74	0.02
111	SLV 5	50	277	1938	-13.87	48.99	0
111	SLV 6	50	277	1938	-13.87	48.99	0
111	SLV 7	-19	-627	2253	30.81	-19.77	0.01
111	SLV 8	-19	-627	2253	30.81	-19.77	0.01
111	SLV 9	19	326	1723	-16.19	20.31	-0.01
111	SLV 10	19	326	1723	-16.19	20.31	-0.01
111	SLV 11	-50	-578	2037	28.49	-48.45	0
111	SLV 12	-50	-578	2037	28.49	-48.45	0
111	SLV 13	-41	66	1582	-3.26	-37.2	-0.02
111	SLV 14	-41	66	1582	-3.26	-37.2	-0.02
111	SLV 15	-62	-205	1676	10.15	-57.83	-0.01
111	SLV 16	-62	-205	1676	10.15	-57.83	-0.01
112	SLU 1	0	-169	2179	8.19	-0.24	0
112	SLU 2	0	-169	2179	8.19	-0.24	0
112	SLU 3	0	-169	2179	8.19	-0.24	0
112	SLU 4	0	-169	2179	8.19	-0.24	0
112	SLU 5	0	-169	2179	8.19	-0.24	0
112	SLU 6	0	-169	2179	8.19	-0.24	0
112	SLU 7	0	-169	2179	8.19	-0.24	0
112	SLU 8	0	-169	2179	8.19	-0.24	0
112	SLU 9	0	-169	2179	8.19	-0.24	0
112	SLU 10	0	-191	2492	9.4	-0.33	0
112	SLU 11	0	-191	2492	9.4	-0.33	0
112	SLU 12	0	-191	2492	9.4	-0.33	0
112	SLU 13	0	-191	2492	9.4	-0.33	0
112	SLU 14	0	-191	2492	9.4	-0.33	0
112	SLU 15	0	-191	2492	9.4	-0.33	0
112	SLU 16	0	-191	2492	9.4	-0.33	0
112	SLU 17	0	-191	2492	9.4	-0.33	0
112	SLU 18	0	-201	2626	9.92	-0.38	0
112	SLU 19	0	-201	2626	9.92	-0.38	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
112	SLU 20	0	-201	2626	9.92	-0.38	0
112	SLU 21	0	-201	2626	9.92	-0.38	0
112	SLU 22	0	-185	2371	9.04	-0.29	0
112	SLU 23	0	-185	2371	9.04	-0.29	0
112	SLU 24	0	-185	2371	9.04	-0.29	0
112	SLU 25	0	-185	2371	9.04	-0.29	0
112	SLU 26	0	-185	2371	9.04	-0.29	0
112	SLU 27	0	-185	2371	9.04	-0.29	0
112	SLU 28	0	-185	2371	9.04	-0.29	0
112	SLU 29	0	-185	2371	9.04	-0.29	0
112	SLU 30	0	-185	2371	9.04	-0.29	0
112	SLU 31	0	-208	2684	10.25	-0.38	0
112	SLU 32	0	-208	2684	10.25	-0.38	0
112	SLU 33	0	-208	2684	10.25	-0.38	0
112	SLU 34	0	-208	2684	10.25	-0.38	0
112	SLU 35	0	-208	2684	10.25	-0.38	0
112	SLU 36	0	-208	2684	10.25	-0.38	0
112	SLU 37	0	-208	2684	10.25	-0.38	0
112	SLU 38	0	-208	2684	10.25	-0.38	0
112	SLU 39	0	-218	2818	10.76	-0.43	0
112	SLU 40	0	-218	2818	10.76	-0.43	0
112	SLU 41	0	-218	2818	10.76	-0.43	0
112	SLU 42	0	-218	2818	10.76	-0.43	0
112	SLU 43	0	-213	2767	10.36	-0.29	0
112	SLU 44	0	-213	2767	10.36	-0.29	0
112	SLU 45	0	-213	2767	10.36	-0.29	0
112	SLU 46	0	-213	2767	10.36	-0.29	0
112	SLU 47	0	-213	2767	10.36	-0.29	0
112	SLU 48	0	-213	2767	10.36	-0.29	0
112	SLU 49	0	-213	2767	10.36	-0.29	0
112	SLU 50	0	-213	2767	10.36	-0.29	0
112	SLU 51	0	-213	2767	10.36	-0.29	0
112	SLU 52	0	-236	3080	11.57	-0.39	0
112	SLU 53	0	-236	3080	11.57	-0.39	0
112	SLU 54	0	-236	3080	11.57	-0.39	0
112	SLU 55	0	-236	3080	11.57	-0.39	0
112	SLU 56	0	-236	3080	11.57	-0.39	0
112	SLU 57	0	-236	3080	11.57	-0.39	0
112	SLU 58	0	-236	3080	11.57	-0.39	0
112	SLU 59	0	-236	3080	11.57	-0.39	0
112	SLU 60	0	-246	3214	12.09	-0.43	0
112	SLU 61	0	-246	3214	12.09	-0.43	0
112	SLU 62	0	-246	3214	12.09	-0.43	0
112	SLU 63	0	-246	3214	12.09	-0.43	0
112	SLU 64	0	-230	2959	11.2	-0.34	0
112	SLU 65	0	-230	2959	11.2	-0.34	0
112	SLU 66	0	-230	2959	11.2	-0.34	0
112	SLU 67	0	-230	2959	11.2	-0.34	0
112	SLU 68	0	-230	2959	11.2	-0.34	0
112	SLU 69	0	-230	2959	11.2	-0.34	0
112	SLU 70	0	-230	2959	11.2	-0.34	0
112	SLU 71	0	-230	2959	11.2	-0.34	0
112	SLU 72	0	-230	2959	11.2	-0.34	0
112	SLU 73	0	-253	3272	12.41	-0.44	0
112	SLU 74	0	-253	3272	12.41	-0.44	0
112	SLU 75	0	-253	3272	12.41	-0.44	0
112	SLU 76	0	-253	3272	12.41	-0.44	0
112	SLU 77	0	-253	3272	12.41	-0.44	0
112	SLU 78	0	-253	3272	12.41	-0.44	0
112	SLU 79	0	-253	3272	12.41	-0.44	0
112	SLU 80	0	-253	3272	12.41	-0.44	0
112	SLU 81	0	-263	3406	12.93	-0.48	0
112	SLU 82	0	-263	3406	12.93	-0.48	0
112	SLU 83	0	-263	3406	12.93	-0.48	0
112	SLU 84	0	-263	3406	12.93	-0.48	0
112	SLE RA 1	0	-173	2234	8.43	-0.25	0
112	SLE RA 2	0	-173	2234	8.43	-0.25	0
112	SLE RA 3	0	-173	2234	8.43	-0.25	0
112	SLE RA 4	0	-173	2234	8.43	-0.25	0
112	SLE RA 5	0	-173	2234	8.43	-0.25	0
112	SLE RA 6	0	-173	2234	8.43	-0.25	0
112	SLE RA 7	0	-173	2234	8.43	-0.25	0
112	SLE RA 8	0	-173	2234	8.43	-0.25	0
112	SLE RA 9	0	-173	2234	8.43	-0.25	0
112	SLE RA 10	0	-189	2443	9.24	-0.32	0
112	SLE RA 11	0	-189	2443	9.24	-0.32	0
112	SLE RA 12	0	-189	2443	9.24	-0.32	0
112	SLE RA 13	0	-189	2443	9.24	-0.32	0
112	SLE RA 14	0	-189	2443	9.24	-0.32	0
112	SLE RA 15	0	-189	2443	9.24	-0.32	0
112	SLE RA 16	0	-189	2443	9.24	-0.32	0
112	SLE RA 17	0	-189	2443	9.24	-0.32	0
112	SLE RA 18	0	-195	2532	9.58	-0.34	0
112	SLE RA 19	0	-195	2532	9.58	-0.34	0
112	SLE RA 20	0	-195	2532	9.58	-0.34	0
112	SLE RA 21	0	-195	2532	9.58	-0.34	0
112	SLE FR 1	0	-173	2234	8.43	-0.25	0
112	SLE FR 2	0	-173	2234	8.43	-0.25	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
112	SLE FR 3	0	-173	2234	8.43	-0.25	0
112	SLE FR 4	0	-180	2323	8.78	-0.28	0
112	SLE FR 5	0	-180	2323	8.78	-0.28	0
112	SLE FR 6	0	-184	2383	9.01	-0.3	0
112	SLE QP 1	0	-173	2234	8.43	-0.25	0
112	SLE QP 2	0	-180	2323	8.78	-0.28	0
112	SLD 1	18	-69	2126	3.47	17.56	0.01
112	SLD 2	18	-69	2126	3.47	17.56	0.01
112	SLD 3	28	-196	2158	9.69	26.35	0.01
112	SLD 4	28	-196	2158	9.69	26.35	0.01
112	SLD 5	-10	46	2217	-2.24	-8.25	0.01
112	SLD 6	-10	46	2217	-2.24	-8.25	0.01
112	SLD 7	23	-378	2321	18.47	21.04	0
112	SLD 8	23	-378	2321	18.47	21.04	0
112	SLD 9	-24	18	2325	-0.92	-21.59	0
112	SLD 10	-24	18	2325	-0.92	-21.59	0
112	SLD 11	10	-406	2430	19.79	7.7	-0.01
112	SLD 12	10	-406	2430	19.79	7.7	-0.01
112	SLD 13	-28	-164	2489	7.87	-26.91	-0.01
112	SLD 14	-28	-164	2489	7.87	-26.91	-0.01
112	SLD 15	-18	-291	2520	14.08	-18.12	-0.01
112	SLD 16	-18	-291	2520	14.08	-18.12	-0.01
112	SLV 1	42	83	1860	-3.78	42.66	0.03
112	SLV 2	42	83	1860	-3.78	42.66	0.03
112	SLV 3	68	-220	1937	11.03	65.24	0.03
112	SLV 4	68	-220	1937	11.03	65.24	0.03
112	SLV 5	-27	359	2068	-17.45	-21.64	0.02
112	SLV 6	-27	359	2068	-17.45	-21.64	0.02
112	SLV 7	60	-652	2324	31.91	53.63	0
112	SLV 8	60	-652	2324	31.91	53.63	0
112	SLV 9	-60	292	2322	-14.36	-54.18	0
112	SLV 10	-60	292	2322	-14.36	-54.18	0
112	SLV 11	27	-718	2579	35.01	21.09	-0.02
112	SLV 12	27	-718	2579	35.01	21.09	-0.02
112	SLV 13	-68	-139	2709	6.53	-65.8	-0.03
112	SLV 14	-68	-139	2709	6.53	-65.8	-0.03
112	SLV 15	-42	-442	2786	21.33	-43.22	-0.03
112	SLV 16	-42	-442	2786	21.33	-43.22	-0.03
113	SLU 1	0	0	1092	0	0	0
113	SLU 2	0	0	1092	0	0	0
113	SLU 3	0	0	1092	0	0	0
113	SLU 4	0	0	1092	0	0	0
113	SLU 5	0	0	1092	0	0	0
113	SLU 6	0	0	1092	0	0	0
113	SLU 7	0	0	1092	0	0	0
113	SLU 8	0	0	1092	0	0	0
113	SLU 9	0	0	1092	0	0	0
113	SLU 10	0	0	1296	0	0	0
113	SLU 11	0	0	1296	0	0	0
113	SLU 12	0	0	1296	0	0	0
113	SLU 13	0	0	1296	0	0	0
113	SLU 14	0	0	1296	0	0	0
113	SLU 15	0	0	1296	0	0	0
113	SLU 16	0	0	1296	0	0	0
113	SLU 17	0	0	1296	0	0	0
113	SLU 18	0	0	1384	0	0	0
113	SLU 19	0	0	1384	0	0	0
113	SLU 20	0	0	1384	0	0	0
113	SLU 21	0	0	1384	0	0	0
113	SLU 22	0	0	1218	0	0	0
113	SLU 23	0	0	1218	0	0	0
113	SLU 24	0	0	1218	0	0	0
113	SLU 25	0	0	1218	0	0	0
113	SLU 26	0	0	1218	0	0	0
113	SLU 27	0	0	1218	0	0	0
113	SLU 28	0	0	1218	0	0	0
113	SLU 29	0	0	1218	0	0	0
113	SLU 30	0	0	1218	0	0	0
113	SLU 31	0	0	1422	0	0	0
113	SLU 32	0	0	1422	0	0	0
113	SLU 33	0	0	1422	0	0	0
113	SLU 34	0	0	1422	0	0	0
113	SLU 35	0	0	1422	0	0	0
113	SLU 36	0	0	1422	0	0	0
113	SLU 37	0	0	1422	0	0	0
113	SLU 38	0	0	1422	0	0	0
113	SLU 39	0	0	1510	0	0	0
113	SLU 40	0	0	1510	0	0	0
113	SLU 41	0	0	1510	0	0	0
113	SLU 42	0	0	1510	0	0	0
113	SLU 43	0	0	1376	0	0	0
113	SLU 44	0	0	1376	0	0	0
113	SLU 45	0	0	1376	0	0	0
113	SLU 46	0	0	1376	0	0	0
113	SLU 47	0	0	1376	0	0	0
113	SLU 48	0	0	1376	0	0	0
113	SLU 49	0	0	1376	0	0	0
113	SLU 50	0	0	1376	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
113	SLU 51	0	0	1376	0	0	0
113	SLU 52	0	0	1581	0	0	0
113	SLU 53	0	0	1581	0	0	0
113	SLU 54	0	0	1581	0	0	0
113	SLU 55	0	0	1581	0	0	0
113	SLU 56	0	0	1581	0	0	0
113	SLU 57	0	0	1581	0	0	0
113	SLU 58	0	0	1581	0	0	0
113	SLU 59	0	0	1581	0	0	0
113	SLU 60	0	0	1668	0	0	0
113	SLU 61	0	0	1668	0	0	0
113	SLU 62	0	0	1668	0	0	0
113	SLU 63	0	0	1668	0	0	0
113	SLU 64	0	0	1502	0	0	0
113	SLU 65	0	0	1502	0	0	0
113	SLU 66	0	0	1502	0	0	0
113	SLU 67	0	0	1502	0	0	0
113	SLU 68	0	0	1502	0	0	0
113	SLU 69	0	0	1502	0	0	0
113	SLU 70	0	0	1502	0	0	0
113	SLU 71	0	0	1502	0	0	0
113	SLU 72	0	0	1502	0	0	0
113	SLU 73	0	0	1707	0	0	0
113	SLU 74	0	0	1707	0	0	0
113	SLU 75	0	0	1707	0	0	0
113	SLU 76	0	0	1707	0	0	0
113	SLU 77	0	0	1707	0	0	0
113	SLU 78	0	0	1707	0	0	0
113	SLU 79	0	0	1707	0	0	0
113	SLU 80	0	0	1707	0	0	0
113	SLU 81	0	0	1794	0	0	0
113	SLU 82	0	0	1794	0	0	0
113	SLU 83	0	0	1794	0	0	0
113	SLU 84	0	0	1794	0	0	0
113	SLE RA 1	0	0	1128	0	0	0
113	SLE RA 2	0	0	1128	0	0	0
113	SLE RA 3	0	0	1128	0	0	0
113	SLE RA 4	0	0	1128	0	0	0
113	SLE RA 5	0	0	1128	0	0	0
113	SLE RA 6	0	0	1128	0	0	0
113	SLE RA 7	0	0	1128	0	0	0
113	SLE RA 8	0	0	1128	0	0	0
113	SLE RA 9	0	0	1128	0	0	0
113	SLE RA 10	0	0	1264	0	0	0
113	SLE RA 11	0	0	1264	0	0	0
113	SLE RA 12	0	0	1264	0	0	0
113	SLE RA 13	0	0	1264	0	0	0
113	SLE RA 14	0	0	1264	0	0	0
113	SLE RA 15	0	0	1264	0	0	0
113	SLE RA 16	0	0	1264	0	0	0
113	SLE RA 17	0	0	1264	0	0	0
113	SLE RA 18	0	0	1323	0	0	0
113	SLE RA 19	0	0	1323	0	0	0
113	SLE RA 20	0	0	1323	0	0	0
113	SLE RA 21	0	0	1323	0	0	0
113	SLE FR 1	0	0	1128	0	0	0
113	SLE FR 2	0	0	1128	0	0	0
113	SLE FR 3	0	0	1128	0	0	0
113	SLE FR 4	0	0	1186	0	0	0
113	SLE FR 5	0	0	1186	0	0	0
113	SLE FR 6	0	0	1225	0	0	0
113	SLE QP 1	0	0	1128	0	0	0
113	SLE QP 2	0	0	1186	0	0	0
113	SLD 1	-3	0	1196	-0.05	5.8	0
113	SLD 2	-3	0	1196	-0.05	5.8	0
113	SLD 3	-3	-1	1179	0.05	5.59	0
113	SLD 4	-3	-1	1179	0.05	5.59	0
113	SLD 5	-1	2	1216	-0.17	2.06	0
113	SLD 6	-1	2	1216	-0.17	2.06	0
113	SLD 7	-1	-2	1157	0.17	1.36	0
113	SLD 8	-1	-2	1157	0.17	1.36	0
113	SLD 9	1	2	1215	-0.17	-1.36	0
113	SLD 10	1	2	1215	-0.17	-1.36	0
113	SLD 11	1	-2	1157	0.17	-2.06	0
113	SLD 12	1	-2	1157	0.17	-2.06	0
113	SLD 13	3	1	1194	-0.05	-5.59	0
113	SLD 14	3	1	1194	-0.05	-5.59	0
113	SLD 15	3	0	1176	0.05	-5.8	0
113	SLD 16	3	0	1176	0.05	-5.8	0
113	SLV 1	-8	1	1213	-0.14	14.8	0
113	SLV 2	-8	1	1213	-0.14	14.8	0
113	SLV 3	-9	-2	1165	0.14	14.25	0
113	SLV 4	-9	-2	1165	0.14	14.25	0
113	SLV 5	-2	5	1267	-0.47	5.27	0
113	SLV 6	-2	5	1267	-0.47	5.27	0
113	SLV 7	-3	-5	1107	0.47	3.44	0
113	SLV 8	-3	-5	1107	0.47	3.44	0
113	SLV 9	3	5	1265	-0.47	-3.44	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
113	SLV 10	3	5	1265	-0.47	-3.44	0
113	SLV 11	2	-5	1105	0.47	-5.27	0
113	SLV 12	2	-5	1105	0.47	-5.27	0
113	SLV 13	9	2	1207	-0.14	-14.25	0
113	SLV 14	9	2	1207	-0.14	-14.25	0
113	SLV 15	8	-1	1159	0.14	-14.8	0
113	SLV 16	8	-1	1159	0.14	-14.8	0
114	SLU 1	0	-159	1877	7.9	0.23	0
114	SLU 2	0	-159	1877	7.9	0.23	0
114	SLU 3	0	-159	1877	7.9	0.23	0
114	SLU 4	0	-159	1877	7.9	0.23	0
114	SLU 5	0	-159	1877	7.9	0.23	0
114	SLU 6	0	-159	1877	7.9	0.23	0
114	SLU 7	0	-159	1877	7.9	0.23	0
114	SLU 8	0	-159	1877	7.9	0.23	0
114	SLU 9	0	-159	1877	7.9	0.23	0
114	SLU 10	0	-170	2146	8.54	0.32	0
114	SLU 11	0	-170	2146	8.54	0.32	0
114	SLU 12	0	-170	2146	8.54	0.32	0
114	SLU 13	0	-170	2146	8.54	0.32	0
114	SLU 14	0	-170	2146	8.54	0.32	0
114	SLU 15	0	-170	2146	8.54	0.32	0
114	SLU 16	0	-170	2146	8.54	0.32	0
114	SLU 17	0	-170	2146	8.54	0.32	0
114	SLU 18	0	-175	2260	8.81	0.36	0
114	SLU 19	0	-175	2260	8.81	0.36	0
114	SLU 20	0	-175	2260	8.81	0.36	0
114	SLU 21	0	-175	2260	8.81	0.36	0
114	SLU 22	0	-169	2042	8.43	0.28	0
114	SLU 23	0	-169	2042	8.43	0.28	0
114	SLU 24	0	-169	2042	8.43	0.28	0
114	SLU 25	0	-169	2042	8.43	0.28	0
114	SLU 26	0	-169	2042	8.43	0.28	0
114	SLU 27	0	-169	2042	8.43	0.28	0
114	SLU 28	0	-169	2042	8.43	0.28	0
114	SLU 29	0	-169	2042	8.43	0.28	0
114	SLU 30	0	-169	2042	8.43	0.28	0
114	SLU 31	0	-180	2310	9.07	0.37	0
114	SLU 32	0	-180	2310	9.07	0.37	0
114	SLU 33	0	-180	2310	9.07	0.37	0
114	SLU 34	0	-180	2310	9.07	0.37	0
114	SLU 35	0	-180	2310	9.07	0.37	0
114	SLU 36	0	-180	2310	9.07	0.37	0
114	SLU 37	0	-180	2310	9.07	0.37	0
114	SLU 38	0	-180	2310	9.07	0.37	0
114	SLU 39	0	-185	2425	9.34	0.41	0
114	SLU 40	0	-185	2425	9.34	0.41	0
114	SLU 41	0	-185	2425	9.34	0.41	0
114	SLU 42	0	-185	2425	9.34	0.41	0
114	SLU 43	0	-204	2384	10.09	0.28	0
114	SLU 44	0	-204	2384	10.09	0.28	0
114	SLU 45	0	-204	2384	10.09	0.28	0
114	SLU 46	0	-204	2384	10.09	0.28	0
114	SLU 47	0	-204	2384	10.09	0.28	0
114	SLU 48	0	-204	2384	10.09	0.28	0
114	SLU 49	0	-204	2384	10.09	0.28	0
114	SLU 50	0	-204	2384	10.09	0.28	0
114	SLU 51	0	-204	2384	10.09	0.28	0
114	SLU 52	0	-214	2652	10.73	0.38	0
114	SLU 53	0	-214	2652	10.73	0.38	0
114	SLU 54	0	-214	2652	10.73	0.38	0
114	SLU 55	0	-214	2652	10.73	0.38	0
114	SLU 56	0	-214	2652	10.73	0.38	0
114	SLU 57	0	-214	2652	10.73	0.38	0
114	SLU 58	0	-214	2652	10.73	0.38	0
114	SLU 59	0	-214	2652	10.73	0.38	0
114	SLU 60	0	-219	2767	11	0.42	0
114	SLU 61	0	-219	2767	11	0.42	0
114	SLU 62	0	-219	2767	11	0.42	0
114	SLU 63	0	-219	2767	11	0.42	0
114	SLU 64	0	-213	2549	10.62	0.33	0
114	SLU 65	0	-213	2549	10.62	0.33	0
114	SLU 66	0	-213	2549	10.62	0.33	0
114	SLU 67	0	-213	2549	10.62	0.33	0
114	SLU 68	0	-213	2549	10.62	0.33	0
114	SLU 69	0	-213	2549	10.62	0.33	0
114	SLU 70	0	-213	2549	10.62	0.33	0
114	SLU 71	0	-213	2549	10.62	0.33	0
114	SLU 72	0	-213	2549	10.62	0.33	0
114	SLU 73	0	-224	2817	11.26	0.42	0
114	SLU 74	0	-224	2817	11.26	0.42	0
114	SLU 75	0	-224	2817	11.26	0.42	0
114	SLU 76	0	-224	2817	11.26	0.42	0
114	SLU 77	0	-224	2817	11.26	0.42	0
114	SLU 78	0	-224	2817	11.26	0.42	0
114	SLU 79	0	-224	2817	11.26	0.42	0
114	SLU 80	0	-224	2817	11.26	0.42	0
114	SLU 81	0	-229	2932	11.53	0.46	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
114	SLU 82	0	-229	2932	11.53	0.46	0
114	SLU 83	0	-229	2932	11.53	0.46	0
114	SLU 84	0	-229	2932	11.53	0.46	0
114	SLE RA 1	0	-162	1924	8.05	0.25	0
114	SLE RA 2	0	-162	1924	8.05	0.25	0
114	SLE RA 3	0	-162	1924	8.05	0.25	0
114	SLE RA 4	0	-162	1924	8.05	0.25	0
114	SLE RA 5	0	-162	1924	8.05	0.25	0
114	SLE RA 6	0	-162	1924	8.05	0.25	0
114	SLE RA 7	0	-162	1924	8.05	0.25	0
114	SLE RA 8	0	-162	1924	8.05	0.25	0
114	SLE RA 9	0	-162	1924	8.05	0.25	0
114	SLE RA 10	0	-169	2103	8.48	0.31	0
114	SLE RA 11	0	-169	2103	8.48	0.31	0
114	SLE RA 12	0	-169	2103	8.48	0.31	0
114	SLE RA 13	0	-169	2103	8.48	0.31	0
114	SLE RA 14	0	-169	2103	8.48	0.31	0
114	SLE RA 15	0	-169	2103	8.48	0.31	0
114	SLE RA 16	0	-169	2103	8.48	0.31	0
114	SLE RA 17	0	-169	2103	8.48	0.31	0
114	SLE RA 18	0	-172	2180	8.66	0.33	0
114	SLE RA 19	0	-172	2180	8.66	0.33	0
114	SLE RA 20	0	-172	2180	8.66	0.33	0
114	SLE RA 21	0	-172	2180	8.66	0.33	0
114	SLE FR 1	0	-162	1924	8.05	0.25	0
114	SLE FR 2	0	-162	1924	8.05	0.25	0
114	SLE FR 3	0	-162	1924	8.05	0.25	0
114	SLE FR 4	0	-165	2001	8.24	0.27	0
114	SLE FR 5	0	-165	2001	8.24	0.27	0
114	SLE FR 6	0	-167	2052	8.36	0.29	0
114	SLE QP 1	0	-162	1924	8.05	0.25	0
114	SLE QP 2	0	-165	2001	8.24	0.27	0
114	SLD 1	23	-146	2136	7.18	21.84	0.01
114	SLD 2	23	-146	2136	7.18	21.84	0.01
114	SLD 3	13	-257	2186	12.64	13.53	0.01
114	SLD 4	13	-257	2186	12.64	13.53	0.01
114	SLD 5	22	9	1964	-0.37	19.35	0
114	SLD 6	22	9	1964	-0.37	19.35	0
114	SLD 7	-11	-361	2134	17.85	-8.36	0.01
114	SLD 8	-11	-361	2134	17.85	-8.36	0.01
114	SLD 9	11	31	1868	-1.37	8.9	-0.01
114	SLD 10	11	31	1868	-1.37	8.9	-0.01
114	SLD 11	-21	-339	2038	16.84	-18.8	0
114	SLD 12	-21	-339	2038	16.84	-18.8	0
114	SLD 13	-13	-73	1815	3.83	-12.99	-0.01
114	SLD 14	-13	-73	1815	3.83	-12.99	-0.01
114	SLD 15	-23	-184	1866	9.3	-21.3	-0.01
114	SLD 16	-23	-184	1866	9.3	-21.3	-0.01
114	SLV 1	56	-119	2314	5.69	53.07	0.02
114	SLV 2	56	-119	2314	5.69	53.07	0.02
114	SLV 3	31	-382	2438	18.64	31.85	0.03
114	SLV 4	31	-382	2438	18.64	31.85	0.03
114	SLV 5	54	248	1908	-12.17	48.29	0
114	SLV 6	54	248	1908	-12.17	48.29	0
114	SLV 7	-28	-629	2319	31	-22.44	0.02
114	SLV 8	-28	-629	2319	31	-22.44	0.02
114	SLV 9	28	299	1683	-14.53	22.98	-0.02
114	SLV 10	28	299	1683	-14.53	22.98	-0.02
114	SLV 11	-54	-578	2094	28.64	-47.75	0
114	SLV 12	-54	-578	2094	28.64	-47.75	0
114	SLV 13	-31	51	1564	-2.17	-31.31	-0.03
114	SLV 14	-31	51	1564	-2.17	-31.31	-0.03
114	SLV 15	-56	-212	1688	10.78	-52.53	-0.02
114	SLV 16	-56	-212	1688	10.78	-52.53	-0.02
115	SLU 1	0	-215	2189	10.25	-0.3	0
115	SLU 2	0	-215	2189	10.25	-0.3	0
115	SLU 3	0	-215	2189	10.25	-0.3	0
115	SLU 4	0	-215	2189	10.25	-0.3	0
115	SLU 5	0	-215	2189	10.25	-0.3	0
115	SLU 6	0	-215	2189	10.25	-0.3	0
115	SLU 7	0	-215	2189	10.25	-0.3	0
115	SLU 8	0	-215	2189	10.25	-0.3	0
115	SLU 9	0	-215	2189	10.25	-0.3	0
115	SLU 10	0	-238	2522	11.51	-0.41	0
115	SLU 11	0	-238	2522	11.51	-0.41	0
115	SLU 12	0	-238	2522	11.51	-0.41	0
115	SLU 13	0	-238	2522	11.51	-0.41	0
115	SLU 14	0	-238	2522	11.51	-0.41	0
115	SLU 15	0	-238	2522	11.51	-0.41	0
115	SLU 16	0	-238	2522	11.51	-0.41	0
115	SLU 17	0	-238	2522	11.51	-0.41	0
115	SLU 18	0	-248	2665	12.05	-0.45	0
115	SLU 19	0	-248	2665	12.05	-0.45	0
115	SLU 20	0	-248	2665	12.05	-0.45	0
115	SLU 21	0	-248	2665	12.05	-0.45	0
115	SLU 22	0	-232	2391	11.16	-0.36	0
115	SLU 23	0	-232	2391	11.16	-0.36	0
115	SLU 24	0	-232	2391	11.16	-0.36	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
115	SLU 25	0	-232	2391	11.16	-0.36	0
115	SLU 26	0	-232	2391	11.16	-0.36	0
115	SLU 27	0	-232	2391	11.16	-0.36	0
115	SLU 28	0	-232	2391	11.16	-0.36	0
115	SLU 29	0	-232	2391	11.16	-0.36	0
115	SLU 30	0	-232	2391	11.16	-0.36	0
115	SLU 31	0	-256	2724	12.42	-0.46	0
115	SLU 32	0	-256	2724	12.42	-0.46	0
115	SLU 33	0	-256	2724	12.42	-0.46	0
115	SLU 34	0	-256	2724	12.42	-0.46	0
115	SLU 35	0	-256	2724	12.42	-0.46	0
115	SLU 36	0	-256	2724	12.42	-0.46	0
115	SLU 37	0	-256	2724	12.42	-0.46	0
115	SLU 38	0	-256	2724	12.42	-0.46	0
115	SLU 39	0	-266	2866	12.96	-0.51	0
115	SLU 40	0	-266	2866	12.96	-0.51	0
115	SLU 41	0	-266	2866	12.96	-0.51	0
115	SLU 42	0	-266	2866	12.96	-0.51	0
115	SLU 43	0	-273	2777	13.01	-0.37	0
115	SLU 44	0	-273	2777	13.01	-0.37	0
115	SLU 45	0	-273	2777	13.01	-0.37	0
115	SLU 46	0	-273	2777	13.01	-0.37	0
115	SLU 47	0	-273	2777	13.01	-0.37	0
115	SLU 48	0	-273	2777	13.01	-0.37	0
115	SLU 49	0	-273	2777	13.01	-0.37	0
115	SLU 50	0	-273	2777	13.01	-0.37	0
115	SLU 51	0	-273	2777	13.01	-0.37	0
115	SLU 52	0	-296	3110	14.27	-0.48	0
115	SLU 53	0	-296	3110	14.27	-0.48	0
115	SLU 54	0	-296	3110	14.27	-0.48	0
115	SLU 55	0	-296	3110	14.27	-0.48	0
115	SLU 56	0	-296	3110	14.27	-0.48	0
115	SLU 57	0	-296	3110	14.27	-0.48	0
115	SLU 58	0	-296	3110	14.27	-0.48	0
115	SLU 59	0	-296	3110	14.27	-0.48	0
115	SLU 60	0	-307	3253	14.81	-0.52	0
115	SLU 61	0	-307	3253	14.81	-0.52	0
115	SLU 62	0	-307	3253	14.81	-0.52	0
115	SLU 63	0	-307	3253	14.81	-0.52	0
115	SLU 64	0	-291	2978	13.92	-0.43	0
115	SLU 65	0	-291	2978	13.92	-0.43	0
115	SLU 66	0	-291	2978	13.92	-0.43	0
115	SLU 67	0	-291	2978	13.92	-0.43	0
115	SLU 68	0	-291	2978	13.92	-0.43	0
115	SLU 69	0	-291	2978	13.92	-0.43	0
115	SLU 70	0	-291	2978	13.92	-0.43	0
115	SLU 71	0	-291	2978	13.92	-0.43	0
115	SLU 72	0	-291	2978	13.92	-0.43	0
115	SLU 73	0	-314	3311	15.18	-0.53	0
115	SLU 74	0	-314	3311	15.18	-0.53	0
115	SLU 75	0	-314	3311	15.18	-0.53	0
115	SLU 76	0	-314	3311	15.18	-0.53	0
115	SLU 77	0	-314	3311	15.18	-0.53	0
115	SLU 78	0	-314	3311	15.18	-0.53	0
115	SLU 79	0	-314	3311	15.18	-0.53	0
115	SLU 80	0	-314	3311	15.18	-0.53	0
115	SLU 81	0	-324	3454	15.72	-0.58	0
115	SLU 82	0	-324	3454	15.72	-0.58	0
115	SLU 83	0	-324	3454	15.72	-0.58	0
115	SLU 84	0	-324	3454	15.72	-0.58	0
115	SLE RA 1	0	-220	2247	10.51	-0.32	0
115	SLE RA 2	0	-220	2247	10.51	-0.32	0
115	SLE RA 3	0	-220	2247	10.51	-0.32	0
115	SLE RA 4	0	-220	2247	10.51	-0.32	0
115	SLE RA 5	0	-220	2247	10.51	-0.32	0
115	SLE RA 6	0	-220	2247	10.51	-0.32	0
115	SLE RA 7	0	-220	2247	10.51	-0.32	0
115	SLE RA 8	0	-220	2247	10.51	-0.32	0
115	SLE RA 9	0	-220	2247	10.51	-0.32	0
115	SLE RA 10	0	-235	2469	11.35	-0.39	0
115	SLE RA 11	0	-235	2469	11.35	-0.39	0
115	SLE RA 12	0	-235	2469	11.35	-0.39	0
115	SLE RA 13	0	-235	2469	11.35	-0.39	0
115	SLE RA 14	0	-235	2469	11.35	-0.39	0
115	SLE RA 15	0	-235	2469	11.35	-0.39	0
115	SLE RA 16	0	-235	2469	11.35	-0.39	0
115	SLE RA 17	0	-235	2469	11.35	-0.39	0
115	SLE RA 18	0	-242	2564	11.71	-0.42	0
115	SLE RA 19	0	-242	2564	11.71	-0.42	0
115	SLE RA 20	0	-242	2564	11.71	-0.42	0
115	SLE RA 21	0	-242	2564	11.71	-0.42	0
115	SLE FR 1	0	-220	2247	10.51	-0.32	0
115	SLE FR 2	0	-220	2247	10.51	-0.32	0
115	SLE FR 3	0	-220	2247	10.51	-0.32	0
115	SLE FR 4	0	-226	2342	10.87	-0.35	0
115	SLE FR 5	0	-226	2342	10.87	-0.35	0
115	SLE FR 6	0	-231	2405	11.11	-0.37	0
115	SLE QP 1	0	-220	2247	10.51	-0.32	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
115	SLE QP 2	0	-226	2342	10.87	-0.35	0
115	SLD 1	10	-110	2115	5.28	12.63	0.02
115	SLD 2	10	-110	2115	5.28	12.63	0.02
115	SLD 3	22	-238	2174	11.58	21.26	0.01
115	SLD 4	22	-238	2174	11.58	21.26	0.01
115	SLD 5	-14	3	2184	-0.36	-9.54	0.01
115	SLD 6	-14	3	2184	-0.36	-9.54	0.01
115	SLD 7	24	-424	2382	20.63	19.22	0
115	SLD 8	24	-424	2382	20.63	19.22	0
115	SLD 9	-24	-29	2302	1.11	-19.91	0
115	SLD 10	-24	-29	2302	1.11	-19.91	0
115	SLD 11	14	-456	2500	22.09	8.85	-0.01
115	SLD 12	14	-456	2500	22.09	8.85	-0.01
115	SLD 13	-22	-215	2510	10.16	-21.95	-0.01
115	SLD 14	-22	-215	2510	10.16	-21.95	-0.01
115	SLD 15	-10	-343	2569	16.45	-13.32	-0.02
115	SLD 16	-10	-343	2569	16.45	-13.32	-0.02
115	SLV 1	24	49	1806	-2.36	30.85	0.04
115	SLV 2	24	49	1806	-2.36	30.85	0.04
115	SLV 3	54	-257	1951	12.65	53.17	0.03
115	SLV 4	54	-257	1951	12.65	53.17	0.03
115	SLV 5	-38	319	1962	-15.87	-24.84	0.03
115	SLV 6	-38	319	1962	-15.87	-24.84	0.03
115	SLV 7	61	-699	2444	34.17	49.57	0
115	SLV 8	61	-699	2444	34.17	49.57	0
115	SLV 9	-62	246	2240	-12.44	-50.26	0
115	SLV 10	-62	246	2240	-12.44	-50.26	0
115	SLV 11	38	-772	2722	37.61	24.15	-0.03
115	SLV 12	38	-772	2722	37.61	24.15	-0.03
115	SLV 13	-54	-196	2733	9.08	-53.87	-0.03
115	SLV 14	-54	-196	2733	9.08	-53.87	-0.03
115	SLV 15	-24	-502	2878	24.1	-31.54	-0.04
115	SLV 16	-24	-502	2878	24.1	-31.54	-0.04
116	SLU 1	0	0	1079	0	0	0
116	SLU 2	0	0	1079	0	0	0
116	SLU 3	0	0	1079	0	0	0
116	SLU 4	0	0	1079	0	0	0
116	SLU 5	0	0	1079	0	0	0
116	SLU 6	0	0	1079	0	0	0
116	SLU 7	0	0	1079	0	0	0
116	SLU 8	0	0	1079	0	0	0
116	SLU 9	0	0	1079	0	0	0
116	SLU 10	0	0	1286	0	0	0
116	SLU 11	0	0	1286	0	0	0
116	SLU 12	0	0	1286	0	0	0
116	SLU 13	0	0	1286	0	0	0
116	SLU 14	0	0	1286	0	0	0
116	SLU 15	0	0	1286	0	0	0
116	SLU 16	0	0	1286	0	0	0
116	SLU 17	0	0	1286	0	0	0
116	SLU 18	0	0	1375	0	0	0
116	SLU 19	0	0	1375	0	0	0
116	SLU 20	0	0	1375	0	0	0
116	SLU 21	0	0	1375	0	0	0
116	SLU 22	0	0	1205	0	0	0
116	SLU 23	0	0	1205	0	0	0
116	SLU 24	0	0	1205	0	0	0
116	SLU 25	0	0	1205	0	0	0
116	SLU 26	0	0	1205	0	0	0
116	SLU 27	0	0	1205	0	0	0
116	SLU 28	0	0	1205	0	0	0
116	SLU 29	0	0	1205	0	0	0
116	SLU 30	0	0	1205	0	0	0
116	SLU 31	0	0	1412	0	0	0
116	SLU 32	0	0	1412	0	0	0
116	SLU 33	0	0	1412	0	0	0
116	SLU 34	0	0	1412	0	0	0
116	SLU 35	0	0	1412	0	0	0
116	SLU 36	0	0	1412	0	0	0
116	SLU 37	0	0	1412	0	0	0
116	SLU 38	0	0	1412	0	0	0
116	SLU 39	0	0	1500	0	0	0
116	SLU 40	0	0	1500	0	0	0
116	SLU 41	0	0	1500	0	0	0
116	SLU 42	0	0	1500	0	0	0
116	SLU 43	0	0	1360	0	0	0
116	SLU 44	0	0	1360	0	0	0
116	SLU 45	0	0	1360	0	0	0
116	SLU 46	0	0	1360	0	0	0
116	SLU 47	0	0	1360	0	0	0
116	SLU 48	0	0	1360	0	0	0
116	SLU 49	0	0	1360	0	0	0
116	SLU 50	0	0	1360	0	0	0
116	SLU 51	0	0	1360	0	0	0
116	SLU 52	0	0	1567	0	0	0
116	SLU 53	0	0	1567	0	0	0
116	SLU 54	0	0	1567	0	0	0
116	SLU 55	0	0	1567	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
116	SLU 56	0	0	1567	0	0	0
116	SLU 57	0	0	1567	0	0	0
116	SLU 58	0	0	1567	0	0	0
116	SLU 59	0	0	1567	0	0	0
116	SLU 60	0	0	1655	0	0	0
116	SLU 61	0	0	1655	0	0	0
116	SLU 62	0	0	1655	0	0	0
116	SLU 63	0	0	1655	0	0	0
116	SLU 64	0	0	1486	0	0	0
116	SLU 65	0	0	1486	0	0	0
116	SLU 66	0	0	1486	0	0	0
116	SLU 67	0	0	1486	0	0	0
116	SLU 68	0	0	1486	0	0	0
116	SLU 69	0	0	1486	0	0	0
116	SLU 70	0	0	1486	0	0	0
116	SLU 71	0	0	1486	0	0	0
116	SLU 72	0	0	1486	0	0	0
116	SLU 73	0	0	1692	0	0	0
116	SLU 74	0	0	1692	0	0	0
116	SLU 75	0	0	1692	0	0	0
116	SLU 76	0	0	1692	0	0	0
116	SLU 77	0	0	1692	0	0	0
116	SLU 78	0	0	1692	0	0	0
116	SLU 79	0	0	1692	0	0	0
116	SLU 80	0	0	1692	0	0	0
116	SLU 81	0	0	1781	0	0	0
116	SLU 82	0	0	1781	0	0	0
116	SLU 83	0	0	1781	0	0	0
116	SLU 84	0	0	1781	0	0	0
116	SLE RA 1	0	0	1115	0	0	0
116	SLE RA 2	0	0	1115	0	0	0
116	SLE RA 3	0	0	1115	0	0	0
116	SLE RA 4	0	0	1115	0	0	0
116	SLE RA 5	0	0	1115	0	0	0
116	SLE RA 6	0	0	1115	0	0	0
116	SLE RA 7	0	0	1115	0	0	0
116	SLE RA 8	0	0	1115	0	0	0
116	SLE RA 9	0	0	1115	0	0	0
116	SLE RA 10	0	0	1253	0	0	0
116	SLE RA 11	0	0	1253	0	0	0
116	SLE RA 12	0	0	1253	0	0	0
116	SLE RA 13	0	0	1253	0	0	0
116	SLE RA 14	0	0	1253	0	0	0
116	SLE RA 15	0	0	1253	0	0	0
116	SLE RA 16	0	0	1253	0	0	0
116	SLE RA 17	0	0	1253	0	0	0
116	SLE RA 18	0	0	1312	0	0	0
116	SLE RA 19	0	0	1312	0	0	0
116	SLE RA 20	0	0	1312	0	0	0
116	SLE RA 21	0	0	1312	0	0	0
116	SLE FR 1	0	0	1115	0	0	0
116	SLE FR 2	0	0	1115	0	0	0
116	SLE FR 3	0	0	1115	0	0	0
116	SLE FR 4	0	0	1174	0	0	0
116	SLE FR 5	0	0	1174	0	0	0
116	SLE FR 6	0	0	1214	0	0	0
116	SLE QP 1	0	0	1115	0	0	0
116	SLE QP 2	0	0	1174	0	0	0
116	SLD 1	-2	0	1195	-0.01	4.16	0
116	SLD 2	-2	0	1195	-0.01	4.16	0
116	SLD 3	-3	-1	1156	0.01	4	0
116	SLD 4	-3	-1	1156	0.01	4	0
116	SLD 5	-1	2	1239	-0.05	1.49	0
116	SLD 6	-1	2	1239	-0.05	1.49	0
116	SLD 7	-1	-2	1110	0.04	0.96	0
116	SLD 8	-1	-2	1110	0.04	0.96	0
116	SLD 9	1	2	1238	-0.05	-0.96	0
116	SLD 10	1	2	1238	-0.05	-0.96	0
116	SLD 11	1	-2	1110	0.04	-1.48	0
116	SLD 12	1	-2	1110	0.04	-1.48	0
116	SLD 13	3	1	1192	-0.01	-4	0
116	SLD 14	3	1	1192	-0.01	-4	0
116	SLD 15	2	0	1154	0.01	-4.15	0
116	SLD 16	2	0	1154	0.01	-4.15	0
116	SLV 1	-6	1	1231	-0.04	10.61	0
116	SLV 2	-6	1	1231	-0.04	10.61	0
116	SLV 3	-6	-2	1123	0.04	10.2	0
116	SLV 4	-6	-2	1123	0.04	10.2	0
116	SLV 5	-1	5	1355	-0.13	3.81	0
116	SLV 6	-1	5	1355	-0.13	3.81	0
116	SLV 7	-2	-6	995	0.13	2.43	0
116	SLV 8	-2	-6	995	0.13	2.43	0
116	SLV 9	2	6	1354	-0.13	-2.43	0
116	SLV 10	2	6	1354	-0.13	-2.43	0
116	SLV 11	1	-5	993	0.13	-3.81	0
116	SLV 12	1	-5	993	0.13	-3.81	0
116	SLV 13	6	2	1226	-0.04	-10.2	0
116	SLV 14	6	2	1226	-0.04	-10.2	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
116	SLV 15	6	-1	1118	0.04	-10.61	0
116	SLV 16	6	-1	1118	0.04	-10.61	0
117	SLU 1	0	-183	1906	9.16	0.3	0
117	SLU 2	0	-183	1906	9.16	0.3	0
117	SLU 3	0	-183	1906	9.16	0.3	0
117	SLU 4	0	-183	1906	9.16	0.3	0
117	SLU 5	0	-183	1906	9.16	0.3	0
117	SLU 6	0	-183	1906	9.16	0.3	0
117	SLU 7	0	-183	1906	9.16	0.3	0
117	SLU 8	0	-183	1906	9.16	0.3	0
117	SLU 9	0	-183	1906	9.16	0.3	0
117	SLU 10	0	-190	2195	9.68	0.4	0
117	SLU 11	0	-190	2195	9.68	0.4	0
117	SLU 12	0	-190	2195	9.68	0.4	0
117	SLU 13	0	-190	2195	9.68	0.4	0
117	SLU 14	0	-190	2195	9.68	0.4	0
117	SLU 15	0	-190	2195	9.68	0.4	0
117	SLU 16	0	-190	2195	9.68	0.4	0
117	SLU 17	0	-190	2195	9.68	0.4	0
117	SLU 18	0	-193	2318	9.9	0.45	0
117	SLU 19	0	-193	2318	9.9	0.45	0
117	SLU 20	0	-193	2318	9.9	0.45	0
117	SLU 21	0	-193	2318	9.9	0.45	0
117	SLU 22	0	-191	2081	9.65	0.36	0
117	SLU 23	0	-191	2081	9.65	0.36	0
117	SLU 24	0	-191	2081	9.65	0.36	0
117	SLU 25	0	-191	2081	9.65	0.36	0
117	SLU 26	0	-191	2081	9.65	0.36	0
117	SLU 27	0	-191	2081	9.65	0.36	0
117	SLU 28	0	-191	2081	9.65	0.36	0
117	SLU 29	0	-191	2081	9.65	0.36	0
117	SLU 30	0	-191	2081	9.65	0.36	0
117	SLU 31	0	-199	2369	10.16	0.46	0
117	SLU 32	0	-199	2369	10.16	0.46	0
117	SLU 33	0	-199	2369	10.16	0.46	0
117	SLU 34	0	-199	2369	10.16	0.46	0
117	SLU 35	0	-199	2369	10.16	0.46	0
117	SLU 36	0	-199	2369	10.16	0.46	0
117	SLU 37	0	-199	2369	10.16	0.46	0
117	SLU 38	0	-199	2369	10.16	0.46	0
117	SLU 39	0	-202	2492	10.38	0.5	0
117	SLU 40	0	-202	2492	10.38	0.5	0
117	SLU 41	0	-202	2492	10.38	0.5	0
117	SLU 42	0	-202	2492	10.38	0.5	0
117	SLU 43	0	-235	2419	11.75	0.37	0
117	SLU 44	0	-235	2419	11.75	0.37	0
117	SLU 45	0	-235	2419	11.75	0.37	0
117	SLU 46	0	-235	2419	11.75	0.37	0
117	SLU 47	0	-235	2419	11.75	0.37	0
117	SLU 48	0	-235	2419	11.75	0.37	0
117	SLU 49	0	-235	2419	11.75	0.37	0
117	SLU 50	0	-235	2419	11.75	0.37	0
117	SLU 51	0	-235	2419	11.75	0.37	0
117	SLU 52	0	-242	2707	12.26	0.48	0
117	SLU 53	0	-242	2707	12.26	0.48	0
117	SLU 54	0	-242	2707	12.26	0.48	0
117	SLU 55	0	-242	2707	12.26	0.48	0
117	SLU 56	0	-242	2707	12.26	0.48	0
117	SLU 57	0	-242	2707	12.26	0.48	0
117	SLU 58	0	-242	2707	12.26	0.48	0
117	SLU 59	0	-242	2707	12.26	0.48	0
117	SLU 60	0	-245	2831	12.48	0.52	0
117	SLU 61	0	-245	2831	12.48	0.52	0
117	SLU 62	0	-245	2831	12.48	0.52	0
117	SLU 63	0	-245	2831	12.48	0.52	0
117	SLU 64	0	-243	2593	12.23	0.43	0
117	SLU 65	0	-243	2593	12.23	0.43	0
117	SLU 66	0	-243	2593	12.23	0.43	0
117	SLU 67	0	-243	2593	12.23	0.43	0
117	SLU 68	0	-243	2593	12.23	0.43	0
117	SLU 69	0	-243	2593	12.23	0.43	0
117	SLU 70	0	-243	2593	12.23	0.43	0
117	SLU 71	0	-243	2593	12.23	0.43	0
117	SLU 72	0	-243	2593	12.23	0.43	0
117	SLU 73	0	-251	2881	12.75	0.53	0
117	SLU 74	0	-251	2881	12.75	0.53	0
117	SLU 75	0	-251	2881	12.75	0.53	0
117	SLU 76	0	-251	2881	12.75	0.53	0
117	SLU 77	0	-251	2881	12.75	0.53	0
117	SLU 78	0	-251	2881	12.75	0.53	0
117	SLU 79	0	-251	2881	12.75	0.53	0
117	SLU 80	0	-251	2881	12.75	0.53	0
117	SLU 81	0	-254	3005	12.97	0.57	0
117	SLU 82	0	-254	3005	12.97	0.57	0
117	SLU 83	0	-254	3005	12.97	0.57	0
117	SLU 84	0	-254	3005	12.97	0.57	0
117	SLE RA 1	0	-185	1956	9.3	0.32	0
117	SLE RA 2	0	-185	1956	9.3	0.32	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
117	SLE RA 3	0	-185	1956	9.3	0.32	0
117	SLE RA 4	0	-185	1956	9.3	0.32	0
117	SLE RA 5	0	-185	1956	9.3	0.32	0
117	SLE RA 6	0	-185	1956	9.3	0.32	0
117	SLE RA 7	0	-185	1956	9.3	0.32	0
117	SLE RA 8	0	-185	1956	9.3	0.32	0
117	SLE RA 9	0	-185	1956	9.3	0.32	0
117	SLE RA 10	0	-190	2148	9.65	0.39	0
117	SLE RA 11	0	-190	2148	9.65	0.39	0
117	SLE RA 12	0	-190	2148	9.65	0.39	0
117	SLE RA 13	0	-190	2148	9.65	0.39	0
117	SLE RA 14	0	-190	2148	9.65	0.39	0
117	SLE RA 15	0	-190	2148	9.65	0.39	0
117	SLE RA 16	0	-190	2148	9.65	0.39	0
117	SLE RA 17	0	-190	2148	9.65	0.39	0
117	SLE RA 18	0	-192	2231	9.79	0.41	0
117	SLE RA 19	0	-192	2231	9.79	0.41	0
117	SLE RA 20	0	-192	2231	9.79	0.41	0
117	SLE RA 21	0	-192	2231	9.79	0.41	0
117	SLE FR 1	0	-185	1956	9.3	0.32	0
117	SLE FR 2	0	-185	1956	9.3	0.32	0
117	SLE FR 3	0	-185	1956	9.3	0.32	0
117	SLE FR 4	0	-187	2039	9.45	0.35	0
117	SLE FR 5	0	-187	2039	9.45	0.35	0
117	SLE FR 6	0	-189	2093	9.55	0.37	0
117	SLE QP 1	0	-185	1956	9.3	0.32	0
117	SLE QP 2	0	-187	2039	9.45	0.35	0
117	SLD 1	18	-174	2181	8.61	17.73	0.01
117	SLD 2	18	-174	2181	8.61	17.73	0.01
117	SLD 3	7	-281	2249	14.03	9.79	0.01
117	SLD 4	7	-281	2249	14.03	9.79	0.01
117	SLD 5	22	-20	1978	0.97	17.6	0
117	SLD 6	22	-20	1978	0.97	17.6	0
117	SLD 7	-14	-379	2205	19.05	-8.86	0.01
117	SLD 8	-14	-379	2205	19.05	-8.86	0.01
117	SLD 9	14	4	1872	-0.15	9.55	-0.01
117	SLD 10	14	4	1872	-0.15	9.55	-0.01
117	SLD 11	-22	-354	2099	17.93	-16.9	0
117	SLD 12	-22	-354	2099	17.93	-16.9	0
117	SLD 13	-7	-93	1828	4.87	-9.1	-0.01
117	SLD 14	-7	-93	1828	4.87	-9.1	-0.01
117	SLD 15	-18	-201	1896	10.29	-17.04	-0.01
117	SLD 16	-18	-201	1896	10.29	-17.04	-0.01
117	SLV 1	44	-155	2370	7.4	43.15	0.03
117	SLV 2	44	-155	2370	7.4	43.15	0.03
117	SLV 3	16	-410	2535	20.29	22.8	0.03
117	SLV 4	16	-410	2535	20.29	22.8	0.03
117	SLV 5	56	210	1889	-10.71	44.05	0
117	SLV 6	56	210	1889	-10.71	44.05	0
117	SLV 7	-38	-641	2437	32.25	-23.78	0.02
117	SLV 8	-38	-641	2437	32.25	-23.78	0.02
117	SLV 9	38	267	1641	-13.35	24.47	-0.02
117	SLV 10	38	267	1641	-13.35	24.47	-0.02
117	SLV 11	-56	-584	2188	29.61	-43.36	0.01
117	SLV 12	-56	-584	2188	29.61	-43.36	0.01
117	SLV 13	-16	35	1543	-1.39	-22.11	-0.03
117	SLV 14	-16	35	1543	-1.39	-22.11	-0.03
117	SLV 15	-44	-220	1707	11.5	-42.46	-0.02
117	SLV 16	-44	-220	1707	11.5	-42.46	-0.02
118	SLU 1	0	-270	2232	13.39	-0.52	0
118	SLU 2	0	-270	2232	13.39	-0.52	0
118	SLU 3	0	-270	2232	13.39	-0.52	0
118	SLU 4	0	-270	2232	13.39	-0.52	0
118	SLU 5	0	-270	2232	13.39	-0.52	0
118	SLU 6	0	-270	2232	13.39	-0.52	0
118	SLU 7	0	-270	2232	13.39	-0.52	0
118	SLU 8	0	-270	2232	13.39	-0.52	0
118	SLU 9	0	-270	2232	13.39	-0.52	0
118	SLU 10	0	-295	2599	14.87	-0.67	-0.01
118	SLU 11	0	-295	2599	14.87	-0.67	-0.01
118	SLU 12	0	-295	2599	14.87	-0.67	-0.01
118	SLU 13	0	-295	2599	14.87	-0.67	-0.01
118	SLU 14	0	-295	2599	14.87	-0.67	-0.01
118	SLU 15	0	-295	2599	14.87	-0.67	-0.01
118	SLU 16	0	-295	2599	14.87	-0.67	-0.01
118	SLU 17	0	-295	2599	14.87	-0.67	-0.01
118	SLU 18	-1	-306	2756	15.51	-0.74	-0.01
118	SLU 19	-1	-306	2756	15.51	-0.74	-0.01
118	SLU 20	-1	-306	2756	15.51	-0.74	-0.01
118	SLU 21	-1	-306	2756	15.51	-0.74	-0.01
118	SLU 22	0	-289	2450	14.46	-0.6	-0.01
118	SLU 23	0	-289	2450	14.46	-0.6	-0.01
118	SLU 24	0	-289	2450	14.46	-0.6	-0.01
118	SLU 25	0	-289	2450	14.46	-0.6	-0.01
118	SLU 26	0	-289	2450	14.46	-0.6	-0.01
118	SLU 27	0	-289	2450	14.46	-0.6	-0.01
118	SLU 28	0	-289	2450	14.46	-0.6	-0.01
118	SLU 29	0	-289	2450	14.46	-0.6	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
118	SLU 30	0	-289	2450	14.46	-0.6	-0.01
118	SLU 31	-1	-314	2817	15.94	-0.75	-0.01
118	SLU 32	-1	-314	2817	15.94	-0.75	-0.01
118	SLU 33	-1	-314	2817	15.94	-0.75	-0.01
118	SLU 34	-1	-314	2817	15.94	-0.75	-0.01
118	SLU 35	-1	-314	2817	15.94	-0.75	-0.01
118	SLU 36	-1	-314	2817	15.94	-0.75	-0.01
118	SLU 37	-1	-314	2817	15.94	-0.75	-0.01
118	SLU 38	-1	-314	2817	15.94	-0.75	-0.01
118	SLU 39	-1	-325	2974	16.57	-0.82	-0.01
118	SLU 40	-1	-325	2974	16.57	-0.82	-0.01
118	SLU 41	-1	-325	2974	16.57	-0.82	-0.01
118	SLU 42	-1	-325	2974	16.57	-0.82	-0.01
118	SLU 43	-1	-344	2827	17.05	-0.64	-0.01
118	SLU 44	-1	-344	2827	17.05	-0.64	-0.01
118	SLU 45	-1	-344	2827	17.05	-0.64	-0.01
118	SLU 46	-1	-344	2827	17.05	-0.64	-0.01
118	SLU 47	-1	-344	2827	17.05	-0.64	-0.01
118	SLU 48	-1	-344	2827	17.05	-0.64	-0.01
118	SLU 49	-1	-344	2827	17.05	-0.64	-0.01
118	SLU 50	-1	-344	2827	17.05	-0.64	-0.01
118	SLU 51	-1	-344	2827	17.05	-0.64	-0.01
118	SLU 52	-1	-369	3194	18.53	-0.8	-0.01
118	SLU 53	-1	-369	3194	18.53	-0.8	-0.01
118	SLU 54	-1	-369	3194	18.53	-0.8	-0.01
118	SLU 55	-1	-369	3194	18.53	-0.8	-0.01
118	SLU 56	-1	-369	3194	18.53	-0.8	-0.01
118	SLU 57	-1	-369	3194	18.53	-0.8	-0.01
118	SLU 58	-1	-369	3194	18.53	-0.8	-0.01
118	SLU 59	-1	-369	3194	18.53	-0.8	-0.01
118	SLU 60	-1	-380	3351	19.16	-0.86	-0.01
118	SLU 61	-1	-380	3351	19.16	-0.86	-0.01
118	SLU 62	-1	-380	3351	19.16	-0.86	-0.01
118	SLU 63	-1	-380	3351	19.16	-0.86	-0.01
118	SLU 64	-1	-363	3045	18.11	-0.72	-0.01
118	SLU 65	-1	-363	3045	18.11	-0.72	-0.01
118	SLU 66	-1	-363	3045	18.11	-0.72	-0.01
118	SLU 67	-1	-363	3045	18.11	-0.72	-0.01
118	SLU 68	-1	-363	3045	18.11	-0.72	-0.01
118	SLU 69	-1	-363	3045	18.11	-0.72	-0.01
118	SLU 70	-1	-363	3045	18.11	-0.72	-0.01
118	SLU 71	-1	-363	3045	18.11	-0.72	-0.01
118	SLU 72	-1	-363	3045	18.11	-0.72	-0.01
118	SLU 73	-1	-389	3412	19.59	-0.88	-0.01
118	SLU 74	-1	-389	3412	19.59	-0.88	-0.01
118	SLU 75	-1	-389	3412	19.59	-0.88	-0.01
118	SLU 76	-1	-389	3412	19.59	-0.88	-0.01
118	SLU 77	-1	-389	3412	19.59	-0.88	-0.01
118	SLU 78	-1	-389	3412	19.59	-0.88	-0.01
118	SLU 79	-1	-389	3412	19.59	-0.88	-0.01
118	SLU 80	-1	-389	3412	19.59	-0.88	-0.01
118	SLU 81	-1	-399	3569	20.23	-0.95	-0.01
118	SLU 82	-1	-399	3569	20.23	-0.95	-0.01
118	SLU 83	-1	-399	3569	20.23	-0.95	-0.01
118	SLU 84	-1	-399	3569	20.23	-0.95	-0.01
118	SLE RA 1	0	-275	2294	13.7	-0.54	0
118	SLE RA 2	0	-275	2294	13.7	-0.54	0
118	SLE RA 3	0	-275	2294	13.7	-0.54	0
118	SLE RA 4	0	-275	2294	13.7	-0.54	0
118	SLE RA 5	0	-275	2294	13.7	-0.54	0
118	SLE RA 6	0	-275	2294	13.7	-0.54	0
118	SLE RA 7	0	-275	2294	13.7	-0.54	0
118	SLE RA 8	0	-275	2294	13.7	-0.54	0
118	SLE RA 9	0	-275	2294	13.7	-0.54	0
118	SLE RA 10	0	-292	2539	14.69	-0.64	-0.01
118	SLE RA 11	0	-292	2539	14.69	-0.64	-0.01
118	SLE RA 12	0	-292	2539	14.69	-0.64	-0.01
118	SLE RA 13	0	-292	2539	14.69	-0.64	-0.01
118	SLE RA 14	0	-292	2539	14.69	-0.64	-0.01
118	SLE RA 15	0	-292	2539	14.69	-0.64	-0.01
118	SLE RA 16	0	-292	2539	14.69	-0.64	-0.01
118	SLE RA 17	0	-292	2539	14.69	-0.64	-0.01
118	SLE RA 18	0	-299	2644	15.11	-0.69	-0.01
118	SLE RA 19	0	-299	2644	15.11	-0.69	-0.01
118	SLE RA 20	0	-299	2644	15.11	-0.69	-0.01
118	SLE RA 21	0	-299	2644	15.11	-0.69	-0.01
118	SLE FR 1	0	-275	2294	13.7	-0.54	0
118	SLE FR 2	0	-275	2294	13.7	-0.54	0
118	SLE FR 3	0	-275	2294	13.7	-0.54	0
118	SLE FR 4	0	-282	2399	14.12	-0.58	-0.01
118	SLE FR 5	0	-282	2399	14.12	-0.58	-0.01
118	SLE FR 6	0	-287	2469	14.4	-0.61	-0.01
118	SLE QP 1	0	-275	2294	13.7	-0.54	0
118	SLE QP 2	0	-282	2399	14.12	-0.58	-0.01
118	SLD 1	3	-163	2122	8.41	6.97	0.01
118	SLD 2	3	-163	2122	8.41	6.97	0.01
118	SLD 3	15	-288	2216	14.62	14.3	0.01
118	SLD 4	15	-288	2216	14.62	14.3	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
118	SLD 5	-17	-57	2173	3	-9.45	0.01
118	SLD 6	-17	-57	2173	3	-9.45	0.01
118	SLD 7	22	-474	2487	23.68	15.01	-0.01
118	SLD 8	22	-474	2487	23.68	15.01	-0.01
118	SLD 9	-23	-91	2311	4.56	-16.18	0
118	SLD 10	-23	-91	2311	4.56	-16.18	0
118	SLD 11	16	-508	2625	25.25	8.28	-0.02
118	SLD 12	16	-508	2625	25.25	8.28	-0.02
118	SLD 13	-16	-277	2582	13.62	-15.47	-0.02
118	SLD 14	-16	-277	2582	13.62	-15.47	-0.02
118	SLD 15	-4	-402	2676	19.83	-8.13	-0.02
118	SLD 16	-4	-402	2676	19.83	-8.13	-0.02
118	SLV 1	7	1	1743	0.63	17.53	0.04
118	SLV 2	7	1	1743	0.63	17.53	0.04
118	SLV 3	38	-296	1972	15.39	36.6	0.03
118	SLV 4	38	-296	1972	15.39	36.6	0.03
118	SLV 5	-45	253	1855	-12.32	-24.08	0.02
118	SLV 6	-45	253	1855	-12.32	-24.08	0.02
118	SLV 7	58	-737	2618	36.89	39.5	-0.01
118	SLV 8	58	-737	2618	36.89	39.5	-0.01
118	SLV 9	-58	173	2180	-8.65	-40.66	0
118	SLV 10	-58	173	2180	-8.65	-40.66	0
118	SLV 11	44	-818	2943	40.56	22.91	-0.03
118	SLV 12	44	-818	2943	40.56	22.91	-0.03
118	SLV 13	-39	-269	2825	12.85	-37.76	-0.04
118	SLV 14	-39	-269	2825	12.85	-37.76	-0.04
118	SLV 15	-8	-566	3055	27.61	-18.69	-0.05
118	SLV 16	-8	-566	3055	27.61	-18.69	-0.05
119	SLU 1	0	0	1066	0	0	0
119	SLU 2	0	0	1066	0	0	0
119	SLU 3	0	0	1066	0	0	0
119	SLU 4	0	0	1066	0	0	0
119	SLU 5	0	0	1066	0	0	0
119	SLU 6	0	0	1066	0	0	0
119	SLU 7	0	0	1066	0	0	0
119	SLU 8	0	0	1066	0	0	0
119	SLU 9	0	0	1066	0	0	0
119	SLU 10	0	0	1279	0	0	0
119	SLU 11	0	0	1279	0	0	0
119	SLU 12	0	0	1279	0	0	0
119	SLU 13	0	0	1279	0	0	0
119	SLU 14	0	0	1279	0	0	0
119	SLU 15	0	0	1279	0	0	0
119	SLU 16	0	0	1279	0	0	0
119	SLU 17	0	0	1279	0	0	0
119	SLU 18	0	0	1370	0	0	0
119	SLU 19	0	0	1370	0	0	0
119	SLU 20	0	0	1370	0	0	0
119	SLU 21	0	0	1370	0	0	0
119	SLU 22	0	0	1194	0	0	0
119	SLU 23	0	0	1194	0	0	0
119	SLU 24	0	0	1194	0	0	0
119	SLU 25	0	0	1194	0	0	0
119	SLU 26	0	0	1194	0	0	0
119	SLU 27	0	0	1194	0	0	0
119	SLU 28	0	0	1194	0	0	0
119	SLU 29	0	0	1194	0	0	0
119	SLU 30	0	0	1194	0	0	0
119	SLU 31	0	0	1407	0	0	0
119	SLU 32	0	0	1407	0	0	0
119	SLU 33	0	0	1407	0	0	0
119	SLU 34	0	0	1407	0	0	0
119	SLU 35	0	0	1407	0	0	0
119	SLU 36	0	0	1407	0	0	0
119	SLU 37	0	0	1407	0	0	0
119	SLU 38	0	0	1407	0	0	0
119	SLU 39	0	0	1498	0	0	0
119	SLU 40	0	0	1498	0	0	0
119	SLU 41	0	0	1498	0	0	0
119	SLU 42	0	0	1498	0	0	0
119	SLU 43	0	0	1342	0	0	0
119	SLU 44	0	0	1342	0	0	0
119	SLU 45	0	0	1342	0	0	0
119	SLU 46	0	0	1342	0	0	0
119	SLU 47	0	0	1342	0	0	0
119	SLU 48	0	0	1342	0	0	0
119	SLU 49	0	0	1342	0	0	0
119	SLU 50	0	0	1342	0	0	0
119	SLU 51	0	0	1342	0	0	0
119	SLU 52	0	0	1555	0	0	0
119	SLU 53	0	0	1555	0	0	0
119	SLU 54	0	0	1555	0	0	0
119	SLU 55	0	0	1555	0	0	0
119	SLU 56	0	0	1555	0	0	0
119	SLU 57	0	0	1555	0	0	0
119	SLU 58	0	0	1555	0	0	0
119	SLU 59	0	0	1555	0	0	0
119	SLU 60	0	0	1646	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
119	SLU 61	0	0	1646	0	0	0
119	SLU 62	0	0	1646	0	0	0
119	SLU 63	0	0	1646	0	0	0
119	SLU 64	0	0	1470	0	0	0
119	SLU 65	0	0	1470	0	0	0
119	SLU 66	0	0	1470	0	0	0
119	SLU 67	0	0	1470	0	0	0
119	SLU 68	0	0	1470	0	0	0
119	SLU 69	0	0	1470	0	0	0
119	SLU 70	0	0	1470	0	0	0
119	SLU 71	0	0	1470	0	0	0
119	SLU 72	0	0	1470	0	0	0
119	SLU 73	0	0	1683	0	0	0
119	SLU 74	0	0	1683	0	0	0
119	SLU 75	0	0	1683	0	0	0
119	SLU 76	0	0	1683	0	0	0
119	SLU 77	0	0	1683	0	0	0
119	SLU 78	0	0	1683	0	0	0
119	SLU 79	0	0	1683	0	0	0
119	SLU 80	0	0	1683	0	0	0
119	SLU 81	0	0	1774	0	0	0
119	SLU 82	0	0	1774	0	0	0
119	SLU 83	0	0	1774	0	0	0
119	SLU 84	0	0	1774	0	0	0
119	SLE RA 1	0	0	1102	0	0	0
119	SLE RA 2	0	0	1102	0	0	0
119	SLE RA 3	0	0	1102	0	0	0
119	SLE RA 4	0	0	1102	0	0	0
119	SLE RA 5	0	0	1102	0	0	0
119	SLE RA 6	0	0	1102	0	0	0
119	SLE RA 7	0	0	1102	0	0	0
119	SLE RA 8	0	0	1102	0	0	0
119	SLE RA 9	0	0	1102	0	0	0
119	SLE RA 10	0	0	1245	0	0	0
119	SLE RA 11	0	0	1245	0	0	0
119	SLE RA 12	0	0	1245	0	0	0
119	SLE RA 13	0	0	1245	0	0	0
119	SLE RA 14	0	0	1245	0	0	0
119	SLE RA 15	0	0	1245	0	0	0
119	SLE RA 16	0	0	1245	0	0	0
119	SLE RA 17	0	0	1245	0	0	0
119	SLE RA 18	0	0	1305	0	0	0
119	SLE RA 19	0	0	1305	0	0	0
119	SLE RA 20	0	0	1305	0	0	0
119	SLE RA 21	0	0	1305	0	0	0
119	SLE FR 1	0	0	1102	0	0	0
119	SLE FR 2	0	0	1102	0	0	0
119	SLE FR 3	0	0	1102	0	0	0
119	SLE FR 4	0	0	1163	0	0	0
119	SLE FR 5	0	0	1163	0	0	0
119	SLE FR 6	0	0	1204	0	0	0
119	SLE QP 1	0	0	1102	0	0	0
119	SLE QP 2	0	0	1163	0	0	0
119	SLD 1	-1	0	1180	-0.06	2.39	0
119	SLD 2	-1	0	1180	-0.06	2.39	0
119	SLD 3	-2	-1	1149	0.06	2.29	0
119	SLD 4	-2	-1	1149	0.06	2.29	0
119	SLD 5	0	2	1215	-0.2	0.87	0
119	SLD 6	0	2	1215	-0.2	0.87	0
119	SLD 7	-1	-2	1112	0.21	0.53	0
119	SLD 8	-1	-2	1112	0.21	0.53	0
119	SLD 9	1	2	1214	-0.2	-0.53	0
119	SLD 10	1	2	1214	-0.2	-0.53	0
119	SLD 11	0	-2	1112	0.21	-0.87	0
119	SLD 12	0	-2	1112	0.21	-0.87	0
119	SLD 13	2	1	1178	-0.06	-2.29	0
119	SLD 14	2	1	1178	-0.06	-2.29	0
119	SLD 15	1	0	1147	0.06	-2.39	0
119	SLD 16	1	0	1147	0.06	-2.39	0
119	SLV 1	-4	1	1209	-0.17	6.11	0
119	SLV 2	-4	1	1209	-0.17	6.11	0
119	SLV 3	-4	-2	1122	0.18	5.83	0
119	SLV 4	-4	-2	1122	0.18	5.83	0
119	SLV 5	-1	5	1308	-0.58	2.24	0
119	SLV 6	-1	5	1308	-0.58	2.24	0
119	SLV 7	-2	-6	1020	0.58	1.34	0
119	SLV 8	-2	-6	1020	0.58	1.34	0
119	SLV 9	2	6	1307	-0.58	-1.34	0
119	SLV 10	2	6	1307	-0.58	-1.34	0
119	SLV 11	1	-5	1018	0.58	-2.24	0
119	SLV 12	1	-5	1018	0.58	-2.24	0
119	SLV 13	4	2	1204	-0.17	-5.83	0
119	SLV 14	4	2	1204	-0.17	-5.83	0
119	SLV 15	4	-1	1118	0.17	-6.11	0
119	SLV 16	4	-1	1118	0.17	-6.11	0
120	SLU 1	0	-224	1964	11.56	0.51	0
120	SLU 2	0	-224	1964	11.56	0.51	0
120	SLU 3	0	-224	1964	11.56	0.51	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
120	SLU 4	0	-224	1964	11.56	0.51	0
120	SLU 5	0	-224	1964	11.56	0.51	0
120	SLU 6	0	-224	1964	11.56	0.51	0
120	SLU 7	0	-224	1964	11.56	0.51	0
120	SLU 8	0	-224	1964	11.56	0.51	0
120	SLU 9	0	-224	1964	11.56	0.51	0
120	SLU 10	1	-233	2285	12.26	0.67	0
120	SLU 11	1	-233	2285	12.26	0.67	0
120	SLU 12	1	-233	2285	12.26	0.67	0
120	SLU 13	1	-233	2285	12.26	0.67	0
120	SLU 14	1	-233	2285	12.26	0.67	0
120	SLU 15	1	-233	2285	12.26	0.67	0
120	SLU 16	1	-233	2285	12.26	0.67	0
120	SLU 17	1	-233	2285	12.26	0.67	0
120	SLU 18	1	-236	2423	12.56	0.73	0
120	SLU 19	1	-236	2423	12.56	0.73	0
120	SLU 20	1	-236	2423	12.56	0.73	0
120	SLU 21	1	-236	2423	12.56	0.73	0
120	SLU 22	0	-234	2155	12.18	0.6	0
120	SLU 23	0	-234	2155	12.18	0.6	0
120	SLU 24	0	-234	2155	12.18	0.6	0
120	SLU 25	0	-234	2155	12.18	0.6	0
120	SLU 26	0	-234	2155	12.18	0.6	0
120	SLU 27	0	-234	2155	12.18	0.6	0
120	SLU 28	0	-234	2155	12.18	0.6	0
120	SLU 29	0	-234	2155	12.18	0.6	0
120	SLU 30	0	-234	2155	12.18	0.6	0
120	SLU 31	1	-242	2475	12.87	0.75	0.01
120	SLU 32	1	-242	2475	12.87	0.75	0.01
120	SLU 33	1	-242	2475	12.87	0.75	0.01
120	SLU 34	1	-242	2475	12.87	0.75	0.01
120	SLU 35	1	-242	2475	12.87	0.75	0.01
120	SLU 36	1	-242	2475	12.87	0.75	0.01
120	SLU 37	1	-242	2475	12.87	0.75	0.01
120	SLU 38	1	-242	2475	12.87	0.75	0.01
120	SLU 39	1	-246	2613	13.17	0.81	0.01
120	SLU 40	1	-246	2613	13.17	0.81	0.01
120	SLU 41	1	-246	2613	13.17	0.81	0.01
120	SLU 42	1	-246	2613	13.17	0.81	0.01
120	SLU 43	1	-288	2489	14.82	0.64	0
120	SLU 44	1	-288	2489	14.82	0.64	0
120	SLU 45	1	-288	2489	14.82	0.64	0
120	SLU 46	1	-288	2489	14.82	0.64	0
120	SLU 47	1	-288	2489	14.82	0.64	0
120	SLU 48	1	-288	2489	14.82	0.64	0
120	SLU 49	1	-288	2489	14.82	0.64	0
120	SLU 50	1	-288	2489	14.82	0.64	0
120	SLU 51	1	-288	2489	14.82	0.64	0
120	SLU 52	1	-297	2809	15.52	0.79	0.01
120	SLU 53	1	-297	2809	15.52	0.79	0.01
120	SLU 54	1	-297	2809	15.52	0.79	0.01
120	SLU 55	1	-297	2809	15.52	0.79	0.01
120	SLU 56	1	-297	2809	15.52	0.79	0.01
120	SLU 57	1	-297	2809	15.52	0.79	0.01
120	SLU 58	1	-297	2809	15.52	0.79	0.01
120	SLU 59	1	-297	2809	15.52	0.79	0.01
120	SLU 60	1	-300	2947	15.81	0.86	0.01
120	SLU 61	1	-300	2947	15.81	0.86	0.01
120	SLU 62	1	-300	2947	15.81	0.86	0.01
120	SLU 63	1	-300	2947	15.81	0.86	0.01
120	SLU 64	1	-298	2679	15.44	0.72	0
120	SLU 65	1	-298	2679	15.44	0.72	0
120	SLU 66	1	-298	2679	15.44	0.72	0
120	SLU 67	1	-298	2679	15.44	0.72	0
120	SLU 68	1	-298	2679	15.44	0.72	0
120	SLU 69	1	-298	2679	15.44	0.72	0
120	SLU 70	1	-298	2679	15.44	0.72	0
120	SLU 71	1	-298	2679	15.44	0.72	0
120	SLU 72	1	-298	2679	15.44	0.72	0
120	SLU 73	1	-306	3000	16.13	0.87	0.01
120	SLU 74	1	-306	3000	16.13	0.87	0.01
120	SLU 75	1	-306	3000	16.13	0.87	0.01
120	SLU 76	1	-306	3000	16.13	0.87	0.01
120	SLU 77	1	-306	3000	16.13	0.87	0.01
120	SLU 78	1	-306	3000	16.13	0.87	0.01
120	SLU 79	1	-306	3000	16.13	0.87	0.01
120	SLU 80	1	-306	3000	16.13	0.87	0.01
120	SLU 81	1	-310	3137	16.43	0.94	0.01
120	SLU 82	1	-310	3137	16.43	0.94	0.01
120	SLU 83	1	-310	3137	16.43	0.94	0.01
120	SLU 84	1	-310	3137	16.43	0.94	0.01
120	SLE RA 1	0	-227	2019	11.74	0.54	0
120	SLE RA 2	0	-227	2019	11.74	0.54	0
120	SLE RA 3	0	-227	2019	11.74	0.54	0
120	SLE RA 4	0	-227	2019	11.74	0.54	0
120	SLE RA 5	0	-227	2019	11.74	0.54	0
120	SLE RA 6	0	-227	2019	11.74	0.54	0
120	SLE RA 7	0	-227	2019	11.74	0.54	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
120	SLE RA 8	0	-227	2019	11.74	0.54	0
120	SLE RA 9	0	-227	2019	11.74	0.54	0
120	SLE RA 10	1	-233	2233	12.2	0.64	0
120	SLE RA 11	1	-233	2233	12.2	0.64	0
120	SLE RA 12	1	-233	2233	12.2	0.64	0
120	SLE RA 13	1	-233	2233	12.2	0.64	0
120	SLE RA 14	1	-233	2233	12.2	0.64	0
120	SLE RA 15	1	-233	2233	12.2	0.64	0
120	SLE RA 16	1	-233	2233	12.2	0.64	0
120	SLE RA 17	1	-233	2233	12.2	0.64	0
120	SLE RA 18	1	-235	2324	12.4	0.68	0
120	SLE RA 19	1	-235	2324	12.4	0.68	0
120	SLE RA 20	1	-235	2324	12.4	0.68	0
120	SLE RA 21	1	-235	2324	12.4	0.68	0
120	SLE FR 1	0	-227	2019	11.74	0.54	0
120	SLE FR 2	0	-227	2019	11.74	0.54	0
120	SLE FR 3	0	-227	2019	11.74	0.54	0
120	SLE FR 4	0	-229	2110	11.94	0.58	0
120	SLE FR 5	0	-229	2110	11.94	0.58	0
120	SLE FR 6	1	-231	2172	12.07	0.61	0
120	SLE QP 1	0	-227	2019	11.74	0.54	0
120	SLE QP 2	0	-229	2110	11.94	0.58	0
120	SLD 1	13	-132	2271	11.33	12.54	0.01
120	SLD 2	13	-132	2271	11.33	12.54	0.01
120	SLD 3	2	-235	2364	16.57	5.96	0.02
120	SLD 4	2	-235	2364	16.57	5.96	0.02
120	SLD 5	21	-44	2017	3.81	14.14	0
120	SLD 6	21	-44	2017	3.81	14.14	0
120	SLD 7	-15	-388	2328	21.28	-7.78	0.01
120	SLD 8	-15	-388	2328	21.28	-7.78	0.01
120	SLD 9	16	-71	1892	2.6	8.94	0
120	SLD 10	16	-71	1892	2.6	8.94	0
120	SLD 11	-20	-415	2204	20.07	-12.98	0
120	SLD 12	-20	-415	2204	20.07	-12.98	0
120	SLD 13	-1	-223	1857	7.31	-4.8	-0.01
120	SLD 14	-1	-223	1857	7.31	-4.8	-0.01
120	SLD 15	-12	-327	1950	12.55	-11.38	-0.01
120	SLD 16	-12	-327	1950	12.55	-11.38	-0.01
120	SLV 1	33	0	2484	10.47	30.27	0.03
120	SLV 2	33	0	2484	10.47	30.27	0.03
120	SLV 3	5	-244	2710	22.87	13.35	0.04
120	SLV 4	5	-244	2710	22.87	13.35	0.04
120	SLV 5	53	210	1880	-7.3	35.15	0
120	SLV 6	53	210	1880	-7.3	35.15	0
120	SLV 7	-41	-605	2633	34.02	-21.25	0.02
120	SLV 8	-41	-605	2633	34.02	-21.25	0.02
120	SLV 9	42	146	1588	-10.14	22.41	-0.02
120	SLV 10	42	146	1588	-10.14	22.41	-0.02
120	SLV 11	-52	-669	2341	31.18	-33.99	0.01
120	SLV 12	-52	-669	2341	31.18	-33.99	0.01
120	SLV 13	-4	-214	1511	1.01	-12.19	-0.03
120	SLV 14	-4	-214	1511	1.01	-12.19	-0.03
120	SLV 15	-32	-459	1737	13.4	-29.11	-0.02
120	SLV 16	-32	-459	1737	13.4	-29.11	-0.02
121	SLU 1	-3	-318	2448	18.26	-1.1	0.01
121	SLU 2	-3	-318	2448	18.26	-1.1	0.01
121	SLU 3	-3	-318	2448	18.26	-1.1	0.01
121	SLU 4	-3	-318	2448	18.26	-1.1	0.01
121	SLU 5	-3	-318	2448	18.26	-1.1	0.01
121	SLU 6	-3	-318	2448	18.26	-1.1	0.01
121	SLU 7	-3	-318	2448	18.26	-1.1	0.01
121	SLU 8	-3	-318	2448	18.26	-1.1	0.01
121	SLU 9	-3	-318	2448	18.26	-1.1	0.01
121	SLU 10	-4	-344	2898	20.4	-1.4	0.02
121	SLU 11	-4	-344	2898	20.4	-1.4	0.02
121	SLU 12	-4	-344	2898	20.4	-1.4	0.02
121	SLU 13	-4	-344	2898	20.4	-1.4	0.02
121	SLU 14	-4	-344	2898	20.4	-1.4	0.02
121	SLU 15	-4	-344	2898	20.4	-1.4	0.02
121	SLU 16	-4	-344	2898	20.4	-1.4	0.02
121	SLU 17	-4	-344	2898	20.4	-1.4	0.02
121	SLU 18	-4	-355	3091	21.32	-1.53	0.02
121	SLU 19	-4	-355	3091	21.32	-1.53	0.02
121	SLU 20	-4	-355	3091	21.32	-1.53	0.02
121	SLU 21	-4	-355	3091	21.32	-1.53	0.02
121	SLU 22	-4	-339	2710	19.72	-1.26	0.01
121	SLU 23	-4	-339	2710	19.72	-1.26	0.01
121	SLU 24	-4	-339	2710	19.72	-1.26	0.01
121	SLU 25	-4	-339	2710	19.72	-1.26	0.01
121	SLU 26	-4	-339	2710	19.72	-1.26	0.01
121	SLU 27	-4	-339	2710	19.72	-1.26	0.01
121	SLU 28	-4	-339	2710	19.72	-1.26	0.01
121	SLU 29	-4	-339	2710	19.72	-1.26	0.01
121	SLU 30	-4	-339	2710	19.72	-1.26	0.01
121	SLU 31	-4	-365	3160	21.87	-1.57	0.02
121	SLU 32	-4	-365	3160	21.87	-1.57	0.02
121	SLU 33	-4	-365	3160	21.87	-1.57	0.02
121	SLU 34	-4	-365	3160	21.87	-1.57	0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
121	SLU 35	-4	-365	3160	21.87	-1.57	0.02
121	SLU 36	-4	-365	3160	21.87	-1.57	0.02
121	SLU 37	-4	-365	3160	21.87	-1.57	0.02
121	SLU 38	-4	-365	3160	21.87	-1.57	0.02
121	SLU 39	-5	-376	3352	22.79	-1.7	0.02
121	SLU 40	-5	-376	3352	22.79	-1.7	0.02
121	SLU 41	-5	-376	3352	22.79	-1.7	0.02
121	SLU 42	-5	-376	3352	22.79	-1.7	0.02
121	SLU 43	-4	-407	3092	23.23	-1.37	0.02
121	SLU 44	-4	-407	3092	23.23	-1.37	0.02
121	SLU 45	-4	-407	3092	23.23	-1.37	0.02
121	SLU 46	-4	-407	3092	23.23	-1.37	0.02
121	SLU 47	-4	-407	3092	23.23	-1.37	0.02
121	SLU 48	-4	-407	3092	23.23	-1.37	0.02
121	SLU 49	-4	-407	3092	23.23	-1.37	0.02
121	SLU 50	-4	-407	3092	23.23	-1.37	0.02
121	SLU 51	-4	-407	3092	23.23	-1.37	0.02
121	SLU 52	-5	-433	3542	25.37	-1.67	0.02
121	SLU 53	-5	-433	3542	25.37	-1.67	0.02
121	SLU 54	-5	-433	3542	25.37	-1.67	0.02
121	SLU 55	-5	-433	3542	25.37	-1.67	0.02
121	SLU 56	-5	-433	3542	25.37	-1.67	0.02
121	SLU 57	-5	-433	3542	25.37	-1.67	0.02
121	SLU 58	-5	-433	3542	25.37	-1.67	0.02
121	SLU 59	-5	-433	3542	25.37	-1.67	0.02
121	SLU 60	-5	-444	3735	26.29	-1.81	0.02
121	SLU 61	-5	-444	3735	26.29	-1.81	0.02
121	SLU 62	-5	-444	3735	26.29	-1.81	0.02
121	SLU 63	-5	-444	3735	26.29	-1.81	0.02
121	SLU 64	-4	-427	3354	24.7	-1.53	0.02
121	SLU 65	-4	-427	3354	24.7	-1.53	0.02
121	SLU 66	-4	-427	3354	24.7	-1.53	0.02
121	SLU 67	-4	-427	3354	24.7	-1.53	0.02
121	SLU 68	-4	-427	3354	24.7	-1.53	0.02
121	SLU 69	-4	-427	3354	24.7	-1.53	0.02
121	SLU 70	-4	-427	3354	24.7	-1.53	0.02
121	SLU 71	-4	-427	3354	24.7	-1.53	0.02
121	SLU 72	-4	-427	3354	24.7	-1.53	0.02
121	SLU 73	-5	-453	3804	26.84	-1.84	0.02
121	SLU 74	-5	-453	3804	26.84	-1.84	0.02
121	SLU 75	-5	-453	3804	26.84	-1.84	0.02
121	SLU 76	-5	-453	3804	26.84	-1.84	0.02
121	SLU 77	-5	-453	3804	26.84	-1.84	0.02
121	SLU 78	-5	-453	3804	26.84	-1.84	0.02
121	SLU 79	-5	-453	3804	26.84	-1.84	0.02
121	SLU 80	-5	-453	3804	26.84	-1.84	0.02
121	SLU 81	-5	-464	3997	27.76	-1.97	0.02
121	SLU 82	-5	-464	3997	27.76	-1.97	0.02
121	SLU 83	-5	-464	3997	27.76	-1.97	0.02
121	SLU 84	-5	-464	3997	27.76	-1.97	0.02
121	SLE RA 1	-3	-324	2522	18.68	-1.14	0.01
121	SLE RA 2	-3	-324	2522	18.68	-1.14	0.01
121	SLE RA 3	-3	-324	2522	18.68	-1.14	0.01
121	SLE RA 4	-3	-324	2522	18.68	-1.14	0.01
121	SLE RA 5	-3	-324	2522	18.68	-1.14	0.01
121	SLE RA 6	-3	-324	2522	18.68	-1.14	0.01
121	SLE RA 7	-3	-324	2522	18.68	-1.14	0.01
121	SLE RA 8	-3	-324	2522	18.68	-1.14	0.01
121	SLE RA 9	-3	-324	2522	18.68	-1.14	0.01
121	SLE RA 10	-4	-341	2823	20.1	-1.35	0.01
121	SLE RA 11	-4	-341	2823	20.1	-1.35	0.01
121	SLE RA 12	-4	-341	2823	20.1	-1.35	0.01
121	SLE RA 13	-4	-341	2823	20.1	-1.35	0.01
121	SLE RA 14	-4	-341	2823	20.1	-1.35	0.01
121	SLE RA 15	-4	-341	2823	20.1	-1.35	0.01
121	SLE RA 16	-4	-341	2823	20.1	-1.35	0.01
121	SLE RA 17	-4	-341	2823	20.1	-1.35	0.01
121	SLE RA 18	-4	-349	2951	20.72	-1.44	0.02
121	SLE RA 19	-4	-349	2951	20.72	-1.44	0.02
121	SLE RA 20	-4	-349	2951	20.72	-1.44	0.02
121	SLE RA 21	-4	-349	2951	20.72	-1.44	0.02
121	SLE FR 1	-3	-324	2522	18.68	-1.14	0.01
121	SLE FR 2	-3	-324	2522	18.68	-1.14	0.01
121	SLE FR 3	-3	-324	2522	18.68	-1.14	0.01
121	SLE FR 4	-3	-332	2651	19.29	-1.23	0.01
121	SLE FR 5	-3	-332	2651	19.29	-1.23	0.01
121	SLE FR 6	-4	-336	2737	19.7	-1.29	0.01
121	SLE QP 1	-3	-324	2522	18.68	-1.14	0.01
121	SLE QP 2	-3	-332	2651	19.29	-1.23	0.01
121	SLD 1	-2	-207	2259	13.16	1.9	0
121	SLD 2	-2	-207	2259	13.16	1.9	0
121	SLD 3	7	-325	2417	19.45	6.28	0.01
121	SLD 4	7	-325	2417	19.45	6.28	0.01
121	SLD 5	-15	-116	2294	7.9	-6.94	-0.01
121	SLD 6	-15	-116	2294	7.9	-6.94	-0.01
121	SLD 7	12	-508	2820	28.88	7.67	0.03
121	SLD 8	12	-508	2820	28.88	7.67	0.03
121	SLD 9	-19	-155	2482	9.69	-10.13	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
121	SLD 10	-19	-155	2482	9.69	-10.13	-0.01
121	SLD 11	8	-547	3008	30.67	4.48	0.04
121	SLD 12	8	-547	3008	30.67	4.48	0.04
121	SLD 13	-13	-338	2885	19.12	-8.74	0.02
121	SLD 14	-13	-338	2885	19.12	-8.74	0.02
121	SLD 15	-5	-456	3043	25.42	-4.36	0.03
121	SLD 16	-5	-456	3043	25.42	-4.36	0.03
121	SLV 1	1	-37	1724	4.8	6.26	-0.03
121	SLV 2	1	-37	1724	4.8	6.26	-0.03
121	SLV 3	22	-317	2105	19.78	17.67	0.01
121	SLV 4	22	-317	2105	19.78	17.67	0.01
121	SLV 5	-34	181	1794	-7.78	-16.29	-0.06
121	SLV 6	-34	181	1794	-7.78	-16.29	-0.06
121	SLV 7	36	-751	3067	42.15	21.74	0.07
121	SLV 8	36	-751	3067	42.15	21.74	0.07
121	SLV 9	-43	88	2236	-3.58	-24.21	-0.04
121	SLV 10	-43	88	2236	-3.58	-24.21	-0.04
121	SLV 11	27	-844	3509	46.35	13.83	0.08
121	SLV 12	27	-844	3509	46.35	13.83	0.08
121	SLV 13	-29	-346	3197	18.8	-20.13	0.02
121	SLV 14	-29	-346	3197	18.8	-20.13	0.02
121	SLV 15	-8	-626	3579	33.78	-8.72	0.05
121	SLV 16	-8	-626	3579	33.78	-8.72	0.05
122	SLU 1	0	0	1046	0	0	0
122	SLU 2	0	0	1046	0	0	0
122	SLU 3	0	0	1046	0	0	0
122	SLU 4	0	0	1046	0	0	0
122	SLU 5	0	0	1046	0	0	0
122	SLU 6	0	0	1046	0	0	0
122	SLU 7	0	0	1046	0	0	0
122	SLU 8	0	0	1046	0	0	0
122	SLU 9	0	0	1046	0	0	0
122	SLU 10	0	0	1270	0	0	0
122	SLU 11	0	0	1270	0	0	0
122	SLU 12	0	0	1270	0	0	0
122	SLU 13	0	0	1270	0	0	0
122	SLU 14	0	0	1270	0	0	0
122	SLU 15	0	0	1270	0	0	0
122	SLU 16	0	0	1270	0	0	0
122	SLU 17	0	0	1270	0	0	0
122	SLU 18	0	0	1366	0	0	0
122	SLU 19	0	0	1366	0	0	0
122	SLU 20	0	0	1366	0	0	0
122	SLU 21	0	0	1366	0	0	0
122	SLU 22	0	0	1178	0	0	0
122	SLU 23	0	0	1178	0	0	0
122	SLU 24	0	0	1178	0	0	0
122	SLU 25	0	0	1178	0	0	0
122	SLU 26	0	0	1178	0	0	0
122	SLU 27	0	0	1178	0	0	0
122	SLU 28	0	0	1178	0	0	0
122	SLU 29	0	0	1178	0	0	0
122	SLU 30	0	0	1178	0	0	0
122	SLU 31	0	0	1402	0	0	0
122	SLU 32	0	0	1402	0	0	0
122	SLU 33	0	0	1402	0	0	0
122	SLU 34	0	0	1402	0	0	0
122	SLU 35	0	0	1402	0	0	0
122	SLU 36	0	0	1402	0	0	0
122	SLU 37	0	0	1402	0	0	0
122	SLU 38	0	0	1402	0	0	0
122	SLU 39	0	0	1498	0	0	0
122	SLU 40	0	0	1498	0	0	0
122	SLU 41	0	0	1498	0	0	0
122	SLU 42	0	0	1498	0	0	0
122	SLU 43	0	0	1315	0	0	0
122	SLU 44	0	0	1315	0	0	0
122	SLU 45	0	0	1315	0	0	0
122	SLU 46	0	0	1315	0	0	0
122	SLU 47	0	0	1315	0	0	0
122	SLU 48	0	0	1315	0	0	0
122	SLU 49	0	0	1315	0	0	0
122	SLU 50	0	0	1315	0	0	0
122	SLU 51	0	0	1315	0	0	0
122	SLU 52	0	0	1539	0	0	0
122	SLU 53	0	0	1539	0	0	0
122	SLU 54	0	0	1539	0	0	0
122	SLU 55	0	0	1539	0	0	0
122	SLU 56	0	0	1539	0	0	0
122	SLU 57	0	0	1539	0	0	0
122	SLU 58	0	0	1539	0	0	0
122	SLU 59	0	0	1539	0	0	0
122	SLU 60	0	0	1635	0	0	0
122	SLU 61	0	0	1635	0	0	0
122	SLU 62	0	0	1635	0	0	0
122	SLU 63	0	0	1635	0	0	0
122	SLU 64	0	0	1447	0	0	0
122	SLU 65	0	0	1447	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
122	SLU 66	0	0	1447	0	0	0
122	SLU 67	0	0	1447	0	0	0
122	SLU 68	0	0	1447	0	0	0
122	SLU 69	0	0	1447	0	0	0
122	SLU 70	0	0	1447	0	0	0
122	SLU 71	0	0	1447	0	0	0
122	SLU 72	0	0	1447	0	0	0
122	SLU 73	0	0	1671	0	0	0
122	SLU 74	0	0	1671	0	0	0
122	SLU 75	0	0	1671	0	0	0
122	SLU 76	0	0	1671	0	0	0
122	SLU 77	0	0	1671	0	0	0
122	SLU 78	0	0	1671	0	0	0
122	SLU 79	0	0	1671	0	0	0
122	SLU 80	0	0	1671	0	0	0
122	SLU 81	0	0	1767	0	0	0
122	SLU 82	0	0	1767	0	0	0
122	SLU 83	0	0	1767	0	0	0
122	SLU 84	0	0	1767	0	0	0
122	SLE RA 1	0	0	1084	0	0	0
122	SLE RA 2	0	0	1084	0	0	0
122	SLE RA 3	0	0	1084	0	0	0
122	SLE RA 4	0	0	1084	0	0	0
122	SLE RA 5	0	0	1084	0	0	0
122	SLE RA 6	0	0	1084	0	0	0
122	SLE RA 7	0	0	1084	0	0	0
122	SLE RA 8	0	0	1084	0	0	0
122	SLE RA 9	0	0	1084	0	0	0
122	SLE RA 10	0	0	1233	0	0	0
122	SLE RA 11	0	0	1233	0	0	0
122	SLE RA 12	0	0	1233	0	0	0
122	SLE RA 13	0	0	1233	0	0	0
122	SLE RA 14	0	0	1233	0	0	0
122	SLE RA 15	0	0	1233	0	0	0
122	SLE RA 16	0	0	1233	0	0	0
122	SLE RA 17	0	0	1233	0	0	0
122	SLE RA 18	0	0	1297	0	0	0
122	SLE RA 19	0	0	1297	0	0	0
122	SLE RA 20	0	0	1297	0	0	0
122	SLE RA 21	0	0	1297	0	0	0
122	SLE FR 1	0	0	1084	0	0	0
122	SLE FR 2	0	0	1084	0	0	0
122	SLE FR 3	0	0	1084	0	0	0
122	SLE FR 4	0	0	1148	0	0	0
122	SLE FR 5	0	0	1148	0	0	0
122	SLE FR 6	0	0	1191	0	0	0
122	SLE QP 1	0	0	1084	0	0	0
122	SLE QP 2	0	0	1148	0	0	0
122	SLD 1	1	0	1195	0.18	0.93	0
122	SLD 2	1	0	1195	0.18	0.93	0
122	SLD 3	1	-1	1103	-0.19	0.88	0
122	SLD 4	1	-1	1103	-0.19	0.88	0
122	SLD 5	0	2	1301	0.62	0.36	0
122	SLD 6	0	2	1301	0.62	0.36	0
122	SLD 7	0	-2	996	-0.63	0.19	0
122	SLD 8	0	-2	996	-0.63	0.19	0
122	SLD 9	0	2	1300	0.62	-0.19	0
122	SLD 10	0	2	1300	0.62	-0.19	0
122	SLD 11	0	-2	995	-0.62	-0.36	0
122	SLD 12	0	-2	995	-0.62	-0.36	0
122	SLD 13	-1	1	1193	0.19	-0.88	0
122	SLD 14	-1	1	1193	0.19	-0.88	0
122	SLD 15	-1	0	1101	-0.19	-0.93	0
122	SLD 16	-1	0	1101	-0.19	-0.93	0
122	SLV 1	2	1	1280	0.52	2.38	0
122	SLV 2	2	1	1280	0.52	2.38	0
122	SLV 3	2	-2	1021	-0.53	2.25	0
122	SLV 4	2	-2	1021	-0.53	2.25	0
122	SLV 5	1	6	1579	1.76	0.92	0
122	SLV 6	1	6	1579	1.76	0.92	0
122	SLV 7	0	-7	718	-1.76	0.47	0
122	SLV 8	0	-7	718	-1.76	0.47	0
122	SLV 9	0	7	1578	1.76	-0.47	0
122	SLV 10	0	7	1578	1.76	-0.47	0
122	SLV 11	-1	-6	717	-1.76	-0.92	0
122	SLV 12	-1	-6	717	-1.76	-0.92	0
122	SLV 13	-2	2	1274	0.53	-2.25	0
122	SLV 14	-2	2	1274	0.53	-2.25	0
122	SLV 15	-2	-1	1016	-0.52	-2.38	0
122	SLV 16	-2	-1	1016	-0.52	-2.38	0
123	SLU 1	3	-260	2175	15.64	1.04	-0.01
123	SLU 2	3	-260	2175	15.64	1.04	-0.01
123	SLU 3	3	-260	2175	15.64	1.04	-0.01
123	SLU 4	3	-260	2175	15.64	1.04	-0.01
123	SLU 5	3	-260	2175	15.64	1.04	-0.01
123	SLU 6	3	-260	2175	15.64	1.04	-0.01
123	SLU 7	3	-260	2175	15.64	1.04	-0.01
123	SLU 8	3	-260	2175	15.64	1.04	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
123	SLU 9	3	-260	2175	15.64	1.04	-0.01
123	SLU 10	4	-269	2568	16.85	1.33	-0.01
123	SLU 11	4	-269	2568	16.85	1.33	-0.01
123	SLU 12	4	-269	2568	16.85	1.33	-0.01
123	SLU 13	4	-269	2568	16.85	1.33	-0.01
123	SLU 14	4	-269	2568	16.85	1.33	-0.01
123	SLU 15	4	-269	2568	16.85	1.33	-0.01
123	SLU 16	4	-269	2568	16.85	1.33	-0.01
123	SLU 17	4	-269	2568	16.85	1.33	-0.01
123	SLU 18	4	-272	2737	17.37	1.45	-0.01
123	SLU 19	4	-272	2737	17.37	1.45	-0.01
123	SLU 20	4	-272	2737	17.37	1.45	-0.01
123	SLU 21	4	-272	2737	17.37	1.45	-0.01
123	SLU 22	4	-270	2404	16.57	1.2	-0.01
123	SLU 23	4	-270	2404	16.57	1.2	-0.01
123	SLU 24	4	-270	2404	16.57	1.2	-0.01
123	SLU 25	4	-270	2404	16.57	1.2	-0.01
123	SLU 26	4	-270	2404	16.57	1.2	-0.01
123	SLU 27	4	-270	2404	16.57	1.2	-0.01
123	SLU 28	4	-270	2404	16.57	1.2	-0.01
123	SLU 29	4	-270	2404	16.57	1.2	-0.01
123	SLU 30	4	-270	2404	16.57	1.2	-0.01
123	SLU 31	4	-279	2797	17.78	1.49	-0.01
123	SLU 32	4	-279	2797	17.78	1.49	-0.01
123	SLU 33	4	-279	2797	17.78	1.49	-0.01
123	SLU 34	4	-279	2797	17.78	1.49	-0.01
123	SLU 35	4	-279	2797	17.78	1.49	-0.01
123	SLU 36	4	-279	2797	17.78	1.49	-0.01
123	SLU 37	4	-279	2797	17.78	1.49	-0.01
123	SLU 38	4	-279	2797	17.78	1.49	-0.01
123	SLU 39	5	-282	2966	18.29	1.61	-0.02
123	SLU 40	5	-282	2966	18.29	1.61	-0.02
123	SLU 41	5	-282	2966	18.29	1.61	-0.02
123	SLU 42	5	-282	2966	18.29	1.61	-0.02
123	SLU 43	4	-335	2749	20.01	1.29	-0.01
123	SLU 44	4	-335	2749	20.01	1.29	-0.01
123	SLU 45	4	-335	2749	20.01	1.29	-0.01
123	SLU 46	4	-335	2749	20.01	1.29	-0.01
123	SLU 47	4	-335	2749	20.01	1.29	-0.01
123	SLU 48	4	-335	2749	20.01	1.29	-0.01
123	SLU 49	4	-335	2749	20.01	1.29	-0.01
123	SLU 50	4	-335	2749	20.01	1.29	-0.01
123	SLU 51	4	-335	2749	20.01	1.29	-0.01
123	SLU 52	5	-343	3142	21.22	1.58	-0.02
123	SLU 53	5	-343	3142	21.22	1.58	-0.02
123	SLU 54	5	-343	3142	21.22	1.58	-0.02
123	SLU 55	5	-343	3142	21.22	1.58	-0.02
123	SLU 56	5	-343	3142	21.22	1.58	-0.02
123	SLU 57	5	-343	3142	21.22	1.58	-0.02
123	SLU 58	5	-343	3142	21.22	1.58	-0.02
123	SLU 59	5	-343	3142	21.22	1.58	-0.02
123	SLU 60	5	-347	3311	21.74	1.71	-0.02
123	SLU 61	5	-347	3311	21.74	1.71	-0.02
123	SLU 62	5	-347	3311	21.74	1.71	-0.02
123	SLU 63	5	-347	3311	21.74	1.71	-0.02
123	SLU 64	4	-345	2978	20.94	1.45	-0.02
123	SLU 65	4	-345	2978	20.94	1.45	-0.02
123	SLU 66	4	-345	2978	20.94	1.45	-0.02
123	SLU 67	4	-345	2978	20.94	1.45	-0.02
123	SLU 68	4	-345	2978	20.94	1.45	-0.02
123	SLU 69	4	-345	2978	20.94	1.45	-0.02
123	SLU 70	4	-345	2978	20.94	1.45	-0.02
123	SLU 71	4	-345	2978	20.94	1.45	-0.02
123	SLU 72	4	-345	2978	20.94	1.45	-0.02
123	SLU 73	5	-353	3371	22.15	1.74	-0.02
123	SLU 74	5	-353	3371	22.15	1.74	-0.02
123	SLU 75	5	-353	3371	22.15	1.74	-0.02
123	SLU 76	5	-353	3371	22.15	1.74	-0.02
123	SLU 77	5	-353	3371	22.15	1.74	-0.02
123	SLU 78	5	-353	3371	22.15	1.74	-0.02
123	SLU 79	5	-353	3371	22.15	1.74	-0.02
123	SLU 80	5	-353	3371	22.15	1.74	-0.02
123	SLU 81	5	-357	3540	22.67	1.87	-0.02
123	SLU 82	5	-357	3540	22.67	1.87	-0.02
123	SLU 83	5	-357	3540	22.67	1.87	-0.02
123	SLU 84	5	-357	3540	22.67	1.87	-0.02
123	SLE RA 1	3	-263	2240	15.9	1.08	-0.01
123	SLE RA 2	3	-263	2240	15.9	1.08	-0.01
123	SLE RA 3	3	-263	2240	15.9	1.08	-0.01
123	SLE RA 4	3	-263	2240	15.9	1.08	-0.01
123	SLE RA 5	3	-263	2240	15.9	1.08	-0.01
123	SLE RA 6	3	-263	2240	15.9	1.08	-0.01
123	SLE RA 7	3	-263	2240	15.9	1.08	-0.01
123	SLE RA 8	3	-263	2240	15.9	1.08	-0.01
123	SLE RA 9	3	-263	2240	15.9	1.08	-0.01
123	SLE RA 10	4	-269	2503	16.71	1.28	-0.01
123	SLE RA 11	4	-269	2503	16.71	1.28	-0.01
123	SLE RA 12	4	-269	2503	16.71	1.28	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
123	SLE RA 13	4	-269	2503	16.71	1.28	-0.01
123	SLE RA 14	4	-269	2503	16.71	1.28	-0.01
123	SLE RA 15	4	-269	2503	16.71	1.28	-0.01
123	SLE RA 16	4	-269	2503	16.71	1.28	-0.01
123	SLE RA 17	4	-269	2503	16.71	1.28	-0.01
123	SLE RA 18	4	-271	2615	17.06	1.36	-0.01
123	SLE RA 19	4	-271	2615	17.06	1.36	-0.01
123	SLE RA 20	4	-271	2615	17.06	1.36	-0.01
123	SLE RA 21	4	-271	2615	17.06	1.36	-0.01
123	SLE FR 1	3	-263	2240	15.9	1.08	-0.01
123	SLE FR 2	3	-263	2240	15.9	1.08	-0.01
123	SLE FR 3	3	-263	2240	15.9	1.08	-0.01
123	SLE FR 4	3	-265	2353	16.25	1.17	-0.01
123	SLE FR 5	3	-265	2353	16.25	1.17	-0.01
123	SLE FR 6	4	-267	2428	16.48	1.22	-0.01
123	SLE QP 1	3	-263	2240	15.9	1.08	-0.01
123	SLE QP 2	3	-265	2353	16.25	1.17	-0.01
123	SLD 1	12	-162	2561	15.89	7.21	-0.01
123	SLD 2	12	-162	2561	15.89	7.21	-0.01
123	SLD 3	5	-259	2704	21.2	3.36	-0.03
123	SLD 4	5	-259	2704	21.2	3.36	-0.03
123	SLD 5	17	-88	2197	8.09	8.82	0.01
123	SLD 6	17	-88	2197	8.09	8.82	0.01
123	SLD 7	-7	-411	2676	25.79	-4.01	-0.03
123	SLD 8	-7	-411	2676	25.79	-4.01	-0.03
123	SLD 9	14	-120	2029	6.71	6.34	0.01
123	SLD 10	14	-120	2029	6.71	6.34	0.01
123	SLD 11	-10	-443	2508	24.41	-6.49	-0.03
123	SLD 12	-10	-443	2508	24.41	-6.49	-0.03
123	SLD 13	2	-272	2001	11.3	-1.03	0
123	SLD 14	2	-272	2001	11.3	-1.03	0
123	SLD 15	-5	-369	2145	16.61	-4.88	-0.01
123	SLD 16	-5	-369	2145	16.61	-4.88	-0.01
123	SLV 1	24	-22	2838	15.35	16.29	-0.01
123	SLV 2	24	-22	2838	15.35	16.29	-0.01
123	SLV 3	6	-251	3184	27.95	6.37	-0.05
123	SLV 4	6	-251	3184	27.95	6.37	-0.05
123	SLV 5	38	156	1974	-3.14	20.74	0.04
123	SLV 6	38	156	1974	-3.14	20.74	0.04
123	SLV 7	-24	-609	3126	38.88	-12.32	-0.07
123	SLV 8	-24	-609	3126	38.88	-12.32	-0.07
123	SLV 9	31	78	1579	-6.38	14.65	0.05
123	SLV 10	31	78	1579	-6.38	14.65	0.05
123	SLV 11	-31	-687	2732	35.64	-18.41	-0.06
123	SLV 12	-31	-687	2732	35.64	-18.41	-0.06
123	SLV 13	1	-280	1522	4.54	-4.04	0.02
123	SLV 14	1	-280	1522	4.54	-4.04	0.02
123	SLV 15	-18	-509	1867	17.15	-13.95	-0.01
123	SLV 16	-18	-509	1867	17.15	-13.95	-0.01
124	SLU 1	-456	-419	3031	12.38	-14.05	-0.02
124	SLU 2	-456	-419	3031	12.38	-14.05	-0.02
124	SLU 3	-456	-419	3031	12.38	-14.05	-0.02
124	SLU 4	-456	-419	3031	12.38	-14.05	-0.02
124	SLU 5	-456	-419	3031	12.38	-14.05	-0.02
124	SLU 6	-456	-419	3031	12.38	-14.05	-0.02
124	SLU 7	-456	-419	3031	12.38	-14.05	-0.02
124	SLU 8	-456	-419	3031	12.38	-14.05	-0.02
124	SLU 9	-456	-419	3031	12.38	-14.05	-0.02
124	SLU 10	-576	-484	3646	14.01	-18.27	-0.04
124	SLU 11	-576	-484	3646	14.01	-18.27	-0.04
124	SLU 12	-576	-484	3646	14.01	-18.27	-0.04
124	SLU 13	-576	-484	3646	14.01	-18.27	-0.04
124	SLU 14	-576	-484	3646	14.01	-18.27	-0.04
124	SLU 15	-576	-484	3646	14.01	-18.27	-0.04
124	SLU 16	-576	-484	3646	14.01	-18.27	-0.04
124	SLU 17	-576	-484	3646	14.01	-18.27	-0.04
124	SLU 18	-628	-511	3910	14.7	-20.09	-0.05
124	SLU 19	-628	-511	3910	14.7	-20.09	-0.05
124	SLU 20	-628	-511	3910	14.7	-20.09	-0.05
124	SLU 21	-628	-511	3910	14.7	-20.09	-0.05
124	SLU 22	-522	-459	3384	13.44	-16.33	-0.03
124	SLU 23	-522	-459	3384	13.44	-16.33	-0.03
124	SLU 24	-522	-459	3384	13.44	-16.33	-0.03
124	SLU 25	-522	-459	3384	13.44	-16.33	-0.03
124	SLU 26	-522	-459	3384	13.44	-16.33	-0.03
124	SLU 27	-522	-459	3384	13.44	-16.33	-0.03
124	SLU 28	-522	-459	3384	13.44	-16.33	-0.03
124	SLU 29	-522	-459	3384	13.44	-16.33	-0.03
124	SLU 30	-522	-459	3384	13.44	-16.33	-0.03
124	SLU 31	-643	-523	3999	15.06	-20.56	-0.05
124	SLU 32	-643	-523	3999	15.06	-20.56	-0.05
124	SLU 33	-643	-523	3999	15.06	-20.56	-0.05
124	SLU 34	-643	-523	3999	15.06	-20.56	-0.05
124	SLU 35	-643	-523	3999	15.06	-20.56	-0.05
124	SLU 36	-643	-523	3999	15.06	-20.56	-0.05
124	SLU 37	-643	-523	3999	15.06	-20.56	-0.05
124	SLU 38	-643	-523	3999	15.06	-20.56	-0.05
124	SLU 39	-694	-551	4263	15.76	-22.37	-0.06



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
124	SLU 40	-694	-551	4263	15.76	-22.37	-0.06
124	SLU 41	-694	-551	4263	15.76	-22.37	-0.06
124	SLU 42	-694	-551	4263	15.76	-22.37	-0.06
124	SLU 43	-571	-531	3820	15.74	-17.48	-0.02
124	SLU 44	-571	-531	3820	15.74	-17.48	-0.02
124	SLU 45	-571	-531	3820	15.74	-17.48	-0.02
124	SLU 46	-571	-531	3820	15.74	-17.48	-0.02
124	SLU 47	-571	-531	3820	15.74	-17.48	-0.02
124	SLU 48	-571	-531	3820	15.74	-17.48	-0.02
124	SLU 49	-571	-531	3820	15.74	-17.48	-0.02
124	SLU 50	-571	-531	3820	15.74	-17.48	-0.02
124	SLU 51	-571	-531	3820	15.74	-17.48	-0.02
124	SLU 52	-691	-596	4435	17.36	-21.7	-0.05
124	SLU 53	-691	-596	4435	17.36	-21.7	-0.05
124	SLU 54	-691	-596	4435	17.36	-21.7	-0.05
124	SLU 55	-691	-596	4435	17.36	-21.7	-0.05
124	SLU 56	-691	-596	4435	17.36	-21.7	-0.05
124	SLU 57	-691	-596	4435	17.36	-21.7	-0.05
124	SLU 58	-691	-596	4435	17.36	-21.7	-0.05
124	SLU 59	-691	-596	4435	17.36	-21.7	-0.05
124	SLU 60	-742	-623	4699	18.06	-23.52	-0.05
124	SLU 61	-742	-623	4699	18.06	-23.52	-0.05
124	SLU 62	-742	-623	4699	18.06	-23.52	-0.05
124	SLU 63	-742	-623	4699	18.06	-23.52	-0.05
124	SLU 64	-637	-571	4172	16.79	-19.76	-0.03
124	SLU 65	-637	-571	4172	16.79	-19.76	-0.03
124	SLU 66	-637	-571	4172	16.79	-19.76	-0.03
124	SLU 67	-637	-571	4172	16.79	-19.76	-0.03
124	SLU 68	-637	-571	4172	16.79	-19.76	-0.03
124	SLU 69	-637	-571	4172	16.79	-19.76	-0.03
124	SLU 70	-637	-571	4172	16.79	-19.76	-0.03
124	SLU 71	-637	-571	4172	16.79	-19.76	-0.03
124	SLU 72	-637	-571	4172	16.79	-19.76	-0.03
124	SLU 73	-757	-635	4788	18.42	-23.99	-0.06
124	SLU 74	-757	-635	4788	18.42	-23.99	-0.06
124	SLU 75	-757	-635	4788	18.42	-23.99	-0.06
124	SLU 76	-757	-635	4788	18.42	-23.99	-0.06
124	SLU 77	-757	-635	4788	18.42	-23.99	-0.06
124	SLU 78	-757	-635	4788	18.42	-23.99	-0.06
124	SLU 79	-757	-635	4788	18.42	-23.99	-0.06
124	SLU 80	-757	-635	4788	18.42	-23.99	-0.06
124	SLU 81	-808	-663	5051	19.11	-25.8	-0.07
124	SLU 82	-808	-663	5051	19.11	-25.8	-0.07
124	SLU 83	-808	-663	5051	19.11	-25.8	-0.07
124	SLU 84	-808	-663	5051	19.11	-25.8	-0.07
124	SLE RA 1	-475	-430	3132	12.68	-14.7	-0.02
124	SLE RA 2	-475	-430	3132	12.68	-14.7	-0.02
124	SLE RA 3	-475	-430	3132	12.68	-14.7	-0.02
124	SLE RA 4	-475	-430	3132	12.68	-14.7	-0.02
124	SLE RA 5	-475	-430	3132	12.68	-14.7	-0.02
124	SLE RA 6	-475	-430	3132	12.68	-14.7	-0.02
124	SLE RA 7	-475	-430	3132	12.68	-14.7	-0.02
124	SLE RA 8	-475	-430	3132	12.68	-14.7	-0.02
124	SLE RA 9	-475	-430	3132	12.68	-14.7	-0.02
124	SLE RA 10	-555	-473	3542	13.77	-17.52	-0.04
124	SLE RA 11	-555	-473	3542	13.77	-17.52	-0.04
124	SLE RA 12	-555	-473	3542	13.77	-17.52	-0.04
124	SLE RA 13	-555	-473	3542	13.77	-17.52	-0.04
124	SLE RA 14	-555	-473	3542	13.77	-17.52	-0.04
124	SLE RA 15	-555	-473	3542	13.77	-17.52	-0.04
124	SLE RA 16	-555	-473	3542	13.77	-17.52	-0.04
124	SLE RA 17	-555	-473	3542	13.77	-17.52	-0.04
124	SLE RA 18	-590	-492	3718	14.23	-18.73	-0.04
124	SLE RA 19	-590	-492	3718	14.23	-18.73	-0.04
124	SLE RA 20	-590	-492	3718	14.23	-18.73	-0.04
124	SLE RA 21	-590	-492	3718	14.23	-18.73	-0.04
124	SLE FR 1	-475	-430	3132	12.68	-14.7	-0.02
124	SLE FR 2	-475	-430	3132	12.68	-14.7	-0.02
124	SLE FR 3	-475	-430	3132	12.68	-14.7	-0.02
124	SLE FR 4	-510	-449	3308	13.15	-15.91	-0.03
124	SLE FR 5	-510	-449	3308	13.15	-15.91	-0.03
124	SLE FR 6	-532	-461	3425	13.46	-16.71	-0.03
124	SLE QP 1	-475	-430	3132	12.68	-14.7	-0.02
124	SLE QP 2	-510	-449	3308	13.15	-15.91	-0.03
124	SLD 1	-387	-361	2724	9.8	-11.36	0
124	SLD 2	-387	-361	2724	9.8	-11.36	0
124	SLD 3	-401	-439	2979	13.26	-10.73	0.03
124	SLD 4	-401	-439	2979	13.26	-10.73	0.03
124	SLD 5	-452	-304	2747	6.9	-15.51	-0.07
124	SLD 6	-452	-304	2747	6.9	-15.51	-0.07
124	SLD 7	-498	-564	3595	18.43	-13.39	0.03
124	SLD 8	-498	-564	3595	18.43	-13.39	0.03
124	SLD 9	-521	-333	3021	7.86	-18.43	-0.09
124	SLD 10	-521	-333	3021	7.86	-18.43	-0.09
124	SLD 11	-567	-593	3869	19.4	-16.31	0
124	SLD 12	-567	-593	3869	19.4	-16.31	0
124	SLD 13	-618	-458	3637	13.03	-21.09	-0.09
124	SLD 14	-618	-458	3637	13.03	-21.09	-0.09



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
124	SLD 15	-632	-536	3891	16.49	-20.45	-0.06
124	SLD 16	-632	-536	3891	16.49	-20.45	-0.06
124	SLV 1	-219	-242	1927	5.23	-5.21	0.04
124	SLV 2	-219	-242	1927	5.23	-5.21	0.04
124	SLV 3	-255	-427	2539	13.5	-3.62	0.1
124	SLV 4	-255	-427	2539	13.5	-3.62	0.1
124	SLV 5	-367	-106	1965	-1.78	-15.11	-0.11
124	SLV 6	-367	-106	1965	-1.78	-15.11	-0.11
124	SLV 7	-488	-723	4005	25.8	-9.81	0.11
124	SLV 8	-488	-723	4005	25.8	-9.81	0.11
124	SLV 9	-531	-175	2610	0.49	-22	-0.17
124	SLV 10	-531	-175	2610	0.49	-22	-0.17
124	SLV 11	-652	-791	4650	28.07	-16.71	0.05
124	SLV 12	-652	-791	4650	28.07	-16.71	0.05
124	SLV 13	-764	-470	4076	12.79	-28.19	-0.16
124	SLV 14	-764	-470	4076	12.79	-28.19	-0.16
124	SLV 15	-800	-655	4688	21.07	-26.6	-0.1
124	SLV 16	-800	-655	4688	21.07	-26.6	-0.1
125	SLU 1	-390	-3	2353	0.94	-22.31	-0.01
125	SLU 2	-390	-3	2353	0.94	-22.31	-0.01
125	SLU 3	-390	-3	2353	0.94	-22.31	-0.01
125	SLU 4	-390	-3	2353	0.94	-22.31	-0.01
125	SLU 5	-390	-3	2353	0.94	-22.31	-0.01
125	SLU 6	-390	-3	2353	0.94	-22.31	-0.01
125	SLU 7	-390	-3	2353	0.94	-22.31	-0.01
125	SLU 8	-390	-3	2353	0.94	-22.31	-0.01
125	SLU 9	-390	-3	2353	0.94	-22.31	-0.01
125	SLU 10	-522	-3	2825	1.1	-29.53	-0.02
125	SLU 11	-522	-3	2825	1.1	-29.53	-0.02
125	SLU 12	-522	-3	2825	1.1	-29.53	-0.02
125	SLU 13	-522	-3	2825	1.1	-29.53	-0.02
125	SLU 14	-522	-3	2825	1.1	-29.53	-0.02
125	SLU 15	-522	-3	2825	1.1	-29.53	-0.02
125	SLU 16	-522	-3	2825	1.1	-29.53	-0.02
125	SLU 17	-522	-3	2825	1.1	-29.53	-0.02
125	SLU 18	-579	-4	3027	1.17	-32.62	-0.02
125	SLU 19	-579	-4	3027	1.17	-32.62	-0.02
125	SLU 20	-579	-4	3027	1.17	-32.62	-0.02
125	SLU 21	-579	-4	3027	1.17	-32.62	-0.02
125	SLU 22	-461	-3	2624	1.04	-26.2	-0.02
125	SLU 23	-461	-3	2624	1.04	-26.2	-0.02
125	SLU 24	-461	-3	2624	1.04	-26.2	-0.02
125	SLU 25	-461	-3	2624	1.04	-26.2	-0.02
125	SLU 26	-461	-3	2624	1.04	-26.2	-0.02
125	SLU 27	-461	-3	2624	1.04	-26.2	-0.02
125	SLU 28	-461	-3	2624	1.04	-26.2	-0.02
125	SLU 29	-461	-3	2624	1.04	-26.2	-0.02
125	SLU 30	-461	-3	2624	1.04	-26.2	-0.02
125	SLU 31	-593	-4	3096	1.2	-33.41	-0.02
125	SLU 32	-593	-4	3096	1.2	-33.41	-0.02
125	SLU 33	-593	-4	3096	1.2	-33.41	-0.02
125	SLU 34	-593	-4	3096	1.2	-33.41	-0.02
125	SLU 35	-593	-4	3096	1.2	-33.41	-0.02
125	SLU 36	-593	-4	3096	1.2	-33.41	-0.02
125	SLU 37	-593	-4	3096	1.2	-33.41	-0.02
125	SLU 38	-593	-4	3096	1.2	-33.41	-0.02
125	SLU 39	-650	-4	3298	1.27	-36.5	-0.02
125	SLU 40	-650	-4	3298	1.27	-36.5	-0.02
125	SLU 41	-650	-4	3298	1.27	-36.5	-0.02
125	SLU 42	-650	-4	3298	1.27	-36.5	-0.02
125	SLU 43	-483	-4	2966	1.19	-27.68	-0.02
125	SLU 44	-483	-4	2966	1.19	-27.68	-0.02
125	SLU 45	-483	-4	2966	1.19	-27.68	-0.02
125	SLU 46	-483	-4	2966	1.19	-27.68	-0.02
125	SLU 47	-483	-4	2966	1.19	-27.68	-0.02
125	SLU 48	-483	-4	2966	1.19	-27.68	-0.02
125	SLU 49	-483	-4	2966	1.19	-27.68	-0.02
125	SLU 50	-483	-4	2966	1.19	-27.68	-0.02
125	SLU 51	-483	-4	2966	1.19	-27.68	-0.02
125	SLU 52	-615	-4	3437	1.35	-34.89	-0.02
125	SLU 53	-615	-4	3437	1.35	-34.89	-0.02
125	SLU 54	-615	-4	3437	1.35	-34.89	-0.02
125	SLU 55	-615	-4	3437	1.35	-34.89	-0.02
125	SLU 56	-615	-4	3437	1.35	-34.89	-0.02
125	SLU 57	-615	-4	3437	1.35	-34.89	-0.02
125	SLU 58	-615	-4	3437	1.35	-34.89	-0.02
125	SLU 59	-615	-4	3437	1.35	-34.89	-0.02
125	SLU 60	-672	-4	3640	1.42	-37.98	-0.02
125	SLU 61	-672	-4	3640	1.42	-37.98	-0.02
125	SLU 62	-672	-4	3640	1.42	-37.98	-0.02
125	SLU 63	-672	-4	3640	1.42	-37.98	-0.02
125	SLU 64	-554	-4	3237	1.29	-31.56	-0.02
125	SLU 65	-554	-4	3237	1.29	-31.56	-0.02
125	SLU 66	-554	-4	3237	1.29	-31.56	-0.02
125	SLU 67	-554	-4	3237	1.29	-31.56	-0.02
125	SLU 68	-554	-4	3237	1.29	-31.56	-0.02
125	SLU 69	-554	-4	3237	1.29	-31.56	-0.02
125	SLU 70	-554	-4	3237	1.29	-31.56	-0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
125	SLU 71	-554	-4	3237	1.29	-31.56	-0.02
125	SLU 72	-554	-4	3237	1.29	-31.56	-0.02
125	SLU 73	-686	-5	3709	1.45	-38.77	-0.02
125	SLU 74	-686	-5	3709	1.45	-38.77	-0.02
125	SLU 75	-686	-5	3709	1.45	-38.77	-0.02
125	SLU 76	-686	-5	3709	1.45	-38.77	-0.02
125	SLU 77	-686	-5	3709	1.45	-38.77	-0.02
125	SLU 78	-686	-5	3709	1.45	-38.77	-0.02
125	SLU 79	-686	-5	3709	1.45	-38.77	-0.02
125	SLU 80	-686	-5	3709	1.45	-38.77	-0.02
125	SLU 81	-742	-5	3911	1.52	-41.87	-0.02
125	SLU 82	-742	-5	3911	1.52	-41.87	-0.02
125	SLU 83	-742	-5	3911	1.52	-41.87	-0.02
125	SLU 84	-742	-5	3911	1.52	-41.87	-0.02
125	SLE RA 1	-411	-3	2430	0.97	-23.42	-0.01
125	SLE RA 2	-411	-3	2430	0.97	-23.42	-0.01
125	SLE RA 3	-411	-3	2430	0.97	-23.42	-0.01
125	SLE RA 4	-411	-3	2430	0.97	-23.42	-0.01
125	SLE RA 5	-411	-3	2430	0.97	-23.42	-0.01
125	SLE RA 6	-411	-3	2430	0.97	-23.42	-0.01
125	SLE RA 7	-411	-3	2430	0.97	-23.42	-0.01
125	SLE RA 8	-411	-3	2430	0.97	-23.42	-0.01
125	SLE RA 9	-411	-3	2430	0.97	-23.42	-0.01
125	SLE RA 10	-498	-3	2745	1.08	-28.23	-0.02
125	SLE RA 11	-498	-3	2745	1.08	-28.23	-0.02
125	SLE RA 12	-498	-3	2745	1.08	-28.23	-0.02
125	SLE RA 13	-498	-3	2745	1.08	-28.23	-0.02
125	SLE RA 14	-498	-3	2745	1.08	-28.23	-0.02
125	SLE RA 15	-498	-3	2745	1.08	-28.23	-0.02
125	SLE RA 16	-498	-3	2745	1.08	-28.23	-0.02
125	SLE RA 17	-498	-3	2745	1.08	-28.23	-0.02
125	SLE RA 18	-536	-4	2880	1.12	-30.29	-0.02
125	SLE RA 19	-536	-4	2880	1.12	-30.29	-0.02
125	SLE RA 20	-536	-4	2880	1.12	-30.29	-0.02
125	SLE RA 21	-536	-4	2880	1.12	-30.29	-0.02
125	SLE FR 1	-411	-3	2430	0.97	-23.42	-0.01
125	SLE FR 2	-411	-3	2430	0.97	-23.42	-0.01
125	SLE FR 3	-411	-3	2430	0.97	-23.42	-0.01
125	SLE FR 4	-448	-3	2565	1.01	-25.48	-0.02
125	SLE FR 5	-448	-3	2565	1.01	-25.48	-0.02
125	SLE FR 6	-473	-3	2655	1.05	-26.86	-0.02
125	SLE QP 1	-411	-3	2430	0.97	-23.42	-0.01
125	SLE QP 2	-448	-3	2565	1.01	-25.48	-0.02
125	SLD 1	-300	-13	2213	3.04	-15.8	-0.01
125	SLD 2	-300	-13	2213	3.04	-15.8	-0.01
125	SLD 3	-271	-10	2368	7.39	-16.78	-0.01
125	SLD 4	-271	-10	2368	7.39	-16.78	-0.01
125	SLD 5	-448	-11	2225	-4.96	-21.09	0
125	SLD 6	-448	-11	2225	-4.96	-21.09	0
125	SLD 7	-351	-1	2740	9.51	-24.36	-0.03
125	SLD 8	-351	-1	2740	9.51	-24.36	-0.03
125	SLD 9	-546	-6	2390	-7.48	-26.61	0
125	SLD 10	-546	-6	2390	-7.48	-26.61	0
125	SLD 11	-448	4	2905	6.99	-29.88	-0.03
125	SLD 12	-448	4	2905	6.99	-29.88	-0.03
125	SLD 13	-626	4	2762	-5.36	-34.19	-0.02
125	SLD 14	-626	4	2762	-5.36	-34.19	-0.02
125	SLD 15	-597	7	2917	-1.01	-35.17	-0.03
125	SLD 16	-597	7	2917	-1.01	-35.17	-0.03
125	SLV 1	-98	-29	1733	5.94	-2.59	0.01
125	SLV 2	-98	-29	1733	5.94	-2.59	0.01
125	SLV 3	-29	-20	2105	17.17	-4.96	-0.01
125	SLV 4	-29	-20	2105	17.17	-4.96	-0.01
125	SLV 5	-448	-23	1750	-14.54	-15.02	0.03
125	SLV 6	-448	-23	1750	-14.54	-15.02	0.03
125	SLV 7	-218	4	2993	22.89	-22.92	-0.05
125	SLV 8	-218	4	2993	22.89	-22.92	-0.05
125	SLV 9	-679	-10	2137	-20.86	-28.05	0.02
125	SLV 10	-679	-10	2137	-20.86	-28.05	0.02
125	SLV 11	-449	17	3380	16.57	-35.95	-0.06
125	SLV 12	-449	17	3380	16.57	-35.95	-0.06
125	SLV 13	-868	14	3025	-15.14	-46.01	-0.02
125	SLV 14	-868	14	3025	-15.14	-46.01	-0.02
125	SLV 15	-799	22	3397	-3.91	-48.38	-0.04
125	SLV 16	-799	22	3397	-3.91	-48.38	-0.04
126	SLU 1	-325	0	2156	0.44	-16.83	0
126	SLU 2	-325	0	2156	0.44	-16.83	0
126	SLU 3	-325	0	2156	0.44	-16.83	0
126	SLU 4	-325	0	2156	0.44	-16.83	0
126	SLU 5	-325	0	2156	0.44	-16.83	0
126	SLU 6	-325	0	2156	0.44	-16.83	0
126	SLU 7	-325	0	2156	0.44	-16.83	0
126	SLU 8	-325	0	2156	0.44	-16.83	0
126	SLU 9	-325	0	2156	0.44	-16.83	0
126	SLU 10	-445	-1	2585	0.53	-22.92	0
126	SLU 11	-445	-1	2585	0.53	-22.92	0
126	SLU 12	-445	-1	2585	0.53	-22.92	0
126	SLU 13	-445	-1	2585	0.53	-22.92	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
126	SLU 14	-445	-1	2585	0.53	-22.92	0
126	SLU 15	-445	-1	2585	0.53	-22.92	0
126	SLU 16	-445	-1	2585	0.53	-22.92	0
126	SLU 17	-445	-1	2585	0.53	-22.92	0
126	SLU 18	-496	-1	2769	0.56	-25.53	0
126	SLU 19	-496	-1	2769	0.56	-25.53	0
126	SLU 20	-496	-1	2769	0.56	-25.53	0
126	SLU 21	-496	-1	2769	0.56	-25.53	0
126	SLU 22	-389	0	2405	0.49	-20.06	0
126	SLU 23	-389	0	2405	0.49	-20.06	0
126	SLU 24	-389	0	2405	0.49	-20.06	0
126	SLU 25	-389	0	2405	0.49	-20.06	0
126	SLU 26	-389	0	2405	0.49	-20.06	0
126	SLU 27	-389	0	2405	0.49	-20.06	0
126	SLU 28	-389	0	2405	0.49	-20.06	0
126	SLU 29	-389	0	2405	0.49	-20.06	0
126	SLU 30	-389	0	2405	0.49	-20.06	0
126	SLU 31	-508	-1	2833	0.58	-26.15	0
126	SLU 32	-508	-1	2833	0.58	-26.15	0
126	SLU 33	-508	-1	2833	0.58	-26.15	0
126	SLU 34	-508	-1	2833	0.58	-26.15	0
126	SLU 35	-508	-1	2833	0.58	-26.15	0
126	SLU 36	-508	-1	2833	0.58	-26.15	0
126	SLU 37	-508	-1	2833	0.58	-26.15	0
126	SLU 38	-508	-1	2833	0.58	-26.15	0
126	SLU 39	-560	-1	3017	0.61	-28.75	0
126	SLU 40	-560	-1	3017	0.61	-28.75	0
126	SLU 41	-560	-1	3017	0.61	-28.75	0
126	SLU 42	-560	-1	3017	0.61	-28.75	0
126	SLU 43	-401	-1	2718	0.56	-20.77	0
126	SLU 44	-401	-1	2718	0.56	-20.77	0
126	SLU 45	-401	-1	2718	0.56	-20.77	0
126	SLU 46	-401	-1	2718	0.56	-20.77	0
126	SLU 47	-401	-1	2718	0.56	-20.77	0
126	SLU 48	-401	-1	2718	0.56	-20.77	0
126	SLU 49	-401	-1	2718	0.56	-20.77	0
126	SLU 50	-401	-1	2718	0.56	-20.77	0
126	SLU 51	-401	-1	2718	0.56	-20.77	0
126	SLU 52	-521	-1	3146	0.64	-26.86	0
126	SLU 53	-521	-1	3146	0.64	-26.86	0
126	SLU 54	-521	-1	3146	0.64	-26.86	0
126	SLU 55	-521	-1	3146	0.64	-26.86	0
126	SLU 56	-521	-1	3146	0.64	-26.86	0
126	SLU 57	-521	-1	3146	0.64	-26.86	0
126	SLU 58	-521	-1	3146	0.64	-26.86	0
126	SLU 59	-521	-1	3146	0.64	-26.86	0
126	SLU 60	-572	-1	3330	0.68	-29.47	0
126	SLU 61	-572	-1	3330	0.68	-29.47	0
126	SLU 62	-572	-1	3330	0.68	-29.47	0
126	SLU 63	-572	-1	3330	0.68	-29.47	0
126	SLU 64	-465	-1	2966	0.61	-24	0
126	SLU 65	-465	-1	2966	0.61	-24	0
126	SLU 66	-465	-1	2966	0.61	-24	0
126	SLU 67	-465	-1	2966	0.61	-24	0
126	SLU 68	-465	-1	2966	0.61	-24	0
126	SLU 69	-465	-1	2966	0.61	-24	0
126	SLU 70	-465	-1	2966	0.61	-24	0
126	SLU 71	-465	-1	2966	0.61	-24	0
126	SLU 72	-465	-1	2966	0.61	-24	0
126	SLU 73	-584	-1	3395	0.69	-30.09	0
126	SLU 74	-584	-1	3395	0.69	-30.09	0
126	SLU 75	-584	-1	3395	0.69	-30.09	0
126	SLU 76	-584	-1	3395	0.69	-30.09	0
126	SLU 77	-584	-1	3395	0.69	-30.09	0
126	SLU 78	-584	-1	3395	0.69	-30.09	0
126	SLU 79	-584	-1	3395	0.69	-30.09	0
126	SLU 80	-584	-1	3395	0.69	-30.09	0
126	SLU 81	-636	-1	3579	0.73	-32.7	0
126	SLU 82	-636	-1	3579	0.73	-32.7	0
126	SLU 83	-636	-1	3579	0.73	-32.7	0
126	SLU 84	-636	-1	3579	0.73	-32.7	0
126	SLE RA 1	-344	0	2227	0.46	-17.75	0
126	SLE RA 2	-344	0	2227	0.46	-17.75	0
126	SLE RA 3	-344	0	2227	0.46	-17.75	0
126	SLE RA 4	-344	0	2227	0.46	-17.75	0
126	SLE RA 5	-344	0	2227	0.46	-17.75	0
126	SLE RA 6	-344	0	2227	0.46	-17.75	0
126	SLE RA 7	-344	0	2227	0.46	-17.75	0
126	SLE RA 8	-344	0	2227	0.46	-17.75	0
126	SLE RA 9	-344	0	2227	0.46	-17.75	0
126	SLE RA 10	-423	0	2513	0.51	-21.81	0
126	SLE RA 11	-423	0	2513	0.51	-21.81	0
126	SLE RA 12	-423	0	2513	0.51	-21.81	0
126	SLE RA 13	-423	0	2513	0.51	-21.81	0
126	SLE RA 14	-423	0	2513	0.51	-21.81	0
126	SLE RA 15	-423	0	2513	0.51	-21.81	0
126	SLE RA 16	-423	0	2513	0.51	-21.81	0
126	SLE RA 17	-423	0	2513	0.51	-21.81	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
126	SLE RA 18	-457	-1	2635	0.54	-23.55	0
126	SLE RA 19	-457	-1	2635	0.54	-23.55	0
126	SLE RA 20	-457	-1	2635	0.54	-23.55	0
126	SLE RA 21	-457	-1	2635	0.54	-23.55	0
126	SLE FR 1	-344	0	2227	0.46	-17.75	0
126	SLE FR 2	-344	0	2227	0.46	-17.75	0
126	SLE FR 3	-344	0	2227	0.46	-17.75	0
126	SLE FR 4	-378	0	2350	0.48	-19.49	0
126	SLE FR 5	-378	0	2350	0.48	-19.49	0
126	SLE FR 6	-401	0	2431	0.5	-20.65	0
126	SLE QP 1	-344	0	2227	0.46	-17.75	0
126	SLE QP 2	-378	0	2350	0.48	-19.49	0
126	SLD 1	-217	-15	2135	3.41	-10.97	-0.02
126	SLD 2	-217	-15	2135	3.41	-10.97	-0.02
126	SLD 3	-195	-9	2234	12.78	-10.03	-0.02
126	SLD 4	-195	-9	2234	12.78	-10.03	-0.02
126	SLD 5	-364	-14	2135	-12.86	-18.35	-0.01
126	SLD 6	-364	-14	2135	-12.86	-18.35	-0.01
126	SLD 7	-288	6	2466	18.39	-15.24	0.01
126	SLD 8	-288	6	2466	18.39	-15.24	0.01
126	SLD 9	-467	-7	2234	-17.42	-23.75	0
126	SLD 10	-467	-7	2234	-17.42	-23.75	0
126	SLD 11	-391	13	2565	13.82	-20.63	0.02
126	SLD 12	-391	13	2565	13.82	-20.63	0.02
126	SLD 13	-561	8	2465	-11.82	-28.95	0.02
126	SLD 14	-561	8	2465	-11.82	-28.95	0.02
126	SLD 15	-538	14	2565	-2.45	-28.02	0.03
126	SLD 16	-538	14	2565	-2.45	-28.02	0.03
126	SLV 1	1	-36	1841	7.48	0.62	-0.05
126	SLV 2	1	-36	1841	7.48	0.62	-0.05
126	SLV 3	54	-20	2081	31.86	2.84	-0.04
126	SLV 4	54	-20	2081	31.86	2.84	-0.04
126	SLV 5	-346	-35	1832	-34.39	-16.82	-0.04
126	SLV 6	-346	-35	1832	-34.39	-16.82	-0.04
126	SLV 7	-166	17	2634	46.87	-9.43	0.01
126	SLV 8	-166	17	2634	46.87	-9.43	0.01
126	SLV 9	-589	-18	2066	-45.91	-29.55	-0.01
126	SLV 10	-589	-18	2066	-45.91	-29.55	-0.01
126	SLV 11	-410	34	2867	35.36	-22.17	0.04
126	SLV 12	-410	34	2867	35.36	-22.17	0.04
126	SLV 13	-810	19	2618	-30.9	-41.82	0.04
126	SLV 14	-810	19	2618	-30.9	-41.82	0.04
126	SLV 15	-756	35	2858	-6.52	-39.61	0.06
126	SLV 16	-756	35	2858	-6.52	-39.61	0.06
127	SLU 1	-245	0	2094	0.23	-13.05	0
127	SLU 2	-245	0	2094	0.23	-13.05	0
127	SLU 3	-245	0	2094	0.23	-13.05	0
127	SLU 4	-245	0	2094	0.23	-13.05	0
127	SLU 5	-245	0	2094	0.23	-13.05	0
127	SLU 6	-245	0	2094	0.23	-13.05	0
127	SLU 7	-245	0	2094	0.23	-13.05	0
127	SLU 8	-245	0	2094	0.23	-13.05	0
127	SLU 9	-245	0	2094	0.23	-13.05	0
127	SLU 10	-345	0	2513	0.28	-18.24	0
127	SLU 11	-345	0	2513	0.28	-18.24	0
127	SLU 12	-345	0	2513	0.28	-18.24	0
127	SLU 13	-345	0	2513	0.28	-18.24	0
127	SLU 14	-345	0	2513	0.28	-18.24	0
127	SLU 15	-345	0	2513	0.28	-18.24	0
127	SLU 16	-345	0	2513	0.28	-18.24	0
127	SLU 17	-345	0	2513	0.28	-18.24	0
127	SLU 18	-388	0	2693	0.29	-20.46	0
127	SLU 19	-388	0	2693	0.29	-20.46	0
127	SLU 20	-388	0	2693	0.29	-20.46	0
127	SLU 21	-388	0	2693	0.29	-20.46	0
127	SLU 22	-297	0	2339	0.26	-15.77	0
127	SLU 23	-297	0	2339	0.26	-15.77	0
127	SLU 24	-297	0	2339	0.26	-15.77	0
127	SLU 25	-297	0	2339	0.26	-15.77	0
127	SLU 26	-297	0	2339	0.26	-15.77	0
127	SLU 27	-297	0	2339	0.26	-15.77	0
127	SLU 28	-297	0	2339	0.26	-15.77	0
127	SLU 29	-297	0	2339	0.26	-15.77	0
127	SLU 30	-297	0	2339	0.26	-15.77	0
127	SLU 31	-397	0	2758	0.3	-20.95	0
127	SLU 32	-397	0	2758	0.3	-20.95	0
127	SLU 33	-397	0	2758	0.3	-20.95	0
127	SLU 34	-397	0	2758	0.3	-20.95	0
127	SLU 35	-397	0	2758	0.3	-20.95	0
127	SLU 36	-397	0	2758	0.3	-20.95	0
127	SLU 37	-397	0	2758	0.3	-20.95	0
127	SLU 38	-397	0	2758	0.3	-20.95	0
127	SLU 39	-440	0	2937	0.32	-23.18	0
127	SLU 40	-440	0	2937	0.32	-23.18	0
127	SLU 41	-440	0	2937	0.32	-23.18	0
127	SLU 42	-440	0	2937	0.32	-23.18	0
127	SLU 43	-301	0	2639	0.29	-16.03	0
127	SLU 44	-301	0	2639	0.29	-16.03	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
127	SLU 45	-301	0	2639	0.29	-16.03	0
127	SLU 46	-301	0	2639	0.29	-16.03	0
127	SLU 47	-301	0	2639	0.29	-16.03	0
127	SLU 48	-301	0	2639	0.29	-16.03	0
127	SLU 49	-301	0	2639	0.29	-16.03	0
127	SLU 50	-301	0	2639	0.29	-16.03	0
127	SLU 51	-301	0	2639	0.29	-16.03	0
127	SLU 52	-401	0	3058	0.33	-21.22	0
127	SLU 53	-401	0	3058	0.33	-21.22	0
127	SLU 54	-401	0	3058	0.33	-21.22	0
127	SLU 55	-401	0	3058	0.33	-21.22	0
127	SLU 56	-401	0	3058	0.33	-21.22	0
127	SLU 57	-401	0	3058	0.33	-21.22	0
127	SLU 58	-401	0	3058	0.33	-21.22	0
127	SLU 59	-401	0	3058	0.33	-21.22	0
127	SLU 60	-443	0	3237	0.35	-23.45	0
127	SLU 61	-443	0	3237	0.35	-23.45	0
127	SLU 62	-443	0	3237	0.35	-23.45	0
127	SLU 63	-443	0	3237	0.35	-23.45	0
127	SLU 64	-353	0	2883	0.32	-18.75	0
127	SLU 65	-353	0	2883	0.32	-18.75	0
127	SLU 66	-353	0	2883	0.32	-18.75	0
127	SLU 67	-353	0	2883	0.32	-18.75	0
127	SLU 68	-353	0	2883	0.32	-18.75	0
127	SLU 69	-353	0	2883	0.32	-18.75	0
127	SLU 70	-353	0	2883	0.32	-18.75	0
127	SLU 71	-353	0	2883	0.32	-18.75	0
127	SLU 72	-353	0	2883	0.32	-18.75	0
127	SLU 73	-453	0	3302	0.36	-23.94	0
127	SLU 74	-453	0	3302	0.36	-23.94	0
127	SLU 75	-453	0	3302	0.36	-23.94	0
127	SLU 76	-453	0	3302	0.36	-23.94	0
127	SLU 77	-453	0	3302	0.36	-23.94	0
127	SLU 78	-453	0	3302	0.36	-23.94	0
127	SLU 79	-453	0	3302	0.36	-23.94	0
127	SLU 80	-453	0	3302	0.36	-23.94	0
127	SLU 81	-495	0	3482	0.38	-26.16	0
127	SLU 82	-495	0	3482	0.38	-26.16	0
127	SLU 83	-495	0	3482	0.38	-26.16	0
127	SLU 84	-495	0	3482	0.38	-26.16	0
127	SLE RA 1	-260	0	2164	0.24	-13.82	0
127	SLE RA 2	-260	0	2164	0.24	-13.82	0
127	SLE RA 3	-260	0	2164	0.24	-13.82	0
127	SLE RA 4	-260	0	2164	0.24	-13.82	0
127	SLE RA 5	-260	0	2164	0.24	-13.82	0
127	SLE RA 6	-260	0	2164	0.24	-13.82	0
127	SLE RA 7	-260	0	2164	0.24	-13.82	0
127	SLE RA 8	-260	0	2164	0.24	-13.82	0
127	SLE RA 9	-260	0	2164	0.24	-13.82	0
127	SLE RA 10	-327	0	2443	0.27	-17.28	0
127	SLE RA 11	-327	0	2443	0.27	-17.28	0
127	SLE RA 12	-327	0	2443	0.27	-17.28	0
127	SLE RA 13	-327	0	2443	0.27	-17.28	0
127	SLE RA 14	-327	0	2443	0.27	-17.28	0
127	SLE RA 15	-327	0	2443	0.27	-17.28	0
127	SLE RA 16	-327	0	2443	0.27	-17.28	0
127	SLE RA 17	-327	0	2443	0.27	-17.28	0
127	SLE RA 18	-355	0	2563	0.28	-18.77	0
127	SLE RA 19	-355	0	2563	0.28	-18.77	0
127	SLE RA 20	-355	0	2563	0.28	-18.77	0
127	SLE RA 21	-355	0	2563	0.28	-18.77	0
127	SLE FR 1	-260	0	2164	0.24	-13.82	0
127	SLE FR 2	-260	0	2164	0.24	-13.82	0
127	SLE FR 3	-260	0	2164	0.24	-13.82	0
127	SLE FR 4	-289	0	2284	0.25	-15.31	0
127	SLE FR 5	-289	0	2284	0.25	-15.31	0
127	SLE FR 6	-308	0	2364	0.26	-16.3	0
127	SLE QP 1	-260	0	2164	0.24	-13.82	0
127	SLE QP 2	-289	0	2284	0.25	-15.31	0
127	SLD 1	-116	-17	2145	3.21	-5.11	-0.03
127	SLD 2	-116	-17	2145	3.21	-5.11	-0.03
127	SLD 3	-97	-6	2217	18.3	-6	-0.02
127	SLD 4	-97	-6	2217	18.3	-6	-0.02
127	SLD 5	-266	-20	2134	-21.74	-10.9	-0.03
127	SLD 6	-266	-20	2134	-21.74	-10.9	-0.03
127	SLD 7	-202	13	2372	28.55	-13.86	0.02
127	SLD 8	-202	13	2372	28.55	-13.86	0.02
127	SLD 9	-376	-14	2196	-28.05	-16.75	-0.02
127	SLD 10	-376	-14	2196	-28.05	-16.75	-0.02
127	SLD 11	-311	20	2434	22.25	-19.71	0.03
127	SLD 12	-311	20	2434	22.25	-19.71	0.03
127	SLD 13	-480	6	2351	-17.79	-24.61	0.02
127	SLD 14	-480	6	2351	-17.79	-24.61	0.02
127	SLD 15	-461	16	2423	-2.71	-25.5	0.03
127	SLD 16	-461	16	2423	-2.71	-25.5	0.03
127	SLV 1	118	-41	1956	7.02	8.78	-0.08
127	SLV 2	118	-41	1956	7.02	8.78	-0.08
127	SLV 3	164	-16	2129	46.61	6.65	-0.04



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
127	SLV 4	164	-16	2129	46.61	6.65	-0.04
127	SLV 5	-237	-51	1923	-57.77	-4.86	-0.09
127	SLV 6	-237	-51	1923	-57.77	-4.86	-0.09
127	SLV 7	-83	34	2500	74.21	-11.95	0.05
127	SLV 8	-83	34	2500	74.21	-11.95	0.05
127	SLV 9	-494	-34	2068	-73.71	-18.67	-0.05
127	SLV 10	-494	-34	2068	-73.71	-18.67	-0.05
127	SLV 11	-340	51	2645	58.27	-25.76	0.09
127	SLV 12	-340	51	2645	58.27	-25.76	0.09
127	SLV 13	-741	16	2439	-46.11	-37.26	0.04
127	SLV 14	-741	16	2439	-46.11	-37.26	0.04
127	SLV 15	-695	41	2612	-6.51	-39.39	0.08
127	SLV 16	-695	41	2612	-6.51	-39.39	0.08
128	SLU 1	-184	0	2030	0.14	-10	0
128	SLU 2	-184	0	2030	0.14	-10	0
128	SLU 3	-184	0	2030	0.14	-10	0
128	SLU 4	-184	0	2030	0.14	-10	0
128	SLU 5	-184	0	2030	0.14	-10	0
128	SLU 6	-184	0	2030	0.14	-10	0
128	SLU 7	-184	0	2030	0.14	-10	0
128	SLU 8	-184	0	2030	0.14	-10	0
128	SLU 9	-184	0	2030	0.14	-10	0
128	SLU 10	-267	0	2437	0.17	-14.38	0
128	SLU 11	-267	0	2437	0.17	-14.38	0
128	SLU 12	-267	0	2437	0.17	-14.38	0
128	SLU 13	-267	0	2437	0.17	-14.38	0
128	SLU 14	-267	0	2437	0.17	-14.38	0
128	SLU 15	-267	0	2437	0.17	-14.38	0
128	SLU 16	-267	0	2437	0.17	-14.38	0
128	SLU 17	-267	0	2437	0.17	-14.38	0
128	SLU 18	-302	0	2612	0.18	-16.26	0
128	SLU 19	-302	0	2612	0.18	-16.26	0
128	SLU 20	-302	0	2612	0.18	-16.26	0
128	SLU 21	-302	0	2612	0.18	-16.26	0
128	SLU 22	-226	0	2269	0.16	-12.23	0
128	SLU 23	-226	0	2269	0.16	-12.23	0
128	SLU 24	-226	0	2269	0.16	-12.23	0
128	SLU 25	-226	0	2269	0.16	-12.23	0
128	SLU 26	-226	0	2269	0.16	-12.23	0
128	SLU 27	-226	0	2269	0.16	-12.23	0
128	SLU 28	-226	0	2269	0.16	-12.23	0
128	SLU 29	-226	0	2269	0.16	-12.23	0
128	SLU 30	-226	0	2269	0.16	-12.23	0
128	SLU 31	-309	0	2676	0.19	-16.61	0
128	SLU 32	-309	0	2676	0.19	-16.61	0
128	SLU 33	-309	0	2676	0.19	-16.61	0
128	SLU 34	-309	0	2676	0.19	-16.61	0
128	SLU 35	-309	0	2676	0.19	-16.61	0
128	SLU 36	-309	0	2676	0.19	-16.61	0
128	SLU 37	-309	0	2676	0.19	-16.61	0
128	SLU 38	-309	0	2676	0.19	-16.61	0
128	SLU 39	-344	0	2851	0.2	-18.49	0
128	SLU 40	-344	0	2851	0.2	-18.49	0
128	SLU 41	-344	0	2851	0.2	-18.49	0
128	SLU 42	-344	0	2851	0.2	-18.49	0
128	SLU 43	-225	0	2557	0.18	-12.24	0
128	SLU 44	-225	0	2557	0.18	-12.24	0
128	SLU 45	-225	0	2557	0.18	-12.24	0
128	SLU 46	-225	0	2557	0.18	-12.24	0
128	SLU 47	-225	0	2557	0.18	-12.24	0
128	SLU 48	-225	0	2557	0.18	-12.24	0
128	SLU 49	-225	0	2557	0.18	-12.24	0
128	SLU 50	-225	0	2557	0.18	-12.24	0
128	SLU 51	-225	0	2557	0.18	-12.24	0
128	SLU 52	-307	0	2964	0.21	-16.62	0
128	SLU 53	-307	0	2964	0.21	-16.62	0
128	SLU 54	-307	0	2964	0.21	-16.62	0
128	SLU 55	-307	0	2964	0.21	-16.62	0
128	SLU 56	-307	0	2964	0.21	-16.62	0
128	SLU 57	-307	0	2964	0.21	-16.62	0
128	SLU 58	-307	0	2964	0.21	-16.62	0
128	SLU 59	-307	0	2964	0.21	-16.62	0
128	SLU 60	-343	0	3139	0.22	-18.5	0
128	SLU 61	-343	0	3139	0.22	-18.5	0
128	SLU 62	-343	0	3139	0.22	-18.5	0
128	SLU 63	-343	0	3139	0.22	-18.5	0
128	SLU 64	-267	0	2796	0.19	-14.46	0
128	SLU 65	-267	0	2796	0.19	-14.46	0
128	SLU 66	-267	0	2796	0.19	-14.46	0
128	SLU 67	-267	0	2796	0.19	-14.46	0
128	SLU 68	-267	0	2796	0.19	-14.46	0
128	SLU 69	-267	0	2796	0.19	-14.46	0
128	SLU 70	-267	0	2796	0.19	-14.46	0
128	SLU 71	-267	0	2796	0.19	-14.46	0
128	SLU 72	-267	0	2796	0.19	-14.46	0
128	SLU 73	-350	0	3203	0.22	-18.85	0
128	SLU 74	-350	0	3203	0.22	-18.85	0
128	SLU 75	-350	0	3203	0.22	-18.85	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
128	SLU 76	-350	0	3203	0.22	-18.85	0
128	SLU 77	-350	0	3203	0.22	-18.85	0
128	SLU 78	-350	0	3203	0.22	-18.85	0
128	SLU 79	-350	0	3203	0.22	-18.85	0
128	SLU 80	-350	0	3203	0.22	-18.85	0
128	SLU 81	-385	0	3378	0.23	-20.72	0
128	SLU 82	-385	0	3378	0.23	-20.72	0
128	SLU 83	-385	0	3378	0.23	-20.72	0
128	SLU 84	-385	0	3378	0.23	-20.72	0
128	SLE RA 1	-196	0	2098	0.15	-10.64	0
128	SLE RA 2	-196	0	2098	0.15	-10.64	0
128	SLE RA 3	-196	0	2098	0.15	-10.64	0
128	SLE RA 4	-196	0	2098	0.15	-10.64	0
128	SLE RA 5	-196	0	2098	0.15	-10.64	0
128	SLE RA 6	-196	0	2098	0.15	-10.64	0
128	SLE RA 7	-196	0	2098	0.15	-10.64	0
128	SLE RA 8	-196	0	2098	0.15	-10.64	0
128	SLE RA 9	-196	0	2098	0.15	-10.64	0
128	SLE RA 10	-251	0	2370	0.16	-13.56	0
128	SLE RA 11	-251	0	2370	0.16	-13.56	0
128	SLE RA 12	-251	0	2370	0.16	-13.56	0
128	SLE RA 13	-251	0	2370	0.16	-13.56	0
128	SLE RA 14	-251	0	2370	0.16	-13.56	0
128	SLE RA 15	-251	0	2370	0.16	-13.56	0
128	SLE RA 16	-251	0	2370	0.16	-13.56	0
128	SLE RA 17	-251	0	2370	0.16	-13.56	0
128	SLE RA 18	-275	0	2486	0.17	-14.81	0
128	SLE RA 19	-275	0	2486	0.17	-14.81	0
128	SLE RA 20	-275	0	2486	0.17	-14.81	0
128	SLE RA 21	-275	0	2486	0.17	-14.81	0
128	SLE FR 1	-196	0	2098	0.15	-10.64	0
128	SLE FR 2	-196	0	2098	0.15	-10.64	0
128	SLE FR 3	-196	0	2098	0.15	-10.64	0
128	SLE FR 4	-220	0	2214	0.15	-11.89	0
128	SLE FR 5	-220	0	2214	0.15	-11.89	0
128	SLE FR 6	-235	0	2292	0.16	-12.72	0
128	SLE QP 1	-196	0	2098	0.15	-10.64	0
128	SLE QP 2	-220	0	2214	0.15	-11.89	0
128	SLD 1	-35	-5	2126	2.77	-2.05	-0.01
128	SLD 2	-35	-5	2126	2.77	-2.05	-0.01
128	SLD 3	-19	-20	2179	23.67	-1.28	-0.06
128	SLD 4	-19	-20	2179	23.67	-1.28	-0.06
128	SLD 5	-189	21	2109	-30.76	-10.11	0.06
128	SLD 6	-189	21	2109	-30.76	-10.11	0.06
128	SLD 7	-134	-28	2283	38.91	-7.54	-0.08
128	SLD 8	-134	-28	2283	38.91	-7.54	-0.08
128	SLD 9	-305	28	2146	-38.6	-16.24	0.08
128	SLD 10	-305	28	2146	-38.6	-16.24	0.08
128	SLD 11	-250	-21	2320	31.07	-13.67	-0.06
128	SLD 12	-250	-21	2320	31.07	-13.67	-0.06
128	SLD 13	-421	20	2250	-23.37	-22.49	0.05
128	SLD 14	-421	20	2250	-23.37	-22.49	0.05
128	SLD 15	-404	5	2302	-2.47	-21.72	0.01
128	SLD 16	-404	5	2302	-2.47	-21.72	0.01
128	SLV 1	216	-13	2006	5.61	11.32	-0.04
128	SLV 2	216	-13	2006	5.61	11.32	-0.04
128	SLV 3	255	-50	2133	61.01	13.15	-0.14
128	SLV 4	255	-50	2133	61.01	13.15	-0.14
128	SLV 5	-149	52	1958	-82.23	-7.71	0.14
128	SLV 6	-149	52	1958	-82.23	-7.71	0.14
128	SLV 7	-18	-71	2384	102.43	-1.6	-0.2
128	SLV 8	-18	-71	2384	102.43	-1.6	-0.2
128	SLV 9	-422	71	2045	-102.13	-22.18	0.2
128	SLV 10	-422	71	2045	-102.13	-22.18	0.2
128	SLV 11	-291	-52	2471	82.54	-16.07	-0.14
128	SLV 12	-291	-52	2471	82.54	-16.07	-0.14
128	SLV 13	-694	49	2295	-60.7	-36.93	0.14
128	SLV 14	-694	49	2295	-60.7	-36.93	0.14
128	SLV 15	-655	13	2423	-5.3	-35.1	0.04
128	SLV 16	-655	13	2423	-5.3	-35.1	0.04
129	SLU 1	-150	0	1966	0.09	-8.9	0
129	SLU 2	-150	0	1966	0.09	-8.9	0
129	SLU 3	-150	0	1966	0.09	-8.9	0
129	SLU 4	-150	0	1966	0.09	-8.9	0
129	SLU 5	-150	0	1966	0.09	-8.9	0
129	SLU 6	-150	0	1966	0.09	-8.9	0
129	SLU 7	-150	0	1966	0.09	-8.9	0
129	SLU 8	-150	0	1966	0.09	-8.9	0
129	SLU 9	-150	0	1966	0.09	-8.9	0
129	SLU 10	-223	0	2362	0.11	-13	0
129	SLU 11	-223	0	2362	0.11	-13	0
129	SLU 12	-223	0	2362	0.11	-13	0
129	SLU 13	-223	0	2362	0.11	-13	0
129	SLU 14	-223	0	2362	0.11	-13	0
129	SLU 15	-223	0	2362	0.11	-13	0
129	SLU 16	-223	0	2362	0.11	-13	0
129	SLU 17	-223	0	2362	0.11	-13	0
129	SLU 18	-254	0	2532	0.12	-14.76	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
129	SLU 19	-254	0	2532	0.12	-14.76	0
129	SLU 20	-254	0	2532	0.12	-14.76	0
129	SLU 21	-254	0	2532	0.12	-14.76	0
129	SLU 22	-186	0	2199	0.11	-10.95	0
129	SLU 23	-186	0	2199	0.11	-10.95	0
129	SLU 24	-186	0	2199	0.11	-10.95	0
129	SLU 25	-186	0	2199	0.11	-10.95	0
129	SLU 26	-186	0	2199	0.11	-10.95	0
129	SLU 27	-186	0	2199	0.11	-10.95	0
129	SLU 28	-186	0	2199	0.11	-10.95	0
129	SLU 29	-186	0	2199	0.11	-10.95	0
129	SLU 30	-186	0	2199	0.11	-10.95	0
129	SLU 31	-259	0	2595	0.13	-15.06	0
129	SLU 32	-259	0	2595	0.13	-15.06	0
129	SLU 33	-259	0	2595	0.13	-15.06	0
129	SLU 34	-259	0	2595	0.13	-15.06	0
129	SLU 35	-259	0	2595	0.13	-15.06	0
129	SLU 36	-259	0	2595	0.13	-15.06	0
129	SLU 37	-259	0	2595	0.13	-15.06	0
129	SLU 38	-259	0	2595	0.13	-15.06	0
129	SLU 39	-290	0	2765	0.13	-16.82	0
129	SLU 40	-290	0	2765	0.13	-16.82	0
129	SLU 41	-290	0	2765	0.13	-16.82	0
129	SLU 42	-290	0	2765	0.13	-16.82	0
129	SLU 43	-183	0	2476	0.12	-10.86	0
129	SLU 44	-183	0	2476	0.12	-10.86	0
129	SLU 45	-183	0	2476	0.12	-10.86	0
129	SLU 46	-183	0	2476	0.12	-10.86	0
129	SLU 47	-183	0	2476	0.12	-10.86	0
129	SLU 48	-183	0	2476	0.12	-10.86	0
129	SLU 49	-183	0	2476	0.12	-10.86	0
129	SLU 50	-183	0	2476	0.12	-10.86	0
129	SLU 51	-183	0	2476	0.12	-10.86	0
129	SLU 52	-256	0	2872	0.14	-14.97	0
129	SLU 53	-256	0	2872	0.14	-14.97	0
129	SLU 54	-256	0	2872	0.14	-14.97	0
129	SLU 55	-256	0	2872	0.14	-14.97	0
129	SLU 56	-256	0	2872	0.14	-14.97	0
129	SLU 57	-256	0	2872	0.14	-14.97	0
129	SLU 58	-256	0	2872	0.14	-14.97	0
129	SLU 59	-256	0	2872	0.14	-14.97	0
129	SLU 60	-287	0	3041	0.15	-16.73	0
129	SLU 61	-287	0	3041	0.15	-16.73	0
129	SLU 62	-287	0	3041	0.15	-16.73	0
129	SLU 63	-287	0	3041	0.15	-16.73	0
129	SLU 64	-219	0	2709	0.13	-12.92	0
129	SLU 65	-219	0	2709	0.13	-12.92	0
129	SLU 66	-219	0	2709	0.13	-12.92	0
129	SLU 67	-219	0	2709	0.13	-12.92	0
129	SLU 68	-219	0	2709	0.13	-12.92	0
129	SLU 69	-219	0	2709	0.13	-12.92	0
129	SLU 70	-219	0	2709	0.13	-12.92	0
129	SLU 71	-219	0	2709	0.13	-12.92	0
129	SLU 72	-219	0	2709	0.13	-12.92	0
129	SLU 73	-292	0	3105	0.15	-17.02	0
129	SLU 74	-292	0	3105	0.15	-17.02	0
129	SLU 75	-292	0	3105	0.15	-17.02	0
129	SLU 76	-292	0	3105	0.15	-17.02	0
129	SLU 77	-292	0	3105	0.15	-17.02	0
129	SLU 78	-292	0	3105	0.15	-17.02	0
129	SLU 79	-292	0	3105	0.15	-17.02	0
129	SLU 80	-292	0	3105	0.15	-17.02	0
129	SLU 81	-323	0	3275	0.16	-18.78	0
129	SLU 82	-323	0	3275	0.16	-18.78	0
129	SLU 83	-323	0	3275	0.16	-18.78	0
129	SLU 84	-323	0	3275	0.16	-18.78	0
129	SLE RA 1	-160	0	2032	0.1	-9.48	0
129	SLE RA 2	-160	0	2032	0.1	-9.48	0
129	SLE RA 3	-160	0	2032	0.1	-9.48	0
129	SLE RA 4	-160	0	2032	0.1	-9.48	0
129	SLE RA 5	-160	0	2032	0.1	-9.48	0
129	SLE RA 6	-160	0	2032	0.1	-9.48	0
129	SLE RA 7	-160	0	2032	0.1	-9.48	0
129	SLE RA 8	-160	0	2032	0.1	-9.48	0
129	SLE RA 9	-160	0	2032	0.1	-9.48	0
129	SLE RA 10	-209	0	2296	0.11	-12.22	0
129	SLE RA 11	-209	0	2296	0.11	-12.22	0
129	SLE RA 12	-209	0	2296	0.11	-12.22	0
129	SLE RA 13	-209	0	2296	0.11	-12.22	0
129	SLE RA 14	-209	0	2296	0.11	-12.22	0
129	SLE RA 15	-209	0	2296	0.11	-12.22	0
129	SLE RA 16	-209	0	2296	0.11	-12.22	0
129	SLE RA 17	-209	0	2296	0.11	-12.22	0
129	SLE RA 18	-230	0	2410	0.12	-13.4	0
129	SLE RA 19	-230	0	2410	0.12	-13.4	0
129	SLE RA 20	-230	0	2410	0.12	-13.4	0
129	SLE RA 21	-230	0	2410	0.12	-13.4	0
129	SLE FR 1	-160	0	2032	0.1	-9.48	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione		
		x	y	z		x	y	z
129	SLE FR 2	-160	0	2032		0.1	-9.48	0
129	SLE FR 3	-160	0	2032		0.1	-9.48	0
129	SLE FR 4	-181	0	2146		0.1	-10.66	0
129	SLE FR 5	-181	0	2146		0.1	-10.66	0
129	SLE FR 6	-195	0	2221		0.11	-11.44	0
129	SLE QP 1	-160	0	2032		0.1	-9.48	0
129	SLE QP 2	-181	0	2146		0.1	-10.66	0
129	SLD 1	35	-5	2085		2.09	1.19	-0.01
129	SLD 2	35	-5	2085		2.09	1.19	-0.01
129	SLD 3	20	-23	2124		28.42	0.42	-0.08
129	SLD 4	20	-23	2124		28.42	0.42	-0.08
129	SLD 5	-94	26	2068		-39.24	-5.94	0.1
129	SLD 6	-94	26	2068		-39.24	-5.94	0.1
129	SLD 7	-143	-35	2198		48.53	-8.5	-0.13
129	SLD 8	-143	-35	2198		48.53	-8.5	-0.13
129	SLD 9	-219	35	2093		-48.32	-12.82	0.13
129	SLD 10	-219	35	2093		-48.32	-12.82	0.13
129	SLD 11	-269	-26	2223		39.44	-15.37	-0.1
129	SLD 12	-269	-26	2223		39.44	-15.37	-0.1
129	SLD 13	-383	23	2168		-28.21	-21.74	0.08
129	SLD 14	-383	23	2168		-28.21	-21.74	0.08
129	SLD 15	-398	5	2206		-1.88	-22.51	0.01
129	SLD 16	-398	5	2206		-1.88	-22.51	0.01
129	SLV 1	330	-12	2001		3.41	17.36	-0.03
129	SLV 2	330	-12	2001		3.41	17.36	-0.03
129	SLV 3	294	-58	2097		73.93	15.47	-0.21
129	SLV 4	294	-58	2097		73.93	15.47	-0.21
129	SLV 5	27	68	1957		-105.85	0.61	0.25
129	SLV 6	27	68	1957		-105.85	0.61	0.25
129	SLV 7	-93	-89	2276		129.2	-5.68	-0.32
129	SLV 8	-93	-89	2276		129.2	-5.68	-0.32
129	SLV 9	-269	89	2015		-128.99	-15.63	0.32
129	SLV 10	-269	89	2015		-128.99	-15.63	0.32
129	SLV 11	-389	-68	2334		106.06	-21.93	-0.25
129	SLV 12	-389	-68	2334		106.06	-21.93	-0.25
129	SLV 13	-656	58	2194		-73.72	-36.78	0.21
129	SLV 14	-656	58	2194		-73.72	-36.78	0.21
129	SLV 15	-692	12	2290		-3.21	-38.67	0.03
129	SLV 16	-692	12	2290		-3.21	-38.67	0.03
130	SLU 1	-136	0	1911		0.07	-7.37	0
130	SLU 2	-136	0	1911		0.07	-7.37	0
130	SLU 3	-136	0	1911		0.07	-7.37	0
130	SLU 4	-136	0	1911		0.07	-7.37	0
130	SLU 5	-136	0	1911		0.07	-7.37	0
130	SLU 6	-136	0	1911		0.07	-7.37	0
130	SLU 7	-136	0	1911		0.07	-7.37	0
130	SLU 8	-136	0	1911		0.07	-7.37	0
130	SLU 9	-136	0	1911		0.07	-7.37	0
130	SLU 10	-204	0	2298		0.08	-11.01	0
130	SLU 11	-204	0	2298		0.08	-11.01	0
130	SLU 12	-204	0	2298		0.08	-11.01	0
130	SLU 13	-204	0	2298		0.08	-11.01	0
130	SLU 14	-204	0	2298		0.08	-11.01	0
130	SLU 15	-204	0	2298		0.08	-11.01	0
130	SLU 16	-204	0	2298		0.08	-11.01	0
130	SLU 17	-204	0	2298		0.08	-11.01	0
130	SLU 18	-233	0	2464		0.09	-12.57	0
130	SLU 19	-233	0	2464		0.09	-12.57	0
130	SLU 20	-233	0	2464		0.09	-12.57	0
130	SLU 21	-233	0	2464		0.09	-12.57	0
130	SLU 22	-169	0	2139		0.08	-9.13	0
130	SLU 23	-169	0	2139		0.08	-9.13	0
130	SLU 24	-169	0	2139		0.08	-9.13	0
130	SLU 25	-169	0	2139		0.08	-9.13	0
130	SLU 26	-169	0	2139		0.08	-9.13	0
130	SLU 27	-169	0	2139		0.08	-9.13	0
130	SLU 28	-169	0	2139		0.08	-9.13	0
130	SLU 29	-169	0	2139		0.08	-9.13	0
130	SLU 30	-169	0	2139		0.08	-9.13	0
130	SLU 31	-237	0	2527		0.09	-12.77	0
130	SLU 32	-237	0	2527		0.09	-12.77	0
130	SLU 33	-237	0	2527		0.09	-12.77	0
130	SLU 34	-237	0	2527		0.09	-12.77	0
130	SLU 35	-237	0	2527		0.09	-12.77	0
130	SLU 36	-237	0	2527		0.09	-12.77	0
130	SLU 37	-237	0	2527		0.09	-12.77	0
130	SLU 38	-237	0	2527		0.09	-12.77	0
130	SLU 39	-266	0	2693		0.1	-14.33	0
130	SLU 40	-266	0	2693		0.1	-14.33	0
130	SLU 41	-266	0	2693		0.1	-14.33	0
130	SLU 42	-266	0	2693		0.1	-14.33	0
130	SLU 43	-165	0	2406		0.08	-8.97	0
130	SLU 44	-165	0	2406		0.08	-8.97	0
130	SLU 45	-165	0	2406		0.08	-8.97	0
130	SLU 46	-165	0	2406		0.08	-8.97	0
130	SLU 47	-165	0	2406		0.08	-8.97	0
130	SLU 48	-165	0	2406		0.08	-8.97	0
130	SLU 49	-165	0	2406		0.08	-8.97	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
130	SLU 50	-165	0	2406	0.08	-8.97	0
130	SLU 51	-165	0	2406	0.08	-8.97	0
130	SLU 52	-233	0	2793	0.1	-12.62	0
130	SLU 53	-233	0	2793	0.1	-12.62	0
130	SLU 54	-233	0	2793	0.1	-12.62	0
130	SLU 55	-233	0	2793	0.1	-12.62	0
130	SLU 56	-233	0	2793	0.1	-12.62	0
130	SLU 57	-233	0	2793	0.1	-12.62	0
130	SLU 58	-233	0	2793	0.1	-12.62	0
130	SLU 59	-233	0	2793	0.1	-12.62	0
130	SLU 60	-262	0	2959	0.1	-14.18	0
130	SLU 61	-262	0	2959	0.1	-14.18	0
130	SLU 62	-262	0	2959	0.1	-14.18	0
130	SLU 63	-262	0	2959	0.1	-14.18	0
130	SLU 64	-198	0	2634	0.09	-10.73	0
130	SLU 65	-198	0	2634	0.09	-10.73	0
130	SLU 66	-198	0	2634	0.09	-10.73	0
130	SLU 67	-198	0	2634	0.09	-10.73	0
130	SLU 68	-198	0	2634	0.09	-10.73	0
130	SLU 69	-198	0	2634	0.09	-10.73	0
130	SLU 70	-198	0	2634	0.09	-10.73	0
130	SLU 71	-198	0	2634	0.09	-10.73	0
130	SLU 72	-198	0	2634	0.09	-10.73	0
130	SLU 73	-266	0	3022	0.11	-14.38	0
130	SLU 74	-266	0	3022	0.11	-14.38	0
130	SLU 75	-266	0	3022	0.11	-14.38	0
130	SLU 76	-266	0	3022	0.11	-14.38	0
130	SLU 77	-266	0	3022	0.11	-14.38	0
130	SLU 78	-266	0	3022	0.11	-14.38	0
130	SLU 79	-266	0	3022	0.11	-14.38	0
130	SLU 80	-266	0	3022	0.11	-14.38	0
130	SLU 81	-295	0	3188	0.11	-15.94	0
130	SLU 82	-295	0	3188	0.11	-15.94	0
130	SLU 83	-295	0	3188	0.11	-15.94	0
130	SLU 84	-295	0	3188	0.11	-15.94	0
130	SLE RA 1	-145	0	1976	0.07	-7.87	0
130	SLE RA 2	-145	0	1976	0.07	-7.87	0
130	SLE RA 3	-145	0	1976	0.07	-7.87	0
130	SLE RA 4	-145	0	1976	0.07	-7.87	0
130	SLE RA 5	-145	0	1976	0.07	-7.87	0
130	SLE RA 6	-145	0	1976	0.07	-7.87	0
130	SLE RA 7	-145	0	1976	0.07	-7.87	0
130	SLE RA 8	-145	0	1976	0.07	-7.87	0
130	SLE RA 9	-145	0	1976	0.07	-7.87	0
130	SLE RA 10	-190	0	2234	0.08	-10.3	0
130	SLE RA 11	-190	0	2234	0.08	-10.3	0
130	SLE RA 12	-190	0	2234	0.08	-10.3	0
130	SLE RA 13	-190	0	2234	0.08	-10.3	0
130	SLE RA 14	-190	0	2234	0.08	-10.3	0
130	SLE RA 15	-190	0	2234	0.08	-10.3	0
130	SLE RA 16	-190	0	2234	0.08	-10.3	0
130	SLE RA 17	-190	0	2234	0.08	-10.3	0
130	SLE RA 18	-210	0	2345	0.08	-11.34	0
130	SLE RA 19	-210	0	2345	0.08	-11.34	0
130	SLE RA 20	-210	0	2345	0.08	-11.34	0
130	SLE RA 21	-210	0	2345	0.08	-11.34	0
130	SLE FR 1	-145	0	1976	0.07	-7.87	0
130	SLE FR 2	-145	0	1976	0.07	-7.87	0
130	SLE FR 3	-145	0	1976	0.07	-7.87	0
130	SLE FR 4	-165	0	2087	0.07	-8.91	0
130	SLE FR 5	-165	0	2087	0.07	-8.91	0
130	SLE FR 6	-178	0	2160	0.08	-9.61	0
130	SLE QP 1	-145	0	1976	0.07	-7.87	0
130	SLE QP 2	-165	0	2087	0.07	-8.91	0
130	SLD 1	63	-4	2035	1.07	3.55	-0.01
130	SLD 2	63	-4	2035	1.07	3.55	-0.01
130	SLD 3	50	-25	2064	32.25	2.88	-0.08
130	SLD 4	50	-25	2064	32.25	2.88	-0.08
130	SLD 5	-76	30	2026	-46.92	-4.16	0.12
130	SLD 6	-76	30	2026	-46.92	-4.16	0.12
130	SLD 7	-121	-39	2125	57.02	-6.39	-0.14
130	SLD 8	-121	-39	2125	57.02	-6.39	-0.14
130	SLD 9	-209	39	2048	-56.87	-11.44	0.14
130	SLD 10	-209	39	2048	-56.87	-11.44	0.14
130	SLD 11	-253	-30	2147	47.07	-13.66	-0.12
130	SLD 12	-253	-30	2147	47.07	-13.66	-0.12
130	SLD 13	-379	25	2109	-32.11	-20.7	0.08
130	SLD 14	-379	25	2109	-32.11	-20.7	0.08
130	SLD 15	-393	4	2138	-0.92	-21.37	0.01
130	SLD 16	-393	4	2138	-0.92	-21.37	0.01
130	SLV 1	374	-11	1963	0.29	20.53	-0.01
130	SLV 2	374	-11	1963	0.29	20.53	-0.01
130	SLV 3	341	-64	2038	84.69	18.9	-0.22
130	SLV 4	341	-64	2038	84.69	18.9	-0.22
130	SLV 5	47	78	1937	-127.87	2.38	0.31
130	SLV 6	47	78	1937	-127.87	2.38	0.31
130	SLV 7	-63	-101	2185	153.46	-3.03	-0.38
130	SLV 8	-63	-101	2185	153.46	-3.03	-0.38



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
130	SLV 9	-266	101	1989	-153.31	-14.79	0.38
130	SLV 10	-266	101	1989	-153.31	-14.79	0.38
130	SLV 11	-376	-78	2237	128.01	-20.21	-0.31
130	SLV 12	-376	-78	2237	128.01	-20.21	-0.31
130	SLV 13	-670	64	2136	-84.54	-36.73	0.22
130	SLV 14	-670	64	2136	-84.54	-36.73	0.22
130	SLV 15	-703	11	2210	-0.14	-38.35	0.01
130	SLV 16	-703	11	2210	-0.14	-38.35	0.01
131	SLU 1	-165	0	1896	0.05	-9.63	0
131	SLU 2	-165	0	1896	0.05	-9.63	0
131	SLU 3	-165	0	1896	0.05	-9.63	0
131	SLU 4	-165	0	1896	0.05	-9.63	0
131	SLU 5	-165	0	1896	0.05	-9.63	0
131	SLU 6	-165	0	1896	0.05	-9.63	0
131	SLU 7	-165	0	1896	0.05	-9.63	0
131	SLU 8	-165	0	1896	0.05	-9.63	0
131	SLU 9	-165	0	1896	0.05	-9.63	0
131	SLU 10	-240	0	2289	0.06	-13.95	0
131	SLU 11	-240	0	2289	0.06	-13.95	0
131	SLU 12	-240	0	2289	0.06	-13.95	0
131	SLU 13	-240	0	2289	0.06	-13.95	0
131	SLU 14	-240	0	2289	0.06	-13.95	0
131	SLU 15	-240	0	2289	0.06	-13.95	0
131	SLU 16	-240	0	2289	0.06	-13.95	0
131	SLU 17	-240	0	2289	0.06	-13.95	0
131	SLU 18	-273	0	2457	0.06	-15.8	0
131	SLU 19	-273	0	2457	0.06	-15.8	0
131	SLU 20	-273	0	2457	0.06	-15.8	0
131	SLU 21	-273	0	2457	0.06	-15.8	0
131	SLU 22	-202	0	2126	0.06	-11.77	0
131	SLU 23	-202	0	2126	0.06	-11.77	0
131	SLU 24	-202	0	2126	0.06	-11.77	0
131	SLU 25	-202	0	2126	0.06	-11.77	0
131	SLU 26	-202	0	2126	0.06	-11.77	0
131	SLU 27	-202	0	2126	0.06	-11.77	0
131	SLU 28	-202	0	2126	0.06	-11.77	0
131	SLU 29	-202	0	2126	0.06	-11.77	0
131	SLU 30	-202	0	2126	0.06	-11.77	0
131	SLU 31	-278	0	2519	0.07	-16.09	0
131	SLU 32	-278	0	2519	0.07	-16.09	0
131	SLU 33	-278	0	2519	0.07	-16.09	0
131	SLU 34	-278	0	2519	0.07	-16.09	0
131	SLU 35	-278	0	2519	0.07	-16.09	0
131	SLU 36	-278	0	2519	0.07	-16.09	0
131	SLU 37	-278	0	2519	0.07	-16.09	0
131	SLU 38	-278	0	2519	0.07	-16.09	0
131	SLU 39	-310	0	2687	0.07	-17.94	0
131	SLU 40	-310	0	2687	0.07	-17.94	0
131	SLU 41	-310	0	2687	0.07	-17.94	0
131	SLU 42	-310	0	2687	0.07	-17.94	0
131	SLU 43	-201	0	2386	0.06	-11.78	0
131	SLU 44	-201	0	2386	0.06	-11.78	0
131	SLU 45	-201	0	2386	0.06	-11.78	0
131	SLU 46	-201	0	2386	0.06	-11.78	0
131	SLU 47	-201	0	2386	0.06	-11.78	0
131	SLU 48	-201	0	2386	0.06	-11.78	0
131	SLU 49	-201	0	2386	0.06	-11.78	0
131	SLU 50	-201	0	2386	0.06	-11.78	0
131	SLU 51	-201	0	2386	0.06	-11.78	0
131	SLU 52	-277	0	2779	0.07	-16.1	0
131	SLU 53	-277	0	2779	0.07	-16.1	0
131	SLU 54	-277	0	2779	0.07	-16.1	0
131	SLU 55	-277	0	2779	0.07	-16.1	0
131	SLU 56	-277	0	2779	0.07	-16.1	0
131	SLU 57	-277	0	2779	0.07	-16.1	0
131	SLU 58	-277	0	2779	0.07	-16.1	0
131	SLU 59	-277	0	2779	0.07	-16.1	0
131	SLU 60	-309	0	2947	0.08	-17.96	0
131	SLU 61	-309	0	2947	0.08	-17.96	0
131	SLU 62	-309	0	2947	0.08	-17.96	0
131	SLU 63	-309	0	2947	0.08	-17.96	0
131	SLU 64	-238	0	2616	0.07	-13.92	0
131	SLU 65	-238	0	2616	0.07	-13.92	0
131	SLU 66	-238	0	2616	0.07	-13.92	0
131	SLU 67	-238	0	2616	0.07	-13.92	0
131	SLU 68	-238	0	2616	0.07	-13.92	0
131	SLU 69	-238	0	2616	0.07	-13.92	0
131	SLU 70	-238	0	2616	0.07	-13.92	0
131	SLU 71	-238	0	2616	0.07	-13.92	0
131	SLU 72	-238	0	2616	0.07	-13.92	0
131	SLU 73	-314	0	3009	0.08	-18.24	0
131	SLU 74	-314	0	3009	0.08	-18.24	0
131	SLU 75	-314	0	3009	0.08	-18.24	0
131	SLU 76	-314	0	3009	0.08	-18.24	0
131	SLU 77	-314	0	3009	0.08	-18.24	0
131	SLU 78	-314	0	3009	0.08	-18.24	0
131	SLU 79	-314	0	3009	0.08	-18.24	0
131	SLU 80	-314	0	3009	0.08	-18.24	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
131	SLU 81	-347	0	3177	0.08	-20.09	0
131	SLU 82	-347	0	3177	0.08	-20.09	0
131	SLU 83	-347	0	3177	0.08	-20.09	0
131	SLU 84	-347	0	3177	0.08	-20.09	0
131	SLE RA 1	-175	0	1962	0.05	-10.24	0
131	SLE RA 2	-175	0	1962	0.05	-10.24	0
131	SLE RA 3	-175	0	1962	0.05	-10.24	0
131	SLE RA 4	-175	0	1962	0.05	-10.24	0
131	SLE RA 5	-175	0	1962	0.05	-10.24	0
131	SLE RA 6	-175	0	1962	0.05	-10.24	0
131	SLE RA 7	-175	0	1962	0.05	-10.24	0
131	SLE RA 8	-175	0	1962	0.05	-10.24	0
131	SLE RA 9	-175	0	1962	0.05	-10.24	0
131	SLE RA 10	-226	0	2224	0.06	-13.12	0
131	SLE RA 11	-226	0	2224	0.06	-13.12	0
131	SLE RA 12	-226	0	2224	0.06	-13.12	0
131	SLE RA 13	-226	0	2224	0.06	-13.12	0
131	SLE RA 14	-226	0	2224	0.06	-13.12	0
131	SLE RA 15	-226	0	2224	0.06	-13.12	0
131	SLE RA 16	-226	0	2224	0.06	-13.12	0
131	SLE RA 17	-226	0	2224	0.06	-13.12	0
131	SLE RA 18	-247	0	2336	0.06	-14.35	0
131	SLE RA 19	-247	0	2336	0.06	-14.35	0
131	SLE RA 20	-247	0	2336	0.06	-14.35	0
131	SLE RA 21	-247	0	2336	0.06	-14.35	0
131	SLE FR 1	-175	0	1962	0.05	-10.24	0
131	SLE FR 2	-175	0	1962	0.05	-10.24	0
131	SLE FR 3	-175	0	1962	0.05	-10.24	0
131	SLE FR 4	-197	0	2074	0.05	-11.47	0
131	SLE FR 5	-197	0	2074	0.05	-11.47	0
131	SLE FR 6	-211	0	2149	0.06	-12.3	0
131	SLE QP 1	-175	0	1962	0.05	-10.24	0
131	SLE QP 2	-197	0	2074	0.05	-11.47	0
131	SLD 1	43	-4	2016	-0.33	2.04	-0.02
131	SLD 2	43	-4	2016	-0.33	2.04	-0.02
131	SLD 3	29	-26	2041	35.28	1.27	-0.14
131	SLD 4	29	-26	2041	35.28	1.27	-0.14
131	SLD 5	-104	32	2020	-54.07	-6.25	0.18
131	SLD 6	-104	32	2020	-54.07	-6.25	0.18
131	SLD 7	-150	-41	2101	64.63	-8.82	-0.23
131	SLD 8	-150	-41	2101	64.63	-8.82	-0.23
131	SLD 9	-244	41	2047	-64.52	-14.12	0.23
131	SLD 10	-244	41	2047	-64.52	-14.12	0.23
131	SLD 11	-289	-32	2128	54.18	-16.7	-0.18
131	SLD 12	-289	-32	2128	54.18	-16.7	-0.18
131	SLD 13	-423	26	2107	-35.17	-24.22	0.14
131	SLD 14	-423	26	2107	-35.17	-24.22	0.14
131	SLD 15	-436	4	2132	0.44	-24.99	0.02
131	SLD 16	-436	4	2132	0.44	-24.99	0.02
131	SLV 1	370	-10	1936	-4	20.53	-0.04
131	SLV 2	370	-10	1936	-4	20.53	-0.04
131	SLV 3	335	-68	2000	93.44	18.52	-0.37
131	SLV 4	335	-68	2000	93.44	18.52	-0.37
131	SLV 5	26	84	1936	-148.95	1.18	0.49
131	SLV 6	26	84	1936	-148.95	1.18	0.49
131	SLV 7	-90	-107	2148	175.85	-5.53	-0.61
131	SLV 8	-90	-107	2148	175.85	-5.53	-0.61
131	SLV 9	-304	107	2000	-175.75	-17.41	0.61
131	SLV 10	-304	107	2000	-175.75	-17.41	0.61
131	SLV 11	-420	-84	2212	149.05	-24.13	-0.49
131	SLV 12	-420	-84	2212	149.05	-24.13	-0.49
131	SLV 13	-729	68	2149	-93.33	-41.46	0.37
131	SLV 14	-729	68	2149	-93.33	-41.46	0.37
131	SLV 15	-764	10	2212	4.11	-43.48	0.04
131	SLV 16	-764	10	2212	4.11	-43.48	0.04
132	SLU 1	-177	0	1928	0.04	-9.34	0
132	SLU 2	-177	0	1928	0.04	-9.34	0
132	SLU 3	-177	0	1928	0.04	-9.34	0
132	SLU 4	-177	0	1928	0.04	-9.34	0
132	SLU 5	-177	0	1928	0.04	-9.34	0
132	SLU 6	-177	0	1928	0.04	-9.34	0
132	SLU 7	-177	0	1928	0.04	-9.34	0
132	SLU 8	-177	0	1928	0.04	-9.34	0
132	SLU 9	-177	0	1928	0.04	-9.34	0
132	SLU 10	-254	0	2340	0.04	-13.44	0
132	SLU 11	-254	0	2340	0.04	-13.44	0
132	SLU 12	-254	0	2340	0.04	-13.44	0
132	SLU 13	-254	0	2340	0.04	-13.44	0
132	SLU 14	-254	0	2340	0.04	-13.44	0
132	SLU 15	-254	0	2340	0.04	-13.44	0
132	SLU 16	-254	0	2340	0.04	-13.44	0
132	SLU 17	-254	0	2340	0.04	-13.44	0
132	SLU 18	-287	0	2516	0.05	-15.19	0
132	SLU 19	-287	0	2516	0.05	-15.19	0
132	SLU 20	-287	0	2516	0.05	-15.19	0
132	SLU 21	-287	0	2516	0.05	-15.19	0
132	SLU 22	-215	0	2168	0.04	-11.36	0
132	SLU 23	-215	0	2168	0.04	-11.36	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
132	SLU 24	-215	0	2168	0.04	-11.36	0
132	SLU 25	-215	0	2168	0.04	-11.36	0
132	SLU 26	-215	0	2168	0.04	-11.36	0
132	SLU 27	-215	0	2168	0.04	-11.36	0
132	SLU 28	-215	0	2168	0.04	-11.36	0
132	SLU 29	-215	0	2168	0.04	-11.36	0
132	SLU 30	-215	0	2168	0.04	-11.36	0
132	SLU 31	-293	0	2579	0.05	-15.45	0
132	SLU 32	-293	0	2579	0.05	-15.45	0
132	SLU 33	-293	0	2579	0.05	-15.45	0
132	SLU 34	-293	0	2579	0.05	-15.45	0
132	SLU 35	-293	0	2579	0.05	-15.45	0
132	SLU 36	-293	0	2579	0.05	-15.45	0
132	SLU 37	-293	0	2579	0.05	-15.45	0
132	SLU 38	-293	0	2579	0.05	-15.45	0
132	SLU 39	-326	0	2755	0.05	-17.21	0
132	SLU 40	-326	0	2755	0.05	-17.21	0
132	SLU 41	-326	0	2755	0.05	-17.21	0
132	SLU 42	-326	0	2755	0.05	-17.21	0
132	SLU 43	-217	0	2424	0.05	-11.46	0
132	SLU 44	-217	0	2424	0.05	-11.46	0
132	SLU 45	-217	0	2424	0.05	-11.46	0
132	SLU 46	-217	0	2424	0.05	-11.46	0
132	SLU 47	-217	0	2424	0.05	-11.46	0
132	SLU 48	-217	0	2424	0.05	-11.46	0
132	SLU 49	-217	0	2424	0.05	-11.46	0
132	SLU 50	-217	0	2424	0.05	-11.46	0
132	SLU 51	-217	0	2424	0.05	-11.46	0
132	SLU 52	-294	0	2836	0.05	-15.55	0
132	SLU 53	-294	0	2836	0.05	-15.55	0
132	SLU 54	-294	0	2836	0.05	-15.55	0
132	SLU 55	-294	0	2836	0.05	-15.55	0
132	SLU 56	-294	0	2836	0.05	-15.55	0
132	SLU 57	-294	0	2836	0.05	-15.55	0
132	SLU 58	-294	0	2836	0.05	-15.55	0
132	SLU 59	-294	0	2836	0.05	-15.55	0
132	SLU 60	-327	0	3012	0.06	-17.3	0
132	SLU 61	-327	0	3012	0.06	-17.3	0
132	SLU 62	-327	0	3012	0.06	-17.3	0
132	SLU 63	-327	0	3012	0.06	-17.3	0
132	SLU 64	-255	0	2664	0.05	-13.47	0
132	SLU 65	-255	0	2664	0.05	-13.47	0
132	SLU 66	-255	0	2664	0.05	-13.47	0
132	SLU 67	-255	0	2664	0.05	-13.47	0
132	SLU 68	-255	0	2664	0.05	-13.47	0
132	SLU 69	-255	0	2664	0.05	-13.47	0
132	SLU 70	-255	0	2664	0.05	-13.47	0
132	SLU 71	-255	0	2664	0.05	-13.47	0
132	SLU 72	-255	0	2664	0.05	-13.47	0
132	SLU 73	-333	0	3075	0.06	-17.56	0
132	SLU 74	-333	0	3075	0.06	-17.56	0
132	SLU 75	-333	0	3075	0.06	-17.56	0
132	SLU 76	-333	0	3075	0.06	-17.56	0
132	SLU 77	-333	0	3075	0.06	-17.56	0
132	SLU 78	-333	0	3075	0.06	-17.56	0
132	SLU 79	-333	0	3075	0.06	-17.56	0
132	SLU 80	-333	0	3075	0.06	-17.56	0
132	SLU 81	-366	0	3252	0.06	-19.32	0
132	SLU 82	-366	0	3252	0.06	-19.32	0
132	SLU 83	-366	0	3252	0.06	-19.32	0
132	SLU 84	-366	0	3252	0.06	-19.32	0
132	SLE RA 1	-188	0	1996	0.04	-9.92	0
132	SLE RA 2	-188	0	1996	0.04	-9.92	0
132	SLE RA 3	-188	0	1996	0.04	-9.92	0
132	SLE RA 4	-188	0	1996	0.04	-9.92	0
132	SLE RA 5	-188	0	1996	0.04	-9.92	0
132	SLE RA 6	-188	0	1996	0.04	-9.92	0
132	SLE RA 7	-188	0	1996	0.04	-9.92	0
132	SLE RA 8	-188	0	1996	0.04	-9.92	0
132	SLE RA 9	-188	0	1996	0.04	-9.92	0
132	SLE RA 10	-239	0	2271	0.04	-12.65	0
132	SLE RA 11	-239	0	2271	0.04	-12.65	0
132	SLE RA 12	-239	0	2271	0.04	-12.65	0
132	SLE RA 13	-239	0	2271	0.04	-12.65	0
132	SLE RA 14	-239	0	2271	0.04	-12.65	0
132	SLE RA 15	-239	0	2271	0.04	-12.65	0
132	SLE RA 16	-239	0	2271	0.04	-12.65	0
132	SLE RA 17	-239	0	2271	0.04	-12.65	0
132	SLE RA 18	-262	0	2388	0.04	-13.82	0
132	SLE RA 19	-262	0	2388	0.04	-13.82	0
132	SLE RA 20	-262	0	2388	0.04	-13.82	0
132	SLE RA 21	-262	0	2388	0.04	-13.82	0
132	SLE FR 1	-188	0	1996	0.04	-9.92	0
132	SLE FR 2	-188	0	1996	0.04	-9.92	0
132	SLE FR 3	-188	0	1996	0.04	-9.92	0
132	SLE FR 4	-210	0	2114	0.04	-11.09	0
132	SLE FR 5	-210	0	2114	0.04	-11.09	0
132	SLE FR 6	-225	0	2192	0.04	-11.87	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
132	SLE QP 1	-188	0	1996	0.04	-9.92	0
132	SLE QP 2	-210	0	2114	0.04	-11.09	0
132	SLD 1	29	-4	2041	-2.25	2.26	-0.02
132	SLD 2	29	-4	2041	-2.25	2.26	-0.02
132	SLD 3	16	-27	2065	37.84	1.6	-0.18
132	SLD 4	16	-27	2065	37.84	1.6	-0.18
132	SLD 5	-118	33	2056	-61.45	-6.09	0.23
132	SLD 6	-118	33	2056	-61.45	-6.09	0.23
132	SLD 7	-162	-42	2135	72.19	-8.27	-0.29
132	SLD 8	-162	-42	2135	72.19	-8.27	-0.29
132	SLD 9	-258	42	2093	-72.11	-13.91	0.29
132	SLD 10	-258	42	2093	-72.11	-13.91	0.29
132	SLD 11	-302	-33	2172	61.53	-16.08	-0.23
132	SLD 12	-302	-33	2172	61.53	-16.08	-0.23
132	SLD 13	-436	27	2163	-37.76	-23.78	0.18
132	SLD 14	-436	27	2163	-37.76	-23.78	0.18
132	SLD 15	-449	4	2187	2.33	-24.43	0.02
132	SLD 16	-449	4	2187	2.33	-24.43	0.02
132	SLV 1	356	-10	1938	-9.87	20.49	-0.05
132	SLV 2	356	-10	1938	-9.87	20.49	-0.05
132	SLV 3	322	-70	2003	101	18.8	-0.47
132	SLV 4	322	-70	2003	101	18.8	-0.47
132	SLV 5	12	88	1964	-171.09	0.95	0.62
132	SLV 6	12	88	1964	-171.09	0.95	0.62
132	SLV 7	-103	-112	2178	198.49	-4.69	-0.77
132	SLV 8	-103	-112	2178	198.49	-4.69	-0.77
132	SLV 9	-317	112	2050	-198.41	-17.49	0.78
132	SLV 10	-317	112	2050	-198.41	-17.49	0.78
132	SLV 11	-432	-88	2264	171.17	-23.12	-0.62
132	SLV 12	-432	-88	2264	171.17	-23.12	-0.62
132	SLV 13	-742	70	2225	-100.93	-40.97	0.47
132	SLV 14	-742	70	2225	-100.93	-40.97	0.47
132	SLV 15	-776	10	2290	9.95	-42.66	0.05
132	SLV 16	-776	10	2290	9.95	-42.66	0.05
133	SLU 1	-194	0	1997	0.02	-10.47	0
133	SLU 2	-194	0	1997	0.02	-10.47	0
133	SLU 3	-194	0	1997	0.02	-10.47	0
133	SLU 4	-194	0	1997	0.02	-10.47	0
133	SLU 5	-194	0	1997	0.02	-10.47	0
133	SLU 6	-194	0	1997	0.02	-10.47	0
133	SLU 7	-194	0	1997	0.02	-10.47	0
133	SLU 8	-194	0	1997	0.02	-10.47	0
133	SLU 9	-194	0	1997	0.02	-10.47	0
133	SLU 10	-273	0	2438	0.03	-14.73	0
133	SLU 11	-273	0	2438	0.03	-14.73	0
133	SLU 12	-273	0	2438	0.03	-14.73	0
133	SLU 13	-273	0	2438	0.03	-14.73	0
133	SLU 14	-273	0	2438	0.03	-14.73	0
133	SLU 15	-273	0	2438	0.03	-14.73	0
133	SLU 16	-273	0	2438	0.03	-14.73	0
133	SLU 17	-273	0	2438	0.03	-14.73	0
133	SLU 18	-307	0	2627	0.03	-16.56	0
133	SLU 19	-307	0	2627	0.03	-16.56	0
133	SLU 20	-307	0	2627	0.03	-16.56	0
133	SLU 21	-307	0	2627	0.03	-16.56	0
133	SLU 22	-234	0	2252	0.03	-12.61	0
133	SLU 23	-234	0	2252	0.03	-12.61	0
133	SLU 24	-234	0	2252	0.03	-12.61	0
133	SLU 25	-234	0	2252	0.03	-12.61	0
133	SLU 26	-234	0	2252	0.03	-12.61	0
133	SLU 27	-234	0	2252	0.03	-12.61	0
133	SLU 28	-234	0	2252	0.03	-12.61	0
133	SLU 29	-234	0	2252	0.03	-12.61	0
133	SLU 30	-234	0	2252	0.03	-12.61	0
133	SLU 31	-313	0	2693	0.03	-16.87	0
133	SLU 32	-313	0	2693	0.03	-16.87	0
133	SLU 33	-313	0	2693	0.03	-16.87	0
133	SLU 34	-313	0	2693	0.03	-16.87	0
133	SLU 35	-313	0	2693	0.03	-16.87	0
133	SLU 36	-313	0	2693	0.03	-16.87	0
133	SLU 37	-313	0	2693	0.03	-16.87	0
133	SLU 38	-313	0	2693	0.03	-16.87	0
133	SLU 39	-347	0	2882	0.03	-18.7	0
133	SLU 40	-347	0	2882	0.03	-18.7	0
133	SLU 41	-347	0	2882	0.03	-18.7	0
133	SLU 42	-347	0	2882	0.03	-18.7	0
133	SLU 43	-239	0	2508	0.03	-12.88	0
133	SLU 44	-239	0	2508	0.03	-12.88	0
133	SLU 45	-239	0	2508	0.03	-12.88	0
133	SLU 46	-239	0	2508	0.03	-12.88	0
133	SLU 47	-239	0	2508	0.03	-12.88	0
133	SLU 48	-239	0	2508	0.03	-12.88	0
133	SLU 49	-239	0	2508	0.03	-12.88	0
133	SLU 50	-239	0	2508	0.03	-12.88	0
133	SLU 51	-239	0	2508	0.03	-12.88	0
133	SLU 52	-318	0	2949	0.03	-17.14	0
133	SLU 53	-318	0	2949	0.03	-17.14	0
133	SLU 54	-318	0	2949	0.03	-17.14	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
133	SLU 55	-318	0	2949	0.03	-17.14	0
133	SLU 56	-318	0	2949	0.03	-17.14	0
133	SLU 57	-318	0	2949	0.03	-17.14	0
133	SLU 58	-318	0	2949	0.03	-17.14	0
133	SLU 59	-318	0	2949	0.03	-17.14	0
133	SLU 60	-352	0	3138	0.04	-18.97	0
133	SLU 61	-352	0	3138	0.04	-18.97	0
133	SLU 62	-352	0	3138	0.04	-18.97	0
133	SLU 63	-352	0	3138	0.04	-18.97	0
133	SLU 64	-279	0	2763	0.03	-15.02	0
133	SLU 65	-279	0	2763	0.03	-15.02	0
133	SLU 66	-279	0	2763	0.03	-15.02	0
133	SLU 67	-279	0	2763	0.03	-15.02	0
133	SLU 68	-279	0	2763	0.03	-15.02	0
133	SLU 69	-279	0	2763	0.03	-15.02	0
133	SLU 70	-279	0	2763	0.03	-15.02	0
133	SLU 71	-279	0	2763	0.03	-15.02	0
133	SLU 72	-279	0	2763	0.03	-15.02	0
133	SLU 73	-358	0	3204	0.04	-19.28	0
133	SLU 74	-358	0	3204	0.04	-19.28	0
133	SLU 75	-358	0	3204	0.04	-19.28	0
133	SLU 76	-358	0	3204	0.04	-19.28	0
133	SLU 77	-358	0	3204	0.04	-19.28	0
133	SLU 78	-358	0	3204	0.04	-19.28	0
133	SLU 79	-358	0	3204	0.04	-19.28	0
133	SLU 80	-358	0	3204	0.04	-19.28	0
133	SLU 81	-392	0	3393	0.04	-21.11	0
133	SLU 82	-392	0	3393	0.04	-21.11	0
133	SLU 83	-392	0	3393	0.04	-21.11	0
133	SLU 84	-392	0	3393	0.04	-21.11	0
133	SLE RA 1	-206	0	2070	0.02	-11.08	0
133	SLE RA 2	-206	0	2070	0.02	-11.08	0
133	SLE RA 3	-206	0	2070	0.02	-11.08	0
133	SLE RA 4	-206	0	2070	0.02	-11.08	0
133	SLE RA 5	-206	0	2070	0.02	-11.08	0
133	SLE RA 6	-206	0	2070	0.02	-11.08	0
133	SLE RA 7	-206	0	2070	0.02	-11.08	0
133	SLE RA 8	-206	0	2070	0.02	-11.08	0
133	SLE RA 9	-206	0	2070	0.02	-11.08	0
133	SLE RA 10	-258	0	2364	0.03	-13.92	0
133	SLE RA 11	-258	0	2364	0.03	-13.92	0
133	SLE RA 12	-258	0	2364	0.03	-13.92	0
133	SLE RA 13	-258	0	2364	0.03	-13.92	0
133	SLE RA 14	-258	0	2364	0.03	-13.92	0
133	SLE RA 15	-258	0	2364	0.03	-13.92	0
133	SLE RA 16	-258	0	2364	0.03	-13.92	0
133	SLE RA 17	-258	0	2364	0.03	-13.92	0
133	SLE RA 18	-281	0	2490	0.03	-15.14	0
133	SLE RA 19	-281	0	2490	0.03	-15.14	0
133	SLE RA 20	-281	0	2490	0.03	-15.14	0
133	SLE RA 21	-281	0	2490	0.03	-15.14	0
133	SLE FR 1	-206	0	2070	0.02	-11.08	0
133	SLE FR 2	-206	0	2070	0.02	-11.08	0
133	SLE FR 3	-206	0	2070	0.02	-11.08	0
133	SLE FR 4	-228	0	2196	0.03	-12.3	0
133	SLE FR 5	-228	0	2196	0.03	-12.3	0
133	SLE FR 6	-243	0	2280	0.03	-13.11	0
133	SLE QP 1	-206	0	2070	0.02	-11.08	0
133	SLE QP 2	-228	0	2196	0.03	-12.3	0
133	SLD 1	6	-4	2108	-4.96	0.7	-0.04
133	SLD 2	6	-4	2108	-4.96	0.7	-0.04
133	SLD 3	-8	-28	2135	40.34	-0.14	-0.21
133	SLD 4	-8	-28	2135	40.34	-0.14	-0.21
133	SLD 5	-136	35	2128	-70.17	-7.13	0.25
133	SLD 6	-136	35	2128	-70.17	-7.13	0.25
133	SLD 7	-184	-44	2218	80.82	-9.93	-0.32
133	SLD 8	-184	-44	2218	80.82	-9.93	-0.32
133	SLD 9	-272	44	2173	-80.77	-14.67	0.32
133	SLD 10	-272	44	2173	-80.77	-14.67	0.32
133	SLD 11	-321	-35	2263	70.22	-17.47	-0.25
133	SLD 12	-321	-35	2263	70.22	-17.47	-0.25
133	SLD 13	-448	28	2256	-40.29	-24.46	0.21
133	SLD 14	-448	28	2256	-40.29	-24.46	0.21
133	SLD 15	-463	4	2283	5.01	-25.3	0.04
133	SLD 16	-463	4	2283	5.01	-25.3	0.04
133	SLV 1	328	-9	1985	-18.08	18.54	-0.08
133	SLV 2	328	-9	1985	-18.08	18.54	-0.08
133	SLV 3	289	-73	2060	108.35	16.25	-0.55
133	SLV 4	289	-73	2060	108.35	16.25	-0.55
133	SLV 5	-1	96	2019	-197.16	0.43	0.68
133	SLV 6	-1	96	2019	-197.16	0.43	0.68
133	SLV 7	-133	-120	2268	224.28	-7.21	-0.87
133	SLV 8	-133	-120	2268	224.28	-7.21	-0.87
133	SLV 9	-323	120	2123	-224.23	-17.39	0.87
133	SLV 10	-323	120	2123	-224.23	-17.39	0.87
133	SLV 11	-455	-95	2373	197.21	-25.03	-0.68
133	SLV 12	-455	-95	2373	197.21	-25.03	-0.68
133	SLV 13	-745	73	2332	-108.3	-40.85	0.55



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
133	SLV 14	-745	73	2332	-108.3	-40.85	0.55
133	SLV 15	-785	9	2407	18.13	-43.14	0.08
133	SLV 16	-785	9	2407	18.13	-43.14	0.08
134	SLU 1	-175	0	2084	0.01	-8.6	0
134	SLU 2	-175	0	2084	0.01	-8.6	0
134	SLU 3	-175	0	2084	0.01	-8.6	0
134	SLU 4	-175	0	2084	0.01	-8.6	0
134	SLU 5	-175	0	2084	0.01	-8.6	0
134	SLU 6	-175	0	2084	0.01	-8.6	0
134	SLU 7	-175	0	2084	0.01	-8.6	0
134	SLU 8	-175	0	2084	0.01	-8.6	0
134	SLU 9	-175	0	2084	0.01	-8.6	0
134	SLU 10	-244	0	2558	0.01	-12.01	0
134	SLU 11	-244	0	2558	0.01	-12.01	0
134	SLU 12	-244	0	2558	0.01	-12.01	0
134	SLU 13	-244	0	2558	0.01	-12.01	0
134	SLU 14	-244	0	2558	0.01	-12.01	0
134	SLU 15	-244	0	2558	0.01	-12.01	0
134	SLU 16	-244	0	2558	0.01	-12.01	0
134	SLU 17	-244	0	2558	0.01	-12.01	0
134	SLU 18	-273	0	2761	0.01	-13.47	0
134	SLU 19	-273	0	2761	0.01	-13.47	0
134	SLU 20	-273	0	2761	0.01	-13.47	0
134	SLU 21	-273	0	2761	0.01	-13.47	0
134	SLU 22	-210	0	2356	0.01	-10.31	0
134	SLU 23	-210	0	2356	0.01	-10.31	0
134	SLU 24	-210	0	2356	0.01	-10.31	0
134	SLU 25	-210	0	2356	0.01	-10.31	0
134	SLU 26	-210	0	2356	0.01	-10.31	0
134	SLU 27	-210	0	2356	0.01	-10.31	0
134	SLU 28	-210	0	2356	0.01	-10.31	0
134	SLU 29	-210	0	2356	0.01	-10.31	0
134	SLU 30	-210	0	2356	0.01	-10.31	0
134	SLU 31	-279	0	2830	0.01	-13.72	0
134	SLU 32	-279	0	2830	0.01	-13.72	0
134	SLU 33	-279	0	2830	0.01	-13.72	0
134	SLU 34	-279	0	2830	0.01	-13.72	0
134	SLU 35	-279	0	2830	0.01	-13.72	0
134	SLU 36	-279	0	2830	0.01	-13.72	0
134	SLU 37	-279	0	2830	0.01	-13.72	0
134	SLU 38	-279	0	2830	0.01	-13.72	0
134	SLU 39	-308	0	3034	0.01	-15.18	0
134	SLU 40	-308	0	3034	0.01	-15.18	0
134	SLU 41	-308	0	3034	0.01	-15.18	0
134	SLU 42	-308	0	3034	0.01	-15.18	0
134	SLU 43	-216	0	2616	0.01	-10.59	0
134	SLU 44	-216	0	2616	0.01	-10.59	0
134	SLU 45	-216	0	2616	0.01	-10.59	0
134	SLU 46	-216	0	2616	0.01	-10.59	0
134	SLU 47	-216	0	2616	0.01	-10.59	0
134	SLU 48	-216	0	2616	0.01	-10.59	0
134	SLU 49	-216	0	2616	0.01	-10.59	0
134	SLU 50	-216	0	2616	0.01	-10.59	0
134	SLU 51	-216	0	2616	0.01	-10.59	0
134	SLU 52	-285	0	3090	0.02	-14	0
134	SLU 53	-285	0	3090	0.02	-14	0
134	SLU 54	-285	0	3090	0.02	-14	0
134	SLU 55	-285	0	3090	0.02	-14	0
134	SLU 56	-285	0	3090	0.02	-14	0
134	SLU 57	-285	0	3090	0.02	-14	0
134	SLU 58	-285	0	3090	0.02	-14	0
134	SLU 59	-285	0	3090	0.02	-14	0
134	SLU 60	-314	0	3293	0.02	-15.46	0
134	SLU 61	-314	0	3293	0.02	-15.46	0
134	SLU 62	-314	0	3293	0.02	-15.46	0
134	SLU 63	-314	0	3293	0.02	-15.46	0
134	SLU 64	-250	0	2888	0.01	-12.3	0
134	SLU 65	-250	0	2888	0.01	-12.3	0
134	SLU 66	-250	0	2888	0.01	-12.3	0
134	SLU 67	-250	0	2888	0.01	-12.3	0
134	SLU 68	-250	0	2888	0.01	-12.3	0
134	SLU 69	-250	0	2888	0.01	-12.3	0
134	SLU 70	-250	0	2888	0.01	-12.3	0
134	SLU 71	-250	0	2888	0.01	-12.3	0
134	SLU 72	-250	0	2888	0.01	-12.3	0
134	SLU 73	-319	0	3362	0.02	-15.71	0
134	SLU 74	-319	0	3362	0.02	-15.71	0
134	SLU 75	-319	0	3362	0.02	-15.71	0
134	SLU 76	-319	0	3362	0.02	-15.71	0
134	SLU 77	-319	0	3362	0.02	-15.71	0
134	SLU 78	-319	0	3362	0.02	-15.71	0
134	SLU 79	-319	0	3362	0.02	-15.71	0
134	SLU 80	-319	0	3362	0.02	-15.71	0
134	SLU 81	-349	0	3565	0.02	-17.17	0
134	SLU 82	-349	0	3565	0.02	-17.17	0
134	SLU 83	-349	0	3565	0.02	-17.17	0
134	SLU 84	-349	0	3565	0.02	-17.17	0
134	SLE RA 1	-185	0	2162	0.01	-9.08	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
134	SLE RA 2	-185	0	2162	0.01	-9.08	0
134	SLE RA 3	-185	0	2162	0.01	-9.08	0
134	SLE RA 4	-185	0	2162	0.01	-9.08	0
134	SLE RA 5	-185	0	2162	0.01	-9.08	0
134	SLE RA 6	-185	0	2162	0.01	-9.08	0
134	SLE RA 7	-185	0	2162	0.01	-9.08	0
134	SLE RA 8	-185	0	2162	0.01	-9.08	0
134	SLE RA 9	-185	0	2162	0.01	-9.08	0
134	SLE RA 10	-231	0	2478	0.01	-11.36	0
134	SLE RA 11	-231	0	2478	0.01	-11.36	0
134	SLE RA 12	-231	0	2478	0.01	-11.36	0
134	SLE RA 13	-231	0	2478	0.01	-11.36	0
134	SLE RA 14	-231	0	2478	0.01	-11.36	0
134	SLE RA 15	-231	0	2478	0.01	-11.36	0
134	SLE RA 16	-231	0	2478	0.01	-11.36	0
134	SLE RA 17	-231	0	2478	0.01	-11.36	0
134	SLE RA 18	-251	0	2613	0.01	-12.33	0
134	SLE RA 19	-251	0	2613	0.01	-12.33	0
134	SLE RA 20	-251	0	2613	0.01	-12.33	0
134	SLE RA 21	-251	0	2613	0.01	-12.33	0
134	SLE FR 1	-185	0	2162	0.01	-9.08	0
134	SLE FR 2	-185	0	2162	0.01	-9.08	0
134	SLE FR 3	-185	0	2162	0.01	-9.08	0
134	SLE FR 4	-205	0	2297	0.01	-10.06	0
134	SLE FR 5	-205	0	2297	0.01	-10.06	0
134	SLE FR 6	-218	0	2387	0.01	-10.71	0
134	SLE QP 1	-185	0	2162	0.01	-9.08	0
134	SLE QP 2	-205	0	2297	0.01	-10.06	0
134	SLD 1	21	31	2202	-8.87	2.2	0.17
134	SLD 2	21	31	2202	-8.87	2.2	0.17
134	SLD 3	7	3	2235	42.97	1.53	0.01
134	SLD 4	7	3	2235	42.97	1.53	0.01
134	SLD 5	-115	51	2219	-81.27	-5.36	0.29
134	SLD 6	-115	51	2219	-81.27	-5.36	0.29
134	SLD 7	-163	-41	2328	91.51	-7.6	-0.24
134	SLD 8	-163	-41	2328	91.51	-7.6	-0.24
134	SLD 9	-247	41	2266	-91.49	-12.51	0.24
134	SLD 10	-247	41	2266	-91.49	-12.51	0.24
134	SLD 11	-294	-51	2375	81.29	-14.76	-0.29
134	SLD 12	-294	-51	2375	81.29	-14.76	-0.29
134	SLD 13	-417	-3	2359	-42.94	-21.65	-0.01
134	SLD 14	-417	-3	2359	-42.94	-21.65	-0.01
134	SLD 15	-431	-31	2392	8.89	-22.32	-0.17
134	SLD 16	-431	-31	2392	8.89	-22.32	-0.17
134	SLV 1	332	81	2068	-29.59	19	0.45
134	SLV 2	332	81	2068	-29.59	19	0.45
134	SLV 3	293	3	2160	116.04	17.18	0.01
134	SLV 4	293	3	2160	116.04	17.18	0.01
134	SLV 5	16	142	2089	-229.74	1.42	0.8
134	SLV 6	16	142	2089	-229.74	1.42	0.8
134	SLV 7	-115	-117	2395	255.69	-4.65	-0.66
134	SLV 8	-115	-117	2395	255.69	-4.65	-0.66
134	SLV 9	-294	117	2199	-255.66	-15.47	0.66
134	SLV 10	-294	117	2199	-255.66	-15.47	0.66
134	SLV 11	-425	-142	2505	229.76	-21.54	-0.8
134	SLV 12	-425	-142	2505	229.76	-21.54	-0.8
134	SLV 13	-702	-3	2435	-116.01	-37.3	-0.01
134	SLV 14	-702	-3	2435	-116.01	-37.3	-0.01
134	SLV 15	-741	-81	2527	29.62	-39.12	-0.45
134	SLV 16	-741	-81	2527	29.62	-39.12	-0.45
135	SLU 1	-145	0	2161	0	-7.27	0
135	SLU 2	-145	0	2161	0	-7.27	0
135	SLU 3	-145	0	2161	0	-7.27	0
135	SLU 4	-145	0	2161	0	-7.27	0
135	SLU 5	-145	0	2161	0	-7.27	0
135	SLU 6	-145	0	2161	0	-7.27	0
135	SLU 7	-145	0	2161	0	-7.27	0
135	SLU 8	-145	0	2161	0	-7.27	0
135	SLU 9	-145	0	2161	0	-7.27	0
135	SLU 10	-200	0	2663	0	-10.07	0
135	SLU 11	-200	0	2663	0	-10.07	0
135	SLU 12	-200	0	2663	0	-10.07	0
135	SLU 13	-200	0	2663	0	-10.07	0
135	SLU 14	-200	0	2663	0	-10.07	0
135	SLU 15	-200	0	2663	0	-10.07	0
135	SLU 16	-200	0	2663	0	-10.07	0
135	SLU 17	-200	0	2663	0	-10.07	0
135	SLU 18	-224	0	2878	0	-11.27	0
135	SLU 19	-224	0	2878	0	-11.27	0
135	SLU 20	-224	0	2878	0	-11.27	0
135	SLU 21	-224	0	2878	0	-11.27	0
135	SLU 22	-173	0	2448	0	-8.67	0
135	SLU 23	-173	0	2448	0	-8.67	0
135	SLU 24	-173	0	2448	0	-8.67	0
135	SLU 25	-173	0	2448	0	-8.67	0
135	SLU 26	-173	0	2448	0	-8.67	0
135	SLU 27	-173	0	2448	0	-8.67	0
135	SLU 28	-173	0	2448	0	-8.67	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
135	SLU 29	-173	0	2448	0	-8.67	0
135	SLU 30	-173	0	2448	0	-8.67	0
135	SLU 31	-228	0	2950	0	-11.47	0
135	SLU 32	-228	0	2950	0	-11.47	0
135	SLU 33	-228	0	2950	0	-11.47	0
135	SLU 34	-228	0	2950	0	-11.47	0
135	SLU 35	-228	0	2950	0	-11.47	0
135	SLU 36	-228	0	2950	0	-11.47	0
135	SLU 37	-228	0	2950	0	-11.47	0
135	SLU 38	-228	0	2950	0	-11.47	0
135	SLU 39	-252	0	3165	0	-12.68	0
135	SLU 40	-252	0	3165	0	-12.68	0
135	SLU 41	-252	0	3165	0	-12.68	0
135	SLU 42	-252	0	3165	0	-12.68	0
135	SLU 43	-179	0	2710	0	-8.97	0
135	SLU 44	-179	0	2710	0	-8.97	0
135	SLU 45	-179	0	2710	0	-8.97	0
135	SLU 46	-179	0	2710	0	-8.97	0
135	SLU 47	-179	0	2710	0	-8.97	0
135	SLU 48	-179	0	2710	0	-8.97	0
135	SLU 49	-179	0	2710	0	-8.97	0
135	SLU 50	-179	0	2710	0	-8.97	0
135	SLU 51	-179	0	2710	0	-8.97	0
135	SLU 52	-234	0	3213	0	-11.77	0
135	SLU 53	-234	0	3213	0	-11.77	0
135	SLU 54	-234	0	3213	0	-11.77	0
135	SLU 55	-234	0	3213	0	-11.77	0
135	SLU 56	-234	0	3213	0	-11.77	0
135	SLU 57	-234	0	3213	0	-11.77	0
135	SLU 58	-234	0	3213	0	-11.77	0
135	SLU 59	-234	0	3213	0	-11.77	0
135	SLU 60	-258	0	3428	0	-12.97	0
135	SLU 61	-258	0	3428	0	-12.97	0
135	SLU 62	-258	0	3428	0	-12.97	0
135	SLU 63	-258	0	3428	0	-12.97	0
135	SLU 64	-207	0	2998	0	-10.37	0
135	SLU 65	-207	0	2998	0	-10.37	0
135	SLU 66	-207	0	2998	0	-10.37	0
135	SLU 67	-207	0	2998	0	-10.37	0
135	SLU 68	-207	0	2998	0	-10.37	0
135	SLU 69	-207	0	2998	0	-10.37	0
135	SLU 70	-207	0	2998	0	-10.37	0
135	SLU 71	-207	0	2998	0	-10.37	0
135	SLU 72	-207	0	2998	0	-10.37	0
135	SLU 73	-262	0	3500	0	-13.17	0
135	SLU 74	-262	0	3500	0	-13.17	0
135	SLU 75	-262	0	3500	0	-13.17	0
135	SLU 76	-262	0	3500	0	-13.17	0
135	SLU 77	-262	0	3500	0	-13.17	0
135	SLU 78	-262	0	3500	0	-13.17	0
135	SLU 79	-262	0	3500	0	-13.17	0
135	SLU 80	-262	0	3500	0	-13.17	0
135	SLU 81	-286	0	3715	0	-14.37	0
135	SLU 82	-286	0	3715	0	-14.37	0
135	SLU 83	-286	0	3715	0	-14.37	0
135	SLU 84	-286	0	3715	0	-14.37	0
135	SLE RA 1	-153	0	2243	0	-7.67	0
135	SLE RA 2	-153	0	2243	0	-7.67	0
135	SLE RA 3	-153	0	2243	0	-7.67	0
135	SLE RA 4	-153	0	2243	0	-7.67	0
135	SLE RA 5	-153	0	2243	0	-7.67	0
135	SLE RA 6	-153	0	2243	0	-7.67	0
135	SLE RA 7	-153	0	2243	0	-7.67	0
135	SLE RA 8	-153	0	2243	0	-7.67	0
135	SLE RA 9	-153	0	2243	0	-7.67	0
135	SLE RA 10	-190	0	2578	0	-9.54	0
135	SLE RA 11	-190	0	2578	0	-9.54	0
135	SLE RA 12	-190	0	2578	0	-9.54	0
135	SLE RA 13	-190	0	2578	0	-9.54	0
135	SLE RA 14	-190	0	2578	0	-9.54	0
135	SLE RA 15	-190	0	2578	0	-9.54	0
135	SLE RA 16	-190	0	2578	0	-9.54	0
135	SLE RA 17	-190	0	2578	0	-9.54	0
135	SLE RA 18	-206	0	2721	0	-10.34	0
135	SLE RA 19	-206	0	2721	0	-10.34	0
135	SLE RA 20	-206	0	2721	0	-10.34	0
135	SLE RA 21	-206	0	2721	0	-10.34	0
135	SLE FR 1	-153	0	2243	0	-7.67	0
135	SLE FR 2	-153	0	2243	0	-7.67	0
135	SLE FR 3	-153	0	2243	0	-7.67	0
135	SLE FR 4	-169	0	2386	0	-8.47	0
135	SLE FR 5	-169	0	2386	0	-8.47	0
135	SLE FR 6	-179	0	2482	0	-9	0
135	SLE QP 1	-153	0	2243	0	-7.67	0
135	SLE QP 2	-169	0	2386	0	-8.47	0
135	SLD 1	50	35	2295	-45.53	3.08	0.15
135	SLD 2	50	35	2295	-45.53	3.08	0.15
135	SLD 3	35	-2	2335	14.31	2.26	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
135	SLD 4	35	-2	2335	14.31	2.26	-0.01
135	SLD 5	-80	65	2298	-104.43	-3.76	0.29
135	SLD 6	-80	65	2298	-104.43	-3.76	0.29
135	SLD 7	-131	-55	2432	95.06	-6.49	-0.24
135	SLD 8	-131	-55	2432	95.06	-6.49	-0.24
135	SLD 9	-206	55	2340	-95.06	-10.45	0.24
135	SLD 10	-206	55	2340	-95.06	-10.45	0.24
135	SLD 11	-258	-65	2475	104.42	-13.18	-0.29
135	SLD 12	-258	-65	2475	104.42	-13.18	-0.29
135	SLD 13	-372	2	2438	-14.32	-19.2	0.01
135	SLD 14	-372	2	2438	-14.32	-19.2	0.01
135	SLD 15	-388	-35	2478	45.53	-20.02	-0.15
135	SLD 16	-388	-35	2478	45.53	-20.02	-0.15
135	SLV 1	351	92	2162	-123.65	18.97	0.41
135	SLV 2	351	92	2162	-123.65	18.97	0.41
135	SLV 3	308	-10	2275	45.08	16.7	-0.04
135	SLV 4	308	-10	2275	45.08	16.7	-0.04
135	SLV 5	52	182	2147	-293.01	3.2	0.8
135	SLV 6	52	182	2147	-293.01	3.2	0.8
135	SLV 7	-90	-157	2525	269.44	-4.36	-0.69
135	SLV 8	-90	-157	2525	269.44	-4.36	-0.69
135	SLV 9	-247	158	2248	-269.44	-12.58	0.69
135	SLV 10	-247	158	2248	-269.44	-12.58	0.69
135	SLV 11	-389	-182	2625	293.01	-20.14	-0.8
135	SLV 12	-389	-182	2625	293.01	-20.14	-0.8
135	SLV 13	-646	10	2497	-45.09	-33.64	0.04
135	SLV 14	-646	10	2497	-45.09	-33.64	0.04
135	SLV 15	-688	-92	2610	123.65	-35.91	-0.41
135	SLV 16	-688	-92	2610	123.65	-35.91	-0.41
136	SLU 1	-103	0	2217	-0.01	-4.86	0
136	SLU 2	-103	0	2217	-0.01	-4.86	0
136	SLU 3	-103	0	2217	-0.01	-4.86	0
136	SLU 4	-103	0	2217	-0.01	-4.86	0
136	SLU 5	-103	0	2217	-0.01	-4.86	0
136	SLU 6	-103	0	2217	-0.01	-4.86	0
136	SLU 7	-103	0	2217	-0.01	-4.86	0
136	SLU 8	-103	0	2217	-0.01	-4.86	0
136	SLU 9	-103	0	2217	-0.01	-4.86	0
136	SLU 10	-141	0	2739	-0.01	-6.69	0
136	SLU 11	-141	0	2739	-0.01	-6.69	0
136	SLU 12	-141	0	2739	-0.01	-6.69	0
136	SLU 13	-141	0	2739	-0.01	-6.69	0
136	SLU 14	-141	0	2739	-0.01	-6.69	0
136	SLU 15	-141	0	2739	-0.01	-6.69	0
136	SLU 16	-141	0	2739	-0.01	-6.69	0
136	SLU 17	-141	0	2739	-0.01	-6.69	0
136	SLU 18	-157	0	2963	-0.02	-7.47	0
136	SLU 19	-157	0	2963	-0.02	-7.47	0
136	SLU 20	-157	0	2963	-0.02	-7.47	0
136	SLU 21	-157	0	2963	-0.02	-7.47	0
136	SLU 22	-122	0	2515	-0.01	-5.77	0
136	SLU 23	-122	0	2515	-0.01	-5.77	0
136	SLU 24	-122	0	2515	-0.01	-5.77	0
136	SLU 25	-122	0	2515	-0.01	-5.77	0
136	SLU 26	-122	0	2515	-0.01	-5.77	0
136	SLU 27	-122	0	2515	-0.01	-5.77	0
136	SLU 28	-122	0	2515	-0.01	-5.77	0
136	SLU 29	-122	0	2515	-0.01	-5.77	0
136	SLU 30	-122	0	2515	-0.01	-5.77	0
136	SLU 31	-160	0	3037	-0.02	-7.6	0
136	SLU 32	-160	0	3037	-0.02	-7.6	0
136	SLU 33	-160	0	3037	-0.02	-7.6	0
136	SLU 34	-160	0	3037	-0.02	-7.6	0
136	SLU 35	-160	0	3037	-0.02	-7.6	0
136	SLU 36	-160	0	3037	-0.02	-7.6	0
136	SLU 37	-160	0	3037	-0.02	-7.6	0
136	SLU 38	-160	0	3037	-0.02	-7.6	0
136	SLU 39	-177	0	3260	-0.02	-8.38	0
136	SLU 40	-177	0	3260	-0.02	-8.38	0
136	SLU 41	-177	0	3260	-0.02	-8.38	0
136	SLU 42	-177	0	3260	-0.02	-8.38	0
136	SLU 43	-127	0	2781	-0.01	-6.01	0
136	SLU 44	-127	0	2781	-0.01	-6.01	0
136	SLU 45	-127	0	2781	-0.01	-6.01	0
136	SLU 46	-127	0	2781	-0.01	-6.01	0
136	SLU 47	-127	0	2781	-0.01	-6.01	0
136	SLU 48	-127	0	2781	-0.01	-6.01	0
136	SLU 49	-127	0	2781	-0.01	-6.01	0
136	SLU 50	-127	0	2781	-0.01	-6.01	0
136	SLU 51	-127	0	2781	-0.01	-6.01	0
136	SLU 52	-165	0	3302	-0.02	-7.83	0
136	SLU 53	-165	0	3302	-0.02	-7.83	0
136	SLU 54	-165	0	3302	-0.02	-7.83	0
136	SLU 55	-165	0	3302	-0.02	-7.83	0
136	SLU 56	-165	0	3302	-0.02	-7.83	0
136	SLU 57	-165	0	3302	-0.02	-7.83	0
136	SLU 58	-165	0	3302	-0.02	-7.83	0
136	SLU 59	-165	0	3302	-0.02	-7.83	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
136	SLU 60	-182	0	3526	-0.02	-8.62	0
136	SLU 61	-182	0	3526	-0.02	-8.62	0
136	SLU 62	-182	0	3526	-0.02	-8.62	0
136	SLU 63	-182	0	3526	-0.02	-8.62	0
136	SLU 64	-146	0	3078	-0.02	-6.92	0
136	SLU 65	-146	0	3078	-0.02	-6.92	0
136	SLU 66	-146	0	3078	-0.02	-6.92	0
136	SLU 67	-146	0	3078	-0.02	-6.92	0
136	SLU 68	-146	0	3078	-0.02	-6.92	0
136	SLU 69	-146	0	3078	-0.02	-6.92	0
136	SLU 70	-146	0	3078	-0.02	-6.92	0
136	SLU 71	-146	0	3078	-0.02	-6.92	0
136	SLU 72	-146	0	3078	-0.02	-6.92	0
136	SLU 73	-184	0	3600	-0.02	-8.75	0
136	SLU 74	-184	0	3600	-0.02	-8.75	0
136	SLU 75	-184	0	3600	-0.02	-8.75	0
136	SLU 76	-184	0	3600	-0.02	-8.75	0
136	SLU 77	-184	0	3600	-0.02	-8.75	0
136	SLU 78	-184	0	3600	-0.02	-8.75	0
136	SLU 79	-184	0	3600	-0.02	-8.75	0
136	SLU 80	-184	0	3600	-0.02	-8.75	0
136	SLU 81	-201	0	3824	-0.02	-9.53	0
136	SLU 82	-201	0	3824	-0.02	-9.53	0
136	SLU 83	-201	0	3824	-0.02	-9.53	0
136	SLU 84	-201	0	3824	-0.02	-9.53	0
136	SLE RA 1	-108	0	2302	-0.01	-5.12	0
136	SLE RA 2	-108	0	2302	-0.01	-5.12	0
136	SLE RA 3	-108	0	2302	-0.01	-5.12	0
136	SLE RA 4	-108	0	2302	-0.01	-5.12	0
136	SLE RA 5	-108	0	2302	-0.01	-5.12	0
136	SLE RA 6	-108	0	2302	-0.01	-5.12	0
136	SLE RA 7	-108	0	2302	-0.01	-5.12	0
136	SLE RA 8	-108	0	2302	-0.01	-5.12	0
136	SLE RA 9	-108	0	2302	-0.01	-5.12	0
136	SLE RA 10	-134	0	2650	-0.01	-6.34	0
136	SLE RA 11	-134	0	2650	-0.01	-6.34	0
136	SLE RA 12	-134	0	2650	-0.01	-6.34	0
136	SLE RA 13	-134	0	2650	-0.01	-6.34	0
136	SLE RA 14	-134	0	2650	-0.01	-6.34	0
136	SLE RA 15	-134	0	2650	-0.01	-6.34	0
136	SLE RA 16	-134	0	2650	-0.01	-6.34	0
136	SLE RA 17	-134	0	2650	-0.01	-6.34	0
136	SLE RA 18	-145	0	2799	-0.01	-6.86	0
136	SLE RA 19	-145	0	2799	-0.01	-6.86	0
136	SLE RA 20	-145	0	2799	-0.01	-6.86	0
136	SLE RA 21	-145	0	2799	-0.01	-6.86	0
136	SLE FR 1	-108	0	2302	-0.01	-5.12	0
136	SLE FR 2	-108	0	2302	-0.01	-5.12	0
136	SLE FR 3	-108	0	2302	-0.01	-5.12	0
136	SLE FR 4	-119	0	2452	-0.01	-5.64	0
136	SLE FR 5	-119	0	2452	-0.01	-5.64	0
136	SLE FR 6	-126	0	2551	-0.01	-5.99	0
136	SLE QP 1	-108	0	2302	-0.01	-5.12	0
136	SLE QP 2	-119	0	2452	-0.01	-5.64	0
136	SLD 1	96	39	2370	-47.53	5.5	0.13
136	SLD 2	96	39	2370	-47.53	5.5	0.13
136	SLD 3	82	-9	2419	21.27	4.89	-0.02
136	SLD 4	82	-9	2419	21.27	4.89	-0.02
136	SLD 5	-34	84	2353	-118.62	-1.37	0.27
136	SLD 6	-34	84	2353	-118.62	-1.37	0.27
136	SLD 7	-80	-75	2516	110.72	-3.42	-0.24
136	SLD 8	-80	-75	2516	110.72	-3.42	-0.24
136	SLD 9	-159	76	2388	-110.75	-7.87	0.24
136	SLD 10	-159	76	2388	-110.75	-7.87	0.24
136	SLD 11	-204	-84	2550	118.59	-9.92	-0.27
136	SLD 12	-204	-84	2550	118.59	-9.92	-0.27
136	SLD 13	-320	9	2484	-21.3	-16.18	0.02
136	SLD 14	-320	9	2484	-21.3	-16.18	0.02
136	SLD 15	-334	-39	2533	47.5	-16.79	-0.13
136	SLD 16	-334	-39	2533	47.5	-16.79	-0.13
136	SLV 1	391	104	2249	-129.96	20.79	0.35
136	SLV 2	391	104	2249	-129.96	20.79	0.35
136	SLV 3	353	-31	2386	64.29	19.11	-0.09
136	SLV 4	353	-31	2386	64.29	19.11	-0.09
136	SLV 5	91	237	2183	-333.61	4.83	0.76
136	SLV 6	91	237	2183	-333.61	4.83	0.76
136	SLV 7	-35	-215	2639	313.89	-0.77	-0.68
136	SLV 8	-35	-215	2639	313.89	-0.77	-0.68
136	SLV 9	-204	215	2264	-313.92	-10.52	0.68
136	SLV 10	-204	215	2264	-313.92	-10.52	0.68
136	SLV 11	-329	-237	2720	333.59	-16.12	-0.76
136	SLV 12	-329	-237	2720	333.59	-16.12	-0.76
136	SLV 13	-591	31	2517	-64.31	-30.4	0.09
136	SLV 14	-591	31	2517	-64.31	-30.4	0.09
136	SLV 15	-629	-104	2654	129.94	-32.07	-0.35
136	SLV 16	-629	-104	2654	129.94	-32.07	-0.35
137	SLU 1	-64	0	2250	-0.01	-3.12	0
137	SLU 2	-64	0	2250	-0.01	-3.12	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione			
		x	y	z		x	y	z	
137	SLU 3	-64	0	2250		-0.01	-3.12	0	0
137	SLU 4	-64	0	2250		-0.01	-3.12	0	0
137	SLU 5	-64	0	2250		-0.01	-3.12	0	0
137	SLU 6	-64	0	2250		-0.01	-3.12	0	0
137	SLU 7	-64	0	2250		-0.01	-3.12	0	0
137	SLU 8	-64	0	2250		-0.01	-3.12	0	0
137	SLU 9	-64	0	2250		-0.01	-3.12	0	0
137	SLU 10	-88	0	2783		-0.01	-4.3	0	0
137	SLU 11	-88	0	2783		-0.01	-4.3	0	0
137	SLU 12	-88	0	2783		-0.01	-4.3	0	0
137	SLU 13	-88	0	2783		-0.01	-4.3	0	0
137	SLU 14	-88	0	2783		-0.01	-4.3	0	0
137	SLU 15	-88	0	2783		-0.01	-4.3	0	0
137	SLU 16	-88	0	2783		-0.01	-4.3	0	0
137	SLU 17	-88	0	2783		-0.01	-4.3	0	0
137	SLU 18	-98	0	3011		-0.02	-4.81	0	0
137	SLU 19	-98	0	3011		-0.02	-4.81	0	0
137	SLU 20	-98	0	3011		-0.02	-4.81	0	0
137	SLU 21	-98	0	3011		-0.02	-4.81	0	0
137	SLU 22	-76	0	2554		-0.01	-3.7	0	0
137	SLU 23	-76	0	2554		-0.01	-3.7	0	0
137	SLU 24	-76	0	2554		-0.01	-3.7	0	0
137	SLU 25	-76	0	2554		-0.01	-3.7	0	0
137	SLU 26	-76	0	2554		-0.01	-3.7	0	0
137	SLU 27	-76	0	2554		-0.01	-3.7	0	0
137	SLU 28	-76	0	2554		-0.01	-3.7	0	0
137	SLU 29	-76	0	2554		-0.01	-3.7	0	0
137	SLU 30	-76	0	2554		-0.01	-3.7	0	0
137	SLU 31	-99	0	3086		-0.02	-4.88	0	0
137	SLU 32	-99	0	3086		-0.02	-4.88	0	0
137	SLU 33	-99	0	3086		-0.02	-4.88	0	0
137	SLU 34	-99	0	3086		-0.02	-4.88	0	0
137	SLU 35	-99	0	3086		-0.02	-4.88	0	0
137	SLU 36	-99	0	3086		-0.02	-4.88	0	0
137	SLU 37	-99	0	3086		-0.02	-4.88	0	0
137	SLU 38	-99	0	3086		-0.02	-4.88	0	0
137	SLU 39	-109	0	3314		-0.02	-5.38	0	0
137	SLU 40	-109	0	3314		-0.02	-5.38	0	0
137	SLU 41	-109	0	3314		-0.02	-5.38	0	0
137	SLU 42	-109	0	3314		-0.02	-5.38	0	0
137	SLU 43	-79	0	2821		-0.02	-3.86	0	0
137	SLU 44	-79	0	2821		-0.02	-3.86	0	0
137	SLU 45	-79	0	2821		-0.02	-3.86	0	0
137	SLU 46	-79	0	2821		-0.02	-3.86	0	0
137	SLU 47	-79	0	2821		-0.02	-3.86	0	0
137	SLU 48	-79	0	2821		-0.02	-3.86	0	0
137	SLU 49	-79	0	2821		-0.02	-3.86	0	0
137	SLU 50	-79	0	2821		-0.02	-3.86	0	0
137	SLU 51	-79	0	2821		-0.02	-3.86	0	0
137	SLU 52	-103	0	3354		-0.02	-5.04	0	0
137	SLU 53	-103	0	3354		-0.02	-5.04	0	0
137	SLU 54	-103	0	3354		-0.02	-5.04	0	0
137	SLU 55	-103	0	3354		-0.02	-5.04	0	0
137	SLU 56	-103	0	3354		-0.02	-5.04	0	0
137	SLU 57	-103	0	3354		-0.02	-5.04	0	0
137	SLU 58	-103	0	3354		-0.02	-5.04	0	0
137	SLU 59	-103	0	3354		-0.02	-5.04	0	0
137	SLU 60	-113	0	3582		-0.02	-5.54	0	0
137	SLU 61	-113	0	3582		-0.02	-5.54	0	0
137	SLU 62	-113	0	3582		-0.02	-5.54	0	0
137	SLU 63	-113	0	3582		-0.02	-5.54	0	0
137	SLU 64	-91	0	3125		-0.02	-4.44	0	0
137	SLU 65	-91	0	3125		-0.02	-4.44	0	0
137	SLU 66	-91	0	3125		-0.02	-4.44	0	0
137	SLU 67	-91	0	3125		-0.02	-4.44	0	0
137	SLU 68	-91	0	3125		-0.02	-4.44	0	0
137	SLU 69	-91	0	3125		-0.02	-4.44	0	0
137	SLU 70	-91	0	3125		-0.02	-4.44	0	0
137	SLU 71	-91	0	3125		-0.02	-4.44	0	0
137	SLU 72	-91	0	3125		-0.02	-4.44	0	0
137	SLU 73	-114	0	3657		-0.02	-5.62	0	0
137	SLU 74	-114	0	3657		-0.02	-5.62	0	0
137	SLU 75	-114	0	3657		-0.02	-5.62	0	0
137	SLU 76	-114	0	3657		-0.02	-5.62	0	0
137	SLU 77	-114	0	3657		-0.02	-5.62	0	0
137	SLU 78	-114	0	3657		-0.02	-5.62	0	0
137	SLU 79	-114	0	3657		-0.02	-5.62	0	0
137	SLU 80	-114	0	3657		-0.02	-5.62	0	0
137	SLU 81	-125	0	3886		-0.02	-6.12	0	0
137	SLU 82	-125	0	3886		-0.02	-6.12	0	0
137	SLU 83	-125	0	3886		-0.02	-6.12	0	0
137	SLU 84	-125	0	3886		-0.02	-6.12	0	0
137	SLE RA 1	-67	0	2337		-0.01	-3.29	0	0
137	SLE RA 2	-67	0	2337		-0.01	-3.29	0	0
137	SLE RA 3	-67	0	2337		-0.01	-3.29	0	0
137	SLE RA 4	-67	0	2337		-0.01	-3.29	0	0
137	SLE RA 5	-67	0	2337		-0.01	-3.29	0	0
137	SLE RA 6	-67	0	2337		-0.01	-3.29	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione		
		x	y	z		x	y	z
137	SLE RA 7	-67	0	2337		-0.01	-3.29	0
137	SLE RA 8	-67	0	2337		-0.01	-3.29	0
137	SLE RA 9	-67	0	2337		-0.01	-3.29	0
137	SLE RA 10	-83	0	2692		-0.01	-4.07	0
137	SLE RA 11	-83	0	2692		-0.01	-4.07	0
137	SLE RA 12	-83	0	2692		-0.01	-4.07	0
137	SLE RA 13	-83	0	2692		-0.01	-4.07	0
137	SLE RA 14	-83	0	2692		-0.01	-4.07	0
137	SLE RA 15	-83	0	2692		-0.01	-4.07	0
137	SLE RA 16	-83	0	2692		-0.01	-4.07	0
137	SLE RA 17	-83	0	2692		-0.01	-4.07	0
137	SLE RA 18	-90	0	2844		-0.02	-4.41	0
137	SLE RA 19	-90	0	2844		-0.02	-4.41	0
137	SLE RA 20	-90	0	2844		-0.02	-4.41	0
137	SLE RA 21	-90	0	2844		-0.02	-4.41	0
137	SLE FR 1	-67	0	2337		-0.01	-3.29	0
137	SLE FR 2	-67	0	2337		-0.01	-3.29	0
137	SLE FR 3	-67	0	2337		-0.01	-3.29	0
137	SLE FR 4	-74	0	2489		-0.01	-3.63	0
137	SLE FR 5	-74	0	2489		-0.01	-3.63	0
137	SLE FR 6	-79	0	2591		-0.01	-3.85	0
137	SLE QP 1	-67	0	2337		-0.01	-3.29	0
137	SLE QP 2	-74	0	2489		-0.01	-3.63	0
137	SLD 1	138	42	2422		-48.35	7.06	0.09
137	SLD 2	138	42	2422		-48.35	7.06	0.09
137	SLD 3	125	-19	2479		29.29	6.46	-0.03
137	SLD 4	125	-19	2479		29.29	6.46	-0.03
137	SLD 5	8	107	2383		-132.27	0.49	0.22
137	SLD 6	8	107	2383		-132.27	0.49	0.22
137	SLD 7	-33	-100	2572		126.53	-1.52	-0.2
137	SLD 8	-33	-100	2572		126.53	-1.52	-0.2
137	SLD 9	-115	100	2406		-126.56	-5.74	0.2
137	SLD 10	-115	100	2406		-126.56	-5.74	0.2
137	SLD 11	-156	-106	2595		132.24	-7.75	-0.22
137	SLD 12	-156	-106	2595		132.24	-7.75	-0.22
137	SLD 13	-273	20	2499		-29.32	-13.71	0.03
137	SLD 14	-273	20	2499		-29.32	-13.71	0.03
137	SLD 15	-286	-42	2556		48.32	-14.31	-0.09
137	SLD 16	-286	-42	2556		48.32	-14.31	-0.09
137	SLV 1	428	115	2320		-133.38	21.72	0.25
137	SLV 2	428	115	2320		-133.38	21.72	0.25
137	SLV 3	395	-59	2479		85.86	20.07	-0.1
137	SLV 4	395	-59	2479		85.86	20.07	-0.1
137	SLV 5	127	299	2197		-372.53	6.49	0.61
137	SLV 6	127	299	2197		-372.53	6.49	0.61
137	SLV 7	16	-282	2728		358.25	0.97	-0.57
137	SLV 8	16	-282	2728		358.25	0.97	-0.57
137	SLV 9	-164	282	2250		-358.28	-8.22	0.57
137	SLV 10	-164	282	2250		-358.28	-8.22	0.57
137	SLV 11	-275	-299	2782		372.5	-13.74	-0.61
137	SLV 12	-275	-299	2782		372.5	-13.74	-0.61
137	SLV 13	-543	59	2499		-85.89	-27.32	0.1
137	SLV 14	-543	59	2499		-85.89	-27.32	0.1
137	SLV 15	-576	-115	2659		133.35	-28.97	-0.25
137	SLV 16	-576	-115	2659		133.35	-28.97	-0.25
138	SLU 1	-29	0	2267		-0.01	-1.3	0
138	SLU 2	-29	0	2267		-0.01	-1.3	0
138	SLU 3	-29	0	2267		-0.01	-1.3	0
138	SLU 4	-29	0	2267		-0.01	-1.3	0
138	SLU 5	-29	0	2267		-0.01	-1.3	0
138	SLU 6	-29	0	2267		-0.01	-1.3	0
138	SLU 7	-29	0	2267		-0.01	-1.3	0
138	SLU 8	-29	0	2267		-0.01	-1.3	0
138	SLU 9	-29	0	2267		-0.01	-1.3	0
138	SLU 10	-39	0	2804		-0.01	-1.75	0
138	SLU 11	-39	0	2804		-0.01	-1.75	0
138	SLU 12	-39	0	2804		-0.01	-1.75	0
138	SLU 13	-39	0	2804		-0.01	-1.75	0
138	SLU 14	-39	0	2804		-0.01	-1.75	0
138	SLU 15	-39	0	2804		-0.01	-1.75	0
138	SLU 16	-39	0	2804		-0.01	-1.75	0
138	SLU 17	-39	0	2804		-0.01	-1.75	0
138	SLU 18	-44	0	3034		-0.01	-1.94	0
138	SLU 19	-44	0	3034		-0.01	-1.94	0
138	SLU 20	-44	0	3034		-0.01	-1.94	0
138	SLU 21	-44	0	3034		-0.01	-1.94	0
138	SLU 22	-34	0	2572		-0.01	-1.53	0
138	SLU 23	-34	0	2572		-0.01	-1.53	0
138	SLU 24	-34	0	2572		-0.01	-1.53	0
138	SLU 25	-34	0	2572		-0.01	-1.53	0
138	SLU 26	-34	0	2572		-0.01	-1.53	0
138	SLU 27	-34	0	2572		-0.01	-1.53	0
138	SLU 28	-34	0	2572		-0.01	-1.53	0
138	SLU 29	-34	0	2572		-0.01	-1.53	0
138	SLU 30	-34	0	2572		-0.01	-1.53	0
138	SLU 31	-44	0	3110		-0.01	-1.97	0
138	SLU 32	-44	0	3110		-0.01	-1.97	0
138	SLU 33	-44	0	3110		-0.01	-1.97	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione			
		x	y	z		x	y	z	
138	SLU 34	-44	0	3110		-0.01	-1.97	0	
138	SLU 35	-44	0	3110		-0.01	-1.97	0	
138	SLU 36	-44	0	3110		-0.01	-1.97	0	
138	SLU 37	-44	0	3110		-0.01	-1.97	0	
138	SLU 38	-44	0	3110		-0.01	-1.97	0	
138	SLU 39	-49	0	3340		-0.01	-2.17	0	
138	SLU 40	-49	0	3340		-0.01	-2.17	0	
138	SLU 41	-49	0	3340		-0.01	-2.17	0	
138	SLU 42	-49	0	3340		-0.01	-2.17	0	
138	SLU 43	-36	0	2842		-0.01	-1.61	0	
138	SLU 44	-36	0	2842		-0.01	-1.61	0	
138	SLU 45	-36	0	2842		-0.01	-1.61	0	
138	SLU 46	-36	0	2842		-0.01	-1.61	0	
138	SLU 47	-36	0	2842		-0.01	-1.61	0	
138	SLU 48	-36	0	2842		-0.01	-1.61	0	
138	SLU 49	-36	0	2842		-0.01	-1.61	0	
138	SLU 50	-36	0	2842		-0.01	-1.61	0	
138	SLU 51	-36	0	2842		-0.01	-1.61	0	
138	SLU 52	-46	0	3379		-0.01	-2.06	0	
138	SLU 53	-46	0	3379		-0.01	-2.06	0	
138	SLU 54	-46	0	3379		-0.01	-2.06	0	
138	SLU 55	-46	0	3379		-0.01	-2.06	0	
138	SLU 56	-46	0	3379		-0.01	-2.06	0	
138	SLU 57	-46	0	3379		-0.01	-2.06	0	
138	SLU 58	-46	0	3379		-0.01	-2.06	0	
138	SLU 59	-46	0	3379		-0.01	-2.06	0	
138	SLU 60	-51	0	3610		-0.01	-2.25	0	
138	SLU 61	-51	0	3610		-0.01	-2.25	0	
138	SLU 62	-51	0	3610		-0.01	-2.25	0	
138	SLU 63	-51	0	3610		-0.01	-2.25	0	
138	SLU 64	-41	0	3148		-0.01	-1.84	0	
138	SLU 65	-41	0	3148		-0.01	-1.84	0	
138	SLU 66	-41	0	3148		-0.01	-1.84	0	
138	SLU 67	-41	0	3148		-0.01	-1.84	0	
138	SLU 68	-41	0	3148		-0.01	-1.84	0	
138	SLU 69	-41	0	3148		-0.01	-1.84	0	
138	SLU 70	-41	0	3148		-0.01	-1.84	0	
138	SLU 71	-41	0	3148		-0.01	-1.84	0	
138	SLU 72	-41	0	3148		-0.01	-1.84	0	
138	SLU 73	-51	0	3685		-0.01	-2.29	0	
138	SLU 74	-51	0	3685		-0.01	-2.29	0	
138	SLU 75	-51	0	3685		-0.01	-2.29	0	
138	SLU 76	-51	0	3685		-0.01	-2.29	0	
138	SLU 77	-51	0	3685		-0.01	-2.29	0	
138	SLU 78	-51	0	3685		-0.01	-2.29	0	
138	SLU 79	-51	0	3685		-0.01	-2.29	0	
138	SLU 80	-51	0	3685		-0.01	-2.29	0	
138	SLU 81	-56	0	3915		-0.01	-2.48	0	
138	SLU 82	-56	0	3915		-0.01	-2.48	0	
138	SLU 83	-56	0	3915		-0.01	-2.48	0	
138	SLU 84	-56	0	3915		-0.01	-2.48	0	
138	SLE RA 1	-31	0	2354		-0.01	-1.37	0	
138	SLE RA 2	-31	0	2354		-0.01	-1.37	0	
138	SLE RA 3	-31	0	2354		-0.01	-1.37	0	
138	SLE RA 4	-31	0	2354		-0.01	-1.37	0	
138	SLE RA 5	-31	0	2354		-0.01	-1.37	0	
138	SLE RA 6	-31	0	2354		-0.01	-1.37	0	
138	SLE RA 7	-31	0	2354		-0.01	-1.37	0	
138	SLE RA 8	-31	0	2354		-0.01	-1.37	0	
138	SLE RA 9	-31	0	2354		-0.01	-1.37	0	
138	SLE RA 10	-37	0	2712		-0.01	-1.66	0	
138	SLE RA 11	-37	0	2712		-0.01	-1.66	0	
138	SLE RA 12	-37	0	2712		-0.01	-1.66	0	
138	SLE RA 13	-37	0	2712		-0.01	-1.66	0	
138	SLE RA 14	-37	0	2712		-0.01	-1.66	0	
138	SLE RA 15	-37	0	2712		-0.01	-1.66	0	
138	SLE RA 16	-37	0	2712		-0.01	-1.66	0	
138	SLE RA 17	-37	0	2712		-0.01	-1.66	0	
138	SLE RA 18	-40	0	2866		-0.01	-1.79	0	
138	SLE RA 19	-40	0	2866		-0.01	-1.79	0	
138	SLE RA 20	-40	0	2866		-0.01	-1.79	0	
138	SLE RA 21	-40	0	2866		-0.01	-1.79	0	
138	SLE FR 1	-31	0	2354		-0.01	-1.37	0	
138	SLE FR 2	-31	0	2354		-0.01	-1.37	0	
138	SLE FR 3	-31	0	2354		-0.01	-1.37	0	
138	SLE FR 4	-34	0	2508		-0.01	-1.49	0	
138	SLE FR 5	-34	0	2508		-0.01	-1.49	0	
138	SLE FR 6	-35	0	2610		-0.01	-1.58	0	
138	SLE QP 1	-31	0	2354		-0.01	-1.37	0	
138	SLE QP 2	-34	0	2508		-0.01	-1.49	0	
138	SLD 1	177	46	2457		-47.51	9.11	0.02	
138	SLD 2	177	46	2457		-47.51	9.11	0.02	
138	SLD 3	169	-33	2521		37.48	8.73	0	
138	SLD 4	169	-33	2521		37.48	8.73	0	
138	SLD 5	42	133	2396		-143.16	2.26	0.04	
138	SLD 6	42	133	2396		-143.16	2.26	0.04	
138	SLD 7	15	-129	2608		140.14	1	-0.03	
138	SLD 8	15	-129	2608		140.14	1	-0.03	



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
138	SLD 9	-82	129	2407	-140.16	-3.99	0.03
138	SLD 10	-82	129	2407	-140.16	-3.99	0.03
138	SLD 11	-109	-133	2619	143.14	-5.25	-0.04
138	SLD 12	-109	-133	2619	143.14	-5.25	-0.04
138	SLD 13	-236	33	2494	-37.5	-11.72	0
138	SLD 14	-236	33	2494	-37.5	-11.72	0
138	SLD 15	-244	-46	2558	47.49	-12.1	-0.02
138	SLD 16	-244	-46	2558	47.49	-12.1	-0.02
138	SLV 1	465	128	2375	-132.47	23.6	0.06
138	SLV 2	465	128	2375	-132.47	23.6	0.06
138	SLV 3	444	-94	2554	107.46	22.61	0
138	SLV 4	444	-94	2554	107.46	22.61	0
138	SLV 5	149	375	2196	-403.64	7.53	0.11
138	SLV 6	149	375	2196	-403.64	7.53	0.11
138	SLV 7	76	-365	2794	396.12	4.24	-0.09
138	SLV 8	76	-365	2794	396.12	4.24	-0.09
138	SLV 9	-143	365	2221	-396.14	-7.22	0.1
138	SLV 10	-143	365	2221	-396.14	-7.22	0.1
138	SLV 11	-216	-375	2819	403.62	-10.52	-0.11
138	SLV 12	-216	-375	2819	403.62	-10.52	-0.11
138	SLV 13	-511	94	2461	-107.47	-25.59	0
138	SLV 14	-511	94	2461	-107.47	-25.59	0
138	SLV 15	-532	-128	2640	132.46	-26.58	-0.06
138	SLV 16	-532	-128	2640	132.46	-26.58	-0.06
139	SLU 1	2	0	2753	0	0.03	0
139	SLU 2	2	0	2753	0	0.03	0
139	SLU 3	2	0	2753	0	0.03	0
139	SLU 4	2	0	2753	0	0.03	0
139	SLU 5	2	0	2753	0	0.03	0
139	SLU 6	2	0	2753	0	0.03	0
139	SLU 7	2	0	2753	0	0.03	0
139	SLU 8	2	0	2753	0	0.03	0
139	SLU 9	2	0	2753	0	0.03	0
139	SLU 10	2	0	3402	0	0.03	0
139	SLU 11	2	0	3402	0	0.03	0
139	SLU 12	2	0	3402	0	0.03	0
139	SLU 13	2	0	3402	0	0.03	0
139	SLU 14	2	0	3402	0	0.03	0
139	SLU 15	2	0	3402	0	0.03	0
139	SLU 16	2	0	3402	0	0.03	0
139	SLU 17	2	0	3402	0	0.03	0
139	SLU 18	3	0	3680	0	0.03	0
139	SLU 19	3	0	3680	0	0.03	0
139	SLU 20	3	0	3680	0	0.03	0
139	SLU 21	3	0	3680	0	0.03	0
139	SLU 22	2	0	3123	0	0.03	0
139	SLU 23	2	0	3123	0	0.03	0
139	SLU 24	2	0	3123	0	0.03	0
139	SLU 25	2	0	3123	0	0.03	0
139	SLU 26	2	0	3123	0	0.03	0
139	SLU 27	2	0	3123	0	0.03	0
139	SLU 28	2	0	3123	0	0.03	0
139	SLU 29	2	0	3123	0	0.03	0
139	SLU 30	2	0	3123	0	0.03	0
139	SLU 31	3	0	3772	0	0.04	0
139	SLU 32	3	0	3772	0	0.04	0
139	SLU 33	3	0	3772	0	0.04	0
139	SLU 34	3	0	3772	0	0.04	0
139	SLU 35	3	0	3772	0	0.04	0
139	SLU 36	3	0	3772	0	0.04	0
139	SLU 37	3	0	3772	0	0.04	0
139	SLU 38	3	0	3772	0	0.04	0
139	SLU 39	3	0	4050	0	0.04	0
139	SLU 40	3	0	4050	0	0.04	0
139	SLU 41	3	0	4050	0	0.04	0
139	SLU 42	3	0	4050	0	0.04	0
139	SLU 43	2	0	3452	0	0.04	0
139	SLU 44	2	0	3452	0	0.04	0
139	SLU 45	2	0	3452	0	0.04	0
139	SLU 46	2	0	3452	0	0.04	0
139	SLU 47	2	0	3452	0	0.04	0
139	SLU 48	2	0	3452	0	0.04	0
139	SLU 49	2	0	3452	0	0.04	0
139	SLU 50	2	0	3452	0	0.04	0
139	SLU 51	2	0	3452	0	0.04	0
139	SLU 52	3	0	4101	0	0.04	0
139	SLU 53	3	0	4101	0	0.04	0
139	SLU 54	3	0	4101	0	0.04	0
139	SLU 55	3	0	4101	0	0.04	0
139	SLU 56	3	0	4101	0	0.04	0
139	SLU 57	3	0	4101	0	0.04	0
139	SLU 58	3	0	4101	0	0.04	0
139	SLU 59	3	0	4101	0	0.04	0
139	SLU 60	3	0	4379	0	0.04	0
139	SLU 61	3	0	4379	0	0.04	0
139	SLU 62	3	0	4379	0	0.04	0
139	SLU 63	3	0	4379	0	0.04	0
139	SLU 64	2	0	3822	0	0.04	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
139	SLU 65	2	0	3822	0	0.04	0
139	SLU 66	2	0	3822	0	0.04	0
139	SLU 67	2	0	3822	0	0.04	0
139	SLU 68	2	0	3822	0	0.04	0
139	SLU 69	2	0	3822	0	0.04	0
139	SLU 70	2	0	3822	0	0.04	0
139	SLU 71	2	0	3822	0	0.04	0
139	SLU 72	2	0	3822	0	0.04	0
139	SLU 73	3	0	4471	0	0.04	0
139	SLU 74	3	0	4471	0	0.04	0
139	SLU 75	3	0	4471	0	0.04	0
139	SLU 76	3	0	4471	0	0.04	0
139	SLU 77	3	0	4471	0	0.04	0
139	SLU 78	3	0	4471	0	0.04	0
139	SLU 79	3	0	4471	0	0.04	0
139	SLU 80	3	0	4471	0	0.04	0
139	SLU 81	4	0	4749	-0.01	0.04	0
139	SLU 82	4	0	4749	-0.01	0.04	0
139	SLU 83	4	0	4749	-0.01	0.04	0
139	SLU 84	4	0	4749	-0.01	0.04	0
139	SLE RA 1	2	0	2859	0	0.03	0
139	SLE RA 2	2	0	2859	0	0.03	0
139	SLE RA 3	2	0	2859	0	0.03	0
139	SLE RA 4	2	0	2859	0	0.03	0
139	SLE RA 5	2	0	2859	0	0.03	0
139	SLE RA 6	2	0	2859	0	0.03	0
139	SLE RA 7	2	0	2859	0	0.03	0
139	SLE RA 8	2	0	2859	0	0.03	0
139	SLE RA 9	2	0	2859	0	0.03	0
139	SLE RA 10	2	0	3291	0	0.03	0
139	SLE RA 11	2	0	3291	0	0.03	0
139	SLE RA 12	2	0	3291	0	0.03	0
139	SLE RA 13	2	0	3291	0	0.03	0
139	SLE RA 14	2	0	3291	0	0.03	0
139	SLE RA 15	2	0	3291	0	0.03	0
139	SLE RA 16	2	0	3291	0	0.03	0
139	SLE RA 17	2	0	3291	0	0.03	0
139	SLE RA 18	3	0	3477	0	0.03	0
139	SLE RA 19	3	0	3477	0	0.03	0
139	SLE RA 20	3	0	3477	0	0.03	0
139	SLE RA 21	3	0	3477	0	0.03	0
139	SLE FR 1	2	0	2859	0	0.03	0
139	SLE FR 2	2	0	2859	0	0.03	0
139	SLE FR 3	2	0	2859	0	0.03	0
139	SLE FR 4	2	0	3044	0	0.03	0
139	SLE FR 5	2	0	3044	0	0.03	0
139	SLE FR 6	2	0	3168	0	0.03	0
139	SLE QP 1	2	0	2859	0	0.03	0
139	SLE QP 2	2	0	3044	0	0.03	0
139	SLD 1	209	47	3021	-43.5	10.26	0.02
139	SLD 2	209	47	3021	-43.5	10.26	0.02
139	SLD 3	204	-49	3074	44.55	10	0.02
139	SLD 4	204	-49	3074	44.55	10	0.02
139	SLD 5	72	159	2956	-146.6	3.5	0.01
139	SLD 6	72	159	2956	-146.6	3.5	0.01
139	SLD 7	54	-159	3134	146.91	2.62	0
139	SLD 8	54	-159	3134	146.91	2.62	0
139	SLD 9	-50	159	2954	-146.92	-2.56	0
139	SLD 10	-50	159	2954	-146.92	-2.56	0
139	SLD 11	-68	-159	3132	146.6	-3.44	-0.01
139	SLD 12	-68	-159	3132	146.6	-3.44	-0.01
139	SLD 13	-200	49	3014	-44.56	-9.94	-0.02
139	SLD 14	-200	49	3014	-44.56	-9.94	-0.02
139	SLD 15	-205	-47	3068	43.5	-10.2	-0.02
139	SLD 16	-205	-47	3068	43.5	-10.2	-0.02
139	SLV 1	491	132	2977	-122.98	24.2	0.06
139	SLV 2	491	132	2977	-122.98	24.2	0.06
139	SLV 3	478	-137	3127	125.52	23.57	0.05
139	SLV 4	478	-137	3127	125.52	23.57	0.05
139	SLV 5	168	448	2798	-413.78	8.23	0.04
139	SLV 6	168	448	2798	-413.78	8.23	0.04
139	SLV 7	126	-449	3295	414.53	6.15	-0.01
139	SLV 8	126	-449	3295	414.53	6.15	-0.01
139	SLV 9	-122	449	2793	-414.54	-6.09	0.01
139	SLV 10	-122	449	2793	-414.54	-6.09	0.01
139	SLV 11	-164	-448	3291	413.77	-8.17	-0.04
139	SLV 12	-164	-448	3291	413.77	-8.17	-0.04
139	SLV 13	-474	137	2962	-125.52	-23.51	-0.05
139	SLV 14	-474	137	2962	-125.52	-23.51	-0.05
139	SLV 15	-487	-132	3111	122.97	-24.14	-0.06
139	SLV 16	-487	-132	3111	122.97	-24.14	-0.06
140	SLU 1	34	0	2226	-0.01	1.64	0
140	SLU 2	34	0	2226	-0.01	1.64	0
140	SLU 3	34	0	2226	-0.01	1.64	0
140	SLU 4	34	0	2226	-0.01	1.64	0
140	SLU 5	34	0	2226	-0.01	1.64	0
140	SLU 6	34	0	2226	-0.01	1.64	0
140	SLU 7	34	0	2226	-0.01	1.64	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione		
		x	y	z		x	y	z
140	SLU 8	34	0	2226		-0.01	1.64	0
140	SLU 9	34	0	2226		-0.01	1.64	0
140	SLU 10	47	0	2754		-0.01	2.3	0
140	SLU 11	47	0	2754		-0.01	2.3	0
140	SLU 12	47	0	2754		-0.01	2.3	0
140	SLU 13	47	0	2754		-0.01	2.3	0
140	SLU 14	47	0	2754		-0.01	2.3	0
140	SLU 15	47	0	2754		-0.01	2.3	0
140	SLU 16	47	0	2754		-0.01	2.3	0
140	SLU 17	47	0	2754		-0.01	2.3	0
140	SLU 18	53	0	2980		-0.01	2.58	0
140	SLU 19	53	0	2980		-0.01	2.58	0
140	SLU 20	53	0	2980		-0.01	2.58	0
140	SLU 21	53	0	2980		-0.01	2.58	0
140	SLU 22	40	0	2527		-0.01	1.95	0
140	SLU 23	40	0	2527		-0.01	1.95	0
140	SLU 24	40	0	2527		-0.01	1.95	0
140	SLU 25	40	0	2527		-0.01	1.95	0
140	SLU 26	40	0	2527		-0.01	1.95	0
140	SLU 27	40	0	2527		-0.01	1.95	0
140	SLU 28	40	0	2527		-0.01	1.95	0
140	SLU 29	40	0	2527		-0.01	1.95	0
140	SLU 30	40	0	2527		-0.01	1.95	0
140	SLU 31	53	0	3054		-0.01	2.61	0
140	SLU 32	53	0	3054		-0.01	2.61	0
140	SLU 33	53	0	3054		-0.01	2.61	0
140	SLU 34	53	0	3054		-0.01	2.61	0
140	SLU 35	53	0	3054		-0.01	2.61	0
140	SLU 36	53	0	3054		-0.01	2.61	0
140	SLU 37	53	0	3054		-0.01	2.61	0
140	SLU 38	53	0	3054		-0.01	2.61	0
140	SLU 39	59	0	3280		-0.01	2.89	0
140	SLU 40	59	0	3280		-0.01	2.89	0
140	SLU 41	59	0	3280		-0.01	2.89	0
140	SLU 42	59	0	3280		-0.01	2.89	0
140	SLU 43	42	0	2791		-0.01	2.02	0
140	SLU 44	42	0	2791		-0.01	2.02	0
140	SLU 45	42	0	2791		-0.01	2.02	0
140	SLU 46	42	0	2791		-0.01	2.02	0
140	SLU 47	42	0	2791		-0.01	2.02	0
140	SLU 48	42	0	2791		-0.01	2.02	0
140	SLU 49	42	0	2791		-0.01	2.02	0
140	SLU 50	42	0	2791		-0.01	2.02	0
140	SLU 51	42	0	2791		-0.01	2.02	0
140	SLU 52	55	0	3319		-0.01	2.68	0
140	SLU 53	55	0	3319		-0.01	2.68	0
140	SLU 54	55	0	3319		-0.01	2.68	0
140	SLU 55	55	0	3319		-0.01	2.68	0
140	SLU 56	55	0	3319		-0.01	2.68	0
140	SLU 57	55	0	3319		-0.01	2.68	0
140	SLU 58	55	0	3319		-0.01	2.68	0
140	SLU 59	55	0	3319		-0.01	2.68	0
140	SLU 60	61	0	3545		-0.01	2.96	0
140	SLU 61	61	0	3545		-0.01	2.96	0
140	SLU 62	61	0	3545		-0.01	2.96	0
140	SLU 63	61	0	3545		-0.01	2.96	0
140	SLU 64	48	0	3092		-0.01	2.34	0
140	SLU 65	48	0	3092		-0.01	2.34	0
140	SLU 66	48	0	3092		-0.01	2.34	0
140	SLU 67	48	0	3092		-0.01	2.34	0
140	SLU 68	48	0	3092		-0.01	2.34	0
140	SLU 69	48	0	3092		-0.01	2.34	0
140	SLU 70	48	0	3092		-0.01	2.34	0
140	SLU 71	48	0	3092		-0.01	2.34	0
140	SLU 72	48	0	3092		-0.01	2.34	0
140	SLU 73	61	0	3619		-0.01	2.99	0
140	SLU 74	61	0	3619		-0.01	2.99	0
140	SLU 75	61	0	3619		-0.01	2.99	0
140	SLU 76	61	0	3619		-0.01	2.99	0
140	SLU 77	61	0	3619		-0.01	2.99	0
140	SLU 78	61	0	3619		-0.01	2.99	0
140	SLU 79	61	0	3619		-0.01	2.99	0
140	SLU 80	61	0	3619		-0.01	2.99	0
140	SLU 81	67	0	3845		-0.01	3.28	0
140	SLU 82	67	0	3845		-0.01	3.28	0
140	SLU 83	67	0	3845		-0.01	3.28	0
140	SLU 84	67	0	3845		-0.01	3.28	0
140	SLE RA 1	36	0	2312		-0.01	1.73	0
140	SLE RA 2	36	0	2312		-0.01	1.73	0
140	SLE RA 3	36	0	2312		-0.01	1.73	0
140	SLE RA 4	36	0	2312		-0.01	1.73	0
140	SLE RA 5	36	0	2312		-0.01	1.73	0
140	SLE RA 6	36	0	2312		-0.01	1.73	0
140	SLE RA 7	36	0	2312		-0.01	1.73	0
140	SLE RA 8	36	0	2312		-0.01	1.73	0
140	SLE RA 9	36	0	2312		-0.01	1.73	0
140	SLE RA 10	45	0	2664		-0.01	2.17	0
140	SLE RA 11	45	0	2664		-0.01	2.17	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione		
		x	y	z		x	y	z
140	SLE RA 12	45	0	2664		-0.01	2.17	0
140	SLE RA 13	45	0	2664		-0.01	2.17	0
140	SLE RA 14	45	0	2664		-0.01	2.17	0
140	SLE RA 15	45	0	2664		-0.01	2.17	0
140	SLE RA 16	45	0	2664		-0.01	2.17	0
140	SLE RA 17	45	0	2664		-0.01	2.17	0
140	SLE RA 18	48	0	2815		-0.01	2.35	0
140	SLE RA 19	48	0	2815		-0.01	2.35	0
140	SLE RA 20	48	0	2815		-0.01	2.35	0
140	SLE RA 21	48	0	2815		-0.01	2.35	0
140	SLE FR 1	36	0	2312		-0.01	1.73	0
140	SLE FR 2	36	0	2312		-0.01	1.73	0
140	SLE FR 3	36	0	2312		-0.01	1.73	0
140	SLE FR 4	40	0	2463		-0.01	1.92	0
140	SLE FR 5	40	0	2463		-0.01	1.92	0
140	SLE FR 6	42	0	2563		-0.01	2.04	0
140	SLE QP 1	36	0	2312		-0.01	1.73	0
140	SLE QP 2	40	0	2463		-0.01	1.92	0
140	SLD 1	239	31	2453		-36.66	12.02	0.02
140	SLD 2	239	31	2453		-36.66	12.02	0.02
140	SLD 3	247	-46	2516		46.59	12.38	0
140	SLD 4	247	-46	2516		46.59	12.38	0
140	SLD 5	87	127	2365		-137.26	4.4	0.03
140	SLD 6	87	127	2365		-137.26	4.4	0.03
140	SLD 7	114	-131	2574		140.23	5.6	-0.03
140	SLD 8	114	-131	2574		140.23	5.6	-0.03
140	SLD 9	-35	131	2352		-140.25	-1.77	0.03
140	SLD 10	-35	131	2352		-140.25	-1.77	0.03
140	SLD 11	-8	-127	2561		137.25	-0.57	-0.03
140	SLD 12	-8	-127	2561		137.25	-0.57	-0.03
140	SLD 13	-168	46	2410		-46.61	-8.55	0
140	SLD 14	-168	46	2410		-46.61	-8.55	0
140	SLD 15	-160	-31	2473		36.64	-8.19	-0.02
140	SLD 16	-160	-31	2473		36.64	-8.19	-0.02
140	SLV 1	509	91	2426		-105.08	25.74	0.05
140	SLV 2	509	91	2426		-105.08	25.74	0.05
140	SLV 3	530	-127	2602		129.76	26.67	0
140	SLV 4	530	-127	2602		129.76	26.67	0
140	SLV 5	149	358	2183		-387.71	7.65	0.09
140	SLV 6	149	358	2183		-387.71	7.65	0.09
140	SLV 7	218	-369	2773		395.1	10.75	-0.08
140	SLV 8	218	-369	2773		395.1	10.75	-0.08
140	SLV 9	-139	369	2153		-395.11	-6.92	0.08
140	SLV 10	-139	369	2153		-395.11	-6.92	0.08
140	SLV 11	-70	-358	2742		387.69	-3.82	-0.09
140	SLV 12	-70	-358	2742		387.69	-3.82	-0.09
140	SLV 13	-451	127	2323		-129.77	-22.84	0
140	SLV 14	-451	127	2323		-129.77	-22.84	0
140	SLV 15	-430	-91	2500		105.07	-21.91	-0.05
140	SLV 16	-430	-91	2500		105.07	-21.91	-0.05
141	SLU 1	67	0	2207		-0.01	3.17	0
141	SLU 2	67	0	2207		-0.01	3.17	0
141	SLU 3	67	0	2207		-0.01	3.17	0
141	SLU 4	67	0	2207		-0.01	3.17	0
141	SLU 5	67	0	2207		-0.01	3.17	0
141	SLU 6	67	0	2207		-0.01	3.17	0
141	SLU 7	67	0	2207		-0.01	3.17	0
141	SLU 8	67	0	2207		-0.01	3.17	0
141	SLU 9	67	0	2207		-0.01	3.17	0
141	SLU 10	92	0	2728		-0.01	4.34	0
141	SLU 11	92	0	2728		-0.01	4.34	0
141	SLU 12	92	0	2728		-0.01	4.34	0
141	SLU 13	92	0	2728		-0.01	4.34	0
141	SLU 14	92	0	2728		-0.01	4.34	0
141	SLU 15	92	0	2728		-0.01	4.34	0
141	SLU 16	92	0	2728		-0.01	4.34	0
141	SLU 17	92	0	2728		-0.01	4.34	0
141	SLU 18	103	0	2951		-0.02	4.84	0
141	SLU 19	103	0	2951		-0.02	4.84	0
141	SLU 20	103	0	2951		-0.02	4.84	0
141	SLU 21	103	0	2951		-0.02	4.84	0
141	SLU 22	80	0	2504		-0.01	3.75	0
141	SLU 23	80	0	2504		-0.01	3.75	0
141	SLU 24	80	0	2504		-0.01	3.75	0
141	SLU 25	80	0	2504		-0.01	3.75	0
141	SLU 26	80	0	2504		-0.01	3.75	0
141	SLU 27	80	0	2504		-0.01	3.75	0
141	SLU 28	80	0	2504		-0.01	3.75	0
141	SLU 29	80	0	2504		-0.01	3.75	0
141	SLU 30	80	0	2504		-0.01	3.75	0
141	SLU 31	105	0	3025		-0.02	4.92	0
141	SLU 32	105	0	3025		-0.02	4.92	0
141	SLU 33	105	0	3025		-0.02	4.92	0
141	SLU 34	105	0	3025		-0.02	4.92	0
141	SLU 35	105	0	3025		-0.02	4.92	0
141	SLU 36	105	0	3025		-0.02	4.92	0
141	SLU 37	105	0	3025		-0.02	4.92	0
141	SLU 38	105	0	3025		-0.02	4.92	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
141	SLU 39	115	0	3248	-0.02	5.43	0
141	SLU 40	115	0	3248	-0.02	5.43	0
141	SLU 41	115	0	3248	-0.02	5.43	0
141	SLU 42	115	0	3248	-0.02	5.43	0
141	SLU 43	83	0	2767	-0.01	3.92	0
141	SLU 44	83	0	2767	-0.01	3.92	0
141	SLU 45	83	0	2767	-0.01	3.92	0
141	SLU 46	83	0	2767	-0.01	3.92	0
141	SLU 47	83	0	2767	-0.01	3.92	0
141	SLU 48	83	0	2767	-0.01	3.92	0
141	SLU 49	83	0	2767	-0.01	3.92	0
141	SLU 50	83	0	2767	-0.01	3.92	0
141	SLU 51	83	0	2767	-0.01	3.92	0
141	SLU 52	108	0	3288	-0.02	5.09	0
141	SLU 53	108	0	3288	-0.02	5.09	0
141	SLU 54	108	0	3288	-0.02	5.09	0
141	SLU 55	108	0	3288	-0.02	5.09	0
141	SLU 56	108	0	3288	-0.02	5.09	0
141	SLU 57	108	0	3288	-0.02	5.09	0
141	SLU 58	108	0	3288	-0.02	5.09	0
141	SLU 59	108	0	3288	-0.02	5.09	0
141	SLU 60	119	0	3512	-0.02	5.59	0
141	SLU 61	119	0	3512	-0.02	5.59	0
141	SLU 62	119	0	3512	-0.02	5.59	0
141	SLU 63	119	0	3512	-0.02	5.59	0
141	SLU 64	96	0	3064	-0.02	4.5	0
141	SLU 65	96	0	3064	-0.02	4.5	0
141	SLU 66	96	0	3064	-0.02	4.5	0
141	SLU 67	96	0	3064	-0.02	4.5	0
141	SLU 68	96	0	3064	-0.02	4.5	0
141	SLU 69	96	0	3064	-0.02	4.5	0
141	SLU 70	96	0	3064	-0.02	4.5	0
141	SLU 71	96	0	3064	-0.02	4.5	0
141	SLU 72	96	0	3064	-0.02	4.5	0
141	SLU 73	121	0	3585	-0.02	5.67	0
141	SLU 74	121	0	3585	-0.02	5.67	0
141	SLU 75	121	0	3585	-0.02	5.67	0
141	SLU 76	121	0	3585	-0.02	5.67	0
141	SLU 77	121	0	3585	-0.02	5.67	0
141	SLU 78	121	0	3585	-0.02	5.67	0
141	SLU 79	121	0	3585	-0.02	5.67	0
141	SLU 80	121	0	3585	-0.02	5.67	0
141	SLU 81	131	0	3809	-0.02	6.18	0
141	SLU 82	131	0	3809	-0.02	6.18	0
141	SLU 83	131	0	3809	-0.02	6.18	0
141	SLU 84	131	0	3809	-0.02	6.18	0
141	SLE RA 1	71	0	2292	-0.01	3.34	0
141	SLE RA 2	71	0	2292	-0.01	3.34	0
141	SLE RA 3	71	0	2292	-0.01	3.34	0
141	SLE RA 4	71	0	2292	-0.01	3.34	0
141	SLE RA 5	71	0	2292	-0.01	3.34	0
141	SLE RA 6	71	0	2292	-0.01	3.34	0
141	SLE RA 7	71	0	2292	-0.01	3.34	0
141	SLE RA 8	71	0	2292	-0.01	3.34	0
141	SLE RA 9	71	0	2292	-0.01	3.34	0
141	SLE RA 10	88	0	2639	-0.01	4.12	0
141	SLE RA 11	88	0	2639	-0.01	4.12	0
141	SLE RA 12	88	0	2639	-0.01	4.12	0
141	SLE RA 13	88	0	2639	-0.01	4.12	0
141	SLE RA 14	88	0	2639	-0.01	4.12	0
141	SLE RA 15	88	0	2639	-0.01	4.12	0
141	SLE RA 16	88	0	2639	-0.01	4.12	0
141	SLE RA 17	88	0	2639	-0.01	4.12	0
141	SLE RA 18	95	0	2788	-0.01	4.45	0
141	SLE RA 19	95	0	2788	-0.01	4.45	0
141	SLE RA 20	95	0	2788	-0.01	4.45	0
141	SLE RA 21	95	0	2788	-0.01	4.45	0
141	SLE FR 1	71	0	2292	-0.01	3.34	0
141	SLE FR 2	71	0	2292	-0.01	3.34	0
141	SLE FR 3	71	0	2292	-0.01	3.34	0
141	SLE FR 4	78	0	2440	-0.01	3.67	0
141	SLE FR 5	78	0	2440	-0.01	3.67	0
141	SLE FR 6	83	0	2540	-0.01	3.89	0
141	SLE QP 1	71	0	2292	-0.01	3.34	0
141	SLE QP 2	78	0	2440	-0.01	3.67	0
141	SLD 1	274	19	2454	-28.86	13.62	-0.01
141	SLD 2	274	19	2454	-28.86	13.62	-0.01
141	SLD 3	286	-42	2510	46.92	14.18	0.05
141	SLD 4	286	-42	2510	46.92	14.18	0.05
141	SLD 5	119	98	2359	-123.59	5.79	-0.09
141	SLD 6	119	98	2359	-123.59	5.79	-0.09
141	SLD 7	158	-104	2546	128.99	7.69	0.1
141	SLD 8	158	-104	2546	128.99	7.69	0.1
141	SLD 9	-2	105	2335	-129.02	-0.34	-0.1
141	SLD 10	-2	105	2335	-129.02	-0.34	-0.1
141	SLD 11	37	-97	2522	123.57	1.55	0.09
141	SLD 12	37	-97	2522	123.57	1.55	0.09
141	SLD 13	-130	42	2371	-46.95	-6.84	-0.05



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
141	SLD 14	-130	42	2371	-46.95	-6.84	-0.05
141	SLD 15	-118	-19	2427	28.83	-6.27	0.01
141	SLD 16	-118	-19	2427	28.83	-6.27	0.01
141	SLV 1	539	57	2458	-84.29	27.06	-0.04
141	SLV 2	539	57	2458	-84.29	27.06	-0.04
141	SLV 3	571	-114	2616	129.34	28.6	0.12
141	SLV 4	571	-114	2616	129.34	28.6	0.12
141	SLV 5	168	276	2207	-349.3	8.35	-0.26
141	SLV 6	168	276	2207	-349.3	8.35	-0.26
141	SLV 7	274	-293	2732	362.8	13.49	0.29
141	SLV 8	274	-293	2732	362.8	13.49	0.29
141	SLV 9	-118	293	2149	-362.82	-6.14	-0.29
141	SLV 10	-118	293	2149	-362.82	-6.14	-0.29
141	SLV 11	-12	-276	2674	349.28	-1.01	0.26
141	SLV 12	-12	-276	2674	349.28	-1.01	0.26
141	SLV 13	-415	114	2265	-129.36	-21.26	-0.12
141	SLV 14	-415	114	2265	-129.36	-21.26	-0.12
141	SLV 15	-383	-57	2423	84.27	-19.72	0.04
141	SLV 16	-383	-57	2423	84.27	-19.72	0.04
142	SLU 1	108	0	2170	-0.01	5.21	0
142	SLU 2	108	0	2170	-0.01	5.21	0
142	SLU 3	108	0	2170	-0.01	5.21	0
142	SLU 4	108	0	2170	-0.01	5.21	0
142	SLU 5	108	0	2170	-0.01	5.21	0
142	SLU 6	108	0	2170	-0.01	5.21	0
142	SLU 7	108	0	2170	-0.01	5.21	0
142	SLU 8	108	0	2170	-0.01	5.21	0
142	SLU 9	108	0	2170	-0.01	5.21	0
142	SLU 10	149	0	2679	-0.01	7.24	0
142	SLU 11	149	0	2679	-0.01	7.24	0
142	SLU 12	149	0	2679	-0.01	7.24	0
142	SLU 13	149	0	2679	-0.01	7.24	0
142	SLU 14	149	0	2679	-0.01	7.24	0
142	SLU 15	149	0	2679	-0.01	7.24	0
142	SLU 16	149	0	2679	-0.01	7.24	0
142	SLU 17	149	0	2679	-0.01	7.24	0
142	SLU 18	166	0	2897	-0.02	8.11	0
142	SLU 19	166	0	2897	-0.02	8.11	0
142	SLU 20	166	0	2897	-0.02	8.11	0
142	SLU 21	166	0	2897	-0.02	8.11	0
142	SLU 22	128	0	2460	-0.01	6.21	0
142	SLU 23	128	0	2460	-0.01	6.21	0
142	SLU 24	128	0	2460	-0.01	6.21	0
142	SLU 25	128	0	2460	-0.01	6.21	0
142	SLU 26	128	0	2460	-0.01	6.21	0
142	SLU 27	128	0	2460	-0.01	6.21	0
142	SLU 28	128	0	2460	-0.01	6.21	0
142	SLU 29	128	0	2460	-0.01	6.21	0
142	SLU 30	128	0	2460	-0.01	6.21	0
142	SLU 31	169	0	2969	-0.02	8.24	0
142	SLU 32	169	0	2969	-0.02	8.24	0
142	SLU 33	169	0	2969	-0.02	8.24	0
142	SLU 34	169	0	2969	-0.02	8.24	0
142	SLU 35	169	0	2969	-0.02	8.24	0
142	SLU 36	169	0	2969	-0.02	8.24	0
142	SLU 37	169	0	2969	-0.02	8.24	0
142	SLU 38	169	0	2969	-0.02	8.24	0
142	SLU 39	186	0	3187	-0.02	9.11	0
142	SLU 40	186	0	3187	-0.02	9.11	0
142	SLU 41	186	0	3187	-0.02	9.11	0
142	SLU 42	186	0	3187	-0.02	9.11	0
142	SLU 43	133	0	2721	-0.01	6.43	0
142	SLU 44	133	0	2721	-0.01	6.43	0
142	SLU 45	133	0	2721	-0.01	6.43	0
142	SLU 46	133	0	2721	-0.01	6.43	0
142	SLU 47	133	0	2721	-0.01	6.43	0
142	SLU 48	133	0	2721	-0.01	6.43	0
142	SLU 49	133	0	2721	-0.01	6.43	0
142	SLU 50	133	0	2721	-0.01	6.43	0
142	SLU 51	133	0	2721	-0.01	6.43	0
142	SLU 52	174	0	3230	-0.02	8.46	0
142	SLU 53	174	0	3230	-0.02	8.46	0
142	SLU 54	174	0	3230	-0.02	8.46	0
142	SLU 55	174	0	3230	-0.02	8.46	0
142	SLU 56	174	0	3230	-0.02	8.46	0
142	SLU 57	174	0	3230	-0.02	8.46	0
142	SLU 58	174	0	3230	-0.02	8.46	0
142	SLU 59	174	0	3230	-0.02	8.46	0
142	SLU 60	191	0	3448	-0.02	9.33	0
142	SLU 61	191	0	3448	-0.02	9.33	0
142	SLU 62	191	0	3448	-0.02	9.33	0
142	SLU 63	191	0	3448	-0.02	9.33	0
142	SLU 64	153	0	3011	-0.02	7.43	0
142	SLU 65	153	0	3011	-0.02	7.43	0
142	SLU 66	153	0	3011	-0.02	7.43	0
142	SLU 67	153	0	3011	-0.02	7.43	0
142	SLU 68	153	0	3011	-0.02	7.43	0
142	SLU 69	153	0	3011	-0.02	7.43	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
142	SLU 70	153	0	3011	-0.02	7.43	0
142	SLU 71	153	0	3011	-0.02	7.43	0
142	SLU 72	153	0	3011	-0.02	7.43	0
142	SLU 73	194	0	3520	-0.02	9.46	0
142	SLU 74	194	0	3520	-0.02	9.46	0
142	SLU 75	194	0	3520	-0.02	9.46	0
142	SLU 76	194	0	3520	-0.02	9.46	0
142	SLU 77	194	0	3520	-0.02	9.46	0
142	SLU 78	194	0	3520	-0.02	9.46	0
142	SLU 79	194	0	3520	-0.02	9.46	0
142	SLU 80	194	0	3520	-0.02	9.46	0
142	SLU 81	212	0	3738	-0.02	10.33	0
142	SLU 82	212	0	3738	-0.02	10.33	0
142	SLU 83	212	0	3738	-0.02	10.33	0
142	SLU 84	212	0	3738	-0.02	10.33	0
142	SLE RA 1	113	0	2253	-0.01	5.49	0
142	SLE RA 2	113	0	2253	-0.01	5.49	0
142	SLE RA 3	113	0	2253	-0.01	5.49	0
142	SLE RA 4	113	0	2253	-0.01	5.49	0
142	SLE RA 5	113	0	2253	-0.01	5.49	0
142	SLE RA 6	113	0	2253	-0.01	5.49	0
142	SLE RA 7	113	0	2253	-0.01	5.49	0
142	SLE RA 8	113	0	2253	-0.01	5.49	0
142	SLE RA 9	113	0	2253	-0.01	5.49	0
142	SLE RA 10	141	0	2592	-0.01	6.85	0
142	SLE RA 11	141	0	2592	-0.01	6.85	0
142	SLE RA 12	141	0	2592	-0.01	6.85	0
142	SLE RA 13	141	0	2592	-0.01	6.85	0
142	SLE RA 14	141	0	2592	-0.01	6.85	0
142	SLE RA 15	141	0	2592	-0.01	6.85	0
142	SLE RA 16	141	0	2592	-0.01	6.85	0
142	SLE RA 17	141	0	2592	-0.01	6.85	0
142	SLE RA 18	152	0	2737	-0.01	7.43	0
142	SLE RA 19	152	0	2737	-0.01	7.43	0
142	SLE RA 20	152	0	2737	-0.01	7.43	0
142	SLE RA 21	152	0	2737	-0.01	7.43	0
142	SLE FR 1	113	0	2253	-0.01	5.49	0
142	SLE FR 2	113	0	2253	-0.01	5.49	0
142	SLE FR 3	113	0	2253	-0.01	5.49	0
142	SLE FR 4	125	0	2398	-0.01	6.07	0
142	SLE FR 5	125	0	2398	-0.01	6.07	0
142	SLE FR 6	133	0	2495	-0.01	6.46	0
142	SLE QP 1	113	0	2253	-0.01	5.49	0
142	SLE QP 2	125	0	2398	-0.01	6.07	0
142	SLD 1	324	9	2432	-21.36	16.51	-0.01
142	SLD 2	324	9	2432	-21.36	16.51	-0.01
142	SLD 3	337	-38	2481	45.59	17.11	0.06
142	SLD 4	337	-38	2481	45.59	17.11	0.06
142	SLD 5	165	74	2335	-107.96	8.3	-0.12
142	SLD 6	165	74	2335	-107.96	8.3	-0.12
142	SLD 7	209	-82	2496	115.21	10.28	0.13
142	SLD 8	209	-82	2496	115.21	10.28	0.13
142	SLD 9	41	83	2300	-115.23	1.86	-0.13
142	SLD 10	41	83	2300	-115.23	1.86	-0.13
142	SLD 11	86	-74	2461	107.93	3.84	0.12
142	SLD 12	86	-74	2461	107.93	3.84	0.12
142	SLD 13	-87	38	2315	-45.61	-4.96	-0.07
142	SLD 14	-87	38	2315	-45.61	-4.96	-0.07
142	SLD 15	-73	-9	2364	21.34	-4.37	0.01
142	SLD 16	-73	-9	2364	21.34	-4.37	0.01
142	SLV 1	591	31	2468	-63.9	30.62	-0.04
142	SLV 2	591	31	2468	-63.9	30.62	-0.04
142	SLV 3	628	-101	2603	124.59	32.23	0.17
142	SLV 4	628	-101	2603	124.59	32.23	0.17
142	SLV 5	210	210	2213	-305.05	10.99	-0.33
142	SLV 6	210	210	2213	-305.05	10.99	-0.33
142	SLV 7	331	-231	2666	323.24	16.36	0.37
142	SLV 8	331	-231	2666	323.24	16.36	0.37
142	SLV 9	-81	231	2131	-323.26	-4.22	-0.37
142	SLV 10	-81	231	2131	-323.26	-4.22	-0.37
142	SLV 11	40	-210	2583	305.02	1.15	0.33
142	SLV 12	40	-210	2583	305.02	1.15	0.33
142	SLV 13	-377	101	2193	-124.61	-20.09	-0.17
142	SLV 14	-377	101	2193	-124.61	-20.09	-0.17
142	SLV 15	-341	-31	2328	63.87	-18.48	0.04
142	SLV 16	-341	-31	2328	63.87	-18.48	0.04
143	SLU 1	147	0	2109	0	7.26	0
143	SLU 2	147	0	2109	0	7.26	0
143	SLU 3	147	0	2109	0	7.26	0
143	SLU 4	147	0	2109	0	7.26	0
143	SLU 5	147	0	2109	0	7.26	0
143	SLU 6	147	0	2109	0	7.26	0
143	SLU 7	147	0	2109	0	7.26	0
143	SLU 8	147	0	2109	0	7.26	0
143	SLU 9	147	0	2109	0	7.26	0
143	SLU 10	203	0	2597	0	10.03	0
143	SLU 11	203	0	2597	0	10.03	0
143	SLU 12	203	0	2597	0	10.03	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
143	SLU 13	203	0	2597	0	10.03	0
143	SLU 14	203	0	2597	0	10.03	0
143	SLU 15	203	0	2597	0	10.03	0
143	SLU 16	203	0	2597	0	10.03	0
143	SLU 17	203	0	2597	0	10.03	0
143	SLU 18	227	0	2806	0	11.22	0
143	SLU 19	227	0	2806	0	11.22	0
143	SLU 20	227	0	2806	0	11.22	0
143	SLU 21	227	0	2806	0	11.22	0
143	SLU 22	175	0	2388	0	8.66	0
143	SLU 23	175	0	2388	0	8.66	0
143	SLU 24	175	0	2388	0	8.66	0
143	SLU 25	175	0	2388	0	8.66	0
143	SLU 26	175	0	2388	0	8.66	0
143	SLU 27	175	0	2388	0	8.66	0
143	SLU 28	175	0	2388	0	8.66	0
143	SLU 29	175	0	2388	0	8.66	0
143	SLU 30	175	0	2388	0	8.66	0
143	SLU 31	231	0	2876	0	11.43	0
143	SLU 32	231	0	2876	0	11.43	0
143	SLU 33	231	0	2876	0	11.43	0
143	SLU 34	231	0	2876	0	11.43	0
143	SLU 35	231	0	2876	0	11.43	0
143	SLU 36	231	0	2876	0	11.43	0
143	SLU 37	231	0	2876	0	11.43	0
143	SLU 38	231	0	2876	0	11.43	0
143	SLU 39	255	0	3085	-0.01	12.61	0
143	SLU 40	255	0	3085	-0.01	12.61	0
143	SLU 41	255	0	3085	-0.01	12.61	0
143	SLU 42	255	0	3085	-0.01	12.61	0
143	SLU 43	181	0	2646	0	8.96	0
143	SLU 44	181	0	2646	0	8.96	0
143	SLU 45	181	0	2646	0	8.96	0
143	SLU 46	181	0	2646	0	8.96	0
143	SLU 47	181	0	2646	0	8.96	0
143	SLU 48	181	0	2646	0	8.96	0
143	SLU 49	181	0	2646	0	8.96	0
143	SLU 50	181	0	2646	0	8.96	0
143	SLU 51	181	0	2646	0	8.96	0
143	SLU 52	237	0	3133	0	11.73	0
143	SLU 53	237	0	3133	0	11.73	0
143	SLU 54	237	0	3133	0	11.73	0
143	SLU 55	237	0	3133	0	11.73	0
143	SLU 56	237	0	3133	0	11.73	0
143	SLU 57	237	0	3133	0	11.73	0
143	SLU 58	237	0	3133	0	11.73	0
143	SLU 59	237	0	3133	0	11.73	0
143	SLU 60	262	0	3342	-0.01	12.91	0
143	SLU 61	262	0	3342	-0.01	12.91	0
143	SLU 62	262	0	3342	-0.01	12.91	0
143	SLU 63	262	0	3342	-0.01	12.91	0
143	SLU 64	210	0	2925	0	10.36	0
143	SLU 65	210	0	2925	0	10.36	0
143	SLU 66	210	0	2925	0	10.36	0
143	SLU 67	210	0	2925	0	10.36	0
143	SLU 68	210	0	2925	0	10.36	0
143	SLU 69	210	0	2925	0	10.36	0
143	SLU 70	210	0	2925	0	10.36	0
143	SLU 71	210	0	2925	0	10.36	0
143	SLU 72	210	0	2925	0	10.36	0
143	SLU 73	266	0	3413	-0.01	13.13	0
143	SLU 74	266	0	3413	-0.01	13.13	0
143	SLU 75	266	0	3413	-0.01	13.13	0
143	SLU 76	266	0	3413	-0.01	13.13	0
143	SLU 77	266	0	3413	-0.01	13.13	0
143	SLU 78	266	0	3413	-0.01	13.13	0
143	SLU 79	266	0	3413	-0.01	13.13	0
143	SLU 80	266	0	3413	-0.01	13.13	0
143	SLU 81	290	0	3622	-0.01	14.31	0
143	SLU 82	290	0	3622	-0.01	14.31	0
143	SLU 83	290	0	3622	-0.01	14.31	0
143	SLU 84	290	0	3622	-0.01	14.31	0
143	SLE RA 1	155	0	2188	0	7.66	0
143	SLE RA 2	155	0	2188	0	7.66	0
143	SLE RA 3	155	0	2188	0	7.66	0
143	SLE RA 4	155	0	2188	0	7.66	0
143	SLE RA 5	155	0	2188	0	7.66	0
143	SLE RA 6	155	0	2188	0	7.66	0
143	SLE RA 7	155	0	2188	0	7.66	0
143	SLE RA 8	155	0	2188	0	7.66	0
143	SLE RA 9	155	0	2188	0	7.66	0
143	SLE RA 10	192	0	2514	0	9.51	0
143	SLE RA 11	192	0	2514	0	9.51	0
143	SLE RA 12	192	0	2514	0	9.51	0
143	SLE RA 13	192	0	2514	0	9.51	0
143	SLE RA 14	192	0	2514	0	9.51	0
143	SLE RA 15	192	0	2514	0	9.51	0
143	SLE RA 16	192	0	2514	0	9.51	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
143	SLE RA 17	192	0	2514	0	9.51	0
143	SLE RA 18	209	0	2653	0	10.3	0
143	SLE RA 19	209	0	2653	0	10.3	0
143	SLE RA 20	209	0	2653	0	10.3	0
143	SLE RA 21	209	0	2653	0	10.3	0
143	SLE FR 1	155	0	2188	0	7.66	0
143	SLE FR 2	155	0	2188	0	7.66	0
143	SLE FR 3	155	0	2188	0	7.66	0
143	SLE FR 4	171	0	2328	0	8.45	0
143	SLE FR 5	171	0	2328	0	8.45	0
143	SLE FR 6	182	0	2421	0	8.98	0
143	SLE QP 1	155	0	2188	0	7.66	0
143	SLE QP 2	171	0	2328	0	8.45	0
143	SLD 1	372	3	2379	-14.88	19.05	0
143	SLD 2	372	3	2379	-14.88	19.05	0
143	SLD 3	387	-33	2420	43.24	19.83	0.08
143	SLD 4	387	-33	2420	43.24	19.83	0.08
143	SLD 5	209	55	2282	-92.61	10.44	-0.12
143	SLD 6	209	55	2282	-92.61	10.44	-0.12
143	SLD 7	259	-64	2417	101.12	13.06	0.14
143	SLD 8	259	-64	2417	101.12	13.06	0.14
143	SLD 9	84	64	2239	-101.12	3.85	-0.14
143	SLD 10	84	64	2239	-101.12	3.85	-0.14
143	SLD 11	134	-54	2374	92.61	6.46	0.12
143	SLD 12	134	-54	2374	92.61	6.46	0.12
143	SLD 13	-45	33	2236	-43.24	-2.93	-0.08
143	SLD 14	-45	33	2236	-43.24	-2.93	-0.08
143	SLD 15	-30	-3	2277	14.88	-2.15	0
143	SLD 16	-30	-3	2277	14.88	-2.15	0
143	SLV 1	643	12	2439	-45.8	33.32	-0.02
143	SLV 2	643	12	2439	-45.8	33.32	-0.02
143	SLV 3	684	-87	2552	117.31	35.48	0.2
143	SLV 4	684	-87	2552	117.31	35.48	0.2
143	SLV 5	250	154	2190	-261.13	12.64	-0.33
143	SLV 6	250	154	2190	-261.13	12.64	-0.33
143	SLV 7	388	-177	2566	282.58	19.83	0.39
143	SLV 8	388	-177	2566	282.58	19.83	0.39
143	SLV 9	-45	177	2090	-282.58	-2.93	-0.39
143	SLV 10	-45	177	2090	-282.58	-2.93	-0.39
143	SLV 11	92	-154	2466	261.12	4.27	0.33
143	SLV 12	92	-154	2466	261.12	4.27	0.33
143	SLV 13	-342	87	2104	-117.32	-18.58	-0.2
143	SLV 14	-342	87	2104	-117.32	-18.58	-0.2
143	SLV 15	-301	-12	2217	45.79	-16.42	0.02
143	SLV 16	-301	-12	2217	45.79	-16.42	0.02
144	SLU 1	176	0	2030	0.01	8.73	0
144	SLU 2	176	0	2030	0.01	8.73	0
144	SLU 3	176	0	2030	0.01	8.73	0
144	SLU 4	176	0	2030	0.01	8.73	0
144	SLU 5	176	0	2030	0.01	8.73	0
144	SLU 6	176	0	2030	0.01	8.73	0
144	SLU 7	176	0	2030	0.01	8.73	0
144	SLU 8	176	0	2030	0.01	8.73	0
144	SLU 9	176	0	2030	0.01	8.73	0
144	SLU 10	245	0	2489	0.01	12.26	0
144	SLU 11	245	0	2489	0.01	12.26	0
144	SLU 12	245	0	2489	0.01	12.26	0
144	SLU 13	245	0	2489	0.01	12.26	0
144	SLU 14	245	0	2489	0.01	12.26	0
144	SLU 15	245	0	2489	0.01	12.26	0
144	SLU 16	245	0	2489	0.01	12.26	0
144	SLU 17	245	0	2489	0.01	12.26	0
144	SLU 18	275	0	2686	0.01	13.77	0
144	SLU 19	275	0	2686	0.01	13.77	0
144	SLU 20	275	0	2686	0.01	13.77	0
144	SLU 21	275	0	2686	0.01	13.77	0
144	SLU 22	211	0	2294	0.01	10.48	0
144	SLU 23	211	0	2294	0.01	10.48	0
144	SLU 24	211	0	2294	0.01	10.48	0
144	SLU 25	211	0	2294	0.01	10.48	0
144	SLU 26	211	0	2294	0.01	10.48	0
144	SLU 27	211	0	2294	0.01	10.48	0
144	SLU 28	211	0	2294	0.01	10.48	0
144	SLU 29	211	0	2294	0.01	10.48	0
144	SLU 30	211	0	2294	0.01	10.48	0
144	SLU 31	280	0	2753	0.01	14.02	0
144	SLU 32	280	0	2753	0.01	14.02	0
144	SLU 33	280	0	2753	0.01	14.02	0
144	SLU 34	280	0	2753	0.01	14.02	0
144	SLU 35	280	0	2753	0.01	14.02	0
144	SLU 36	280	0	2753	0.01	14.02	0
144	SLU 37	280	0	2753	0.01	14.02	0
144	SLU 38	280	0	2753	0.01	14.02	0
144	SLU 39	310	0	2950	0.01	15.53	0
144	SLU 40	310	0	2950	0.01	15.53	0
144	SLU 41	310	0	2950	0.01	15.53	0
144	SLU 42	310	0	2950	0.01	15.53	0
144	SLU 43	216	0	2548	0.01	10.75	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
144	SLU 44	216	0	2548	0.01	10.75	0
144	SLU 45	216	0	2548	0.01	10.75	0
144	SLU 46	216	0	2548	0.01	10.75	0
144	SLU 47	216	0	2548	0.01	10.75	0
144	SLU 48	216	0	2548	0.01	10.75	0
144	SLU 49	216	0	2548	0.01	10.75	0
144	SLU 50	216	0	2548	0.01	10.75	0
144	SLU 51	216	0	2548	0.01	10.75	0
144	SLU 52	286	0	3007	0.01	14.28	0
144	SLU 53	286	0	3007	0.01	14.28	0
144	SLU 54	286	0	3007	0.01	14.28	0
144	SLU 55	286	0	3007	0.01	14.28	0
144	SLU 56	286	0	3007	0.01	14.28	0
144	SLU 57	286	0	3007	0.01	14.28	0
144	SLU 58	286	0	3007	0.01	14.28	0
144	SLU 59	286	0	3007	0.01	14.28	0
144	SLU 60	316	0	3204	0.01	15.79	0
144	SLU 61	316	0	3204	0.01	15.79	0
144	SLU 62	316	0	3204	0.01	15.79	0
144	SLU 63	316	0	3204	0.01	15.79	0
144	SLU 64	251	0	2812	0.01	12.5	0
144	SLU 65	251	0	2812	0.01	12.5	0
144	SLU 66	251	0	2812	0.01	12.5	0
144	SLU 67	251	0	2812	0.01	12.5	0
144	SLU 68	251	0	2812	0.01	12.5	0
144	SLU 69	251	0	2812	0.01	12.5	0
144	SLU 70	251	0	2812	0.01	12.5	0
144	SLU 71	251	0	2812	0.01	12.5	0
144	SLU 72	251	0	2812	0.01	12.5	0
144	SLU 73	321	0	3271	0.01	16.03	0
144	SLU 74	321	0	3271	0.01	16.03	0
144	SLU 75	321	0	3271	0.01	16.03	0
144	SLU 76	321	0	3271	0.01	16.03	0
144	SLU 77	321	0	3271	0.01	16.03	0
144	SLU 78	321	0	3271	0.01	16.03	0
144	SLU 79	321	0	3271	0.01	16.03	0
144	SLU 80	321	0	3271	0.01	16.03	0
144	SLU 81	351	0	3468	0.01	17.55	0
144	SLU 82	351	0	3468	0.01	17.55	0
144	SLU 83	351	0	3468	0.01	17.55	0
144	SLU 84	351	0	3468	0.01	17.55	0
144	SLE RA 1	186	0	2105	0.01	9.23	0
144	SLE RA 2	186	0	2105	0.01	9.23	0
144	SLE RA 3	186	0	2105	0.01	9.23	0
144	SLE RA 4	186	0	2105	0.01	9.23	0
144	SLE RA 5	186	0	2105	0.01	9.23	0
144	SLE RA 6	186	0	2105	0.01	9.23	0
144	SLE RA 7	186	0	2105	0.01	9.23	0
144	SLE RA 8	186	0	2105	0.01	9.23	0
144	SLE RA 9	186	0	2105	0.01	9.23	0
144	SLE RA 10	232	0	2411	0.01	11.58	0
144	SLE RA 11	232	0	2411	0.01	11.58	0
144	SLE RA 12	232	0	2411	0.01	11.58	0
144	SLE RA 13	232	0	2411	0.01	11.58	0
144	SLE RA 14	232	0	2411	0.01	11.58	0
144	SLE RA 15	232	0	2411	0.01	11.58	0
144	SLE RA 16	232	0	2411	0.01	11.58	0
144	SLE RA 17	232	0	2411	0.01	11.58	0
144	SLE RA 18	252	0	2542	0.01	12.59	0
144	SLE RA 19	252	0	2542	0.01	12.59	0
144	SLE RA 20	252	0	2542	0.01	12.59	0
144	SLE RA 21	252	0	2542	0.01	12.59	0
144	SLE FR 1	186	0	2105	0.01	9.23	0
144	SLE FR 2	186	0	2105	0.01	9.23	0
144	SLE FR 3	186	0	2105	0.01	9.23	0
144	SLE FR 4	206	0	2236	0.01	10.24	0
144	SLE FR 5	206	0	2236	0.01	10.24	0
144	SLE FR 6	219	0	2324	0.01	10.91	0
144	SLE QP 1	186	0	2105	0.01	9.23	0
144	SLE QP 2	206	0	2236	0.01	10.24	0
144	SLD 1	416	-1	2296	-40.52	21.78	0
144	SLD 2	416	-1	2296	-40.52	21.78	0
144	SLD 3	430	-29	2329	9.81	22.44	0.09
144	SLD 4	430	-29	2329	9.81	22.44	0.09
144	SLD 5	247	41	2204	-88.48	12.7	-0.12
144	SLD 6	247	41	2204	-88.48	12.7	-0.12
144	SLD 7	294	-50	2314	79.28	14.9	0.15
144	SLD 8	294	-50	2314	79.28	14.9	0.15
144	SLD 9	117	50	2158	-79.26	5.58	-0.15
144	SLD 10	117	50	2158	-79.26	5.58	-0.15
144	SLD 11	164	-41	2269	88.5	7.78	0.12
144	SLD 12	164	-41	2269	88.5	7.78	0.12
144	SLD 13	-19	29	2144	-9.78	-1.96	-0.09
144	SLD 14	-19	29	2144	-9.78	-1.96	-0.09
144	SLD 15	-5	1	2177	40.54	-1.3	-0.01
144	SLD 16	-5	1	2177	40.54	-1.3	-0.01
144	SLV 1	700	0	2369	-109.24	37.38	0
144	SLV 2	700	0	2369	-109.24	37.38	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
144	SLV 3	738	-76	2461	31.17	39.16	0.23
144	SLV 4	738	-76	2461	31.17	39.16	0.23
144	SLV 5	296	115	2136	-245.73	15.68	-0.34
144	SLV 6	296	115	2136	-245.73	15.68	-0.34
144	SLV 7	423	-138	2443	222.32	21.61	0.41
144	SLV 8	423	-138	2443	222.32	21.61	0.41
144	SLV 9	-12	138	2029	-222.3	-1.13	-0.41
144	SLV 10	-12	138	2029	-222.3	-1.13	-0.41
144	SLV 11	116	-115	2336	245.75	4.8	0.34
144	SLV 12	116	-115	2336	245.75	4.8	0.34
144	SLV 13	-327	76	2012	-31.15	-18.68	-0.23
144	SLV 14	-327	76	2012	-31.15	-18.68	-0.23
144	SLV 15	-288	0	2104	109.26	-16.9	0
144	SLV 16	-288	0	2104	109.26	-16.9	0
145	SLU 1	190	0	1944	0.02	10.2	0
145	SLU 2	190	0	1944	0.02	10.2	0
145	SLU 3	190	0	1944	0.02	10.2	0
145	SLU 4	190	0	1944	0.02	10.2	0
145	SLU 5	190	0	1944	0.02	10.2	0
145	SLU 6	190	0	1944	0.02	10.2	0
145	SLU 7	190	0	1944	0.02	10.2	0
145	SLU 8	190	0	1944	0.02	10.2	0
145	SLU 9	190	0	1944	0.02	10.2	0
145	SLU 10	268	0	2370	0.03	14.32	0
145	SLU 11	268	0	2370	0.03	14.32	0
145	SLU 12	268	0	2370	0.03	14.32	0
145	SLU 13	268	0	2370	0.03	14.32	0
145	SLU 14	268	0	2370	0.03	14.32	0
145	SLU 15	268	0	2370	0.03	14.32	0
145	SLU 16	268	0	2370	0.03	14.32	0
145	SLU 17	268	0	2370	0.03	14.32	0
145	SLU 18	301	0	2552	0.03	16.09	0
145	SLU 19	301	0	2552	0.03	16.09	0
145	SLU 20	301	0	2552	0.03	16.09	0
145	SLU 21	301	0	2552	0.03	16.09	0
145	SLU 22	229	0	2190	0.03	12.28	0
145	SLU 23	229	0	2190	0.03	12.28	0
145	SLU 24	229	0	2190	0.03	12.28	0
145	SLU 25	229	0	2190	0.03	12.28	0
145	SLU 26	229	0	2190	0.03	12.28	0
145	SLU 27	229	0	2190	0.03	12.28	0
145	SLU 28	229	0	2190	0.03	12.28	0
145	SLU 29	229	0	2190	0.03	12.28	0
145	SLU 30	229	0	2190	0.03	12.28	0
145	SLU 31	307	0	2616	0.03	16.4	0
145	SLU 32	307	0	2616	0.03	16.4	0
145	SLU 33	307	0	2616	0.03	16.4	0
145	SLU 34	307	0	2616	0.03	16.4	0
145	SLU 35	307	0	2616	0.03	16.4	0
145	SLU 36	307	0	2616	0.03	16.4	0
145	SLU 37	307	0	2616	0.03	16.4	0
145	SLU 38	307	0	2616	0.03	16.4	0
145	SLU 39	340	0	2799	0.03	18.16	0
145	SLU 40	340	0	2799	0.03	18.16	0
145	SLU 41	340	0	2799	0.03	18.16	0
145	SLU 42	340	0	2799	0.03	18.16	0
145	SLU 43	234	0	2442	0.03	12.55	0
145	SLU 44	234	0	2442	0.03	12.55	0
145	SLU 45	234	0	2442	0.03	12.55	0
145	SLU 46	234	0	2442	0.03	12.55	0
145	SLU 47	234	0	2442	0.03	12.55	0
145	SLU 48	234	0	2442	0.03	12.55	0
145	SLU 49	234	0	2442	0.03	12.55	0
145	SLU 50	234	0	2442	0.03	12.55	0
145	SLU 51	234	0	2442	0.03	12.55	0
145	SLU 52	312	0	2868	0.03	16.67	0
145	SLU 53	312	0	2868	0.03	16.67	0
145	SLU 54	312	0	2868	0.03	16.67	0
145	SLU 55	312	0	2868	0.03	16.67	0
145	SLU 56	312	0	2868	0.03	16.67	0
145	SLU 57	312	0	2868	0.03	16.67	0
145	SLU 58	312	0	2868	0.03	16.67	0
145	SLU 59	312	0	2868	0.03	16.67	0
145	SLU 60	345	0	3051	0.03	18.44	0
145	SLU 61	345	0	3051	0.03	18.44	0
145	SLU 62	345	0	3051	0.03	18.44	0
145	SLU 63	345	0	3051	0.03	18.44	0
145	SLU 64	273	0	2689	0.03	14.63	0
145	SLU 65	273	0	2689	0.03	14.63	0
145	SLU 66	273	0	2689	0.03	14.63	0
145	SLU 67	273	0	2689	0.03	14.63	0
145	SLU 68	273	0	2689	0.03	14.63	0
145	SLU 69	273	0	2689	0.03	14.63	0
145	SLU 70	273	0	2689	0.03	14.63	0
145	SLU 71	273	0	2689	0.03	14.63	0
145	SLU 72	273	0	2689	0.03	14.63	0
145	SLU 73	350	0	3115	0.03	18.75	0
145	SLU 74	350	0	3115	0.03	18.75	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
145	SLU 75	350	0	3115	0.03	18.75	0
145	SLU 76	350	0	3115	0.03	18.75	0
145	SLU 77	350	0	3115	0.03	18.75	0
145	SLU 78	350	0	3115	0.03	18.75	0
145	SLU 79	350	0	3115	0.03	18.75	0
145	SLU 80	350	0	3115	0.03	18.75	0
145	SLU 81	384	0	3297	0.04	20.51	0
145	SLU 82	384	0	3297	0.04	20.51	0
145	SLU 83	384	0	3297	0.04	20.51	0
145	SLU 84	384	0	3297	0.04	20.51	0
145	SLE RA 1	201	0	2014	0.02	10.79	0
145	SLE RA 2	201	0	2014	0.02	10.79	0
145	SLE RA 3	201	0	2014	0.02	10.79	0
145	SLE RA 4	201	0	2014	0.02	10.79	0
145	SLE RA 5	201	0	2014	0.02	10.79	0
145	SLE RA 6	201	0	2014	0.02	10.79	0
145	SLE RA 7	201	0	2014	0.02	10.79	0
145	SLE RA 8	201	0	2014	0.02	10.79	0
145	SLE RA 9	201	0	2014	0.02	10.79	0
145	SLE RA 10	253	0	2298	0.03	13.54	0
145	SLE RA 11	253	0	2298	0.03	13.54	0
145	SLE RA 12	253	0	2298	0.03	13.54	0
145	SLE RA 13	253	0	2298	0.03	13.54	0
145	SLE RA 14	253	0	2298	0.03	13.54	0
145	SLE RA 15	253	0	2298	0.03	13.54	0
145	SLE RA 16	253	0	2298	0.03	13.54	0
145	SLE RA 17	253	0	2298	0.03	13.54	0
145	SLE RA 18	275	0	2420	0.03	14.72	0
145	SLE RA 19	275	0	2420	0.03	14.72	0
145	SLE RA 20	275	0	2420	0.03	14.72	0
145	SLE RA 21	275	0	2420	0.03	14.72	0
145	SLE FR 1	201	0	2014	0.02	10.79	0
145	SLE FR 2	201	0	2014	0.02	10.79	0
145	SLE FR 3	201	0	2014	0.02	10.79	0
145	SLE FR 4	224	0	2136	0.02	11.97	0
145	SLE FR 5	224	0	2136	0.02	11.97	0
145	SLE FR 6	238	0	2217	0.03	12.76	0
145	SLE QP 1	201	0	2014	0.02	10.79	0
145	SLE QP 2	224	0	2136	0.02	11.97	0
145	SLD 1	441	26	2192	-37.93	23.95	0.02
145	SLD 2	441	26	2192	-37.93	23.95	0.02
145	SLD 3	455	3	2220	6.15	24.75	0.12
145	SLD 4	455	3	2220	6.15	24.75	0.12
145	SLD 5	267	44	2111	-78.2	14.34	-0.15
145	SLD 6	267	44	2111	-78.2	14.34	-0.15
145	SLD 7	315	-35	2203	68.7	17.03	0.2
145	SLD 8	315	-35	2203	68.7	17.03	0.2
145	SLD 9	132	35	2069	-68.65	6.92	-0.2
145	SLD 10	132	35	2069	-68.65	6.92	-0.2
145	SLD 11	180	-44	2161	78.25	9.6	0.15
145	SLD 12	180	-44	2161	78.25	9.6	0.15
145	SLD 13	-8	-3	2052	-6.1	-0.81	-0.12
145	SLD 14	-8	-3	2052	-6.1	-0.81	-0.12
145	SLD 15	6	-26	2080	37.97	0	-0.02
145	SLD 16	6	-26	2080	37.97	0	-0.02
145	SLV 1	735	69	2262	-101.59	40.1	0.04
145	SLV 2	735	69	2262	-101.59	40.1	0.04
145	SLV 3	773	5	2338	20.26	42.29	0.32
145	SLV 4	773	5	2338	20.26	42.29	0.32
145	SLV 5	319	118	2058	-215.27	17.1	-0.41
145	SLV 6	319	118	2058	-215.27	17.1	-0.41
145	SLV 7	447	-96	2311	190.9	24.38	0.52
145	SLV 8	447	-96	2311	190.9	24.38	0.52
145	SLV 9	0	96	1960	-190.85	-0.43	-0.52
145	SLV 10	0	96	1960	-190.85	-0.43	-0.52
145	SLV 11	128	-118	2213	215.31	6.84	0.41
145	SLV 12	128	-118	2213	215.31	6.84	0.41
145	SLV 13	-326	-5	1934	-20.22	-18.34	-0.32
145	SLV 14	-326	-5	1934	-20.22	-18.34	-0.32
145	SLV 15	-288	-69	2010	101.63	-16.16	-0.04
145	SLV 16	-288	-69	2010	101.63	-16.16	-0.04
146	SLU 1	172	0	1879	0.03	9.14	0
146	SLU 2	172	0	1879	0.03	9.14	0
146	SLU 3	172	0	1879	0.03	9.14	0
146	SLU 4	172	0	1879	0.03	9.14	0
146	SLU 5	172	0	1879	0.03	9.14	0
146	SLU 6	172	0	1879	0.03	9.14	0
146	SLU 7	172	0	1879	0.03	9.14	0
146	SLU 8	172	0	1879	0.03	9.14	0
146	SLU 9	172	0	1879	0.03	9.14	0
146	SLU 10	247	0	2277	0.04	13.19	0
146	SLU 11	247	0	2277	0.04	13.19	0
146	SLU 12	247	0	2277	0.04	13.19	0
146	SLU 13	247	0	2277	0.04	13.19	0
146	SLU 14	247	0	2277	0.04	13.19	0
146	SLU 15	247	0	2277	0.04	13.19	0
146	SLU 16	247	0	2277	0.04	13.19	0
146	SLU 17	247	0	2277	0.04	13.19	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
146	SLU 18	280	0	2448	0.04	14.93	0
146	SLU 19	280	0	2448	0.04	14.93	0
146	SLU 20	280	0	2448	0.04	14.93	0
146	SLU 21	280	0	2448	0.04	14.93	0
146	SLU 22	209	0	2111	0.04	11.12	0
146	SLU 23	209	0	2111	0.04	11.12	0
146	SLU 24	209	0	2111	0.04	11.12	0
146	SLU 25	209	0	2111	0.04	11.12	0
146	SLU 26	209	0	2111	0.04	11.12	0
146	SLU 27	209	0	2111	0.04	11.12	0
146	SLU 28	209	0	2111	0.04	11.12	0
146	SLU 29	209	0	2111	0.04	11.12	0
146	SLU 30	209	0	2111	0.04	11.12	0
146	SLU 31	284	0	2509	0.04	15.18	0
146	SLU 32	284	0	2509	0.04	15.18	0
146	SLU 33	284	0	2509	0.04	15.18	0
146	SLU 34	284	0	2509	0.04	15.18	0
146	SLU 35	284	0	2509	0.04	15.18	0
146	SLU 36	284	0	2509	0.04	15.18	0
146	SLU 37	284	0	2509	0.04	15.18	0
146	SLU 38	284	0	2509	0.04	15.18	0
146	SLU 39	317	0	2680	0.05	16.92	0
146	SLU 40	317	0	2680	0.05	16.92	0
146	SLU 41	317	0	2680	0.05	16.92	0
146	SLU 42	317	0	2680	0.05	16.92	0
146	SLU 43	211	0	2363	0.04	11.2	0
146	SLU 44	211	0	2363	0.04	11.2	0
146	SLU 45	211	0	2363	0.04	11.2	0
146	SLU 46	211	0	2363	0.04	11.2	0
146	SLU 47	211	0	2363	0.04	11.2	0
146	SLU 48	211	0	2363	0.04	11.2	0
146	SLU 49	211	0	2363	0.04	11.2	0
146	SLU 50	211	0	2363	0.04	11.2	0
146	SLU 51	211	0	2363	0.04	11.2	0
146	SLU 52	286	0	2761	0.05	15.25	0
146	SLU 53	286	0	2761	0.05	15.25	0
146	SLU 54	286	0	2761	0.05	15.25	0
146	SLU 55	286	0	2761	0.05	15.25	0
146	SLU 56	286	0	2761	0.05	15.25	0
146	SLU 57	286	0	2761	0.05	15.25	0
146	SLU 58	286	0	2761	0.05	15.25	0
146	SLU 59	286	0	2761	0.05	15.25	0
146	SLU 60	318	0	2932	0.05	16.99	0
146	SLU 61	318	0	2932	0.05	16.99	0
146	SLU 62	318	0	2932	0.05	16.99	0
146	SLU 63	318	0	2932	0.05	16.99	0
146	SLU 64	248	0	2595	0.05	13.18	0
146	SLU 65	248	0	2595	0.05	13.18	0
146	SLU 66	248	0	2595	0.05	13.18	0
146	SLU 67	248	0	2595	0.05	13.18	0
146	SLU 68	248	0	2595	0.05	13.18	0
146	SLU 69	248	0	2595	0.05	13.18	0
146	SLU 70	248	0	2595	0.05	13.18	0
146	SLU 71	248	0	2595	0.05	13.18	0
146	SLU 72	248	0	2595	0.05	13.18	0
146	SLU 73	323	0	2993	0.05	17.24	0
146	SLU 74	323	0	2993	0.05	17.24	0
146	SLU 75	323	0	2993	0.05	17.24	0
146	SLU 76	323	0	2993	0.05	17.24	0
146	SLU 77	323	0	2993	0.05	17.24	0
146	SLU 78	323	0	2993	0.05	17.24	0
146	SLU 79	323	0	2993	0.05	17.24	0
146	SLU 80	323	0	2993	0.05	17.24	0
146	SLU 81	356	0	3164	0.05	18.98	0
146	SLU 82	356	0	3164	0.05	18.98	0
146	SLU 83	356	0	3164	0.05	18.98	0
146	SLU 84	356	0	3164	0.05	18.98	0
146	SLE RA 1	182	0	1945	0.04	9.71	0
146	SLE RA 2	182	0	1945	0.04	9.71	0
146	SLE RA 3	182	0	1945	0.04	9.71	0
146	SLE RA 4	182	0	1945	0.04	9.71	0
146	SLE RA 5	182	0	1945	0.04	9.71	0
146	SLE RA 6	182	0	1945	0.04	9.71	0
146	SLE RA 7	182	0	1945	0.04	9.71	0
146	SLE RA 8	182	0	1945	0.04	9.71	0
146	SLE RA 9	182	0	1945	0.04	9.71	0
146	SLE RA 10	233	0	2211	0.04	12.41	0
146	SLE RA 11	233	0	2211	0.04	12.41	0
146	SLE RA 12	233	0	2211	0.04	12.41	0
146	SLE RA 13	233	0	2211	0.04	12.41	0
146	SLE RA 14	233	0	2211	0.04	12.41	0
146	SLE RA 15	233	0	2211	0.04	12.41	0
146	SLE RA 16	233	0	2211	0.04	12.41	0
146	SLE RA 17	233	0	2211	0.04	12.41	0
146	SLE RA 18	254	0	2324	0.04	13.57	0
146	SLE RA 19	254	0	2324	0.04	13.57	0
146	SLE RA 20	254	0	2324	0.04	13.57	0
146	SLE RA 21	254	0	2324	0.04	13.57	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
146	SLE FR 1	182	0	1945	0.04	9.71	0
146	SLE FR 2	182	0	1945	0.04	9.71	0
146	SLE FR 3	182	0	1945	0.04	9.71	0
146	SLE FR 4	204	0	2059	0.04	10.86	0
146	SLE FR 5	204	0	2059	0.04	10.86	0
146	SLE FR 6	218	0	2135	0.04	11.64	0
146	SLE QP 1	182	0	1945	0.04	9.71	0
146	SLE QP 2	204	0	2059	0.04	10.86	0
146	SLD 1	428	26	2103	-35.54	23.51	-0.1
146	SLD 2	428	26	2103	-35.54	23.51	-0.1
146	SLD 3	441	3	2128	3.62	24.15	-0.01
146	SLD 4	441	3	2128	3.62	24.15	-0.01
146	SLD 5	252	42	2034	-70.03	13.68	-0.16
146	SLD 6	252	42	2034	-70.03	13.68	-0.16
146	SLD 7	295	-34	2117	60.51	15.82	0.13
146	SLD 8	295	-34	2117	60.51	15.82	0.13
146	SLD 9	114	34	2001	-60.44	5.9	-0.13
146	SLD 10	114	34	2001	-60.44	5.9	-0.13
146	SLD 11	156	-42	2084	70.11	8.05	0.16
146	SLD 12	156	-42	2084	70.11	8.05	0.16
146	SLD 13	-33	-3	1990	-3.55	-2.42	0.01
146	SLD 14	-33	-3	1990	-3.55	-2.42	0.01
146	SLD 15	-20	-26	2015	35.62	-1.78	0.1
146	SLD 16	-20	-26	2015	35.62	-1.78	0.1
146	SLV 1	730	66	2157	-94.52	40.64	-0.25
146	SLV 2	730	66	2157	-94.52	40.64	-0.25
146	SLV 3	764	6	2223	12.54	42.3	-0.01
146	SLV 4	764	6	2223	12.54	42.3	-0.01
146	SLV 5	311	111	1988	-190.7	17.28	-0.43
146	SLV 6	311	111	1988	-190.7	17.28	-0.43
146	SLV 7	423	-90	2209	166.16	22.81	0.35
146	SLV 8	423	-90	2209	166.16	22.81	0.35
146	SLV 9	-15	90	1909	-166.08	-1.08	-0.35
146	SLV 10	-15	90	1909	-166.08	-1.08	-0.35
146	SLV 11	97	-111	2130	190.78	4.45	0.43
146	SLV 12	97	-111	2130	190.78	4.45	0.43
146	SLV 13	-356	-6	1894	-12.46	-20.57	0.01
146	SLV 14	-356	-6	1894	-12.46	-20.57	0.01
146	SLV 15	-322	-66	1961	94.6	-18.91	0.25
146	SLV 16	-322	-66	1961	94.6	-18.91	0.25
147	SLU 1	159	0	1851	0.05	9.3	0
147	SLU 2	159	0	1851	0.05	9.3	0
147	SLU 3	159	0	1851	0.05	9.3	0
147	SLU 4	159	0	1851	0.05	9.3	0
147	SLU 5	159	0	1851	0.05	9.3	0
147	SLU 6	159	0	1851	0.05	9.3	0
147	SLU 7	159	0	1851	0.05	9.3	0
147	SLU 8	159	0	1851	0.05	9.3	0
147	SLU 9	159	0	1851	0.05	9.3	0
147	SLU 10	233	0	2231	0.05	13.46	0
147	SLU 11	233	0	2231	0.05	13.46	0
147	SLU 12	233	0	2231	0.05	13.46	0
147	SLU 13	233	0	2231	0.05	13.46	0
147	SLU 14	233	0	2231	0.05	13.46	0
147	SLU 15	233	0	2231	0.05	13.46	0
147	SLU 16	233	0	2231	0.05	13.46	0
147	SLU 17	233	0	2231	0.05	13.46	0
147	SLU 18	264	0	2395	0.06	15.25	0
147	SLU 19	264	0	2395	0.06	15.25	0
147	SLU 20	264	0	2395	0.06	15.25	0
147	SLU 21	264	0	2395	0.06	15.25	0
147	SLU 22	195	0	2074	0.05	11.36	0
147	SLU 23	195	0	2074	0.05	11.36	0
147	SLU 24	195	0	2074	0.05	11.36	0
147	SLU 25	195	0	2074	0.05	11.36	0
147	SLU 26	195	0	2074	0.05	11.36	0
147	SLU 27	195	0	2074	0.05	11.36	0
147	SLU 28	195	0	2074	0.05	11.36	0
147	SLU 29	195	0	2074	0.05	11.36	0
147	SLU 30	195	0	2074	0.05	11.36	0
147	SLU 31	269	0	2455	0.06	15.52	0
147	SLU 32	269	0	2455	0.06	15.52	0
147	SLU 33	269	0	2455	0.06	15.52	0
147	SLU 34	269	0	2455	0.06	15.52	0
147	SLU 35	269	0	2455	0.06	15.52	0
147	SLU 36	269	0	2455	0.06	15.52	0
147	SLU 37	269	0	2455	0.06	15.52	0
147	SLU 38	269	0	2455	0.06	15.52	0
147	SLU 39	300	0	2618	0.06	17.31	0
147	SLU 40	300	0	2618	0.06	17.31	0
147	SLU 41	300	0	2618	0.06	17.31	0
147	SLU 42	300	0	2618	0.06	17.31	0
147	SLU 43	195	0	2329	0.06	11.39	0
147	SLU 44	195	0	2329	0.06	11.39	0
147	SLU 45	195	0	2329	0.06	11.39	0
147	SLU 46	195	0	2329	0.06	11.39	0
147	SLU 47	195	0	2329	0.06	11.39	0
147	SLU 48	195	0	2329	0.06	11.39	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
147	SLU 49	195	0	2329	0.06	11.39	0
147	SLU 50	195	0	2329	0.06	11.39	0
147	SLU 51	195	0	2329	0.06	11.39	0
147	SLU 52	268	0	2710	0.07	15.55	0
147	SLU 53	268	0	2710	0.07	15.55	0
147	SLU 54	268	0	2710	0.07	15.55	0
147	SLU 55	268	0	2710	0.07	15.55	0
147	SLU 56	268	0	2710	0.07	15.55	0
147	SLU 57	268	0	2710	0.07	15.55	0
147	SLU 58	268	0	2710	0.07	15.55	0
147	SLU 59	268	0	2710	0.07	15.55	0
147	SLU 60	300	0	2873	0.07	17.33	0
147	SLU 61	300	0	2873	0.07	17.33	0
147	SLU 62	300	0	2873	0.07	17.33	0
147	SLU 63	300	0	2873	0.07	17.33	0
147	SLU 64	231	0	2553	0.06	13.45	0
147	SLU 65	231	0	2553	0.06	13.45	0
147	SLU 66	231	0	2553	0.06	13.45	0
147	SLU 67	231	0	2553	0.06	13.45	0
147	SLU 68	231	0	2553	0.06	13.45	0
147	SLU 69	231	0	2553	0.06	13.45	0
147	SLU 70	231	0	2553	0.06	13.45	0
147	SLU 71	231	0	2553	0.06	13.45	0
147	SLU 72	231	0	2553	0.06	13.45	0
147	SLU 73	304	0	2934	0.07	17.61	0
147	SLU 74	304	0	2934	0.07	17.61	0
147	SLU 75	304	0	2934	0.07	17.61	0
147	SLU 76	304	0	2934	0.07	17.61	0
147	SLU 77	304	0	2934	0.07	17.61	0
147	SLU 78	304	0	2934	0.07	17.61	0
147	SLU 79	304	0	2934	0.07	17.61	0
147	SLU 80	304	0	2934	0.07	17.61	0
147	SLU 81	336	0	3097	0.08	19.39	0
147	SLU 82	336	0	3097	0.08	19.39	0
147	SLU 83	336	0	3097	0.08	19.39	0
147	SLU 84	336	0	3097	0.08	19.39	0
147	SLE RA 1	170	0	1915	0.05	9.89	0
147	SLE RA 2	170	0	1915	0.05	9.89	0
147	SLE RA 3	170	0	1915	0.05	9.89	0
147	SLE RA 4	170	0	1915	0.05	9.89	0
147	SLE RA 5	170	0	1915	0.05	9.89	0
147	SLE RA 6	170	0	1915	0.05	9.89	0
147	SLE RA 7	170	0	1915	0.05	9.89	0
147	SLE RA 8	170	0	1915	0.05	9.89	0
147	SLE RA 9	170	0	1915	0.05	9.89	0
147	SLE RA 10	219	0	2168	0.05	12.67	0
147	SLE RA 11	219	0	2168	0.05	12.67	0
147	SLE RA 12	219	0	2168	0.05	12.67	0
147	SLE RA 13	219	0	2168	0.05	12.67	0
147	SLE RA 14	219	0	2168	0.05	12.67	0
147	SLE RA 15	219	0	2168	0.05	12.67	0
147	SLE RA 16	219	0	2168	0.05	12.67	0
147	SLE RA 17	219	0	2168	0.05	12.67	0
147	SLE RA 18	240	0	2277	0.06	13.85	0
147	SLE RA 19	240	0	2277	0.06	13.85	0
147	SLE RA 20	240	0	2277	0.06	13.85	0
147	SLE RA 21	240	0	2277	0.06	13.85	0
147	SLE FR 1	170	0	1915	0.05	9.89	0
147	SLE FR 2	170	0	1915	0.05	9.89	0
147	SLE FR 3	170	0	1915	0.05	9.89	0
147	SLE FR 4	191	0	2023	0.05	11.08	0
147	SLE FR 5	191	0	2023	0.05	11.08	0
147	SLE FR 6	205	0	2096	0.05	11.87	0
147	SLE QP 1	170	0	1915	0.05	9.89	0
147	SLE QP 2	191	0	2023	0.05	11.08	0
147	SLD 1	412	25	2051	-33.08	23.55	-0.07
147	SLD 2	412	25	2051	-33.08	23.55	-0.07
147	SLD 3	425	3	2077	1.88	24.28	0
147	SLD 4	425	3	2077	1.88	24.28	0
147	SLD 5	237	42	1992	-62.9	13.72	-0.12
147	SLD 6	237	42	1992	-62.9	13.72	-0.12
147	SLD 7	281	-33	2079	53.61	16.14	0.1
147	SLD 8	281	-33	2079	53.61	16.14	0.1
147	SLD 9	101	33	1968	-53.51	6.02	-0.1
147	SLD 10	101	33	1968	-53.51	6.02	-0.1
147	SLD 11	144	-42	2055	63	8.44	0.12
147	SLD 12	144	-42	2055	63	8.44	0.12
147	SLD 13	-44	-3	1969	-1.78	-2.12	0
147	SLD 14	-44	-3	1969	-1.78	-2.12	0
147	SLD 15	-31	-25	1996	33.18	-1.39	0.07
147	SLD 16	-31	-25	1996	33.18	-1.39	0.07
147	SLV 1	712	64	2085	-87.29	40.43	-0.17
147	SLV 2	712	64	2085	-87.29	40.43	-0.17
147	SLV 3	745	6	2152	7.13	42.32	0
147	SLV 4	745	6	2152	7.13	42.32	0
147	SLV 5	297	108	1941	-169.36	17.02	-0.31
147	SLV 6	297	108	1941	-169.36	17.02	-0.31
147	SLV 7	407	-87	2163	145.38	23.32	0.26



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
147	SLV 8	407	-87	2163	145.38	23.32	0.26
147	SLV 9	-26	87	1883	-145.28	-1.15	-0.26
147	SLV 10	-26	87	1883	-145.28	-1.15	-0.26
147	SLV 11	84	-108	2106	169.46	5.14	0.31
147	SLV 12	84	-108	2106	169.46	5.14	0.31
147	SLV 13	-364	-6	1895	-7.03	-20.16	0
147	SLV 14	-364	-6	1895	-7.03	-20.16	0
147	SLV 15	-331	-64	1961	87.39	-18.27	0.17
147	SLV 16	-331	-64	1961	87.39	-18.27	0.17
148	SLU 1	135	0	1866	0.06	7.38	0
148	SLU 2	135	0	1866	0.06	7.38	0
148	SLU 3	135	0	1866	0.06	7.38	0
148	SLU 4	135	0	1866	0.06	7.38	0
148	SLU 5	135	0	1866	0.06	7.38	0
148	SLU 6	135	0	1866	0.06	7.38	0
148	SLU 7	135	0	1866	0.06	7.38	0
148	SLU 8	135	0	1866	0.06	7.38	0
148	SLU 9	135	0	1866	0.06	7.38	0
148	SLU 10	202	0	2243	0.07	10.99	0
148	SLU 11	202	0	2243	0.07	10.99	0
148	SLU 12	202	0	2243	0.07	10.99	0
148	SLU 13	202	0	2243	0.07	10.99	0
148	SLU 14	202	0	2243	0.07	10.99	0
148	SLU 15	202	0	2243	0.07	10.99	0
148	SLU 16	202	0	2243	0.07	10.99	0
148	SLU 17	202	0	2243	0.07	10.99	0
148	SLU 18	231	0	2404	0.08	12.54	0
148	SLU 19	231	0	2404	0.08	12.54	0
148	SLU 20	231	0	2404	0.08	12.54	0
148	SLU 21	231	0	2404	0.08	12.54	0
148	SLU 22	168	0	2088	0.07	9.13	0
148	SLU 23	168	0	2088	0.07	9.13	0
148	SLU 24	168	0	2088	0.07	9.13	0
148	SLU 25	168	0	2088	0.07	9.13	0
148	SLU 26	168	0	2088	0.07	9.13	0
148	SLU 27	168	0	2088	0.07	9.13	0
148	SLU 28	168	0	2088	0.07	9.13	0
148	SLU 29	168	0	2088	0.07	9.13	0
148	SLU 30	168	0	2088	0.07	9.13	0
148	SLU 31	234	0	2465	0.08	12.74	0
148	SLU 32	234	0	2465	0.08	12.74	0
148	SLU 33	234	0	2465	0.08	12.74	0
148	SLU 34	234	0	2465	0.08	12.74	0
148	SLU 35	234	0	2465	0.08	12.74	0
148	SLU 36	234	0	2465	0.08	12.74	0
148	SLU 37	234	0	2465	0.08	12.74	0
148	SLU 38	234	0	2465	0.08	12.74	0
148	SLU 39	263	0	2626	0.09	14.29	0
148	SLU 40	263	0	2626	0.09	14.29	0
148	SLU 41	263	0	2626	0.09	14.29	0
148	SLU 42	263	0	2626	0.09	14.29	0
148	SLU 43	164	0	2349	0.08	8.99	0
148	SLU 44	164	0	2349	0.08	8.99	0
148	SLU 45	164	0	2349	0.08	8.99	0
148	SLU 46	164	0	2349	0.08	8.99	0
148	SLU 47	164	0	2349	0.08	8.99	0
148	SLU 48	164	0	2349	0.08	8.99	0
148	SLU 49	164	0	2349	0.08	8.99	0
148	SLU 50	164	0	2349	0.08	8.99	0
148	SLU 51	164	0	2349	0.08	8.99	0
148	SLU 52	231	0	2726	0.09	12.6	0
148	SLU 53	231	0	2726	0.09	12.6	0
148	SLU 54	231	0	2726	0.09	12.6	0
148	SLU 55	231	0	2726	0.09	12.6	0
148	SLU 56	231	0	2726	0.09	12.6	0
148	SLU 57	231	0	2726	0.09	12.6	0
148	SLU 58	231	0	2726	0.09	12.6	0
148	SLU 59	231	0	2726	0.09	12.6	0
148	SLU 60	260	0	2888	0.1	14.15	0
148	SLU 61	260	0	2888	0.1	14.15	0
148	SLU 62	260	0	2888	0.1	14.15	0
148	SLU 63	260	0	2888	0.1	14.15	0
148	SLU 64	197	0	2572	0.09	10.74	0
148	SLU 65	197	0	2572	0.09	10.74	0
148	SLU 66	197	0	2572	0.09	10.74	0
148	SLU 67	197	0	2572	0.09	10.74	0
148	SLU 68	197	0	2572	0.09	10.74	0
148	SLU 69	197	0	2572	0.09	10.74	0
148	SLU 70	197	0	2572	0.09	10.74	0
148	SLU 71	197	0	2572	0.09	10.74	0
148	SLU 72	197	0	2572	0.09	10.74	0
148	SLU 73	264	0	2948	0.1	14.35	0
148	SLU 74	264	0	2948	0.1	14.35	0
148	SLU 75	264	0	2948	0.1	14.35	0
148	SLU 76	264	0	2948	0.1	14.35	0
148	SLU 77	264	0	2948	0.1	14.35	0
148	SLU 78	264	0	2948	0.1	14.35	0
148	SLU 79	264	0	2948	0.1	14.35	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
148	SLU 80	264	0	2948	0.1	14.35	0
148	SLU 81	292	0	3110	0.1	15.9	0
148	SLU 82	292	0	3110	0.1	15.9	0
148	SLU 83	292	0	3110	0.1	15.9	0
148	SLU 84	292	0	3110	0.1	15.9	0
148	SLE RA 1	144	0	1929	0.07	7.88	0
148	SLE RA 2	144	0	1929	0.07	7.88	0
148	SLE RA 3	144	0	1929	0.07	7.88	0
148	SLE RA 4	144	0	1929	0.07	7.88	0
148	SLE RA 5	144	0	1929	0.07	7.88	0
148	SLE RA 6	144	0	1929	0.07	7.88	0
148	SLE RA 7	144	0	1929	0.07	7.88	0
148	SLE RA 8	144	0	1929	0.07	7.88	0
148	SLE RA 9	144	0	1929	0.07	7.88	0
148	SLE RA 10	189	0	2180	0.07	10.29	0
148	SLE RA 11	189	0	2180	0.07	10.29	0
148	SLE RA 12	189	0	2180	0.07	10.29	0
148	SLE RA 13	189	0	2180	0.07	10.29	0
148	SLE RA 14	189	0	2180	0.07	10.29	0
148	SLE RA 15	189	0	2180	0.07	10.29	0
148	SLE RA 16	189	0	2180	0.07	10.29	0
148	SLE RA 17	189	0	2180	0.07	10.29	0
148	SLE RA 18	208	0	2288	0.08	11.32	0
148	SLE RA 19	208	0	2288	0.08	11.32	0
148	SLE RA 20	208	0	2288	0.08	11.32	0
148	SLE RA 21	208	0	2288	0.08	11.32	0
148	SLE FR 1	144	0	1929	0.07	7.88	0
148	SLE FR 2	144	0	1929	0.07	7.88	0
148	SLE FR 3	144	0	1929	0.07	7.88	0
148	SLE FR 4	163	0	2037	0.07	8.91	0
148	SLE FR 5	163	0	2037	0.07	8.91	0
148	SLE FR 6	176	0	2109	0.07	9.6	0
148	SLE QP 1	144	0	1929	0.07	7.88	0
148	SLE QP 2	163	0	2037	0.07	8.91	0
148	SLD 1	375	24	2055	-30.11	20.62	-0.03
148	SLD 2	375	24	2055	-30.11	20.62	-0.03
148	SLD 3	387	3	2086	0.64	21.27	0
148	SLD 4	387	3	2086	0.64	21.27	0
148	SLD 5	207	39	1995	-55.62	11.45	-0.06
148	SLD 6	207	39	1995	-55.62	11.45	-0.06
148	SLD 7	250	-32	2099	46.88	13.59	0.05
148	SLD 8	250	-32	2099	46.88	13.59	0.05
148	SLD 9	77	32	1975	-46.74	4.23	-0.05
148	SLD 10	77	32	1975	-46.74	4.23	-0.05
148	SLD 11	119	-40	2079	55.76	6.37	0.06
148	SLD 12	119	-40	2079	55.76	6.37	0.06
148	SLD 13	-61	-3	1988	-0.5	-3.45	0
148	SLD 14	-61	-3	1988	-0.5	-3.45	0
148	SLD 15	-48	-24	2019	30.25	-2.81	0.03
148	SLD 16	-48	-24	2019	30.25	-2.81	0.03
148	SLV 1	661	61	2077	-78.86	36.54	-0.09
148	SLV 2	661	61	2077	-78.86	36.54	-0.09
148	SLV 3	692	6	2154	3.28	38.1	0.01
148	SLV 4	692	6	2154	3.28	38.1	0.01
148	SLV 5	265	101	1931	-148.19	14.83	-0.17
148	SLV 6	265	101	1931	-148.19	14.83	-0.17
148	SLV 7	370	-81	2190	125.61	20.03	0.15
148	SLV 8	370	-81	2190	125.61	20.03	0.15
148	SLV 9	-43	81	1884	-125.48	-2.21	-0.15
148	SLV 10	-43	81	1884	-125.48	-2.21	-0.15
148	SLV 11	61	-101	2143	148.33	2.99	0.17
148	SLV 12	61	-101	2143	148.33	2.99	0.17
148	SLV 13	-366	-6	1920	-3.14	-20.28	-0.01
148	SLV 14	-366	-6	1920	-3.14	-20.28	-0.01
148	SLV 15	-334	-61	1997	79	-18.72	0.09
148	SLV 16	-334	-61	1997	79	-18.72	0.09
149	SLU 1	152	0	1916	0.09	9.01	0
149	SLU 2	152	0	1916	0.09	9.01	0
149	SLU 3	152	0	1916	0.09	9.01	0
149	SLU 4	152	0	1916	0.09	9.01	0
149	SLU 5	152	0	1916	0.09	9.01	0
149	SLU 6	152	0	1916	0.09	9.01	0
149	SLU 7	152	0	1916	0.09	9.01	0
149	SLU 8	152	0	1916	0.09	9.01	0
149	SLU 9	152	0	1916	0.09	9.01	0
149	SLU 10	225	0	2300	0.1	13.12	0
149	SLU 11	225	0	2300	0.1	13.12	0
149	SLU 12	225	0	2300	0.1	13.12	0
149	SLU 13	225	0	2300	0.1	13.12	0
149	SLU 14	225	0	2300	0.1	13.12	0
149	SLU 15	225	0	2300	0.1	13.12	0
149	SLU 16	225	0	2300	0.1	13.12	0
149	SLU 17	225	0	2300	0.1	13.12	0
149	SLU 18	256	0	2464	0.11	14.87	0
149	SLU 19	256	0	2464	0.11	14.87	0
149	SLU 20	256	0	2464	0.11	14.87	0
149	SLU 21	256	0	2464	0.11	14.87	0
149	SLU 22	189	0	2142	0.1	11.07	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
149	SLU 23	189	0	2142	0.1	11.07	0
149	SLU 24	189	0	2142	0.1	11.07	0
149	SLU 25	189	0	2142	0.1	11.07	0
149	SLU 26	189	0	2142	0.1	11.07	0
149	SLU 27	189	0	2142	0.1	11.07	0
149	SLU 28	189	0	2142	0.1	11.07	0
149	SLU 29	189	0	2142	0.1	11.07	0
149	SLU 30	189	0	2142	0.1	11.07	0
149	SLU 31	261	0	2526	0.11	15.17	0
149	SLU 32	261	0	2526	0.11	15.17	0
149	SLU 33	261	0	2526	0.11	15.17	0
149	SLU 34	261	0	2526	0.11	15.17	0
149	SLU 35	261	0	2526	0.11	15.17	0
149	SLU 36	261	0	2526	0.11	15.17	0
149	SLU 37	261	0	2526	0.11	15.17	0
149	SLU 38	261	0	2526	0.11	15.17	0
149	SLU 39	292	0	2690	0.12	16.93	0
149	SLU 40	292	0	2690	0.12	16.93	0
149	SLU 41	292	0	2690	0.12	16.93	0
149	SLU 42	292	0	2690	0.12	16.93	0
149	SLU 43	186	0	2413	0.11	11.01	0
149	SLU 44	186	0	2413	0.11	11.01	0
149	SLU 45	186	0	2413	0.11	11.01	0
149	SLU 46	186	0	2413	0.11	11.01	0
149	SLU 47	186	0	2413	0.11	11.01	0
149	SLU 48	186	0	2413	0.11	11.01	0
149	SLU 49	186	0	2413	0.11	11.01	0
149	SLU 50	186	0	2413	0.11	11.01	0
149	SLU 51	186	0	2413	0.11	11.01	0
149	SLU 52	258	0	2797	0.13	15.12	0
149	SLU 53	258	0	2797	0.13	15.12	0
149	SLU 54	258	0	2797	0.13	15.12	0
149	SLU 55	258	0	2797	0.13	15.12	0
149	SLU 56	258	0	2797	0.13	15.12	0
149	SLU 57	258	0	2797	0.13	15.12	0
149	SLU 58	258	0	2797	0.13	15.12	0
149	SLU 59	258	0	2797	0.13	15.12	0
149	SLU 60	289	0	2961	0.13	16.87	0
149	SLU 61	289	0	2961	0.13	16.87	0
149	SLU 62	289	0	2961	0.13	16.87	0
149	SLU 63	289	0	2961	0.13	16.87	0
149	SLU 64	222	0	2639	0.12	13.07	0
149	SLU 65	222	0	2639	0.12	13.07	0
149	SLU 66	222	0	2639	0.12	13.07	0
149	SLU 67	222	0	2639	0.12	13.07	0
149	SLU 68	222	0	2639	0.12	13.07	0
149	SLU 69	222	0	2639	0.12	13.07	0
149	SLU 70	222	0	2639	0.12	13.07	0
149	SLU 71	222	0	2639	0.12	13.07	0
149	SLU 72	222	0	2639	0.12	13.07	0
149	SLU 73	294	0	3023	0.14	17.17	0
149	SLU 74	294	0	3023	0.14	17.17	0
149	SLU 75	294	0	3023	0.14	17.17	0
149	SLU 76	294	0	3023	0.14	17.17	0
149	SLU 77	294	0	3023	0.14	17.17	0
149	SLU 78	294	0	3023	0.14	17.17	0
149	SLU 79	294	0	3023	0.14	17.17	0
149	SLU 80	294	0	3023	0.14	17.17	0
149	SLU 81	326	0	3188	0.14	18.93	0
149	SLU 82	326	0	3188	0.14	18.93	0
149	SLU 83	326	0	3188	0.14	18.93	0
149	SLU 84	326	0	3188	0.14	18.93	0
149	SLE RA 1	163	0	1980	0.09	9.6	0
149	SLE RA 2	163	0	1980	0.09	9.6	0
149	SLE RA 3	163	0	1980	0.09	9.6	0
149	SLE RA 4	163	0	1980	0.09	9.6	0
149	SLE RA 5	163	0	1980	0.09	9.6	0
149	SLE RA 6	163	0	1980	0.09	9.6	0
149	SLE RA 7	163	0	1980	0.09	9.6	0
149	SLE RA 8	163	0	1980	0.09	9.6	0
149	SLE RA 9	163	0	1980	0.09	9.6	0
149	SLE RA 10	211	0	2236	0.1	12.34	0
149	SLE RA 11	211	0	2236	0.1	12.34	0
149	SLE RA 12	211	0	2236	0.1	12.34	0
149	SLE RA 13	211	0	2236	0.1	12.34	0
149	SLE RA 14	211	0	2236	0.1	12.34	0
149	SLE RA 15	211	0	2236	0.1	12.34	0
149	SLE RA 16	211	0	2236	0.1	12.34	0
149	SLE RA 17	211	0	2236	0.1	12.34	0
149	SLE RA 18	232	0	2346	0.11	13.51	0
149	SLE RA 19	232	0	2346	0.11	13.51	0
149	SLE RA 20	232	0	2346	0.11	13.51	0
149	SLE RA 21	232	0	2346	0.11	13.51	0
149	SLE FR 1	163	0	1980	0.09	9.6	0
149	SLE FR 2	163	0	1980	0.09	9.6	0
149	SLE FR 3	163	0	1980	0.09	9.6	0
149	SLE FR 4	183	0	2090	0.1	10.77	0
149	SLE FR 5	183	0	2090	0.1	10.77	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
149	SLE FR 6	197	0	2163	0.1	11.55	0
149	SLE QP 1	163	0	1980	0.09	9.6	0
149	SLE QP 2	183	0	2090	0.1	10.77	0
149	SLD 1	381	22	2109	-26.34	21.62	-0.04
149	SLD 2	381	22	2109	-26.34	21.62	-0.04
149	SLD 3	395	3	2149	-0.26	22.33	0
149	SLD 4	395	3	2149	-0.26	22.33	0
149	SLD 5	222	35	2035	-47.38	12.95	-0.06
149	SLD 6	222	35	2035	-47.38	12.95	-0.06
149	SLD 7	268	-28	2168	39.54	15.32	0.05
149	SLD 8	268	-28	2168	39.54	15.32	0.05
149	SLD 9	99	28	2012	-39.34	6.23	-0.05
149	SLD 10	99	28	2012	-39.34	6.23	-0.05
149	SLD 11	145	-35	2145	47.58	8.59	0.06
149	SLD 12	145	-35	2145	47.58	8.59	0.06
149	SLD 13	-28	-3	2031	0.46	-0.79	0
149	SLD 14	-28	-3	2031	0.46	-0.79	0
149	SLD 15	-14	-22	2071	26.53	-0.08	0.04
149	SLD 16	-14	-22	2071	26.53	-0.08	0.04
149	SLV 1	649	55	2131	-68.53	36.36	-0.09
149	SLV 2	649	55	2131	-68.53	36.36	-0.09
149	SLV 3	683	7	2229	0.43	38.1	-0.01
149	SLV 4	683	7	2229	0.43	38.1	-0.01
149	SLV 5	273	89	1954	-125.07	15.81	-0.15
149	SLV 6	273	89	1954	-125.07	15.81	-0.15
149	SLV 7	384	-71	2281	104.77	21.61	0.12
149	SLV 8	384	-71	2281	104.77	21.61	0.12
149	SLV 9	-17	71	1899	-104.58	-0.07	-0.12
149	SLV 10	-17	71	1899	-104.58	-0.07	-0.12
149	SLV 11	94	-90	2227	125.26	5.74	0.15
149	SLV 12	94	-90	2227	125.26	5.74	0.15
149	SLV 13	-316	-7	1951	-0.23	-16.55	0.01
149	SLV 14	-316	-7	1951	-0.23	-16.55	0.01
149	SLV 15	-283	-55	2049	68.72	-14.81	0.09
149	SLV 16	-283	-55	2049	68.72	-14.81	0.09
150	SLU 1	187	0	1971	0.13	10.14	0
150	SLU 2	187	0	1971	0.13	10.14	0
150	SLU 3	187	0	1971	0.13	10.14	0
150	SLU 4	187	0	1971	0.13	10.14	0
150	SLU 5	187	0	1971	0.13	10.14	0
150	SLU 6	187	0	1971	0.13	10.14	0
150	SLU 7	187	0	1971	0.13	10.14	0
150	SLU 8	187	0	1971	0.13	10.14	0
150	SLU 9	187	0	1971	0.13	10.14	0
150	SLU 10	270	0	2364	0.16	14.51	0
150	SLU 11	270	0	2364	0.16	14.51	0
150	SLU 12	270	0	2364	0.16	14.51	0
150	SLU 13	270	0	2364	0.16	14.51	0
150	SLU 14	270	0	2364	0.16	14.51	0
150	SLU 15	270	0	2364	0.16	14.51	0
150	SLU 16	270	0	2364	0.16	14.51	0
150	SLU 17	270	0	2364	0.16	14.51	0
150	SLU 18	306	0	2533	0.16	16.39	0
150	SLU 19	306	0	2533	0.16	16.39	0
150	SLU 20	306	0	2533	0.16	16.39	0
150	SLU 21	306	0	2533	0.16	16.39	0
150	SLU 22	230	0	2202	0.15	12.37	0
150	SLU 23	230	0	2202	0.15	12.37	0
150	SLU 24	230	0	2202	0.15	12.37	0
150	SLU 25	230	0	2202	0.15	12.37	0
150	SLU 26	230	0	2202	0.15	12.37	0
150	SLU 27	230	0	2202	0.15	12.37	0
150	SLU 28	230	0	2202	0.15	12.37	0
150	SLU 29	230	0	2202	0.15	12.37	0
150	SLU 30	230	0	2202	0.15	12.37	0
150	SLU 31	313	0	2595	0.17	16.75	0
150	SLU 32	313	0	2595	0.17	16.75	0
150	SLU 33	313	0	2595	0.17	16.75	0
150	SLU 34	313	0	2595	0.17	16.75	0
150	SLU 35	313	0	2595	0.17	16.75	0
150	SLU 36	313	0	2595	0.17	16.75	0
150	SLU 37	313	0	2595	0.17	16.75	0
150	SLU 38	313	0	2595	0.17	16.75	0
150	SLU 39	348	0	2764	0.18	18.62	0
150	SLU 40	348	0	2764	0.18	18.62	0
150	SLU 41	348	0	2764	0.18	18.62	0
150	SLU 42	348	0	2764	0.18	18.62	0
150	SLU 43	229	0	2484	0.17	12.41	0
150	SLU 44	229	0	2484	0.17	12.41	0
150	SLU 45	229	0	2484	0.17	12.41	0
150	SLU 46	229	0	2484	0.17	12.41	0
150	SLU 47	229	0	2484	0.17	12.41	0
150	SLU 48	229	0	2484	0.17	12.41	0
150	SLU 49	229	0	2484	0.17	12.41	0
150	SLU 50	229	0	2484	0.17	12.41	0
150	SLU 51	229	0	2484	0.17	12.41	0
150	SLU 52	312	0	2877	0.19	16.79	0
150	SLU 53	312	0	2877	0.19	16.79	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
150	SLU 54	312	0	2877	0.19	16.79	0
150	SLU 55	312	0	2877	0.19	16.79	0
150	SLU 56	312	0	2877	0.19	16.79	0
150	SLU 57	312	0	2877	0.19	16.79	0
150	SLU 58	312	0	2877	0.19	16.79	0
150	SLU 59	312	0	2877	0.19	16.79	0
150	SLU 60	348	0	3045	0.2	18.66	0
150	SLU 61	348	0	3045	0.2	18.66	0
150	SLU 62	348	0	3045	0.2	18.66	0
150	SLU 63	348	0	3045	0.2	18.66	0
150	SLU 64	272	0	2715	0.18	14.65	0
150	SLU 65	272	0	2715	0.18	14.65	0
150	SLU 66	272	0	2715	0.18	14.65	0
150	SLU 67	272	0	2715	0.18	14.65	0
150	SLU 68	272	0	2715	0.18	14.65	0
150	SLU 69	272	0	2715	0.18	14.65	0
150	SLU 70	272	0	2715	0.18	14.65	0
150	SLU 71	272	0	2715	0.18	14.65	0
150	SLU 72	272	0	2715	0.18	14.65	0
150	SLU 73	355	0	3108	0.2	19.02	0
150	SLU 74	355	0	3108	0.2	19.02	0
150	SLU 75	355	0	3108	0.2	19.02	0
150	SLU 76	355	0	3108	0.2	19.02	0
150	SLU 77	355	0	3108	0.2	19.02	0
150	SLU 78	355	0	3108	0.2	19.02	0
150	SLU 79	355	0	3108	0.2	19.02	0
150	SLU 80	355	0	3108	0.2	19.02	0
150	SLU 81	390	0	3276	0.21	20.9	0
150	SLU 82	390	0	3276	0.21	20.9	0
150	SLU 83	390	0	3276	0.21	20.9	0
150	SLU 84	390	0	3276	0.21	20.9	0
150	SLE RA 1	200	0	2037	0.14	10.78	0
150	SLE RA 2	200	0	2037	0.14	10.78	0
150	SLE RA 3	200	0	2037	0.14	10.78	0
150	SLE RA 4	200	0	2037	0.14	10.78	0
150	SLE RA 5	200	0	2037	0.14	10.78	0
150	SLE RA 6	200	0	2037	0.14	10.78	0
150	SLE RA 7	200	0	2037	0.14	10.78	0
150	SLE RA 8	200	0	2037	0.14	10.78	0
150	SLE RA 9	200	0	2037	0.14	10.78	0
150	SLE RA 10	255	0	2299	0.15	13.69	0
150	SLE RA 11	255	0	2299	0.15	13.69	0
150	SLE RA 12	255	0	2299	0.15	13.69	0
150	SLE RA 13	255	0	2299	0.15	13.69	0
150	SLE RA 14	255	0	2299	0.15	13.69	0
150	SLE RA 15	255	0	2299	0.15	13.69	0
150	SLE RA 16	255	0	2299	0.15	13.69	0
150	SLE RA 17	255	0	2299	0.15	13.69	0
150	SLE RA 18	279	0	2412	0.16	14.94	0
150	SLE RA 19	279	0	2412	0.16	14.94	0
150	SLE RA 20	279	0	2412	0.16	14.94	0
150	SLE RA 21	279	0	2412	0.16	14.94	0
150	SLE FR 1	200	0	2037	0.14	10.78	0
150	SLE FR 2	200	0	2037	0.14	10.78	0
150	SLE FR 3	200	0	2037	0.14	10.78	0
150	SLE FR 4	223	0	2150	0.14	12.03	0
150	SLE FR 5	223	0	2150	0.14	12.03	0
150	SLE FR 6	239	0	2225	0.15	12.86	0
150	SLE QP 1	200	0	2037	0.14	10.78	0
150	SLE QP 2	223	0	2150	0.14	12.03	0
150	SLD 1	421	18	2182	-21.72	22.54	-0.02
150	SLD 2	421	18	2182	-21.72	22.54	-0.02
150	SLD 3	406	3	2235	-0.94	21.83	-0.01
150	SLD 4	406	3	2235	-0.94	21.83	-0.01
150	SLD 5	306	28	2080	-37.93	16.25	-0.04
150	SLD 6	306	28	2080	-37.93	16.25	-0.04
150	SLD 7	255	-22	2255	31.33	13.89	0.03
150	SLD 8	255	-22	2255	31.33	13.89	0.03
150	SLD 9	192	22	2044	-31.05	10.16	-0.03
150	SLD 10	192	22	2044	-31.05	10.16	-0.03
150	SLD 11	141	-28	2220	38.22	7.8	0.04
150	SLD 12	141	-28	2220	38.22	7.8	0.04
150	SLD 13	41	-3	2064	1.23	2.22	0.01
150	SLD 14	41	-3	2064	1.23	2.22	0.01
150	SLD 15	26	-18	2117	22.01	1.51	0.02
150	SLD 16	26	-18	2117	22.01	1.51	0.02
150	SLV 1	689	46	2224	-56.22	36.85	-0.06
150	SLV 2	689	46	2224	-56.22	36.85	-0.06
150	SLV 3	653	8	2352	-1.79	35.17	-0.02
150	SLV 4	653	8	2352	-1.79	35.17	-0.02
150	SLV 5	418	71	1978	-99.32	22.03	-0.09
150	SLV 6	418	71	1978	-99.32	22.03	-0.09
150	SLV 7	298	-55	2404	82.11	16.41	0.07
150	SLV 8	298	-55	2404	82.11	16.41	0.07
150	SLV 9	149	55	1895	-81.83	7.64	-0.07
150	SLV 10	149	55	1895	-81.83	7.64	-0.07
150	SLV 11	29	-71	2321	99.6	2.02	0.09
150	SLV 12	29	-71	2321	99.6	2.02	0.09



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
150	SLV 13	-207	-8	1947	2.08	-11.11	0.02
150	SLV 14	-207	-8	1947	2.08	-11.11	0.02
150	SLV 15	-243	-46	2075	56.5	-12.8	0.06
150	SLV 16	-243	-46	2075	56.5	-12.8	0.06
151	SLU 1	249	0	2025	0.22	13.28	0
151	SLU 2	249	0	2025	0.22	13.28	0
151	SLU 3	249	0	2025	0.22	13.28	0
151	SLU 4	249	0	2025	0.22	13.28	0
151	SLU 5	249	0	2025	0.22	13.28	0
151	SLU 6	249	0	2025	0.22	13.28	0
151	SLU 7	249	0	2025	0.22	13.28	0
151	SLU 8	249	0	2025	0.22	13.28	0
151	SLU 9	249	0	2025	0.22	13.28	0
151	SLU 10	349	0	2427	0.25	18.52	0
151	SLU 11	349	0	2427	0.25	18.52	0
151	SLU 12	349	0	2427	0.25	18.52	0
151	SLU 13	349	0	2427	0.25	18.52	0
151	SLU 14	349	0	2427	0.25	18.52	0
151	SLU 15	349	0	2427	0.25	18.52	0
151	SLU 16	349	0	2427	0.25	18.52	0
151	SLU 17	349	0	2427	0.25	18.52	0
151	SLU 18	392	0	2599	0.27	20.77	0
151	SLU 19	392	0	2599	0.27	20.77	0
151	SLU 20	392	0	2599	0.27	20.77	0
151	SLU 21	392	0	2599	0.27	20.77	0
151	SLU 22	302	0	2260	0.24	16.02	0
151	SLU 23	302	0	2260	0.24	16.02	0
151	SLU 24	302	0	2260	0.24	16.02	0
151	SLU 25	302	0	2260	0.24	16.02	0
151	SLU 26	302	0	2260	0.24	16.02	0
151	SLU 27	302	0	2260	0.24	16.02	0
151	SLU 28	302	0	2260	0.24	16.02	0
151	SLU 29	302	0	2260	0.24	16.02	0
151	SLU 30	302	0	2260	0.24	16.02	0
151	SLU 31	402	0	2661	0.28	21.27	0
151	SLU 32	402	0	2661	0.28	21.27	0
151	SLU 33	402	0	2661	0.28	21.27	0
151	SLU 34	402	0	2661	0.28	21.27	0
151	SLU 35	402	0	2661	0.28	21.27	0
151	SLU 36	402	0	2661	0.28	21.27	0
151	SLU 37	402	0	2661	0.28	21.27	0
151	SLU 38	402	0	2661	0.28	21.27	0
151	SLU 39	445	0	2833	0.29	23.51	0
151	SLU 40	445	0	2833	0.29	23.51	0
151	SLU 41	445	0	2833	0.29	23.51	0
151	SLU 42	445	0	2833	0.29	23.51	0
151	SLU 43	306	0	2553	0.27	16.32	0
151	SLU 44	306	0	2553	0.27	16.32	0
151	SLU 45	306	0	2553	0.27	16.32	0
151	SLU 46	306	0	2553	0.27	16.32	0
151	SLU 47	306	0	2553	0.27	16.32	0
151	SLU 48	306	0	2553	0.27	16.32	0
151	SLU 49	306	0	2553	0.27	16.32	0
151	SLU 50	306	0	2553	0.27	16.32	0
151	SLU 51	306	0	2553	0.27	16.32	0
151	SLU 52	406	0	2954	0.31	21.56	0
151	SLU 53	406	0	2954	0.31	21.56	0
151	SLU 54	406	0	2954	0.31	21.56	0
151	SLU 55	406	0	2954	0.31	21.56	0
151	SLU 56	406	0	2954	0.31	21.56	0
151	SLU 57	406	0	2954	0.31	21.56	0
151	SLU 58	406	0	2954	0.31	21.56	0
151	SLU 59	406	0	2954	0.31	21.56	0
151	SLU 60	449	0	3126	0.33	23.81	0
151	SLU 61	449	0	3126	0.33	23.81	0
151	SLU 62	449	0	3126	0.33	23.81	0
151	SLU 63	449	0	3126	0.33	23.81	0
151	SLU 64	358	0	2787	0.3	19.07	0
151	SLU 65	358	0	2787	0.3	19.07	0
151	SLU 66	358	0	2787	0.3	19.07	0
151	SLU 67	358	0	2787	0.3	19.07	0
151	SLU 68	358	0	2787	0.3	19.07	0
151	SLU 69	358	0	2787	0.3	19.07	0
151	SLU 70	358	0	2787	0.3	19.07	0
151	SLU 71	358	0	2787	0.3	19.07	0
151	SLU 72	358	0	2787	0.3	19.07	0
151	SLU 73	459	0	3188	0.33	24.31	0
151	SLU 74	459	0	3188	0.33	24.31	0
151	SLU 75	459	0	3188	0.33	24.31	0
151	SLU 76	459	0	3188	0.33	24.31	0
151	SLU 77	459	0	3188	0.33	24.31	0
151	SLU 78	459	0	3188	0.33	24.31	0
151	SLU 79	459	0	3188	0.33	24.31	0
151	SLU 80	459	0	3188	0.33	24.31	0
151	SLU 81	502	0	3360	0.35	26.56	0
151	SLU 82	502	0	3360	0.35	26.56	0
151	SLU 83	502	0	3360	0.35	26.56	0
151	SLU 84	502	0	3360	0.35	26.56	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione		
		x	y	z		x	y	z
151	SLE RA 1	264	0	2092		0.22	14.06	0
151	SLE RA 2	264	0	2092		0.22	14.06	0
151	SLE RA 3	264	0	2092		0.22	14.06	0
151	SLE RA 4	264	0	2092		0.22	14.06	0
151	SLE RA 5	264	0	2092		0.22	14.06	0
151	SLE RA 6	264	0	2092		0.22	14.06	0
151	SLE RA 7	264	0	2092		0.22	14.06	0
151	SLE RA 8	264	0	2092		0.22	14.06	0
151	SLE RA 9	264	0	2092		0.22	14.06	0
151	SLE RA 10	331	0	2360		0.25	17.56	0
151	SLE RA 11	331	0	2360		0.25	17.56	0
151	SLE RA 12	331	0	2360		0.25	17.56	0
151	SLE RA 13	331	0	2360		0.25	17.56	0
151	SLE RA 14	331	0	2360		0.25	17.56	0
151	SLE RA 15	331	0	2360		0.25	17.56	0
151	SLE RA 16	331	0	2360		0.25	17.56	0
151	SLE RA 17	331	0	2360		0.25	17.56	0
151	SLE RA 18	360	0	2475		0.26	19.06	0
151	SLE RA 19	360	0	2475		0.26	19.06	0
151	SLE RA 20	360	0	2475		0.26	19.06	0
151	SLE RA 21	360	0	2475		0.26	19.06	0
151	SLE FR 1	264	0	2092		0.22	14.06	0
151	SLE FR 2	264	0	2092		0.22	14.06	0
151	SLE FR 3	264	0	2092		0.22	14.06	0
151	SLE FR 4	293	0	2207		0.23	15.56	0
151	SLE FR 5	293	0	2207		0.23	15.56	0
151	SLE FR 6	312	0	2283		0.24	16.56	0
151	SLE QP 1	264	0	2092		0.22	14.06	0
151	SLE QP 2	293	0	2207		0.23	15.56	0
151	SLD 1	481	5	2270		-16.51	24.74	-0.01
151	SLD 2	481	5	2270		-16.51	24.74	-0.01
151	SLD 3	463	15	2341		-1.45	25.54	-0.02
151	SLD 4	463	15	2341		-1.45	25.54	-0.02
151	SLD 5	376	-15	2119		-27.62	17.1	0
151	SLD 6	376	-15	2119		-27.62	17.1	0
151	SLD 7	317	20	2354		22.56	19.77	-0.01
151	SLD 8	317	20	2354		22.56	19.77	-0.01
151	SLD 9	268	-21	2060		-22.09	11.35	0.01
151	SLD 10	268	-21	2060		-22.09	11.35	0.01
151	SLD 11	210	14	2295		28.09	14.03	-0.01
151	SLD 12	210	14	2295		28.09	14.03	-0.01
151	SLD 13	122	-16	2074		1.92	5.58	0.02
151	SLD 14	122	-16	2074		1.92	5.58	0.02
151	SLD 15	105	-5	2144		16.98	6.38	0.01
151	SLD 16	105	-5	2144		16.98	6.38	0.01
151	SLV 1	736	12	2353		-42.62	37.22	-0.03
151	SLV 2	736	12	2353		-42.62	37.22	-0.03
151	SLV 3	695	38	2523		-3.53	39.14	-0.04
151	SLV 4	695	38	2523		-3.53	39.14	-0.04
151	SLV 5	489	-36	1993		-71.91	19.14	0.01
151	SLV 6	489	-36	1993		-71.91	19.14	0.01
151	SLV 7	350	51	2559		58.39	25.55	-0.04
151	SLV 8	350	51	2559		58.39	25.55	-0.04
151	SLV 9	235	-52	1855		-57.93	5.57	0.03
151	SLV 10	235	-52	1855		-57.93	5.57	0.03
151	SLV 11	97	36	2421		72.38	11.98	-0.02
151	SLV 12	97	36	2421		72.38	11.98	-0.02
151	SLV 13	-109	-39	1891		4	-8.02	0.04
151	SLV 14	-109	-39	1891		4	-8.02	0.04
151	SLV 15	-151	-12	2061		43.09	-6.1	0.03
151	SLV 16	-151	-12	2061		43.09	-6.1	0.03
152	SLU 1	326	0	2075		0.42	16.82	0
152	SLU 2	326	0	2075		0.42	16.82	0
152	SLU 3	326	0	2075		0.42	16.82	0
152	SLU 4	326	0	2075		0.42	16.82	0
152	SLU 5	326	0	2075		0.42	16.82	0
152	SLU 6	326	0	2075		0.42	16.82	0
152	SLU 7	326	0	2075		0.42	16.82	0
152	SLU 8	326	0	2075		0.42	16.82	0
152	SLU 9	326	0	2075		0.42	16.82	0
152	SLU 10	446	-1	2483		0.49	22.87	0
152	SLU 11	446	-1	2483		0.49	22.87	0
152	SLU 12	446	-1	2483		0.49	22.87	0
152	SLU 13	446	-1	2483		0.49	22.87	0
152	SLU 14	446	-1	2483		0.49	22.87	0
152	SLU 15	446	-1	2483		0.49	22.87	0
152	SLU 16	446	-1	2483		0.49	22.87	0
152	SLU 17	446	-1	2483		0.49	22.87	0
152	SLU 18	497	-1	2657		0.52	25.47	0
152	SLU 19	497	-1	2657		0.52	25.47	0
152	SLU 20	497	-1	2657		0.52	25.47	0
152	SLU 21	497	-1	2657		0.52	25.47	0
152	SLU 22	390	-1	2312		0.46	20.04	0
152	SLU 23	390	-1	2312		0.46	20.04	0
152	SLU 24	390	-1	2312		0.46	20.04	0
152	SLU 25	390	-1	2312		0.46	20.04	0
152	SLU 26	390	-1	2312		0.46	20.04	0
152	SLU 27	390	-1	2312		0.46	20.04	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
152	SLU 28	390	-1	2312	0.46	20.04	0
152	SLU 29	390	-1	2312	0.46	20.04	0
152	SLU 30	390	-1	2312	0.46	20.04	0
152	SLU 31	509	-1	2719	0.53	26.09	0
152	SLU 32	509	-1	2719	0.53	26.09	0
152	SLU 33	509	-1	2719	0.53	26.09	0
152	SLU 34	509	-1	2719	0.53	26.09	0
152	SLU 35	509	-1	2719	0.53	26.09	0
152	SLU 36	509	-1	2719	0.53	26.09	0
152	SLU 37	509	-1	2719	0.53	26.09	0
152	SLU 38	509	-1	2719	0.53	26.09	0
152	SLU 39	560	-1	2894	0.56	28.69	0
152	SLU 40	560	-1	2894	0.56	28.69	0
152	SLU 41	560	-1	2894	0.56	28.69	0
152	SLU 42	560	-1	2894	0.56	28.69	0
152	SLU 43	402	-1	2617	0.53	20.76	0
152	SLU 44	402	-1	2617	0.53	20.76	0
152	SLU 45	402	-1	2617	0.53	20.76	0
152	SLU 46	402	-1	2617	0.53	20.76	0
152	SLU 47	402	-1	2617	0.53	20.76	0
152	SLU 48	402	-1	2617	0.53	20.76	0
152	SLU 49	402	-1	2617	0.53	20.76	0
152	SLU 50	402	-1	2617	0.53	20.76	0
152	SLU 51	402	-1	2617	0.53	20.76	0
152	SLU 52	522	-1	3024	0.6	26.82	0
152	SLU 53	522	-1	3024	0.6	26.82	0
152	SLU 54	522	-1	3024	0.6	26.82	0
152	SLU 55	522	-1	3024	0.6	26.82	0
152	SLU 56	522	-1	3024	0.6	26.82	0
152	SLU 57	522	-1	3024	0.6	26.82	0
152	SLU 58	522	-1	3024	0.6	26.82	0
152	SLU 59	522	-1	3024	0.6	26.82	0
152	SLU 60	573	-1	3199	0.63	29.41	0
152	SLU 61	573	-1	3199	0.63	29.41	0
152	SLU 62	573	-1	3199	0.63	29.41	0
152	SLU 63	573	-1	3199	0.63	29.41	0
152	SLU 64	466	-1	2853	0.57	23.98	0
152	SLU 65	466	-1	2853	0.57	23.98	0
152	SLU 66	466	-1	2853	0.57	23.98	0
152	SLU 67	466	-1	2853	0.57	23.98	0
152	SLU 68	466	-1	2853	0.57	23.98	0
152	SLU 69	466	-1	2853	0.57	23.98	0
152	SLU 70	466	-1	2853	0.57	23.98	0
152	SLU 71	466	-1	2853	0.57	23.98	0
152	SLU 72	466	-1	2853	0.57	23.98	0
152	SLU 73	585	-1	3261	0.64	30.04	0
152	SLU 74	585	-1	3261	0.64	30.04	0
152	SLU 75	585	-1	3261	0.64	30.04	0
152	SLU 76	585	-1	3261	0.64	30.04	0
152	SLU 77	585	-1	3261	0.64	30.04	0
152	SLU 78	585	-1	3261	0.64	30.04	0
152	SLU 79	585	-1	3261	0.64	30.04	0
152	SLU 80	585	-1	3261	0.64	30.04	0
152	SLU 81	636	-1	3435	0.67	32.63	0
152	SLU 82	636	-1	3435	0.67	32.63	0
152	SLU 83	636	-1	3435	0.67	32.63	0
152	SLU 84	636	-1	3435	0.67	32.63	0
152	SLE RA 1	344	0	2143	0.43	17.74	0
152	SLE RA 2	344	0	2143	0.43	17.74	0
152	SLE RA 3	344	0	2143	0.43	17.74	0
152	SLE RA 4	344	0	2143	0.43	17.74	0
152	SLE RA 5	344	0	2143	0.43	17.74	0
152	SLE RA 6	344	0	2143	0.43	17.74	0
152	SLE RA 7	344	0	2143	0.43	17.74	0
152	SLE RA 8	344	0	2143	0.43	17.74	0
152	SLE RA 9	344	0	2143	0.43	17.74	0
152	SLE RA 10	424	-1	2415	0.48	21.78	0
152	SLE RA 11	424	-1	2415	0.48	21.78	0
152	SLE RA 12	424	-1	2415	0.48	21.78	0
152	SLE RA 13	424	-1	2415	0.48	21.78	0
152	SLE RA 14	424	-1	2415	0.48	21.78	0
152	SLE RA 15	424	-1	2415	0.48	21.78	0
152	SLE RA 16	424	-1	2415	0.48	21.78	0
152	SLE RA 17	424	-1	2415	0.48	21.78	0
152	SLE RA 18	458	-1	2531	0.5	23.51	0
152	SLE RA 19	458	-1	2531	0.5	23.51	0
152	SLE RA 20	458	-1	2531	0.5	23.51	0
152	SLE RA 21	458	-1	2531	0.5	23.51	0
152	SLE FR 1	344	0	2143	0.43	17.74	0
152	SLE FR 2	344	0	2143	0.43	17.74	0
152	SLE FR 3	344	0	2143	0.43	17.74	0
152	SLE FR 4	379	-1	2259	0.45	19.47	0
152	SLE FR 5	379	-1	2259	0.45	19.47	0
152	SLE FR 6	401	-1	2337	0.47	20.62	0
152	SLE QP 1	344	0	2143	0.43	17.74	0
152	SLE QP 2	379	-1	2259	0.45	19.47	0
152	SLD 1	559	7	2369	-10.97	28.86	-0.01
152	SLD 2	559	7	2369	-10.97	28.86	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
152	SLD 3	539	13	2464	-1.59	28.03	-0.02
152	SLD 4	539	13	2464	-1.59	28.03	-0.02
152	SLD 5	463	-8	2147	-17.21	23.54	0
152	SLD 6	463	-8	2147	-17.21	23.54	0
152	SLD 7	396	13	2466	14.07	20.79	-0.01
152	SLD 8	396	13	2466	14.07	20.79	-0.01
152	SLD 9	361	-14	2053	-13.17	18.16	0.01
152	SLD 10	361	-14	2053	-13.17	18.16	0.01
152	SLD 11	294	7	2371	18.11	15.4	-0.01
152	SLD 12	294	7	2371	18.11	15.4	-0.01
152	SLD 13	218	-14	2055	2.49	10.91	0.01
152	SLD 14	218	-14	2055	2.49	10.91	0.01
152	SLD 15	198	-8	2150	11.88	10.08	0.01
152	SLD 16	198	-8	2150	11.88	10.08	0.01
152	SLV 1	804	17	2513	-28.56	41.63	-0.03
152	SLV 2	804	17	2513	-28.56	41.63	-0.03
152	SLV 3	756	33	2744	-4.38	39.68	-0.04
152	SLV 4	756	33	2744	-4.38	39.68	-0.04
152	SLV 5	578	-20	1986	-44.93	29.08	0.01
152	SLV 6	578	-20	1986	-44.93	29.08	0.01
152	SLV 7	420	34	2754	35.68	22.57	-0.03
152	SLV 8	420	34	2754	35.68	22.57	-0.03
152	SLV 9	337	-35	1765	-34.78	16.37	0.03
152	SLV 10	337	-35	1765	-34.78	16.37	0.03
152	SLV 11	179	18	2532	45.83	9.86	-0.01
152	SLV 12	179	18	2532	45.83	9.86	-0.01
152	SLV 13	1	-34	1775	5.28	-0.74	0.04
152	SLV 14	1	-34	1775	5.28	-0.74	0.04
152	SLV 15	-47	-18	2005	29.47	-2.69	0.02
152	SLV 16	-47	-18	2005	29.47	-2.69	0.02
153	SLU 1	389	-3	2254	0.88	22.2	0.01
153	SLU 2	389	-3	2254	0.88	22.2	0.01
153	SLU 3	389	-3	2254	0.88	22.2	0.01
153	SLU 4	389	-3	2254	0.88	22.2	0.01
153	SLU 5	389	-3	2254	0.88	22.2	0.01
153	SLU 6	389	-3	2254	0.88	22.2	0.01
153	SLU 7	389	-3	2254	0.88	22.2	0.01
153	SLU 8	389	-3	2254	0.88	22.2	0.01
153	SLU 9	389	-3	2254	0.88	22.2	0.01
153	SLU 10	521	-3	2697	1.01	29.41	0.02
153	SLU 11	521	-3	2697	1.01	29.41	0.02
153	SLU 12	521	-3	2697	1.01	29.41	0.02
153	SLU 13	521	-3	2697	1.01	29.41	0.02
153	SLU 14	521	-3	2697	1.01	29.41	0.02
153	SLU 15	521	-3	2697	1.01	29.41	0.02
153	SLU 16	521	-3	2697	1.01	29.41	0.02
153	SLU 17	521	-3	2697	1.01	29.41	0.02
153	SLU 18	577	-4	2887	1.07	32.5	0.02
153	SLU 19	577	-4	2887	1.07	32.5	0.02
153	SLU 20	577	-4	2887	1.07	32.5	0.02
153	SLU 21	577	-4	2887	1.07	32.5	0.02
153	SLU 22	459	-3	2509	0.96	26.08	0.01
153	SLU 23	459	-3	2509	0.96	26.08	0.01
153	SLU 24	459	-3	2509	0.96	26.08	0.01
153	SLU 25	459	-3	2509	0.96	26.08	0.01
153	SLU 26	459	-3	2509	0.96	26.08	0.01
153	SLU 27	459	-3	2509	0.96	26.08	0.01
153	SLU 28	459	-3	2509	0.96	26.08	0.01
153	SLU 29	459	-3	2509	0.96	26.08	0.01
153	SLU 30	459	-3	2509	0.96	26.08	0.01
153	SLU 31	592	-4	2952	1.1	33.28	0.02
153	SLU 32	592	-4	2952	1.1	33.28	0.02
153	SLU 33	592	-4	2952	1.1	33.28	0.02
153	SLU 34	592	-4	2952	1.1	33.28	0.02
153	SLU 35	592	-4	2952	1.1	33.28	0.02
153	SLU 36	592	-4	2952	1.1	33.28	0.02
153	SLU 37	592	-4	2952	1.1	33.28	0.02
153	SLU 38	592	-4	2952	1.1	33.28	0.02
153	SLU 39	648	-4	3142	1.15	36.37	0.02
153	SLU 40	648	-4	3142	1.15	36.37	0.02
153	SLU 41	648	-4	3142	1.15	36.37	0.02
153	SLU 42	648	-4	3142	1.15	36.37	0.02
153	SLU 43	481	-4	2843	1.11	27.53	0.02
153	SLU 44	481	-4	2843	1.11	27.53	0.02
153	SLU 45	481	-4	2843	1.11	27.53	0.02
153	SLU 46	481	-4	2843	1.11	27.53	0.02
153	SLU 47	481	-4	2843	1.11	27.53	0.02
153	SLU 48	481	-4	2843	1.11	27.53	0.02
153	SLU 49	481	-4	2843	1.11	27.53	0.02
153	SLU 50	481	-4	2843	1.11	27.53	0.02
153	SLU 51	481	-4	2843	1.11	27.53	0.02
153	SLU 52	613	-4	3286	1.25	34.74	0.02
153	SLU 53	613	-4	3286	1.25	34.74	0.02
153	SLU 54	613	-4	3286	1.25	34.74	0.02
153	SLU 55	613	-4	3286	1.25	34.74	0.02
153	SLU 56	613	-4	3286	1.25	34.74	0.02
153	SLU 57	613	-4	3286	1.25	34.74	0.02
153	SLU 58	613	-4	3286	1.25	34.74	0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
153	SLU 59	613	-4	3286	1.25	34.74	0.02
153	SLU 60	670	-4	3476	1.31	37.83	0.02
153	SLU 61	670	-4	3476	1.31	37.83	0.02
153	SLU 62	670	-4	3476	1.31	37.83	0.02
153	SLU 63	670	-4	3476	1.31	37.83	0.02
153	SLU 64	552	-4	3098	1.2	31.41	0.02
153	SLU 65	552	-4	3098	1.2	31.41	0.02
153	SLU 66	552	-4	3098	1.2	31.41	0.02
153	SLU 67	552	-4	3098	1.2	31.41	0.02
153	SLU 68	552	-4	3098	1.2	31.41	0.02
153	SLU 69	552	-4	3098	1.2	31.41	0.02
153	SLU 70	552	-4	3098	1.2	31.41	0.02
153	SLU 71	552	-4	3098	1.2	31.41	0.02
153	SLU 72	552	-4	3098	1.2	31.41	0.02
153	SLU 73	684	-4	3541	1.33	38.61	0.02
153	SLU 74	684	-4	3541	1.33	38.61	0.02
153	SLU 75	684	-4	3541	1.33	38.61	0.02
153	SLU 76	684	-4	3541	1.33	38.61	0.02
153	SLU 77	684	-4	3541	1.33	38.61	0.02
153	SLU 78	684	-4	3541	1.33	38.61	0.02
153	SLU 79	684	-4	3541	1.33	38.61	0.02
153	SLU 80	684	-4	3541	1.33	38.61	0.02
153	SLU 81	741	-5	3731	1.39	41.7	0.02
153	SLU 82	741	-5	3731	1.39	41.7	0.02
153	SLU 83	741	-5	3731	1.39	41.7	0.02
153	SLU 84	741	-5	3731	1.39	41.7	0.02
153	SLE RA 1	409	-3	2327	0.9	23.31	0.01
153	SLE RA 2	409	-3	2327	0.9	23.31	0.01
153	SLE RA 3	409	-3	2327	0.9	23.31	0.01
153	SLE RA 4	409	-3	2327	0.9	23.31	0.01
153	SLE RA 5	409	-3	2327	0.9	23.31	0.01
153	SLE RA 6	409	-3	2327	0.9	23.31	0.01
153	SLE RA 7	409	-3	2327	0.9	23.31	0.01
153	SLE RA 8	409	-3	2327	0.9	23.31	0.01
153	SLE RA 9	409	-3	2327	0.9	23.31	0.01
153	SLE RA 10	497	-3	2622	0.99	28.11	0.01
153	SLE RA 11	497	-3	2622	0.99	28.11	0.01
153	SLE RA 12	497	-3	2622	0.99	28.11	0.01
153	SLE RA 13	497	-3	2622	0.99	28.11	0.01
153	SLE RA 14	497	-3	2622	0.99	28.11	0.01
153	SLE RA 15	497	-3	2622	0.99	28.11	0.01
153	SLE RA 16	497	-3	2622	0.99	28.11	0.01
153	SLE RA 17	497	-3	2622	0.99	28.11	0.01
153	SLE RA 18	535	-3	2749	1.03	30.17	0.02
153	SLE RA 19	535	-3	2749	1.03	30.17	0.02
153	SLE RA 20	535	-3	2749	1.03	30.17	0.02
153	SLE RA 21	535	-3	2749	1.03	30.17	0.02
153	SLE FR 1	409	-3	2327	0.9	23.31	0.01
153	SLE FR 2	409	-3	2327	0.9	23.31	0.01
153	SLE FR 3	409	-3	2327	0.9	23.31	0.01
153	SLE FR 4	447	-3	2454	0.94	25.37	0.01
153	SLE FR 5	447	-3	2454	0.94	25.37	0.01
153	SLE FR 6	472	-3	2538	0.97	26.74	0.01
153	SLE QP 1	409	-3	2327	0.9	23.31	0.01
153	SLE QP 2	447	-3	2454	0.94	25.37	0.01
153	SLD 1	621	3	2640	-4.99	33.99	0.02
153	SLD 2	621	3	2640	-4.99	33.99	0.02
153	SLD 3	595	6	2785	-0.64	34.86	0.03
153	SLD 4	595	6	2785	-0.64	34.86	0.03
153	SLD 5	538	-6	2289	-7.44	26.62	0
153	SLD 6	538	-6	2289	-7.44	26.62	0
153	SLD 7	452	4	2773	7.07	29.54	0.03
153	SLD 8	452	4	2773	7.07	29.54	0.03
153	SLD 9	441	-11	2134	-5.19	21.19	0
153	SLD 10	441	-11	2134	-5.19	21.19	0
153	SLD 11	355	0	2618	9.32	24.11	0.03
153	SLD 12	355	0	2618	9.32	24.11	0.03
153	SLD 13	298	-13	2122	2.52	15.87	0
153	SLD 14	298	-13	2122	2.52	15.87	0
153	SLD 15	273	-10	2268	6.87	16.74	0.01
153	SLD 16	273	-10	2268	6.87	16.74	0.01
153	SLV 1	857	12	2889	-14	45.69	0.02
153	SLV 2	857	12	2889	-14	45.69	0.02
153	SLV 3	797	21	3237	-2.84	47.8	0.05
153	SLV 4	797	21	3237	-2.84	47.8	0.05
153	SLV 5	662	-11	2056	-20.47	28.26	-0.02
153	SLV 6	662	-11	2056	-20.47	28.26	-0.02
153	SLV 7	460	16	3217	16.73	35.3	0.06
153	SLV 8	460	16	3217	16.73	35.3	0.06
153	SLV 9	434	-23	1690	-14.85	15.43	-0.03
153	SLV 10	434	-23	1690	-14.85	15.43	-0.03
153	SLV 11	231	5	2852	22.35	22.47	0.05
153	SLV 12	231	5	2852	22.35	22.47	0.05
153	SLV 13	96	-27	1670	4.72	2.93	-0.02
153	SLV 14	96	-27	1670	4.72	2.93	-0.02
153	SLV 15	36	-19	2019	15.88	5.04	0.01
153	SLV 16	36	-19	2019	15.88	5.04	0.01
154	SLU 1	446	-376	2793	10.3	13.69	0.03



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
154	SLU 2	446	-376	2793	10.3	13.69	0.03
154	SLU 3	446	-376	2793	10.3	13.69	0.03
154	SLU 4	446	-376	2793	10.3	13.69	0.03
154	SLU 5	446	-376	2793	10.3	13.69	0.03
154	SLU 6	446	-376	2793	10.3	13.69	0.03
154	SLU 7	446	-376	2793	10.3	13.69	0.03
154	SLU 8	446	-376	2793	10.3	13.69	0.03
154	SLU 9	446	-376	2793	10.3	13.69	0.03
154	SLU 10	562	-428	3345	11.32	17.82	0.05
154	SLU 11	562	-428	3345	11.32	17.82	0.05
154	SLU 12	562	-428	3345	11.32	17.82	0.05
154	SLU 13	562	-428	3345	11.32	17.82	0.05
154	SLU 14	562	-428	3345	11.32	17.82	0.05
154	SLU 15	562	-428	3345	11.32	17.82	0.05
154	SLU 16	562	-428	3345	11.32	17.82	0.05
154	SLU 17	562	-428	3345	11.32	17.82	0.05
154	SLU 18	613	-451	3582	11.76	19.6	0.06
154	SLU 19	613	-451	3582	11.76	19.6	0.06
154	SLU 20	613	-451	3582	11.76	19.6	0.06
154	SLU 21	613	-451	3582	11.76	19.6	0.06
154	SLU 22	510	-409	3110	11.01	15.93	0.04
154	SLU 23	510	-409	3110	11.01	15.93	0.04
154	SLU 24	510	-409	3110	11.01	15.93	0.04
154	SLU 25	510	-409	3110	11.01	15.93	0.04
154	SLU 26	510	-409	3110	11.01	15.93	0.04
154	SLU 27	510	-409	3110	11.01	15.93	0.04
154	SLU 28	510	-409	3110	11.01	15.93	0.04
154	SLU 29	510	-409	3110	11.01	15.93	0.04
154	SLU 30	510	-409	3110	11.01	15.93	0.04
154	SLU 31	627	-461	3662	12.03	20.06	0.06
154	SLU 32	627	-461	3662	12.03	20.06	0.06
154	SLU 33	627	-461	3662	12.03	20.06	0.06
154	SLU 34	627	-461	3662	12.03	20.06	0.06
154	SLU 35	627	-461	3662	12.03	20.06	0.06
154	SLU 36	627	-461	3662	12.03	20.06	0.06
154	SLU 37	627	-461	3662	12.03	20.06	0.06
154	SLU 38	627	-461	3662	12.03	20.06	0.06
154	SLU 39	677	-483	3899	12.47	21.84	0.07
154	SLU 40	677	-483	3899	12.47	21.84	0.07
154	SLU 41	677	-483	3899	12.47	21.84	0.07
154	SLU 42	677	-483	3899	12.47	21.84	0.07
154	SLU 43	557	-478	3522	13.15	17.03	0.03
154	SLU 44	557	-478	3522	13.15	17.03	0.03
154	SLU 45	557	-478	3522	13.15	17.03	0.03
154	SLU 46	557	-478	3522	13.15	17.03	0.03
154	SLU 47	557	-478	3522	13.15	17.03	0.03
154	SLU 48	557	-478	3522	13.15	17.03	0.03
154	SLU 49	557	-478	3522	13.15	17.03	0.03
154	SLU 50	557	-478	3522	13.15	17.03	0.03
154	SLU 51	557	-478	3522	13.15	17.03	0.03
154	SLU 52	674	-530	4075	14.17	21.16	0.06
154	SLU 53	674	-530	4075	14.17	21.16	0.06
154	SLU 54	674	-530	4075	14.17	21.16	0.06
154	SLU 55	674	-530	4075	14.17	21.16	0.06
154	SLU 56	674	-530	4075	14.17	21.16	0.06
154	SLU 57	674	-530	4075	14.17	21.16	0.06
154	SLU 58	674	-530	4075	14.17	21.16	0.06
154	SLU 59	674	-530	4075	14.17	21.16	0.06
154	SLU 60	724	-552	4311	14.61	22.94	0.07
154	SLU 61	724	-552	4311	14.61	22.94	0.07
154	SLU 62	724	-552	4311	14.61	22.94	0.07
154	SLU 63	724	-552	4311	14.61	22.94	0.07
154	SLU 64	622	-510	3839	13.86	19.26	0.04
154	SLU 65	622	-510	3839	13.86	19.26	0.04
154	SLU 66	622	-510	3839	13.86	19.26	0.04
154	SLU 67	622	-510	3839	13.86	19.26	0.04
154	SLU 68	622	-510	3839	13.86	19.26	0.04
154	SLU 69	622	-510	3839	13.86	19.26	0.04
154	SLU 70	622	-510	3839	13.86	19.26	0.04
154	SLU 71	622	-510	3839	13.86	19.26	0.04
154	SLU 72	622	-510	3839	13.86	19.26	0.04
154	SLU 73	738	-563	4392	14.88	23.4	0.07
154	SLU 74	738	-563	4392	14.88	23.4	0.07
154	SLU 75	738	-563	4392	14.88	23.4	0.07
154	SLU 76	738	-563	4392	14.88	23.4	0.07
154	SLU 77	738	-563	4392	14.88	23.4	0.07
154	SLU 78	738	-563	4392	14.88	23.4	0.07
154	SLU 79	738	-563	4392	14.88	23.4	0.07
154	SLU 80	738	-563	4392	14.88	23.4	0.07
154	SLU 81	789	-585	4628	15.31	25.17	0.08
154	SLU 82	789	-585	4628	15.31	25.17	0.08
154	SLU 83	789	-585	4628	15.31	25.17	0.08
154	SLU 84	789	-585	4628	15.31	25.17	0.08
154	SLE RA 1	464	-385	2884	10.5	14.33	0.03
154	SLE RA 2	464	-385	2884	10.5	14.33	0.03
154	SLE RA 3	464	-385	2884	10.5	14.33	0.03
154	SLE RA 4	464	-385	2884	10.5	14.33	0.03
154	SLE RA 5	464	-385	2884	10.5	14.33	0.03



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
154	SLE RA 6	464	-385	2884	10.5	14.33	0.03
154	SLE RA 7	464	-385	2884	10.5	14.33	0.03
154	SLE RA 8	464	-385	2884	10.5	14.33	0.03
154	SLE RA 9	464	-385	2884	10.5	14.33	0.03
154	SLE RA 10	542	-420	3252	11.18	17.08	0.05
154	SLE RA 11	542	-420	3252	11.18	17.08	0.05
154	SLE RA 12	542	-420	3252	11.18	17.08	0.05
154	SLE RA 13	542	-420	3252	11.18	17.08	0.05
154	SLE RA 14	542	-420	3252	11.18	17.08	0.05
154	SLE RA 15	542	-420	3252	11.18	17.08	0.05
154	SLE RA 16	542	-420	3252	11.18	17.08	0.05
154	SLE RA 17	542	-420	3252	11.18	17.08	0.05
154	SLE RA 18	575	-435	3410	11.48	18.27	0.05
154	SLE RA 19	575	-435	3410	11.48	18.27	0.05
154	SLE RA 20	575	-435	3410	11.48	18.27	0.05
154	SLE RA 21	575	-435	3410	11.48	18.27	0.05
154	SLE FR 1	464	-385	2884	10.5	14.33	0.03
154	SLE FR 2	464	-385	2884	10.5	14.33	0.03
154	SLE FR 3	464	-385	2884	10.5	14.33	0.03
154	SLE FR 4	497	-400	3042	10.8	15.51	0.04
154	SLE FR 5	497	-400	3042	10.8	15.51	0.04
154	SLE FR 6	520	-410	3147	10.99	16.3	0.04
154	SLE QP 1	464	-385	2884	10.5	14.33	0.03
154	SLE QP 2	497	-400	3042	10.8	15.51	0.04
154	SLD 1	604	-404	3342	10.58	20.56	0.09
154	SLD 2	604	-404	3342	10.58	20.56	0.09
154	SLD 3	619	-470	3570	13.46	20.05	0.07
154	SLD 4	619	-470	3570	13.46	20.05	0.07
154	SLD 5	507	-300	2786	6.36	17.8	0.09
154	SLD 6	507	-300	2786	6.36	17.8	0.09
154	SLD 7	556	-522	3545	15.96	16.1	0.01
154	SLD 8	556	-522	3545	15.96	16.1	0.01
154	SLD 9	439	-278	2538	5.63	14.92	0.07
154	SLD 10	439	-278	2538	5.63	14.92	0.07
154	SLD 11	487	-500	3297	15.23	13.22	-0.02
154	SLD 12	487	-500	3297	15.23	13.22	-0.02
154	SLD 13	376	-330	2513	8.14	10.97	0.01
154	SLD 14	376	-330	2513	8.14	10.97	0.01
154	SLD 15	391	-397	2741	11.02	10.46	-0.02
154	SLD 16	391	-397	2741	11.02	10.46	-0.02
154	SLV 1	747	-408	3746	10.24	27.46	0.17
154	SLV 2	747	-408	3746	10.24	27.46	0.17
154	SLV 3	785	-566	4291	17.09	26.2	0.11
154	SLV 4	785	-566	4291	17.09	26.2	0.11
154	SLV 5	516	-164	2425	0.24	21	0.17
154	SLV 6	516	-164	2425	0.24	21	0.17
154	SLV 7	640	-689	4244	23.07	16.81	-0.03
154	SLV 8	640	-689	4244	23.07	16.81	-0.03
154	SLV 9	354	-112	1839	-1.48	14.2	0.11
154	SLV 10	354	-112	1839	-1.48	14.2	0.11
154	SLV 11	479	-637	3658	21.35	10.02	-0.1
154	SLV 12	479	-637	3658	21.35	10.02	-0.1
154	SLV 13	210	-235	1792	4.5	4.81	-0.04
154	SLV 14	210	-235	1792	4.5	4.81	-0.04
154	SLV 15	247	-392	2337	11.35	3.56	-0.1
154	SLV 16	247	-392	2337	11.35	3.56	-0.1

1.3 Risposta modale

Modo: identificativo del modo di vibrare.

Periodo: periodo. [s]

Massa X: massa partecipante in direzione globale X. Il valore è adimensionale.

Massa Y: massa partecipante in direzione globale Y. Il valore è adimensionale.

Massa Z: massa partecipante in direzione globale Z. Il valore è adimensionale.

Massa rot. X: massa rotazionale partecipante attorno la direzione globale X. Il valore è adimensionale.

Massa rot. Y: massa rotazionale partecipante attorno la direzione globale Y. Il valore è adimensionale.

Massa rot. Z: massa rotazionale partecipante attorno la direzione globale Z. Il valore è adimensionale.

Massa sX: massa partecipante in direzione Sisma X. Il valore è adimensionale.

Massa sY: massa partecipante in direzione Sisma Y. Il valore è adimensionale.

Totale masse partecipanti:

Traslazione X: 0.924504

Traslazione Y: 0.972985

Traslazione Z: 0

Rotazione X: 0.907664

Rotazione Y: 0.911258

Rotazione Z: 0.832495

Modo	Periodo	Massa X	Massa Y	Massa Z	Massa rot. X	Massa rot. Y	Massa rot. Z	Massa sX	Massa sY
1	2.330719417	0.000000004	0.001048236	0	0.001434698	0.000000014	0.000422481	0.000000004	0.001048236



Modo	Periodo	Massa X	Massa Y	Massa Z	Massa rot. X	Massa rot. Y	Massa rot. Z	Massa sX	Massa sY
2	2.093064624	0.000001118	0.456584246	0	0.565466301	0.000001691	0.02153078	0.000001118	0.456584246
3	2.049514792	0.000036058	0.028437616	0	0.033886222	0.00005003	0.010985161	0.000036058	0.028437616
4	1.967821663	0.000049399	0.003334448	0	0.003980354	0.000061591	0.008163094	0.000049399	0.003334448
5	1.812566408	0.000000333	0.056319566	0	0.046889731	0.000000337	0.004048879	0.000000333	0.056319566
6	1.605462172	0.000000415	0.00396911	0	0.00805023	0.000000279	0.000273823	0.000000415	0.00396911
7	1.275729923	0.000000018	0.036914886	0	0.011385966	0.000000166	0.002272672	0.000000018	0.036914886
8	1.040449454	0.00000034	0.000002966	0	0.000002041	0.000005608	0.002597769	0.00000034	0.000002966
9	1.003819878	0.000060763	0.000104728	0	0.00001468	0.000063389	0.000002937	0.000060763	0.000104728
10	0.921377987	0.00000952	0.009561388	0	0.001004941	0.000011062	0.00065407	0.00000952	0.009561388
11	0.894587715	0.007427387	0.000144675	0	0.000003899	0.007727837	0.001650655	0.007427387	0.000144675
12	0.887449372	0.009642063	0.000077674	0	0.000000234	0.009972268	0.017548164	0.009642063	0.000077674
13	0.845469531	0.032686469	0.000078635	0	0.000004272	0.036544265	0.032326156	0.032686469	0.000078635
14	0.823323019	0.000947768	0.00090029	0	0.000829203	0.001016118	0.001364119	0.000947768	0.00090029
15	0.819199564	0.001866828	0.004847486	0	0.000325764	0.001944811	0.000045033	0.001866828	0.004847486
16	0.786352658	0.001708614	0.000008021	0	0.000044138	0.001701043	0.000200691	0.001708614	0.000008021
17	0.780853388	0.000171487	0.012447095	0	0.000628541	0.000212955	0.002122246	0.000171487	0.012447095
18	0.760531067	0.000051618	0.053492765	0	0.001514575	0.000059026	0.003847036	0.000051618	0.053492765
19	0.741591531	0.001221767	0.000008727	0	0.000004916	0.000057972	0.001746699	0.001221767	0.000008727
20	0.693624182	0.000007864	0.000002405	0	0.00000027	0.000090431	0.000255506	0.000007864	0.000002405
21	0.685819368	0.000005888	0.000017682	0	0.000201034	0.000055979	0.000001215	0.000005888	0.000017682
22	0.654731151	0.000004268	0.003946693	0	0.001418765	0.000002387	0.000304619	0.000004268	0.003946693
23	0.633522153	0.007404359	0.000001759	0	0.000088292	0.001562176	0.006819026	0.007404359	0.000001759
24	0.628227085	0.016466376	0.000001077	0	0.000035343	0.002046199	0.013051415	0.016466376	0.000001077
25	0.587491113	0.00030676	0.003841338	0	0.007674184	0.000439585	0.000000056	0.00030676	0.003841338
26	0.58171694	0.068680216	0.000005699	0	0.000018755	0.095235383	0.058281992	0.068680216	0.000005699
27	0.559916318	0.000938286	0.000117498	0	0.000083387	0.001340727	0.0009613	0.000938286	0.000117498
28	0.499421366	0.000015442	0.000005329	0	0.000003753	0.00000026	0.00002842	0.000015442	0.000005329
29	0.474018803	0.000002519	0.000442035	0	0.000216131	0.000000825	0.001395261	0.000002519	0.000442035
30	0.458864125	0.000044627	0.000473454	0	0.000000177	0.000143804	0.000032003	0.000044627	0.000473454
31	0.44494051	0.000501801	0.006605328	0	0.007934278	0.000299114	0.000832723	0.000501801	0.006605328
32	0.441196884	0.00096532	0.003271013	0	0.006116273	0.000354546	0.000346346	0.00096532	0.003271013
33	0.427626432	0.000317383	0.002086237	0	0.001366452	0.000000502	0.000200689	0.000317383	0.002086237
34	0.410254718	0.002545651	0.001705866	0	0.0000035	0.000000788	0.002434286	0.002545651	0.001705866
35	0.400367976	0.004152361	0.002309598	0	0.000000403	0.000279769	0.007852319	0.004152361	0.002309598
36	0.384462351	0.014558645	0.000866705	0	0.000173989	0.002305501	0.01015484	0.014558645	0.000866705
37	0.37305969	0.010081634	0.001463392	0	0.001545953	0.000000364	0.010543114	0.010081634	0.001463392
38	0.367240456	0.000772812	0.007622402	0	0.012828949	0.000089736	0.000115345	0.000772812	0.007622402
39	0.345240197	0.000059829	0.004293977	0	0.003410948	0.000015797	0.001185506	0.000059829	0.004293977
40	0.30066317	0.000002926	0.003479647	0	0.000167596	0.000000576	0.000084017	0.000002926	0.003479647
41	0.289151606	0.000549255	0.000072375	0	0.000034664	0.00007513	0.000124367	0.000549255	0.000072375
42	0.254106754	0.000025042	0.002418782	0	0.000922206	0.000006572	0.000279561	0.000025042	0.002418782
43	0.238111303	0.009813954	0.000020813	0	0.000019904	0.000067718	0.008074292	0.009813954	0.000020813
44	0.211735624	0.001433418	0.003908734	0	0.000226233	0.000003738	0.000880198	0.001433418	0.003908734
45	0.207373144	0.0000815871	0.005822286	0	0.000146708	0.000007375	0.002434794	0.0000815871	0.005822286
46	0.171702897	0.000011485	0.010223398	0	0.005016187	0.000006434	0.000632856	0.000011485	0.010223398
47	0.154162745	0.01185283	0.000012049	0	0.000031452	0.007401281	0.009066327	0.01185283	0.000012049
48	0.124285748	0.000030323	0.01507234	0	0.006045607	0.000013252	0.000554669	0.000030323	0.01507234
49	0.109449501	0.034499958	0.000014803	0	0.000000057	0.02900005	0.032009387	0.034499958	0.000014803
50	0.079170023	0.000156055	0.016367187	0	0.004165867	0.000179994	0.000316846	0.000156055	0.016367187
51	0.062845122	0.420750678	0.000000052	0	0.000002019	0.588124969	0.387340454	0.420750678	0.000000052
52	0.037477753	0.257863409	0.001887887	0	0.001837667	0.142224932	0.142222553	0.257863409	0.001887887
53	0.036005362	0.002717835	0.206145756	0	0.174588161	0.001345792	0.020591167	0.002717835	0.206145756
54	0.016490651	0.000011961	0.000008026	0	0.000662575	0.000002846	0.00000698	0.000011961	0.000008026
55	0.014581885	0.000067059	0.000082316	0	0.000343929	0.000004276	0.000183061	0.000067059	0.000082316
56	0.013573724	0.000011001	0.000003419	0	0.00133267	0.000014995	0.000001429	0.000011001	0.000003419
57	0.012399742	0.000062161	0.000004406	0	0.000663513	0.000000267	0.000005498	0.000062161	0.000004406
58	0.011300876	0.000002913	0.000005683	0	0.000021818	0.000002332	0.000102558	0.000002913	0.000005683
59	0.010762072	0.00006765	0.000054324	0	0.000012591	0.000006299	0.000000999	0.00006765	0.000054324
60	0.006762882	0.000040499	0.00001834	0	0.000008661	0.00007264	0.000074744	0.000040499	0.00001834

1.4 Equilibrio globale forze

Contributo: Nome attribuito al sistema risultante.

Fx: Componente X di forza del sistema risultante. [daN]

Fy: Componente Y di forza del sistema risultante. [daN]

Fz: Componente Z di forza del sistema risultante. [daN]

Mx: Componente di momento attorno l'asse X del sistema risultante. [daN*m]

My: Componente di momento attorno l'asse Y del sistema risultante. [daN*m]

Mz: Componente di momento attorno l'asse Z del sistema risultante. [daN*m]

Bilancio in condizione di carico: Pesi strutturali

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	-0.008	0	-262502.68	3451962.75	-960965.92	-0.1
Reazioni	0.008	0	262502.68	-3451962.75	960965.92	0.1
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

Bilancio in condizione di carico: Permanenti portati

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	0	-57322.32	757576.98	-207942.71	0
Reazioni	0	0	57322.32	-757576.98	207942.71	0
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0



Bilancio in condizione di carico: Variabile A

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	0	-65221.757	862430.79	-236212.21	0
Reazioni	0	0	65221.757	-862430.79	236212.21	0
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

Bilancio in condizione di carico: Sisma X SLV

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	81491.444	0	0	0	299169.53	1070991.35
Reazioni	-81491.444	0	0	0	-299169.53	-1070991.35
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

Bilancio in condizione di carico: Sisma Y SLV

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	24125.157	0	-88567.73	0	-87465.87
Reazioni	0	-24125.157	0	88567.73	0	87465.87
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

Bilancio in condizione di carico: Sisma X SLD

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	34971.086	0	0	0	128385.05	459603.22
Reazioni	-34971.086	0	0	0	-128385.05	-459603.22
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

Bilancio in condizione di carico: Sisma Y SLD

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	8399.719	0	-30836.86	0	-30453.22
Reazioni	0	-8399.719	0	30836.86	0	30453.22
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

Bilancio in condizione di carico: Rig Ux

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	0	0	0	0	0
Reazioni	0	0	0	0	0	0
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

Bilancio in condizione di carico: Rig Uy

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	0	0	0	0	0
Reazioni	0	0	0	0	0	0
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

Bilancio in condizione di carico: Rig Rz

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	0	0	0	0	0
Reazioni	0	0	0	0	0	0
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

1.5 Risposta di spettro

Spettro: condizione elementare corrispondente allo spettro.

N.b.: nome breve della condizione elementare.

Fx: componente della forza lungo l'asse X. [daN]

Fy: componente della forza lungo l'asse Y. [daN]

Fz: componente della forza lungo l'asse Z. [daN]

Mx: componente della coppia attorno all'asse X. [daN*m]

My: componente della coppia attorno all'asse Y. [daN*m]

Mz: componente della coppia attorno all'asse Z. [daN*m]

Max X: massima reazione lungo l'asse X.

Valore: valore massimo della reazione. [daN]

Angolo: angolo d'ingresso del sisma che provoca il valore massimo della reazione. [deg]

Max Y: massima reazione lungo l'asse Y.

Valore: valore massimo della reazione. [daN]

Angolo: angolo d'ingresso del sisma che provoca il valore massimo della reazione. [deg]

Max Z: massima reazione lungo l'asse Z.

Valore: valore massimo della reazione. [daN]

Angolo: angolo d'ingresso del sisma che provoca il valore massimo della reazione. [deg]

Spettro	Fx	Fy	Fz	Mx	My	Mz	Max X		Max Y		Max Z	
N.b.							Valore	Angolo	Valore	Angolo	Valore	Angolo
SLV X	41371.98	931.74	0	2649.7658	1.345E05	5.498E05	41371.98	0	21037.61	91	0	0
SLV Y	931.74	21036.59	0	6.086E04	2018.2411	7.630E04	41371.98	0	21037.61	91	0	0



Spettro	Fx	Fy	Fz	Mx	My	Mz	Max X		Max Y		Max Z	
N.b.							Valore	Angolo	Valore	Angolo	Valore	Angolo
X SLD	17639.67	394.57	0	1122.481	5.745E04	2.346E05	17639.67	0	8363.62	91	0	0
Y SLD	394.57	8363	0	2.382E04	854.476	30350.33	17639.67	0	8363.62	91	0	0

1.6 Annotazioni solutore

Informazioni: informazioni fornite dal solutore al termine del calcolo del modello.

Informazioni

1.7 Statistiche soluzione

Tipo di equazioni	Lineari
Tecnica di soluzione	Intel MKL PARDISO
Numero equazioni	14646
Elemento min. diagonale	2912.63100461
Elemento max diagonale	468776680.47995
Rapporto max/min	160946.12731182
Elementi non nulli	682600

TABULATI DI CALCOLO – VERIFICHE
CIVICI 43-45
STATO DI FATTO



Sommario

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1 Verifiche

1.1 Verifica regolarità strutturale

Le unità di misura elencate nel capitolo sono in [m, daN] ove non espressamente specificato.

Livello:

Descr: descrizione livello.

Quota: quota livello. [m]

Q: quota livello. [m]

Qinf: quota livello precedente. [m]

Comb: combinazione.

A1: a1 (Distribuzione masse).

A1n: a1 numeratore (distanza tra centro massa vs. centro rigidezza [se presente] o centro dell'ingombro del piano). [m]

A1d: a1 denominatore (ingombro del piano nella medesima direzione [x o y globale]). [m]

A1r: a1 rapporto (distanza centro massa/rigidezza su ingombro del piano).

A2: a2 (Distribuzione rigidezze).

A2n: a2 numeratore (rigidezza max [x o y globale]).

A2d: a2 denominatore (rigidezza min [x o y globale]).

A2r: a2 rapporto (rigidezza max/min).

A3: a3 (Forma compatta).

A3n: a3 numeratore (area convessa). [m²]

A3d: a3 denominatore (area piano). [m²]

A3r: a3 rapporto (area convessa/area piano).

B: b (Rapporto lati).

Bn: b numeratore (lato max [x o y globale]). [m]

Bd: b denominatore (lato min [x o y globale]). [m]

Br: b rapporto (lato max/min).

C: c (Rapporto rigidezze piano).

Cn: c numeratore (rigidezza elementi verticali).

Cd: c denominatore (rigidezza piano).

Cr: c rapporto (rigidezza elementi verticali/rigidezza piano).

E1: e1 (Variazione masse).

E1n: e1 numeratore (massa max). [daN]

E1d: e1 denominatore (massa min). [daN]

E1r: e1 rapporto (massa max/min).

E2: e2 (Riduzione rigidezze).

E2n: e2 numeratore (rigidezza relativa alla traslazione KUmax). [daN/m]

E2d: e2 denominatore (rigidezza relativa alla traslazione KUmin). [daN/m]

E2r: e2 rapporto (variazione massima in decremento Kmax/Kmin).

E3: e3 (Incremento rigidezze).

E3n: e3 numeratore (rigidezza relativa alla traslazione KUmax). [daN/m]

E3d: e3 denominatore (rigidezza relativa alla traslazione KUmin). [daN/m]

E3r: e3 rapporto (variazione massima in incremento Kmax/Kmin).

F: f (Rapporto Capacità/Domanda).

Fn: f numeratore (rapporto capacità/domanda massimo [c/d max]). [daN]

Fd: f denominatore (rapporto capacità/domanda minimo [c/d min]). [daN]

Fr: f rapporto (variazione massima [rapporto (c/d max)/(c/d min)]).

G1: g1 (Rastremazione di piano).

G1n: g1 numeratore (L1). [m]

G1d: g1 denominatore (L2). [m]

G1r: g1 rapporto (L1/L2).

G2: g2 (Rastremazione totale).

G2n: g2 numeratore (L0). [m]

G2d: g2 denominatore (Li). [m]

G2r: g2 rapporto (L0/Li).

Capacità/Domanda in X:

VrdX: taglio resistente complessivo in direzione X. [daN]

VedX: taglio agente complessivo in direzione X. [daN]

|Rd/Ed|: |Rd/Ed| (rapporto capacità/domanda in termini di resistenza a taglio).

Capacità/Domanda in Y:

VrdY: taglio resistente complessivo in direzione Y. [daN]

VedY: taglio agente complessivo in direzione Y. [daN]

Verifica regolarità strutturale

Controllo regolarità edificio secondo D.M. 17-01-18 (N.T.C.) §7.2.1 - §C7.2.1

Avvertenze



La seguente procedura valuta la regolarità della costruzione secondo quanto indicato nelle NTC 2018 §7.2.1.

Tali valutazioni sono a carattere puramente informativo e vengono condotte sulla base del modello e delle verifiche presenti alla sua generazione, con le limitazioni indicate nella manualistica.

In ogni caso l'impostazione di regolarità della costruzione, in pianta ed elevazione, va indicata nelle preferenze di analisi dall'utente utilizzatore del software.

Sintesi dei risultati

Orizzontamenti considerati nella valutazione

Nessun livello di fondazione trovato

Livelli di elevazione considerati: Rialzato(L2), Primo(L3),

Regolarità in pianta - NO

L'edificio risulta NON regolare in pianta, in base alle condizioni indicate in NTC 2018 §7.2.1

Ok - Criterio A1 (Distribuzione masse) rispettato, con rapporto massimo 0 (limite=0,2) al livello Rialzato

N.V. - Criterio A2 (Distribuzione rigidezze) non valutabile al livello Rialzato

Ok - Criterio A3 (Forma compatta) rispettato, con rapporto massimo 1 (limite=1,05) al livello Primo

Ok - Criterio B (Rapporto lati) rispettato, con rapporto massimo 1,28 (limite=4) al livello Primo

No - Criterio C (Rapporto rigidezze piano) NON rispettato, con rapporto massimo > 999 (limite=0) al livello Rialzato

Regolarità in altezza - NO

L'edificio risulta NON regolare in altezza, in base alle condizioni indicate in NTC 2018 §7.2.1

Ok - Criterio D (Altezza elementi sismoresistenti) rispettato, con rapporto massimo 1 (limite=1,01)

Ok - Criterio E1 (Variazione masse) rispettato, con rapporto massimo 1,02 (limite=1,25) tra il livello Primo ed il precedente

N.V. - Criterio E2 (Riduzione rigidezze) non valutabile tra il livello Primo ed il precedente

N.V. - Criterio E3 (Incremento rigidezze) non valutabile tra il livello Primo ed il precedente

No - Criterio F (Rapporto Capacità/Domanda) NON rispettato, con rapporto massimo 31.6/10.9=2.9 (limite=1,3) tra il livello Primo ed il precedente

Ok - Criterio G1 (Rastremazione di piano) rispettato, con rapporto massimo 0,01 (limite=0,1) tra il livello Primo ed il precedente

Ok - Criterio G2 (Rastremazione totale) rispettato, con rapporto massimo 0,01 (limite=0,3) tra il livello Primo ed il precedente

Valori per piano

Verifiche di regolarità in pianta

Livello		A1			A2			A3			B			C		
Descr	Quota	A1n	A1d	A1r	A2n	A2d	A2r	A3n	A3d	A3r	Bn	Bd	Br	Cn	Cd	Cr
Rialzato	1.07	0	9.46	0				114.1199	114.1225	1	12.06	9.46	1.28	9999	1	9999
Primo	4.99	0	9.31	0				110.9191	110.9191	1	11.91	9.31	1.28	9999	1	9999

Verifiche di regolarità in elevazione

Rapporto di regolarità per la condizione D (Altezza elementi sismoresistenti): 3.92/3.92=0.01.

Livello		E1			E2			E3			F			G1			G2			
Descr	Q	Qinf	E1n	E1d	E1r	E2n	E2d	E2r	E3n	E3d	E3r	Fn	Fd	Fr	G1n	G1d	G1r	G2n	G2d	G2r
Primo	4.99	1.07	77865	76118	1.02							31.6	10.9	2.92	0.07	9.46	0.01	0.07	9.46	0.01

Dettaglio delle resistenze di piano a taglio (per valutazione punto F)

Livello			Capacità/Domanda in X			Capacità/Domanda in Y		
Descr	Q	Comb	VrdX	VedX	Rd/Ed	VrdY	VedY	Rd/Ed
Rialzato	1.07	SLV 1	138827	-39437	3.5	76043	-6680	11.4
Rialzato	1.07	SLV 2	138827	-39437	3.5	76043	-6680	11.4
Rialzato	1.07	SLV 3	138887	-39495	3.5	75962	7000	10.9
Rialzato	1.07	SLV 4	138887	-39495	3.5	75962	7000	10.9
Rialzato	1.07	SLV 5	138828	-11742	11.8	76157	-22752	3.3
Rialzato	1.07	SLV 6	138828	-11742	11.8	76157	-22752	3.3
Rialzato	1.07	SLV 7	139028	-11937	11.6	75889	22849	3.3
Rialzato	1.07	SLV 8	139028	-11937	11.6	75889	22849	3.3
Rialzato	1.07	SLV 9	138832	11937	11.6	76175	-22849	3.3
Rialzato	1.07	SLV 10	138832	11937	11.6	76175	-22849	3.3
Rialzato	1.07	SLV 11	139069	11742	11.8	75907	22752	3.3
Rialzato	1.07	SLV 12	139069	11742	11.8	75907	22752	3.3
Rialzato	1.07	SLV 13	138878	39495	3.5	76101	-7000	10.9
Rialzato	1.07	SLV 14	138878	39495	3.5	76101	-7000	10.9
Rialzato	1.07	SLV 15	138967	39437	3.5	76021	6680	11.4
Rialzato	1.07	SLV 16	138967	39437	3.5	76021	6680	11.4
Primo	4.99	SLV 1	70860	-19961	3.5	61210	-2163	28.3
Primo	4.99	SLV 2	70860	-19961	3.5	61210	-2163	28.3
Primo	4.99	SLV 3	70832	-19981	3.5	61212	1934	31.6
Primo	4.99	SLV 4	70832	-19981	3.5	61212	1934	31.6
Primo	4.99	SLV 5	76476	-5958	12.8	61205	-6863	8.9
Primo	4.99	SLV 6	76476	-5958	12.8	61205	-6863	8.9
Primo	4.99	SLV 7	75786	-6024	12.6	61211	6795	9
Primo	4.99	SLV 8	75786	-6024	12.6	61211	6795	9
Primo	4.99	SLV 9	76981	6024	12.8	61202	-6795	9
Primo	4.99	SLV 10	76981	6024	12.8	61202	-6795	9
Primo	4.99	SLV 11	76220	5958	12.8	61208	6863	8.9
Primo	4.99	SLV 12	76220	5958	12.8	61208	6863	8.9
Primo	4.99	SLV 13	69320	19981	3.5	61201	-1934	31.6
Primo	4.99	SLV 14	69320	19981	3.5	61201	-1934	31.6
Primo	4.99	SLV 15	69372	19961	3.5	61203	2163	28.3
Primo	4.99	SLV 16	69372	19961	3.5	61203	2163	28.3



1.2 Verifica sismica globale

Desc.: descrizione.

Stato limite: (muratura) V=Taglio; PF=Pressoflessione; PFFP=Pressoflessione fuori piano; R=Ribaltamento.

Molt.: moltiplicatore minimo della azione sismica che produce lo stato limite.

Comb.: combinazione.

PGA: accelerazione al suolo.

iPGA (ZE): indicatore di rischio sismico in termini di PGA ovvero rapporto tra l'azione sismica massima sopportabile dall'elemento e l'azione sismica massima che si utilizzerebbe nel progetto nuovo (§C8.3).

TR: tempo di ritorno.

(TR/TRrif)^.41: indicatore di rischio sismico in termini di periodo di ritorno.

fa: fattore di accelerazione.

Stato limite: (muratura) V=Taglio; PF=Presso flessione; PFFP=Pressoflessione fuori piano; R=Ribaltamento.

Coeff.s.: coefficiente minimo prodotto dallo stato limite.

Verifica: stato di verifica.

Maschio: maschio.

Stato limite: (maschio muratura) V=Taglio; PF=Presso flessione; PFFP=Presso flessione fuori piano; R=Ribaltamento.

Trave: trave di collegamento in muratura.

Stato limite: (trave muratura) V=Taglio; F=Flessione.

S. L.: stato limite di riferimento.

TR,C: periodo di ritorno di capacità.

PGA,C: accelerazione di aggancio di capacità.

TR,Rif: periodo di ritorno di riferimento.

PGA,Rif: accelerazione di aggancio di riferimento.

Tipo rottura: tipo di rottura che fornisce il valore minimo degli elementi considerati.

PAM: perdita media annua attesa.

Classe PAM: classe di rischio PAM.

IS-V: indice di sicurezza.

Classe IS-V: classe di rischio IS-V.

Verifica di elementi dotati di indicatori di rischio sismico mediante analisi con fattore q

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.) § C8.7.1

Accelerazioni e tempi di ritorno

Accelerazione di aggancio SLO (ag/g_SLO*S*ST) PGA,SLOrif = 0.081

Accelerazione di aggancio SLD (ag/g_SLD*S*ST) PGA,SLDrif = 0.101

Accelerazione di aggancio SLV (ag/g_SLV*S*ST) PGA,SLVrif = 0.244

Tr,SLOrif = 30 anni

Tr,SLDrif = 50 anni

Tr,SLVrif = 475 anni

Moltiplicatori minimi delle condizioni sismiche

(Il valore di ZE corrisponde al valore di I.R. PGA secondo quanto riportato nella Circolare 7 21-01-19 §C8.3)

Rottura a taglio

Moltiplicatore: 0

Trave di accoppiamento 1

Lunghezza: 1; altezza: 2; spessore: 0.45; distanza: 0

Combinazione SLV 1 V = -2016 V orto = 0 Vp = 6554 Vt = 7500

Tempo di ritorno 0 anni

Indicatore iTr=(Tr/Tr,SLVrif)^.41 = 0

PGA 0

Indicatore iPGA=PGA/PGA,SLVrif = 0

Fattore di accelerazione fa = 0

Rottura a flessione

Moltiplicatore: 0.377

Maschio 6

Lunghezza: 0.375; altezza: 2.6; spessore: 0.45 sezione a quota -1.53

Combinazione SLV 1 N = -1220 M = 215.12 σ0 = 7228 fd = 143750 Mu = 215.15

Tempo di ritorno 38 anni

Indicatore iTr=(Tr/Tr,SLVrif)^.41 = 0.355

PGA 0.088

Indicatore iPGA=PGA/PGA,SLVrif = 0.359

Fattore di accelerazione fa = 0.3577

Rottura a pressoflessione nel piano ortogonale

Moltiplicatore: 0.935



Maschio 28

Lunghezza: 9.01; altezza: 3.92; spessore: 0.3; sezione a quota: 3.03

Combinazione SLV 1 fd= 143750 Ta= 0.09 Wa= 540 N= -9766 M= 1419.95 Mc= 1421.52

Tempo di ritorno 393 anni

Indicatore $iTr=(Tr/Tr,SLVrif)^{.41} = 0.925$

PGA 0.227

Indicatore $iPGA=PGA/PGA,SLVrif = 0.931$

Fattore di accelerazione $fa = 0.9309$

Rottura per meccanismi locali di collasso

Moltiplicatore: 0.043

Maschio 15

Lunghezza: 4.704; altezza: 3.92; spessore: 0.3 f.agg.= 0 a.lim.= 4.94622

Combinazione SLV 1 N top= -8652 N base= -14873 T orto= 3 $\alpha_0= 0.052$ M*= 1699.9 e*= 0.896 a0*= 0.4216

Tempo di ritorno 0 anni

Indicatore $iTr=(Tr/Tr,SLVrif)^{.41} = 0$

PGA 0

Indicatore $iPGA=PGA/PGA,SLVrif = 0$

Fattore di accelerazione $fa = 0$

Indicatori minimi riferiti al solo materiale muratura

Desc.	Stato limite	Molt.	Comb.	PGA	IPGA (ZE)	TR	$(Tr/TRrif)^{.41}$	fa
Maschio 6	PF	0.377	SLV 1	0.0878	0.3593	38	0.355	0.3577
Maschio 6	V	0.331	SLV 1	0.0765	0.3133	27	0.3086	0.3097
Maschio 28	PFFP	0.935	SLV 1	0.2275	0.9311	393	0.9252	0.9309
Maschio 15	R	0.043	SLV 1	0	0	0	0	0
Trave di accoppiamento 4	PF	1.089	SLV 15	0.2654	1.0864	608	1.1065	1.086
Trave di accoppiamento 1	V	0	SLV 1	0	0	0	0	0

Coefficienti di sicurezza riferiti al solo materiale muratura

Desc.	Stato limite	Coeff.s.	Comb.	Verifica
Maschio 1	PF SLU	122.72	SLU 39	Si
Maschio 1	V SLU	1000	SLU 1	Si
Maschio 1	PF	9.609	SLV 11	Si
Maschio 1	V	4.031	SLV 11	Si
Maschio 1	PFFP	12.119	SLV 15	Si
Maschio 1	R	0.278	SLV 3	No
Maschio 3	PF SLU	3.077	SLU 81	Si
Maschio 3	V SLU	3.334	SLU 81	Si
Maschio 3	PF	2.13	SLV 15	Si
Maschio 3	V	2.622	SLV 3	Si
Maschio 3	PFFP	11.734	SLV 15	Si
Maschio 3	R	0.25	SLV 3	No
Maschio 4	PF SLU	406.851	SLU 39	Si
Maschio 4	V SLU	523.155	SLU 81	Si
Maschio 4	PF	30.71	SLV 3	Si
Maschio 4	V	3.765	SLV 3	Si
Maschio 4	PFFP	15.298	SLV 11	Si
Maschio 4	R	0.238	SLV 1	No
Maschio 5	PF SLU	3.193	SLU 81	Si
Maschio 5	V SLU	3.421	SLU 81	Si
Maschio 5	PF	2.14	SLV 3	Si
Maschio 5	V	2.588	SLV 15	Si
Maschio 5	PFFP	11.926	SLV 3	Si
Maschio 5	R	0.249	SLV 15	No
Maschio 6	PF SLU	1.05	SLU 39	Si
Maschio 6	V SLU	0.72	SLU 39	No
Maschio 6	PF	0	SLV 1	No
Maschio 6	V	0	SLV 1	No
Maschio 6	PFFP	15.842	SLV 15	Si
Maschio 6	R	0.262	SLV 3	No
Maschio 7	PF SLU	118.361	SLU 81	Si
Maschio 7	V SLU	508.286	SLU 81	Si
Maschio 7	PF	8.453	SLV 15	Si
Maschio 7	V	2.218	SLV 15	Si
Maschio 7	PFFP	24.486	SLV 5	Si
Maschio 7	R	0.253	SLV 13	No
Maschio 8	PF SLU	1.573	SLU 39	Si
Maschio 8	V SLU	1.832	SLU 39	Si
Maschio 8	PF	0	SLV 13	No
Maschio 8	V	0	SLV 13	No
Maschio 8	PFFP	18.173	SLV 1	Si
Maschio 8	R	0.262	SLV 13	No
Maschio 9	PF SLU	4.938	SLU 81	Si
Maschio 9	V SLU	5.867	SLU 81	Si
Maschio 9	PF	3.891	SLV 13	Si
Maschio 9	V	2.89	SLV 1	Si
Maschio 9	PFFP	15.312	SLV 9	Si
Maschio 9	R	0.261	SLV 1	No
Maschio 10	PF SLU	654.078	SLU 81	Si
Maschio 10	V SLU	333.406	SLU 81	Si
Maschio 10	PF	13.22	SLV 13	Si
Maschio 10	V	3.253	SLV 13	Si
Maschio 10	PFFP	17.161	SLV 5	Si
Maschio 10	R	0.04	SLV 9	No



Desc.	Stato limite	Coeff.s.	Comb.	Verifica
Maschio 11	PF SLU	4.986	SLU 81	Si
Maschio 11	V SLU	6.132	SLU 81	Si
Maschio 11	PF	4.012	SLV 1	Si
Maschio 11	V	2.957	SLV 13	Si
Maschio 11	PFFP	15.655	SLV 5	Si
Maschio 11	R	0.259	SLV 13	No
Maschio 12	PF SLU	13.799	SLU 64	Si
Maschio 12	V SLU	9.262	SLU 81	Si
Maschio 12	PF	5.458	SLV 7	Si
Maschio 12	V	3.397	SLV 5	Si
Maschio 12	PFFP	12.241	SLV 3	Si
Maschio 12	R	0.279	SLV 13	No
Maschio 13	PF SLU	9.593	SLU 43	Si
Maschio 13	V SLU	6.453	SLU 81	Si
Maschio 13	PF	4.744	SLV 11	Si
Maschio 13	V	3.288	SLV 7	Si
Maschio 13	PFFP	12.944	SLV 1	Si
Maschio 13	R	0.283	SLV 15	No
Maschio 14	PF SLU	62.72	SLU 39	Si
Maschio 14	V SLU	1000	SLU 1	Si
Maschio 14	PF	3.888	SLV 9	Si
Maschio 14	V	4.257	SLV 9	Si
Maschio 14	PFFP	0	SLV 13	No
Maschio 14	R	0.052	SLV 3	No
Maschio 15	PF SLU	2.756	SLU 39	Si
Maschio 15	V SLU	9.057	SLU 39	Si
Maschio 15	PF	2.193	SLV 15	Si
Maschio 15	V	1.593	SLV 1	Si
Maschio 15	PFFP	2.059	SLV 15	Si
Maschio 15	R	0.034	SLV 13	No
Maschio 16	PF SLU	42.332	SLU 43	Si
Maschio 16	V SLU	1000	SLU 1	Si
Maschio 16	PF	3.994	SLV 9	Si
Maschio 16	V	1.839	SLV 7	Si
Maschio 16	PFFP	1.095	SLV 1	Si
Maschio 16	R	0.064	SLV 3	No
Maschio 17	PF SLU	2.392	SLU 39	Si
Maschio 17	V SLU	2.174	SLU 81	Si
Maschio 17	PF	0	SLV 1	No
Maschio 17	V	0	SLV 1	No
Maschio 17	PFFP	1.517	SLV 15	Si
Maschio 17	R	0	SLV 1	No
Maschio 18	PF SLU	3.775	SLU 81	Si
Maschio 18	V SLU	10.8	SLU 81	Si
Maschio 18	PF	1.07	SLV 15	Si
Maschio 18	V	1.352	SLV 15	Si
Maschio 18	PFFP	2.766	SLV 15	Si
Maschio 18	R	0.037	SLV 3	No
Maschio 19	PF SLU	3.666	SLU 81	Si
Maschio 19	V SLU	2.841	SLU 81	Si
Maschio 19	PF	1.784	SLV 15	Si
Maschio 19	V	1.516	SLV 15	Si
Maschio 19	PFFP	1.928	SLV 11	Si
Maschio 19	R	0	SLV 1	No
Maschio 20	PF SLU	1.776	SLU 81	Si
Maschio 20	V SLU	1.69	SLU 81	Si
Maschio 20	PF	1.101	SLV 3	Si
Maschio 20	V	0.68	SLV 3	No
Maschio 20	PFFP	2.505	SLV 7	Si
Maschio 20	R	0	SLV 4	No
Maschio 21	PF SLU	3.968	SLU 39	Si
Maschio 21	V SLU	10.641	SLU 81	Si
Maschio 21	PF	1.184	SLV 3	Si
Maschio 21	V	2.032	SLV 15	Si
Maschio 21	PFFP	2.883	SLV 7	Si
Maschio 21	R	0.04	SLV 1	No
Maschio 22	PF SLU	2.523	SLU 39	Si
Maschio 22	V SLU	2.379	SLU 39	Si
Maschio 22	PF	0	SLV 13	No
Maschio 22	V	0	SLV 13	No
Maschio 22	PFFP	1.537	SLV 3	Si
Maschio 22	R	0	SLV 1	No
Maschio 23	PF SLU	71.98	SLU 43	Si
Maschio 23	V SLU	163.036	SLU 81	Si
Maschio 23	PF	1.373	SLV 15	Si
Maschio 23	V	2.421	SLV 15	Si
Maschio 23	PFFP	3.513	SLV 11	Si
Maschio 23	R	0	SLV 5	No
Maschio 24	PF SLU	4.672	SLU 39	Si
Maschio 24	V SLU	3.79	SLU 81	Si
Maschio 24	PF	3.55	SLV 3	Si
Maschio 24	V	2.967	SLV 1	Si
Maschio 24	PFFP	1.653	SLV 13	Si
Maschio 24	R	0.001	SLV 13	No
Maschio 25	PF SLU	295.347	SLU 39	Si
Maschio 25	V SLU	254.752	SLU 81	Si
Maschio 25	PF	5.74	SLV 13	Si
Maschio 25	V	3.27	SLV 13	Si
Maschio 25	PFFP	1.896	SLV 5	Si



Desc.	Stato limite	Coeff.s.	Comb.	Verifica
Maschio 25	R	0.04	SLV 13	No
Maschio 26	PF SLU	4.642	SLU 39	Si
Maschio 26	V SLU	3.917	SLU 81	Si
Maschio 26	PF	3.574	SLV 15	Si
Maschio 26	V	3.042	SLV 13	Si
Maschio 26	PFFP	1.674	SLV 1	Si
Maschio 26	R	0	SLV 1	No
Maschio 27	PF SLU	2.849	SLU 39	Si
Maschio 27	V SLU	9.32	SLU 39	Si
Maschio 27	PF	2.239	SLV 3	Si
Maschio 27	V	1.605	SLV 13	Si
Maschio 27	PFFP	2.078	SLV 3	Si
Maschio 27	R	0	SLV 5	No
Maschio 28	PF SLU	70.16	SLU 39	Si
Maschio 28	V SLU	1000	SLU 1	Si
Maschio 28	PF	3.929	SLV 5	Si
Maschio 28	V	4.369	SLV 5	Si
Maschio 28	PFFP	0	SLV 1	No
Maschio 28	R	0.056	SLV 13	No

Verifica maschi in muratura

Maschio	Stato limite	Molt.	Comb.	PGA	iPGA (ZE)	TR	(TR/TRrif)^.41	Verifica
1	PF	2.77	SLV 15	0.362	1.483	1618	1.653	Si
	V	2.74	SLV 15	0.362	1.483	1618	1.653	Si
	PFFP	3.2	SLV 15	0.362	1.483	1618	1.653	Si
	R	0.293	SLV 3	0.067	0.275	20	0.273	No
3	PF	2.424	SLV 15	0.362	1.483	1618	1.653	Si
	V	2.137	SLV 15	0.362	1.483	1618	1.653	Si
	PFFP	2.776	SLV 15	0.362	1.483	1618	1.653	Si
	R	0.274	SLV 3	0.062	0.256	17	0.255	No
4	PF	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	3.715	SLV 3	0.362	1.483	1618	1.653	Si
	PFFP	1000	SLV 1	0.362	1.483	1618	1.653	Si
	R	0.273	SLV 1	0.062	0.256	17	0.255	No
5	PF	2.439	SLV 3	0.362	1.483	1618	1.653	Si
	V	2.135	SLV 3	0.362	1.483	1618	1.653	Si
	PFFP	2.851	SLV 3	0.362	1.483	1618	1.653	Si
	R	0.274	SLV 15	0.062	0.256	17	0.255	No
6	PF	0.377	SLV 1	0.088	0.359	38	0.355	No
	V	0.331	SLV 1	0.077	0.313	27	0.309	No
	PFFP	2.305	SLV 15	0.362	1.483	1618	1.653	Si
	R	0.273	SLV 1	0.062	0.256	17	0.255	No
7	PF	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	2.218	SLV 1	0.362	1.483	1618	1.653	Si
	PFFP	1000	SLV 1	0.362	1.483	1618	1.653	Si
	R	0.265	SLV 3	0.061	0.249	16	0.249	No
8	PF	0.829	SLV 13	0.2	0.82	280	0.805	No
	V	0.753	SLV 13	0.181	0.741	214	0.721	No
	PFFP	2.457	SLV 1	0.362	1.483	1618	1.653	Si
	R	0.272	SLV 15	0.062	0.256	17	0.255	No
9	PF	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	3.209	SLV 13	0.362	1.483	1618	1.653	Si
	PFFP	1000	SLV 1	0.362	1.483	1618	1.653	Si
	R	0.277	SLV 1	0.064	0.262	18	0.261	No
10	PF	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	3.205	SLV 13	0.362	1.483	1618	1.653	Si
	PFFP	1000	SLV 1	0.362	1.483	1618	1.653	Si
	R	0.258	SLV 3	0.059	0.242	14	0.236	No
11	PF	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	3.256	SLV 1	0.362	1.483	1618	1.653	Si
	PFFP	1000	SLV 1	0.362	1.483	1618	1.653	Si
	R	0.276	SLV 13	0.064	0.262	18	0.261	No
12	PF	2.644	SLV 3	0.362	1.483	1618	1.653	Si
	V	2.62	SLV 3	0.362	1.483	1618	1.653	Si
	PFFP	2.812	SLV 3	0.362	1.483	1618	1.653	Si
	R	0.291	SLV 13	0.067	0.275	20	0.273	No
13	PF	3.221	SLV 1	0.362	1.483	1618	1.653	Si
	V	2.97	SLV 5	0.362	1.483	1618	1.653	Si
	PFFP	3.229	SLV 1	0.362	1.483	1618	1.653	Si
	R	0.294	SLV 15	0.067	0.275	20	0.273	No
14	PF	1.706	SLV 15	0.362	1.483	1618	1.653	Si
	V	1.703	SLV 15	0.362	1.483	1618	1.653	Si
	PFFP	0.942	SLV 15	0.229	0.938	401	0.933	No
	R	0.057	SLV 1	0	0	0	0	No
15	PF	3.41	SLV 1	0.362	1.483	1618	1.653	Si
	V	1.527	SLV 15	0.362	1.483	1618	1.653	Si
	PFFP	1.955	SLV 15	0.362	1.483	1618	1.653	Si
	R	0.043	SLV 1	0	0	0	0	No
16	PF	3.984	SLV 7	0.362	1.483	1618	1.653	Si
	V	1.71	SLV 7	0.362	1.483	1618	1.653	Si
	PFFP	1.093	SLV 1	0.266	1.09	615	1.112	Si
	R	0.063	SLV 1	0	0	0	0	No
17	PF	0.698	SLV 3	0.167	0.683	176	0.666	No
	V	0.586	SLV 3	0.139	0.569	116	0.561	No
	PFFP	1.357	SLV 15	0.329	1.348	1181	1.453	Si
	R	0.043	SLV 1	0	0	0	0	No
18	PF	1.035	SLV 15	0.253	1.034	525	1.042	Si
	V	1.017	SLV 15	0.248	1.016	498	1.02	Si



Maschio	Stato limite	Molt.	Comb.	PGA	iPGA (ZE)	TR	(TR/TRrif)^.41	Verifica
19	PFFP	2.431	SLV 15	0.362	1.483	1618	1.653	Si
	R	0.047	SLV 3	0	0	0	0	No
	PF	1.884	SLV 3	0.362	1.483	1618	1.653	Si
	V	1.417	SLV 15	0.344	1.407	1359	1.539	Si
20	PFFP	1.786	SLV 11	0.362	1.483	1618	1.653	Si
	R	0.045	SLV 3	0	0	0	0	No
	PF	1.103	SLV 13	0.269	1.1	631	1.123	Si
	V	0.779	SLV 3	0.188	0.769	236	0.751	No
21	PFFP	2.361	SLV 7	0.362	1.483	1618	1.653	Si
	R	0.048	SLV 1	0	0	0	0	No
	PF	1.099	SLV 3	0.268	1.096	625	1.119	Si
	V	1.08	SLV 3	0.263	1.078	594	1.096	Si
22	PFFP	2.631	SLV 7	0.362	1.483	1618	1.653	Si
	R	0.048	SLV 1	0	0	0	0	No
	PF	0.784	SLV 15	0.189	0.774	240	0.756	No
	V	0.655	SLV 15	0.156	0.64	152	0.627	No
23	PFFP	1.378	SLV 3	0.334	1.369	1241	1.483	Si
	R	0.043	SLV 3	0	0	0	0	No
	PF	1.378	SLV 15	0.334	1.369	1241	1.483	Si
	V	1.311	SLV 15	0.318	1.303	1056	1.388	Si
24	PFFP	3.479	SLV 11	0.362	1.483	1618	1.653	Si
	R	0.046	SLV 1	0	0	0	0	No
	PF	3.595	SLV 13	0.362	1.483	1618	1.653	Si
	V	2.93	SLV 1	0.362	1.483	1618	1.653	Si
25	PFFP	1.557	SLV 13	0.362	1.483	1618	1.653	Si
	R	0.047	SLV 1	0	0	0	0	No
	PF	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	2.792	SLV 13	0.362	1.483	1618	1.653	Si
26	PFFP	1.847	SLV 5	0.362	1.483	1618	1.653	Si
	R	0.048	SLV 1	0	0	0	0	No
	PF	3.792	SLV 1	0.362	1.483	1618	1.653	Si
	V	2.967	SLV 13	0.362	1.483	1618	1.653	Si
27	PFFP	1.58	SLV 1	0.362	1.483	1618	1.653	Si
	R	0.046	SLV 1	0	0	0	0	No
	PF	3.587	SLV 13	0.362	1.483	1618	1.653	Si
	V	1.533	SLV 3	0.362	1.483	1618	1.653	Si
28	PFFP	1.973	SLV 3	0.362	1.483	1618	1.653	Si
	R	0.043	SLV 1	0	0	0	0	No
	PF	1.751	SLV 3	0.362	1.483	1618	1.653	Si
	V	1.747	SLV 3	0.362	1.483	1618	1.653	Si
	PFFP	0.935	SLV 1	0.227	0.931	393	0.925	No
	R	0.057	SLV 1	0	0	0	0	No

Verifica travi di collegamento in muratura

Trave	Stato limite	Molt.	Comb.	PGA	iPGA (ZE)	TR	(TR/TRrif)^.41	Verifica
1	F	3.122	SLV 1	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
2	F	1.111	SLV 3	0.271	1.108	645	1.134	Si
	V	0	SLV 1	0	0	0	0	No
3	F	3.237	SLV 13	0.362	1.483	1618	1.653	Si
	V	0.067	SLV 13	0	0	0	0	No
4	F	1.089	SLV 15	0.265	1.086	608	1.107	Si
	V	0	SLV 1	0	0	0	0	No
5	F	1.919	SLV 1	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
6	F	1.692	SLV 3	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
7	F	2.696	SLV 3	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
8	F	1.143	SLV 3	0.278	1.139	700	1.172	Si
	V	0	SLV 1	0	0	0	0	No
9	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
10	F	1.188	SLV 15	0.289	1.183	784	1.228	Si
	V	0	SLV 1	0	0	0	0	No
11	F	2.189	SLV 11	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
12	F	1.291	SLV 15	0.314	1.283	1004	1.359	Si
	V	0	SLV 1	0	0	0	0	No
13	F	1.714	SLV 3	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
14	F	1.881	SLV 13	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
15	F	1.123	SLV 15	0.274	1.12	665	1.148	Si
	V	0	SLV 1	0	0	0	0	No
16	F	3.202	SLV 3	0.362	1.483	1618	1.653	Si
	V	0.098	SLV 3	0.02	0.08	1	0.08	No
17	F	1.991	SLV 3	0.362	1.483	1618	1.653	Si
	V	0.18	SLV 3	0.041	0.169	6	0.167	No
18	F	1.404	SLV 3	0.341	1.394	1319	1.52	Si
	V	0	SLV 1	0	0	0	0	No
19	F	1.734	SLV 15	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
20	F	1.803	SLV 1	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
21	F	3.302	SLV 3	0.362	1.483	1618	1.653	Si
	V	0.102	SLV 3	0.02	0.08	1	0.08	No
22	F	3.42	SLV 15	0.362	1.483	1618	1.653	Si



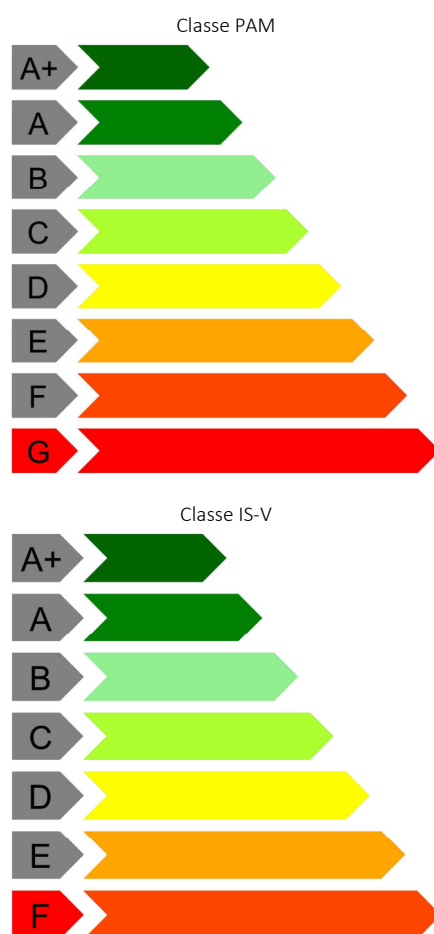
Trave	Stato limite	Molt.	Comb.	PGA	IPGA (ζE)	TR	$(TR/TR_{rif})^{4.1}$	Verifica
	V	0	SLV 1	0	0	0	0	No
23	F	3.104	SLV 15	0.362	1.483	1618	1.653	Si
	V	0.128	SLV 13	0.026	0.107	2	0.106	No
24	F	3.851	SLV 3	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
25	F	1.334	SLV 3	0.324	1.326	1117	1.42	Si
	V	0	SLV 1	0	0	0	0	No

Periodi di ritorno e accelerazioni di aggancio per gli Stati Limite

S. L.	TR,C	PGA,C	TR,Rif	PGA,Rif	Tipo rottura
Stato limite di salvaguardia della vita	0	0	475	0.244	ribaltamento maschio muratura

Coefficienti relativi alle Linee guida per la classificazione del rischio sismico delle costruzioni secondo il D.M. 24 09/01/2020

TR,C	TR,Rif	PAM	Classe PAM	IS-V	Classe IS-V	Tipo rottura
0	475	8.22	G	0	F	ribaltamento maschio muratura



1.3 Verifiche maschi in muratura

Le unità di misura elencate nel capitolo sono in [m, daN, s] ove non espressamente specificato.

X_{ini.}: coordinate del punto iniziale del maschio. [m]

Y_{ini.}: coordinate del punto iniziale del maschio. [m]

X_{fin.}: coordinate del punto finale del maschio. [m]

Y_{fin.}: coordinate del punto finale del maschio. [m]

Quota i.: livello o falda inferiore.

Quota s.: livello o falda superiore.

l: lunghezza del maschio. [m]

Sp.: spessore. [m]

h_{netta}: altezza netta (a filo solai). [m]

h_{ini.}: altezza nel modello al punto iniziale. [m]



h fin.: altezza nel modello al punto finale. [m]
a: distanza tra irrigidimenti laterali. [m]
a.s.,sx: lunghezza di appoggio del solaio di sinistra. [m]
a.s.,dx: lunghezza di appoggio del solaio di destra. [m]
fb: resistenza normalizzata a compressione verticale dei blocchi. [daN/m²]
fk: resistenza caratteristica a compressione della muratura utilizzata. [daN/m²]
fvk0: resistenza caratteristica a taglio in assenza di carichi verticali. [daN/m²]
fmedio: resistenza media a compressione della muratura utilizzata. [daN/m²]
τ0: resistenza media a taglio in assenza di azioni normali [C8.7.1.16]. [daN/m²]
fvo: resistenza media a taglio in assenza di azioni normali [C8.7.1.17]. [daN/m²]
μ: coefficiente di attrito [C8.7.1.17].
φ: coefficiente di ammortamento o ingranamento secondo Circolare 7 21-01-19 §C8.7.1.3.1.1.
fv,lim: valore massimo della resistenza a taglio che può essere impiegata nel calcolo. [daN/m²]
E: modulo di elasticità longitudinale della muratura utilizzato. [daN/m²]
G: modulo di elasticità tangenziale della muratura utilizzato. [daN/m²]
FC: fattore di confidenza della muratura.
Comb.: combinazione.
Quota: quota della sezione di verifica. [m]
N: sforzo normale. [daN]
M: momento flettente nel piano. [daN*m]
σ0: tensione media di compressione. [daN/m²]
Mu: momento flettente ultimo. [daN*m]
c.s.: coefficiente di sicurezza.
Verifica: stato di verifica.
V par: taglio nel piano. [daN]
σN: tensione media di compressione sulla parte reagente. [daN/m²]
l': lunghezza della parte compressa della parete. [m]
fvd: resistenza a taglio di calcolo. [daN/m²]
Vt scorr.: taglio ultimo per verifica a scorrimento. [daN]
Vt fess.diag.: taglio ultimo per verifica a fessurazione diagonale regolare [C8.7.1.17]. [daN]
Vt,lim: taglio limite [C8.7.1.18]. [daN]
c.s.: coefficiente di sicurezza a taglio.
fd: resistenza a compressione di calcolo. [daN/m²]
Sa: accelerazione massima, adimensionalizzata rispetto a g, che l'elemento strutturale subisce durante il sisma.
M: momento flettente fuori piano. [daN*m]
Mc: momento di collasso per azioni perpendicolari al piano. [daN*m]
Coeff.s.: coefficiente di sicurezza.
N top: sforzo normale in sommità. [daN]
N base: sforzo normale al piede. [daN]
V orto: taglio fuori piano. [daN]
α0: moltiplicatore secondo [C8.7.1.1].
M*: massa partecipante al cinematisimo. [daN/(m/s²)]
e*: frazione di massa partecipante della muratura [C8.7.1.5].
α0*: accelerazione spettrale di attivazione del meccanismo [C8.7.1.8]. [m/s²]
αLim: accelerazione limite [C7.2.11]. [m/s²]
Stato limite: pF_SLU=Presso flessione per azioni non sismiche; V_SLU=Taglio per azioni non sismiche; PF_SLV=Presso flessione per azioni sismiche; V_SLV=Taglio per azioni sismiche; PFFP_SLV=Presso flessione fuori piano per azioni sismiche; R_SLV=Ribaltamento per azioni sismiche.

Maschio 1

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota l.	Quota s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-9.429	-17.728	-9.428	-8.718	L1	L2	9.01	0.45	2.6	2.6	2.6			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ0	fvo	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 41	-1.53	-63707	-349.94	15713	231638.64	661.936	Si
SLU 41	1.07	-37377	-1216.81	9219	149327.4	122.72	Si
SLU 83	-1.53	-76544	-310.78	18879	264913.87	852.418	Si
SLU 83	1.07	-43965	-1310.61	10844	171697.41	131.006	Si
SLU 84	-1.53	-76544	-310.78	18879	264913.87	852.418	Si
SLU 84	1.07	-43965	-1310.61	10844	171697.41	131.006	Si
SLU 21	-1.53	-59072	-244.7	14570	218521.87	893.034	Si
SLU 21	1.07	-34062	-1045.73	8401	137624.04	131.606	Si
SLU 42	-1.53	-63707	-349.94	15713	231638.64	661.936	Si
SLU 42	1.07	-37377	-1216.81	9219	149327.4	122.72	Si
SLU 20	-1.53	-59072	-244.7	14570	218521.87	893.034	Si
SLU 20	1.07	-34062	-1045.73	8401	137624.04	131.606	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 81	-1.53	-765.44	-310.78	18879	264913.87	852.418	Si
SLU 81	1.07	-43965	-1310.61	10844	171697.41	131.006	Si
SLU 82	-1.53	-765.44	-310.78	18879	264913.87	852.418	Si
SLU 82	1.07	-43965	-1310.61	10844	171697.41	131.006	Si
SLU 39	-1.53	-63707	-349.94	15713	231638.64	661.936	Si
SLU 39	1.07	-37377	-1216.81	9219	149327.4	122.72	Si
SLU 40	-1.53	-63707	-349.94	15713	231638.64	661.936	Si
SLU 40	1.07	-37377	-1216.81	9219	149327.4	122.72	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 11	-1.53	-47603	20173.21	11741	193844.18	9.609	Si
SLV 11	1.07	-25157	5756.81	6205	107579.23	18.687	Si
SLV 15	-1.53	-39280	6405.37	9688	162924.85	25.436	Si
SLV 15	1.07	-19079	3846.15	4706	82640.6	21.487	Si
SLV 6	-1.53	-55618	-20314.81	13718	222429.21	10.949	Si
SLV 6	1.07	-31560	-7085.93	7784	133120.6	18.787	Si
SLV 10	-1.53	-48281	-20049.12	11908	196306.83	9.791	Si
SLV 10	1.07	-26075	-5382	6431	111284.01	20.677	Si
SLV 16	-1.53	-39280	6405.37	9688	162924.85	25.436	Si
SLV 16	1.07	-19079	3846.15	4706	82640.6	21.487	Si
SLV 9	-1.53	-48281	-20049.12	11908	196306.83	9.791	Si
SLV 9	1.07	-26075	-5382	6431	111284.01	20.677	Si
SLV 12	-1.53	-47603	20173.21	11741	193844.18	9.609	Si
SLV 12	1.07	-25157	5756.81	6205	107579.23	18.687	Si
SLV 8	-1.53	-54940	19907.52	13550	220057.01	11.054	Si
SLV 8	1.07	-30643	4052.88	7558	129507.33	31.954	Si
SLV 5	-1.53	-55618	-20314.81	13718	222429.21	10.949	Si
SLV 5	1.07	-31560	-7085.93	7784	133120.6	18.787	Si
SLV 7	-1.53	-54940	19907.52	13550	220057.01	11.054	Si
SLV 7	1.07	-30643	4052.88	7558	129507.33	31.954	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 54	-1.53	-68615	0	-129.05		16923	9.01	7812	31674			1000	Si
SLU 54	1.07	-38156	0	-978.26		9411	9.01	6810	27613			1000	Si
SLU 56	-1.53	-68615	0	-129.05		16923	9.01	7812	31674			1000	Si
SLU 56	1.07	-38156	0	-978.26		9411	9.01	6810	27613			1000	Si
SLU 61	-1.53	-71910	0	-205.53		17736	9.01	7920	32113			1000	Si
SLU 61	1.07	-40650	0	-1139.53		10026	9.01	6892	27945			1000	Si
SLU 55	-1.53	-68615	0	-129.05		16923	9.01	7812	31674			1000	Si
SLU 55	1.07	-38156	0	-978.26		9411	9.01	6810	27613			1000	Si
SLU 1	-1.53	-48090	0	10.26		11861	9.01	7137	28937			1000	Si
SLU 1	1.07	-25749	0	-508.17		6351	9.01	6402	25958			1000	Si
SLU 60	-1.53	-71910	0	-205.53		17736	9.01	7920	32113			1000	Si
SLU 60	1.07	-40650	0	-1139.53		10026	9.01	6892	27945			1000	Si
SLU 58	-1.53	-68615	0	-129.05		16923	9.01	7812	31674			1000	Si
SLU 58	1.07	-38156	0	-978.26		9411	9.01	6810	27613			1000	Si
SLU 59	-1.53	-68615	0	-129.05		16923	9.01	7812	31674			1000	Si
SLU 59	1.07	-38156	0	-978.26		9411	9.01	6810	27613			1000	Si
SLU 57	-1.53	-68615	0	-129.05		16923	9.01	7812	31674			1000	Si
SLU 57	1.07	-38156	0	-978.26		9411	9.01	6810	27613			1000	Si
SLU 53	-1.53	-68615	0	-129.05		16923	9.01	7812	31674			1000	Si
SLU 53	1.07	-38156	0	-978.26		9411	9.01	6810	27613			1000	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 9	-1.53	-48281	-10776	-20049.12		11908	9.01	10715	43444			4.03	Si
SLV 9	1.07	-26075	-7949	-5382		6431	9.01	9620	39002			4.91	Si
SLV 13	-1.53	-39483	-3283	-5661.33		9738	9.01	10281	41684			12.7	Si
SLV 13	1.07	-19354	-2462	504.5		4773	9.01	9288	37658			15.3	Si
SLV 8	-1.53	-54940	10776	19907.52		13550	9.01	11043	44776			4.16	Si
SLV 8	1.07	-30643	7949	4052.88		7558	9.01	9845	39916			5.02	Si
SLV 12	-1.53	-47603	10743	20173.21		11741	9.01	10681	43308			4.03	Si
SLV 12	1.07	-25157	7898	5756.81		6205	9.01	9574	38819			4.91	Si
SLV 6	-1.53	-55618	-10743	-20314.81		13718	9.01	11077	44911			4.18	Si
SLV 6	1.07	-31560	-7898	-7085.93		7784	9.01	9890	40100			5.08	Si
SLV 14	-1.53	-39483	-3283	-5661.33		9738	9.01	10281	41684			12.7	Si
SLV 14	1.07	-19354	-2462	504.5		4773	9.01	9288	37658			15.3	Si
SLV 10	-1.53	-48281	-10776	-20049.12		11908	9.01	10715	43444			4.03	Si
SLV 10	1.07	-26075	-7949	-5382		6431	9.01	9620	39002			4.91	Si
SLV 7	-1.53	-54940	10776	19907.52		13550	9.01	11043	44776			4.16	Si
SLV 7	1.07	-30643	7949	4052.88		7558	9.01	9845	39916			5.02	Si
SLV 5	-1.53	-55618	-10743	-20314.81		13718	9.01	11077	44911			4.18	Si
SLV 5	1.07	-31560	-7898	-7085.93		7784	9.01	9890	40100			5.08	Si
SLV 11	-1.53	-47603	10743	20173.21		11741	9.01	10681	43308			4.03	Si
SLV 11	1.07	-25157	7898	5756.81		6205	9.01	9574	38819			4.91	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota -0.23 W_a 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 15	143750	0.24	7306	-29624	517.1	6266.86	12.12	Si
SLV 16	143750	0.24	7306	-29624	517.1	6266.86	12.12	Si
SLV 13	143750	0.24	7324	-29696	517.1	6281.09	12.15	Si
SLV 14	143750	0.24	7324	-29696	517.1	6281.09	12.15	Si
SLV 11	143750	0.24	9019	-36566	517.1	7620.05	14.74	Si
SLV 12	143750	0.24	9019	-36566	517.1	7620.05	14.74	Si



Comb.	fd	Sa	σ0	N	M	Mc	Coeff.s.	Verifica
SLV 10	143750	0.24	9078	-36805	517.1	7665.94	14.82	Si
SLV 9	143750	0.24	9078	-36805	517.1	7665.94	14.82	Si
SLV 8	143750	0.24	10504	-42588	517.1	8758.48	16.94	Si
SLV 7	143750	0.24	10504	-42588	517.1	8758.48	16.94	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = -0.23 Wa = 0.08 Ta = 0.0251

Comb.	N top	N base	V orto	α0	M*	e*	a0*	aLim	Verifica
SLV 3	-37363	-63738	150	0.101	5313.9	0.925	1.58412	5.70385	No
SLV 4	-37363	-63738	150	0.101	5313.9	0.925	1.58412	5.70385	No
SLV 2	-37639	-63941	55	0.103	5341.6	0.926	1.61407	5.70385	No
SLV 1	-37639	-63941	55	0.103	5341.6	0.926	1.61407	5.70385	No
SLV 13	-19354	-39483	-164	0.109	3518.8	0.901	1.76415	5.70385	No
SLV 14	-19354	-39483	-164	0.109	3518.8	0.901	1.76415	5.70385	No
SLV 15	-19079	-39280	-69	0.113	3491.8	0.9	1.82245	5.70385	No
SLV 16	-19079	-39280	-69	0.113	3491.8	0.9	1.82245	5.70385	No
SLV 7	-30643	-54940	185	0.102	4639.1	0.917	1.62237	2.39898	No
SLV 8	-30643	-54940	185	0.102	4639.1	0.917	1.62237	2.39898	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	122.72	SLV 39	Si
V_SLV	1000	SLV 1	Si
PF_SLV	9.609	SLV 11	Si
V_SLV	4.031	SLV 11	Si
PFFP_SLV	12.119	SLV 15	Si
R_SLV	0.278	SLV 3	No

Maschio 3

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s,sx	a.s,dx
-8.545	-17.728	-9.429	-17.728	L1	L2	0.884	0.45	2.6	2.6	2.6			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ0	fv0	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 82	0.47	-7566	-708.69	19009	2565.18	3.62	Si
SLU 82	0.87	-7668	-841.56	19267	2589.18	3.077	Si
SLU 83	0.47	-7566	-708.69	19009	2565.18	3.62	Si
SLU 83	0.87	-7668	-841.56	19267	2589.18	3.077	Si
SLU 84	0.47	-7566	-708.69	19009	2565.18	3.62	Si
SLU 84	0.87	-7668	-841.56	19267	2589.18	3.077	Si
SLU 42	0.47	-6544	-613.8	16441	2309.84	3.763	Si
SLU 42	0.87	-6691	-754.92	16810	2348.25	3.111	Si
SLU 81	0.47	-7566	-708.69	19009	2565.18	3.62	Si
SLU 81	0.87	-7668	-841.56	19267	2589.18	3.077	Si
SLU 78	0.47	-7064	-663.39	17749	2443.43	3.683	Si
SLU 78	0.87	-7117	-765.96	17881	2456.46	3.207	Si
SLU 41	0.47	-6544	-613.8	16441	2309.84	3.763	Si
SLU 41	0.87	-6691	-754.92	16810	2348.25	3.111	Si
SLU 39	0.47	-6544	-613.8	16441	2309.84	3.763	Si
SLU 39	0.87	-6691	-754.92	16810	2348.25	3.111	Si
SLU 40	0.47	-6544	-613.8	16441	2309.84	3.763	Si
SLU 40	0.87	-6691	-754.92	16810	2348.25	3.111	Si
SLU 77	0.47	-7064	-663.39	17749	2443.43	3.683	Si
SLU 77	0.87	-7117	-765.96	17881	2456.46	3.207	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γM = 2

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLV 4	0.47	-4987	-96.74	12530	1979.37	20.46	Si
SLV 4	0.87	-4862	-612.95	12215	1935.06	3.157	Si
SLV 11	0.47	-3750	-482.69	9423	1530.68	3.171	Si
SLV 11	0.87	-3959	-441.54	9946	1608.25	3.642	Si
SLV 7	0.47	-4058	-285.08	10197	1645.01	5.77	Si
SLV 7	0.87	-4175	-520.33	10488	1687.68	3.244	Si
SLV 12	0.47	-3750	-482.69	9423	1530.68	3.171	Si
SLV 12	0.87	-3959	-441.54	9946	1608.25	3.642	Si
SLV 13	0.47	-4449	-791.61	11177	1787.44	2.258	Si
SLV 13	0.87	-4516	-350.94	11346	1811.64	5.162	Si
SLV 8	0.47	-4058	-285.08	10197	1645.01	5.77	Si
SLV 8	0.87	-4175	-520.33	10488	1687.68	3.244	Si
SLV 3	0.47	-4987	-96.74	12530	1979.37	20.46	Si
SLV 3	0.87	-4862	-612.95	12215	1935.06	3.157	Si
SLV 15	0.47	-3961	-755.43	9951	1608.9	2.13	Si
SLV 15	0.87	-4143	-350.34	10408	1675.98	4.784	Si
SLV 16	0.47	-3961	-755.43	9951	1608.9	2.13	Si
SLV 16	0.87	-4143	-350.34	10408	1675.98	4.784	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 14	0.47	-4449	-791.61	11177	1787.44	2.258	Si
SLV 14	0.87	-4516	-350.94	11346	1811.64	5.162	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 42	0.47	-6544	916	-613.8		16441	0.8845	7748	3084			3.37	Si
SLU 42	0.87	-6691	918	-754.92		16810	0.8845	7797	3103			3.38	Si
SLU 40	0.47	-6544	916	-613.8		16441	0.8845	7748	3084			3.37	Si
SLU 40	0.87	-6691	918	-754.92		16810	0.8845	7797	3103			3.38	Si
SLU 81	0.47	-7566	966	-708.69		19009	0.8845	8090	3220			3.33	Si
SLU 81	0.87	-7668	968	-841.56		19267	0.8845	8124	3234			3.34	Si
SLU 41	0.47	-6544	916	-613.8		16441	0.8845	7748	3084			3.37	Si
SLU 41	0.87	-6691	918	-754.92		16810	0.8845	7797	3103			3.38	Si
SLU 75	0.47	-7064	835	-663.39		17749	0.8845	7922	3153			3.78	Si
SLU 75	0.87	-7117	837	-765.96		17881	0.8845	7940	3160			3.77	Si
SLU 77	0.47	-7064	835	-663.39		17749	0.8845	7922	3153			3.78	Si
SLU 77	0.87	-7117	837	-765.96		17881	0.8845	7940	3160			3.77	Si
SLU 83	0.47	-7566	966	-708.69		19009	0.8845	8090	3220			3.33	Si
SLU 83	0.87	-7668	968	-841.56		19267	0.8845	8124	3234			3.34	Si
SLU 82	0.47	-7566	966	-708.69		19009	0.8845	8090	3220			3.33	Si
SLU 82	0.87	-7668	968	-841.56		19267	0.8845	8124	3234			3.34	Si
SLU 84	0.47	-7566	966	-708.69		19009	0.8845	8090	3220			3.33	Si
SLU 84	0.87	-7668	968	-841.56		19267	0.8845	8124	3234			3.34	Si
SLU 39	0.47	-6544	916	-613.8		16441	0.8845	7748	3084			3.37	Si
SLU 39	0.87	-6691	918	-754.92		16810	0.8845	7797	3103			3.38	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 1	0.47	-5475	1412	-132.91		13757	0.8845	11085	4412			3.12	Si
SLV 1	0.87	-5235	1260	-613.56		13152	0.8845	10964	4364			3.46	Si
SLV 7	0.47	-4058	1171	-285.08		10197	0.8845	10373	4128			3.53	Si
SLV 7	0.87	-4175	1131	-520.33		10488	0.8845	10431	4152			3.67	Si
SLV 3	0.47	-4987	1645	-96.74		12530	0.8845	10839	4314			2.62	Si
SLV 3	0.87	-4862	1495	-612.95		12215	0.8845	10776	4289			2.87	Si
SLV 14	0.47	-4449	-720	-791.61		12468	0.7929	10827	3863			5.37	Si
SLV 14	0.87	-4516	-567	-350.94		11346	0.8845	10603	4220			7.44	Si
SLV 13	0.47	-4449	-720	-791.61		12468	0.7929	10827	3863			5.37	Si
SLV 13	0.87	-4516	-567	-350.94		11346	0.8845	10603	4220			7.44	Si
SLV 2	0.47	-5475	1412	-132.91		13757	0.8845	11085	4412			3.12	Si
SLV 2	0.87	-5235	1260	-613.56		13152	0.8845	10964	4364			3.46	Si
SLV 8	0.47	-4058	1171	-285.08		10197	0.8845	10373	4128			3.53	Si
SLV 8	0.87	-4175	1131	-520.33		10488	0.8845	10431	4152			3.67	Si
SLV 12	0.47	-3750	531	-482.69		9423	0.8845	10218	4067			7.66	Si
SLV 12	0.87	-3959	583	-441.54		9946	0.8845	10323	4109			7.05	Si
SLV 4	0.47	-4987	1645	-96.74		12530	0.8845	10839	4314			2.62	Si
SLV 4	0.87	-4862	1495	-612.95		12215	0.8845	10776	4289			2.87	Si
SLV 11	0.47	-3750	531	-482.69		9423	0.8845	10218	4067			7.66	Si
SLV 11	0.87	-3959	583	-441.54		9946	0.8845	10323	4109			7.05	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota -0.23 W_a 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 16	143750	0.24	6951	-2767	50.03	587.08	11.73	Si
SLV 15	143750	0.24	6951	-2767	50.03	587.08	11.73	Si
SLV 11	143750	0.24	7436	-2959	50.03	625.36	12.5	Si
SLV 12	143750	0.24	7436	-2959	50.03	625.36	12.5	Si
SLV 14	143750	0.24	8029	-3196	50.03	671.79	13.43	Si
SLV 13	143750	0.24	8029	-3196	50.03	671.79	13.43	Si
SLV 8	143750	0.24	8929	-3554	50.03	741.19	14.81	Si
SLV 7	143750	0.24	8929	-3554	50.03	741.19	14.81	Si
SLV 9	143750	0.24	11029	-4390	50.03	898.55	17.96	Si
SLV 10	143750	0.24	11029	-4390	50.03	898.55	17.96	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = -0.23 $W_a = 0.08$ $T_a = 0.0251$

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 3	-4157	-5995	-56	0.091	570.9	0.93	1.42638	5.70385	No
SLV 4	-4157	-5995	-56	0.091	570.9	0.93	1.42638	5.70385	No
SLV 14	-3329	-4464	55	0.092	487.6	0.921	1.45887	5.70385	No
SLV 13	-3329	-4464	55	0.092	487.6	0.921	1.45887	5.70385	No
SLV 2	-4496	-6782	4	0.101	605.1	0.934	1.56719	5.70385	No
SLV 1	-4496	-6782	4	0.101	605.1	0.934	1.56719	5.70385	No
SLV 15	-2990	-3677	-5	0.106	453.6	0.917	1.67766	5.70385	No
SLV 16	-2990	-3677	-5	0.106	453.6	0.917	1.67766	5.70385	No
SLV 7	-3353	-4266	-108	0.08	490	0.922	1.26214	2.39898	No
SLV 8	-3353	-4266	-108	0.08	490	0.922	1.26214	2.39898	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	3.077	SLU 81	Si
V_SLU	3.334	SLU 81	Si
PF_SLV	2.13	SLV 15	Si
V_SLV	2.622	SLV 3	Si
PFFP_SLV	11.734	SLV 15	Si
R_SLV	0.25	SLV 3	No



Maschio 4

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
0.227	-17.728	-7.545	-17.728	L1	L2	7.772	0.45	2.6	2.6	2.6			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 42	0.47	-52743	-374.61	15081	167007.52	445.813	Si
SLU 42	0.87	-50067	-394.16	14316	160362.65	406.851	Si
SLU 40	0.47	-52743	-374.61	15081	167007.52	445.813	Si
SLU 40	0.87	-50067	-394.16	14316	160362.65	406.851	Si
SLU 82	0.47	-59625	-375.19	17049	183201.68	488.287	Si
SLU 82	0.87	-56163	-395.69	16059	175215.87	442.813	Si
SLU 39	0.47	-52743	-374.61	15081	167007.52	445.813	Si
SLU 39	0.87	-50067	-394.16	14316	160362.65	406.851	Si
SLU 20	0.47	-46452	-310.72	13282	151073.41	486.199	Si
SLU 20	0.87	-43802	-327.16	12525	144037.7	440.265	Si
SLU 19	0.47	-46452	-310.72	13282	151073.41	486.199	Si
SLU 19	0.87	-43802	-327.16	12525	144037.7	440.265	Si
SLU 81	0.47	-59625	-375.19	17049	183201.68	488.287	Si
SLU 81	0.87	-56163	-395.69	16059	175215.87	442.813	Si
SLU 41	0.47	-52743	-374.61	15081	167007.52	445.813	Si
SLU 41	0.87	-50067	-394.16	14316	160362.65	406.851	Si
SLU 18	0.47	-46452	-310.72	13282	151073.41	486.199	Si
SLU 18	0.87	-43802	-327.16	12525	144037.7	440.265	Si
SLU 21	0.47	-46452	-310.72	13282	151073.41	486.199	Si
SLU 21	0.87	-43802	-327.16	12525	144037.7	440.265	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 8	0.47	-31528	500.87	9015	113474.22	226.555	Si
SLV 8	0.87	-29023	-1268.08	8299	105119.46	82.897	Si
SLV 7	0.47	-31528	500.87	9015	113474.22	226.555	Si
SLV 7	0.87	-29023	-1268.08	8299	105119.46	82.897	Si
SLV 3	0.47	-34193	2680.29	9777	122236.31	45.606	Si
SLV 3	0.87	-31606	-3703.52	9037	113733.38	30.71	Si
SLV 16	0.47	-33972	-3096.14	9714	121517.3	39.248	Si
SLV 16	0.87	-31329	3369.36	8958	112814.76	33.483	Si
SLV 15	0.47	-33972	-3096.14	9714	121517.3	39.248	Si
SLV 15	0.87	-31329	3369.36	8958	112814.76	33.483	Si
SLV 13	0.47	-36190	-2961	10348	128720.89	43.472	Si
SLV 13	0.87	-33460	3403.7	9567	119840.19	35.209	Si
SLV 1	0.47	-36411	2815.43	10411	129431.02	45.972	Si
SLV 1	0.87	-33737	-3669.18	9647	120748.06	32.909	Si
SLV 2	0.47	-36411	2815.43	10411	129431.02	45.972	Si
SLV 2	0.87	-33737	-3669.18	9647	120748.06	32.909	Si
SLV 4	0.47	-34193	2680.29	9777	122236.31	45.606	Si
SLV 4	0.87	-31606	-3703.52	9037	113733.38	30.71	Si
SLV 14	0.47	-36190	-2961	10348	128720.89	43.472	Si
SLV 14	0.87	-33460	3403.7	9567	119840.19	35.209	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	l'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 81	0.47	-59625	51	-375.19		17049	7.7717	7829	27379			532.14	Si
SLU 81	0.87	-56163	51	-395.69		16059	7.7717	7697	26918			523.16	Si
SLU 82	0.47	-59625	51	-375.19		17049	7.7717	7829	27379			532.14	Si
SLU 82	0.87	-56163	51	-395.69		16059	7.7717	7697	26918			523.16	Si
SLU 42	0.47	-52743	49	-374.61		15081	7.7717	7566	26462			540.06	Si
SLU 42	0.87	-50067	49	-394.16		14316	7.7717	7464	26105			532.77	Si
SLU 40	0.47	-52743	49	-374.61		15081	7.7717	7566	26462			540.06	Si
SLU 40	0.87	-50067	49	-394.16		14316	7.7717	7464	26105			532.77	Si
SLU 73	0.47	-54728	44	-304.46		15649	7.7717	7642	26726			605.22	Si
SLU 73	0.87	-51266	44	-322.04		14659	7.7717	7510	26265			594.76	Si
SLU 41	0.47	-52743	49	-374.61		15081	7.7717	7566	26462			540.06	Si
SLU 41	0.87	-50067	49	-394.16		14316	7.7717	7464	26105			532.77	Si
SLU 80	0.47	-54728	44	-304.46		15649	7.7717	7642	26726			605.22	Si
SLU 80	0.87	-51266	44	-322.04		14659	7.7717	7510	26265			594.76	Si
SLU 39	0.47	-52743	49	-374.61		15081	7.7717	7566	26462			540.06	Si
SLU 39	0.87	-50067	49	-394.16		14316	7.7717	7464	26105			532.77	Si
SLU 84	0.47	-59625	51	-375.19		17049	7.7717	7829	27379			532.14	Si
SLU 84	0.87	-56163	51	-395.69		16059	7.7717	7697	26918			523.16	Si
SLU 83	0.47	-59625	51	-375.19		17049	7.7717	7829	27379			532.14	Si
SLU 83	0.87	-56163	51	-395.69		16059	7.7717	7697	26918			523.16	Si



Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLV 13	0.47	-36190	-9508	-2961		10348	7.7717	10403	36382			3.83	Si
SLV 13	0.87	-33460	-6493	3403.7		9567	7.7717	10247	35836			5.52	Si
SLV 14	0.47	-36190	-9508	-2961		10348	7.7717	10403	36382			3.83	Si
SLV 14	0.87	-33460	-6493	3403.7		9567	7.7717	10247	35836			5.52	Si
SLV 3	0.47	-34193	9557	2680.29		9777	7.7717	10289	35983			3.77	Si
SLV 3	0.87	-31606	6541	-3703.52		9037	7.7717	10141	35465			5.42	Si
SLV 15	0.47	-33972	-9456	-3096.14		9714	7.7717	10276	35938			3.8	Si
SLV 15	0.87	-31329	-6416	3369.36		8958	7.7717	10125	35410			5.52	Si
SLV 7	0.47	-31528	2964	500.87		9015	7.7717	10136	35450			11.96	Si
SLV 7	0.87	-29023	2097	-1268.08		8299	7.7717	9993	34949			16.67	Si
SLV 8	0.47	-31528	2964	500.87		9015	7.7717	10136	35450			11.96	Si
SLV 8	0.87	-29023	2097	-1268.08		8299	7.7717	9993	34949			16.67	Si
SLV 16	0.47	-33972	-9456	-3096.14		9714	7.7717	10276	35938			3.8	Si
SLV 16	0.87	-31329	-6416	3369.36		8958	7.7717	10125	35410			5.52	Si
SLV 2	0.47	-36411	9504	2815.43		10411	7.7717	10416	36426			3.83	Si
SLV 2	0.87	-33737	6464	-3669.18		9647	7.7717	10263	35891			5.55	Si
SLV 4	0.47	-34193	9557	2680.29		9777	7.7717	10289	35983			3.77	Si
SLV 4	0.87	-31606	6541	-3703.52		9037	7.7717	10141	35465			5.42	Si
SLV 1	0.47	-36411	9504	2815.43		10411	7.7717	10416	36426			3.83	Si
SLV 1	0.87	-33737	6464	-3669.18		9647	7.7717	10263	35891			5.55	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota -0.23 Wa 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 12	143750	0.24	9247	-32338	439.62	6725.48	15.3	Si
SLV 11	143750	0.24	9247	-32338	439.62	6725.48	15.3	Si
SLV 8	143750	0.24	9256	-32371	439.62	6731.71	15.31	Si
SLV 7	143750	0.24	9256	-32371	439.62	6731.71	15.31	Si
SLV 15	143750	0.24	9973	-34877	439.62	7206.93	16.39	Si
SLV 16	143750	0.24	9973	-34877	439.62	7206.93	16.39	Si
SLV 4	143750	0.24	10004	-34986	439.62	7227.39	16.44	Si
SLV 3	143750	0.24	10004	-34986	439.62	7227.39	16.44	Si
SLV 14	143750	0.24	10604	-37086	439.62	7620.26	17.33	Si
SLV 13	143750	0.24	10604	-37086	439.62	7620.26	17.33	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = -0.23 Wa = 0.08 Ta = 0.0251

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 2	-31601	-44077	715	0.086	4520.4	0.924	1.3577	5.70385	No
SLV 1	-31601	-44077	715	0.086	4520.4	0.924	1.3577	5.70385	No
SLV 14	-31409	-44005	713	0.086	4501.1	0.924	1.35894	5.70385	No
SLV 13	-31409	-44005	713	0.086	4501.1	0.924	1.35894	5.70385	No
SLV 15	-29367	-41854	-672	0.087	4295.9	0.921	1.37995	5.70385	No
SLV 16	-29367	-41854	-672	0.087	4295.9	0.921	1.37995	5.70385	No
SLV 3	-29559	-41926	-670	0.088	4315.2	0.922	1.3804	5.70385	No
SLV 4	-29559	-41926	-670	0.088	4315.2	0.922	1.3804	5.70385	No
SLV 12	-27053	-39370	-2288	0.042	4063.8	0.918	0.66031	2.39898	No
SLV 11	-27053	-39370	-2288	0.042	4063.8	0.918	0.66031	2.39898	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	406.851	SLU 39	Si
V_SLU	523.155	SLU 81	Si
PF_SLV	30.71	SLV 3	Si
V_SLV	3.765	SLV 3	Si
PFFP_SLV	15.298	SLV 11	Si
R_SLV	0.238	SLV 1	No

Maschio 5

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
2.185	-17.729	1.227	-17.729	L1	L2	0.958	0.45	2.6	2.6	2.6			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _k	f _{vk0}	f _{medio}	τ_0	f _{v0}	μ	ϕ	f _{v,lim}	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 78	0.47	-7603	772.41	17641	2852.54	3.693	Si
SLU 78	0.87	-7643	860.3	17734	2863.36	3.328	Si
SLU 40	0.47	-7047	717.94	16350	2697.19	3.757	Si
SLU 40	0.87	-7187	848.43	16675	2737.1	3.226	Si
SLU 83	0.47	-8145	826.85	18899	2995.65	3.623	Si
SLU 83	0.87	-8237	945.44	19111	3019	3.193	Si
SLU 42	0.47	-7047	717.94	16350	2697.19	3.757	Si
SLU 42	0.87	-7187	848.43	16675	2737.1	3.226	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 82	0.47	-8145	826.85	18899	2995.65	3.623	Si
SLU 82	0.87	-8237	945.44	19111	3019	3.193	Si
SLU 77	0.47	-7603	772.41	17641	2852.54	3.693	Si
SLU 77	0.87	-7643	860.3	17734	2863.36	3.328	Si
SLU 84	0.47	-8145	826.85	18899	2995.65	3.623	Si
SLU 84	0.87	-8237	945.44	19111	3019	3.193	Si
SLU 81	0.47	-8145	826.85	18899	2995.65	3.623	Si
SLU 81	0.87	-8237	945.44	19111	3019	3.193	Si
SLU 41	0.47	-7047	717.94	16350	2697.19	3.757	Si
SLU 41	0.87	-7187	848.43	16675	2737.1	3.226	Si
SLU 39	0.47	-7047	717.94	16350	2697.19	3.757	Si
SLU 39	0.87	-7187	848.43	16675	2737.1	3.226	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 8	0.47	-4048	571.56	9393	1789.6	3.131	Si
SLV 8	0.87	-4253	512.95	9869	1872.31	3.65	Si
SLV 2	0.47	-4787	912.62	11108	2084.17	2.284	Si
SLV 2	0.87	-4880	471.33	11322	2120.33	4.499	Si
SLV 3	0.47	-4270	878.11	9906	1878.83	2.14	Si
SLV 3	0.87	-4475	467.41	10384	1961.01	4.196	Si
SLV 12	0.47	-4376	343.31	10154	1921.62	5.597	Si
SLV 12	0.87	-4468	555.91	10366	1957.92	3.522	Si
SLV 1	0.47	-4787	912.62	11108	2084.17	2.284	Si
SLV 1	0.87	-4880	471.33	11322	2120.33	4.499	Si
SLV 11	0.47	-4376	343.31	10154	1921.62	5.597	Si
SLV 11	0.87	-4468	555.91	10366	1957.92	3.522	Si
SLV 7	0.47	-4048	571.56	9393	1789.6	3.131	Si
SLV 7	0.87	-4253	512.95	9869	1872.31	3.65	Si
SLV 4	0.47	-4270	878.11	9906	1878.83	2.14	Si
SLV 4	0.87	-4475	467.41	10384	1961.01	4.196	Si
SLV 6	0.47	-5774	686.59	13398	2462.06	3.586	Si
SLV 6	0.87	-5602	526.02	12997	2397.24	4.557	Si
SLV 5	0.47	-5774	686.59	13398	2462.06	3.586	Si
SLV 5	0.87	-5602	526.02	12997	2397.24	4.557	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 75	0.47	-7603	-879	772.41		17641	0.9578	7908	3408			3.88	Si
SLU 75	0.87	-7643	-881	860.3		17734	0.9578	7920	3414			3.87	Si
SLU 42	0.47	-7047	-965	717.94		16350	0.9578	7736	3334			3.46	Si
SLU 42	0.87	-7187	-967	848.43		16675	0.9578	7779	3353			3.47	Si
SLU 77	0.47	-7603	-879	772.41		17641	0.9578	7908	3408			3.88	Si
SLU 77	0.87	-7643	-881	860.3		17734	0.9578	7920	3414			3.87	Si
SLU 81	0.47	-8145	-1017	826.85		18899	0.9578	8075	3480			3.42	Si
SLU 81	0.87	-8237	-1019	945.44		19111	0.9578	8104	3493			3.43	Si
SLU 40	0.47	-7047	-965	717.94		16350	0.9578	7736	3334			3.46	Si
SLU 40	0.87	-7187	-967	848.43		16675	0.9578	7779	3353			3.47	Si
SLU 84	0.47	-8145	-1017	826.85		18899	0.9578	8075	3480			3.42	Si
SLU 84	0.87	-8237	-1019	945.44		19111	0.9578	8104	3493			3.43	Si
SLU 39	0.47	-7047	-965	717.94		16350	0.9578	7736	3334			3.46	Si
SLU 39	0.87	-7187	-967	848.43		16675	0.9578	7779	3353			3.47	Si
SLU 41	0.47	-7047	-965	717.94		16350	0.9578	7736	3334			3.46	Si
SLU 41	0.87	-7187	-967	848.43		16675	0.9578	7779	3353			3.47	Si
SLU 82	0.47	-8145	-1017	826.85		18899	0.9578	8075	3480			3.42	Si
SLU 82	0.87	-8237	-1019	945.44		19111	0.9578	8104	3493			3.43	Si
SLU 83	0.47	-8145	-1017	826.85		18899	0.9578	8075	3480			3.42	Si
SLU 83	0.87	-8237	-1019	945.44		19111	0.9578	8104	3493			3.43	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 4	0.47	-4270	550	878.11		11576	0.8196	10648	3928			7.14	Si
SLV 4	0.87	-4475	576	467.41		10384	0.9578	10410	4487			7.79	Si
SLV 12	0.47	-4376	-1221	343.31		10154	0.9578	10364	4467			3.66	Si
SLV 12	0.87	-4468	-1238	555.91		10366	0.9578	10406	4485			3.62	Si
SLV 11	0.47	-4376	-1221	343.31		10154	0.9578	10364	4467			3.66	Si
SLV 11	0.87	-4468	-1238	555.91		10366	0.9578	10406	4485			3.62	Si
SLV 3	0.47	-4270	550	878.11		11576	0.8196	10648	3928			7.14	Si
SLV 3	0.87	-4475	576	467.41		10384	0.9578	10410	4487			7.79	Si
SLV 2	0.47	-4787	783	912.62		12303	0.8648	10794	4200			5.36	Si
SLV 2	0.87	-4880	813	471.33		11322	0.9578	10598	4568			5.62	Si
SLV 13	0.47	-5881	-1524	151.79		13646	0.9578	11063	4768			3.13	Si
SLV 13	0.87	-5594	-1552	614.53		12979	0.9578	10929	4710			3.04	Si
SLV 15	0.47	-5363	-1757	117.28		12445	0.9578	10822	4664			2.66	Si
SLV 15	0.87	-5189	-1789	610.61		12041	0.9578	10741	4629			2.59	Si
SLV 16	0.47	-5363	-1757	117.28		12445	0.9578	10822	4664			2.66	Si
SLV 16	0.87	-5189	-1789	610.61		12041	0.9578	10741	4629			2.59	Si
SLV 14	0.47	-5881	-1524	151.79		13646	0.9578	11063	4768			3.13	Si
SLV 14	0.87	-5594	-1552	614.53		12979	0.9578	10929	4710			3.04	Si
SLV 1	0.47	-4787	783	912.62		12303	0.8648	10794	4200			5.36	Si
SLV 1	0.87	-4880	813	471.33		11322	0.9578	10598	4568			5.62	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota -0.23 Wa 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 3	143750	0.24	7072	-3048	54.18	646.1	11.93	Si
SLV 4	143750	0.24	7072	-3048	54.18	646.1	11.93	Si



Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 7	143750	0.24	7443	-3208	54.18	677.83	12.51	Si
SLV 8	143750	0.24	7443	-3208	54.18	677.83	12.51	Si
SLV 1	143750	0.24	8187	-3529	54.18	740.72	13.67	Si
SLV 2	143750	0.24	8187	-3529	54.18	740.72	13.67	Si
SLV 12	143750	0.24	8877	-3826	54.18	798.26	14.73	Si
SLV 11	143750	0.24	8877	-3826	54.18	798.26	14.73	Si
SLV 5	143750	0.24	11160	-4810	54.18	983.38	18.15	Si
SLV 6	143750	0.24	11160	-4810	54.18	983.38	18.15	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = -0.23 Wa = 0.08 Ta = 0.0251

Comb.	N top	N base	V orto	α_0	M*	e*	α_0^*	aLim	Verifica
SLV 15	-4502	-6352	-63	0.091	618.3	0.93	1.41942	5.70385	No
SLV 16	-4502	-6352	-63	0.091	618.3	0.93	1.41942	5.70385	No
SLV 2	-3625	-4906	62	0.092	530	0.922	1.44995	5.70385	No
SLV 1	-3625	-4906	62	0.092	530	0.922	1.44995	5.70385	No
SLV 13	-4864	-7229	2	0.101	654.9	0.934	1.57262	5.70385	No
SLV 14	-4864	-7229	2	0.101	654.9	0.934	1.57262	5.70385	No
SLV 4	-3262	-4029	-3	0.106	493.6	0.917	1.68255	5.70385	No
SLV 3	-3262	-4029	-3	0.106	493.6	0.917	1.68255	5.70385	No
SLV 11	-3644	-4516	-119	0.08	531.9	0.922	1.25724	2.39898	No
SLV 12	-3644	-4516	-119	0.08	531.9	0.922	1.25724	2.39898	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	3.193	SLU 81	Si
V_SLU	3.421	SLU 81	Si
PF_SLV	2.14	SLV 3	Si
V_SLV	2.588	SLV 15	Si
PFFP_SLV	11.926	SLV 3	Si
R_SLV	0.249	SLV 15	No

Maschio 6

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota s.	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-9.054	-13.248	-9.429	-13.248	L1	L2	0.375	0.45	2.6	2.6	2.6			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 40	-1.53	-1504	239.22	8915	251.18	1.05	Si
SLU 40	0.57	-4536	-308.01	26882	569.83	1.85	Si
SLU 34	-1.53	-1492	213.11	8843	249.4	1.17	Si
SLU 34	0.57	-4128	-275.16	24464	541.55	1.968	Si
SLU 38	-1.53	-1492	213.11	8843	249.4	1.17	Si
SLU 38	0.57	-4128	-275.16	24464	541.55	1.968	Si
SLU 33	-1.53	-1492	213.11	8843	249.4	1.17	Si
SLU 33	0.57	-4128	-275.16	24464	541.55	1.968	Si
SLU 35	-1.53	-1492	213.11	8843	249.4	1.17	Si
SLU 35	0.57	-4128	-275.16	24464	541.55	1.968	Si
SLU 37	-1.53	-1492	213.11	8843	249.4	1.17	Si
SLU 37	0.57	-4128	-275.16	24464	541.55	1.968	Si
SLU 39	-1.53	-1504	239.22	8915	251.18	1.05	Si
SLU 39	0.57	-4536	-308.01	26882	569.83	1.85	Si
SLU 41	-1.53	-1504	239.22	8915	251.18	1.05	Si
SLU 41	0.57	-4536	-308.01	26882	569.83	1.85	Si
SLU 36	-1.53	-1492	213.11	8843	249.4	1.17	Si
SLU 36	0.57	-4128	-275.16	24464	541.55	1.968	Si
SLU 42	-1.53	-1504	239.22	8915	251.18	1.05	Si
SLU 42	0.57	-4536	-308.01	26882	569.83	1.85	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 3	-1.53	-859	327.22	0	0	0	No, $e > l/2$
SLV 3	0.57	-4612	-332.25	27334	671.35	2.021	Si
SLV 1	-1.53	-852	329.51	0	0	0	No, $e > l/2$
SLV 1	0.57	-4624	-333.32	27404	672.57	2.018	Si
SLV 9	-1.53	-1606	95.13	9520	277.74	2.92	Si
SLV 9	0.57	-2615	-149.17	15498	428.15	2.87	Si
SLV 4	-1.53	-859	327.22	0	0	0	No, $e > l/2$
SLV 4	0.57	-4612	-332.25	27334	671.35	2.021	Si
SLV 5	-1.53	-1255	204.53	7438	220.99	1.08	Si
SLV 5	0.57	-3549	-234.73	21031	550.86	2.347	Si
SLV 6	-1.53	-1255	204.53	7438	220.99	1.08	Si
SLV 6	0.57	-3549	-234.73	21031	550.86	2.347	Si
SLV 2	-1.53	-852	329.51	0	0	0	No, $e > l/2$
SLV 2	0.57	-4624	-333.32	27404	672.57	2.018	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 7	-1.53	-1276	196.93	7564	224.49	1.14	Si
SLV 7	0.57	-3510	-231.18	20798	546.01	2.362	Si
SLV 8	-1.53	-1276	196.93	7564	224.49	1.14	Si
SLV 8	0.57	-3510	-231.18	20798	546.01	2.362	Si
SLV 10	-1.53	-1606	95.13	9520	277.74	2.92	Si
SLV 10	0.57	-2615	-149.17	15498	428.15	2.87	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 40	-1.53	-1504	575	239.22		39138	0.0854	10774	414			0.72	No, Vu<V
SLU 40	0.57	-4536	608	-308.01		28096	0.3588	9302	1502			2.47	Si
SLU 83	-1.53	-1916	635	263.67		28454	0.1496	9349	630			0.99	No, Vu<V
SLU 83	0.57	-5142	671	-340.34		31399	0.3639	9742	1595			2.38	Si
SLU 81	-1.53	-1916	635	263.67		28454	0.1496	9349	630			0.99	No, Vu<V
SLU 81	0.57	-5142	671	-340.34		31399	0.3639	9742	1595			2.38	Si
SLU 39	-1.53	-1504	575	239.22		39138	0.0854	10774	414			0.72	No, Vu<V
SLU 39	0.57	-4536	608	-308.01		28096	0.3588	9302	1502			2.47	Si
SLU 41	-1.53	-1504	575	239.22		39138	0.0854	10774	414			0.72	No, Vu<V
SLU 41	0.57	-4536	608	-308.01		28096	0.3588	9302	1502			2.47	Si
SLU 82	-1.53	-1916	635	263.67		28454	0.1496	9349	630			0.99	No, Vu<V
SLU 82	0.57	-5142	671	-340.34		31399	0.3639	9742	1595			2.38	Si
SLU 37	-1.53	-1492	513	213.11		24741	0.134	8854	534			1.04	Si
SLU 37	0.57	-4128	542	-275.16		25305	0.3625	8930	1457			2.69	Si
SLU 42	-1.53	-1504	575	239.22		39138	0.0854	10774	414			0.72	No, Vu<V
SLU 42	0.57	-4536	608	-308.01		28096	0.3588	9302	1502			2.47	Si
SLU 33	-1.53	-1492	513	213.11		24741	0.134	8854	534			1.04	Si
SLU 33	0.57	-4128	542	-275.16		25305	0.3625	8930	1457			2.69	Si
SLU 84	-1.53	-1916	635	263.67		28454	0.1496	9349	630			0.99	No, Vu<V
SLU 84	0.57	-5142	671	-340.34		31399	0.3639	9742	1595			2.38	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 5	-1.53	-1255	459	204.53		37903	0.0736	15914	527			1.15	Si
SLV 5	0.57	-3549	475	-234.73		21663	0.3641	12666	2075			4.37	Si
SLV 9	-1.53	-1606	242	95.13		9520	0.375	10237	1728			7.14	Si
SLV 9	0.57	-2615	298	-149.17		15498	0.375	11433	1929			6.47	Si
SLV 7	-1.53	-1276	464	196.93		28476	0.0996	14029	629			1.35	Si
SLV 7	0.57	-3510	450	-231.18		21375	0.3649	12608	2070			4.6	Si
SLV 4	-1.53	-859	716	327.22		0	0	8333	0			0	No, Vu<V
SLV 4	0.57	-4612	666	-332.25		29591	0.3464	14252	2221			3.34	Si
SLV 10	-1.53	-1606	242	95.13		9520	0.375	10237	1728			7.14	Si
SLV 10	0.57	-2615	298	-149.17		15498	0.375	11433	1929			6.47	Si
SLV 6	-1.53	-1255	459	204.53		37903	0.0736	15914	527			1.15	Si
SLV 6	0.57	-3549	475	-234.73		21663	0.3641	12666	2075			4.37	Si
SLV 8	-1.53	-1276	464	196.93		28476	0.0996	14029	629			1.35	Si
SLV 8	0.57	-3510	450	-231.18		21375	0.3649	12608	2070			4.6	Si
SLV 1	-1.53	-852	715	329.51		0	0	8333	0			0	No, Vu<V
SLV 1	0.57	-4624	673	-333.32		29679	0.3462	14269	2223			3.3	Si
SLV 2	-1.53	-852	715	329.51		0	0	8333	0			0	No, Vu<V
SLV 2	0.57	-4624	673	-333.32		29679	0.3462	14269	2223			3.3	Si
SLV 3	-1.53	-859	716	327.22		0	0	8333	0			0	No, Vu<V
SLV 3	0.57	-4612	666	-332.25		29591	0.3464	14252	2221			3.34	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota -0.23 Wa 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 15	143750	0.24	9759	-1647	21.52	340.94	15.84	Si
SLV 16	143750	0.24	9759	-1647	21.52	340.94	15.84	Si
SLV 13	143750	0.24	9805	-1655	21.52	342.4	15.91	Si
SLV 14	143750	0.24	9805	-1655	21.52	342.4	15.91	Si
SLV 12	143750	0.24	14215	-2399	21.52	476.92	22.16	Si
SLV 11	143750	0.24	14215	-2399	21.52	476.92	22.16	Si
SLV 9	143750	0.24	14368	-2424	21.52	481.37	22.37	Si
SLV 10	143750	0.24	14368	-2424	21.52	481.37	22.37	Si
SLV 8	143750	0.24	18080	-3051	21.52	584.88	27.18	Si
SLV 7	143750	0.24	18080	-3051	21.52	584.88	27.18	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = -0.23 Wa = 0.08 Ta = 0.0251

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 3	-2647	-859	-1	0.097	331.6	0.947	1.49543	5.70385	No
SLV 4	-2647	-859	-1	0.097	331.6	0.947	1.49543	5.70385	No
SLV 2	-2654	-852	-1	0.097	332.3	0.947	1.49668	5.70385	No
SLV 1	-2654	-852	-1	0.097	332.3	0.947	1.49668	5.70385	No
SLV 14	-1027	-2024	1	0.11	168.3	0.909	1.75518	5.70385	No
SLV 13	-1027	-2024	1	0.11	168.3	0.909	1.75518	5.70385	No
SLV 15	-1021	-2030	1	0.11	167.7	0.909	1.76141	5.70385	No
SLV 16	-1021	-2030	1	0.11	167.7	0.909	1.76141	5.70385	No
SLV 8	-2070	-1276	-1	0.1	273.1	0.937	1.55183	2.39898	No
SLV 7	-2070	-1276	-1	0.1	273.1	0.937	1.55183	2.39898	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	1.05	SLU 39	Si
V_SLU	0.72	SLU 39	No
PF_SLV	0	SLV 1	No



Stato limite	Coeff.s.	Comb.	Verifica
V_SLV	0	SLV 1	No
PFFP_SLV	15.842	SLV 15	Si
R_SLV	0.262	SLV 3	No

Maschio 7

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
0.81	-13.248	-8.054	-13.248	L1	L2	8.864	0.45	2.6	2.6	2.6			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ0	fv0	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 78	-1.53	-111520	-2532.99	27958	324615.28	128.155	Si
SLU 78	0.57	-90965	-2392.74	22805	290288.78	121.321	Si
SLU 82	-1.53	-120321	-2740.61	30165	335789.85	122.524	Si
SLU 82	0.57	-99767	-2588.67	25012	306398.59	118.361	Si
SLU 80	-1.53	-111520	-2532.99	27958	324615.28	128.155	Si
SLU 80	0.57	-90965	-2392.74	22805	290288.78	121.321	Si
SLU 81	-1.53	-120321	-2740.61	30165	335789.85	122.524	Si
SLU 81	0.57	-99767	-2588.67	25012	306398.59	118.361	Si
SLU 77	-1.53	-111520	-2532.99	27958	324615.28	128.155	Si
SLU 77	0.57	-90965	-2392.74	22805	290288.78	121.321	Si
SLU 75	-1.53	-111520	-2532.99	27958	324615.28	128.155	Si
SLU 75	0.57	-90965	-2392.74	22805	290288.78	121.321	Si
SLU 84	-1.53	-120321	-2740.61	30165	335789.85	122.524	Si
SLU 84	0.57	-99767	-2588.67	25012	306398.59	118.361	Si
SLU 79	-1.53	-111520	-2532.99	27958	324615.28	128.155	Si
SLU 79	0.57	-90965	-2392.74	22805	290288.78	121.321	Si
SLU 76	-1.53	-111520	-2532.99	27958	324615.28	128.155	Si
SLU 76	0.57	-90965	-2392.74	22805	290288.78	121.321	Si
SLU 83	-1.53	-120321	-2740.61	30165	335789.85	122.524	Si
SLU 83	0.57	-99767	-2588.67	25012	306398.59	118.361	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γM = 2

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLV 14	-1.53	-73320	-31994.86	18381	276067.16	8.628	Si
SLV 14	0.57	-57568	8239.3	14432	225004.31	27.309	Si
SLV 4	-1.53	-73170	28680.43	18344	275603.62	9.609	Si
SLV 4	0.57	-57412	-11371.01	14393	224475.14	19.741	Si
SLV 15	-1.53	-73379	-32682.75	18396	276251.18	8.453	Si
SLV 15	0.57	-57677	7870.44	14460	225372.67	28.635	Si
SLV 12	-1.53	-73375	-12008.16	18395	276239.33	23.004	Si
SLV 12	0.57	-57711	705.6	14468	225488.38	319.568	Si
SLV 2	-1.53	-73111	29368.31	18329	275419.38	9.378	Si
SLV 2	0.57	-57303	-11002.16	14366	224106.26	20.369	Si
SLV 11	-1.53	-73375	-12008.16	18395	276239.33	23.004	Si
SLV 11	0.57	-57711	705.6	14468	225488.38	319.568	Si
SLV 3	-1.53	-73170	28680.43	18344	275603.62	9.609	Si
SLV 3	0.57	-57412	-11371.01	14393	224475.14	19.741	Si
SLV 13	-1.53	-73320	-31994.86	18381	276067.16	8.628	Si
SLV 13	0.57	-57568	8239.3	14432	225004.31	27.309	Si
SLV 1	-1.53	-73111	29368.31	18329	275419.38	9.378	Si
SLV 1	0.57	-57303	-11002.16	14366	224106.26	20.369	Si
SLV 16	-1.53	-73379	-32682.75	18396	276251.18	8.453	Si
SLV 16	0.57	-57677	7870.44	14460	225372.67	28.635	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, γM = 3

Comb.	Quota	N	V par	M	σ0	σN	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 79	-1.53	-111520	-64	-2532.99		27958	8.864	9283	37029			576.79	Si
SLU 79	0.57	-90965	-64	-2392.74		22805	8.864	8596	34289			534.1	Si
SLU 81	-1.53	-120321	-70	-2740.61		30165	8.864	9578	38203			547.57	Si
SLU 81	0.57	-99767	-70	-2588.67		25012	8.864	8890	35462			508.29	Si
SLU 75	-1.53	-111520	-64	-2532.99		27958	8.864	9283	37029			576.79	Si
SLU 75	0.57	-90965	-64	-2392.74		22805	8.864	8596	34289			534.1	Si
SLU 76	-1.53	-111520	-64	-2532.99		27958	8.864	9283	37029			576.79	Si
SLU 76	0.57	-90965	-64	-2392.74		22805	8.864	8596	34289			534.1	Si
SLU 83	-1.53	-120321	-70	-2740.61		30165	8.864	9578	38203			547.57	Si
SLU 83	0.57	-99767	-70	-2588.67		25012	8.864	8890	35462			508.29	Si
SLU 74	-1.53	-111520	-64	-2532.99		27958	8.864	9283	37029			576.79	Si
SLU 74	0.57	-90965	-64	-2392.74		22805	8.864	8596	34289			534.1	Si
SLU 82	-1.53	-120321	-70	-2740.61		30165	8.864	9578	38203			547.57	Si
SLU 82	0.57	-99767	-70	-2588.67		25012	8.864	8890	35462			508.29	Si
SLU 84	-1.53	-120321	-70	-2740.61		30165	8.864	9578	38203			547.57	Si
SLU 84	0.57	-99767	-70	-2588.67		25012	8.864	8890	35462			508.29	Si
SLU 73	-1.53	-111520	-64	-2532.99		27958	8.864	9283	37029			576.79	Si
SLU 73	0.57	-90965	-64	-2392.74		22805	8.864	8596	34289			534.1	Si
SLU 78	-1.53	-111520	-64	-2532.99		27958	8.864	9283	37029			576.79	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 78	0.57	-90965	-64	-2392.74		22805	8.864	8596	34289			534.1	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 3	-1.53	-73170	19437	28680.43		18344	8.864	12002	47874			2.46	Si
SLV 3	0.57	-57412	19896	-11371.01		14393	8.864	11212	44722			2.25	Si
SLV 1	-1.53	-73111	19649	29368.31		18329	8.864	11999	47862			2.44	Si
SLV 1	0.57	-57303	20104	-11002.16		14366	8.864	11207	44701			2.22	Si
SLV 4	-1.53	-73170	19437	28680.43		18344	8.864	12002	47874			2.46	Si
SLV 4	0.57	-57412	19896	-11371.01		14393	8.864	11212	44722			2.25	Si
SLV 13	-1.53	-73320	-19520	-31994.86		18381	8.864	12010	47904			2.45	Si
SLV 13	0.57	-57568	-19979	8239.3		14432	8.864	11220	44754			2.24	Si
SLV 14	-1.53	-73320	-19520	-31994.86		18381	8.864	12010	47904			2.45	Si
SLV 14	0.57	-57568	-19979	8239.3		14432	8.864	11220	44754			2.24	Si
SLV 11	-1.53	-73375	-6270	-12008.16		18395	8.864	12012	47915			7.64	Si
SLV 11	0.57	-57711	-6399	705.6		14468	8.864	11227	44782			7	Si
SLV 2	-1.53	-73111	19649	29368.31		18329	8.864	11999	47862			2.44	Si
SLV 2	0.57	-57303	20104	-11002.16		14366	8.864	11207	44701			2.22	Si
SLV 16	-1.53	-73379	-19732	-32682.75		18396	8.864	12013	47916			2.43	Si
SLV 16	0.57	-57677	-20187	7870.44		14460	8.864	11225	44775			2.22	Si
SLV 15	-1.53	-73379	-19732	-32682.75		18396	8.864	12013	47916			2.43	Si
SLV 15	0.57	-57677	-20187	7870.44		14460	8.864	11225	44775			2.22	Si
SLV 12	-1.53	-73375	-6270	-12008.16		18395	8.864	12012	47915			7.64	Si
SLV 12	0.57	-57711	-6399	705.6		14468	8.864	11227	44782			7	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota -0.23 W_a 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 6	143750	0.24	15965	-63683	508.72	12456.42	24.49	Si
SLV 5	143750	0.24	15965	-63683	508.72	12456.42	24.49	Si
SLV 2	143750	0.24	15974	-63717	508.72	12462.08	24.5	Si
SLV 1	143750	0.24	15974	-63717	508.72	12462.08	24.5	Si
SLV 9	143750	0.24	15982	-63747	508.72	12467.13	24.51	Si
SLV 10	143750	0.24	15982	-63747	508.72	12467.13	24.51	Si
SLV 4	143750	0.24	15997	-63811	508.72	12477.63	24.53	Si
SLV 3	143750	0.24	15997	-63811	508.72	12477.63	24.53	Si
SLV 14	143750	0.24	16028	-63932	508.72	12497.74	24.57	Si
SLV 13	143750	0.24	16028	-63932	508.72	12497.74	24.57	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = -0.23 $W_a = 0.08$ $T_a = 0.0251$

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 13	-52403	-73320	399	0.093	6807.8	0.94	1.44078	5.70385	No
SLV 14	-52403	-73320	399	0.093	6807.8	0.94	1.44078	5.70385	No
SLV 3	-52148	-73170	-399	0.093	6782.1	0.94	1.44152	5.70385	No
SLV 4	-52148	-73170	-399	0.093	6782.1	0.94	1.44152	5.70385	No
SLV 16	-52467	-73379	-85	0.098	6814.4	0.94	1.51911	5.70385	No
SLV 15	-52467	-73379	-85	0.098	6814.4	0.94	1.51911	5.70385	No
SLV 2	-52083	-73111	85	0.098	6775.5	0.939	1.52069	5.70385	No
SLV 1	-52083	-73111	85	0.098	6775.5	0.939	1.52069	5.70385	No
SLV 7	-52336	-73312	-854	0.086	6801.1	0.94	1.32682	2.39898	No
SLV 8	-52336	-73312	-854	0.086	6801.1	0.94	1.32682	2.39898	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	118.361	SLU 81	Si
V_SLU	508.286	SLU 81	Si
PF_SLV	8.453	SLV 15	Si
V_SLV	2.218	SLV 15	Si
PFFP_SLV	24.486	SLV 5	Si
R_SLV	0.253	SLV 13	No

Maschio 8

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.sx	a.s.dx
2.185	-13.249	1.81	-13.249	L1	L2	0.375	0.45	2.6	2.6	2.6			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 40	-1.53	-2259	-225.13	13389	354.02	1.573	Si
SLU 40	0.57	-4792	296.49	28397	585.29	1.974	Si
SLU 41	-1.53	-2259	-225.13	13389	354.02	1.573	Si
SLU 41	0.57	-4792	296.49	28397	585.29	1.974	Si
SLU 42	-1.53	-2259	-225.13	13389	354.02	1.573	Si
SLU 42	0.57	-4792	296.49	28397	585.29	1.974	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 37	-1.53	-2185	-200.03	12950	344.61	1.723	Si
SLU 37	0.57	-4368	264.7	25883	558.75	2.111	Si
SLU 83	-1.53	-2783	-247.24	16491	416.15	1.683	Si
SLU 83	0.57	-5444	327.31	32260	616.5	1.884	Si
SLU 33	-1.53	-2185	-200.03	12950	344.61	1.723	Si
SLU 33	0.57	-4368	264.7	25883	558.75	2.111	Si
SLU 39	-1.53	-2259	-225.13	13389	354.02	1.573	Si
SLU 39	0.57	-4792	296.49	28397	585.29	1.974	Si
SLU 82	-1.53	-2783	-247.24	16491	416.15	1.683	Si
SLU 82	0.57	-5444	327.31	32260	616.5	1.884	Si
SLU 81	-1.53	-2783	-247.24	16491	416.15	1.683	Si
SLU 81	0.57	-5444	327.31	32260	616.5	1.884	Si
SLU 84	-1.53	-2783	-247.24	16491	416.15	1.683	Si
SLU 84	0.57	-5444	327.31	32260	616.5	1.884	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 12	-1.53	-2371	-172.83	14049	393.42	2.276	Si
SLV 12	0.57	-3639	197.5	21562	561.85	2.845	Si
SLV 16	-1.53	-1828	-299.99	10835	312.43	1.041	Si
SLV 16	0.57	-4812	316.44	28517	691.73	2.186	Si
SLV 5	-1.53	-1574	-98.41	9328	272.62	2.77	Si
SLV 5	0.57	-2880	167.4	17064	464.52	2.775	Si
SLV 14	-1.53	-1537	-307.97	0	0	0	No, $e > l/2$
SLV 14	0.57	-4869	333.02	28855	697.4	2.094	Si
SLV 13	-1.53	-1537	-307.97	0	0	0	No, $e > l/2$
SLV 13	0.57	-4869	333.02	28855	697.4	2.094	Si
SLV 10	-1.53	-1400	-199.42	8298	244.74	1.227	Si
SLV 10	0.57	-3829	252.77	22688	584.57	2.313	Si
SLV 11	-1.53	-2371	-172.83	14049	393.42	2.276	Si
SLV 11	0.57	-3639	197.5	21562	561.85	2.845	Si
SLV 15	-1.53	-1828	-299.99	10835	312.43	1.041	Si
SLV 15	0.57	-4812	316.44	28517	691.73	2.186	Si
SLV 6	-1.53	-1574	-98.41	9328	272.62	2.77	Si
SLV 6	0.57	-2880	167.4	17064	464.52	2.775	Si
SLV 9	-1.53	-1400	-199.42	8298	244.74	1.227	Si
SLV 9	0.57	-3829	252.77	22688	584.57	2.313	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 40	-1.53	-2259	-524	-225.13		19049	0.2636	8095	960			1.83	Si
SLU 40	0.57	-4792	-543	296.49		28397	0.375	9342	1576			2.9	Si
SLU 81	-1.53	-2783	-577	-247.24		20894	0.296	8341	1111			1.93	Si
SLU 81	0.57	-5444	-598	327.31		32260	0.375	9857	1663			2.78	Si
SLU 41	-1.53	-2259	-524	-225.13		19049	0.2636	8095	960			1.83	Si
SLU 41	0.57	-4792	-543	296.49		28397	0.375	9342	1576			2.9	Si
SLU 37	-1.53	-2185	-467	-200.03		16868	0.2879	7805	1011			2.17	Si
SLU 37	0.57	-4368	-484	264.7		25883	0.375	9007	1520			3.14	Si
SLU 39	-1.53	-2259	-524	-225.13		19049	0.2636	8095	960			1.83	Si
SLU 39	0.57	-4792	-543	296.49		28397	0.375	9342	1576			2.9	Si
SLU 82	-1.53	-2783	-577	-247.24		20894	0.296	8341	1111			1.93	Si
SLU 82	0.57	-5444	-598	327.31		32260	0.375	9857	1663			2.78	Si
SLU 38	-1.53	-2185	-467	-200.03		16868	0.2879	7805	1011			2.17	Si
SLU 38	0.57	-4368	-484	264.7		25883	0.375	9007	1520			3.14	Si
SLU 42	-1.53	-2259	-524	-225.13		19049	0.2636	8095	960			1.83	Si
SLU 42	0.57	-4792	-543	296.49		28397	0.375	9342	1576			2.9	Si
SLU 84	-1.53	-2783	-577	-247.24		20894	0.296	8341	1111			1.93	Si
SLU 84	0.57	-5444	-598	327.31		32260	0.375	9857	1663			2.78	Si
SLU 83	-1.53	-2783	-577	-247.24		20894	0.296	8341	1111			1.93	Si
SLU 83	0.57	-5444	-598	327.31		32260	0.375	9857	1663			2.78	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 11	-1.53	-2371	-356	-172.83		15324	0.3438	11398	1763			4.96	Si
SLV 11	0.57	-3639	-327	197.5		21562	0.375	12646	2134			6.53	Si
SLV 15	-1.53	-1828	-619	-299.99		57805	0.0703	16250	514			0.83	No, $V_u < V$
SLV 15	0.57	-4812	-592	316.44		29280	0.3652	14189	2332			3.94	Si
SLV 14	-1.53	-1537	-654	-307.97		0	0	8333	0			0	No, $V_u < V$
SLV 14	0.57	-4869	-646	333.02		30282	0.3573	14390	2314			3.58	Si
SLV 16	-1.53	-1828	-619	-299.99		57805	0.0703	16250	514			0.83	No, $V_u < V$
SLV 16	0.57	-4812	-592	316.44		29280	0.3652	14189	2332			3.94	Si
SLV 9	-1.53	-1400	-472	-199.42		23003	0.1353	12934	787			1.67	Si
SLV 9	0.57	-3829	-508	252.77		23345	0.3644	13002	2132			4.2	Si
SLV 6	-1.53	-1574	-281	-98.41		9329	0.375	10199	1721			6.13	Si
SLV 6	0.57	-2880	-335	167.4		17064	0.375	11746	1982			5.92	Si
SLV 12	-1.53	-2371	-356	-172.83		15324	0.3438	11398	1763			4.96	Si
SLV 12	0.57	-3639	-327	197.5		21562	0.375	12646	2134			6.53	Si
SLV 13	-1.53	-1537	-654	-307.97		0	0	8333	0			0	No, $V_u < V$
SLV 13	0.57	-4869	-646	333.02		30282	0.3573	14390	2314			3.58	Si
SLV 5	-1.53	-1574	-281	-98.41		9329	0.375	10199	1721			6.13	Si
SLV 5	0.57	-2880	-335	167.4		17064	0.375	11746	1982			5.92	Si
SLV 10	-1.53	-1400	-472	-199.42		23003	0.1353	12934	787			1.67	Si
SLV 10	0.57	-3829	-508	252.77		23345	0.3644	13002	2132			4.2	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota -0.23 Wa 0.08 denominatore 8 $\gamma_M = 2$



Comb.	fd	Sa	σ0	N	M	Mc	Coeff.s.	Verifica
SLV 2	143750	0.24	11357	-1916	21.52	391.13	18.17	Si
SLV 1	143750	0.24	11357	-1916	21.52	391.13	18.17	Si
SLV 4	143750	0.24	11378	-1920	21.52	391.77	18.2	Si
SLV 3	143750	0.24	11378	-1920	21.52	391.77	18.2	Si
SLV 5	143750	0.24	16104	-2718	21.52	530.87	24.67	Si
SLV 6	143750	0.24	16104	-2718	21.52	530.87	24.67	Si
SLV 7	143750	0.24	16174	-2729	21.52	532.81	24.76	Si
SLV 8	143750	0.24	16174	-2729	21.52	532.81	24.76	Si
SLV 9	143750	0.24	20194	-3408	21.52	640.03	29.74	Si
SLV 10	143750	0.24	20194	-3408	21.52	640.03	29.74	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = -0.23 Wa = 0.08 Ta = 0.0251

Comb.	N top	N base	V orto	α0	M*	e*	a0*	aLim	Verifica
SLV 13	-2642	-1537	-2	0.097	331.1	0.946	1.49256	5.70385	No
SLV 14	-2642	-1537	-2	0.097	331.1	0.946	1.49256	5.70385	No
SLV 15	-2567	-1828	3	0.097	323.4	0.945	1.49312	5.70385	No
SLV 16	-2567	-1828	3	0.097	323.4	0.945	1.49312	5.70385	No
SLV 2	-1101	-2116	-1	0.108	175.7	0.911	1.72993	5.70385	No
SLV 1	-1101	-2116	-1	0.108	175.7	0.911	1.72993	5.70385	No
SLV 3	-1026	-2408	3	0.108	168.2	0.909	1.73174	5.70385	No
SLV 4	-1026	-2408	3	0.108	168.2	0.909	1.73174	5.70385	No
SLV 9	-2190	-1400	-7	0.097	285.3	0.939	1.50163	2.39898	No
SLV 10	-2190	-1400	-7	0.097	285.3	0.939	1.50163	2.39898	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.573	SLV 39	Si
V_SLV	1.832	SLV 39	Si
PF_SLV	0	SLV 13	No
V_SLV	0	SLV 13	No
PFFP_SLV	18.173	SLV 1	Si
R_SLV	0.262	SLV 13	No

Maschio 9

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-7.101	-8.718	-9.428	-8.718	L1	L2	2.327	0.45	2.6	2.6	2.6			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ0	fv0	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 83	0.47	-18706	-3208.92	17864	16991.41	5.295	Si
SLU 83	0.87	-18227	-3377.22	17406	16675.27	4.938	Si
SLU 82	0.47	-18706	-3208.92	17864	16991.41	5.295	Si
SLU 82	0.87	-18227	-3377.22	17406	16675.27	4.938	Si
SLU 79	0.47	-17388	-2962.35	16606	16107.05	5.437	Si
SLU 79	0.87	-16861	-3109.1	16102	15739.47	5.062	Si
SLU 76	0.47	-17388	-2962.35	16606	16107.05	5.437	Si
SLU 76	0.87	-16861	-3109.1	16102	15739.47	5.062	Si
SLU 80	0.47	-17388	-2962.35	16606	16107.05	5.437	Si
SLU 80	0.87	-16861	-3109.1	16102	15739.47	5.062	Si
SLU 78	0.47	-17388	-2962.35	16606	16107.05	5.437	Si
SLU 78	0.87	-16861	-3109.1	16102	15739.47	5.062	Si
SLU 77	0.47	-17388	-2962.35	16606	16107.05	5.437	Si
SLU 77	0.87	-16861	-3109.1	16102	15739.47	5.062	Si
SLU 75	0.47	-17388	-2962.35	16606	16107.05	5.437	Si
SLU 75	0.87	-16861	-3109.1	16102	15739.47	5.062	Si
SLU 81	0.47	-18706	-3208.92	17864	16991.41	5.295	Si
SLU 81	0.87	-18227	-3377.22	17406	16675.27	4.938	Si
SLU 84	0.47	-18706	-3208.92	17864	16991.41	5.295	Si
SLU 84	0.87	-18227	-3377.22	17406	16675.27	4.938	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γM = 2

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLV 11	0.47	-12638	-2099.11	12069	13251.7	6.313	Si
SLV 11	0.87	-11874	-2002	11339	12533.05	6.26	Si
SLV 10	0.47	-10112	-2334.36	9657	10835.84	4.642	Si
SLV 10	0.87	-9700	-2175.56	9263	10430.06	4.794	Si
SLV 12	0.47	-12638	-2099.11	12069	13251.7	6.313	Si
SLV 12	0.87	-11874	-2002	11339	12533.05	6.26	Si
SLV 14	0.47	-10694	-2930.02	10212	11402.02	3.891	Si
SLV 14	0.87	-9886	-2296.45	9441	10613.75	4.622	Si
SLV 6	0.47	-10372	-1753.22	9905	11089.47	6.325	Si
SLV 6	0.87	-10192	-2019.87	9733	10913.92	5.403	Si
SLV 16	0.47	-11451	-2859.44	10936	12130.95	4.242	Si
SLV 16	0.87	-10538	-2244.38	10064	11251.46	5.013	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 13	0.47	-10694	-2930.02	10212	11402.02	3.891	Si
SLV 13	0.87	-9886	-2296.45	9441	10613.75	4.622	Si
SLV 15	0.47	-11451	-2859.44	10936	12130.95	4.242	Si
SLV 15	0.87	-10538	-2244.38	10064	11251.46	5.013	Si
SLV 9	0.47	-10112	-2334.36	9657	10835.84	4.642	Si
SLV 9	0.87	-9700	-2175.56	9263	10430.06	4.794	Si
SLV 5	0.47	-10372	-1753.22	9905	11089.47	6.325	Si
SLV 5	0.87	-10192	-2019.87	9733	10913.92	5.403	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 41	0.47	-16267	1333	-2825.43		15535	2.327	7627	7986			5.99	Si
SLU 41	0.87	-15961	1334	-2980.04		15242	2.327	7588	7946			5.96	Si
SLU 77	0.47	-17388	1210	-2962.35		16606	2.327	7770	8136			6.72	Si
SLU 77	0.87	-16861	1210	-3109.1		16102	2.327	7702	8066			6.66	Si
SLU 75	0.47	-17388	1210	-2962.35		16606	2.327	7770	8136			6.72	Si
SLU 75	0.87	-16861	1210	-3109.1		16102	2.327	7702	8066			6.66	Si
SLU 40	0.47	-16267	1333	-2825.43		15535	2.327	7627	7986			5.99	Si
SLU 40	0.87	-15961	1334	-2980.04		15242	2.327	7588	7946			5.96	Si
SLU 42	0.47	-16267	1333	-2825.43		15535	2.327	7627	7986			5.99	Si
SLU 42	0.87	-15961	1334	-2980.04		15242	2.327	7588	7946			5.96	Si
SLU 84	0.47	-18706	1405	-3208.92		17864	2.327	7937	8312			5.91	Si
SLU 84	0.87	-18227	1406	-3377.22		17406	2.327	7876	8248			5.87	Si
SLU 81	0.47	-18706	1405	-3208.92		17864	2.327	7937	8312			5.91	Si
SLU 81	0.87	-18227	1406	-3377.22		17406	2.327	7876	8248			5.87	Si
SLU 83	0.47	-18706	1405	-3208.92		17864	2.327	7937	8312			5.91	Si
SLU 83	0.87	-18227	1406	-3377.22		17406	2.327	7876	8248			5.87	Si
SLU 39	0.47	-16267	1333	-2825.43		15535	2.327	7627	7986			5.99	Si
SLU 39	0.87	-15961	1334	-2980.04		15242	2.327	7588	7946			5.96	Si
SLU 82	0.47	-18706	1405	-3208.92		17864	2.327	7937	8312			5.91	Si
SLU 82	0.87	-18227	1406	-3377.22		17406	2.327	7876	8248			5.87	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 1	0.47	-11559	3820	-992.89		11038	2.327	10541	11038			2.89	Si
SLV 1	0.87	-11528	3615	-1777.49		11009	2.327	10535	11032			3.05	Si
SLV 4	0.47	-12316	3479	-922.31		11762	2.327	10686	11189			3.22	Si
SLV 4	0.87	-12180	3273	-1725.42		11632	2.327	10660	11162			3.41	Si
SLV 6	0.47	-10372	2128	-1753.22		9905	2.327	10314	10801			5.08	Si
SLV 6	0.87	-10192	2069	-2019.87		9733	2.327	10280	10765			5.2	Si
SLV 14	0.47	-10694	-2149	-2930.02		10212	2.327	10376	10865			5.06	Si
SLV 14	0.87	-9886	-1942	-2296.45		9441	2.327	10222	10703			5.51	Si
SLV 2	0.47	-11559	3820	-992.89		11038	2.327	10541	11038			2.89	Si
SLV 2	0.87	-11528	3615	-1777.49		11009	2.327	10535	11032			3.05	Si
SLV 15	0.47	-11451	-2489	-2859.44		10936	2.327	10520	11016			4.43	Si
SLV 15	0.87	-10538	-2284	-2244.38		10064	2.327	10346	10834			4.74	Si
SLV 3	0.47	-12316	3479	-922.31		11762	2.327	10686	11189			3.22	Si
SLV 3	0.87	-12180	3273	-1725.42		11632	2.327	10660	11162			3.41	Si
SLV 16	0.47	-11451	-2489	-2859.44		10936	2.327	10520	11016			4.43	Si
SLV 16	0.87	-10538	-2284	-2244.38		10064	2.327	10346	10834			4.74	Si
SLV 5	0.47	-10372	2128	-1753.22		9905	2.327	10314	10801			5.08	Si
SLV 5	0.87	-10192	2069	-2019.87		9733	2.327	10280	10765			5.2	Si
SLV 13	0.47	-10694	-2149	-2930.02		10212	2.327	10376	10865			5.06	Si
SLV 13	0.87	-9886	-1942	-2296.45		9441	2.327	10222	10703			5.51	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota -0.23 W_a 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 9	143750	0.24	9256	-9692	131.63	2015.48	15.31	Si
SLV 10	143750	0.24	9256	-9692	131.63	2015.48	15.31	Si
SLV 14	143750	0.24	9327	-9767	131.63	2029.75	15.42	Si
SLV 13	143750	0.24	9327	-9767	131.63	2029.75	15.42	Si
SLV 6	143750	0.24	9986	-10456	131.63	2160.41	16.41	Si
SLV 5	143750	0.24	9986	-10456	131.63	2160.41	16.41	Si
SLV 15	143750	0.24	10118	-10595	131.63	2186.52	16.61	Si
SLV 16	143750	0.24	10118	-10595	131.63	2186.52	16.61	Si
SLV 1	143750	0.24	11761	-12315	131.63	2504.18	19.02	Si
SLV 2	143750	0.24	11761	-12315	131.63	2504.18	19.02	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzaria = -0.23 $W_a = 0.08$ $T_a = 0.0251$

Comb.	N top	N base	V orto	α_0	M*	e*	α_0^*	aLim	Verifica
SLV 2	-10126	-14862	106	0.095	1420.3	0.927	1.4887	5.70385	No
SLV 1	-10126	-14862	106	0.095	1420.3	0.927	1.4887	5.70385	No
SLV 15	-9766	-12726	-105	0.095	1384.1	0.926	1.49644	5.70385	No
SLV 16	-9766	-12726	-105	0.095	1384.1	0.926	1.49644	5.70385	No
SLV 3	-10759	-16112	-21	0.101	1484.2	0.93	1.57861	5.70385	No
SLV 4	-10759	-16112	-21	0.101	1484.2	0.93	1.57861	5.70385	No
SLV 13	-9133	-11476	22	0.103	1320.4	0.923	1.62054	5.70385	No
SLV 14	-9133	-11476	22	0.103	1320.4	0.923	1.62054	5.70385	No
SLV 11	-10852	-15370	-224	0.086	1493.6	0.93	1.33858	2.39898	No
SLV 12	-10852	-15370	-224	0.086	1493.6	0.93	1.33858	2.39898	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	4.938	SLU 81	Si



Stato limite	Coeff.s.	Comb.	Verifica
V_SLU	5.867	SLU 81	Si
PF_SLV	3.891	SLV 13	Si
V_SLV	2.89	SLV 1	Si
PFFP_SLV	15.312	SLV 9	Si
R_SLV	0.261	SLV 1	No

Maschio 10

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota s.	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-1.141	-8.718	-6.101	-8.718	L1	L2	4.96	0.45	2.6	2.6	2.6			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 62	0.47	-40641	-114.93	18209	78260.68	680.95	Si
SLU 62	0.87	-38807	-97.74	17387	75700.01	774.529	Si
SLU 82	0.47	-45090	-128.56	20202	84091.28	654.078	Si
SLU 82	0.87	-43241	-109.7	19373	81733.49	745.069	Si
SLU 84	0.47	-45090	-128.56	20202	84091.28	654.078	Si
SLU 84	0.87	-43241	-109.7	19373	81733.49	745.069	Si
SLU 40	0.47	-39538	-114.86	17714	76730.92	668.038	Si
SLU 40	0.87	-38109	-98.55	17074	74699.92	757.958	Si
SLU 42	0.47	-39538	-114.86	17714	76730.92	668.038	Si
SLU 42	0.87	-38109	-98.55	17074	74699.92	757.958	Si
SLU 81	0.47	-45090	-128.56	20202	84091.28	654.078	Si
SLU 81	0.87	-43241	-109.7	19373	81733.49	745.069	Si
SLU 41	0.47	-39538	-114.86	17714	76730.92	668.038	Si
SLU 41	0.87	-38109	-98.55	17074	74699.92	757.958	Si
SLU 39	0.47	-39538	-114.86	17714	76730.92	668.038	Si
SLU 39	0.87	-38109	-98.55	17074	74699.92	757.958	Si
SLU 83	0.47	-45090	-128.56	20202	84091.28	654.078	Si
SLU 83	0.87	-43241	-109.7	19373	81733.49	745.069	Si
SLU 63	0.47	-40641	-114.93	18209	78260.68	680.95	Si
SLU 63	0.87	-38807	-97.74	17387	75700.01	774.529	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 9	0.47	-23936	-1485.83	10724	54151.18	36.445	Si
SLV 9	0.87	-22606	-1096.39	10128	51414.79	46.895	Si
SLV 14	0.47	-26199	-4442.68	11738	58732.49	13.22	Si
SLV 14	0.87	-24796	-3237.99	11109	55902.75	17.265	Si
SLV 13	0.47	-26199	-4442.68	11738	58732.49	13.22	Si
SLV 13	0.87	-24796	-3237.99	11109	55902.75	17.265	Si
SLV 10	0.47	-23936	-1485.83	10724	54151.18	36.445	Si
SLV 10	0.87	-22606	-1096.39	10128	51414.79	46.895	Si
SLV 4	0.47	-28125	4296.37	12601	62557.83	14.561	Si
SLV 4	0.87	-26689	3115.2	11957	59710.85	19.168	Si
SLV 15	0.47	-28136	-4375.55	12606	62578.85	14.302	Si
SLV 15	0.87	-26677	-3183.91	11952	59687.21	18.747	Si
SLV 16	0.47	-28136	-4375.55	12606	62578.85	14.302	Si
SLV 16	0.87	-26677	-3183.91	11952	59687.21	18.747	Si
SLV 1	0.47	-26189	4229.24	11733	58711.08	13.882	Si
SLV 1	0.87	-24808	3061.12	11115	55926.79	18.27	Si
SLV 3	0.47	-28125	4296.37	12601	62557.83	14.561	Si
SLV 3	0.87	-26689	3115.2	11957	59710.85	19.168	Si
SLV 2	0.47	-26189	4229.24	11733	58711.08	13.882	Si
SLV 2	0.87	-24808	3061.12	11115	55926.79	18.27	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 76	0.47	-41641	-51	-116.58		18656	4.96	8043	17952			349.2	Si
SLU 76	0.87	-39791	-51	-98.97		17828	4.96	7933	17706			344.38	Si
SLU 77	0.47	-41641	-51	-116.58		18656	4.96	8043	17952			349.2	Si
SLU 77	0.87	-39791	-51	-98.97		17828	4.96	7933	17706			344.38	Si
SLU 79	0.47	-41641	-51	-116.58		18656	4.96	8043	17952			349.2	Si
SLU 79	0.87	-39791	-51	-98.97		17828	4.96	7933	17706			344.38	Si
SLU 81	0.47	-45090	-54	-128.56		20202	4.96	8249	18412			337.96	Si
SLU 81	0.87	-43241	-54	-109.7		19373	4.96	8139	18165			333.41	Si
SLU 80	0.47	-41641	-51	-116.58		18656	4.96	8043	17952			349.2	Si
SLU 80	0.87	-39791	-51	-98.97		17828	4.96	7933	17706			344.38	Si
SLU 75	0.47	-41641	-51	-116.58		18656	4.96	8043	17952			349.2	Si
SLU 75	0.87	-39791	-51	-98.97		17828	4.96	7933	17706			344.38	Si
SLU 82	0.47	-45090	-54	-128.56		20202	4.96	8249	18412			337.96	Si
SLU 82	0.87	-43241	-54	-109.7		19373	4.96	8139	18165			333.41	Si
SLU 84	0.47	-45090	-54	-128.56		20202	4.96	8249	18412			337.96	Si
SLU 84	0.87	-43241	-54	-109.7		19373	4.96	8139	18165			333.41	Si
SLU 83	0.47	-45090	-54	-128.56		20202	4.96	8249	18412			337.96	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 83	0.87	-43241	-54	-109.7		19373	4.96	8139	18165			333.41	Si
SLU 78	0.47	-41641	-51	-116.58		18656	4.96	8043	17952			349.2	Si
SLU 78	0.87	-39791	-51	-98.97		17828	4.96	7933	17706			344.38	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 14	0.47	-26199	-7329	-4442.68		11738	4.96	10681	23840			3.25	Si
SLV 14	0.87	-24796	-6873	-3237.99		11109	4.96	10555	23559			3.43	Si
SLV 15	0.47	-28136	-7333	-4375.55		12606	4.96	10854	24227			3.3	Si
SLV 15	0.87	-26677	-6877	-3183.91		11952	4.96	10724	23935			3.48	Si
SLV 3	0.47	-28125	7258	4296.37		12601	4.96	10854	24225			3.34	Si
SLV 3	0.87	-26689	6802	3115.2		11957	4.96	10725	23938			3.52	Si
SLV 16	0.47	-28136	-7333	-4375.55		12606	4.96	10854	24227			3.3	Si
SLV 16	0.87	-26677	-6877	-3183.91		11952	4.96	10724	23935			3.48	Si
SLV 4	0.47	-28125	7258	4296.37		12601	4.96	10854	24225			3.34	Si
SLV 4	0.87	-26689	6802	3115.2		11957	4.96	10725	23938			3.52	Si
SLV 1	0.47	-26189	7263	4229.24		11733	4.96	10680	23838			3.28	Si
SLV 1	0.87	-24808	6807	3061.12		11115	4.96	10556	23562			3.46	Si
SLV 9	0.47	-23936	-2217	-1485.83		10724	4.96	10478	23387			10.55	Si
SLV 9	0.87	-22606	-2079	-1096.39		10128	4.96	10359	23121			11.12	Si
SLV 13	0.47	-26199	-7329	-4442.68		11738	4.96	10681	23840			3.25	Si
SLV 13	0.87	-24796	-6873	-3237.99		11109	4.96	10555	23559			3.43	Si
SLV 2	0.47	-26189	7263	4229.24		11733	4.96	10680	23838			3.28	Si
SLV 2	0.87	-24808	6807	3061.12		11115	4.96	10556	23562			3.46	Si
SLV 10	0.47	-23936	-2217	-1485.83		10724	4.96	10478	23387			10.55	Si
SLV 10	0.87	-22606	-2079	-1096.39		10128	4.96	10359	23121			11.12	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota -0.23 W_a 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 5	143750	0.24	10487	-23408	280.57	4814.71	17.16	Si
SLV 6	143750	0.24	10487	-23408	280.57	4814.71	17.16	Si
SLV 9	143750	0.24	10489	-23412	280.57	4815.43	17.16	Si
SLV 10	143750	0.24	10489	-23412	280.57	4815.43	17.16	Si
SLV 1	143750	0.24	11424	-25499	280.57	5200.84	18.54	Si
SLV 2	143750	0.24	11424	-25499	280.57	5200.84	18.54	Si
SLV 13	143750	0.24	11430	-25512	280.57	5203.19	18.55	Si
SLV 14	143750	0.24	11430	-25512	280.57	5203.19	18.55	Si
SLV 3	143750	0.24	12229	-27295	280.57	5526.75	19.7	Si
SLV 4	143750	0.24	12229	-27295	280.57	5526.75	19.7	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = -0.23 $W_a = 0.08$ $T_a = 0.0251$

Comb.	N top	N base	V orto	α_0	M*	e*	α_0^*	aLim	Verifica
SLV 9	-20546	-27853	2523	0.006	2923	0.925	0.09679	2.39898	No
SLV 10	-20546	-27853	2523	0.006	2923	0.925	0.09679	2.39898	No
SLV 5	-20547	-27847	2522	0.006	2923.1	0.925	0.0975	2.39898	No
SLV 6	-20547	-27847	2522	0.006	2923.1	0.925	0.0975	2.39898	No
SLV 8	-26720	-33590	-2566	0.02	3546.1	0.936	0.31614	2.39898	No
SLV 7	-26720	-33590	-2566	0.02	3546.1	0.936	0.31614	2.39898	No
SLV 11	-26720	-33595	-2565	0.02	3546	0.936	0.31664	2.39898	No
SLV 12	-26720	-33595	-2565	0.02	3546	0.936	0.31664	2.39898	No
SLV 3	-24561	-31573	-786	0.075	3327.8	0.933	1.17366	5.70385	No
SLV 4	-24561	-31573	-786	0.075	3327.8	0.933	1.17366	5.70385	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	654.078	SLU 81	Si
V_SLU	333.406	SLU 81	Si
PF_SLV	13.22	SLV 13	Si
V_SLV	3.253	SLV 13	Si
PFFP_SLV	17.161	SLV 5	Si
R_SLV	0.04	SLV 9	No

Maschio 11

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota s.	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
2.186	-8.719	-0.141	-8.718	L1	L2	2.327	0.45	2.6	2.6	2.6			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 84	0.47	-19030	3188.29	18173	17201.88	5.395	Si
SLU 84	0.87	-18511	3382.29	17678	16863.78	4.986	Si
SLU 41	0.47	-16544	2809.79	15799	15515.47	5.522	Si
SLU 41	0.87	-16202	2987.54	15473	15270.55	5.111	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 39	0.47	-16544	2809.79	15799	15515.47	5.522	Si
SLU 39	0.87	-16202	2987.54	15473	15270.55	5.111	Si
SLU 40	0.47	-16544	2809.79	15799	15515.47	5.522	Si
SLU 40	0.87	-16202	2987.54	15473	15270.55	5.111	Si
SLU 81	0.47	-19030	3188.29	18173	17201.88	5.395	Si
SLU 81	0.87	-18511	3382.29	17678	16863.78	4.986	Si
SLU 75	0.47	-17693	2941.23	16897	16315.94	5.547	Si
SLU 75	0.87	-17129	3111.26	16357	15927.23	5.119	Si
SLU 42	0.47	-16544	2809.79	15799	15515.47	5.522	Si
SLU 42	0.87	-16202	2987.54	15473	15270.55	5.111	Si
SLU 77	0.47	-17693	2941.23	16897	16315.94	5.547	Si
SLU 77	0.87	-17129	3111.26	16357	15927.23	5.119	Si
SLU 82	0.47	-19030	3188.29	18173	17201.88	5.395	Si
SLU 82	0.87	-18511	3382.29	17678	16863.78	4.986	Si
SLU 83	0.47	-19030	3188.29	18173	17201.88	5.395	Si
SLU 83	0.87	-18511	3382.29	17678	16863.78	4.986	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 6	0.47	-10342	2315.16	9877	11060.74	4.778	Si
SLV 6	0.87	-9914	2156.12	9468	10641.41	4.935	Si
SLV 4	0.47	-11625	2814.08	11102	12296.71	4.37	Si
SLV 4	0.87	-10699	2217.4	10218	11407.81	5.145	Si
SLV 5	0.47	-10342	2315.16	9877	11060.74	4.778	Si
SLV 5	0.87	-9914	2156.12	9468	10641.41	4.935	Si
SLV 7	0.47	-12807	2068.68	12231	13409.82	6.482	Si
SLV 7	0.87	-12019	2000.51	11478	12670.34	6.334	Si
SLV 8	0.47	-12807	2068.68	12231	13409.82	6.482	Si
SLV 8	0.87	-12019	2000.51	11478	12670.34	6.334	Si
SLV 10	0.47	-10617	1750.19	10139	11327.39	6.472	Si
SLV 10	0.87	-10414	2016.9	9945	11130.26	5.518	Si
SLV 2	0.47	-10885	2888.02	10395	11587.69	4.012	Si
SLV 2	0.87	-10068	2264.08	9615	10792.44	4.767	Si
SLV 3	0.47	-11625	2814.08	11102	12296.71	4.37	Si
SLV 3	0.87	-10699	2217.4	10218	11407.81	5.145	Si
SLV 9	0.47	-10617	1750.19	10139	11327.39	6.472	Si
SLV 9	0.87	-10414	2016.9	9945	11130.26	5.518	Si
SLV 1	0.47	-10885	2888.02	10395	11587.69	4.012	Si
SLV 1	0.87	-10068	2264.08	9615	10792.44	4.767	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 41	0.47	-16544	-1287	2809.79		15799	2.327	7662	8023			6.23	Si
SLU 41	0.87	-16202	-1287	2987.54		15473	2.327	7619	7978			6.2	Si
SLU 84	0.47	-19030	-1351	3188.29		18173	2.327	7979	8355			6.18	Si
SLU 84	0.87	-18511	-1351	3382.29		17678	2.327	7913	8286			6.13	Si
SLU 40	0.47	-16544	-1287	2809.79		15799	2.327	7662	8023			6.23	Si
SLU 40	0.87	-16202	-1287	2987.54		15473	2.327	7619	7978			6.2	Si
SLU 82	0.47	-19030	-1351	3188.29		18173	2.327	7979	8355			6.18	Si
SLU 82	0.87	-18511	-1351	3382.29		17678	2.327	7913	8286			6.13	Si
SLU 81	0.47	-19030	-1351	3188.29		18173	2.327	7979	8355			6.18	Si
SLU 81	0.87	-18511	-1351	3382.29		17678	2.327	7913	8286			6.13	Si
SLU 83	0.47	-19030	-1351	3188.29		18173	2.327	7979	8355			6.18	Si
SLU 83	0.87	-18511	-1351	3382.29		17678	2.327	7913	8286			6.13	Si
SLU 39	0.47	-16544	-1287	2809.79		15799	2.327	7662	8023			6.23	Si
SLU 39	0.87	-16202	-1287	2987.54		15473	2.327	7619	7978			6.2	Si
SLU 75	0.47	-17693	-1159	2941.23		16897	2.327	7808	8177			7.06	Si
SLU 75	0.87	-17129	-1159	3111.26		16357	2.327	7737	8101			6.99	Si
SLU 77	0.47	-17693	-1159	2941.23		16897	2.327	7808	8177			7.06	Si
SLU 77	0.87	-17129	-1159	3111.26		16357	2.327	7737	8101			6.99	Si
SLU 42	0.47	-16544	-1287	2809.79		15799	2.327	7662	8023			6.23	Si
SLU 42	0.87	-16202	-1287	2987.54		15473	2.327	7619	7978			6.2	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 9	0.47	-10617	-2026	1750.19		10139	2.327	10361	10850			5.35	Si
SLV 9	0.87	-10414	-2005	2016.9		9945	2.327	10322	10809			5.39	Si
SLV 2	0.47	-10885	2185	2888.02		10395	2.327	10412	10903			4.99	Si
SLV 2	0.87	-10068	1969	2264.08		9615	2.327	10256	10740			5.45	Si
SLV 10	0.47	-10617	-2026	1750.19		10139	2.327	10361	10850			5.35	Si
SLV 10	0.87	-10414	-2005	2016.9		9945	2.327	10322	10809			5.39	Si
SLV 13	0.47	-11799	-3749	1004.79		11268	2.327	10587	11086			2.96	Si
SLV 13	0.87	-11733	-3557	1800.01		11205	2.327	10574	11073			3.11	Si
SLV 14	0.47	-11799	-3749	1004.79		11268	2.327	10587	11086			2.96	Si
SLV 14	0.87	-11733	-3557	1800.01		11205	2.327	10574	11073			3.11	Si
SLV 4	0.47	-11625	2489	2814.08		11102	2.327	10554	11051			4.44	Si
SLV 4	0.87	-10699	2297	2217.4		10218	2.327	10377	10866			4.73	Si
SLV 16	0.47	-12539	-3446	930.84		11974	2.327	10728	11234			3.26	Si
SLV 16	0.87	-12365	-3230	1753.33		11808	2.327	10695	11199			3.47	Si
SLV 3	0.47	-11625	2489	2814.08		11102	2.327	10554	11051			4.44	Si
SLV 3	0.87	-10699	2297	2217.4		10218	2.327	10377	10866			4.73	Si
SLV 1	0.47	-10885	2185	2888.02		10395	2.327	10412	10903			4.99	Si
SLV 1	0.87	-10068	1969	2264.08		9615	2.327	10256	10740			5.45	Si
SLV 15	0.47	-12539	-3446	930.84		11974	2.327	10728	11234			3.26	Si
SLV 15	0.87	-12365	-3230	1753.33		11808	2.327	10695	11199			3.47	Si



Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota -0.23 Wa 0.08 denominatore 8 $\gamma M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 6	143750	0.24	9482	-9929	131.63	2060.72	15.66	Si
SLV 5	143750	0.24	9482	-9929	131.63	2060.72	15.66	Si
SLV 2	143750	0.24	9524	-9973	131.63	2069.08	15.72	Si
SLV 1	143750	0.24	9524	-9973	131.63	2069.08	15.72	Si
SLV 10	143750	0.24	10232	-10714	131.63	2208.87	16.78	Si
SLV 9	143750	0.24	10232	-10714	131.63	2208.87	16.78	Si
SLV 4	143750	0.24	10310	-10796	131.63	2224.16	16.9	Si
SLV 3	143750	0.24	10310	-10796	131.63	2224.16	16.9	Si
SLV 14	143750	0.24	12023	-12590	131.63	2554.07	19.4	Si
SLV 13	143750	0.24	12023	-12590	131.63	2554.07	19.4	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = -0.23 Wa = 0.08 Ta = 0.0251

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 14	-10327	-15451	112	0.094	1440.6	0.928	1.47763	5.70385	No
SLV 13	-10327	-15451	112	0.094	1440.6	0.928	1.47763	5.70385	No
SLV 4	-9913	-12673	-111	0.095	1398.9	0.926	1.48571	5.70385	No
SLV 3	-9913	-12673	-111	0.095	1398.9	0.926	1.48571	5.70385	No
SLV 16	-10940	-16744	-24	0.101	1502.4	0.93	1.57141	5.70385	No
SLV 15	-10940	-16744	-24	0.101	1502.4	0.93	1.57141	5.70385	No
SLV 2	-9300	-11380	25	0.102	1337.2	0.924	1.61229	5.70385	No
SLV 1	-9300	-11380	25	0.102	1337.2	0.924	1.61229	5.70385	No
SLV 7	-10988	-15606	-239	0.085	1507.2	0.931	1.32016	2.39898	No
SLV 8	-10988	-15606	-239	0.085	1507.2	0.931	1.32016	2.39898	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	4.986	SLU 81	Si
V_SLU	6.132	SLU 81	Si
PF_SLV	4.012	SLV 1	Si
V_SLV	2.957	SLV 13	Si
PFFP_SLV	15.655	SLV 5	Si
R_SLV	0.259	SLV 13	No

Maschio 12

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s,sx	a.s,dx
2.185	-17.729	2.185	-12.974	L1	L2	4.755	0.45	2.6	2.6	2.6			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 70	-1.53	-37358	3961.91	17459	69781.73	17.613	Si
SLU 70	0.57	-23435	3494.84	10952	48225.52	13.799	Si
SLU 67	-1.53	-37358	3961.91	17459	69781.73	17.613	Si
SLU 67	0.57	-23435	3494.84	10952	48225.52	13.799	Si
SLU 72	-1.53	-37358	3961.91	17459	69781.73	17.613	Si
SLU 72	0.57	-23435	3494.84	10952	48225.52	13.799	Si
SLU 44	-1.53	-34552	3330	16148	65863.36	19.779	Si
SLU 44	0.57	-21373	3206.98	9988	44583.03	13.902	Si
SLU 71	-1.53	-37358	3961.91	17459	69781.73	17.613	Si
SLU 71	0.57	-23435	3494.84	10952	48225.52	13.799	Si
SLU 65	-1.53	-37358	3961.91	17459	69781.73	17.613	Si
SLU 65	0.57	-23435	3494.84	10952	48225.52	13.799	Si
SLU 66	-1.53	-37358	3961.91	17459	69781.73	17.613	Si
SLU 66	0.57	-23435	3494.84	10952	48225.52	13.799	Si
SLU 64	-1.53	-37358	3961.91	17459	69781.73	17.613	Si
SLU 64	0.57	-23435	3494.84	10952	48225.52	13.799	Si
SLU 69	-1.53	-37358	3961.91	17459	69781.73	17.613	Si
SLU 69	0.57	-23435	3494.84	10952	48225.52	13.799	Si
SLU 68	-1.53	-37358	3961.91	17459	69781.73	17.613	Si
SLU 68	0.57	-23435	3494.84	10952	48225.52	13.799	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 1	-1.53	-21982	-1470.79	10273	47868.72	32.546	Si
SLV 1	0.57	-13335	3154.29	6232	30087.99	9.539	Si
SLV 4	-1.53	-21257	3129.2	9934	46428.82	14.837	Si
SLV 4	0.57	-12199	3212.25	5701	27649.03	8.607	Si
SLV 15	-1.53	-36935	7891.68	17262	75408.48	9.555	Si
SLV 15	0.57	-23844	2312.41	11143	51519.27	22.279	Si
SLV 11	-1.53	-30601	11591.46	14301	64239.07	5.542	Si
SLV 11	0.57	-18442	2694.98	8619	40752.67	15.122	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 7	-1.53	-25898	10162.72	12103	55472.75	5.458	Si
SLV 7	0.57	-14948	2964.93	6986	33507.32	11.301	Si
SLV 12	-1.53	-30601	11591.46	14301	64239.07	5.542	Si
SLV 12	0.57	-18442	2694.98	8619	40752.67	15.122	Si
SLV 3	-1.53	-21257	3129.2	9934	46428.82	14.837	Si
SLV 3	0.57	-12199	3212.25	5701	27649.03	8.607	Si
SLV 16	-1.53	-36935	7891.68	17262	75408.48	9.555	Si
SLV 16	0.57	-23844	2312.41	11143	51519.27	22.279	Si
SLV 2	-1.53	-21982	-1470.79	10273	47868.72	32.546	Si
SLV 2	0.57	-13335	3154.29	6232	30087.99	9.539	Si
SLV 8	-1.53	-25898	10162.72	12103	55472.75	5.458	Si
SLV 8	0.57	-14948	2964.93	6986	33507.32	11.301	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 84	-1.53	-44052	-1689	5470.42		20587	4.755	8301	17761			10.51	Si
SLU 84	0.57	-28515	-1694	4036.22		13327	4.755	7332	15690			9.26	Si
SLU 82	-1.53	-44052	-1689	5470.42		20587	4.755	8301	17761			10.51	Si
SLU 82	0.57	-28515	-1694	4036.22		13327	4.755	7332	15690			9.26	Si
SLU 83	-1.53	-44052	-1689	5470.42		20587	4.755	8301	17761			10.51	Si
SLU 83	0.57	-28515	-1694	4036.22		13327	4.755	7332	15690			9.26	Si
SLU 76	-1.53	-42043	-1629	5017.87		19649	4.755	8175	17493			10.74	Si
SLU 76	0.57	-26991	-1633	3873.81		12614	4.755	7237	15486			9.48	Si
SLU 75	-1.53	-42043	-1629	5017.87		19649	4.755	8175	17493			10.74	Si
SLU 75	0.57	-26991	-1633	3873.81		12614	4.755	7237	15486			9.48	Si
SLU 78	-1.53	-42043	-1629	5017.87		19649	4.755	8175	17493			10.74	Si
SLU 78	0.57	-26991	-1633	3873.81		12614	4.755	7237	15486			9.48	Si
SLU 80	-1.53	-42043	-1629	5017.87		19649	4.755	8175	17493			10.74	Si
SLU 80	0.57	-26991	-1633	3873.81		12614	4.755	7237	15486			9.48	Si
SLU 81	-1.53	-44052	-1689	5470.42		20587	4.755	8301	17761			10.51	Si
SLU 81	0.57	-28515	-1694	4036.22		13327	4.755	7332	15690			9.26	Si
SLU 79	-1.53	-42043	-1629	5017.87		19649	4.755	8175	17493			10.74	Si
SLU 79	0.57	-26991	-1633	3873.81		12614	4.755	7237	15486			9.48	Si
SLU 77	-1.53	-42043	-1629	5017.87		19649	4.755	8175	17493			10.74	Si
SLU 77	0.57	-26991	-1633	3873.81		12614	4.755	7237	15486			9.48	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 8	-1.53	-25898	4600	10162.72		12103	4.755	10754	23011			5	Si
SLV 8	0.57	-14948	3986	2964.93		6986	4.755	9731	20821			5.22	Si
SLV 7	-1.53	-25898	4600	10162.72		12103	4.755	10754	23011			5	Si
SLV 7	0.57	-14948	3986	2964.93		6986	4.755	9731	20821			5.22	Si
SLV 10	-1.53	-33020	-6923	-3741.83		15432	4.755	11420	24435			3.53	Si
SLV 10	0.57	-22231	-6314	2501.77		10390	4.755	10411	22278			3.53	Si
SLV 12	-1.53	-30601	4594	11591.46		14301	4.755	11194	23952			5.21	Si
SLV 12	0.57	-18442	4004	2694.98		8619	4.755	10057	21520			5.37	Si
SLV 2	-1.53	-21982	-2878	-1470.79		10273	4.755	10388	22228			7.72	Si
SLV 2	0.57	-13335	-2743	3154.29		6232	4.755	9580	20498			7.47	Si
SLV 6	-1.53	-28316	-6916	-5170.57		13234	4.755	10980	23495			3.4	Si
SLV 6	0.57	-18738	-6333	2771.72		8757	4.755	10085	21579			3.41	Si
SLV 5	-1.53	-28316	-6916	-5170.57		13234	4.755	10980	23495			3.4	Si
SLV 5	0.57	-18738	-6333	2771.72		8757	4.755	10085	21579			3.41	Si
SLV 11	-1.53	-30601	4594	11591.46		14301	4.755	11194	23952			5.21	Si
SLV 11	0.57	-18442	4004	2694.98		8619	4.755	10057	21520			5.37	Si
SLV 9	-1.53	-33020	-6923	-3741.83		15432	4.755	11420	24435			3.53	Si
SLV 9	0.57	-22231	-6314	2501.77		10390	4.755	10411	22278			3.53	Si
SLV 1	-1.53	-21982	-2878	-1470.79		10273	4.755	10388	22228			7.72	Si
SLV 1	0.57	-13335	-2743	3154.29		6232	4.755	9580	20498			7.47	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota -0.23 Wa 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ0	N	M	Mc	Coeff.s.	Verifica
SLV 4	143750	0.24	7385	-15802	272.9	3340.59	12.24	Si
SLV 3	143750	0.24	7385	-15802	272.9	3340.59	12.24	Si
SLV 2	143750	0.24	7871	-16842	272.9	3545.39	12.99	Si
SLV 1	143750	0.24	7871	-16842	272.9	3545.39	12.99	Si
SLV 8	143750	0.24	8875	-18991	272.9	3962.58	14.52	Si
SLV 7	143750	0.24	8875	-18991	272.9	3962.58	14.52	Si
SLV 5	143750	0.24	10496	-22458	272.9	4618.98	16.93	Si
SLV 6	143750	0.24	10496	-22458	272.9	4618.98	16.93	Si
SLV 12	143750	0.24	10639	-22764	272.9	4675.98	17.13	Si
SLV 11	143750	0.24	10639	-22764	272.9	4675.98	17.13	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = -0.23 Wa = 0.08 Ta = 0.0251

Comb.	N top	N base	V orto	α_0	M*	e*	α_0^*	aLim	Verifica
SLV 14	-22003	-37661	-20	0.102	3034.6	0.93	1.59183	5.70385	No
SLV 13	-22003	-37661	-20	0.102	3034.6	0.93	1.59183	5.70385	No
SLV 16	-21036	-36935	-15	0.103	2937.1	0.928	1.6072	5.70385	No
SLV 15	-21036	-36935	-15	0.103	2937.1	0.928	1.6072	5.70385	No
SLV 1	-10679	-21982	21	0.113	1902.7	0.902	1.81778	5.70385	No
SLV 2	-10679	-21982	21	0.113	1902.7	0.902	1.81778	5.70385	No
SLV 3	-9712	-21257	27	0.114	1807.9	0.899	1.84551	5.70385	No
SLV 4	-9712	-21257	27	0.114	1807.9	0.899	1.84551	5.70385	No
SLV 10	-19168	-33020	-12	0.104	2749	0.924	1.63502	2.39898	No
SLV 9	-19168	-33020	-12	0.104	2749	0.924	1.63502	2.39898	No



Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	13.799	SLU 64	Si
V_SLU	9.262	SLU 81	Si
PF_SLV	5.458	SLV 7	Si
V_SLV	3.397	SLV 5	Si
PFFP_SLV	12.241	SLV 3	Si
R_SLV	0.279	SLV 13	No

Maschio 13

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
2.185	-12.024	2.186	-8.719	L1	L2	3.305	0.45	2.6	2.6	2.6			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	$\tau 0$	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma 0$	Mu	c.s.	Verifica
SLU 44	-1.53	-23142	1283.42	15560	30936.95	24.105	Si
SLU 44	0.57	-15171	-2286.01	10201	21930.3	9.593	Si
SLU 46	-1.53	-23142	1283.42	15560	30936.95	24.105	Si
SLU 46	0.57	-15171	-2286.01	10201	21930.3	9.593	Si
SLU 51	-1.53	-23142	1283.42	15560	30936.95	24.105	Si
SLU 51	0.57	-15171	-2286.01	10201	21930.3	9.593	Si
SLU 45	-1.53	-23142	1283.42	15560	30936.95	24.105	Si
SLU 45	0.57	-15171	-2286.01	10201	21930.3	9.593	Si
SLU 43	-1.53	-23142	1283.42	15560	30936.95	24.105	Si
SLU 43	0.57	-15171	-2286.01	10201	21930.3	9.593	Si
SLU 48	-1.53	-23142	1283.42	15560	30936.95	24.105	Si
SLU 48	0.57	-15171	-2286.01	10201	21930.3	9.593	Si
SLU 50	-1.53	-23142	1283.42	15560	30936.95	24.105	Si
SLU 50	0.57	-15171	-2286.01	10201	21930.3	9.593	Si
SLU 49	-1.53	-23142	1283.42	15560	30936.95	24.105	Si
SLU 49	0.57	-15171	-2286.01	10201	21930.3	9.593	Si
SLU 47	-1.53	-23142	1283.42	15560	30936.95	24.105	Si
SLU 47	0.57	-15171	-2286.01	10201	21930.3	9.593	Si
SLU 64	-1.53	-24798	1566.81	16674	32591.21	20.801	Si
SLU 64	0.57	-16587	-2463.17	11153	23656.84	9.604	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma 0$	Mu	c.s.	Verifica
SLV 16	-1.53	-23646	3999.17	15899	33990.39	8.499	Si
SLV 16	0.57	-17120	-2704.75	11511	25625.08	9.474	Si
SLV 8	-1.53	-18827	5783.82	12659	27888.87	4.822	Si
SLV 8	0.57	-13791	-2627.73	9273	21060.24	8.015	Si
SLV 7	-1.53	-18827	5783.82	12659	27888.87	4.822	Si
SLV 7	0.57	-13791	-2627.73	9273	21060.24	8.015	Si
SLV 6	-1.53	-17773	-3927.96	11950	26497.45	6.746	Si
SLV 6	0.57	-10425	-908.49	7009	16238.35	17.874	Si
SLV 5	-1.53	-17773	-3927.96	11950	26497.45	6.746	Si
SLV 5	0.57	-10425	-908.49	7009	16238.35	17.874	Si
SLV 15	-1.53	-23646	3999.17	15899	33990.39	8.499	Si
SLV 15	0.57	-17120	-2704.75	11511	25625.08	9.474	Si
SLV 12	-1.53	-21222	6528.96	14269	30973.41	4.744	Si
SLV 12	0.57	-15871	-2941	10671	23936.52	8.139	Si
SLV 11	-1.53	-21222	6528.96	14269	30973.41	4.744	Si
SLV 11	0.57	-15871	-2941	10671	23936.52	8.139	Si
SLV 10	-1.53	-20167	-3182.82	13560	29627.89	9.309	Si
SLV 10	0.57	-12505	-1221.76	8408	19241.99	15.749	Si
SLV 9	-1.53	-20167	-3182.82	13560	29627.89	9.309	Si
SLV 9	0.57	-12505	-1221.76	8408	19241.99	15.749	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma 0$	σN	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 79	-1.53	-27548	1624	2118.23		18523	3.305	8025	11936			7.35	Si
SLU 79	0.57	-19037	1634	-2704.44		12800	3.305	7262	10801			6.61	Si
SLU 82	-1.53	-28727	1684	2354.55		19315	3.305	8131	12093			7.18	Si
SLU 82	0.57	-20087	1695	-2807.84		13506	3.305	7356	10941			6.45	Si
SLU 78	-1.53	-27548	1624	2118.23		18523	3.305	8025	11936			7.35	Si
SLU 78	0.57	-19037	1634	-2704.44		12800	3.305	7262	10801			6.61	Si
SLU 83	-1.53	-28727	1684	2354.55		19315	3.305	8131	12093			7.18	Si
SLU 83	0.57	-20087	1695	-2807.84		13506	3.305	7356	10941			6.45	Si
SLU 84	-1.53	-28727	1684	2354.55		19315	3.305	8131	12093			7.18	Si
SLU 84	0.57	-20087	1695	-2807.84		13506	3.305	7356	10941			6.45	Si
SLU 81	-1.53	-28727	1684	2354.55		19315	3.305	8131	12093			7.18	Si
SLU 81	0.57	-20087	1695	-2807.84		13506	3.305	7356	10941			6.45	Si
SLU 76	-1.53	-27548	1624	2118.23		18523	3.305	8025	11936			7.35	Si
SLU 76	0.57	-19037	1634	-2704.44		12800	3.305	7262	10801			6.61	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 77	-1.53	-27548	1624	2118.23		18523	3.305	8025	11936			7.35	Si
SLU 77	0.57	-19037	1634	-2704.44		12800	3.305	7262	10801			6.61	Si
SLU 80	-1.53	-27548	1624	2118.23		18523	3.305	8025	11936			7.35	Si
SLU 80	0.57	-19037	1634	-2704.44		12800	3.305	7262	10801			6.61	Si
SLU 75	-1.53	-27548	1624	2118.23		18523	3.305	8025	11936			7.35	Si
SLU 75	0.57	-19037	1634	-2704.44		12800	3.305	7262	10801			6.61	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 12	-1.53	-21222	5025	6528.96		14269	3.305	11187	16638			3.31	Si
SLV 12	0.57	-15871	4607	-2941		10671	3.305	10468	15568			3.38	Si
SLV 3	-1.53	-15665	2117	1515.37		10533	3.305	10440	15527			7.33	Si
SLV 3	0.57	-10186	2124	-1660.51		6849	3.305	9703	14431			6.79	Si
SLV 10	-1.53	-20167	-2598	-3182.82		13560	3.305	11045	16427			6.32	Si
SLV 10	0.57	-12505	-2236	-1221.76		8408	3.305	10015	14895			6.66	Si
SLV 11	-1.53	-21222	5025	6528.96		14269	3.305	11187	16638			3.31	Si
SLV 11	0.57	-15871	4607	-2941		10671	3.305	10468	15568			3.38	Si
SLV 6	-1.53	-17773	-2709	-3927.96		11950	3.305	10723	15948			5.89	Si
SLV 6	0.57	-10425	-2276	-908.49		7009	3.305	9735	14479			6.36	Si
SLV 5	-1.53	-17773	-2709	-3927.96		11950	3.305	10723	15948			5.89	Si
SLV 5	0.57	-10425	-2276	-908.49		7009	3.305	9735	14479			6.36	Si
SLV 9	-1.53	-20167	-2598	-3182.82		13560	3.305	11045	16427			6.32	Si
SLV 9	0.57	-12505	-2236	-1221.76		8408	3.305	10015	14895			6.66	Si
SLV 8	-1.53	-18827	4914	5783.82		12659	3.305	10865	16159			3.29	Si
SLV 8	0.57	-13791	4567	-2627.73		9273	3.305	10188	15152			3.32	Si
SLV 7	-1.53	-18827	4914	5783.82		12659	3.305	10865	16159			3.29	Si
SLV 7	0.57	-13791	4567	-2627.73		9273	3.305	10188	15152			3.32	Si
SLV 4	-1.53	-15665	2117	1515.37		10533	3.305	10440	15527			7.33	Si
SLV 4	0.57	-10186	2124	-1660.51		6849	3.305	9703	14431			6.79	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota -0.23 Wa 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 2	143750	0.24	7840	-11660	189.68	2455.23	12.94	Si
SLV 1	143750	0.24	7840	-11660	189.68	2455.23	12.94	Si
SLV 3	143750	0.24	8372	-12451	189.68	2609.56	13.76	Si
SLV 4	143750	0.24	8372	-12451	189.68	2609.56	13.76	Si
SLV 6	143750	0.24	8912	-13254	189.68	2764.73	14.58	Si
SLV 5	143750	0.24	8912	-13254	189.68	2764.73	14.58	Si
SLV 10	143750	0.24	10363	-15412	189.68	3173.55	16.73	Si
SLV 9	143750	0.24	10363	-15412	189.68	3173.55	16.73	Si
SLV 8	143750	0.24	10685	-15891	189.68	3262.76	17.2	Si
SLV 7	143750	0.24	10685	-15891	189.68	3262.76	17.2	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = -0.23 Wa = 0.08 Ta = 0.0251

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 15	-14060	-23646	-15	0.103	1984.9	0.926	1.61353	5.70385	No
SLV 16	-14060	-23646	-15	0.103	1984.9	0.926	1.61353	5.70385	No
SLV 13	-13304	-23330	-3	0.104	1908.8	0.924	1.64038	5.70385	No
SLV 14	-13304	-23330	-3	0.104	1908.8	0.924	1.64038	5.70385	No
SLV 3	-8123	-15665	5	0.112	1391.5	0.905	1.8002	5.70385	No
SLV 4	-8123	-15665	5	0.112	1391.5	0.905	1.8002	5.70385	No
SLV 1	-7368	-15349	17	0.113	1317.1	0.902	1.81735	5.70385	No
SLV 2	-7368	-15349	17	0.113	1317.1	0.902	1.81735	5.70385	No
SLV 11	-12863	-21222	-22	0.104	1864.5	0.923	1.63178	2.39898	No
SLV 12	-12863	-21222	-22	0.104	1864.5	0.923	1.63178	2.39898	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	9.593	SLU 43	Si
V_SLU	6.453	SLU 81	Si
PF_SLV	4.744	SLV 11	Si
V_SLV	3.288	SLV 7	Si
PFFP_SLV	12.944	SLV 1	Si
R_SLV	0.283	SLV 15	No

Maschio 14

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-9.429	-17.728	-9.428	-8.718	L2	L3	9.01	0.3	3.92	3.92	3.92			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	32000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 19	1.07	-32256	-1554.15	11933	124025.99	79.803	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 19	4.99	-996	70.56	368	4466.41	63.303	Si
SLU 40	1.07	-35177	-1788.08	13014	133155.67	74.468	Si
SLU 40	4.99	-1214	86.69	449	5437.4	62.72	Si
SLU 21	1.07	-32256	-1554.15	11933	124025.99	79.803	Si
SLU 21	4.99	-996	70.56	368	4466.41	63.303	Si
SLU 82	1.07	-41601	-1952.75	15391	152003.7	77.841	Si
SLU 82	4.99	-1237	86.14	458	5542.19	64.341	Si
SLU 39	1.07	-35177	-1788.08	13014	133155.67	74.468	Si
SLU 39	4.99	-1214	86.69	449	5437.4	62.72	Si
SLU 41	1.07	-35177	-1788.08	13014	133155.67	74.468	Si
SLU 41	4.99	-1214	86.69	449	5437.4	62.72	Si
SLU 42	1.07	-35177	-1788.08	13014	133155.67	74.468	Si
SLU 42	4.99	-1214	86.69	449	5437.4	62.72	Si
SLU 20	1.07	-32256	-1554.15	11933	124025.99	79.803	Si
SLU 20	4.99	-996	70.56	368	4466.41	63.303	Si
SLU 18	1.07	-32256	-1554.15	11933	124025.99	79.803	Si
SLU 18	4.99	-996	70.56	368	4466.41	63.303	Si
SLU 81	1.07	-41601	-1952.75	15391	152003.7	77.841	Si
SLU 81	4.99	-1237	86.14	458	5542.19	64.341	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 10	1.07	-24560	-7733.89	9086	102413.95	13.242	Si
SLV 10	4.99	-446	516.03	165	2006.49	3.888	Si
SLV 15	1.07	-18402	4572.66	6808	78281.45	17.119	Si
SLV 15	4.99	-259	-178.4	96	1166.49	6.539	Si
SLV 7	1.07	-29614	5672.57	10956	121449.38	21.41	Si
SLV 7	4.99	-600	-452.04	222	2699.73	5.972	Si
SLV 6	1.07	-29758	-9711.33	11009	121980.15	12.561	Si
SLV 6	4.99	-604	551.91	223	2716.43	4.922	Si
SLV 12	1.07	-24416	7650.01	9033	101862.82	13.315	Si
SLV 12	4.99	-442	-487.92	164	1989.78	4.078	Si
SLV 16	1.07	-18402	4572.66	6808	78281.45	17.119	Si
SLV 16	4.99	-259	-178.4	96	1166.49	6.539	Si
SLV 11	1.07	-24416	7650.01	9033	101862.82	13.315	Si
SLV 11	4.99	-442	-487.92	164	1989.78	4.078	Si
SLV 5	1.07	-29758	-9711.33	11009	121980.15	12.561	Si
SLV 5	4.99	-604	551.91	223	2716.43	4.922	Si
SLV 8	1.07	-29614	5672.57	10956	121449.38	21.41	Si
SLV 8	4.99	-600	-452.04	222	2699.73	5.972	Si
SLV 9	1.07	-24560	-7733.89	9086	102413.95	13.242	Si
SLV 9	4.99	-446	516.03	165	2006.49	3.888	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLU 59	1.07	-36429	0	-1497.44		13477	9.01	7353	19874			1000	Si
SLU 59	4.99	-819	0	53.81		303	9.01	5596	15126			1000	Si
SLU 61	1.07	-38680	0	-1718.81		14310	9.01	7464	20174			1000	Si
SLU 61	4.99	-1019	0	70		377	9.01	5606	15153			1000	Si
SLU 60	1.07	-38680	0	-1718.81		14310	9.01	7464	20174			1000	Si
SLU 60	4.99	-1019	0	70		377	9.01	5606	15153			1000	Si
SLU 58	1.07	-36429	0	-1497.44		13477	9.01	7353	19874			1000	Si
SLU 58	4.99	-819	0	53.81		303	9.01	5596	15126			1000	Si
SLU 1	1.07	-24751	0	-816.24		9157	9.01	6776	18317			1000	Si
SLU 1	4.99	-327	0	16.59		121	9.01	5572	15060			1000	Si
SLU 55	1.07	-36429	0	-1497.44		13477	9.01	7353	19874			1000	Si
SLU 55	4.99	-819	0	53.81		303	9.01	5596	15126			1000	Si
SLU 53	1.07	-36429	0	-1497.44		13477	9.01	7353	19874			1000	Si
SLU 53	4.99	-819	0	53.81		303	9.01	5596	15126			1000	Si
SLU 56	1.07	-36429	0	-1497.44		13477	9.01	7353	19874			1000	Si
SLU 56	4.99	-819	0	53.81		303	9.01	5596	15126			1000	Si
SLU 57	1.07	-36429	0	-1497.44		13477	9.01	7353	19874			1000	Si
SLU 57	4.99	-819	0	53.81		303	9.01	5596	15126			1000	Si
SLU 54	1.07	-36429	0	-1497.44		13477	9.01	7353	19874			1000	Si
SLU 54	4.99	-819	0	53.81		303	9.01	5596	15126			1000	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLV 13	1.07	-18445	-2084	-42.51		6824	9.01	9698	26214			12.58	Si
SLV 13	4.99	-260	-316	122.78		96	9.01	8353	22577			71.55	Si
SLV 6	1.07	-29758	-6345	-9711.33		11009	9.01	10535	28477			4.49	Si
SLV 6	4.99	-604	-933	551.91		223	9.01	8378	22646			24.26	Si
SLV 12	1.07	-24416	6345	7650.01		9033	9.01	10140	27408			4.32	Si
SLV 12	4.99	-442	933	-487.92		164	9.01	8366	22613			24.23	Si
SLV 5	1.07	-29758	-6345	-9711.33		11009	9.01	10535	28477			4.49	Si
SLV 5	4.99	-604	-933	551.91		223	9.01	8378	22646			24.26	Si
SLV 9	1.07	-24560	-6444	-7733.89		9086	9.01	10151	27437			4.26	Si
SLV 9	4.99	-446	-953	516.03		165	9.01	8366	22614			23.73	Si
SLV 7	1.07	-29614	6444	5672.57		10956	9.01	10525	28448			4.41	Si
SLV 7	4.99	-600	953	-452.04		222	9.01	8378	22645			23.76	Si
SLV 10	1.07	-24560	-6444	-7733.89		9086	9.01	10151	27437			4.26	Si
SLV 10	4.99	-446	-953	516.03		165	9.01	8366	22614			23.73	Si
SLV 8	1.07	-29614	6444	5672.57		10956	9.01	10525	28448			4.41	Si
SLV 8	4.99	-600	953	-452.04		222	9.01	8378	22645			23.76	Si
SLV 14	1.07	-18445	-2084	-42.51		6824	9.01	9698	26214			12.58	Si
SLV 14	4.99	-260	-316	122.78		96	9.01	8353	22577			71.55	Si
SLV 11	1.07	-24416	6345	7650.01		9033	9.01	10140	27408			4.32	Si
SLV 11	4.99	-442	933	-487.92		164	9.01	8366	22613			24.23	Si



Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.03 Wa 0.05 denominatore 8 γM = 2

Comb.	fd	Sa	σ0	N	M	Mc	Coeff.s.	Verifica
SLV 15	143750	0.47	0	-9644	1518.92	0	0	No, e>t/2
SLV 14	143750	0.47	0	-9667	1518.92	0	0	No, e>t/2
SLV 16	143750	0.47	0	-9644	1518.92	0	0	No, e>t/2
SLV 13	143750	0.47	0	-9667	1518.92	0	0	No, e>t/2
SLV 12	143750	0.47	4390	-11867	1518.92	1716.11	1.13	Si
SLV 11	143750	0.47	4390	-11867	1518.92	1716.11	1.13	Si
SLV 9	143750	0.47	4418	-11943	1518.92	1726.62	1.14	Si
SLV 10	143750	0.47	4418	-11943	1518.92	1726.62	1.14	Si
SLV 7	143750	0.47	5104	-13795	1518.92	1982.85	1.31	Si
SLV 8	143750	0.47	5104	-13795	1518.92	1982.85	1.31	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.03 Wa = 0.05 Ta = 0.0855

Comb.	N top	N base	V orto	α0	M*	e*	a0*	aLim	Verifica
SLV 3	-786	-35729	-71	0.067	1955.5	0.966	1.00356	19.26035	No
SLV 4	-786	-35729	-71	0.067	1955.5	0.966	1.00356	19.26035	No
SLV 2	-787	-35772	-70	0.067	1955.5	0.966	1.00562	19.26035	No
SLV 1	-787	-35772	-70	0.067	1955.5	0.966	1.00562	19.26035	No
SLV 13	-260	-18445	70	0.068	1945.5	0.987	1.00576	19.26035	No
SLV 14	-260	-18445	70	0.068	1945.5	0.987	1.00576	19.26035	No
SLV 15	-259	-18402	69	0.068	1945.5	0.987	1.00789	19.26035	No
SLV 16	-259	-18402	69	0.068	1945.5	0.987	1.00789	19.26035	No
SLV 8	-600	-29614	-24	0.072	1951	0.973	1.07423	4.54431	No
SLV 7	-600	-29614	-24	0.072	1951	0.973	1.07423	4.54431	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	62.72	SLU 39	Si
V_SLU	1000	SLU 1	Si
PF_SLV	3.888	SLV 9	Si
V_SLV	4.257	SLV 9	Si
PFFP_SLV	0	SLV 13	No
R_SLV	0.052	SLV 3	No

Maschio 15

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-4.725	-13.248	-9.429	-13.248	L2	L3	4.704	0.3	3.92	3.92	3.92			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ0	fv0	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 38	1.07	-20672	-13850.9	14649	39876.94	2.879	Si
SLU 38	3.17	-19510	-5708.69	13825	38098.94	6.674	Si
SLU 40	1.07	-23104	-15755.81	16372	43418.31	2.756	Si
SLU 40	3.17	-22586	-6660.01	16005	42684.25	6.409	Si
SLU 41	1.07	-23104	-15755.81	16372	43418.31	2.756	Si
SLU 41	3.17	-22586	-6660.01	16005	42684.25	6.409	Si
SLU 39	1.07	-23104	-15755.81	16372	43418.31	2.756	Si
SLU 39	3.17	-22586	-6660.01	16005	42684.25	6.409	Si
SLU 37	1.07	-20672	-13850.9	14649	39876.94	2.879	Si
SLU 37	3.17	-19510	-5708.69	13825	38098.94	6.674	Si
SLU 42	1.07	-23104	-15755.81	16372	43418.31	2.756	Si
SLU 42	3.17	-22586	-6660.01	16005	42684.25	6.409	Si
SLU 82	1.07	-26118	-17182.44	18508	47472.42	2.763	Si
SLU 82	3.17	-24416	-7118.57	17302	45229.06	6.354	Si
SLU 83	1.07	-26118	-17182.44	18508	47472.42	2.763	Si
SLU 83	3.17	-24416	-7118.57	17302	45229.06	6.354	Si
SLU 81	1.07	-26118	-17182.44	18508	47472.42	2.763	Si
SLU 81	3.17	-24416	-7118.57	17302	45229.06	6.354	Si
SLU 84	1.07	-26118	-17182.44	18508	47472.42	2.763	Si
SLU 84	3.17	-24416	-7118.57	17302	45229.06	6.354	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γM = 2

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLV 7	1.07	-14326	-7019.78	10152	30895.86	4.401	Si
SLV 7	3.17	-12480	-4177.29	8843	27227.65	6.518	Si
SLV 11	1.07	-15671	-11493.11	11105	33508.07	2.915	Si
SLV 11	3.17	-12101	-2669.93	8575	26463.4	9.912	Si
SLV 13	1.07	-17201	-16542.18	12189	36421.31	2.202	Si
SLV 13	3.17	-11679	-971.24	8276	25609.02	26.367	Si
SLV 8	1.07	-14326	-7019.78	10152	30895.86	4.401	Si
SLV 8	3.17	-12480	-4177.29	8843	27227.65	6.518	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 10	1.07	-15612	-11231.85	11063	33394.75	2.973	Si
SLV 10	3.17	-12133	-2762.07	8597	26527.93	9.604	Si
SLV 12	1.07	-15671	-11493.11	11105	33508.07	2.915	Si
SLV 12	3.17	-12101	-2669.93	8575	26463.4	9.912	Si
SLV 14	1.07	-17201	-16542.18	12189	36421.31	2.202	Si
SLV 14	3.17	-11679	-971.24	8276	25609.02	26.367	Si
SLV 16	1.07	-17219	-16620.55	12202	36454.55	2.193	Si
SLV 16	3.17	-11670	-943.59	8269	25589.55	27.119	Si
SLV 9	1.07	-15612	-11231.85	11063	33394.75	2.973	Si
SLV 9	3.17	-12133	-2762.07	8597	26527.93	9.604	Si
SLV 15	1.07	-17219	-16620.55	12202	36454.55	2.193	Si
SLV 15	3.17	-11670	-943.59	8269	25589.55	27.119	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 82	1.07	-26118	1131	-17182.44		18508	4.704	8023	11322			10.01	Si
SLU 82	3.17	-24416	1132	-7118.57		17302	4.704	7862	11095			9.8	Si
SLU 40	1.07	-23104	1197	-15755.81		16372	4.704	7738	10920			9.12	Si
SLU 40	3.17	-22586	1198	-6660.01		16005	4.704	7690	10851			9.06	Si
SLU 21	1.07	-20794	951	-13585.5		14735	4.704	7520	10612			11.15	Si
SLU 21	3.17	-19678	952	-5745.15		13944	4.704	7415	10464			10.99	Si
SLU 83	1.07	-26118	1131	-17182.44		18508	4.704	8023	11322			10.01	Si
SLU 83	3.17	-24416	1132	-7118.57		17302	4.704	7862	11095			9.8	Si
SLU 41	1.07	-23104	1197	-15755.81		16372	4.704	7738	10920			9.12	Si
SLU 41	3.17	-22586	1198	-6660.01		16005	4.704	7690	10851			9.06	Si
SLU 20	1.07	-20794	951	-13585.5		14735	4.704	7520	10612			11.15	Si
SLU 20	3.17	-19678	952	-5745.15		13944	4.704	7415	10464			10.99	Si
SLU 42	1.07	-23104	1197	-15755.81		16372	4.704	7738	10920			9.12	Si
SLU 42	3.17	-22586	1198	-6660.01		16005	4.704	7690	10851			9.06	Si
SLU 81	1.07	-26118	1131	-17182.44		18508	4.704	8023	11322			10.01	Si
SLU 81	3.17	-24416	1132	-7118.57		17302	4.704	7862	11095			9.8	Si
SLU 39	1.07	-23104	1197	-15755.81		16372	4.704	7738	10920			9.12	Si
SLU 39	3.17	-22586	1198	-6660.01		16005	4.704	7690	10851			9.06	Si
SLU 84	1.07	-26118	1131	-17182.44		18508	4.704	8023	11322			10.01	Si
SLU 84	3.17	-24416	1132	-7118.57		17302	4.704	7862	11095			9.8	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 3	1.07	-12737	8905	-1709.46		9026	4.704	10139	14307			1.61	Si
SLV 3	3.17	-12933	7557	-5968.12		9165	4.704	10166	14347			1.9	Si
SLV 1	1.07	-12720	8981	-1631.08		9013	4.704	10136	14304			1.59	Si
SLV 1	3.17	-12943	7651	-5995.77		9171	4.704	10168	14348			1.88	Si
SLV 4	1.07	-12737	8905	-1709.46		9026	4.704	10139	14307			1.61	Si
SLV 4	3.17	-12933	7557	-5968.12		9165	4.704	10166	14347			1.9	Si
SLV 5	1.07	-14268	3027	-6758.52		10110	4.704	10355	14613			4.83	Si
SLV 5	3.17	-12512	2655	-4269.43		8866	4.704	10107	14262			5.37	Si
SLV 14	1.07	-17201	-8286	-16542.18		13747	4.1709	11083	13868			1.67	Si
SLV 14	3.17	-11679	-6936	-971.24		8276	4.704	9989	14096			2.03	Si
SLV 6	1.07	-14268	3027	-6758.52		10110	4.704	10355	14613			4.83	Si
SLV 6	3.17	-12512	2655	-4269.43		8866	4.704	10107	14262			5.37	Si
SLV 16	1.07	-17219	-8362	-16620.55		13797	4.1602	11093	13844			1.66	Si
SLV 16	3.17	-11670	-7030	-943.59		8269	4.704	9987	14094			2	Si
SLV 13	1.07	-17201	-8286	-16542.18		13747	4.1709	11083	13868			1.67	Si
SLV 13	3.17	-11679	-6936	-971.24		8276	4.704	9989	14096			2.03	Si
SLV 2	1.07	-12720	8981	-1631.08		9013	4.704	10136	14304			1.59	Si
SLV 2	3.17	-12943	7651	-5995.77		9171	4.704	10168	14348			1.88	Si
SLV 15	1.07	-17219	-8362	-16620.55		13797	4.1602	11093	13844			1.66	Si
SLV 15	3.17	-11670	-7030	-943.59		8269	4.704	9987	14094			2	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.03 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 15	143750	0.47	8274	-11676	793	1632.85	2.06	Si
SLV 16	143750	0.47	8274	-11676	793	1632.85	2.06	Si
SLV 13	143750	0.47	8283	-11689	793	1634.52	2.06	Si
SLV 14	143750	0.47	8283	-11689	793	1634.52	2.06	Si
SLV 12	143750	0.47	8589	-12121	793	1690.35	2.13	Si
SLV 11	143750	0.47	8589	-12121	793	1690.35	2.13	Si
SLV 9	143750	0.47	8620	-12164	793	1695.87	2.14	Si
SLV 10	143750	0.47	8620	-12164	793	1695.87	2.14	Si
SLV 7	143750	0.47	8868	-12515	793	1741.01	2.2	Si
SLV 8	143750	0.47	8868	-12515	793	1741.01	2.2	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.03 Wa = 0.05 Ta = 0.0855

Comb.	N top	N base	V orto	α_0	M*	e*	α_0^*	aLim	Verifica
SLV 14	-8671	-17201	155	0.041	1701.8	0.896	0.66322	19.26035	No
SLV 13	-8671	-17201	155	0.041	1701.8	0.896	0.66322	19.26035	No
SLV 4	-8635	-12737	-155	0.041	1698.2	0.896	0.6634	19.26035	No
SLV 3	-8635	-12737	-155	0.041	1698.2	0.896	0.6634	19.26035	No
SLV 16	-8667	-17219	-80	0.046	1701.4	0.896	0.75248	19.26035	No
SLV 15	-8667	-17219	-80	0.046	1701.4	0.896	0.75248	19.26035	No
SLV 1	-8638	-12720	79	0.046	1698.6	0.896	0.75284	19.26035	No
SLV 2	-8638	-12720	79	0.046	1698.6	0.896	0.75284	19.26035	No
SLV 8	-8642	-14326	-401	0.023	1698.9	0.896	0.36944	4.54431	No
SLV 7	-8642	-14326	-401	0.023	1698.9	0.896	0.36944	4.54431	No



Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	2.756	SLU 39	Si
V_SLU	9.057	SLU 39	Si
PF_SLV	2.193	SLV 15	Si
V_SLV	1.593	SLV 1	Si
PFFP_SLV	2.059	SLV 15	Si
R_SLV	0.034	SLV 13	No

Maschio 16

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-3.67	-17.728	-3.67	-8.718	L2	L3	9.01	0.21	3.92	3.92	3.92			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 43	1.07	-21786	179.14	11514	84272.79	470.424	Si
SLU 43	4.99	-615	-65.17	325	2758.82	42.332	Si
SLU 50	1.07	-21786	179.14	11514	84272.79	470.424	Si
SLU 50	4.99	-615	-65.17	325	2758.82	42.332	Si
SLU 46	1.07	-21786	179.14	11514	84272.79	470.424	Si
SLU 46	4.99	-615	-65.17	325	2758.82	42.332	Si
SLU 45	1.07	-21786	179.14	11514	84272.79	470.424	Si
SLU 45	4.99	-615	-65.17	325	2758.82	42.332	Si
SLU 1	1.07	-17533	106.11	9266	70000.54	659.713	Si
SLU 1	4.99	-564	-55.21	298	2531.31	45.85	Si
SLU 49	1.07	-21786	179.14	11514	84272.79	470.424	Si
SLU 49	4.99	-615	-65.17	325	2758.82	42.332	Si
SLU 51	1.07	-21786	179.14	11514	84272.79	470.424	Si
SLU 51	4.99	-615	-65.17	325	2758.82	42.332	Si
SLU 44	1.07	-21786	179.14	11514	84272.79	470.424	Si
SLU 44	4.99	-615	-65.17	325	2758.82	42.332	Si
SLU 48	1.07	-21786	179.14	11514	84272.79	470.424	Si
SLU 48	4.99	-615	-65.17	325	2758.82	42.332	Si
SLU 47	1.07	-21786	179.14	11514	84272.79	470.424	Si
SLU 47	4.99	-615	-65.17	325	2758.82	42.332	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 11	1.07	-19998	20172.11	10569	82298.93	4.08	Si
SLV 11	4.99	-895	356.18	473	4016.12	11.276	Si
SLV 12	1.07	-19998	20172.11	10569	82298.93	4.08	Si
SLV 12	4.99	-895	356.18	473	4016.12	11.276	Si
SLV 10	1.07	-20021	-20625.79	10581	82382.79	3.994	Si
SLV 10	4.99	-865	-487.87	457	3882.81	7.959	Si
SLV 7	1.07	-19984	20564.19	10562	82246.55	4	Si
SLV 7	4.99	-909	338.44	480	4078.03	12.05	Si
SLV 6	1.07	-20007	-20233.71	10574	82330.42	4.069	Si
SLV 6	4.99	-879	-505.61	465	3944.73	7.802	Si
SLV 9	1.07	-20021	-20625.79	10581	82382.79	3.994	Si
SLV 9	4.99	-865	-487.87	457	3882.81	7.959	Si
SLV 8	1.07	-19984	20564.19	10562	82246.55	4	Si
SLV 8	4.99	-909	338.44	480	4078.03	12.05	Si
SLV 5	1.07	-20007	-20233.71	10574	82330.42	4.069	Si
SLV 5	4.99	-879	-505.61	465	3944.73	7.802	Si
SLV 14	1.07	-20029	-6803.95	10586	82414.53	12.113	Si
SLV 14	4.99	-859	-171.75	454	3857.23	22.459	Si
SLV 13	1.07	-20029	-6803.95	10586	82414.53	12.113	Si
SLV 13	4.99	-859	-171.75	454	3857.23	22.459	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 54	1.07	-27493	0	-179.86		14530	9.01	7493	14177			1000	Si
SLU 54	4.99	-1400	0	-114.19		740	9.01	5654	10698			1000	Si
SLU 1	1.07	-17533	0	106.11		9266	9.01	6791	12849			1000	Si
SLU 1	4.99	-564	0	-55.21		298	9.01	5595	10587			1000	Si
SLU 58	1.07	-27493	0	-179.86		14530	9.01	7493	14177			1000	Si
SLU 58	4.99	-1400	0	-114.19		740	9.01	5654	10698			1000	Si
SLU 57	1.07	-27493	0	-179.86		14530	9.01	7493	14177			1000	Si
SLU 57	4.99	-1400	0	-114.19		740	9.01	5654	10698			1000	Si
SLU 61	1.07	-29939	0	-333.72		15823	9.01	7665	14504			1000	Si
SLU 61	4.99	-1737	0	-135.2		918	9.01	5678	10743			1000	Si
SLU 59	1.07	-27493	0	-179.86		14530	9.01	7493	14177			1000	Si
SLU 59	4.99	-1400	0	-114.19		740	9.01	5654	10698			1000	Si
SLU 60	1.07	-29939	0	-333.72		15823	9.01	7665	14504			1000	Si
SLU 60	4.99	-1737	0	-135.2		918	9.01	5678	10743			1000	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 55	1.07	-27493	0	-179.86		14530	9.01	7493	14177			1000	Si
SLU 55	4.99	-1400	0	-114.19		740	9.01	5654	10698			1000	Si
SLU 53	1.07	-27493	0	-179.86		14530	9.01	7493	14177			1000	Si
SLU 53	4.99	-1400	0	-114.19		740	9.01	5654	10698			1000	Si
SLU 56	1.07	-27493	0	-179.86		14530	9.01	7493	14177			1000	Si
SLU 56	4.99	-1400	0	-114.19		740	9.01	5654	10698			1000	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 3	1.07	-19976	3250	6742.35		10557	9.01	10445	19763			6.08	Si
SLV 3	4.99	-915	501	22.32		483	9.01	8430	15950			31.86	Si
SLV 7	1.07	-19984	10747	20564.19		10562	9.01	10446	19764			1.84	Si
SLV 7	4.99	-909	1942	338.44		480	9.01	8429	15949			8.21	Si
SLV 6	1.07	-20007	-10731	-20233.71		10574	9.01	10448	19769			1.84	Si
SLV 6	4.99	-879	-1996	-505.61		465	9.01	8426	15943			7.99	Si
SLV 4	1.07	-19976	3250	6742.35		10557	9.01	10445	19763			6.08	Si
SLV 4	4.99	-915	501	22.32		483	9.01	8430	15950			31.86	Si
SLV 10	1.07	-20021	-10748	-20625.79		10581	9.01	10450	19772			1.84	Si
SLV 10	4.99	-865	-1942	-487.87		457	9.01	8425	15941			8.21	Si
SLV 9	1.07	-20021	-10748	-20625.79		10581	9.01	10450	19772			1.84	Si
SLV 9	4.99	-865	-1942	-487.87		457	9.01	8425	15941			8.21	Si
SLV 5	1.07	-20007	-10731	-20233.71		10574	9.01	10448	19769			1.84	Si
SLV 5	4.99	-879	-1996	-505.61		465	9.01	8426	15943			7.99	Si
SLV 8	1.07	-19984	10747	20564.19		10562	9.01	10446	19764			1.84	Si
SLV 8	4.99	-909	1942	338.44		480	9.01	8429	15949			8.21	Si
SLV 11	1.07	-19998	10730	20172.11		10569	9.01	10447	19767			1.84	Si
SLV 11	4.99	-895	1996	356.18		473	9.01	8428	15946			7.99	Si
SLV 12	1.07	-19998	10730	20172.11		10569	9.01	10447	19767			1.84	Si
SLV 12	4.99	-895	1996	356.18		473	9.01	8428	15946			7.99	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.03 Wa 0.04 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 2	143750	0.47	6290	-11902	1082.64	1185.37	1.09	Si
SLV 1	143750	0.47	6290	-11902	1082.64	1185.37	1.09	Si
SLV 5	143750	0.47	6292	-11904	1082.64	1185.59	1.1	Si
SLV 6	143750	0.47	6292	-11904	1082.64	1185.59	1.1	Si
SLV 3	143750	0.47	6323	-11963	1082.64	1191.14	1.1	Si
SLV 4	143750	0.47	6323	-11963	1082.64	1191.14	1.1	Si
SLV 9	143750	0.47	6325	-11968	1082.64	1191.56	1.1	Si
SLV 10	143750	0.47	6325	-11968	1082.64	1191.56	1.1	Si
SLV 8	143750	0.47	6400	-12109	1082.64	1204.83	1.11	Si
SLV 7	143750	0.47	6400	-12109	1082.64	1204.83	1.11	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 3.03 Wa = 0.04 Ta = 0.1222

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 4	-915	-19976	-3	0.05	1381	0.95	0.76499	12.00193	No
SLV 3	-915	-19976	-3	0.05	1381	0.95	0.76499	12.00193	No
SLV 14	-859	-20029	3	0.05	1378.9	0.952	0.76578	12.00193	No
SLV 13	-859	-20029	3	0.05	1378.9	0.952	0.76578	12.00193	No
SLV 2	-906	-19982	-1	0.05	1380.6	0.95	0.76915	12.00193	No
SLV 1	-906	-19982	-1	0.05	1380.6	0.95	0.76915	12.00193	No
SLV 16	-868	-20022	1	0.05	1379.2	0.952	0.7697	12.00193	No
SLV 15	-868	-20022	1	0.05	1379.2	0.952	0.7697	12.00193	No
SLV 8	-909	-19984	-4	0.05	1380.7	0.95	0.76277	4.88098	No
SLV 7	-909	-19984	-4	0.05	1380.7	0.95	0.76277	4.88098	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	42.332	SLU 43	Si
V_SLU	1000	SLU 1	Si
PF_SLV	3.994	SLV 9	Si
V_SLV	1.839	SLV 7	Si
PFFP_SLV	1.095	SLV 1	Si
R_SLV	0.064	SLV 3	No

Maschio 17

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-8.545	-17.728	-9.429	-17.728	L2	L3	0.884	0.3	3.92	3.92	3.92			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 42	2.07	-2649	113.18	9985	1028.05	9.083	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 42	3.97	-3746	-572.58	14118	1369.61	2.392	Si
SLU 40	2.07	-2649	113.18	9985	1028.05	9.083	Si
SLU 40	3.97	-3746	-572.58	14118	1369.61	2.392	Si
SLU 20	2.07	-2453	86.12	9244	961.62	11.166	Si
SLU 20	3.97	-3245	-485.39	12230	1219.68	2.513	Si
SLU 81	2.07	-3110	107.02	11722	1177.62	11.003	Si
SLU 81	3.97	-4022	-597.01	15157	1447.66	2.425	Si
SLU 21	2.07	-2453	86.12	9244	961.62	11.166	Si
SLU 21	3.97	-3245	-485.39	12230	1219.68	2.513	Si
SLU 83	2.07	-3110	107.02	11722	1177.62	11.003	Si
SLU 83	3.97	-4022	-597.01	15157	1447.66	2.425	Si
SLU 39	2.07	-2649	113.18	9985	1028.05	9.083	Si
SLU 39	3.97	-3746	-572.58	14118	1369.61	2.392	Si
SLU 84	2.07	-3110	107.02	11722	1177.62	11.003	Si
SLU 84	3.97	-4022	-597.01	15157	1447.66	2.425	Si
SLU 41	2.07	-2649	113.18	9985	1028.05	9.083	Si
SLU 41	3.97	-3746	-572.58	14118	1369.61	2.392	Si
SLU 82	2.07	-3110	107.02	11722	1177.62	11.003	Si
SLU 82	3.97	-4022	-597.01	15157	1447.66	2.425	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 8	2.07	-1236	261.66	4658	525.82	2.01	Si
SLV 8	3.97	-2365	-485.83	8915	969.79	1.996	Si
SLV 16	2.07	-2845	-609.48	10720	1147.62	1.883	Si
SLV 16	3.97	-865	240.82	3258	372.16	1.545	Si
SLV 3	2.07	-818	695.6	0	0	0	No, $e \geq l/2$
SLV 3	3.97	-3130	-811.21	11796	1250.57	1.542	Si
SLV 1	2.07	-1067	676.03	0	0	0	No, $e \geq l/2$
SLV 1	3.97	-3106	-774.49	11704	1241.87	1.603	Si
SLV 13	2.07	-3094	-629.05	11661	1237.76	1.968	Si
SLV 13	3.97	-840	277.53	3167	361.95	1.304	Si
SLV 15	2.07	-2845	-609.48	10720	1147.62	1.883	Si
SLV 15	3.97	-865	240.82	3258	372.16	1.545	Si
SLV 7	2.07	-1236	261.66	4658	525.82	2.01	Si
SLV 7	3.97	-2365	-485.83	8915	969.79	1.996	Si
SLV 2	2.07	-1067	676.03	0	0	0	No, $e \geq l/2$
SLV 2	3.97	-3106	-774.49	11704	1241.87	1.603	Si
SLV 14	2.07	-3094	-629.05	11661	1237.76	1.968	Si
SLV 14	3.97	-840	277.53	3167	361.95	1.304	Si
SLV 4	2.07	-818	695.6	0	0	0	No, $e \geq l/2$
SLV 4	3.97	-3130	-811.21	11796	1250.57	1.542	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLU 41	2.07	-2649	838	113.18		9985	0.8845	6887	1827			2.18	Si
SLU 41	3.97	-3746	838	-572.58		14383	0.8682	7473	1947			2.32	Si
SLU 39	2.07	-2649	838	113.18		9985	0.8845	6887	1827			2.18	Si
SLU 39	3.97	-3746	838	-572.58		14383	0.8682	7473	1947			2.32	Si
SLU 40	2.07	-2649	838	113.18		9985	0.8845	6887	1827			2.18	Si
SLU 40	3.97	-3746	838	-572.58		14383	0.8682	7473	1947			2.32	Si
SLU 75	2.07	-2903	735	84.31		10941	0.8845	7014	1861			2.53	Si
SLU 75	3.97	-3496	735	-505.71		13174	0.8845	7312	1940			2.64	Si
SLU 83	2.07	-3110	869	107.02		11722	0.8845	7119	1889			2.17	Si
SLU 83	3.97	-4022	870	-597.01		15210	0.8814	7584	2005			2.31	Si
SLU 77	2.07	-2903	735	84.31		10941	0.8845	7014	1861			2.53	Si
SLU 77	3.97	-3496	735	-505.71		13174	0.8845	7312	1940			2.64	Si
SLU 42	2.07	-2649	838	113.18		9985	0.8845	6887	1827			2.18	Si
SLU 42	3.97	-3746	838	-572.58		14383	0.8682	7473	1947			2.32	Si
SLU 84	2.07	-3110	869	107.02		11722	0.8845	7119	1889			2.17	Si
SLU 84	3.97	-4022	870	-597.01		15210	0.8814	7584	2005			2.31	Si
SLU 81	2.07	-3110	869	107.02		11722	0.8845	7119	1889			2.17	Si
SLU 81	3.97	-4022	870	-597.01		15210	0.8814	7584	2005			2.31	Si
SLU 82	2.07	-3110	869	107.02		11722	0.8845	7119	1889			2.17	Si
SLU 82	3.97	-4022	870	-597.01		15210	0.8814	7584	2005			2.31	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLV 4	2.07	-818	1647	695.6		0	0	8333	0			0	No, $V_u < V$
SLV 4	3.97	-3130	1457	-811.21		18997	0.5492	12133	1999			1.37	Si
SLV 15	2.07	-2845	-752	-609.48		13864	0.6839	11106	2279			3.03	Si
SLV 15	3.97	-865	-586	240.82		5868	0.4911	9507	1401			2.39	Si
SLV 3	2.07	-818	1647	695.6		0	0	8333	0			0	No, $V_u < V$
SLV 3	3.97	-3130	1457	-811.21		18997	0.5492	12133	1999			1.37	Si
SLV 1	2.07	-1067	1521	676.03		0	0	8333	0			0	No, $V_u < V$
SLV 1	3.97	-3106	1355	-774.49		17892	0.5786	11912	2068			1.53	Si
SLV 16	2.07	-2845	-752	-609.48		13864	0.6839	11106	2279			3.03	Si
SLV 16	3.97	-865	-586	240.82		5868	0.4911	9507	1401			2.39	Si
SLV 7	2.07	-1236	955	261.66		5957	0.6917	9525	1976			2.07	Si
SLV 7	3.97	-2365	861	-485.83		11097	0.7106	10553	2250			2.61	Si
SLV 8	2.07	-1236	955	261.66		5957	0.6917	9525	1976			2.07	Si
SLV 8	3.97	-2365	861	-485.83		11097	0.7106	10553	2250			2.61	Si
SLV 13	2.07	-3094	-879	-629.05		14388	0.7168	11211	2411			2.74	Si
SLV 13	3.97	-840	-688	277.53		8340	0.3358	10001	1008			1.47	Si
SLV 2	2.07	-1067	1521	676.03		0	0	8333	0			0	No, $V_u < V$
SLV 2	3.97	-3106	1355	-774.49		17892	0.5786	11912	2068			1.53	Si
SLV 14	2.07	-3094	-879	-629.05		14388	0.7168	11211	2411			2.74	Si
SLV 14	3.97	-840	-688	277.53		8340	0.3358	10001	1008			1.47	Si



Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.03 W_a 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 16	143750	0.47	5841	-1550	145.94	221.37	1.52	Si
SLV 15	143750	0.47	5841	-1550	145.94	221.37	1.52	Si
SLV 14	143750	0.47	6067	-1610	145.94	229.47	1.57	Si
SLV 13	143750	0.47	6067	-1610	145.94	229.47	1.57	Si
SLV 11	143750	0.47	6763	-1794	145.94	254.27	1.74	Si
SLV 12	143750	0.47	6763	-1794	145.94	254.27	1.74	Si
SLV 9	143750	0.47	7514	-1994	145.94	280.69	1.92	Si
SLV 10	143750	0.47	7514	-1994	145.94	280.69	1.92	Si
SLV 7	143750	0.47	7778	-2064	145.94	289.87	1.99	Si
SLV 8	143750	0.47	7778	-2064	145.94	289.87	1.99	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.03 $W_a = 0.05$ $T_a = 0.0855$

Comb.	N top	N base	V orto	σ_0	M*	e*	a0*	aLim	Verifica
SLV 12	-764	-1750	-147	0	239.1	0.89	0	4.54431	No
SLV 5	-872	-2750	147	0	248.7	0.889	0	4.54431	No
SLV 2	-886	-2706	309	0	249.9	0.889	0	19.26035	No
SLV 6	-872	-2750	147	0	248.7	0.889	0	4.54431	No
SLV 14	-772	-2033	-273	0	239.8	0.89	0	19.26035	No
SLV 3	-863	-2467	273	0	247.9	0.889	0	19.26035	No
SLV 1	-886	-2706	309	0	249.9	0.889	0	19.26035	No
SLV 4	-863	-2467	273	0	247.9	0.889	0	19.26035	No
SLV 11	-764	-1750	-147	0	239.1	0.89	0	4.54431	No
SLV 13	-772	-2033	-273	0	239.8	0.89	0	19.26035	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	2.392	SLU 39	Si
V_SLU	2.174	SLU 81	Si
PF_SLV	0	SLV 1	No
V_SLV	0	SLV 1	No
PFFP_SLV	1.517	SLV 15	Si
R_SLV	0	SLV 1	No

Maschio 18

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-6.558	-17.728	-7.545	-17.728	L2	L3	0.986	0.3	3.92	3.92	3.92			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 18	2.07	-6325	138.59	21377	2300.69	16.6	Si
SLU 18	4.07	-4654	-466.11	15728	1851.89	3.973	Si
SLU 83	2.07	-7903	160.72	26708	2619.42	16.298	Si
SLU 83	4.07	-5752	-572.15	19439	2159.59	3.775	Si
SLU 42	2.07	-7145	167.02	24148	2479.08	14.843	Si
SLU 42	4.07	-5378	-545.2	18175	2060.35	3.779	Si
SLU 81	2.07	-7903	160.72	26708	2619.42	16.298	Si
SLU 81	4.07	-5752	-572.15	19439	2159.59	3.775	Si
SLU 40	2.07	-7145	167.02	24148	2479.08	14.843	Si
SLU 40	4.07	-5378	-545.2	18175	2060.35	3.779	Si
SLU 19	2.07	-6325	138.59	21377	2300.69	16.6	Si
SLU 19	4.07	-4654	-466.11	15728	1851.89	3.973	Si
SLU 41	2.07	-7145	167.02	24148	2479.08	14.843	Si
SLU 41	4.07	-5378	-545.2	18175	2060.35	3.779	Si
SLU 84	2.07	-7903	160.72	26708	2619.42	16.298	Si
SLU 84	4.07	-5752	-572.15	19439	2159.59	3.775	Si
SLU 82	2.07	-7903	160.72	26708	2619.42	16.298	Si
SLU 82	4.07	-5752	-572.15	19439	2159.59	3.775	Si
SLU 39	2.07	-7145	167.02	24148	2479.08	14.843	Si
SLU 39	4.07	-5378	-545.2	18175	2060.35	3.779	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 1	2.07	-4603	1063.24	15556	1980.95	1.863	Si
SLV 1	4.07	-3856	-1282.3	13032	1698.84	1.325	Si
SLV 4	2.07	-4456	1074.02	15060	1926.7	1.794	Si
SLV 4	4.07	-3758	-1279.48	12701	1660.69	1.298	Si
SLV 2	2.07	-4603	1063.24	15556	1980.95	1.863	Si
SLV 2	4.07	-3856	-1282.3	13032	1698.84	1.325	Si
SLV 15	2.07	-3935	-973.21	13299	1729.35	1.777	Si
SLV 15	4.07	-1737	762.29	5871	815.54	1.07	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 13	2.07	-4082	-983.98	13795	1785.69	1.815	Si
SLV 13	4.07	-1835	759.47	6202	859.09	1.131	Si
SLV 16	2.07	-3935	-973.21	13299	1729.35	1.777	Si
SLV 16	4.07	-1737	762.29	5871	815.54	1.07	Si
SLV 3	2.07	-4456	1074.02	15060	1926.7	1.794	Si
SLV 3	4.07	-3758	-1279.48	12701	1660.69	1.298	Si
SLV 7	2.07	-4102	370.05	13865	1793.58	4.847	Si
SLV 7	4.07	-2936	-561.57	9924	1330.51	2.369	Si
SLV 8	2.07	-4102	370.05	13865	1793.58	4.847	Si
SLV 8	4.07	-2936	-561.57	9924	1330.51	2.369	Si
SLV 14	2.07	-4082	-983.98	13795	1785.69	1.815	Si
SLV 14	4.07	-1835	759.47	6202	859.09	1.131	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 62	2.07	-7083	160	132.29		23937	0.9863	8747	2588			16.19	Si
SLU 62	4.07	-5028	193	-493.06		16992	0.9863	7821	2314			12	Si
SLU 42	2.07	-7145	198	167.02		24148	0.9863	8775	2597			13.13	Si
SLU 42	4.07	-5378	214	-545.2		18175	0.9863	7979	2361			11.04	Si
SLU 63	2.07	-7083	160	132.29		23937	0.9863	8747	2588			16.19	Si
SLU 63	4.07	-5028	193	-493.06		16992	0.9863	7821	2314			12	Si
SLU 40	2.07	-7145	198	167.02		24148	0.9863	8775	2597			13.13	Si
SLU 40	4.07	-5378	214	-545.2		18175	0.9863	7979	2361			11.04	Si
SLU 41	2.07	-7145	198	167.02		24148	0.9863	8775	2597			13.13	Si
SLU 41	4.07	-5378	214	-545.2		18175	0.9863	7979	2361			11.04	Si
SLU 39	2.07	-7145	198	167.02		24148	0.9863	8775	2597			13.13	Si
SLU 39	4.07	-5378	214	-545.2		18175	0.9863	7979	2361			11.04	Si
SLU 83	2.07	-7903	194	160.72		26708	0.9863	9117	2698			13.91	Si
SLU 83	4.07	-5752	223	-572.15		19439	0.9863	8147	2411			10.8	Si
SLU 84	2.07	-7903	194	160.72		26708	0.9863	9117	2698			13.91	Si
SLU 84	4.07	-5752	223	-572.15		19439	0.9863	8147	2411			10.8	Si
SLU 81	2.07	-7903	194	160.72		26708	0.9863	9117	2698			13.91	Si
SLU 81	4.07	-5752	223	-572.15		19439	0.9863	8147	2411			10.8	Si
SLU 82	2.07	-7903	194	160.72		26708	0.9863	9117	2698			13.91	Si
SLU 82	4.07	-5752	223	-572.15		19439	0.9863	8147	2411			10.8	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 3	2.07	-4456	1385	1074.02		19638	0.7564	12261	2782			2.01	Si
SLV 3	4.07	-3758	755	-1279.48		27346	0.4581	13803	1897			2.51	Si
SLV 2	2.07	-4603	1336	1063.24		19509	0.7865	12235	2887			2.16	Si
SLV 2	4.07	-3856	755	-1282.3		26676	0.4819	13668	1976			2.62	Si
SLV 15	2.07	-3935	-1210	-973.21		17786	0.7375	11890	2631			2.17	Si
SLV 15	4.07	-1737	-559	762.29		35518	0.163	15437	755			1.35	Si
SLV 16	2.07	-3935	-1210	-973.21		17786	0.7375	11890	2631			2.17	Si
SLV 16	4.07	-1737	-559	762.29		35518	0.163	15437	755			1.35	Si
SLV 14	2.07	-4082	-1259	-983.98		17991	0.7563	11932	2707			2.15	Si
SLV 14	4.07	-1835	-559	759.47		25709	0.238	13475	962			1.72	Si
SLV 8	2.07	-4102	534	370.05		13865	0.9863	11106	3286			6.16	Si
SLV 8	4.07	-2936	296	-561.57		10807	0.9057	10495	2852			9.65	Si
SLV 4	2.07	-4456	1385	1074.02		19638	0.7564	12261	2782			2.01	Si
SLV 4	4.07	-3758	755	-1279.48		27346	0.4581	13803	1897			2.51	Si
SLV 7	2.07	-4102	534	370.05		13865	0.9863	11106	3286			6.16	Si
SLV 7	4.07	-2936	296	-561.57		10807	0.9057	10495	2852			9.65	Si
SLV 13	2.07	-4082	-1259	-983.98		17991	0.7563	11932	2707			2.15	Si
SLV 13	4.07	-1835	-559	759.47		25709	0.238	13475	962			1.72	Si
SLV 1	2.07	-4603	1336	1063.24		19509	0.7865	12235	2887			2.16	Si
SLV 1	4.07	-3856	755	-1282.3		26676	0.4819	13668	1976			2.62	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.03 W_a 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 16	143750	0.47	11162	-3303	162.74	450.17	2.77	Si
SLV 15	143750	0.47	11162	-3303	162.74	450.17	2.77	Si
SLV 12	143750	0.47	11354	-3360	162.74	457.12	2.81	Si
SLV 11	143750	0.47	11354	-3360	162.74	457.12	2.81	Si
SLV 13	143750	0.47	11514	-3407	162.74	462.86	2.84	Si
SLV 14	143750	0.47	11514	-3407	162.74	462.86	2.84	Si
SLV 7	143750	0.47	11870	-3512	162.74	475.66	2.92	Si
SLV 8	143750	0.47	11870	-3512	162.74	475.66	2.92	Si
SLV 9	143750	0.47	12525	-3706	162.74	498.93	3.07	Si
SLV 10	143750	0.47	12525	-3706	162.74	498.93	3.07	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.03 W_a = 0.05 T_a = 0.0855

Comb.	N top	N base	V orto	α_0	M*	e*	α_0^*	α_{lim}	Verifica
SLV 3	-1107	-2985	-29	0.043	289.5	0.889	0.70929	19.26035	No
SLV 4	-1107	-2985	-29	0.043	289.5	0.889	0.70929	19.26035	No
SLV 13	-1097	-5750	29	0.043	288.6	0.889	0.70963	19.26035	No
SLV 14	-1097	-5750	29	0.043	288.6	0.889	0.70963	19.26035	No
SLV 1	-1120	-3128	-20	0.048	290.7	0.889	0.77786	19.26035	No
SLV 2	-1120	-3128	-20	0.048	290.7	0.889	0.77786	19.26035	No
SLV 15	-1084	-5607	20	0.048	287.4	0.889	0.78048	19.26035	No
SLV 16	-1084	-5607	20	0.048	287.4	0.889	0.78048	19.26035	No
SLV 9	-1121	-4999	23	0.046	290.8	0.889	0.75682	4.54431	No
SLV 10	-1121	-4999	23	0.046	290.8	0.889	0.75682	4.54431	No



Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	3.775	SLU 81	Si
V_SLU	10.8	SLU 81	Si
PF_SLV	1.07	SLV 15	Si
V_SLV	1.352	SLV 15	Si
PFFP_SLV	2.766	SLV 15	Si
R_SLV	0.037	SLV 3	No

Maschio 19

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-3.283	-17.728	-5.158	-17.728	L2	L3	1.876	0.3	3.92	3.92	3.92			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	$\tau 0$	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma 0$	Mu	c.s.	Verifica
SLU 40	3.07	-8785	181.58	15612	6659.44	36.675	Si
SLU 40	4.07	-7598	1591.83	13503	5944.41	3.734	Si
SLU 82	3.07	-9647	168.45	17145	7143.07	42.405	Si
SLU 82	4.07	-8123	1709.87	14437	6267.98	3.666	Si
SLU 39	3.07	-8785	181.58	15612	6659.44	36.675	Si
SLU 39	4.07	-7598	1591.83	13503	5944.41	3.734	Si
SLU 61	3.07	-8587	129.5	15260	6544.23	50.535	Si
SLU 61	4.07	-7088	1497.23	12596	5619.14	3.753	Si
SLU 41	3.07	-8785	181.58	15612	6659.44	36.675	Si
SLU 41	4.07	-7598	1591.83	13503	5944.41	3.734	Si
SLU 81	3.07	-9647	168.45	17145	7143.07	42.405	Si
SLU 81	4.07	-8123	1709.87	14437	6267.98	3.666	Si
SLU 60	3.07	-8587	129.5	15260	6544.23	50.535	Si
SLU 60	4.07	-7088	1497.23	12596	5619.14	3.753	Si
SLU 84	3.07	-9647	168.45	17145	7143.07	42.405	Si
SLU 84	4.07	-8123	1709.87	14437	6267.98	3.666	Si
SLU 83	3.07	-9647	168.45	17145	7143.07	42.405	Si
SLU 83	4.07	-8123	1709.87	14437	6267.98	3.666	Si
SLU 42	3.07	-8785	181.58	15612	6659.44	36.675	Si
SLU 42	4.07	-7598	1591.83	13503	5944.41	3.734	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma 0$	Mu	c.s.	Verifica
SLV 13	3.07	-5784	-997.06	10280	4968.22	4.983	Si
SLV 13	4.07	-4928	2318.14	8758	4290.27	1.851	Si
SLV 16	3.07	-5615	-969.26	9979	4835.68	4.989	Si
SLV 16	4.07	-4853	2370.77	8625	4230.02	1.784	Si
SLV 9	3.07	-5574	-313.1	9907	4803.93	15.343	Si
SLV 9	4.07	-4361	1207.68	7750	3830.29	3.172	Si
SLV 4	3.07	-4451	1077.56	7910	3903.66	3.623	Si
SLV 4	4.07	-2983	-626.53	5302	2676.23	4.271	Si
SLV 12	3.07	-5010	-220.45	8903	4355.86	19.759	Si
SLV 12	4.07	-4111	1383.11	7306	3625	2.621	Si
SLV 10	3.07	-5574	-313.1	9907	4803.93	15.343	Si
SLV 10	4.07	-4361	1207.68	7750	3830.29	3.172	Si
SLV 14	3.07	-5784	-997.06	10280	4968.22	4.983	Si
SLV 14	4.07	-4928	2318.14	8758	4290.27	1.851	Si
SLV 11	3.07	-5010	-220.45	8903	4355.86	19.759	Si
SLV 11	4.07	-4111	1383.11	7306	3625	2.621	Si
SLV 15	3.07	-5615	-969.26	9979	4835.68	4.989	Si
SLV 15	4.07	-4853	2370.77	8625	4230.02	1.784	Si
SLV 3	3.07	-4451	1077.56	7910	3903.66	3.623	Si
SLV 3	4.07	-2983	-626.53	5302	2676.23	4.271	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma 0$	σN	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 84	3.07	-9647	-795	168.45	17145	1.8756	7842	4412				5.55	Si
SLU 84	4.07	-8123	-1482	1709.87	14437	1.8756	7480	4209				2.84	Si
SLU 39	3.07	-8785	-744	181.58	15612	1.8756	7637	4297				5.77	Si
SLU 39	4.07	-7598	-1401	1591.83	13503	1.8756	7356	4139				2.95	Si
SLU 83	3.07	-9647	-795	168.45	17145	1.8756	7842	4412				5.55	Si
SLU 83	4.07	-8123	-1482	1709.87	14437	1.8756	7480	4209				2.84	Si
SLU 62	3.07	-8587	-693	129.5	15260	1.8756	7590	4271				6.16	Si
SLU 62	4.07	-7088	-1281	1497.23	12596	1.8756	7235	4071				3.18	Si
SLU 40	3.07	-8785	-744	181.58	15612	1.8756	7637	4297				5.77	Si
SLU 40	4.07	-7598	-1401	1591.83	13503	1.8756	7356	4139				2.95	Si
SLU 82	3.07	-9647	-795	168.45	17145	1.8756	7842	4412				5.55	Si
SLU 82	4.07	-8123	-1482	1709.87	14437	1.8756	7480	4209				2.84	Si
SLU 42	3.07	-8785	-744	181.58	15612	1.8756	7637	4297				5.77	Si
SLU 42	4.07	-7598	-1401	1591.83	13503	1.8756	7356	4139				2.95	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 81	3.07	-9647	-795	168.45		17145	1.8756	7842	4412			5.55	Si
SLU 81	4.07	-8123	-1482	1709.87		14437	1.8756	7480	4209			2.84	Si
SLU 63	3.07	-8587	-693	129.5		15260	1.8756	7590	4271			6.16	Si
SLU 63	4.07	-7088	-1281	1497.23		12596	1.8756	7235	4071			3.18	Si
SLU 41	3.07	-8785	-744	181.58		15612	1.8756	7637	4297			5.77	Si
SLU 41	4.07	-7598	-1401	1591.83		13503	1.8756	7356	4139			2.95	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 16	3.07	-5615	-3539	-969.26		9979	1.8756	10329	5812			1.64	Si
SLV 16	4.07	-4853	-2862	2370.77		12001	1.3479	10734	4340			1.52	Si
SLV 15	3.07	-5615	-3539	-969.26		9979	1.8756	10329	5812			1.64	Si
SLV 15	4.07	-4853	-2862	2370.77		12001	1.3479	10734	4340			1.52	Si
SLV 12	3.07	-5010	-1405	-220.45		8903	1.8756	10114	5691			4.05	Si
SLV 12	4.07	-4111	-1482	1383.11		7596	1.8042	9852	5333			3.6	Si
SLV 3	3.07	-4451	2718	1077.56		7910	1.8756	9915	5579			2.05	Si
SLV 3	4.07	-2983	1382	-626.53		5302	1.8756	9394	5286			3.83	Si
SLV 11	3.07	-5010	-1405	-220.45		8903	1.8756	10114	5691			4.05	Si
SLV 11	4.07	-4111	-1482	1383.11		7596	1.8042	9852	5333			3.6	Si
SLV 4	3.07	-4451	2718	1077.56		7910	1.8756	9915	5579			2.05	Si
SLV 4	4.07	-2983	1382	-626.53		5302	1.8756	9394	5286			3.83	Si
SLV 14	3.07	-5784	-3490	-997.06		10280	1.8756	10389	5846			1.67	Si
SLV 14	4.07	-4928	-2772	2318.14		11715	1.4022	10676	4491			1.62	Si
SLV 2	3.07	-4620	2766	1049.76		8211	1.8756	9975	5613			2.03	Si
SLV 2	4.07	-3058	1472	-679.16		5435	1.8756	9420	5301			3.6	Si
SLV 13	3.07	-5784	-3490	-997.06		10280	1.8756	10389	5846			1.67	Si
SLV 13	4.07	-4928	-2772	2318.14		11715	1.4022	10676	4491			1.62	Si
SLV 1	3.07	-4620	2766	1049.76		8211	1.8756	9975	5613			2.03	Si
SLV 1	4.07	-3058	1472	-679.16		5435	1.8756	9420	5301			3.6	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.03 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 12	143750	0.47	7532	-4238	309.47	596.5	1.93	Si
SLV 11	143750	0.47	7532	-4238	309.47	596.5	1.93	Si
SLV 16	143750	0.47	7690	-4327	309.47	608.18	1.97	Si
SLV 15	143750	0.47	7690	-4327	309.47	608.18	1.97	Si
SLV 7	143750	0.47	7770	-4372	309.47	614.12	1.98	Si
SLV 8	143750	0.47	7770	-4372	309.47	614.12	1.98	Si
SLV 13	143750	0.47	8064	-4537	309.47	635.69	2.05	Si
SLV 14	143750	0.47	8064	-4537	309.47	635.69	2.05	Si
SLV 3	143750	0.47	8485	-4774	309.47	666.44	2.15	Si
SLV 4	143750	0.47	8485	-4774	309.47	666.44	2.15	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 3.03 Wa = 0.05 Ta = 0.0855

Comb.	N top	N base	V orto	α_0	M*	e*	α_0^*	aLim	Verifica
SLV 1	-1793	-9810	-235	0	522.4	0.889	0	19.26035	No
SLV 2	-1793	-9810	-235	0	522.4	0.889	0	19.26035	No
SLV 8	-1918	-8198	-280	0	533.6	0.889	0	4.54431	No
SLV 13	-1861	-3290	350	0	528.4	0.889	0	19.26035	No
SLV 7	-1918	-8198	-280	0	533.6	0.889	0	4.54431	No
SLV 14	-1861	-3290	350	0	528.4	0.889	0	19.26035	No
SLV 3	-1840	-10119	-350	0	526.5	0.889	0	19.26035	No
SLV 10	-1783	-5211	279	0	521.4	0.889	0	4.54431	No
SLV 9	-1783	-5211	279	0	521.4	0.889	0	4.54431	No
SLV 4	-1840	-10119	-350	0	526.5	0.889	0	19.26035	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	3.666	SLU 81	Si
V_SLU	2.841	SLU 81	Si
PF_SLV	1.784	SLV 15	Si
V_SLV	1.516	SLV 15	Si
PFFP_SLV	1.928	SLV 11	Si
R_SLV	0	SLV 1	No

Maschio 20

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-2.153	-17.728	-2.783	-17.728	L2	L3	0.63	0.3	3.92	3.92	3.92			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 39	3.07	-4471	292.58	23662	998.88	3.414	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 39	4.07	-3852	-503.68	20389	909.47	1.806	Si
SLU 62	3.07	-4314	274.23	22830	977.65	3.565	Si
SLU 62	4.07	-3611	-465.45	19112	870.32	1.87	Si
SLU 63	3.07	-4314	274.23	22830	977.65	3.565	Si
SLU 63	4.07	-3611	-465.45	19112	870.32	1.87	Si
SLU 41	3.07	-4471	292.58	23662	998.88	3.414	Si
SLU 41	4.07	-3852	-503.68	20389	909.47	1.806	Si
SLU 84	3.07	-4872	313.69	25786	1048.54	3.343	Si
SLU 84	4.07	-4130	-535.89	21859	951.55	1.776	Si
SLU 82	3.07	-4872	313.69	25786	1048.54	3.343	Si
SLU 82	4.07	-4130	-535.89	21859	951.55	1.776	Si
SLU 40	3.07	-4471	292.58	23662	998.88	3.414	Si
SLU 40	4.07	-3852	-503.68	20389	909.47	1.806	Si
SLU 81	3.07	-4872	313.69	25786	1048.54	3.343	Si
SLU 81	4.07	-4130	-535.89	21859	951.55	1.776	Si
SLU 83	3.07	-4872	313.69	25786	1048.54	3.343	Si
SLU 83	4.07	-4130	-535.89	21859	951.55	1.776	Si
SLU 42	3.07	-4471	292.58	23662	998.88	3.414	Si
SLU 42	4.07	-3852	-503.68	20389	909.47	1.806	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 14	3.07	-2027	-139.8	10731	582.37	4.166	Si
SLV 14	4.07	-1048	234.78	5545	314.93	1.341	Si
SLV 16	3.07	-1999	-127.25	10578	574.87	4.518	Si
SLV 16	4.07	-1060	213.54	5611	318.51	1.492	Si
SLV 3	3.07	-3018	448.34	15974	826.15	1.843	Si
SLV 3	4.07	-3012	-748.93	15942	824.74	1.101	Si
SLV 1	3.07	-3047	435.8	16126	832.85	1.911	Si
SLV 1	4.07	-2999	-727.69	15875	821.83	1.129	Si
SLV 4	3.07	-3018	448.34	15974	826.15	1.843	Si
SLV 4	4.07	-3012	-748.93	15942	824.74	1.101	Si
SLV 15	3.07	-1999	-127.25	10578	574.87	4.518	Si
SLV 15	4.07	-1060	213.54	5611	318.51	1.492	Si
SLV 8	3.07	-2628	261.52	13907	733.25	2.804	Si
SLV 8	4.07	-2343	-436.86	12403	663.04	1.518	Si
SLV 2	3.07	-3047	435.8	16126	832.85	1.911	Si
SLV 2	4.07	-2999	-727.69	15875	821.83	1.129	Si
SLV 7	3.07	-2628	261.52	13907	733.25	2.804	Si
SLV 7	4.07	-2343	-436.86	12403	663.04	1.518	Si
SLV 13	3.07	-2027	-139.8	10731	582.37	4.166	Si
SLV 13	4.07	-1048	234.78	5545	314.93	1.341	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLU 41	3.07	-4471	709	292.58		23662	0.6298	8710	1646			2.32	Si
SLU 41	4.07	-3852	824	-503.68		23243	0.5525	8655	1434			1.74	Si
SLU 62	3.07	-4314	655	274.23		22830	0.6298	8600	1625			2.48	Si
SLU 62	4.07	-3611	756	-465.45		21571	0.558	8432	1411			1.87	Si
SLU 81	3.07	-4872	754	313.69		25786	0.6298	8994	1699			2.25	Si
SLU 81	4.07	-4130	874	-535.89		24785	0.5554	8860	1476			1.69	Si
SLU 42	3.07	-4471	709	292.58		23662	0.6298	8710	1646			2.32	Si
SLU 42	4.07	-3852	824	-503.68		23243	0.5525	8655	1434			1.74	Si
SLU 84	3.07	-4872	754	313.69		25786	0.6298	8994	1699			2.25	Si
SLU 84	4.07	-4130	874	-535.89		24785	0.5554	8860	1476			1.69	Si
SLU 82	3.07	-4872	754	313.69		25786	0.6298	8994	1699			2.25	Si
SLU 82	4.07	-4130	874	-535.89		24785	0.5554	8860	1476			1.69	Si
SLU 40	3.07	-4471	709	292.58		23662	0.6298	8710	1646			2.32	Si
SLU 40	4.07	-3852	824	-503.68		23243	0.5525	8655	1434			1.74	Si
SLU 63	3.07	-4314	655	274.23		22830	0.6298	8600	1625			2.48	Si
SLU 63	4.07	-3611	756	-465.45		21571	0.558	8432	1411			1.87	Si
SLU 83	3.07	-4872	754	313.69		25786	0.6298	8994	1699			2.25	Si
SLU 83	4.07	-4130	874	-535.89		24785	0.5554	8860	1476			1.69	Si
SLU 39	3.07	-4471	709	292.58		23662	0.6298	8710	1646			2.32	Si
SLU 39	4.07	-3852	824	-503.68		23243	0.5525	8655	1434			1.74	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLV 14	3.07	-2027	-574	-139.8		10731	0.6298	10479	1980			3.45	Si
SLV 14	4.07	-1048	-597	234.78		12821	0.2724	10898	890			1.49	Si
SLV 13	3.07	-2027	-574	-139.8		10731	0.6298	10479	1980			3.45	Si
SLV 13	4.07	-1048	-597	234.78		12821	0.2724	10898	890			1.49	Si
SLV 7	3.07	-2628	696	261.52		13907	0.6298	11115	2100			3.02	Si
SLV 7	4.07	-2343	816	-436.86		20266	0.3855	12386	1432			1.76	Si
SLV 4	3.07	-3018	1296	448.34		20159	0.499	12365	1851			1.43	Si
SLV 4	4.07	-3012	1426	-748.93		50514	0.1988	16250	969			0.68	No, Vu<V
SLV 1	3.07	-3047	1261	435.8		19697	0.5156	12273	1898			1.51	Si
SLV 1	4.07	-2999	1361	-727.69		46098	0.2169	16250	1057			0.78	No, Vu<V
SLV 8	3.07	-2628	696	261.52		13907	0.6298	11115	2100			3.02	Si
SLV 8	4.07	-2343	816	-436.86		20266	0.3855	12386	1432			1.76	Si
SLV 3	3.07	-3018	1296	448.34		20159	0.499	12365	1851			1.43	Si
SLV 3	4.07	-3012	1426	-748.93		50514	0.1988	16250	969			0.68	No, Vu<V
SLV 2	3.07	-3047	1261	435.8		19697	0.5156	12273	1898			1.51	Si
SLV 2	4.07	-2999	1361	-727.69		46098	0.2169	16250	1057			0.78	No, Vu<V
SLV 15	3.07	-1999	-538	-127.25		10578	0.6298	10449	1974			3.67	Si
SLV 15	4.07	-1060	-532	213.54		10380	0.3404	10409	1063			2	Si
SLV 16	3.07	-1999	-538	-127.25		10578	0.6298	10449	1974			3.67	Si
SLV 16	4.07	-1060	-532	213.54		10380	0.3404	10409	1063			2	Si



Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.03 Wa 0.05 denominatore 8 γM = 2

Comb.	fd	Sa	σ0	N	M	Mc	Coeff.s.	Verifica
SLV 7	143750	0.47	10004	-1890	103.91	260.32	2.51	Si
SLV 8	143750	0.47	10004	-1890	103.91	260.32	2.51	Si
SLV 4	143750	0.47	10018	-1893	103.91	260.64	2.51	Si
SLV 3	143750	0.47	10018	-1893	103.91	260.64	2.51	Si
SLV 12	143750	0.47	10208	-1929	103.91	265.14	2.55	Si
SLV 11	143750	0.47	10208	-1929	103.91	265.14	2.55	Si
SLV 1	143750	0.47	10233	-1933	103.91	265.73	2.56	Si
SLV 2	143750	0.47	10233	-1933	103.91	265.73	2.56	Si
SLV 16	143750	0.47	10697	-2021	103.91	276.62	2.66	Si
SLV 15	143750	0.47	10697	-2021	103.91	276.62	2.66	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.03 Wa = 0.05 Ta = 0.0855

Comb.	N top	N base	V orto	α0	M*	e*	a0*	aLim	Verifica
SLV 1	-724	2	14	0	0	0	0	19.26035	No, Trazione
SLV 4	-724	194	-4	0	0	0	0	19.26035	No, Trazione
SLV 2	-724	2	14	0	0	0	0	19.26035	No, Trazione
SLV 3	-724	194	-4	0	0	0	0	19.26035	No, Trazione
SLV 16	-634	-4978	-14	0.047	178.2	0.889	0.77639	19.26035	No
SLV 15	-634	-4978	-14	0.047	178.2	0.889	0.77639	19.26035	No
SLV 13	-633	-5170	4	0.055	178.2	0.889	0.89153	19.26035	No
SLV 14	-633	-5170	4	0.055	178.2	0.889	0.89153	19.26035	No
SLV 12	-665	-2944	-31	0.034	181.1	0.889	0.55641	4.54431	No
SLV 11	-665	-2944	-31	0.034	181.1	0.889	0.55641	4.54431	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	1.776	SLU 81	Si
V_SLU	1.69	SLU 81	Si
PF_SLV	1.101	SLV 3	Si
V_SLV	0.68	SLV 3	No
PFFP_SLV	2.505	SLV 7	Si
R_SLV	0	SLV 4	No

Maschio 21

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
0.227	-17.728	-0.753	-17.728	L2	L3	0.98	0.3	3.92	3.92	3.92			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ0	fv0	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 81	2.07	-7969	-119.96	27105	2605.44	21.719	Si
SLU 81	4.07	-5803	542.88	19739	2154.53	3.969	Si
SLU 42	2.07	-7210	-128.43	24524	2469.3	19.226	Si
SLU 42	4.07	-5427	518.33	18460	2056.71	3.968	Si
SLU 83	2.07	-7969	-119.96	27105	2605.44	21.719	Si
SLU 83	4.07	-5803	542.88	19739	2154.53	3.969	Si
SLU 39	2.07	-7210	-128.43	24524	2469.3	19.226	Si
SLU 39	4.07	-5427	518.33	18460	2056.71	3.968	Si
SLU 19	2.07	-6379	-105.57	21698	2293.22	21.722	Si
SLU 19	4.07	-4696	442.68	15972	1849.79	4.179	Si
SLU 41	2.07	-7210	-128.43	24524	2469.3	19.226	Si
SLU 41	4.07	-5427	518.33	18460	2056.71	3.968	Si
SLU 82	2.07	-7969	-119.96	27105	2605.44	21.719	Si
SLU 82	4.07	-5803	542.88	19739	2154.53	3.969	Si
SLU 40	2.07	-7210	-128.43	24524	2469.3	19.226	Si
SLU 40	4.07	-5427	518.33	18460	2056.71	3.968	Si
SLU 84	2.07	-7969	-119.96	27105	2605.44	21.719	Si
SLU 84	4.07	-5803	542.88	19739	2154.53	3.969	Si
SLU 18	2.07	-6379	-105.57	21698	2293.22	21.722	Si
SLU 18	4.07	-4696	442.68	15972	1849.79	4.179	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γM = 2

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLV 2	2.07	-4265	990.05	14506	1841.68	1.86	Si
SLV 2	4.07	-2017	-745.63	6860	932.76	1.251	Si
SLV 12	2.07	-4079	-346.2	13872	1771.58	5.117	Si
SLV 12	4.07	-2903	536.06	9875	1307.66	2.439	Si
SLV 3	2.07	-4115	979.87	13998	1785.5	1.822	Si
SLV 3	4.07	-1913	-749.49	6508	887.63	1.184	Si
SLV 15	2.07	-4327	-1041.96	14718	1864.88	1.79	Si
SLV 15	4.07	-3622	1235.19	12320	1595.84	1.292	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 16	2.07	-4327	-1041.96	14718	1864.88	1.79	Si
SLV 16	4.07	-3622	1235.19	12320	1595.84	1.292	Si
SLV 1	2.07	-4265	990.05	14506	1841.68	1.86	Si
SLV 1	4.07	-2017	-745.63	6860	932.76	1.251	Si
SLV 11	2.07	-4079	-346.2	13872	1771.58	5.117	Si
SLV 11	4.07	-2903	536.06	9875	1307.66	2.439	Si
SLV 13	2.07	-4477	-1031.77	15227	1920.19	1.861	Si
SLV 13	4.07	-3725	1239.05	12671	1636.14	1.32	Si
SLV 14	2.07	-4477	-1031.77	15227	1920.19	1.861	Si
SLV 14	4.07	-3725	1239.05	12671	1636.14	1.32	Si
SLV 4	2.07	-4115	979.87	13998	1785.5	1.822	Si
SLV 4	4.07	-1913	-749.49	6508	887.63	1.184	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 42	2.07	-7210	-158	-128.43		24524	0.98	8825	2595			16.39	Si
SLU 42	4.07	-5427	-218	518.33		18460	0.98	8017	2357			10.83	Si
SLU 41	2.07	-7210	-158	-128.43		24524	0.98	8825	2595			16.39	Si
SLU 41	4.07	-5427	-218	518.33		18460	0.98	8017	2357			10.83	Si
SLU 40	2.07	-7210	-158	-128.43		24524	0.98	8825	2595			16.39	Si
SLU 40	4.07	-5427	-218	518.33		18460	0.98	8017	2357			10.83	Si
SLU 63	2.07	-7138	-123	-97.1		24279	0.98	8793	2585			20.96	Si
SLU 63	4.07	-5072	-195	467.23		17251	0.98	7856	2310			11.87	Si
SLU 83	2.07	-7969	-152	-119.96		27105	0.98	9169	2696			17.76	Si
SLU 83	4.07	-5803	-226	542.88		19739	0.98	8187	2407			10.64	Si
SLU 39	2.07	-7210	-158	-128.43		24524	0.98	8825	2595			16.39	Si
SLU 39	4.07	-5427	-218	518.33		18460	0.98	8017	2357			10.83	Si
SLU 84	2.07	-7969	-152	-119.96		27105	0.98	9169	2696			17.76	Si
SLU 84	4.07	-5803	-226	542.88		19739	0.98	8187	2407			10.64	Si
SLU 62	2.07	-7138	-123	-97.1		24279	0.98	8793	2585			20.96	Si
SLU 62	4.07	-5072	-195	467.23		17251	0.98	7856	2310			11.87	Si
SLU 82	2.07	-7969	-152	-119.96		27105	0.98	9169	2696			17.76	Si
SLU 82	4.07	-5803	-226	542.88		19739	0.98	8187	2407			10.64	Si
SLU 81	2.07	-7969	-152	-119.96		27105	0.98	9169	2696			17.76	Si
SLU 81	4.07	-5803	-226	542.88		19739	0.98	8187	2407			10.64	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 13	2.07	-4477	-1297	-1031.77		19166	0.7786	12167	2842			2.19	Si
SLV 13	4.07	-3725	-717	1239.05		26297	0.4722	13593	1926			2.69	Si
SLV 16	2.07	-4327	-1346	-1041.96		19293	0.7476	12192	2734			2.03	Si
SLV 16	4.07	-3622	-715	1235.19		27014	0.4469	13736	1842			2.58	Si
SLV 14	2.07	-4477	-1297	-1031.77		19166	0.7786	12167	2842			2.19	Si
SLV 14	4.07	-3725	-717	1239.05		26297	0.4722	13593	1926			2.69	Si
SLV 11	2.07	-4079	-508	-346.2		13872	0.98	11108	3266			6.43	Si
SLV 11	4.07	-2903	-280	536.06		10564	0.9161	10446	2871			10.26	Si
SLV 1	2.07	-4265	1260	990.05		18377	0.7736	12009	2787			2.21	Si
SLV 1	4.07	-2017	519	-745.63		18629	0.3609	12059	1306			2.51	Si
SLV 15	2.07	-4327	-1346	-1041.96		19293	0.7476	12192	2734			2.03	Si
SLV 15	4.07	-3622	-715	1235.19		27014	0.4469	13736	1842			2.58	Si
SLV 3	2.07	-4115	1212	979.87		18153	0.7557	11964	2712			2.24	Si
SLV 3	4.07	-1913	521	-749.49		21628	0.2949	12659	1120			2.15	Si
SLV 4	2.07	-4115	1212	979.87		18153	0.7557	11964	2712			2.24	Si
SLV 4	4.07	-1913	521	-749.49		21628	0.2949	12659	1120			2.15	Si
SLV 12	2.07	-4079	-508	-346.2		13872	0.98	11108	3266			6.43	Si
SLV 12	4.07	-2903	-280	536.06		10564	0.9161	10446	2871			10.26	Si
SLV 2	2.07	-4265	1260	990.05		18377	0.7736	12009	2787			2.21	Si
SLV 2	4.07	-2017	519	-745.63		18629	0.3609	12059	1306			2.51	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.03 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 8	143750	0.47	11689	-3437	161.7	466.17	2.88	Si
SLV 7	143750	0.47	11689	-3437	161.7	466.17	2.88	Si
SLV 4	143750	0.47	11859	-3486	161.7	472.21	2.92	Si
SLV 3	143750	0.47	11859	-3486	161.7	472.21	2.92	Si
SLV 12	143750	0.47	11897	-3498	161.7	473.57	2.93	Si
SLV 11	143750	0.47	11897	-3498	161.7	473.57	2.93	Si
SLV 1	143750	0.47	12212	-3590	161.7	484.73	3	Si
SLV 2	143750	0.47	12212	-3590	161.7	484.73	3	Si
SLV 15	143750	0.47	12552	-3690	161.7	496.67	3.07	Si
SLV 16	143750	0.47	12552	-3690	161.7	496.67	3.07	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 3.03 Wa = 0.05 Ta = 0.0855

Comb.	N top	N base	V orto	α_0	M*	e*	α_0^*	α_{lim}	Verifica
SLV 1	-1102	-5942	22	0.047	287.8	0.889	0.7644	19.26035	No
SLV 2	-1102	-5942	22	0.047	287.8	0.889	0.7644	19.26035	No
SLV 16	-1089	-2888	-22	0.047	286.7	0.889	0.76531	19.26035	No
SLV 15	-1089	-2888	-22	0.047	286.7	0.889	0.76531	19.26035	No
SLV 13	-1102	-3034	-10	0.052	287.9	0.889	0.85487	19.26035	No
SLV 14	-1102	-3034	-10	0.052	287.9	0.889	0.85487	19.26035	No
SLV 4	-1089	-5797	10	0.052	286.6	0.889	0.85632	19.26035	No
SLV 3	-1089	-5797	10	0.052	286.6	0.889	0.85632	19.26035	No
SLV 5	-1117	-5094	24	0.045	289.2	0.889	0.74145	4.54431	No
SLV 6	-1117	-5094	24	0.045	289.2	0.889	0.74145	4.54431	No



Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	3.968	SLU 39	Si
V_SLU	10.641	SLU 81	Si
PF_SLV	1.184	SLV 3	Si
V_SLV	2.032	SLV 15	Si
PFFP_SLV	2.883	SLV 7	Si
R_SLV	0.04	SLV 1	No

Maschio 22

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
2.185	-17.729	1.227	-17.729	L2	L3	0.958	0.3	3.92	3.92	3.92			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 83	2.07	-3562	-55.87	12397	1446.13	25.882	Si
SLU 83	3.97	-4215	646.04	14671	1655.1	2.562	Si
SLU 40	2.07	-3050	-66.29	10614	1270.11	19.16	Si
SLU 40	3.97	-3925	620.09	13661	1564.44	2.523	Si
SLU 82	2.07	-3562	-55.87	12397	1446.13	25.882	Si
SLU 82	3.97	-4215	646.04	14671	1655.1	2.562	Si
SLU 84	2.07	-3562	-55.87	12397	1446.13	25.882	Si
SLU 84	3.97	-4215	646.04	14671	1655.1	2.562	Si
SLU 39	2.07	-3050	-66.29	10614	1270.11	19.16	Si
SLU 39	3.97	-3925	620.09	13661	1564.44	2.523	Si
SLU 21	2.07	-2811	-44.5	9784	1184.54	26.622	Si
SLU 21	3.97	-3401	525.6	11838	1392.14	2.649	Si
SLU 42	2.07	-3050	-66.29	10614	1270.11	19.16	Si
SLU 42	3.97	-3925	620.09	13661	1564.44	2.523	Si
SLU 81	2.07	-3562	-55.87	12397	1446.13	25.882	Si
SLU 81	3.97	-4215	646.04	14671	1655.1	2.562	Si
SLU 20	2.07	-2811	-44.5	9784	1184.54	26.622	Si
SLU 20	3.97	-3401	525.6	11838	1392.14	2.649	Si
SLU 41	2.07	-3050	-66.29	10614	1270.11	19.16	Si
SLU 41	3.97	-3925	620.09	13661	1564.44	2.523	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 16	2.07	-1054	-763.72	0	0	0	No, $e \geq l/2$
SLV 16	3.97	-3221	880.32	11209	1400.86	1.591	Si
SLV 2	2.07	-3375	749.16	11746	1460.82	1.95	Si
SLV 2	3.97	-945	-304.94	3288	440.29	1.444	Si
SLV 11	2.07	-1468	-263.67	5108	673.45	2.554	Si
SLV 11	3.97	-2427	532.65	8447	1081.91	2.031	Si
SLV 13	2.07	-1317	-744.29	0	0	0	No, $e \geq l/2$
SLV 13	3.97	-3219	836.03	11203	1400.13	1.675	Si
SLV 4	2.07	-3112	729.74	10831	1358.24	1.861	Si
SLV 4	3.97	-947	-260.65	3295	441.14	1.692	Si
SLV 14	2.07	-1317	-744.29	0	0	0	No, $e \geq l/2$
SLV 14	3.97	-3219	836.03	11203	1400.13	1.675	Si
SLV 15	2.07	-1054	-763.72	0	0	0	No, $e \geq l/2$
SLV 15	3.97	-3221	880.32	11209	1400.86	1.591	Si
SLV 1	2.07	-3375	749.16	11746	1460.82	1.95	Si
SLV 1	3.97	-945	-304.94	3288	440.29	1.444	Si
SLV 12	2.07	-1468	-263.67	5108	673.45	2.554	Si
SLV 12	3.97	-2427	532.65	8447	1081.91	2.031	Si
SLV 3	2.07	-3112	729.74	10831	1358.24	1.861	Si
SLV 3	3.97	-947	-260.65	3295	441.14	1.692	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 83	2.07	-3562	-870	-55.87	12397	0.9578	7208	2071				2.38	Si
SLU 83	3.97	-4215	-870	646.04	14671	0.9578	7512	2158				2.48	Si
SLU 42	2.07	-3050	-842	-66.29	10614	0.9578	6971	2003				2.38	Si
SLU 42	3.97	-3925	-842	620.09	13661	0.9578	7377	2120				2.52	Si
SLU 82	2.07	-3562	-870	-55.87	12397	0.9578	7208	2071				2.38	Si
SLU 82	3.97	-4215	-870	646.04	14671	0.9578	7512	2158				2.48	Si
SLU 40	2.07	-3050	-842	-66.29	10614	0.9578	6971	2003				2.38	Si
SLU 40	3.97	-3925	-842	620.09	13661	0.9578	7377	2120				2.52	Si
SLU 39	2.07	-3050	-842	-66.29	10614	0.9578	6971	2003				2.38	Si
SLU 39	3.97	-3925	-842	620.09	13661	0.9578	7377	2120				2.52	Si
SLU 75	2.07	-3313	-733	-39.58	11529	0.9578	7093	2038				2.78	Si
SLU 75	3.97	-3665	-734	546.7	12755	0.9578	7256	2085				2.84	Si
SLU 77	2.07	-3313	-733	-39.58	11529	0.9578	7093	2038				2.78	Si
SLU 77	3.97	-3665	-734	546.7	12755	0.9578	7256	2085				2.84	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 81	2.07	-3562	-870	-55.87		12397	0.9578	7208	2071			2.38	Si
SLU 81	3.97	-4215	-870	646.04		14671	0.9578	7512	2158			2.48	Si
SLU 41	2.07	-3050	-842	-66.29		10614	0.9578	6971	2003			2.38	Si
SLU 41	3.97	-3925	-842	620.09		13661	0.9578	7377	2120			2.52	Si
SLU 84	2.07	-3562	-870	-55.87		12397	0.9578	7208	2071			2.38	Si
SLU 84	3.97	-4215	-870	646.04		14671	0.9578	7512	2158			2.48	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 14	2.07	-1317	-1632	-744.29		0	0	8333	0			0	No, Vu<V
SLV 14	3.97	-3219	-1419	836.03		16320	0.6575	11597	2287			1.61	Si
SLV 4	2.07	-3112	872	729.74		14149	0.7332	11163	2455			2.81	Si
SLV 4	3.97	-947	659	-260.65		5168	0.6107	9367	1716			2.6	Si
SLV 12	2.07	-1468	-993	-263.67		5450	0.8977	9423	2538			2.56	Si
SLV 12	3.97	-2427	-899	532.65		10395	0.7782	10412	2431			2.7	Si
SLV 13	2.07	-1317	-1632	-744.29		0	0	8333	0			0	No, Vu<V
SLV 13	3.97	-3219	-1419	836.03		16320	0.6575	11597	2287			1.61	Si
SLV 15	2.07	-1054	-1762	-763.72		0	0	8333	0			0	No, Vu<V
SLV 15	3.97	-3221	-1533	880.32		17410	0.6167	11815	2186			1.43	Si
SLV 11	2.07	-1468	-993	-263.67		5450	0.8977	9423	2538			2.56	Si
SLV 11	3.97	-2427	-899	532.65		10395	0.7782	10412	2431			2.7	Si
SLV 2	2.07	-3375	1003	749.16		14597	0.7707	11253	2602			2.59	Si
SLV 2	3.97	-945	773	-304.94		6724	0.4684	9678	1360			1.76	Si
SLV 3	2.07	-3112	872	729.74		14149	0.7332	11163	2455			2.81	Si
SLV 3	3.97	-947	659	-260.65		5168	0.6107	9367	1716			2.6	Si
SLV 1	2.07	-3375	1003	749.16		14597	0.7707	11253	2602			2.59	Si
SLV 1	3.97	-945	773	-304.94		6724	0.4684	9678	1360			1.76	Si
SLV 16	2.07	-1054	-1762	-763.72		0	0	8333	0			0	No, Vu<V
SLV 16	3.97	-3221	-1533	880.32		17410	0.6167	11815	2186			1.43	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.03 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 3	143750	0.47	5923	-1702	158.03	242.91	1.54	Si
SLV 4	143750	0.47	5923	-1702	158.03	242.91	1.54	Si
SLV 1	143750	0.47	6143	-1765	158.03	251.44	1.59	Si
SLV 2	143750	0.47	6143	-1765	158.03	251.44	1.59	Si
SLV 8	143750	0.47	6776	-1947	158.03	275.85	1.75	Si
SLV 7	143750	0.47	6776	-1947	158.03	275.85	1.75	Si
SLV 5	143750	0.47	7508	-2157	158.03	303.7	1.92	Si
SLV 6	143750	0.47	7508	-2157	158.03	303.7	1.92	Si
SLV 11	143750	0.47	7727	-2220	158.03	311.96	1.97	Si
SLV 12	143750	0.47	7727	-2220	158.03	311.96	1.97	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 3.03 Wa = 0.05 Ta = 0.0855

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 9	-961	-3019	150	0	270.8	0.889	0	4.54431	No
SLV 13	-972	-2980	306	0	271.8	0.889	0	19.26035	No
SLV 7	-824	-1917	-150	0	258.6	0.89	0	4.54431	No
SLV 14	-972	-2980	306	0	271.8	0.889	0	19.26035	No
SLV 10	-961	-3019	150	0	270.8	0.889	0	4.54431	No
SLV 2	-841	-2218	-267	0	260.2	0.89	0	19.26035	No
SLV 1	-841	-2218	-267	0	260.2	0.89	0	19.26035	No
SLV 4	-812	-1956	-306	0	257.6	0.89	0	19.26035	No
SLV 8	-824	-1917	-150	0	258.6	0.89	0	4.54431	No
SLV 3	-812	-1956	-306	0	257.6	0.89	0	19.26035	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	2.523	SLU 39	Si
V_SLU	2.379	SLU 39	Si
PF_SLV	0	SLV 13	No
V_SLV	0	SLV 13	No
PFFP_SLV	1.537	SLV 3	Si
R_SLV	0	SLV 1	No

Maschio 23

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-3.415	-13.248	-3.925	-13.248	L2	L3	0.51	0.3	3.92	3.92	3.92			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 48	1.07	-2753	-6.36	17981	547.41	86.058	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 48	3.17	-2110	6.21	13780	447.29	71.98	Si
SLU 47	1.07	-2753	-6.36	17981	547.41	86.058	Si
SLU 47	3.17	-2110	6.21	13780	447.29	71.98	Si
SLU 43	1.07	-2753	-6.36	17981	547.41	86.058	Si
SLU 43	3.17	-2110	6.21	13780	447.29	71.98	Si
SLU 49	1.07	-2753	-6.36	17981	547.41	86.058	Si
SLU 49	3.17	-2110	6.21	13780	447.29	71.98	Si
SLU 44	1.07	-2753	-6.36	17981	547.41	86.058	Si
SLU 44	3.17	-2110	6.21	13780	447.29	71.98	Si
SLU 45	1.07	-2753	-6.36	17981	547.41	86.058	Si
SLU 45	3.17	-2110	6.21	13780	447.29	71.98	Si
SLU 46	1.07	-2753	-6.36	17981	547.41	86.058	Si
SLU 46	3.17	-2110	6.21	13780	447.29	71.98	Si
SLU 68	1.07	-3046	-7.12	19895	587.42	82.538	Si
SLU 68	3.17	-2678	6.94	17491	536.6	77.316	Si
SLU 50	1.07	-2753	-6.36	17981	547.41	86.058	Si
SLU 50	3.17	-2110	6.21	13780	447.29	71.98	Si
SLU 51	1.07	-2753	-6.36	17981	547.41	86.058	Si
SLU 51	3.17	-2110	6.21	13780	447.29	71.98	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 11	1.07	-2480	-131.07	16196	548.87	4.188	Si
SLV 11	3.17	-2297	99.31	15002	514.15	5.177	Si
SLV 15	1.07	-2475	-399.02	16166	548.01	1.373	Si
SLV 15	3.17	-2300	300.25	15021	514.71	1.714	Si
SLV 13	1.07	-2474	-394.15	16159	547.8	1.39	Si
SLV 13	3.17	-2305	296.71	15056	515.72	1.738	Si
SLV 2	1.07	-2484	387.68	16221	549.6	1.418	Si
SLV 2	3.17	-2314	-289.2	15116	517.51	1.789	Si
SLV 14	1.07	-2474	-394.15	16159	547.8	1.39	Si
SLV 14	3.17	-2305	296.71	15056	515.72	1.738	Si
SLV 12	1.07	-2480	-131.07	16196	548.87	4.188	Si
SLV 12	3.17	-2297	99.31	15002	514.15	5.177	Si
SLV 3	1.07	-2485	382.81	16228	549.81	1.436	Si
SLV 3	3.17	-2309	-285.66	15082	516.5	1.808	Si
SLV 16	1.07	-2475	-399.02	16166	548.01	1.373	Si
SLV 16	3.17	-2300	300.25	15021	514.71	1.714	Si
SLV 4	1.07	-2485	382.81	16228	549.81	1.436	Si
SLV 4	3.17	-2309	-285.66	15082	516.5	1.808	Si
SLV 1	1.07	-2484	387.68	16221	549.6	1.418	Si
SLV 1	3.17	-2314	-289.2	15116	517.51	1.789	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLU 75	1.07	-3748	-8	-8.39		24482	0.5103	8820	1350			168.83	Si
SLU 75	3.17	-3980	-8	8.15		25995	0.5103	9022	1381			173.44	Si
SLU 73	1.07	-3748	-8	-8.39		24482	0.5103	8820	1350			168.83	Si
SLU 73	3.17	-3980	-8	8.15		25995	0.5103	9022	1381			173.44	Si
SLU 76	1.07	-3748	-8	-8.39		24482	0.5103	8820	1350			168.83	Si
SLU 76	3.17	-3980	-8	8.15		25995	0.5103	9022	1381			173.44	Si
SLU 83	1.07	-4049	-9	-8.93		26448	0.5103	9082	1390			163.04	Si
SLU 83	3.17	-4538	-8	8.67		29640	0.5103	9508	1456			171.43	Si
SLU 78	1.07	-3748	-8	-8.39		24482	0.5103	8820	1350			168.83	Si
SLU 78	3.17	-3980	-8	8.15		25995	0.5103	9022	1381			173.44	Si
SLU 74	1.07	-3748	-8	-8.39		24482	0.5103	8820	1350			168.83	Si
SLU 74	3.17	-3980	-8	8.15		25995	0.5103	9022	1381			173.44	Si
SLU 82	1.07	-4049	-9	-8.93		26448	0.5103	9082	1390			163.04	Si
SLU 82	3.17	-4538	-8	8.67		29640	0.5103	9508	1456			171.43	Si
SLU 84	1.07	-4049	-9	-8.93		26448	0.5103	9082	1390			163.04	Si
SLU 84	3.17	-4538	-8	8.67		29640	0.5103	9508	1456			171.43	Si
SLU 81	1.07	-4049	-9	-8.93		26448	0.5103	9082	1390			163.04	Si
SLU 81	3.17	-4538	-8	8.67		29640	0.5103	9508	1456			171.43	Si
SLU 79	1.07	-3748	-8	-8.39		24482	0.5103	8820	1350			168.83	Si
SLU 79	3.17	-3980	-8	8.15		25995	0.5103	9022	1381			173.44	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLV 12	1.07	-2480	-153	-131.07		16196	0.5103	11573	1772			11.6	Si
SLV 12	3.17	-2297	-81	99.31		15002	0.5103	11334	1735			21.39	Si
SLV 1	1.07	-2484	485	387.68		27853	0.2972	13904	1240			2.56	Si
SLV 1	3.17	-2314	247	-289.2		19748	0.3906	12283	1440			5.83	Si
SLV 4	1.07	-2485	484	382.81		27306	0.3033	13794	1255			2.59	Si
SLV 4	3.17	-2309	247	-285.66		19516	0.3944	12237	1448			5.86	Si
SLV 15	1.07	-2475	-495	-399.02		29270	0.2819	14187	1200			2.42	Si
SLV 15	3.17	-2300	-258	300.25		20505	0.3739	12434	1395			5.41	Si
SLV 3	1.07	-2485	484	382.81		27306	0.3033	13794	1255			2.59	Si
SLV 3	3.17	-2309	247	-285.66		19516	0.3944	12237	1448			5.86	Si
SLV 11	1.07	-2480	-153	-131.07		16196	0.5103	11573	1772			11.6	Si
SLV 11	3.17	-2297	-81	99.31		15002	0.5103	11334	1735			21.39	Si
SLV 2	1.07	-2484	485	387.68		27853	0.2972	13904	1240			2.56	Si
SLV 2	3.17	-2314	247	-289.2		19748	0.3906	12283	1440			5.83	Si
SLV 14	1.07	-2474	-495	-394.15		28677	0.2876	14069	1214			2.45	Si
SLV 14	3.17	-2305	-258	296.71		20254	0.3794	12384	1409			5.47	Si
SLV 13	1.07	-2474	-495	-394.15		28677	0.2876	14069	1214			2.45	Si
SLV 13	3.17	-2305	-258	296.71		20254	0.3794	12384	1409			5.47	Si
SLV 16	1.07	-2475	-495	-399.02		29270	0.2819	14187	1200			2.42	Si
SLV 16	3.17	-2300	-258	300.25		20505	0.3739	12434	1395			5.41	Si



Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.03 Wa 0.05 denominatore 8 γM = 2

Comb.	fd	Sa	σ0	N	M	Mc	Coeff.s.	Verifica
SLV 12	143750	0.47	15002	-2297	86.04	302.24	3.51	Si
SLV 11	143750	0.47	15002	-2297	86.04	302.24	3.51	Si
SLV 8	143750	0.47	15021	-2300	86.04	302.55	3.52	Si
SLV 7	143750	0.47	15021	-2300	86.04	302.55	3.52	Si
SLV 16	143750	0.47	15021	-2300	86.04	302.56	3.52	Si
SLV 15	143750	0.47	15021	-2300	86.04	302.56	3.52	Si
SLV 13	143750	0.47	15056	-2305	86.04	303.16	3.52	Si
SLV 14	143750	0.47	15056	-2305	86.04	303.16	3.52	Si
SLV 4	143750	0.47	15082	-2309	86.04	303.61	3.53	Si
SLV 3	143750	0.47	15082	-2309	86.04	303.61	3.53	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.03 Wa = 0.05 Ta = 0.0855

Comb.	N top	N base	V orto	α0	M*	e*	a0*	aLim	Verifica
SLV 9	-662	-2476	119	0	158.1	0.89	0	4.54431	No
SLV 12	-646	-2480	-120	0	156.6	0.89	0	4.54431	No
SLV 8	-646	-2483	-119	0	156.6	0.89	0	4.54431	No
SLV 6	-662	-2479	120	0	158.1	0.89	0	4.54431	No
SLV 5	-662	-2479	120	0	158.1	0.89	0	4.54431	No
SLV 10	-662	-2476	119	0	158.1	0.89	0	4.54431	No
SLV 11	-646	-2480	-120	0	156.6	0.89	0	4.54431	No
SLV 7	-646	-2483	-119	0	156.6	0.89	0	4.54431	No
SLV 15	-652	-2475	-36	0.025	157.2	0.89	0.41	19.26035	No
SLV 16	-652	-2475	-36	0.025	157.2	0.89	0.41	19.26035	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	71.98	SLU 43	Si
V_SLU	163.036	SLU 81	Si
PF_SLV	1.373	SLV 15	Si
V_SLV	2.421	SLV 15	Si
PFFP_SLV	3.513	SLV 11	Si
R_SLV	0	SLV 5	No

Maschio 24

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s,sx	a.s,dx
-7.101	-8.718	-9.428	-8.718	L2	L3	2.327	0.3	3.92	3.92	3.92			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ0	fv0	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 21	2.07	-7907	-981.33	11326	7920.33	8.071	Si
SLU 21	3.97	-6818	-1440.64	9766	6981.31	4.846	Si
SLU 40	2.07	-8734	-1093.8	12511	8601.19	7.864	Si
SLU 40	3.97	-7843	-1683.85	11235	7866.84	4.672	Si
SLU 20	2.07	-7907	-981.33	11326	7920.33	8.071	Si
SLU 20	3.97	-6818	-1440.64	9766	6981.31	4.846	Si
SLU 81	2.07	-9974	-1209.77	14287	9569.17	7.91	Si
SLU 81	3.97	-8451	-1767.66	12105	8371.17	4.736	Si
SLU 39	2.07	-8734	-1093.8	12511	8601.19	7.864	Si
SLU 39	3.97	-7843	-1683.85	11235	7866.84	4.672	Si
SLU 84	2.07	-9974	-1209.77	14287	9569.17	7.91	Si
SLU 84	3.97	-8451	-1767.66	12105	8371.17	4.736	Si
SLU 41	2.07	-8734	-1093.8	12511	8601.19	7.864	Si
SLU 41	3.97	-7843	-1683.85	11235	7866.84	4.672	Si
SLU 42	2.07	-8734	-1093.8	12511	8601.19	7.864	Si
SLU 42	3.97	-7843	-1683.85	11235	7866.84	4.672	Si
SLU 83	2.07	-9974	-1209.77	14287	9569.17	7.91	Si
SLU 83	3.97	-8451	-1767.66	12105	8371.17	4.736	Si
SLU 82	2.07	-9974	-1209.77	14287	9569.17	7.91	Si
SLU 82	3.97	-8451	-1767.66	12105	8371.17	4.736	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γM = 2

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLV 3	2.07	-5849	357.9	8379	6338.72	17.711	Si
SLV 3	3.97	-4948	-1527.64	7088	5422.97	3.55	Si
SLV 15	2.07	-6357	-1656.16	9106	6844.67	4.133	Si
SLV 15	3.97	-3591	-153.09	5144	4002.2	26.142	Si
SLV 13	2.07	-5912	-1638.86	8468	6401.44	3.906	Si
SLV 13	3.97	-3481	-79.34	4986	3884.31	48.957	Si
SLV 2	2.07	-5404	375.21	7741	5889.34	15.696	Si
SLV 2	3.97	-4837	-1453.89	6930	5309.17	3.652	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 8	2.07	-6546	-367.21	9377	7031.55	19.148	Si
SLV 8	3.97	-4602	-1132.59	6592	5065.44	4.472	Si
SLV 4	2.07	-5849	357.9	8379	6338.72	17.711	Si
SLV 4	3.97	-4948	-1527.64	7088	5422.97	3.55	Si
SLV 7	2.07	-6546	-367.21	9377	7031.55	19.148	Si
SLV 7	3.97	-4602	-1132.59	6592	5065.44	4.472	Si
SLV 1	2.07	-5404	375.21	7741	5889.34	15.696	Si
SLV 1	3.97	-4837	-1453.89	6930	5309.17	3.652	Si
SLV 14	2.07	-5912	-1638.86	8468	6401.44	3.906	Si
SLV 14	3.97	-3481	-79.34	4986	3884.31	48.957	Si
SLV 16	2.07	-6357	-1656.16	9106	6844.67	4.133	Si
SLV 16	3.97	-3591	-153.09	5144	4002.2	26.142	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 84	2.07	-9974	1321	-1209.77		14287	2.327	7461	5208			3.94	Si
SLU 84	3.97	-8451	1321	-1767.66		12105	2.327	7170	5005			3.79	Si
SLU 40	2.07	-8734	1284	-1093.8		12511	2.327	7224	5043			3.93	Si
SLU 40	3.97	-7843	1284	-1683.85		11235	2.327	7054	4924			3.84	Si
SLU 82	2.07	-9974	1321	-1209.77		14287	2.327	7461	5208			3.94	Si
SLU 82	3.97	-8451	1321	-1767.66		12105	2.327	7170	5005			3.79	Si
SLU 81	2.07	-9974	1321	-1209.77		14287	2.327	7461	5208			3.94	Si
SLU 81	3.97	-8451	1321	-1767.66		12105	2.327	7170	5005			3.79	Si
SLU 77	2.07	-9125	1109	-1069.9		13072	2.327	7298	5095			4.59	Si
SLU 77	3.97	-7365	1109	-1502.68		10549	2.327	6962	4860			4.38	Si
SLU 83	2.07	-9974	1321	-1209.77		14287	2.327	7461	5208			3.94	Si
SLU 83	3.97	-8451	1321	-1767.66		12105	2.327	7170	5005			3.79	Si
SLU 42	2.07	-8734	1284	-1093.8		12511	2.327	7224	5043			3.93	Si
SLU 42	3.97	-7843	1284	-1683.85		11235	2.327	7054	4924			3.84	Si
SLU 41	2.07	-8734	1284	-1093.8		12511	2.327	7224	5043			3.93	Si
SLU 41	3.97	-7843	1284	-1683.85		11235	2.327	7054	4924			3.84	Si
SLU 39	2.07	-8734	1284	-1093.8		12511	2.327	7224	5043			3.93	Si
SLU 39	3.97	-7843	1284	-1683.85		11235	2.327	7054	4924			3.84	Si
SLU 75	2.07	-9125	1109	-1069.9		13072	2.327	7298	5095			4.59	Si
SLU 75	3.97	-7365	1109	-1502.68		10549	2.327	6962	4860			4.38	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ0	σN	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 4	2.07	-5849	2217	357.9		8379	2.327	10009	6987			3.15	Si
SLV 4	3.97	-4948	1700	-1527.64		7088	2.327	9751	6807			4	Si
SLV 14	2.07	-5912	-1080	-1638.86		8468	2.327	10027	7000			6.48	Si
SLV 14	3.97	-3481	-564	-79.34		4986	2.327	9330	6514			11.56	Si
SLV 5	2.07	-5063	1260	-309.52		7252	2.327	9784	6830			5.42	Si
SLV 5	3.97	-4234	1200	-886.75		6065	2.327	9546	6664			5.55	Si
SLV 2	2.07	-5404	2325	375.21		7741	2.327	9882	6898			2.97	Si
SLV 2	3.97	-4837	1861	-1453.89		6930	2.327	9719	6785			3.65	Si
SLV 3	2.07	-5849	2217	357.9		8379	2.327	10009	6987			3.15	Si
SLV 3	3.97	-4948	1700	-1527.64		7088	2.327	9751	6807			4	Si
SLV 6	2.07	-5063	1260	-309.52		7252	2.327	9784	6830			5.42	Si
SLV 6	3.97	-4234	1200	-886.75		6065	2.327	9546	6664			5.55	Si
SLV 15	2.07	-6357	-1189	-1656.16		9106	2.327	10154	7089			5.96	Si
SLV 15	3.97	-3591	-725	-153.09		5144	2.327	9362	6536			9.02	Si
SLV 13	2.07	-5912	-1080	-1638.86		8468	2.327	10027	7000			6.48	Si
SLV 13	3.97	-3481	-564	-79.34		4986	2.327	9330	6514			11.56	Si
SLV 1	2.07	-5404	2325	375.21		7741	2.327	9882	6898			2.97	Si
SLV 1	3.97	-4837	1861	-1453.89		6930	2.327	9719	6785			3.65	Si
SLV 16	2.07	-6357	-1189	-1656.16		9106	2.327	10154	7089			5.96	Si
SLV 16	3.97	-3591	-725	-153.09		5144	2.327	9362	6536			9.02	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.03 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 14	143750	0.47	6396	-4465	383.94	634.65	1.65	Si
SLV 13	143750	0.47	6396	-4465	383.94	634.65	1.65	Si
SLV 10	143750	0.47	6407	-4472	383.94	635.69	1.66	Si
SLV 9	143750	0.47	6407	-4472	383.94	635.69	1.66	Si
SLV 15	143750	0.47	6708	-4683	383.94	663.84	1.73	Si
SLV 16	143750	0.47	6708	-4683	383.94	663.84	1.73	Si
SLV 6	143750	0.47	6728	-4697	383.94	665.75	1.73	Si
SLV 5	143750	0.47	6728	-4697	383.94	665.75	1.73	Si
SLV 12	143750	0.47	7447	-5199	383.94	732.31	1.91	Si
SLV 11	143750	0.47	7447	-5199	383.94	732.31	1.91	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.03 Wa = 0.05 Ta = 0.0855

Comb.	N top	N base	V orto	α_0	M*	e*	α_0^*	α_{lim}	Verifica
SLV 14	-2215	-6075	266	0.001	647.2	0.889	0.02427	19.26035	No
SLV 13	-2215	-6075	266	0.001	647.2	0.889	0.02427	19.26035	No
SLV 4	-2351	-7497	-266	0.003	659.4	0.889	0.04127	19.26035	No
SLV 3	-2351	-7497	-266	0.003	659.4	0.889	0.04127	19.26035	No
SLV 16	-2258	-6588	233	0.009	651.1	0.889	0.14479	19.26035	No
SLV 15	-2258	-6588	233	0.009	651.1	0.889	0.14479	19.26035	No
SLV 2	-2308	-6984	-233	0.009	655.5	0.889	0.14987	19.26035	No
SLV 1	-2308	-6984	-233	0.009	655.5	0.889	0.14987	19.26035	No
SLV 10	-2197	-5795	130	0.031	645.7	0.889	0.499	4.54431	No
SLV 9	-2197	-5795	130	0.031	645.7	0.889	0.499	4.54431	No



Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	4.672	SLU 39	Si
V_SLU	3.79	SLU 81	Si
PF_SLV	3.55	SLV 3	Si
V_SLV	2.967	SLV 1	Si
PFFP_SLV	1.653	SLV 13	Si
R_SLV	0.001	SLV 13	No

Maschio 25

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-1.141	-8.718	-6.101	-8.718	L2	L3	4.96	0.3	3.92	3.92	3.92			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 38	2.07	-19395	-131.14	13034	40402.97	308.088	Si
SLU 38	3.97	-15235	-44.25	10239	33034.7	746.548	Si
SLU 83	2.07	-24468	-163.06	16443	48430.68	297.002	Si
SLU 83	3.97	-19047	-55.73	12801	39814.54	714.413	Si
SLU 42	2.07	-21627	-149.2	14534	44065.5	295.347	Si
SLU 42	3.97	-17690	-48.91	11888	37468.07	766.075	Si
SLU 81	2.07	-24468	-163.06	16443	48430.68	297.002	Si
SLU 81	3.97	-19047	-55.73	12801	39814.54	714.413	Si
SLU 41	2.07	-21627	-149.2	14534	44065.5	295.347	Si
SLU 41	3.97	-17690	-48.91	11888	37468.07	766.075	Si
SLU 37	2.07	-19395	-131.14	13034	40402.97	308.088	Si
SLU 37	3.97	-15235	-44.25	10239	33034.7	746.548	Si
SLU 39	2.07	-21627	-149.2	14534	44065.5	295.347	Si
SLU 39	3.97	-17690	-48.91	11888	37468.07	766.075	Si
SLU 82	2.07	-24468	-163.06	16443	48430.68	297.002	Si
SLU 82	3.97	-19047	-55.73	12801	39814.54	714.413	Si
SLU 40	2.07	-21627	-149.2	14534	44065.5	295.347	Si
SLU 40	3.97	-17690	-48.91	11888	37468.07	766.075	Si
SLU 84	2.07	-24468	-163.06	16443	48430.68	297.002	Si
SLU 84	3.97	-19047	-55.73	12801	39814.54	714.413	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 1	2.07	-13987	5418.51	9400	32018.63	5.909	Si
SLV 1	3.97	-9454	-2487.29	6354	22227.61	8.936	Si
SLV 4	2.07	-14238	5396.82	9569	32545.37	6.03	Si
SLV 4	3.97	-9489	-2512.58	6377	22304.6	8.877	Si
SLV 15	2.07	-14216	-5592.07	9554	32499.74	5.812	Si
SLV 15	3.97	-9513	2421.42	6393	22358.46	9.234	Si
SLV 16	2.07	-14216	-5592.07	9554	32499.74	5.812	Si
SLV 16	3.97	-9513	2421.42	6393	22358.46	9.234	Si
SLV 13	2.07	-13965	-5570.38	9385	31972.85	5.74	Si
SLV 13	3.97	-9479	2446.7	6370	22281.49	9.107	Si
SLV 9	2.07	-13679	-1698.96	9193	31372.06	18.465	Si
SLV 9	3.97	-9430	749.31	6337	22172.79	29.591	Si
SLV 14	2.07	-13965	-5570.38	9385	31972.85	5.74	Si
SLV 14	3.97	-9479	2446.7	6370	22281.49	9.107	Si
SLV 10	2.07	-13679	-1698.96	9193	31372.06	18.465	Si
SLV 10	3.97	-9430	749.31	6337	22172.79	29.591	Si
SLV 3	2.07	-14238	5396.82	9569	32545.37	6.03	Si
SLV 3	3.97	-9489	-2512.58	6377	22304.6	8.877	Si
SLV 2	2.07	-13987	5418.51	9400	32018.63	5.909	Si
SLV 2	3.97	-9454	-2487.29	6354	22227.61	8.936	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 75	2.07	-22235	-41	-145.01		14943	4.96	7548	11231			274.04	Si
SLU 75	3.97	-16593	-41	-51.07		11151	4.96	7042	10479			255.71	Si
SLU 82	2.07	-24468	-42	-163.06		16443	4.96	7748	11529			271.76	Si
SLU 82	3.97	-19047	-42	-55.73		12801	4.96	7262	10806			254.75	Si
SLU 81	2.07	-24468	-42	-163.06		16443	4.96	7748	11529			271.76	Si
SLU 81	3.97	-19047	-42	-55.73		12801	4.96	7262	10806			254.75	Si
SLU 80	2.07	-22235	-41	-145.01		14943	4.96	7548	11231			274.04	Si
SLU 80	3.97	-16593	-41	-51.07		11151	4.96	7042	10479			255.71	Si
SLU 78	2.07	-22235	-41	-145.01		14943	4.96	7548	11231			274.04	Si
SLU 78	3.97	-16593	-41	-51.07		11151	4.96	7042	10479			255.71	Si
SLU 73	2.07	-22235	-41	-145.01		14943	4.96	7548	11231			274.04	Si
SLU 73	3.97	-16593	-41	-51.07		11151	4.96	7042	10479			255.71	Si
SLU 74	2.07	-22235	-41	-145.01		14943	4.96	7548	11231			274.04	Si
SLU 74	3.97	-16593	-41	-51.07		11151	4.96	7042	10479			255.71	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 84	2.07	-24468	-42	-163.06		16443	4.96	7748	11529			271.76	Si
SLU 84	3.97	-19047	-42	-55.73		12801	4.96	7262	10806			254.75	Si
SLU 83	2.07	-24468	-42	-163.06		16443	4.96	7748	11529			271.76	Si
SLU 83	3.97	-19047	-42	-55.73		12801	4.96	7262	10806			254.75	Si
SLU 77	2.07	-22235	-41	-145.01		14943	4.96	7548	11231			274.04	Si
SLU 77	3.97	-16593	-41	-51.07		11151	4.96	7042	10479			255.71	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 14	2.07	-13965	-4647	-5570.38		9385	4.96	10210	15193			3.27	Si
SLV 14	3.97	-9479	-3686	2446.7		6370	4.96	9607	14296			3.88	Si
SLV 4	2.07	-14238	4588	5396.82		9569	4.96	10247	15248			3.32	Si
SLV 4	3.97	-9489	3628	-2512.58		6377	4.96	9609	14298			3.94	Si
SLV 13	2.07	-13965	-4647	-5570.38		9385	4.96	10210	15193			3.27	Si
SLV 13	3.97	-9479	-3686	2446.7		6370	4.96	9607	14296			3.88	Si
SLV 15	2.07	-14216	-4636	-5592.07		9554	4.96	10244	15243			3.29	Si
SLV 15	3.97	-9513	-3723	2421.42		6393	4.96	9612	14303			3.84	Si
SLV 2	2.07	-13987	4578	5418.51		9400	4.96	10213	15197			3.32	Si
SLV 2	3.97	-9454	3664	-2487.29		6354	4.96	9604	14291			3.9	Si
SLV 16	2.07	-14216	-4636	-5592.07		9554	4.96	10244	15243			3.29	Si
SLV 16	3.97	-9513	-3723	2421.42		6393	4.96	9612	14303			3.84	Si
SLV 3	2.07	-14238	4588	5396.82		9569	4.96	10247	15248			3.32	Si
SLV 3	3.97	-9489	3628	-2512.58		6377	4.96	9609	14298			3.94	Si
SLV 9	2.07	-13679	-1430	-1698.96		9193	4.96	10172	15136			10.58	Si
SLV 9	3.97	-9430	-1071	749.31		6337	4.96	9601	14286			13.34	Si
SLV 1	2.07	-13987	4578	5418.51		9400	4.96	10213	15197			3.32	Si
SLV 1	3.97	-9454	3664	-2487.29		6354	4.96	9604	14291			3.9	Si
SLV 10	2.07	-13679	-1430	-1698.96		9193	4.96	10172	15136			10.58	Si
SLV 10	3.97	-9430	-1071	749.31		6337	4.96	9601	14286			13.34	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.03 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 5	143750	0.47	7401	-11013	818.38	1551.9	1.9	Si
SLV 6	143750	0.47	7401	-11013	818.38	1551.9	1.9	Si
SLV 9	143750	0.47	7403	-11016	818.38	1552.29	1.9	Si
SLV 10	143750	0.47	7403	-11016	818.38	1552.29	1.9	Si
SLV 1	143750	0.47	7566	-11259	818.38	1584.26	1.94	Si
SLV 2	143750	0.47	7566	-11259	818.38	1584.26	1.94	Si
SLV 13	143750	0.47	7573	-11269	818.38	1585.54	1.94	Si
SLV 14	143750	0.47	7573	-11269	818.38	1585.54	1.94	Si
SLV 3	143750	0.47	7710	-11473	818.38	1612.3	1.97	Si
SLV 4	143750	0.47	7710	-11473	818.38	1612.3	1.97	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 3.03 Wa = 0.05 Ta = 0.0855

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 14	-5039	-16237	110	0.047	1408	0.889	0.76923	19.26035	No
SLV 13	-5039	-16237	110	0.047	1408	0.889	0.76923	19.26035	No
SLV 3	-4997	-16351	-111	0.047	1404.2	0.889	0.76951	19.26035	No
SLV 4	-4997	-16351	-111	0.047	1404.2	0.889	0.76951	19.26035	No
SLV 2	-5038	-16364	94	0.049	1407.9	0.889	0.79514	19.26035	No
SLV 1	-5038	-16364	94	0.049	1407.9	0.889	0.79514	19.26035	No
SLV 16	-4998	-16223	-94	0.049	1404.3	0.889	0.79549	19.26035	No
SLV 15	-4998	-16223	-94	0.049	1404.3	0.889	0.79549	19.26035	No
SLV 7	-4949	-16291	-344	0.024	1399.9	0.889	0.39613	4.54431	No
SLV 8	-4949	-16291	-344	0.024	1399.9	0.889	0.39613	4.54431	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	295.347	SLU 39	Si
V_SLU	254.752	SLU 81	Si
PF_SLV	5.74	SLV 13	Si
V_SLV	3.27	SLV 13	Si
PFFP_SLV	1.896	SLV 5	Si
R_SLV	0.04	SLV 13	No

Maschio 26

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
2.186	-8.719	-0.141	-8.718	L2	L3	2.327	0.3	3.92	3.92	3.92			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 84	2.07	-10191	1107.29	14598	9732.09	8.789	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 84	3.97	-8464	1781.25	12125	8382.25	4.706	Si
SLU 41	2.07	-8910	1013.65	12764	8742.64	8.625	Si
SLU 41	3.97	-7856	1697.13	11253	7877.63	4.642	Si
SLU 42	2.07	-8910	1013.65	12764	8742.64	8.625	Si
SLU 42	3.97	-7856	1697.13	11253	7877.63	4.642	Si
SLU 20	2.07	-8075	902.73	11567	8060.74	8.929	Si
SLU 20	3.97	-6829	1451.77	9782	6990.91	4.815	Si
SLU 40	2.07	-8910	1013.65	12764	8742.64	8.625	Si
SLU 40	3.97	-7856	1697.13	11253	7877.63	4.642	Si
SLU 81	2.07	-10191	1107.29	14598	9732.09	8.789	Si
SLU 81	3.97	-8464	1781.25	12125	8382.25	4.706	Si
SLU 83	2.07	-10191	1107.29	14598	9732.09	8.789	Si
SLU 83	3.97	-8464	1781.25	12125	8382.25	4.706	Si
SLU 21	2.07	-8075	902.73	11567	8060.74	8.929	Si
SLU 21	3.97	-6829	1451.77	9782	6990.91	4.815	Si
SLU 82	2.07	-10191	1107.29	14598	9732.09	8.789	Si
SLU 82	3.97	-8464	1781.25	12125	8382.25	4.706	Si
SLU 39	2.07	-8910	1013.65	12764	8742.64	8.625	Si
SLU 39	3.97	-7856	1697.13	11253	7877.63	4.642	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 12	2.07	-6625	263.44	9490	7109.34	26.987	Si
SLV 12	3.97	-4570	1110.41	6547	5032.57	4.532	Si
SLV 2	2.07	-6101	1572.84	8740	6591.21	4.191	Si
SLV 2	3.97	-3532	111.74	5059	3939.09	35.252	Si
SLV 13	2.07	-5559	-448.07	7964	6046.74	13.495	Si
SLV 13	3.97	-4815	1445.76	6898	5286.45	3.657	Si
SLV 15	2.07	-5964	-446.13	8543	6453.49	14.465	Si
SLV 15	3.97	-4910	1506.48	7033	5383.55	3.574	Si
SLV 4	2.07	-6506	1574.78	9319	6991.98	4.44	Si
SLV 4	3.97	-3626	172.46	5194	4039.49	23.423	Si
SLV 14	2.07	-5559	-448.07	7964	6046.74	13.495	Si
SLV 14	3.97	-4815	1445.76	6898	5286.45	3.657	Si
SLV 16	2.07	-5964	-446.13	8543	6453.49	14.465	Si
SLV 16	3.97	-4910	1506.48	7033	5383.55	3.574	Si
SLV 11	2.07	-6625	263.44	9490	7109.34	26.987	Si
SLV 11	3.97	-4570	1110.41	6547	5032.57	4.532	Si
SLV 1	2.07	-6101	1572.84	8740	6591.21	4.191	Si
SLV 1	3.97	-3532	111.74	5059	3939.09	35.252	Si
SLV 3	2.07	-6506	1574.78	9319	6991.98	4.44	Si
SLV 3	3.97	-3626	172.46	5194	4039.49	23.423	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLU 77	2.07	-9335	-1068	968.14		13373	2.327	7339	5123			4.79	Si
SLU 77	3.97	-7376	-1068	1513.96		10566	2.327	6964	4862			4.55	Si
SLU 40	2.07	-8910	-1249	1013.65		12764	2.327	7257	5066			4.06	Si
SLU 40	3.97	-7856	-1249	1697.13		11253	2.327	7056	4926			3.94	Si
SLU 39	2.07	-8910	-1249	1013.65		12764	2.327	7257	5066			4.06	Si
SLU 39	3.97	-7856	-1249	1697.13		11253	2.327	7056	4926			3.94	Si
SLU 75	2.07	-9335	-1068	968.14		13373	2.327	7339	5123			4.79	Si
SLU 75	3.97	-7376	-1068	1513.96		10566	2.327	6964	4862			4.55	Si
SLU 83	2.07	-10191	-1278	1107.29		14598	2.327	7502	5237			4.1	Si
SLU 83	3.97	-8464	-1278	1781.25		12125	2.327	7172	5007			3.92	Si
SLU 84	2.07	-10191	-1278	1107.29		14598	2.327	7502	5237			4.1	Si
SLU 84	3.97	-8464	-1278	1781.25		12125	2.327	7172	5007			3.92	Si
SLU 42	2.07	-8910	-1249	1013.65		12764	2.327	7257	5066			4.06	Si
SLU 42	3.97	-7856	-1249	1697.13		11253	2.327	7056	4926			3.94	Si
SLU 81	2.07	-10191	-1278	1107.29		14598	2.327	7502	5237			4.1	Si
SLU 81	3.97	-8464	-1278	1781.25		12125	2.327	7172	5007			3.92	Si
SLU 41	2.07	-8910	-1249	1013.65		12764	2.327	7257	5066			4.06	Si
SLU 41	3.97	-7856	-1249	1697.13		11253	2.327	7056	4926			3.94	Si
SLU 82	2.07	-10191	-1278	1107.29		14598	2.327	7502	5237			4.1	Si
SLU 82	3.97	-8464	-1278	1781.25		12125	2.327	7172	5007			3.92	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLV 15	2.07	-5964	-2161	-446.13		8543	2.327	10042	7010			3.24	Si
SLV 15	3.97	-4910	-1678	1506.48		7033	2.327	9740	6799			4.05	Si
SLV 1	2.07	-6101	1083	1572.84		8740	2.327	10081	7038			6.5	Si
SLV 1	3.97	-3532	600	111.74		5059	2.327	9345	6524			10.87	Si
SLV 16	2.07	-5964	-2161	-446.13		8543	2.327	10042	7010			3.24	Si
SLV 16	3.97	-4910	-1678	1506.48		7033	2.327	9740	6799			4.05	Si
SLV 2	2.07	-6101	1083	1572.84		8740	2.327	10081	7038			6.5	Si
SLV 2	3.97	-3532	600	111.74		5059	2.327	9345	6524			10.87	Si
SLV 10	2.07	-5278	-1239	257		7560	2.327	9845	6873			5.55	Si
SLV 10	3.97	-4256	-1196	908.01		6097	2.327	9553	6669			5.57	Si
SLV 4	2.07	-6506	1200	1574.78		9319	2.327	10197	7119			5.93	Si
SLV 4	3.97	-3626	774	172.46		5194	2.327	9372	6543			8.45	Si
SLV 9	2.07	-5278	-1239	257		7560	2.327	9845	6873			5.55	Si
SLV 9	3.97	-4256	-1196	908.01		6097	2.327	9553	6669			5.57	Si
SLV 3	2.07	-6506	1200	1574.78		9319	2.327	10197	7119			5.93	Si
SLV 3	3.97	-3626	774	172.46		5194	2.327	9372	6543			8.45	Si
SLV 14	2.07	-5559	-2278	-448.07		7964	2.327	9926	6929			3.04	Si
SLV 14	3.97	-4815	-1852	1445.76		6898	2.327	9713	6781			3.66	Si
SLV 13	2.07	-5559	-2278	-448.07		7964	2.327	9926	6929			3.04	Si
SLV 13	3.97	-4815	-1852	1445.76		6898	2.327	9713	6781			3.66	Si



Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.03 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 2	143750	0.47	6481	-4525	383.94	642.68	1.67	Si
SLV 1	143750	0.47	6481	-4525	383.94	642.68	1.67	Si
SLV 5	143750	0.47	6548	-4571	383.94	648.97	1.69	Si
SLV 6	143750	0.47	6548	-4571	383.94	648.97	1.69	Si
SLV 4	143750	0.47	6739	-4704	383.94	666.71	1.74	Si
SLV 3	143750	0.47	6739	-4704	383.94	666.71	1.74	Si
SLV 9	143750	0.47	6863	-4791	383.94	678.33	1.77	Si
SLV 10	143750	0.47	6863	-4791	383.94	678.33	1.77	Si
SLV 7	143750	0.47	7406	-5170	383.94	728.53	1.9	Si
SLV 8	143750	0.47	7406	-5170	383.94	728.53	1.9	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.03 Wa = 0.05 Ta = 0.0855

Comb.	N top	N base	V orto	σ_0	M*	e*	a0*	aLim	Verifica
SLV 16	-2378	-7562	-293	0	661.8	0.889	0	19.26035	No
SLV 1	-2258	-6299	293	0	651.1	0.889	0	19.26035	No
SLV 2	-2258	-6299	293	0	651.1	0.889	0	19.26035	No
SLV 15	-2378	-7562	-293	0	661.8	0.889	0	19.26035	No
SLV 3	-2299	-6794	234	0.009	654.7	0.889	0.14561	19.26035	No
SLV 4	-2299	-6794	234	0.009	654.7	0.889	0.14561	19.26035	No
SLV 14	-2337	-7066	-234	0.009	658.1	0.889	0.14943	19.26035	No
SLV 13	-2337	-7066	-234	0.009	658.1	0.889	0.14943	19.26035	No
SLV 6	-2238	-5989	178	0.02	649.3	0.889	0.33501	4.54431	No
SLV 5	-2238	-5989	178	0.02	649.3	0.889	0.33501	4.54431	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	4.642	SLU 39	Si
V_SLU	3.917	SLU 81	Si
PF_SLV	3.574	SLV 15	Si
V_SLV	3.042	SLV 13	Si
PFFP_SLV	1.674	SLV 1	Si
R_SLV	0	SLV 1	No

Maschio 27

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
2.185	-13.249	-2.615	-13.248	L2	L3	4.8	0.3	3.92	3.92	3.92			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 41	1.07	-24074	16115.9	16719	45914.98	2.849	Si
SLU 41	3.17	-23231	7285.96	16133	44707.71	6.136	Si
SLU 83	1.07	-27216	17537.61	18901	50157.95	2.86	Si
SLU 83	3.17	-25116	7820.52	17443	47367.21	6.057	Si
SLU 38	1.07	-21545	14143.89	14963	42207.34	2.984	Si
SLU 38	3.17	-20070	6270.57	13939	39923.14	6.367	Si
SLU 40	1.07	-24074	16115.9	16719	45914.98	2.849	Si
SLU 40	3.17	-23231	7285.96	16133	44707.71	6.136	Si
SLU 37	1.07	-21545	14143.89	14963	42207.34	2.984	Si
SLU 37	3.17	-20070	6270.57	13939	39923.14	6.367	Si
SLU 39	1.07	-24074	16115.9	16719	45914.98	2.849	Si
SLU 39	3.17	-23231	7285.96	16133	44707.71	6.136	Si
SLU 81	1.07	-27216	17537.61	18901	50157.95	2.86	Si
SLU 81	3.17	-25116	7820.52	17443	47367.21	6.057	Si
SLU 84	1.07	-27216	17537.61	18901	50157.95	2.86	Si
SLU 84	3.17	-25116	7820.52	17443	47367.21	6.057	Si
SLU 82	1.07	-27216	17537.61	18901	50157.95	2.86	Si
SLU 82	3.17	-25116	7820.52	17443	47367.21	6.057	Si
SLU 42	1.07	-24074	16115.9	16719	45914.98	2.849	Si
SLU 42	3.17	-23231	7285.96	16133	44707.71	6.136	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 4	1.07	-17680	17049.01	12279	38166.09	2.239	Si
SLV 4	3.17	-12021	1343.57	8348	26877.25	20.004	Si
SLV 5	1.07	-16356	11182.2	11359	35603.02	3.184	Si
SLV 5	3.17	-12491	2847.47	8675	27847.95	9.78	Si
SLV 2	1.07	-17750	16822.37	12328	38300.15	2.277	Si
SLV 2	3.17	-12031	1197.23	8356	26898.67	22.467	Si
SLV 11	1.07	-14858	7329.88	10319	32645.71	4.454	Si
SLV 11	3.17	-12840	4896.07	8917	28565.23	5.834	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 8	1.07	-16123	11937.67	11197	35146.78	2.944	Si
SLV 8	3.17	-12456	3335.25	8651	27776.97	8.328	Si
SLV 12	1.07	-14858	7329.88	10319	32645.71	4.454	Si
SLV 12	3.17	-12840	4896.07	8917	28565.23	5.834	Si
SLV 1	1.07	-17750	16822.37	12328	38300.15	2.277	Si
SLV 1	3.17	-12031	1197.23	8356	26898.67	22.467	Si
SLV 6	1.07	-16356	11182.2	11359	35603.02	3.184	Si
SLV 6	3.17	-12491	2847.47	8675	27847.95	9.78	Si
SLV 7	1.07	-16123	11937.67	11197	35146.78	2.944	Si
SLV 7	3.17	-12456	3335.25	8651	27776.97	8.328	Si
SLV 3	1.07	-17680	17049.01	12279	38166.09	2.239	Si
SLV 3	3.17	-12021	1343.57	8348	26877.25	20.004	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 83	1.07	-27216	-1122	17537.61		18901	4.7997	8076	11628			10.36	Si
SLU 83	3.17	-25116	-1124	7820.52		17443	4.7997	7881	11348			10.1	Si
SLU 82	1.07	-27216	-1122	17537.61		18901	4.7997	8076	11628			10.36	Si
SLU 82	3.17	-25116	-1124	7820.52		17443	4.7997	7881	11348			10.1	Si
SLU 21	1.07	-21660	-944	13874.27		15042	4.7997	7561	10887			11.53	Si
SLU 21	3.17	-20239	-945	6296.88		14056	4.7997	7430	10698			11.32	Si
SLU 84	1.07	-27216	-1122	17537.61		18901	4.7997	8076	11628			10.36	Si
SLU 84	3.17	-25116	-1124	7820.52		17443	4.7997	7881	11348			10.1	Si
SLU 42	1.07	-24074	-1189	16115.9		16719	4.7997	7785	11209			9.43	Si
SLU 42	3.17	-23231	-1191	7285.96		16133	4.7997	7707	11097			9.32	Si
SLU 40	1.07	-24074	-1189	16115.9		16719	4.7997	7785	11209			9.43	Si
SLU 40	3.17	-23231	-1191	7285.96		16133	4.7997	7707	11097			9.32	Si
SLU 41	1.07	-24074	-1189	16115.9		16719	4.7997	7785	11209			9.43	Si
SLU 41	3.17	-23231	-1191	7285.96		16133	4.7997	7707	11097			9.32	Si
SLU 20	1.07	-21660	-944	13874.27		15042	4.7997	7561	10887			11.53	Si
SLU 20	3.17	-20239	-945	6296.88		14056	4.7997	7430	10698			11.32	Si
SLU 39	1.07	-24074	-1189	16115.9		16719	4.7997	7785	11209			9.43	Si
SLU 39	3.17	-23231	-1191	7285.96		16133	4.7997	7707	11097			9.32	Si
SLU 81	1.07	-27216	-1122	17537.61		18901	4.7997	8076	11628			10.36	Si
SLU 81	3.17	-25116	-1124	7820.52		17443	4.7997	7881	11348			10.1	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 15	1.07	-13464	-9141	1689.71		9351	4.7997	10203	14692			1.61	Si
SLV 15	3.17	-13300	-7680	6546.31		9237	4.7997	10181	14659			1.91	Si
SLV 1	1.07	-17750	8534	16822.37		13582	4.3563	11050	14441			1.69	Si
SLV 1	3.17	-12031	7070	1197.23		8356	4.7997	10004	14405			2.04	Si
SLV 3	1.07	-17680	8554	17049.01		13685	4.3066	11070	14303			1.67	Si
SLV 3	3.17	-12021	7119	1343.57		8348	4.7997	10003	14403			2.02	Si
SLV 2	1.07	-17750	8534	16822.37		13582	4.3563	11050	14441			1.69	Si
SLV 2	3.17	-12031	7070	1197.23		8356	4.7997	10004	14405			2.04	Si
SLV 9	1.07	-15091	-2992	6574.41		10481	4.7997	10429	15017			5.02	Si
SLV 9	3.17	-12875	-2608	4408.29		8941	4.7997	10122	14574			5.59	Si
SLV 4	1.07	-17680	8554	17049.01		13685	4.3066	11070	14303			1.67	Si
SLV 4	3.17	-12021	7119	1343.57		8348	4.7997	10003	14403			2.02	Si
SLV 16	1.07	-13464	-9141	1689.71		9351	4.7997	10203	14692			1.61	Si
SLV 16	3.17	-13300	-7680	6546.31		9237	4.7997	10181	14659			1.91	Si
SLV 14	1.07	-13534	-9161	1463.07		9399	4.7997	10213	14706			1.61	Si
SLV 14	3.17	-13310	-7729	6399.97		9244	4.7997	10182	14661			1.9	Si
SLV 13	1.07	-13534	-9161	1463.07		9399	4.7997	10213	14706			1.61	Si
SLV 13	3.17	-13310	-7729	6399.97		9244	4.7997	10182	14661			1.9	Si
SLV 10	1.07	-15091	-2992	6574.41		10481	4.7997	10429	15017			5.02	Si
SLV 10	3.17	-12875	-2608	4408.29		8941	4.7997	10122	14574			5.59	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.03 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 3	143750	0.47	8356	-12031	809.14	1681.29	2.08	Si
SLV 4	143750	0.47	8356	-12031	809.14	1681.29	2.08	Si
SLV 2	143750	0.47	8357	-12034	809.14	1681.57	2.08	Si
SLV 1	143750	0.47	8357	-12034	809.14	1681.57	2.08	Si
SLV 8	143750	0.47	8678	-12495	809.14	1741.2	2.15	Si
SLV 7	143750	0.47	8678	-12495	809.14	1741.2	2.15	Si
SLV 6	143750	0.47	8683	-12503	809.14	1742.15	2.15	Si
SLV 5	143750	0.47	8683	-12503	809.14	1742.15	2.15	Si
SLV 12	143750	0.47	8956	-12895	809.14	1792.54	2.22	Si
SLV 11	143750	0.47	8956	-12895	809.14	1792.54	2.22	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 3.03 Wa = 0.05 Ta = 0.0855

Comb.	N top	N base	V orto	α_0	M*	e*	α_0^*	aLim	Verifica
SLV 5	-8852	-16356	850	0	1736.8	0.896	0	4.54431	No
SLV 10	-8840	-15091	861	0	1735.7	0.896	0	4.54431	No
SLV 12	-8821	-14858	850	0	1733.8	0.896	0	4.54431	No
SLV 9	-8840	-15091	861	0	1735.7	0.896	0	4.54431	No
SLV 11	-8821	-14858	850	0	1733.8	0.896	0	4.54431	No
SLV 7	-8832	-16123	861	0	1734.9	0.896	0	4.54431	No
SLV 8	-8832	-16123	861	0	1734.9	0.896	0	4.54431	No
SLV 6	-8852	-16356	850	0	1736.8	0.896	0	4.54431	No
SLV 14	-8820	-13534	274	0.033	1733.8	0.896	0.52796	19.26035	No
SLV 13	-8820	-13534	274	0.033	1733.8	0.896	0.52796	19.26035	No



Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	2.849	SLU 39	Si
V_SLU	9.32	SLU 39	Si
PF_SLV	2.239	SLV 3	Si
V_SLV	1.605	SLV 13	Si
PFFP_SLV	2.078	SLV 3	Si
R_SLV	0	SLV 5	No

Maschio 28

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
2.185	-17.729	2.186	-8.719	L2	L3	9.01	0.3	3.92	3.92	3.92			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 20	1.07	-31802	-1658.89	11765	122574.88	73.89	Si
SLU 20	4.99	-1016	62.83	376	4557.57	72.541	Si
SLU 40	1.07	-34681	-1876.13	12831	131629.73	70.16	Si
SLU 40	4.99	-1238	77.59	458	5544.16	71.459	Si
SLU 81	1.07	-41016	-2105.27	15174	150357.47	71.42	Si
SLU 81	4.99	-1263	76.34	467	5655.23	74.077	Si
SLU 39	1.07	-34681	-1876.13	12831	131629.73	70.16	Si
SLU 39	4.99	-1238	77.59	458	5544.16	71.459	Si
SLU 21	1.07	-31802	-1658.89	11765	122574.88	73.89	Si
SLU 21	4.99	-1016	62.83	376	4557.57	72.541	Si
SLU 41	1.07	-34681	-1876.13	12831	131629.73	70.16	Si
SLU 41	4.99	-1238	77.59	458	5544.16	71.459	Si
SLU 42	1.07	-34681	-1876.13	12831	131629.73	70.16	Si
SLU 42	4.99	-1238	77.59	458	5544.16	71.459	Si
SLU 84	1.07	-41016	-2105.27	15174	150357.47	71.42	Si
SLU 84	4.99	-1263	76.34	467	5655.23	74.077	Si
SLU 82	1.07	-41016	-2105.27	15174	150357.47	71.42	Si
SLU 82	4.99	-1263	76.34	467	5655.23	74.077	Si
SLU 83	1.07	-41016	-2105.27	15174	150357.47	71.42	Si
SLU 83	4.99	-1263	76.34	467	5655.23	74.077	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 12	1.07	-29238	5036.85	10817	120055.2	23.835	Si
SLV 12	4.99	-616	-466.38	228	2770.69	5.941	Si
SLV 11	1.07	-29238	5036.85	10817	120055.2	23.835	Si
SLV 11	4.99	-616	-466.38	228	2770.69	5.941	Si
SLV 7	1.07	-24043	7595.67	8895	100427.2	13.222	Si
SLV 7	4.99	-458	-500.56	170	2061.99	4.119	Si
SLV 3	1.07	-18030	5317.14	6670	76791.41	14.442	Si
SLV 3	4.99	-273	-183.14	101	1228.1	6.706	Si
SLV 8	1.07	-24043	7595.67	8895	100427.2	13.222	Si
SLV 8	4.99	-458	-500.56	170	2061.99	4.119	Si
SLV 6	1.07	-24181	-7443.84	8946	100958.71	13.563	Si
SLV 6	4.99	-454	520.3	168	2044.26	3.929	Si
SLV 9	1.07	-29376	-10002.66	10868	120567.13	12.054	Si
SLV 9	4.99	-612	554.49	227	2752.99	4.965	Si
SLV 4	1.07	-18030	5317.14	6670	76791.41	14.442	Si
SLV 4	4.99	-273	-183.14	101	1228.1	6.706	Si
SLV 10	1.07	-29376	-10002.66	10868	120567.13	12.054	Si
SLV 10	4.99	-612	554.49	227	2752.99	4.965	Si
SLV 5	1.07	-24181	-7443.84	8946	100958.71	13.563	Si
SLV 5	4.99	-454	520.3	168	2044.26	3.929	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 53	1.07	-35919	1	-1693.97		13288	9.01	7327	19806			1000	Si
SLU 53	4.99	-837	0	46.55		310	9.01	5597	15128			1000	Si
SLU 60	1.07	-38137	1	-1888.02		14109	9.01	7437	20102			1000	Si
SLU 60	4.99	-1041	0	61.58		385	9.01	5607	15156			1000	Si
SLU 61	1.07	-38137	1	-1888.02		14109	9.01	7437	20102			1000	Si
SLU 61	4.99	-1041	0	61.58		385	9.01	5607	15156			1000	Si
SLU 56	1.07	-35919	1	-1693.97		13288	9.01	7327	19806			1000	Si
SLU 56	4.99	-837	0	46.55		310	9.01	5597	15128			1000	Si
SLU 1	1.07	-24408	1	-1012.06		9030	9.01	6760	18271			1000	Si
SLU 1	4.99	-336	0	12.72		124	9.01	5572	15061			1000	Si
SLU 59	1.07	-35919	1	-1693.97		13288	9.01	7327	19806			1000	Si
SLU 59	4.99	-837	0	46.55		310	9.01	5597	15128			1000	Si
SLU 54	1.07	-35919	1	-1693.97		13288	9.01	7327	19806			1000	Si
SLU 54	4.99	-837	0	46.55		310	9.01	5597	15128			1000	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 58	1.07	-35919	1	-1693.97		13288	9.01	7327	19806			1000	Si
SLU 58	4.99	-837	0	46.55		310	9.01	5597	15128			1000	Si
SLU 55	1.07	-35919	1	-1693.97		13288	9.01	7327	19806			1000	Si
SLU 55	4.99	-837	0	46.55		310	9.01	5597	15128			1000	Si
SLU 57	1.07	-35919	1	-1693.97		13288	9.01	7327	19806			1000	Si
SLU 57	4.99	-837	0	46.55		310	9.01	5597	15128			1000	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 2	1.07	-18072	-1959	805.29		6686	9.01	9670	26139			13.35	Si
SLV 2	4.99	-272	-304	123.12		100	9.01	8353	22579			74.31	Si
SLV 6	1.07	-24181	-6262	-7443.84		8946	9.01	10123	27361			4.37	Si
SLV 6	4.99	-454	-946	520.3		168	9.01	8367	22616			23.92	Si
SLV 8	1.07	-24043	6211	7595.67		8895	9.01	10112	27334			4.4	Si
SLV 8	4.99	-458	932	-500.56		170	9.01	8367	22617			24.26	Si
SLV 5	1.07	-24181	-6262	-7443.84		8946	9.01	10123	27361			4.37	Si
SLV 5	4.99	-454	-946	520.3		168	9.01	8367	22616			23.92	Si
SLV 11	1.07	-29238	6264	5036.85		10817	9.01	10497	28373			4.53	Si
SLV 11	4.99	-616	946	-466.38		228	9.01	8379	22648			23.95	Si
SLV 7	1.07	-24043	6211	7595.67		8895	9.01	10112	27334			4.4	Si
SLV 7	4.99	-458	932	-500.56		170	9.01	8367	22617			24.26	Si
SLV 1	1.07	-18072	-1959	805.29		6686	9.01	9670	26139			13.35	Si
SLV 1	4.99	-272	-304	123.12		100	9.01	8353	22579			74.31	Si
SLV 10	1.07	-29376	-6209	-10002.66		10868	9.01	10507	28400			4.57	Si
SLV 10	4.99	-612	-932	554.49		227	9.01	8379	22647			24.29	Si
SLV 9	1.07	-29376	-6209	-10002.66		10868	9.01	10507	28400			4.57	Si
SLV 9	4.99	-612	-932	554.49		227	9.01	8379	22647			24.29	Si
SLV 12	1.07	-29238	6264	5036.85		10817	9.01	10497	28373			4.53	Si
SLV 12	4.99	-616	946	-466.38		228	9.01	8379	22648			23.95	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.03 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 1	143750	0.47	0	-9554	1518.92	0	0	No, $e > t/2$
SLV 3	143750	0.47	0	-9575	1518.92	0	0	No, $e > t/2$
SLV 4	143750	0.47	0	-9575	1518.92	0	0	No, $e > t/2$
SLV 2	143750	0.47	0	-9554	1518.92	0	0	No, $e > t/2$
SLV 5	143750	0.47	4364	-11797	1518.92	1706.33	1.12	Si
SLV 6	143750	0.47	4364	-11797	1518.92	1706.33	1.12	Si
SLV 7	143750	0.47	4391	-11868	1518.92	1716.19	1.13	Si
SLV 8	143750	0.47	4391	-11868	1518.92	1716.19	1.13	Si
SLV 10	143750	0.47	5084	-13741	1518.92	1975.38	1.3	Si
SLV 9	143750	0.47	5084	-13741	1518.92	1975.38	1.3	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 3.03 Wa = 0.05 Ta = 0.0855

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 13	-798	-35388	19	0.072	1955.8	0.966	1.07912	19.26035	No
SLV 14	-798	-35388	19	0.072	1955.8	0.966	1.07912	19.26035	No
SLV 16	-799	-35347	19	0.072	1955.9	0.966	1.07983	19.26035	No
SLV 15	-799	-35347	19	0.072	1955.9	0.966	1.07983	19.26035	No
SLV 3	-273	-18030	-19	0.074	1945.7	0.987	1.08341	19.26035	No
SLV 4	-273	-18030	-19	0.074	1945.7	0.987	1.08341	19.26035	No
SLV 2	-272	-18072	-18	0.074	1945.7	0.987	1.08415	19.26035	No
SLV 1	-272	-18072	-18	0.074	1945.7	0.987	1.08415	19.26035	No
SLV 9	-612	-29376	7	0.074	1951.3	0.972	1.09926	4.54431	No
SLV 10	-612	-29376	7	0.074	1951.3	0.972	1.09926	4.54431	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	70.16	SLU 39	Si
V_SLU	1000	SLU 1	Si
PF_SLV	3.929	SLV 5	Si
V_SLV	4.369	SLV 5	Si
PFFP_SLV	0	SLV 1	No
R_SLV	0.056	SLV 13	No

1.4 Verifiche travi di accoppiamento in muratura

Le unità di misura elencate nel capitolo sono in [m, daN] ove non espressamente specificato.

X ini.: coordinata punto iniziale. [m]

Y ini.: coordinata punto iniziale. [m]

Z ini.inf.: coordinata punto iniziale. [m]

Z ini.sup.: coordinata punto iniziale. [m]

H ini.: altezza della sezione iniziale. [m]

X fin.: coordinata punto finale. [m]

Y fin.: coordinata punto finale. [m]

Z fin.inf.: coordinata punto finale. [m]



Z fin.sup: coordinata punto finale. [m]
H fin.: altezza della sezione finale. [m]
Luce: lunghezza della trave. [m]
Spessore: spessore. [m]
R. Trazione: resistenza a trazione dell'elemento teso disposto orizzontalmente. [daN]
fb: resistenza normalizzata a compressione in direzione orizzontale dei blocchi. [daN/m²]
fhk: resistenza caratteristica a compressione della muratura utilizzata in direzione orizzontale. [daN/m²]
fvk0: resistenza caratteristica a taglio in assenza di carichi verticali. [daN/m²]
fhmedio: resistenza media a compressione della muratura utilizzata in direzione orizzontale. [daN/m²]
τ0: resistenza media a taglio in assenza di azioni normali [C8.7.1.16]. [daN/m²]
fv0: resistenza media a taglio in assenza di azioni normali [C8.7.1.17]. [daN/m²]
μ: coefficiente di attrito [C8.7.1.17].
φ: coefficiente di ammassamento o ingranamento secondo Circolare 7 21-01-19 §C8.7.1.3.1.1.
fvk,lim: valore caratteristico massimo della resistenza a taglio che può essere impiegata nel calcolo (§11.10.3.3). [daN/m²]
E: modulo di elasticità longitudinale della muratura utilizzato. [daN/m²]
G: modulo di elasticità tangenziale della muratura utilizzato. [daN/m²]
FC: fattore di confidenza della muratura.
Sezione: sezione di verifica.
γM: fattore parziale di sicurezza del materiale.
N: sforzo normale. [daN]
M: momento flettente nel piano. [daN*m]
Mu: momento ultimo. [daN*m]
Comb.: combinazione.
c.s.: coefficiente di sicurezza.
Verifica: stato di verifica.
M: momento flettente. [daN*m]
V: taglio nel piano. [daN]
Vt: resistenza a taglio secondo [7.8.4]. [daN]
Vp: resistenza a taglio secondo [7.8.6]. [daN]
Vt fess. diag.: resistenza a taglio per fessurazione diagonale secondo §C8.7.1.3.1.1 formule [C8.7.1.16] ovvero [C8.7.1.17]. [daN]
Vt,lim: taglio limite [C8.1.7.18]. [daN]
Stato limite: pF_SLV=Presso flessione per azioni sismiche; V_SLV=Taglio per azioni sismiche.
Coeff.s.: coefficiente di sicurezza.

Trave di accoppiamento 1

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-7.545	-17.728	-1.53	0.47	2	-8.545	-17.728	-1.53	0.47	2	1	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fhk	fvk0	fhmedio	τ0	fv0	μ	φ	fvk,lim	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-1704	-124.4	3165.81	SLU 83	25.45	Si
fin.	3	-747	-1340.74	3165.81	SLU 83	2.36	Si
ini.	3	-1608	-152.81	3165.81	SLU 79	20.72	Si
fin.	3	-743	-1223.7	3165.81	SLU 79	2.59	Si
ini.	3	-1608	-152.81	3165.81	SLU 78	20.72	Si
fin.	3	-743	-1223.7	3165.81	SLU 78	2.59	Si
ini.	3	-1704	-124.4	3165.81	SLU 82	25.45	Si
fin.	3	-747	-1340.74	3165.81	SLU 82	2.36	Si
ini.	3	-1608	-152.81	3165.81	SLU 75	20.72	Si
fin.	3	-743	-1223.7	3165.81	SLU 75	2.59	Si
ini.	3	-1608	-152.81	3165.81	SLU 73	20.72	Si
fin.	3	-743	-1223.7	3165.81	SLU 73	2.59	Si
ini.	3	-1704	-124.4	3165.81	SLU 81	25.45	Si
fin.	3	-747	-1340.74	3165.81	SLU 81	2.36	Si
ini.	3	-1608	-152.81	3165.81	SLU 74	20.72	Si
fin.	3	-743	-1223.7	3165.81	SLU 74	2.59	Si
ini.	3	-1704	-124.4	3165.81	SLU 84	25.45	Si
fin.	3	-747	-1340.74	3165.81	SLU 84	2.36	Si
ini.	3	-1608	-152.81	3165.81	SLU 76	20.72	Si
fin.	3	-743	-1223.7	3165.81	SLU 76	2.59	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-124.4	-3679			3466	1304	SLU 83	0.35	No
fin.	3	0	-1340.74	-185			3466	1304	SLU 83	7.05	Si
ini.	3	0	-124.4	-3679			3466	1304	SLU 81	0.35	No
fin.	3	0	-1340.74	-185			3466	1304	SLU 81	7.05	Si
ini.	3	0	-63.18	-3342			3466	1304	SLU 41	0.39	No
fin.	3	0	-1188.61	-216			3466	1304	SLU 41	6.05	Si



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-63.18	-3342			3466	1304	SLU 39	0.39	No
fin.	3	0	-1188.61	-216			3466	1304	SLU 39	6.05	Si
ini.	3	0	-63.18	-3342			3466	1304	SLU 40	0.39	No
fin.	3	0	-1188.61	-216			3466	1304	SLU 40	6.05	Si
ini.	3	0	-152.81	-3302			3466	1304	SLU 75	0.4	No
fin.	3	0	-1223.7	-118			3466	1304	SLU 75	11.03	Si
ini.	3	0	-124.4	-3679			3466	1304	SLU 84	0.35	No
fin.	3	0	-1340.74	-185			3466	1304	SLU 84	7.05	Si
ini.	3	0	-63.18	-3342			3466	1304	SLU 42	0.39	No
fin.	3	0	-1188.61	-216			3466	1304	SLU 42	6.05	Si
ini.	3	0	-152.81	-3302			3466	1304	SLU 77	0.4	No
fin.	3	0	-1223.7	-118			3466	1304	SLU 77	11.03	Si
ini.	3	0	-124.4	-3679			3466	1304	SLU 82	0.35	No
fin.	3	0	-1340.74	-185			3466	1304	SLU 82	7.05	Si

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-1286	-156.59	3277.21	SLV 5	20.93	Si
fin.	2	-654	-1041.27	3277.21	SLV 5	3.15	Si
ini.	2	-1408	453.77	3277.21	SLV 3	7.22	Si
fin.	2	-22	-1565.03	3277.21	SLV 3	2.09	Si
ini.	2	-1113	182.28	3277.21	SLV 8	17.98	Si
fin.	2	-189	-993.2	3277.21	SLV 8	3.3	Si
ini.	2	-1460	352.11	3277.21	SLV 2	9.31	Si
fin.	2	-162	-1579.46	3277.21	SLV 2	2.07	Si
ini.	2	-790	-762.45	3277.21	SLV 13	4.3	Si
fin.	2	-1104	6.28	3277.21	SLV 13	521.58	Si
ini.	2	-1408	453.77	3277.21	SLV 4	7.22	Si
fin.	2	-22	-1565.03	3277.21	SLV 4	2.09	Si
ini.	2	-1460	352.11	3277.21	SLV 1	9.31	Si
fin.	2	-162	-1579.46	3277.21	SLV 1	2.07	Si
ini.	2	-1286	-156.59	3277.21	SLV 6	20.93	Si
fin.	2	-654	-1041.27	3277.21	SLV 6	3.15	Si
ini.	2	-790	-762.45	3277.21	SLV 14	4.3	Si
fin.	2	-1104	6.28	3277.21	SLV 14	521.58	Si
ini.	2	-1113	182.28	3277.21	SLV 7	17.98	Si
fin.	2	-189	-993.2	3277.21	SLV 7	3.3	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	182.28	-2651			5199	1957	SLV 7	0.74	No
fin.	2	0	-993.2	-1049			5199	1957	SLV 7	1.86	Si
ini.	2	0	352.11	-4202			5199	1957	SLV 2	0.47	No
fin.	2	0	-1579.46	-1887			5199	1957	SLV 2	1.04	Si
ini.	2	0	-156.59	-2690			5199	1957	SLV 5	0.73	No
fin.	2	0	-1041.27	-170			5199	1957	SLV 5	11.48	Si
ini.	2	0	453.77	-4191			5199	1957	SLV 3	0.47	No
fin.	2	0	-1565.03	-2151			5199	1957	SLV 3	0.91	No
ini.	2	0	-156.59	-2690			5199	1957	SLV 6	0.73	No
fin.	2	0	-1041.27	-170			5199	1957	SLV 6	11.48	Si
ini.	2	0	453.77	-4191			5199	1957	SLV 4	0.47	No
fin.	2	0	-1565.03	-2151			5199	1957	SLV 4	0.91	No
ini.	2	0	-762.45	158			5199	1957	SLV 14	12.39	Si
fin.	2	0	6.28	2139			5199	1957	SLV 14	0.91	No
ini.	2	0	-762.45	158			5199	1957	SLV 13	12.39	Si
fin.	2	0	6.28	2139			5199	1957	SLV 13	0.91	No
ini.	2	0	352.11	-4202			5199	1957	SLV 1	0.47	No
fin.	2	0	-1579.46	-1887			5199	1957	SLV 1	1.04	Si
ini.	2	0	182.28	-2651			5199	1957	SLV 8	0.74	No
fin.	2	0	-993.2	-1049			5199	1957	SLV 8	1.86	Si

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	2.075	SLV 1	Si
V_SLV	0.466	SLV 1	No
PF_SLU	2.361	SLU 81	Si
V_SLU	0.355	SLU 81	No

Trave di accoppiamento 2

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-7.545	-17.728	0.87	1.07	0.2	-8.545	-17.728	0.87	1.07	0.2	1	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb _m	f _{hk}	f _{vk0}	f _{hmedio}	t ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	431	-62.37	91.32	SLU 83	1.46	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
fin.	3	-227	-135.66	91.32	SLU 83	0.67	No
ini.	3	377	-59.82	91.32	SLU 80	1.53	Si
fin.	3	-183	-122.47	91.32	SLU 80	0.75	No
ini.	3	431	-62.37	91.32	SLU 84	1.46	Si
fin.	3	-227	-135.66	91.32	SLU 84	0.67	No
ini.	3	377	-59.82	91.32	SLU 76	1.53	Si
fin.	3	-183	-122.47	91.32	SLU 76	0.75	No
ini.	3	377	-59.82	91.32	SLU 79	1.53	Si
fin.	3	-183	-122.47	91.32	SLU 79	0.75	No
ini.	3	377	-59.82	91.32	SLU 75	1.53	Si
fin.	3	-183	-122.47	91.32	SLU 75	0.75	No
ini.	3	377	-59.82	91.32	SLU 77	1.53	Si
fin.	3	-183	-122.47	91.32	SLU 77	0.75	No
ini.	3	377	-59.82	91.32	SLU 78	1.53	Si
fin.	3	-183	-122.47	91.32	SLU 78	0.75	No
ini.	3	431	-62.37	91.32	SLU 81	1.46	Si
fin.	3	-227	-135.66	91.32	SLU 81	0.67	No
ini.	3	431	-62.37	91.32	SLU 82	1.46	Si
fin.	3	-227	-135.66	91.32	SLU 82	0.67	No

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-59.82	433			231	87	SLU 79	0.2	No
fin.	3	0	-122.47	-722			231	87	SLU 79	0.12	No
ini.	3	0	-59.82	433			231	87	SLU 78	0.2	No
fin.	3	0	-122.47	-722			231	87	SLU 78	0.12	No
ini.	3	0	-62.37	455			231	87	SLU 83	0.19	No
fin.	3	0	-135.66	-794			231	87	SLU 83	0.11	No
ini.	3	0	-62.37	455			231	87	SLU 84	0.19	No
fin.	3	0	-135.66	-794			231	87	SLU 84	0.11	No
ini.	3	0	-62.37	455			231	87	SLU 82	0.19	No
fin.	3	0	-135.66	-794			231	87	SLU 82	0.11	No
ini.	3	0	-59.82	433			231	87	SLU 80	0.2	No
fin.	3	0	-122.47	-722			231	87	SLU 80	0.12	No
ini.	3	0	-59.82	433			231	87	SLU 76	0.2	No
fin.	3	0	-122.47	-722			231	87	SLU 76	0.12	No
ini.	3	0	-59.82	433			231	87	SLU 77	0.2	No
fin.	3	0	-122.47	-722			231	87	SLU 77	0.12	No
ini.	3	0	-59.82	433			231	87	SLU 75	0.2	No
fin.	3	0	-122.47	-722			231	87	SLU 75	0.12	No
ini.	3	0	-62.37	455			231	87	SLU 81	0.19	No
fin.	3	0	-135.66	-794			231	87	SLU 81	0.11	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	310	-30.09	136.99	SLV 8	4.55	Si
fin.	2	-268	-95.09	136.99	SLV 8	1.44	Si
ini.	2	-430	-84.37	136.99	SLV 15	1.62	Si
fin.	2	127	-22.73	136.99	SLV 15	6.03	Si
ini.	2	-430	-84.37	136.99	SLV 16	1.62	Si
fin.	2	127	-22.73	136.99	SLV 16	6.03	Si
ini.	2	502	-28.38	136.99	SLV 6	4.83	Si
fin.	2	-42	-89.1	136.99	SLV 6	1.54	Si
ini.	2	502	-28.38	136.99	SLV 5	4.83	Si
fin.	2	-42	-89.1	136.99	SLV 5	1.54	Si
ini.	2	869	0.57	136.99	SLV 2	240.4	Si
fin.	2	-292	-129.03	136.99	SLV 2	1.06	Si
ini.	2	310	-30.09	136.99	SLV 7	4.55	Si
fin.	2	-268	-95.09	136.99	SLV 7	1.44	Si
ini.	2	869	0.57	136.99	SLV 1	240.4	Si
fin.	2	-292	-129.03	136.99	SLV 1	1.06	Si
ini.	2	811	0.06	136.99	SLV 3	2298.32	Si
fin.	2	-360	-130.82	136.99	SLV 3	1.05	Si
ini.	2	811	0.06	136.99	SLV 4	2298.32	Si
fin.	2	-360	-130.82	136.99	SLV 4	1.05	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	0.06	25			347	130	SLV 4	5.18	Si
fin.	2	0	-130.82	-792			347	130	SLV 4	0.16	No
ini.	2	0	0.06	25			347	130	SLV 3	5.18	Si
fin.	2	0	-130.82	-792			347	130	SLV 3	0.16	No
ini.	2	0	0.57	49			347	130	SLV 2	2.65	Si
fin.	2	0	-129.03	-796			347	130	SLV 2	0.16	No
ini.	2	0	-28.38	261			347	130	SLV 5	0.5	No
fin.	2	0	-89.1	-564			347	130	SLV 5	0.23	No
ini.	2	0	0.57	49			347	130	SLV 1	2.65	Si
fin.	2	0	-129.03	-796			347	130	SLV 1	0.16	No
ini.	2	0	-83.86	573			347	130	SLV 13	0.23	No
fin.	2	0	-20.94	-119			347	130	SLV 13	1.09	Si
ini.	2	0	-30.09	180			347	130	SLV 8	0.72	No
fin.	2	0	-95.09	-550			347	130	SLV 8	0.24	No
ini.	2	0	-30.09	180			347	130	SLV 7	0.72	No
fin.	2	0	-95.09	-550			347	130	SLV 7	0.24	No
ini.	2	0	-83.86	573			347	130	SLV 14	0.23	No
fin.	2	0	-20.94	-119			347	130	SLV 14	1.09	Si
ini.	2	0	-28.38	261			347	130	SLV 6	0.5	No
fin.	2	0	-89.1	-564			347	130	SLV 6	0.23	No



Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.047	SLV 3	Si
V_SLV	0.164	SLV 1	No
PF_SLU	0.673	SLU 81	No
V_SLU	0.11	SLU 81	No

Trave di accoppiamento 3

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
1.227	-17.729	-1.53	0.47	2	0.227	-17.728	-1.53	0.47	2	1	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _{tk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-745	-1086.26	3165.81	SLU 73	2.91	Si
fin.	3	-1613	-143.08	3165.81	SLU 73	22.13	Si
ini.	3	-746	-1191.71	3165.81	SLU 82	2.66	Si
fin.	3	-1708	-111.18	3165.81	SLU 82	28.48	Si
ini.	3	-745	-1086.26	3165.81	SLU 78	2.91	Si
fin.	3	-1613	-143.08	3165.81	SLU 78	22.13	Si
ini.	3	-746	-1191.71	3165.81	SLU 81	2.66	Si
fin.	3	-1708	-111.18	3165.81	SLU 81	28.48	Si
ini.	3	-745	-1086.26	3165.81	SLU 74	2.91	Si
fin.	3	-1613	-143.08	3165.81	SLU 74	22.13	Si
ini.	3	-745	-1086.26	3165.81	SLU 76	2.91	Si
fin.	3	-1613	-143.08	3165.81	SLU 76	22.13	Si
ini.	3	-745	-1086.26	3165.81	SLU 75	2.91	Si
fin.	3	-1613	-143.08	3165.81	SLU 75	22.13	Si
ini.	3	-746	-1191.71	3165.81	SLU 84	2.66	Si
fin.	3	-1708	-111.18	3165.81	SLU 84	28.48	Si
ini.	3	-745	-1086.26	3165.81	SLU 79	2.91	Si
fin.	3	-1613	-143.08	3165.81	SLU 79	22.13	Si
ini.	3	-746	-1191.71	3165.81	SLU 83	2.66	Si
fin.	3	-1708	-111.18	3165.81	SLU 83	28.48	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	γM	N	M	V	V _t	V _p	V _t fess. diag.	V _{t,lim}	Comb.	c.s.	Verifica
ini.	3	0	-1191.71	-220			3466	1304	SLU 83	5.94	Si
fin.	3	0	-111.18	3348			3466	1304	SLU 83	0.39	No
ini.	3	0	-1057.68	-132			3466	1304	SLU 40	9.88	Si
fin.	3	0	-48.42	3058			3466	1304	SLU 40	0.43	No
ini.	3	0	-1191.71	-220			3466	1304	SLU 82	5.94	Si
fin.	3	0	-111.18	3348			3466	1304	SLU 82	0.39	No
ini.	3	0	-1086.26	-261			3466	1304	SLU 77	5	Si
fin.	3	0	-143.08	2991			3466	1304	SLU 77	0.44	No
ini.	3	0	-1191.71	-220			3466	1304	SLU 81	5.94	Si
fin.	3	0	-111.18	3348			3466	1304	SLU 81	0.39	No
ini.	3	0	-1086.26	-261			3466	1304	SLU 75	5	Si
fin.	3	0	-143.08	2991			3466	1304	SLU 75	0.44	No
ini.	3	0	-1057.68	-132			3466	1304	SLU 39	9.88	Si
fin.	3	0	-48.42	3058			3466	1304	SLU 39	0.43	No
ini.	3	0	-1057.68	-132			3466	1304	SLU 42	9.88	Si
fin.	3	0	-48.42	3058			3466	1304	SLU 42	0.43	No
ini.	3	0	-1191.71	-220			3466	1304	SLU 84	5.94	Si
fin.	3	0	-111.18	3348			3466	1304	SLU 84	0.39	No
ini.	3	0	-1057.68	-132			3466	1304	SLU 41	9.88	Si
fin.	3	0	-48.42	3058			3466	1304	SLU 41	0.43	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-8	-1369.6	3277.21	SLV 15	2.39	Si
fin.	2	-1357	507.61	3277.21	SLV 15	6.46	Si
ini.	2	-484	-1111.1	3277.21	SLV 9	2.95	Si
fin.	2	-1279	-128.87	3277.21	SLV 9	25.43	Si
ini.	2	-1129	-10.4	3277.21	SLV 2	315.03	Si
fin.	2	-852	-810.89	3277.21	SLV 2	4.04	Si
ini.	2	-54	-1489.17	3277.21	SLV 13	2.2	Si
fin.	2	-1411	411.28	3277.21	SLV 13	7.97	Si
ini.	2	-1083	109.17	3277.21	SLV 3	30.02	Si
fin.	2	-798	-714.56	3277.21	SLV 3	4.59	Si
ini.	2	-8	-1369.6	3277.21	SLV 16	2.39	Si
fin.	2	-1357	507.61	3277.21	SLV 16	6.46	Si
ini.	2	-1083	109.17	3277.21	SLV 4	30.02	Si
fin.	2	-798	-714.56	3277.21	SLV 4	4.59	Si
ini.	2	-1129	-10.4	3277.21	SLV 1	315.03	Si
fin.	2	-852	-810.89	3277.21	SLV 1	4.04	Si



Sezione	γM	N	M	μ	Comb.	c.s.	Verifica
ini.	2	-484	-1111.1	3277.21	SLV 10	2.95	Si
fin.	2	-1279	-128.87	3277.21	SLV 10	25.43	Si
ini.	2	-54	-1489.17	3277.21	SLV 14	2.2	Si
fin.	2	-1411	411.28	3277.21	SLV 14	7.97	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-1369.6	1913			5199	1957	SLV 16	1.02	Si
fin.	2	0	507.61	3981			5199	1957	SLV 16	0.49	No
ini.	2	0	-712.53	784			5199	1957	SLV 12	2.5	Si
fin.	2	0	192.25	2414			5199	1957	SLV 12	0.81	No
ini.	2	0	-1369.6	1913			5199	1957	SLV 15	1.02	Si
fin.	2	0	507.61	3981			5199	1957	SLV 15	0.49	No
ini.	2	0	-10.4	-2412			5199	1957	SLV 1	0.81	No
fin.	2	0	-810.89	-369			5199	1957	SLV 1	5.3	Si
ini.	2	0	-10.4	-2412			5199	1957	SLV 2	0.81	No
fin.	2	0	-810.89	-369			5199	1957	SLV 2	5.3	Si
ini.	2	0	-1111.1	-62			5199	1957	SLV 10	31.61	Si
fin.	2	0	-128.87	2513			5199	1957	SLV 10	0.78	No
ini.	2	0	-712.53	784			5199	1957	SLV 11	2.5	Si
fin.	2	0	192.25	2414			5199	1957	SLV 11	0.81	No
ini.	2	0	-1489.17	1659			5199	1957	SLV 14	1.18	Si
fin.	2	0	411.28	4011			5199	1957	SLV 14	0.49	No
ini.	2	0	-1111.1	-62			5199	1957	SLV 9	31.61	Si
fin.	2	0	-128.87	2513			5199	1957	SLV 9	0.78	No
ini.	2	0	-1489.17	1659			5199	1957	SLV 13	1.18	Si
fin.	2	0	411.28	4011			5199	1957	SLV 13	0.49	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	2.201	SLV 13	Si
V_SLV	0.488	SLV 13	No
PF_SLU	2.657	SLU 81	Si
V_SLU	0.39	SLU 81	No

Trave di accoppiamento 4

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
1.227	-17.729	0.87	1.07	0.2	0.227	-17.728	0.87	1.07	0.2	1	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f_b	f_{hk}	f_{vk0}	f_{hmedio}	τ_0	f_{v0}	μ	ϕ	$f_{vk,lim}$	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	γM	N	M	μ	Comb.	c.s.	Verifica
ini.	3	-242	-137.71	91.32	SLU 81	0.66	No
fin.	3	399	-64.47	91.32	SLU 81	1.42	Si
ini.	3	-197	-124.38	91.32	SLU 80	0.73	No
fin.	3	349	-61.65	91.32	SLU 80	1.48	Si
ini.	3	-197	-124.38	91.32	SLU 75	0.73	No
fin.	3	349	-61.65	91.32	SLU 75	1.48	Si
ini.	3	-242	-137.71	91.32	SLU 83	0.66	No
fin.	3	399	-64.47	91.32	SLU 83	1.42	Si
ini.	3	-197	-124.38	91.32	SLU 79	0.73	No
fin.	3	349	-61.65	91.32	SLU 79	1.48	Si
ini.	3	-242	-137.71	91.32	SLU 82	0.66	No
fin.	3	399	-64.47	91.32	SLU 82	1.42	Si
ini.	3	-242	-137.71	91.32	SLU 84	0.66	No
fin.	3	399	-64.47	91.32	SLU 84	1.42	Si
ini.	3	-197	-124.38	91.32	SLU 76	0.73	No
fin.	3	349	-61.65	91.32	SLU 76	1.48	Si
ini.	3	-197	-124.38	91.32	SLU 77	0.73	No
fin.	3	349	-61.65	91.32	SLU 77	1.48	Si
ini.	3	-197	-124.38	91.32	SLU 78	0.73	No
fin.	3	349	-61.65	91.32	SLU 78	1.48	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-124.38	731			231	87	SLU 80	0.12	No
fin.	3	0	-61.65	-442			231	87	SLU 80	0.2	No
ini.	3	0	-137.71	803			231	87	SLU 84	0.11	No
fin.	3	0	-64.47	-466			231	87	SLU 84	0.19	No
ini.	3	0	-124.38	731			231	87	SLU 79	0.12	No
fin.	3	0	-61.65	-442			231	87	SLU 79	0.2	No
ini.	3	0	-137.71	803			231	87	SLU 83	0.11	No
fin.	3	0	-64.47	-466			231	87	SLU 83	0.19	No
ini.	3	0	-124.38	731			231	87	SLU 78	0.12	No
fin.	3	0	-61.65	-442			231	87	SLU 78	0.2	No
ini.	3	0	-137.71	803			231	87	SLU 81	0.11	No



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
fin.	3	0	-64.47	-466			231	87	SLU 81	0.19	No
ini.	3	0	-137.71	803			231	87	SLU 82	0.11	No
fin.	3	0	-64.47	-466			231	87	SLU 82	0.19	No
ini.	3	0	-124.38	731			231	87	SLU 75	0.12	No
fin.	3	0	-61.65	-442			231	87	SLU 75	0.2	No
ini.	3	0	-124.38	731			231	87	SLU 77	0.12	No
fin.	3	0	-61.65	-442			231	87	SLU 77	0.2	No
ini.	3	0	-124.38	731			231	87	SLU 76	0.12	No
fin.	3	0	-61.65	-442			231	87	SLU 76	0.2	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-57	-91.81	136.99	SLV 9	1.49	Si
fin.	2	491	-28.91	136.99	SLV 9	4.74	Si
ini.	2	-307	-131.07	136.99	SLV 13	1.05	Si
fin.	2	867	1.69	136.99	SLV 13	81.05	Si
ini.	2	125	-23.23	136.99	SLV 3	5.9	Si
fin.	2	-462	-87.59	136.99	SLV 3	1.56	Si
ini.	2	-275	-95.14	136.99	SLV 11	1.44	Si
fin.	2	295	-30.33	136.99	SLV 11	4.52	Si
ini.	2	125	-23.23	136.99	SLV 4	5.9	Si
fin.	2	-462	-87.59	136.99	SLV 4	1.56	Si
ini.	2	-373	-132.07	136.99	SLV 16	1.04	Si
fin.	2	808	1.26	136.99	SLV 16	108.31	Si
ini.	2	-275	-95.14	136.99	SLV 12	1.44	Si
fin.	2	295	-30.33	136.99	SLV 12	4.52	Si
ini.	2	-307	-131.07	136.99	SLV 14	1.05	Si
fin.	2	867	1.69	136.99	SLV 14	81.05	Si
ini.	2	-57	-91.81	136.99	SLV 10	1.49	Si
fin.	2	491	-28.91	136.99	SLV 10	4.74	Si
ini.	2	-373	-132.07	136.99	SLV 15	1.04	Si
fin.	2	808	1.26	136.99	SLV 15	108.31	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-22.23	126			347	130	SLV 1	1.03	Si
fin.	2	0	-87.16	-577			347	130	SLV 1	0.23	No
ini.	2	0	-131.07	804			347	130	SLV 14	0.16	No
fin.	2	0	1.69	-52			347	130	SLV 14	2.51	Si
ini.	2	0	-132.07	797			347	130	SLV 15	0.16	No
fin.	2	0	1.26	-32			347	130	SLV 15	4.09	Si
ini.	2	0	-131.07	804			347	130	SLV 13	0.16	No
fin.	2	0	1.69	-52			347	130	SLV 13	2.51	Si
ini.	2	0	-22.23	126			347	130	SLV 2	1.03	Si
fin.	2	0	-87.16	-577			347	130	SLV 2	0.23	No
ini.	2	0	-91.81	575			347	130	SLV 10	0.23	No
fin.	2	0	-28.91	-259			347	130	SLV 10	0.5	No
ini.	2	0	-23.23	119			347	130	SLV 3	1.09	Si
fin.	2	0	-87.59	-557			347	130	SLV 3	0.23	No
ini.	2	0	-23.23	119			347	130	SLV 4	1.09	Si
fin.	2	0	-87.59	-557			347	130	SLV 4	0.23	No
ini.	2	0	-91.81	575			347	130	SLV 9	0.23	No
fin.	2	0	-28.91	-259			347	130	SLV 9	0.5	No
ini.	2	0	-132.07	797			347	130	SLV 16	0.16	No
fin.	2	0	1.26	-32			347	130	SLV 16	4.09	Si

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.037	SLV 15	Si
V_SLV	0.162	SLV 13	No
PF_SLU	0.663	SLU 81	No
V_SLU	0.108	SLU 81	No

Trave di accoppiamento 5

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-8.054	-13.248	0.57	1.07	0.5	-9.054	-13.248	0.57	1.07	0.5	1	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	2050	37.29	540.81	SLU 82	14.5	Si
fin.	3	1118	-251.35	540.81	SLU 82	2.15	Si
ini.	3	1912	48.79	540.81	SLU 39	11.08	Si
fin.	3	1014	-229.75	540.81	SLU 39	2.35	Si
ini.	3	2050	37.29	540.81	SLU 84	14.5	Si
fin.	3	1118	-251.35	540.81	SLU 84	2.15	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	1797	20.34	540.81	SLU 77	26.59	Si
fin.	3	1007	-224.01	540.81	SLU 77	2.41	Si
ini.	3	2050	37.29	540.81	SLU 83	14.5	Si
fin.	3	1118	-251.35	540.81	SLU 83	2.15	Si
ini.	3	2050	37.29	540.81	SLU 81	14.5	Si
fin.	3	1118	-251.35	540.81	SLU 81	2.15	Si
ini.	3	1912	48.79	540.81	SLU 42	11.08	Si
fin.	3	1014	-229.75	540.81	SLU 42	2.35	Si
ini.	3	1912	48.79	540.81	SLU 40	11.08	Si
fin.	3	1014	-229.75	540.81	SLU 40	2.35	Si
ini.	3	1797	20.34	540.81	SLU 75	26.59	Si
fin.	3	1007	-224.01	540.81	SLU 75	2.41	Si
ini.	3	1912	48.79	540.81	SLU 41	11.08	Si
fin.	3	1014	-229.75	540.81	SLU 41	2.35	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	37.29	1025			578	217	SLU 81	0.21	No
fin.	3	0	-251.35	-2159			578	217	SLU 81	0.1	No
ini.	3	0	20.34	997			578	217	SLU 77	0.22	No
fin.	3	0	-224.01	-1959			578	217	SLU 77	0.11	No
ini.	3	0	37.29	1025			578	217	SLU 83	0.21	No
fin.	3	0	-251.35	-2159			578	217	SLU 83	0.1	No
ini.	3	0	37.29	1025			578	217	SLU 84	0.21	No
fin.	3	0	-251.35	-2159			578	217	SLU 84	0.1	No
ini.	3	0	20.34	997			578	217	SLU 75	0.22	No
fin.	3	0	-224.01	-1959			578	217	SLU 75	0.11	No
ini.	3	0	20.34	997			578	217	SLU 79	0.22	No
fin.	3	0	-224.01	-1959			578	217	SLU 79	0.11	No
ini.	3	0	37.29	1025			578	217	SLU 82	0.21	No
fin.	3	0	-251.35	-2159			578	217	SLU 82	0.1	No
ini.	3	0	20.34	997			578	217	SLU 76	0.22	No
fin.	3	0	-224.01	-1959			578	217	SLU 76	0.11	No
ini.	3	0	20.34	997			578	217	SLU 80	0.22	No
fin.	3	0	-224.01	-1959			578	217	SLU 80	0.11	No
ini.	3	0	20.34	997			578	217	SLU 78	0.22	No
fin.	3	0	-224.01	-1959			578	217	SLU 78	0.11	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-1349	-338.71	652.21	SLV 13	1.93	Si
fin.	2	165	135.04	652.21	SLV 13	4.83	Si
ini.	2	3448	328.29	652.21	SLV 2	1.99	Si
fin.	2	1096	-404.33	652.21	SLV 2	1.61	Si
ini.	2	1804	98.14	652.21	SLV 6	6.65	Si
fin.	2	798	-215.59	652.21	SLV 6	3.03	Si
ini.	2	3418	325.46	652.21	SLV 4	2	Si
fin.	2	1072	-404.3	652.21	SLV 4	1.61	Si
ini.	2	-1379	-341.53	652.21	SLV 16	1.91	Si
fin.	2	141	135.07	652.21	SLV 16	4.83	Si
ini.	2	3448	328.29	652.21	SLV 1	1.99	Si
fin.	2	1096	-404.33	652.21	SLV 1	1.61	Si
ini.	2	-1349	-338.71	652.21	SLV 14	1.93	Si
fin.	2	165	135.04	652.21	SLV 14	4.83	Si
ini.	2	-1379	-341.53	652.21	SLV 15	1.91	Si
fin.	2	141	135.07	652.21	SLV 15	4.83	Si
ini.	2	1804	98.14	652.21	SLV 5	6.65	Si
fin.	2	798	-215.59	652.21	SLV 5	3.03	Si
ini.	2	3418	325.46	652.21	SLV 3	2	Si
fin.	2	1072	-404.3	652.21	SLV 3	1.61	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	328.29	-363			867	326	SLV 1	0.9	No
fin.	2	0	-404.33	-2139			867	326	SLV 1	0.15	No
ini.	2	0	-338.71	1790			867	326	SLV 13	0.18	No
fin.	2	0	135.04	-322			867	326	SLV 13	1.01	Si
ini.	2	0	-338.71	1790			867	326	SLV 14	0.18	No
fin.	2	0	135.04	-322			867	326	SLV 14	1.01	Si
ini.	2	0	98.14	378			867	326	SLV 6	0.86	No
fin.	2	0	-215.59	-1512			867	326	SLV 6	0.22	No
ini.	2	0	-341.53	1800			867	326	SLV 15	0.18	No
fin.	2	0	135.07	-314			867	326	SLV 15	1.04	Si
ini.	2	0	98.14	378			867	326	SLV 5	0.86	No
fin.	2	0	-215.59	-1512			867	326	SLV 5	0.22	No
ini.	2	0	325.46	-353			867	326	SLV 4	0.92	No
fin.	2	0	-404.3	-2132			867	326	SLV 4	0.15	No
ini.	2	0	-341.53	1800			867	326	SLV 16	0.18	No
fin.	2	0	135.07	-314			867	326	SLV 16	1.04	Si
ini.	2	0	325.46	-353			867	326	SLV 3	0.92	No
fin.	2	0	-404.3	-2132			867	326	SLV 3	0.15	No
ini.	2	0	328.29	-363			867	326	SLV 2	0.9	No
fin.	2	0	-404.33	-2139			867	326	SLV 2	0.15	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.613	SLV 1	Si



Stato limite	Coeff.s.	Comb.	Verifica
V SLV	0.152	SLV 1	No
PF SLU	2.152	SLU 81	Si
V SLU	0.101	SLU 81	No

Trave di accoppiamento 6

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
1.81	-13.249	0.57	1.07	0.5	0.81	-13.248	0.57	1.07	0.5	1	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb _u	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	1132	-251.15	540.81	SLU 77	2.15	Si
fin.	3	1666	7.19	540.81	SLU 77	75.22	Si
ini.	3	1132	-251.15	540.81	SLU 75	2.15	Si
fin.	3	1666	7.19	540.81	SLU 75	75.22	Si
ini.	3	1157	-260.7	540.81	SLU 40	2.07	Si
fin.	3	1778	42.23	540.81	SLU 40	12.81	Si
ini.	3	1157	-260.7	540.81	SLU 39	2.07	Si
fin.	3	1778	42.23	540.81	SLU 39	12.81	Si
ini.	3	1157	-260.7	540.81	SLU 42	2.07	Si
fin.	3	1778	42.23	540.81	SLU 42	12.81	Si
ini.	3	1266	-283.42	540.81	SLU 84	1.91	Si
fin.	3	1903	26.11	540.81	SLU 84	20.71	Si
ini.	3	1266	-283.42	540.81	SLU 81	1.91	Si
fin.	3	1903	26.11	540.81	SLU 81	20.71	Si
ini.	3	1266	-283.42	540.81	SLU 82	1.91	Si
fin.	3	1903	26.11	540.81	SLU 82	20.71	Si
ini.	3	1157	-260.7	540.81	SLU 41	2.07	Si
fin.	3	1778	42.23	540.81	SLU 41	12.81	Si
ini.	3	1266	-283.42	540.81	SLU 83	1.91	Si
fin.	3	1903	26.11	540.81	SLU 83	20.71	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-283.42	1830			578	217	SLU 82	0.12	No
fin.	3	0	26.11	-878			578	217	SLU 82	0.25	No
ini.	3	0	-251.15	1660			578	217	SLU 76	0.13	No
fin.	3	0	7.19	-864			578	217	SLU 76	0.25	No
ini.	3	0	-251.15	1660			578	217	SLU 78	0.13	No
fin.	3	0	7.19	-864			578	217	SLU 78	0.25	No
ini.	3	0	-251.15	1660			578	217	SLU 80	0.13	No
fin.	3	0	7.19	-864			578	217	SLU 80	0.25	No
ini.	3	0	-251.15	1660			578	217	SLU 75	0.13	No
fin.	3	0	7.19	-864			578	217	SLU 75	0.25	No
ini.	3	0	-283.42	1830			578	217	SLU 83	0.12	No
fin.	3	0	26.11	-878			578	217	SLU 83	0.25	No
ini.	3	0	-283.42	1830			578	217	SLU 84	0.12	No
fin.	3	0	26.11	-878			578	217	SLU 84	0.25	No
ini.	3	0	-251.15	1660			578	217	SLU 77	0.13	No
fin.	3	0	7.19	-864			578	217	SLU 77	0.25	No
ini.	3	0	-251.15	1660			578	217	SLU 79	0.13	No
fin.	3	0	7.19	-864			578	217	SLU 79	0.25	No
ini.	3	0	-283.42	1830			578	217	SLU 81	0.12	No
fin.	3	0	26.11	-878			578	217	SLU 81	0.25	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	1391	-443.37	652.21	SLV 13	1.47	Si
fin.	2	3083	354.84	652.21	SLV 13	1.84	Si
ini.	2	1391	-443.37	652.21	SLV 14	1.47	Si
fin.	2	3083	354.84	652.21	SLV 14	1.84	Si
ini.	2	863	-258.99	652.21	SLV 10	2.52	Si
fin.	2	1618	110.95	652.21	SLV 10	5.88	Si
ini.	2	-23	145.67	652.21	SLV 3	4.48	Si
fin.	2	-1171	-393.22	652.21	SLV 3	1.66	Si
ini.	2	1412	-429	652.21	SLV 16	1.52	Si
fin.	2	3067	343.02	652.21	SLV 16	1.9	Si
ini.	2	-23	145.67	652.21	SLV 4	4.48	Si
fin.	2	-1171	-393.22	652.21	SLV 4	1.66	Si
ini.	2	-44	131.31	652.21	SLV 1	4.97	Si
fin.	2	-1155	-381.4	652.21	SLV 1	1.71	Si
ini.	2	863	-258.99	652.21	SLV 9	2.52	Si
fin.	2	1618	110.95	652.21	SLV 9	5.88	Si
ini.	2	1412	-429	652.21	SLV 15	1.52	Si
fin.	2	3067	343.02	652.21	SLV 15	1.9	Si
ini.	2	-44	131.31	652.21	SLV 2	4.97	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
fin.	2	-1155	-381.4	652.21	SLV 2	1.71	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-258.99	1354			867	326	SLV 9	0.24	No
fin.	2	0	110.95	-317			867	326	SLV 9	1.03	Si
ini.	2	0	-443.37	1911			867	326	SLV 14	0.17	No
fin.	2	0	354.84	340			867	326	SLV 14	0.96	No
ini.	2	0	-258.99	1354			867	326	SLV 10	0.24	No
fin.	2	0	110.95	-317			867	326	SLV 10	1.03	Si
ini.	2	0	145.67	167			867	326	SLV 3	1.95	Si
fin.	2	0	-393.22	-1615			867	326	SLV 3	0.2	No
ini.	2	0	-429	1876			867	326	SLV 16	0.17	No
fin.	2	0	343.02	323			867	326	SLV 16	1.01	Si
ini.	2	0	131.31	203			867	326	SLV 2	1.61	Si
fin.	2	0	-381.4	-1598			867	326	SLV 2	0.2	No
ini.	2	0	145.67	167			867	326	SLV 4	1.95	Si
fin.	2	0	-393.22	-1615			867	326	SLV 4	0.2	No
ini.	2	0	131.31	203			867	326	SLV 1	1.61	Si
fin.	2	0	-381.4	-1598			867	326	SLV 1	0.2	No
ini.	2	0	-443.37	1911			867	326	SLV 13	0.17	No
fin.	2	0	354.84	340			867	326	SLV 13	0.96	No
ini.	2	0	-429	1876			867	326	SLV 15	0.17	No
fin.	2	0	343.02	323			867	326	SLV 15	1.01	Si

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV		SLV 13	Si
V_SLV	0.171	SLV 13	No
PF_SLU	1.908	SLU 81	Si
V_SLU	0.119	SLU 81	No

Trave di accoppiamento 7

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-6.101	-8.718	-1.53	0.47	2	-7.101	-8.718	-1.53	0.47	2	1	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-2802	-95.71	3165.81	SLU 74	33.08	Si
fin.	3	-2175	-832.25	3165.81	SLU 74	3.8	Si
ini.	3	-2967	-90.96	3165.81	SLU 82	34.8	Si
fin.	3	-2276	-904.87	3165.81	SLU 82	3.5	Si
ini.	3	-2802	-95.71	3165.81	SLU 78	33.08	Si
fin.	3	-2175	-832.25	3165.81	SLU 78	3.8	Si
ini.	3	-2802	-95.71	3165.81	SLU 75	33.08	Si
fin.	3	-2175	-832.25	3165.81	SLU 75	3.8	Si
ini.	3	-2967	-90.96	3165.81	SLU 81	34.8	Si
fin.	3	-2276	-904.87	3165.81	SLU 81	3.5	Si
ini.	3	-2802	-95.71	3165.81	SLU 76	33.08	Si
fin.	3	-2175	-832.25	3165.81	SLU 76	3.8	Si
ini.	3	-2967	-90.96	3165.81	SLU 83	34.8	Si
fin.	3	-2276	-904.87	3165.81	SLU 83	3.5	Si
ini.	3	-2802	-95.71	3165.81	SLU 79	33.08	Si
fin.	3	-2175	-832.25	3165.81	SLU 79	3.8	Si
ini.	3	-2802	-95.71	3165.81	SLU 73	33.08	Si
fin.	3	-2175	-832.25	3165.81	SLU 73	3.8	Si
ini.	3	-2967	-90.96	3165.81	SLU 84	34.8	Si
fin.	3	-2276	-904.87	3165.81	SLU 84	3.5	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-90.96	-3697			3466	1304	SLU 83	0.35	No
fin.	3	0	-904.87	217			3466	1304	SLU 83	6.01	Si
ini.	3	0	-90.96	-3697			3466	1304	SLU 81	0.35	No
fin.	3	0	-904.87	217			3466	1304	SLU 81	6.01	Si
ini.	3	0	-95.71	-3373			3466	1304	SLU 74	0.39	No
fin.	3	0	-832.25	207			3466	1304	SLU 74	6.31	Si
ini.	3	0	-90.96	-3697			3466	1304	SLU 82	0.35	No
fin.	3	0	-904.87	217			3466	1304	SLU 82	6.01	Si
ini.	3	0	-95.71	-3373			3466	1304	SLU 76	0.39	No
fin.	3	0	-832.25	207			3466	1304	SLU 76	6.31	Si
ini.	3	0	-95.71	-3373			3466	1304	SLU 73	0.39	No
fin.	3	0	-832.25	207			3466	1304	SLU 73	6.31	Si
ini.	3	0	-90.96	-3697			3466	1304	SLU 84	0.35	No
fin.	3	0	-904.87	217			3466	1304	SLU 84	6.01	Si



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-95.71	-3373			3466	1304	SLU 79	0.39	No
fin.	3	0	-832.25	207			3466	1304	SLU 79	6.31	Si
ini.	3	0	-95.71	-3373			3466	1304	SLU 78	0.39	No
fin.	3	0	-832.25	207			3466	1304	SLU 78	6.31	Si
ini.	3	0	-95.71	-3373			3466	1304	SLU 75	0.39	No
fin.	3	0	-832.25	207			3466	1304	SLU 75	6.31	Si

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-1314	-862.78	3277.21	SLV 16	3.8	Si
fin.	2	-1923	402.62	3277.21	SLV 16	8.14	Si
ini.	2	-2523	703.62	3277.21	SLV 1	4.66	Si
fin.	2	-1125	-1483.89	3277.21	SLV 1	2.21	Si
ini.	2	-1161	-859.72	3277.21	SLV 14	3.81	Si
fin.	2	-1840	474.04	3277.21	SLV 14	6.91	Si
ini.	2	-2379	149.83	3277.21	SLV 7	21.87	Si
fin.	2	-1556	-953.36	3277.21	SLV 7	3.44	Si
ini.	2	-2676	700.56	3277.21	SLV 3	4.68	Si
fin.	2	-1208	-1555.31	3277.21	SLV 3	2.11	Si
ini.	2	-1314	-862.78	3277.21	SLV 15	3.8	Si
fin.	2	-1923	402.62	3277.21	SLV 15	8.14	Si
ini.	2	-2676	700.56	3277.21	SLV 4	4.68	Si
fin.	2	-1208	-1555.31	3277.21	SLV 4	2.11	Si
ini.	2	-1161	-859.72	3277.21	SLV 13	3.81	Si
fin.	2	-1840	474.04	3277.21	SLV 13	6.91	Si
ini.	2	-2523	703.62	3277.21	SLV 2	4.66	Si
fin.	2	-1125	-1483.89	3277.21	SLV 2	2.21	Si
ini.	2	-2379	149.83	3277.21	SLV 8	21.87	Si
fin.	2	-1556	-953.36	3277.21	SLV 8	3.44	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-859.72	892			5199	1957	SLV 14	2.19	Si
fin.	2	0	474.04	2878			5199	1957	SLV 14	0.68	No
ini.	2	0	-862.78	759			5199	1957	SLV 16	2.58	Si
fin.	2	0	402.62	2925			5199	1957	SLV 16	0.67	No
ini.	2	0	-859.72	892			5199	1957	SLV 13	2.19	Si
fin.	2	0	474.04	2878			5199	1957	SLV 13	0.68	No
ini.	2	0	700.56	-5176			5199	1957	SLV 4	0.38	No
fin.	2	0	-1555.31	-2603			5199	1957	SLV 4	0.75	No
ini.	2	0	149.83	-3255			5199	1957	SLV 8	0.6	No
fin.	2	0	-953.36	-612			5199	1957	SLV 8	3.19	Si
ini.	2	0	700.56	-5176			5199	1957	SLV 3	0.38	No
fin.	2	0	-1555.31	-2603			5199	1957	SLV 3	0.75	No
ini.	2	0	149.83	-3255			5199	1957	SLV 7	0.6	No
fin.	2	0	-953.36	-612			5199	1957	SLV 7	3.19	Si
ini.	2	0	703.62	-5042			5199	1957	SLV 2	0.39	No
fin.	2	0	-1483.89	-2650			5199	1957	SLV 2	0.74	No
ini.	2	0	-862.78	759			5199	1957	SLV 15	2.58	Si
fin.	2	0	402.62	2925			5199	1957	SLV 15	0.67	No
ini.	2	0	703.62	-5042			5199	1957	SLV 1	0.39	No
fin.	2	0	-1483.89	-2650			5199	1957	SLV 1	0.74	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	2.107	SLV 3	Si
V_SLV	0.378	SLV 3	No
PF_SLU	3.499	SLU 81	Si
V_SLU	0.353	SLU 81	No

Trave di accoppiamento 8

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-6.101	-8.718	0.87	1.07	0.2	-7.101	-8.718	0.87	1.07	0.2	1	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _{tk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	113	-86.7	91.32	SLU 83	1.05	Si
fin.	3	-70	-109.81	91.32	SLU 83	0.83	No
ini.	3	95	-80.76	91.32	SLU 78	1.13	Si
fin.	3	-61	-100.67	91.32	SLU 78	0.91	No
ini.	3	95	-80.76	91.32	SLU 74	1.13	Si
fin.	3	-61	-100.67	91.32	SLU 74	0.91	No
ini.	3	95	-80.76	91.32	SLU 76	1.13	Si
fin.	3	-61	-100.67	91.32	SLU 76	0.91	No
ini.	3	95	-80.76	91.32	SLU 79	1.13	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
fin.	3	-61	-100.67	91.32	SLU 79	0.91	No
ini.	3	113	-86.7	91.32	SLU 81	1.05	Si
fin.	3	-70	-109.81	91.32	SLU 81	0.83	No
ini.	3	95	-80.76	91.32	SLU 75	1.13	Si
fin.	3	-61	-100.67	91.32	SLU 75	0.91	No
ini.	3	113	-86.7	91.32	SLU 82	1.05	Si
fin.	3	-70	-109.81	91.32	SLU 82	0.83	No
ini.	3	113	-86.7	91.32	SLU 84	1.05	Si
fin.	3	-70	-109.81	91.32	SLU 84	0.83	No
ini.	3	95	-80.76	91.32	SLU 73	1.13	Si
fin.	3	-61	-100.67	91.32	SLU 73	0.91	No

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-86.7	558			231	87	SLU 81	0.16	No
fin.	3	0	-109.81	-668			231	87	SLU 81	0.13	No
ini.	3	0	-80.76	521			231	87	SLU 73	0.17	No
fin.	3	0	-100.67	-616			231	87	SLU 73	0.14	No
ini.	3	0	-80.76	521			231	87	SLU 79	0.17	No
fin.	3	0	-100.67	-616			231	87	SLU 79	0.14	No
ini.	3	0	-80.76	521			231	87	SLU 76	0.17	No
fin.	3	0	-100.67	-616			231	87	SLU 76	0.14	No
ini.	3	0	-80.76	521			231	87	SLU 78	0.17	No
fin.	3	0	-100.67	-616			231	87	SLU 78	0.14	No
ini.	3	0	-86.7	558			231	87	SLU 84	0.16	No
fin.	3	0	-109.81	-668			231	87	SLU 84	0.13	No
ini.	3	0	-86.7	558			231	87	SLU 82	0.16	No
fin.	3	0	-109.81	-668			231	87	SLU 82	0.13	No
ini.	3	0	-86.7	558			231	87	SLU 83	0.16	No
fin.	3	0	-109.81	-668			231	87	SLU 83	0.13	No
ini.	3	0	-80.76	521			231	87	SLU 75	0.17	No
fin.	3	0	-100.67	-616			231	87	SLU 75	0.14	No
ini.	3	0	-80.76	521			231	87	SLU 74	0.17	No
fin.	3	0	-100.67	-616			231	87	SLU 74	0.14	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	520	-0.48	136.99	SLV 2	284.81	Si
fin.	2	-487	-123.8	136.99	SLV 2	1.11	Si
ini.	2	520	-0.48	136.99	SLV 1	284.81	Si
fin.	2	-487	-123.8	136.99	SLV 1	1.11	Si
ini.	2	562	0.68	136.99	SLV 4	201.08	Si
fin.	2	-498	-127.91	136.99	SLV 4	1.07	Si
ini.	2	-462	-107.61	136.99	SLV 13	1.27	Si
fin.	2	429	-1.15	136.99	SLV 13	119.6	Si
ini.	2	-462	-107.61	136.99	SLV 14	1.27	Si
fin.	2	429	-1.15	136.99	SLV 14	119.6	Si
ini.	2	267	-35.46	136.99	SLV 8	3.86	Si
fin.	2	-191	-89.77	136.99	SLV 8	1.53	Si
ini.	2	-421	-106.45	136.99	SLV 16	1.29	Si
fin.	2	418	-5.25	136.99	SLV 16	26.08	Si
ini.	2	562	0.68	136.99	SLV 3	201.08	Si
fin.	2	-498	-127.91	136.99	SLV 3	1.07	Si
ini.	2	-421	-106.45	136.99	SLV 15	1.29	Si
fin.	2	418	-5.25	136.99	SLV 15	26.08	Si
ini.	2	267	-35.46	136.99	SLV 7	3.86	Si
fin.	2	-191	-89.77	136.99	SLV 7	1.53	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-0.48	45			347	130	SLV 2	2.91	Si
fin.	2	0	-123.8	-668			347	130	SLV 2	0.2	No
ini.	2	0	-107.61	640			347	130	SLV 13	0.2	No
fin.	2	0	-1.15	-123			347	130	SLV 13	1.06	Si
ini.	2	0	0.68	54			347	130	SLV 3	2.41	Si
fin.	2	0	-127.91	-677			347	130	SLV 3	0.19	No
ini.	2	0	-35.46	273			347	130	SLV 7	0.48	No
fin.	2	0	-89.77	-496			347	130	SLV 7	0.26	No
ini.	2	0	-107.61	640			347	130	SLV 14	0.2	No
fin.	2	0	-1.15	-123			347	130	SLV 14	1.06	Si
ini.	2	0	-35.46	273			347	130	SLV 8	0.48	No
fin.	2	0	-89.77	-496			347	130	SLV 8	0.26	No
ini.	2	0	-106.45	650			347	130	SLV 15	0.2	No
fin.	2	0	-5.25	-132			347	130	SLV 15	0.99	No
ini.	2	0	-0.48	45			347	130	SLV 1	2.91	Si
fin.	2	0	-123.8	-668			347	130	SLV 1	0.2	No
ini.	2	0	0.68	54			347	130	SLV 4	2.41	Si
fin.	2	0	-127.91	-677			347	130	SLV 4	0.19	No
ini.	2	0	-106.45	650			347	130	SLV 16	0.2	No
fin.	2	0	-5.25	-132			347	130	SLV 16	0.99	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.071	SLV 3	Si
V_SLV	0.193	SLV 3	No
PF_SLU	0.832	SLU 81	No
V_SLU	0.13	SLU 81	No



Trave di accoppiamento 9

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-0.141	-8.718	-1.53	0.47	2	-1.141	-8.718	-1.53	0.47	2	1	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	f _{tk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-2044	-676.81	3165.81	SLU 82	4.68	Si
fin.	3	-3052	-105.4	3165.81	SLU 82	30.04	Si
ini.	3	-1968	-627.05	3165.81	SLU 79	5.05	Si
fin.	3	-2881	-107.34	3165.81	SLU 79	29.49	Si
ini.	3	-2044	-676.81	3165.81	SLU 84	4.68	Si
fin.	3	-3052	-105.4	3165.81	SLU 84	30.04	Si
ini.	3	-1968	-627.05	3165.81	SLU 78	5.05	Si
fin.	3	-2881	-107.34	3165.81	SLU 78	29.49	Si
ini.	3	-1968	-627.05	3165.81	SLU 73	5.05	Si
fin.	3	-2881	-107.34	3165.81	SLU 73	29.49	Si
ini.	3	-2044	-676.81	3165.81	SLU 81	4.68	Si
fin.	3	-3052	-105.4	3165.81	SLU 81	30.04	Si
ini.	3	-1968	-627.05	3165.81	SLU 75	5.05	Si
fin.	3	-2881	-107.34	3165.81	SLU 75	29.49	Si
ini.	3	-2044	-676.81	3165.81	SLU 83	4.68	Si
fin.	3	-3052	-105.4	3165.81	SLU 83	30.04	Si
ini.	3	-1968	-627.05	3165.81	SLU 76	5.05	Si
fin.	3	-2881	-107.34	3165.81	SLU 76	29.49	Si
ini.	3	-1968	-627.05	3165.81	SLU 74	5.05	Si
fin.	3	-2881	-107.34	3165.81	SLU 74	29.49	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-627.05	-2955			3466	1304	SLU 73	0.44	No
fin.	3	0	-107.34	3774			3466	1304	SLU 73	0.35	No
ini.	3	0	-627.05	-2955			3466	1304	SLU 75	0.44	No
fin.	3	0	-107.34	3774			3466	1304	SLU 75	0.35	No
ini.	3	0	-627.05	-2955			3466	1304	SLU 76	0.44	No
fin.	3	0	-107.34	3774			3466	1304	SLU 76	0.35	No
ini.	3	0	-676.81	-3114			3466	1304	SLU 84	0.42	No
fin.	3	0	-105.4	4126			3466	1304	SLU 84	0.32	No
ini.	3	0	-627.05	-2955			3466	1304	SLU 78	0.44	No
fin.	3	0	-107.34	3774			3466	1304	SLU 78	0.35	No
ini.	3	0	-676.81	-3114			3466	1304	SLU 81	0.42	No
fin.	3	0	-105.4	4126			3466	1304	SLU 81	0.32	No
ini.	3	0	-676.81	-3114			3466	1304	SLU 83	0.42	No
fin.	3	0	-105.4	4126			3466	1304	SLU 83	0.32	No
ini.	3	0	-627.05	-2955			3466	1304	SLU 74	0.44	No
fin.	3	0	-107.34	3774			3466	1304	SLU 74	0.35	No
ini.	3	0	-627.05	-2955			3466	1304	SLU 79	0.44	No
fin.	3	0	-107.34	3774			3466	1304	SLU 79	0.35	No
ini.	3	0	-676.81	-3114			3466	1304	SLU 82	0.42	No
fin.	3	0	-105.4	4126			3466	1304	SLU 82	0.32	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-2175	159.73	3277.21	SLV 2	20.52	Si
fin.	2	-1134	-792.21	3277.21	SLV 2	4.14	Si
ini.	2	-623	-988.17	3277.21	SLV 15	3.32	Si
fin.	2	-2806	622.8	3277.21	SLV 15	5.26	Si
ini.	2	-1298	-701.37	3277.21	SLV 12	4.67	Si
fin.	2	-2452	118.63	3277.21	SLV 12	27.63	Si
ini.	2	-536	-912.37	3277.21	SLV 13	3.59	Si
fin.	2	-2654	628.68	3277.21	SLV 13	5.21	Si
ini.	2	-536	-912.37	3277.21	SLV 14	3.59	Si
fin.	2	-2654	628.68	3277.21	SLV 14	5.21	Si
ini.	2	-2262	83.93	3277.21	SLV 3	39.05	Si
fin.	2	-1286	-798.09	3277.21	SLV 3	4.11	Si
ini.	2	-1298	-701.37	3277.21	SLV 11	4.67	Si
fin.	2	-2452	118.63	3277.21	SLV 11	27.63	Si
ini.	2	-623	-988.17	3277.21	SLV 16	3.32	Si
fin.	2	-2806	622.8	3277.21	SLV 16	5.26	Si
ini.	2	-2262	83.93	3277.21	SLV 4	39.05	Si
fin.	2	-1286	-798.09	3277.21	SLV 4	4.11	Si
ini.	2	-2175	159.73	3277.21	SLV 1	20.52	Si
fin.	2	-1134	-792.21	3277.21	SLV 1	4.14	Si



Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-988.17	618			5199	1957	SLV 16	3.17	Si
fin.	2	0	622.8	5476			5199	1957	SLV 16	0.36	No
ini.	2	0	159.73	-4699			5199	1957	SLV 2	0.42	No
fin.	2	0	-792.21	-657			5199	1957	SLV 2	2.98	Si
ini.	2	0	-912.37	740			5199	1957	SLV 14	2.64	Si
fin.	2	0	628.68	5326			5199	1957	SLV 14	0.37	No
ini.	2	0	-701.37	-1427			5199	1957	SLV 11	1.37	Si
fin.	2	0	118.63	3557			5199	1957	SLV 11	0.55	No
ini.	2	0	83.93	-4820			5199	1957	SLV 3	0.41	No
fin.	2	0	-798.09	-507			5199	1957	SLV 3	3.86	Si
ini.	2	0	-988.17	618			5199	1957	SLV 15	3.17	Si
fin.	2	0	622.8	5476			5199	1957	SLV 15	0.36	No
ini.	2	0	83.93	-4820			5199	1957	SLV 4	0.41	No
fin.	2	0	-798.09	-507			5199	1957	SLV 4	3.86	Si
ini.	2	0	-912.37	740			5199	1957	SLV 13	2.64	Si
fin.	2	0	628.68	5326			5199	1957	SLV 13	0.37	No
ini.	2	0	-701.37	-1427			5199	1957	SLV 12	1.37	Si
fin.	2	0	118.63	3557			5199	1957	SLV 12	0.55	No
ini.	2	0	159.73	-4699			5199	1957	SLV 1	0.42	No
fin.	2	0	-792.21	-657			5199	1957	SLV 1	2.98	Si

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV		SLV 15	Si
V_SLV	0.357	SLV 15	No
PF_SLU	4.678	SLU 81	Si
V_SLU	0.316	SLU 81	No

Trave di accoppiamento 10

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-0.141	-8.718	0.87	1.07	0.2	-1.141	-8.718	0.87	1.07	0.2	1	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-42	-101.14	91.32	SLU 73	0.9	No
fin.	3	83	-82.07	91.32	SLU 73	1.11	Si
ini.	3	-42	-101.14	91.32	SLU 78	0.9	No
fin.	3	83	-82.07	91.32	SLU 78	1.11	Si
ini.	3	-42	-101.14	91.32	SLU 74	0.9	No
fin.	3	83	-82.07	91.32	SLU 74	1.11	Si
ini.	3	-48	-110.28	91.32	SLU 84	0.83	No
fin.	3	100	-88.05	91.32	SLU 84	1.04	Si
ini.	3	-42	-101.14	91.32	SLU 76	0.9	No
fin.	3	83	-82.07	91.32	SLU 76	1.11	Si
ini.	3	-42	-101.14	91.32	SLU 75	0.9	No
fin.	3	83	-82.07	91.32	SLU 75	1.11	Si
ini.	3	-42	-101.14	91.32	SLU 79	0.9	No
fin.	3	83	-82.07	91.32	SLU 79	1.11	Si
ini.	3	-48	-110.28	91.32	SLU 82	0.83	No
fin.	3	100	-88.05	91.32	SLU 82	1.04	Si
ini.	3	-48	-110.28	91.32	SLU 81	0.83	No
fin.	3	100	-88.05	91.32	SLU 81	1.04	Si
ini.	3	-48	-110.28	91.32	SLU 83	0.83	No
fin.	3	100	-88.05	91.32	SLU 83	1.04	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-101.14	616			231	87	SLU 76	0.14	No
fin.	3	0	-82.07	-529			231	87	SLU 76	0.16	No
ini.	3	0	-101.14	616			231	87	SLU 74	0.14	No
fin.	3	0	-82.07	-529			231	87	SLU 74	0.16	No
ini.	3	0	-101.14	616			231	87	SLU 75	0.14	No
fin.	3	0	-82.07	-529			231	87	SLU 75	0.16	No
ini.	3	0	-110.28	668			231	87	SLU 82	0.13	No
fin.	3	0	-88.05	-567			231	87	SLU 82	0.15	No
ini.	3	0	-101.14	616			231	87	SLU 78	0.14	No
fin.	3	0	-82.07	-529			231	87	SLU 78	0.16	No
ini.	3	0	-101.14	616			231	87	SLU 79	0.14	No
fin.	3	0	-82.07	-529			231	87	SLU 79	0.16	No
ini.	3	0	-110.28	668			231	87	SLU 81	0.13	No
fin.	3	0	-88.05	-567			231	87	SLU 81	0.15	No
ini.	3	0	-110.28	668			231	87	SLU 84	0.13	No
fin.	3	0	-88.05	-567			231	87	SLU 84	0.15	No



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-110.28	668			231	87	SLU 83	0.13	No
fin.	3	0	-88.05	-567			231	87	SLU 83	0.15	No
ini.	3	0	-101.14	616			231	87	SLU 73	0.14	No
fin.	3	0	-82.07	-529			231	87	SLU 73	0.16	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-169	-89.83	136.99	SLV 12	1.53	Si
fin.	2	261	-35.77	136.99	SLV 12	3.83	Si
ini.	2	411	-4.18	136.99	SLV 1	32.76	Si
fin.	2	-486	-111.49	136.99	SLV 1	1.23	Si
ini.	2	401	-8.63	136.99	SLV 4	15.87	Si
fin.	2	-446	-110.49	136.99	SLV 4	1.24	Si
ini.	2	-169	-89.83	136.99	SLV 11	1.53	Si
fin.	2	261	-35.77	136.99	SLV 11	3.83	Si
ini.	2	-458	-125.55	136.99	SLV 16	1.09	Si
fin.	2	570	2.67	136.99	SLV 16	51.36	Si
ini.	2	-448	-121.1	136.99	SLV 14	1.13	Si
fin.	2	531	1.67	136.99	SLV 14	82.22	Si
ini.	2	-458	-125.55	136.99	SLV 15	1.09	Si
fin.	2	570	2.67	136.99	SLV 15	51.36	Si
ini.	2	-448	-121.1	136.99	SLV 13	1.13	Si
fin.	2	531	1.67	136.99	SLV 13	82.22	Si
ini.	2	411	-4.18	136.99	SLV 2	32.76	Si
fin.	2	-486	-111.49	136.99	SLV 2	1.23	Si
ini.	2	401	-8.63	136.99	SLV 3	15.87	Si
fin.	2	-446	-110.49	136.99	SLV 3	1.24	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-4.18	136			347	130	SLV 1	0.96	No
fin.	2	0	-111.49	-662			347	130	SLV 1	0.2	No
ini.	2	0	-121.1	658			347	130	SLV 14	0.2	No
fin.	2	0	1.67	-36			347	130	SLV 14	3.6	Si
ini.	2	0	-121.1	658			347	130	SLV 13	0.2	No
fin.	2	0	1.67	-36			347	130	SLV 13	3.6	Si
ini.	2	0	-125.55	666			347	130	SLV 16	0.2	No
fin.	2	0	2.67	-44			347	130	SLV 16	2.97	Si
ini.	2	0	-8.63	144			347	130	SLV 4	0.91	No
fin.	2	0	-110.49	-670			347	130	SLV 4	0.19	No
ini.	2	0	-89.83	493			347	130	SLV 12	0.26	No
fin.	2	0	-35.77	-272			347	130	SLV 12	0.48	No
ini.	2	0	-4.18	136			347	130	SLV 2	0.96	No
fin.	2	0	-111.49	-662			347	130	SLV 2	0.2	No
ini.	2	0	-125.55	666			347	130	SLV 15	0.2	No
fin.	2	0	2.67	-44			347	130	SLV 15	2.97	Si
ini.	2	0	-89.83	493			347	130	SLV 11	0.26	No
fin.	2	0	-35.77	-272			347	130	SLV 11	0.48	No
ini.	2	0	-8.63	144			347	130	SLV 3	0.91	No
fin.	2	0	-110.49	-670			347	130	SLV 3	0.19	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.091	SLV 15	Si
V_SLV	0.195	SLV 3	No
PF_SLU	0.828	SLU 81	No
V_SLU	0.13	SLU 81	No

Trave di accoppiamento 11

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
2.185	-12.974	0.57	1.07	0.5	2.185	-12.024	0.57	1.07	0.5	0.95	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _{tk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-127	-9.76	540.81	SLU 74	55.43	Si
fin.	3	-602	-283.31	540.81	SLU 74	1.91	Si
ini.	3	-127	-9.76	540.81	SLU 79	55.43	Si
fin.	3	-602	-283.31	540.81	SLU 79	1.91	Si
ini.	3	-116	-0.7	540.81	SLU 82	770.52	Si
fin.	3	-651	-306.91	540.81	SLU 82	1.76	Si
ini.	3	-127	-9.76	540.81	SLU 76	55.43	Si
fin.	3	-602	-283.31	540.81	SLU 76	1.91	Si
ini.	3	-116	-0.7	540.81	SLU 81	770.52	Si
fin.	3	-651	-306.91	540.81	SLU 81	1.76	Si
ini.	3	-116	-0.7	540.81	SLU 84	770.52	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
fin.	3	-651	-306.91	540.81	SLU 84	1.76	Si
ini.	3	-116	-0.7	540.81	SLU 83	770.52	Si
fin.	3	-651	-306.91	540.81	SLU 83	1.76	Si
ini.	3	-127	-9.76	540.81	SLU 78	55.43	Si
fin.	3	-602	-283.31	540.81	SLU 78	1.91	Si
ini.	3	-127	-9.76	540.81	SLU 75	55.43	Si
fin.	3	-602	-283.31	540.81	SLU 75	1.91	Si
ini.	3	-127	-9.76	540.81	SLU 73	55.43	Si
fin.	3	-602	-283.31	540.81	SLU 73	1.91	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-9.76	484			578	217	SLU 75	0.45	No
fin.	3	0	-283.31	-1316			578	217	SLU 75	0.17	No
ini.	3	0	-9.76	484			578	217	SLU 78	0.45	No
fin.	3	0	-283.31	-1316			578	217	SLU 78	0.17	No
ini.	3	0	-0.7	474			578	217	SLU 81	0.46	No
fin.	3	0	-306.91	-1406			578	217	SLU 81	0.15	No
ini.	3	0	-9.76	484			578	217	SLU 74	0.45	No
fin.	3	0	-283.31	-1316			578	217	SLU 74	0.17	No
ini.	3	0	-0.7	474			578	217	SLU 83	0.46	No
fin.	3	0	-306.91	-1406			578	217	SLU 83	0.15	No
ini.	3	0	-9.76	484			578	217	SLU 79	0.45	No
fin.	3	0	-283.31	-1316			578	217	SLU 79	0.17	No
ini.	3	0	-0.7	474			578	217	SLU 82	0.46	No
fin.	3	0	-306.91	-1406			578	217	SLU 82	0.15	No
ini.	3	0	-9.76	484			578	217	SLU 76	0.45	No
fin.	3	0	-283.31	-1316			578	217	SLU 76	0.17	No
ini.	3	0	-0.7	474			578	217	SLU 84	0.46	No
fin.	3	0	-306.91	-1406			578	217	SLU 84	0.15	No
ini.	3	0	-9.76	484			578	217	SLU 73	0.45	No
fin.	3	0	-283.31	-1316			578	217	SLU 73	0.17	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	65	82.74	652.21	SLV 16	7.88	Si
fin.	2	-678	-336.62	652.21	SLV 16	1.94	Si
ini.	2	-126	-25.67	652.21	SLV 13	25.41	Si
fin.	2	-464	-225.88	652.21	SLV 13	2.89	Si
ini.	2	180	145.98	652.21	SLV 8	4.47	Si
fin.	2	-698	-340.18	652.21	SLV 8	1.92	Si
ini.	2	65	82.74	652.21	SLV 15	7.88	Si
fin.	2	-678	-336.62	652.21	SLV 15	1.94	Si
ini.	2	230	175.17	652.21	SLV 12	3.72	Si
fin.	2	-804	-398.16	652.21	SLV 12	1.64	Si
ini.	2	-456	-215.4	652.21	SLV 6	3.03	Si
fin.	2	14	28.94	652.21	SLV 6	22.54	Si
ini.	2	230	175.17	652.21	SLV 11	3.72	Si
fin.	2	-804	-398.16	652.21	SLV 11	1.64	Si
ini.	2	-126	-25.67	652.21	SLV 14	25.41	Si
fin.	2	-464	-225.88	652.21	SLV 14	2.89	Si
ini.	2	-456	-215.4	652.21	SLV 5	3.03	Si
fin.	2	14	28.94	652.21	SLV 5	22.54	Si
ini.	2	180	145.98	652.21	SLV 7	4.47	Si
fin.	2	-698	-340.18	652.21	SLV 7	1.92	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	175.17	-169			867	326	SLV 11	1.93	Si
fin.	2	0	-398.16	-1563			867	326	SLV 11	0.21	No
ini.	2	0	-25.67	490			867	326	SLV 13	0.67	No
fin.	2	0	-225.88	-1068			867	326	SLV 13	0.31	No
ini.	2	0	-25.67	490			867	326	SLV 14	0.67	No
fin.	2	0	-225.88	-1068			867	326	SLV 14	0.31	No
ini.	2	0	82.74	167			867	326	SLV 16	1.95	Si
fin.	2	0	-336.62	-1411			867	326	SLV 16	0.23	No
ini.	2	0	145.98	-134			867	326	SLV 8	2.44	Si
fin.	2	0	-340.18	-1350			867	326	SLV 8	0.24	No
ini.	2	0	82.74	167			867	326	SLV 15	1.95	Si
fin.	2	0	-336.62	-1411			867	326	SLV 15	0.23	No
ini.	2	0	-215.4	942			867	326	SLV 6	0.35	No
fin.	2	0	28.94	-206			867	326	SLV 6	1.58	Si
ini.	2	0	-215.4	942			867	326	SLV 5	0.35	No
fin.	2	0	28.94	-206			867	326	SLV 5	1.58	Si
ini.	2	0	145.98	-134			867	326	SLV 7	2.44	Si
fin.	2	0	-340.18	-1350			867	326	SLV 7	0.24	No
ini.	2	0	175.17	-169			867	326	SLV 12	1.93	Si
fin.	2	0	-398.16	-1563			867	326	SLV 12	0.21	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF SLV	1.638	SLV 11	Si
V SLV	0.209	SLV 11	No
PF SLU	1.762	SLU 81	Si
V SLU	0.155	SLU 81	No



Trave di accoppiamento 12

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-3.925	-13.248	3.17	4.99	1.82	-4.725	-13.248	3.17	4.99	1.82	0.8	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-1201	-1304.68	2683.72	SLU 41	2.06	Si
fin.	3	-1201	730.15	2683.72	SLU 41	3.68	Si
ini.	3	-1136	-1334.75	2683.72	SLU 82	2.01	Si
fin.	3	-1136	759.23	2683.72	SLU 82	3.53	Si
ini.	3	-1136	-1334.75	2683.72	SLU 84	2.01	Si
fin.	3	-1136	759.23	2683.72	SLU 84	3.53	Si
ini.	3	-1136	-1334.75	2683.72	SLU 81	2.01	Si
fin.	3	-1136	759.23	2683.72	SLU 81	3.53	Si
ini.	3	-1201	-1304.68	2683.72	SLU 40	2.06	Si
fin.	3	-1201	730.15	2683.72	SLU 40	3.68	Si
ini.	3	-868	-1114.81	2683.72	SLU 77	2.41	Si
fin.	3	-868	646.51	2683.72	SLU 77	4.15	Si
ini.	3	-868	-1114.81	2683.72	SLU 75	2.41	Si
fin.	3	-868	646.51	2683.72	SLU 75	4.15	Si
ini.	3	-1201	-1304.68	2683.72	SLU 39	2.06	Si
fin.	3	-1201	730.15	2683.72	SLU 39	3.68	Si
ini.	3	-1201	-1304.68	2683.72	SLU 42	2.06	Si
fin.	3	-1201	730.15	2683.72	SLU 42	3.68	Si
ini.	3	-1136	-1334.75	2683.72	SLU 83	2.01	Si
fin.	3	-1136	759.23	2683.72	SLU 83	3.53	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-1334.75	5196			2103	791	SLU 83	0.15	No
fin.	3	0	759.23	573			2103	791	SLU 83	1.38	Si
ini.	3	0	-1334.75	5196			2103	791	SLU 84	0.15	No
fin.	3	0	759.23	573			2103	791	SLU 84	1.38	Si
ini.	3	0	-1114.79	4412			2103	791	SLU 62	0.18	No
fin.	3	0	639.05	387			2103	791	SLU 62	2.05	Si
ini.	3	0	-1334.75	5196			2103	791	SLU 81	0.15	No
fin.	3	0	759.23	573			2103	791	SLU 81	1.38	Si
ini.	3	0	-1334.75	5196			2103	791	SLU 82	0.15	No
fin.	3	0	759.23	573			2103	791	SLU 82	1.38	Si
ini.	3	0	-1304.68	4992			2103	791	SLU 42	0.16	No
fin.	3	0	730.15	660			2103	791	SLU 42	1.2	Si
ini.	3	0	-1304.68	4992			2103	791	SLU 41	0.16	No
fin.	3	0	730.15	660			2103	791	SLU 41	1.2	Si
ini.	3	0	-1304.68	4992			2103	791	SLU 40	0.16	No
fin.	3	0	730.15	660			2103	791	SLU 40	1.2	Si
ini.	3	0	-1114.79	4412			2103	791	SLU 63	0.18	No
fin.	3	0	639.05	387			2103	791	SLU 63	2.05	Si
ini.	3	0	-1304.68	4992			2103	791	SLU 39	0.16	No
fin.	3	0	730.15	660			2103	791	SLU 39	1.2	Si

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-753	-1034.81	2850.81	SLV 4	2.75	Si
fin.	2	-1427	-1588.36	2850.81	SLV 4	1.79	Si
ini.	2	129	-87.32	2850.81	SLV 14	32.65	Si
fin.	2	803	2275.82	2850.81	SLV 14	1.25	Si
ini.	2	129	-87.32	2850.81	SLV 13	32.65	Si
fin.	2	803	2275.82	2850.81	SLV 13	1.25	Si
ini.	2	190	-87.86	2850.81	SLV 16	32.45	Si
fin.	2	868	2285.5	2850.81	SLV 16	1.25	Si
ini.	2	-814	-1034.27	2850.81	SLV 2	2.76	Si
fin.	2	-1492	-1598.03	2850.81	SLV 2	1.78	Si
ini.	2	-814	-1034.27	2850.81	SLV 1	2.76	Si
fin.	2	-1492	-1598.03	2850.81	SLV 1	1.78	Si
ini.	2	-69	-419.93	2850.81	SLV 11	6.79	Si
fin.	2	140	940.94	2850.81	SLV 11	3.03	Si
ini.	2	190	-87.86	2850.81	SLV 15	32.45	Si
fin.	2	868	2285.5	2850.81	SLV 15	1.25	Si
ini.	2	-69	-419.93	2850.81	SLV 12	6.79	Si
fin.	2	140	940.94	2850.81	SLV 12	3.03	Si
ini.	2	-753	-1034.81	2850.81	SLV 3	2.75	Si
fin.	2	-1427	-1588.36	2850.81	SLV 3	1.79	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-87.32	4959			3154	1187	SLV 14	0.24	No
fin.	2	0	2275.82	2709			3154	1187	SLV 14	0.44	No
ini.	2	0	-1034.27	-337			3154	1187	SLV 2	3.53	Si



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
fin.	2	0	-1598.03	-2571			3154	1187	SLV 2	0.46	No
ini.	2	0	-87.86	4992			3154	1187	SLV 16	0.24	No
fin.	2	0	2285.5	2740			3154	1187	SLV 16	0.43	No
ini.	2	0	-87.86	4992			3154	1187	SLV 15	0.24	No
fin.	2	0	2285.5	2740			3154	1187	SLV 15	0.43	No
ini.	2	0	-419.93	3177			3154	1187	SLV 11	0.37	No
fin.	2	0	940.94	928			3154	1187	SLV 11	1.28	Si
ini.	2	0	-419.93	3177			3154	1187	SLV 12	0.37	No
fin.	2	0	940.94	928			3154	1187	SLV 12	1.28	Si
ini.	2	0	-418.12	3067			3154	1187	SLV 9	0.39	No
fin.	2	0	908.69	824			3154	1187	SLV 9	1.44	Si
ini.	2	0	-87.32	4959			3154	1187	SLV 13	0.24	No
fin.	2	0	2275.82	2709			3154	1187	SLV 13	0.44	No
ini.	2	0	-1034.27	-337			3154	1187	SLV 1	3.53	Si
fin.	2	0	-1598.03	-2571			3154	1187	SLV 1	0.46	No
ini.	2	0	-418.12	3067			3154	1187	SLV 10	0.39	No
fin.	2	0	908.69	824			3154	1187	SLV 10	1.44	Si

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.247	SLV 15	Si
V_SLV	0.238	SLV 15	No
PF_SLU	2.011	SLU 81	Si
V_SLU	0.152	SLU 81	No

Trave di accoppiamento 13

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-7.545	-17.728	1.07	2.07	1	-8.545	-17.728	1.07	2.07	1	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _{tk}	f _{vk0}	f _{hmedio}	t ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-476	227.9	1248.72	SLU 40	5.48	Si
fin.	3	150	-265.96	1248.72	SLU 40	4.7	Si
ini.	3	-467	194.83	1248.72	SLU 63	6.41	Si
fin.	3	100	-227.19	1248.72	SLU 63	5.5	Si
ini.	3	-476	227.9	1248.72	SLU 39	5.48	Si
fin.	3	150	-265.96	1248.72	SLU 39	4.7	Si
ini.	3	-529	232.57	1248.72	SLU 84	5.37	Si
fin.	3	129	-270.58	1248.72	SLU 84	4.61	Si
ini.	3	-467	194.83	1248.72	SLU 62	6.41	Si
fin.	3	100	-227.19	1248.72	SLU 62	5.5	Si
ini.	3	-476	227.9	1248.72	SLU 42	5.48	Si
fin.	3	150	-265.96	1248.72	SLU 42	4.7	Si
ini.	3	-529	232.57	1248.72	SLU 83	5.37	Si
fin.	3	129	-270.58	1248.72	SLU 83	4.61	Si
ini.	3	-529	232.57	1248.72	SLU 81	5.37	Si
fin.	3	129	-270.58	1248.72	SLU 81	4.61	Si
ini.	3	-529	232.57	1248.72	SLU 82	5.37	Si
fin.	3	129	-270.58	1248.72	SLU 82	4.61	Si
ini.	3	-476	227.9	1248.72	SLU 41	5.48	Si
fin.	3	150	-265.96	1248.72	SLU 41	4.7	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	227.9	-247			1155	435	SLU 40	1.76	Si
fin.	3	0	-265.96	-1384			1155	435	SLU 40	0.31	No
ini.	3	0	227.9	-247			1155	435	SLU 39	1.76	Si
fin.	3	0	-265.96	-1384			1155	435	SLU 39	0.31	No
ini.	3	0	232.57	-181			1155	435	SLU 81	2.4	Si
fin.	3	0	-270.58	-1520			1155	435	SLU 81	0.29	No
ini.	3	0	232.57	-181			1155	435	SLU 83	2.4	Si
fin.	3	0	-270.58	-1520			1155	435	SLU 83	0.29	No
ini.	3	0	232.57	-181			1155	435	SLU 82	2.4	Si
fin.	3	0	-270.58	-1520			1155	435	SLU 82	0.29	No
ini.	3	0	232.57	-181			1155	435	SLU 84	2.4	Si
fin.	3	0	-270.58	-1520			1155	435	SLU 84	0.29	No
ini.	3	0	227.9	-247			1155	435	SLU 42	1.76	Si
fin.	3	0	-265.96	-1384			1155	435	SLU 42	0.31	No
ini.	3	0	227.9	-247			1155	435	SLU 41	1.76	Si
fin.	3	0	-265.96	-1384			1155	435	SLU 41	0.31	No
ini.	3	0	193.13	-77			1155	435	SLU 77	5.67	Si
fin.	3	0	-223.31	-1361			1155	435	SLU 77	0.32	No
ini.	3	0	193.13	-77			1155	435	SLU 75	5.67	Si
fin.	3	0	-223.31	-1361			1155	435	SLU 75	0.32	No



Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-545	865.57	1415.81	SLV 3	1.64	Si
fin.	2	572	-638.93	1415.81	SLV 3	2.22	Si
ini.	2	-52	-674.02	1415.81	SLV 13	2.1	Si
fin.	2	-567	421.11	1415.81	SLV 13	3.36	Si
ini.	2	-181	-655.11	1415.81	SLV 15	2.16	Si
fin.	2	-697	427.82	1415.81	SLV 15	3.31	Si
ini.	2	-416	846.67	1415.81	SLV 1	1.67	Si
fin.	2	702	-645.63	1415.81	SLV 1	2.19	Si
ini.	2	-568	355.39	1415.81	SLV 7	3.98	Si
fin.	2	-23	-257.75	1415.81	SLV 7	5.49	Si
ini.	2	-568	355.39	1415.81	SLV 8	3.98	Si
fin.	2	-23	-257.75	1415.81	SLV 8	5.49	Si
ini.	2	-416	846.67	1415.81	SLV 2	1.67	Si
fin.	2	702	-645.63	1415.81	SLV 2	2.19	Si
ini.	2	-181	-655.11	1415.81	SLV 16	2.16	Si
fin.	2	-697	427.82	1415.81	SLV 16	3.31	Si
ini.	2	-545	865.57	1415.81	SLV 4	1.64	Si
fin.	2	572	-638.93	1415.81	SLV 4	2.22	Si
ini.	2	-52	-674.02	1415.81	SLV 14	2.1	Si
fin.	2	-567	421.11	1415.81	SLV 14	3.36	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	865.57	-1788			1733	652	SLV 4	0.36	No
fin.	2	0	-638.93	-2555			1733	652	SLV 4	0.26	No
ini.	2	0	355.39	-597			1733	652	SLV 8	1.09	Si
fin.	2	0	-257.75	-1474			1733	652	SLV 8	0.44	No
ini.	2	0	355.39	-597			1733	652	SLV 7	1.09	Si
fin.	2	0	-257.75	-1474			1733	652	SLV 7	0.44	No
ini.	2	0	846.67	-1716			1733	652	SLV 2	0.38	No
fin.	2	0	-645.63	-2471			1733	652	SLV 2	0.26	No
ini.	2	0	-674.02	1930			1733	652	SLV 14	0.34	No
fin.	2	0	421.11	901			1733	652	SLV 14	0.72	No
ini.	2	0	-655.11	1857			1733	652	SLV 16	0.35	No
fin.	2	0	427.82	816			1733	652	SLV 16	0.8	No
ini.	2	0	865.57	-1788			1733	652	SLV 3	0.36	No
fin.	2	0	-638.93	-2555			1733	652	SLV 3	0.26	No
ini.	2	0	-674.02	1930			1733	652	SLV 13	0.34	No
fin.	2	0	421.11	901			1733	652	SLV 13	0.72	No
ini.	2	0	846.67	-1716			1733	652	SLV 1	0.38	No
fin.	2	0	-645.63	-2471			1733	652	SLV 1	0.26	No
ini.	2	0	-655.11	1857			1733	652	SLV 15	0.35	No
fin.	2	0	427.82	816			1733	652	SLV 15	0.8	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF SLV	1.636	SLV 3	Si
V SLV	0.255	SLV 3	No
PF SLU	4.615	SLU 81	Si
V SLU	0.286	SLU 81	No

Trave di accoppiamento 14

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-7.545	-17.728	3.97	4.99	1.02	-8.545	-17.728	3.97	4.99	1.02	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	f _{tk}	f _{vk0}	f _{hmedio}	τ ₀	f _{vd}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-704	166.83	1283.72	SLU 18	7.69	Si
fin.	3	-704	5.84	1283.72	SLU 18	219.74	Si
ini.	3	-839	202.91	1283.72	SLU 39	6.33	Si
fin.	3	-839	-2.71	1283.72	SLU 39	474.14	Si
ini.	3	-870	201.5	1283.72	SLU 84	6.37	Si
fin.	3	-870	7.15	1283.72	SLU 84	179.45	Si
ini.	3	-839	202.91	1283.72	SLU 42	6.33	Si
fin.	3	-839	-2.71	1283.72	SLU 42	474.14	Si
ini.	3	-870	201.5	1283.72	SLU 82	6.37	Si
fin.	3	-870	7.15	1283.72	SLU 82	179.45	Si
ini.	3	-839	202.91	1283.72	SLU 41	6.33	Si
fin.	3	-839	-2.71	1283.72	SLU 41	474.14	Si
ini.	3	-870	201.5	1283.72	SLU 81	6.37	Si
fin.	3	-870	7.15	1283.72	SLU 81	179.45	Si
ini.	3	-870	201.5	1283.72	SLU 83	6.37	Si
fin.	3	-870	7.15	1283.72	SLU 83	179.45	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-839	202.91	1283.72	SLU 40	6.33	Si
fin.	3	-839	-2.71	1283.72	SLU 40	474.14	Si
ini.	3	-704	166.83	1283.72	SLU 19	7.69	Si
fin.	3	-704	5.84	1283.72	SLU 19	219.74	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	202.91	941			1178	443	SLU 39	0.47	No
fin.	3	0	-2.71	-1556			1178	443	SLU 39	0.28	No
ini.	3	0	201.5	1052			1178	443	SLU 81	0.42	No
fin.	3	0	7.15	-1663			1178	443	SLU 81	0.27	No
ini.	3	0	202.91	941			1178	443	SLU 40	0.47	No
fin.	3	0	-2.71	-1556			1178	443	SLU 40	0.28	No
ini.	3	0	165.42	954			1178	443	SLU 63	0.47	No
fin.	3	0	15.7	-1449			1178	443	SLU 63	0.31	No
ini.	3	0	201.5	1052			1178	443	SLU 82	0.42	No
fin.	3	0	7.15	-1663			1178	443	SLU 82	0.27	No
ini.	3	0	201.5	1052			1178	443	SLU 83	0.42	No
fin.	3	0	7.15	-1663			1178	443	SLU 83	0.27	No
ini.	3	0	202.91	941			1178	443	SLU 42	0.47	No
fin.	3	0	-2.71	-1556			1178	443	SLU 42	0.28	No
ini.	3	0	202.91	941			1178	443	SLU 41	0.47	No
fin.	3	0	-2.71	-1556			1178	443	SLU 41	0.28	No
ini.	3	0	201.5	1052			1178	443	SLU 84	0.42	No
fin.	3	0	7.15	-1663			1178	443	SLU 84	0.27	No
ini.	3	0	165.42	954			1178	443	SLU 62	0.47	No
fin.	3	0	15.7	-1449			1178	443	SLU 62	0.31	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-861	-80.8	1450.81	SLV 15	17.96	Si
fin.	2	-299	763.85	1450.81	SLV 15	1.9	Si
ini.	2	91	226.61	1450.81	SLV 2	6.4	Si
fin.	2	-471	-729.44	1450.81	SLV 2	1.99	Si
ini.	2	-686	-131.72	1450.81	SLV 13	11.01	Si
fin.	2	-70	779.07	1450.81	SLV 13	1.86	Si
ini.	2	91	226.61	1450.81	SLV 1	6.4	Si
fin.	2	-471	-729.44	1450.81	SLV 1	1.99	Si
ini.	2	-686	-131.72	1450.81	SLV 14	11.01	Si
fin.	2	-70	779.07	1450.81	SLV 14	1.86	Si
ini.	2	-210	-65.72	1450.81	SLV 10	22.08	Si
fin.	2	56	268.84	1450.81	SLV 10	5.4	Si
ini.	2	-84	277.53	1450.81	SLV 4	5.23	Si
fin.	2	-699	-744.66	1450.81	SLV 4	1.95	Si
ini.	2	-861	-80.8	1450.81	SLV 16	17.96	Si
fin.	2	-299	763.85	1450.81	SLV 16	1.9	Si
ini.	2	-84	277.53	1450.81	SLV 3	5.23	Si
fin.	2	-699	-744.66	1450.81	SLV 3	1.95	Si
ini.	2	-210	-65.72	1450.81	SLV 9	22.08	Si
fin.	2	56	268.84	1450.81	SLV 9	5.4	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-80.8	1663			1768	665	SLV 15	0.4	No
fin.	2	0	763.85	261			1768	665	SLV 15	2.54	Si
ini.	2	0	-131.72	1751			1768	665	SLV 13	0.38	No
fin.	2	0	779.07	367			1768	665	SLV 13	1.81	Si
ini.	2	0	-80.8	1663			1768	665	SLV 16	0.4	No
fin.	2	0	763.85	261			1768	665	SLV 16	2.54	Si
ini.	2	0	211.52	98			1768	665	SLV 8	6.76	Si
fin.	2	0	-234.43	-1323			1768	665	SLV 8	0.5	No
ini.	2	0	226.61	-495			1768	665	SLV 1	1.34	Si
fin.	2	0	-729.44	-1880			1768	665	SLV 1	0.35	No
ini.	2	0	277.53	-584			1768	665	SLV 4	1.14	Si
fin.	2	0	-744.66	-1986			1768	665	SLV 4	0.33	No
ini.	2	0	211.52	98			1768	665	SLV 7	6.76	Si
fin.	2	0	-234.43	-1323			1768	665	SLV 7	0.5	No
ini.	2	0	226.61	-495			1768	665	SLV 2	1.34	Si
fin.	2	0	-729.44	-1880			1768	665	SLV 2	0.35	No
ini.	2	0	-131.72	1751			1768	665	SLV 14	0.38	No
fin.	2	0	779.07	367			1768	665	SLV 14	1.81	Si
ini.	2	0	277.53	-584			1768	665	SLV 3	1.14	Si
fin.	2	0	-744.66	-1986			1768	665	SLV 3	0.33	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.862	SLV 13	Si
V_SLV	0.335	SLV 3	No
PF_SLU	6.327	SLU 39	Si
V_SLU	0.267	SLU 81	No

Trave di accoppiamento 15

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)



Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-5.158	-17.728	4.07	4.99	0.92	-6.558	-17.728	4.07	4.99	0.92	1.4	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-1036	-341.36	1108.72	SLU 39	3.25	Si
fin.	3	-1036	47.18	1108.72	SLU 39	23.5	Si
ini.	3	-1064	-365.45	1108.72	SLU 84	3.03	Si
fin.	3	-1064	50.72	1108.72	SLU 84	21.86	Si
ini.	3	-895	-318.49	1108.72	SLU 63	3.48	Si
fin.	3	-895	42.48	1108.72	SLU 63	26.1	Si
ini.	3	-1064	-365.45	1108.72	SLU 83	3.03	Si
fin.	3	-1064	50.72	1108.72	SLU 83	21.86	Si
ini.	3	-1036	-341.36	1108.72	SLU 40	3.25	Si
fin.	3	-1036	47.18	1108.72	SLU 40	23.5	Si
ini.	3	-895	-318.49	1108.72	SLU 62	3.48	Si
fin.	3	-895	42.48	1108.72	SLU 62	26.1	Si
ini.	3	-1036	-341.36	1108.72	SLU 41	3.25	Si
fin.	3	-1036	47.18	1108.72	SLU 41	23.5	Si
ini.	3	-1064	-365.45	1108.72	SLU 82	3.03	Si
fin.	3	-1064	50.72	1108.72	SLU 82	21.86	Si
ini.	3	-1064	-365.45	1108.72	SLU 81	3.03	Si
fin.	3	-1064	50.72	1108.72	SLU 81	21.86	Si
ini.	3	-1036	-341.36	1108.72	SLU 42	3.25	Si
fin.	3	-1036	47.18	1108.72	SLU 42	23.5	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-318.49	2479			709	267	SLU 63	0.11	No
fin.	3	0	42.48	-1704			709	267	SLU 63	0.16	No
ini.	3	0	-341.36	2706			709	267	SLU 41	0.1	No
fin.	3	0	47.18	-1808			709	267	SLU 41	0.15	No
ini.	3	0	-365.45	2865			709	267	SLU 84	0.09	No
fin.	3	0	50.72	-1942			709	267	SLU 84	0.14	No
ini.	3	0	-365.45	2865			709	267	SLU 81	0.09	No
fin.	3	0	50.72	-1942			709	267	SLU 81	0.14	No
ini.	3	0	-365.45	2865			709	267	SLU 82	0.09	No
fin.	3	0	50.72	-1942			709	267	SLU 82	0.14	No
ini.	3	0	-365.45	2865			709	267	SLU 83	0.09	No
fin.	3	0	50.72	-1942			709	267	SLU 83	0.14	No
ini.	3	0	-341.36	2706			709	267	SLU 39	0.1	No
fin.	3	0	47.18	-1808			709	267	SLU 39	0.15	No
ini.	3	0	-341.36	2706			709	267	SLU 40	0.1	No
fin.	3	0	47.18	-1808			709	267	SLU 40	0.15	No
ini.	3	0	-341.36	2706			709	267	SLU 42	0.1	No
fin.	3	0	47.18	-1808			709	267	SLU 42	0.15	No
ini.	3	0	-318.49	2479			709	267	SLU 62	0.11	No
fin.	3	0	42.48	-1704			709	267	SLU 62	0.16	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-1479	-1155.34	1275.81	SLV 15	1.1	Si
fin.	2	-564	734.3	1275.81	SLV 15	1.74	Si
ini.	2	-1205	-505.43	1275.81	SLV 12	2.52	Si
fin.	2	-895	250.87	1275.81	SLV 12	5.09	Si
ini.	2	-1205	-505.43	1275.81	SLV 11	2.52	Si
fin.	2	-895	250.87	1275.81	SLV 11	5.09	Si
ini.	2	-1184	-1133.45	1275.81	SLV 14	1.13	Si
fin.	2	-292	726.65	1275.81	SLV 14	1.76	Si
ini.	2	-1184	-1133.45	1275.81	SLV 13	1.13	Si
fin.	2	-292	726.65	1275.81	SLV 13	1.76	Si
ini.	2	288	774.48	1275.81	SLV 4	1.65	Si
fin.	2	-604	-672.42	1275.81	SLV 4	1.9	Si
ini.	2	288	774.48	1275.81	SLV 3	1.65	Si
fin.	2	-604	-672.42	1275.81	SLV 3	1.9	Si
ini.	2	-1479	-1155.34	1275.81	SLV 16	1.1	Si
fin.	2	-564	734.3	1275.81	SLV 16	1.74	Si
ini.	2	583	796.37	1275.81	SLV 2	1.6	Si
fin.	2	-332	-680.06	1275.81	SLV 2	1.88	Si
ini.	2	583	796.37	1275.81	SLV 1	1.6	Si
fin.	2	-332	-680.06	1275.81	SLV 1	1.88	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	774.48	5			1063	400	SLV 4	73.88	Si
fin.	2	0	-672.42	-2314			1063	400	SLV 4	0.17	No
ini.	2	0	-1133.45	2696			1063	400	SLV 13	0.15	No
fin.	2	0	726.65	402			1063	400	SLV 13	1	No
ini.	2	0	-505.43	1828			1063	400	SLV 11	0.22	No
fin.	2	0	250.87	-455			1063	400	SLV 11	0.88	No
ini.	2	0	796.37	-35			1063	400	SLV 2	11.36	Si



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
fin.	2	0	-680.06	-2365			1063	400	SLV 2	0.17	No
ini.	2	0	-1133.45	2696			1063	400	SLV 14	0.15	No
fin.	2	0	726.65	402			1063	400	SLV 14	1	No
ini.	2	0	-1155.34	2737			1063	400	SLV 16	0.15	No
fin.	2	0	734.3	454			1063	400	SLV 16	0.88	No
ini.	2	0	774.48	5			1063	400	SLV 3	73.88	Si
fin.	2	0	-672.42	-2314			1063	400	SLV 3	0.17	No
ini.	2	0	796.37	-35			1063	400	SLV 1	11.36	Si
fin.	2	0	-680.06	-2365			1063	400	SLV 1	0.17	No
ini.	2	0	-1155.34	2737			1063	400	SLV 15	0.15	No
fin.	2	0	734.3	454			1063	400	SLV 15	0.88	No
ini.	2	0	-505.43	1828			1063	400	SLV 12	0.22	No
fin.	2	0	250.87	-455			1063	400	SLV 12	0.88	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.104	SLV 15	Si
V_SLV	0.146	SLV 15	No
PF_SLU	3.034	SLU 81	Si
V_SLU	0.093	SLU 81	No

Trave di accoppiamento 16

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-2.783	-17.728	1.07	3.07	2	-3.283	-17.728	1.07	3.07	2	0.5	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-1410	243.41	2998.72	SLU 82	12.32	Si
fin.	3	-1515	-164.11	2998.72	SLU 82	18.27	Si
ini.	3	-1410	243.41	2998.72	SLU 81	12.32	Si
fin.	3	-1515	-164.11	2998.72	SLU 81	18.27	Si
ini.	3	-1277	250.4	2998.72	SLU 42	11.98	Si
fin.	3	-1364	-138.15	2998.72	SLU 42	21.71	Si
ini.	3	-1410	243.41	2998.72	SLU 84	12.32	Si
fin.	3	-1515	-164.11	2998.72	SLU 84	18.27	Si
ini.	3	-1129	202.23	2998.72	SLU 21	14.83	Si
fin.	3	-1211	-129.15	2998.72	SLU 21	23.22	Si
ini.	3	-1277	250.4	2998.72	SLU 40	11.98	Si
fin.	3	-1364	-138.15	2998.72	SLU 40	21.71	Si
ini.	3	-1277	250.4	2998.72	SLU 39	11.98	Si
fin.	3	-1364	-138.15	2998.72	SLU 39	21.71	Si
ini.	3	-1277	250.4	2998.72	SLU 41	11.98	Si
fin.	3	-1364	-138.15	2998.72	SLU 41	21.71	Si
ini.	3	-1410	243.41	2998.72	SLU 83	12.32	Si
fin.	3	-1515	-164.11	2998.72	SLU 83	18.27	Si
ini.	3	-1129	202.23	2998.72	SLU 18	14.83	Si
fin.	3	-1211	-129.15	2998.72	SLU 18	23.22	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	250.4	-1794			2311	870	SLU 42	0.48	No
fin.	3	0	-138.15	-390			2311	870	SLU 42	2.23	Si
ini.	3	0	195.25	-1707			2311	870	SLU 63	0.51	No
fin.	3	0	-155.11	-340			2311	870	SLU 63	2.56	Si
ini.	3	0	250.4	-1794			2311	870	SLU 41	0.48	No
fin.	3	0	-138.15	-390			2311	870	SLU 41	2.23	Si
ini.	3	0	250.4	-1794			2311	870	SLU 39	0.48	No
fin.	3	0	-138.15	-390			2311	870	SLU 39	2.23	Si
ini.	3	0	243.41	-1940			2311	870	SLU 83	0.45	No
fin.	3	0	-164.11	-402			2311	870	SLU 83	2.17	Si
ini.	3	0	243.41	-1940			2311	870	SLU 82	0.45	No
fin.	3	0	-164.11	-402			2311	870	SLU 82	2.17	Si
ini.	3	0	243.41	-1940			2311	870	SLU 84	0.45	No
fin.	3	0	-164.11	-402			2311	870	SLU 84	2.17	Si
ini.	3	0	250.4	-1794			2311	870	SLU 40	0.48	No
fin.	3	0	-138.15	-390			2311	870	SLU 40	2.23	Si
ini.	3	0	195.25	-1707			2311	870	SLU 62	0.51	No
fin.	3	0	-155.11	-340			2311	870	SLU 62	2.56	Si
ini.	3	0	243.41	-1940			2311	870	SLU 81	0.45	No
fin.	3	0	-164.11	-402			2311	870	SLU 81	2.17	Si

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-1001	-884.33	3165.81	SLV 14	3.58	Si
fin.	2	-1502	414.4	3165.81	SLV 14	7.64	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-1001	-884.33	3165.81	SLV 13	3.58	Si
fin.	2	-1502	414.4	3165.81	SLV 13	7.64	Si
ini.	2	-517	1043.55	3165.81	SLV 3	3.03	Si
fin.	2	-157	-626.11	3165.81	SLV 3	5.06	Si
ini.	2	-986	-858.33	3165.81	SLV 16	3.69	Si
fin.	2	-1452	357.96	3165.81	SLV 16	8.84	Si
ini.	2	-986	-858.33	3165.81	SLV 15	3.69	Si
fin.	2	-1452	357.96	3165.81	SLV 15	8.84	Si
ini.	2	-532	1017.55	3165.81	SLV 1	3.11	Si
fin.	2	-206	-569.66	3165.81	SLV 1	5.56	Si
ini.	2	-664	408.24	3165.81	SLV 7	7.75	Si
fin.	2	-553	-347.54	3165.81	SLV 7	9.11	Si
ini.	2	-517	1043.55	3165.81	SLV 4	3.03	Si
fin.	2	-157	-626.11	3165.81	SLV 4	5.06	Si
ini.	2	-664	408.24	3165.81	SLV 8	7.75	Si
fin.	2	-553	-347.54	3165.81	SLV 8	9.11	Si
ini.	2	-532	1017.55	3165.81	SLV 2	3.11	Si
fin.	2	-206	-569.66	3165.81	SLV 2	5.56	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	408.24	-2262			3466	1304	SLV 8	0.58	No
fin.	2	0	-347.54	-1825			3466	1304	SLV 8	0.71	No
ini.	2	0	1043.55	-4284			3466	1304	SLV 4	0.3	No
fin.	2	0	-626.11	-4210			3466	1304	SLV 4	0.31	No
ini.	2	0	-858.33	2134			3466	1304	SLV 15	0.61	No
fin.	2	0	357.96	3579			3466	1304	SLV 15	0.36	No
ini.	2	0	1017.55	-4092			3466	1304	SLV 2	0.32	No
fin.	2	0	-569.66	-3918			3466	1304	SLV 2	0.33	No
ini.	2	0	408.24	-2262			3466	1304	SLV 7	0.58	No
fin.	2	0	-347.54	-1825			3466	1304	SLV 7	0.71	No
ini.	2	0	-884.33	2327			3466	1304	SLV 14	0.56	No
fin.	2	0	414.4	3871			3466	1304	SLV 14	0.34	No
ini.	2	0	-884.33	2327			3466	1304	SLV 13	0.56	No
fin.	2	0	414.4	3871			3466	1304	SLV 13	0.34	No
ini.	2	0	1043.55	-4284			3466	1304	SLV 3	0.3	No
fin.	2	0	-626.11	-4210			3466	1304	SLV 3	0.31	No
ini.	2	0	-858.33	2134			3466	1304	SLV 16	0.61	No
fin.	2	0	357.96	3579			3466	1304	SLV 16	0.36	No
ini.	2	0	1017.55	-4092			3466	1304	SLV 1	0.32	No
fin.	2	0	-569.66	-3918			3466	1304	SLV 1	0.33	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	3.034	SLV 3	Si
V_SLV	0.304	SLV 3	No
PF_SLU	11.976	SLU 39	Si
V_SLU	0.448	SLU 81	No

Trave di accoppiamento 17

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-2.783	-17.728	3.87	4.99	1.12	-3.283	-17.728	3.87	4.99	1.12	0.5	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-202	-266.85	1458.72	SLU 62	5.47	Si
fin.	3	-202	-605.89	1458.72	SLU 62	2.41	Si
ini.	3	-292	-283.01	1458.72	SLU 42	5.15	Si
fin.	3	-292	-660.23	1458.72	SLU 42	2.21	Si
ini.	3	-269	-304.75	1458.72	SLU 84	4.79	Si
fin.	3	-269	-699.38	1458.72	SLU 84	2.09	Si
ini.	3	-292	-283.01	1458.72	SLU 39	5.15	Si
fin.	3	-292	-660.23	1458.72	SLU 39	2.21	Si
ini.	3	-269	-304.75	1458.72	SLU 83	4.79	Si
fin.	3	-269	-699.38	1458.72	SLU 83	2.09	Si
ini.	3	-269	-304.75	1458.72	SLU 82	4.79	Si
fin.	3	-269	-699.38	1458.72	SLU 82	2.09	Si
ini.	3	-269	-304.75	1458.72	SLU 81	4.79	Si
fin.	3	-269	-699.38	1458.72	SLU 81	2.09	Si
ini.	3	-292	-283.01	1458.72	SLU 40	5.15	Si
fin.	3	-292	-660.23	1458.72	SLU 40	2.21	Si
ini.	3	-202	-266.85	1458.72	SLU 63	5.47	Si
fin.	3	-202	-605.89	1458.72	SLU 63	2.41	Si
ini.	3	-292	-283.01	1458.72	SLU 41	5.15	Si
fin.	3	-292	-660.23	1458.72	SLU 41	2.21	Si



Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-266.85	111			1294	487	SLU 62	4.4	Si
fin.	3	0	-605.89	-1039			1294	487	SLU 62	0.47	No
ini.	3	0	-304.75	124			1294	487	SLU 82	3.92	Si
fin.	3	0	-699.38	-1185			1294	487	SLU 82	0.41	No
ini.	3	0	-283.01	112			1294	487	SLU 40	4.35	Si
fin.	3	0	-660.23	-1104			1294	487	SLU 40	0.44	No
ini.	3	0	-304.75	124			1294	487	SLU 83	3.92	Si
fin.	3	0	-699.38	-1185			1294	487	SLU 83	0.41	No
ini.	3	0	-304.75	124			1294	487	SLU 81	3.92	Si
fin.	3	0	-699.38	-1185			1294	487	SLU 81	0.41	No
ini.	3	0	-266.85	111			1294	487	SLU 63	4.4	Si
fin.	3	0	-605.89	-1039			1294	487	SLU 63	0.47	No
ini.	3	0	-283.01	112			1294	487	SLU 39	4.35	Si
fin.	3	0	-660.23	-1104			1294	487	SLU 39	0.44	No
ini.	3	0	-304.75	124			1294	487	SLU 84	3.92	Si
fin.	3	0	-699.38	-1185			1294	487	SLU 84	0.41	No
ini.	3	0	-283.01	112			1294	487	SLU 42	4.35	Si
fin.	3	0	-660.23	-1104			1294	487	SLU 42	0.44	No
ini.	3	0	-283.01	112			1294	487	SLU 41	4.35	Si
fin.	3	0	-660.23	-1104			1294	487	SLU 41	0.44	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	299	-286.96	1625.81	SLV 6	5.67	Si
fin.	2	271	-511	1625.81	SLV 6	3.18	Si
ini.	2	-274	-534.34	1625.81	SLV 1	3.04	Si
fin.	2	-488	-973.05	1625.81	SLV 1	1.67	Si
ini.	2	-554	-521.19	1625.81	SLV 4	3.12	Si
fin.	2	-792	-980.89	1625.81	SLV 4	1.66	Si
ini.	2	-554	-521.19	1625.81	SLV 3	3.12	Si
fin.	2	-792	-980.89	1625.81	SLV 3	1.66	Si
ini.	2	-274	-534.34	1625.81	SLV 2	3.04	Si
fin.	2	-488	-973.05	1625.81	SLV 2	1.67	Si
ini.	2	431	216.28	1625.81	SLV 13	7.52	Si
fin.	2	668	321	1625.81	SLV 13	5.06	Si
ini.	2	299	-286.96	1625.81	SLV 5	5.67	Si
fin.	2	271	-511	1625.81	SLV 5	3.18	Si
ini.	2	431	216.28	1625.81	SLV 14	7.52	Si
fin.	2	668	321	1625.81	SLV 14	5.06	Si
ini.	2	-634	-243.13	1625.81	SLV 7	6.69	Si
fin.	2	-742	-537.11	1625.81	SLV 7	3.03	Si
ini.	2	-634	-243.13	1625.81	SLV 8	6.69	Si
fin.	2	-742	-537.11	1625.81	SLV 8	3.03	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	229.43	788			1941	730	SLV 16	0.93	No
fin.	2	0	313.16	148			1941	730	SLV 16	4.94	Si
ini.	2	0	216.28	854			1941	730	SLV 14	0.85	No
fin.	2	0	321	225			1941	730	SLV 14	3.24	Si
ini.	2	0	-521.19	-716			1941	730	SLV 3	1.02	Si
fin.	2	0	-980.89	-1393			1941	730	SLV 3	0.52	No
ini.	2	0	-534.34	-649			1941	730	SLV 2	1.12	Si
fin.	2	0	-973.05	-1316			1941	730	SLV 2	0.55	No
ini.	2	0	-243.13	-267			1941	730	SLV 8	2.74	Si
fin.	2	0	-537.11	-944			1941	730	SLV 8	0.77	No
ini.	2	0	216.28	854			1941	730	SLV 13	0.85	No
fin.	2	0	321	225			1941	730	SLV 13	3.24	Si
ini.	2	0	-521.19	-716			1941	730	SLV 4	1.02	Si
fin.	2	0	-980.89	-1393			1941	730	SLV 4	0.52	No
ini.	2	0	-243.13	-267			1941	730	SLV 7	2.74	Si
fin.	2	0	-537.11	-944			1941	730	SLV 7	0.77	No
ini.	2	0	229.43	788			1941	730	SLV 15	0.93	No
fin.	2	0	313.16	148			1941	730	SLV 15	4.94	Si
ini.	2	0	-534.34	-649			1941	730	SLV 1	1.12	Si
fin.	2	0	-973.05	-1316			1941	730	SLV 1	0.55	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.657	SLV 3	Si
V_SLV	0.524	SLV 3	No
PF_SLU	2.086	SLU 81	Si
V_SLU	0.411	SLU 81	No

Trave di accoppiamento 18

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-0.753	-17.728	4.07	4.99	0.92	-2.153	-17.728	4.07	4.99	0.92	1.4	0.3	3500



Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	f _{hk}	f _{vk0}	f _{medio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-1022	52.49	1108.72	SLU 81	21.12	Si
fin.	3	-912	-281.47	1108.72	SLU 81	3.94	Si
ini.	3	-1001	48.35	1108.72	SLU 40	22.93	Si
fin.	3	-896	-260.5	1108.72	SLU 40	4.26	Si
ini.	3	-857	44.33	1108.72	SLU 62	25.01	Si
fin.	3	-762	-246.85	1108.72	SLU 62	4.49	Si
ini.	3	-1001	48.35	1108.72	SLU 42	22.93	Si
fin.	3	-896	-260.5	1108.72	SLU 42	4.26	Si
ini.	3	-1001	48.35	1108.72	SLU 41	22.93	Si
fin.	3	-896	-260.5	1108.72	SLU 41	4.26	Si
ini.	3	-1022	52.49	1108.72	SLU 82	21.12	Si
fin.	3	-912	-281.47	1108.72	SLU 82	3.94	Si
ini.	3	-1022	52.49	1108.72	SLU 83	21.12	Si
fin.	3	-912	-281.47	1108.72	SLU 83	3.94	Si
ini.	3	-857	44.33	1108.72	SLU 63	25.01	Si
fin.	3	-762	-246.85	1108.72	SLU 63	4.49	Si
ini.	3	-1022	52.49	1108.72	SLU 84	21.12	Si
fin.	3	-912	-281.47	1108.72	SLU 84	3.94	Si
ini.	3	-1001	48.35	1108.72	SLU 39	22.93	Si
fin.	3	-896	-260.5	1108.72	SLU 39	4.26	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	48.35	1899			709	267	SLU 41	0.14	No
fin.	3	0	-260.5	-2317			709	267	SLU 41	0.12	No
ini.	3	0	52.49	2036			709	267	SLU 84	0.13	No
fin.	3	0	-281.47	-2452			709	267	SLU 84	0.11	No
ini.	3	0	44.33	1785			709	267	SLU 62	0.15	No
fin.	3	0	-246.85	-2121			709	267	SLU 62	0.13	No
ini.	3	0	52.49	2036			709	267	SLU 83	0.13	No
fin.	3	0	-281.47	-2452			709	267	SLU 83	0.11	No
ini.	3	0	48.35	1899			709	267	SLU 40	0.14	No
fin.	3	0	-260.5	-2317			709	267	SLU 40	0.12	No
ini.	3	0	48.35	1899			709	267	SLU 42	0.14	No
fin.	3	0	-260.5	-2317			709	267	SLU 42	0.12	No
ini.	3	0	52.49	2036			709	267	SLU 81	0.13	No
fin.	3	0	-281.47	-2452			709	267	SLU 81	0.11	No
ini.	3	0	48.35	1899			709	267	SLU 39	0.14	No
fin.	3	0	-260.5	-2317			709	267	SLU 39	0.12	No
ini.	3	0	44.33	1785			709	267	SLU 63	0.15	No
fin.	3	0	-246.85	-2121			709	267	SLU 63	0.13	No
ini.	3	0	52.49	2036			709	267	SLU 82	0.13	No
fin.	3	0	-281.47	-2452			709	267	SLU 82	0.11	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-284	-665.56	1275.81	SLV 13	1.92	Si
fin.	2	584	664.2	1275.81	SLV 13	1.92	Si
ini.	2	-562	723.32	1275.81	SLV 4	1.76	Si
fin.	2	-1326	-949.52	1275.81	SLV 4	1.34	Si
ini.	2	-564	-656.52	1275.81	SLV 16	1.94	Si
fin.	2	294	645.13	1275.81	SLV 16	1.98	Si
ini.	2	-281	714.28	1275.81	SLV 2	1.79	Si
fin.	2	-1035	-930.45	1275.81	SLV 2	1.37	Si
ini.	2	-281	714.28	1275.81	SLV 1	1.79	Si
fin.	2	-1035	-930.45	1275.81	SLV 1	1.37	Si
ini.	2	-284	-665.56	1275.81	SLV 14	1.92	Si
fin.	2	584	664.2	1275.81	SLV 14	1.92	Si
ini.	2	-564	-656.52	1275.81	SLV 15	1.94	Si
fin.	2	294	645.13	1275.81	SLV 15	1.98	Si
ini.	2	-889	250.92	1275.81	SLV 8	5.08	Si
fin.	2	-1098	-413.64	1275.81	SLV 8	3.08	Si
ini.	2	-562	723.32	1275.81	SLV 3	1.76	Si
fin.	2	-1326	-949.52	1275.81	SLV 3	1.34	Si
ini.	2	-889	250.92	1275.81	SLV 7	5.08	Si
fin.	2	-1098	-413.64	1275.81	SLV 7	3.08	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	250.92	523			1063	400	SLV 8	0.76	No
fin.	2	0	-413.64	-1558			1063	400	SLV 8	0.26	No
ini.	2	0	714.28	-256			1063	400	SLV 1	1.56	Si
fin.	2	0	-930.45	-2273			1063	400	SLV 1	0.18	No
ini.	2	0	723.32	-310			1063	400	SLV 4	1.29	Si
fin.	2	0	-949.52	-2311			1063	400	SLV 4	0.17	No
ini.	2	0	-665.56	2305			1063	400	SLV 14	0.17	No
fin.	2	0	664.2	2			1063	400	SLV 14	207.08	Si
ini.	2	0	-665.56	2305			1063	400	SLV 13	0.17	No
fin.	2	0	664.2	2			1063	400	SLV 13	207.08	Si
ini.	2	0	250.92	523			1063	400	SLV 7	0.76	No



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
fin.	2	0	-413.64	-1558			1063	400	SLV 7	0.26	No
ini.	2	0	723.32	-310			1063	400	SLV 3	1.29	Si
fin.	2	0	-949.52	-2311			1063	400	SLV 3	0.17	No
ini.	2	0	-656.52	2251			1063	400	SLV 15	0.18	No
fin.	2	0	645.13	-35			1063	400	SLV 15	11.34	Si
ini.	2	0	714.28	-256			1063	400	SLV 2	1.56	Si
fin.	2	0	-930.45	-2273			1063	400	SLV 2	0.18	No
ini.	2	0	-656.52	2251			1063	400	SLV 16	0.18	No
fin.	2	0	645.13	-35			1063	400	SLV 16	11.34	Si

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.344	SLV 3	Si
V_SLV	0.173	SLV 3	No
PF_SLU	3.939	SLU 81	Si
V_SLU	0.109	SLU 81	No

Trave di accoppiamento 19

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
1.227	-17.729	1.07	2.07	1	0.227	-17.728	1.07	2.07	1	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	93	-239.96	1248.72	SLU 84	5.2	Si
fin.	3	-548	197.69	1248.72	SLU 84	6.32	Si
ini.	3	117	-237.84	1248.72	SLU 41	5.25	Si
fin.	3	-493	195.46	1248.72	SLU 41	6.39	Si
ini.	3	67	-200.01	1248.72	SLU 62	6.24	Si
fin.	3	-484	164.39	1248.72	SLU 62	7.6	Si
ini.	3	117	-237.84	1248.72	SLU 42	5.25	Si
fin.	3	-493	195.46	1248.72	SLU 42	6.39	Si
ini.	3	67	-200.01	1248.72	SLU 63	6.24	Si
fin.	3	-484	164.39	1248.72	SLU 63	7.6	Si
ini.	3	117	-237.84	1248.72	SLU 40	5.25	Si
fin.	3	-493	195.46	1248.72	SLU 40	6.39	Si
ini.	3	93	-239.96	1248.72	SLU 82	5.2	Si
fin.	3	-548	197.69	1248.72	SLU 82	6.32	Si
ini.	3	117	-237.84	1248.72	SLU 39	5.25	Si
fin.	3	-493	195.46	1248.72	SLU 39	6.39	Si
ini.	3	93	-239.96	1248.72	SLU 81	5.2	Si
fin.	3	-548	197.69	1248.72	SLU 81	6.32	Si
ini.	3	93	-239.96	1248.72	SLU 83	5.2	Si
fin.	3	-548	197.69	1248.72	SLU 83	6.32	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-237.84	1314			1155	435	SLU 39	0.33	No
fin.	3	0	195.46	188			1155	435	SLU 39	2.31	Si
ini.	3	0	-196.41	1298			1155	435	SLU 75	0.33	No
fin.	3	0	162.69	22			1155	435	SLU 75	19.87	Si
ini.	3	0	-237.84	1314			1155	435	SLU 41	0.33	No
fin.	3	0	195.46	188			1155	435	SLU 41	2.31	Si
ini.	3	0	-239.96	1446			1155	435	SLU 84	0.3	No
fin.	3	0	197.69	118			1155	435	SLU 84	3.7	Si
ini.	3	0	-237.84	1314			1155	435	SLU 42	0.33	No
fin.	3	0	195.46	188			1155	435	SLU 42	2.31	Si
ini.	3	0	-239.96	1446			1155	435	SLU 82	0.3	No
fin.	3	0	197.69	118			1155	435	SLU 82	3.7	Si
ini.	3	0	-237.84	1314			1155	435	SLU 40	0.33	No
fin.	3	0	195.46	188			1155	435	SLU 40	2.31	Si
ini.	3	0	-239.96	1446			1155	435	SLU 81	0.3	No
fin.	3	0	197.69	118			1155	435	SLU 81	3.7	Si
ini.	3	0	-196.41	1298			1155	435	SLU 77	0.33	No
fin.	3	0	162.69	22			1155	435	SLU 77	19.87	Si
ini.	3	0	-239.96	1446			1155	435	SLU 83	0.3	No
fin.	3	0	197.69	118			1155	435	SLU 83	3.7	Si

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-820	473.67	1415.81	SLV 3	2.99	Si
fin.	2	-262	-675.31	1415.81	SLV 3	2.1	Si
ini.	2	786	-660.02	1415.81	SLV 14	2.15	Si
fin.	2	-359	831.99	1415.81	SLV 14	1.7	Si
ini.	2	-21	-252.13	1415.81	SLV 12	5.62	Si
fin.	2	-568	336.32	1415.81	SLV 12	4.21	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-21	-252.13	1415.81	SLV 11	5.62	Si
fin.	2	-568	336.32	1415.81	SLV 11	4.21	Si
ini.	2	652	-653.91	1415.81	SLV 16	2.17	Si
fin.	2	-492	849.54	1415.81	SLV 16	1.67	Si
ini.	2	652	-653.91	1415.81	SLV 15	2.17	Si
fin.	2	-492	849.54	1415.81	SLV 15	1.67	Si
ini.	2	-820	473.67	1415.81	SLV 4	2.99	Si
fin.	2	-262	-675.31	1415.81	SLV 4	2.1	Si
ini.	2	-685	467.56	1415.81	SLV 1	3.03	Si
fin.	2	-128	-692.87	1415.81	SLV 1	2.04	Si
ini.	2	-685	467.56	1415.81	SLV 2	3.03	Si
fin.	2	-128	-692.87	1415.81	SLV 2	2.04	Si
ini.	2	786	-660.02	1415.81	SLV 13	2.15	Si
fin.	2	-359	831.99	1415.81	SLV 13	1.7	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-653.91	2564			1733	652	SLV 16	0.25	No
fin.	2	0	849.54	1734			1733	652	SLV 16	0.38	No
ini.	2	0	-252.13	1440			1733	652	SLV 11	0.45	No
fin.	2	0	336.32	444			1733	652	SLV 11	1.47	Si
ini.	2	0	-252.13	1440			1733	652	SLV 12	0.45	No
fin.	2	0	336.32	444			1733	652	SLV 12	1.47	Si
ini.	2	0	473.67	-902			1733	652	SLV 4	0.72	No
fin.	2	0	-675.31	-1940			1733	652	SLV 4	0.34	No
ini.	2	0	-660.02	2487			1733	652	SLV 13	0.26	No
fin.	2	0	831.99	1737			1733	652	SLV 13	0.38	No
ini.	2	0	-653.91	2564			1733	652	SLV 15	0.25	No
fin.	2	0	849.54	1734			1733	652	SLV 15	0.38	No
ini.	2	0	467.56	-978			1733	652	SLV 2	0.67	No
fin.	2	0	-692.87	-1937			1733	652	SLV 2	0.34	No
ini.	2	0	-660.02	2487			1733	652	SLV 14	0.26	No
fin.	2	0	831.99	1737			1733	652	SLV 14	0.38	No
ini.	2	0	473.67	-902			1733	652	SLV 3	0.72	No
fin.	2	0	-675.31	-1940			1733	652	SLV 3	0.34	No
ini.	2	0	467.56	-978			1733	652	SLV 1	0.67	No
fin.	2	0	-692.87	-1937			1733	652	SLV 1	0.34	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.667	SLV 15	Si
V_SLV	0.254	SLV 15	No
PF_SLU	5.204	SLU 81	Si
V_SLU	0.301	SLU 81	No

Trave di accoppiamento 20

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
1.227	-17.729	3.97	4.99	1.02	0.227	-17.728	3.97	4.99	1.02	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-706	4.94	1283.72	SLU 21	260.03	Si
fin.	3	-706	141.41	1283.72	SLU 21	9.08	Si
ini.	3	-843	-4.49	1283.72	SLU 42	286.01	Si
fin.	3	-843	173.61	1283.72	SLU 42	7.39	Si
ini.	3	-871	6.55	1283.72	SLU 82	196.12	Si
fin.	3	-871	169.94	1283.72	SLU 82	7.55	Si
ini.	3	-871	6.55	1283.72	SLU 84	196.12	Si
fin.	3	-871	169.94	1283.72	SLU 84	7.55	Si
ini.	3	-706	4.94	1283.72	SLU 20	260.03	Si
fin.	3	-706	141.41	1283.72	SLU 20	9.08	Si
ini.	3	-871	6.55	1283.72	SLU 83	196.12	Si
fin.	3	-871	169.94	1283.72	SLU 83	7.55	Si
ini.	3	-843	-4.49	1283.72	SLU 41	286.01	Si
fin.	3	-843	173.61	1283.72	SLU 41	7.39	Si
ini.	3	-843	-4.49	1283.72	SLU 39	286.01	Si
fin.	3	-843	173.61	1283.72	SLU 39	7.39	Si
ini.	3	-871	6.55	1283.72	SLU 81	196.12	Si
fin.	3	-871	169.94	1283.72	SLU 81	7.55	Si
ini.	3	-843	-4.49	1283.72	SLU 40	286.01	Si
fin.	3	-843	173.61	1283.72	SLU 40	7.39	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-4.49	1595			1178	443	SLU 42	0.28	No



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
fin.	3	0	173.61	-872			1178	443	SLU 42	0.51	No
ini.	3	0	6.55	1685			1178	443	SLU 83	0.26	No
fin.	3	0	169.94	-981			1178	443	SLU 83	0.45	No
ini.	3	0	-4.49	1595			1178	443	SLU 39	0.28	No
fin.	3	0	173.61	-872			1178	443	SLU 39	0.51	No
ini.	3	0	15.97	1456			1178	443	SLU 62	0.3	No
fin.	3	0	137.73	-894			1178	443	SLU 62	0.5	No
ini.	3	0	-4.49	1595			1178	443	SLU 40	0.28	No
fin.	3	0	173.61	-872			1178	443	SLU 40	0.51	No
ini.	3	0	6.55	1685			1178	443	SLU 82	0.26	No
fin.	3	0	169.94	-981			1178	443	SLU 82	0.45	No
ini.	3	0	-4.49	1595			1178	443	SLU 41	0.28	No
fin.	3	0	173.61	-872			1178	443	SLU 41	0.51	No
ini.	3	0	15.97	1456			1178	443	SLU 63	0.3	No
fin.	3	0	137.73	-894			1178	443	SLU 63	0.5	No
ini.	3	0	6.55	1685			1178	443	SLU 81	0.26	No
fin.	3	0	169.94	-981			1178	443	SLU 81	0.45	No
ini.	3	0	6.55	1685			1178	443	SLU 84	0.26	No
fin.	3	0	169.94	-981			1178	443	SLU 84	0.45	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	49	300.41	1450.81	SLV 6	4.83	Si
fin.	2	-185	-85.53	1450.81	SLV 6	16.96	Si
ini.	2	-632	-774.96	1450.81	SLV 16	1.87	Si
fin.	2	-98	273.42	1450.81	SLV 16	5.31	Si
ini.	2	-128	813.16	1450.81	SLV 2	1.78	Si
fin.	2	-662	-159.15	1450.81	SLV 2	9.12	Si
ini.	2	-399	-746.55	1450.81	SLV 14	1.94	Si
fin.	2	87	222.14	1450.81	SLV 14	6.53	Si
ini.	2	-361	784.75	1450.81	SLV 3	1.85	Si
fin.	2	-847	-107.87	1450.81	SLV 3	13.45	Si
ini.	2	-632	-774.96	1450.81	SLV 15	1.87	Si
fin.	2	-98	273.42	1450.81	SLV 15	5.31	Si
ini.	2	-128	813.16	1450.81	SLV 1	1.78	Si
fin.	2	-662	-159.15	1450.81	SLV 1	9.12	Si
ini.	2	-361	784.75	1450.81	SLV 4	1.85	Si
fin.	2	-847	-107.87	1450.81	SLV 4	13.45	Si
ini.	2	49	300.41	1450.81	SLV 5	4.83	Si
fin.	2	-185	-85.53	1450.81	SLV 5	16.96	Si
ini.	2	-399	-746.55	1450.81	SLV 13	1.94	Si
fin.	2	87	222.14	1450.81	SLV 13	6.53	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-746.55	1918			1768	665	SLV 13	0.35	No
fin.	2	0	222.14	574			1768	665	SLV 13	1.16	Si
ini.	2	0	-746.55	1918			1768	665	SLV 14	0.35	No
fin.	2	0	222.14	574			1768	665	SLV 14	1.16	Si
ini.	2	0	-774.96	2016			1768	665	SLV 15	0.33	No
fin.	2	0	273.42	663			1768	665	SLV 15	1	Si
ini.	2	0	-774.96	2016			1768	665	SLV 16	0.33	No
fin.	2	0	273.42	663			1768	665	SLV 16	1	Si
ini.	2	0	784.75	-337			1768	665	SLV 3	1.97	Si
fin.	2	0	-107.87	-1682			1768	665	SLV 3	0.4	No
ini.	2	0	784.75	-337			1768	665	SLV 4	1.97	Si
fin.	2	0	-107.87	-1682			1768	665	SLV 4	0.4	No
ini.	2	0	-262.21	1307			1768	665	SLV 12	0.51	No
fin.	2	0	199.79	-54			1768	665	SLV 12	12.34	Si
ini.	2	0	-262.21	1307			1768	665	SLV 11	0.51	No
fin.	2	0	199.79	-54			1768	665	SLV 11	12.34	Si
ini.	2	0	813.16	-435			1768	665	SLV 1	1.53	Si
fin.	2	0	-159.15	-1771			1768	665	SLV 1	0.38	No
ini.	2	0	813.16	-435			1768	665	SLV 2	1.53	Si
fin.	2	0	-159.15	-1771			1768	665	SLV 2	0.38	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.784	SLV 1	Si
V_SLV	0.33	SLV 15	No
PF_SLU	7.394	SLU 39	Si
V_SLU	0.263	SLU 81	No

Trave di accoppiamento 21

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-6.101	-8.718	1.07	2.07	1	-7.101	-8.718	1.07	2.07	1	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti



fb	fhk	fvk0	fhmedio	τ_0	fv0	μ	ϕ	fvk,lim	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	γM	N	M	μ	Comb.	c.s.	Verifica
ini.	3	-156	-16.33	1248.72	SLU 39	76.48	Si
fin.	3	16	-76.45	1248.72	SLU 39	16.33	Si
ini.	3	-196	-27.39	1248.72	SLU 75	45.59	Si
fin.	3	-40	-67.78	1248.72	SLU 75	18.42	Si
ini.	3	-156	-16.33	1248.72	SLU 42	76.48	Si
fin.	3	16	-76.45	1248.72	SLU 42	16.33	Si
ini.	3	-198	-24.22	1248.72	SLU 84	51.57	Si
fin.	3	-15	-79.55	1248.72	SLU 84	15.7	Si
ini.	3	-196	-27.39	1248.72	SLU 77	45.59	Si
fin.	3	-40	-67.78	1248.72	SLU 77	18.42	Si
ini.	3	-156	-16.33	1248.72	SLU 40	76.48	Si
fin.	3	16	-76.45	1248.72	SLU 40	16.33	Si
ini.	3	-156	-16.33	1248.72	SLU 41	76.48	Si
fin.	3	16	-76.45	1248.72	SLU 41	16.33	Si
ini.	3	-198	-24.22	1248.72	SLU 81	51.57	Si
fin.	3	-15	-79.55	1248.72	SLU 81	15.7	Si
ini.	3	-198	-24.22	1248.72	SLU 82	51.57	Si
fin.	3	-15	-79.55	1248.72	SLU 82	15.7	Si
ini.	3	-198	-24.22	1248.72	SLU 83	51.57	Si
fin.	3	-15	-79.55	1248.72	SLU 83	15.7	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-27.39	496			1155	435	SLU 75	0.88	No
fin.	3	0	-67.78	-807			1155	435	SLU 75	0.54	No
ini.	3	0	-27.39	496			1155	435	SLU 76	0.88	No
fin.	3	0	-67.78	-807			1155	435	SLU 76	0.54	No
ini.	3	0	-27.39	496			1155	435	SLU 73	0.88	No
fin.	3	0	-67.78	-807			1155	435	SLU 73	0.54	No
ini.	3	0	-27.39	496			1155	435	SLU 74	0.88	No
fin.	3	0	-67.78	-807			1155	435	SLU 74	0.54	No
ini.	3	0	-24.22	500			1155	435	SLU 82	0.87	No
fin.	3	0	-79.55	-864			1155	435	SLU 82	0.5	No
ini.	3	0	-27.39	496			1155	435	SLU 78	0.88	No
fin.	3	0	-67.78	-807			1155	435	SLU 78	0.54	No
ini.	3	0	-24.22	500			1155	435	SLU 83	0.87	No
fin.	3	0	-79.55	-864			1155	435	SLU 83	0.5	No
ini.	3	0	-24.22	500			1155	435	SLU 84	0.87	No
fin.	3	0	-79.55	-864			1155	435	SLU 84	0.5	No
ini.	3	0	-27.39	496			1155	435	SLU 79	0.88	No
fin.	3	0	-67.78	-807			1155	435	SLU 79	0.54	No
ini.	3	0	-24.22	500			1155	435	SLU 81	0.87	No
fin.	3	0	-79.55	-864			1155	435	SLU 81	0.5	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	γM	N	M	μ	Comb.	c.s.	Verifica
ini.	2	-383	379.69	1415.81	SLV 3	3.73	Si
fin.	2	464	-453.81	1415.81	SLV 3	3.12	Si
ini.	2	88	-428.87	1415.81	SLV 14	3.3	Si
fin.	2	-589	381.61	1415.81	SLV 14	3.71	Si
ini.	2	223	-440.82	1415.81	SLV 16	3.21	Si
fin.	2	-443	355.7	1415.81	SLV 16	3.98	Si
ini.	2	-14	78.57	1415.81	SLV 8	18.02	Si
fin.	2	317	-200.7	1415.81	SLV 8	7.05	Si
ini.	2	-517	391.64	1415.81	SLV 2	3.62	Si
fin.	2	318	-427.9	1415.81	SLV 2	3.31	Si
ini.	2	-517	391.64	1415.81	SLV 1	3.62	Si
fin.	2	318	-427.9	1415.81	SLV 1	3.31	Si
ini.	2	88	-428.87	1415.81	SLV 13	3.3	Si
fin.	2	-589	381.61	1415.81	SLV 13	3.71	Si
ini.	2	223	-440.82	1415.81	SLV 15	3.21	Si
fin.	2	-443	355.7	1415.81	SLV 15	3.98	Si
ini.	2	-14	78.57	1415.81	SLV 7	18.02	Si
fin.	2	317	-200.7	1415.81	SLV 7	7.05	Si
ini.	2	-383	379.69	1415.81	SLV 4	3.73	Si
fin.	2	464	-453.81	1415.81	SLV 4	3.12	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	379.69	-861			1733	652	SLV 4	0.76	No
fin.	2	0	-453.81	-1666			1733	652	SLV 4	0.39	No
ini.	2	0	78.57	-47			1733	652	SLV 8	13.9	Si
fin.	2	0	-200.7	-894			1733	652	SLV 8	0.73	No
ini.	2	0	-440.82	1565			1733	652	SLV 16	0.42	No
fin.	2	0	355.7	581			1733	652	SLV 16	1.12	Si
ini.	2	0	-440.82	1565			1733	652	SLV 15	0.42	No
fin.	2	0	355.7	581			1733	652	SLV 15	1.12	Si
ini.	2	0	379.69	-861			1733	652	SLV 3	0.76	No
fin.	2	0	-453.81	-1666			1733	652	SLV 3	0.39	No
ini.	2	0	78.57	-47			1733	652	SLV 7	13.9	Si
fin.	2	0	-200.7	-894			1733	652	SLV 7	0.73	No
ini.	2	0	-428.87	1595			1733	652	SLV 14	0.41	No
fin.	2	0	381.61	593			1733	652	SLV 14	1.1	Si



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	391.64	-831			1733	652	SLV 2	0.79	No
fin.	2	0	-427.9	-1653			1733	652	SLV 2	0.39	No
ini.	2	0	-428.87	1595			1733	652	SLV 13	0.41	No
fin.	2	0	381.61	593			1733	652	SLV 13	1.1	Si
ini.	2	0	391.64	-831			1733	652	SLV 1	0.79	No
fin.	2	0	-427.9	-1653			1733	652	SLV 1	0.39	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	3.12	SLV 3	Si
V_SLV	0.392	SLV 3	No
PF_SLU	15.698	SLU 81	Si
V_SLU	0.503	SLU 81	No

Trave di accoppiamento 22

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-6.101	-8.718	3.97	4.99	1.02	-7.101	-8.718	3.97	4.99	1.02	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb _m	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-1321	-18.83	1283.72	SLU 82	68.17	Si
fin.	3	-1321	149.48	1283.72	SLU 82	8.59	Si
ini.	3	-1108	-18.04	1283.72	SLU 63	71.14	Si
fin.	3	-1108	133.85	1283.72	SLU 63	9.59	Si
ini.	3	-1284	-14.63	1283.72	SLU 40	87.75	Si
fin.	3	-1284	135.99	1283.72	SLU 40	9.44	Si
ini.	3	-1321	-18.83	1283.72	SLU 83	68.17	Si
fin.	3	-1321	149.48	1283.72	SLU 83	8.59	Si
ini.	3	-1321	-18.83	1283.72	SLU 84	68.17	Si
fin.	3	-1321	149.48	1283.72	SLU 84	8.59	Si
ini.	3	-1284	-14.63	1283.72	SLU 39	87.75	Si
fin.	3	-1284	135.99	1283.72	SLU 39	9.44	Si
ini.	3	-1284	-14.63	1283.72	SLU 41	87.75	Si
fin.	3	-1284	135.99	1283.72	SLU 41	9.44	Si
ini.	3	-1321	-18.83	1283.72	SLU 81	68.17	Si
fin.	3	-1321	149.48	1283.72	SLU 81	8.59	Si
ini.	3	-1284	-14.63	1283.72	SLU 42	87.75	Si
fin.	3	-1284	135.99	1283.72	SLU 42	9.44	Si
ini.	3	-1108	-18.04	1283.72	SLU 62	71.14	Si
fin.	3	-1108	133.85	1283.72	SLU 62	9.59	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-14.63	1506			1178	443	SLU 39	0.29	No
fin.	3	0	135.99	-1057			1178	443	SLU 39	0.42	No
ini.	3	0	-14.63	1506			1178	443	SLU 41	0.29	No
fin.	3	0	135.99	-1057			1178	443	SLU 41	0.42	No
ini.	3	0	-14.63	1506			1178	443	SLU 42	0.29	No
fin.	3	0	135.99	-1057			1178	443	SLU 42	0.42	No
ini.	3	0	-18.83	1634			1178	443	SLU 83	0.27	No
fin.	3	0	149.48	-1161			1178	443	SLU 83	0.38	No
ini.	3	0	-18.83	1634			1178	443	SLU 84	0.27	No
fin.	3	0	149.48	-1161			1178	443	SLU 84	0.38	No
ini.	3	0	-18.83	1634			1178	443	SLU 82	0.27	No
fin.	3	0	149.48	-1161			1178	443	SLU 82	0.38	No
ini.	3	0	-18.04	1444			1178	443	SLU 63	0.31	No
fin.	3	0	133.85	-1036			1178	443	SLU 63	0.43	No
ini.	3	0	-14.63	1506			1178	443	SLU 40	0.29	No
fin.	3	0	135.99	-1057			1178	443	SLU 40	0.42	No
ini.	3	0	-18.04	1444			1178	443	SLU 62	0.31	No
fin.	3	0	133.85	-1036			1178	443	SLU 62	0.43	No
ini.	3	0	-18.83	1634			1178	443	SLU 81	0.27	No
fin.	3	0	149.48	-1161			1178	443	SLU 81	0.38	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	225	389.83	1450.81	SLV 3	3.72	Si
fin.	2	-136	-316.93	1450.81	SLV 3	4.58	Si
ini.	2	-236	-89.15	1450.81	SLV 12	16.27	Si
fin.	2	-165	207.27	1450.81	SLV 12	7	Si
ini.	2	-89	363.85	1450.81	SLV 1	3.99	Si
fin.	2	-429	-322.28	1450.81	SLV 1	4.5	Si
ini.	2	-1362	-419.66	1450.81	SLV 13	3.46	Si
fin.	2	-1001	474.59	1450.81	SLV 13	3.06	Si
ini.	2	-1048	-393.68	1450.81	SLV 15	3.69	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
fin.	2	-708	479.94	1450.81	SLV 15	3.02	Si
ini.	2	-1362	-419.66	1450.81	SLV 14	3.46	Si
fin.	2	-1001	474.59	1450.81	SLV 14	3.06	Si
ini.	2	225	389.83	1450.81	SLV 4	3.72	Si
fin.	2	-136	-316.93	1450.81	SLV 4	4.58	Si
ini.	2	-89	363.85	1450.81	SLV 2	3.99	Si
fin.	2	-429	-322.28	1450.81	SLV 2	4.5	Si
ini.	2	-236	-89.15	1450.81	SLV 11	16.27	Si
fin.	2	-165	207.27	1450.81	SLV 11	7	Si
ini.	2	-1048	-393.68	1450.81	SLV 16	3.69	Si
fin.	2	-708	479.94	1450.81	SLV 16	3.02	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	363.85	-36			1768	665	SLV 2	18.26	Si
fin.	2	0	-322.28	-1462			1768	665	SLV 2	0.45	No
ini.	2	0	-419.66	1762			1768	665	SLV 14	0.38	No
fin.	2	0	474.59	310			1768	665	SLV 14	2.15	Si
ini.	2	0	-393.68	1703			1768	665	SLV 15	0.39	No
fin.	2	0	479.94	234			1768	665	SLV 15	2.84	Si
ini.	2	0	-419.66	1762			1768	665	SLV 13	0.38	No
fin.	2	0	474.59	310			1768	665	SLV 13	2.15	Si
ini.	2	0	-393.68	1703			1768	665	SLV 16	0.39	No
fin.	2	0	479.94	234			1768	665	SLV 16	2.84	Si
ini.	2	0	-175.73	1201			1768	665	SLV 10	0.55	No
fin.	2	0	189.45	-222			1768	665	SLV 10	2.99	Si
ini.	2	0	389.83	-95			1768	665	SLV 3	6.98	Si
fin.	2	0	-316.93	-1538			1768	665	SLV 3	0.43	No
ini.	2	0	-175.73	1201			1768	665	SLV 9	0.55	No
fin.	2	0	189.45	-222			1768	665	SLV 9	2.99	Si
ini.	2	0	363.85	-36			1768	665	SLV 1	18.26	Si
fin.	2	0	-322.28	-1462			1768	665	SLV 1	0.45	No
ini.	2	0	389.83	-95			1768	665	SLV 4	6.98	Si
fin.	2	0	-316.93	-1538			1768	665	SLV 4	0.43	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	3.023	SLV 15	Si
V_SLV	0.378	SLV 13	No
PF_SLU	8.588	SLU 81	Si
V_SLU	0.271	SLU 81	No

Trave di accoppiamento 23

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-0.141	-8.718	1.07	2.07	1	-1.141	-8.718	1.07	2.07	1	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{vd}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-25	-125.01	1248.72	SLU 84	9.99	Si
fin.	3	-173	16.34	1248.72	SLU 84	76.4	Si
ini.	3	-49	-109.45	1248.72	SLU 77	11.41	Si
fin.	3	-174	10.46	1248.72	SLU 77	119.42	Si
ini.	3	-25	-125.01	1248.72	SLU 83	9.99	Si
fin.	3	-173	16.34	1248.72	SLU 83	76.4	Si
ini.	3	7	-116.03	1248.72	SLU 41	10.76	Si
fin.	3	-135	18.18	1248.72	SLU 41	68.7	Si
ini.	3	7	-116.03	1248.72	SLU 39	10.76	Si
fin.	3	-135	18.18	1248.72	SLU 39	68.7	Si
ini.	3	-49	-109.45	1248.72	SLU 75	11.41	Si
fin.	3	-174	10.46	1248.72	SLU 75	119.42	Si
ini.	3	7	-116.03	1248.72	SLU 42	10.76	Si
fin.	3	-135	18.18	1248.72	SLU 42	68.7	Si
ini.	3	-25	-125.01	1248.72	SLU 81	9.99	Si
fin.	3	-173	16.34	1248.72	SLU 81	76.4	Si
ini.	3	7	-116.03	1248.72	SLU 40	10.76	Si
fin.	3	-135	18.18	1248.72	SLU 40	68.7	Si
ini.	3	-25	-125.01	1248.72	SLU 82	9.99	Si
fin.	3	-173	16.34	1248.72	SLU 82	76.4	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-125.01	826			1155	435	SLU 82	0.53	No
fin.	3	0	16.34	-538			1155	435	SLU 82	0.81	No
ini.	3	0	-109.45	765			1155	435	SLU 75	0.57	No
fin.	3	0	10.46	-539			1155	435	SLU 75	0.81	No



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-109.45	765			1155	435	SLU 80	0.57	No
fin.	3	0	10.46	-539			1155	435	SLU 80	0.81	No
ini.	3	0	-125.01	826			1155	435	SLU 81	0.53	No
fin.	3	0	16.34	-538			1155	435	SLU 81	0.81	No
ini.	3	0	-109.45	765			1155	435	SLU 76	0.57	No
fin.	3	0	10.46	-539			1155	435	SLU 76	0.81	No
ini.	3	0	-109.45	765			1155	435	SLU 79	0.57	No
fin.	3	0	10.46	-539			1155	435	SLU 79	0.81	No
ini.	3	0	-125.01	826			1155	435	SLU 83	0.53	No
fin.	3	0	16.34	-538			1155	435	SLU 83	0.81	No
ini.	3	0	-109.45	765			1155	435	SLU 78	0.57	No
fin.	3	0	10.46	-539			1155	435	SLU 78	0.81	No
ini.	3	0	-109.45	765			1155	435	SLU 77	0.57	No
fin.	3	0	10.46	-539			1155	435	SLU 77	0.81	No
ini.	3	0	-125.01	826			1155	435	SLU 84	0.53	No
fin.	3	0	16.34	-538			1155	435	SLU 84	0.81	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-583	372.56	1415.81	SLV 1	3.8	Si
fin.	2	138	-388.91	1415.81	SLV 1	3.64	Si
ini.	2	447	-498.81	1415.81	SLV 16	2.84	Si
fin.	2	-405	390.76	1415.81	SLV 16	3.62	Si
ini.	2	297	-480.78	1415.81	SLV 14	2.94	Si
fin.	2	-553	409.09	1415.81	SLV 14	3.46	Si
ini.	2	297	-480.78	1415.81	SLV 13	2.94	Si
fin.	2	-553	409.09	1415.81	SLV 13	3.46	Si
ini.	2	314	-221.18	1415.81	SLV 12	6.4	Si
fin.	2	9	90.07	1415.81	SLV 12	15.72	Si
ini.	2	314	-221.18	1415.81	SLV 11	6.4	Si
fin.	2	9	90.07	1415.81	SLV 11	15.72	Si
ini.	2	447	-498.81	1415.81	SLV 15	2.84	Si
fin.	2	-405	390.76	1415.81	SLV 15	3.62	Si
ini.	2	-433	354.53	1415.81	SLV 4	3.99	Si
fin.	2	286	-407.25	1415.81	SLV 4	3.48	Si
ini.	2	-433	354.53	1415.81	SLV 3	3.99	Si
fin.	2	286	-407.25	1415.81	SLV 3	3.48	Si
ini.	2	-583	372.56	1415.81	SLV 2	3.8	Si
fin.	2	138	-388.91	1415.81	SLV 2	3.64	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	372.56	-672			1733	652	SLV 1	0.97	No
fin.	2	0	-388.91	-1597			1733	652	SLV 1	0.41	No
ini.	2	0	354.53	-702			1733	652	SLV 3	0.93	No
fin.	2	0	-407.25	-1558			1733	652	SLV 3	0.42	No
ini.	2	0	-498.81	1668			1733	652	SLV 15	0.39	No
fin.	2	0	390.76	786			1733	652	SLV 15	0.83	No
ini.	2	0	372.56	-672			1733	652	SLV 2	0.97	No
fin.	2	0	-388.91	-1597			1733	652	SLV 2	0.41	No
ini.	2	0	-161.08	903			1733	652	SLV 9	0.72	No
fin.	2	0	151.18	-120			1733	652	SLV 9	5.46	Si
ini.	2	0	-161.08	903			1733	652	SLV 10	0.72	No
fin.	2	0	151.18	-120			1733	652	SLV 10	5.46	Si
ini.	2	0	354.53	-702			1733	652	SLV 4	0.93	No
fin.	2	0	-407.25	-1558			1733	652	SLV 4	0.42	No
ini.	2	0	-480.78	1698			1733	652	SLV 13	0.38	No
fin.	2	0	409.09	746			1733	652	SLV 13	0.87	No
ini.	2	0	-480.78	1698			1733	652	SLV 14	0.38	No
fin.	2	0	409.09	746			1733	652	SLV 14	0.87	No
ini.	2	0	-498.81	1668			1733	652	SLV 16	0.39	No
fin.	2	0	390.76	786			1733	652	SLV 16	0.83	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	2.838	SLV 15	Si
V_SLV	0.384	SLV 13	No
PF_SLU	9.989	SLU 81	Si
V_SLU	0.526	SLU 81	No

Trave di accoppiamento 24

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-0.141	-8.718	3.97	4.99	1.02	-1.141	-8.718	3.97	4.99	1.02	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb ₀	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2



Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	γM	N	M	μ_u	Comb.	c.s.	Verifica
ini.	3	-1068	123.38	1283.72	SLU 63	10.4	Si
fin.	3	-1068	-14.56	1283.72	SLU 63	88.17	Si
ini.	3	-1279	139.06	1283.72	SLU 83	9.23	Si
fin.	3	-1279	-16	1283.72	SLU 83	80.25	Si
ini.	3	-1249	127.89	1283.72	SLU 39	10.04	Si
fin.	3	-1249	-13.23	1283.72	SLU 39	97.01	Si
ini.	3	-1249	127.89	1283.72	SLU 42	10.04	Si
fin.	3	-1249	-13.23	1283.72	SLU 42	97.01	Si
ini.	3	-1279	139.06	1283.72	SLU 81	9.23	Si
fin.	3	-1279	-16	1283.72	SLU 81	80.25	Si
ini.	3	-1279	139.06	1283.72	SLU 84	9.23	Si
fin.	3	-1279	-16	1283.72	SLU 84	80.25	Si
ini.	3	-1249	127.89	1283.72	SLU 41	10.04	Si
fin.	3	-1249	-13.23	1283.72	SLU 41	97.01	Si
ini.	3	-1249	127.89	1283.72	SLU 40	10.04	Si
fin.	3	-1249	-13.23	1283.72	SLU 40	97.01	Si
ini.	3	-1068	123.38	1283.72	SLU 62	10.4	Si
fin.	3	-1068	-14.56	1283.72	SLU 62	88.17	Si
ini.	3	-1279	139.06	1283.72	SLU 82	9.23	Si
fin.	3	-1279	-16	1283.72	SLU 82	80.25	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	127.89	1846			1178	443	SLU 41	0.24	No
fin.	3	0	-13.23	-1531			1178	443	SLU 41	0.29	No
ini.	3	0	123.38	1673			1178	443	SLU 63	0.27	No
fin.	3	0	-14.56	-1417			1178	443	SLU 63	0.31	No
ini.	3	0	123.38	1673			1178	443	SLU 62	0.27	No
fin.	3	0	-14.56	-1417			1178	443	SLU 62	0.31	No
ini.	3	0	139.06	1942			1178	443	SLU 83	0.23	No
fin.	3	0	-16	-1630			1178	443	SLU 83	0.27	No
ini.	3	0	139.06	1942			1178	443	SLU 81	0.23	No
fin.	3	0	-16	-1630			1178	443	SLU 81	0.27	No
ini.	3	0	127.89	1846			1178	443	SLU 42	0.24	No
fin.	3	0	-13.23	-1531			1178	443	SLU 42	0.29	No
ini.	3	0	139.06	1942			1178	443	SLU 82	0.23	No
fin.	3	0	-16	-1630			1178	443	SLU 82	0.27	No
ini.	3	0	139.06	1942			1178	443	SLU 84	0.23	No
fin.	3	0	-16	-1630			1178	443	SLU 84	0.27	No
ini.	3	0	127.89	1846			1178	443	SLU 39	0.24	No
fin.	3	0	-13.23	-1531			1178	443	SLU 39	0.29	No
ini.	3	0	127.89	1846			1178	443	SLU 40	0.24	No
fin.	3	0	-13.23	-1531			1178	443	SLU 40	0.29	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	γM	N	M	μ_u	Comb.	c.s.	Verifica
ini.	2	-535	429.27	1450.81	SLV 4	3.38	Si
fin.	2	-997	-357.76	1450.81	SLV 4	4.06	Si
ini.	2	-254	-276.22	1450.81	SLV 15	5.25	Si
fin.	2	232	357.1	1450.81	SLV 15	4.06	Si
ini.	2	-824	418.33	1450.81	SLV 2	3.47	Si
fin.	2	-1310	-380.01	1450.81	SLV 2	3.82	Si
ini.	2	-543	-287.16	1450.81	SLV 14	5.05	Si
fin.	2	-81	334.85	1450.81	SLV 14	4.33	Si
ini.	2	-824	418.33	1450.81	SLV 1	3.47	Si
fin.	2	-1310	-380.01	1450.81	SLV 1	3.82	Si
ini.	2	-254	-276.22	1450.81	SLV 16	5.25	Si
fin.	2	232	357.1	1450.81	SLV 16	4.06	Si
ini.	2	-535	429.27	1450.81	SLV 3	3.38	Si
fin.	2	-997	-357.76	1450.81	SLV 3	4.06	Si
ini.	2	-99	195.1	1450.81	SLV 7	7.44	Si
fin.	2	-202	-81.61	1450.81	SLV 7	17.78	Si
ini.	2	-543	-287.16	1450.81	SLV 13	5.05	Si
fin.	2	-81	334.85	1450.81	SLV 13	4.33	Si
ini.	2	-99	195.1	1450.81	SLV 8	7.44	Si
fin.	2	-202	-81.61	1450.81	SLV 8	17.78	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	429.27	38			1768	665	SLV 4	17.57	Si
fin.	2	0	-357.76	-1644			1768	665	SLV 4	0.4	No
ini.	2	0	-276.22	1810			1768	665	SLV 16	0.37	No
fin.	2	0	357.1	131			1768	665	SLV 16	5.09	Si
ini.	2	0	-276.22	1810			1768	665	SLV 15	0.37	No
fin.	2	0	357.1	131			1768	665	SLV 15	5.09	Si
ini.	2	0	-16.55	1262			1768	665	SLV 11	0.53	No
fin.	2	0	132.85	-431			1768	665	SLV 11	1.55	Si
ini.	2	0	-287.16	1749			1768	665	SLV 13	0.38	No
fin.	2	0	334.85	79			1768	665	SLV 13	8.38	Si
ini.	2	0	-287.16	1749			1768	665	SLV 14	0.38	No
fin.	2	0	334.85	79			1768	665	SLV 14	8.38	Si
ini.	2	0	-16.55	1262			1768	665	SLV 12	0.53	No
fin.	2	0	132.85	-431			1768	665	SLV 12	1.55	Si
ini.	2	0	429.27	38			1768	665	SLV 3	17.57	Si
fin.	2	0	-357.76	-1644			1768	665	SLV 3	0.4	No
ini.	2	0	418.33	-24			1768	665	SLV 2	28.12	Si



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
fin.	2	0	-380.01	-1695			1768	665	SLV 2	0.39	No
ini.	2	0	418.33	-24			1768	665	SLV 1	28.12	Si
fin.	2	0	-380.01	-1695			1768	665	SLV 1	0.39	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	3.38	SLV 3	Si
V_SLV	0.367	SLV 15	No
PF_SLU	9.231	SLU 81	Si
V_SLU	0.228	SLU 81	No

Trave di accoppiamento 25

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-2.615	-13.248	3.17	4.99	1.82	-3.415	-13.248	3.17	4.99	1.82	0.8	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-1127	620.87	2683.72	SLU 81	4.32	Si
fin.	3	-1127	-1358.26	2683.72	SLU 81	1.98	Si
ini.	3	-1194	609.01	2683.72	SLU 41	4.41	Si
fin.	3	-1194	-1325.78	2683.72	SLU 41	2.02	Si
ini.	3	-860	518.77	2683.72	SLU 77	5.17	Si
fin.	3	-860	-1136.06	2683.72	SLU 77	2.36	Si
ini.	3	-1127	620.87	2683.72	SLU 84	4.32	Si
fin.	3	-1127	-1358.26	2683.72	SLU 84	1.98	Si
ini.	3	-860	518.77	2683.72	SLU 75	5.17	Si
fin.	3	-860	-1136.06	2683.72	SLU 75	2.36	Si
ini.	3	-1127	620.87	2683.72	SLU 83	4.32	Si
fin.	3	-1127	-1358.26	2683.72	SLU 83	1.98	Si
ini.	3	-1194	609.01	2683.72	SLU 39	4.41	Si
fin.	3	-1194	-1325.78	2683.72	SLU 39	2.02	Si
ini.	3	-1127	620.87	2683.72	SLU 82	4.32	Si
fin.	3	-1127	-1358.26	2683.72	SLU 82	1.98	Si
ini.	3	-1194	609.01	2683.72	SLU 40	4.41	Si
fin.	3	-1194	-1325.78	2683.72	SLU 40	2.02	Si
ini.	3	-1194	609.01	2683.72	SLU 42	4.41	Si
fin.	3	-1194	-1325.78	2683.72	SLU 42	2.02	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	609.01	-460			2103	791	SLU 42	1.72	Si
fin.	3	0	-1325.78	-4854			2103	791	SLU 42	0.16	No
ini.	3	0	609.01	-460			2103	791	SLU 39	1.72	Si
fin.	3	0	-1325.78	-4854			2103	791	SLU 39	0.16	No
ini.	3	0	620.87	-351			2103	791	SLU 83	2.26	Si
fin.	3	0	-1358.26	-5039			2103	791	SLU 83	0.16	No
ini.	3	0	620.87	-351			2103	791	SLU 82	2.26	Si
fin.	3	0	-1358.26	-5039			2103	791	SLU 82	0.16	No
ini.	3	0	513.93	-189			2103	791	SLU 62	4.18	Si
fin.	3	0	-1135.72	-4270			2103	791	SLU 62	0.19	No
ini.	3	0	609.01	-460			2103	791	SLU 41	1.72	Si
fin.	3	0	-1325.78	-4854			2103	791	SLU 41	0.16	No
ini.	3	0	609.01	-460			2103	791	SLU 40	1.72	Si
fin.	3	0	-1325.78	-4854			2103	791	SLU 40	0.16	No
ini.	3	0	620.87	-351			2103	791	SLU 81	2.26	Si
fin.	3	0	-1358.26	-5039			2103	791	SLU 81	0.16	No
ini.	3	0	513.93	-189			2103	791	SLU 63	4.18	Si
fin.	3	0	-1135.72	-4270			2103	791	SLU 63	0.19	No
ini.	3	0	620.87	-351			2103	791	SLU 84	2.26	Si
fin.	3	0	-1358.26	-5039			2103	791	SLU 84	0.16	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	852	2201.24	2850.81	SLV 4	1.3	Si
fin.	2	165	-97.27	2850.81	SLV 4	29.31	Si
ini.	2	-1465	-1680.51	2850.81	SLV 13	1.7	Si
fin.	2	-778	-1051.31	2850.81	SLV 13	2.71	Si
ini.	2	144	849.39	2850.81	SLV 7	3.36	Si
fin.	2	-66	-433.91	2850.81	SLV 7	6.57	Si
ini.	2	852	2201.24	2850.81	SLV 3	1.3	Si
fin.	2	165	-97.27	2850.81	SLV 3	29.31	Si
ini.	2	783	2196.78	2850.81	SLV 2	1.3	Si
fin.	2	99	-95.47	2850.81	SLV 2	29.86	Si
ini.	2	-1465	-1680.51	2850.81	SLV 14	1.7	Si
fin.	2	-778	-1051.31	2850.81	SLV 14	2.71	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-1396	-1676.05	2850.81	SLV 15	1.7	Si
fin.	2	-712	-1053.11	2850.81	SLV 15	2.71	Si
ini.	2	-1396	-1676.05	2850.81	SLV 16	1.7	Si
fin.	2	-712	-1053.11	2850.81	SLV 16	2.71	Si
ini.	2	783	2196.78	2850.81	SLV 1	1.3	Si
fin.	2	99	-95.47	2850.81	SLV 1	29.86	Si
ini.	2	144	849.39	2850.81	SLV 8	3.36	Si
fin.	2	-66	-433.91	2850.81	SLV 8	6.57	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	2201.24	-2610			3154	1187	SLV 3	0.45	No
fin.	2	0	-97.27	-4892			3154	1187	SLV 3	0.24	No
ini.	2	0	-1676.05	2694			3154	1187	SLV 16	0.44	No
fin.	2	0	-1053.11	428			3154	1187	SLV 16	2.77	Si
ini.	2	0	-1676.05	2694			3154	1187	SLV 15	0.44	No
fin.	2	0	-1053.11	428			3154	1187	SLV 15	2.77	Si
ini.	2	0	2196.78	-2617			3154	1187	SLV 1	0.45	No
fin.	2	0	-95.47	-4894			3154	1187	SLV 1	0.24	No
ini.	2	0	2201.24	-2610			3154	1187	SLV 4	0.45	No
fin.	2	0	-97.27	-4892			3154	1187	SLV 4	0.24	No
ini.	2	0	849.39	-746			3154	1187	SLV 8	1.59	Si
fin.	2	0	-433.91	-3027			3154	1187	SLV 8	0.39	No
ini.	2	0	849.39	-746			3154	1187	SLV 7	1.59	Si
fin.	2	0	-433.91	-3027			3154	1187	SLV 7	0.39	No
ini.	2	0	2196.78	-2617			3154	1187	SLV 2	0.45	No
fin.	2	0	-95.47	-4894			3154	1187	SLV 2	0.24	No
ini.	2	0	834.53	-767			3154	1187	SLV 5	1.55	Si
fin.	2	0	-427.92	-3035			3154	1187	SLV 5	0.39	No
ini.	2	0	834.53	-767			3154	1187	SLV 6	1.55	Si
fin.	2	0	-427.92	-3035			3154	1187	SLV 6	0.39	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.295	SLV 3	Si
V_SLV	0.243	SLV 1	No
PF_SLU	1.976	SLU 81	Si
V_SLU	0.157	SLU 81	No