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INTERVENTO

FONDO COMPLEMENTARE AL PIANO NAZIONALE DI RIPRESA E RESILIENZA
PROGRAMMA "SICURO, VERDE E SOCIALE: RIQUALIFICAZIONE DELL'EDILIZIA RESIDENZIALE PUBBLICA"

**PROGETTO DI MANUTENZIONE STRAORDINARIA PER IL RESTAURO E RISANAMENTO
CONSERVATIVO DI DUE CASAMENTI A CORTE SITI IN
COMUNE DI BOLOGNA LOCALITA' CIRENAICA.
VIA LIBIA CIV. 29÷51 PER COMPLESSIVI 70 ALLOGGI
DI ERP CON RELATIVE PERTINENZE E PARTI COMUNI**

LOTTO **3053/PN_2**

PROGETTO ESECUTIVO

TAV.		OGGETTO TABULATI DI CALCOLO CIVICO 35 STATO DI FATTO			DATA		
TAB_05					Settembre 2022		
SCALA					N. DISEGNO		
VERSIONE	DESCRIZIONE		DATA	REDATTO	VERIFICATO		APPROVATO
00	PRIMA EMISSIONE		Settembre 2022	F. DALMONTE	N. LEONE		N. LEONE
01							
02							
03							

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TABULATI DI CALCOLO
CIVICO 35
STATO DI FATTO



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1 Risultati numerici

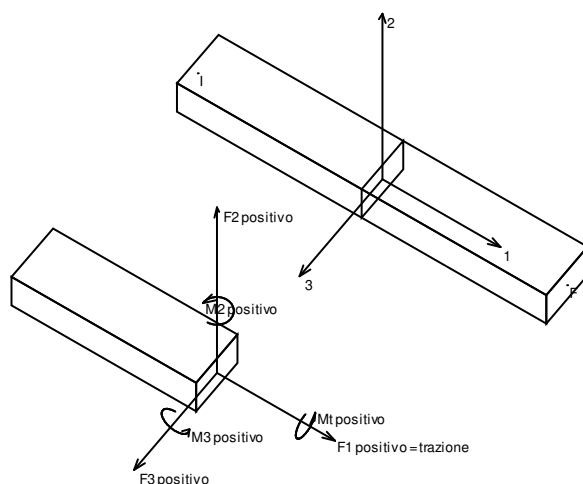
1.1 Sollecitazioni

1.1.1 Sollecitazioni aste

1.1.1.1 Convenzioni di segno aste

Le abbreviazioni relative alle sollecitazioni sugli elementi aste sono da intendersi:

- $F1$ (N): sforzo normale nell'asta;
- $F2$: sforzo di taglio agente nella direzione dell'asse locale 2;
- $F3$: sforzo di taglio agente nella direzione dell'asse locale 3;
- $M1$ (Mt): momento attorno all'asse locale 1; equivale al momento torcente;
- $M2$: momento attorno all'asse locale 2;
- $M3$: momento attorno all'asse locale 3.



La convenzione sui segni per i parametri di sollecitazione delle aste è la seguente:

presa un'asta con nodo iniziale i e nodo finale f , asse 1 che va da i a f , assi 2 e 3 presi secondo quanto indicato nei paragrafi successivi relativi al sistema locale delle aste sezionando l'asta in un punto e considerando la sezione sinistra del punto in cui si è effettuato il taglio (sezione da cui esce il versore asse 1) i parametri di sollecitazione sono positivi se hanno verso e direzione concordi con il sistema di riferimento locale dell'asta 1, 2, 3 (per i momenti si adotta la regola della mano destra).

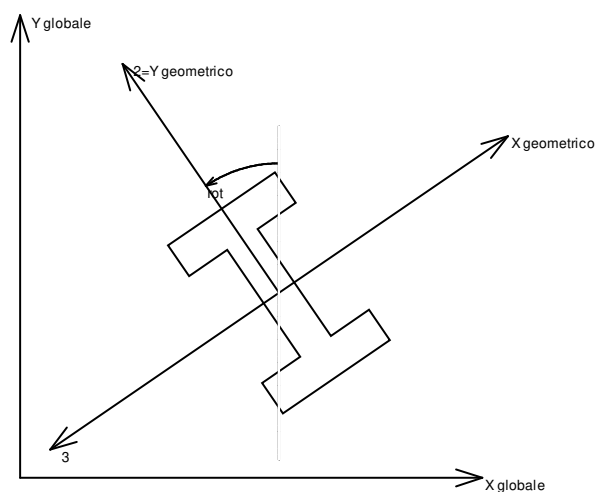
Il sistema è definito diversamente per tre categorie di aste, a seconda che siano originate da:

- aste verticali ad esempio pilastri e colonne;
- aste non verticali non di c.a., ad esempio travi di acciaio o legno;
- aste non verticali in c.a.: travi in c.a. di piano, falda o a quota generica.

Nel seguito si indica con 1, 2 e 3 il sistema locale dell'asta che non sempre coincide con gli assi principali della sezione. Si ricorda che per assi principali si intendono gli assi rispetto a cui si ha il raggio di inerzia minimo e massimo. Gli assi 1, 2 e 3 rispettano la regola della mano destra.

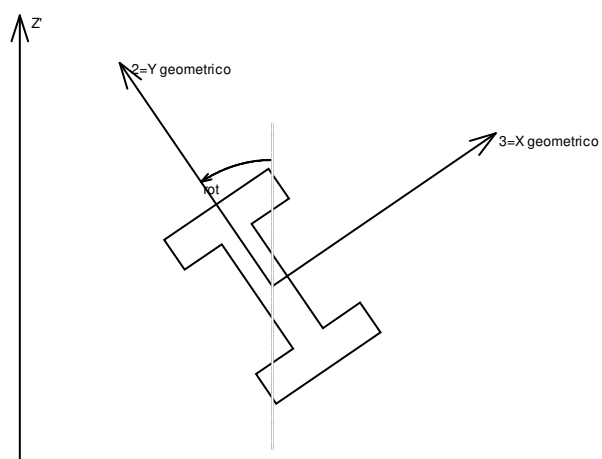


Sistema locale aste verticali



Nella figura si considera l'asse 1 uscente dal foglio (l'osservatore guarda in direzione opposta a quella dell'asse 1).

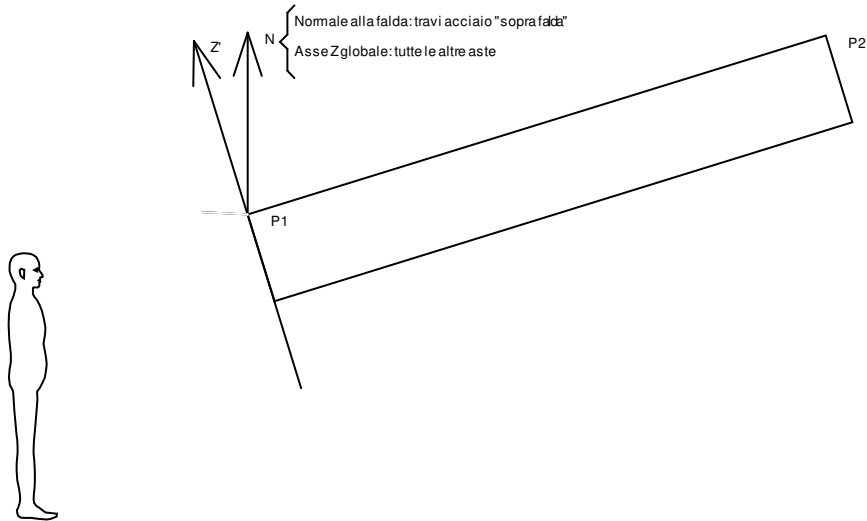
Sistema locale aste non verticali



Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1).

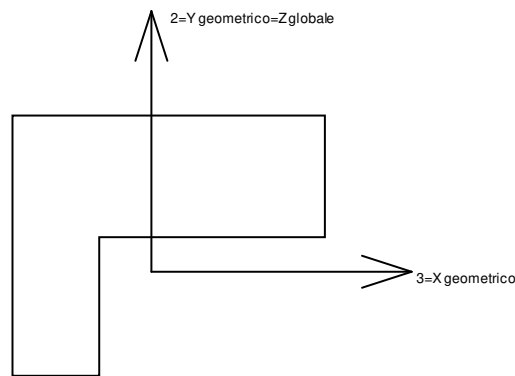
L'asse Z' è illustrato nella figura seguente dove:

- P1 è il punto di inserimento iniziale dell'asta;
- P2 è il punto di inserimento finale dell'asta;
- N è la normale al piano o falda di inserimento;



Z' è quindi l'intersezione tra il piano passante per $P1$, $P2$ contenente N e il piano della sezione iniziale dell'asta.

Sistema locale aste derivanti da travi in c.a.



Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1). L'asse 2 è sempre verticale e quindi coincidente con l'asse Z globale nonché con l'asse y geometrico. L'asse 3 coincide con l'asse x geometrico. Si sottolinea il fatto che gli assi 2 e 3 non corrispondono agli assi principali della sezione.

1.1.2 Sollecitazioni gusci

1.1.2.1 Convenzioni di segno gusci

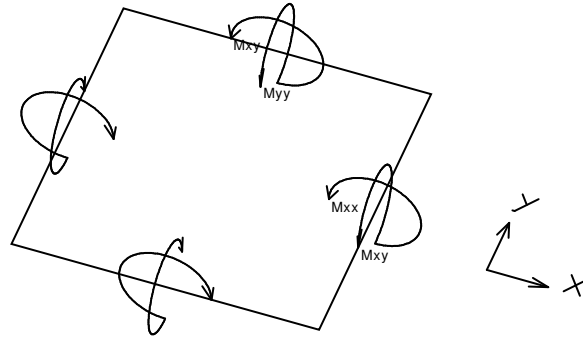
Sono individuate distinte convenzioni di segno in relazione al tipo di elemento strutturale a cui il guscio si riferisce:

- convenzione per gusci non verticali, originati ad esempio da piastre e platee;
- convenzione per gusci verticali, originati ad esempio da pareti e muri.

Convenzione di segno per gusci non verticali

Il sistema di riferimento nel quale sono espressi i parametri di sollecitazione è così definito: origine appartenente al piano dell'elemento, asse x e y contenuti nel piano dell'elemento e terzo asse (z) ortogonale al piano dell'elemento a formare una terna destrorsa. In particolare l'asse x ha proiezione in pianta parallela ed equivale all'asse globale X . Nel caso di piastre orizzontali (caso più comune) gli assi x , y e z locali all'elemento sono paralleli ed equivale agli assi X , Y e Z globali. Si sottolinea che non ha alcun interesse collocare esattamente nel piano dell'elemento la posizione dell'origine in quanto i parametri di sollecitazione sono invarianti rispetto a tale posizione.

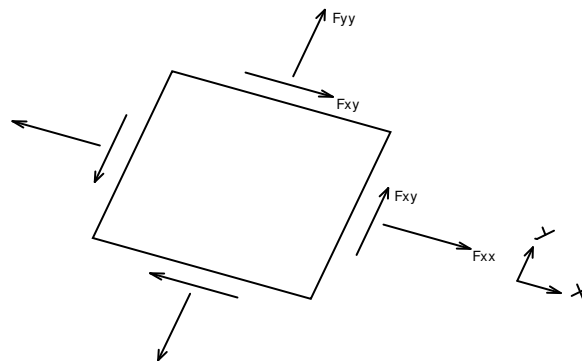
In figura è mostrato un elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione M_{xx} , M_{yy} , M_{xy} .



Si definiscono:

- M_{xx} : momento flettente [Forza*Lunghezza/Lunghezza] agente sul bordo di normale x (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- M_{yy} : momento flettente [Forza*Lunghezza/Lunghezza] agente sul bordo di normale y (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- M_{xy} : momento torcente [Forza*Lunghezza/Lunghezza] agente sui bordi (verso positivo indicato dalla freccia in figura).

Per quanto riguarda le sollecitazioni estensionali si faccia riferimento alla figura seguente dove per lo stesso elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione F_{xx} , F_{yy} , F_{xy} .



Si definiscono:

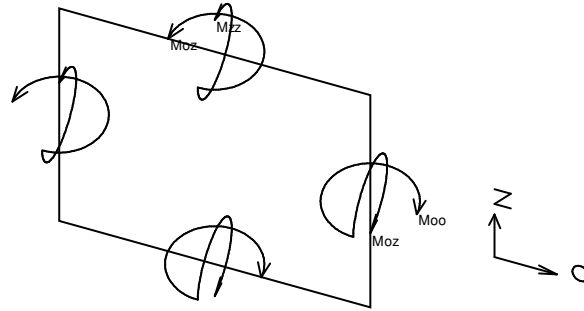
- F_{xx} : sforzo estensionale [Forza/Lunghezza] agente sul bordo di normale x (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- F_{yy} : sforzo estensionale [Forza/Lunghezza] agente sul bordo di normale all'asse y (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- F_{xy} : sforzo di taglio [Forza/Lunghezza] agente sui bordi (verso positivo indicato dalla freccia in figura).

Vengono riportati inoltre i tagli fuori dal piano dell'elemento guscio:

- V_x : taglio fuori piano [Forza/Lunghezza] applicato al bordo di normale parallela all'asse x;
- V_y : taglio fuori piano [Forza/Lunghezza] applicato al bordo di normale parallela all'asse y.

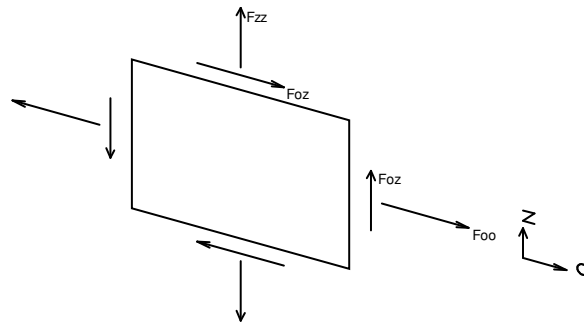
Convenzione di segno per gusci verticali

Il sistema di riferimento nel quale sono espressi i parametri di sollecitazione è così definito: origine appartenente al piano dell'elemento, asse O (ascisse) e z (ordinate) contenuti nel piano dell'elemento e terzo asse ortogonale al piano dell'elemento a formare una terna destrorsa. In particolare l'asse O è orizzontale e l'asse z parallelo ed equiverso con l'asse Z globale. Si sottolinea che non ha alcun interesse collocare esattamente nel piano dell'elemento la posizione dell'origine in quanto i parametri di sollecitazione sono invarianti rispetto a tale posizione. In figura è mostrato un elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione M_{xx} , M_{yy} , M_{xy} , F_{xx} , F_{yy} , F_{xy} .



- Moo: momento flettente distribuito $[Forza * Lunghezza / Lunghezza]$ applicato al bordo di normale parallela all'asse O (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- Mzz: momento flettente distribuito $[Forza * Lunghezza / Lunghezza]$ applicato al bordo di normale parallela all'asse z (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- Moz: momento 'torcente' distribuito $[Forza * Lunghezza / Lunghezza]$ applicato sui bordi (verso positivo indicato dalla freccia in figura).

Per quanto riguarda le sollecitazioni estensionali si faccia riferimento alla figura seguente dove per lo stesso elemento infinitesimo di shell con indicato il sistema di riferimento i parametri di sollecitazione Foo, Fzz, Foz sono rispettivamente:



- Fzz: sforzo tensionale distribuito $[Forza / Lunghezza]$ applicato al bordo di normale parallela all'asse z (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- Foo: sforzo tensionale distribuito $[Forza / Lunghezza]$ applicato al bordo di normale parallela all'asse O (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- Foz: sforzo tagliante distribuito $[Forza / Lunghezza]$ applicato sui bordi (verso positivo indicato dalla freccia in figura).

Vengono riportati inoltre i tagli fuori dal piano dell'elemento guscio:

- Vo: taglio fuori piano applicato al bordo di normale parallela all'asse O;
- Vz: taglio fuori piano applicato al bordo di normale parallela all'asse z.

1.1.2.2 Sollecitazioni estreme gusci

Shell: elemento guscio a cui si riferiscono le sollecitazioni.

Ind: indice del guscio.

Cont.: contesto a cui si riferiscono le sollecitazioni.

N.br.: nome breve della condizione o combinazione di carico.

Nodo: nodo su cui si basa il guscio a cui si riferisce la sollecitazione.

Ind: indice del nodo.

Sollecitazione: valori della sollecitazione.

M11: componente M11 della sollecitazione del guscio nel nodo indicato. $[daN * m / m]$

M12: componente M12 della sollecitazione del guscio nel nodo indicato. $[daN * m / m]$

M22: componente M22 della sollecitazione del guscio nel nodo indicato. $[daN * m / m]$

F11: componente F11 della sollecitazione del guscio nel nodo indicato. $[daN / m]$

F12: componente F12 della sollecitazione del guscio nel nodo indicato. $[daN / m]$

F22: componente F22 della sollecitazione del guscio nel nodo indicato. $[daN / m]$

V13: componente V13 della sollecitazione del guscio nel nodo indicato. $[daN / m]$

V23: componente V23 della sollecitazione del guscio nel nodo indicato. $[daN / m]$

Sollecitazioni con momento M11 minimo

Vengono mostrati i soli 5 gusci più sollecitati.



Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
504	SLV 5	1180	-2440	-738	-2917	259	-2240	411	5805	10394
350	SLV 9	1180	-1685	-382	-3060	547	1780	-393	5859	10358
344	SLV 9	180	-1679	1017	-3314	-1909	2204	-7635	-4212	21803
381	SLV 7	129	-1442	-214	-1178	-785	-87	-7862	-1007	-2845
253	SLV 11	1061	-1397	239	-3184	655	-1820	2304	-3361	14330

Sollecitazioni con momento M11 massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
504	SLV 11	1180	2473	754	2975	-761	-3254	-7798	-6000	-10622
350	SLV 7	1180	1713	386	3121	-1154	-3577	-8642	-5982	-10580
344	SLV 7	180	1679	-1017	3313	-1991	78	-7963	4211	-21800
381	SLV 9	129	1442	214	1177	-848	695	-5745	1006	2845
253	SLV 5	1061	1441	-243	3284	-1087	2082	-11741	3500	-14839

Sollecitazioni con momento M22 minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
344	SLV 7	130	-1031	-164	-4122	-2001	154	-7961	4211	-21800
247	SLV 9	14	-902	-1	-3606	-1908	-126	-7301	-1003	-16522
246	SLV 9	14	-902	-1	-3606	-1680	-552	-7194	962	-16521
253	SLV 7	1061	-1246	191	-3371	792	-1179	2732	-3626	15165
176	SLV 7	1061	-1382	-222	-3369	675	1957	2378	3814	15168

Sollecitazioni con momento M22 massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
344	SLV 9	130	1031	164	4122	-1961	1653	-7621	-4212	21803
246	SLV 7	14	902	1	3608	-1350	508	-5055	-962	16529
247	SLV 7	14	902	1	3608	-1123	163	-4950	1003	16530
253	SLV 9	1061	1290	-195	3471	-1225	1441	-12169	3765	-15674
176	SLV 9	1061	1426	226	3469	-1086	-2186	-11810	-3960	-15677

Sollecitazioni con sforzo F11 minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
1408	SLV 7	972	54	0	0	-116195	-32	-27112	-1	1
1255	SLV 7	1076	45	0	7	-115813	-30	34167	-2	-30
1401	SLV 9	246	-3	0	0	-113732	31	-36955	12	-1
1285	SLV 9	28	0	0	0	-105168	25	37694	7	4
1422	SLV 7	118	-17	0	-24	-103083	-29	58816	141	-55

Sollecitazioni con sforzo F11 massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
1255	SLV 9	1076	-45	0	-7	118687	31	-38643	2	30
1408	SLV 9	972	-54	0	0	117643	32	22677	1	-1
1401	SLV 7	246	3	0	0	113824	-31	32553	-12	1
1285	SLV 7	28	0	0	0	105229	-25	-43065	-7	-4
1422	SLV 9	118	17	0	24	103117	29	-64720	-141	54

Sollecitazioni con sforzo F22 minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
1286	SLV 7	28	0	0	0	-5	-23	-225119	0	0
1430	SLV 9	118	0	0	39	-4	27	-186700	0	-2
1256	SLV 9	1076	-38	0	-5	24458	32	-162507	74	0
1255	SLV 7	972	59	0	-4	61082	-29	-136516	-2	-30
1285	SLV 9	246	-4	0	-3	51556	25	-130943	7	4

Sollecitazioni con sforzo F22 massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
1286	SLV 9	28	0	0	0	5	23	220340	0	0
1430	SLV 7	118	0	0	-39	4	-27	180871	0	0
1256	SLV 7	1076	38	0	5	-23216	-31	157219	-74	0
1255	SLV 9	972	-59	0	4	-61462	30	134447	2	30
1285	SLV 7	246	4	0	3	-51615	-25	125677	-7	-4

1.1.2.3 Sollecitazioni estreme gusci non verticali

Shell: elemento guscio a cui si riferiscono le sollecitazioni.

Ind: indice del guscio.

Cont.: contesto a cui si riferiscono le sollecitazioni.

N.br.: nome breve della condizione o combinazione di carico.

Nodo: nodo su cui si basa il guscio a cui si riferisce la sollecitazione.

Ind: indice del nodo.



Sollecitazione: valori della sollecitazione.

Mxx: componente Mxx della sollecitazione del guscio nel nodo indicato. [daN*m/m]

Mxy: componente Mxy della sollecitazione del guscio nel nodo indicato. [daN*m/m]

Myy: componente Myy della sollecitazione del guscio nel nodo indicato. [daN*m/m]

Fxx: componente Fxx della sollecitazione del guscio nel nodo indicato. [daN/m]

Fxy: componente Fxy della sollecitazione del guscio nel nodo indicato. [daN/m]

Fyy: componente Fyy della sollecitazione del guscio nel nodo indicato. [daN/m]

Vx: componente Vo della sollecitazione del guscio nel nodo indicato. [daN/m]

Vy: componente Vz della sollecitazione del guscio nel nodo indicato. [daN/m]

Sollecitazioni con momento Mxx minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy

Sollecitazioni con momento Mxx massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy

Sollecitazioni con momento Myy minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy

Sollecitazioni con momento Myy massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy

Sollecitazioni con sforzo Fxx minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy

Sollecitazioni con sforzo Fxx massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy

Sollecitazioni con sforzo Fyy minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy

Sollecitazioni con sforzo Fyy massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy

1.1.2.4 Sollecitazioni estreme gusci verticali

Shell: elemento guscio a cui si riferiscono le sollecitazioni.

Ind: indice del guscio.

Cont.: contesto a cui si riferiscono le sollecitazioni.

N.br.: nome breve della condizione o combinazione di carico.

Nodo: nodo su cui si basa il guscio a cui si riferisce la sollecitazione.

Ind: indice del nodo.

Sollecitazione: valori della sollecitazione.

Moo: componente Moo della sollecitazione del guscio nel nodo indicato. [daN*m/m]

Moz: componente Moz della sollecitazione del guscio nel nodo indicato. [daN*m/m]

Mzz: componente Mzz della sollecitazione del guscio nel nodo indicato. [daN*m/m]

Foo: componente Foo della sollecitazione del guscio nel nodo indicato. [daN/m]

Foz: componente Foz della sollecitazione del guscio nel nodo indicato. [daN/m]

Fzz: componente Fzz della sollecitazione del guscio nel nodo indicato. [daN/m]

Vo: componente Vo della sollecitazione del guscio nel nodo indicato. [daN/m]

Vz: componente Vz della sollecitazione del guscio nel nodo indicato. [daN/m]

Sollecitazioni con momento Moo minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
504	SLV 5	1180	-2440	-738	-2917	259	-2240	411	5805	10394
350	SLV 9	1180	-1685	-382	-3060	547	1780	-393	5859	10358
344	SLV 9	180	-1679	1017	-3314	-1909	2204	-7635	-4212	21803
381	SLV 7	129	-1442	-214	-1178	-785	-87	-7862	-1007	-2845
253	SLV 5	1061	-1441	-243	-3284	-1087	-2082	-11741	3500	14839



Sollecitazioni con momento Moo massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
504	SLV 11	1180	2473	754	2975	-761	-3254	-7798	-6000	-10622
350	SLV 7	1180	1713	386	3121	-1154	-3577	-8642	-5982	-10580
344	SLV 7	180	1679	-1017	3313	-1991	78	-7963	4211	-21800
381	SLV 9	129	1442	214	1177	-848	695	-5745	1006	2845
253	SLV 11	1061	1397	239	3184	655	1820	2304	-3361	-14330

Sollecitazioni con momento Mzz minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
344	SLV 7	130	-1031	-164	-4122	-2001	154	-7961	4211	-21800
246	SLV 7	14	-902	1	-3608	-1350	-508	-5055	-962	-16529
247	SLV 7	14	-902	1	-3608	-1123	-163	-4950	1003	-16530
253	SLV 9	1061	-1290	-195	-3471	-1225	-1441	-12169	3765	15674
176	SLV 9	1061	-1426	226	-3469	-1086	2186	-11810	-3960	15677

Sollecitazioni con momento Mzz massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
344	SLV 9	130	1031	164	4122	-1961	1653	-7621	-4212	21803
246	SLV 9	14	902	-1	3606	-1680	552	-7194	962	16521
247	SLV 9	14	902	-1	3606	-1908	126	-7301	-1003	16522
253	SLV 7	1061	1246	191	3371	792	1179	2732	-3626	-15165
176	SLV 7	1061	1382	-222	3369	675	-1957	2378	3814	-15168

Sollecitazioni con sforzo Foo minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
1408	SLV 7	972	-54	0	0	-116195	32	-27112	-1	-1
1255	SLV 7	1076	-45	0	-7	-115813	30	34167	-2	30
1401	SLV 9	246	3	0	0	-113732	-31	-36955	12	1
1285	SLV 9	28	0	0	0	-105168	-25	37694	7	-4
1422	SLV 7	118	17	0	24	-103083	29	58816	141	55

Sollecitazioni con sforzo Foo massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
1255	SLV 9	1076	45	0	7	118687	-31	-38643	2	-30
1408	SLV 9	972	54	0	0	117643	-32	22677	1	1
1401	SLV 7	246	-3	0	0	113824	31	32553	-12	-1
1285	SLV 7	28	0	0	0	105229	25	-43065	-7	4
1422	SLV 9	118	-17	0	-24	103117	-29	-64720	-141	-54

Sollecitazioni con sforzo Fzz minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
1286	SLV 7	28	0	0	0	-5	23	-225119	0	0
1430	SLV 9	118	0	0	-39	-4	-27	-186700	0	2
1256	SLV 9	1076	38	0	5	24458	-32	-162507	74	0
1255	SLV 7	972	-59	0	4	61082	29	-136516	-2	30
1285	SLV 9	246	4	0	3	51556	-25	-130943	7	-4

Sollecitazioni con sforzo Fzz massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
1286	SLV 9	28	0	0	0	5	-23	220340	0	0
1430	SLV 7	118	0	0	39	4	27	180871	0	0
1256	SLV 7	1076	-38	0	-5	-23216	31	157219	-74	0
1255	SLV 9	972	59	0	-4	-61462	-30	134447	2	-30
1285	SLV 7	246	-4	0	-3	-51615	25	125677	-7	4

1.1.3 Sollecitazioni gusci armati

1.1.3.1 Convenzioni di segno gusci

Sono individuate distinte convenzioni di segno in relazione al tipo di elemento strutturale a cui il guscio si riferisce:

- convenzione per gusci non verticali, originati ad esempio da piastre e platee;
- convenzione per gusci verticali, originati ad esempio da pareti e muri.

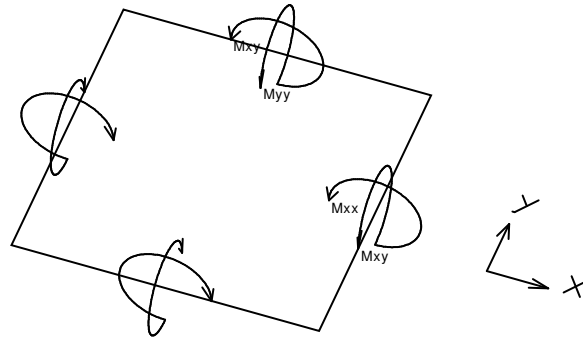
Convenzione di segno per gusci non verticali

Il sistema di riferimento nel quale sono espressi i parametri di sollecitazione è così definito: origine appartenente al piano dell'elemento, asse x e y contenuti nel piano dell'elemento e terzo asse (z) ortogonale al piano dell'elemento a formare una terna destrorsa. In particolare l'asse x ha proiezione in pianta parallela ed equivale all'asse globale X. Nel caso di piastre orizzontali (caso più comune) gli assi x, y e z locali all'elemento sono paralleli ed equivalgono agli assi X, Y e Z globali. Si sottolinea che non ha alcun interesse collocare esattamente nel piano dell'elemento la posizione dell'origine in quanto i parametri di sollecitazione sono invarianti rispetto a tale



posizione.

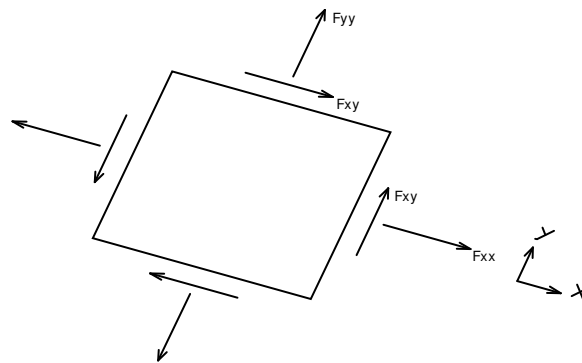
In figura è mostrato un elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione M_{xx} , M_{yy} , M_{xy} .



Si definiscono:

- M_{xx} : momento flettente [Forza*Lunghezza/Lunghezza] agente sul bordo di normale x (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- M_{yy} : momento flettente [Forza*Lunghezza/Lunghezza] agente sul bordo di normale y (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- M_{xy} : momento torcente [Forza*Lunghezza/Lunghezza] agente sui bordi (verso positivo indicato dalla freccia in figura).

Per quanto riguarda le sollecitazioni estensionali si faccia riferimento alla figura seguente dove per lo stesso elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione F_{xx} , F_{yy} , F_{xy} .



Si definiscono:

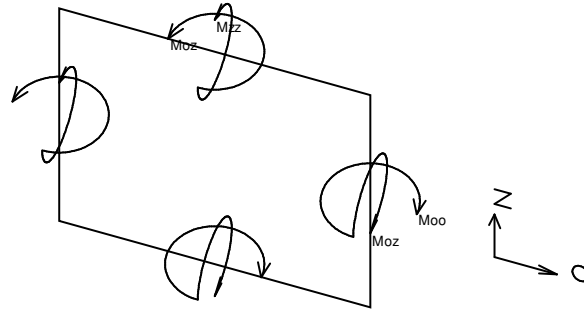
- F_{xx} : sforzo estensionale [Forza/Lunghezza] agente sul bordo di normale x (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- F_{yy} : sforzo estensionale [Forza/Lunghezza] agente sul bordo di normale all'asse y (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- F_{xy} : sforzo di taglio [Forza/Lunghezza] agente sui bordi (verso positivo indicato dalla freccia in figura).

Vengono riportati inoltre i tagli fuori dal piano dell'elemento guscio:

- V_x : taglio fuori piano [Forza/Lunghezza] applicato al bordo di normale parallela all'asse x;
- V_y : taglio fuori piano [Forza/Lunghezza] applicato al bordo di normale parallela all'asse y.

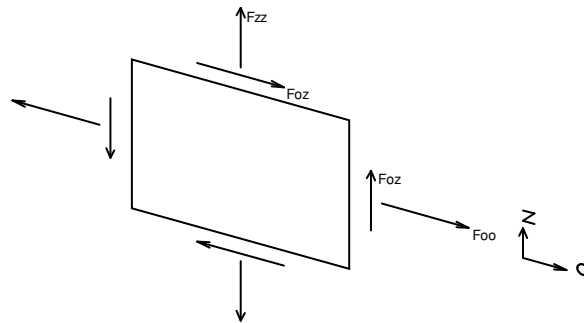
Convenzione di segno per gusci verticali

Il sistema di riferimento nel quale sono espressi i parametri di sollecitazione è così definito: origine appartenente al piano dell'elemento, asse O (ascisse) e z (ordinate) contenuti nel piano dell'elemento e terzo asse ortogonale al piano dell'elemento a formare una terna destrorsa. In particolare l'asse O è orizzontale e l'asse z parallelo ed equiverso con l'asse Z globale. Si sottolinea che non ha alcun interesse collocare esattamente nel piano dell'elemento la posizione dell'origine in quanto i parametri di sollecitazione sono invarianti rispetto a tale posizione. In figura è mostrato un elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione M_{xx} , M_{yy} , M_{xy} .



- Moo: momento flettente distribuito $[Forza \cdot Lunghezza / Lunghezza]$ applicato al bordo di normale parallela all'asse O (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- Mzz: momento flettente distribuito $[Forza \cdot Lunghezza / Lunghezza]$ applicato al bordo di normale parallela all'asse z (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- Moz: momento 'torcente' distribuito $[Forza \cdot Lunghezza / Lunghezza]$ applicato sui bordi (verso positivo indicato dalla freccia in figura).

Per quanto riguarda le sollecitazioni estensionali si faccia riferimento alla figura seguente dove per lo stesso elemento infinitesimo di shell con indicato il sistema di riferimento i parametri di sollecitazione Foo, Fzz, Foz sono rispettivamente:



- Fzz: sforzo tensionale distribuito $[Forza / Lunghezza]$ applicato al bordo di normale parallela all'asse z (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- Foo: sforzo tensionale distribuito $[Forza / Lunghezza]$ applicato al bordo di normale parallela all'asse O (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- Foz: sforzo tagliante distribuito $[Forza / Lunghezza]$ applicato sui bordi (verso positivo indicato dalla freccia in figura).

Vengono riportati inoltre i tagli fuori dal piano dell'elemento guscio:

- Vo: taglio fuori piano applicato al bordo di normale parallela all'asse O;
- Vz: taglio fuori piano applicato al bordo di normale parallela all'asse z.

1.1.4 Sollecitazioni gusci muratura

1.1.4.1 Convenzioni di segno gusci muratura

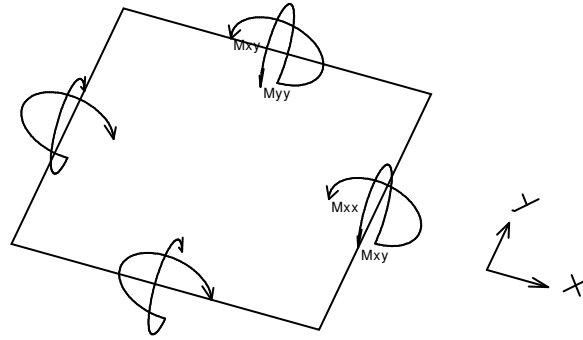
Sono individuate distinte convenzioni di segno in relazione al tipo di elemento strutturale a cui il guscio muratura si riferisce:

- convenzione per gusci non verticali, originati ad esempio da piastre e platee;
- convenzione per gusci verticali, originati ad esempio da pareti e muri.

Convenzione di segno per gusci non verticali

Il sistema di riferimento nel quale sono espressi i parametri di sollecitazione è così definito: origine appartenente al piano dell'elemento, asse x e y contenuti nel piano dell'elemento e terzo asse (z) ortogonale al piano dell'elemento a formare una terna destrorsa. In particolare l'asse x ha proiezione in pianta parallela ed equivale all'asse globale X. Nel caso di piastre orizzontali (caso più comune) gli assi x, y e z locali all'elemento sono paralleli ed equivale agli assi X, Y e Z globali. Si sottolinea che non ha alcun interesse collocare esattamente nel piano dell'elemento la posizione dell'origine in quanto i parametri di sollecitazione sono invarianti rispetto a tale posizione.

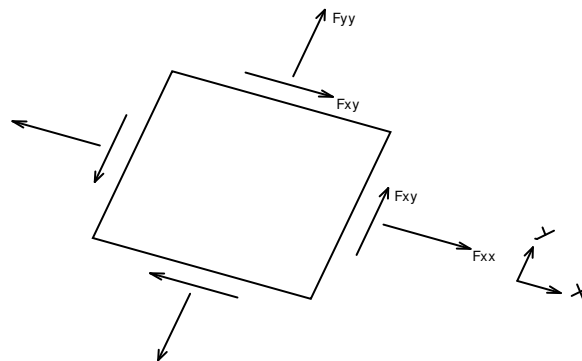
In figura è mostrato un elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione Mxx, Myy, Mxy.



Si definiscono:

- M_{xx} : momento flettente [Forza*Lunghezza/Lunghezza] agente sul bordo di normale x (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- M_{yy} : momento flettente [Forza*Lunghezza/Lunghezza] agente sul bordo di normale y (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- M_{xy} : momento torcente [Forza*Lunghezza/Lunghezza] agente sui bordi (verso positivo indicato dalla freccia in figura).

Per quanto riguarda le sollecitazioni estensionali si faccia riferimento alla figura seguente dove per lo stesso elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione F_{xx} , F_{yy} , F_{xy} .

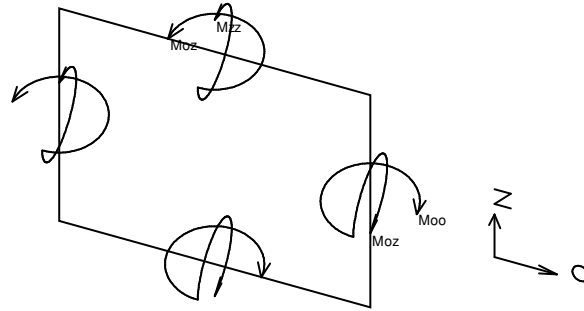


Si definiscono:

- F_{xx} : sforzo tensionale [Forza/Lunghezza] agente sul bordo di normale x (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- F_{yy} : sforzo tensionale [Forza/Lunghezza] agente sul bordo di normale all'asse y (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- F_{xy} : sforzo tagliente [Forza/Lunghezza] agente sui bordi (verso positivo indicato dalla freccia in figura).

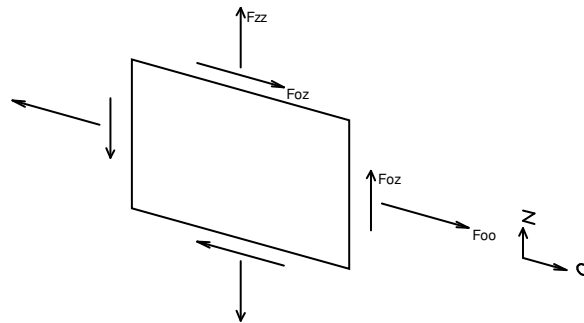
Convenzione di segno per gusci verticali

Il sistema di riferimento nel quale sono espressi i parametri di sollecitazione è così definito: origine appartenente al piano dell'elemento, asse O (ascisse) e z (ordinate) contenuti nel piano dell'elemento e terzo asse ortogonale al piano dell'elemento a formare una terna destrorsa. In particolare l'asse O è orizzontale e l'asse z parallelo ed equiverso con l'asse Z globale. Si sottolinea che non ha alcun interesse collocare esattamente nel piano dell'elemento la posizione dell'origine in quanto i parametri di sollecitazione sono invarianti rispetto a tale posizione. In figura è mostrato un elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione M_{xx} , M_{zz} , M_{xz} .



- Moo: momento flettente distribuito $[Forza * Lunghezza / Lunghezza]$ applicato al bordo di normale parallela all'asse O (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- Mzz: momento flettente distribuito $[Forza * Lunghezza / Lunghezza]$ applicato al bordo di normale parallela all'asse z (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- Moz: momento 'torcente' distribuito $[Forza * Lunghezza / Lunghezza]$ applicato sui bordi (verso positivo indicato dalla freccia in figura).

Per quanto riguarda le sollecitazioni estensionali si faccia riferimento alla figura seguente dove per lo stesso elemento infinitesimo di shell con indicato il sistema di riferimento i parametri di sollecitazione Foo, Fzz, Foz sono rispettivamente:



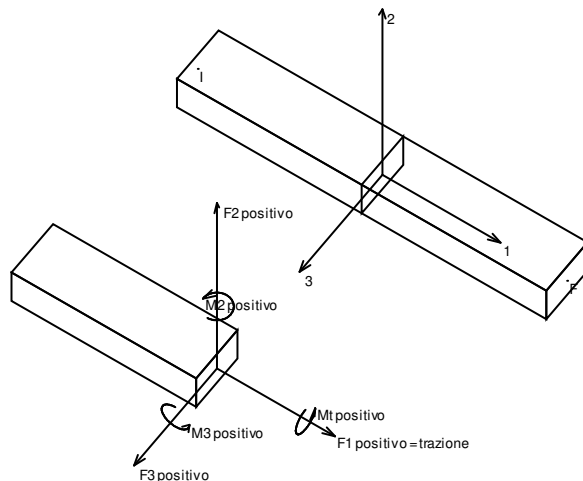
- Fzz: sforzo tensionale distribuito $[Forza / Lunghezza]$ applicato al bordo di normale parallela all'asse z (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- Foo: sforzo tensionale distribuito $[Forza / Lunghezza]$ applicato al bordo di normale parallela all'asse O (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- Foz: sforzo tagliante distribuito $[Forza / Lunghezza]$ applicato sui bordi (verso positivo indicato dalla freccia in figura).

1.1.5 Sollecitazioni aste in muratura

1.1.5.1 Convenzioni di segno aste

Le abbreviazioni relative alle sollecitazioni sugli elementi aste sono da intendersi:

- F1 (N): sforzo normale nell'asta;
- F2: sforzo di taglio agente nella direzione dell'asse locale 2;
- F3: sforzo di taglio agente nella direzione dell'asse locale 3;
- M1 (Mt): momento attorno all'asse locale 1; equivale al momento torcente;
- M2: momento attorno all'asse locale 2;
- M3: momento attorno all'asse locale 3.



La convenzione sui segni per i parametri di sollecitazione delle aste è la seguente:

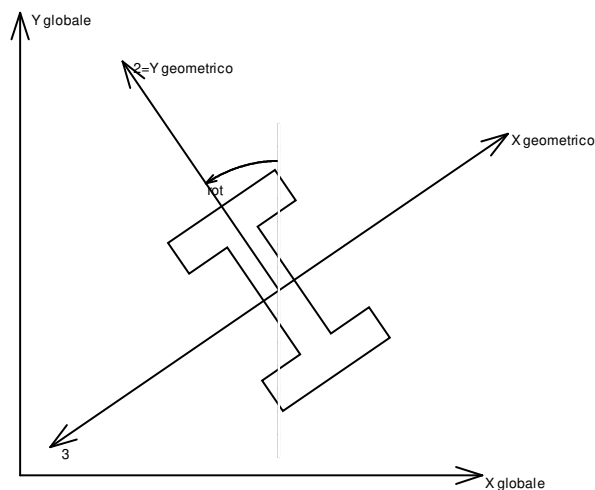
presa un'asta con nodo iniziale i e nodo finale f , asse 1 che va da i a f , assi 2 e 3 presi secondo quanto indicato nei paragrafi successivi relativi al sistema locale delle aste sezionando l'asta in un punto e considerando la sezione sinistra del punto in cui si è effettuato il taglio (sezione da cui esce il versore asse 1) i parametri di sollecitazione sono positivi se hanno verso e direzione concordi con il sistema di riferimento locale dell'asta 1, 2, 3 (per i momenti si adotta la regola della mano destra).

Il sistema è definito diversamente per tre categorie di aste, a seconda che siano originate da:

- aste verticali ad esempio pilastri e colonne;
- aste non verticali non di c.a., ad esempio travi di acciaio o legno;
- aste non verticali in c.a.: travi in c.a. di piano, falda o a quota generica.

Nel seguito si indica con 1, 2 e 3 il sistema locale dell'asta che non sempre coincide con gli assi principali della sezione. Si ricorda che per assi principali si intendono gli assi rispetto a cui si ha il raggio di inerzia minimo e massimo. Gli assi 1, 2 e 3 rispettano la regola della mano destra.

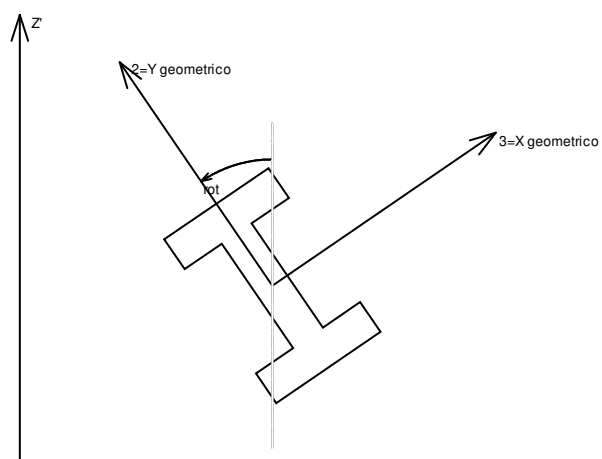
Sistema locale aste verticali



Nella figura si considera l'asse 1 uscente dal foglio (l'osservatore guarda in direzione opposta a quella dell'asse 1).



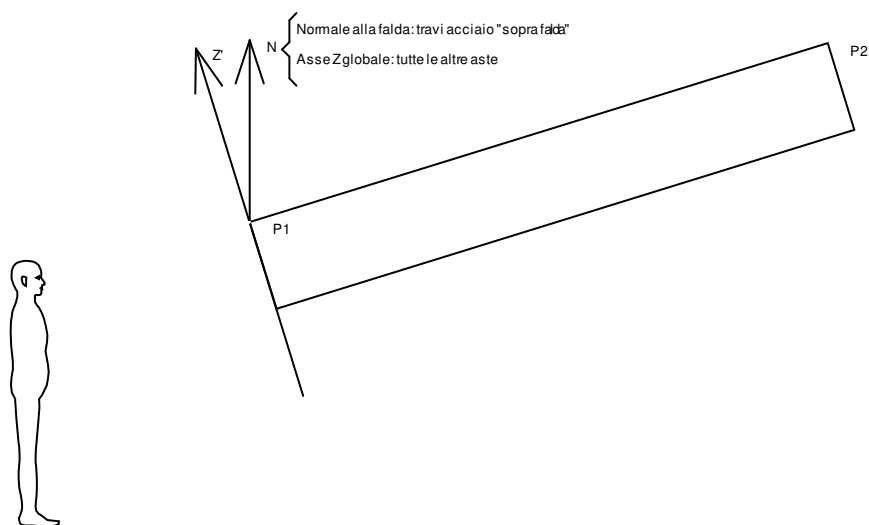
Sistema locale aste non verticali



Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1).

L'asse Z' è illustrato nella figura seguente dove:

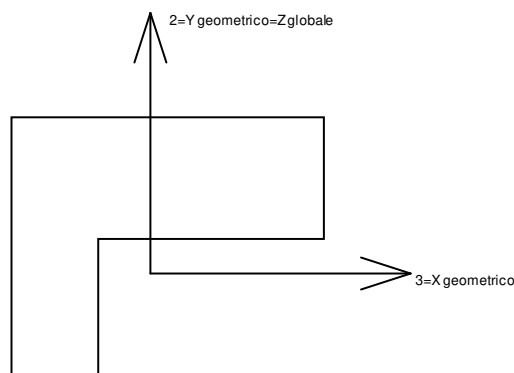
- P1 è il punto di inserimento iniziale dell'asta;
- P2 è il punto di inserimento finale dell'asta;
- N è la normale al piano o falda di inserimento;



Z' è quindi l'intersezione tra il piano passante per P1, P2 contenente N e il piano della sezione iniziale dell'asta.



Sistema locale aste derivanti da travi in c.a.



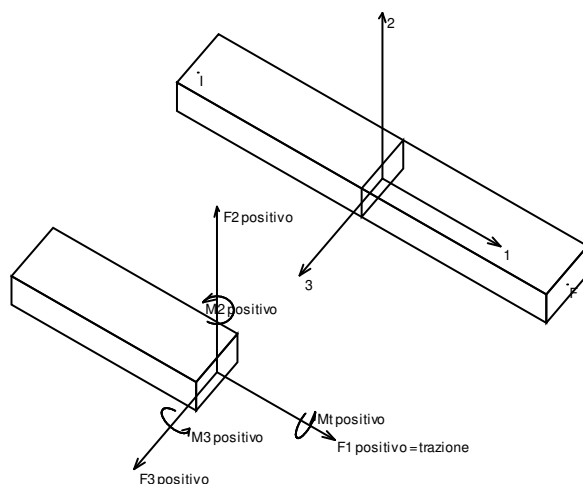
Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1). L'asse 2 è sempre verticale e quindi coincidente con l'asse Z globale nonché con l'asse y geometrico. L'asse 3 coincide con l'asse x geometrico. Si sottolinea il fatto che gli assi 2 e 3 non corrispondono agli assi principali della sezione.

1.1.6 Sollecitazioni aste in muratura FRCM

1.1.6.1 Convenzioni di segno aste

Le abbreviazioni relative alle sollecitazioni sugli elementi aste sono da intendersi:

- F1 (N): sforzo normale nell'asta;
- F2: sforzo di taglio agente nella direzione dell'asse locale 2;
- F3: sforzo di taglio agente nella direzione dell'asse locale 3;
- M1 (Mt): momento attorno all'asse locale 1; equivale al momento torcente;
- M2: momento attorno all'asse locale 2;
- M3: momento attorno all'asse locale 3.



La convenzione sui segni per i parametri di sollecitazione delle aste è la seguente:

presa un'asta con nodo iniziale i e nodo finale f, asse 1 che va da i a f, assi 2 e 3 presi secondo quanto indicato nei paragrafi successivi relativi al sistema locale delle aste sezionando l'asta in un punto e considerando la sezione sinistra del punto in cui si è effettuato il taglio (sezione da cui esce il versore asse 1) i parametri di sollecitazione sono positivi se hanno verso e direzione concordi con il sistema di riferimento locale dell'asta 1, 2, 3 (per i momenti si adotta la regola della mano destra).

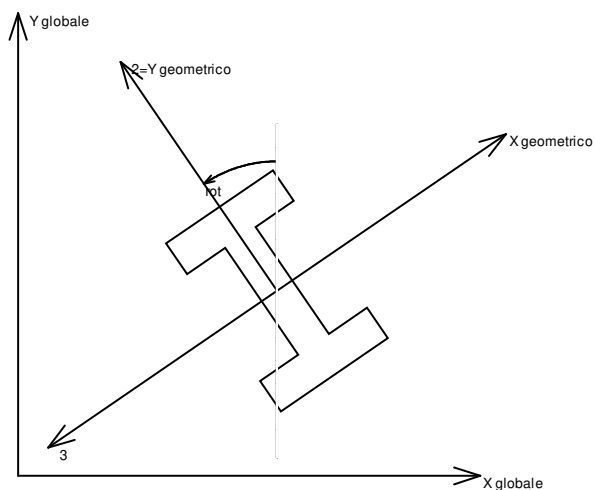
Il sistema è definito diversamente per tre categorie di aste, a seconda che siano originate da:

- aste verticali ad esempio pilastri e colonne;
- aste non verticali non di c.a., ad esempio travi di acciaio o legno;
- aste non verticali in c.a.: travi in c.a. di piano, falda o a quota generica.

Nel seguito si indica con 1, 2 e 3 il sistema locale dell'asta che non sempre coincide con gli assi principali della sezione. Si ricorda che per assi principali si intendono gli assi rispetto a cui si ha il raggio di inerzia minimo e massimo. Gli assi 1, 2 e 3 rispettano la regola della mano destra.

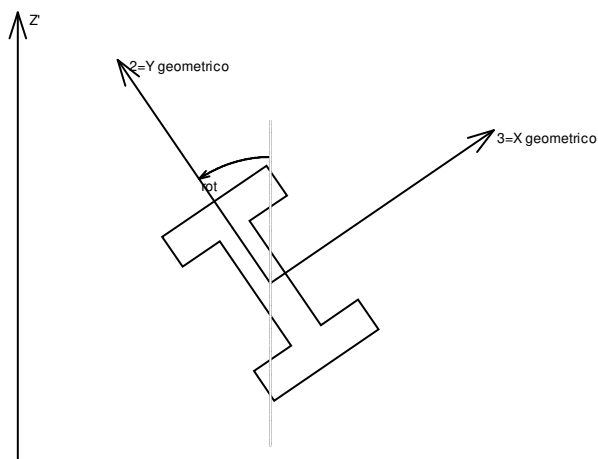


Sistema locale aste verticali



Nella figura si considera l'asse 1 uscente dal foglio (l'osservatore guarda in direzione opposta a quella dell'asse 1).

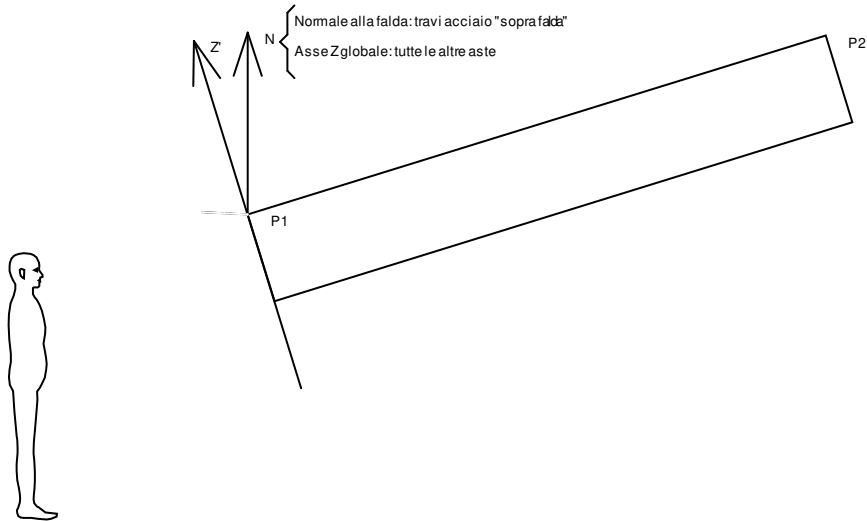
Sistema locale aste non verticali



Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1).

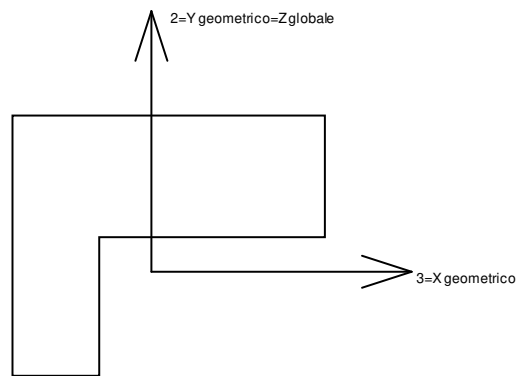
L'asse Z' è illustrato nella figura seguente dove:

- P1 è il punto di inserimento iniziale dell'asta;
- P2 è il punto di inserimento finale dell'asta;
- N è la normale al piano o falda di inserimento;



Z' è quindi l'intersezione tra il piano passante per $P1, P2$ contenente N e il piano della sezione iniziale dell'asta.

Sistema locale aste derivanti da travi in c.a.



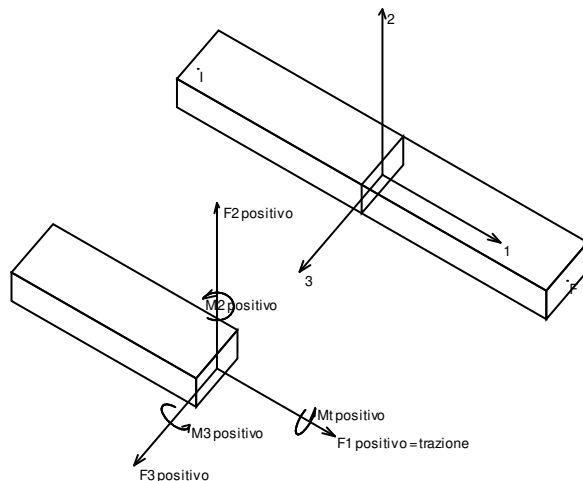
Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1). L'asse 2 è sempre verticale e quindi coincidente con l'asse Z globale nonché con l'asse y geometrico. L'asse 3 coincide con l'asse x geometrico. Si sottolinea il fatto che gli assi 2 e 3 non corrispondono agli assi principali della sezione.

1.1.7 Sollecitazioni aste in muratura armata

1.1.7.1 Convenzioni di segno aste

Le abbreviazioni relative alle sollecitazioni sugli elementi aste sono da intendersi:

- $F1 (N)$: sforzo normale nell'asta;
- $F2$: sforzo di taglio agente nella direzione dell'asse locale 2;
- $F3$: sforzo di taglio agente nella direzione dell'asse locale 3;
- $M1 (Mt)$: momento attorno all'asse locale 1; equivale al momento torcente;
- $M2$: momento attorno all'asse locale 2;
- $M3$: momento attorno all'asse locale 3.



La convenzione sui segni per i parametri di sollecitazione delle aste è la seguente:

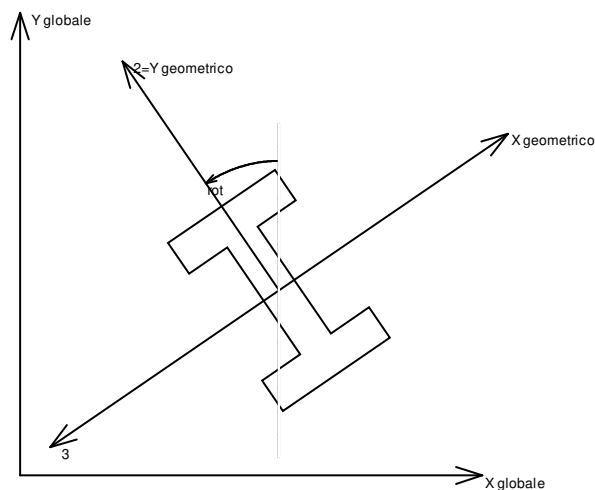
presa un'asta con nodo iniziale i e nodo finale f , asse 1 che va da i a f , assi 2 e 3 presi secondo quanto indicato nei paragrafi successivi relativi al sistema locale delle aste sezionando l'asta in un punto e considerando la sezione sinistra del punto in cui si è effettuato il taglio (sezione da cui esce il versore asse 1) i parametri di sollecitazione sono positivi se hanno verso e direzione concordi con il sistema di riferimento locale dell'asta 1, 2, 3 (per i momenti si adotta la regola della mano destra).

Il sistema è definito diversamente per tre categorie di aste, a seconda che siano originate da:

- aste verticali ad esempio pilastri e colonne;
- aste non verticali non di c.a., ad esempio travi di acciaio o legno;
- aste non verticali in c.a.: travi in c.a. di piano, falda o a quota generica.

Nel seguito si indica con 1, 2 e 3 il sistema locale dell'asta che non sempre coincide con gli assi principali della sezione. Si ricorda che per assi principali si intendono gli assi rispetto a cui si ha il raggio di inerzia minimo e massimo. Gli assi 1, 2 e 3 rispettano la regola della mano destra.

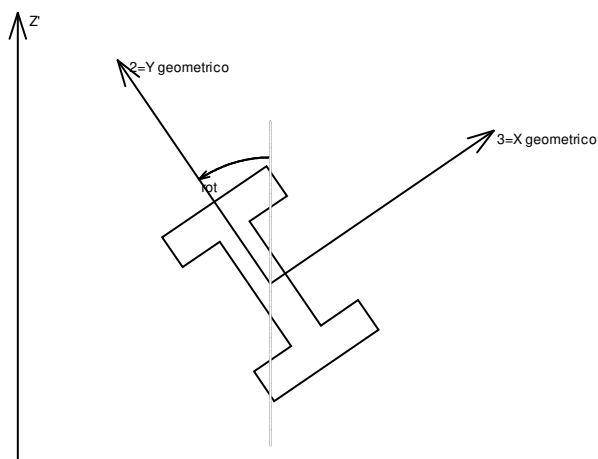
Sistema locale aste verticali



Nella figura si considera l'asse 1 uscente dal foglio (l'osservatore guarda in direzione opposta a quella dell'asse 1).



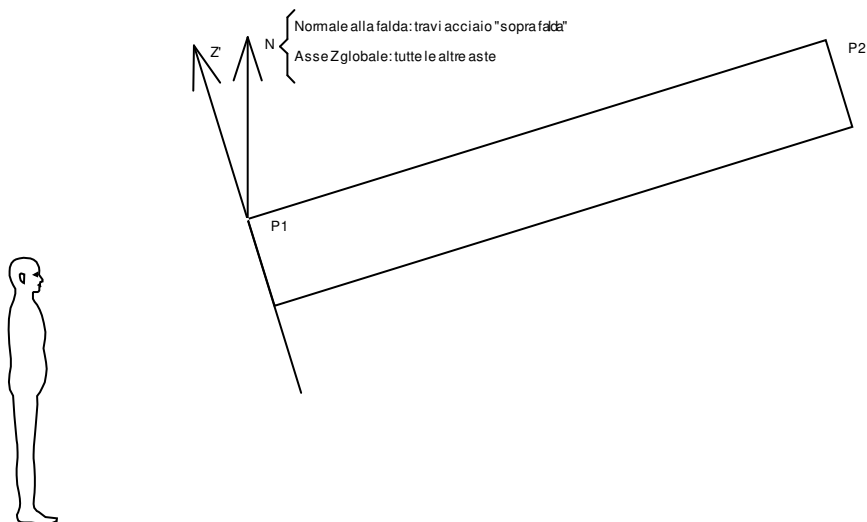
Sistema locale aste non verticali



Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1).

L'asse Z' è illustrato nella figura seguente dove:

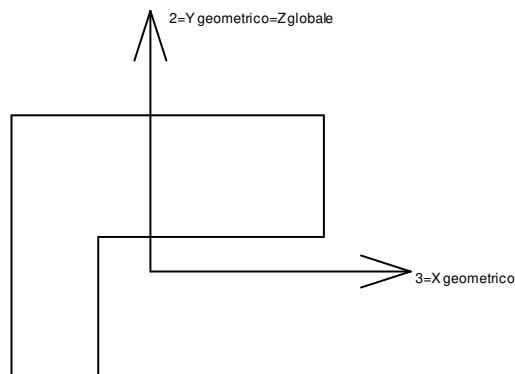
- P1 è il punto di inserimento iniziale dell'asta;
- P2 è il punto di inserimento finale dell'asta;
- N è la normale al piano o falda di inserimento;



Z' è quindi l'intersezione tra il piano passante per P1, P2 contenente N e il piano della sezione iniziale dell'asta.



Sistema locale aste derivanti da travi in c.a.



Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1). L'asse 2 è sempre verticale e quindi coincidente con l'asse Z globale nonché con l'asse y geometrico. L'asse 3 coincide con l'asse x geometrico. Si sottolinea il fatto che gli assi 2 e 3 non corrispondono agli assi principali della sezione.

1.2 Reazioni nodali

1.2.1 Reazioni nodali estreme

Nodo: Nodo sollecitato dalla reazione vincolare.

Ind.: indice del nodo.

Cont.: Contesto a cui si riferisce la reazione vincolare.

N.br.: nome breve della condizione o combinazione di carico.

Reazione a traslazione: reazione vincolare traslazionale del nodo.

x: componente X della reazione vincolare del nodo. [daN]

y: componente Y della reazione vincolare del nodo. [daN]

z: componente Z della reazione vincolare del nodo. [daN]

Reazione a rotazione: reazione vincolare rotazionale del nodo.

x: componente X della reazione a rotazione del nodo. [daN*m]

y: componente Y della reazione a rotazione del nodo. [daN*m]

z: componente Z della reazione a rotazione del nodo. [daN*m]

Reazioni Fx minime

Vengono mostrati i soli 5 nodi più sollecitati.

Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
142	SLV 15	-1255	-661	5157	20.76	-29.52	0.73
83	SLV 15	-1211	9	2056	5.54	-50.29	0
82	SLV 15	-1141	4	2042	16	-46.12	0.02
130	SLV 15	-1116	-718	3646	223.62	-94.53	4.89
81	SLV 15	-1065	-19	2121	30.78	-43.09	0

Reazioni Fx massime

Vengono mostrati i soli 5 nodi più sollecitati.

Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
121	SLV 1	1187	-4	207	3.17	61.36	-0.21
61	SLV 3	1115	15	1986	-0.44	53.26	0.25
120	SLV 3	1112	99	930	-6.28	33.91	0.68
122	SLV 3	1099	-2	1346	24.18	55.26	-0.85
132	SLV 3	1074	18	2694	20.26	22.36	-3.93

Reazioni Fy minime

Vengono mostrati i soli 5 nodi più sollecitati.

Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
14	SLV 7	80	-5025	2414	1847.85	3.31	0.86
130	SLV 7	-524	-3552	2272	1109.23	-52.5	11.76
58	SLV 9	7	-1887	1253	-129.93	3.72	0.53
15	SLV 7	251	-1541	1998	651.51	10.66	5.03
13	SLV 7	130	-1540	2139	670.38	4.95	-7.33

Reazioni Fy massime

Vengono mostrati i soli 5 nodi più sollecitati.

Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
14	SLV 9	-81	5022	3518	-1846.7	-3.39	-0.86



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
130	SLV 9	-602	3553	2218	-1109.15	-52.76	-11.75
58	SLV 7	-7	1890	906	129.82	-3.84	-0.51
15	SLV 9	-347	1540	2893	-651.07	-14.2	-5.03
13	SLV 9	-30	1539	2953	-669.93	-1.59	7.33

Reazioni Fz minime

Vengono mostrati i soli 5 nodi più sollecitati.

Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
113	SLV X	-432	-350	-2745	14.82	-19.66	-0.09
110	SLV X	-8	-223	-1905	-8.4	-13.58	0.04
107	SLV X	-24	-216	-1395	-8.04	-26.32	-0.04
2	SLV Y	-88	-385	-1366	14.55	2.42	-0.14
104	SLV X	-47	-211	-1144	-8.11	-39.52	-0.02

Reazioni Fz massime

Vengono mostrati i soli 5 nodi più sollecitati.

Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
120	SLV 15	-77	-717	6278	25.49	-13.02	-0.1
113	SLV 1	713	279	5942	-12.95	30.27	0.09
84	SLU 81	-786	17	5888	-0.26	-28.19	0
60	SLU 81	739	10	5695	-0.55	28.68	0
142	SLU 81	-1061	-689	5173	19.72	-22.56	-0.02

1.2.2 Reazioni nodali in combinazioni di carico

Nodo: Nodo sollecitato dalla reazione vincolare.

Ind.: indice del nodo.

Cont.: Contesto a cui si riferisce la reazione vincolare.

N.br.: nome breve della condizione o combinazione di carico.

Reazione a traslazione: reazione vincolare traslazionale del nodo.

x: componente X della reazione vincolare del nodo. [daN]

y: componente Y della reazione vincolare del nodo. [daN]

z: componente Z della reazione vincolare del nodo. [daN]

Reazione a rotazione: reazione vincolare rotazionale del nodo.

x: componente X della reazione a rotazione del nodo. [daN*m]

y: componente Y della reazione a rotazione del nodo. [daN*m]

z: componente Z della reazione a rotazione del nodo. [daN*m]

Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
2	SLU 1	430	379	2893	-10.52	12.5	-0.01
2	SLU 2	430	379	2893	-10.52	12.5	-0.01
2	SLU 3	430	379	2893	-10.52	12.5	-0.01
2	SLU 4	430	379	2893	-10.52	12.5	-0.01
2	SLU 5	430	379	2893	-10.52	12.5	-0.01
2	SLU 6	430	379	2893	-10.52	12.5	-0.01
2	SLU 7	430	379	2893	-10.52	12.5	-0.01
2	SLU 8	430	379	2893	-10.52	12.5	-0.01
2	SLU 9	430	379	2893	-10.52	12.5	-0.01
2	SLU 10	506	457	3418	-12.89	14.73	-0.01
2	SLU 11	506	457	3418	-12.89	14.73	-0.01
2	SLU 12	506	457	3418	-12.89	14.73	-0.01
2	SLU 13	506	457	3418	-12.89	14.73	-0.01
2	SLU 14	506	457	3418	-12.89	14.73	-0.01
2	SLU 15	506	457	3418	-12.89	14.73	-0.01
2	SLU 16	506	457	3418	-12.89	14.73	-0.01
2	SLU 17	506	457	3418	-12.89	14.73	-0.01
2	SLU 18	539	491	3643	-13.91	15.68	-0.01
2	SLU 19	539	491	3643	-13.91	15.68	-0.01
2	SLU 20	539	491	3643	-13.91	15.68	-0.01
2	SLU 21	539	491	3643	-13.91	15.68	-0.01
2	SLU 22	480	421	3207	-11.75	14.01	-0.01
2	SLU 23	480	421	3207	-11.75	14.01	-0.01
2	SLU 24	480	421	3207	-11.75	14.01	-0.01
2	SLU 25	480	421	3207	-11.75	14.01	-0.01
2	SLU 26	480	421	3207	-11.75	14.01	-0.01
2	SLU 27	480	421	3207	-11.75	14.01	-0.01
2	SLU 28	480	421	3207	-11.75	14.01	-0.01
2	SLU 29	480	421	3207	-11.75	14.01	-0.01
2	SLU 30	480	421	3207	-11.75	14.01	-0.01
2	SLU 31	556	500	3732	-14.12	16.23	-0.01
2	SLU 32	556	500	3732	-14.12	16.23	-0.01
2	SLU 33	556	500	3732	-14.12	16.23	-0.01
2	SLU 34	556	500	3732	-14.12	16.23	-0.01
2	SLU 35	556	500	3732	-14.12	16.23	-0.01
2	SLU 36	556	500	3732	-14.12	16.23	-0.01
2	SLU 37	556	500	3732	-14.12	16.23	-0.01
2	SLU 38	556	500	3732	-14.12	16.23	-0.01
2	SLU 39	589	534	3957	-15.14	17.19	-0.01
2	SLU 40	589	534	3957	-15.14	17.19	-0.01
2	SLU 41	589	534	3957	-15.14	17.19	-0.01
2	SLU 42	589	534	3957	-15.14	17.19	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
2	SLU 43	542	478	3653	-13.26	15.74	-0.02
2	SLU 44	542	478	3653	-13.26	15.74	-0.02
2	SLU 45	542	478	3653	-13.26	15.74	-0.02
2	SLU 46	542	478	3653	-13.26	15.74	-0.02
2	SLU 47	542	478	3653	-13.26	15.74	-0.02
2	SLU 48	542	478	3653	-13.26	15.74	-0.02
2	SLU 49	542	478	3653	-13.26	15.74	-0.02
2	SLU 50	542	478	3653	-13.26	15.74	-0.02
2	SLU 51	542	478	3653	-13.26	15.74	-0.02
2	SLU 52	618	556	4178	-15.63	17.96	-0.01
2	SLU 53	618	556	4178	-15.63	17.96	-0.01
2	SLU 54	618	556	4178	-15.63	17.96	-0.01
2	SLU 55	618	556	4178	-15.63	17.96	-0.01
2	SLU 56	618	556	4178	-15.63	17.96	-0.01
2	SLU 57	618	556	4178	-15.63	17.96	-0.01
2	SLU 58	618	556	4178	-15.63	17.96	-0.01
2	SLU 59	618	556	4178	-15.63	17.96	-0.01
2	SLU 60	651	590	4403	-16.65	18.92	-0.01
2	SLU 61	651	590	4403	-16.65	18.92	-0.01
2	SLU 62	651	590	4403	-16.65	18.92	-0.01
2	SLU 63	651	590	4403	-16.65	18.92	-0.01
2	SLU 64	592	520	3967	-14.48	17.24	-0.02
2	SLU 65	592	520	3967	-14.48	17.24	-0.02
2	SLU 66	592	520	3967	-14.48	17.24	-0.02
2	SLU 67	592	520	3967	-14.48	17.24	-0.02
2	SLU 68	592	520	3967	-14.48	17.24	-0.02
2	SLU 69	592	520	3967	-14.48	17.24	-0.02
2	SLU 70	592	520	3967	-14.48	17.24	-0.02
2	SLU 71	592	520	3967	-14.48	17.24	-0.02
2	SLU 72	592	520	3967	-14.48	17.24	-0.02
2	SLU 73	668	599	4492	-16.86	19.47	-0.02
2	SLU 74	668	599	4492	-16.86	19.47	-0.02
2	SLU 75	668	599	4492	-16.86	19.47	-0.02
2	SLU 76	668	599	4492	-16.86	19.47	-0.02
2	SLU 77	668	599	4492	-16.86	19.47	-0.02
2	SLU 78	668	599	4492	-16.86	19.47	-0.02
2	SLU 79	668	599	4492	-16.86	19.47	-0.02
2	SLU 80	668	599	4492	-16.86	19.47	-0.02
2	SLU 81	701	633	4717	-17.87	20.42	-0.01
2	SLU 82	701	633	4717	-17.87	20.42	-0.01
2	SLU 83	701	633	4717	-17.87	20.42	-0.01
2	SLU 84	701	633	4717	-17.87	20.42	-0.01
2	SLE RA 1	444	391	2982	-10.87	12.93	-0.01
2	SLE RA 2	444	391	2982	-10.87	12.93	-0.01
2	SLE RA 3	444	391	2982	-10.87	12.93	-0.01
2	SLE RA 4	444	391	2982	-10.87	12.93	-0.01
2	SLE RA 5	444	391	2982	-10.87	12.93	-0.01
2	SLE RA 6	444	391	2982	-10.87	12.93	-0.01
2	SLE RA 7	444	391	2982	-10.87	12.93	-0.01
2	SLE RA 8	444	391	2982	-10.87	12.93	-0.01
2	SLE RA 9	444	391	2982	-10.87	12.93	-0.01
2	SLE RA 10	495	443	3333	-12.45	14.42	-0.01
2	SLE RA 11	495	443	3333	-12.45	14.42	-0.01
2	SLE RA 12	495	443	3333	-12.45	14.42	-0.01
2	SLE RA 13	495	443	3333	-12.45	14.42	-0.01
2	SLE RA 14	495	443	3333	-12.45	14.42	-0.01
2	SLE RA 15	495	443	3333	-12.45	14.42	-0.01
2	SLE RA 16	495	443	3333	-12.45	14.42	-0.01
2	SLE RA 17	495	443	3333	-12.45	14.42	-0.01
2	SLE RA 18	517	466	3483	-13.13	15.05	-0.01
2	SLE RA 19	517	466	3483	-13.13	15.05	-0.01
2	SLE RA 20	517	466	3483	-13.13	15.05	-0.01
2	SLE RA 21	517	466	3483	-13.13	15.05	-0.01
2	SLE FR 1	444	391	2982	-10.87	12.93	-0.01
2	SLE FR 2	444	391	2982	-10.87	12.93	-0.01
2	SLE FR 3	444	391	2982	-10.87	12.93	-0.01
2	SLE FR 4	466	413	3133	-11.55	13.57	-0.01
2	SLE FR 5	466	413	3133	-11.55	13.57	-0.01
2	SLE FR 6	481	428	3233	-12	13.99	-0.01
2	SLE QP 1	444	391	2982	-10.87	12.93	-0.01
2	SLE QP 2	466	413	3133	-11.55	13.57	-0.01
2	SLD 1	627	398	3807	-10.84	19.13	-0.06
2	SLD 2	627	398	3807	-10.84	19.13	-0.06
2	SLD 3	605	300	3459	-7.13	19.74	-0.09
2	SLD 4	605	300	3459	-7.13	19.74	-0.09
2	SLD 5	548	557	3863	-16.98	14.32	0.03
2	SLD 6	548	557	3863	-16.98	14.32	0.03
2	SLD 7	474	231	2702	-4.59	16.34	-0.09
2	SLD 8	474	231	2702	-4.59	16.34	-0.09
2	SLD 9	458	596	3563	-18.51	10.8	0.07
2	SLD 10	458	596	3563	-18.51	10.8	0.07
2	SLD 11	385	269	2402	-6.12	12.82	-0.05
2	SLD 12	385	269	2402	-6.12	12.82	-0.05
2	SLD 13	328	526	2806	-15.97	7.4	0.07
2	SLD 14	328	526	2806	-15.97	7.4	0.07
2	SLD 15	306	428	2458	-12.26	8	0.03
2	SLD 16	306	428	2458	-12.26	8	0.03
2	SLV 1	844	373	4728	-9.68	26.65	-0.12
2	SLV 2	844	373	4728	-9.68	26.65	-0.12



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
2	SLV 3	791	143	3909	-0.95	28.1	-0.21
2	SLV 4	791	143	3909	-0.95	28.1	-0.21
2	SLV 5	660	751	4854	-24.23	15.29	0.09
2	SLV 6	660	751	4854	-24.23	15.29	0.09
2	SLV 7	484	-18	2122	4.87	20.13	-0.2
2	SLV 8	484	-18	2122	4.87	20.13	-0.2
2	SLV 9	449	844	4143	-27.97	7.01	0.18
2	SLV 10	449	844	4143	-27.97	7.01	0.18
2	SLV 11	273	75	1411	1.13	11.84	-0.11
2	SLV 12	273	75	1411	1.13	11.84	-0.11
2	SLV 13	141	684	2357	-22.15	-0.96	0.18
2	SLV 14	141	684	2357	-22.15	-0.96	0.18
2	SLV 15	88	453	1537	-13.42	0.49	0.1
2	SLV 16	88	453	1537	-13.42	0.49	0.1
3	SLU 1	395	3	2371	-1.01	18.33	-0.01
3	SLU 2	395	3	2371	-1.01	18.33	-0.01
3	SLU 3	395	3	2371	-1.01	18.33	-0.01
3	SLU 4	395	3	2371	-1.01	18.33	-0.01
3	SLU 5	395	3	2371	-1.01	18.33	-0.01
3	SLU 6	395	3	2371	-1.01	18.33	-0.01
3	SLU 7	395	3	2371	-1.01	18.33	-0.01
3	SLU 8	395	3	2371	-1.01	18.33	-0.01
3	SLU 9	395	3	2371	-1.01	18.33	-0.01
3	SLU 10	463	4	2784	-1.24	21.62	-0.01
3	SLU 11	463	4	2784	-1.24	21.62	-0.01
3	SLU 12	463	4	2784	-1.24	21.62	-0.01
3	SLU 13	463	4	2784	-1.24	21.62	-0.01
3	SLU 14	463	4	2784	-1.24	21.62	-0.01
3	SLU 15	463	4	2784	-1.24	21.62	-0.01
3	SLU 16	463	4	2784	-1.24	21.62	-0.01
3	SLU 17	463	4	2784	-1.24	21.62	-0.01
3	SLU 18	493	4	2961	-1.34	23.03	-0.01
3	SLU 19	493	4	2961	-1.34	23.03	-0.01
3	SLU 20	493	4	2961	-1.34	23.03	-0.01
3	SLU 21	493	4	2961	-1.34	23.03	-0.01
3	SLU 22	444	4	2623	-1.13	20.63	-0.01
3	SLU 23	444	4	2623	-1.13	20.63	-0.01
3	SLU 24	444	4	2623	-1.13	20.63	-0.01
3	SLU 25	444	4	2623	-1.13	20.63	-0.01
3	SLU 26	444	4	2623	-1.13	20.63	-0.01
3	SLU 27	444	4	2623	-1.13	20.63	-0.01
3	SLU 28	444	4	2623	-1.13	20.63	-0.01
3	SLU 29	444	4	2623	-1.13	20.63	-0.01
3	SLU 30	444	4	2623	-1.13	20.63	-0.01
3	SLU 31	513	4	3035	-1.36	23.92	-0.01
3	SLU 32	513	4	3035	-1.36	23.92	-0.01
3	SLU 33	513	4	3035	-1.36	23.92	-0.01
3	SLU 34	513	4	3035	-1.36	23.92	-0.01
3	SLU 35	513	4	3035	-1.36	23.92	-0.01
3	SLU 36	513	4	3035	-1.36	23.92	-0.01
3	SLU 37	513	4	3035	-1.36	23.92	-0.01
3	SLU 38	513	4	3035	-1.36	23.92	-0.01
3	SLU 39	542	4	3212	-1.46	25.32	-0.02
3	SLU 40	542	4	3212	-1.46	25.32	-0.02
3	SLU 41	542	4	3212	-1.46	25.32	-0.02
3	SLU 42	542	4	3212	-1.46	25.32	-0.02
3	SLU 43	496	4	2996	-1.27	23.05	-0.01
3	SLU 44	496	4	2996	-1.27	23.05	-0.01
3	SLU 45	496	4	2996	-1.27	23.05	-0.01
3	SLU 46	496	4	2996	-1.27	23.05	-0.01
3	SLU 47	496	4	2996	-1.27	23.05	-0.01
3	SLU 48	496	4	2996	-1.27	23.05	-0.01
3	SLU 49	496	4	2996	-1.27	23.05	-0.01
3	SLU 50	496	4	2996	-1.27	23.05	-0.01
3	SLU 51	496	4	2996	-1.27	23.05	-0.01
3	SLU 52	565	5	3409	-1.5	26.34	-0.02
3	SLU 53	565	5	3409	-1.5	26.34	-0.02
3	SLU 54	565	5	3409	-1.5	26.34	-0.02
3	SLU 55	565	5	3409	-1.5	26.34	-0.02
3	SLU 56	565	5	3409	-1.5	26.34	-0.02
3	SLU 57	565	5	3409	-1.5	26.34	-0.02
3	SLU 58	565	5	3409	-1.5	26.34	-0.02
3	SLU 59	565	5	3409	-1.5	26.34	-0.02
3	SLU 60	594	5	3586	-1.6	27.75	-0.02
3	SLU 61	594	5	3586	-1.6	27.75	-0.02
3	SLU 62	594	5	3586	-1.6	27.75	-0.02
3	SLU 63	594	5	3586	-1.6	27.75	-0.02
3	SLU 64	546	4	3248	-1.39	25.34	-0.02
3	SLU 65	546	4	3248	-1.39	25.34	-0.02
3	SLU 66	546	4	3248	-1.39	25.34	-0.02
3	SLU 67	546	4	3248	-1.39	25.34	-0.02
3	SLU 68	546	4	3248	-1.39	25.34	-0.02
3	SLU 69	546	4	3248	-1.39	25.34	-0.02
3	SLU 70	546	4	3248	-1.39	25.34	-0.02
3	SLU 71	546	4	3248	-1.39	25.34	-0.02
3	SLU 72	546	4	3248	-1.39	25.34	-0.02
3	SLU 73	614	5	3660	-1.62	28.63	-0.02
3	SLU 74	614	5	3660	-1.62	28.63	-0.02
3	SLU 75	614	5	3660	-1.62	28.63	-0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
3	SLU 76	614	5	3660	-1.62	28.63	-0.02
3	SLU 77	614	5	3660	-1.62	28.63	-0.02
3	SLU 78	614	5	3660	-1.62	28.63	-0.02
3	SLU 79	614	5	3660	-1.62	28.63	-0.02
3	SLU 80	614	5	3660	-1.62	28.63	-0.02
3	SLU 81	644	5	3837	-1.72	30.04	-0.02
3	SLU 82	644	5	3837	-1.72	30.04	-0.02
3	SLU 83	644	5	3837	-1.72	30.04	-0.02
3	SLU 84	644	5	3837	-1.72	30.04	-0.02
3	SLE RA 1	409	3	2443	-1.04	18.99	-0.01
3	SLE RA 2	409	3	2443	-1.04	18.99	-0.01
3	SLE RA 3	409	3	2443	-1.04	18.99	-0.01
3	SLE RA 4	409	3	2443	-1.04	18.99	-0.01
3	SLE RA 5	409	3	2443	-1.04	18.99	-0.01
3	SLE RA 6	409	3	2443	-1.04	18.99	-0.01
3	SLE RA 7	409	3	2443	-1.04	18.99	-0.01
3	SLE RA 8	409	3	2443	-1.04	18.99	-0.01
3	SLE RA 9	409	3	2443	-1.04	18.99	-0.01
3	SLE RA 10	455	4	2718	-1.2	21.18	-0.01
3	SLE RA 11	455	4	2718	-1.2	21.18	-0.01
3	SLE RA 12	455	4	2718	-1.2	21.18	-0.01
3	SLE RA 13	455	4	2718	-1.2	21.18	-0.01
3	SLE RA 14	455	4	2718	-1.2	21.18	-0.01
3	SLE RA 15	455	4	2718	-1.2	21.18	-0.01
3	SLE RA 16	455	4	2718	-1.2	21.18	-0.01
3	SLE RA 17	455	4	2718	-1.2	21.18	-0.01
3	SLE RA 18	474	4	2836	-1.26	22.12	-0.01
3	SLE RA 19	474	4	2836	-1.26	22.12	-0.01
3	SLE RA 20	474	4	2836	-1.26	22.12	-0.01
3	SLE RA 21	474	4	2836	-1.26	22.12	-0.01
3	SLE FR 1	409	3	2443	-1.04	18.99	-0.01
3	SLE FR 2	409	3	2443	-1.04	18.99	-0.01
3	SLE FR 3	409	3	2443	-1.04	18.99	-0.01
3	SLE FR 4	428	3	2561	-1.11	19.93	-0.01
3	SLE FR 5	428	3	2561	-1.11	19.93	-0.01
3	SLE FR 6	442	4	2639	-1.15	20.55	-0.01
3	SLE QP 1	409	3	2443	-1.04	18.99	-0.01
3	SLE QP 2	428	3	2561	-1.11	19.93	-0.01
3	SLD 1	678	-9	2963	3.06	30.81	-0.05
3	SLD 2	678	-9	2963	3.06	30.81	-0.05
3	SLD 3	643	-6	2745	7.67	29.74	-0.04
3	SLD 4	643	-6	2745	7.67	29.74	-0.04
3	SLD 5	556	-5	3011	-6.84	24.82	-0.04
3	SLD 6	556	-5	3011	-6.84	24.82	-0.04
3	SLD 7	440	5	2287	8.51	21.24	0
3	SLD 8	440	5	2287	8.51	21.24	0
3	SLD 9	417	2	2835	-10.73	18.61	-0.03
3	SLD 10	417	2	2835	-10.73	18.61	-0.03
3	SLD 11	301	12	2111	4.63	15.03	0.02
3	SLD 12	301	12	2111	4.63	15.03	0.02
3	SLD 13	214	13	2376	-9.89	10.12	0.01
3	SLD 14	214	13	2376	-9.89	10.12	0.01
3	SLD 15	179	16	2159	-5.28	9.04	0.03
3	SLD 16	179	16	2159	-5.28	9.04	0.03
3	SLV 1	1014	-28	3514	9.4	45.53	-0.1
3	SLV 2	1014	-28	3514	9.4	45.53	-0.1
3	SLV 3	932	-20	3002	21.03	42.96	-0.07
3	SLV 4	932	-20	3002	21.03	42.96	-0.07
3	SLV 5	730	-17	3623	-15.6	31.5	-0.09
3	SLV 6	730	-17	3623	-15.6	31.5	-0.09
3	SLV 7	454	7	1917	23.17	22.95	0.02
3	SLV 8	454	7	1917	23.17	22.95	0.02
3	SLV 9	403	-1	3204	-25.39	16.91	-0.05
3	SLV 10	403	-1	3204	-25.39	16.91	-0.05
3	SLV 11	127	24	1499	13.38	8.36	0.07
3	SLV 12	127	24	1499	13.38	8.36	0.07
3	SLV 13	-75	27	2119	-23.24	-3.11	0.05
3	SLV 14	-75	27	2119	-23.24	-3.11	0.05
3	SLV 15	-157	35	1608	-11.61	-5.67	0.08
3	SLV 16	-157	35	1608	-11.61	-5.67	0.08
4	SLU 1	293	0	2198	-0.43	11.5	0.01
4	SLU 2	293	0	2198	-0.43	11.5	0.01
4	SLU 3	293	0	2198	-0.43	11.5	0.01
4	SLU 4	293	0	2198	-0.43	11.5	0.01
4	SLU 5	293	0	2198	-0.43	11.5	0.01
4	SLU 6	293	0	2198	-0.43	11.5	0.01
4	SLU 7	293	0	2198	-0.43	11.5	0.01
4	SLU 8	293	0	2198	-0.43	11.5	0.01
4	SLU 9	293	0	2198	-0.43	11.5	0.01
4	SLU 10	347	0	2570	-0.54	13.62	0.01
4	SLU 11	347	0	2570	-0.54	13.62	0.01
4	SLU 12	347	0	2570	-0.54	13.62	0.01
4	SLU 13	347	0	2570	-0.54	13.62	0.01
4	SLU 14	347	0	2570	-0.54	13.62	0.01
4	SLU 15	347	0	2570	-0.54	13.62	0.01
4	SLU 16	347	0	2570	-0.54	13.62	0.01
4	SLU 17	347	0	2570	-0.54	13.62	0.01
4	SLU 18	370	0	2729	-0.59	14.52	0.01
4	SLU 19	370	0	2729	-0.59	14.52	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
4	SLU 20	370	0	2729	-0.59	14.52	0.01
4	SLU 21	370	0	2729	-0.59	14.52	0.01
4	SLU 22	333	0	2430	-0.49	13.04	0.01
4	SLU 23	333	0	2430	-0.49	13.04	0.01
4	SLU 24	333	0	2430	-0.49	13.04	0.01
4	SLU 25	333	0	2430	-0.49	13.04	0.01
4	SLU 26	333	0	2430	-0.49	13.04	0.01
4	SLU 27	333	0	2430	-0.49	13.04	0.01
4	SLU 28	333	0	2430	-0.49	13.04	0.01
4	SLU 29	333	0	2430	-0.49	13.04	0.01
4	SLU 30	333	0	2430	-0.49	13.04	0.01
4	SLU 31	386	0	2801	-0.6	15.16	0.01
4	SLU 32	386	0	2801	-0.6	15.16	0.01
4	SLU 33	386	0	2801	-0.6	15.16	0.01
4	SLU 34	386	0	2801	-0.6	15.16	0.01
4	SLU 35	386	0	2801	-0.6	15.16	0.01
4	SLU 36	386	0	2801	-0.6	15.16	0.01
4	SLU 37	386	0	2801	-0.6	15.16	0.01
4	SLU 38	386	0	2801	-0.6	15.16	0.01
4	SLU 39	409	0	2961	-0.65	16.06	0.01
4	SLU 40	409	0	2961	-0.65	16.06	0.01
4	SLU 41	409	0	2961	-0.65	16.06	0.01
4	SLU 42	409	0	2961	-0.65	16.06	0.01
4	SLU 43	368	0	2778	-0.54	14.43	0.01
4	SLU 44	368	0	2778	-0.54	14.43	0.01
4	SLU 45	368	0	2778	-0.54	14.43	0.01
4	SLU 46	368	0	2778	-0.54	14.43	0.01
4	SLU 47	368	0	2778	-0.54	14.43	0.01
4	SLU 48	368	0	2778	-0.54	14.43	0.01
4	SLU 49	368	0	2778	-0.54	14.43	0.01
4	SLU 50	368	0	2778	-0.54	14.43	0.01
4	SLU 51	368	0	2778	-0.54	14.43	0.01
4	SLU 52	421	0	3150	-0.65	16.54	0.01
4	SLU 53	421	0	3150	-0.65	16.54	0.01
4	SLU 54	421	0	3150	-0.65	16.54	0.01
4	SLU 55	421	0	3150	-0.65	16.54	0.01
4	SLU 56	421	0	3150	-0.65	16.54	0.01
4	SLU 57	421	0	3150	-0.65	16.54	0.01
4	SLU 58	421	0	3150	-0.65	16.54	0.01
4	SLU 59	421	0	3150	-0.65	16.54	0.01
4	SLU 60	444	0	3309	-0.7	17.45	0.01
4	SLU 61	444	0	3309	-0.7	17.45	0.01
4	SLU 62	444	0	3309	-0.7	17.45	0.01
4	SLU 63	444	0	3309	-0.7	17.45	0.01
4	SLU 64	407	0	3010	-0.59	15.97	0.01
4	SLU 65	407	0	3010	-0.59	15.97	0.01
4	SLU 66	407	0	3010	-0.59	15.97	0.01
4	SLU 67	407	0	3010	-0.59	15.97	0.01
4	SLU 68	407	0	3010	-0.59	15.97	0.01
4	SLU 69	407	0	3010	-0.59	15.97	0.01
4	SLU 70	407	0	3010	-0.59	15.97	0.01
4	SLU 71	407	0	3010	-0.59	15.97	0.01
4	SLU 72	407	0	3010	-0.59	15.97	0.01
4	SLU 73	461	0	3381	-0.71	18.08	0.01
4	SLU 74	461	0	3381	-0.71	18.08	0.01
4	SLU 75	461	0	3381	-0.71	18.08	0.01
4	SLU 76	461	0	3381	-0.71	18.08	0.01
4	SLU 77	461	0	3381	-0.71	18.08	0.01
4	SLU 78	461	0	3381	-0.71	18.08	0.01
4	SLU 79	461	0	3381	-0.71	18.08	0.01
4	SLU 80	461	0	3381	-0.71	18.08	0.01
4	SLU 81	483	1	3541	-0.76	18.99	0.01
4	SLU 82	483	1	3541	-0.76	18.99	0.01
4	SLU 83	483	1	3541	-0.76	18.99	0.01
4	SLU 84	483	1	3541	-0.76	18.99	0.01
4	SLE RA 1	305	0	2264	-0.44	11.94	0.01
4	SLE RA 2	305	0	2264	-0.44	11.94	0.01
4	SLE RA 3	305	0	2264	-0.44	11.94	0.01
4	SLE RA 4	305	0	2264	-0.44	11.94	0.01
4	SLE RA 5	305	0	2264	-0.44	11.94	0.01
4	SLE RA 6	305	0	2264	-0.44	11.94	0.01
4	SLE RA 7	305	0	2264	-0.44	11.94	0.01
4	SLE RA 8	305	0	2264	-0.44	11.94	0.01
4	SLE RA 9	305	0	2264	-0.44	11.94	0.01
4	SLE RA 10	340	0	2512	-0.52	13.35	0.01
4	SLE RA 11	340	0	2512	-0.52	13.35	0.01
4	SLE RA 12	340	0	2512	-0.52	13.35	0.01
4	SLE RA 13	340	0	2512	-0.52	13.35	0.01
4	SLE RA 14	340	0	2512	-0.52	13.35	0.01
4	SLE RA 15	340	0	2512	-0.52	13.35	0.01
4	SLE RA 16	340	0	2512	-0.52	13.35	0.01
4	SLE RA 17	340	0	2512	-0.52	13.35	0.01
4	SLE RA 18	355	0	2618	-0.55	13.96	0.01
4	SLE RA 19	355	0	2618	-0.55	13.96	0.01
4	SLE RA 20	355	0	2618	-0.55	13.96	0.01
4	SLE RA 21	355	0	2618	-0.55	13.96	0.01
4	SLE FR 1	305	0	2264	-0.44	11.94	0.01
4	SLE FR 2	305	0	2264	-0.44	11.94	0.01
4	SLE FR 3	305	0	2264	-0.44	11.94	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
4	SLE FR 4	320	0	2371	-0.48	12.55	0.01
4	SLE FR 5	320	0	2371	-0.48	12.55	0.01
4	SLE FR 6	330	0	2441	-0.5	12.95	0.01
4	SLE QP 1	305	0	2264	-0.44	11.94	0.01
4	SLE QP 2	320	0	2371	-0.48	12.55	0.01
4	SLD 1	575	-18	2598	6.55	23.03	-0.02
4	SLD 2	575	-18	2598	6.55	23.03	-0.02
4	SLD 3	546	-11	2460	16.8	21.95	-0.05
4	SLD 4	546	-11	2460	16.8	21.95	-0.05
4	SLD 5	442	-15	2648	-13.92	17.33	0.04
4	SLD 6	442	-15	2648	-13.92	17.33	0.04
4	SLD 7	342	7	2188	20.26	13.73	-0.05
4	SLD 8	342	7	2188	20.26	13.73	-0.05
4	SLD 9	297	-6	2553	-21.21	11.36	0.06
4	SLD 10	297	-6	2553	-21.21	11.36	0.06
4	SLD 11	198	16	2093	12.97	7.77	-0.02
4	SLD 12	198	16	2093	12.97	7.77	-0.02
4	SLD 13	94	12	2282	-17.75	3.15	0.06
4	SLD 14	94	12	2282	-17.75	3.15	0.06
4	SLD 15	64	19	2143	-7.5	2.07	0.04
4	SLD 16	64	19	2143	-7.5	2.07	0.04
4	SLV 1	921	-45	2913	17.39	37.2	-0.07
4	SLV 2	921	-45	2913	17.39	37.2	-0.07
4	SLV 3	850	-29	2587	43.36	34.63	-0.13
4	SLV 4	850	-29	2587	43.36	34.63	-0.13
4	SLV 5	608	-37	3026	-34.49	23.84	0.08
4	SLV 6	608	-37	3026	-34.49	23.84	0.08
4	SLV 7	371	15	1942	52.05	15.27	-0.12
4	SLV 8	371	15	1942	52.05	15.27	-0.12
4	SLV 9	269	-15	2799	-53	9.82	0.14
4	SLV 10	269	-15	2799	-53	9.82	0.14
4	SLV 11	32	38	1715	33.54	1.26	-0.06
4	SLV 12	32	38	1715	33.54	1.26	-0.06
4	SLV 13	-210	30	2154	-44.31	-9.53	0.14
4	SLV 14	-210	30	2154	-44.31	-9.53	0.14
4	SLV 15	-281	45	1828	-18.35	-12.1	0.08
4	SLV 16	-281	45	1828	-18.35	-12.1	0.08
5	SLU 1	193	0	2129	-0.22	8.53	0
5	SLU 2	193	0	2129	-0.22	8.53	0
5	SLU 3	193	0	2129	-0.22	8.53	0
5	SLU 4	193	0	2129	-0.22	8.53	0
5	SLU 5	193	0	2129	-0.22	8.53	0
5	SLU 6	193	0	2129	-0.22	8.53	0
5	SLU 7	193	0	2129	-0.22	8.53	0
5	SLU 8	193	0	2129	-0.22	8.53	0
5	SLU 9	193	0	2129	-0.22	8.53	0
5	SLU 10	230	0	2485	-0.3	10.15	0
5	SLU 11	230	0	2485	-0.3	10.15	0
5	SLU 12	230	0	2485	-0.3	10.15	0
5	SLU 13	230	0	2485	-0.3	10.15	0
5	SLU 14	230	0	2485	-0.3	10.15	0
5	SLU 15	230	0	2485	-0.3	10.15	0
5	SLU 16	230	0	2485	-0.3	10.15	0
5	SLU 17	230	0	2485	-0.3	10.15	0
5	SLU 18	246	0	2638	-0.33	10.85	0
5	SLU 19	246	0	2638	-0.33	10.85	0
5	SLU 20	246	0	2638	-0.33	10.85	0
5	SLU 21	246	0	2638	-0.33	10.85	0
5	SLU 22	221	0	2354	-0.26	9.72	0
5	SLU 23	221	0	2354	-0.26	9.72	0
5	SLU 24	221	0	2354	-0.26	9.72	0
5	SLU 25	221	0	2354	-0.26	9.72	0
5	SLU 26	221	0	2354	-0.26	9.72	0
5	SLU 27	221	0	2354	-0.26	9.72	0
5	SLU 28	221	0	2354	-0.26	9.72	0
5	SLU 29	221	0	2354	-0.26	9.72	0
5	SLU 30	221	0	2354	-0.26	9.72	0
5	SLU 31	258	0	2711	-0.34	11.35	0
5	SLU 32	258	0	2711	-0.34	11.35	0
5	SLU 33	258	0	2711	-0.34	11.35	0
5	SLU 34	258	0	2711	-0.34	11.35	0
5	SLU 35	258	0	2711	-0.34	11.35	0
5	SLU 36	258	0	2711	-0.34	11.35	0
5	SLU 37	258	0	2711	-0.34	11.35	0
5	SLU 38	258	0	2711	-0.34	11.35	0
5	SLU 39	273	0	2864	-0.37	12.05	0
5	SLU 40	273	0	2864	-0.37	12.05	0
5	SLU 41	273	0	2864	-0.37	12.05	0
5	SLU 42	273	0	2864	-0.37	12.05	0
5	SLU 43	242	0	2691	-0.28	10.67	0
5	SLU 44	242	0	2691	-0.28	10.67	0
5	SLU 45	242	0	2691	-0.28	10.67	0
5	SLU 46	242	0	2691	-0.28	10.67	0
5	SLU 47	242	0	2691	-0.28	10.67	0
5	SLU 48	242	0	2691	-0.28	10.67	0
5	SLU 49	242	0	2691	-0.28	10.67	0
5	SLU 50	242	0	2691	-0.28	10.67	0
5	SLU 51	242	0	2691	-0.28	10.67	0
5	SLU 52	279	0	3047	-0.35	12.3	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
5	SLU 53	279	0	3047	-0.35	12.3	0
5	SLU 54	279	0	3047	-0.35	12.3	0
5	SLU 55	279	0	3047	-0.35	12.3	0
5	SLU 56	279	0	3047	-0.35	12.3	0
5	SLU 57	279	0	3047	-0.35	12.3	0
5	SLU 58	279	0	3047	-0.35	12.3	0
5	SLU 59	279	0	3047	-0.35	12.3	0
5	SLU 60	294	0	3200	-0.39	13	0
5	SLU 61	294	0	3200	-0.39	13	0
5	SLU 62	294	0	3200	-0.39	13	0
5	SLU 63	294	0	3200	-0.39	13	0
5	SLU 64	270	0	2916	-0.31	11.87	0
5	SLU 65	270	0	2916	-0.31	11.87	0
5	SLU 66	270	0	2916	-0.31	11.87	0
5	SLU 67	270	0	2916	-0.31	11.87	0
5	SLU 68	270	0	2916	-0.31	11.87	0
5	SLU 69	270	0	2916	-0.31	11.87	0
5	SLU 70	270	0	2916	-0.31	11.87	0
5	SLU 71	270	0	2916	-0.31	11.87	0
5	SLU 72	270	0	2916	-0.31	11.87	0
5	SLU 73	306	0	3272	-0.39	13.5	0
5	SLU 74	306	0	3272	-0.39	13.5	0
5	SLU 75	306	0	3272	-0.39	13.5	0
5	SLU 76	306	0	3272	-0.39	13.5	0
5	SLU 77	306	0	3272	-0.39	13.5	0
5	SLU 78	306	0	3272	-0.39	13.5	0
5	SLU 79	306	0	3272	-0.39	13.5	0
5	SLU 80	306	0	3272	-0.39	13.5	0
5	SLU 81	322	0	3425	-0.43	14.19	0
5	SLU 82	322	0	3425	-0.43	14.19	0
5	SLU 83	322	0	3425	-0.43	14.19	0
5	SLU 84	322	0	3425	-0.43	14.19	0
5	SLE RA 1	201	0	2193	-0.23	8.87	0
5	SLE RA 2	201	0	2193	-0.23	8.87	0
5	SLE RA 3	201	0	2193	-0.23	8.87	0
5	SLE RA 4	201	0	2193	-0.23	8.87	0
5	SLE RA 5	201	0	2193	-0.23	8.87	0
5	SLE RA 6	201	0	2193	-0.23	8.87	0
5	SLE RA 7	201	0	2193	-0.23	8.87	0
5	SLE RA 8	201	0	2193	-0.23	8.87	0
5	SLE RA 9	201	0	2193	-0.23	8.87	0
5	SLE RA 10	226	0	2431	-0.28	9.95	0
5	SLE RA 11	226	0	2431	-0.28	9.95	0
5	SLE RA 12	226	0	2431	-0.28	9.95	0
5	SLE RA 13	226	0	2431	-0.28	9.95	0
5	SLE RA 14	226	0	2431	-0.28	9.95	0
5	SLE RA 15	226	0	2431	-0.28	9.95	0
5	SLE RA 16	226	0	2431	-0.28	9.95	0
5	SLE RA 17	226	0	2431	-0.28	9.95	0
5	SLE RA 18	236	0	2533	-0.31	10.42	0
5	SLE RA 19	236	0	2533	-0.31	10.42	0
5	SLE RA 20	236	0	2533	-0.31	10.42	0
5	SLE RA 21	236	0	2533	-0.31	10.42	0
5	SLE FR 1	201	0	2193	-0.23	8.87	0
5	SLE FR 2	201	0	2193	-0.23	8.87	0
5	SLE FR 3	201	0	2193	-0.23	8.87	0
5	SLE FR 4	212	0	2295	-0.25	9.33	0
5	SLE FR 5	212	0	2295	-0.25	9.33	0
5	SLE FR 6	219	0	2363	-0.27	9.64	0
5	SLE QP 1	201	0	2193	-0.23	8.87	0
5	SLE QP 2	212	0	2295	-0.25	9.33	0
5	SLD 1	476	-12	2436	8.58	20.07	-0.04
5	SLD 2	476	-12	2436	8.58	20.07	-0.04
5	SLD 3	448	-24	2337	25.32	18.98	-0.09
5	SLD 4	448	-24	2337	25.32	18.98	-0.09
5	SLD 5	334	15	2487	-23	14.22	0.06
5	SLD 6	334	15	2487	-23	14.22	0.06
5	SLD 7	240	-25	2158	32.81	10.56	-0.1
5	SLD 8	240	-25	2158	32.81	10.56	-0.1
5	SLD 9	184	25	2433	-33.32	8.1	0.1
5	SLD 10	184	25	2433	-33.32	8.1	0.1
5	SLD 11	90	-15	2103	22.49	4.45	-0.06
5	SLD 12	90	-15	2103	22.49	4.45	-0.06
5	SLD 13	-24	24	2254	-25.83	-0.31	0.09
5	SLD 14	-24	24	2254	-25.83	-0.31	0.09
5	SLD 15	-52	12	2155	-9.08	-1.41	0.04
5	SLD 16	-52	12	2155	-9.08	-1.41	0.04
5	SLV 1	833	-30	2634	22.39	34.58	-0.1
5	SLV 2	833	-30	2634	22.39	34.58	-0.1
5	SLV 3	765	-59	2401	64.91	31.97	-0.22
5	SLV 4	765	-59	2401	64.91	31.97	-0.22
5	SLV 5	501	36	2750	-57.95	20.87	0.15
5	SLV 6	501	36	2750	-57.95	20.87	0.15
5	SLV 7	275	-62	1975	83.79	12.17	-0.24
5	SLV 8	275	-62	1975	83.79	12.17	-0.24
5	SLV 9	148	62	2616	-84.3	6.5	0.24
5	SLV 10	148	62	2616	-84.3	6.5	0.24
5	SLV 11	-77	-35	1841	57.44	-2.2	-0.15
5	SLV 12	-77	-35	1841	57.44	-2.2	-0.15



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
5	SLV 13	-342	59	2189	-65.42	-13.31	0.22
5	SLV 14	-342	59	2189	-65.42	-13.31	0.22
5	SLV 15	-409	30	1957	-22.9	-15.92	0.1
5	SLV 16	-409	30	1957	-22.9	-15.92	0.1
6	SLU 1	90	0	2004	-0.14	3.49	0
6	SLU 2	90	0	2004	-0.14	3.49	0
6	SLU 3	90	0	2004	-0.14	3.49	0
6	SLU 4	90	0	2004	-0.14	3.49	0
6	SLU 5	90	0	2004	-0.14	3.49	0
6	SLU 6	90	0	2004	-0.14	3.49	0
6	SLU 7	90	0	2004	-0.14	3.49	0
6	SLU 8	90	0	2004	-0.14	3.49	0
6	SLU 9	90	0	2004	-0.14	3.49	0
6	SLU 10	108	0	2336	-0.21	4.17	0
6	SLU 11	108	0	2336	-0.21	4.17	0
6	SLU 12	108	0	2336	-0.21	4.17	0
6	SLU 13	108	0	2336	-0.21	4.17	0
6	SLU 14	108	0	2336	-0.21	4.17	0
6	SLU 15	108	0	2336	-0.21	4.17	0
6	SLU 16	108	0	2336	-0.21	4.17	0
6	SLU 17	108	0	2336	-0.21	4.17	0
6	SLU 18	116	0	2478	-0.24	4.47	0
6	SLU 19	116	0	2478	-0.24	4.47	0
6	SLU 20	116	0	2478	-0.24	4.47	0
6	SLU 21	116	0	2478	-0.24	4.47	0
6	SLU 22	105	0	2216	-0.17	4.04	0
6	SLU 23	105	0	2216	-0.17	4.04	0
6	SLU 24	105	0	2216	-0.17	4.04	0
6	SLU 25	105	0	2216	-0.17	4.04	0
6	SLU 26	105	0	2216	-0.17	4.04	0
6	SLU 27	105	0	2216	-0.17	4.04	0
6	SLU 28	105	0	2216	-0.17	4.04	0
6	SLU 29	105	0	2216	-0.17	4.04	0
6	SLU 30	105	0	2216	-0.17	4.04	0
6	SLU 31	123	0	2548	-0.24	4.72	0
6	SLU 32	123	0	2548	-0.24	4.72	0
6	SLU 33	123	0	2548	-0.24	4.72	0
6	SLU 34	123	0	2548	-0.24	4.72	0
6	SLU 35	123	0	2548	-0.24	4.72	0
6	SLU 36	123	0	2548	-0.24	4.72	0
6	SLU 37	123	0	2548	-0.24	4.72	0
6	SLU 38	123	0	2548	-0.24	4.72	0
6	SLU 39	131	0	2690	-0.27	5.02	0
6	SLU 40	131	0	2690	-0.27	5.02	0
6	SLU 41	131	0	2690	-0.27	5.02	0
6	SLU 42	131	0	2690	-0.27	5.02	0
6	SLU 43	112	0	2533	-0.17	4.34	0
6	SLU 44	112	0	2533	-0.17	4.34	0
6	SLU 45	112	0	2533	-0.17	4.34	0
6	SLU 46	112	0	2533	-0.17	4.34	0
6	SLU 47	112	0	2533	-0.17	4.34	0
6	SLU 48	112	0	2533	-0.17	4.34	0
6	SLU 49	112	0	2533	-0.17	4.34	0
6	SLU 50	112	0	2533	-0.17	4.34	0
6	SLU 51	112	0	2533	-0.17	4.34	0
6	SLU 52	130	0	2865	-0.24	5.03	0
6	SLU 53	130	0	2865	-0.24	5.03	0
6	SLU 54	130	0	2865	-0.24	5.03	0
6	SLU 55	130	0	2865	-0.24	5.03	0
6	SLU 56	130	0	2865	-0.24	5.03	0
6	SLU 57	130	0	2865	-0.24	5.03	0
6	SLU 58	130	0	2865	-0.24	5.03	0
6	SLU 59	130	0	2865	-0.24	5.03	0
6	SLU 60	138	0	3007	-0.27	5.32	0
6	SLU 61	138	0	3007	-0.27	5.32	0
6	SLU 62	138	0	3007	-0.27	5.32	0
6	SLU 63	138	0	3007	-0.27	5.32	0
6	SLU 64	127	0	2745	-0.2	4.89	0
6	SLU 65	127	0	2745	-0.2	4.89	0
6	SLU 66	127	0	2745	-0.2	4.89	0
6	SLU 67	127	0	2745	-0.2	4.89	0
6	SLU 68	127	0	2745	-0.2	4.89	0
6	SLU 69	127	0	2745	-0.2	4.89	0
6	SLU 70	127	0	2745	-0.2	4.89	0
6	SLU 71	127	0	2745	-0.2	4.89	0
6	SLU 72	127	0	2745	-0.2	4.89	0
6	SLU 73	145	0	3077	-0.27	5.58	0
6	SLU 74	145	0	3077	-0.27	5.58	0
6	SLU 75	145	0	3077	-0.27	5.58	0
6	SLU 76	145	0	3077	-0.27	5.58	0
6	SLU 77	145	0	3077	-0.27	5.58	0
6	SLU 78	145	0	3077	-0.27	5.58	0
6	SLU 79	145	0	3077	-0.27	5.58	0
6	SLU 80	145	0	3077	-0.27	5.58	0
6	SLU 81	153	0	3219	-0.3	5.87	0
6	SLU 82	153	0	3219	-0.3	5.87	0
6	SLU 83	153	0	3219	-0.3	5.87	0
6	SLU 84	153	0	3219	-0.3	5.87	0
6	SLE RA 1	94	0	2065	-0.15	3.64	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
6	SLE RA 2	94	0	2065	-0.15	3.64	0
6	SLE RA 3	94	0	2065	-0.15	3.64	0
6	SLE RA 4	94	0	2065	-0.15	3.64	0
6	SLE RA 5	94	0	2065	-0.15	3.64	0
6	SLE RA 6	94	0	2065	-0.15	3.64	0
6	SLE RA 7	94	0	2065	-0.15	3.64	0
6	SLE RA 8	94	0	2065	-0.15	3.64	0
6	SLE RA 9	94	0	2065	-0.15	3.64	0
6	SLE RA 10	107	0	2286	-0.19	4.1	0
6	SLE RA 11	107	0	2286	-0.19	4.1	0
6	SLE RA 12	107	0	2286	-0.19	4.1	0
6	SLE RA 13	107	0	2286	-0.19	4.1	0
6	SLE RA 14	107	0	2286	-0.19	4.1	0
6	SLE RA 15	107	0	2286	-0.19	4.1	0
6	SLE RA 16	107	0	2286	-0.19	4.1	0
6	SLE RA 17	107	0	2286	-0.19	4.1	0
6	SLE RA 18	112	0	2381	-0.21	4.3	0
6	SLE RA 19	112	0	2381	-0.21	4.3	0
6	SLE RA 20	112	0	2381	-0.21	4.3	0
6	SLE RA 21	112	0	2381	-0.21	4.3	0
6	SLE FR 1	94	0	2065	-0.15	3.64	0
6	SLE FR 2	94	0	2065	-0.15	3.64	0
6	SLE FR 3	94	0	2065	-0.15	3.64	0
6	SLE FR 4	100	0	2160	-0.17	3.84	0
6	SLE FR 5	100	0	2160	-0.17	3.84	0
6	SLE FR 6	103	0	2223	-0.18	3.97	0
6	SLE QP 1	94	0	2065	-0.15	3.64	0
6	SLE QP 2	100	0	2160	-0.17	3.84	0
6	SLD 1	373	-13	2135	9.62	14.27	-0.07
6	SLD 2	373	-13	2135	9.62	14.27	-0.07
6	SLD 3	344	-30	2064	32.99	13.22	-0.16
6	SLD 4	344	-30	2064	32.99	13.22	-0.16
6	SLD 5	225	23	2259	-32.67	8.57	0.12
6	SLD 6	225	23	2259	-32.67	8.57	0.12
6	SLD 7	130	-35	2024	45.22	5.05	-0.19
6	SLD 8	130	-35	2024	45.22	5.05	-0.19
6	SLD 9	70	36	2296	-45.56	2.63	0.19
6	SLD 10	70	36	2296	-45.56	2.63	0.19
6	SLD 11	-26	-22	2060	32.34	-0.89	-0.12
6	SLD 12	-26	-22	2060	32.34	-0.89	-0.12
6	SLD 13	-145	30	2255	-33.33	-5.54	0.16
6	SLD 14	-145	30	2255	-33.33	-5.54	0.16
6	SLD 15	-173	13	2185	-9.96	-6.59	0.07
6	SLD 16	-173	13	2185	-9.96	-6.59	0.07
6	SLV 1	742	-33	2093	25.03	28.38	-0.17
6	SLV 2	742	-33	2093	25.03	28.38	-0.17
6	SLV 3	673	-77	1927	84.56	25.86	-0.41
6	SLV 4	673	-77	1927	84.56	25.86	-0.41
6	SLV 5	396	56	2392	-82.9	15.02	0.3
6	SLV 6	396	56	2392	-82.9	15.02	0.3
6	SLV 7	168	-89	1837	115.54	6.63	-0.47
6	SLV 8	168	-89	1837	115.54	6.63	-0.47
6	SLV 9	31	89	2482	-115.87	1.05	0.48
6	SLV 10	31	89	2482	-115.87	1.05	0.48
6	SLV 11	-196	-56	1927	82.56	-7.34	-0.3
6	SLV 12	-196	-56	1927	82.56	-7.34	-0.3
6	SLV 13	-474	77	2392	-84.9	-18.18	0.41
6	SLV 14	-474	77	2392	-84.9	-18.18	0.41
6	SLV 15	-542	33	2226	-25.37	-20.7	0.17
6	SLV 16	-542	33	2226	-25.37	-20.7	0.17
7	SLU 1	66	0	1843	-0.09	3.3	0
7	SLU 2	66	0	1843	-0.09	3.3	0
7	SLU 3	66	0	1843	-0.09	3.3	0
7	SLU 4	66	0	1843	-0.09	3.3	0
7	SLU 5	66	0	1843	-0.09	3.3	0
7	SLU 6	66	0	1843	-0.09	3.3	0
7	SLU 7	66	0	1843	-0.09	3.3	0
7	SLU 8	66	0	1843	-0.09	3.3	0
7	SLU 9	66	0	1843	-0.09	3.3	0
7	SLU 10	83	0	2144	-0.16	4.08	0
7	SLU 11	83	0	2144	-0.16	4.08	0
7	SLU 12	83	0	2144	-0.16	4.08	0
7	SLU 13	83	0	2144	-0.16	4.08	0
7	SLU 14	83	0	2144	-0.16	4.08	0
7	SLU 15	83	0	2144	-0.16	4.08	0
7	SLU 16	83	0	2144	-0.16	4.08	0
7	SLU 17	83	0	2144	-0.16	4.08	0
7	SLU 18	90	0	2273	-0.19	4.41	0
7	SLU 19	90	0	2273	-0.19	4.41	0
7	SLU 20	90	0	2273	-0.19	4.41	0
7	SLU 21	90	0	2273	-0.19	4.41	0
7	SLU 22	78	0	2036	-0.12	3.85	0
7	SLU 23	78	0	2036	-0.12	3.85	0
7	SLU 24	78	0	2036	-0.12	3.85	0
7	SLU 25	78	0	2036	-0.12	3.85	0
7	SLU 26	78	0	2036	-0.12	3.85	0
7	SLU 27	78	0	2036	-0.12	3.85	0
7	SLU 28	78	0	2036	-0.12	3.85	0
7	SLU 29	78	0	2036	-0.12	3.85	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
7	SLU 30	78	0	2036	-0.12	3.85	0
7	SLU 31	95	0	2337	-0.19	4.63	0
7	SLU 32	95	0	2337	-0.19	4.63	0
7	SLU 33	95	0	2337	-0.19	4.63	0
7	SLU 34	95	0	2337	-0.19	4.63	0
7	SLU 35	95	0	2337	-0.19	4.63	0
7	SLU 36	95	0	2337	-0.19	4.63	0
7	SLU 37	95	0	2337	-0.19	4.63	0
7	SLU 38	95	0	2337	-0.19	4.63	0
7	SLU 39	102	0	2466	-0.21	4.96	0
7	SLU 40	102	0	2466	-0.21	4.96	0
7	SLU 41	102	0	2466	-0.21	4.96	0
7	SLU 42	102	0	2466	-0.21	4.96	0
7	SLU 43	82	0	2329	-0.11	4.1	0
7	SLU 44	82	0	2329	-0.11	4.1	0
7	SLU 45	82	0	2329	-0.11	4.1	0
7	SLU 46	82	0	2329	-0.11	4.1	0
7	SLU 47	82	0	2329	-0.11	4.1	0
7	SLU 48	82	0	2329	-0.11	4.1	0
7	SLU 49	82	0	2329	-0.11	4.1	0
7	SLU 50	82	0	2329	-0.11	4.1	0
7	SLU 51	82	0	2329	-0.11	4.1	0
7	SLU 52	98	0	2630	-0.18	4.88	0
7	SLU 53	98	0	2630	-0.18	4.88	0
7	SLU 54	98	0	2630	-0.18	4.88	0
7	SLU 55	98	0	2630	-0.18	4.88	0
7	SLU 56	98	0	2630	-0.18	4.88	0
7	SLU 57	98	0	2630	-0.18	4.88	0
7	SLU 58	98	0	2630	-0.18	4.88	0
7	SLU 59	98	0	2630	-0.18	4.88	0
7	SLU 60	105	0	2759	-0.21	5.21	0
7	SLU 61	105	0	2759	-0.21	5.21	0
7	SLU 62	105	0	2759	-0.21	5.21	0
7	SLU 63	105	0	2759	-0.21	5.21	0
7	SLU 64	94	0	2523	-0.14	4.65	0
7	SLU 65	94	0	2523	-0.14	4.65	0
7	SLU 66	94	0	2523	-0.14	4.65	0
7	SLU 67	94	0	2523	-0.14	4.65	0
7	SLU 68	94	0	2523	-0.14	4.65	0
7	SLU 69	94	0	2523	-0.14	4.65	0
7	SLU 70	94	0	2523	-0.14	4.65	0
7	SLU 71	94	0	2523	-0.14	4.65	0
7	SLU 72	94	0	2523	-0.14	4.65	0
7	SLU 73	110	0	2824	-0.2	5.43	0
7	SLU 74	110	0	2824	-0.2	5.43	0
7	SLU 75	110	0	2824	-0.2	5.43	0
7	SLU 76	110	0	2824	-0.2	5.43	0
7	SLU 77	110	0	2824	-0.2	5.43	0
7	SLU 78	110	0	2824	-0.2	5.43	0
7	SLU 79	110	0	2824	-0.2	5.43	0
7	SLU 80	110	0	2824	-0.2	5.43	0
7	SLU 81	117	0	2953	-0.23	5.76	0
7	SLU 82	117	0	2953	-0.23	5.76	0
7	SLU 83	117	0	2953	-0.23	5.76	0
7	SLU 84	117	0	2953	-0.23	5.76	0
7	SLE RA 1	70	0	1898	-0.1	3.46	0
7	SLE RA 2	70	0	1898	-0.1	3.46	0
7	SLE RA 3	70	0	1898	-0.1	3.46	0
7	SLE RA 4	70	0	1898	-0.1	3.46	0
7	SLE RA 5	70	0	1898	-0.1	3.46	0
7	SLE RA 6	70	0	1898	-0.1	3.46	0
7	SLE RA 7	70	0	1898	-0.1	3.46	0
7	SLE RA 8	70	0	1898	-0.1	3.46	0
7	SLE RA 9	70	0	1898	-0.1	3.46	0
7	SLE RA 10	80	0	2099	-0.14	3.98	0
7	SLE RA 11	80	0	2099	-0.14	3.98	0
7	SLE RA 12	80	0	2099	-0.14	3.98	0
7	SLE RA 13	80	0	2099	-0.14	3.98	0
7	SLE RA 14	80	0	2099	-0.14	3.98	0
7	SLE RA 15	80	0	2099	-0.14	3.98	0
7	SLE RA 16	80	0	2099	-0.14	3.98	0
7	SLE RA 17	80	0	2099	-0.14	3.98	0
7	SLE RA 18	85	0	2185	-0.16	4.2	0
7	SLE RA 19	85	0	2185	-0.16	4.2	0
7	SLE RA 20	85	0	2185	-0.16	4.2	0
7	SLE RA 21	85	0	2185	-0.16	4.2	0
7	SLE FR 1	70	0	1898	-0.1	3.46	0
7	SLE FR 2	70	0	1898	-0.1	3.46	0
7	SLE FR 3	70	0	1898	-0.1	3.46	0
7	SLE FR 4	74	0	1984	-0.12	3.68	0
7	SLE FR 5	74	0	1984	-0.12	3.68	0
7	SLE FR 6	77	0	2041	-0.13	3.83	0
7	SLE QP 1	70	0	1898	-0.1	3.46	0
7	SLE QP 2	74	0	1984	-0.12	3.68	0
7	SLD 1	376	-14	1961	9.49	15.43	-0.11
7	SLD 2	376	-14	1961	9.49	15.43	-0.11
7	SLD 3	345	-36	1910	39.13	14.25	-0.26
7	SLD 4	345	-36	1910	39.13	14.25	-0.26
7	SLD 5	212	28	2054	-42.19	9	0.21



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
7	SLD 6	212	28	2054	-42.19	9	0.21
7	SLD 7	108	-43	1884	56.61	5.05	-0.32
7	SLD 8	108	-43	1884	56.61	5.05	-0.32
7	SLD 9	40	43	2083	-56.85	2.31	0.32
7	SLD 10	40	43	2083	-56.85	2.31	0.32
7	SLD 11	-63	-28	1913	41.95	-1.64	-0.21
7	SLD 12	-63	-28	1913	41.95	-1.64	-0.21
7	SLD 13	-196	36	2058	-39.37	-6.88	0.26
7	SLD 14	-196	36	2058	-39.37	-6.88	0.26
7	SLD 15	-227	14	2007	-9.73	-8.07	0.11
7	SLD 16	-227	14	2007	-9.73	-8.07	0.11
7	SLV 1	784	-37	1925	24.66	31.32	-0.27
7	SLV 2	784	-37	1925	24.66	31.32	-0.27
7	SLV 3	710	-91	1804	100.34	28.49	-0.67
7	SLV 4	710	-91	1804	100.34	28.49	-0.67
7	SLV 5	400	71	2149	-107.47	16.28	0.52
7	SLV 6	400	71	2149	-107.47	16.28	0.52
7	SLV 7	152	-109	1747	144.8	6.82	-0.8
7	SLV 8	152	-109	1747	144.8	6.82	-0.8
7	SLV 9	-4	109	2221	-145.04	0.54	0.8
7	SLV 10	-4	109	2221	-145.04	0.54	0.8
7	SLV 11	-251	-71	1818	107.23	-8.92	-0.52
7	SLV 12	-251	-71	1818	107.23	-8.92	-0.52
7	SLV 13	-561	91	2163	-100.58	-21.12	0.67
7	SLV 14	-561	91	2163	-100.58	-21.12	0.67
7	SLV 15	-635	37	2043	-24.9	-23.96	0.27
7	SLV 16	-635	37	2043	-24.9	-23.96	0.27
8	SLU 1	98	0	1737	-0.06	3.43	0
8	SLU 2	98	0	1737	-0.06	3.43	0
8	SLU 3	98	0	1737	-0.06	3.43	0
8	SLU 4	98	0	1737	-0.06	3.43	0
8	SLU 5	98	0	1737	-0.06	3.43	0
8	SLU 6	98	0	1737	-0.06	3.43	0
8	SLU 7	98	0	1737	-0.06	3.43	0
8	SLU 8	98	0	1737	-0.06	3.43	0
8	SLU 9	98	0	1737	-0.06	3.43	0
8	SLU 10	124	0	2022	-0.12	4.32	0
8	SLU 11	124	0	2022	-0.12	4.32	0
8	SLU 12	124	0	2022	-0.12	4.32	0
8	SLU 13	124	0	2022	-0.12	4.32	0
8	SLU 14	124	0	2022	-0.12	4.32	0
8	SLU 15	124	0	2022	-0.12	4.32	0
8	SLU 16	124	0	2022	-0.12	4.32	0
8	SLU 17	124	0	2022	-0.12	4.32	0
8	SLU 18	135	0	2144	-0.14	4.71	0
8	SLU 19	135	0	2144	-0.14	4.71	0
8	SLU 20	135	0	2144	-0.14	4.71	0
8	SLU 21	135	0	2144	-0.14	4.71	0
8	SLU 22	115	0	1920	-0.08	4.01	0
8	SLU 23	115	0	1920	-0.08	4.01	0
8	SLU 24	115	0	1920	-0.08	4.01	0
8	SLU 25	115	0	1920	-0.08	4.01	0
8	SLU 26	115	0	1920	-0.08	4.01	0
8	SLU 27	115	0	1920	-0.08	4.01	0
8	SLU 28	115	0	1920	-0.08	4.01	0
8	SLU 29	115	0	1920	-0.08	4.01	0
8	SLU 30	115	0	1920	-0.08	4.01	0
8	SLU 31	141	0	2205	-0.14	4.9	0
8	SLU 32	141	0	2205	-0.14	4.9	0
8	SLU 33	141	0	2205	-0.14	4.9	0
8	SLU 34	141	0	2205	-0.14	4.9	0
8	SLU 35	141	0	2205	-0.14	4.9	0
8	SLU 36	141	0	2205	-0.14	4.9	0
8	SLU 37	141	0	2205	-0.14	4.9	0
8	SLU 38	141	0	2205	-0.14	4.9	0
8	SLU 39	152	0	2327	-0.16	5.29	0
8	SLU 40	152	0	2327	-0.16	5.29	0
8	SLU 41	152	0	2327	-0.16	5.29	0
8	SLU 42	152	0	2327	-0.16	5.29	0
8	SLU 43	121	0	2195	-0.07	4.26	0
8	SLU 44	121	0	2195	-0.07	4.26	0
8	SLU 45	121	0	2195	-0.07	4.26	0
8	SLU 46	121	0	2195	-0.07	4.26	0
8	SLU 47	121	0	2195	-0.07	4.26	0
8	SLU 48	121	0	2195	-0.07	4.26	0
8	SLU 49	121	0	2195	-0.07	4.26	0
8	SLU 50	121	0	2195	-0.07	4.26	0
8	SLU 51	121	0	2195	-0.07	4.26	0
8	SLU 52	147	0	2480	-0.13	5.15	0
8	SLU 53	147	0	2480	-0.13	5.15	0
8	SLU 54	147	0	2480	-0.13	5.15	0
8	SLU 55	147	0	2480	-0.13	5.15	0
8	SLU 56	147	0	2480	-0.13	5.15	0
8	SLU 57	147	0	2480	-0.13	5.15	0
8	SLU 58	147	0	2480	-0.13	5.15	0
8	SLU 59	147	0	2480	-0.13	5.15	0
8	SLU 60	158	0	2602	-0.15	5.53	0
8	SLU 61	158	0	2602	-0.15	5.53	0
8	SLU 62	158	0	2602	-0.15	5.53	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
8	SLU 63	158	0	2602	-0.15	5.53	0
8	SLU 64	138	0	2378	-0.09	4.84	0
8	SLU 65	138	0	2378	-0.09	4.84	0
8	SLU 66	138	0	2378	-0.09	4.84	0
8	SLU 67	138	0	2378	-0.09	4.84	0
8	SLU 68	138	0	2378	-0.09	4.84	0
8	SLU 69	138	0	2378	-0.09	4.84	0
8	SLU 70	138	0	2378	-0.09	4.84	0
8	SLU 71	138	0	2378	-0.09	4.84	0
8	SLU 72	138	0	2378	-0.09	4.84	0
8	SLU 73	164	0	2663	-0.15	5.73	0
8	SLU 74	164	0	2663	-0.15	5.73	0
8	SLU 75	164	0	2663	-0.15	5.73	0
8	SLU 76	164	0	2663	-0.15	5.73	0
8	SLU 77	164	0	2663	-0.15	5.73	0
8	SLU 78	164	0	2663	-0.15	5.73	0
8	SLU 79	164	0	2663	-0.15	5.73	0
8	SLU 80	164	0	2663	-0.15	5.73	0
8	SLU 81	175	0	2785	-0.17	6.12	0
8	SLU 82	175	0	2785	-0.17	6.12	0
8	SLU 83	175	0	2785	-0.17	6.12	0
8	SLU 84	175	0	2785	-0.17	6.12	0
8	SLE RA 1	103	0	1789	-0.07	3.59	0
8	SLE RA 2	103	0	1789	-0.07	3.59	0
8	SLE RA 3	103	0	1789	-0.07	3.59	0
8	SLE RA 4	103	0	1789	-0.07	3.59	0
8	SLE RA 5	103	0	1789	-0.07	3.59	0
8	SLE RA 6	103	0	1789	-0.07	3.59	0
8	SLE RA 7	103	0	1789	-0.07	3.59	0
8	SLE RA 8	103	0	1789	-0.07	3.59	0
8	SLE RA 9	103	0	1789	-0.07	3.59	0
8	SLE RA 10	120	0	1979	-0.1	4.19	0
8	SLE RA 11	120	0	1979	-0.1	4.19	0
8	SLE RA 12	120	0	1979	-0.1	4.19	0
8	SLE RA 13	120	0	1979	-0.1	4.19	0
8	SLE RA 14	120	0	1979	-0.1	4.19	0
8	SLE RA 15	120	0	1979	-0.1	4.19	0
8	SLE RA 16	120	0	1979	-0.1	4.19	0
8	SLE RA 17	120	0	1979	-0.1	4.19	0
8	SLE RA 18	127	0	2060	-0.12	4.45	0
8	SLE RA 19	127	0	2060	-0.12	4.45	0
8	SLE RA 20	127	0	2060	-0.12	4.45	0
8	SLE RA 21	127	0	2060	-0.12	4.45	0
8	SLE FR 1	103	0	1789	-0.07	3.59	0
8	SLE FR 2	103	0	1789	-0.07	3.59	0
8	SLE FR 3	103	0	1789	-0.07	3.59	0
8	SLE FR 4	110	0	1870	-0.08	3.85	0
8	SLE FR 5	110	0	1870	-0.08	3.85	0
8	SLE FR 6	115	0	1925	-0.09	4.02	0
8	SLE QP 1	103	0	1789	-0.07	3.59	0
8	SLE QP 2	110	0	1870	-0.08	3.85	0
8	SLD 1	425	-15	1860	7.73	15.6	-0.12
8	SLD 2	425	-15	1860	7.73	15.6	-0.12
8	SLD 3	392	-38	1819	43.3	14.39	-0.32
8	SLD 4	392	-38	1819	43.3	14.39	-0.32
8	SLD 5	255	32	1930	-51.69	9.21	0.27
8	SLD 6	255	32	1930	-51.69	9.21	0.27
8	SLD 7	144	-47	1792	66.89	5.18	-0.4
8	SLD 8	144	-47	1792	66.89	5.18	-0.4
8	SLD 9	76	47	1949	-67.05	2.52	0.4
8	SLD 10	76	47	1949	-67.05	2.52	0.4
8	SLD 11	-35	-31	1811	51.53	-1.51	-0.27
8	SLD 12	-35	-31	1811	51.53	-1.51	-0.27
8	SLD 13	-172	38	1922	-43.47	-6.69	0.32
8	SLD 14	-172	38	1922	-43.47	-6.69	0.32
8	SLD 15	-205	15	1881	-7.89	-7.9	0.12
8	SLD 16	-205	15	1881	-7.89	-7.9	0.12
8	SLV 1	852	-38	1844	20.04	31.51	-0.31
8	SLV 2	852	-38	1844	20.04	31.51	-0.31
8	SLV 3	772	-98	1744	111.03	28.6	-0.82
8	SLV 4	772	-98	1744	111.03	28.6	-0.82
8	SLV 5	455	80	2015	-132.05	16.56	0.68
8	SLV 6	455	80	2015	-132.05	16.56	0.68
8	SLV 7	187	-120	1680	171.26	6.86	-1.02
8	SLV 8	187	-120	1680	171.26	6.86	-1.02
8	SLV 9	33	120	2061	-171.42	0.84	1.02
8	SLV 10	33	120	2061	-171.42	0.84	1.02
8	SLV 11	-235	-79	1726	131.89	-8.86	-0.68
8	SLV 12	-235	-79	1726	131.89	-8.86	-0.68
8	SLV 13	-552	98	1997	-111.19	-20.9	0.82
8	SLV 14	-552	98	1997	-111.19	-20.9	0.82
8	SLV 15	-633	38	1897	-20.2	-23.81	0.31
8	SLV 16	-633	38	1897	-20.2	-23.81	0.31
9	SLU 1	187	0	1770	-0.02	7.58	0
9	SLU 2	187	0	1770	-0.02	7.58	0
9	SLU 3	187	0	1770	-0.02	7.58	0
9	SLU 4	187	0	1770	-0.02	7.58	0
9	SLU 5	187	0	1770	-0.02	7.58	0
9	SLU 6	187	0	1770	-0.02	7.58	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
9	SLU 7	187	0	1770	-0.02	7.58	0
9	SLU 8	187	0	1770	-0.02	7.58	0
9	SLU 9	187	0	1770	-0.02	7.58	0
9	SLU 10	234	0	2070	-0.06	9.45	0
9	SLU 11	234	0	2070	-0.06	9.45	0
9	SLU 12	234	0	2070	-0.06	9.45	0
9	SLU 13	234	0	2070	-0.06	9.45	0
9	SLU 14	234	0	2070	-0.06	9.45	0
9	SLU 15	234	0	2070	-0.06	9.45	0
9	SLU 16	234	0	2070	-0.06	9.45	0
9	SLU 17	234	0	2070	-0.06	9.45	0
9	SLU 18	254	0	2198	-0.07	10.25	0
9	SLU 19	254	0	2198	-0.07	10.25	0
9	SLU 20	254	0	2198	-0.07	10.25	0
9	SLU 21	254	0	2198	-0.07	10.25	0
9	SLU 22	216	0	1962	-0.03	8.74	0
9	SLU 23	216	0	1962	-0.03	8.74	0
9	SLU 24	216	0	1962	-0.03	8.74	0
9	SLU 25	216	0	1962	-0.03	8.74	0
9	SLU 26	216	0	1962	-0.03	8.74	0
9	SLU 27	216	0	1962	-0.03	8.74	0
9	SLU 28	216	0	1962	-0.03	8.74	0
9	SLU 29	216	0	1962	-0.03	8.74	0
9	SLU 30	216	0	1962	-0.03	8.74	0
9	SLU 31	263	0	2261	-0.07	10.61	0
9	SLU 32	263	0	2261	-0.07	10.61	0
9	SLU 33	263	0	2261	-0.07	10.61	0
9	SLU 34	263	0	2261	-0.07	10.61	0
9	SLU 35	263	0	2261	-0.07	10.61	0
9	SLU 36	263	0	2261	-0.07	10.61	0
9	SLU 37	263	0	2261	-0.07	10.61	0
9	SLU 38	263	0	2261	-0.07	10.61	0
9	SLU 39	284	0	2390	-0.09	11.41	0
9	SLU 40	284	0	2390	-0.09	11.41	0
9	SLU 41	284	0	2390	-0.09	11.41	0
9	SLU 42	284	0	2390	-0.09	11.41	0
9	SLU 43	233	0	2235	-0.02	9.46	0
9	SLU 44	233	0	2235	-0.02	9.46	0
9	SLU 45	233	0	2235	-0.02	9.46	0
9	SLU 46	233	0	2235	-0.02	9.46	0
9	SLU 47	233	0	2235	-0.02	9.46	0
9	SLU 48	233	0	2235	-0.02	9.46	0
9	SLU 49	233	0	2235	-0.02	9.46	0
9	SLU 50	233	0	2235	-0.02	9.46	0
9	SLU 51	233	0	2235	-0.02	9.46	0
9	SLU 52	280	0	2535	-0.06	11.33	0
9	SLU 53	280	0	2535	-0.06	11.33	0
9	SLU 54	280	0	2535	-0.06	11.33	0
9	SLU 55	280	0	2535	-0.06	11.33	0
9	SLU 56	280	0	2535	-0.06	11.33	0
9	SLU 57	280	0	2535	-0.06	11.33	0
9	SLU 58	280	0	2535	-0.06	11.33	0
9	SLU 59	280	0	2535	-0.06	11.33	0
9	SLU 60	300	0	2664	-0.08	12.13	0
9	SLU 61	300	0	2664	-0.08	12.13	0
9	SLU 62	300	0	2664	-0.08	12.13	0
9	SLU 63	300	0	2664	-0.08	12.13	0
9	SLU 64	262	0	2427	-0.04	10.62	0
9	SLU 65	262	0	2427	-0.04	10.62	0
9	SLU 66	262	0	2427	-0.04	10.62	0
9	SLU 67	262	0	2427	-0.04	10.62	0
9	SLU 68	262	0	2427	-0.04	10.62	0
9	SLU 69	262	0	2427	-0.04	10.62	0
9	SLU 70	262	0	2427	-0.04	10.62	0
9	SLU 71	262	0	2427	-0.04	10.62	0
9	SLU 72	262	0	2427	-0.04	10.62	0
9	SLU 73	309	0	2727	-0.07	12.49	0
9	SLU 74	309	0	2727	-0.07	12.49	0
9	SLU 75	309	0	2727	-0.07	12.49	0
9	SLU 76	309	0	2727	-0.07	12.49	0
9	SLU 77	309	0	2727	-0.07	12.49	0
9	SLU 78	309	0	2727	-0.07	12.49	0
9	SLU 79	309	0	2727	-0.07	12.49	0
9	SLU 80	309	0	2727	-0.07	12.49	0
9	SLU 81	330	0	2855	-0.09	13.29	0
9	SLU 82	330	0	2855	-0.09	13.29	0
9	SLU 83	330	0	2855	-0.09	13.29	0
9	SLU 84	330	0	2855	-0.09	13.29	0
9	SLE RA 1	195	0	1825	-0.03	7.91	0
9	SLE RA 2	195	0	1825	-0.03	7.91	0
9	SLE RA 3	195	0	1825	-0.03	7.91	0
9	SLE RA 4	195	0	1825	-0.03	7.91	0
9	SLE RA 5	195	0	1825	-0.03	7.91	0
9	SLE RA 6	195	0	1825	-0.03	7.91	0
9	SLE RA 7	195	0	1825	-0.03	7.91	0
9	SLE RA 8	195	0	1825	-0.03	7.91	0
9	SLE RA 9	195	0	1825	-0.03	7.91	0
9	SLE RA 10	227	0	2025	-0.05	9.16	0
9	SLE RA 11	227	0	2025	-0.05	9.16	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
9	SLE RA 12	227	0	2025	-0.05	9.16	0
9	SLE RA 13	227	0	2025	-0.05	9.16	0
9	SLE RA 14	227	0	2025	-0.05	9.16	0
9	SLE RA 15	227	0	2025	-0.05	9.16	0
9	SLE RA 16	227	0	2025	-0.05	9.16	0
9	SLE RA 17	227	0	2025	-0.05	9.16	0
9	SLE RA 18	240	0	2110	-0.06	9.69	0
9	SLE RA 19	240	0	2110	-0.06	9.69	0
9	SLE RA 20	240	0	2110	-0.06	9.69	0
9	SLE RA 21	240	0	2110	-0.06	9.69	0
9	SLE FR 1	195	0	1825	-0.03	7.91	0
9	SLE FR 2	195	0	1825	-0.03	7.91	0
9	SLE FR 3	195	0	1825	-0.03	7.91	0
9	SLE FR 4	209	0	1910	-0.04	8.45	0
9	SLE FR 5	209	0	1910	-0.04	8.45	0
9	SLE FR 6	218	0	1967	-0.04	8.8	0
9	SLE QP 1	195	0	1825	-0.03	7.91	0
9	SLE QP 2	209	0	1910	-0.04	8.45	0
9	SLD 1	536	-13	1987	3.74	21.11	-0.09
9	SLD 2	536	-13	1987	3.74	21.11	-0.09
9	SLD 3	500	-38	1941	45.77	19.72	-0.31
9	SLD 4	500	-38	1941	45.77	19.72	-0.31
9	SLD 5	362	34	2003	-62.65	14.36	0.3
9	SLD 6	362	34	2003	-62.65	14.36	0.3
9	SLD 7	241	-50	1851	77.45	9.72	-0.42
9	SLD 8	241	-50	1851	77.45	9.72	-0.42
9	SLD 9	177	50	1970	-77.52	7.18	0.42
9	SLD 10	177	50	1970	-77.52	7.18	0.42
9	SLD 11	55	-34	1818	62.58	2.54	-0.3
9	SLD 12	55	-34	1818	62.58	2.54	-0.3
9	SLD 13	-82	38	1879	-45.84	-2.82	0.31
9	SLD 14	-82	38	1879	-45.84	-2.82	0.31
9	SLD 15	-119	13	1834	-3.81	-4.21	0.09
9	SLD 16	-119	13	1834	-3.81	-4.21	0.09
9	SLV 1	980	-33	2095	9.65	38.26	-0.23
9	SLV 2	980	-33	2095	9.65	38.26	-0.23
9	SLV 3	892	-97	1981	117.28	34.89	-0.78
9	SLV 4	892	-97	1981	117.28	34.89	-0.78
9	SLV 5	574	87	2139	-160.37	22.5	0.77
9	SLV 6	574	87	2139	-160.37	22.5	0.77
9	SLV 7	279	-126	1759	198.4	11.27	-1.07
9	SLV 8	279	-126	1759	198.4	11.27	-1.07
9	SLV 9	138	126	2062	-198.47	5.63	1.07
9	SLV 10	138	126	2062	-198.47	5.63	1.07
9	SLV 11	-157	-87	1682	160.3	-5.61	-0.77
9	SLV 12	-157	-87	1682	160.3	-5.61	-0.77
9	SLV 13	-474	97	1839	-117.35	-17.99	0.78
9	SLV 14	-474	97	1839	-117.35	-17.99	0.78
9	SLV 15	-563	33	1725	-9.72	-21.36	0.23
9	SLV 16	-563	33	1725	-9.72	-21.36	0.23
10	SLU 1	225	0	1945	0.03	7.91	0
10	SLU 2	225	0	1945	0.03	7.91	0
10	SLU 3	225	0	1945	0.03	7.91	0
10	SLU 4	225	0	1945	0.03	7.91	0
10	SLU 5	225	0	1945	0.03	7.91	0
10	SLU 6	225	0	1945	0.03	7.91	0
10	SLU 7	225	0	1945	0.03	7.91	0
10	SLU 8	225	0	1945	0.03	7.91	0
10	SLU 9	225	0	1945	0.03	7.91	0
10	SLU 10	281	0	2291	0.02	9.87	0
10	SLU 11	281	0	2291	0.02	9.87	0
10	SLU 12	281	0	2291	0.02	9.87	0
10	SLU 13	281	0	2291	0.02	9.87	0
10	SLU 14	281	0	2291	0.02	9.87	0
10	SLU 15	281	0	2291	0.02	9.87	0
10	SLU 16	281	0	2291	0.02	9.87	0
10	SLU 17	281	0	2291	0.02	9.87	0
10	SLU 18	305	0	2439	0.02	10.71	0
10	SLU 19	305	0	2439	0.02	10.71	0
10	SLU 20	305	0	2439	0.02	10.71	0
10	SLU 21	305	0	2439	0.02	10.71	0
10	SLU 22	259	0	2165	0.03	9.11	0
10	SLU 23	259	0	2165	0.03	9.11	0
10	SLU 24	259	0	2165	0.03	9.11	0
10	SLU 25	259	0	2165	0.03	9.11	0
10	SLU 26	259	0	2165	0.03	9.11	0
10	SLU 27	259	0	2165	0.03	9.11	0
10	SLU 28	259	0	2165	0.03	9.11	0
10	SLU 29	259	0	2165	0.03	9.11	0
10	SLU 30	259	0	2165	0.03	9.11	0
10	SLU 31	315	0	2511	0.03	11.07	0
10	SLU 32	315	0	2511	0.03	11.07	0
10	SLU 33	315	0	2511	0.03	11.07	0
10	SLU 34	315	0	2511	0.03	11.07	0
10	SLU 35	315	0	2511	0.03	11.07	0
10	SLU 36	315	0	2511	0.03	11.07	0
10	SLU 37	315	0	2511	0.03	11.07	0
10	SLU 38	315	0	2511	0.03	11.07	0
10	SLU 39	339	0	2659	0.02	11.91	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
10	SLU 40	339	0	2659	0.02	11.91	0
10	SLU 41	339	0	2659	0.02	11.91	0
10	SLU 42	339	0	2659	0.02	11.91	0
10	SLU 43	280	0	2454	0.03	9.87	0
10	SLU 44	280	0	2454	0.03	9.87	0
10	SLU 45	280	0	2454	0.03	9.87	0
10	SLU 46	280	0	2454	0.03	9.87	0
10	SLU 47	280	0	2454	0.03	9.87	0
10	SLU 48	280	0	2454	0.03	9.87	0
10	SLU 49	280	0	2454	0.03	9.87	0
10	SLU 50	280	0	2454	0.03	9.87	0
10	SLU 51	280	0	2454	0.03	9.87	0
10	SLU 52	336	0	2799	0.03	11.83	0
10	SLU 53	336	0	2799	0.03	11.83	0
10	SLU 54	336	0	2799	0.03	11.83	0
10	SLU 55	336	0	2799	0.03	11.83	0
10	SLU 56	336	0	2799	0.03	11.83	0
10	SLU 57	336	0	2799	0.03	11.83	0
10	SLU 58	336	0	2799	0.03	11.83	0
10	SLU 59	336	0	2799	0.03	11.83	0
10	SLU 60	360	0	2948	0.03	12.66	0
10	SLU 61	360	0	2948	0.03	12.66	0
10	SLU 62	360	0	2948	0.03	12.66	0
10	SLU 63	360	0	2948	0.03	12.66	0
10	SLU 64	315	0	2673	0.03	11.07	0
10	SLU 65	315	0	2673	0.03	11.07	0
10	SLU 66	315	0	2673	0.03	11.07	0
10	SLU 67	315	0	2673	0.03	11.07	0
10	SLU 68	315	0	2673	0.03	11.07	0
10	SLU 69	315	0	2673	0.03	11.07	0
10	SLU 70	315	0	2673	0.03	11.07	0
10	SLU 71	315	0	2673	0.03	11.07	0
10	SLU 72	315	0	2673	0.03	11.07	0
10	SLU 73	371	0	3019	0.03	13.03	0
10	SLU 74	371	0	3019	0.03	13.03	0
10	SLU 75	371	0	3019	0.03	13.03	0
10	SLU 76	371	0	3019	0.03	13.03	0
10	SLU 77	371	0	3019	0.03	13.03	0
10	SLU 78	371	0	3019	0.03	13.03	0
10	SLU 79	371	0	3019	0.03	13.03	0
10	SLU 80	371	0	3019	0.03	13.03	0
10	SLU 81	395	0	3167	0.03	13.87	0
10	SLU 82	395	0	3167	0.03	13.87	0
10	SLU 83	395	0	3167	0.03	13.87	0
10	SLU 84	395	0	3167	0.03	13.87	0
10	SLE RA 1	235	0	2008	0.03	8.25	0
10	SLE RA 2	235	0	2008	0.03	8.25	0
10	SLE RA 3	235	0	2008	0.03	8.25	0
10	SLE RA 4	235	0	2008	0.03	8.25	0
10	SLE RA 5	235	0	2008	0.03	8.25	0
10	SLE RA 6	235	0	2008	0.03	8.25	0
10	SLE RA 7	235	0	2008	0.03	8.25	0
10	SLE RA 8	235	0	2008	0.03	8.25	0
10	SLE RA 9	235	0	2008	0.03	8.25	0
10	SLE RA 10	272	0	2239	0.02	9.56	0
10	SLE RA 11	272	0	2239	0.02	9.56	0
10	SLE RA 12	272	0	2239	0.02	9.56	0
10	SLE RA 13	272	0	2239	0.02	9.56	0
10	SLE RA 14	272	0	2239	0.02	9.56	0
10	SLE RA 15	272	0	2239	0.02	9.56	0
10	SLE RA 16	272	0	2239	0.02	9.56	0
10	SLE RA 17	272	0	2239	0.02	9.56	0
10	SLE RA 18	288	0	2337	0.02	10.12	0
10	SLE RA 19	288	0	2337	0.02	10.12	0
10	SLE RA 20	288	0	2337	0.02	10.12	0
10	SLE RA 21	288	0	2337	0.02	10.12	0
10	SLE FR 1	235	0	2008	0.03	8.25	0
10	SLE FR 2	235	0	2008	0.03	8.25	0
10	SLE FR 3	235	0	2008	0.03	8.25	0
10	SLE FR 4	251	0	2107	0.03	8.81	0
10	SLE FR 5	251	0	2107	0.03	8.81	0
10	SLE FR 6	261	0	2173	0.02	9.19	0
10	SLE QP 1	235	0	2008	0.03	8.25	0
10	SLE QP 2	251	0	2107	0.03	8.81	0
10	SLD 1	556	37	2221	-3.08	20.18	0.28
10	SLD 2	556	37	2221	-3.08	20.18	0.28
10	SLD 3	520	8	2162	47.55	18.91	0.06
10	SLD 4	520	8	2162	47.55	18.91	0.06
10	SLD 5	396	55	2232	-77.68	14.15	0.41
10	SLD 6	396	55	2232	-77.68	14.15	0.41
10	SLD 7	278	-41	2033	91.06	9.91	-0.31
10	SLD 8	278	-41	2033	91.06	9.91	-0.31
10	SLD 9	223	41	2181	-91.01	7.71	0.31
10	SLD 10	223	41	2181	-91.01	7.71	0.31
10	SLD 11	105	-55	1982	77.73	3.47	-0.41
10	SLD 12	105	-55	1982	77.73	3.47	-0.41
10	SLD 13	-19	-8	2052	-47.5	-1.29	-0.06
10	SLD 14	-19	-8	2052	-47.5	-1.29	-0.06
10	SLD 15	-55	-37	1992	3.13	-2.56	-0.28



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
10	SLD 16	-55	-37	1992	3.13	-2.56	-0.28
10	SLV 1	969	94	2383	-8.03	35.58	0.7
10	SLV 2	969	94	2383	-8.03	35.58	0.7
10	SLV 3	883	21	2231	121.72	32.5	0.15
10	SLV 4	883	21	2231	121.72	32.5	0.15
10	SLV 5	597	140	2419	-199.18	21.52	1.04
10	SLV 6	597	140	2419	-199.18	21.52	1.04
10	SLV 7	310	-105	1914	233.32	11.24	-0.79
10	SLV 8	310	-105	1914	233.32	11.24	-0.79
10	SLV 9	192	105	2299	-233.27	6.38	0.79
10	SLV 10	192	105	2299	-233.27	6.38	0.79
10	SLV 11	-96	-140	1794	199.23	-3.89	-1.05
10	SLV 12	-96	-140	1794	199.23	-3.89	-1.05
10	SLV 13	-382	-21	1982	-121.67	-14.87	-0.15
10	SLV 14	-382	-21	1982	-121.67	-14.87	-0.15
10	SLV 15	-468	-94	1831	8.08	-17.95	-0.7
10	SLV 16	-468	-94	1831	8.08	-17.95	-0.7
11	SLU 1	185	0	2141	0.08	6.15	0
11	SLU 2	185	0	2141	0.08	6.15	0
11	SLU 3	185	0	2141	0.08	6.15	0
11	SLU 4	185	0	2141	0.08	6.15	0
11	SLU 5	185	0	2141	0.08	6.15	0
11	SLU 6	185	0	2141	0.08	6.15	0
11	SLU 7	185	0	2141	0.08	6.15	0
11	SLU 8	185	0	2141	0.08	6.15	0
11	SLU 9	185	0	2141	0.08	6.15	0
11	SLU 10	232	0	2536	0.12	7.72	0
11	SLU 11	232	0	2536	0.12	7.72	0
11	SLU 12	232	0	2536	0.12	7.72	0
11	SLU 13	232	0	2536	0.12	7.72	0
11	SLU 14	232	0	2536	0.12	7.72	0
11	SLU 15	232	0	2536	0.12	7.72	0
11	SLU 16	232	0	2536	0.12	7.72	0
11	SLU 17	232	0	2536	0.12	7.72	0
11	SLU 18	252	0	2705	0.14	8.39	0
11	SLU 19	252	0	2705	0.14	8.39	0
11	SLU 20	252	0	2705	0.14	8.39	0
11	SLU 21	252	0	2705	0.14	8.39	0
11	SLU 22	213	0	2390	0.1	7.08	0
11	SLU 23	213	0	2390	0.1	7.08	0
11	SLU 24	213	0	2390	0.1	7.08	0
11	SLU 25	213	0	2390	0.1	7.08	0
11	SLU 26	213	0	2390	0.1	7.08	0
11	SLU 27	213	0	2390	0.1	7.08	0
11	SLU 28	213	0	2390	0.1	7.08	0
11	SLU 29	213	0	2390	0.1	7.08	0
11	SLU 30	213	0	2390	0.1	7.08	0
11	SLU 31	260	0	2785	0.15	8.65	0
11	SLU 32	260	0	2785	0.15	8.65	0
11	SLU 33	260	0	2785	0.15	8.65	0
11	SLU 34	260	0	2785	0.15	8.65	0
11	SLU 35	260	0	2785	0.15	8.65	0
11	SLU 36	260	0	2785	0.15	8.65	0
11	SLU 37	260	0	2785	0.15	8.65	0
11	SLU 38	260	0	2785	0.15	8.65	0
11	SLU 39	280	0	2954	0.16	9.32	0
11	SLU 40	280	0	2954	0.16	9.32	0
11	SLU 41	280	0	2954	0.16	9.32	0
11	SLU 42	280	0	2954	0.16	9.32	0
11	SLU 43	231	0	2697	0.1	7.68	0
11	SLU 44	231	0	2697	0.1	7.68	0
11	SLU 45	231	0	2697	0.1	7.68	0
11	SLU 46	231	0	2697	0.1	7.68	0
11	SLU 47	231	0	2697	0.1	7.68	0
11	SLU 48	231	0	2697	0.1	7.68	0
11	SLU 49	231	0	2697	0.1	7.68	0
11	SLU 50	231	0	2697	0.1	7.68	0
11	SLU 51	231	0	2697	0.1	7.68	0
11	SLU 52	277	0	3092	0.14	9.24	0
11	SLU 53	277	0	3092	0.14	9.24	0
11	SLU 54	277	0	3092	0.14	9.24	0
11	SLU 55	277	0	3092	0.14	9.24	0
11	SLU 56	277	0	3092	0.14	9.24	0
11	SLU 57	277	0	3092	0.14	9.24	0
11	SLU 58	277	0	3092	0.14	9.24	0
11	SLU 59	277	0	3092	0.14	9.24	0
11	SLU 60	297	0	3262	0.16	9.91	0
11	SLU 61	297	0	3262	0.16	9.91	0
11	SLU 62	297	0	3262	0.16	9.91	0
11	SLU 63	297	0	3262	0.16	9.91	0
11	SLU 64	259	0	2946	0.12	8.61	0
11	SLU 65	259	0	2946	0.12	8.61	0
11	SLU 66	259	0	2946	0.12	8.61	0
11	SLU 67	259	0	2946	0.12	8.61	0
11	SLU 68	259	0	2946	0.12	8.61	0
11	SLU 69	259	0	2946	0.12	8.61	0
11	SLU 70	259	0	2946	0.12	8.61	0
11	SLU 71	259	0	2946	0.12	8.61	0
11	SLU 72	259	0	2946	0.12	8.61	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
11	SLU 73	305	0	3342	0.16	10.17	0
11	SLU 74	305	0	3342	0.16	10.17	0
11	SLU 75	305	0	3342	0.16	10.17	0
11	SLU 76	305	0	3342	0.16	10.17	0
11	SLU 77	305	0	3342	0.16	10.17	0
11	SLU 78	305	0	3342	0.16	10.17	0
11	SLU 79	305	0	3342	0.16	10.17	0
11	SLU 80	305	0	3342	0.16	10.17	0
11	SLU 81	325	-1	3511	0.18	10.85	0
11	SLU 82	325	-1	3511	0.18	10.85	0
11	SLU 83	325	-1	3511	0.18	10.85	0
11	SLU 84	325	-1	3511	0.18	10.85	0
11	SLE RA 1	193	0	2212	0.09	6.42	0
11	SLE RA 2	193	0	2212	0.09	6.42	0
11	SLE RA 3	193	0	2212	0.09	6.42	0
11	SLE RA 4	193	0	2212	0.09	6.42	0
11	SLE RA 5	193	0	2212	0.09	6.42	0
11	SLE RA 6	193	0	2212	0.09	6.42	0
11	SLE RA 7	193	0	2212	0.09	6.42	0
11	SLE RA 8	193	0	2212	0.09	6.42	0
11	SLE RA 9	193	0	2212	0.09	6.42	0
11	SLE RA 10	224	0	2475	0.12	7.46	0
11	SLE RA 11	224	0	2475	0.12	7.46	0
11	SLE RA 12	224	0	2475	0.12	7.46	0
11	SLE RA 13	224	0	2475	0.12	7.46	0
11	SLE RA 14	224	0	2475	0.12	7.46	0
11	SLE RA 15	224	0	2475	0.12	7.46	0
11	SLE RA 16	224	0	2475	0.12	7.46	0
11	SLE RA 17	224	0	2475	0.12	7.46	0
11	SLE RA 18	237	0	2588	0.13	7.91	0
11	SLE RA 19	237	0	2588	0.13	7.91	0
11	SLE RA 20	237	0	2588	0.13	7.91	0
11	SLE RA 21	237	0	2588	0.13	7.91	0
11	SLE FR 1	193	0	2212	0.09	6.42	0
11	SLE FR 2	193	0	2212	0.09	6.42	0
11	SLE FR 3	193	0	2212	0.09	6.42	0
11	SLE FR 4	206	0	2325	0.1	6.87	0
11	SLE FR 5	206	0	2325	0.1	6.87	0
11	SLE FR 6	215	0	2400	0.11	7.16	0
11	SLE QP 1	193	0	2212	0.09	6.42	0
11	SLE QP 2	206	0	2325	0.1	6.87	0
11	SLD 1	501	39	2445	-50.75	18.71	0.19
11	SLD 2	501	39	2445	-50.75	18.71	0.19
11	SLD 3	466	-2	2369	13.52	17.37	0
11	SLD 4	466	-2	2369	13.52	17.37	0
11	SLD 5	347	73	2476	-112.62	12.44	0.35
11	SLD 6	347	73	2476	-112.62	12.44	0.35
11	SLD 7	232	-62	2223	101.59	7.99	-0.29
11	SLD 8	232	-62	2223	101.59	7.99	-0.29
11	SLD 9	180	61	2426	-101.39	5.74	0.29
11	SLD 10	180	61	2426	-101.39	5.74	0.29
11	SLD 11	66	-73	2173	112.82	1.29	-0.35
11	SLD 12	66	-73	2173	112.82	1.29	-0.35
11	SLD 13	-54	1	2280	-13.32	-3.64	0
11	SLD 14	-54	1	2280	-13.32	-3.64	0
11	SLD 15	-88	-39	2204	50.95	-4.97	-0.2
11	SLD 16	-88	-39	2204	50.95	-4.97	-0.2
11	SLV 1	900	99	2616	-130.1	34.74	0.49
11	SLV 2	900	99	2616	-130.1	34.74	0.49
11	SLV 3	816	-4	2422	34.71	31.51	0
11	SLV 4	816	-4	2422	34.71	31.51	0
11	SLV 5	541	186	2706	-288.93	20.13	0.89
11	SLV 6	541	186	2706	-288.93	20.13	0.89
11	SLV 7	262	-158	2060	260.45	9.36	-0.75
11	SLV 8	262	-158	2060	260.45	9.36	-0.75
11	SLV 9	150	158	2589	-260.25	4.38	0.74
11	SLV 10	150	158	2589	-260.25	4.38	0.74
11	SLV 11	-129	-187	1943	289.13	-6.4	-0.9
11	SLV 12	-129	-187	1943	289.13	-6.4	-0.9
11	SLV 13	-404	4	2227	-34.51	-17.77	-0.01
11	SLV 14	-404	4	2227	-34.51	-17.77	-0.01
11	SLV 15	-487	-99	2033	130.3	-21.01	-0.5
11	SLV 16	-487	-99	2033	130.3	-21.01	-0.5
12	SLU 1	118	0	2275	0.14	4.49	0
12	SLU 2	118	0	2275	0.14	4.49	0
12	SLU 3	118	0	2275	0.14	4.49	0
12	SLU 4	118	0	2275	0.14	4.49	0
12	SLU 5	118	0	2275	0.14	4.49	0
12	SLU 6	118	0	2275	0.14	4.49	0
12	SLU 7	118	0	2275	0.14	4.49	0
12	SLU 8	118	0	2275	0.14	4.49	0
12	SLU 9	118	0	2275	0.14	4.49	0
12	SLU 10	149	-1	2705	0.21	5.65	0
12	SLU 11	149	-1	2705	0.21	5.65	0
12	SLU 12	149	-1	2705	0.21	5.65	0
12	SLU 13	149	-1	2705	0.21	5.65	0
12	SLU 14	149	-1	2705	0.21	5.65	0
12	SLU 15	149	-1	2705	0.21	5.65	0
12	SLU 16	149	-1	2705	0.21	5.65	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
12	SLU 17	149	-1	2705	0.21	5.65	0
12	SLU 18	162	-1	2889	0.25	6.15	0
12	SLU 19	162	-1	2889	0.25	6.15	0
12	SLU 20	162	-1	2889	0.25	6.15	0
12	SLU 21	162	-1	2889	0.25	6.15	0
12	SLU 22	136	0	2545	0.18	5.18	0
12	SLU 23	136	0	2545	0.18	5.18	0
12	SLU 24	136	0	2545	0.18	5.18	0
12	SLU 25	136	0	2545	0.18	5.18	0
12	SLU 26	136	0	2545	0.18	5.18	0
12	SLU 27	136	0	2545	0.18	5.18	0
12	SLU 28	136	0	2545	0.18	5.18	0
12	SLU 29	136	0	2545	0.18	5.18	0
12	SLU 30	136	0	2545	0.18	5.18	0
12	SLU 31	167	-1	2975	0.26	6.34	0
12	SLU 32	167	-1	2975	0.26	6.34	0
12	SLU 33	167	-1	2975	0.26	6.34	0
12	SLU 34	167	-1	2975	0.26	6.34	0
12	SLU 35	167	-1	2975	0.26	6.34	0
12	SLU 36	167	-1	2975	0.26	6.34	0
12	SLU 37	167	-1	2975	0.26	6.34	0
12	SLU 38	167	-1	2975	0.26	6.34	0
12	SLU 39	180	-1	3159	0.29	6.84	0
12	SLU 40	180	-1	3159	0.29	6.84	0
12	SLU 41	180	-1	3159	0.29	6.84	0
12	SLU 42	180	-1	3159	0.29	6.84	0
12	SLU 43	147	0	2865	0.16	5.6	0
12	SLU 44	147	0	2865	0.16	5.6	0
12	SLU 45	147	0	2865	0.16	5.6	0
12	SLU 46	147	0	2865	0.16	5.6	0
12	SLU 47	147	0	2865	0.16	5.6	0
12	SLU 48	147	0	2865	0.16	5.6	0
12	SLU 49	147	0	2865	0.16	5.6	0
12	SLU 50	147	0	2865	0.16	5.6	0
12	SLU 51	147	0	2865	0.16	5.6	0
12	SLU 52	178	-1	3295	0.24	6.76	0
12	SLU 53	178	-1	3295	0.24	6.76	0
12	SLU 54	178	-1	3295	0.24	6.76	0
12	SLU 55	178	-1	3295	0.24	6.76	0
12	SLU 56	178	-1	3295	0.24	6.76	0
12	SLU 57	178	-1	3295	0.24	6.76	0
12	SLU 58	178	-1	3295	0.24	6.76	0
12	SLU 59	178	-1	3295	0.24	6.76	0
12	SLU 60	191	-1	3479	0.28	7.26	0
12	SLU 61	191	-1	3479	0.28	7.26	0
12	SLU 62	191	-1	3479	0.28	7.26	0
12	SLU 63	191	-1	3479	0.28	7.26	0
12	SLU 64	165	0	3135	0.2	6.29	0
12	SLU 65	165	0	3135	0.2	6.29	0
12	SLU 66	165	0	3135	0.2	6.29	0
12	SLU 67	165	0	3135	0.2	6.29	0
12	SLU 68	165	0	3135	0.2	6.29	0
12	SLU 69	165	0	3135	0.2	6.29	0
12	SLU 70	165	0	3135	0.2	6.29	0
12	SLU 71	165	0	3135	0.2	6.29	0
12	SLU 72	165	0	3135	0.2	6.29	0
12	SLU 73	196	-1	3565	0.28	7.45	0
12	SLU 74	196	-1	3565	0.28	7.45	0
12	SLU 75	196	-1	3565	0.28	7.45	0
12	SLU 76	196	-1	3565	0.28	7.45	0
12	SLU 77	196	-1	3565	0.28	7.45	0
12	SLU 78	196	-1	3565	0.28	7.45	0
12	SLU 79	196	-1	3565	0.28	7.45	0
12	SLU 80	196	-1	3565	0.28	7.45	0
12	SLU 81	209	-1	3749	0.32	7.95	0
12	SLU 82	209	-1	3749	0.32	7.95	0
12	SLU 83	209	-1	3749	0.32	7.95	0
12	SLU 84	209	-1	3749	0.32	7.95	0
12	SLE RA 1	123	0	2352	0.15	4.69	0
12	SLE RA 2	123	0	2352	0.15	4.69	0
12	SLE RA 3	123	0	2352	0.15	4.69	0
12	SLE RA 4	123	0	2352	0.15	4.69	0
12	SLE RA 5	123	0	2352	0.15	4.69	0
12	SLE RA 6	123	0	2352	0.15	4.69	0
12	SLE RA 7	123	0	2352	0.15	4.69	0
12	SLE RA 8	123	0	2352	0.15	4.69	0
12	SLE RA 9	123	0	2352	0.15	4.69	0
12	SLE RA 10	144	0	2639	0.2	5.46	0
12	SLE RA 11	144	0	2639	0.2	5.46	0
12	SLE RA 12	144	0	2639	0.2	5.46	0
12	SLE RA 13	144	0	2639	0.2	5.46	0
12	SLE RA 14	144	0	2639	0.2	5.46	0
12	SLE RA 15	144	0	2639	0.2	5.46	0
12	SLE RA 16	144	0	2639	0.2	5.46	0
12	SLE RA 17	144	0	2639	0.2	5.46	0
12	SLE RA 18	153	-1	2762	0.22	5.79	0
12	SLE RA 19	153	-1	2762	0.22	5.79	0
12	SLE RA 20	153	-1	2762	0.22	5.79	0
12	SLE RA 21	153	-1	2762	0.22	5.79	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
12	SLE FR 1	123	0	2352	0.15	4.69	0
12	SLE FR 2	123	0	2352	0.15	4.69	0
12	SLE FR 3	123	0	2352	0.15	4.69	0
12	SLE FR 4	132	0	2475	0.17	5.02	0
12	SLE FR 5	132	0	2475	0.17	5.02	0
12	SLE FR 6	138	0	2557	0.19	5.24	0
12	SLE QP 1	123	0	2352	0.15	4.69	0
12	SLE QP 2	132	0	2475	0.17	5.02	0
12	SLD 1	416	54	2582	-61.58	16.4	0.01
12	SLD 2	416	54	2582	-61.58	16.4	0.01
12	SLD 3	385	-20	2491	28.53	15.2	0.12
12	SLD 4	385	-20	2491	28.53	15.2	0.12
12	SLD 5	264	127	2645	-155.03	10.25	-0.18
12	SLD 6	264	127	2645	-155.03	10.25	-0.18
12	SLD 7	161	-117	2341	145.35	6.26	0.21
12	SLD 8	161	-117	2341	145.35	6.26	0.21
12	SLD 9	103	116	2609	-145.01	3.78	-0.22
12	SLD 10	103	116	2609	-145.01	3.78	-0.22
12	SLD 11	0	-127	2305	155.37	-0.21	0.17
12	SLD 12	0	-127	2305	155.37	-0.21	0.17
12	SLD 13	-121	19	2459	-28.19	-5.17	-0.13
12	SLD 14	-121	19	2459	-28.19	-5.17	-0.13
12	SLD 15	-152	-54	2368	61.92	-6.37	-0.01
12	SLD 16	-152	-54	2368	61.92	-6.37	-0.01
12	SLV 1	800	137	2737	-158.05	31.79	0.02
12	SLV 2	800	137	2737	-158.05	31.79	0.02
12	SLV 3	725	-50	2504	73.12	28.92	0.32
12	SLV 4	725	-50	2504	73.12	28.92	0.32
12	SLV 5	446	325	2908	-397.9	17.4	-0.45
12	SLV 6	446	325	2908	-397.9	17.4	-0.45
12	SLV 7	196	-300	2130	372.66	7.84	0.55
12	SLV 8	196	-300	2130	372.66	7.84	0.55
12	SLV 9	67	299	2820	-372.32	2.19	-0.55
12	SLV 10	67	299	2820	-372.32	2.19	-0.55
12	SLV 11	-182	-326	2042	398.24	-7.36	0.45
12	SLV 12	-182	-326	2042	398.24	-7.36	0.45
12	SLV 13	-461	49	2446	-72.78	-18.89	-0.32
12	SLV 14	-461	49	2446	-72.78	-18.89	-0.32
12	SLV 15	-536	-138	2213	158.39	-21.76	-0.02
12	SLV 16	-536	-138	2213	158.39	-21.76	-0.02
13	SLU 1	44	0	2338	0.19	1.48	0
13	SLU 2	44	0	2338	0.19	1.48	0
13	SLU 3	44	0	2338	0.19	1.48	0
13	SLU 4	44	0	2338	0.19	1.48	0
13	SLU 5	44	0	2338	0.19	1.48	0
13	SLU 6	44	0	2338	0.19	1.48	0
13	SLU 7	44	0	2338	0.19	1.48	0
13	SLU 8	44	0	2338	0.19	1.48	0
13	SLU 9	44	0	2338	0.19	1.48	0
13	SLU 10	58	-1	2786	0.28	1.92	0
13	SLU 11	58	-1	2786	0.28	1.92	0
13	SLU 12	58	-1	2786	0.28	1.92	0
13	SLU 13	58	-1	2786	0.28	1.92	0
13	SLU 14	58	-1	2786	0.28	1.92	0
13	SLU 15	58	-1	2786	0.28	1.92	0
13	SLU 16	58	-1	2786	0.28	1.92	0
13	SLU 17	58	-1	2786	0.28	1.92	0
13	SLU 18	63	-1	2978	0.32	2.12	0
13	SLU 19	63	-1	2978	0.32	2.12	0
13	SLU 20	63	-1	2978	0.32	2.12	0
13	SLU 21	63	-1	2978	0.32	2.12	0
13	SLU 22	52	-1	2618	0.24	1.72	0
13	SLU 23	52	-1	2618	0.24	1.72	0
13	SLU 24	52	-1	2618	0.24	1.72	0
13	SLU 25	52	-1	2618	0.24	1.72	0
13	SLU 26	52	-1	2618	0.24	1.72	0
13	SLU 27	52	-1	2618	0.24	1.72	0
13	SLU 28	52	-1	2618	0.24	1.72	0
13	SLU 29	52	-1	2618	0.24	1.72	0
13	SLU 30	52	-1	2618	0.24	1.72	0
13	SLU 31	65	-1	3066	0.33	2.17	0
13	SLU 32	65	-1	3066	0.33	2.17	0
13	SLU 33	65	-1	3066	0.33	2.17	0
13	SLU 34	65	-1	3066	0.33	2.17	0
13	SLU 35	65	-1	3066	0.33	2.17	0
13	SLU 36	65	-1	3066	0.33	2.17	0
13	SLU 37	65	-1	3066	0.33	2.17	0
13	SLU 38	65	-1	3066	0.33	2.17	0
13	SLU 39	71	-1	3258	0.37	2.36	0
13	SLU 40	71	-1	3258	0.37	2.36	0
13	SLU 41	71	-1	3258	0.37	2.36	0
13	SLU 42	71	-1	3258	0.37	2.36	0
13	SLU 43	55	0	2944	0.23	1.84	0
13	SLU 44	55	0	2944	0.23	1.84	0
13	SLU 45	55	0	2944	0.23	1.84	0
13	SLU 46	55	0	2944	0.23	1.84	0
13	SLU 47	55	0	2944	0.23	1.84	0
13	SLU 48	55	0	2944	0.23	1.84	0
13	SLU 49	55	0	2944	0.23	1.84	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
13	SLU 50	55	0	2944	0.23	1.84	0
13	SLU 51	55	0	2944	0.23	1.84	0
13	SLU 52	68	-1	3391	0.32	2.28	0
13	SLU 53	68	-1	3391	0.32	2.28	0
13	SLU 54	68	-1	3391	0.32	2.28	0
13	SLU 55	68	-1	3391	0.32	2.28	0
13	SLU 56	68	-1	3391	0.32	2.28	0
13	SLU 57	68	-1	3391	0.32	2.28	0
13	SLU 58	68	-1	3391	0.32	2.28	0
13	SLU 59	68	-1	3391	0.32	2.28	0
13	SLU 60	74	-1	3583	0.35	2.48	0
13	SLU 61	74	-1	3583	0.35	2.48	0
13	SLU 62	74	-1	3583	0.35	2.48	0
13	SLU 63	74	-1	3583	0.35	2.48	0
13	SLU 64	62	-1	3224	0.28	2.08	0
13	SLU 65	62	-1	3224	0.28	2.08	0
13	SLU 66	62	-1	3224	0.28	2.08	0
13	SLU 67	62	-1	3224	0.28	2.08	0
13	SLU 68	62	-1	3224	0.28	2.08	0
13	SLU 69	62	-1	3224	0.28	2.08	0
13	SLU 70	62	-1	3224	0.28	2.08	0
13	SLU 71	62	-1	3224	0.28	2.08	0
13	SLU 72	62	-1	3224	0.28	2.08	0
13	SLU 73	76	-1	3671	0.37	2.53	0
13	SLU 74	76	-1	3671	0.37	2.53	0
13	SLU 75	76	-1	3671	0.37	2.53	0
13	SLU 76	76	-1	3671	0.37	2.53	0
13	SLU 77	76	-1	3671	0.37	2.53	0
13	SLU 78	76	-1	3671	0.37	2.53	0
13	SLU 79	76	-1	3671	0.37	2.53	0
13	SLU 80	76	-1	3671	0.37	2.53	0
13	SLU 81	81	-1	3863	0.41	2.72	0
13	SLU 82	81	-1	3863	0.41	2.72	0
13	SLU 83	81	-1	3863	0.41	2.72	0
13	SLU 84	81	-1	3863	0.41	2.72	0
13	SLE RA 1	46	0	2418	0.2	1.55	0
13	SLE RA 2	46	0	2418	0.2	1.55	0
13	SLE RA 3	46	0	2418	0.2	1.55	0
13	SLE RA 4	46	0	2418	0.2	1.55	0
13	SLE RA 5	46	0	2418	0.2	1.55	0
13	SLE RA 6	46	0	2418	0.2	1.55	0
13	SLE RA 7	46	0	2418	0.2	1.55	0
13	SLE RA 8	46	0	2418	0.2	1.55	0
13	SLE RA 9	46	0	2418	0.2	1.55	0
13	SLE RA 10	55	-1	2717	0.26	1.85	0
13	SLE RA 11	55	-1	2717	0.26	1.85	0
13	SLE RA 12	55	-1	2717	0.26	1.85	0
13	SLE RA 13	55	-1	2717	0.26	1.85	0
13	SLE RA 14	55	-1	2717	0.26	1.85	0
13	SLE RA 15	55	-1	2717	0.26	1.85	0
13	SLE RA 16	55	-1	2717	0.26	1.85	0
13	SLE RA 17	55	-1	2717	0.26	1.85	0
13	SLE RA 18	59	-1	2845	0.29	1.97	0
13	SLE RA 19	59	-1	2845	0.29	1.97	0
13	SLE RA 20	59	-1	2845	0.29	1.97	0
13	SLE RA 21	59	-1	2845	0.29	1.97	0
13	SLE FR 1	46	0	2418	0.2	1.55	0
13	SLE FR 2	46	0	2418	0.2	1.55	0
13	SLE FR 3	46	0	2418	0.2	1.55	0
13	SLE FR 4	50	0	2546	0.23	1.68	0
13	SLE FR 5	50	0	2546	0.23	1.68	0
13	SLE FR 6	53	-1	2631	0.25	1.76	0
13	SLE QP 1	46	0	2418	0.2	1.55	0
13	SLE QP 2	50	0	2546	0.23	1.68	0
13	SLD 1	336	121	2632	-53.08	13.37	0.58
13	SLD 2	336	121	2632	-53.08	13.37	0.58
13	SLD 3	308	-230	2530	99.52	12.21	-1.09
13	SLD 4	308	-230	2530	99.52	12.21	-1.09
13	SLD 5	179	567	2726	-247.21	6.94	2.7
13	SLD 6	179	567	2726	-247.21	6.94	2.7
13	SLD 7	84	-601	2387	261.46	3.08	-2.86
13	SLD 8	84	-601	2387	261.46	3.08	-2.86
13	SLD 9	16	600	2705	-261	0.27	2.86
13	SLD 10	16	600	2705	-261	0.27	2.86
13	SLD 11	-79	-568	2366	247.67	-3.59	-2.7
13	SLD 12	-79	-568	2366	247.67	-3.59	-2.7
13	SLD 13	-207	229	2562	-99.06	-8.86	1.09
13	SLD 14	-207	229	2562	-99.06	-8.86	1.09
13	SLD 15	-236	-122	2460	53.54	-10.02	-0.58
13	SLD 16	-236	-122	2460	53.54	-10.02	-0.58
13	SLV 1	722	311	2762	-136.61	29.16	1.48
13	SLV 2	722	311	2762	-136.61	29.16	1.48
13	SLV 3	655	-588	2502	254.88	26.42	-2.8
13	SLV 4	655	-588	2502	254.88	26.42	-2.8
13	SLV 5	353	1456	3005	-634.58	14.07	6.93
13	SLV 6	353	1456	3005	-634.58	14.07	6.93
13	SLV 7	130	-1540	2139	670.38	4.95	-7.33
13	SLV 8	130	-1540	2139	670.38	4.95	-7.33
13	SLV 9	-30	1539	2953	-669.93	-1.59	7.33



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
13	SLV 10	-30	1539	2953	-669.93	-1.59	7.33
13	SLV 11	-253	-1457	2087	635.04	-10.72	-6.93
13	SLV 12	-253	-1457	2087	635.04	-10.72	-6.93
13	SLV 13	-555	587	2590	-254.42	-23.07	2.8
13	SLV 14	-555	587	2590	-254.42	-23.07	2.8
13	SLV 15	-622	-312	2330	137.07	-25.81	-1.48
13	SLV 16	-622	-312	2330	137.07	-25.81	-1.48
14	SLU 1	-1	-1	2722	0.48	-0.05	0
14	SLU 2	-1	-1	2722	0.48	-0.05	0
14	SLU 3	-1	-1	2722	0.48	-0.05	0
14	SLU 4	-1	-1	2722	0.48	-0.05	0
14	SLU 5	-1	-1	2722	0.48	-0.05	0
14	SLU 6	-1	-1	2722	0.48	-0.05	0
14	SLU 7	-1	-1	2722	0.48	-0.05	0
14	SLU 8	-1	-1	2722	0.48	-0.05	0
14	SLU 9	-1	-1	2722	0.48	-0.05	0
14	SLU 10	0	-1	3248	0.68	-0.01	0
14	SLU 11	0	-1	3248	0.68	-0.01	0
14	SLU 12	0	-1	3248	0.68	-0.01	0
14	SLU 13	0	-1	3248	0.68	-0.01	0
14	SLU 14	0	-1	3248	0.68	-0.01	0
14	SLU 15	0	-1	3248	0.68	-0.01	0
14	SLU 16	0	-1	3248	0.68	-0.01	0
14	SLU 17	0	-1	3248	0.68	-0.01	0
14	SLU 18	1	-2	3474	0.76	0	0
14	SLU 19	1	-2	3474	0.76	0	0
14	SLU 20	1	-2	3474	0.76	0	0
14	SLU 21	1	-2	3474	0.76	0	0
14	SLU 22	-1	-1	3050	0.6	-0.04	0
14	SLU 23	-1	-1	3050	0.6	-0.04	0
14	SLU 24	-1	-1	3050	0.6	-0.04	0
14	SLU 25	-1	-1	3050	0.6	-0.04	0
14	SLU 26	-1	-1	3050	0.6	-0.04	0
14	SLU 27	-1	-1	3050	0.6	-0.04	0
14	SLU 28	-1	-1	3050	0.6	-0.04	0
14	SLU 29	-1	-1	3050	0.6	-0.04	0
14	SLU 30	-1	-1	3050	0.6	-0.04	0
14	SLU 31	0	-2	3576	0.8	0	0
14	SLU 32	0	-2	3576	0.8	0	0
14	SLU 33	0	-2	3576	0.8	0	0
14	SLU 34	0	-2	3576	0.8	0	0
14	SLU 35	0	-2	3576	0.8	0	0
14	SLU 36	0	-2	3576	0.8	0	0
14	SLU 37	0	-2	3576	0.8	0	0
14	SLU 38	0	-2	3576	0.8	0	0
14	SLU 39	1	-2	3802	0.88	0.01	0
14	SLU 40	1	-2	3802	0.88	0.01	0
14	SLU 41	1	-2	3802	0.88	0.01	0
14	SLU 42	1	-2	3802	0.88	0.01	0
14	SLU 43	-2	-1	3426	0.58	-0.07	0
14	SLU 44	-2	-1	3426	0.58	-0.07	0
14	SLU 45	-2	-1	3426	0.58	-0.07	0
14	SLU 46	-2	-1	3426	0.58	-0.07	0
14	SLU 47	-2	-1	3426	0.58	-0.07	0
14	SLU 48	-2	-1	3426	0.58	-0.07	0
14	SLU 49	-2	-1	3426	0.58	-0.07	0
14	SLU 50	-2	-1	3426	0.58	-0.07	0
14	SLU 51	-2	-1	3426	0.58	-0.07	0
14	SLU 52	0	-2	3953	0.78	-0.03	0
14	SLU 53	0	-2	3953	0.78	-0.03	0
14	SLU 54	0	-2	3953	0.78	-0.03	0
14	SLU 55	0	-2	3953	0.78	-0.03	0
14	SLU 56	0	-2	3953	0.78	-0.03	0
14	SLU 57	0	-2	3953	0.78	-0.03	0
14	SLU 58	0	-2	3953	0.78	-0.03	0
14	SLU 59	0	-2	3953	0.78	-0.03	0
14	SLU 60	0	-2	4178	0.86	-0.02	0
14	SLU 61	0	-2	4178	0.86	-0.02	0
14	SLU 62	0	-2	4178	0.86	-0.02	0
14	SLU 63	0	-2	4178	0.86	-0.02	0
14	SLU 64	-1	-2	3754	0.7	-0.06	0
14	SLU 65	-1	-2	3754	0.7	-0.06	0
14	SLU 66	-1	-2	3754	0.7	-0.06	0
14	SLU 67	-1	-2	3754	0.7	-0.06	0
14	SLU 68	-1	-2	3754	0.7	-0.06	0
14	SLU 69	-1	-2	3754	0.7	-0.06	0
14	SLU 70	-1	-2	3754	0.7	-0.06	0
14	SLU 71	-1	-2	3754	0.7	-0.06	0
14	SLU 72	-1	-2	3754	0.7	-0.06	0
14	SLU 73	0	-2	4281	0.9	-0.02	0
14	SLU 74	0	-2	4281	0.9	-0.02	0
14	SLU 75	0	-2	4281	0.9	-0.02	0
14	SLU 76	0	-2	4281	0.9	-0.02	0
14	SLU 77	0	-2	4281	0.9	-0.02	0
14	SLU 78	0	-2	4281	0.9	-0.02	0
14	SLU 79	0	-2	4281	0.9	-0.02	0
14	SLU 80	0	-2	4281	0.9	-0.02	0
14	SLU 81	0	-2	4506	0.99	-0.01	0
14	SLU 82	0	-2	4506	0.99	-0.01	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
14	SLU 83	0	-2	4506	0.99	-0.01	0
14	SLU 84	0	-2	4506	0.99	-0.01	0
14	SLE RA 1	-1	-1	2816	0.51	-0.05	0
14	SLE RA 2	-1	-1	2816	0.51	-0.05	0
14	SLE RA 3	-1	-1	2816	0.51	-0.05	0
14	SLE RA 4	-1	-1	2816	0.51	-0.05	0
14	SLE RA 5	-1	-1	2816	0.51	-0.05	0
14	SLE RA 6	-1	-1	2816	0.51	-0.05	0
14	SLE RA 7	-1	-1	2816	0.51	-0.05	0
14	SLE RA 8	-1	-1	2816	0.51	-0.05	0
14	SLE RA 9	-1	-1	2816	0.51	-0.05	0
14	SLE RA 10	0	-1	3167	0.65	-0.02	0
14	SLE RA 11	0	-1	3167	0.65	-0.02	0
14	SLE RA 12	0	-1	3167	0.65	-0.02	0
14	SLE RA 13	0	-1	3167	0.65	-0.02	0
14	SLE RA 14	0	-1	3167	0.65	-0.02	0
14	SLE RA 15	0	-1	3167	0.65	-0.02	0
14	SLE RA 16	0	-1	3167	0.65	-0.02	0
14	SLE RA 17	0	-1	3167	0.65	-0.02	0
14	SLE RA 18	0	-1	3317	0.7	-0.01	0
14	SLE RA 19	0	-1	3317	0.7	-0.01	0
14	SLE RA 20	0	-1	3317	0.7	-0.01	0
14	SLE RA 21	0	-1	3317	0.7	-0.01	0
14	SLE FR 1	-1	-1	2816	0.51	-0.05	0
14	SLE FR 2	-1	-1	2816	0.51	-0.05	0
14	SLE FR 3	-1	-1	2816	0.51	-0.05	0
14	SLE FR 4	-1	-1	2966	0.57	-0.04	0
14	SLE FR 5	-1	-1	2966	0.57	-0.04	0
14	SLE FR 6	0	-1	3066	0.61	-0.03	0
14	SLE QP 1	-1	-1	2816	0.51	-0.05	0
14	SLE QP 2	-1	-1	2966	0.57	-0.04	0
14	SLD 1	283	394	3000	-144.95	11.74	0.05
14	SLD 2	283	394	3000	-144.95	11.74	0.05
14	SLD 3	255	-749	2875	275.44	10.58	0.23
14	SLD 4	255	-749	2875	275.44	10.58	0.23
14	SLD 5	127	1851	3165	-680.68	5.26	-0.25
14	SLD 6	127	1851	3165	-680.68	5.26	-0.25
14	SLD 7	34	-1959	2751	720.62	1.39	0.33
14	SLD 8	34	-1959	2751	720.62	1.39	0.33
14	SLD 9	-35	1957	3182	-719.48	-1.46	-0.33
14	SLD 10	-35	1957	3182	-719.48	-1.46	-0.33
14	SLD 11	-128	-1854	2768	681.82	-5.33	0.25
14	SLD 12	-128	-1854	2768	681.82	-5.33	0.25
14	SLD 13	-256	746	3057	-274.3	-10.66	-0.23
14	SLD 14	-256	746	3057	-274.3	-10.66	-0.23
14	SLD 15	-284	-397	2933	146.09	-11.82	-0.05
14	SLD 16	-284	-397	2933	146.09	-11.82	-0.05
14	SLV 1	665	1013	3053	-372.78	27.64	0.12
14	SLV 2	665	1013	3053	-372.78	27.64	0.12
14	SLV 3	599	-1919	2734	705.72	24.91	0.57
14	SLV 4	599	-1919	2734	705.72	24.91	0.57
14	SLV 5	299	4751	3475	-1747.16	12.4	-0.65
14	SLV 6	299	4751	3475	-1747.16	12.4	-0.65
14	SLV 7	80	-5025	2414	1847.85	3.31	0.86
14	SLV 8	80	-5025	2414	1847.85	3.31	0.86
14	SLV 9	-81	5022	3518	-1846.7	-3.39	-0.86
14	SLV 10	-81	5022	3518	-1846.7	-3.39	-0.86
14	SLV 11	-300	-4754	2457	1748.3	-12.47	0.65
14	SLV 12	-300	-4754	2457	1748.3	-12.47	0.65
14	SLV 13	-601	1917	3198	-704.58	-24.98	-0.57
14	SLV 14	-601	1917	3198	-704.58	-24.98	-0.57
14	SLV 15	-666	-1016	2880	373.92	-27.71	-0.12
14	SLV 16	-666	-1016	2880	373.92	-27.71	-0.12
15	SLU 1	-43	0	2244	0.18	-1.59	0
15	SLU 2	-43	0	2244	0.18	-1.59	0
15	SLU 3	-43	0	2244	0.18	-1.59	0
15	SLU 4	-43	0	2244	0.18	-1.59	0
15	SLU 5	-43	0	2244	0.18	-1.59	0
15	SLU 6	-43	0	2244	0.18	-1.59	0
15	SLU 7	-43	0	2244	0.18	-1.59	0
15	SLU 8	-43	0	2244	0.18	-1.59	0
15	SLU 9	-43	0	2244	0.18	-1.59	0
15	SLU 10	-54	-1	2678	0.27	-1.98	0
15	SLU 11	-54	-1	2678	0.27	-1.98	0
15	SLU 12	-54	-1	2678	0.27	-1.98	0
15	SLU 13	-54	-1	2678	0.27	-1.98	0
15	SLU 14	-54	-1	2678	0.27	-1.98	0
15	SLU 15	-54	-1	2678	0.27	-1.98	0
15	SLU 16	-54	-1	2678	0.27	-1.98	0
15	SLU 17	-54	-1	2678	0.27	-1.98	0
15	SLU 18	-58	-1	2864	0.3	-2.15	0
15	SLU 19	-58	-1	2864	0.3	-2.15	0
15	SLU 20	-58	-1	2864	0.3	-2.15	0
15	SLU 21	-58	-1	2864	0.3	-2.15	0
15	SLU 22	-50	0	2514	0.23	-1.83	0
15	SLU 23	-50	0	2514	0.23	-1.83	0
15	SLU 24	-50	0	2514	0.23	-1.83	0
15	SLU 25	-50	0	2514	0.23	-1.83	0
15	SLU 26	-50	0	2514	0.23	-1.83	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
15	SLU 27	-50	0	2514	0.23	-1.83	0
15	SLU 28	-50	0	2514	0.23	-1.83	0
15	SLU 29	-50	0	2514	0.23	-1.83	0
15	SLU 30	-50	0	2514	0.23	-1.83	0
15	SLU 31	-60	-1	2947	0.31	-2.22	0
15	SLU 32	-60	-1	2947	0.31	-2.22	0
15	SLU 33	-60	-1	2947	0.31	-2.22	0
15	SLU 34	-60	-1	2947	0.31	-2.22	0
15	SLU 35	-60	-1	2947	0.31	-2.22	0
15	SLU 36	-60	-1	2947	0.31	-2.22	0
15	SLU 37	-60	-1	2947	0.31	-2.22	0
15	SLU 38	-60	-1	2947	0.31	-2.22	0
15	SLU 39	-65	-1	3133	0.35	-2.38	0
15	SLU 40	-65	-1	3133	0.35	-2.38	0
15	SLU 41	-65	-1	3133	0.35	-2.38	0
15	SLU 42	-65	-1	3133	0.35	-2.38	0
15	SLU 43	-54	0	2825	0.22	-1.99	0
15	SLU 44	-54	0	2825	0.22	-1.99	0
15	SLU 45	-54	0	2825	0.22	-1.99	0
15	SLU 46	-54	0	2825	0.22	-1.99	0
15	SLU 47	-54	0	2825	0.22	-1.99	0
15	SLU 48	-54	0	2825	0.22	-1.99	0
15	SLU 49	-54	0	2825	0.22	-1.99	0
15	SLU 50	-54	0	2825	0.22	-1.99	0
15	SLU 51	-54	0	2825	0.22	-1.99	0
15	SLU 52	-65	-1	3259	0.3	-2.38	0
15	SLU 53	-65	-1	3259	0.3	-2.38	0
15	SLU 54	-65	-1	3259	0.3	-2.38	0
15	SLU 55	-65	-1	3259	0.3	-2.38	0
15	SLU 56	-65	-1	3259	0.3	-2.38	0
15	SLU 57	-65	-1	3259	0.3	-2.38	0
15	SLU 58	-65	-1	3259	0.3	-2.38	0
15	SLU 59	-65	-1	3259	0.3	-2.38	0
15	SLU 60	-69	-1	3445	0.34	-2.55	0
15	SLU 61	-69	-1	3445	0.34	-2.55	0
15	SLU 62	-69	-1	3445	0.34	-2.55	0
15	SLU 63	-69	-1	3445	0.34	-2.55	0
15	SLU 64	-61	-1	3094	0.27	-2.22	0
15	SLU 65	-61	-1	3094	0.27	-2.22	0
15	SLU 66	-61	-1	3094	0.27	-2.22	0
15	SLU 67	-61	-1	3094	0.27	-2.22	0
15	SLU 68	-61	-1	3094	0.27	-2.22	0
15	SLU 69	-61	-1	3094	0.27	-2.22	0
15	SLU 70	-61	-1	3094	0.27	-2.22	0
15	SLU 71	-61	-1	3094	0.27	-2.22	0
15	SLU 72	-61	-1	3094	0.27	-2.22	0
15	SLU 73	-71	-1	3528	0.35	-2.61	0
15	SLU 74	-71	-1	3528	0.35	-2.61	0
15	SLU 75	-71	-1	3528	0.35	-2.61	0
15	SLU 76	-71	-1	3528	0.35	-2.61	0
15	SLU 77	-71	-1	3528	0.35	-2.61	0
15	SLU 78	-71	-1	3528	0.35	-2.61	0
15	SLU 79	-71	-1	3528	0.35	-2.61	0
15	SLU 80	-71	-1	3528	0.35	-2.61	0
15	SLU 81	-76	-1	3714	0.39	-2.78	0
15	SLU 82	-76	-1	3714	0.39	-2.78	0
15	SLU 83	-76	-1	3714	0.39	-2.78	0
15	SLU 84	-76	-1	3714	0.39	-2.78	0
15	SLE RA 1	-45	0	2321	0.19	-1.66	0
15	SLE RA 2	-45	0	2321	0.19	-1.66	0
15	SLE RA 3	-45	0	2321	0.19	-1.66	0
15	SLE RA 4	-45	0	2321	0.19	-1.66	0
15	SLE RA 5	-45	0	2321	0.19	-1.66	0
15	SLE RA 6	-45	0	2321	0.19	-1.66	0
15	SLE RA 7	-45	0	2321	0.19	-1.66	0
15	SLE RA 8	-45	0	2321	0.19	-1.66	0
15	SLE RA 9	-45	0	2321	0.19	-1.66	0
15	SLE RA 10	-52	-1	2610	0.25	-1.92	0
15	SLE RA 11	-52	-1	2610	0.25	-1.92	0
15	SLE RA 12	-52	-1	2610	0.25	-1.92	0
15	SLE RA 13	-52	-1	2610	0.25	-1.92	0
15	SLE RA 14	-52	-1	2610	0.25	-1.92	0
15	SLE RA 15	-52	-1	2610	0.25	-1.92	0
15	SLE RA 16	-52	-1	2610	0.25	-1.92	0
15	SLE RA 17	-52	-1	2610	0.25	-1.92	0
15	SLE RA 18	-55	-1	2734	0.28	-2.03	0
15	SLE RA 19	-55	-1	2734	0.28	-2.03	0
15	SLE RA 20	-55	-1	2734	0.28	-2.03	0
15	SLE RA 21	-55	-1	2734	0.28	-2.03	0
15	SLE FR 1	-45	0	2321	0.19	-1.66	0
15	SLE FR 2	-45	0	2321	0.19	-1.66	0
15	SLE FR 3	-45	0	2321	0.19	-1.66	0
15	SLE FR 4	-48	0	2445	0.22	-1.77	0
15	SLE FR 5	-48	0	2445	0.22	-1.77	0
15	SLE FR 6	-50	-1	2528	0.23	-1.85	0
15	SLE QP 1	-45	0	2321	0.19	-1.66	0
15	SLE QP 2	-48	0	2445	0.22	-1.77	0
15	SLD 1	197	119	2462	-48.83	8.51	-0.4
15	SLD 2	197	119	2462	-48.83	8.51	-0.4



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
15	SLD 3	226	-231	2362	99.01	9.72	0.75
15	SLD 4	226	-231	2362	99.01	9.72	0.75
15	SLD 5	-19	566	2600	-238.73	-0.51	-1.86
15	SLD 6	-19	566	2600	-238.73	-0.51	-1.86
15	SLD 7	78	-601	2270	254.09	3.5	1.96
15	SLD 8	78	-601	2270	254.09	3.5	1.96
15	SLD 9	-175	600	2620	-253.65	-7.04	-1.96
15	SLD 10	-175	600	2620	-253.65	-7.04	-1.96
15	SLD 11	-78	-567	2290	239.17	-3.03	1.86
15	SLD 12	-78	-567	2290	239.17	-3.03	1.86
15	SLD 13	-323	230	2528	-98.57	-13.26	-0.75
15	SLD 14	-323	230	2528	-98.57	-13.26	-0.75
15	SLD 15	-294	-120	2429	49.27	-12.05	0.4
15	SLD 16	-294	-120	2429	49.27	-12.05	0.4
15	SLV 1	528	306	2491	-125.64	22.37	-1.02
15	SLV 2	528	306	2491	-125.64	22.37	-1.02
15	SLV 3	597	-593	2237	253.65	25.23	1.92
15	SLV 4	597	-593	2237	253.65	25.23	1.92
15	SLV 5	19	1454	2844	-612.8	1.14	-4.76
15	SLV 6	19	1454	2844	-612.8	1.14	-4.76
15	SLV 7	251	-1541	1998	651.51	10.66	5.03
15	SLV 8	251	-1541	1998	651.51	10.66	5.03
15	SLV 9	-347	1540	2893	-651.07	-14.2	-5.03
15	SLV 10	-347	1540	2893	-651.07	-14.2	-5.03
15	SLV 11	-116	-1455	2046	613.24	-4.68	4.76
15	SLV 12	-116	-1455	2046	613.24	-4.68	4.76
15	SLV 13	-694	592	2653	-253.22	-28.77	-1.92
15	SLV 14	-694	592	2653	-253.22	-28.77	-1.92
15	SLV 15	-624	-307	2399	126.08	-25.91	1.02
15	SLV 16	-624	-307	2399	126.08	-25.91	1.02
16	SLU 1	-105	0	2203	0.13	-4.18	0
16	SLU 2	-105	0	2203	0.13	-4.18	0
16	SLU 3	-105	0	2203	0.13	-4.18	0
16	SLU 4	-105	0	2203	0.13	-4.18	0
16	SLU 5	-105	0	2203	0.13	-4.18	0
16	SLU 6	-105	0	2203	0.13	-4.18	0
16	SLU 7	-105	0	2203	0.13	-4.18	0
16	SLU 8	-105	0	2203	0.13	-4.18	0
16	SLU 9	-105	0	2203	0.13	-4.18	0
16	SLU 10	-131	-1	2627	0.21	-5.21	0
16	SLU 11	-131	-1	2627	0.21	-5.21	0
16	SLU 12	-131	-1	2627	0.21	-5.21	0
16	SLU 13	-131	-1	2627	0.21	-5.21	0
16	SLU 14	-131	-1	2627	0.21	-5.21	0
16	SLU 15	-131	-1	2627	0.21	-5.21	0
16	SLU 16	-131	-1	2627	0.21	-5.21	0
16	SLU 17	-131	-1	2627	0.21	-5.21	0
16	SLU 18	-142	-1	2809	0.24	-5.65	0
16	SLU 19	-142	-1	2809	0.24	-5.65	0
16	SLU 20	-142	-1	2809	0.24	-5.65	0
16	SLU 21	-142	-1	2809	0.24	-5.65	0
16	SLU 22	-120	0	2466	0.17	-4.8	0
16	SLU 23	-120	0	2466	0.17	-4.8	0
16	SLU 24	-120	0	2466	0.17	-4.8	0
16	SLU 25	-120	0	2466	0.17	-4.8	0
16	SLU 26	-120	0	2466	0.17	-4.8	0
16	SLU 27	-120	0	2466	0.17	-4.8	0
16	SLU 28	-120	0	2466	0.17	-4.8	0
16	SLU 29	-120	0	2466	0.17	-4.8	0
16	SLU 30	-120	0	2466	0.17	-4.8	0
16	SLU 31	-146	-1	2890	0.25	-5.82	0
16	SLU 32	-146	-1	2890	0.25	-5.82	0
16	SLU 33	-146	-1	2890	0.25	-5.82	0
16	SLU 34	-146	-1	2890	0.25	-5.82	0
16	SLU 35	-146	-1	2890	0.25	-5.82	0
16	SLU 36	-146	-1	2890	0.25	-5.82	0
16	SLU 37	-146	-1	2890	0.25	-5.82	0
16	SLU 38	-146	-1	2890	0.25	-5.82	0
16	SLU 39	-157	-1	3071	0.28	-6.26	0
16	SLU 40	-157	-1	3071	0.28	-6.26	0
16	SLU 41	-157	-1	3071	0.28	-6.26	0
16	SLU 42	-157	-1	3071	0.28	-6.26	0
16	SLU 43	-131	0	2773	0.16	-5.23	0
16	SLU 44	-131	0	2773	0.16	-5.23	0
16	SLU 45	-131	0	2773	0.16	-5.23	0
16	SLU 46	-131	0	2773	0.16	-5.23	0
16	SLU 47	-131	0	2773	0.16	-5.23	0
16	SLU 48	-131	0	2773	0.16	-5.23	0
16	SLU 49	-131	0	2773	0.16	-5.23	0
16	SLU 50	-131	0	2773	0.16	-5.23	0
16	SLU 51	-131	0	2773	0.16	-5.23	0
16	SLU 52	-157	-1	3197	0.23	-6.25	0
16	SLU 53	-157	-1	3197	0.23	-6.25	0
16	SLU 54	-157	-1	3197	0.23	-6.25	0
16	SLU 55	-157	-1	3197	0.23	-6.25	0
16	SLU 56	-157	-1	3197	0.23	-6.25	0
16	SLU 57	-157	-1	3197	0.23	-6.25	0
16	SLU 58	-157	-1	3197	0.23	-6.25	0
16	SLU 59	-157	-1	3197	0.23	-6.25	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
16	SLU 60	-168	-1	3379	0.27	-6.69	0
16	SLU 61	-168	-1	3379	0.27	-6.69	0
16	SLU 62	-168	-1	3379	0.27	-6.69	0
16	SLU 63	-168	-1	3379	0.27	-6.69	0
16	SLU 64	-147	0	3036	0.2	-5.84	0
16	SLU 65	-147	0	3036	0.2	-5.84	0
16	SLU 66	-147	0	3036	0.2	-5.84	0
16	SLU 67	-147	0	3036	0.2	-5.84	0
16	SLU 68	-147	0	3036	0.2	-5.84	0
16	SLU 69	-147	0	3036	0.2	-5.84	0
16	SLU 70	-147	0	3036	0.2	-5.84	0
16	SLU 71	-147	0	3036	0.2	-5.84	0
16	SLU 72	-147	0	3036	0.2	-5.84	0
16	SLU 73	-172	-1	3460	0.27	-6.86	0
16	SLU 74	-172	-1	3460	0.27	-6.86	0
16	SLU 75	-172	-1	3460	0.27	-6.86	0
16	SLU 76	-172	-1	3460	0.27	-6.86	0
16	SLU 77	-172	-1	3460	0.27	-6.86	0
16	SLU 78	-172	-1	3460	0.27	-6.86	0
16	SLU 79	-172	-1	3460	0.27	-6.86	0
16	SLU 80	-172	-1	3460	0.27	-6.86	0
16	SLU 81	-183	-1	3642	0.31	-7.3	0
16	SLU 82	-183	-1	3642	0.31	-7.3	0
16	SLU 83	-183	-1	3642	0.31	-7.3	0
16	SLU 84	-183	-1	3642	0.31	-7.3	0
16	SLE RA 1	-109	0	2278	0.14	-4.36	0
16	SLE RA 2	-109	0	2278	0.14	-4.36	0
16	SLE RA 3	-109	0	2278	0.14	-4.36	0
16	SLE RA 4	-109	0	2278	0.14	-4.36	0
16	SLE RA 5	-109	0	2278	0.14	-4.36	0
16	SLE RA 6	-109	0	2278	0.14	-4.36	0
16	SLE RA 7	-109	0	2278	0.14	-4.36	0
16	SLE RA 8	-109	0	2278	0.14	-4.36	0
16	SLE RA 9	-109	0	2278	0.14	-4.36	0
16	SLE RA 10	-127	0	2561	0.19	-5.04	0
16	SLE RA 11	-127	0	2561	0.19	-5.04	0
16	SLE RA 12	-127	0	2561	0.19	-5.04	0
16	SLE RA 13	-127	0	2561	0.19	-5.04	0
16	SLE RA 14	-127	0	2561	0.19	-5.04	0
16	SLE RA 15	-127	0	2561	0.19	-5.04	0
16	SLE RA 16	-127	0	2561	0.19	-5.04	0
16	SLE RA 17	-127	0	2561	0.19	-5.04	0
16	SLE RA 18	-134	-1	2682	0.22	-5.33	0
16	SLE RA 19	-134	-1	2682	0.22	-5.33	0
16	SLE RA 20	-134	-1	2682	0.22	-5.33	0
16	SLE RA 21	-134	-1	2682	0.22	-5.33	0
16	SLE FR 1	-109	0	2278	0.14	-4.36	0
16	SLE FR 2	-109	0	2278	0.14	-4.36	0
16	SLE FR 3	-109	0	2278	0.14	-4.36	0
16	SLE FR 4	-117	0	2399	0.16	-4.65	0
16	SLE FR 5	-117	0	2399	0.16	-4.65	0
16	SLE FR 6	-122	0	2480	0.18	-4.85	0
16	SLE QP 1	-109	0	2278	0.14	-4.36	0
16	SLE QP 2	-117	0	2399	0.16	-4.65	0
16	SLD 1	123	18	2389	-23.44	5.34	0.11
16	SLD 2	123	18	2389	-23.44	5.34	0.11
16	SLD 3	156	-57	2297	63.72	6.65	-0.25
16	SLD 4	156	-57	2297	63.72	6.65	-0.25
16	SLD 5	-94	118	2535	-139.11	-3.64	0.58
16	SLD 6	-94	118	2535	-139.11	-3.64	0.58
16	SLD 7	15	-130	2229	151.43	0.73	-0.62
16	SLD 8	15	-130	2229	151.43	0.73	-0.62
16	SLD 9	-248	130	2569	-151.1	-10.03	0.62
16	SLD 10	-248	130	2569	-151.1	-10.03	0.62
16	SLD 11	-139	-119	2263	139.44	-5.66	-0.58
16	SLD 12	-139	-119	2263	139.44	-5.66	-0.58
16	SLD 13	-389	56	2501	-63.39	-15.95	0.25
16	SLD 14	-389	56	2501	-63.39	-15.95	0.25
16	SLD 15	-357	-18	2409	23.77	-14.64	-0.11
16	SLD 16	-357	-18	2409	23.77	-14.64	-0.11
16	SLV 1	446	46	2382	-60.53	18.79	0.29
16	SLV 2	446	46	2382	-60.53	18.79	0.29
16	SLV 3	525	-145	2147	163.07	21.94	-0.63
16	SLV 4	525	-145	2147	163.07	21.94	-0.63
16	SLV 5	-68	304	2750	-357.17	-2.4	1.48
16	SLV 6	-68	304	2750	-357.17	-2.4	1.48
16	SLV 7	196	-334	1967	388.16	8.11	-1.58
16	SLV 8	196	-334	1967	388.16	8.11	-1.58
16	SLV 9	-429	333	2831	-387.83	-17.41	1.58
16	SLV 10	-429	333	2831	-387.83	-17.41	1.58
16	SLV 11	-165	-305	2048	357.49	-6.9	-1.48
16	SLV 12	-165	-305	2048	357.49	-6.9	-1.48
16	SLV 13	-758	144	2651	-162.74	-31.24	0.63
16	SLV 14	-758	144	2651	-162.74	-31.24	0.63
16	SLV 15	-679	-47	2416	60.86	-28.09	-0.29
16	SLV 16	-679	-47	2416	60.86	-28.09	-0.29
17	SLU 1	-171	0	2105	0.08	-6.03	0
17	SLU 2	-171	0	2105	0.08	-6.03	0
17	SLU 3	-171	0	2105	0.08	-6.03	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
17	SLU 4	-171	0	2105	0.08	-6.03	0
17	SLU 5	-171	0	2105	0.08	-6.03	0
17	SLU 6	-171	0	2105	0.08	-6.03	0
17	SLU 7	-171	0	2105	0.08	-6.03	0
17	SLU 8	-171	0	2105	0.08	-6.03	0
17	SLU 9	-171	0	2105	0.08	-6.03	0
17	SLU 10	-213	0	2505	0.12	-7.53	0
17	SLU 11	-213	0	2505	0.12	-7.53	0
17	SLU 12	-213	0	2505	0.12	-7.53	0
17	SLU 13	-213	0	2505	0.12	-7.53	0
17	SLU 14	-213	0	2505	0.12	-7.53	0
17	SLU 15	-213	0	2505	0.12	-7.53	0
17	SLU 16	-213	0	2505	0.12	-7.53	0
17	SLU 17	-213	0	2505	0.12	-7.53	0
17	SLU 18	-231	0	2677	0.14	-8.17	0
17	SLU 19	-231	0	2677	0.14	-8.17	0
17	SLU 20	-231	0	2677	0.14	-8.17	0
17	SLU 21	-231	0	2677	0.14	-8.17	0
17	SLU 22	-196	0	2353	0.1	-6.93	0
17	SLU 23	-196	0	2353	0.1	-6.93	0
17	SLU 24	-196	0	2353	0.1	-6.93	0
17	SLU 25	-196	0	2353	0.1	-6.93	0
17	SLU 26	-196	0	2353	0.1	-6.93	0
17	SLU 27	-196	0	2353	0.1	-6.93	0
17	SLU 28	-196	0	2353	0.1	-6.93	0
17	SLU 29	-196	0	2353	0.1	-6.93	0
17	SLU 30	-196	0	2353	0.1	-6.93	0
17	SLU 31	-238	0	2753	0.15	-8.43	0
17	SLU 32	-238	0	2753	0.15	-8.43	0
17	SLU 33	-238	0	2753	0.15	-8.43	0
17	SLU 34	-238	0	2753	0.15	-8.43	0
17	SLU 35	-238	0	2753	0.15	-8.43	0
17	SLU 36	-238	0	2753	0.15	-8.43	0
17	SLU 37	-238	0	2753	0.15	-8.43	0
17	SLU 38	-238	0	2753	0.15	-8.43	0
17	SLU 39	-257	0	2925	0.17	-9.07	0
17	SLU 40	-257	0	2925	0.17	-9.07	0
17	SLU 41	-257	0	2925	0.17	-9.07	0
17	SLU 42	-257	0	2925	0.17	-9.07	0
17	SLU 43	-214	0	2651	0.09	-7.54	0
17	SLU 44	-214	0	2651	0.09	-7.54	0
17	SLU 45	-214	0	2651	0.09	-7.54	0
17	SLU 46	-214	0	2651	0.09	-7.54	0
17	SLU 47	-214	0	2651	0.09	-7.54	0
17	SLU 48	-214	0	2651	0.09	-7.54	0
17	SLU 49	-214	0	2651	0.09	-7.54	0
17	SLU 50	-214	0	2651	0.09	-7.54	0
17	SLU 51	-214	0	2651	0.09	-7.54	0
17	SLU 52	-256	0	3052	0.14	-9.03	0
17	SLU 53	-256	0	3052	0.14	-9.03	0
17	SLU 54	-256	0	3052	0.14	-9.03	0
17	SLU 55	-256	0	3052	0.14	-9.03	0
17	SLU 56	-256	0	3052	0.14	-9.03	0
17	SLU 57	-256	0	3052	0.14	-9.03	0
17	SLU 58	-256	0	3052	0.14	-9.03	0
17	SLU 59	-256	0	3052	0.14	-9.03	0
17	SLU 60	-274	0	3223	0.16	-9.68	0
17	SLU 61	-274	0	3223	0.16	-9.68	0
17	SLU 62	-274	0	3223	0.16	-9.68	0
17	SLU 63	-274	0	3223	0.16	-9.68	0
17	SLU 64	-239	0	2899	0.12	-8.43	0
17	SLU 65	-239	0	2899	0.12	-8.43	0
17	SLU 66	-239	0	2899	0.12	-8.43	0
17	SLU 67	-239	0	2899	0.12	-8.43	0
17	SLU 68	-239	0	2899	0.12	-8.43	0
17	SLU 69	-239	0	2899	0.12	-8.43	0
17	SLU 70	-239	0	2899	0.12	-8.43	0
17	SLU 71	-239	0	2899	0.12	-8.43	0
17	SLU 72	-239	0	2899	0.12	-8.43	0
17	SLU 73	-281	0	3300	0.16	-9.93	0
17	SLU 74	-281	0	3300	0.16	-9.93	0
17	SLU 75	-281	0	3300	0.16	-9.93	0
17	SLU 76	-281	0	3300	0.16	-9.93	0
17	SLU 77	-281	0	3300	0.16	-9.93	0
17	SLU 78	-281	0	3300	0.16	-9.93	0
17	SLU 79	-281	0	3300	0.16	-9.93	0
17	SLU 80	-281	0	3300	0.16	-9.93	0
17	SLU 81	-299	-1	3471	0.18	-10.57	0
17	SLU 82	-299	-1	3471	0.18	-10.57	0
17	SLU 83	-299	-1	3471	0.18	-10.57	0
17	SLU 84	-299	-1	3471	0.18	-10.57	0
17	SLE RA 1	-178	0	2176	0.09	-6.29	0
17	SLE RA 2	-178	0	2176	0.09	-6.29	0
17	SLE RA 3	-178	0	2176	0.09	-6.29	0
17	SLE RA 4	-178	0	2176	0.09	-6.29	0
17	SLE RA 5	-178	0	2176	0.09	-6.29	0
17	SLE RA 6	-178	0	2176	0.09	-6.29	0
17	SLE RA 7	-178	0	2176	0.09	-6.29	0
17	SLE RA 8	-178	0	2176	0.09	-6.29	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
17	SLE RA 9	-178	0	2176	0.09	-6.29	0
17	SLE RA 10	-206	0	2443	0.12	-7.29	0
17	SLE RA 11	-206	0	2443	0.12	-7.29	0
17	SLE RA 12	-206	0	2443	0.12	-7.29	0
17	SLE RA 13	-206	0	2443	0.12	-7.29	0
17	SLE RA 14	-206	0	2443	0.12	-7.29	0
17	SLE RA 15	-206	0	2443	0.12	-7.29	0
17	SLE RA 16	-206	0	2443	0.12	-7.29	0
17	SLE RA 17	-206	0	2443	0.12	-7.29	0
17	SLE RA 18	-218	0	2557	0.13	-7.72	0
17	SLE RA 19	-218	0	2557	0.13	-7.72	0
17	SLE RA 20	-218	0	2557	0.13	-7.72	0
17	SLE RA 21	-218	0	2557	0.13	-7.72	0
17	SLE FR 1	-178	0	2176	0.09	-6.29	0
17	SLE FR 2	-178	0	2176	0.09	-6.29	0
17	SLE FR 3	-178	0	2176	0.09	-6.29	0
17	SLE FR 4	-190	0	2290	0.1	-6.72	0
17	SLE FR 5	-190	0	2290	0.1	-6.72	0
17	SLE FR 6	-198	0	2366	0.11	-7	0
17	SLE QP 1	-178	0	2176	0.09	-6.29	0
17	SLE QP 2	-190	0	2290	0.1	-6.72	0
17	SLD 1	52	-1	2251	-8.93	3.44	0.05
17	SLD 2	52	-1	2251	-8.93	3.44	0.05
17	SLD 3	89	-40	2172	52.07	4.93	-0.02
17	SLD 4	89	-40	2172	52.07	4.93	-0.02
17	SLD 5	-173	58	2399	-95.13	-5.94	0.11
17	SLD 6	-173	58	2399	-95.13	-5.94	0.11
17	SLD 7	-51	-71	2134	108.21	-0.96	-0.1
17	SLD 8	-51	-71	2134	108.21	-0.96	-0.1
17	SLD 9	-330	70	2446	-108.01	-12.48	0.1
17	SLD 10	-330	70	2446	-108.01	-12.48	0.1
17	SLD 11	-207	-59	2181	95.33	-7.5	-0.11
17	SLD 12	-207	-59	2181	95.33	-7.5	-0.11
17	SLD 13	-469	39	2408	-51.87	-18.37	0.02
17	SLD 14	-469	39	2408	-51.87	-18.37	0.02
17	SLD 15	-433	0	2329	9.13	-16.88	-0.05
17	SLD 16	-433	0	2329	9.13	-16.88	-0.05
17	SLV 1	377	-1	2206	-23.37	17.09	0.12
17	SLV 2	377	-1	2206	-23.37	17.09	0.12
17	SLV 3	467	-101	2003	133.08	20.72	-0.04
17	SLV 4	467	-101	2003	133.08	20.72	-0.04
17	SLV 5	-155	150	2573	-244.23	-5.08	0.29
17	SLV 6	-155	150	2573	-244.23	-5.08	0.29
17	SLV 7	142	-181	1896	277.28	7.02	-0.27
17	SLV 8	142	-181	1896	277.28	7.02	-0.27
17	SLV 9	-523	180	2684	-277.08	-20.45	0.27
17	SLV 10	-523	180	2684	-277.08	-20.45	0.27
17	SLV 11	-225	-150	2007	244.43	-8.36	-0.29
17	SLV 12	-225	-150	2007	244.43	-8.36	-0.29
17	SLV 13	-847	100	2577	-132.89	-34.15	0.04
17	SLV 14	-847	100	2577	-132.89	-34.15	0.04
17	SLV 15	-758	1	2374	23.57	-30.52	-0.12
17	SLV 16	-758	1	2374	23.57	-30.52	-0.12
18	SLU 1	-230	0	1939	0.02	-8.73	0
18	SLU 2	-230	0	1939	0.02	-8.73	0
18	SLU 3	-230	0	1939	0.02	-8.73	0
18	SLU 4	-230	0	1939	0.02	-8.73	0
18	SLU 5	-230	0	1939	0.02	-8.73	0
18	SLU 6	-230	0	1939	0.02	-8.73	0
18	SLU 7	-230	0	1939	0.02	-8.73	0
18	SLU 8	-230	0	1939	0.02	-8.73	0
18	SLU 9	-230	0	1939	0.02	-8.73	0
18	SLU 10	-286	0	2299	0.03	-10.84	0
18	SLU 11	-286	0	2299	0.03	-10.84	0
18	SLU 12	-286	0	2299	0.03	-10.84	0
18	SLU 13	-286	0	2299	0.03	-10.84	0
18	SLU 14	-286	0	2299	0.03	-10.84	0
18	SLU 15	-286	0	2299	0.03	-10.84	0
18	SLU 16	-286	0	2299	0.03	-10.84	0
18	SLU 17	-286	0	2299	0.03	-10.84	0
18	SLU 18	-310	0	2454	0.03	-11.75	0
18	SLU 19	-310	0	2454	0.03	-11.75	0
18	SLU 20	-310	0	2454	0.03	-11.75	0
18	SLU 21	-310	0	2454	0.03	-11.75	0
18	SLU 22	-265	0	2162	0.03	-10.03	0
18	SLU 23	-265	0	2162	0.03	-10.03	0
18	SLU 24	-265	0	2162	0.03	-10.03	0
18	SLU 25	-265	0	2162	0.03	-10.03	0
18	SLU 26	-265	0	2162	0.03	-10.03	0
18	SLU 27	-265	0	2162	0.03	-10.03	0
18	SLU 28	-265	0	2162	0.03	-10.03	0
18	SLU 29	-265	0	2162	0.03	-10.03	0
18	SLU 30	-265	0	2162	0.03	-10.03	0
18	SLU 31	-321	0	2522	0.04	-12.14	0
18	SLU 32	-321	0	2522	0.04	-12.14	0
18	SLU 33	-321	0	2522	0.04	-12.14	0
18	SLU 34	-321	0	2522	0.04	-12.14	0
18	SLU 35	-321	0	2522	0.04	-12.14	0
18	SLU 36	-321	0	2522	0.04	-12.14	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
18	SLU 37	-321	0	2522	0.04	-12.14	0
18	SLU 38	-321	0	2522	0.04	-12.14	0
18	SLU 39	-345	0	2677	0.04	-13.05	0
18	SLU 40	-345	0	2677	0.04	-13.05	0
18	SLU 41	-345	0	2677	0.04	-13.05	0
18	SLU 42	-345	0	2677	0.04	-13.05	0
18	SLU 43	-287	0	2444	0.03	-10.9	0
18	SLU 44	-287	0	2444	0.03	-10.9	0
18	SLU 45	-287	0	2444	0.03	-10.9	0
18	SLU 46	-287	0	2444	0.03	-10.9	0
18	SLU 47	-287	0	2444	0.03	-10.9	0
18	SLU 48	-287	0	2444	0.03	-10.9	0
18	SLU 49	-287	0	2444	0.03	-10.9	0
18	SLU 50	-287	0	2444	0.03	-10.9	0
18	SLU 51	-287	0	2444	0.03	-10.9	0
18	SLU 52	-343	0	2804	0.04	-13.02	0
18	SLU 53	-343	0	2804	0.04	-13.02	0
18	SLU 54	-343	0	2804	0.04	-13.02	0
18	SLU 55	-343	0	2804	0.04	-13.02	0
18	SLU 56	-343	0	2804	0.04	-13.02	0
18	SLU 57	-343	0	2804	0.04	-13.02	0
18	SLU 58	-343	0	2804	0.04	-13.02	0
18	SLU 59	-343	0	2804	0.04	-13.02	0
18	SLU 60	-367	0	2959	0.04	-13.92	0
18	SLU 61	-367	0	2959	0.04	-13.92	0
18	SLU 62	-367	0	2959	0.04	-13.92	0
18	SLU 63	-367	0	2959	0.04	-13.92	0
18	SLU 64	-322	0	2667	0.03	-12.2	0
18	SLU 65	-322	0	2667	0.03	-12.2	0
18	SLU 66	-322	0	2667	0.03	-12.2	0
18	SLU 67	-322	0	2667	0.03	-12.2	0
18	SLU 68	-322	0	2667	0.03	-12.2	0
18	SLU 69	-322	0	2667	0.03	-12.2	0
18	SLU 70	-322	0	2667	0.03	-12.2	0
18	SLU 71	-322	0	2667	0.03	-12.2	0
18	SLU 72	-322	0	2667	0.03	-12.2	0
18	SLU 73	-378	0	3028	0.04	-14.32	0
18	SLU 74	-378	0	3028	0.04	-14.32	0
18	SLU 75	-378	0	3028	0.04	-14.32	0
18	SLU 76	-378	0	3028	0.04	-14.32	0
18	SLU 77	-378	0	3028	0.04	-14.32	0
18	SLU 78	-378	0	3028	0.04	-14.32	0
18	SLU 79	-378	0	3028	0.04	-14.32	0
18	SLU 80	-378	0	3028	0.04	-14.32	0
18	SLU 81	-402	0	3182	0.04	-15.22	0
18	SLU 82	-402	0	3182	0.04	-15.22	0
18	SLU 83	-402	0	3182	0.04	-15.22	0
18	SLU 84	-402	0	3182	0.04	-15.22	0
18	SLE RA 1	-240	0	2003	0.03	-9.1	0
18	SLE RA 2	-240	0	2003	0.03	-9.1	0
18	SLE RA 3	-240	0	2003	0.03	-9.1	0
18	SLE RA 4	-240	0	2003	0.03	-9.1	0
18	SLE RA 5	-240	0	2003	0.03	-9.1	0
18	SLE RA 6	-240	0	2003	0.03	-9.1	0
18	SLE RA 7	-240	0	2003	0.03	-9.1	0
18	SLE RA 8	-240	0	2003	0.03	-9.1	0
18	SLE RA 9	-240	0	2003	0.03	-9.1	0
18	SLE RA 10	-277	0	2243	0.03	-10.51	0
18	SLE RA 11	-277	0	2243	0.03	-10.51	0
18	SLE RA 12	-277	0	2243	0.03	-10.51	0
18	SLE RA 13	-277	0	2243	0.03	-10.51	0
18	SLE RA 14	-277	0	2243	0.03	-10.51	0
18	SLE RA 15	-277	0	2243	0.03	-10.51	0
18	SLE RA 16	-277	0	2243	0.03	-10.51	0
18	SLE RA 17	-277	0	2243	0.03	-10.51	0
18	SLE RA 18	-293	0	2346	0.03	-11.11	0
18	SLE RA 19	-293	0	2346	0.03	-11.11	0
18	SLE RA 20	-293	0	2346	0.03	-11.11	0
18	SLE RA 21	-293	0	2346	0.03	-11.11	0
18	SLE FR 1	-240	0	2003	0.03	-9.1	0
18	SLE FR 2	-240	0	2003	0.03	-9.1	0
18	SLE FR 3	-240	0	2003	0.03	-9.1	0
18	SLE FR 4	-256	0	2106	0.03	-9.7	0
18	SLE FR 5	-256	0	2106	0.03	-9.7	0
18	SLE FR 6	-267	0	2174	0.03	-10.11	0
18	SLE QP 1	-240	0	2003	0.03	-9.1	0
18	SLE QP 2	-256	0	2106	0.03	-9.7	0
18	SLD 1	-8	-10	2049	0.57	0.12	0.02
18	SLD 2	-8	-10	2049	0.57	0.12	0.02
18	SLD 3	31	-37	1984	47.56	1.6	0.01
18	SLD 4	31	-37	1984	47.56	1.6	0.01
18	SLD 5	-241	37	2187	-71.08	-9	0.02
18	SLD 6	-241	37	2187	-71.08	-9	0.02
18	SLD 7	-110	-52	1970	85.56	-4.07	-0.01
18	SLD 8	-110	-52	1970	85.56	-4.07	-0.01
18	SLD 9	-402	51	2241	-85.5	-15.34	0.01
18	SLD 10	-402	51	2241	-85.5	-15.34	0.01
18	SLD 11	-271	-38	2024	71.14	-10.4	-0.02
18	SLD 12	-271	-38	2024	71.14	-10.4	-0.02



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
18	SLD 13	-543	37	2227	-47.51	-21.01	-0.01
18	SLD 14	-543	37	2227	-47.51	-21.01	-0.01
18	SLD 15	-504	10	2162	-0.51	-19.53	-0.02
18	SLD 16	-504	10	2162	-0.51	-19.53	-0.02
18	SLV 1	324	-26	1978	1.04	13.32	0.05
18	SLV 2	324	-26	1978	1.04	13.32	0.05
18	SLV 3	420	-94	1812	121.48	16.92	0.03
18	SLV 4	420	-94	1812	121.48	16.92	0.03
18	SLV 5	-228	95	2320	-182.33	-8.27	0.05
18	SLV 6	-228	95	2320	-182.33	-8.27	0.05
18	SLV 7	92	-132	1765	219.13	3.75	-0.03
18	SLV 8	92	-132	1765	219.13	3.75	-0.03
18	SLV 9	-604	131	2446	-219.07	-23.16	0.03
18	SLV 10	-604	131	2446	-219.07	-23.16	0.03
18	SLV 11	-284	-96	1891	182.38	-11.14	-0.05
18	SLV 12	-284	-96	1891	182.38	-11.14	-0.05
18	SLV 13	-932	94	2400	-121.43	-36.33	-0.03
18	SLV 14	-932	94	2400	-121.43	-36.33	-0.03
18	SLV 15	-836	26	2233	-0.99	-32.73	-0.05
18	SLV 16	-836	26	2233	-0.99	-32.73	-0.05
19	SLU 1	-221	0	1756	-0.02	-8.58	0
19	SLU 2	-221	0	1756	-0.02	-8.58	0
19	SLU 3	-221	0	1756	-0.02	-8.58	0
19	SLU 4	-221	0	1756	-0.02	-8.58	0
19	SLU 5	-221	0	1756	-0.02	-8.58	0
19	SLU 6	-221	0	1756	-0.02	-8.58	0
19	SLU 7	-221	0	1756	-0.02	-8.58	0
19	SLU 8	-221	0	1756	-0.02	-8.58	0
19	SLU 9	-221	0	1756	-0.02	-8.58	0
19	SLU 10	-275	0	2071	-0.05	-10.66	0
19	SLU 11	-275	0	2071	-0.05	-10.66	0
19	SLU 12	-275	0	2071	-0.05	-10.66	0
19	SLU 13	-275	0	2071	-0.05	-10.66	0
19	SLU 14	-275	0	2071	-0.05	-10.66	0
19	SLU 15	-275	0	2071	-0.05	-10.66	0
19	SLU 16	-275	0	2071	-0.05	-10.66	0
19	SLU 17	-275	0	2071	-0.05	-10.66	0
19	SLU 18	-298	0	2207	-0.06	-11.55	0
19	SLU 19	-298	0	2207	-0.06	-11.55	0
19	SLU 20	-298	0	2207	-0.06	-11.55	0
19	SLU 21	-298	0	2207	-0.06	-11.55	0
19	SLU 22	-255	0	1951	-0.03	-9.87	0
19	SLU 23	-255	0	1951	-0.03	-9.87	0
19	SLU 24	-255	0	1951	-0.03	-9.87	0
19	SLU 25	-255	0	1951	-0.03	-9.87	0
19	SLU 26	-255	0	1951	-0.03	-9.87	0
19	SLU 27	-255	0	1951	-0.03	-9.87	0
19	SLU 28	-255	0	1951	-0.03	-9.87	0
19	SLU 29	-255	0	1951	-0.03	-9.87	0
19	SLU 30	-255	0	1951	-0.03	-9.87	0
19	SLU 31	-309	0	2266	-0.06	-11.94	0
19	SLU 32	-309	0	2266	-0.06	-11.94	0
19	SLU 33	-309	0	2266	-0.06	-11.94	0
19	SLU 34	-309	0	2266	-0.06	-11.94	0
19	SLU 35	-309	0	2266	-0.06	-11.94	0
19	SLU 36	-309	0	2266	-0.06	-11.94	0
19	SLU 37	-309	0	2266	-0.06	-11.94	0
19	SLU 38	-309	0	2266	-0.06	-11.94	0
19	SLU 39	-332	0	2402	-0.07	-12.83	0
19	SLU 40	-332	0	2402	-0.07	-12.83	0
19	SLU 41	-332	0	2402	-0.07	-12.83	0
19	SLU 42	-332	0	2402	-0.07	-12.83	0
19	SLU 43	-276	0	2215	-0.03	-10.71	0
19	SLU 44	-276	0	2215	-0.03	-10.71	0
19	SLU 45	-276	0	2215	-0.03	-10.71	0
19	SLU 46	-276	0	2215	-0.03	-10.71	0
19	SLU 47	-276	0	2215	-0.03	-10.71	0
19	SLU 48	-276	0	2215	-0.03	-10.71	0
19	SLU 49	-276	0	2215	-0.03	-10.71	0
19	SLU 50	-276	0	2215	-0.03	-10.71	0
19	SLU 51	-276	0	2215	-0.03	-10.71	0
19	SLU 52	-330	0	2531	-0.06	-12.79	0
19	SLU 53	-330	0	2531	-0.06	-12.79	0
19	SLU 54	-330	0	2531	-0.06	-12.79	0
19	SLU 55	-330	0	2531	-0.06	-12.79	0
19	SLU 56	-330	0	2531	-0.06	-12.79	0
19	SLU 57	-330	0	2531	-0.06	-12.79	0
19	SLU 58	-330	0	2531	-0.06	-12.79	0
19	SLU 59	-330	0	2531	-0.06	-12.79	0
19	SLU 60	-353	0	2666	-0.07	-13.68	0
19	SLU 61	-353	0	2666	-0.07	-13.68	0
19	SLU 62	-353	0	2666	-0.07	-13.68	0
19	SLU 63	-353	0	2666	-0.07	-13.68	0
19	SLU 64	-310	0	2410	-0.04	-12	0
19	SLU 65	-310	0	2410	-0.04	-12	0
19	SLU 66	-310	0	2410	-0.04	-12	0
19	SLU 67	-310	0	2410	-0.04	-12	0
19	SLU 68	-310	0	2410	-0.04	-12	0
19	SLU 69	-310	0	2410	-0.04	-12	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
19	SLU 70	-310	0	2410	-0.04	-12	0
19	SLU 71	-310	0	2410	-0.04	-12	0
19	SLU 72	-310	0	2410	-0.04	-12	0
19	SLU 73	-363	0	2726	-0.06	-14.08	0
19	SLU 74	-363	0	2726	-0.06	-14.08	0
19	SLU 75	-363	0	2726	-0.06	-14.08	0
19	SLU 76	-363	0	2726	-0.06	-14.08	0
19	SLU 77	-363	0	2726	-0.06	-14.08	0
19	SLU 78	-363	0	2726	-0.06	-14.08	0
19	SLU 79	-363	0	2726	-0.06	-14.08	0
19	SLU 80	-363	0	2726	-0.06	-14.08	0
19	SLU 81	-386	0	2861	-0.08	-14.97	0
19	SLU 82	-386	0	2861	-0.08	-14.97	0
19	SLU 83	-386	0	2861	-0.08	-14.97	0
19	SLU 84	-386	0	2861	-0.08	-14.97	0
19	SLE RA 1	-231	0	1811	-0.03	-8.95	0
19	SLE RA 2	-231	0	1811	-0.03	-8.95	0
19	SLE RA 3	-231	0	1811	-0.03	-8.95	0
19	SLE RA 4	-231	0	1811	-0.03	-8.95	0
19	SLE RA 5	-231	0	1811	-0.03	-8.95	0
19	SLE RA 6	-231	0	1811	-0.03	-8.95	0
19	SLE RA 7	-231	0	1811	-0.03	-8.95	0
19	SLE RA 8	-231	0	1811	-0.03	-8.95	0
19	SLE RA 9	-231	0	1811	-0.03	-8.95	0
19	SLE RA 10	-267	0	2022	-0.05	-10.33	0
19	SLE RA 11	-267	0	2022	-0.05	-10.33	0
19	SLE RA 12	-267	0	2022	-0.05	-10.33	0
19	SLE RA 13	-267	0	2022	-0.05	-10.33	0
19	SLE RA 14	-267	0	2022	-0.05	-10.33	0
19	SLE RA 15	-267	0	2022	-0.05	-10.33	0
19	SLE RA 16	-267	0	2022	-0.05	-10.33	0
19	SLE RA 17	-267	0	2022	-0.05	-10.33	0
19	SLE RA 18	-282	0	2112	-0.05	-10.92	0
19	SLE RA 19	-282	0	2112	-0.05	-10.92	0
19	SLE RA 20	-282	0	2112	-0.05	-10.92	0
19	SLE RA 21	-282	0	2112	-0.05	-10.92	0
19	SLE FR 1	-231	0	1811	-0.03	-8.95	0
19	SLE FR 2	-231	0	1811	-0.03	-8.95	0
19	SLE FR 3	-231	0	1811	-0.03	-8.95	0
19	SLE FR 4	-246	0	1901	-0.03	-9.54	0
19	SLE FR 5	-246	0	1901	-0.03	-9.54	0
19	SLE FR 6	-256	0	1962	-0.04	-9.94	0
19	SLE QP 1	-231	0	1811	-0.03	-8.95	0
19	SLE QP 2	-246	0	1901	-0.03	-9.54	0
19	SLD 1	21	-15	1855	6.51	1.32	0.04
19	SLD 2	21	-15	1855	6.51	1.32	0.04
19	SLD 3	63	-37	1804	44.74	3.01	0.06
19	SLD 4	63	-37	1804	44.74	3.01	0.06
19	SLD 5	-231	30	1966	-56.05	-8.84	-0.02
19	SLD 6	-231	30	1966	-56.05	-8.84	-0.02
19	SLD 7	-89	-46	1794	71.38	-3.21	0.05
19	SLD 8	-89	-46	1794	71.38	-3.21	0.05
19	SLD 9	-404	46	2009	-71.45	-15.87	-0.05
19	SLD 10	-404	46	2009	-71.45	-15.87	-0.05
19	SLD 11	-262	-30	1837	55.98	-10.24	0.02
19	SLD 12	-262	-30	1837	55.98	-10.24	0.02
19	SLD 13	-556	37	1999	-44.81	-22.09	-0.06
19	SLD 14	-556	37	1999	-44.81	-22.09	-0.06
19	SLD 15	-514	15	1948	-6.58	-20.4	-0.04
19	SLD 16	-514	15	1948	-6.58	-20.4	-0.04
19	SLV 1	380	-37	1797	16.42	15.92	0.1
19	SLV 2	380	-37	1797	16.42	15.92	0.1
19	SLV 3	483	-95	1666	114.29	20.02	0.14
19	SLV 4	483	-95	1666	114.29	20.02	0.14
19	SLV 5	-215	76	2068	-143.53	-8.11	-0.04
19	SLV 6	-215	76	2068	-143.53	-8.11	-0.04
19	SLV 7	129	-116	1633	182.7	5.54	0.11
19	SLV 8	129	-116	1633	182.7	5.54	0.11
19	SLV 9	-622	116	2170	-182.77	-24.62	-0.11
19	SLV 10	-622	116	2170	-182.77	-24.62	-0.11
19	SLV 11	-278	-76	1735	143.46	-10.97	0.04
19	SLV 12	-278	-76	1735	143.46	-10.97	0.04
19	SLV 13	-976	95	2137	-114.36	-39.1	-0.14
19	SLV 14	-976	95	2137	-114.36	-39.1	-0.14
19	SLV 15	-873	37	2006	-16.49	-35	-0.1
19	SLV 16	-873	37	2006	-16.49	-35	-0.1
20	SLU 1	-155	0	1662	-0.07	-6.02	0
20	SLU 2	-155	0	1662	-0.07	-6.02	0
20	SLU 3	-155	0	1662	-0.07	-6.02	0
20	SLU 4	-155	0	1662	-0.07	-6.02	0
20	SLU 5	-155	0	1662	-0.07	-6.02	0
20	SLU 6	-155	0	1662	-0.07	-6.02	0
20	SLU 7	-155	0	1662	-0.07	-6.02	0
20	SLU 8	-155	0	1662	-0.07	-6.02	0
20	SLU 9	-155	0	1662	-0.07	-6.02	0
20	SLU 10	-192	0	1953	-0.11	-7.44	0
20	SLU 11	-192	0	1953	-0.11	-7.44	0
20	SLU 12	-192	0	1953	-0.11	-7.44	0
20	SLU 13	-192	0	1953	-0.11	-7.44	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
20	SLU 14	-192	0	1953	-0.11	-7.44	0
20	SLU 15	-192	0	1953	-0.11	-7.44	0
20	SLU 16	-192	0	1953	-0.11	-7.44	0
20	SLU 17	-192	0	1953	-0.11	-7.44	0
20	SLU 18	-208	0	2078	-0.13	-8.05	0
20	SLU 19	-208	0	2078	-0.13	-8.05	0
20	SLU 20	-208	0	2078	-0.13	-8.05	0
20	SLU 21	-208	0	2078	-0.13	-8.05	0
20	SLU 22	-179	0	1841	-0.09	-6.95	0
20	SLU 23	-179	0	1841	-0.09	-6.95	0
20	SLU 24	-179	0	1841	-0.09	-6.95	0
20	SLU 25	-179	0	1841	-0.09	-6.95	0
20	SLU 26	-179	0	1841	-0.09	-6.95	0
20	SLU 27	-179	0	1841	-0.09	-6.95	0
20	SLU 28	-179	0	1841	-0.09	-6.95	0
20	SLU 29	-179	0	1841	-0.09	-6.95	0
20	SLU 30	-179	0	1841	-0.09	-6.95	0
20	SLU 31	-216	0	2132	-0.13	-8.37	0
20	SLU 32	-216	0	2132	-0.13	-8.37	0
20	SLU 33	-216	0	2132	-0.13	-8.37	0
20	SLU 34	-216	0	2132	-0.13	-8.37	0
20	SLU 35	-216	0	2132	-0.13	-8.37	0
20	SLU 36	-216	0	2132	-0.13	-8.37	0
20	SLU 37	-216	0	2132	-0.13	-8.37	0
20	SLU 38	-216	0	2132	-0.13	-8.37	0
20	SLU 39	-232	0	2257	-0.15	-8.98	0
20	SLU 40	-232	0	2257	-0.15	-8.98	0
20	SLU 41	-232	0	2257	-0.15	-8.98	0
20	SLU 42	-232	0	2257	-0.15	-8.98	0
20	SLU 43	-193	0	2099	-0.08	-7.51	0
20	SLU 44	-193	0	2099	-0.08	-7.51	0
20	SLU 45	-193	0	2099	-0.08	-7.51	0
20	SLU 46	-193	0	2099	-0.08	-7.51	0
20	SLU 47	-193	0	2099	-0.08	-7.51	0
20	SLU 48	-193	0	2099	-0.08	-7.51	0
20	SLU 49	-193	0	2099	-0.08	-7.51	0
20	SLU 50	-193	0	2099	-0.08	-7.51	0
20	SLU 51	-193	0	2099	-0.08	-7.51	0
20	SLU 52	-230	0	2390	-0.13	-8.93	0
20	SLU 53	-230	0	2390	-0.13	-8.93	0
20	SLU 54	-230	0	2390	-0.13	-8.93	0
20	SLU 55	-230	0	2390	-0.13	-8.93	0
20	SLU 56	-230	0	2390	-0.13	-8.93	0
20	SLU 57	-230	0	2390	-0.13	-8.93	0
20	SLU 58	-230	0	2390	-0.13	-8.93	0
20	SLU 59	-230	0	2390	-0.13	-8.93	0
20	SLU 60	-246	0	2515	-0.15	-9.53	0
20	SLU 61	-246	0	2515	-0.15	-9.53	0
20	SLU 62	-246	0	2515	-0.15	-9.53	0
20	SLU 63	-246	0	2515	-0.15	-9.53	0
20	SLU 64	-217	0	2278	-0.1	-8.44	0
20	SLU 65	-217	0	2278	-0.1	-8.44	0
20	SLU 66	-217	0	2278	-0.1	-8.44	0
20	SLU 67	-217	0	2278	-0.1	-8.44	0
20	SLU 68	-217	0	2278	-0.1	-8.44	0
20	SLU 69	-217	0	2278	-0.1	-8.44	0
20	SLU 70	-217	0	2278	-0.1	-8.44	0
20	SLU 71	-217	0	2278	-0.1	-8.44	0
20	SLU 72	-217	0	2278	-0.1	-8.44	0
20	SLU 73	-254	0	2569	-0.15	-9.86	0
20	SLU 74	-254	0	2569	-0.15	-9.86	0
20	SLU 75	-254	0	2569	-0.15	-9.86	0
20	SLU 76	-254	0	2569	-0.15	-9.86	0
20	SLU 77	-254	0	2569	-0.15	-9.86	0
20	SLU 78	-254	0	2569	-0.15	-9.86	0
20	SLU 79	-254	0	2569	-0.15	-9.86	0
20	SLU 80	-254	0	2569	-0.15	-9.86	0
20	SLU 81	-270	0	2694	-0.17	-10.46	0
20	SLU 82	-270	0	2694	-0.17	-10.46	0
20	SLU 83	-270	0	2694	-0.17	-10.46	0
20	SLU 84	-270	0	2694	-0.17	-10.46	0
20	SLE RA 1	-162	0	1713	-0.07	-6.29	0
20	SLE RA 2	-162	0	1713	-0.07	-6.29	0
20	SLE RA 3	-162	0	1713	-0.07	-6.29	0
20	SLE RA 4	-162	0	1713	-0.07	-6.29	0
20	SLE RA 5	-162	0	1713	-0.07	-6.29	0
20	SLE RA 6	-162	0	1713	-0.07	-6.29	0
20	SLE RA 7	-162	0	1713	-0.07	-6.29	0
20	SLE RA 8	-162	0	1713	-0.07	-6.29	0
20	SLE RA 9	-162	0	1713	-0.07	-6.29	0
20	SLE RA 10	-186	0	1907	-0.1	-7.23	0
20	SLE RA 11	-186	0	1907	-0.1	-7.23	0
20	SLE RA 12	-186	0	1907	-0.1	-7.23	0
20	SLE RA 13	-186	0	1907	-0.1	-7.23	0
20	SLE RA 14	-186	0	1907	-0.1	-7.23	0
20	SLE RA 15	-186	0	1907	-0.1	-7.23	0
20	SLE RA 16	-186	0	1907	-0.1	-7.23	0
20	SLE RA 17	-186	0	1907	-0.1	-7.23	0
20	SLE RA 18	-197	0	1990	-0.12	-7.64	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
20	SLE RA 19	-197	0	1990	-0.12	-7.64	0
20	SLE RA 20	-197	0	1990	-0.12	-7.64	0
20	SLE RA 21	-197	0	1990	-0.12	-7.64	0
20	SLE FR 1	-162	0	1713	-0.07	-6.29	0
20	SLE FR 2	-162	0	1713	-0.07	-6.29	0
20	SLE FR 3	-162	0	1713	-0.07	-6.29	0
20	SLE FR 4	-172	0	1796	-0.09	-6.69	0
20	SLE FR 5	-172	0	1796	-0.09	-6.69	0
20	SLE FR 6	-179	0	1852	-0.09	-6.96	0
20	SLE QP 1	-162	0	1713	-0.07	-6.29	0
20	SLE QP 2	-172	0	1796	-0.09	-6.69	0
20	SLD 1	91	37	1780	-41.56	3.67	0.03
20	SLD 2	91	37	1780	-41.56	3.67	0.03
20	SLD 3	134	15	1735	-9.7	5.28	0.02
20	SLD 4	134	15	1735	-9.7	5.28	0.02
20	SLD 5	-158	43	1859	-60.85	-6.02	0.02
20	SLD 6	-158	43	1859	-60.85	-6.02	0.02
20	SLD 7	-16	-28	1710	45.36	-0.66	-0.01
20	SLD 8	-16	-28	1710	45.36	-0.66	-0.01
20	SLD 9	-329	28	1882	-45.53	-12.72	0.01
20	SLD 10	-329	28	1882	-45.53	-12.72	0.01
20	SLD 11	-186	-43	1734	60.68	-7.36	-0.02
20	SLD 12	-186	-43	1734	60.68	-7.36	-0.02
20	SLD 13	-479	-15	1857	9.53	-18.66	-0.02
20	SLD 14	-479	-15	1857	9.53	-18.66	-0.02
20	SLD 15	-436	-37	1812	41.39	-17.06	-0.03
20	SLD 16	-436	-37	1812	41.39	-17.06	-0.03
20	SLV 1	446	93	1759	-105.98	17.62	0.08
20	SLV 2	446	93	1759	-105.98	17.62	0.08
20	SLV 3	549	39	1649	-24.52	21.48	0.05
20	SLV 4	549	39	1649	-24.52	21.48	0.05
20	SLV 5	-143	110	1952	-155.39	-5.26	0.05
20	SLV 6	-143	110	1952	-155.39	-5.26	0.05
20	SLV 7	200	-70	1585	116.12	7.62	-0.02
20	SLV 8	200	-70	1585	116.12	7.62	-0.02
20	SLV 9	-545	70	2007	-116.29	-21	0.02
20	SLV 10	-545	70	2007	-116.29	-21	0.02
20	SLV 11	-202	-110	1640	155.22	-8.12	-0.05
20	SLV 12	-202	-110	1640	155.22	-8.12	-0.05
20	SLV 13	-893	-39	1943	24.35	-34.86	-0.05
20	SLV 14	-893	-39	1943	24.35	-34.86	-0.05
20	SLV 15	-790	-93	1833	105.81	-31	-0.08
20	SLV 16	-790	-93	1833	105.81	-31	-0.08
21	SLU 1	-93	0	1707	-0.11	-4.01	0
21	SLU 2	-93	0	1707	-0.11	-4.01	0
21	SLU 3	-93	0	1707	-0.11	-4.01	0
21	SLU 4	-93	0	1707	-0.11	-4.01	0
21	SLU 5	-93	0	1707	-0.11	-4.01	0
21	SLU 6	-93	0	1707	-0.11	-4.01	0
21	SLU 7	-93	0	1707	-0.11	-4.01	0
21	SLU 8	-93	0	1707	-0.11	-4.01	0
21	SLU 9	-93	0	1707	-0.11	-4.01	0
21	SLU 10	-114	0	2006	-0.17	-4.91	0
21	SLU 11	-114	0	2006	-0.17	-4.91	0
21	SLU 12	-114	0	2006	-0.17	-4.91	0
21	SLU 13	-114	0	2006	-0.17	-4.91	0
21	SLU 14	-114	0	2006	-0.17	-4.91	0
21	SLU 15	-114	0	2006	-0.17	-4.91	0
21	SLU 16	-114	0	2006	-0.17	-4.91	0
21	SLU 17	-114	0	2006	-0.17	-4.91	0
21	SLU 18	-123	0	2135	-0.19	-5.29	0
21	SLU 19	-123	0	2135	-0.19	-5.29	0
21	SLU 20	-123	0	2135	-0.19	-5.29	0
21	SLU 21	-123	0	2135	-0.19	-5.29	0
21	SLU 22	-109	0	1889	-0.13	-4.66	0
21	SLU 23	-109	0	1889	-0.13	-4.66	0
21	SLU 24	-109	0	1889	-0.13	-4.66	0
21	SLU 25	-109	0	1889	-0.13	-4.66	0
21	SLU 26	-109	0	1889	-0.13	-4.66	0
21	SLU 27	-109	0	1889	-0.13	-4.66	0
21	SLU 28	-109	0	1889	-0.13	-4.66	0
21	SLU 29	-109	0	1889	-0.13	-4.66	0
21	SLU 30	-109	0	1889	-0.13	-4.66	0
21	SLU 31	-129	0	2188	-0.19	-5.56	0
21	SLU 32	-129	0	2188	-0.19	-5.56	0
21	SLU 33	-129	0	2188	-0.19	-5.56	0
21	SLU 34	-129	0	2188	-0.19	-5.56	0
21	SLU 35	-129	0	2188	-0.19	-5.56	0
21	SLU 36	-129	0	2188	-0.19	-5.56	0
21	SLU 37	-129	0	2188	-0.19	-5.56	0
21	SLU 38	-129	0	2188	-0.19	-5.56	0
21	SLU 39	-138	0	2317	-0.22	-5.94	0
21	SLU 40	-138	0	2317	-0.22	-5.94	0
21	SLU 41	-138	0	2317	-0.22	-5.94	0
21	SLU 42	-138	0	2317	-0.22	-5.94	0
21	SLU 43	-116	0	2156	-0.13	-5	0
21	SLU 44	-116	0	2156	-0.13	-5	0
21	SLU 45	-116	0	2156	-0.13	-5	0
21	SLU 46	-116	0	2156	-0.13	-5	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
21	SLU 47	-116	0	2156	-0.13	-5	0
21	SLU 48	-116	0	2156	-0.13	-5	0
21	SLU 49	-116	0	2156	-0.13	-5	0
21	SLU 50	-116	0	2156	-0.13	-5	0
21	SLU 51	-116	0	2156	-0.13	-5	0
21	SLU 52	-137	0	2456	-0.19	-5.89	0
21	SLU 53	-137	0	2456	-0.19	-5.89	0
21	SLU 54	-137	0	2456	-0.19	-5.89	0
21	SLU 55	-137	0	2456	-0.19	-5.89	0
21	SLU 56	-137	0	2456	-0.19	-5.89	0
21	SLU 57	-137	0	2456	-0.19	-5.89	0
21	SLU 58	-137	0	2456	-0.19	-5.89	0
21	SLU 59	-137	0	2456	-0.19	-5.89	0
21	SLU 60	-145	0	2584	-0.21	-6.28	0
21	SLU 61	-145	0	2584	-0.21	-6.28	0
21	SLU 62	-145	0	2584	-0.21	-6.28	0
21	SLU 63	-145	0	2584	-0.21	-6.28	0
21	SLU 64	-131	0	2338	-0.15	-5.64	0
21	SLU 65	-131	0	2338	-0.15	-5.64	0
21	SLU 66	-131	0	2338	-0.15	-5.64	0
21	SLU 67	-131	0	2338	-0.15	-5.64	0
21	SLU 68	-131	0	2338	-0.15	-5.64	0
21	SLU 69	-131	0	2338	-0.15	-5.64	0
21	SLU 70	-131	0	2338	-0.15	-5.64	0
21	SLU 71	-131	0	2338	-0.15	-5.64	0
21	SLU 72	-131	0	2338	-0.15	-5.64	0
21	SLU 73	-152	0	2638	-0.22	-6.54	0
21	SLU 74	-152	0	2638	-0.22	-6.54	0
21	SLU 75	-152	0	2638	-0.22	-6.54	0
21	SLU 76	-152	0	2638	-0.22	-6.54	0
21	SLU 77	-152	0	2638	-0.22	-6.54	0
21	SLU 78	-152	0	2638	-0.22	-6.54	0
21	SLU 79	-152	0	2638	-0.22	-6.54	0
21	SLU 80	-152	0	2638	-0.22	-6.54	0
21	SLU 81	-161	0	2766	-0.24	-6.92	0
21	SLU 82	-161	0	2766	-0.24	-6.92	0
21	SLU 83	-161	0	2766	-0.24	-6.92	0
21	SLU 84	-161	0	2766	-0.24	-6.92	0
21	SLE RA 1	-98	0	1759	-0.11	-4.2	0
21	SLE RA 2	-98	0	1759	-0.11	-4.2	0
21	SLE RA 3	-98	0	1759	-0.11	-4.2	0
21	SLE RA 4	-98	0	1759	-0.11	-4.2	0
21	SLE RA 5	-98	0	1759	-0.11	-4.2	0
21	SLE RA 6	-98	0	1759	-0.11	-4.2	0
21	SLE RA 7	-98	0	1759	-0.11	-4.2	0
21	SLE RA 8	-98	0	1759	-0.11	-4.2	0
21	SLE RA 9	-98	0	1759	-0.11	-4.2	0
21	SLE RA 10	-111	0	1958	-0.15	-4.8	0
21	SLE RA 11	-111	0	1958	-0.15	-4.8	0
21	SLE RA 12	-111	0	1958	-0.15	-4.8	0
21	SLE RA 13	-111	0	1958	-0.15	-4.8	0
21	SLE RA 14	-111	0	1958	-0.15	-4.8	0
21	SLE RA 15	-111	0	1958	-0.15	-4.8	0
21	SLE RA 16	-111	0	1958	-0.15	-4.8	0
21	SLE RA 17	-111	0	1958	-0.15	-4.8	0
21	SLE RA 18	-117	0	2044	-0.17	-5.05	0
21	SLE RA 19	-117	0	2044	-0.17	-5.05	0
21	SLE RA 20	-117	0	2044	-0.17	-5.05	0
21	SLE RA 21	-117	0	2044	-0.17	-5.05	0
21	SLE FR 1	-98	0	1759	-0.11	-4.2	0
21	SLE FR 2	-98	0	1759	-0.11	-4.2	0
21	SLE FR 3	-98	0	1759	-0.11	-4.2	0
21	SLE FR 4	-104	0	1844	-0.13	-4.45	0
21	SLE FR 5	-104	0	1844	-0.13	-4.45	0
21	SLE FR 6	-107	0	1901	-0.14	-4.62	0
21	SLE QP 1	-98	0	1759	-0.11	-4.2	0
21	SLE QP 2	-104	0	1844	-0.13	-4.45	0
21	SLD 1	153	33	1842	-36.88	6.03	0.06
21	SLD 2	153	33	1842	-36.88	6.03	0.06
21	SLD 3	195	14	1792	-10.51	7.71	0.08
21	SLD 4	195	14	1792	-10.51	7.71	0.08
21	SLD 5	-91	40	1920	-51.14	-3.86	-0.02
21	SLD 6	-91	40	1920	-51.14	-3.86	-0.02
21	SLD 7	50	-26	1752	36.74	1.75	0.06
21	SLD 8	50	-26	1752	36.74	1.75	0.06
21	SLD 9	-257	26	1936	-37	-10.65	-0.06
21	SLD 10	-257	26	1936	-37	-10.65	-0.06
21	SLD 11	-116	-40	1768	50.88	-5.05	0.02
21	SLD 12	-116	-40	1768	50.88	-5.05	0.02
21	SLD 13	-402	-14	1896	10.25	-16.62	-0.08
21	SLD 14	-402	-14	1896	10.25	-16.62	-0.08
21	SLD 15	-360	-33	1846	36.62	-14.93	-0.06
21	SLD 16	-360	-33	1846	36.62	-14.93	-0.06
21	SLV 1	498	85	1841	-93.97	20.13	0.13
21	SLV 2	498	85	1841	-93.97	20.13	0.13
21	SLV 3	599	35	1719	-26.7	24.15	0.19
21	SLV 4	599	35	1719	-26.7	24.15	0.19
21	SLV 5	-76	101	2027	-130.31	-3.17	-0.04
21	SLV 6	-76	101	2027	-130.31	-3.17	-0.04



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
21	SLV 7	260	-65	1623	93.93	10.22	0.14
21	SLV 8	260	-65	1623	93.93	10.22	0.14
21	SLV 9	-467	65	2066	-94.19	-19.13	-0.14
21	SLV 10	-467	65	2066	-94.19	-19.13	-0.14
21	SLV 11	-131	-101	1661	130.05	-5.74	0.04
21	SLV 12	-131	-101	1661	130.05	-5.74	0.04
21	SLV 13	-806	-35	1969	26.44	-33.06	-0.19
21	SLV 14	-806	-35	1969	26.44	-33.06	-0.19
21	SLV 15	-706	-85	1848	93.71	-29.04	-0.13
21	SLV 16	-706	-85	1848	93.71	-29.04	-0.13
22	SLU 1	-83	0	1856	-0.16	-3.6	0
22	SLU 2	-83	0	1856	-0.16	-3.6	0
22	SLU 3	-83	0	1856	-0.16	-3.6	0
22	SLU 4	-83	0	1856	-0.16	-3.6	0
22	SLU 5	-83	0	1856	-0.16	-3.6	0
22	SLU 6	-83	0	1856	-0.16	-3.6	0
22	SLU 7	-83	0	1856	-0.16	-3.6	0
22	SLU 8	-83	0	1856	-0.16	-3.6	0
22	SLU 9	-83	0	1856	-0.16	-3.6	0
22	SLU 10	-98	0	2190	-0.23	-4.26	0
22	SLU 11	-98	0	2190	-0.23	-4.26	0
22	SLU 12	-98	0	2190	-0.23	-4.26	0
22	SLU 13	-98	0	2190	-0.23	-4.26	0
22	SLU 14	-98	0	2190	-0.23	-4.26	0
22	SLU 15	-98	0	2190	-0.23	-4.26	0
22	SLU 16	-98	0	2190	-0.23	-4.26	0
22	SLU 17	-98	0	2190	-0.23	-4.26	0
22	SLU 18	-105	0	2333	-0.26	-4.54	0
22	SLU 19	-105	0	2333	-0.26	-4.54	0
22	SLU 20	-105	0	2333	-0.26	-4.54	0
22	SLU 21	-105	0	2333	-0.26	-4.54	0
22	SLU 22	-97	0	2057	-0.19	-4.16	0
22	SLU 23	-97	0	2057	-0.19	-4.16	0
22	SLU 24	-97	0	2057	-0.19	-4.16	0
22	SLU 25	-97	0	2057	-0.19	-4.16	0
22	SLU 26	-97	0	2057	-0.19	-4.16	0
22	SLU 27	-97	0	2057	-0.19	-4.16	0
22	SLU 28	-97	0	2057	-0.19	-4.16	0
22	SLU 29	-97	0	2057	-0.19	-4.16	0
22	SLU 30	-97	0	2057	-0.19	-4.16	0
22	SLU 31	-112	0	2390	-0.26	-4.82	0
22	SLU 32	-112	0	2390	-0.26	-4.82	0
22	SLU 33	-112	0	2390	-0.26	-4.82	0
22	SLU 34	-112	0	2390	-0.26	-4.82	0
22	SLU 35	-112	0	2390	-0.26	-4.82	0
22	SLU 36	-112	0	2390	-0.26	-4.82	0
22	SLU 37	-112	0	2390	-0.26	-4.82	0
22	SLU 38	-112	0	2390	-0.26	-4.82	0
22	SLU 39	-118	0	2533	-0.29	-5.1	0
22	SLU 40	-118	0	2533	-0.29	-5.1	0
22	SLU 41	-118	0	2533	-0.29	-5.1	0
22	SLU 42	-118	0	2533	-0.29	-5.1	0
22	SLU 43	-103	0	2345	-0.19	-4.48	0
22	SLU 44	-103	0	2345	-0.19	-4.48	0
22	SLU 45	-103	0	2345	-0.19	-4.48	0
22	SLU 46	-103	0	2345	-0.19	-4.48	0
22	SLU 47	-103	0	2345	-0.19	-4.48	0
22	SLU 48	-103	0	2345	-0.19	-4.48	0
22	SLU 49	-103	0	2345	-0.19	-4.48	0
22	SLU 50	-103	0	2345	-0.19	-4.48	0
22	SLU 51	-103	0	2345	-0.19	-4.48	0
22	SLU 52	-119	0	2679	-0.26	-5.14	0
22	SLU 53	-119	0	2679	-0.26	-5.14	0
22	SLU 54	-119	0	2679	-0.26	-5.14	0
22	SLU 55	-119	0	2679	-0.26	-5.14	0
22	SLU 56	-119	0	2679	-0.26	-5.14	0
22	SLU 57	-119	0	2679	-0.26	-5.14	0
22	SLU 58	-119	0	2679	-0.26	-5.14	0
22	SLU 59	-119	0	2679	-0.26	-5.14	0
22	SLU 60	-125	0	2822	-0.29	-5.43	0
22	SLU 61	-125	0	2822	-0.29	-5.43	0
22	SLU 62	-125	0	2822	-0.29	-5.43	0
22	SLU 63	-125	0	2822	-0.29	-5.43	0
22	SLU 64	-117	0	2545	-0.22	-5.05	0
22	SLU 65	-117	0	2545	-0.22	-5.05	0
22	SLU 66	-117	0	2545	-0.22	-5.05	0
22	SLU 67	-117	0	2545	-0.22	-5.05	0
22	SLU 68	-117	0	2545	-0.22	-5.05	0
22	SLU 69	-117	0	2545	-0.22	-5.05	0
22	SLU 70	-117	0	2545	-0.22	-5.05	0
22	SLU 71	-117	0	2545	-0.22	-5.05	0
22	SLU 72	-117	0	2545	-0.22	-5.05	0
22	SLU 73	-132	0	2879	-0.29	-5.7	0
22	SLU 74	-132	0	2879	-0.29	-5.7	0
22	SLU 75	-132	0	2879	-0.29	-5.7	0
22	SLU 76	-132	0	2879	-0.29	-5.7	0
22	SLU 77	-132	0	2879	-0.29	-5.7	0
22	SLU 78	-132	0	2879	-0.29	-5.7	0
22	SLU 79	-132	0	2879	-0.29	-5.7	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
22	SLU 80	-132	0	2879	-0.29	-5.7	0
22	SLU 81	-139	0	3022	-0.32	-5.99	0
22	SLU 82	-139	0	3022	-0.32	-5.99	0
22	SLU 83	-139	0	3022	-0.32	-5.99	0
22	SLU 84	-139	0	3022	-0.32	-5.99	0
22	SLE RA 1	-87	0	1914	-0.17	-3.76	0
22	SLE RA 2	-87	0	1914	-0.17	-3.76	0
22	SLE RA 3	-87	0	1914	-0.17	-3.76	0
22	SLE RA 4	-87	0	1914	-0.17	-3.76	0
22	SLE RA 5	-87	0	1914	-0.17	-3.76	0
22	SLE RA 6	-87	0	1914	-0.17	-3.76	0
22	SLE RA 7	-87	0	1914	-0.17	-3.76	0
22	SLE RA 8	-87	0	1914	-0.17	-3.76	0
22	SLE RA 9	-87	0	1914	-0.17	-3.76	0
22	SLE RA 10	-97	0	2136	-0.21	-4.2	0
22	SLE RA 11	-97	0	2136	-0.21	-4.2	0
22	SLE RA 12	-97	0	2136	-0.21	-4.2	0
22	SLE RA 13	-97	0	2136	-0.21	-4.2	0
22	SLE RA 14	-97	0	2136	-0.21	-4.2	0
22	SLE RA 15	-97	0	2136	-0.21	-4.2	0
22	SLE RA 16	-97	0	2136	-0.21	-4.2	0
22	SLE RA 17	-97	0	2136	-0.21	-4.2	0
22	SLE RA 18	-101	0	2232	-0.23	-4.39	0
22	SLE RA 19	-101	0	2232	-0.23	-4.39	0
22	SLE RA 20	-101	0	2232	-0.23	-4.39	0
22	SLE RA 21	-101	0	2232	-0.23	-4.39	0
22	SLE FR 1	-87	0	1914	-0.17	-3.76	0
22	SLE FR 2	-87	0	1914	-0.17	-3.76	0
22	SLE FR 3	-87	0	1914	-0.17	-3.76	0
22	SLE FR 4	-91	0	2009	-0.19	-3.95	0
22	SLE FR 5	-91	0	2009	-0.19	-3.95	0
22	SLE FR 6	-94	0	2073	-0.2	-4.07	0
22	SLE QP 1	-87	0	1914	-0.17	-3.76	0
22	SLE QP 2	-91	0	2009	-0.19	-3.95	0
22	SLD 1	136	28	2006	-30.64	5.15	0.02
22	SLD 2	136	28	2006	-30.64	5.15	0.02
22	SLD 3	176	11	1941	-9.88	6.68	0.02
22	SLD 4	176	11	1941	-9.88	6.68	0.02
22	SLD 5	-84	33	2108	-40.79	-3.54	0.02
22	SLD 6	-84	33	2108	-40.79	-3.54	0.02
22	SLD 7	50	-21	1889	28.38	1.56	-0.01
22	SLD 8	50	-21	1889	28.38	1.56	-0.01
22	SLD 9	-233	21	2129	-28.75	-9.45	0.01
22	SLD 10	-233	21	2129	-28.75	-9.45	0.01
22	SLD 11	-99	-33	1910	40.42	-4.36	-0.02
22	SLD 12	-99	-33	1910	40.42	-4.36	-0.02
22	SLD 13	-359	-11	2077	9.51	-14.58	-0.02
22	SLD 14	-359	-11	2077	9.51	-14.58	-0.02
22	SLD 15	-319	-28	2012	30.26	-13.05	-0.02
22	SLD 16	-319	-28	2012	30.26	-13.05	-0.02
22	SLV 1	442	70	2003	-77.97	17.41	0.06
22	SLV 2	442	70	2003	-77.97	17.41	0.06
22	SLV 3	538	30	1847	-25.15	21.04	0.04
22	SLV 4	538	30	1847	-25.15	21.04	0.04
22	SLV 5	-76	83	2244	-103.64	-3.05	0.04
22	SLV 6	-76	83	2244	-103.64	-3.05	0.04
22	SLV 7	242	-53	1724	72.44	9.06	-0.01
22	SLV 8	242	-53	1724	72.44	9.06	-0.01
22	SLV 9	-425	53	2294	-72.81	-16.95	0.01
22	SLV 10	-425	53	2294	-72.81	-16.95	0.01
22	SLV 11	-107	-83	1774	103.27	-4.84	-0.04
22	SLV 12	-107	-83	1774	103.27	-4.84	-0.04
22	SLV 13	-720	-29	2171	24.78	-28.93	-0.04
22	SLV 14	-720	-29	2171	24.78	-28.93	-0.04
22	SLV 15	-625	-70	2015	77.6	-25.3	-0.06
22	SLV 16	-625	-70	2015	77.6	-25.3	-0.06
23	SLU 1	-163	0	2014	-0.24	-7.85	0
23	SLU 2	-163	0	2014	-0.24	-7.85	0
23	SLU 3	-163	0	2014	-0.24	-7.85	0
23	SLU 4	-163	0	2014	-0.24	-7.85	0
23	SLU 5	-163	0	2014	-0.24	-7.85	0
23	SLU 6	-163	0	2014	-0.24	-7.85	0
23	SLU 7	-163	0	2014	-0.24	-7.85	0
23	SLU 8	-163	0	2014	-0.24	-7.85	0
23	SLU 9	-163	0	2014	-0.24	-7.85	0
23	SLU 10	-194	0	2386	-0.33	-9.38	0
23	SLU 11	-194	0	2386	-0.33	-9.38	0
23	SLU 12	-194	0	2386	-0.33	-9.38	0
23	SLU 13	-194	0	2386	-0.33	-9.38	0
23	SLU 14	-194	0	2386	-0.33	-9.38	0
23	SLU 15	-194	0	2386	-0.33	-9.38	0
23	SLU 16	-194	0	2386	-0.33	-9.38	0
23	SLU 17	-194	0	2386	-0.33	-9.38	0
23	SLU 18	-207	0	2545	-0.37	-10.04	0
23	SLU 19	-207	0	2545	-0.37	-10.04	0
23	SLU 20	-207	0	2545	-0.37	-10.04	0
23	SLU 21	-207	0	2545	-0.37	-10.04	0
23	SLU 22	-187	0	2233	-0.29	-8.99	0
23	SLU 23	-187	0	2233	-0.29	-8.99	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
23	SLU 24	-187	0	2233	-0.29	-8.99	0
23	SLU 25	-187	0	2233	-0.29	-8.99	0
23	SLU 26	-187	0	2233	-0.29	-8.99	0
23	SLU 27	-187	0	2233	-0.29	-8.99	0
23	SLU 28	-187	0	2233	-0.29	-8.99	0
23	SLU 29	-187	0	2233	-0.29	-8.99	0
23	SLU 30	-187	0	2233	-0.29	-8.99	0
23	SLU 31	-218	0	2605	-0.37	-10.52	0
23	SLU 32	-218	0	2605	-0.37	-10.52	0
23	SLU 33	-218	0	2605	-0.37	-10.52	0
23	SLU 34	-218	0	2605	-0.37	-10.52	0
23	SLU 35	-218	0	2605	-0.37	-10.52	0
23	SLU 36	-218	0	2605	-0.37	-10.52	0
23	SLU 37	-218	0	2605	-0.37	-10.52	0
23	SLU 38	-218	0	2605	-0.37	-10.52	0
23	SLU 39	-231	0	2764	-0.41	-11.18	0
23	SLU 40	-231	0	2764	-0.41	-11.18	0
23	SLU 41	-231	0	2764	-0.41	-11.18	0
23	SLU 42	-231	0	2764	-0.41	-11.18	0
23	SLU 43	-204	0	2543	-0.3	-9.82	0
23	SLU 44	-204	0	2543	-0.3	-9.82	0
23	SLU 45	-204	0	2543	-0.3	-9.82	0
23	SLU 46	-204	0	2543	-0.3	-9.82	0
23	SLU 47	-204	0	2543	-0.3	-9.82	0
23	SLU 48	-204	0	2543	-0.3	-9.82	0
23	SLU 49	-204	0	2543	-0.3	-9.82	0
23	SLU 50	-204	0	2543	-0.3	-9.82	0
23	SLU 51	-204	0	2543	-0.3	-9.82	0
23	SLU 52	-234	0	2915	-0.39	-11.35	0
23	SLU 53	-234	0	2915	-0.39	-11.35	0
23	SLU 54	-234	0	2915	-0.39	-11.35	0
23	SLU 55	-234	0	2915	-0.39	-11.35	0
23	SLU 56	-234	0	2915	-0.39	-11.35	0
23	SLU 57	-234	0	2915	-0.39	-11.35	0
23	SLU 58	-234	0	2915	-0.39	-11.35	0
23	SLU 59	-234	0	2915	-0.39	-11.35	0
23	SLU 60	-247	0	3074	-0.43	-12.01	0
23	SLU 61	-247	0	3074	-0.43	-12.01	0
23	SLU 62	-247	0	3074	-0.43	-12.01	0
23	SLU 63	-247	0	3074	-0.43	-12.01	0
23	SLU 64	-228	0	2762	-0.35	-10.96	0
23	SLU 65	-228	0	2762	-0.35	-10.96	0
23	SLU 66	-228	0	2762	-0.35	-10.96	0
23	SLU 67	-228	0	2762	-0.35	-10.96	0
23	SLU 68	-228	0	2762	-0.35	-10.96	0
23	SLU 69	-228	0	2762	-0.35	-10.96	0
23	SLU 70	-228	0	2762	-0.35	-10.96	0
23	SLU 71	-228	0	2762	-0.35	-10.96	0
23	SLU 72	-228	0	2762	-0.35	-10.96	0
23	SLU 73	-258	0	3134	-0.43	-12.49	0
23	SLU 74	-258	0	3134	-0.43	-12.49	0
23	SLU 75	-258	0	3134	-0.43	-12.49	0
23	SLU 76	-258	0	3134	-0.43	-12.49	0
23	SLU 77	-258	0	3134	-0.43	-12.49	0
23	SLU 78	-258	0	3134	-0.43	-12.49	0
23	SLU 79	-258	0	3134	-0.43	-12.49	0
23	SLU 80	-258	0	3134	-0.43	-12.49	0
23	SLU 81	-271	0	3293	-0.47	-13.14	0
23	SLU 82	-271	0	3293	-0.47	-13.14	0
23	SLU 83	-271	0	3293	-0.47	-13.14	0
23	SLU 84	-271	0	3293	-0.47	-13.14	0
23	SLE RA 1	-170	0	2076	-0.26	-8.18	0
23	SLE RA 2	-170	0	2076	-0.26	-8.18	0
23	SLE RA 3	-170	0	2076	-0.26	-8.18	0
23	SLE RA 4	-170	0	2076	-0.26	-8.18	0
23	SLE RA 5	-170	0	2076	-0.26	-8.18	0
23	SLE RA 6	-170	0	2076	-0.26	-8.18	0
23	SLE RA 7	-170	0	2076	-0.26	-8.18	0
23	SLE RA 8	-170	0	2076	-0.26	-8.18	0
23	SLE RA 9	-170	0	2076	-0.26	-8.18	0
23	SLE RA 10	-190	0	2324	-0.31	-9.2	0
23	SLE RA 11	-190	0	2324	-0.31	-9.2	0
23	SLE RA 12	-190	0	2324	-0.31	-9.2	0
23	SLE RA 13	-190	0	2324	-0.31	-9.2	0
23	SLE RA 14	-190	0	2324	-0.31	-9.2	0
23	SLE RA 15	-190	0	2324	-0.31	-9.2	0
23	SLE RA 16	-190	0	2324	-0.31	-9.2	0
23	SLE RA 17	-190	0	2324	-0.31	-9.2	0
23	SLE RA 18	-199	0	2431	-0.34	-9.64	0
23	SLE RA 19	-199	0	2431	-0.34	-9.64	0
23	SLE RA 20	-199	0	2431	-0.34	-9.64	0
23	SLE RA 21	-199	0	2431	-0.34	-9.64	0
23	SLE FR 1	-170	0	2076	-0.26	-8.18	0
23	SLE FR 2	-170	0	2076	-0.26	-8.18	0
23	SLE FR 3	-170	0	2076	-0.26	-8.18	0
23	SLE FR 4	-179	0	2183	-0.28	-8.62	0
23	SLE FR 5	-179	0	2183	-0.28	-8.62	0
23	SLE FR 6	-185	0	2254	-0.3	-8.91	0
23	SLE QP 1	-170	0	2076	-0.26	-8.18	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
23	SLE QP 2	-179	0	2183	-0.28	-8.62	0
23	SLD 1	34	22	2158	-23.49	0.6	0.02
23	SLD 2	34	22	2158	-23.49	0.6	0.02
23	SLD 3	74	11	2072	-8.65	2.18	0.03
23	SLD 4	74	11	2072	-8.65	2.18	0.03
23	SLD 5	-176	24	2306	-29.74	-8.25	-0.01
23	SLD 6	-176	24	2306	-29.74	-8.25	-0.01
23	SLD 7	-42	-14	2019	19.71	-2.98	0.02
23	SLD 8	-42	-14	2019	19.71	-2.98	0.02
23	SLD 9	-316	14	2347	-20.27	-14.25	-0.02
23	SLD 10	-316	14	2347	-20.27	-14.25	-0.02
23	SLD 11	-182	-24	2060	29.18	-8.98	0.01
23	SLD 12	-182	-24	2060	29.18	-8.98	0.01
23	SLD 13	-432	-11	2294	8.09	-19.41	-0.03
23	SLD 14	-432	-11	2294	8.09	-19.41	-0.03
23	SLD 15	-392	-22	2208	22.93	-17.83	-0.02
23	SLD 16	-392	-22	2208	22.93	-17.83	-0.02
23	SLV 1	321	56	2124	-59.54	13.01	0.05
23	SLV 2	321	56	2124	-59.54	13.01	0.05
23	SLV 3	416	28	1920	-21.89	16.75	0.08
23	SLV 4	416	28	1920	-21.89	16.75	0.08
23	SLV 5	-173	59	2475	-75.16	-7.81	-0.02
23	SLV 6	-173	59	2475	-75.16	-7.81	-0.02
23	SLV 7	144	-33	1795	50.34	4.68	0.06
23	SLV 8	144	-33	1795	50.34	4.68	0.06
23	SLV 9	-502	34	2571	-50.9	-21.91	-0.06
23	SLV 10	-502	34	2571	-50.9	-21.91	-0.06
23	SLV 11	-185	-59	1891	74.6	-9.42	0.02
23	SLV 12	-185	-59	1891	74.6	-9.42	0.02
23	SLV 13	-774	-28	2445	21.33	-33.99	-0.08
23	SLV 14	-774	-28	2445	21.33	-33.99	-0.08
23	SLV 15	-679	-56	2241	58.98	-30.24	-0.05
23	SLV 16	-679	-56	2241	58.98	-30.24	-0.05
24	SLU 1	-263	0	2130	-0.46	-10.92	0
24	SLU 2	-263	0	2130	-0.46	-10.92	0
24	SLU 3	-263	0	2130	-0.46	-10.92	0
24	SLU 4	-263	0	2130	-0.46	-10.92	0
24	SLU 5	-263	0	2130	-0.46	-10.92	0
24	SLU 6	-263	0	2130	-0.46	-10.92	0
24	SLU 7	-263	0	2130	-0.46	-10.92	0
24	SLU 8	-263	0	2130	-0.46	-10.92	0
24	SLU 9	-263	0	2130	-0.46	-10.92	0
24	SLU 10	-311	0	2533	-0.59	-12.99	-0.01
24	SLU 11	-311	0	2533	-0.59	-12.99	-0.01
24	SLU 12	-311	0	2533	-0.59	-12.99	-0.01
24	SLU 13	-311	0	2533	-0.59	-12.99	-0.01
24	SLU 14	-311	0	2533	-0.59	-12.99	-0.01
24	SLU 15	-311	0	2533	-0.59	-12.99	-0.01
24	SLU 16	-311	0	2533	-0.59	-12.99	-0.01
24	SLU 17	-311	0	2533	-0.59	-12.99	-0.01
24	SLU 18	-332	1	2706	-0.65	-13.87	-0.01
24	SLU 19	-332	1	2706	-0.65	-13.87	-0.01
24	SLU 20	-332	1	2706	-0.65	-13.87	-0.01
24	SLU 21	-332	1	2706	-0.65	-13.87	-0.01
24	SLU 22	-299	0	2362	-0.52	-12.42	-0.01
24	SLU 23	-299	0	2362	-0.52	-12.42	-0.01
24	SLU 24	-299	0	2362	-0.52	-12.42	-0.01
24	SLU 25	-299	0	2362	-0.52	-12.42	-0.01
24	SLU 26	-299	0	2362	-0.52	-12.42	-0.01
24	SLU 27	-299	0	2362	-0.52	-12.42	-0.01
24	SLU 28	-299	0	2362	-0.52	-12.42	-0.01
24	SLU 29	-299	0	2362	-0.52	-12.42	-0.01
24	SLU 30	-299	0	2362	-0.52	-12.42	-0.01
24	SLU 31	-348	1	2765	-0.65	-14.48	-0.01
24	SLU 32	-348	1	2765	-0.65	-14.48	-0.01
24	SLU 33	-348	1	2765	-0.65	-14.48	-0.01
24	SLU 34	-348	1	2765	-0.65	-14.48	-0.01
24	SLU 35	-348	1	2765	-0.65	-14.48	-0.01
24	SLU 36	-348	1	2765	-0.65	-14.48	-0.01
24	SLU 37	-348	1	2765	-0.65	-14.48	-0.01
24	SLU 38	-348	1	2765	-0.65	-14.48	-0.01
24	SLU 39	-368	1	2938	-0.71	-15.36	-0.01
24	SLU 40	-368	1	2938	-0.71	-15.36	-0.01
24	SLU 41	-368	1	2938	-0.71	-15.36	-0.01
24	SLU 42	-368	1	2938	-0.71	-15.36	-0.01
24	SLU 43	-329	0	2689	-0.57	-13.69	-0.01
24	SLU 44	-329	0	2689	-0.57	-13.69	-0.01
24	SLU 45	-329	0	2689	-0.57	-13.69	-0.01
24	SLU 46	-329	0	2689	-0.57	-13.69	-0.01
24	SLU 47	-329	0	2689	-0.57	-13.69	-0.01
24	SLU 48	-329	0	2689	-0.57	-13.69	-0.01
24	SLU 49	-329	0	2689	-0.57	-13.69	-0.01
24	SLU 50	-329	0	2689	-0.57	-13.69	-0.01
24	SLU 51	-329	0	2689	-0.57	-13.69	-0.01
24	SLU 52	-378	1	3093	-0.71	-15.75	-0.01
24	SLU 53	-378	1	3093	-0.71	-15.75	-0.01
24	SLU 54	-378	1	3093	-0.71	-15.75	-0.01
24	SLU 55	-378	1	3093	-0.71	-15.75	-0.01
24	SLU 56	-378	1	3093	-0.71	-15.75	-0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
24	SLU 57	-378	1	3093	-0.71	-15.75	-0.01
24	SLU 58	-378	1	3093	-0.71	-15.75	-0.01
24	SLU 59	-378	1	3093	-0.71	-15.75	-0.01
24	SLU 60	-399	1	3266	-0.76	-16.63	-0.01
24	SLU 61	-399	1	3266	-0.76	-16.63	-0.01
24	SLU 62	-399	1	3266	-0.76	-16.63	-0.01
24	SLU 63	-399	1	3266	-0.76	-16.63	-0.01
24	SLU 64	-365	1	2921	-0.64	-15.18	-0.01
24	SLU 65	-365	1	2921	-0.64	-15.18	-0.01
24	SLU 66	-365	1	2921	-0.64	-15.18	-0.01
24	SLU 67	-365	1	2921	-0.64	-15.18	-0.01
24	SLU 68	-365	1	2921	-0.64	-15.18	-0.01
24	SLU 69	-365	1	2921	-0.64	-15.18	-0.01
24	SLU 70	-365	1	2921	-0.64	-15.18	-0.01
24	SLU 71	-365	1	2921	-0.64	-15.18	-0.01
24	SLU 72	-365	1	2921	-0.64	-15.18	-0.01
24	SLU 73	-414	1	3325	-0.77	-17.24	-0.01
24	SLU 74	-414	1	3325	-0.77	-17.24	-0.01
24	SLU 75	-414	1	3325	-0.77	-17.24	-0.01
24	SLU 76	-414	1	3325	-0.77	-17.24	-0.01
24	SLU 77	-414	1	3325	-0.77	-17.24	-0.01
24	SLU 78	-414	1	3325	-0.77	-17.24	-0.01
24	SLU 79	-414	1	3325	-0.77	-17.24	-0.01
24	SLU 80	-414	1	3325	-0.77	-17.24	-0.01
24	SLU 81	-435	1	3498	-0.83	-18.13	-0.01
24	SLU 82	-435	1	3498	-0.83	-18.13	-0.01
24	SLU 83	-435	1	3498	-0.83	-18.13	-0.01
24	SLU 84	-435	1	3498	-0.83	-18.13	-0.01
24	SLE RA 1	-273	0	2196	-0.48	-11.35	0
24	SLE RA 2	-273	0	2196	-0.48	-11.35	0
24	SLE RA 3	-273	0	2196	-0.48	-11.35	0
24	SLE RA 4	-273	0	2196	-0.48	-11.35	0
24	SLE RA 5	-273	0	2196	-0.48	-11.35	0
24	SLE RA 6	-273	0	2196	-0.48	-11.35	0
24	SLE RA 7	-273	0	2196	-0.48	-11.35	0
24	SLE RA 8	-273	0	2196	-0.48	-11.35	0
24	SLE RA 9	-273	0	2196	-0.48	-11.35	0
24	SLE RA 10	-305	0	2465	-0.56	-12.72	-0.01
24	SLE RA 11	-305	0	2465	-0.56	-12.72	-0.01
24	SLE RA 12	-305	0	2465	-0.56	-12.72	-0.01
24	SLE RA 13	-305	0	2465	-0.56	-12.72	-0.01
24	SLE RA 14	-305	0	2465	-0.56	-12.72	-0.01
24	SLE RA 15	-305	0	2465	-0.56	-12.72	-0.01
24	SLE RA 16	-305	0	2465	-0.56	-12.72	-0.01
24	SLE RA 17	-305	0	2465	-0.56	-12.72	-0.01
24	SLE RA 18	-319	0	2580	-0.6	-13.31	-0.01
24	SLE RA 19	-319	0	2580	-0.6	-13.31	-0.01
24	SLE RA 20	-319	0	2580	-0.6	-13.31	-0.01
24	SLE RA 21	-319	0	2580	-0.6	-13.31	-0.01
24	SLE FR 1	-273	0	2196	-0.48	-11.35	0
24	SLE FR 2	-273	0	2196	-0.48	-11.35	0
24	SLE FR 3	-273	0	2196	-0.48	-11.35	0
24	SLE FR 4	-287	0	2311	-0.51	-11.94	-0.01
24	SLE FR 5	-287	0	2311	-0.51	-11.94	-0.01
24	SLE FR 6	-296	0	2388	-0.54	-12.33	-0.01
24	SLE QP 1	-273	0	2196	-0.48	-11.35	0
24	SLE QP 2	-287	0	2311	-0.51	-11.94	-0.01
24	SLD 1	-88	13	2228	-16.33	-3.31	0.01
24	SLD 2	-88	13	2228	-16.33	-3.31	0.01
24	SLD 3	-47	20	2114	-7.28	-1.71	0.01
24	SLD 4	-47	20	2114	-7.28	-1.71	0.01
24	SLD 5	-290	-6	2460	-18.99	-11.78	-0.01
24	SLD 6	-290	-6	2460	-18.99	-11.78	-0.01
24	SLD 7	-152	16	2079	11.19	-6.44	0.01
24	SLD 8	-152	16	2079	11.19	-6.44	0.01
24	SLD 9	-422	-15	2544	-12.22	-17.43	-0.02
24	SLD 10	-422	-15	2544	-12.22	-17.43	-0.02
24	SLD 11	-284	6	2163	17.96	-12.1	0
24	SLD 12	-284	6	2163	17.96	-12.1	0
24	SLD 13	-527	-19	2509	6.25	-22.17	-0.02
24	SLD 14	-527	-19	2509	6.25	-22.17	-0.02
24	SLD 15	-486	-13	2394	15.3	-20.57	-0.02
24	SLD 16	-486	-13	2394	15.3	-20.57	-0.02
24	SLV 1	179	33	2116	-40.8	8.31	0.02
24	SLV 2	179	33	2116	-40.8	8.31	0.02
24	SLV 3	277	49	1845	-17.89	12.1	0.04
24	SLV 4	277	49	1845	-17.89	12.1	0.04
24	SLV 5	-296	-14	2663	-47.34	-11.61	-0.03
24	SLV 6	-296	-14	2663	-47.34	-11.61	-0.03
24	SLV 7	31	39	1761	29.01	1.02	0.04
24	SLV 8	31	39	1761	29.01	1.02	0.04
24	SLV 9	-605	-38	2862	-30.04	-24.9	-0.05
24	SLV 10	-605	-38	2862	-30.04	-24.9	-0.05
24	SLV 11	-278	15	1960	46.31	-12.27	0.02
24	SLV 12	-278	15	1960	46.31	-12.27	0.02
24	SLV 13	-851	-48	2778	16.86	-35.98	-0.05
24	SLV 14	-851	-48	2778	16.86	-35.98	-0.05
24	SLV 15	-753	-32	2507	39.77	-32.19	-0.03
24	SLV 16	-753	-32	2507	39.77	-32.19	-0.03



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
25	SLU 1	-369	3	2341	-1.03	-17.82	0.01
25	SLU 2	-369	3	2341	-1.03	-17.82	0.01
25	SLU 3	-369	3	2341	-1.03	-17.82	0.01
25	SLU 4	-369	3	2341	-1.03	-17.82	0.01
25	SLU 5	-369	3	2341	-1.03	-17.82	0.01
25	SLU 6	-369	3	2341	-1.03	-17.82	0.01
25	SLU 7	-369	3	2341	-1.03	-17.82	0.01
25	SLU 8	-369	3	2341	-1.03	-17.82	0.01
25	SLU 9	-369	3	2341	-1.03	-17.82	0.01
25	SLU 10	-437	4	2802	-1.29	-21.26	0.02
25	SLU 11	-437	4	2802	-1.29	-21.26	0.02
25	SLU 12	-437	4	2802	-1.29	-21.26	0.02
25	SLU 13	-437	4	2802	-1.29	-21.26	0.02
25	SLU 14	-437	4	2802	-1.29	-21.26	0.02
25	SLU 15	-437	4	2802	-1.29	-21.26	0.02
25	SLU 16	-437	4	2802	-1.29	-21.26	0.02
25	SLU 17	-437	4	2802	-1.29	-21.26	0.02
25	SLU 18	-466	4	3000	-1.4	-22.74	0.02
25	SLU 19	-466	4	3000	-1.4	-22.74	0.02
25	SLU 20	-466	4	3000	-1.4	-22.74	0.02
25	SLU 21	-466	4	3000	-1.4	-22.74	0.02
25	SLU 22	-417	4	2598	-1.16	-20.13	0.02
25	SLU 23	-417	4	2598	-1.16	-20.13	0.02
25	SLU 24	-417	4	2598	-1.16	-20.13	0.02
25	SLU 25	-417	4	2598	-1.16	-20.13	0.02
25	SLU 26	-417	4	2598	-1.16	-20.13	0.02
25	SLU 27	-417	4	2598	-1.16	-20.13	0.02
25	SLU 28	-417	4	2598	-1.16	-20.13	0.02
25	SLU 29	-417	4	2598	-1.16	-20.13	0.02
25	SLU 30	-417	4	2598	-1.16	-20.13	0.02
25	SLU 31	-485	4	3059	-1.42	-23.57	0.02
25	SLU 32	-485	4	3059	-1.42	-23.57	0.02
25	SLU 33	-485	4	3059	-1.42	-23.57	0.02
25	SLU 34	-485	4	3059	-1.42	-23.57	0.02
25	SLU 35	-485	4	3059	-1.42	-23.57	0.02
25	SLU 36	-485	4	3059	-1.42	-23.57	0.02
25	SLU 37	-485	4	3059	-1.42	-23.57	0.02
25	SLU 38	-485	4	3059	-1.42	-23.57	0.02
25	SLU 39	-514	5	3257	-1.53	-25.04	0.02
25	SLU 40	-514	5	3257	-1.53	-25.04	0.02
25	SLU 41	-514	5	3257	-1.53	-25.04	0.02
25	SLU 42	-514	5	3257	-1.53	-25.04	0.02
25	SLU 43	-463	4	2955	-1.3	-22.38	0.02
25	SLU 44	-463	4	2955	-1.3	-22.38	0.02
25	SLU 45	-463	4	2955	-1.3	-22.38	0.02
25	SLU 46	-463	4	2955	-1.3	-22.38	0.02
25	SLU 47	-463	4	2955	-1.3	-22.38	0.02
25	SLU 48	-463	4	2955	-1.3	-22.38	0.02
25	SLU 49	-463	4	2955	-1.3	-22.38	0.02
25	SLU 50	-463	4	2955	-1.3	-22.38	0.02
25	SLU 51	-463	4	2955	-1.3	-22.38	0.02
25	SLU 52	-531	5	3416	-1.56	-25.82	0.02
25	SLU 53	-531	5	3416	-1.56	-25.82	0.02
25	SLU 54	-531	5	3416	-1.56	-25.82	0.02
25	SLU 55	-531	5	3416	-1.56	-25.82	0.02
25	SLU 56	-531	5	3416	-1.56	-25.82	0.02
25	SLU 57	-531	5	3416	-1.56	-25.82	0.02
25	SLU 58	-531	5	3416	-1.56	-25.82	0.02
25	SLU 59	-531	5	3416	-1.56	-25.82	0.02
25	SLU 60	-560	5	3614	-1.67	-27.29	0.02
25	SLU 61	-560	5	3614	-1.67	-27.29	0.02
25	SLU 62	-560	5	3614	-1.67	-27.29	0.02
25	SLU 63	-560	5	3614	-1.67	-27.29	0.02
25	SLU 64	-511	5	3212	-1.42	-24.69	0.02
25	SLU 65	-511	5	3212	-1.42	-24.69	0.02
25	SLU 66	-511	5	3212	-1.42	-24.69	0.02
25	SLU 67	-511	5	3212	-1.42	-24.69	0.02
25	SLU 68	-511	5	3212	-1.42	-24.69	0.02
25	SLU 69	-511	5	3212	-1.42	-24.69	0.02
25	SLU 70	-511	5	3212	-1.42	-24.69	0.02
25	SLU 71	-511	5	3212	-1.42	-24.69	0.02
25	SLU 72	-511	5	3212	-1.42	-24.69	0.02
25	SLU 73	-579	5	3673	-1.69	-28.13	0.02
25	SLU 74	-579	5	3673	-1.69	-28.13	0.02
25	SLU 75	-579	5	3673	-1.69	-28.13	0.02
25	SLU 76	-579	5	3673	-1.69	-28.13	0.02
25	SLU 77	-579	5	3673	-1.69	-28.13	0.02
25	SLU 78	-579	5	3673	-1.69	-28.13	0.02
25	SLU 79	-579	5	3673	-1.69	-28.13	0.02
25	SLU 80	-579	5	3673	-1.69	-28.13	0.02
25	SLU 81	-608	6	3871	-1.8	-29.6	0.02
25	SLU 82	-608	6	3871	-1.8	-29.6	0.02
25	SLU 83	-608	6	3871	-1.8	-29.6	0.02
25	SLU 84	-608	6	3871	-1.8	-29.6	0.02
25	SLE RA 1	-383	3	2414	-1.07	-18.48	0.01
25	SLE RA 2	-383	3	2414	-1.07	-18.48	0.01
25	SLE RA 3	-383	3	2414	-1.07	-18.48	0.01
25	SLE RA 4	-383	3	2414	-1.07	-18.48	0.01
25	SLE RA 5	-383	3	2414	-1.07	-18.48	0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
25	SLE RA 6	-383	3	2414	-1.07	-18.48	0.01
25	SLE RA 7	-383	3	2414	-1.07	-18.48	0.01
25	SLE RA 8	-383	3	2414	-1.07	-18.48	0.01
25	SLE RA 9	-383	3	2414	-1.07	-18.48	0.01
25	SLE RA 10	-428	4	2722	-1.24	-20.78	0.02
25	SLE RA 11	-428	4	2722	-1.24	-20.78	0.02
25	SLE RA 12	-428	4	2722	-1.24	-20.78	0.02
25	SLE RA 13	-428	4	2722	-1.24	-20.78	0.02
25	SLE RA 14	-428	4	2722	-1.24	-20.78	0.02
25	SLE RA 15	-428	4	2722	-1.24	-20.78	0.02
25	SLE RA 16	-428	4	2722	-1.24	-20.78	0.02
25	SLE RA 17	-428	4	2722	-1.24	-20.78	0.02
25	SLE RA 18	-447	4	2854	-1.32	-21.76	0.02
25	SLE RA 19	-447	4	2854	-1.32	-21.76	0.02
25	SLE RA 20	-447	4	2854	-1.32	-21.76	0.02
25	SLE RA 21	-447	4	2854	-1.32	-21.76	0.02
25	SLE FR 1	-383	3	2414	-1.07	-18.48	0.01
25	SLE FR 2	-383	3	2414	-1.07	-18.48	0.01
25	SLE FR 3	-383	3	2414	-1.07	-18.48	0.01
25	SLE FR 4	-402	4	2546	-1.14	-19.47	0.02
25	SLE FR 5	-402	4	2546	-1.14	-19.47	0.02
25	SLE FR 6	-415	4	2634	-1.19	-20.12	0.02
25	SLE QP 1	-383	3	2414	-1.07	-18.48	0.01
25	SLE QP 2	-402	4	2546	-1.14	-19.47	0.02
25	SLD 1	-216	15	2352	-9.41	-10.55	0
25	SLD 2	-216	15	2352	-9.41	-10.55	0
25	SLD 3	-169	18	2180	-5.32	-8.95	-0.01
25	SLD 4	-169	18	2180	-5.32	-8.95	-0.01
25	SLD 5	-417	2	2749	-9.82	-19.22	0.03
25	SLD 6	-417	2	2749	-9.82	-19.22	0.03
25	SLD 7	-261	13	2175	3.8	-13.88	-0.01
25	SLD 8	-261	13	2175	3.8	-13.88	-0.01
25	SLD 9	-543	-6	2917	-6.09	-25.05	0.04
25	SLD 10	-543	-6	2917	-6.09	-25.05	0.04
25	SLD 11	-387	5	2343	7.54	-19.71	0
25	SLD 12	-387	5	2343	7.54	-19.71	0
25	SLD 13	-635	-11	2912	3.04	-29.98	0.04
25	SLD 14	-635	-11	2912	3.04	-29.98	0.04
25	SLD 15	-588	-8	2740	7.13	-28.38	0.03
25	SLD 16	-588	-8	2740	7.13	-28.38	0.03
25	SLV 1	34	32	2089	-22.11	1.46	-0.02
25	SLV 2	34	32	2089	-22.11	1.46	-0.02
25	SLV 3	145	40	1683	-11.79	5.25	-0.04
25	SLV 4	145	40	1683	-11.79	5.25	-0.04
25	SLV 5	-439	-1	3026	-23.08	-18.95	0.04
25	SLV 6	-439	-1	3026	-23.08	-18.95	0.04
25	SLV 7	-70	27	1670	11.31	-6.29	-0.04
25	SLV 8	-70	27	1670	11.31	-6.29	-0.04
25	SLV 9	-734	-20	3422	-13.6	-32.64	0.07
25	SLV 10	-734	-20	3422	-13.6	-32.64	0.07
25	SLV 11	-365	8	2066	20.8	-19.98	-0.01
25	SLV 12	-365	8	2066	20.8	-19.98	-0.01
25	SLV 13	-949	-33	3409	9.5	-44.19	0.07
25	SLV 14	-949	-33	3409	9.5	-44.19	0.07
25	SLV 15	-838	-24	3003	19.82	-40.39	0.05
25	SLV 16	-838	-24	3003	19.82	-40.39	0.05
26	SLU 1	-426	387	2927	-10.68	-12.12	0.01
26	SLU 2	-426	387	2927	-10.68	-12.12	0.01
26	SLU 3	-426	387	2927	-10.68	-12.12	0.01
26	SLU 4	-426	387	2927	-10.68	-12.12	0.01
26	SLU 5	-426	387	2927	-10.68	-12.12	0.01
26	SLU 6	-426	387	2927	-10.68	-12.12	0.01
26	SLU 7	-426	387	2927	-10.68	-12.12	0.01
26	SLU 8	-426	387	2927	-10.68	-12.12	0.01
26	SLU 9	-426	387	2927	-10.68	-12.12	0.01
26	SLU 10	-509	477	3527	-13.37	-14.47	0.01
26	SLU 11	-509	477	3527	-13.37	-14.47	0.01
26	SLU 12	-509	477	3527	-13.37	-14.47	0.01
26	SLU 13	-509	477	3527	-13.37	-14.47	0.01
26	SLU 14	-509	477	3527	-13.37	-14.47	0.01
26	SLU 15	-509	477	3527	-13.37	-14.47	0.01
26	SLU 16	-509	477	3527	-13.37	-14.47	0.01
26	SLU 17	-509	477	3527	-13.37	-14.47	0.01
26	SLU 18	-545	516	3785	-14.53	-15.47	0.01
26	SLU 19	-545	516	3785	-14.53	-15.47	0.01
26	SLU 20	-545	516	3785	-14.53	-15.47	0.01
26	SLU 21	-545	516	3785	-14.53	-15.47	0.01
26	SLU 22	-477	431	3255	-11.93	-13.63	0.02
26	SLU 23	-477	431	3255	-11.93	-13.63	0.02
26	SLU 24	-477	431	3255	-11.93	-13.63	0.02
26	SLU 25	-477	431	3255	-11.93	-13.63	0.02
26	SLU 26	-477	431	3255	-11.93	-13.63	0.02
26	SLU 27	-477	431	3255	-11.93	-13.63	0.02
26	SLU 28	-477	431	3255	-11.93	-13.63	0.02
26	SLU 29	-477	431	3255	-11.93	-13.63	0.02
26	SLU 30	-477	431	3255	-11.93	-13.63	0.02
26	SLU 31	-560	521	3855	-14.62	-15.97	0.01
26	SLU 32	-560	521	3855	-14.62	-15.97	0.01
26	SLU 33	-560	521	3855	-14.62	-15.97	0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
26	SLU 34	-560	521	3855	-14.62	-15.97	0.01
26	SLU 35	-560	521	3855	-14.62	-15.97	0.01
26	SLU 36	-560	521	3855	-14.62	-15.97	0.01
26	SLU 37	-560	521	3855	-14.62	-15.97	0.01
26	SLU 38	-560	521	3855	-14.62	-15.97	0.01
26	SLU 39	-596	560	4112	-15.78	-16.98	0.01
26	SLU 40	-596	560	4112	-15.78	-16.98	0.01
26	SLU 41	-596	560	4112	-15.78	-16.98	0.01
26	SLU 42	-596	560	4112	-15.78	-16.98	0.01
26	SLU 43	-536	489	3693	-13.46	-15.24	0.02
26	SLU 44	-536	489	3693	-13.46	-15.24	0.02
26	SLU 45	-536	489	3693	-13.46	-15.24	0.02
26	SLU 46	-536	489	3693	-13.46	-15.24	0.02
26	SLU 47	-536	489	3693	-13.46	-15.24	0.02
26	SLU 48	-536	489	3693	-13.46	-15.24	0.02
26	SLU 49	-536	489	3693	-13.46	-15.24	0.02
26	SLU 50	-536	489	3693	-13.46	-15.24	0.02
26	SLU 51	-536	489	3693	-13.46	-15.24	0.02
26	SLU 52	-619	579	4293	-16.15	-17.58	0.01
26	SLU 53	-619	579	4293	-16.15	-17.58	0.01
26	SLU 54	-619	579	4293	-16.15	-17.58	0.01
26	SLU 55	-619	579	4293	-16.15	-17.58	0.01
26	SLU 56	-619	579	4293	-16.15	-17.58	0.01
26	SLU 57	-619	579	4293	-16.15	-17.58	0.01
26	SLU 58	-619	579	4293	-16.15	-17.58	0.01
26	SLU 59	-619	579	4293	-16.15	-17.58	0.01
26	SLU 60	-655	617	4550	-17.3	-18.59	0.01
26	SLU 61	-655	617	4550	-17.3	-18.59	0.01
26	SLU 62	-655	617	4550	-17.3	-18.59	0.01
26	SLU 63	-655	617	4550	-17.3	-18.59	0.01
26	SLU 64	-587	532	4021	-14.71	-16.74	0.02
26	SLU 65	-587	532	4021	-14.71	-16.74	0.02
26	SLU 66	-587	532	4021	-14.71	-16.74	0.02
26	SLU 67	-587	532	4021	-14.71	-16.74	0.02
26	SLU 68	-587	532	4021	-14.71	-16.74	0.02
26	SLU 69	-587	532	4021	-14.71	-16.74	0.02
26	SLU 70	-587	532	4021	-14.71	-16.74	0.02
26	SLU 71	-587	532	4021	-14.71	-16.74	0.02
26	SLU 72	-587	532	4021	-14.71	-16.74	0.02
26	SLU 73	-671	622	4621	-17.4	-19.09	0.02
26	SLU 74	-671	622	4621	-17.4	-19.09	0.02
26	SLU 75	-671	622	4621	-17.4	-19.09	0.02
26	SLU 76	-671	622	4621	-17.4	-19.09	0.02
26	SLU 77	-671	622	4621	-17.4	-19.09	0.02
26	SLU 78	-671	622	4621	-17.4	-19.09	0.02
26	SLU 79	-671	622	4621	-17.4	-19.09	0.02
26	SLU 80	-671	622	4621	-17.4	-19.09	0.02
26	SLU 81	-706	661	4878	-18.55	-20.1	0.01
26	SLU 82	-706	661	4878	-18.55	-20.1	0.01
26	SLU 83	-706	661	4878	-18.55	-20.1	0.01
26	SLU 84	-706	661	4878	-18.55	-20.1	0.01
26	SLE RA 1	-441	400	3021	-11.04	-12.55	0.01
26	SLE RA 2	-441	400	3021	-11.04	-12.55	0.01
26	SLE RA 3	-441	400	3021	-11.04	-12.55	0.01
26	SLE RA 4	-441	400	3021	-11.04	-12.55	0.01
26	SLE RA 5	-441	400	3021	-11.04	-12.55	0.01
26	SLE RA 6	-441	400	3021	-11.04	-12.55	0.01
26	SLE RA 7	-441	400	3021	-11.04	-12.55	0.01
26	SLE RA 8	-441	400	3021	-11.04	-12.55	0.01
26	SLE RA 9	-441	400	3021	-11.04	-12.55	0.01
26	SLE RA 10	-496	460	3421	-12.83	-14.11	0.01
26	SLE RA 11	-496	460	3421	-12.83	-14.11	0.01
26	SLE RA 12	-496	460	3421	-12.83	-14.11	0.01
26	SLE RA 13	-496	460	3421	-12.83	-14.11	0.01
26	SLE RA 14	-496	460	3421	-12.83	-14.11	0.01
26	SLE RA 15	-496	460	3421	-12.83	-14.11	0.01
26	SLE RA 16	-496	460	3421	-12.83	-14.11	0.01
26	SLE RA 17	-496	460	3421	-12.83	-14.11	0.01
26	SLE RA 18	-520	486	3592	-13.6	-14.78	0.01
26	SLE RA 19	-520	486	3592	-13.6	-14.78	0.01
26	SLE RA 20	-520	486	3592	-13.6	-14.78	0.01
26	SLE RA 21	-520	486	3592	-13.6	-14.78	0.01
26	SLE FR 1	-441	400	3021	-11.04	-12.55	0.01
26	SLE FR 2	-441	400	3021	-11.04	-12.55	0.01
26	SLE FR 3	-441	400	3021	-11.04	-12.55	0.01
26	SLE FR 4	-464	426	3192	-11.81	-13.22	0.01
26	SLE FR 5	-464	426	3192	-11.81	-13.22	0.01
26	SLE FR 6	-480	443	3307	-12.32	-13.67	0.01
26	SLE QP 1	-441	400	3021	-11.04	-12.55	0.01
26	SLE QP 2	-464	426	3192	-11.81	-13.22	0.01
26	SLD 1	-333	422	2835	-11.75	-8.11	-0.06
26	SLD 2	-333	422	2835	-11.75	-8.11	-0.06
26	SLD 3	-312	338	2564	-8.4	-7.34	-0.03
26	SLD 4	-312	338	2564	-8.4	-7.34	-0.03
26	SLD 5	-456	552	3497	-16.86	-12.85	-0.06
26	SLD 6	-456	552	3497	-16.86	-12.85	-0.06
26	SLD 7	-387	272	2592	-5.72	-10.29	0.06
26	SLD 8	-387	272	2592	-5.72	-10.29	0.06
26	SLD 9	-541	579	3793	-17.9	-16.15	-0.03



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
26	SLD 10	-541	579	3793	-17.9	-16.15	-0.03
26	SLD 11	-472	300	2888	-6.76	-13.59	0.09
26	SLD 12	-472	300	2888	-6.76	-13.59	0.09
26	SLD 13	-617	513	3821	-15.21	-19.1	0.05
26	SLD 14	-617	513	3821	-15.21	-19.1	0.05
26	SLD 15	-596	430	3549	-11.87	-18.33	0.09
26	SLD 16	-596	430	3549	-11.87	-18.33	0.09
26	SLV 1	-156	415	2352	-11.63	-1.19	-0.16
26	SLV 2	-156	415	2352	-11.63	-1.19	-0.16
26	SLV 3	-105	218	1711	-3.76	0.64	-0.08
26	SLV 4	-105	218	1711	-3.76	0.64	-0.08
26	SLV 5	-449	721	3913	-23.7	-12.38	-0.17
26	SLV 6	-449	721	3913	-23.7	-12.38	-0.17
26	SLV 7	-280	65	1775	2.55	-6.29	0.12
26	SLV 8	-280	65	1775	2.55	-6.29	0.12
26	SLV 9	-649	786	4610	-26.17	-20.15	-0.09
26	SLV 10	-649	786	4610	-26.17	-20.15	-0.09
26	SLV 11	-480	130	2471	0.08	-14.06	0.2
26	SLV 12	-480	130	2471	0.08	-14.06	0.2
26	SLV 13	-824	633	4674	-19.86	-27.08	0.11
26	SLV 14	-824	633	4674	-19.86	-27.08	0.11
26	SLV 15	-773	436	4032	-11.98	-25.25	0.19
26	SLV 16	-773	436	4032	-11.98	-25.25	0.19
27	SLU 1	3	305	2211	-14.98	1.08	0.01
27	SLU 2	3	305	2211	-14.98	1.08	0.01
27	SLU 3	3	305	2211	-14.98	1.08	0.01
27	SLU 4	3	305	2211	-14.98	1.08	0.01
27	SLU 5	3	305	2211	-14.98	1.08	0.01
27	SLU 6	3	305	2211	-14.98	1.08	0.01
27	SLU 7	3	305	2211	-14.98	1.08	0.01
27	SLU 8	3	305	2211	-14.98	1.08	0.01
27	SLU 9	3	305	2211	-14.98	1.08	0.01
27	SLU 10	4	381	2598	-18.62	1.27	0.02
27	SLU 11	4	381	2598	-18.62	1.27	0.02
27	SLU 12	4	381	2598	-18.62	1.27	0.02
27	SLU 13	4	381	2598	-18.62	1.27	0.02
27	SLU 14	4	381	2598	-18.62	1.27	0.02
27	SLU 15	4	381	2598	-18.62	1.27	0.02
27	SLU 16	4	381	2598	-18.62	1.27	0.02
27	SLU 17	4	381	2598	-18.62	1.27	0.02
27	SLU 18	4	414	2764	-20.18	1.35	0.02
27	SLU 19	4	414	2764	-20.18	1.35	0.02
27	SLU 20	4	414	2764	-20.18	1.35	0.02
27	SLU 21	4	414	2764	-20.18	1.35	0.02
27	SLU 22	4	342	2440	-16.79	1.2	0.01
27	SLU 23	4	342	2440	-16.79	1.2	0.01
27	SLU 24	4	342	2440	-16.79	1.2	0.01
27	SLU 25	4	342	2440	-16.79	1.2	0.01
27	SLU 26	4	342	2440	-16.79	1.2	0.01
27	SLU 27	4	342	2440	-16.79	1.2	0.01
27	SLU 28	4	342	2440	-16.79	1.2	0.01
27	SLU 29	4	342	2440	-16.79	1.2	0.01
27	SLU 30	4	342	2440	-16.79	1.2	0.01
27	SLU 31	4	418	2828	-20.43	1.4	0.02
27	SLU 32	4	418	2828	-20.43	1.4	0.02
27	SLU 33	4	418	2828	-20.43	1.4	0.02
27	SLU 34	4	418	2828	-20.43	1.4	0.02
27	SLU 35	4	418	2828	-20.43	1.4	0.02
27	SLU 36	4	418	2828	-20.43	1.4	0.02
27	SLU 37	4	418	2828	-20.43	1.4	0.02
27	SLU 38	4	418	2828	-20.43	1.4	0.02
27	SLU 39	5	450	2993	-21.99	1.48	0.02
27	SLU 40	5	450	2993	-21.99	1.48	0.02
27	SLU 41	5	450	2993	-21.99	1.48	0.02
27	SLU 42	5	450	2993	-21.99	1.48	0.02
27	SLU 43	4	384	2795	-18.85	1.36	0.02
27	SLU 44	4	384	2795	-18.85	1.36	0.02
27	SLU 45	4	384	2795	-18.85	1.36	0.02
27	SLU 46	4	384	2795	-18.85	1.36	0.02
27	SLU 47	4	384	2795	-18.85	1.36	0.02
27	SLU 48	4	384	2795	-18.85	1.36	0.02
27	SLU 49	4	384	2795	-18.85	1.36	0.02
27	SLU 50	4	384	2795	-18.85	1.36	0.02
27	SLU 51	4	384	2795	-18.85	1.36	0.02
27	SLU 52	5	460	3182	-22.49	1.55	0.02
27	SLU 53	5	460	3182	-22.49	1.55	0.02
27	SLU 54	5	460	3182	-22.49	1.55	0.02
27	SLU 55	5	460	3182	-22.49	1.55	0.02
27	SLU 56	5	460	3182	-22.49	1.55	0.02
27	SLU 57	5	460	3182	-22.49	1.55	0.02
27	SLU 58	5	460	3182	-22.49	1.55	0.02
27	SLU 59	5	460	3182	-22.49	1.55	0.02
27	SLU 60	5	493	3348	-24.05	1.63	0.02
27	SLU 61	5	493	3348	-24.05	1.63	0.02
27	SLU 62	5	493	3348	-24.05	1.63	0.02
27	SLU 63	5	493	3348	-24.05	1.63	0.02
27	SLU 64	5	421	3025	-20.66	1.48	0.02
27	SLU 65	5	421	3025	-20.66	1.48	0.02
27	SLU 66	5	421	3025	-20.66	1.48	0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
27	SLU 67	5	421	3025	-20.66	1.48	0.02
27	SLU 68	5	421	3025	-20.66	1.48	0.02
27	SLU 69	5	421	3025	-20.66	1.48	0.02
27	SLU 70	5	421	3025	-20.66	1.48	0.02
27	SLU 71	5	421	3025	-20.66	1.48	0.02
27	SLU 72	5	421	3025	-20.66	1.48	0.02
27	SLU 73	5	497	3412	-24.3	1.68	0.02
27	SLU 74	5	497	3412	-24.3	1.68	0.02
27	SLU 75	5	497	3412	-24.3	1.68	0.02
27	SLU 76	5	497	3412	-24.3	1.68	0.02
27	SLU 77	5	497	3412	-24.3	1.68	0.02
27	SLU 78	5	497	3412	-24.3	1.68	0.02
27	SLU 79	5	497	3412	-24.3	1.68	0.02
27	SLU 80	5	497	3412	-24.3	1.68	0.02
27	SLU 81	6	530	3578	-25.86	1.76	0.02
27	SLU 82	6	530	3578	-25.86	1.76	0.02
27	SLU 83	6	530	3578	-25.86	1.76	0.02
27	SLU 84	6	530	3578	-25.86	1.76	0.02
27	SLE RA 1	3	316	2276	-15.49	1.11	0.01
27	SLE RA 2	3	316	2276	-15.49	1.11	0.01
27	SLE RA 3	3	316	2276	-15.49	1.11	0.01
27	SLE RA 4	3	316	2276	-15.49	1.11	0.01
27	SLE RA 5	3	316	2276	-15.49	1.11	0.01
27	SLE RA 6	3	316	2276	-15.49	1.11	0.01
27	SLE RA 7	3	316	2276	-15.49	1.11	0.01
27	SLE RA 8	3	316	2276	-15.49	1.11	0.01
27	SLE RA 9	3	316	2276	-15.49	1.11	0.01
27	SLE RA 10	4	366	2534	-17.92	1.24	0.02
27	SLE RA 11	4	366	2534	-17.92	1.24	0.02
27	SLE RA 12	4	366	2534	-17.92	1.24	0.02
27	SLE RA 13	4	366	2534	-17.92	1.24	0.02
27	SLE RA 14	4	366	2534	-17.92	1.24	0.02
27	SLE RA 15	4	366	2534	-17.92	1.24	0.02
27	SLE RA 16	4	366	2534	-17.92	1.24	0.02
27	SLE RA 17	4	366	2534	-17.92	1.24	0.02
27	SLE RA 18	4	388	2645	-18.96	1.3	0.02
27	SLE RA 19	4	388	2645	-18.96	1.3	0.02
27	SLE RA 20	4	388	2645	-18.96	1.3	0.02
27	SLE RA 21	4	388	2645	-18.96	1.3	0.02
27	SLE FR 1	3	316	2276	-15.49	1.11	0.01
27	SLE FR 2	3	316	2276	-15.49	1.11	0.01
27	SLE FR 3	3	316	2276	-15.49	1.11	0.01
27	SLE FR 4	4	337	2387	-16.53	1.17	0.01
27	SLE FR 5	4	337	2387	-16.53	1.17	0.01
27	SLE FR 6	4	352	2461	-17.23	1.21	0.01
27	SLE QP 1	3	316	2276	-15.49	1.11	0.01
27	SLE QP 2	4	337	2387	-16.53	1.17	0.01
27	SLD 1	7	299	2793	-15.3	5.75	0.03
27	SLD 2	7	299	2793	-15.3	5.75	0.03
27	SLD 3	15	155	2584	-8.7	9.5	0.02
27	SLD 4	15	155	2584	-8.7	9.5	0.02
27	SLD 5	-7	544	2826	-26.17	-3.14	0.03
27	SLD 6	-7	544	2826	-26.17	-3.14	0.03
27	SLD 7	18	65	2130	-4.18	9.35	0
27	SLD 8	18	65	2130	-4.18	9.35	0
27	SLD 9	-11	610	2644	-28.89	-7.01	0.03
27	SLD 10	-11	610	2644	-28.89	-7.01	0.03
27	SLD 11	14	131	1948	-6.9	5.48	0
27	SLD 12	14	131	1948	-6.9	5.48	0
27	SLD 13	-8	520	2190	-24.37	-7.16	0.01
27	SLD 14	-8	520	2190	-24.37	-7.16	0.01
27	SLD 15	0	376	1981	-17.77	-3.41	0
27	SLD 16	0	376	1981	-17.77	-3.41	0
27	SLV 1	13	242	3350	-13.32	12.44	0.05
27	SLV 2	13	242	3350	-13.32	12.44	0.05
27	SLV 3	32	-96	2858	2.19	21.98	0.03
27	SLV 4	32	-96	2858	2.19	21.98	0.03
27	SLV 5	-22	822	3421	-39.1	-9.91	0.06
27	SLV 6	-22	822	3421	-39.1	-9.91	0.06
27	SLV 7	41	-306	1783	12.61	21.87	-0.02
27	SLV 8	41	-306	1783	12.61	21.87	-0.02
27	SLV 9	-34	981	2991	-45.68	-19.53	0.05
27	SLV 10	-34	981	2991	-45.68	-19.53	0.05
27	SLV 11	29	-147	1353	6.03	12.25	-0.03
27	SLV 12	29	-147	1353	6.03	12.25	-0.03
27	SLV 13	-25	771	1916	-35.26	-19.64	0
27	SLV 14	-25	771	1916	-35.26	-19.64	0
27	SLV 15	-6	433	1424	-19.75	-10.11	-0.02
27	SLV 16	-6	433	1424	-19.75	-10.11	-0.02
28	SLU 1	0	0	972	0.19	0	0
28	SLU 2	0	0	972	0.19	0	0
28	SLU 3	0	0	972	0.19	0	0
28	SLU 4	0	0	972	0.19	0	0
28	SLU 5	0	0	972	0.19	0	0
28	SLU 6	0	0	972	0.19	0	0
28	SLU 7	0	0	972	0.19	0	0
28	SLU 8	0	0	972	0.19	0	0
28	SLU 9	0	0	972	0.19	0	0
28	SLU 10	0	0	1224	0.26	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
28	SLU 11	0	0	1224	0.26	0	0
28	SLU 12	0	0	1224	0.26	0	0
28	SLU 13	0	0	1224	0.26	0	0
28	SLU 14	0	0	1224	0.26	0	0
28	SLU 15	0	0	1224	0.26	0	0
28	SLU 16	0	0	1224	0.26	0	0
28	SLU 17	0	0	1224	0.26	0	0
28	SLU 18	0	0	1333	0.29	0	0
28	SLU 19	0	0	1333	0.29	0	0
28	SLU 20	0	0	1333	0.29	0	0
28	SLU 21	0	0	1333	0.29	0	0
28	SLU 22	0	0	1114	0.24	0	0
28	SLU 23	0	0	1114	0.24	0	0
28	SLU 24	0	0	1114	0.24	0	0
28	SLU 25	0	0	1114	0.24	0	0
28	SLU 26	0	0	1114	0.24	0	0
28	SLU 27	0	0	1114	0.24	0	0
28	SLU 28	0	0	1114	0.24	0	0
28	SLU 29	0	0	1114	0.24	0	0
28	SLU 30	0	0	1114	0.24	0	0
28	SLU 31	0	0	1367	0.31	0	0
28	SLU 32	0	0	1367	0.31	0	0
28	SLU 33	0	0	1367	0.31	0	0
28	SLU 34	0	0	1367	0.31	0	0
28	SLU 35	0	0	1367	0.31	0	0
28	SLU 36	0	0	1367	0.31	0	0
28	SLU 37	0	0	1367	0.31	0	0
28	SLU 38	0	0	1367	0.31	0	0
28	SLU 39	0	0	1475	0.34	0	0
28	SLU 40	0	0	1475	0.34	0	0
28	SLU 41	0	0	1475	0.34	0	0
28	SLU 42	0	0	1475	0.34	0	0
28	SLU 43	0	0	1214	0.23	0	0
28	SLU 44	0	0	1214	0.23	0	0
28	SLU 45	0	0	1214	0.23	0	0
28	SLU 46	0	0	1214	0.23	0	0
28	SLU 47	0	0	1214	0.23	0	0
28	SLU 48	0	0	1214	0.23	0	0
28	SLU 49	0	0	1214	0.23	0	0
28	SLU 50	0	0	1214	0.23	0	0
28	SLU 51	0	0	1214	0.23	0	0
28	SLU 52	0	0	1467	0.3	0	0
28	SLU 53	0	0	1467	0.3	0	0
28	SLU 54	0	0	1467	0.3	0	0
28	SLU 55	0	0	1467	0.3	0	0
28	SLU 56	0	0	1467	0.3	0	0
28	SLU 57	0	0	1467	0.3	0	0
28	SLU 58	0	0	1467	0.3	0	0
28	SLU 59	0	0	1467	0.3	0	0
28	SLU 60	0	0	1575	0.33	0	0
28	SLU 61	0	0	1575	0.33	0	0
28	SLU 62	0	0	1575	0.33	0	0
28	SLU 63	0	0	1575	0.33	0	0
28	SLU 64	0	0	1357	0.28	0	0
28	SLU 65	0	0	1357	0.28	0	0
28	SLU 66	0	0	1357	0.28	0	0
28	SLU 67	0	0	1357	0.28	0	0
28	SLU 68	0	0	1357	0.28	0	0
28	SLU 69	0	0	1357	0.28	0	0
28	SLU 70	0	0	1357	0.28	0	0
28	SLU 71	0	0	1357	0.28	0	0
28	SLU 72	0	0	1357	0.28	0	0
28	SLU 73	0	0	1609	0.35	0	0
28	SLU 74	0	0	1609	0.35	0	0
28	SLU 75	0	0	1609	0.35	0	0
28	SLU 76	0	0	1609	0.35	0	0
28	SLU 77	0	0	1609	0.35	0	0
28	SLU 78	0	0	1609	0.35	0	0
28	SLU 79	0	0	1609	0.35	0	0
28	SLU 80	0	0	1609	0.35	0	0
28	SLU 81	0	0	1718	0.38	0	0
28	SLU 82	0	0	1718	0.38	0	0
28	SLU 83	0	0	1718	0.38	0	0
28	SLU 84	0	0	1718	0.38	0	0
28	SLE RA 1	0	0	1012	0.2	0	0
28	SLE RA 2	0	0	1012	0.2	0	0
28	SLE RA 3	0	0	1012	0.2	0	0
28	SLE RA 4	0	0	1012	0.2	0	0
28	SLE RA 5	0	0	1012	0.2	0	0
28	SLE RA 6	0	0	1012	0.2	0	0
28	SLE RA 7	0	0	1012	0.2	0	0
28	SLE RA 8	0	0	1012	0.2	0	0
28	SLE RA 9	0	0	1012	0.2	0	0
28	SLE RA 10	0	0	1181	0.25	0	0
28	SLE RA 11	0	0	1181	0.25	0	0
28	SLE RA 12	0	0	1181	0.25	0	0
28	SLE RA 13	0	0	1181	0.25	0	0
28	SLE RA 14	0	0	1181	0.25	0	0
28	SLE RA 15	0	0	1181	0.25	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
28	SLE RA 16	0	0	1181	0.25	0	0
28	SLE RA 17	0	0	1181	0.25	0	0
28	SLE RA 18	0	0	1253	0.27	0	0
28	SLE RA 19	0	0	1253	0.27	0	0
28	SLE RA 20	0	0	1253	0.27	0	0
28	SLE RA 21	0	0	1253	0.27	0	0
28	SLE FR 1	0	0	1012	0.2	0	0
28	SLE FR 2	0	0	1012	0.2	0	0
28	SLE FR 3	0	0	1012	0.2	0	0
28	SLE FR 4	0	0	1085	0.22	0	0
28	SLE FR 5	0	0	1085	0.22	0	0
28	SLE FR 6	0	0	1133	0.24	0	0
28	SLE QP 1	0	0	1012	0.2	0	0
28	SLE QP 2	0	0	1085	0.22	0	0
28	SLD 1	-1	9	1047	-58.77	1.4	-0.02
28	SLD 2	-1	9	1047	-58.77	1.4	-0.02
28	SLD 3	-1	-17	1153	111.64	1.12	-0.03
28	SLD 4	-1	-17	1153	111.64	1.12	-0.03
28	SLD 5	0	42	911	-275.93	0.85	0
28	SLD 6	0	42	911	-275.93	0.85	0
28	SLD 7	-1	-44	1267	292.11	-0.09	-0.01
28	SLD 8	-1	-44	1267	292.11	-0.09	-0.01
28	SLD 9	1	44	902	-291.66	0.09	0.01
28	SLD 10	1	44	902	-291.66	0.09	0.01
28	SLD 11	0	-41	1258	276.38	-0.85	0
28	SLD 12	0	-41	1258	276.38	-0.85	0
28	SLD 13	1	17	1016	-111.19	-1.12	0.03
28	SLD 14	1	17	1016	-111.19	-1.12	0.03
28	SLD 15	1	-9	1122	59.22	-1.4	0.02
28	SLD 16	1	-9	1122	59.22	-1.4	0.02
28	SLV 1	-2	23	987	-151.13	3.57	-0.05
28	SLV 2	-2	23	987	-151.13	3.57	-0.05
28	SLV 3	-2	-43	1261	286.06	2.86	-0.06
28	SLV 4	-2	-43	1261	286.06	2.86	-0.06
28	SLV 5	0	107	640	-708.26	2.16	0
28	SLV 6	0	107	640	-708.26	2.16	0
28	SLV 7	-1	-113	1553	749.06	-0.23	-0.04
28	SLV 8	-1	-113	1553	749.06	-0.23	-0.04
28	SLV 9	1	113	616	-748.61	0.23	0.04
28	SLV 10	1	113	616	-748.61	0.23	0.04
28	SLV 11	0	-106	1529	708.71	-2.16	0
28	SLV 12	0	-106	1529	708.71	-2.16	0
28	SLV 13	2	44	908	-285.61	-2.86	0.06
28	SLV 14	2	44	908	-285.61	-2.86	0.06
28	SLV 15	2	-22	1182	151.58	-3.57	0.05
28	SLV 16	2	-22	1182	151.58	-3.57	0.05
29	SLU 1	-3	301	2273	-14.73	-1.1	-0.02
29	SLU 2	-3	301	2273	-14.73	-1.1	-0.02
29	SLU 3	-3	301	2273	-14.73	-1.1	-0.02
29	SLU 4	-3	301	2273	-14.73	-1.1	-0.02
29	SLU 5	-3	301	2273	-14.73	-1.1	-0.02
29	SLU 6	-3	301	2273	-14.73	-1.1	-0.02
29	SLU 7	-3	301	2273	-14.73	-1.1	-0.02
29	SLU 8	-3	301	2273	-14.73	-1.1	-0.02
29	SLU 9	-3	301	2273	-14.73	-1.1	-0.02
29	SLU 10	-4	382	2716	-18.69	-1.33	-0.02
29	SLU 11	-4	382	2716	-18.69	-1.33	-0.02
29	SLU 12	-4	382	2716	-18.69	-1.33	-0.02
29	SLU 13	-4	382	2716	-18.69	-1.33	-0.02
29	SLU 14	-4	382	2716	-18.69	-1.33	-0.02
29	SLU 15	-4	382	2716	-18.69	-1.33	-0.02
29	SLU 16	-4	382	2716	-18.69	-1.33	-0.02
29	SLU 17	-4	382	2716	-18.69	-1.33	-0.02
29	SLU 18	-4	418	2906	-20.39	-1.42	-0.02
29	SLU 19	-4	418	2906	-20.39	-1.42	-0.02
29	SLU 20	-4	418	2906	-20.39	-1.42	-0.02
29	SLU 21	-4	418	2906	-20.39	-1.42	-0.02
29	SLU 22	-4	336	2512	-16.5	-1.24	-0.02
29	SLU 23	-4	336	2512	-16.5	-1.24	-0.02
29	SLU 24	-4	336	2512	-16.5	-1.24	-0.02
29	SLU 25	-4	336	2512	-16.5	-1.24	-0.02
29	SLU 26	-4	336	2512	-16.5	-1.24	-0.02
29	SLU 27	-4	336	2512	-16.5	-1.24	-0.02
29	SLU 28	-4	336	2512	-16.5	-1.24	-0.02
29	SLU 29	-4	336	2512	-16.5	-1.24	-0.02
29	SLU 30	-4	336	2512	-16.5	-1.24	-0.02
29	SLU 31	-5	417	2955	-20.46	-1.46	-0.02
29	SLU 32	-5	417	2955	-20.46	-1.46	-0.02
29	SLU 33	-5	417	2955	-20.46	-1.46	-0.02
29	SLU 34	-5	417	2955	-20.46	-1.46	-0.02
29	SLU 35	-5	417	2955	-20.46	-1.46	-0.02
29	SLU 36	-5	417	2955	-20.46	-1.46	-0.02
29	SLU 37	-5	417	2955	-20.46	-1.46	-0.02
29	SLU 38	-5	417	2955	-20.46	-1.46	-0.02
29	SLU 39	-5	452	3145	-22.16	-1.56	-0.02
29	SLU 40	-5	452	3145	-22.16	-1.56	-0.02
29	SLU 41	-5	452	3145	-22.16	-1.56	-0.02
29	SLU 42	-5	452	3145	-22.16	-1.56	-0.02
29	SLU 43	-4	379	2873	-18.54	-1.39	-0.02



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
29	SLU 44	-4	379	2873	-18.54	-1.39	-0.02
29	SLU 45	-4	379	2873	-18.54	-1.39	-0.02
29	SLU 46	-4	379	2873	-18.54	-1.39	-0.02
29	SLU 47	-4	379	2873	-18.54	-1.39	-0.02
29	SLU 48	-4	379	2873	-18.54	-1.39	-0.02
29	SLU 49	-4	379	2873	-18.54	-1.39	-0.02
29	SLU 50	-4	379	2873	-18.54	-1.39	-0.02
29	SLU 51	-4	379	2873	-18.54	-1.39	-0.02
29	SLU 52	-5	461	3316	-22.5	-1.61	-0.03
29	SLU 53	-5	461	3316	-22.5	-1.61	-0.03
29	SLU 54	-5	461	3316	-22.5	-1.61	-0.03
29	SLU 55	-5	461	3316	-22.5	-1.61	-0.03
29	SLU 56	-5	461	3316	-22.5	-1.61	-0.03
29	SLU 57	-5	461	3316	-22.5	-1.61	-0.03
29	SLU 58	-5	461	3316	-22.5	-1.61	-0.03
29	SLU 59	-5	461	3316	-22.5	-1.61	-0.03
29	SLU 60	-5	496	3506	-24.2	-1.71	-0.03
29	SLU 61	-5	496	3506	-24.2	-1.71	-0.03
29	SLU 62	-5	496	3506	-24.2	-1.71	-0.03
29	SLU 63	-5	496	3506	-24.2	-1.71	-0.03
29	SLU 64	-5	414	3112	-20.31	-1.52	-0.02
29	SLU 65	-5	414	3112	-20.31	-1.52	-0.02
29	SLU 66	-5	414	3112	-20.31	-1.52	-0.02
29	SLU 67	-5	414	3112	-20.31	-1.52	-0.02
29	SLU 68	-5	414	3112	-20.31	-1.52	-0.02
29	SLU 69	-5	414	3112	-20.31	-1.52	-0.02
29	SLU 70	-5	414	3112	-20.31	-1.52	-0.02
29	SLU 71	-5	414	3112	-20.31	-1.52	-0.02
29	SLU 72	-5	414	3112	-20.31	-1.52	-0.02
29	SLU 73	-5	496	3555	-24.27	-1.75	-0.03
29	SLU 74	-5	496	3555	-24.27	-1.75	-0.03
29	SLU 75	-5	496	3555	-24.27	-1.75	-0.03
29	SLU 76	-5	496	3555	-24.27	-1.75	-0.03
29	SLU 77	-5	496	3555	-24.27	-1.75	-0.03
29	SLU 78	-5	496	3555	-24.27	-1.75	-0.03
29	SLU 79	-5	496	3555	-24.27	-1.75	-0.03
29	SLU 80	-5	496	3555	-24.27	-1.75	-0.03
29	SLU 81	-6	531	3745	-25.97	-1.84	-0.03
29	SLU 82	-6	531	3745	-25.97	-1.84	-0.03
29	SLU 83	-6	531	3745	-25.97	-1.84	-0.03
29	SLU 84	-6	531	3745	-25.97	-1.84	-0.03
29	SLE RA 1	-4	311	2341	-15.23	-1.14	-0.02
29	SLE RA 2	-4	311	2341	-15.23	-1.14	-0.02
29	SLE RA 3	-4	311	2341	-15.23	-1.14	-0.02
29	SLE RA 4	-4	311	2341	-15.23	-1.14	-0.02
29	SLE RA 5	-4	311	2341	-15.23	-1.14	-0.02
29	SLE RA 6	-4	311	2341	-15.23	-1.14	-0.02
29	SLE RA 7	-4	311	2341	-15.23	-1.14	-0.02
29	SLE RA 8	-4	311	2341	-15.23	-1.14	-0.02
29	SLE RA 9	-4	311	2341	-15.23	-1.14	-0.02
29	SLE RA 10	-4	365	2637	-17.88	-1.29	-0.02
29	SLE RA 11	-4	365	2637	-17.88	-1.29	-0.02
29	SLE RA 12	-4	365	2637	-17.88	-1.29	-0.02
29	SLE RA 13	-4	365	2637	-17.88	-1.29	-0.02
29	SLE RA 14	-4	365	2637	-17.88	-1.29	-0.02
29	SLE RA 15	-4	365	2637	-17.88	-1.29	-0.02
29	SLE RA 16	-4	365	2637	-17.88	-1.29	-0.02
29	SLE RA 17	-4	365	2637	-17.88	-1.29	-0.02
29	SLE RA 18	-4	389	2763	-19.01	-1.35	-0.02
29	SLE RA 19	-4	389	2763	-19.01	-1.35	-0.02
29	SLE RA 20	-4	389	2763	-19.01	-1.35	-0.02
29	SLE RA 21	-4	389	2763	-19.01	-1.35	-0.02
29	SLE FR 1	-4	311	2341	-15.23	-1.14	-0.02
29	SLE FR 2	-4	311	2341	-15.23	-1.14	-0.02
29	SLE FR 3	-4	311	2341	-15.23	-1.14	-0.02
29	SLE FR 4	-4	334	2468	-16.37	-1.2	-0.02
29	SLE FR 5	-4	334	2468	-16.37	-1.2	-0.02
29	SLE FR 6	-4	350	2552	-17.12	-1.25	-0.02
29	SLE QP 1	-4	311	2341	-15.23	-1.14	-0.02
29	SLE QP 2	-4	334	2468	-16.37	-1.2	-0.02
29	SLD 1	8	475	2248	-16.27	7.56	-0.01
29	SLD 2	8	475	2248	-16.27	7.56	-0.01
29	SLD 3	0	347	2090	-10.45	4.05	-0.01
29	SLD 4	0	347	2090	-10.45	4.05	-0.01
29	SLD 5	11	571	2643	-25.16	6.75	-0.02
29	SLD 6	11	571	2643	-25.16	6.75	-0.02
29	SLD 7	-14	144	2114	-5.77	-4.96	-0.01
29	SLD 8	-14	144	2114	-5.77	-4.96	-0.01
29	SLD 9	6	524	2822	-26.97	2.55	-0.03
29	SLD 10	6	524	2822	-26.97	2.55	-0.03
29	SLD 11	-19	97	2293	-7.57	-9.16	-0.01
29	SLD 12	-19	97	2293	-7.57	-9.16	-0.01
29	SLD 13	-8	321	2846	-22.28	-6.46	-0.03
29	SLD 14	-8	321	2846	-22.28	-6.46	-0.03
29	SLD 15	-15	193	2688	-16.46	-9.97	-0.03
29	SLD 16	-15	193	2688	-16.46	-9.97	-0.03
29	SLV 1	25	666	1951	-16.12	20.83	0
29	SLV 2	25	666	1951	-16.12	20.83	0
29	SLV 3	6	365	1575	-2.46	11.91	0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
29	SLV 4	6	365	1575	-2.46	11.91	0.01
29	SLV 5	34	890	2883	-37.01	18.93	-0.03
29	SLV 6	34	890	2883	-37.01	18.93	-0.03
29	SLV 7	-29	-113	1630	8.53	-10.8	0.01
29	SLV 8	-29	-113	1630	8.53	-10.8	0.01
29	SLV 9	22	781	3306	-41.26	8.39	-0.04
29	SLV 10	22	781	3306	-41.26	8.39	-0.04
29	SLV 11	-41	-222	2053	4.28	-21.34	-0.01
29	SLV 12	-41	-222	2053	4.28	-21.34	-0.01
29	SLV 13	-14	303	3361	-30.28	-14.32	-0.05
29	SLV 14	-14	303	3361	-30.28	-14.32	-0.05
29	SLV 15	-33	2	2985	-16.61	-23.24	-0.04
29	SLV 16	-33	2	2985	-16.61	-23.24	-0.04
30	SLU 1	0	253	2014	-10.77	0.46	0
30	SLU 2	0	253	2014	-10.77	0.46	0
30	SLU 3	0	253	2014	-10.77	0.46	0
30	SLU 4	0	253	2014	-10.77	0.46	0
30	SLU 5	0	253	2014	-10.77	0.46	0
30	SLU 6	0	253	2014	-10.77	0.46	0
30	SLU 7	0	253	2014	-10.77	0.46	0
30	SLU 8	0	253	2014	-10.77	0.46	0
30	SLU 9	0	253	2014	-10.77	0.46	0
30	SLU 10	0	324	2360	-13.74	0.54	-0.01
30	SLU 11	0	324	2360	-13.74	0.54	-0.01
30	SLU 12	0	324	2360	-13.74	0.54	-0.01
30	SLU 13	0	324	2360	-13.74	0.54	-0.01
30	SLU 14	0	324	2360	-13.74	0.54	-0.01
30	SLU 15	0	324	2360	-13.74	0.54	-0.01
30	SLU 16	0	324	2360	-13.74	0.54	-0.01
30	SLU 17	0	324	2360	-13.74	0.54	-0.01
30	SLU 18	0	354	2508	-15.01	0.57	-0.01
30	SLU 19	0	354	2508	-15.01	0.57	-0.01
30	SLU 20	0	354	2508	-15.01	0.57	-0.01
30	SLU 21	0	354	2508	-15.01	0.57	-0.01
30	SLU 22	0	287	2216	-12.19	0.52	-0.01
30	SLU 23	0	287	2216	-12.19	0.52	-0.01
30	SLU 24	0	287	2216	-12.19	0.52	-0.01
30	SLU 25	0	287	2216	-12.19	0.52	-0.01
30	SLU 26	0	287	2216	-12.19	0.52	-0.01
30	SLU 27	0	287	2216	-12.19	0.52	-0.01
30	SLU 28	0	287	2216	-12.19	0.52	-0.01
30	SLU 29	0	287	2216	-12.19	0.52	-0.01
30	SLU 30	0	287	2216	-12.19	0.52	-0.01
30	SLU 31	0	357	2562	-15.17	0.59	-0.01
30	SLU 32	0	357	2562	-15.17	0.59	-0.01
30	SLU 33	0	357	2562	-15.17	0.59	-0.01
30	SLU 34	0	357	2562	-15.17	0.59	-0.01
30	SLU 35	0	357	2562	-15.17	0.59	-0.01
30	SLU 36	0	357	2562	-15.17	0.59	-0.01
30	SLU 37	0	357	2562	-15.17	0.59	-0.01
30	SLU 38	0	357	2562	-15.17	0.59	-0.01
30	SLU 39	0	388	2710	-16.44	0.63	-0.01
30	SLU 40	0	388	2710	-16.44	0.63	-0.01
30	SLU 41	0	388	2710	-16.44	0.63	-0.01
30	SLU 42	0	388	2710	-16.44	0.63	-0.01
30	SLU 43	0	318	2549	-13.51	0.58	-0.01
30	SLU 44	0	318	2549	-13.51	0.58	-0.01
30	SLU 45	0	318	2549	-13.51	0.58	-0.01
30	SLU 46	0	318	2549	-13.51	0.58	-0.01
30	SLU 47	0	318	2549	-13.51	0.58	-0.01
30	SLU 48	0	318	2549	-13.51	0.58	-0.01
30	SLU 49	0	318	2549	-13.51	0.58	-0.01
30	SLU 50	0	318	2549	-13.51	0.58	-0.01
30	SLU 51	0	318	2549	-13.51	0.58	-0.01
30	SLU 52	1	389	2895	-16.48	0.66	-0.01
30	SLU 53	1	389	2895	-16.48	0.66	-0.01
30	SLU 54	1	389	2895	-16.48	0.66	-0.01
30	SLU 55	1	389	2895	-16.48	0.66	-0.01
30	SLU 56	1	389	2895	-16.48	0.66	-0.01
30	SLU 57	1	389	2895	-16.48	0.66	-0.01
30	SLU 58	1	389	2895	-16.48	0.66	-0.01
30	SLU 59	1	389	2895	-16.48	0.66	-0.01
30	SLU 60	1	419	3043	-17.76	0.69	-0.01
30	SLU 61	1	419	3043	-17.76	0.69	-0.01
30	SLU 62	1	419	3043	-17.76	0.69	-0.01
30	SLU 63	1	419	3043	-17.76	0.69	-0.01
30	SLU 64	0	351	2751	-14.94	0.64	-0.01
30	SLU 65	0	351	2751	-14.94	0.64	-0.01
30	SLU 66	0	351	2751	-14.94	0.64	-0.01
30	SLU 67	0	351	2751	-14.94	0.64	-0.01
30	SLU 68	0	351	2751	-14.94	0.64	-0.01
30	SLU 69	0	351	2751	-14.94	0.64	-0.01
30	SLU 70	0	351	2751	-14.94	0.64	-0.01
30	SLU 71	0	351	2751	-14.94	0.64	-0.01
30	SLU 72	0	351	2751	-14.94	0.64	-0.01
30	SLU 73	1	422	3097	-17.91	0.71	-0.01
30	SLU 74	1	422	3097	-17.91	0.71	-0.01
30	SLU 75	1	422	3097	-17.91	0.71	-0.01
30	SLU 76	1	422	3097	-17.91	0.71	-0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
30	SLU 77	1	422	3097	-17.91	0.71	-0.01
30	SLU 78	1	422	3097	-17.91	0.71	-0.01
30	SLU 79	1	422	3097	-17.91	0.71	-0.01
30	SLU 80	1	422	3097	-17.91	0.71	-0.01
30	SLU 81	1	452	3245	-19.18	0.75	-0.01
30	SLU 82	1	452	3245	-19.18	0.75	-0.01
30	SLU 83	1	452	3245	-19.18	0.75	-0.01
30	SLU 84	1	452	3245	-19.18	0.75	-0.01
30	SLE RA 1	0	263	2072	-11.18	0.48	-0.01
30	SLE RA 2	0	263	2072	-11.18	0.48	-0.01
30	SLE RA 3	0	263	2072	-11.18	0.48	-0.01
30	SLE RA 4	0	263	2072	-11.18	0.48	-0.01
30	SLE RA 5	0	263	2072	-11.18	0.48	-0.01
30	SLE RA 6	0	263	2072	-11.18	0.48	-0.01
30	SLE RA 7	0	263	2072	-11.18	0.48	-0.01
30	SLE RA 8	0	263	2072	-11.18	0.48	-0.01
30	SLE RA 9	0	263	2072	-11.18	0.48	-0.01
30	SLE RA 10	0	310	2302	-13.16	0.53	-0.01
30	SLE RA 11	0	310	2302	-13.16	0.53	-0.01
30	SLE RA 12	0	310	2302	-13.16	0.53	-0.01
30	SLE RA 13	0	310	2302	-13.16	0.53	-0.01
30	SLE RA 14	0	310	2302	-13.16	0.53	-0.01
30	SLE RA 15	0	310	2302	-13.16	0.53	-0.01
30	SLE RA 16	0	310	2302	-13.16	0.53	-0.01
30	SLE RA 17	0	310	2302	-13.16	0.53	-0.01
30	SLE RA 18	0	330	2401	-14.01	0.55	-0.01
30	SLE RA 19	0	330	2401	-14.01	0.55	-0.01
30	SLE RA 20	0	330	2401	-14.01	0.55	-0.01
30	SLE RA 21	0	330	2401	-14.01	0.55	-0.01
30	SLE FR 1	0	263	2072	-11.18	0.48	-0.01
30	SLE FR 2	0	263	2072	-11.18	0.48	-0.01
30	SLE FR 3	0	263	2072	-11.18	0.48	-0.01
30	SLE FR 4	0	283	2171	-12.03	0.5	-0.01
30	SLE FR 5	0	283	2171	-12.03	0.5	-0.01
30	SLE FR 6	0	297	2236	-12.59	0.52	-0.01
30	SLE QP 1	0	263	2072	-11.18	0.48	-0.01
30	SLE QP 2	0	283	2171	-12.03	0.5	-0.01
30	SLD 1	9	253	2431	-10.94	10.57	-0.02
30	SLD 2	9	253	2431	-10.94	10.57	-0.02
30	SLD 3	19	101	2296	-4.39	16.83	-0.02
30	SLD 4	19	101	2296	-4.39	16.83	-0.02
30	SLD 5	-13	505	2453	-21.63	-5.97	-0.02
30	SLD 6	-13	505	2453	-21.63	-5.97	-0.02
30	SLD 7	22	-3	2004	0.19	14.89	0
30	SLD 8	22	-3	2004	0.19	14.89	0
30	SLD 9	-21	569	2337	-24.24	-13.89	-0.01
30	SLD 10	-21	569	2337	-24.24	-13.89	-0.01
30	SLD 11	14	61	1888	-2.43	6.97	0.01
30	SLD 12	14	61	1888	-2.43	6.97	0.01
30	SLD 13	-18	465	2045	-19.66	-15.83	0.01
30	SLD 14	-18	465	2045	-19.66	-15.83	0.01
30	SLD 15	-8	313	1910	-13.11	-9.57	0.01
30	SLD 16	-8	313	1910	-13.11	-9.57	0.01
30	SLV 1	21	207	2790	-9.2	25.12	-0.05
30	SLV 2	21	207	2790	-9.2	25.12	-0.05
30	SLV 3	47	-151	2472	6.17	41.07	-0.04
30	SLV 4	47	-151	2472	6.17	41.07	-0.04
30	SLV 5	-34	803	2838	-34.5	-16.29	-0.04
30	SLV 6	-34	803	2838	-34.5	-16.29	-0.04
30	SLV 7	55	-390	1779	16.75	36.85	0.01
30	SLV 8	55	-390	1779	16.75	36.85	0.01
30	SLV 9	-54	956	2562	-40.8	-35.85	-0.02
30	SLV 10	-54	956	2562	-40.8	-35.85	-0.02
30	SLV 11	34	-237	1503	10.45	17.3	0.03
30	SLV 12	34	-237	1503	10.45	17.3	0.03
30	SLV 13	-46	717	1869	-30.22	-40.07	0.03
30	SLV 14	-46	717	1869	-30.22	-40.07	0.03
30	SLV 15	-20	359	1551	-14.85	-24.12	0.04
30	SLV 16	-20	359	1551	-14.85	-24.12	0.04
31	SLU 1	0	0	1045	0.08	0	0
31	SLU 2	0	0	1045	0.08	0	0
31	SLU 3	0	0	1045	0.08	0	0
31	SLU 4	0	0	1045	0.08	0	0
31	SLU 5	0	0	1045	0.08	0	0
31	SLU 6	0	0	1045	0.08	0	0
31	SLU 7	0	0	1045	0.08	0	0
31	SLU 8	0	0	1045	0.08	0	0
31	SLU 9	0	0	1045	0.08	0	0
31	SLU 10	0	0	1374	0.11	0	0
31	SLU 11	0	0	1374	0.11	0	0
31	SLU 12	0	0	1374	0.11	0	0
31	SLU 13	0	0	1374	0.11	0	0
31	SLU 14	0	0	1374	0.11	0	0
31	SLU 15	0	0	1374	0.11	0	0
31	SLU 16	0	0	1374	0.11	0	0
31	SLU 17	0	0	1374	0.11	0	0
31	SLU 18	0	0	1515	0.12	0	0
31	SLU 19	0	0	1515	0.12	0	0
31	SLU 20	0	0	1515	0.12	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
31	SLU 21	0	0	1515	0.12	0	0
31	SLU 22	0	0	1219	0.1	0	0
31	SLU 23	0	0	1219	0.1	0	0
31	SLU 24	0	0	1219	0.1	0	0
31	SLU 25	0	0	1219	0.1	0	0
31	SLU 26	0	0	1219	0.1	0	0
31	SLU 27	0	0	1219	0.1	0	0
31	SLU 28	0	0	1219	0.1	0	0
31	SLU 29	0	0	1219	0.1	0	0
31	SLU 30	0	0	1219	0.1	0	0
31	SLU 31	0	0	1548	0.13	0	0
31	SLU 32	0	0	1548	0.13	0	0
31	SLU 33	0	0	1548	0.13	0	0
31	SLU 34	0	0	1548	0.13	0	0
31	SLU 35	0	0	1548	0.13	0	0
31	SLU 36	0	0	1548	0.13	0	0
31	SLU 37	0	0	1548	0.13	0	0
31	SLU 38	0	0	1548	0.13	0	0
31	SLU 39	0	0	1689	0.14	0	0
31	SLU 40	0	0	1689	0.14	0	0
31	SLU 41	0	0	1689	0.14	0	0
31	SLU 42	0	0	1689	0.14	0	0
31	SLU 43	0	0	1300	0.1	0	0
31	SLU 44	0	0	1300	0.1	0	0
31	SLU 45	0	0	1300	0.1	0	0
31	SLU 46	0	0	1300	0.1	0	0
31	SLU 47	0	0	1300	0.1	0	0
31	SLU 48	0	0	1300	0.1	0	0
31	SLU 49	0	0	1300	0.1	0	0
31	SLU 50	0	0	1300	0.1	0	0
31	SLU 51	0	0	1300	0.1	0	0
31	SLU 52	0	0	1628	0.13	0	0
31	SLU 53	0	0	1628	0.13	0	0
31	SLU 54	0	0	1628	0.13	0	0
31	SLU 55	0	0	1628	0.13	0	0
31	SLU 56	0	0	1628	0.13	0	0
31	SLU 57	0	0	1628	0.13	0	0
31	SLU 58	0	0	1628	0.13	0	0
31	SLU 59	0	0	1628	0.13	0	0
31	SLU 60	0	0	1769	0.14	0	0
31	SLU 61	0	0	1769	0.14	0	0
31	SLU 62	0	0	1769	0.14	0	0
31	SLU 63	0	0	1769	0.14	0	0
31	SLU 64	0	0	1473	0.11	0	0
31	SLU 65	0	0	1473	0.11	0	0
31	SLU 66	0	0	1473	0.11	0	0
31	SLU 67	0	0	1473	0.11	0	0
31	SLU 68	0	0	1473	0.11	0	0
31	SLU 69	0	0	1473	0.11	0	0
31	SLU 70	0	0	1473	0.11	0	0
31	SLU 71	0	0	1473	0.11	0	0
31	SLU 72	0	0	1473	0.11	0	0
31	SLU 73	0	0	1802	0.15	0	0
31	SLU 74	0	0	1802	0.15	0	0
31	SLU 75	0	0	1802	0.15	0	0
31	SLU 76	0	0	1802	0.15	0	0
31	SLU 77	0	0	1802	0.15	0	0
31	SLU 78	0	0	1802	0.15	0	0
31	SLU 79	0	0	1802	0.15	0	0
31	SLU 80	0	0	1802	0.15	0	0
31	SLU 81	0	0	1943	0.16	0	0
31	SLU 82	0	0	1943	0.16	0	0
31	SLU 83	0	0	1943	0.16	0	0
31	SLU 84	0	0	1943	0.16	0	0
31	SLE RA 1	0	0	1095	0.08	0	0
31	SLE RA 2	0	0	1095	0.08	0	0
31	SLE RA 3	0	0	1095	0.08	0	0
31	SLE RA 4	0	0	1095	0.08	0	0
31	SLE RA 5	0	0	1095	0.08	0	0
31	SLE RA 6	0	0	1095	0.08	0	0
31	SLE RA 7	0	0	1095	0.08	0	0
31	SLE RA 8	0	0	1095	0.08	0	0
31	SLE RA 9	0	0	1095	0.08	0	0
31	SLE RA 10	0	0	1314	0.11	0	0
31	SLE RA 11	0	0	1314	0.11	0	0
31	SLE RA 12	0	0	1314	0.11	0	0
31	SLE RA 13	0	0	1314	0.11	0	0
31	SLE RA 14	0	0	1314	0.11	0	0
31	SLE RA 15	0	0	1314	0.11	0	0
31	SLE RA 16	0	0	1314	0.11	0	0
31	SLE RA 17	0	0	1314	0.11	0	0
31	SLE RA 18	0	0	1408	0.12	0	0
31	SLE RA 19	0	0	1408	0.12	0	0
31	SLE RA 20	0	0	1408	0.12	0	0
31	SLE RA 21	0	0	1408	0.12	0	0
31	SLE FR 1	0	0	1095	0.08	0	0
31	SLE FR 2	0	0	1095	0.08	0	0
31	SLE FR 3	0	0	1095	0.08	0	0
31	SLE FR 4	0	0	1189	0.09	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
31	SLE FR 5	0	0	1189	0.09	0	0
31	SLE FR 6	0	0	1252	0.1	0	0
31	SLE QP 1	0	0	1095	0.08	0	0
31	SLE QP 2	0	0	1189	0.09	0	0
31	SLD 1	-2	-14	1147	-24.44	3.63	0.11
31	SLD 2	-2	-14	1147	-24.44	3.63	0.11
31	SLD 3	-3	26	1267	46.42	2.91	0.09
31	SLD 4	-3	26	1267	46.42	2.91	0.09
31	SLD 5	0	-65	994	-114.74	2.18	0.07
31	SLD 6	0	-65	994	-114.74	2.18	0.07
31	SLD 7	-2	69	1395	121.47	-0.22	-0.01
31	SLD 8	-2	69	1395	121.47	-0.22	-0.01
31	SLD 9	2	-69	983	-121.28	0.22	0.01
31	SLD 10	2	-69	983	-121.28	0.22	0.01
31	SLD 11	0	65	1384	114.93	-2.18	-0.07
31	SLD 12	0	65	1384	114.93	-2.18	-0.07
31	SLD 13	3	-26	1111	-46.23	-2.91	-0.09
31	SLD 14	3	-26	1111	-46.23	-2.91	-0.09
31	SLD 15	2	14	1231	24.63	-3.63	-0.11
31	SLD 16	2	14	1231	24.63	-3.63	-0.11
31	SLV 1	-5	-36	1081	-62.85	9.25	0.28
31	SLV 2	-5	-36	1081	-62.85	9.25	0.28
31	SLV 3	-7	68	1389	118.95	7.42	0.22
31	SLV 4	-7	68	1389	118.95	7.42	0.22
31	SLV 5	0	-167	689	-294.52	5.56	0.17
31	SLV 6	0	-167	689	-294.52	5.56	0.17
31	SLV 7	-4	177	1717	311.48	-0.56	-0.02
31	SLV 8	-4	177	1717	311.48	-0.56	-0.02
31	SLV 9	4	-177	661	-311.29	0.56	0.02
31	SLV 10	4	-177	661	-311.29	0.56	0.02
31	SLV 11	0	167	1690	294.71	-5.56	-0.17
31	SLV 12	0	167	1690	294.71	-5.56	-0.17
31	SLV 13	7	-67	989	-118.76	-7.42	-0.22
31	SLV 14	7	-67	989	-118.76	-7.42	-0.22
31	SLV 15	5	36	1297	63.04	-9.26	-0.28
31	SLV 16	5	36	1297	63.04	-9.26	-0.28
32	SLU 1	0	224	2036	-9.84	-0.48	0
32	SLU 2	0	224	2036	-9.84	-0.48	0
32	SLU 3	0	224	2036	-9.84	-0.48	0
32	SLU 4	0	224	2036	-9.84	-0.48	0
32	SLU 5	0	224	2036	-9.84	-0.48	0
32	SLU 6	0	224	2036	-9.84	-0.48	0
32	SLU 7	0	224	2036	-9.84	-0.48	0
32	SLU 8	0	224	2036	-9.84	-0.48	0
32	SLU 9	0	224	2036	-9.84	-0.48	0
32	SLU 10	0	293	2413	-12.87	-0.58	0
32	SLU 11	0	293	2413	-12.87	-0.58	0
32	SLU 12	0	293	2413	-12.87	-0.58	0
32	SLU 13	0	293	2413	-12.87	-0.58	0
32	SLU 14	0	293	2413	-12.87	-0.58	0
32	SLU 15	0	293	2413	-12.87	-0.58	0
32	SLU 16	0	293	2413	-12.87	-0.58	0
32	SLU 17	0	293	2413	-12.87	-0.58	0
32	SLU 18	0	322	2574	-14.17	-0.62	0
32	SLU 19	0	322	2574	-14.17	-0.62	0
32	SLU 20	0	322	2574	-14.17	-0.62	0
32	SLU 21	0	322	2574	-14.17	-0.62	0
32	SLU 22	0	253	2237	-11.14	-0.54	0
32	SLU 23	0	253	2237	-11.14	-0.54	0
32	SLU 24	0	253	2237	-11.14	-0.54	0
32	SLU 25	0	253	2237	-11.14	-0.54	0
32	SLU 26	0	253	2237	-11.14	-0.54	0
32	SLU 27	0	253	2237	-11.14	-0.54	0
32	SLU 28	0	253	2237	-11.14	-0.54	0
32	SLU 29	0	253	2237	-11.14	-0.54	0
32	SLU 30	0	253	2237	-11.14	-0.54	0
32	SLU 31	0	321	2614	-14.17	-0.64	0
32	SLU 32	0	321	2614	-14.17	-0.64	0
32	SLU 33	0	321	2614	-14.17	-0.64	0
32	SLU 34	0	321	2614	-14.17	-0.64	0
32	SLU 35	0	321	2614	-14.17	-0.64	0
32	SLU 36	0	321	2614	-14.17	-0.64	0
32	SLU 37	0	321	2614	-14.17	-0.64	0
32	SLU 38	0	321	2614	-14.17	-0.64	0
32	SLU 39	-1	351	2775	-15.47	-0.68	0
32	SLU 40	-1	351	2775	-15.47	-0.68	0
32	SLU 41	-1	351	2775	-15.47	-0.68	0
32	SLU 42	-1	351	2775	-15.47	-0.68	0
32	SLU 43	0	281	2579	-12.34	-0.6	0
32	SLU 44	0	281	2579	-12.34	-0.6	0
32	SLU 45	0	281	2579	-12.34	-0.6	0
32	SLU 46	0	281	2579	-12.34	-0.6	0
32	SLU 47	0	281	2579	-12.34	-0.6	0
32	SLU 48	0	281	2579	-12.34	-0.6	0
32	SLU 49	0	281	2579	-12.34	-0.6	0
32	SLU 50	0	281	2579	-12.34	-0.6	0
32	SLU 51	0	281	2579	-12.34	-0.6	0
32	SLU 52	-1	350	2955	-15.37	-0.7	0
32	SLU 53	-1	350	2955	-15.37	-0.7	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
32	SLU 54	-1	350	2955	-15.37	-0.7	0
32	SLU 55	-1	350	2955	-15.37	-0.7	0
32	SLU 56	-1	350	2955	-15.37	-0.7	0
32	SLU 57	-1	350	2955	-15.37	-0.7	0
32	SLU 58	-1	350	2955	-15.37	-0.7	0
32	SLU 59	-1	350	2955	-15.37	-0.7	0
32	SLU 60	-1	379	3117	-16.67	-0.74	0
32	SLU 61	-1	379	3117	-16.67	-0.74	0
32	SLU 62	-1	379	3117	-16.67	-0.74	0
32	SLU 63	-1	379	3117	-16.67	-0.74	0
32	SLU 64	-1	310	2779	-13.65	-0.66	0
32	SLU 65	-1	310	2779	-13.65	-0.66	0
32	SLU 66	-1	310	2779	-13.65	-0.66	0
32	SLU 67	-1	310	2779	-13.65	-0.66	0
32	SLU 68	-1	310	2779	-13.65	-0.66	0
32	SLU 69	-1	310	2779	-13.65	-0.66	0
32	SLU 70	-1	310	2779	-13.65	-0.66	0
32	SLU 71	-1	310	2779	-13.65	-0.66	0
32	SLU 72	-1	310	2779	-13.65	-0.66	0
32	SLU 73	-1	379	3156	-16.68	-0.76	0.01
32	SLU 74	-1	379	3156	-16.68	-0.76	0.01
32	SLU 75	-1	379	3156	-16.68	-0.76	0.01
32	SLU 76	-1	379	3156	-16.68	-0.76	0.01
32	SLU 77	-1	379	3156	-16.68	-0.76	0.01
32	SLU 78	-1	379	3156	-16.68	-0.76	0.01
32	SLU 79	-1	379	3156	-16.68	-0.76	0.01
32	SLU 80	-1	379	3156	-16.68	-0.76	0.01
32	SLU 81	-1	408	3317	-17.97	-0.8	0.01
32	SLU 82	-1	408	3317	-17.97	-0.8	0.01
32	SLU 83	-1	408	3317	-17.97	-0.8	0.01
32	SLU 84	-1	408	3317	-17.97	-0.8	0.01
32	SLE RA 1	0	232	2094	-10.21	-0.5	0
32	SLE RA 2	0	232	2094	-10.21	-0.5	0
32	SLE RA 3	0	232	2094	-10.21	-0.5	0
32	SLE RA 4	0	232	2094	-10.21	-0.5	0
32	SLE RA 5	0	232	2094	-10.21	-0.5	0
32	SLE RA 6	0	232	2094	-10.21	-0.5	0
32	SLE RA 7	0	232	2094	-10.21	-0.5	0
32	SLE RA 8	0	232	2094	-10.21	-0.5	0
32	SLE RA 9	0	232	2094	-10.21	-0.5	0
32	SLE RA 10	0	278	2345	-12.23	-0.56	0
32	SLE RA 11	0	278	2345	-12.23	-0.56	0
32	SLE RA 12	0	278	2345	-12.23	-0.56	0
32	SLE RA 13	0	278	2345	-12.23	-0.56	0
32	SLE RA 14	0	278	2345	-12.23	-0.56	0
32	SLE RA 15	0	278	2345	-12.23	-0.56	0
32	SLE RA 16	0	278	2345	-12.23	-0.56	0
32	SLE RA 17	0	278	2345	-12.23	-0.56	0
32	SLE RA 18	0	298	2452	-13.1	-0.59	0
32	SLE RA 19	0	298	2452	-13.1	-0.59	0
32	SLE RA 20	0	298	2452	-13.1	-0.59	0
32	SLE RA 21	0	298	2452	-13.1	-0.59	0
32	SLE FR 1	0	232	2094	-10.21	-0.5	0
32	SLE FR 2	0	232	2094	-10.21	-0.5	0
32	SLE FR 3	0	232	2094	-10.21	-0.5	0
32	SLE FR 4	0	252	2201	-11.08	-0.52	0
32	SLE FR 5	0	252	2201	-11.08	-0.52	0
32	SLE FR 6	0	265	2273	-11.65	-0.54	0
32	SLE QP 1	0	232	2094	-10.21	-0.5	0
32	SLE QP 2	0	252	2201	-11.08	-0.52	0
32	SLD 1	18	390	2058	-10.94	17.17	0.05
32	SLD 2	18	390	2058	-10.94	17.17	0.05
32	SLD 3	8	258	1971	-5.24	11.34	0.02
32	SLD 4	8	258	1971	-5.24	11.34	0.02
32	SLD 5	21	495	2291	-19.68	13.62	0.07
32	SLD 6	21	495	2291	-19.68	13.62	0.07
32	SLD 7	-14	52	2000	-0.68	-5.8	-0.04
32	SLD 8	-14	52	2000	-0.68	-5.8	-0.04
32	SLD 9	13	452	2403	-21.47	4.76	0.05
32	SLD 10	13	452	2403	-21.47	4.76	0.05
32	SLD 11	-22	9	2112	-2.47	-14.67	-0.06
32	SLD 12	-22	9	2112	-2.47	-14.67	-0.06
32	SLD 13	-9	246	2432	-16.91	-12.39	-0.02
32	SLD 14	-9	246	2432	-16.91	-12.39	-0.02
32	SLD 15	-19	113	2344	-11.21	-18.22	-0.05
32	SLD 16	-19	113	2344	-11.21	-18.22	-0.05
32	SLV 1	46	577	1864	-10.75	43.72	0.13
32	SLV 2	46	577	1864	-10.75	43.72	0.13
32	SLV 3	20	266	1657	2.63	28.92	0.05
32	SLV 4	20	266	1657	2.63	28.92	0.05
32	SLV 5	53	822	2414	-31.28	35.2	0.16
32	SLV 6	53	822	2414	-31.28	35.2	0.16
32	SLV 7	-34	-217	1725	13.34	-14.14	-0.1
32	SLV 8	-34	-217	1725	13.34	-14.14	-0.1
32	SLV 9	33	721	2678	-35.49	13.09	0.11
32	SLV 10	33	721	2678	-35.49	13.09	0.11
32	SLV 11	-54	-319	1989	9.13	-36.25	-0.15
32	SLV 12	-54	-319	1989	9.13	-36.25	-0.15
32	SLV 13	-21	238	2745	-24.79	-29.97	-0.04



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
32	SLV 14	-21	238	2745	-24.79	-29.97	-0.04
32	SLV 15	-47	-74	2539	-11.4	-44.77	-0.12
32	SLV 16	-47	-74	2539	-11.4	-44.77	-0.12
33	SLU 1	0	207	1967	-8.75	0.24	0
33	SLU 2	0	207	1967	-8.75	0.24	0
33	SLU 3	0	207	1967	-8.75	0.24	0
33	SLU 4	0	207	1967	-8.75	0.24	0
33	SLU 5	0	207	1967	-8.75	0.24	0
33	SLU 6	0	207	1967	-8.75	0.24	0
33	SLU 7	0	207	1967	-8.75	0.24	0
33	SLU 8	0	207	1967	-8.75	0.24	0
33	SLU 9	0	207	1967	-8.75	0.24	0
33	SLU 10	0	271	2307	-11.4	0.27	0
33	SLU 11	0	271	2307	-11.4	0.27	0
33	SLU 12	0	271	2307	-11.4	0.27	0
33	SLU 13	0	271	2307	-11.4	0.27	0
33	SLU 14	0	271	2307	-11.4	0.27	0
33	SLU 15	0	271	2307	-11.4	0.27	0
33	SLU 16	0	271	2307	-11.4	0.27	0
33	SLU 17	0	271	2307	-11.4	0.27	0
33	SLU 18	0	298	2453	-12.53	0.29	0
33	SLU 19	0	298	2453	-12.53	0.29	0
33	SLU 20	0	298	2453	-12.53	0.29	0
33	SLU 21	0	298	2453	-12.53	0.29	0
33	SLU 22	0	237	2163	-10.01	0.27	0
33	SLU 23	0	237	2163	-10.01	0.27	0
33	SLU 24	0	237	2163	-10.01	0.27	0
33	SLU 25	0	237	2163	-10.01	0.27	0
33	SLU 26	0	237	2163	-10.01	0.27	0
33	SLU 27	0	237	2163	-10.01	0.27	0
33	SLU 28	0	237	2163	-10.01	0.27	0
33	SLU 29	0	237	2163	-10.01	0.27	0
33	SLU 30	0	237	2163	-10.01	0.27	0
33	SLU 31	0	301	2503	-12.66	0.3	0
33	SLU 32	0	301	2503	-12.66	0.3	0
33	SLU 33	0	301	2503	-12.66	0.3	0
33	SLU 34	0	301	2503	-12.66	0.3	0
33	SLU 35	0	301	2503	-12.66	0.3	0
33	SLU 36	0	301	2503	-12.66	0.3	0
33	SLU 37	0	301	2503	-12.66	0.3	0
33	SLU 38	0	301	2503	-12.66	0.3	0
33	SLU 39	0	328	2649	-13.79	0.31	0
33	SLU 40	0	328	2649	-13.79	0.31	0
33	SLU 41	0	328	2649	-13.79	0.31	0
33	SLU 42	0	328	2649	-13.79	0.31	0
33	SLU 43	0	259	2490	-10.94	0.3	0
33	SLU 44	0	259	2490	-10.94	0.3	0
33	SLU 45	0	259	2490	-10.94	0.3	0
33	SLU 46	0	259	2490	-10.94	0.3	0
33	SLU 47	0	259	2490	-10.94	0.3	0
33	SLU 48	0	259	2490	-10.94	0.3	0
33	SLU 49	0	259	2490	-10.94	0.3	0
33	SLU 50	0	259	2490	-10.94	0.3	0
33	SLU 51	0	259	2490	-10.94	0.3	0
33	SLU 52	0	323	2831	-13.59	0.34	0
33	SLU 53	0	323	2831	-13.59	0.34	0
33	SLU 54	0	323	2831	-13.59	0.34	0
33	SLU 55	0	323	2831	-13.59	0.34	0
33	SLU 56	0	323	2831	-13.59	0.34	0
33	SLU 57	0	323	2831	-13.59	0.34	0
33	SLU 58	0	323	2831	-13.59	0.34	0
33	SLU 59	0	323	2831	-13.59	0.34	0
33	SLU 60	0	350	2976	-14.72	0.35	0
33	SLU 61	0	350	2976	-14.72	0.35	0
33	SLU 62	0	350	2976	-14.72	0.35	0
33	SLU 63	0	350	2976	-14.72	0.35	0
33	SLU 64	0	289	2686	-12.2	0.33	0
33	SLU 65	0	289	2686	-12.2	0.33	0
33	SLU 66	0	289	2686	-12.2	0.33	0
33	SLU 67	0	289	2686	-12.2	0.33	0
33	SLU 68	0	289	2686	-12.2	0.33	0
33	SLU 69	0	289	2686	-12.2	0.33	0
33	SLU 70	0	289	2686	-12.2	0.33	0
33	SLU 71	0	289	2686	-12.2	0.33	0
33	SLU 72	0	289	2686	-12.2	0.33	0
33	SLU 73	0	353	3026	-14.85	0.36	0
33	SLU 74	0	353	3026	-14.85	0.36	0
33	SLU 75	0	353	3026	-14.85	0.36	0
33	SLU 76	0	353	3026	-14.85	0.36	0
33	SLU 77	0	353	3026	-14.85	0.36	0
33	SLU 78	0	353	3026	-14.85	0.36	0
33	SLU 79	0	353	3026	-14.85	0.36	0
33	SLU 80	0	353	3026	-14.85	0.36	0
33	SLU 81	0	380	3172	-15.98	0.38	0
33	SLU 82	0	380	3172	-15.98	0.38	0
33	SLU 83	0	380	3172	-15.98	0.38	0
33	SLU 84	0	380	3172	-15.98	0.38	0
33	SLE RA 1	0	216	2023	-9.11	0.25	0
33	SLE RA 2	0	216	2023	-9.11	0.25	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
33	SLE RA 3	0	216	2023	-9.11	0.25	0
33	SLE RA 4	0	216	2023	-9.11	0.25	0
33	SLE RA 5	0	216	2023	-9.11	0.25	0
33	SLE RA 6	0	216	2023	-9.11	0.25	0
33	SLE RA 7	0	216	2023	-9.11	0.25	0
33	SLE RA 8	0	216	2023	-9.11	0.25	0
33	SLE RA 9	0	216	2023	-9.11	0.25	0
33	SLE RA 10	0	258	2250	-10.87	0.27	0
33	SLE RA 11	0	258	2250	-10.87	0.27	0
33	SLE RA 12	0	258	2250	-10.87	0.27	0
33	SLE RA 13	0	258	2250	-10.87	0.27	0
33	SLE RA 14	0	258	2250	-10.87	0.27	0
33	SLE RA 15	0	258	2250	-10.87	0.27	0
33	SLE RA 16	0	258	2250	-10.87	0.27	0
33	SLE RA 17	0	258	2250	-10.87	0.27	0
33	SLE RA 18	0	276	2347	-11.63	0.28	0
33	SLE RA 19	0	276	2347	-11.63	0.28	0
33	SLE RA 20	0	276	2347	-11.63	0.28	0
33	SLE RA 21	0	276	2347	-11.63	0.28	0
33	SLE FR 1	0	216	2023	-9.11	0.25	0
33	SLE FR 2	0	216	2023	-9.11	0.25	0
33	SLE FR 3	0	216	2023	-9.11	0.25	0
33	SLE FR 4	0	234	2120	-9.86	0.26	0
33	SLE FR 5	0	234	2120	-9.86	0.26	0
33	SLE FR 6	0	246	2185	-10.37	0.26	0
33	SLE QP 1	0	216	2023	-9.11	0.25	0
33	SLE QP 2	0	234	2120	-9.86	0.26	0
33	SLD 1	16	211	2312	-8.91	16.35	-0.02
33	SLD 2	16	211	2312	-8.91	16.35	-0.02
33	SLD 3	26	53	2213	-2.24	23.72	-0.01
33	SLD 4	26	53	2213	-2.24	23.72	-0.01
33	SLD 5	-10	466	2329	-19.7	-6.08	-0.01
33	SLD 6	-10	466	2329	-19.7	-6.08	-0.01
33	SLD 7	23	-59	1997	2.54	18.46	0
33	SLD 8	23	-59	1997	2.54	18.46	0
33	SLD 9	-23	527	2244	-22.27	-17.95	-0.01
33	SLD 10	-23	527	2244	-22.27	-17.95	-0.01
33	SLD 11	10	2	1912	-0.03	6.6	0.01
33	SLD 12	10	2	1912	-0.03	6.6	0.01
33	SLD 13	-26	414	2028	-17.49	-23.2	0.01
33	SLD 14	-26	414	2028	-17.49	-23.2	0.01
33	SLD 15	-16	257	1928	-10.82	-15.84	0.02
33	SLD 16	-16	257	1928	-10.82	-15.84	0.02
33	SLV 1	39	174	2577	-7.35	39.48	-0.04
33	SLV 2	39	174	2577	-7.35	39.48	-0.04
33	SLV 3	64	-196	2342	8.31	58.27	-0.03
33	SLV 4	64	-196	2342	8.31	58.27	-0.03
33	SLV 5	-27	777	2614	-32.86	-16.47	-0.03
33	SLV 6	-27	777	2614	-32.86	-16.47	-0.03
33	SLV 7	58	-456	1830	19.34	46.16	0.01
33	SLV 8	58	-456	1830	19.34	46.16	0.01
33	SLV 9	-58	924	2411	-39.07	-45.64	-0.01
33	SLV 10	-58	924	2411	-39.07	-45.64	-0.01
33	SLV 11	27	-309	1627	13.13	16.99	0.03
33	SLV 12	27	-309	1627	13.13	16.99	0.03
33	SLV 13	-64	664	1899	-28.04	-57.76	0.03
33	SLV 14	-64	664	1899	-28.04	-57.76	0.03
33	SLV 15	-39	294	1664	-12.38	-38.97	0.04
33	SLV 16	-39	294	1664	-12.38	-38.97	0.04
34	SLU 1	0	0	1106	0.06	0	0
34	SLU 2	0	0	1106	0.06	0	0
34	SLU 3	0	0	1106	0.06	0	0
34	SLU 4	0	0	1106	0.06	0	0
34	SLU 5	0	0	1106	0.06	0	0
34	SLU 6	0	0	1106	0.06	0	0
34	SLU 7	0	0	1106	0.06	0	0
34	SLU 8	0	0	1106	0.06	0	0
34	SLU 9	0	0	1106	0.06	0	0
34	SLU 10	0	0	1505	0.1	0	0
34	SLU 11	0	0	1505	0.1	0	0
34	SLU 12	0	0	1505	0.1	0	0
34	SLU 13	0	0	1505	0.1	0	0
34	SLU 14	0	0	1505	0.1	0	0
34	SLU 15	0	0	1505	0.1	0	0
34	SLU 16	0	0	1505	0.1	0	0
34	SLU 17	0	0	1505	0.1	0	0
34	SLU 18	0	0	1676	0.12	0	0
34	SLU 19	0	0	1676	0.12	0	0
34	SLU 20	0	0	1676	0.12	0	0
34	SLU 21	0	0	1676	0.12	0	0
34	SLU 22	0	0	1309	0.08	0	0
34	SLU 23	0	0	1309	0.08	0	0
34	SLU 24	0	0	1309	0.08	0	0
34	SLU 25	0	0	1309	0.08	0	0
34	SLU 26	0	0	1309	0.08	0	0
34	SLU 27	0	0	1309	0.08	0	0
34	SLU 28	0	0	1309	0.08	0	0
34	SLU 29	0	0	1309	0.08	0	0
34	SLU 30	0	0	1309	0.08	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
34	SLU 31	0	0	1708	0.12	0	0
34	SLU 32	0	0	1708	0.12	0	0
34	SLU 33	0	0	1708	0.12	0	0
34	SLU 34	0	0	1708	0.12	0	0
34	SLU 35	0	0	1708	0.12	0	0
34	SLU 36	0	0	1708	0.12	0	0
34	SLU 37	0	0	1708	0.12	0	0
34	SLU 38	0	0	1708	0.12	0	0
34	SLU 39	0	0	1879	0.14	0	0
34	SLU 40	0	0	1879	0.14	0	0
34	SLU 41	0	0	1879	0.14	0	0
34	SLU 42	0	0	1879	0.14	0	0
34	SLU 43	0	0	1368	0.07	0	0
34	SLU 44	0	0	1368	0.07	0	0
34	SLU 45	0	0	1368	0.07	0	0
34	SLU 46	0	0	1368	0.07	0	0
34	SLU 47	0	0	1368	0.07	0	0
34	SLU 48	0	0	1368	0.07	0	0
34	SLU 49	0	0	1368	0.07	0	0
34	SLU 50	0	0	1368	0.07	0	0
34	SLU 51	0	0	1368	0.07	0	0
34	SLU 52	0	0	1767	0.11	0	0
34	SLU 53	0	0	1767	0.11	0	0
34	SLU 54	0	0	1767	0.11	0	0
34	SLU 55	0	0	1767	0.11	0	0
34	SLU 56	0	0	1767	0.11	0	0
34	SLU 57	0	0	1767	0.11	0	0
34	SLU 58	0	0	1767	0.11	0	0
34	SLU 59	0	0	1767	0.11	0	0
34	SLU 60	0	0	1938	0.13	0	0
34	SLU 61	0	0	1938	0.13	0	0
34	SLU 62	0	0	1938	0.13	0	0
34	SLU 63	0	0	1938	0.13	0	0
34	SLU 64	0	0	1571	0.09	0	0
34	SLU 65	0	0	1571	0.09	0	0
34	SLU 66	0	0	1571	0.09	0	0
34	SLU 67	0	0	1571	0.09	0	0
34	SLU 68	0	0	1571	0.09	0	0
34	SLU 69	0	0	1571	0.09	0	0
34	SLU 70	0	0	1571	0.09	0	0
34	SLU 71	0	0	1571	0.09	0	0
34	SLU 72	0	0	1571	0.09	0	0
34	SLU 73	0	0	1970	0.13	0	0
34	SLU 74	0	0	1970	0.13	0	0
34	SLU 75	0	0	1970	0.13	0	0
34	SLU 76	0	0	1970	0.13	0	0
34	SLU 77	0	0	1970	0.13	0	0
34	SLU 78	0	0	1970	0.13	0	0
34	SLU 79	0	0	1970	0.13	0	0
34	SLU 80	0	0	1970	0.13	0	0
34	SLU 81	0	0	2141	0.15	0	0
34	SLU 82	0	0	2141	0.15	0	0
34	SLU 83	0	0	2141	0.15	0	0
34	SLU 84	0	0	2141	0.15	0	0
34	SLE RA 1	0	0	1164	0.06	0	0
34	SLE RA 2	0	0	1164	0.06	0	0
34	SLE RA 3	0	0	1164	0.06	0	0
34	SLE RA 4	0	0	1164	0.06	0	0
34	SLE RA 5	0	0	1164	0.06	0	0
34	SLE RA 6	0	0	1164	0.06	0	0
34	SLE RA 7	0	0	1164	0.06	0	0
34	SLE RA 8	0	0	1164	0.06	0	0
34	SLE RA 9	0	0	1164	0.06	0	0
34	SLE RA 10	0	0	1430	0.09	0	0
34	SLE RA 11	0	0	1430	0.09	0	0
34	SLE RA 12	0	0	1430	0.09	0	0
34	SLE RA 13	0	0	1430	0.09	0	0
34	SLE RA 14	0	0	1430	0.09	0	0
34	SLE RA 15	0	0	1430	0.09	0	0
34	SLE RA 16	0	0	1430	0.09	0	0
34	SLE RA 17	0	0	1430	0.09	0	0
34	SLE RA 18	0	0	1544	0.1	0	0
34	SLE RA 19	0	0	1544	0.1	0	0
34	SLE RA 20	0	0	1544	0.1	0	0
34	SLE RA 21	0	0	1544	0.1	0	0
34	SLE FR 1	0	0	1164	0.06	0	0
34	SLE FR 2	0	0	1164	0.06	0	0
34	SLE FR 3	0	0	1164	0.06	0	0
34	SLE FR 4	0	0	1278	0.08	0	0
34	SLE FR 5	0	0	1278	0.08	0	0
34	SLE FR 6	0	0	1354	0.08	0	0
34	SLE QP 1	0	0	1164	0.06	0	0
34	SLE QP 2	0	0	1278	0.08	0	0
34	SLD 1	-5	0	1247	-15.73	5.11	-0.09
34	SLD 2	-5	0	1247	-15.73	5.11	-0.09
34	SLD 3	-4	0	1337	29.9	6.41	-0.07
34	SLD 4	-4	0	1337	29.9	6.41	-0.07
34	SLD 5	-3	0	1132	-73.87	-0.44	-0.06
34	SLD 6	-3	0	1132	-73.87	-0.44	-0.06



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
34	SLD 7	0	0	1433	78.23	3.9	0.01
34	SLD 8	0	0	1433	78.23	3.9	0.01
34	SLD 9	0	0	1123	-78.08	-3.9	-0.01
34	SLD 10	0	0	1123	-78.08	-3.9	-0.01
34	SLD 11	3	0	1424	74.02	0.44	0.06
34	SLD 12	3	0	1424	74.02	0.44	0.06
34	SLD 13	4	0	1219	-29.75	-6.41	0.07
34	SLD 14	4	0	1219	-29.75	-6.41	0.07
34	SLD 15	5	0	1309	15.88	-5.11	0.09
34	SLD 16	5	0	1309	15.88	-5.11	0.09
34	SLV 1	-12	0	1198	-40.47	13.04	-0.23
34	SLV 2	-12	0	1198	-40.47	13.04	-0.23
34	SLV 3	-10	0	1430	76.6	16.36	-0.18
34	SLV 4	-10	0	1430	76.6	16.36	-0.18
34	SLV 5	-7	-1	903	-189.64	-1.14	-0.15
34	SLV 6	-7	-1	903	-189.64	-1.14	-0.15
34	SLV 7	1	1	1675	200.59	9.96	0.03
34	SLV 8	1	1	1675	200.59	9.96	0.03
34	SLV 9	-1	-1	881	-200.43	-9.96	-0.03
34	SLV 10	-1	-1	881	-200.43	-9.96	-0.03
34	SLV 11	7	0	1653	189.79	1.14	0.15
34	SLV 12	7	0	1653	189.79	1.14	0.15
34	SLV 13	10	0	1126	-76.45	-16.36	0.18
34	SLV 14	10	0	1126	-76.45	-16.36	0.18
34	SLV 15	12	0	1358	40.62	-13.04	0.23
34	SLV 16	12	0	1358	40.62	-13.04	0.23
35	SLU 1	0	126	1907	-5.51	-0.25	0
35	SLU 2	0	126	1907	-5.51	-0.25	0
35	SLU 3	0	126	1907	-5.51	-0.25	0
35	SLU 4	0	126	1907	-5.51	-0.25	0
35	SLU 5	0	126	1907	-5.51	-0.25	0
35	SLU 6	0	126	1907	-5.51	-0.25	0
35	SLU 7	0	126	1907	-5.51	-0.25	0
35	SLU 8	0	126	1907	-5.51	-0.25	0
35	SLU 9	0	126	1907	-5.51	-0.25	0
35	SLU 10	0	175	2245	-7.59	-0.3	0
35	SLU 11	0	175	2245	-7.59	-0.3	0
35	SLU 12	0	175	2245	-7.59	-0.3	0
35	SLU 13	0	175	2245	-7.59	-0.3	0
35	SLU 14	0	175	2245	-7.59	-0.3	0
35	SLU 15	0	175	2245	-7.59	-0.3	0
35	SLU 16	0	175	2245	-7.59	-0.3	0
35	SLU 17	0	175	2245	-7.59	-0.3	0
35	SLU 18	0	196	2390	-8.49	-0.33	0
35	SLU 19	0	196	2390	-8.49	-0.33	0
35	SLU 20	0	196	2390	-8.49	-0.33	0
35	SLU 21	0	196	2390	-8.49	-0.33	0
35	SLU 22	0	146	2086	-6.37	-0.28	0
35	SLU 23	0	146	2086	-6.37	-0.28	0
35	SLU 24	0	146	2086	-6.37	-0.28	0
35	SLU 25	0	146	2086	-6.37	-0.28	0
35	SLU 26	0	146	2086	-6.37	-0.28	0
35	SLU 27	0	146	2086	-6.37	-0.28	0
35	SLU 28	0	146	2086	-6.37	-0.28	0
35	SLU 29	0	146	2086	-6.37	-0.28	0
35	SLU 30	0	146	2086	-6.37	-0.28	0
35	SLU 31	0	195	2424	-8.45	-0.33	0
35	SLU 32	0	195	2424	-8.45	-0.33	0
35	SLU 33	0	195	2424	-8.45	-0.33	0
35	SLU 34	0	195	2424	-8.45	-0.33	0
35	SLU 35	0	195	2424	-8.45	-0.33	0
35	SLU 36	0	195	2424	-8.45	-0.33	0
35	SLU 37	0	195	2424	-8.45	-0.33	0
35	SLU 38	0	195	2424	-8.45	-0.33	0
35	SLU 39	0	216	2569	-9.35	-0.36	0
35	SLU 40	0	216	2569	-9.35	-0.36	0
35	SLU 41	0	216	2569	-9.35	-0.36	0
35	SLU 42	0	216	2569	-9.35	-0.36	0
35	SLU 43	0	157	2417	-6.87	-0.32	0
35	SLU 44	0	157	2417	-6.87	-0.32	0
35	SLU 45	0	157	2417	-6.87	-0.32	0
35	SLU 46	0	157	2417	-6.87	-0.32	0
35	SLU 47	0	157	2417	-6.87	-0.32	0
35	SLU 48	0	157	2417	-6.87	-0.32	0
35	SLU 49	0	157	2417	-6.87	-0.32	0
35	SLU 50	0	157	2417	-6.87	-0.32	0
35	SLU 51	0	157	2417	-6.87	-0.32	0
35	SLU 52	0	206	2755	-8.95	-0.37	0
35	SLU 53	0	206	2755	-8.95	-0.37	0
35	SLU 54	0	206	2755	-8.95	-0.37	0
35	SLU 55	0	206	2755	-8.95	-0.37	0
35	SLU 56	0	206	2755	-8.95	-0.37	0
35	SLU 57	0	206	2755	-8.95	-0.37	0
35	SLU 58	0	206	2755	-8.95	-0.37	0
35	SLU 59	0	206	2755	-8.95	-0.37	0
35	SLU 60	0	227	2900	-9.84	-0.39	0
35	SLU 61	0	227	2900	-9.84	-0.39	0
35	SLU 62	0	227	2900	-9.84	-0.39	0
35	SLU 63	0	227	2900	-9.84	-0.39	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
35	SLU 64	0	177	2596	-7.73	-0.35	0
35	SLU 65	0	177	2596	-7.73	-0.35	0
35	SLU 66	0	177	2596	-7.73	-0.35	0
35	SLU 67	0	177	2596	-7.73	-0.35	0
35	SLU 68	0	177	2596	-7.73	-0.35	0
35	SLU 69	0	177	2596	-7.73	-0.35	0
35	SLU 70	0	177	2596	-7.73	-0.35	0
35	SLU 71	0	177	2596	-7.73	-0.35	0
35	SLU 72	0	177	2596	-7.73	-0.35	0
35	SLU 73	0	226	2935	-9.81	-0.4	0
35	SLU 74	0	226	2935	-9.81	-0.4	0
35	SLU 75	0	226	2935	-9.81	-0.4	0
35	SLU 76	0	226	2935	-9.81	-0.4	0
35	SLU 77	0	226	2935	-9.81	-0.4	0
35	SLU 78	0	226	2935	-9.81	-0.4	0
35	SLU 79	0	226	2935	-9.81	-0.4	0
35	SLU 80	0	226	2935	-9.81	-0.4	0
35	SLU 81	0	247	3080	-10.71	-0.42	0
35	SLU 82	0	247	3080	-10.71	-0.42	0
35	SLU 83	0	247	3080	-10.71	-0.42	0
35	SLU 84	0	247	3080	-10.71	-0.42	0
35	SLE RA 1	0	132	1958	-5.76	-0.26	0
35	SLE RA 2	0	132	1958	-5.76	-0.26	0
35	SLE RA 3	0	132	1958	-5.76	-0.26	0
35	SLE RA 4	0	132	1958	-5.76	-0.26	0
35	SLE RA 5	0	132	1958	-5.76	-0.26	0
35	SLE RA 6	0	132	1958	-5.76	-0.26	0
35	SLE RA 7	0	132	1958	-5.76	-0.26	0
35	SLE RA 8	0	132	1958	-5.76	-0.26	0
35	SLE RA 9	0	132	1958	-5.76	-0.26	0
35	SLE RA 10	0	164	2183	-7.14	-0.3	0
35	SLE RA 11	0	164	2183	-7.14	-0.3	0
35	SLE RA 12	0	164	2183	-7.14	-0.3	0
35	SLE RA 13	0	164	2183	-7.14	-0.3	0
35	SLE RA 14	0	164	2183	-7.14	-0.3	0
35	SLE RA 15	0	164	2183	-7.14	-0.3	0
35	SLE RA 16	0	164	2183	-7.14	-0.3	0
35	SLE RA 17	0	164	2183	-7.14	-0.3	0
35	SLE RA 18	0	178	2280	-7.74	-0.31	0
35	SLE RA 19	0	178	2280	-7.74	-0.31	0
35	SLE RA 20	0	178	2280	-7.74	-0.31	0
35	SLE RA 21	0	178	2280	-7.74	-0.31	0
35	SLE FR 1	0	132	1958	-5.76	-0.26	0
35	SLE FR 2	0	132	1958	-5.76	-0.26	0
35	SLE FR 3	0	132	1958	-5.76	-0.26	0
35	SLE FR 4	0	146	2054	-6.35	-0.28	0
35	SLE FR 5	0	146	2054	-6.35	-0.28	0
35	SLE FR 6	0	155	2119	-6.75	-0.29	0
35	SLE QP 1	0	132	1958	-5.76	-0.26	0
35	SLE QP 2	0	146	2054	-6.35	-0.28	0
35	SLD 1	27	284	1944	-12.05	25.95	0.12
35	SLD 2	27	284	1944	-12.05	25.95	0.12
35	SLD 3	17	148	1899	-6.42	19.03	0.08
35	SLD 4	17	148	1899	-6.42	19.03	0.08
35	SLD 5	23	393	2090	-16.6	18.07	0.11
35	SLD 6	23	393	2090	-16.6	18.07	0.11
35	SLD 7	-10	-60	1939	2.16	-4.97	-0.05
35	SLD 8	-10	-60	1939	2.16	-4.97	-0.05
35	SLD 9	9	351	2170	-14.86	4.41	0.05
35	SLD 10	9	351	2170	-14.86	4.41	0.05
35	SLD 11	-23	-102	2019	3.89	-18.62	-0.11
35	SLD 12	-23	-102	2019	3.89	-18.62	-0.11
35	SLD 13	-18	144	2210	-6.28	-19.59	-0.08
35	SLD 14	-18	144	2210	-6.28	-19.59	-0.08
35	SLD 15	-27	8	2165	-0.65	-26.5	-0.12
35	SLD 16	-27	8	2165	-0.65	-26.5	-0.12
35	SLV 1	67	470	1793	-19.74	64.98	0.31
35	SLV 2	67	470	1793	-19.74	64.98	0.31
35	SLV 3	43	151	1686	-6.53	47.45	0.19
35	SLV 4	43	151	1686	-6.53	47.45	0.19
35	SLV 5	57	727	2139	-30.4	45.88	0.28
35	SLV 6	57	727	2139	-30.4	45.88	0.28
35	SLV 7	-25	-337	1781	13.63	-12.54	-0.13
35	SLV 8	-25	-337	1781	13.63	-12.54	-0.13
35	SLV 9	24	628	2328	-26.33	11.98	0.13
35	SLV 10	24	628	2328	-26.33	11.98	0.13
35	SLV 11	-58	-435	1970	17.7	-46.43	-0.28
35	SLV 12	-58	-435	1970	17.7	-46.43	-0.28
35	SLV 13	-43	141	2423	-6.17	-48	-0.19
35	SLV 14	-43	141	2423	-6.17	-48	-0.19
35	SLV 15	-68	-178	2316	7.04	-65.53	-0.31
35	SLV 16	-68	-178	2316	7.04	-65.53	-0.31
36	SLU 1	0	176	1946	-7.3	0.16	0
36	SLU 2	0	176	1946	-7.3	0.16	0
36	SLU 3	0	176	1946	-7.3	0.16	0
36	SLU 4	0	176	1946	-7.3	0.16	0
36	SLU 5	0	176	1946	-7.3	0.16	0
36	SLU 6	0	176	1946	-7.3	0.16	0
36	SLU 7	0	176	1946	-7.3	0.16	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
36	SLU 8	0	176	1946	-7.3	0.16	0
36	SLU 9	0	176	1946	-7.3	0.16	0
36	SLU 10	0	234	2288	-9.7	0.17	0
36	SLU 11	0	234	2288	-9.7	0.17	0
36	SLU 12	0	234	2288	-9.7	0.17	0
36	SLU 13	0	234	2288	-9.7	0.17	0
36	SLU 14	0	234	2288	-9.7	0.17	0
36	SLU 15	0	234	2288	-9.7	0.17	0
36	SLU 16	0	234	2288	-9.7	0.17	0
36	SLU 17	0	234	2288	-9.7	0.17	0
36	SLU 18	0	259	2435	-10.73	0.18	0
36	SLU 19	0	259	2435	-10.73	0.18	0
36	SLU 20	0	259	2435	-10.73	0.18	0
36	SLU 21	0	259	2435	-10.73	0.18	0
36	SLU 22	0	203	2140	-8.45	0.18	0
36	SLU 23	0	203	2140	-8.45	0.18	0
36	SLU 24	0	203	2140	-8.45	0.18	0
36	SLU 25	0	203	2140	-8.45	0.18	0
36	SLU 26	0	203	2140	-8.45	0.18	0
36	SLU 27	0	203	2140	-8.45	0.18	0
36	SLU 28	0	203	2140	-8.45	0.18	0
36	SLU 29	0	203	2140	-8.45	0.18	0
36	SLU 30	0	203	2140	-8.45	0.18	0
36	SLU 31	0	262	2483	-10.85	0.19	0
36	SLU 32	0	262	2483	-10.85	0.19	0
36	SLU 33	0	262	2483	-10.85	0.19	0
36	SLU 34	0	262	2483	-10.85	0.19	0
36	SLU 35	0	262	2483	-10.85	0.19	0
36	SLU 36	0	262	2483	-10.85	0.19	0
36	SLU 37	0	262	2483	-10.85	0.19	0
36	SLU 38	0	262	2483	-10.85	0.19	0
36	SLU 39	0	287	2630	-11.88	0.19	0
36	SLU 40	0	287	2630	-11.88	0.19	0
36	SLU 41	0	287	2630	-11.88	0.19	0
36	SLU 42	0	287	2630	-11.88	0.19	0
36	SLU 43	0	219	2463	-9.09	0.2	0
36	SLU 44	0	219	2463	-9.09	0.2	0
36	SLU 45	0	219	2463	-9.09	0.2	0
36	SLU 46	0	219	2463	-9.09	0.2	0
36	SLU 47	0	219	2463	-9.09	0.2	0
36	SLU 48	0	219	2463	-9.09	0.2	0
36	SLU 49	0	219	2463	-9.09	0.2	0
36	SLU 50	0	219	2463	-9.09	0.2	0
36	SLU 51	0	219	2463	-9.09	0.2	0
36	SLU 52	0	277	2806	-11.49	0.22	0
36	SLU 53	0	277	2806	-11.49	0.22	0
36	SLU 54	0	277	2806	-11.49	0.22	0
36	SLU 55	0	277	2806	-11.49	0.22	0
36	SLU 56	0	277	2806	-11.49	0.22	0
36	SLU 57	0	277	2806	-11.49	0.22	0
36	SLU 58	0	277	2806	-11.49	0.22	0
36	SLU 59	0	277	2806	-11.49	0.22	0
36	SLU 60	0	302	2952	-12.52	0.22	0
36	SLU 61	0	302	2952	-12.52	0.22	0
36	SLU 62	0	302	2952	-12.52	0.22	0
36	SLU 63	0	302	2952	-12.52	0.22	0
36	SLU 64	0	247	2657	-10.25	0.22	0
36	SLU 65	0	247	2657	-10.25	0.22	0
36	SLU 66	0	247	2657	-10.25	0.22	0
36	SLU 67	0	247	2657	-10.25	0.22	0
36	SLU 68	0	247	2657	-10.25	0.22	0
36	SLU 69	0	247	2657	-10.25	0.22	0
36	SLU 70	0	247	2657	-10.25	0.22	0
36	SLU 71	0	247	2657	-10.25	0.22	0
36	SLU 72	0	247	2657	-10.25	0.22	0
36	SLU 73	0	305	3000	-12.65	0.23	0
36	SLU 74	0	305	3000	-12.65	0.23	0
36	SLU 75	0	305	3000	-12.65	0.23	0
36	SLU 76	0	305	3000	-12.65	0.23	0
36	SLU 77	0	305	3000	-12.65	0.23	0
36	SLU 78	0	305	3000	-12.65	0.23	0
36	SLU 79	0	305	3000	-12.65	0.23	0
36	SLU 80	0	305	3000	-12.65	0.23	0
36	SLU 81	0	330	3147	-13.67	0.24	0
36	SLU 82	0	330	3147	-13.67	0.24	0
36	SLU 83	0	330	3147	-13.67	0.24	0
36	SLU 84	0	330	3147	-13.67	0.24	0
36	SLE RA 1	0	183	2001	-7.63	0.16	0
36	SLE RA 2	0	183	2001	-7.63	0.16	0
36	SLE RA 3	0	183	2001	-7.63	0.16	0
36	SLE RA 4	0	183	2001	-7.63	0.16	0
36	SLE RA 5	0	183	2001	-7.63	0.16	0
36	SLE RA 6	0	183	2001	-7.63	0.16	0
36	SLE RA 7	0	183	2001	-7.63	0.16	0
36	SLE RA 8	0	183	2001	-7.63	0.16	0
36	SLE RA 9	0	183	2001	-7.63	0.16	0
36	SLE RA 10	0	223	2230	-9.23	0.17	0
36	SLE RA 11	0	223	2230	-9.23	0.17	0
36	SLE RA 12	0	223	2230	-9.23	0.17	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
36	SLE RA 13	0	223	2230	-9.23	0.17	0
36	SLE RA 14	0	223	2230	-9.23	0.17	0
36	SLE RA 15	0	223	2230	-9.23	0.17	0
36	SLE RA 16	0	223	2230	-9.23	0.17	0
36	SLE RA 17	0	223	2230	-9.23	0.17	0
36	SLE RA 18	0	239	2328	-9.91	0.18	0
36	SLE RA 19	0	239	2328	-9.91	0.18	0
36	SLE RA 20	0	239	2328	-9.91	0.18	0
36	SLE RA 21	0	239	2328	-9.91	0.18	0
36	SLE FR 1	0	183	2001	-7.63	0.16	0
36	SLE FR 2	0	183	2001	-7.63	0.16	0
36	SLE FR 3	0	183	2001	-7.63	0.16	0
36	SLE FR 4	0	200	2099	-8.31	0.17	0
36	SLE FR 5	0	200	2099	-8.31	0.17	0
36	SLE FR 6	0	211	2164	-8.77	0.17	0
36	SLE QP 1	0	183	2001	-7.63	0.16	0
36	SLE QP 2	0	200	2099	-8.31	0.17	0
36	SLD 1	24	182	2248	-7.54	21.55	-0.01
36	SLD 2	24	182	2248	-7.54	21.55	-0.01
36	SLD 3	33	20	2172	-0.75	29.07	-0.01
36	SLD 4	33	20	2172	-0.75	29.07	-0.01
36	SLD 5	-6	440	2259	-18.38	-4.82	-0.01
36	SLD 6	-6	440	2259	-18.38	-4.82	-0.01
36	SLD 7	23	-99	2006	4.26	20.24	0
36	SLD 8	23	-99	2006	4.26	20.24	0
36	SLD 9	-23	499	2192	-20.89	-19.91	0
36	SLD 10	-23	499	2192	-20.89	-19.91	0
36	SLD 11	6	-39	1939	1.76	5.16	0.01
36	SLD 12	6	-39	1939	1.76	5.16	0.01
36	SLD 13	-33	380	2026	-15.88	-28.74	0.01
36	SLD 14	-33	380	2026	-15.88	-28.74	0.01
36	SLD 15	-24	219	1950	-9.09	-21.22	0.01
36	SLD 16	-24	219	1950	-9.09	-21.22	0.01
36	SLV 1	58	151	2453	-6.25	52.25	-0.03
36	SLV 2	58	151	2453	-6.25	52.25	-0.03
36	SLV 3	80	-229	2274	9.7	71.45	-0.02
36	SLV 4	80	-229	2274	9.7	71.45	-0.02
36	SLV 5	-16	761	2477	-31.88	-13.33	-0.03
36	SLV 6	-16	761	2477	-31.88	-13.33	-0.03
36	SLV 7	57	-504	1880	21.28	50.68	0.01
36	SLV 8	57	-504	1880	21.28	50.68	0.01
36	SLV 9	-57	904	2318	-37.91	-50.34	-0.01
36	SLV 10	-57	904	2318	-37.91	-50.34	-0.01
36	SLV 11	16	-360	1721	15.25	13.67	0.03
36	SLV 12	16	-360	1721	15.25	13.67	0.03
36	SLV 13	-80	629	1924	-26.33	-71.12	0.02
36	SLV 14	-80	629	1924	-26.33	-71.12	0.02
36	SLV 15	-58	250	1745	-10.38	-51.91	0.03
36	SLV 16	-58	250	1745	-10.38	-51.91	0.03
37	SLU 1	0	0	1158	0.04	0	0
37	SLU 2	0	0	1158	0.04	0	0
37	SLU 3	0	0	1158	0.04	0	0
37	SLU 4	0	0	1158	0.04	0	0
37	SLU 5	0	0	1158	0.04	0	0
37	SLU 6	0	0	1158	0.04	0	0
37	SLU 7	0	0	1158	0.04	0	0
37	SLU 8	0	0	1158	0.04	0	0
37	SLU 9	0	0	1158	0.04	0	0
37	SLU 10	0	0	1624	0.09	0	0
37	SLU 11	0	0	1624	0.09	0	0
37	SLU 12	0	0	1624	0.09	0	0
37	SLU 13	0	0	1624	0.09	0	0
37	SLU 14	0	0	1624	0.09	0	0
37	SLU 15	0	0	1624	0.09	0	0
37	SLU 16	0	0	1624	0.09	0	0
37	SLU 17	0	0	1624	0.09	0	0
37	SLU 18	0	0	1823	0.11	0	0
37	SLU 19	0	0	1823	0.11	0	0
37	SLU 20	0	0	1823	0.11	0	0
37	SLU 21	0	0	1823	0.11	0	0
37	SLU 22	0	0	1390	0.06	0	0
37	SLU 23	0	0	1390	0.06	0	0
37	SLU 24	0	0	1390	0.06	0	0
37	SLU 25	0	0	1390	0.06	0	0
37	SLU 26	0	0	1390	0.06	0	0
37	SLU 27	0	0	1390	0.06	0	0
37	SLU 28	0	0	1390	0.06	0	0
37	SLU 29	0	0	1390	0.06	0	0
37	SLU 30	0	0	1390	0.06	0	0
37	SLU 31	0	0	1855	0.11	0	0
37	SLU 32	0	0	1855	0.11	0	0
37	SLU 33	0	0	1855	0.11	0	0
37	SLU 34	0	0	1855	0.11	0	0
37	SLU 35	0	0	1855	0.11	0	0
37	SLU 36	0	0	1855	0.11	0	0
37	SLU 37	0	0	1855	0.11	0	0
37	SLU 38	0	0	1855	0.11	0	0
37	SLU 39	0	0	2054	0.13	0	0
37	SLU 40	0	0	2054	0.13	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
37	SLU 41	0	0	2054	0.13	0	0
37	SLU 42	0	0	2054	0.13	0	0
37	SLU 43	0	0	1427	0.05	0	0
37	SLU 44	0	0	1427	0.05	0	0
37	SLU 45	0	0	1427	0.05	0	0
37	SLU 46	0	0	1427	0.05	0	0
37	SLU 47	0	0	1427	0.05	0	0
37	SLU 48	0	0	1427	0.05	0	0
37	SLU 49	0	0	1427	0.05	0	0
37	SLU 50	0	0	1427	0.05	0	0
37	SLU 51	0	0	1427	0.05	0	0
37	SLU 52	0	0	1892	0.09	0	0
37	SLU 53	0	0	1892	0.09	0	0
37	SLU 54	0	0	1892	0.09	0	0
37	SLU 55	0	0	1892	0.09	0	0
37	SLU 56	0	0	1892	0.09	0	0
37	SLU 57	0	0	1892	0.09	0	0
37	SLU 58	0	0	1892	0.09	0	0
37	SLU 59	0	0	1892	0.09	0	0
37	SLU 60	0	0	2091	0.11	0	0
37	SLU 61	0	0	2091	0.11	0	0
37	SLU 62	0	0	2091	0.11	0	0
37	SLU 63	0	0	2091	0.11	0	0
37	SLU 64	0	0	1658	0.07	0	0
37	SLU 65	0	0	1658	0.07	0	0
37	SLU 66	0	0	1658	0.07	0	0
37	SLU 67	0	0	1658	0.07	0	0
37	SLU 68	0	0	1658	0.07	0	0
37	SLU 69	0	0	1658	0.07	0	0
37	SLU 70	0	0	1658	0.07	0	0
37	SLU 71	0	0	1658	0.07	0	0
37	SLU 72	0	0	1658	0.07	0	0
37	SLU 73	0	0	2123	0.11	0	0
37	SLU 74	0	0	2123	0.11	0	0
37	SLU 75	0	0	2123	0.11	0	0
37	SLU 76	0	0	2123	0.11	0	0
37	SLU 77	0	0	2123	0.11	0	0
37	SLU 78	0	0	2123	0.11	0	0
37	SLU 79	0	0	2123	0.11	0	0
37	SLU 80	0	0	2123	0.11	0	0
37	SLU 81	0	0	2322	0.13	0	0
37	SLU 82	0	0	2322	0.13	0	0
37	SLU 83	0	0	2322	0.13	0	0
37	SLU 84	0	0	2322	0.13	0	0
37	SLE RA 1	0	0	1225	0.05	0	0
37	SLE RA 2	0	0	1225	0.05	0	0
37	SLE RA 3	0	0	1225	0.05	0	0
37	SLE RA 4	0	0	1225	0.05	0	0
37	SLE RA 5	0	0	1225	0.05	0	0
37	SLE RA 6	0	0	1225	0.05	0	0
37	SLE RA 7	0	0	1225	0.05	0	0
37	SLE RA 8	0	0	1225	0.05	0	0
37	SLE RA 9	0	0	1225	0.05	0	0
37	SLE RA 10	0	0	1535	0.08	0	0
37	SLE RA 11	0	0	1535	0.08	0	0
37	SLE RA 12	0	0	1535	0.08	0	0
37	SLE RA 13	0	0	1535	0.08	0	0
37	SLE RA 14	0	0	1535	0.08	0	0
37	SLE RA 15	0	0	1535	0.08	0	0
37	SLE RA 16	0	0	1535	0.08	0	0
37	SLE RA 17	0	0	1535	0.08	0	0
37	SLE RA 18	0	0	1667	0.09	0	0
37	SLE RA 19	0	0	1667	0.09	0	0
37	SLE RA 20	0	0	1667	0.09	0	0
37	SLE RA 21	0	0	1667	0.09	0	0
37	SLE FR 1	0	0	1225	0.05	0	0
37	SLE FR 2	0	0	1225	0.05	0	0
37	SLE FR 3	0	0	1225	0.05	0	0
37	SLE FR 4	0	0	1357	0.06	0	0
37	SLE FR 5	0	0	1357	0.06	0	0
37	SLE FR 6	0	0	1446	0.07	0	0
37	SLE QP 1	0	0	1225	0.05	0	0
37	SLE QP 2	0	0	1357	0.06	0	0
37	SLD 1	-7	-5	1334	-10.09	7.09	-0.12
37	SLD 2	-7	-5	1334	-10.09	7.09	-0.12
37	SLD 3	-5	10	1406	19.21	8.99	-0.09
37	SLD 4	-5	10	1406	19.21	8.99	-0.09
37	SLD 5	-4	-25	1240	-47.42	-0.76	-0.08
37	SLD 6	-4	-25	1240	-47.42	-0.76	-0.08
37	SLD 7	1	26	1482	50.24	5.59	0.02
37	SLD 8	1	26	1482	50.24	5.59	0.02
37	SLD 9	-1	-26	1233	-50.11	-5.59	-0.02
37	SLD 10	-1	-26	1233	-50.11	-5.59	-0.02
37	SLD 11	4	25	1475	47.54	0.76	0.08
37	SLD 12	4	25	1475	47.54	0.76	0.08
37	SLD 13	5	-10	1309	-19.08	-8.99	0.09
37	SLD 14	5	-10	1309	-19.08	-8.99	0.09
37	SLD 15	7	5	1381	10.21	-7.09	0.12
37	SLD 16	7	5	1381	10.21	-7.09	0.12



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
37	SLV 1	-17	-13	1296	-25.98	18.08	-0.31
37	SLV 2	-17	-13	1296	-25.98	18.08	-0.31
37	SLV 3	-13	26	1483	49.18	22.96	-0.23
37	SLV 4	-13	26	1483	49.18	22.96	-0.23
37	SLV 5	-11	-63	1056	-121.74	-1.98	-0.21
37	SLV 6	-11	-63	1056	-121.74	-1.98	-0.21
37	SLV 7	2	67	1678	128.79	14.29	0.05
37	SLV 8	2	67	1678	128.79	14.29	0.05
37	SLV 9	-2	-67	1037	-128.66	-14.29	-0.05
37	SLV 10	-2	-67	1037	-128.66	-14.29	-0.05
37	SLV 11	11	63	1659	121.86	1.98	0.21
37	SLV 12	11	63	1659	121.86	1.98	0.21
37	SLV 13	13	-26	1232	-49.06	-22.96	0.23
37	SLV 14	13	-26	1232	-49.06	-22.96	0.23
37	SLV 15	17	13	1419	26.1	-18.08	0.31
37	SLV 16	17	13	1419	26.1	-18.08	0.31
38	SLU 1	0	72	1752	-4	-0.16	0
38	SLU 2	0	72	1752	-4	-0.16	0
38	SLU 3	0	72	1752	-4	-0.16	0
38	SLU 4	0	72	1752	-4	-0.16	0
38	SLU 5	0	72	1752	-4	-0.16	0
38	SLU 6	0	72	1752	-4	-0.16	0
38	SLU 7	0	72	1752	-4	-0.16	0
38	SLU 8	0	72	1752	-4	-0.16	0
38	SLU 9	0	72	1752	-4	-0.16	0
38	SLU 10	0	112	2050	-5.9	-0.2	0
38	SLU 11	0	112	2050	-5.9	-0.2	0
38	SLU 12	0	112	2050	-5.9	-0.2	0
38	SLU 13	0	112	2050	-5.9	-0.2	0
38	SLU 14	0	112	2050	-5.9	-0.2	0
38	SLU 15	0	112	2050	-5.9	-0.2	0
38	SLU 16	0	112	2050	-5.9	-0.2	0
38	SLU 17	0	112	2050	-5.9	-0.2	0
38	SLU 18	0	129	2178	-6.72	-0.21	0
38	SLU 19	0	129	2178	-6.72	-0.21	0
38	SLU 20	0	129	2178	-6.72	-0.21	0
38	SLU 21	0	129	2178	-6.72	-0.21	0
38	SLU 22	0	88	1910	-4.81	-0.19	0
38	SLU 23	0	88	1910	-4.81	-0.19	0
38	SLU 24	0	88	1910	-4.81	-0.19	0
38	SLU 25	0	88	1910	-4.81	-0.19	0
38	SLU 26	0	88	1910	-4.81	-0.19	0
38	SLU 27	0	88	1910	-4.81	-0.19	0
38	SLU 28	0	88	1910	-4.81	-0.19	0
38	SLU 29	0	88	1910	-4.81	-0.19	0
38	SLU 30	0	88	1910	-4.81	-0.19	0
38	SLU 31	0	128	2208	-6.71	-0.22	0
38	SLU 32	0	128	2208	-6.71	-0.22	0
38	SLU 33	0	128	2208	-6.71	-0.22	0
38	SLU 34	0	128	2208	-6.71	-0.22	0
38	SLU 35	0	128	2208	-6.71	-0.22	0
38	SLU 36	0	128	2208	-6.71	-0.22	0
38	SLU 37	0	128	2208	-6.71	-0.22	0
38	SLU 38	0	128	2208	-6.71	-0.22	0
38	SLU 39	0	146	2336	-7.53	-0.24	0
38	SLU 40	0	146	2336	-7.53	-0.24	0
38	SLU 41	0	146	2336	-7.53	-0.24	0
38	SLU 42	0	146	2336	-7.53	-0.24	0
38	SLU 43	0	88	2223	-4.93	-0.21	0
38	SLU 44	0	88	2223	-4.93	-0.21	0
38	SLU 45	0	88	2223	-4.93	-0.21	0
38	SLU 46	0	88	2223	-4.93	-0.21	0
38	SLU 47	0	88	2223	-4.93	-0.21	0
38	SLU 48	0	88	2223	-4.93	-0.21	0
38	SLU 49	0	88	2223	-4.93	-0.21	0
38	SLU 50	0	88	2223	-4.93	-0.21	0
38	SLU 51	0	88	2223	-4.93	-0.21	0
38	SLU 52	0	128	2522	-6.83	-0.24	0
38	SLU 53	0	128	2522	-6.83	-0.24	0
38	SLU 54	0	128	2522	-6.83	-0.24	0
38	SLU 55	0	128	2522	-6.83	-0.24	0
38	SLU 56	0	128	2522	-6.83	-0.24	0
38	SLU 57	0	128	2522	-6.83	-0.24	0
38	SLU 58	0	128	2522	-6.83	-0.24	0
38	SLU 59	0	128	2522	-6.83	-0.24	0
38	SLU 60	0	145	2650	-7.64	-0.26	0
38	SLU 61	0	145	2650	-7.64	-0.26	0
38	SLU 62	0	145	2650	-7.64	-0.26	0
38	SLU 63	0	145	2650	-7.64	-0.26	0
38	SLU 64	0	104	2381	-5.73	-0.23	0
38	SLU 65	0	104	2381	-5.73	-0.23	0
38	SLU 66	0	104	2381	-5.73	-0.23	0
38	SLU 67	0	104	2381	-5.73	-0.23	0
38	SLU 68	0	104	2381	-5.73	-0.23	0
38	SLU 69	0	104	2381	-5.73	-0.23	0
38	SLU 70	0	104	2381	-5.73	-0.23	0
38	SLU 71	0	104	2381	-5.73	-0.23	0
38	SLU 72	0	104	2381	-5.73	-0.23	0
38	SLU 73	0	144	2680	-7.63	-0.26	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
38	SLU 74	0	144	2680	-7.63	-0.26	0
38	SLU 75	0	144	2680	-7.63	-0.26	0
38	SLU 76	0	144	2680	-7.63	-0.26	0
38	SLU 77	0	144	2680	-7.63	-0.26	0
38	SLU 78	0	144	2680	-7.63	-0.26	0
38	SLU 79	0	144	2680	-7.63	-0.26	0
38	SLU 80	0	144	2680	-7.63	-0.26	0
38	SLU 81	0	161	2808	-8.45	-0.28	0
38	SLU 82	0	161	2808	-8.45	-0.28	0
38	SLU 83	0	161	2808	-8.45	-0.28	0
38	SLU 84	0	161	2808	-8.45	-0.28	0
38	SLE RA 1	0	76	1797	-4.23	-0.17	0
38	SLE RA 2	0	76	1797	-4.23	-0.17	0
38	SLE RA 3	0	76	1797	-4.23	-0.17	0
38	SLE RA 4	0	76	1797	-4.23	-0.17	0
38	SLE RA 5	0	76	1797	-4.23	-0.17	0
38	SLE RA 6	0	76	1797	-4.23	-0.17	0
38	SLE RA 7	0	76	1797	-4.23	-0.17	0
38	SLE RA 8	0	76	1797	-4.23	-0.17	0
38	SLE RA 9	0	76	1797	-4.23	-0.17	0
38	SLE RA 10	0	103	1996	-5.5	-0.19	0
38	SLE RA 11	0	103	1996	-5.5	-0.19	0
38	SLE RA 12	0	103	1996	-5.5	-0.19	0
38	SLE RA 13	0	103	1996	-5.5	-0.19	0
38	SLE RA 14	0	103	1996	-5.5	-0.19	0
38	SLE RA 15	0	103	1996	-5.5	-0.19	0
38	SLE RA 16	0	103	1996	-5.5	-0.19	0
38	SLE RA 17	0	103	1996	-5.5	-0.19	0
38	SLE RA 18	0	115	2081	-6.04	-0.2	0
38	SLE RA 19	0	115	2081	-6.04	-0.2	0
38	SLE RA 20	0	115	2081	-6.04	-0.2	0
38	SLE RA 21	0	115	2081	-6.04	-0.2	0
38	SLE FR 1	0	76	1797	-4.23	-0.17	0
38	SLE FR 2	0	76	1797	-4.23	-0.17	0
38	SLE FR 3	0	76	1797	-4.23	-0.17	0
38	SLE FR 4	0	88	1882	-4.77	-0.18	0
38	SLE FR 5	0	88	1882	-4.77	-0.18	0
38	SLE FR 6	0	96	1939	-5.14	-0.19	0
38	SLE QP 1	0	76	1797	-4.23	-0.17	0
38	SLE QP 2	0	88	1882	-4.77	-0.18	0
38	SLD 1	36	88	1795	-4.82	33.05	0.25
38	SLD 2	36	88	1795	-4.82	33.05	0.25
38	SLD 3	28	-58	1771	1.22	25.63	0.19
38	SLD 4	28	-58	1771	1.22	25.63	0.19
38	SLD 5	24	309	1893	-13.96	21.03	0.17
38	SLD 6	24	309	1893	-13.96	21.03	0.17
38	SLD 7	-5	-177	1812	6.19	-3.68	-0.04
38	SLD 8	-5	-177	1812	6.19	-3.68	-0.04
38	SLD 9	5	353	1952	-15.74	3.32	0.04
38	SLD 10	5	353	1952	-15.74	3.32	0.04
38	SLD 11	-24	-134	1872	4.41	-21.39	-0.17
38	SLD 12	-24	-134	1872	4.41	-21.39	-0.17
38	SLD 13	-28	233	1993	-10.77	-26	-0.19
38	SLD 14	-28	233	1993	-10.77	-26	-0.19
38	SLD 15	-36	88	1969	-4.72	-33.41	-0.25
38	SLD 16	-36	88	1969	-4.72	-33.41	-0.25
38	SLV 1	89	89	1676	-4.89	82.25	0.62
38	SLV 2	89	89	1676	-4.89	82.25	0.62
38	SLV 3	67	-254	1619	9.33	63.49	0.46
38	SLV 4	67	-254	1619	9.33	63.49	0.46
38	SLV 5	59	608	1907	-26.37	53	0.43
38	SLV 6	59	608	1907	-26.37	53	0.43
38	SLV 7	-12	-535	1717	21.02	-9.53	-0.1
38	SLV 8	-12	-535	1717	21.02	-9.53	-0.1
38	SLV 9	12	711	2047	-30.57	9.17	0.1
38	SLV 10	12	711	2047	-30.57	9.17	0.1
38	SLV 11	-59	-432	1857	16.82	-53.36	-0.43
38	SLV 12	-59	-432	1857	16.82	-53.36	-0.43
38	SLV 13	-67	430	2145	-18.88	-63.85	-0.47
38	SLV 14	-67	430	2145	-18.88	-63.85	-0.47
38	SLV 15	-89	87	2088	-4.66	-82.61	-0.62
38	SLV 16	-89	87	2088	-4.66	-82.61	-0.62
39	SLU 1	0	152	1940	-6.3	0.13	0
39	SLU 2	0	152	1940	-6.3	0.13	0
39	SLU 3	0	152	1940	-6.3	0.13	0
39	SLU 4	0	152	1940	-6.3	0.13	0
39	SLU 5	0	152	1940	-6.3	0.13	0
39	SLU 6	0	152	1940	-6.3	0.13	0
39	SLU 7	0	152	1940	-6.3	0.13	0
39	SLU 8	0	152	1940	-6.3	0.13	0
39	SLU 9	0	152	1940	-6.3	0.13	0
39	SLU 10	0	206	2290	-8.49	0.14	0
39	SLU 11	0	206	2290	-8.49	0.14	0
39	SLU 12	0	206	2290	-8.49	0.14	0
39	SLU 13	0	206	2290	-8.49	0.14	0
39	SLU 14	0	206	2290	-8.49	0.14	0
39	SLU 15	0	206	2290	-8.49	0.14	0
39	SLU 16	0	206	2290	-8.49	0.14	0
39	SLU 17	0	206	2290	-8.49	0.14	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
39	SLU 18	0	229	2440	-9.43	0.14	0
39	SLU 19	0	229	2440	-9.43	0.14	0
39	SLU 20	0	229	2440	-9.43	0.14	0
39	SLU 21	0	229	2440	-9.43	0.14	0
39	SLU 22	0	179	2136	-7.38	0.14	0
39	SLU 23	0	179	2136	-7.38	0.14	0
39	SLU 24	0	179	2136	-7.38	0.14	0
39	SLU 25	0	179	2136	-7.38	0.14	0
39	SLU 26	0	179	2136	-7.38	0.14	0
39	SLU 27	0	179	2136	-7.38	0.14	0
39	SLU 28	0	179	2136	-7.38	0.14	0
39	SLU 29	0	179	2136	-7.38	0.14	0
39	SLU 30	0	179	2136	-7.38	0.14	0
39	SLU 31	0	233	2487	-9.57	0.15	0
39	SLU 32	0	233	2487	-9.57	0.15	0
39	SLU 33	0	233	2487	-9.57	0.15	0
39	SLU 34	0	233	2487	-9.57	0.15	0
39	SLU 35	0	233	2487	-9.57	0.15	0
39	SLU 36	0	233	2487	-9.57	0.15	0
39	SLU 37	0	233	2487	-9.57	0.15	0
39	SLU 38	0	233	2487	-9.57	0.15	0
39	SLU 39	0	256	2637	-10.51	0.15	0
39	SLU 40	0	256	2637	-10.51	0.15	0
39	SLU 41	0	256	2637	-10.51	0.15	0
39	SLU 42	0	256	2637	-10.51	0.15	0
39	SLU 43	0	189	2455	-7.82	0.16	0
39	SLU 44	0	189	2455	-7.82	0.16	0
39	SLU 45	0	189	2455	-7.82	0.16	0
39	SLU 46	0	189	2455	-7.82	0.16	0
39	SLU 47	0	189	2455	-7.82	0.16	0
39	SLU 48	0	189	2455	-7.82	0.16	0
39	SLU 49	0	189	2455	-7.82	0.16	0
39	SLU 50	0	189	2455	-7.82	0.16	0
39	SLU 51	0	189	2455	-7.82	0.16	0
39	SLU 52	0	243	2805	-10.01	0.17	0
39	SLU 53	0	243	2805	-10.01	0.17	0
39	SLU 54	0	243	2805	-10.01	0.17	0
39	SLU 55	0	243	2805	-10.01	0.17	0
39	SLU 56	0	243	2805	-10.01	0.17	0
39	SLU 57	0	243	2805	-10.01	0.17	0
39	SLU 58	0	243	2805	-10.01	0.17	0
39	SLU 59	0	243	2805	-10.01	0.17	0
39	SLU 60	0	266	2955	-10.95	0.18	0
39	SLU 61	0	266	2955	-10.95	0.18	0
39	SLU 62	0	266	2955	-10.95	0.18	0
39	SLU 63	0	266	2955	-10.95	0.18	0
39	SLU 64	0	215	2651	-8.9	0.18	0
39	SLU 65	0	215	2651	-8.9	0.18	0
39	SLU 66	0	215	2651	-8.9	0.18	0
39	SLU 67	0	215	2651	-8.9	0.18	0
39	SLU 68	0	215	2651	-8.9	0.18	0
39	SLU 69	0	215	2651	-8.9	0.18	0
39	SLU 70	0	215	2651	-8.9	0.18	0
39	SLU 71	0	215	2651	-8.9	0.18	0
39	SLU 72	0	215	2651	-8.9	0.18	0
39	SLU 73	0	269	3001	-11.09	0.19	0
39	SLU 74	0	269	3001	-11.09	0.19	0
39	SLU 75	0	269	3001	-11.09	0.19	0
39	SLU 76	0	269	3001	-11.09	0.19	0
39	SLU 77	0	269	3001	-11.09	0.19	0
39	SLU 78	0	269	3001	-11.09	0.19	0
39	SLU 79	0	269	3001	-11.09	0.19	0
39	SLU 80	0	269	3001	-11.09	0.19	0
39	SLU 81	0	292	3152	-12.03	0.19	0
39	SLU 82	0	292	3152	-12.03	0.19	0
39	SLU 83	0	292	3152	-12.03	0.19	0
39	SLU 84	0	292	3152	-12.03	0.19	0
39	SLE RA 1	0	160	1996	-6.61	0.13	0
39	SLE RA 2	0	160	1996	-6.61	0.13	0
39	SLE RA 3	0	160	1996	-6.61	0.13	0
39	SLE RA 4	0	160	1996	-6.61	0.13	0
39	SLE RA 5	0	160	1996	-6.61	0.13	0
39	SLE RA 6	0	160	1996	-6.61	0.13	0
39	SLE RA 7	0	160	1996	-6.61	0.13	0
39	SLE RA 8	0	160	1996	-6.61	0.13	0
39	SLE RA 9	0	160	1996	-6.61	0.13	0
39	SLE RA 10	0	196	2230	-8.07	0.14	0
39	SLE RA 11	0	196	2230	-8.07	0.14	0
39	SLE RA 12	0	196	2230	-8.07	0.14	0
39	SLE RA 13	0	196	2230	-8.07	0.14	0
39	SLE RA 14	0	196	2230	-8.07	0.14	0
39	SLE RA 15	0	196	2230	-8.07	0.14	0
39	SLE RA 16	0	196	2230	-8.07	0.14	0
39	SLE RA 17	0	196	2230	-8.07	0.14	0
39	SLE RA 18	0	211	2330	-8.7	0.14	0
39	SLE RA 19	0	211	2330	-8.7	0.14	0
39	SLE RA 20	0	211	2330	-8.7	0.14	0
39	SLE RA 21	0	211	2330	-8.7	0.14	0
39	SLE FR 1	0	160	1996	-6.61	0.13	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
39	SLE FR 2	0	160	1996	-6.61	0.13	0
39	SLE FR 3	0	160	1996	-6.61	0.13	0
39	SLE FR 4	0	175	2096	-7.24	0.14	0
39	SLE FR 5	0	175	2096	-7.24	0.14	0
39	SLE FR 6	0	185	2163	-7.65	0.14	0
39	SLE QP 1	0	160	1996	-6.61	0.13	0
39	SLE QP 2	0	175	2096	-7.24	0.14	0
39	SLD 1	29	159	2216	-6.58	24.92	-0.01
39	SLD 2	29	159	2216	-6.58	24.92	-0.01
39	SLD 3	36	-5	2157	0.3	32.07	-0.01
39	SLD 4	36	-5	2157	0.3	32.07	-0.01
39	SLD 5	-2	420	2221	-17.49	-3.28	-0.01
39	SLD 6	-2	420	2221	-17.49	-3.28	-0.01
39	SLD 7	22	-128	2025	5.47	20.57	0
39	SLD 8	22	-128	2025	5.47	20.57	0
39	SLD 9	-22	478	2168	-19.94	-20.3	0
39	SLD 10	-22	478	2168	-19.94	-20.3	0
39	SLD 11	2	-70	1971	3.01	3.55	0.01
39	SLD 12	2	-70	1971	3.01	3.55	0.01
39	SLD 13	-36	355	2036	-14.77	-31.8	0.01
39	SLD 14	-36	355	2036	-14.77	-31.8	0.01
39	SLD 15	-29	191	1977	-7.89	-24.65	0.01
39	SLD 16	-29	191	1977	-7.89	-24.65	0.01
39	SLV 1	71	133	2379	-5.47	60.46	-0.03
39	SLV 2	71	133	2379	-5.47	60.46	-0.03
39	SLV 3	88	-253	2240	10.69	78.75	-0.02
39	SLV 4	88	-253	2240	10.69	78.75	-0.02
39	SLV 5	-6	748	2392	-31.22	-9.49	-0.02
39	SLV 6	-6	748	2392	-31.22	-9.49	-0.02
39	SLV 7	54	-539	1929	22.66	51.45	0.01
39	SLV 8	54	-539	1929	22.66	51.45	0.01
39	SLV 9	-54	889	2264	-37.13	-51.18	-0.01
39	SLV 10	-54	889	2264	-37.13	-51.18	-0.01
39	SLV 11	6	-398	1801	16.75	9.76	0.02
39	SLV 12	6	-398	1801	16.75	9.76	0.02
39	SLV 13	-88	603	1952	-25.16	-78.48	0.02
39	SLV 14	-88	603	1952	-25.16	-78.48	0.02
39	SLV 15	-71	217	1813	-9	-60.19	0.03
39	SLV 16	-71	217	1813	-9	-60.19	0.03
40	SLU 1	0	0	1210	0.03	0	0
40	SLU 2	0	0	1210	0.03	0	0
40	SLU 3	0	0	1210	0.03	0	0
40	SLU 4	0	0	1210	0.03	0	0
40	SLU 5	0	0	1210	0.03	0	0
40	SLU 6	0	0	1210	0.03	0	0
40	SLU 7	0	0	1210	0.03	0	0
40	SLU 8	0	0	1210	0.03	0	0
40	SLU 9	0	0	1210	0.03	0	0
40	SLU 10	0	0	1735	0.08	0	0
40	SLU 11	0	0	1735	0.08	0	0
40	SLU 12	0	0	1735	0.08	0	0
40	SLU 13	0	0	1735	0.08	0	0
40	SLU 14	0	0	1735	0.08	0	0
40	SLU 15	0	0	1735	0.08	0	0
40	SLU 16	0	0	1735	0.08	0	0
40	SLU 17	0	0	1735	0.08	0	0
40	SLU 18	0	0	1961	0.1	0	0
40	SLU 19	0	0	1961	0.1	0	0
40	SLU 20	0	0	1961	0.1	0	0
40	SLU 21	0	0	1961	0.1	0	0
40	SLU 22	0	0	1467	0.05	0	0
40	SLU 23	0	0	1467	0.05	0	0
40	SLU 24	0	0	1467	0.05	0	0
40	SLU 25	0	0	1467	0.05	0	0
40	SLU 26	0	0	1467	0.05	0	0
40	SLU 27	0	0	1467	0.05	0	0
40	SLU 28	0	0	1467	0.05	0	0
40	SLU 29	0	0	1467	0.05	0	0
40	SLU 30	0	0	1467	0.05	0	0
40	SLU 31	0	0	1993	0.1	0	0
40	SLU 32	0	0	1993	0.1	0	0
40	SLU 33	0	0	1993	0.1	0	0
40	SLU 34	0	0	1993	0.1	0	0
40	SLU 35	0	0	1993	0.1	0	0
40	SLU 36	0	0	1993	0.1	0	0
40	SLU 37	0	0	1993	0.1	0	0
40	SLU 38	0	0	1993	0.1	0	0
40	SLU 39	0	0	2218	0.12	0	0
40	SLU 40	0	0	2218	0.12	0	0
40	SLU 41	0	0	2218	0.12	0	0
40	SLU 42	0	0	2218	0.12	0	0
40	SLU 43	0	0	1485	0.03	0	0
40	SLU 44	0	0	1485	0.03	0	0
40	SLU 45	0	0	1485	0.03	0	0
40	SLU 46	0	0	1485	0.03	0	0
40	SLU 47	0	0	1485	0.03	0	0
40	SLU 48	0	0	1485	0.03	0	0
40	SLU 49	0	0	1485	0.03	0	0
40	SLU 50	0	0	1485	0.03	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
40	SLU 51	0	0	1485	0.03	0	0
40	SLU 52	0	0	2010	0.08	0	0
40	SLU 53	0	0	2010	0.08	0	0
40	SLU 54	0	0	2010	0.08	0	0
40	SLU 55	0	0	2010	0.08	0	0
40	SLU 56	0	0	2010	0.08	0	0
40	SLU 57	0	0	2010	0.08	0	0
40	SLU 58	0	0	2010	0.08	0	0
40	SLU 59	0	0	2010	0.08	0	0
40	SLU 60	0	0	2236	0.1	0	0
40	SLU 61	0	0	2236	0.1	0	0
40	SLU 62	0	0	2236	0.1	0	0
40	SLU 63	0	0	2236	0.1	0	0
40	SLU 64	0	0	1742	0.05	0	0
40	SLU 65	0	0	1742	0.05	0	0
40	SLU 66	0	0	1742	0.05	0	0
40	SLU 67	0	0	1742	0.05	0	0
40	SLU 68	0	0	1742	0.05	0	0
40	SLU 69	0	0	1742	0.05	0	0
40	SLU 70	0	0	1742	0.05	0	0
40	SLU 71	0	0	1742	0.05	0	0
40	SLU 72	0	0	1742	0.05	0	0
40	SLU 73	0	0	2267	0.1	0	0
40	SLU 74	0	0	2267	0.1	0	0
40	SLU 75	0	0	2267	0.1	0	0
40	SLU 76	0	0	2267	0.1	0	0
40	SLU 77	0	0	2267	0.1	0	0
40	SLU 78	0	0	2267	0.1	0	0
40	SLU 79	0	0	2267	0.1	0	0
40	SLU 80	0	0	2267	0.1	0	0
40	SLU 81	0	0	2493	0.12	0	0
40	SLU 82	0	0	2493	0.12	0	0
40	SLU 83	0	0	2493	0.12	0	0
40	SLU 84	0	0	2493	0.12	0	0
40	SLE RA 1	0	0	1283	0.04	0	0
40	SLE RA 2	0	0	1283	0.04	0	0
40	SLE RA 3	0	0	1283	0.04	0	0
40	SLE RA 4	0	0	1283	0.04	0	0
40	SLE RA 5	0	0	1283	0.04	0	0
40	SLE RA 6	0	0	1283	0.04	0	0
40	SLE RA 7	0	0	1283	0.04	0	0
40	SLE RA 8	0	0	1283	0.04	0	0
40	SLE RA 9	0	0	1283	0.04	0	0
40	SLE RA 10	0	0	1634	0.07	0	0
40	SLE RA 11	0	0	1634	0.07	0	0
40	SLE RA 12	0	0	1634	0.07	0	0
40	SLE RA 13	0	0	1634	0.07	0	0
40	SLE RA 14	0	0	1634	0.07	0	0
40	SLE RA 15	0	0	1634	0.07	0	0
40	SLE RA 16	0	0	1634	0.07	0	0
40	SLE RA 17	0	0	1634	0.07	0	0
40	SLE RA 18	0	0	1784	0.08	0	0
40	SLE RA 19	0	0	1784	0.08	0	0
40	SLE RA 20	0	0	1784	0.08	0	0
40	SLE RA 21	0	0	1784	0.08	0	0
40	SLE FR 1	0	0	1283	0.04	0	0
40	SLE FR 2	0	0	1283	0.04	0	0
40	SLE FR 3	0	0	1283	0.04	0	0
40	SLE FR 4	0	0	1433	0.05	0	0
40	SLE FR 5	0	0	1433	0.05	0	0
40	SLE FR 6	0	0	1534	0.06	0	0
40	SLE QP 1	0	0	1283	0.04	0	0
40	SLE QP 2	0	0	1433	0.05	0	0
40	SLD 1	-8	-57	1412	-8.46	8.37	-0.1
40	SLD 2	-8	-57	1412	-8.46	8.37	-0.1
40	SLD 3	-7	109	1482	16.07	10.79	-0.08
40	SLD 4	-7	109	1482	16.07	10.79	-0.08
40	SLD 5	-5	-270	1322	-39.7	-1.15	-0.06
40	SLD 6	-5	-270	1322	-39.7	-1.15	-0.06
40	SLD 7	1	286	1554	42.06	6.9	0.01
40	SLD 8	1	286	1554	42.06	6.9	0.01
40	SLD 9	-1	-285	1313	-41.96	-6.9	-0.01
40	SLD 10	-1	-285	1313	-41.96	-6.9	-0.01
40	SLD 11	5	270	1545	39.8	1.15	0.06
40	SLD 12	5	270	1545	39.8	1.15	0.06
40	SLD 13	7	-109	1385	-15.97	-10.79	0.08
40	SLD 14	7	-109	1385	-15.97	-10.79	0.08
40	SLD 15	8	58	1455	8.56	-8.38	0.1
40	SLD 16	8	58	1455	8.56	-8.38	0.1
40	SLV 1	-21	-147	1378	-21.78	21.35	-0.25
40	SLV 2	-21	-147	1378	-21.78	21.35	-0.25
40	SLV 3	-16	280	1557	41.15	27.54	-0.2
40	SLV 4	-16	280	1557	41.15	27.54	-0.2
40	SLV 5	-13	-692	1146	-101.94	-2.99	-0.16
40	SLV 6	-13	-692	1146	-101.94	-2.99	-0.16
40	SLV 7	2	732	1741	107.82	17.65	0.02
40	SLV 8	2	732	1741	107.82	17.65	0.02
40	SLV 9	-2	-732	1126	-107.72	-17.66	-0.02
40	SLV 10	-2	-732	1126	-107.72	-17.66	-0.02



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
40	SLV 11	13	693	1721	102.04	2.99	0.16
40	SLV 12	13	693	1721	102.04	2.99	0.16
40	SLV 13	16	-280	1310	-41.05	-27.54	0.2
40	SLV 14	16	-280	1310	-41.05	-27.54	0.2
40	SLV 15	21	147	1489	21.88	-21.35	0.25
40	SLV 16	21	147	1489	21.88	-21.35	0.25
41	SLU 1	0	55	1595	-2.58	-0.13	0
41	SLU 2	0	55	1595	-2.58	-0.13	0
41	SLU 3	0	55	1595	-2.58	-0.13	0
41	SLU 4	0	55	1595	-2.58	-0.13	0
41	SLU 5	0	55	1595	-2.58	-0.13	0
41	SLU 6	0	55	1595	-2.58	-0.13	0
41	SLU 7	0	55	1595	-2.58	-0.13	0
41	SLU 8	0	55	1595	-2.58	-0.13	0
41	SLU 9	0	55	1595	-2.58	-0.13	0
41	SLU 10	0	95	1859	-4.17	-0.16	0
41	SLU 11	0	95	1859	-4.17	-0.16	0
41	SLU 12	0	95	1859	-4.17	-0.16	0
41	SLU 13	0	95	1859	-4.17	-0.16	0
41	SLU 14	0	95	1859	-4.17	-0.16	0
41	SLU 15	0	95	1859	-4.17	-0.16	0
41	SLU 16	0	95	1859	-4.17	-0.16	0
41	SLU 17	0	95	1859	-4.17	-0.16	0
41	SLU 18	0	112	1972	-4.85	-0.17	0
41	SLU 19	0	112	1972	-4.85	-0.17	0
41	SLU 20	0	112	1972	-4.85	-0.17	0
41	SLU 21	0	112	1972	-4.85	-0.17	0
41	SLU 22	0	72	1735	-3.27	-0.14	0
41	SLU 23	0	72	1735	-3.27	-0.14	0
41	SLU 24	0	72	1735	-3.27	-0.14	0
41	SLU 25	0	72	1735	-3.27	-0.14	0
41	SLU 26	0	72	1735	-3.27	-0.14	0
41	SLU 27	0	72	1735	-3.27	-0.14	0
41	SLU 28	0	72	1735	-3.27	-0.14	0
41	SLU 29	0	72	1735	-3.27	-0.14	0
41	SLU 30	0	72	1735	-3.27	-0.14	0
41	SLU 31	0	112	1999	-4.87	-0.18	0
41	SLU 32	0	112	1999	-4.87	-0.18	0
41	SLU 33	0	112	1999	-4.87	-0.18	0
41	SLU 34	0	112	1999	-4.87	-0.18	0
41	SLU 35	0	112	1999	-4.87	-0.18	0
41	SLU 36	0	112	1999	-4.87	-0.18	0
41	SLU 37	0	112	1999	-4.87	-0.18	0
41	SLU 38	0	112	1999	-4.87	-0.18	0
41	SLU 39	0	129	2112	-5.55	-0.19	0
41	SLU 40	0	129	2112	-5.55	-0.19	0
41	SLU 41	0	129	2112	-5.55	-0.19	0
41	SLU 42	0	129	2112	-5.55	-0.19	0
41	SLU 43	0	66	2025	-3.12	-0.16	0
41	SLU 44	0	66	2025	-3.12	-0.16	0
41	SLU 45	0	66	2025	-3.12	-0.16	0
41	SLU 46	0	66	2025	-3.12	-0.16	0
41	SLU 47	0	66	2025	-3.12	-0.16	0
41	SLU 48	0	66	2025	-3.12	-0.16	0
41	SLU 49	0	66	2025	-3.12	-0.16	0
41	SLU 50	0	66	2025	-3.12	-0.16	0
41	SLU 51	0	66	2025	-3.12	-0.16	0
41	SLU 52	0	105	2289	-4.71	-0.19	0
41	SLU 53	0	105	2289	-4.71	-0.19	0
41	SLU 54	0	105	2289	-4.71	-0.19	0
41	SLU 55	0	105	2289	-4.71	-0.19	0
41	SLU 56	0	105	2289	-4.71	-0.19	0
41	SLU 57	0	105	2289	-4.71	-0.19	0
41	SLU 58	0	105	2289	-4.71	-0.19	0
41	SLU 59	0	105	2289	-4.71	-0.19	0
41	SLU 60	0	122	2402	-5.39	-0.2	0
41	SLU 61	0	122	2402	-5.39	-0.2	0
41	SLU 62	0	122	2402	-5.39	-0.2	0
41	SLU 63	0	122	2402	-5.39	-0.2	0
41	SLU 64	0	83	2165	-3.81	-0.18	0
41	SLU 65	0	83	2165	-3.81	-0.18	0
41	SLU 66	0	83	2165	-3.81	-0.18	0
41	SLU 67	0	83	2165	-3.81	-0.18	0
41	SLU 68	0	83	2165	-3.81	-0.18	0
41	SLU 69	0	83	2165	-3.81	-0.18	0
41	SLU 70	0	83	2165	-3.81	-0.18	0
41	SLU 71	0	83	2165	-3.81	-0.18	0
41	SLU 72	0	83	2165	-3.81	-0.18	0
41	SLU 73	0	123	2429	-5.4	-0.21	0
41	SLU 74	0	123	2429	-5.4	-0.21	0
41	SLU 75	0	123	2429	-5.4	-0.21	0
41	SLU 76	0	123	2429	-5.4	-0.21	0
41	SLU 77	0	123	2429	-5.4	-0.21	0
41	SLU 78	0	123	2429	-5.4	-0.21	0
41	SLU 79	0	123	2429	-5.4	-0.21	0
41	SLU 80	0	123	2429	-5.4	-0.21	0
41	SLU 81	0	139	2542	-6.08	-0.22	0
41	SLU 82	0	139	2542	-6.08	-0.22	0
41	SLU 83	0	139	2542	-6.08	-0.22	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
41	SLU 84	0	139	2542	-6.08	-0.22	0
41	SLE RA 1	0	60	1635	-2.78	-0.13	0
41	SLE RA 2	0	60	1635	-2.78	-0.13	0
41	SLE RA 3	0	60	1635	-2.78	-0.13	0
41	SLE RA 4	0	60	1635	-2.78	-0.13	0
41	SLE RA 5	0	60	1635	-2.78	-0.13	0
41	SLE RA 6	0	60	1635	-2.78	-0.13	0
41	SLE RA 7	0	60	1635	-2.78	-0.13	0
41	SLE RA 8	0	60	1635	-2.78	-0.13	0
41	SLE RA 9	0	60	1635	-2.78	-0.13	0
41	SLE RA 10	0	86	1811	-3.84	-0.15	0
41	SLE RA 11	0	86	1811	-3.84	-0.15	0
41	SLE RA 12	0	86	1811	-3.84	-0.15	0
41	SLE RA 13	0	86	1811	-3.84	-0.15	0
41	SLE RA 14	0	86	1811	-3.84	-0.15	0
41	SLE RA 15	0	86	1811	-3.84	-0.15	0
41	SLE RA 16	0	86	1811	-3.84	-0.15	0
41	SLE RA 17	0	86	1811	-3.84	-0.15	0
41	SLE RA 18	0	98	1886	-4.29	-0.16	0
41	SLE RA 19	0	98	1886	-4.29	-0.16	0
41	SLE RA 20	0	98	1886	-4.29	-0.16	0
41	SLE RA 21	0	98	1886	-4.29	-0.16	0
41	SLE FR 1	0	60	1635	-2.78	-0.13	0
41	SLE FR 2	0	60	1635	-2.78	-0.13	0
41	SLE FR 3	0	60	1635	-2.78	-0.13	0
41	SLE FR 4	0	71	1710	-3.23	-0.14	0
41	SLE FR 5	0	71	1710	-3.23	-0.14	0
41	SLE FR 6	0	79	1761	-3.54	-0.15	0
41	SLE QP 1	0	60	1635	-2.78	-0.13	0
41	SLE QP 2	0	71	1710	-3.23	-0.14	0
41	SLD 1	42	73	1644	-3.31	37.46	0.38
41	SLD 2	42	73	1644	-3.31	37.46	0.38
41	SLD 3	34	-81	1625	2.58	29.6	0.31
41	SLD 4	34	-81	1625	2.58	29.6	0.31
41	SLD 5	25	307	1719	-12.19	23.05	0.23
41	SLD 6	25	307	1719	-12.19	23.05	0.23
41	SLD 7	-2	-209	1655	7.45	-3.13	-0.02
41	SLD 8	-2	-209	1655	7.45	-3.13	-0.02
41	SLD 9	2	352	1765	-13.92	2.85	0.02
41	SLD 10	2	352	1765	-13.92	2.85	0.02
41	SLD 11	-25	-164	1701	5.73	-23.34	-0.23
41	SLD 12	-25	-164	1701	5.73	-23.34	-0.23
41	SLD 13	-34	224	1796	-9.05	-29.88	-0.31
41	SLD 14	-34	224	1796	-9.05	-29.88	-0.31
41	SLD 15	-42	69	1777	-3.16	-37.74	-0.38
41	SLD 16	-42	69	1777	-3.16	-37.74	-0.38
41	SLV 1	103	76	1552	-3.4	92.98	0.94
41	SLV 2	103	76	1552	-3.4	92.98	0.94
41	SLV 3	84	-288	1507	10.44	73.09	0.75
41	SLV 4	84	-288	1507	10.44	73.09	0.75
41	SLV 5	61	624	1732	-24.28	57.96	0.57
41	SLV 6	61	624	1732	-24.28	57.96	0.57
41	SLV 7	-5	-588	1581	21.86	-8.33	-0.06
41	SLV 8	-5	-588	1581	21.86	-8.33	-0.06
41	SLV 9	5	731	1840	-28.33	8.05	0.06
41	SLV 10	5	731	1840	-28.33	8.05	0.06
41	SLV 11	-61	-481	1689	17.81	-58.24	-0.57
41	SLV 12	-61	-481	1689	17.81	-58.24	-0.57
41	SLV 13	-84	431	1913	-16.91	-73.37	-0.76
41	SLV 14	-84	431	1913	-16.91	-73.37	-0.76
41	SLV 15	-103	67	1868	-3.06	-93.26	-0.94
41	SLV 16	-103	67	1868	-3.06	-93.26	-0.94
42	SLU 1	0	133	1945	-5.46	0.13	0
42	SLU 2	0	133	1945	-5.46	0.13	0
42	SLU 3	0	133	1945	-5.46	0.13	0
42	SLU 4	0	133	1945	-5.46	0.13	0
42	SLU 5	0	133	1945	-5.46	0.13	0
42	SLU 6	0	133	1945	-5.46	0.13	0
42	SLU 7	0	133	1945	-5.46	0.13	0
42	SLU 8	0	133	1945	-5.46	0.13	0
42	SLU 9	0	133	1945	-5.46	0.13	0
42	SLU 10	0	183	2306	-7.45	0.14	0
42	SLU 11	0	183	2306	-7.45	0.14	0
42	SLU 12	0	183	2306	-7.45	0.14	0
42	SLU 13	0	183	2306	-7.45	0.14	0
42	SLU 14	0	183	2306	-7.45	0.14	0
42	SLU 15	0	183	2306	-7.45	0.14	0
42	SLU 16	0	183	2306	-7.45	0.14	0
42	SLU 17	0	183	2306	-7.45	0.14	0
42	SLU 18	0	204	2461	-8.3	0.15	0
42	SLU 19	0	204	2461	-8.3	0.15	0
42	SLU 20	0	204	2461	-8.3	0.15	0
42	SLU 21	0	204	2461	-8.3	0.15	0
42	SLU 22	0	159	2146	-6.48	0.15	0
42	SLU 23	0	159	2146	-6.48	0.15	0
42	SLU 24	0	159	2146	-6.48	0.15	0
42	SLU 25	0	159	2146	-6.48	0.15	0
42	SLU 26	0	159	2146	-6.48	0.15	0
42	SLU 27	0	159	2146	-6.48	0.15	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
42	SLU 28	0	159	2146	-6.48	0.15	0
42	SLU 29	0	159	2146	-6.48	0.15	0
42	SLU 30	0	159	2146	-6.48	0.15	0
42	SLU 31	0	208	2507	-8.47	0.16	0
42	SLU 32	0	208	2507	-8.47	0.16	0
42	SLU 33	0	208	2507	-8.47	0.16	0
42	SLU 34	0	208	2507	-8.47	0.16	0
42	SLU 35	0	208	2507	-8.47	0.16	0
42	SLU 36	0	208	2507	-8.47	0.16	0
42	SLU 37	0	208	2507	-8.47	0.16	0
42	SLU 38	0	208	2507	-8.47	0.16	0
42	SLU 39	0	230	2662	-9.32	0.17	0
42	SLU 40	0	230	2662	-9.32	0.17	0
42	SLU 41	0	230	2662	-9.32	0.17	0
42	SLU 42	0	230	2662	-9.32	0.17	0
42	SLU 43	0	164	2459	-6.74	0.16	0
42	SLU 44	0	164	2459	-6.74	0.16	0
42	SLU 45	0	164	2459	-6.74	0.16	0
42	SLU 46	0	164	2459	-6.74	0.16	0
42	SLU 47	0	164	2459	-6.74	0.16	0
42	SLU 48	0	164	2459	-6.74	0.16	0
42	SLU 49	0	164	2459	-6.74	0.16	0
42	SLU 50	0	164	2459	-6.74	0.16	0
42	SLU 51	0	164	2459	-6.74	0.16	0
42	SLU 52	0	214	2821	-8.73	0.18	0
42	SLU 53	0	214	2821	-8.73	0.18	0
42	SLU 54	0	214	2821	-8.73	0.18	0
42	SLU 55	0	214	2821	-8.73	0.18	0
42	SLU 56	0	214	2821	-8.73	0.18	0
42	SLU 57	0	214	2821	-8.73	0.18	0
42	SLU 58	0	214	2821	-8.73	0.18	0
42	SLU 59	0	214	2821	-8.73	0.18	0
42	SLU 60	0	235	2975	-9.59	0.18	0
42	SLU 61	0	235	2975	-9.59	0.18	0
42	SLU 62	0	235	2975	-9.59	0.18	0
42	SLU 63	0	235	2975	-9.59	0.18	0
42	SLU 64	0	190	2660	-7.76	0.18	0
42	SLU 65	0	190	2660	-7.76	0.18	0
42	SLU 66	0	190	2660	-7.76	0.18	0
42	SLU 67	0	190	2660	-7.76	0.18	0
42	SLU 68	0	190	2660	-7.76	0.18	0
42	SLU 69	0	190	2660	-7.76	0.18	0
42	SLU 70	0	190	2660	-7.76	0.18	0
42	SLU 71	0	190	2660	-7.76	0.18	0
42	SLU 72	0	190	2660	-7.76	0.18	0
42	SLU 73	0	239	3021	-9.75	0.19	0
42	SLU 74	0	239	3021	-9.75	0.19	0
42	SLU 75	0	239	3021	-9.75	0.19	0
42	SLU 76	0	239	3021	-9.75	0.19	0
42	SLU 77	0	239	3021	-9.75	0.19	0
42	SLU 78	0	239	3021	-9.75	0.19	0
42	SLU 79	0	239	3021	-9.75	0.19	0
42	SLU 80	0	239	3021	-9.75	0.19	0
42	SLU 81	0	261	3176	-10.61	0.2	0
42	SLU 82	0	261	3176	-10.61	0.2	0
42	SLU 83	0	261	3176	-10.61	0.2	0
42	SLU 84	0	261	3176	-10.61	0.2	0
42	SLE RA 1	0	140	2002	-5.75	0.13	0
42	SLE RA 2	0	140	2002	-5.75	0.13	0
42	SLE RA 3	0	140	2002	-5.75	0.13	0
42	SLE RA 4	0	140	2002	-5.75	0.13	0
42	SLE RA 5	0	140	2002	-5.75	0.13	0
42	SLE RA 6	0	140	2002	-5.75	0.13	0
42	SLE RA 7	0	140	2002	-5.75	0.13	0
42	SLE RA 8	0	140	2002	-5.75	0.13	0
42	SLE RA 9	0	140	2002	-5.75	0.13	0
42	SLE RA 10	0	174	2243	-7.07	0.14	0
42	SLE RA 11	0	174	2243	-7.07	0.14	0
42	SLE RA 12	0	174	2243	-7.07	0.14	0
42	SLE RA 13	0	174	2243	-7.07	0.14	0
42	SLE RA 14	0	174	2243	-7.07	0.14	0
42	SLE RA 15	0	174	2243	-7.07	0.14	0
42	SLE RA 16	0	174	2243	-7.07	0.14	0
42	SLE RA 17	0	174	2243	-7.07	0.14	0
42	SLE RA 18	0	188	2346	-7.64	0.15	0
42	SLE RA 19	0	188	2346	-7.64	0.15	0
42	SLE RA 20	0	188	2346	-7.64	0.15	0
42	SLE RA 21	0	188	2346	-7.64	0.15	0
42	SLE FR 1	0	140	2002	-5.75	0.13	0
42	SLE FR 2	0	140	2002	-5.75	0.13	0
42	SLE FR 3	0	140	2002	-5.75	0.13	0
42	SLE FR 4	0	155	2105	-6.32	0.14	0
42	SLE FR 5	0	155	2105	-6.32	0.14	0
42	SLE FR 6	0	164	2174	-6.7	0.14	0
42	SLE QP 1	0	140	2002	-5.75	0.13	0
42	SLE QP 2	0	155	2105	-6.32	0.14	0
42	SLD 1	31	142	2205	-5.76	25.63	0
42	SLD 2	31	142	2205	-5.76	25.63	0
42	SLD 3	37	-25	2159	1.2	32.24	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
42	SLD 4	37	-25	2159	1.2	32.24	0
42	SLD 5	0	404	2205	-16.71	-2.24	0
42	SLD 6	0	404	2205	-16.71	-2.24	0
42	SLD 7	20	-152	2052	6.5	19.8	0
42	SLD 8	20	-152	2052	6.5	19.8	0
42	SLD 9	-20	461	2159	-19.13	-19.52	0
42	SLD 10	-20	461	2159	-19.13	-19.52	0
42	SLD 11	0	-94	2006	4.08	2.52	0
42	SLD 12	0	-94	2006	4.08	2.52	0
42	SLD 13	-37	334	2051	-13.84	-31.97	0
42	SLD 14	-37	334	2051	-13.84	-31.97	0
42	SLD 15	-31	167	2005	-6.87	-25.36	0
42	SLD 16	-31	167	2005	-6.87	-25.36	0
42	SLV 1	73	120	2342	-4.8	62.19	0
42	SLV 2	73	120	2342	-4.8	62.19	0
42	SLV 3	88	-271	2234	11.55	79.08	0.01
42	SLV 4	88	-271	2234	11.55	79.08	0.01
42	SLV 5	-1	738	2340	-30.66	-6.87	-0.01
42	SLV 6	-1	738	2340	-30.66	-6.87	-0.01
42	SLV 7	49	-566	1980	23.84	49.44	0.01
42	SLV 8	49	-566	1980	23.84	49.44	0.01
42	SLV 9	-49	876	2231	-36.48	-49.16	-0.01
42	SLV 10	-49	876	2231	-36.48	-49.16	-0.01
42	SLV 11	1	-429	1870	18.03	7.14	0.01
42	SLV 12	1	-429	1870	18.03	7.14	0.01
42	SLV 13	-88	580	1977	-24.18	-78.8	-0.01
42	SLV 14	-88	580	1977	-24.18	-78.8	-0.01
42	SLV 15	-73	189	1869	-7.83	-61.91	0
42	SLV 16	-73	189	1869	-7.83	-61.91	0
43	SLU 1	0	1	1242	0	0	0
43	SLU 2	0	1	1242	0	0	0
43	SLU 3	0	1	1242	0	0	0
43	SLU 4	0	1	1242	0	0	0
43	SLU 5	0	1	1242	0	0	0
43	SLU 6	0	1	1242	0	0	0
43	SLU 7	0	1	1242	0	0	0
43	SLU 8	0	1	1242	0	0	0
43	SLU 9	0	1	1242	0	0	0
43	SLU 10	0	2	1812	0.02	0	0
43	SLU 11	0	2	1812	0.02	0	0
43	SLU 12	0	2	1812	0.02	0	0
43	SLU 13	0	2	1812	0.02	0	0
43	SLU 14	0	2	1812	0.02	0	0
43	SLU 15	0	2	1812	0.02	0	0
43	SLU 16	0	2	1812	0.02	0	0
43	SLU 17	0	2	1812	0.02	0	0
43	SLU 18	0	3	2056	0.03	0	0
43	SLU 19	0	3	2056	0.03	0	0
43	SLU 20	0	3	2056	0.03	0	0
43	SLU 21	0	3	2056	0.03	0	0
43	SLU 22	0	1	1518	0.01	0	0
43	SLU 23	0	1	1518	0.01	0	0
43	SLU 24	0	1	1518	0.01	0	0
43	SLU 25	0	1	1518	0.01	0	0
43	SLU 26	0	1	1518	0.01	0	0
43	SLU 27	0	1	1518	0.01	0	0
43	SLU 28	0	1	1518	0.01	0	0
43	SLU 29	0	1	1518	0.01	0	0
43	SLU 30	0	1	1518	0.01	0	0
43	SLU 31	0	3	2088	0.03	0	0
43	SLU 32	0	3	2088	0.03	0	0
43	SLU 33	0	3	2088	0.03	0	0
43	SLU 34	0	3	2088	0.03	0	0
43	SLU 35	0	3	2088	0.03	0	0
43	SLU 36	0	3	2088	0.03	0	0
43	SLU 37	0	3	2088	0.03	0	0
43	SLU 38	0	3	2088	0.03	0	0
43	SLU 39	0	3	2332	0.04	0	0
43	SLU 40	0	3	2332	0.04	0	0
43	SLU 41	0	3	2332	0.04	0	0
43	SLU 42	0	3	2332	0.04	0	0
43	SLU 43	0	1	1520	-0.01	0	0
43	SLU 44	0	1	1520	-0.01	0	0
43	SLU 45	0	1	1520	-0.01	0	0
43	SLU 46	0	1	1520	-0.01	0	0
43	SLU 47	0	1	1520	-0.01	0	0
43	SLU 48	0	1	1520	-0.01	0	0
43	SLU 49	0	1	1520	-0.01	0	0
43	SLU 50	0	1	1520	-0.01	0	0
43	SLU 51	0	1	1520	-0.01	0	0
43	SLU 52	0	2	2090	0.01	0	0
43	SLU 53	0	2	2090	0.01	0	0
43	SLU 54	0	2	2090	0.01	0	0
43	SLU 55	0	2	2090	0.01	0	0
43	SLU 56	0	2	2090	0.01	0	0
43	SLU 57	0	2	2090	0.01	0	0
43	SLU 58	0	2	2090	0.01	0	0
43	SLU 59	0	2	2090	0.01	0	0
43	SLU 60	0	3	2334	0.02	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
43	SLU 61	0	3	2334	0.02	0	0
43	SLU 62	0	3	2334	0.02	0	0
43	SLU 63	0	3	2334	0.02	0	0
43	SLU 64	0	2	1796	0	0	0
43	SLU 65	0	2	1796	0	0	0
43	SLU 66	0	2	1796	0	0	0
43	SLU 67	0	2	1796	0	0	0
43	SLU 68	0	2	1796	0	0	0
43	SLU 69	0	2	1796	0	0	0
43	SLU 70	0	2	1796	0	0	0
43	SLU 71	0	2	1796	0	0	0
43	SLU 72	0	2	1796	0	0	0
43	SLU 73	0	3	2366	0.02	0	0
43	SLU 74	0	3	2366	0.02	0	0
43	SLU 75	0	3	2366	0.02	0	0
43	SLU 76	0	3	2366	0.02	0	0
43	SLU 77	0	3	2366	0.02	0	0
43	SLU 78	0	3	2366	0.02	0	0
43	SLU 79	0	3	2366	0.02	0	0
43	SLU 80	0	3	2366	0.02	0	0
43	SLU 81	0	3	2610	0.03	0	0
43	SLU 82	0	3	2610	0.03	0	0
43	SLU 83	0	3	2610	0.03	0	0
43	SLU 84	0	3	2610	0.03	0	0
43	SLE RA 1	0	1	1321	0	0	0
43	SLE RA 2	0	1	1321	0	0	0
43	SLE RA 3	0	1	1321	0	0	0
43	SLE RA 4	0	1	1321	0	0	0
43	SLE RA 5	0	1	1321	0	0	0
43	SLE RA 6	0	1	1321	0	0	0
43	SLE RA 7	0	1	1321	0	0	0
43	SLE RA 8	0	1	1321	0	0	0
43	SLE RA 9	0	1	1321	0	0	0
43	SLE RA 10	0	2	1701	0.01	0	0
43	SLE RA 11	0	2	1701	0.01	0	0
43	SLE RA 12	0	2	1701	0.01	0	0
43	SLE RA 13	0	2	1701	0.01	0	0
43	SLE RA 14	0	2	1701	0.01	0	0
43	SLE RA 15	0	2	1701	0.01	0	0
43	SLE RA 16	0	2	1701	0.01	0	0
43	SLE RA 17	0	2	1701	0.01	0	0
43	SLE RA 18	0	2	1864	0.02	0	0
43	SLE RA 19	0	2	1864	0.02	0	0
43	SLE RA 20	0	2	1864	0.02	0	0
43	SLE RA 21	0	2	1864	0.02	0	0
43	SLE FR 1	0	1	1321	0	0	0
43	SLE FR 2	0	1	1321	0	0	0
43	SLE FR 3	0	1	1321	0	0	0
43	SLE FR 4	0	1	1484	0.01	0	0
43	SLE FR 5	0	1	1484	0.01	0	0
43	SLE FR 6	0	2	1592	0.01	0	0
43	SLE QP 1	0	1	1321	0	0	0
43	SLE QP 2	0	1	1484	0.01	0	0
43	SLD 1	-8	-25	1464	-5.53	8.58	0.19
43	SLD 2	-8	-25	1464	-5.53	8.58	0.19
43	SLD 3	-6	52	1533	10.4	11.27	0.16
43	SLD 4	-6	52	1533	10.4	11.27	0.16
43	SLD 5	-5	-124	1372	-25.81	-1.5	0.11
43	SLD 6	-5	-124	1372	-25.81	-1.5	0.11
43	SLD 7	1	134	1604	27.28	7.45	-0.01
43	SLD 8	1	134	1604	27.28	7.45	-0.01
43	SLD 9	-1	-131	1364	-27.27	-7.45	0.01
43	SLD 10	-1	-131	1364	-27.27	-7.45	0.01
43	SLD 11	5	127	1595	25.82	1.49	-0.11
43	SLD 12	5	127	1595	25.82	1.49	-0.11
43	SLD 13	6	-49	1435	-10.39	-11.27	-0.16
43	SLD 14	6	-49	1435	-10.39	-11.27	-0.16
43	SLD 15	8	28	1504	5.54	-8.58	-0.19
43	SLD 16	8	28	1504	5.54	-8.58	-0.19
43	SLV 1	-19	-67	1432	-14.2	21.87	0.48
43	SLV 2	-19	-67	1432	-14.2	21.87	0.48
43	SLV 3	-14	131	1610	26.66	28.75	0.38
43	SLV 4	-14	131	1610	26.66	28.75	0.38
43	SLV 5	-13	-320	1198	-66.24	-3.87	0.28
43	SLV 6	-13	-320	1198	-66.24	-3.87	0.28
43	SLV 7	2	341	1792	69.98	19.06	-0.03
43	SLV 8	2	341	1792	69.98	19.06	-0.03
43	SLV 9	-2	-338	1176	-69.97	-19.06	0.03
43	SLV 10	-2	-338	1176	-69.97	-19.06	0.03
43	SLV 11	13	323	1770	66.25	3.87	-0.28
43	SLV 12	13	323	1770	66.25	3.87	-0.28
43	SLV 13	14	-128	1358	-26.65	-28.75	-0.38
43	SLV 14	14	-128	1358	-26.65	-28.75	-0.38
43	SLV 15	19	70	1536	14.21	-21.87	-0.48
43	SLV 16	19	70	1536	14.21	-21.87	-0.48
44	SLU 1	0	113	1505	-3.68	-0.12	0
44	SLU 2	0	113	1505	-3.68	-0.12	0
44	SLU 3	0	113	1505	-3.68	-0.12	0
44	SLU 4	0	113	1505	-3.68	-0.12	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
44	SLU 5	0	113	1505	-3.68	-0.12	0
44	SLU 6	0	113	1505	-3.68	-0.12	0
44	SLU 7	0	113	1505	-3.68	-0.12	0
44	SLU 8	0	113	1505	-3.68	-0.12	0
44	SLU 9	0	113	1505	-3.68	-0.12	0
44	SLU 10	0	170	1757	-5.71	-0.16	0
44	SLU 11	0	170	1757	-5.71	-0.16	0
44	SLU 12	0	170	1757	-5.71	-0.16	0
44	SLU 13	0	170	1757	-5.71	-0.16	0
44	SLU 14	0	170	1757	-5.71	-0.16	0
44	SLU 15	0	170	1757	-5.71	-0.16	0
44	SLU 16	0	170	1757	-5.71	-0.16	0
44	SLU 17	0	170	1757	-5.71	-0.16	0
44	SLU 18	0	195	1865	-6.58	-0.17	0
44	SLU 19	0	195	1865	-6.58	-0.17	0
44	SLU 20	0	195	1865	-6.58	-0.17	0
44	SLU 21	0	195	1865	-6.58	-0.17	0
44	SLU 22	0	140	1639	-4.63	-0.14	0
44	SLU 23	0	140	1639	-4.63	-0.14	0
44	SLU 24	0	140	1639	-4.63	-0.14	0
44	SLU 25	0	140	1639	-4.63	-0.14	0
44	SLU 26	0	140	1639	-4.63	-0.14	0
44	SLU 27	0	140	1639	-4.63	-0.14	0
44	SLU 28	0	140	1639	-4.63	-0.14	0
44	SLU 29	0	140	1639	-4.63	-0.14	0
44	SLU 30	0	140	1639	-4.63	-0.14	0
44	SLU 31	0	197	1891	-6.66	-0.18	0
44	SLU 32	0	197	1891	-6.66	-0.18	0
44	SLU 33	0	197	1891	-6.66	-0.18	0
44	SLU 34	0	197	1891	-6.66	-0.18	0
44	SLU 35	0	197	1891	-6.66	-0.18	0
44	SLU 36	0	197	1891	-6.66	-0.18	0
44	SLU 37	0	197	1891	-6.66	-0.18	0
44	SLU 38	0	197	1891	-6.66	-0.18	0
44	SLU 39	0	222	2000	-7.53	-0.2	0
44	SLU 40	0	222	2000	-7.53	-0.2	0
44	SLU 41	0	222	2000	-7.53	-0.2	0
44	SLU 42	0	222	2000	-7.53	-0.2	0
44	SLU 43	0	137	1910	-4.46	-0.15	0
44	SLU 44	0	137	1910	-4.46	-0.15	0
44	SLU 45	0	137	1910	-4.46	-0.15	0
44	SLU 46	0	137	1910	-4.46	-0.15	0
44	SLU 47	0	137	1910	-4.46	-0.15	0
44	SLU 48	0	137	1910	-4.46	-0.15	0
44	SLU 49	0	137	1910	-4.46	-0.15	0
44	SLU 50	0	137	1910	-4.46	-0.15	0
44	SLU 51	0	137	1910	-4.46	-0.15	0
44	SLU 52	0	195	2163	-6.49	-0.19	0
44	SLU 53	0	195	2163	-6.49	-0.19	0
44	SLU 54	0	195	2163	-6.49	-0.19	0
44	SLU 55	0	195	2163	-6.49	-0.19	0
44	SLU 56	0	195	2163	-6.49	-0.19	0
44	SLU 57	0	195	2163	-6.49	-0.19	0
44	SLU 58	0	195	2163	-6.49	-0.19	0
44	SLU 59	0	195	2163	-6.49	-0.19	0
44	SLU 60	0	219	2271	-7.36	-0.2	0
44	SLU 61	0	219	2271	-7.36	-0.2	0
44	SLU 62	0	219	2271	-7.36	-0.2	0
44	SLU 63	0	219	2271	-7.36	-0.2	0
44	SLU 64	0	164	2045	-5.41	-0.17	0
44	SLU 65	0	164	2045	-5.41	-0.17	0
44	SLU 66	0	164	2045	-5.41	-0.17	0
44	SLU 67	0	164	2045	-5.41	-0.17	0
44	SLU 68	0	164	2045	-5.41	-0.17	0
44	SLU 69	0	164	2045	-5.41	-0.17	0
44	SLU 70	0	164	2045	-5.41	-0.17	0
44	SLU 71	0	164	2045	-5.41	-0.17	0
44	SLU 72	0	164	2045	-5.41	-0.17	0
44	SLU 73	0	222	2297	-7.44	-0.21	0
44	SLU 74	0	222	2297	-7.44	-0.21	0
44	SLU 75	0	222	2297	-7.44	-0.21	0
44	SLU 76	0	222	2297	-7.44	-0.21	0
44	SLU 77	0	222	2297	-7.44	-0.21	0
44	SLU 78	0	222	2297	-7.44	-0.21	0
44	SLU 79	0	222	2297	-7.44	-0.21	0
44	SLU 80	0	222	2297	-7.44	-0.21	0
44	SLU 81	0	246	2405	-8.3	-0.22	0
44	SLU 82	0	246	2405	-8.3	-0.22	0
44	SLU 83	0	246	2405	-8.3	-0.22	0
44	SLU 84	0	246	2405	-8.3	-0.22	0
44	SLE RA 1	0	120	1543	-3.95	-0.13	0
44	SLE RA 2	0	120	1543	-3.95	-0.13	0
44	SLE RA 3	0	120	1543	-3.95	-0.13	0
44	SLE RA 4	0	120	1543	-3.95	-0.13	0
44	SLE RA 5	0	120	1543	-3.95	-0.13	0
44	SLE RA 6	0	120	1543	-3.95	-0.13	0
44	SLE RA 7	0	120	1543	-3.95	-0.13	0
44	SLE RA 8	0	120	1543	-3.95	-0.13	0
44	SLE RA 9	0	120	1543	-3.95	-0.13	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
44	SLE RA 10	0	159	1712	-5.3	-0.15	0
44	SLE RA 11	0	159	1712	-5.3	-0.15	0
44	SLE RA 12	0	159	1712	-5.3	-0.15	0
44	SLE RA 13	0	159	1712	-5.3	-0.15	0
44	SLE RA 14	0	159	1712	-5.3	-0.15	0
44	SLE RA 15	0	159	1712	-5.3	-0.15	0
44	SLE RA 16	0	159	1712	-5.3	-0.15	0
44	SLE RA 17	0	159	1712	-5.3	-0.15	0
44	SLE RA 18	0	175	1784	-5.88	-0.16	0
44	SLE RA 19	0	175	1784	-5.88	-0.16	0
44	SLE RA 20	0	175	1784	-5.88	-0.16	0
44	SLE RA 21	0	175	1784	-5.88	-0.16	0
44	SLE FR 1	0	120	1543	-3.95	-0.13	0
44	SLE FR 2	0	120	1543	-3.95	-0.13	0
44	SLE FR 3	0	120	1543	-3.95	-0.13	0
44	SLE FR 4	0	137	1615	-4.53	-0.14	0
44	SLE FR 5	0	137	1615	-4.53	-0.14	0
44	SLE FR 6	0	148	1663	-4.92	-0.14	0
44	SLE QP 1	0	120	1543	-3.95	-0.13	0
44	SLE QP 2	0	137	1615	-4.53	-0.14	0
44	SLD 1	44	139	1560	-4.65	38.44	0.44
44	SLD 2	44	139	1560	-4.65	38.44	0.44
44	SLD 3	35	-30	1540	2.07	29.97	0.35
44	SLD 4	35	-30	1540	2.07	29.97	0.35
44	SLD 5	26	395	1629	-14.76	24.29	0.26
44	SLD 6	26	395	1629	-14.76	24.29	0.26
44	SLD 7	-2	-171	1562	7.64	-3.95	-0.02
44	SLD 8	-2	-171	1562	7.64	-3.95	-0.02
44	SLD 9	2	444	1669	-16.7	3.68	0.02
44	SLD 10	2	444	1669	-16.7	3.68	0.02
44	SLD 11	-26	-121	1602	5.7	-24.56	-0.26
44	SLD 12	-26	-121	1602	5.7	-24.56	-0.26
44	SLD 13	-35	304	1691	-11.14	-30.24	-0.36
44	SLD 14	-35	304	1691	-11.14	-30.24	-0.36
44	SLD 15	-44	134	1671	-4.42	-38.72	-0.44
44	SLD 16	-44	134	1671	-4.42	-38.72	-0.44
44	SLV 1	107	143	1483	-4.8	95.34	1.08
44	SLV 2	107	143	1483	-4.8	95.34	1.08
44	SLV 3	86	-257	1435	11.02	73.84	0.86
44	SLV 4	86	-257	1435	11.02	73.84	0.86
44	SLV 5	64	744	1649	-28.59	61.12	0.65
44	SLV 6	64	744	1649	-28.59	61.12	0.65
44	SLV 7	-6	-587	1488	24.11	-10.56	-0.07
44	SLV 8	-6	-587	1488	24.11	-10.56	-0.07
44	SLV 9	6	861	1743	-33.18	10.28	0.07
44	SLV 10	6	861	1743	-33.18	10.28	0.07
44	SLV 11	-64	-470	1582	19.53	-61.39	-0.65
44	SLV 12	-64	-470	1582	19.53	-61.39	-0.65
44	SLV 13	-86	530	1796	-20.08	-74.11	-0.86
44	SLV 14	-86	530	1796	-20.08	-74.11	-0.86
44	SLV 15	-107	131	1748	-4.27	-95.62	-1.08
44	SLV 16	-107	131	1748	-4.27	-95.62	-1.08
45	SLU 1	0	118	1958	-4.81	0.16	0
45	SLU 2	0	118	1958	-4.81	0.16	0
45	SLU 3	0	118	1958	-4.81	0.16	0
45	SLU 4	0	118	1958	-4.81	0.16	0
45	SLU 5	0	118	1958	-4.81	0.16	0
45	SLU 6	0	118	1958	-4.81	0.16	0
45	SLU 7	0	118	1958	-4.81	0.16	0
45	SLU 8	0	118	1958	-4.81	0.16	0
45	SLU 9	0	118	1958	-4.81	0.16	0
45	SLU 10	0	164	2333	-6.62	0.19	0
45	SLU 11	0	164	2333	-6.62	0.19	0
45	SLU 12	0	164	2333	-6.62	0.19	0
45	SLU 13	0	164	2333	-6.62	0.19	0
45	SLU 14	0	164	2333	-6.62	0.19	0
45	SLU 15	0	164	2333	-6.62	0.19	0
45	SLU 16	0	164	2333	-6.62	0.19	0
45	SLU 17	0	164	2333	-6.62	0.19	0
45	SLU 18	0	183	2494	-7.4	0.2	0
45	SLU 19	0	183	2494	-7.4	0.2	0
45	SLU 20	0	183	2494	-7.4	0.2	0
45	SLU 21	0	183	2494	-7.4	0.2	0
45	SLU 22	0	143	2166	-5.79	0.19	0
45	SLU 23	0	143	2166	-5.79	0.19	0
45	SLU 24	0	143	2166	-5.79	0.19	0
45	SLU 25	0	143	2166	-5.79	0.19	0
45	SLU 26	0	143	2166	-5.79	0.19	0
45	SLU 27	0	143	2166	-5.79	0.19	0
45	SLU 28	0	143	2166	-5.79	0.19	0
45	SLU 29	0	143	2166	-5.79	0.19	0
45	SLU 30	0	143	2166	-5.79	0.19	0
45	SLU 31	0	188	2541	-7.6	0.21	0
45	SLU 32	0	188	2541	-7.6	0.21	0
45	SLU 33	0	188	2541	-7.6	0.21	0
45	SLU 34	0	188	2541	-7.6	0.21	0
45	SLU 35	0	188	2541	-7.6	0.21	0
45	SLU 36	0	188	2541	-7.6	0.21	0
45	SLU 37	0	188	2541	-7.6	0.21	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
45	SLU 38	0	188	2541	-7.6	0.21	0
45	SLU 39	0	208	2701	-8.38	0.23	0
45	SLU 40	0	208	2701	-8.38	0.23	0
45	SLU 41	0	208	2701	-8.38	0.23	0
45	SLU 42	0	208	2701	-8.38	0.23	0
45	SLU 43	0	145	2474	-5.92	0.2	0
45	SLU 44	0	145	2474	-5.92	0.2	0
45	SLU 45	0	145	2474	-5.92	0.2	0
45	SLU 46	0	145	2474	-5.92	0.2	0
45	SLU 47	0	145	2474	-5.92	0.2	0
45	SLU 48	0	145	2474	-5.92	0.2	0
45	SLU 49	0	145	2474	-5.92	0.2	0
45	SLU 50	0	145	2474	-5.92	0.2	0
45	SLU 51	0	145	2474	-5.92	0.2	0
45	SLU 52	0	191	2849	-7.73	0.23	0
45	SLU 53	0	191	2849	-7.73	0.23	0
45	SLU 54	0	191	2849	-7.73	0.23	0
45	SLU 55	0	191	2849	-7.73	0.23	0
45	SLU 56	0	191	2849	-7.73	0.23	0
45	SLU 57	0	191	2849	-7.73	0.23	0
45	SLU 58	0	191	2849	-7.73	0.23	0
45	SLU 59	0	191	2849	-7.73	0.23	0
45	SLU 60	0	210	3010	-8.5	0.24	0
45	SLU 61	0	210	3010	-8.5	0.24	0
45	SLU 62	0	210	3010	-8.5	0.24	0
45	SLU 63	0	210	3010	-8.5	0.24	0
45	SLU 64	0	170	2682	-6.9	0.22	0
45	SLU 65	0	170	2682	-6.9	0.22	0
45	SLU 66	0	170	2682	-6.9	0.22	0
45	SLU 67	0	170	2682	-6.9	0.22	0
45	SLU 68	0	170	2682	-6.9	0.22	0
45	SLU 69	0	170	2682	-6.9	0.22	0
45	SLU 70	0	170	2682	-6.9	0.22	0
45	SLU 71	0	170	2682	-6.9	0.22	0
45	SLU 72	0	170	2682	-6.9	0.22	0
45	SLU 73	0	216	3057	-8.71	0.25	0
45	SLU 74	0	216	3057	-8.71	0.25	0
45	SLU 75	0	216	3057	-8.71	0.25	0
45	SLU 76	0	216	3057	-8.71	0.25	0
45	SLU 77	0	216	3057	-8.71	0.25	0
45	SLU 78	0	216	3057	-8.71	0.25	0
45	SLU 79	0	216	3057	-8.71	0.25	0
45	SLU 80	0	216	3057	-8.71	0.25	0
45	SLU 81	0	235	3218	-9.48	0.26	0
45	SLU 82	0	235	3218	-9.48	0.26	0
45	SLU 83	0	235	3218	-9.48	0.26	0
45	SLU 84	0	235	3218	-9.48	0.26	0
45	SLE RA 1	0	125	2017	-5.09	0.17	0
45	SLE RA 2	0	125	2017	-5.09	0.17	0
45	SLE RA 3	0	125	2017	-5.09	0.17	0
45	SLE RA 4	0	125	2017	-5.09	0.17	0
45	SLE RA 5	0	125	2017	-5.09	0.17	0
45	SLE RA 6	0	125	2017	-5.09	0.17	0
45	SLE RA 7	0	125	2017	-5.09	0.17	0
45	SLE RA 8	0	125	2017	-5.09	0.17	0
45	SLE RA 9	0	125	2017	-5.09	0.17	0
45	SLE RA 10	0	156	2267	-6.3	0.19	0
45	SLE RA 11	0	156	2267	-6.3	0.19	0
45	SLE RA 12	0	156	2267	-6.3	0.19	0
45	SLE RA 13	0	156	2267	-6.3	0.19	0
45	SLE RA 14	0	156	2267	-6.3	0.19	0
45	SLE RA 15	0	156	2267	-6.3	0.19	0
45	SLE RA 16	0	156	2267	-6.3	0.19	0
45	SLE RA 17	0	156	2267	-6.3	0.19	0
45	SLE RA 18	0	169	2374	-6.82	0.19	0
45	SLE RA 19	0	169	2374	-6.82	0.19	0
45	SLE RA 20	0	169	2374	-6.82	0.19	0
45	SLE RA 21	0	169	2374	-6.82	0.19	0
45	SLE FR 1	0	125	2017	-5.09	0.17	0
45	SLE FR 2	0	125	2017	-5.09	0.17	0
45	SLE FR 3	0	125	2017	-5.09	0.17	0
45	SLE FR 4	0	138	2124	-5.61	0.17	0
45	SLE FR 5	0	138	2124	-5.61	0.17	0
45	SLE FR 6	0	147	2196	-5.95	0.18	0
45	SLE QP 1	0	125	2017	-5.09	0.17	0
45	SLE QP 2	0	138	2124	-5.61	0.17	0
45	SLD 1	33	128	2215	-5.16	23.43	0.01
45	SLD 2	33	128	2215	-5.16	23.43	0.01
45	SLD 3	27	-40	2180	1.84	29.6	0.01
45	SLD 4	27	-40	2180	1.84	29.6	0.01
45	SLD 5	19	391	2205	-16.1	-2.22	0
45	SLD 6	19	391	2205	-16.1	-2.22	0
45	SLD 7	-1	-170	2088	7.25	18.37	0.01
45	SLD 8	-1	-170	2088	7.25	18.37	0.01
45	SLD 9	1	447	2161	-18.47	-18.03	-0.01
45	SLD 10	1	447	2161	-18.47	-18.03	-0.01
45	SLD 11	-19	-114	2044	4.89	2.57	0
45	SLD 12	-19	-114	2044	4.89	2.57	0
45	SLD 13	-27	317	2069	-13.06	-29.25	-0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
45	SLD 14	-27	317	2069	-13.06	-29.25	-0.01
45	SLD 15	-33	148	2033	-6.06	-23.08	-0.01
45	SLD 16	-33	148	2033	-6.06	-23.08	-0.01
45	SLV 1	80	111	2339	-4.38	56.71	0.02
45	SLV 2	80	111	2339	-4.38	56.71	0.02
45	SLV 3	64	-284	2256	12.07	72.49	0.03
45	SLV 4	64	-284	2256	12.07	72.49	0.03
45	SLV 5	47	729	2315	-30.18	-6.79	-0.01
45	SLV 6	47	729	2315	-30.18	-6.79	-0.01
45	SLV 7	-4	-587	2038	24.64	45.8	0.02
45	SLV 8	-4	-587	2038	24.64	45.8	0.02
45	SLV 9	4	864	2211	-35.86	-45.45	-0.02
45	SLV 10	4	864	2211	-35.86	-45.45	-0.02
45	SLV 11	-47	-452	1934	18.96	7.14	0.01
45	SLV 12	-47	-452	1934	18.96	7.14	0.01
45	SLV 13	-64	561	1993	-23.29	-72.14	-0.03
45	SLV 14	-64	561	1993	-23.29	-72.14	-0.03
45	SLV 15	-79	166	1910	-6.84	-56.36	-0.02
45	SLV 16	-79	166	1910	-6.84	-56.36	-0.02
46	SLU 1	0	0	1295	-0.02	0	0
46	SLU 2	0	0	1295	-0.02	0	0
46	SLU 3	0	0	1295	-0.02	0	0
46	SLU 4	0	0	1295	-0.02	0	0
46	SLU 5	0	0	1295	-0.02	0	0
46	SLU 6	0	0	1295	-0.02	0	0
46	SLU 7	0	0	1295	-0.02	0	0
46	SLU 8	0	0	1295	-0.02	0	0
46	SLU 9	0	0	1295	-0.02	0	0
46	SLU 10	0	0	1923	-0.02	0	0
46	SLU 11	0	0	1923	-0.02	0	0
46	SLU 12	0	0	1923	-0.02	0	0
46	SLU 13	0	0	1923	-0.02	0	0
46	SLU 14	0	0	1923	-0.02	0	0
46	SLU 15	0	0	1923	-0.02	0	0
46	SLU 16	0	0	1923	-0.02	0	0
46	SLU 17	0	0	1923	-0.02	0	0
46	SLU 18	0	0	2193	-0.01	0	0
46	SLU 19	0	0	2193	-0.01	0	0
46	SLU 20	0	0	2193	-0.01	0	0
46	SLU 21	0	0	2193	-0.01	0	0
46	SLU 22	0	0	1596	-0.02	0	0
46	SLU 23	0	0	1596	-0.02	0	0
46	SLU 24	0	0	1596	-0.02	0	0
46	SLU 25	0	0	1596	-0.02	0	0
46	SLU 26	0	0	1596	-0.02	0	0
46	SLU 27	0	0	1596	-0.02	0	0
46	SLU 28	0	0	1596	-0.02	0	0
46	SLU 29	0	0	1596	-0.02	0	0
46	SLU 30	0	0	1596	-0.02	0	0
46	SLU 31	0	0	2225	-0.01	0	0
46	SLU 32	0	0	2225	-0.01	0	0
46	SLU 33	0	0	2225	-0.01	0	0
46	SLU 34	0	0	2225	-0.01	0	0
46	SLU 35	0	0	2225	-0.01	0	0
46	SLU 36	0	0	2225	-0.01	0	0
46	SLU 37	0	0	2225	-0.01	0	0
46	SLU 38	0	0	2225	-0.01	0	0
46	SLU 39	0	0	2494	-0.01	0	0
46	SLU 40	0	0	2494	-0.01	0	0
46	SLU 41	0	0	2494	-0.01	0	0
46	SLU 42	0	0	2494	-0.01	0	0
46	SLU 43	0	0	1579	-0.03	0	0
46	SLU 44	0	0	1579	-0.03	0	0
46	SLU 45	0	0	1579	-0.03	0	0
46	SLU 46	0	0	1579	-0.03	0	0
46	SLU 47	0	0	1579	-0.03	0	0
46	SLU 48	0	0	1579	-0.03	0	0
46	SLU 49	0	0	1579	-0.03	0	0
46	SLU 50	0	0	1579	-0.03	0	0
46	SLU 51	0	0	1579	-0.03	0	0
46	SLU 52	0	0	2208	-0.02	0	0
46	SLU 53	0	0	2208	-0.02	0	0
46	SLU 54	0	0	2208	-0.02	0	0
46	SLU 55	0	0	2208	-0.02	0	0
46	SLU 56	0	0	2208	-0.02	0	0
46	SLU 57	0	0	2208	-0.02	0	0
46	SLU 58	0	0	2208	-0.02	0	0
46	SLU 59	0	0	2208	-0.02	0	0
46	SLU 60	0	0	2478	-0.02	0	0
46	SLU 61	0	0	2478	-0.02	0	0
46	SLU 62	0	0	2478	-0.02	0	0
46	SLU 63	0	0	2478	-0.02	0	0
46	SLU 64	0	0	1881	-0.03	0	0
46	SLU 65	0	0	1881	-0.03	0	0
46	SLU 66	0	0	1881	-0.03	0	0
46	SLU 67	0	0	1881	-0.03	0	0
46	SLU 68	0	0	1881	-0.03	0	0
46	SLU 69	0	0	1881	-0.03	0	0
46	SLU 70	0	0	1881	-0.03	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
46	SLU 71	0	0	1881	-0.03	0	0
46	SLU 72	0	0	1881	-0.03	0	0
46	SLU 73	0	0	2510	-0.02	0	0
46	SLU 74	0	0	2510	-0.02	0	0
46	SLU 75	0	0	2510	-0.02	0	0
46	SLU 76	0	0	2510	-0.02	0	0
46	SLU 77	0	0	2510	-0.02	0	0
46	SLU 78	0	0	2510	-0.02	0	0
46	SLU 79	0	0	2510	-0.02	0	0
46	SLU 80	0	0	2510	-0.02	0	0
46	SLU 81	0	0	2779	-0.02	0	0
46	SLU 82	0	0	2779	-0.02	0	0
46	SLU 83	0	0	2779	-0.02	0	0
46	SLU 84	0	0	2779	-0.02	0	0
46	SLE RA 1	0	0	1381	-0.02	0	0
46	SLE RA 2	0	0	1381	-0.02	0	0
46	SLE RA 3	0	0	1381	-0.02	0	0
46	SLE RA 4	0	0	1381	-0.02	0	0
46	SLE RA 5	0	0	1381	-0.02	0	0
46	SLE RA 6	0	0	1381	-0.02	0	0
46	SLE RA 7	0	0	1381	-0.02	0	0
46	SLE RA 8	0	0	1381	-0.02	0	0
46	SLE RA 9	0	0	1381	-0.02	0	0
46	SLE RA 10	0	0	1800	-0.02	0	0
46	SLE RA 11	0	0	1800	-0.02	0	0
46	SLE RA 12	0	0	1800	-0.02	0	0
46	SLE RA 13	0	0	1800	-0.02	0	0
46	SLE RA 14	0	0	1800	-0.02	0	0
46	SLE RA 15	0	0	1800	-0.02	0	0
46	SLE RA 16	0	0	1800	-0.02	0	0
46	SLE RA 17	0	0	1800	-0.02	0	0
46	SLE RA 18	0	0	1980	-0.02	0	0
46	SLE RA 19	0	0	1980	-0.02	0	0
46	SLE RA 20	0	0	1980	-0.02	0	0
46	SLE RA 21	0	0	1980	-0.02	0	0
46	SLE FR 1	0	0	1381	-0.02	0	0
46	SLE FR 2	0	0	1381	-0.02	0	0
46	SLE FR 3	0	0	1381	-0.02	0	0
46	SLE FR 4	0	0	1560	-0.02	0	0
46	SLE FR 5	0	0	1560	-0.02	0	0
46	SLE FR 6	0	0	1680	-0.02	0	0
46	SLE QP 1	0	0	1381	-0.02	0	0
46	SLE QP 2	0	0	1560	-0.02	0	0
46	SLD 1	-5	-81	1542	-5.05	7.79	-0.08
46	SLD 2	-5	-81	1542	-5.05	7.79	-0.08
46	SLD 3	-7	155	1612	9.39	10.51	-0.11
46	SLD 4	-7	155	1612	9.39	10.51	-0.11
46	SLD 5	1	-383	1449	-23.42	-1.78	0.02
46	SLD 6	1	-383	1449	-23.42	-1.78	0.02
46	SLD 7	-4	405	1682	24.69	7.27	-0.07
46	SLD 8	-4	405	1682	24.69	7.27	-0.07
46	SLD 9	4	-405	1439	-24.73	-7.27	0.07
46	SLD 10	4	-405	1439	-24.73	-7.27	0.07
46	SLD 11	-1	383	1672	23.38	1.78	-0.02
46	SLD 12	-1	383	1672	23.38	1.78	-0.02
46	SLD 13	7	-155	1509	-9.42	-10.51	0.11
46	SLD 14	7	-155	1509	-9.42	-10.51	0.11
46	SLD 15	5	81	1579	5.01	-7.79	0.08
46	SLD 16	5	81	1579	5.01	-7.79	0.08
46	SLV 1	-13	-209	1513	-12.92	19.84	-0.19
46	SLV 2	-13	-209	1513	-12.92	19.84	-0.19
46	SLV 3	-17	397	1693	24.11	26.79	-0.26
46	SLV 4	-17	397	1693	24.11	26.79	-0.26
46	SLV 5	2	-982	1274	-60.05	-4.6	0.05
46	SLV 6	2	-982	1274	-60.05	-4.6	0.05
46	SLV 7	-11	1039	1873	63.38	18.58	-0.18
46	SLV 8	-11	1039	1873	63.38	18.58	-0.18
46	SLV 9	11	-1039	1248	-63.41	-18.58	0.18
46	SLV 10	11	-1039	1248	-63.41	-18.58	0.18
46	SLV 11	-2	982	1847	60.01	4.6	-0.05
46	SLV 12	-2	982	1847	60.01	4.6	-0.05
46	SLV 13	17	-397	1428	-24.15	-26.79	0.26
46	SLV 14	17	-397	1428	-24.15	-26.79	0.26
46	SLV 15	13	209	1608	12.88	-19.84	0.19
46	SLV 16	13	209	1608	12.88	-19.84	0.19
47	SLU 1	0	192	1553	-7.5	-0.14	0
47	SLU 2	0	192	1553	-7.5	-0.14	0
47	SLU 3	0	192	1553	-7.5	-0.14	0
47	SLU 4	0	192	1553	-7.5	-0.14	0
47	SLU 5	0	192	1553	-7.5	-0.14	0
47	SLU 6	0	192	1553	-7.5	-0.14	0
47	SLU 7	0	192	1553	-7.5	-0.14	0
47	SLU 8	0	192	1553	-7.5	-0.14	0
47	SLU 9	0	192	1553	-7.5	-0.14	0
47	SLU 10	0	269	1832	-10.43	-0.2	0
47	SLU 11	0	269	1832	-10.43	-0.2	0
47	SLU 12	0	269	1832	-10.43	-0.2	0
47	SLU 13	0	269	1832	-10.43	-0.2	0
47	SLU 14	0	269	1832	-10.43	-0.2	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
47	SLU 15	0	269	1832	-10.43	-0.2	0
47	SLU 16	0	269	1832	-10.43	-0.2	0
47	SLU 17	0	269	1832	-10.43	-0.2	0
47	SLU 18	0	302	1951	-11.68	-0.22	0
47	SLU 19	0	302	1951	-11.68	-0.22	0
47	SLU 20	0	302	1951	-11.68	-0.22	0
47	SLU 21	0	302	1951	-11.68	-0.22	0
47	SLU 22	0	230	1701	-8.94	-0.18	0
47	SLU 23	0	230	1701	-8.94	-0.18	0
47	SLU 24	0	230	1701	-8.94	-0.18	0
47	SLU 25	0	230	1701	-8.94	-0.18	0
47	SLU 26	0	230	1701	-8.94	-0.18	0
47	SLU 27	0	230	1701	-8.94	-0.18	0
47	SLU 28	0	230	1701	-8.94	-0.18	0
47	SLU 29	0	230	1701	-8.94	-0.18	0
47	SLU 30	0	230	1701	-8.94	-0.18	0
47	SLU 31	0	307	1980	-11.87	-0.23	0
47	SLU 32	0	307	1980	-11.87	-0.23	0
47	SLU 33	0	307	1980	-11.87	-0.23	0
47	SLU 34	0	307	1980	-11.87	-0.23	0
47	SLU 35	0	307	1980	-11.87	-0.23	0
47	SLU 36	0	307	1980	-11.87	-0.23	0
47	SLU 37	0	307	1980	-11.87	-0.23	0
47	SLU 38	0	307	1980	-11.87	-0.23	0
47	SLU 39	0	340	2099	-13.12	-0.25	0
47	SLU 40	0	340	2099	-13.12	-0.25	0
47	SLU 41	0	340	2099	-13.12	-0.25	0
47	SLU 42	0	340	2099	-13.12	-0.25	0
47	SLU 43	0	237	1969	-9.26	-0.18	0
47	SLU 44	0	237	1969	-9.26	-0.18	0
47	SLU 45	0	237	1969	-9.26	-0.18	0
47	SLU 46	0	237	1969	-9.26	-0.18	0
47	SLU 47	0	237	1969	-9.26	-0.18	0
47	SLU 48	0	237	1969	-9.26	-0.18	0
47	SLU 49	0	237	1969	-9.26	-0.18	0
47	SLU 50	0	237	1969	-9.26	-0.18	0
47	SLU 51	0	237	1969	-9.26	-0.18	0
47	SLU 52	0	314	2247	-12.19	-0.23	0
47	SLU 53	0	314	2247	-12.19	-0.23	0
47	SLU 54	0	314	2247	-12.19	-0.23	0
47	SLU 55	0	314	2247	-12.19	-0.23	0
47	SLU 56	0	314	2247	-12.19	-0.23	0
47	SLU 57	0	314	2247	-12.19	-0.23	0
47	SLU 58	0	314	2247	-12.19	-0.23	0
47	SLU 59	0	314	2247	-12.19	-0.23	0
47	SLU 60	0	346	2367	-13.44	-0.26	0
47	SLU 61	0	346	2367	-13.44	-0.26	0
47	SLU 62	0	346	2367	-13.44	-0.26	0
47	SLU 63	0	346	2367	-13.44	-0.26	0
47	SLU 64	0	275	2117	-10.7	-0.21	0
47	SLU 65	0	275	2117	-10.7	-0.21	0
47	SLU 66	0	275	2117	-10.7	-0.21	0
47	SLU 67	0	275	2117	-10.7	-0.21	0
47	SLU 68	0	275	2117	-10.7	-0.21	0
47	SLU 69	0	275	2117	-10.7	-0.21	0
47	SLU 70	0	275	2117	-10.7	-0.21	0
47	SLU 71	0	275	2117	-10.7	-0.21	0
47	SLU 72	0	275	2117	-10.7	-0.21	0
47	SLU 73	0	351	2395	-13.62	-0.26	0
47	SLU 74	0	351	2395	-13.62	-0.26	0
47	SLU 75	0	351	2395	-13.62	-0.26	0
47	SLU 76	0	351	2395	-13.62	-0.26	0
47	SLU 77	0	351	2395	-13.62	-0.26	0
47	SLU 78	0	351	2395	-13.62	-0.26	0
47	SLU 79	0	351	2395	-13.62	-0.26	0
47	SLU 80	0	351	2395	-13.62	-0.26	0
47	SLU 81	0	384	2514	-14.88	-0.29	0
47	SLU 82	0	384	2514	-14.88	-0.29	0
47	SLU 83	0	384	2514	-14.88	-0.29	0
47	SLU 84	0	384	2514	-14.88	-0.29	0
47	SLE RA 1	0	203	1596	-7.92	-0.15	0
47	SLE RA 2	0	203	1596	-7.92	-0.15	0
47	SLE RA 3	0	203	1596	-7.92	-0.15	0
47	SLE RA 4	0	203	1596	-7.92	-0.15	0
47	SLE RA 5	0	203	1596	-7.92	-0.15	0
47	SLE RA 6	0	203	1596	-7.92	-0.15	0
47	SLE RA 7	0	203	1596	-7.92	-0.15	0
47	SLE RA 8	0	203	1596	-7.92	-0.15	0
47	SLE RA 9	0	203	1596	-7.92	-0.15	0
47	SLE RA 10	0	254	1781	-9.86	-0.19	0
47	SLE RA 11	0	254	1781	-9.86	-0.19	0
47	SLE RA 12	0	254	1781	-9.86	-0.19	0
47	SLE RA 13	0	254	1781	-9.86	-0.19	0
47	SLE RA 14	0	254	1781	-9.86	-0.19	0
47	SLE RA 15	0	254	1781	-9.86	-0.19	0
47	SLE RA 16	0	254	1781	-9.86	-0.19	0
47	SLE RA 17	0	254	1781	-9.86	-0.19	0
47	SLE RA 18	0	276	1861	-10.7	-0.21	0
47	SLE RA 19	0	276	1861	-10.7	-0.21	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
47	SLE RA 20	0	276	1861	-10.7	-0.21	0
47	SLE RA 21	0	276	1861	-10.7	-0.21	0
47	SLE FR 1	0	203	1596	-7.92	-0.15	0
47	SLE FR 2	0	203	1596	-7.92	-0.15	0
47	SLE FR 3	0	203	1596	-7.92	-0.15	0
47	SLE FR 4	0	225	1675	-8.75	-0.17	0
47	SLE FR 5	0	225	1675	-8.75	-0.17	0
47	SLE FR 6	0	240	1728	-9.31	-0.18	0
47	SLE QP 1	0	203	1596	-7.92	-0.15	0
47	SLE QP 2	0	225	1675	-8.75	-0.17	0
47	SLD 1	40	227	1624	-8.81	35.75	0.43
47	SLD 2	40	227	1624	-8.81	35.75	0.43
47	SLD 3	30	60	1586	-2.45	26.51	0.33
47	SLD 4	30	60	1586	-2.45	26.51	0.33
47	SLD 5	27	478	1717	-18.4	24.63	0.29
47	SLD 6	27	478	1717	-18.4	24.63	0.29
47	SLD 7	-6	-77	1592	2.77	-6.18	-0.06
47	SLD 8	-6	-77	1592	2.77	-6.18	-0.06
47	SLD 9	5	527	1759	-20.27	5.85	0.06
47	SLD 10	5	527	1759	-20.27	5.85	0.06
47	SLD 11	-27	-28	1634	0.9	-24.96	-0.29
47	SLD 12	-27	-28	1634	0.9	-24.96	-0.29
47	SLD 13	-30	390	1764	-15.05	-26.85	-0.33
47	SLD 14	-30	390	1764	-15.05	-26.85	-0.33
47	SLD 15	-40	223	1727	-8.7	-36.09	-0.43
47	SLD 16	-40	223	1727	-8.7	-36.09	-0.43
47	SLV 1	98	228	1552	-8.87	88.73	1.06
47	SLV 2	98	228	1552	-8.87	88.73	1.06
47	SLV 3	74	-163	1463	6.06	65.19	0.79
47	SLV 4	74	-163	1463	6.06	65.19	0.79
47	SLV 5	67	820	1774	-31.43	62.2	0.71
47	SLV 6	67	820	1774	-31.43	62.2	0.71
47	SLV 7	-15	-486	1476	18.34	-16.26	-0.16
47	SLV 8	-15	-486	1476	18.34	-16.26	-0.16
47	SLV 9	15	936	1874	-35.84	15.92	0.16
47	SLV 10	15	936	1874	-35.84	15.92	0.16
47	SLV 11	-67	-370	1577	13.93	-62.54	-0.71
47	SLV 12	-67	-370	1577	13.93	-62.54	-0.71
47	SLV 13	-74	613	1887	-23.56	-65.53	-0.8
47	SLV 14	-74	613	1887	-23.56	-65.53	-0.8
47	SLV 15	-98	222	1798	-8.63	-89.06	-1.06
47	SLV 16	-98	222	1798	-8.63	-89.06	-1.06
48	SLU 1	0	106	1980	-4.25	0.22	0
48	SLU 2	0	106	1980	-4.25	0.22	0
48	SLU 3	0	106	1980	-4.25	0.22	0
48	SLU 4	0	106	1980	-4.25	0.22	0
48	SLU 5	0	106	1980	-4.25	0.22	0
48	SLU 6	0	106	1980	-4.25	0.22	0
48	SLU 7	0	106	1980	-4.25	0.22	0
48	SLU 8	0	106	1980	-4.25	0.22	0
48	SLU 9	0	106	1980	-4.25	0.22	0
48	SLU 10	0	148	2373	-5.88	0.28	0
48	SLU 11	0	148	2373	-5.88	0.28	0
48	SLU 12	0	148	2373	-5.88	0.28	0
48	SLU 13	0	148	2373	-5.88	0.28	0
48	SLU 14	0	148	2373	-5.88	0.28	0
48	SLU 15	0	148	2373	-5.88	0.28	0
48	SLU 16	0	148	2373	-5.88	0.28	0
48	SLU 17	0	148	2373	-5.88	0.28	0
48	SLU 18	0	166	2541	-6.58	0.31	0
48	SLU 19	0	166	2541	-6.58	0.31	0
48	SLU 20	0	166	2541	-6.58	0.31	0
48	SLU 21	0	166	2541	-6.58	0.31	0
48	SLU 22	0	130	2198	-5.19	0.27	0
48	SLU 23	0	130	2198	-5.19	0.27	0
48	SLU 24	0	130	2198	-5.19	0.27	0
48	SLU 25	0	130	2198	-5.19	0.27	0
48	SLU 26	0	130	2198	-5.19	0.27	0
48	SLU 27	0	130	2198	-5.19	0.27	0
48	SLU 28	0	130	2198	-5.19	0.27	0
48	SLU 29	0	130	2198	-5.19	0.27	0
48	SLU 30	0	130	2198	-5.19	0.27	0
48	SLU 31	0	172	2590	-6.82	0.33	0
48	SLU 32	0	172	2590	-6.82	0.33	0
48	SLU 33	0	172	2590	-6.82	0.33	0
48	SLU 34	0	172	2590	-6.82	0.33	0
48	SLU 35	0	172	2590	-6.82	0.33	0
48	SLU 36	0	172	2590	-6.82	0.33	0
48	SLU 37	0	172	2590	-6.82	0.33	0
48	SLU 38	0	172	2590	-6.82	0.33	0
48	SLU 39	0	190	2758	-7.52	0.35	0
48	SLU 40	0	190	2758	-7.52	0.35	0
48	SLU 41	0	190	2758	-7.52	0.35	0
48	SLU 42	0	190	2758	-7.52	0.35	0
48	SLU 43	0	130	2500	-5.2	0.28	0
48	SLU 44	0	130	2500	-5.2	0.28	0
48	SLU 45	0	130	2500	-5.2	0.28	0
48	SLU 46	0	130	2500	-5.2	0.28	0
48	SLU 47	0	130	2500	-5.2	0.28	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
48	SLU 48	0	130	2500	-5.2	0.28	0
48	SLU 49	0	130	2500	-5.2	0.28	0
48	SLU 50	0	130	2500	-5.2	0.28	0
48	SLU 51	0	130	2500	-5.2	0.28	0
48	SLU 52	0	172	2892	-6.83	0.33	0
48	SLU 53	0	172	2892	-6.83	0.33	0
48	SLU 54	0	172	2892	-6.83	0.33	0
48	SLU 55	0	172	2892	-6.83	0.33	0
48	SLU 56	0	172	2892	-6.83	0.33	0
48	SLU 57	0	172	2892	-6.83	0.33	0
48	SLU 58	0	172	2892	-6.83	0.33	0
48	SLU 59	0	172	2892	-6.83	0.33	0
48	SLU 60	0	190	3060	-7.53	0.36	0
48	SLU 61	0	190	3060	-7.53	0.36	0
48	SLU 62	0	190	3060	-7.53	0.36	0
48	SLU 63	0	190	3060	-7.53	0.36	0
48	SLU 64	0	154	2718	-6.14	0.32	0
48	SLU 65	0	154	2718	-6.14	0.32	0
48	SLU 66	0	154	2718	-6.14	0.32	0
48	SLU 67	0	154	2718	-6.14	0.32	0
48	SLU 68	0	154	2718	-6.14	0.32	0
48	SLU 69	0	154	2718	-6.14	0.32	0
48	SLU 70	0	154	2718	-6.14	0.32	0
48	SLU 71	0	154	2718	-6.14	0.32	0
48	SLU 72	0	154	2718	-6.14	0.32	0
48	SLU 73	0	196	3110	-7.77	0.38	0
48	SLU 74	0	196	3110	-7.77	0.38	0
48	SLU 75	0	196	3110	-7.77	0.38	0
48	SLU 76	0	196	3110	-7.77	0.38	0
48	SLU 77	0	196	3110	-7.77	0.38	0
48	SLU 78	0	196	3110	-7.77	0.38	0
48	SLU 79	0	196	3110	-7.77	0.38	0
48	SLU 80	0	196	3110	-7.77	0.38	0
48	SLU 81	0	214	3278	-8.47	0.4	0
48	SLU 82	0	214	3278	-8.47	0.4	0
48	SLU 83	0	214	3278	-8.47	0.4	0
48	SLU 84	0	214	3278	-8.47	0.4	0
48	SLE RA 1	0	113	2043	-4.52	0.24	0
48	SLE RA 2	0	113	2043	-4.52	0.24	0
48	SLE RA 3	0	113	2043	-4.52	0.24	0
48	SLE RA 4	0	113	2043	-4.52	0.24	0
48	SLE RA 5	0	113	2043	-4.52	0.24	0
48	SLE RA 6	0	113	2043	-4.52	0.24	0
48	SLE RA 7	0	113	2043	-4.52	0.24	0
48	SLE RA 8	0	113	2043	-4.52	0.24	0
48	SLE RA 9	0	113	2043	-4.52	0.24	0
48	SLE RA 10	0	141	2304	-5.6	0.28	0
48	SLE RA 11	0	141	2304	-5.6	0.28	0
48	SLE RA 12	0	141	2304	-5.6	0.28	0
48	SLE RA 13	0	141	2304	-5.6	0.28	0
48	SLE RA 14	0	141	2304	-5.6	0.28	0
48	SLE RA 15	0	141	2304	-5.6	0.28	0
48	SLE RA 16	0	141	2304	-5.6	0.28	0
48	SLE RA 17	0	141	2304	-5.6	0.28	0
48	SLE RA 18	0	153	2416	-6.07	0.29	0
48	SLE RA 19	0	153	2416	-6.07	0.29	0
48	SLE RA 20	0	153	2416	-6.07	0.29	0
48	SLE RA 21	0	153	2416	-6.07	0.29	0
48	SLE FR 1	0	113	2043	-4.52	0.24	0
48	SLE FR 2	0	113	2043	-4.52	0.24	0
48	SLE FR 3	0	113	2043	-4.52	0.24	0
48	SLE FR 4	0	125	2155	-4.98	0.25	0
48	SLE FR 5	0	125	2155	-4.98	0.25	0
48	SLE FR 6	0	133	2229	-5.29	0.26	0
48	SLE QP 1	0	113	2043	-4.52	0.24	0
48	SLE QP 2	0	125	2155	-4.98	0.25	0
48	SLD 1	27	118	2247	-4.65	24.68	0.01
48	SLD 2	27	118	2247	-4.65	24.68	0.01
48	SLD 3	19	-52	2220	2.43	18.65	0.02
48	SLD 4	19	-52	2220	2.43	18.65	0.02
48	SLD 5	19	380	2224	-15.61	16.72	0
48	SLD 6	19	380	2224	-15.61	16.72	0
48	SLD 7	-6	-185	2133	7.97	-3.37	0.01
48	SLD 8	-6	-185	2133	7.97	-3.37	0.01
48	SLD 9	6	436	2177	-17.93	3.87	-0.01
48	SLD 10	6	436	2177	-17.93	3.87	-0.01
48	SLD 11	-19	-130	2085	5.65	-16.22	0
48	SLD 12	-19	-130	2085	5.65	-16.22	0
48	SLD 13	-19	302	2089	-12.39	-18.15	-0.02
48	SLD 14	-19	302	2089	-12.39	-18.15	-0.02
48	SLD 15	-26	133	2062	-5.32	-24.17	-0.01
48	SLD 16	-26	133	2062	-5.32	-24.17	-0.01
48	SLV 1	64	104	2374	-4.05	60.3	0.03
48	SLV 2	64	104	2374	-4.05	60.3	0.03
48	SLV 3	45	-294	2310	12.56	44.91	0.04
48	SLV 4	45	-294	2310	12.56	44.91	0.04
48	SLV 5	48	723	2319	-29.9	41.6	-0.01
48	SLV 6	48	723	2319	-29.9	41.6	-0.01
48	SLV 7	-16	-604	2103	25.48	-9.69	0.03



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
48	SLV 8	-16	-604	2103	25.48	-9.69	0.03
48	SLV 9	16	855	2206	-35.44	10.19	-0.03
48	SLV 10	16	855	2206	-35.44	10.19	-0.03
48	SLV 11	-48	-472	1991	19.94	-41.1	0.01
48	SLV 12	-48	-472	1991	19.94	-41.1	0.01
48	SLV 13	-45	544	1999	-22.52	-44.41	-0.04
48	SLV 14	-45	544	1999	-22.52	-44.41	-0.04
48	SLV 15	-64	146	1935	-5.91	-59.79	-0.03
48	SLV 16	-64	146	1935	-5.91	-59.79	-0.03
49	SLU 1	0	0	1281	-0.06	0	0
49	SLU 2	0	0	1281	-0.06	0	0
49	SLU 3	0	0	1281	-0.06	0	0
49	SLU 4	0	0	1281	-0.06	0	0
49	SLU 5	0	0	1281	-0.06	0	0
49	SLU 6	0	0	1281	-0.06	0	0
49	SLU 7	0	0	1281	-0.06	0	0
49	SLU 8	0	0	1281	-0.06	0	0
49	SLU 9	0	0	1281	-0.06	0	0
49	SLU 10	0	1	1917	-0.09	0	0
49	SLU 11	0	1	1917	-0.09	0	0
49	SLU 12	0	1	1917	-0.09	0	0
49	SLU 13	0	1	1917	-0.09	0	0
49	SLU 14	0	1	1917	-0.09	0	0
49	SLU 15	0	1	1917	-0.09	0	0
49	SLU 16	0	1	1917	-0.09	0	0
49	SLU 17	0	1	1917	-0.09	0	0
49	SLU 18	0	1	2189	-0.1	0	0
49	SLU 19	0	1	2189	-0.1	0	0
49	SLU 20	0	1	2189	-0.1	0	0
49	SLU 21	0	1	2189	-0.1	0	0
49	SLU 22	0	0	1584	-0.07	0	0
49	SLU 23	0	0	1584	-0.07	0	0
49	SLU 24	0	0	1584	-0.07	0	0
49	SLU 25	0	0	1584	-0.07	0	0
49	SLU 26	0	0	1584	-0.07	0	0
49	SLU 27	0	0	1584	-0.07	0	0
49	SLU 28	0	0	1584	-0.07	0	0
49	SLU 29	0	0	1584	-0.07	0	0
49	SLU 30	0	0	1584	-0.07	0	0
49	SLU 31	0	1	2220	-0.1	0	0
49	SLU 32	0	1	2220	-0.1	0	0
49	SLU 33	0	1	2220	-0.1	0	0
49	SLU 34	0	1	2220	-0.1	0	0
49	SLU 35	0	1	2220	-0.1	0	0
49	SLU 36	0	1	2220	-0.1	0	0
49	SLU 37	0	1	2220	-0.1	0	0
49	SLU 38	0	1	2220	-0.1	0	0
49	SLU 39	0	1	2492	-0.12	0	0
49	SLU 40	0	1	2492	-0.12	0	0
49	SLU 41	0	1	2492	-0.12	0	0
49	SLU 42	0	1	2492	-0.12	0	0
49	SLU 43	0	0	1562	-0.07	0	0
49	SLU 44	0	0	1562	-0.07	0	0
49	SLU 45	0	0	1562	-0.07	0	0
49	SLU 46	0	0	1562	-0.07	0	0
49	SLU 47	0	0	1562	-0.07	0	0
49	SLU 48	0	0	1562	-0.07	0	0
49	SLU 49	0	0	1562	-0.07	0	0
49	SLU 50	0	0	1562	-0.07	0	0
49	SLU 51	0	0	1562	-0.07	0	0
49	SLU 52	0	1	2197	-0.1	0	0
49	SLU 53	0	1	2197	-0.1	0	0
49	SLU 54	0	1	2197	-0.1	0	0
49	SLU 55	0	1	2197	-0.1	0	0
49	SLU 56	0	1	2197	-0.1	0	0
49	SLU 57	0	1	2197	-0.1	0	0
49	SLU 58	0	1	2197	-0.1	0	0
49	SLU 59	0	1	2197	-0.1	0	0
49	SLU 60	0	1	2470	-0.12	0	0
49	SLU 61	0	1	2470	-0.12	0	0
49	SLU 62	0	1	2470	-0.12	0	0
49	SLU 63	0	1	2470	-0.12	0	0
49	SLU 64	0	1	1865	-0.09	0	0
49	SLU 65	0	1	1865	-0.09	0	0
49	SLU 66	0	1	1865	-0.09	0	0
49	SLU 67	0	1	1865	-0.09	0	0
49	SLU 68	0	1	1865	-0.09	0	0
49	SLU 69	0	1	1865	-0.09	0	0
49	SLU 70	0	1	1865	-0.09	0	0
49	SLU 71	0	1	1865	-0.09	0	0
49	SLU 72	0	1	1865	-0.09	0	0
49	SLU 73	0	1	2500	-0.12	0	0
49	SLU 74	0	1	2500	-0.12	0	0
49	SLU 75	0	1	2500	-0.12	0	0
49	SLU 76	0	1	2500	-0.12	0	0
49	SLU 77	0	1	2500	-0.12	0	0
49	SLU 78	0	1	2500	-0.12	0	0
49	SLU 79	0	1	2500	-0.12	0	0
49	SLU 80	0	1	2500	-0.12	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
49	SLU 81	0	1	2773	-0.13	0	0
49	SLU 82	0	1	2773	-0.13	0	0
49	SLU 83	0	1	2773	-0.13	0	0
49	SLU 84	0	1	2773	-0.13	0	0
49	SLE RA 1	0	0	1368	-0.06	0	0
49	SLE RA 2	0	0	1368	-0.06	0	0
49	SLE RA 3	0	0	1368	-0.06	0	0
49	SLE RA 4	0	0	1368	-0.06	0	0
49	SLE RA 5	0	0	1368	-0.06	0	0
49	SLE RA 6	0	0	1368	-0.06	0	0
49	SLE RA 7	0	0	1368	-0.06	0	0
49	SLE RA 8	0	0	1368	-0.06	0	0
49	SLE RA 9	0	0	1368	-0.06	0	0
49	SLE RA 10	0	1	1792	-0.08	0	0
49	SLE RA 11	0	1	1792	-0.08	0	0
49	SLE RA 12	0	1	1792	-0.08	0	0
49	SLE RA 13	0	1	1792	-0.08	0	0
49	SLE RA 14	0	1	1792	-0.08	0	0
49	SLE RA 15	0	1	1792	-0.08	0	0
49	SLE RA 16	0	1	1792	-0.08	0	0
49	SLE RA 17	0	1	1792	-0.08	0	0
49	SLE RA 18	0	1	1973	-0.09	0	0
49	SLE RA 19	0	1	1973	-0.09	0	0
49	SLE RA 20	0	1	1973	-0.09	0	0
49	SLE RA 21	0	1	1973	-0.09	0	0
49	SLE FR 1	0	0	1368	-0.06	0	0
49	SLE FR 2	0	0	1368	-0.06	0	0
49	SLE FR 3	0	0	1368	-0.06	0	0
49	SLE FR 4	0	0	1550	-0.07	0	0
49	SLE FR 5	0	0	1550	-0.07	0	0
49	SLE FR 6	0	1	1671	-0.08	0	0
49	SLE QP 1	0	0	1368	-0.06	0	0
49	SLE QP 2	0	0	1550	-0.07	0	0
49	SLD 1	-5	5	1529	-5.73	8.89	0.07
49	SLD 2	-5	5	1529	-5.73	8.89	0.07
49	SLD 3	-6	-9	1611	10.45	6.37	0.09
49	SLD 4	-6	-9	1611	10.45	6.37	0.09
49	SLD 5	1	24	1419	-26.31	6.49	-0.01
49	SLD 6	1	24	1419	-26.31	6.49	-0.01
49	SLD 7	-4	-25	1692	27.62	-1.91	0.06
49	SLD 8	-4	-25	1692	27.62	-1.91	0.06
49	SLD 9	4	26	1407	-27.76	1.91	-0.06
49	SLD 10	4	26	1407	-27.76	1.91	-0.06
49	SLD 11	-1	-23	1680	26.16	-6.49	0.01
49	SLD 12	-1	-23	1680	26.16	-6.49	0.01
49	SLD 13	6	10	1488	-10.59	-6.37	-0.09
49	SLD 14	6	10	1488	-10.59	-6.37	-0.09
49	SLD 15	5	-4	1570	5.59	-8.89	-0.06
49	SLD 16	5	-4	1570	5.59	-8.89	-0.06
49	SLV 1	-12	13	1496	-14.59	22.64	0.16
49	SLV 2	-12	13	1496	-14.59	22.64	0.16
49	SLV 3	-16	-25	1706	26.91	16.18	0.21
49	SLV 4	-16	-25	1706	26.91	16.18	0.21
49	SLV 5	2	61	1215	-67.37	16.59	-0.03
49	SLV 6	2	61	1215	-67.37	16.59	-0.03
49	SLV 7	-11	-64	1915	70.97	-4.94	0.14
49	SLV 8	-11	-64	1915	70.97	-4.94	0.14
49	SLV 9	11	65	1184	-71.11	4.94	-0.14
49	SLV 10	11	65	1184	-71.11	4.94	-0.14
49	SLV 11	-2	-60	1884	67.23	-16.59	0.03
49	SLV 12	-2	-60	1884	67.23	-16.59	0.03
49	SLV 13	16	26	1393	-27.06	-16.19	-0.21
49	SLV 14	16	26	1393	-27.06	-16.19	-0.21
49	SLV 15	12	-12	1603	14.45	-22.65	-0.16
49	SLV 16	12	-12	1603	14.45	-22.65	-0.16
50	SLU 1	0	220	1702	-7.63	-0.21	0
50	SLU 2	0	220	1702	-7.63	-0.21	0
50	SLU 3	0	220	1702	-7.63	-0.21	0
50	SLU 4	0	220	1702	-7.63	-0.21	0
50	SLU 5	0	220	1702	-7.63	-0.21	0
50	SLU 6	0	220	1702	-7.63	-0.21	0
50	SLU 7	0	220	1702	-7.63	-0.21	0
50	SLU 8	0	220	1702	-7.63	-0.21	0
50	SLU 9	0	220	1702	-7.63	-0.21	0
50	SLU 10	0	301	2032	-10.52	-0.29	0
50	SLU 11	0	301	2032	-10.52	-0.29	0
50	SLU 12	0	301	2032	-10.52	-0.29	0
50	SLU 13	0	301	2032	-10.52	-0.29	0
50	SLU 14	0	301	2032	-10.52	-0.29	0
50	SLU 15	0	301	2032	-10.52	-0.29	0
50	SLU 16	0	301	2032	-10.52	-0.29	0
50	SLU 17	0	301	2032	-10.52	-0.29	0
50	SLU 18	0	336	2173	-11.75	-0.33	0
50	SLU 19	0	336	2173	-11.75	-0.33	0
50	SLU 20	0	336	2173	-11.75	-0.33	0
50	SLU 21	0	336	2173	-11.75	-0.33	0
50	SLU 22	0	261	1877	-9.09	-0.26	0
50	SLU 23	0	261	1877	-9.09	-0.26	0
50	SLU 24	0	261	1877	-9.09	-0.26	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
50	SLU 25	0	261	1877	-9.09	-0.26	0
50	SLU 26	0	261	1877	-9.09	-0.26	0
50	SLU 27	0	261	1877	-9.09	-0.26	0
50	SLU 28	0	261	1877	-9.09	-0.26	0
50	SLU 29	0	261	1877	-9.09	-0.26	0
50	SLU 30	0	261	1877	-9.09	-0.26	0
50	SLU 31	0	343	2207	-11.98	-0.34	0
50	SLU 32	0	343	2207	-11.98	-0.34	0
50	SLU 33	0	343	2207	-11.98	-0.34	0
50	SLU 34	0	343	2207	-11.98	-0.34	0
50	SLU 35	0	343	2207	-11.98	-0.34	0
50	SLU 36	0	343	2207	-11.98	-0.34	0
50	SLU 37	0	343	2207	-11.98	-0.34	0
50	SLU 38	0	343	2207	-11.98	-0.34	0
50	SLU 39	0	378	2348	-13.21	-0.38	0
50	SLU 40	0	378	2348	-13.21	-0.38	0
50	SLU 41	0	378	2348	-13.21	-0.38	0
50	SLU 42	0	378	2348	-13.21	-0.38	0
50	SLU 43	0	272	2153	-9.42	-0.25	0
50	SLU 44	0	272	2153	-9.42	-0.25	0
50	SLU 45	0	272	2153	-9.42	-0.25	0
50	SLU 46	0	272	2153	-9.42	-0.25	0
50	SLU 47	0	272	2153	-9.42	-0.25	0
50	SLU 48	0	272	2153	-9.42	-0.25	0
50	SLU 49	0	272	2153	-9.42	-0.25	0
50	SLU 50	0	272	2153	-9.42	-0.25	0
50	SLU 51	0	272	2153	-9.42	-0.25	0
50	SLU 52	0	353	2483	-12.31	-0.34	0
50	SLU 53	0	353	2483	-12.31	-0.34	0
50	SLU 54	0	353	2483	-12.31	-0.34	0
50	SLU 55	0	353	2483	-12.31	-0.34	0
50	SLU 56	0	353	2483	-12.31	-0.34	0
50	SLU 57	0	353	2483	-12.31	-0.34	0
50	SLU 58	0	353	2483	-12.31	-0.34	0
50	SLU 59	0	353	2483	-12.31	-0.34	0
50	SLU 60	0	388	2624	-13.54	-0.38	0
50	SLU 61	0	388	2624	-13.54	-0.38	0
50	SLU 62	0	388	2624	-13.54	-0.38	0
50	SLU 63	0	388	2624	-13.54	-0.38	0
50	SLU 64	0	313	2328	-10.88	-0.3	0
50	SLU 65	0	313	2328	-10.88	-0.3	0
50	SLU 66	0	313	2328	-10.88	-0.3	0
50	SLU 67	0	313	2328	-10.88	-0.3	0
50	SLU 68	0	313	2328	-10.88	-0.3	0
50	SLU 69	0	313	2328	-10.88	-0.3	0
50	SLU 70	0	313	2328	-10.88	-0.3	0
50	SLU 71	0	313	2328	-10.88	-0.3	0
50	SLU 72	0	313	2328	-10.88	-0.3	0
50	SLU 73	0	395	2658	-13.77	-0.39	0
50	SLU 74	0	395	2658	-13.77	-0.39	0
50	SLU 75	0	395	2658	-13.77	-0.39	0
50	SLU 76	0	395	2658	-13.77	-0.39	0
50	SLU 77	0	395	2658	-13.77	-0.39	0
50	SLU 78	0	395	2658	-13.77	-0.39	0
50	SLU 79	0	395	2658	-13.77	-0.39	0
50	SLU 80	0	395	2658	-13.77	-0.39	0
50	SLU 81	0	429	2799	-15	-0.43	0
50	SLU 82	0	429	2799	-15	-0.43	0
50	SLU 83	0	429	2799	-15	-0.43	0
50	SLU 84	0	429	2799	-15	-0.43	0
50	SLE RA 1	0	232	1752	-8.05	-0.22	0
50	SLE RA 2	0	232	1752	-8.05	-0.22	0
50	SLE RA 3	0	232	1752	-8.05	-0.22	0
50	SLE RA 4	0	232	1752	-8.05	-0.22	0
50	SLE RA 5	0	232	1752	-8.05	-0.22	0
50	SLE RA 6	0	232	1752	-8.05	-0.22	0
50	SLE RA 7	0	232	1752	-8.05	-0.22	0
50	SLE RA 8	0	232	1752	-8.05	-0.22	0
50	SLE RA 9	0	232	1752	-8.05	-0.22	0
50	SLE RA 10	0	286	1972	-9.97	-0.28	0
50	SLE RA 11	0	286	1972	-9.97	-0.28	0
50	SLE RA 12	0	286	1972	-9.97	-0.28	0
50	SLE RA 13	0	286	1972	-9.97	-0.28	0
50	SLE RA 14	0	286	1972	-9.97	-0.28	0
50	SLE RA 15	0	286	1972	-9.97	-0.28	0
50	SLE RA 16	0	286	1972	-9.97	-0.28	0
50	SLE RA 17	0	286	1972	-9.97	-0.28	0
50	SLE RA 18	0	309	2066	-10.8	-0.3	0
50	SLE RA 19	0	309	2066	-10.8	-0.3	0
50	SLE RA 20	0	309	2066	-10.8	-0.3	0
50	SLE RA 21	0	309	2066	-10.8	-0.3	0
50	SLE FR 1	0	232	1752	-8.05	-0.22	0
50	SLE FR 2	0	232	1752	-8.05	-0.22	0
50	SLE FR 3	0	232	1752	-8.05	-0.22	0
50	SLE FR 4	0	255	1847	-8.87	-0.25	0
50	SLE FR 5	0	255	1847	-8.87	-0.25	0
50	SLE FR 6	0	271	1909	-9.42	-0.26	0
50	SLE QP 1	0	232	1752	-8.05	-0.22	0
50	SLE QP 2	0	255	1847	-8.87	-0.25	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
50	SLD 1	20	255	1787	-8.91	29.74	0.2
50	SLD 2	20	255	1787	-8.91	29.74	0.2
50	SLD 3	32	92	1734	-2.43	19.79	0.31
50	SLD 4	32	92	1734	-2.43	19.79	0.31
50	SLD 5	-12	502	1909	-18.71	23.84	-0.1
50	SLD 6	-12	502	1909	-18.71	23.84	-0.1
50	SLD 7	28	-41	1733	2.88	-9.32	0.25
50	SLD 8	28	-41	1733	2.88	-9.32	0.25
50	SLD 9	-28	551	1960	-20.63	8.83	-0.25
50	SLD 10	-28	551	1960	-20.63	8.83	-0.25
50	SLD 11	12	8	1784	0.96	-24.33	0.1
50	SLD 12	12	8	1784	0.96	-24.33	0.1
50	SLD 13	-32	418	1959	-15.31	-20.29	-0.31
50	SLD 14	-32	418	1959	-15.31	-20.29	-0.31
50	SLD 15	-20	255	1906	-8.84	-30.24	-0.2
50	SLD 16	-20	255	1906	-8.84	-30.24	-0.2
50	SLV 1	47	254	1704	-8.95	74	0.48
50	SLV 2	47	254	1704	-8.95	74	0.48
50	SLV 3	78	-130	1579	6.29	48.6	0.75
50	SLV 4	78	-130	1579	6.29	48.6	0.75
50	SLV 5	-32	836	1994	-32.01	60.55	-0.26
50	SLV 6	-32	836	1994	-32.01	60.55	-0.26
50	SLV 7	70	-442	1576	18.79	-24.12	0.63
50	SLV 8	70	-442	1576	18.79	-24.12	0.63
50	SLV 9	-70	952	2117	-36.54	23.62	-0.64
50	SLV 10	-70	952	2117	-36.54	23.62	-0.64
50	SLV 11	32	-326	1699	14.27	-61.04	0.26
50	SLV 12	32	-326	1699	14.27	-61.04	0.26
50	SLV 13	-78	640	2114	-24.04	-49.1	-0.76
50	SLV 14	-78	640	2114	-24.04	-49.1	-0.76
50	SLV 15	-48	256	1989	-8.8	-74.5	-0.49
50	SLV 16	-48	256	1989	-8.8	-74.5	-0.49
51	SLU 1	0	96	2015	-3.81	0.36	0
51	SLU 2	0	96	2015	-3.81	0.36	0
51	SLU 3	0	96	2015	-3.81	0.36	0
51	SLU 4	0	96	2015	-3.81	0.36	0
51	SLU 5	0	96	2015	-3.81	0.36	0
51	SLU 6	0	96	2015	-3.81	0.36	0
51	SLU 7	0	96	2015	-3.81	0.36	0
51	SLU 8	0	96	2015	-3.81	0.36	0
51	SLU 9	0	96	2015	-3.81	0.36	0
51	SLU 10	0	135	2429	-5.3	0.46	0
51	SLU 11	0	135	2429	-5.3	0.46	0
51	SLU 12	0	135	2429	-5.3	0.46	0
51	SLU 13	0	135	2429	-5.3	0.46	0
51	SLU 14	0	135	2429	-5.3	0.46	0
51	SLU 15	0	135	2429	-5.3	0.46	0
51	SLU 16	0	135	2429	-5.3	0.46	0
51	SLU 17	0	135	2429	-5.3	0.46	0
51	SLU 18	0	152	2606	-5.93	0.51	0
51	SLU 19	0	152	2606	-5.93	0.51	0
51	SLU 20	0	152	2606	-5.93	0.51	0
51	SLU 21	0	152	2606	-5.93	0.51	0
51	SLU 22	0	120	2246	-4.73	0.43	0
51	SLU 23	0	120	2246	-4.73	0.43	0
51	SLU 24	0	120	2246	-4.73	0.43	0
51	SLU 25	0	120	2246	-4.73	0.43	0
51	SLU 26	0	120	2246	-4.73	0.43	0
51	SLU 27	0	120	2246	-4.73	0.43	0
51	SLU 28	0	120	2246	-4.73	0.43	0
51	SLU 29	0	120	2246	-4.73	0.43	0
51	SLU 30	0	120	2246	-4.73	0.43	0
51	SLU 31	0	159	2660	-6.21	0.54	0
51	SLU 32	0	159	2660	-6.21	0.54	0
51	SLU 33	0	159	2660	-6.21	0.54	0
51	SLU 34	0	159	2660	-6.21	0.54	0
51	SLU 35	0	159	2660	-6.21	0.54	0
51	SLU 36	0	159	2660	-6.21	0.54	0
51	SLU 37	0	159	2660	-6.21	0.54	0
51	SLU 38	0	159	2660	-6.21	0.54	0
51	SLU 39	0	175	2837	-6.85	0.59	0
51	SLU 40	0	175	2837	-6.85	0.59	0
51	SLU 41	0	175	2837	-6.85	0.59	0
51	SLU 42	0	175	2837	-6.85	0.59	0
51	SLU 43	0	117	2541	-4.64	0.43	0
51	SLU 44	0	117	2541	-4.64	0.43	0
51	SLU 45	0	117	2541	-4.64	0.43	0
51	SLU 46	0	117	2541	-4.64	0.43	0
51	SLU 47	0	117	2541	-4.64	0.43	0
51	SLU 48	0	117	2541	-4.64	0.43	0
51	SLU 49	0	117	2541	-4.64	0.43	0
51	SLU 50	0	117	2541	-4.64	0.43	0
51	SLU 51	0	117	2541	-4.64	0.43	0
51	SLU 52	0	156	2954	-6.13	0.54	0
51	SLU 53	0	156	2954	-6.13	0.54	0
51	SLU 54	0	156	2954	-6.13	0.54	0
51	SLU 55	0	156	2954	-6.13	0.54	0
51	SLU 56	0	156	2954	-6.13	0.54	0
51	SLU 57	0	156	2954	-6.13	0.54	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
51	SLU 58	0	156	2954	-6.13	0.54	0
51	SLU 59	0	156	2954	-6.13	0.54	0
51	SLU 60	0	172	3132	-6.76	0.59	0
51	SLU 61	0	172	3132	-6.76	0.59	0
51	SLU 62	0	172	3132	-6.76	0.59	0
51	SLU 63	0	172	3132	-6.76	0.59	0
51	SLU 64	0	141	2772	-5.56	0.51	0
51	SLU 65	0	141	2772	-5.56	0.51	0
51	SLU 66	0	141	2772	-5.56	0.51	0
51	SLU 67	0	141	2772	-5.56	0.51	0
51	SLU 68	0	141	2772	-5.56	0.51	0
51	SLU 69	0	141	2772	-5.56	0.51	0
51	SLU 70	0	141	2772	-5.56	0.51	0
51	SLU 71	0	141	2772	-5.56	0.51	0
51	SLU 72	0	141	2772	-5.56	0.51	0
51	SLU 73	0	180	3185	-7.04	0.62	0
51	SLU 74	0	180	3185	-7.04	0.62	0
51	SLU 75	0	180	3185	-7.04	0.62	0
51	SLU 76	0	180	3185	-7.04	0.62	0
51	SLU 77	0	180	3185	-7.04	0.62	0
51	SLU 78	0	180	3185	-7.04	0.62	0
51	SLU 79	0	180	3185	-7.04	0.62	0
51	SLU 80	0	180	3185	-7.04	0.62	0
51	SLU 81	0	196	3363	-7.68	0.67	0
51	SLU 82	0	196	3363	-7.68	0.67	0
51	SLU 83	0	196	3363	-7.68	0.67	0
51	SLU 84	0	196	3363	-7.68	0.67	0
51	SLE RA 1	0	103	2081	-4.07	0.38	0
51	SLE RA 2	0	103	2081	-4.07	0.38	0
51	SLE RA 3	0	103	2081	-4.07	0.38	0
51	SLE RA 4	0	103	2081	-4.07	0.38	0
51	SLE RA 5	0	103	2081	-4.07	0.38	0
51	SLE RA 6	0	103	2081	-4.07	0.38	0
51	SLE RA 7	0	103	2081	-4.07	0.38	0
51	SLE RA 8	0	103	2081	-4.07	0.38	0
51	SLE RA 9	0	103	2081	-4.07	0.38	0
51	SLE RA 10	0	129	2357	-5.06	0.45	0
51	SLE RA 11	0	129	2357	-5.06	0.45	0
51	SLE RA 12	0	129	2357	-5.06	0.45	0
51	SLE RA 13	0	129	2357	-5.06	0.45	0
51	SLE RA 14	0	129	2357	-5.06	0.45	0
51	SLE RA 15	0	129	2357	-5.06	0.45	0
51	SLE RA 16	0	129	2357	-5.06	0.45	0
51	SLE RA 17	0	129	2357	-5.06	0.45	0
51	SLE RA 18	0	140	2475	-5.49	0.48	0
51	SLE RA 19	0	140	2475	-5.49	0.48	0
51	SLE RA 20	0	140	2475	-5.49	0.48	0
51	SLE RA 21	0	140	2475	-5.49	0.48	0
51	SLE FR 1	0	103	2081	-4.07	0.38	0
51	SLE FR 2	0	103	2081	-4.07	0.38	0
51	SLE FR 3	0	103	2081	-4.07	0.38	0
51	SLE FR 4	0	114	2200	-4.5	0.41	0
51	SLE FR 5	0	114	2200	-4.5	0.41	0
51	SLE FR 6	0	122	2278	-4.78	0.43	0
51	SLE QP 1	0	103	2081	-4.07	0.38	0
51	SLE QP 2	0	114	2200	-4.5	0.41	0
51	SLD 1	-9	291	2309	-4.24	18.4	0.01
51	SLD 2	-9	291	2309	-4.24	18.4	0.01
51	SLD 3	-19	121	2288	2.85	12.44	0.02
51	SLD 4	-19	121	2288	2.85	12.44	0.02
51	SLD 5	12	426	2265	-15.17	14.85	0
51	SLD 6	12	426	2265	-15.17	14.85	0
51	SLD 7	-20	-142	2194	8.45	-5.02	0.02
51	SLD 8	-20	-142	2194	8.45	-5.02	0.02
51	SLD 9	21	371	2206	-17.45	5.84	-0.01
51	SLD 10	21	371	2206	-17.45	5.84	-0.01
51	SLD 11	-12	-197	2134	6.17	-14.03	0.01
51	SLD 12	-12	-197	2134	6.17	-14.03	0.01
51	SLD 13	19	108	2112	-11.84	-11.62	-0.02
51	SLD 14	19	108	2112	-11.84	-11.62	-0.02
51	SLD 15	9	-62	2090	-4.76	-17.58	-0.01
51	SLD 16	9	-62	2090	-4.76	-17.58	-0.01
51	SLV 1	-21	531	2461	-3.78	44.74	0.03
51	SLV 2	-21	531	2461	-3.78	44.74	0.03
51	SLV 3	-46	131	2410	12.85	29.51	0.04
51	SLV 4	-46	131	2410	12.85	29.51	0.04
51	SLV 5	31	846	2354	-29.51	36.8	-0.01
51	SLV 6	31	846	2354	-29.51	36.8	-0.01
51	SLV 7	-51	-487	2186	25.93	-13.95	0.04
51	SLV 8	-51	-487	2186	25.93	-13.95	0.04
51	SLV 9	51	716	2213	-34.93	14.77	-0.03
51	SLV 10	51	716	2213	-34.93	14.77	-0.03
51	SLV 11	-31	-617	2045	20.51	-35.99	0.01
51	SLV 12	-31	-617	2045	20.51	-35.99	0.01
51	SLV 13	46	97	1989	-21.85	-28.7	-0.04
51	SLV 14	46	97	1989	-21.85	-28.7	-0.04
51	SLV 15	21	-303	1938	-5.22	-43.92	-0.03
51	SLV 16	21	-303	1938	-5.22	-43.92	-0.03
52	SLU 1	0	0	1119	-0.07	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
52	SLU 2	0	0	1119	-0.07	0	0
52	SLU 3	0	0	1119	-0.07	0	0
52	SLU 4	0	0	1119	-0.07	0	0
52	SLU 5	0	0	1119	-0.07	0	0
52	SLU 6	0	0	1119	-0.07	0	0
52	SLU 7	0	0	1119	-0.07	0	0
52	SLU 8	0	0	1119	-0.07	0	0
52	SLU 9	0	0	1119	-0.07	0	0
52	SLU 10	0	0	1653	-0.11	0	0
52	SLU 11	0	0	1653	-0.11	0	0
52	SLU 12	0	0	1653	-0.11	0	0
52	SLU 13	0	0	1653	-0.11	0	0
52	SLU 14	0	0	1653	-0.11	0	0
52	SLU 15	0	0	1653	-0.11	0	0
52	SLU 16	0	0	1653	-0.11	0	0
52	SLU 17	0	0	1653	-0.11	0	0
52	SLU 18	0	1	1882	-0.13	0	0
52	SLU 19	0	1	1882	-0.13	0	0
52	SLU 20	0	1	1882	-0.13	0	0
52	SLU 21	0	1	1882	-0.13	0	0
52	SLU 22	0	0	1375	-0.09	-0.01	0
52	SLU 23	0	0	1375	-0.09	-0.01	0
52	SLU 24	0	0	1375	-0.09	-0.01	0
52	SLU 25	0	0	1375	-0.09	-0.01	0
52	SLU 26	0	0	1375	-0.09	-0.01	0
52	SLU 27	0	0	1375	-0.09	-0.01	0
52	SLU 28	0	0	1375	-0.09	-0.01	0
52	SLU 29	0	0	1375	-0.09	-0.01	0
52	SLU 30	0	0	1375	-0.09	-0.01	0
52	SLU 31	0	1	1908	-0.13	-0.01	0
52	SLU 32	0	1	1908	-0.13	-0.01	0
52	SLU 33	0	1	1908	-0.13	-0.01	0
52	SLU 34	0	1	1908	-0.13	-0.01	0
52	SLU 35	0	1	1908	-0.13	-0.01	0
52	SLU 36	0	1	1908	-0.13	-0.01	0
52	SLU 37	0	1	1908	-0.13	-0.01	0
52	SLU 38	0	1	1908	-0.13	-0.01	0
52	SLU 39	0	1	2137	-0.15	-0.01	0
52	SLU 40	0	1	2137	-0.15	-0.01	0
52	SLU 41	0	1	2137	-0.15	-0.01	0
52	SLU 42	0	1	2137	-0.15	-0.01	0
52	SLU 43	0	0	1368	-0.08	-0.01	0
52	SLU 44	0	0	1368	-0.08	-0.01	0
52	SLU 45	0	0	1368	-0.08	-0.01	0
52	SLU 46	0	0	1368	-0.08	-0.01	0
52	SLU 47	0	0	1368	-0.08	-0.01	0
52	SLU 48	0	0	1368	-0.08	-0.01	0
52	SLU 49	0	0	1368	-0.08	-0.01	0
52	SLU 50	0	0	1368	-0.08	-0.01	0
52	SLU 51	0	0	1368	-0.08	-0.01	0
52	SLU 52	0	0	1901	-0.13	-0.01	0
52	SLU 53	0	0	1901	-0.13	-0.01	0
52	SLU 54	0	0	1901	-0.13	-0.01	0
52	SLU 55	0	0	1901	-0.13	-0.01	0
52	SLU 56	0	0	1901	-0.13	-0.01	0
52	SLU 57	0	0	1901	-0.13	-0.01	0
52	SLU 58	0	0	1901	-0.13	-0.01	0
52	SLU 59	0	0	1901	-0.13	-0.01	0
52	SLU 60	0	1	2130	-0.15	-0.01	0
52	SLU 61	0	1	2130	-0.15	-0.01	0
52	SLU 62	0	1	2130	-0.15	-0.01	0
52	SLU 63	0	1	2130	-0.15	-0.01	0
52	SLU 64	0	0	1623	-0.1	-0.01	0
52	SLU 65	0	0	1623	-0.1	-0.01	0
52	SLU 66	0	0	1623	-0.1	-0.01	0
52	SLU 67	0	0	1623	-0.1	-0.01	0
52	SLU 68	0	0	1623	-0.1	-0.01	0
52	SLU 69	0	0	1623	-0.1	-0.01	0
52	SLU 70	0	0	1623	-0.1	-0.01	0
52	SLU 71	0	0	1623	-0.1	-0.01	0
52	SLU 72	0	0	1623	-0.1	-0.01	0
52	SLU 73	0	1	2157	-0.15	-0.01	0
52	SLU 74	0	1	2157	-0.15	-0.01	0
52	SLU 75	0	1	2157	-0.15	-0.01	0
52	SLU 76	0	1	2157	-0.15	-0.01	0
52	SLU 77	0	1	2157	-0.15	-0.01	0
52	SLU 78	0	1	2157	-0.15	-0.01	0
52	SLU 79	0	1	2157	-0.15	-0.01	0
52	SLU 80	0	1	2157	-0.15	-0.01	0
52	SLU 81	0	1	2385	-0.17	-0.01	0
52	SLU 82	0	1	2385	-0.17	-0.01	0
52	SLU 83	0	1	2385	-0.17	-0.01	0
52	SLU 84	0	1	2385	-0.17	-0.01	0
52	SLE RA 1	0	0	1192	-0.07	0	0
52	SLE RA 2	0	0	1192	-0.07	0	0
52	SLE RA 3	0	0	1192	-0.07	0	0
52	SLE RA 4	0	0	1192	-0.07	0	0
52	SLE RA 5	0	0	1192	-0.07	0	0
52	SLE RA 6	0	0	1192	-0.07	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
52	SLE RA 7	0	0	1192	-0.07	0	0
52	SLE RA 8	0	0	1192	-0.07	0	0
52	SLE RA 9	0	0	1192	-0.07	0	0
52	SLE RA 10	0	0	1548	-0.1	0	0
52	SLE RA 11	0	0	1548	-0.1	0	0
52	SLE RA 12	0	0	1548	-0.1	0	0
52	SLE RA 13	0	0	1548	-0.1	0	0
52	SLE RA 14	0	0	1548	-0.1	0	0
52	SLE RA 15	0	0	1548	-0.1	0	0
52	SLE RA 16	0	0	1548	-0.1	0	0
52	SLE RA 17	0	0	1548	-0.1	0	0
52	SLE RA 18	0	0	1701	-0.12	0	0
52	SLE RA 19	0	0	1701	-0.12	0	0
52	SLE RA 20	0	0	1701	-0.12	0	0
52	SLE RA 21	0	0	1701	-0.12	0	0
52	SLE FR 1	0	0	1192	-0.07	0	0
52	SLE FR 2	0	0	1192	-0.07	0	0
52	SLE FR 3	0	0	1192	-0.07	0	0
52	SLE FR 4	0	0	1345	-0.09	0	0
52	SLE FR 5	0	0	1345	-0.09	0	0
52	SLE FR 6	0	0	1446	-0.1	0	0
52	SLE QP 1	0	0	1192	-0.07	0	0
52	SLE QP 2	0	0	1345	-0.09	0	0
52	SLD 1	-3	4	1323	-6.05	6.35	0.09
52	SLD 2	-3	4	1323	-6.05	6.35	0.09
52	SLD 3	-4	-8	1411	10.95	4.25	0.12
52	SLD 4	-4	-8	1411	10.95	4.25	0.12
52	SLD 5	1	20	1204	-27.65	5.09	-0.01
52	SLD 6	1	20	1204	-27.65	5.09	-0.01
52	SLD 7	-3	-20	1499	28.99	-1.92	0.08
52	SLD 8	-3	-20	1499	28.99	-1.92	0.08
52	SLD 9	3	21	1191	-29.17	1.91	-0.08
52	SLD 10	3	21	1191	-29.17	1.91	-0.08
52	SLD 11	-1	-19	1486	27.47	-5.1	0.02
52	SLD 12	-1	-19	1486	27.47	-5.1	0.02
52	SLD 13	4	8	1279	-11.12	-4.26	-0.12
52	SLD 14	4	8	1279	-11.12	-4.26	-0.12
52	SLD 15	3	-4	1367	5.87	-6.36	-0.09
52	SLD 16	3	-4	1367	5.87	-6.36	-0.09
52	SLV 1	-7	11	1287	-15.37	16.17	0.23
52	SLV 2	-7	11	1287	-15.37	16.17	0.23
52	SLV 3	-10	-20	1513	28.22	10.79	0.3
52	SLV 4	-10	-20	1513	28.22	10.79	0.3
52	SLV 5	3	50	984	-70.79	13.01	-0.04
52	SLV 6	3	50	984	-70.79	13.01	-0.04
52	SLV 7	-8	-52	1739	74.52	-4.93	0.2
52	SLV 8	-8	-52	1739	74.52	-4.93	0.2
52	SLV 9	8	53	951	-74.7	4.92	-0.2
52	SLV 10	8	53	951	-74.7	4.92	-0.2
52	SLV 11	-3	-49	1706	70.61	-13.02	0.04
52	SLV 12	-3	-49	1706	70.61	-13.02	0.04
52	SLV 13	10	21	1176	-28.4	-10.8	-0.3
52	SLV 14	10	21	1176	-28.4	-10.8	-0.3
52	SLV 15	7	-10	1403	15.2	-16.18	-0.23
52	SLV 16	7	-10	1403	15.2	-16.18	-0.23
53	SLU 1	0	209	1883	-7.97	-0.34	0
53	SLU 2	0	209	1883	-7.97	-0.34	0
53	SLU 3	0	209	1883	-7.97	-0.34	0
53	SLU 4	0	209	1883	-7.97	-0.34	0
53	SLU 5	0	209	1883	-7.97	-0.34	0
53	SLU 6	0	209	1883	-7.97	-0.34	0
53	SLU 7	0	209	1883	-7.97	-0.34	0
53	SLU 8	0	209	1883	-7.97	-0.34	0
53	SLU 9	0	209	1883	-7.97	-0.34	0
53	SLU 10	0	285	2271	-10.83	-0.48	0
53	SLU 11	0	285	2271	-10.83	-0.48	0
53	SLU 12	0	285	2271	-10.83	-0.48	0
53	SLU 13	0	285	2271	-10.83	-0.48	0
53	SLU 14	0	285	2271	-10.83	-0.48	0
53	SLU 15	0	285	2271	-10.83	-0.48	0
53	SLU 16	0	285	2271	-10.83	-0.48	0
53	SLU 17	0	285	2271	-10.83	-0.48	0
53	SLU 18	0	318	2437	-12.06	-0.54	0
53	SLU 19	0	318	2437	-12.06	-0.54	0
53	SLU 20	0	318	2437	-12.06	-0.54	0
53	SLU 21	0	318	2437	-12.06	-0.54	0
53	SLU 22	0	249	2089	-9.46	-0.42	0
53	SLU 23	0	249	2089	-9.46	-0.42	0
53	SLU 24	0	249	2089	-9.46	-0.42	0
53	SLU 25	0	249	2089	-9.46	-0.42	0
53	SLU 26	0	249	2089	-9.46	-0.42	0
53	SLU 27	0	249	2089	-9.46	-0.42	0
53	SLU 28	0	249	2089	-9.46	-0.42	0
53	SLU 29	0	249	2089	-9.46	-0.42	0
53	SLU 30	0	249	2089	-9.46	-0.42	0
53	SLU 31	0	325	2477	-12.32	-0.57	0
53	SLU 32	0	325	2477	-12.32	-0.57	0
53	SLU 33	0	325	2477	-12.32	-0.57	0
53	SLU 34	0	325	2477	-12.32	-0.57	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
53	SLU 35	0	325	2477	-12.32	-0.57	0
53	SLU 36	0	325	2477	-12.32	-0.57	0
53	SLU 37	0	325	2477	-12.32	-0.57	0
53	SLU 38	0	325	2477	-12.32	-0.57	0
53	SLU 39	0	357	2643	-13.55	-0.63	-0.01
53	SLU 40	0	357	2643	-13.55	-0.63	-0.01
53	SLU 41	0	357	2643	-13.55	-0.63	-0.01
53	SLU 42	0	357	2643	-13.55	-0.63	-0.01
53	SLU 43	0	259	2377	-9.86	-0.41	0
53	SLU 44	0	259	2377	-9.86	-0.41	0
53	SLU 45	0	259	2377	-9.86	-0.41	0
53	SLU 46	0	259	2377	-9.86	-0.41	0
53	SLU 47	0	259	2377	-9.86	-0.41	0
53	SLU 48	0	259	2377	-9.86	-0.41	0
53	SLU 49	0	259	2377	-9.86	-0.41	0
53	SLU 50	0	259	2377	-9.86	-0.41	0
53	SLU 51	0	259	2377	-9.86	-0.41	0
53	SLU 52	0	334	2765	-12.72	-0.56	0
53	SLU 53	0	334	2765	-12.72	-0.56	0
53	SLU 54	0	334	2765	-12.72	-0.56	0
53	SLU 55	0	334	2765	-12.72	-0.56	0
53	SLU 56	0	334	2765	-12.72	-0.56	0
53	SLU 57	0	334	2765	-12.72	-0.56	0
53	SLU 58	0	334	2765	-12.72	-0.56	0
53	SLU 59	0	334	2765	-12.72	-0.56	0
53	SLU 60	0	367	2931	-13.94	-0.62	-0.01
53	SLU 61	0	367	2931	-13.94	-0.62	-0.01
53	SLU 62	0	367	2931	-13.94	-0.62	-0.01
53	SLU 63	0	367	2931	-13.94	-0.62	-0.01
53	SLU 64	0	298	2584	-11.35	-0.49	0
53	SLU 65	0	298	2584	-11.35	-0.49	0
53	SLU 66	0	298	2584	-11.35	-0.49	0
53	SLU 67	0	298	2584	-11.35	-0.49	0
53	SLU 68	0	298	2584	-11.35	-0.49	0
53	SLU 69	0	298	2584	-11.35	-0.49	0
53	SLU 70	0	298	2584	-11.35	-0.49	0
53	SLU 71	0	298	2584	-11.35	-0.49	0
53	SLU 72	0	298	2584	-11.35	-0.49	0
53	SLU 73	0	374	2971	-14.2	-0.64	-0.01
53	SLU 74	0	374	2971	-14.2	-0.64	-0.01
53	SLU 75	0	374	2971	-14.2	-0.64	-0.01
53	SLU 76	0	374	2971	-14.2	-0.64	-0.01
53	SLU 77	0	374	2971	-14.2	-0.64	-0.01
53	SLU 78	0	374	2971	-14.2	-0.64	-0.01
53	SLU 79	0	374	2971	-14.2	-0.64	-0.01
53	SLU 80	0	374	2971	-14.2	-0.64	-0.01
53	SLU 81	0	407	3137	-15.43	-0.7	-0.01
53	SLU 82	0	407	3137	-15.43	-0.7	-0.01
53	SLU 83	0	407	3137	-15.43	-0.7	-0.01
53	SLU 84	0	407	3137	-15.43	-0.7	-0.01
53	SLE RA 1	0	221	1942	-8.4	-0.36	0
53	SLE RA 2	0	221	1942	-8.4	-0.36	0
53	SLE RA 3	0	221	1942	-8.4	-0.36	0
53	SLE RA 4	0	221	1942	-8.4	-0.36	0
53	SLE RA 5	0	221	1942	-8.4	-0.36	0
53	SLE RA 6	0	221	1942	-8.4	-0.36	0
53	SLE RA 7	0	221	1942	-8.4	-0.36	0
53	SLE RA 8	0	221	1942	-8.4	-0.36	0
53	SLE RA 9	0	221	1942	-8.4	-0.36	0
53	SLE RA 10	0	271	2200	-10.31	-0.46	0
53	SLE RA 11	0	271	2200	-10.31	-0.46	0
53	SLE RA 12	0	271	2200	-10.31	-0.46	0
53	SLE RA 13	0	271	2200	-10.31	-0.46	0
53	SLE RA 14	0	271	2200	-10.31	-0.46	0
53	SLE RA 15	0	271	2200	-10.31	-0.46	0
53	SLE RA 16	0	271	2200	-10.31	-0.46	0
53	SLE RA 17	0	271	2200	-10.31	-0.46	0
53	SLE RA 18	0	293	2311	-11.12	-0.5	0
53	SLE RA 19	0	293	2311	-11.12	-0.5	0
53	SLE RA 20	0	293	2311	-11.12	-0.5	0
53	SLE RA 21	0	293	2311	-11.12	-0.5	0
53	SLE FR 1	0	221	1942	-8.4	-0.36	0
53	SLE FR 2	0	221	1942	-8.4	-0.36	0
53	SLE FR 3	0	221	1942	-8.4	-0.36	0
53	SLE FR 4	0	242	2053	-9.22	-0.4	0
53	SLE FR 5	0	242	2053	-9.22	-0.4	0
53	SLE FR 6	0	257	2127	-9.76	-0.43	0
53	SLE QP 1	0	221	1942	-8.4	-0.36	0
53	SLE QP 2	0	242	2053	-9.22	-0.4	0
53	SLD 1	-21	240	1971	-9.14	11.3	0.06
53	SLD 2	-21	240	1971	-9.14	11.3	0.06
53	SLD 3	-6	89	1918	-3.3	21.41	0.15
53	SLD 4	-6	89	1918	-3.3	21.41	0.15
53	SLD 5	-29	471	2109	-18.06	-12.22	-0.11
53	SLD 6	-29	471	2109	-18.06	-12.22	-0.11
53	SLD 7	20	-32	1932	1.42	21.47	0.17
53	SLD 8	20	-32	1932	1.42	21.47	0.17
53	SLD 9	-21	517	2174	-19.86	-22.28	-0.18
53	SLD 10	-21	517	2174	-19.86	-22.28	-0.18



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
53	SLD 11	28	14	1997	-0.37	11.41	0.11
53	SLD 12	28	14	1997	-0.37	11.41	0.11
53	SLD 13	6	396	2188	-15.14	-22.21	-0.15
53	SLD 14	6	396	2188	-15.14	-22.21	-0.15
53	SLD 15	20	245	2135	-9.29	-12.11	-0.07
53	SLD 16	20	245	2135	-9.29	-12.11	-0.07
53	SLV 1	-51	236	1857	-9.02	27.84	0.15
53	SLV 2	-51	236	1857	-9.02	27.84	0.15
53	SLV 3	-13	-119	1731	4.71	53.69	0.36
53	SLV 4	-13	-119	1731	4.71	53.69	0.36
53	SLV 5	-73	779	2185	-29.99	-31.14	-0.29
53	SLV 6	-73	779	2185	-29.99	-31.14	-0.29
53	SLV 7	53	-404	1765	15.79	55.04	0.44
53	SLV 8	53	-404	1765	15.79	55.04	0.44
53	SLV 9	-54	889	2340	-34.22	-55.84	-0.44
53	SLV 10	-54	889	2340	-34.22	-55.84	-0.44
53	SLV 11	72	-294	1921	11.55	30.34	0.28
53	SLV 12	72	-294	1921	11.55	30.34	0.28
53	SLV 13	13	604	2375	-23.14	-54.5	-0.37
53	SLV 14	13	604	2375	-23.14	-54.5	-0.37
53	SLV 15	51	249	2249	-9.41	-28.64	-0.15
53	SLV 16	51	249	2249	-9.41	-28.64	-0.15
54	SLU 1	1	88	2068	-3.22	0.66	0.01
54	SLU 2	1	88	2068	-3.22	0.66	0.01
54	SLU 3	1	88	2068	-3.22	0.66	0.01
54	SLU 4	1	88	2068	-3.22	0.66	0.01
54	SLU 5	1	88	2068	-3.22	0.66	0.01
54	SLU 6	1	88	2068	-3.22	0.66	0.01
54	SLU 7	1	88	2068	-3.22	0.66	0.01
54	SLU 8	1	88	2068	-3.22	0.66	0.01
54	SLU 9	1	88	2068	-3.22	0.66	0.01
54	SLU 10	1	124	2511	-4.49	0.89	0.01
54	SLU 11	1	124	2511	-4.49	0.89	0.01
54	SLU 12	1	124	2511	-4.49	0.89	0.01
54	SLU 13	1	124	2511	-4.49	0.89	0.01
54	SLU 14	1	124	2511	-4.49	0.89	0.01
54	SLU 15	1	124	2511	-4.49	0.89	0.01
54	SLU 16	1	124	2511	-4.49	0.89	0.01
54	SLU 17	1	124	2511	-4.49	0.89	0.01
54	SLU 18	1	139	2700	-5.03	0.98	0.01
54	SLU 19	1	139	2700	-5.03	0.98	0.01
54	SLU 20	1	139	2700	-5.03	0.98	0.01
54	SLU 21	1	139	2700	-5.03	0.98	0.01
54	SLU 22	1	112	2318	-4.05	0.82	0.01
54	SLU 23	1	112	2318	-4.05	0.82	0.01
54	SLU 24	1	112	2318	-4.05	0.82	0.01
54	SLU 25	1	112	2318	-4.05	0.82	0.01
54	SLU 26	1	112	2318	-4.05	0.82	0.01
54	SLU 27	1	112	2318	-4.05	0.82	0.01
54	SLU 28	1	112	2318	-4.05	0.82	0.01
54	SLU 29	1	112	2318	-4.05	0.82	0.01
54	SLU 30	1	112	2318	-4.05	0.82	0.01
54	SLU 31	1	147	2761	-5.32	1.04	0.01
54	SLU 32	1	147	2761	-5.32	1.04	0.01
54	SLU 33	1	147	2761	-5.32	1.04	0.01
54	SLU 34	1	147	2761	-5.32	1.04	0.01
54	SLU 35	1	147	2761	-5.32	1.04	0.01
54	SLU 36	1	147	2761	-5.32	1.04	0.01
54	SLU 37	1	147	2761	-5.32	1.04	0.01
54	SLU 38	1	147	2761	-5.32	1.04	0.01
54	SLU 39	1	163	2950	-5.86	1.13	0.01
54	SLU 40	1	163	2950	-5.86	1.13	0.01
54	SLU 41	1	163	2950	-5.86	1.13	0.01
54	SLU 42	1	163	2950	-5.86	1.13	0.01
54	SLU 43	1	107	2603	-3.91	0.81	0.01
54	SLU 44	1	107	2603	-3.91	0.81	0.01
54	SLU 45	1	107	2603	-3.91	0.81	0.01
54	SLU 46	1	107	2603	-3.91	0.81	0.01
54	SLU 47	1	107	2603	-3.91	0.81	0.01
54	SLU 48	1	107	2603	-3.91	0.81	0.01
54	SLU 49	1	107	2603	-3.91	0.81	0.01
54	SLU 50	1	107	2603	-3.91	0.81	0.01
54	SLU 51	1	107	2603	-3.91	0.81	0.01
54	SLU 52	1	143	3046	-5.18	1.03	0.01
54	SLU 53	1	143	3046	-5.18	1.03	0.01
54	SLU 54	1	143	3046	-5.18	1.03	0.01
54	SLU 55	1	143	3046	-5.18	1.03	0.01
54	SLU 56	1	143	3046	-5.18	1.03	0.01
54	SLU 57	1	143	3046	-5.18	1.03	0.01
54	SLU 58	1	143	3046	-5.18	1.03	0.01
54	SLU 59	1	143	3046	-5.18	1.03	0.01
54	SLU 60	1	158	3235	-5.72	1.13	0.01
54	SLU 61	1	158	3235	-5.72	1.13	0.01
54	SLU 62	1	158	3235	-5.72	1.13	0.01
54	SLU 63	1	158	3235	-5.72	1.13	0.01
54	SLU 64	1	130	2853	-4.73	0.96	0.01
54	SLU 65	1	130	2853	-4.73	0.96	0.01
54	SLU 66	1	130	2853	-4.73	0.96	0.01
54	SLU 67	1	130	2853	-4.73	0.96	0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
54	SLU 68	1	130	2853	-4.73	0.96	0.01
54	SLU 69	1	130	2853	-4.73	0.96	0.01
54	SLU 70	1	130	2853	-4.73	0.96	0.01
54	SLU 71	1	130	2853	-4.73	0.96	0.01
54	SLU 72	1	130	2853	-4.73	0.96	0.01
54	SLU 73	1	166	3296	-6	1.18	0.01
54	SLU 74	1	166	3296	-6	1.18	0.01
54	SLU 75	1	166	3296	-6	1.18	0.01
54	SLU 76	1	166	3296	-6	1.18	0.01
54	SLU 77	1	166	3296	-6	1.18	0.01
54	SLU 78	1	166	3296	-6	1.18	0.01
54	SLU 79	1	166	3296	-6	1.18	0.01
54	SLU 80	1	166	3296	-6	1.18	0.01
54	SLU 81	1	181	3485	-6.54	1.28	0.01
54	SLU 82	1	181	3485	-6.54	1.28	0.01
54	SLU 83	1	181	3485	-6.54	1.28	0.01
54	SLU 84	1	181	3485	-6.54	1.28	0.01
54	SLE RA 1	1	95	2140	-3.46	0.71	0.01
54	SLE RA 2	1	95	2140	-3.46	0.71	0.01
54	SLE RA 3	1	95	2140	-3.46	0.71	0.01
54	SLE RA 4	1	95	2140	-3.46	0.71	0.01
54	SLE RA 5	1	95	2140	-3.46	0.71	0.01
54	SLE RA 6	1	95	2140	-3.46	0.71	0.01
54	SLE RA 7	1	95	2140	-3.46	0.71	0.01
54	SLE RA 8	1	95	2140	-3.46	0.71	0.01
54	SLE RA 9	1	95	2140	-3.46	0.71	0.01
54	SLE RA 10	1	119	2435	-4.31	0.85	0.01
54	SLE RA 11	1	119	2435	-4.31	0.85	0.01
54	SLE RA 12	1	119	2435	-4.31	0.85	0.01
54	SLE RA 13	1	119	2435	-4.31	0.85	0.01
54	SLE RA 14	1	119	2435	-4.31	0.85	0.01
54	SLE RA 15	1	119	2435	-4.31	0.85	0.01
54	SLE RA 16	1	119	2435	-4.31	0.85	0.01
54	SLE RA 17	1	119	2435	-4.31	0.85	0.01
54	SLE RA 18	1	129	2561	-4.67	0.92	0.01
54	SLE RA 19	1	129	2561	-4.67	0.92	0.01
54	SLE RA 20	1	129	2561	-4.67	0.92	0.01
54	SLE RA 21	1	129	2561	-4.67	0.92	0.01
54	SLE FR 1	1	95	2140	-3.46	0.71	0.01
54	SLE FR 2	1	95	2140	-3.46	0.71	0.01
54	SLE FR 3	1	95	2140	-3.46	0.71	0.01
54	SLE FR 4	1	105	2266	-3.82	0.77	0.01
54	SLE FR 5	1	105	2266	-3.82	0.77	0.01
54	SLE FR 6	1	112	2350	-4.06	0.81	0.01
54	SLE QP 1	1	95	2140	-3.46	0.71	0.01
54	SLE QP 2	1	105	2266	-3.82	0.77	0.01
54	SLD 1	-3	281	2409	-11.29	12.01	0.02
54	SLD 2	-3	281	2409	-11.29	12.01	0.02
54	SLD 3	-14	110	2390	-4.15	6.7	0.03
54	SLD 4	-14	110	2390	-4.15	6.7	0.03
54	SLD 5	16	417	2339	-16.89	12.2	0
54	SLD 6	16	417	2339	-16.89	12.2	0
54	SLD 7	-20	-153	2274	6.91	-5.51	0.02
54	SLD 8	-20	-153	2274	6.91	-5.51	0.02
54	SLD 9	21	363	2259	-14.56	7.05	-0.01
54	SLD 10	21	363	2259	-14.56	7.05	-0.01
54	SLD 11	-14	-207	2194	9.25	-10.66	0.01
54	SLD 12	-14	-207	2194	9.25	-10.66	0.01
54	SLD 13	15	101	2143	-3.5	-5.16	-0.01
54	SLD 14	15	101	2143	-3.5	-5.16	-0.01
54	SLD 15	4	-70	2123	3.65	-10.47	-0.01
54	SLD 16	4	-70	2123	3.65	-10.47	-0.01
54	SLV 1	-7	519	2611	-21.42	28.66	0.05
54	SLV 2	-7	519	2611	-21.42	28.66	0.05
54	SLV 3	-35	117	2564	-4.65	15.07	0.06
54	SLV 4	-35	117	2564	-4.65	15.07	0.06
54	SLV 5	40	838	2440	-34.53	29.75	0
54	SLV 6	40	838	2440	-34.53	29.75	0
54	SLV 7	-52	-500	2285	21.36	-15.55	0.04
54	SLV 8	-52	-500	2285	21.36	-15.55	0.04
54	SLV 9	53	711	2248	-29.01	17.09	-0.03
54	SLV 10	53	711	2248	-29.01	17.09	-0.03
54	SLV 11	-38	-628	2092	26.89	-28.21	0.01
54	SLV 12	-38	-628	2092	26.89	-28.21	0.01
54	SLV 13	36	93	1968	-3	-13.53	-0.05
54	SLV 14	36	93	1968	-3	-13.53	-0.05
54	SLV 15	9	-308	1922	13.77	-27.12	-0.03
54	SLV 16	9	-308	1922	13.77	-27.12	-0.03
55	SLU 1	0	0	888	-0.05	-0.01	0
55	SLU 2	0	0	888	-0.05	-0.01	0
55	SLU 3	0	0	888	-0.05	-0.01	0
55	SLU 4	0	0	888	-0.05	-0.01	0
55	SLU 5	0	0	888	-0.05	-0.01	0
55	SLU 6	0	0	888	-0.05	-0.01	0
55	SLU 7	0	0	888	-0.05	-0.01	0
55	SLU 8	0	0	888	-0.05	-0.01	0
55	SLU 9	0	0	888	-0.05	-0.01	0
55	SLU 10	0	1	1241	-0.1	-0.02	0
55	SLU 11	0	1	1241	-0.1	-0.02	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
55	SLU 12	0	1	1241	-0.1	-0.02	0
55	SLU 13	0	1	1241	-0.1	-0.02	0
55	SLU 14	0	1	1241	-0.1	-0.02	0
55	SLU 15	0	1	1241	-0.1	-0.02	0
55	SLU 16	0	1	1241	-0.1	-0.02	0
55	SLU 17	0	1	1241	-0.1	-0.02	0
55	SLU 18	0	1	1392	-0.12	-0.02	0
55	SLU 19	0	1	1392	-0.12	-0.02	0
55	SLU 20	0	1	1392	-0.12	-0.02	0
55	SLU 21	0	1	1392	-0.12	-0.02	0
55	SLU 22	0	0	1069	-0.07	-0.02	0
55	SLU 23	0	0	1069	-0.07	-0.02	0
55	SLU 24	0	0	1069	-0.07	-0.02	0
55	SLU 25	0	0	1069	-0.07	-0.02	0
55	SLU 26	0	0	1069	-0.07	-0.02	0
55	SLU 27	0	0	1069	-0.07	-0.02	0
55	SLU 28	0	0	1069	-0.07	-0.02	0
55	SLU 29	0	0	1069	-0.07	-0.02	0
55	SLU 30	0	0	1069	-0.07	-0.02	0
55	SLU 31	0	1	1422	-0.12	-0.02	0
55	SLU 32	0	1	1422	-0.12	-0.02	0
55	SLU 33	0	1	1422	-0.12	-0.02	0
55	SLU 34	0	1	1422	-0.12	-0.02	0
55	SLU 35	0	1	1422	-0.12	-0.02	0
55	SLU 36	0	1	1422	-0.12	-0.02	0
55	SLU 37	0	1	1422	-0.12	-0.02	0
55	SLU 38	0	1	1422	-0.12	-0.02	0
55	SLU 39	0	1	1573	-0.14	-0.02	0
55	SLU 40	0	1	1573	-0.14	-0.02	0
55	SLU 41	0	1	1573	-0.14	-0.02	0
55	SLU 42	0	1	1573	-0.14	-0.02	0
55	SLU 43	0	0	1092	-0.06	-0.02	0
55	SLU 44	0	0	1092	-0.06	-0.02	0
55	SLU 45	0	0	1092	-0.06	-0.02	0
55	SLU 46	0	0	1092	-0.06	-0.02	0
55	SLU 47	0	0	1092	-0.06	-0.02	0
55	SLU 48	0	0	1092	-0.06	-0.02	0
55	SLU 49	0	0	1092	-0.06	-0.02	0
55	SLU 50	0	0	1092	-0.06	-0.02	0
55	SLU 51	0	0	1092	-0.06	-0.02	0
55	SLU 52	0	1	1445	-0.11	-0.02	0
55	SLU 53	0	1	1445	-0.11	-0.02	0
55	SLU 54	0	1	1445	-0.11	-0.02	0
55	SLU 55	0	1	1445	-0.11	-0.02	0
55	SLU 56	0	1	1445	-0.11	-0.02	0
55	SLU 57	0	1	1445	-0.11	-0.02	0
55	SLU 58	0	1	1445	-0.11	-0.02	0
55	SLU 59	0	1	1445	-0.11	-0.02	0
55	SLU 60	0	1	1597	-0.13	-0.02	0
55	SLU 61	0	1	1597	-0.13	-0.02	0
55	SLU 62	0	1	1597	-0.13	-0.02	0
55	SLU 63	0	1	1597	-0.13	-0.02	0
55	SLU 64	0	0	1273	-0.08	-0.02	0
55	SLU 65	0	0	1273	-0.08	-0.02	0
55	SLU 66	0	0	1273	-0.08	-0.02	0
55	SLU 67	0	0	1273	-0.08	-0.02	0
55	SLU 68	0	0	1273	-0.08	-0.02	0
55	SLU 69	0	0	1273	-0.08	-0.02	0
55	SLU 70	0	0	1273	-0.08	-0.02	0
55	SLU 71	0	0	1273	-0.08	-0.02	0
55	SLU 72	0	0	1273	-0.08	-0.02	0
55	SLU 73	0	1	1626	-0.13	-0.02	0
55	SLU 74	0	1	1626	-0.13	-0.02	0
55	SLU 75	0	1	1626	-0.13	-0.02	0
55	SLU 76	0	1	1626	-0.13	-0.02	0
55	SLU 77	0	1	1626	-0.13	-0.02	0
55	SLU 78	0	1	1626	-0.13	-0.02	0
55	SLU 79	0	1	1626	-0.13	-0.02	0
55	SLU 80	0	1	1626	-0.13	-0.02	0
55	SLU 81	0	1	1777	-0.15	-0.02	0
55	SLU 82	0	1	1777	-0.15	-0.02	0
55	SLU 83	0	1	1777	-0.15	-0.02	0
55	SLU 84	0	1	1777	-0.15	-0.02	0
55	SLE RA 1	0	0	940	-0.06	-0.02	0
55	SLE RA 2	0	0	940	-0.06	-0.02	0
55	SLE RA 3	0	0	940	-0.06	-0.02	0
55	SLE RA 4	0	0	940	-0.06	-0.02	0
55	SLE RA 5	0	0	940	-0.06	-0.02	0
55	SLE RA 6	0	0	940	-0.06	-0.02	0
55	SLE RA 7	0	0	940	-0.06	-0.02	0
55	SLE RA 8	0	0	940	-0.06	-0.02	0
55	SLE RA 9	0	0	940	-0.06	-0.02	0
55	SLE RA 10	0	1	1175	-0.09	-0.02	0
55	SLE RA 11	0	1	1175	-0.09	-0.02	0
55	SLE RA 12	0	1	1175	-0.09	-0.02	0
55	SLE RA 13	0	1	1175	-0.09	-0.02	0
55	SLE RA 14	0	1	1175	-0.09	-0.02	0
55	SLE RA 15	0	1	1175	-0.09	-0.02	0
55	SLE RA 16	0	1	1175	-0.09	-0.02	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
55	SLE RA 17	0	1	1175	-0.09	-0.02	0
55	SLE RA 18	0	1	1276	-0.1	-0.02	0
55	SLE RA 19	0	1	1276	-0.1	-0.02	0
55	SLE RA 20	0	1	1276	-0.1	-0.02	0
55	SLE RA 21	0	1	1276	-0.1	-0.02	0
55	SLE FR 1	0	0	940	-0.06	-0.02	0
55	SLE FR 2	0	0	940	-0.06	-0.02	0
55	SLE FR 3	0	0	940	-0.06	-0.02	0
55	SLE FR 4	0	0	1040	-0.07	-0.02	0
55	SLE FR 5	0	0	1040	-0.07	-0.02	0
55	SLE FR 6	0	0	1108	-0.08	-0.02	0
55	SLE QP 1	0	0	940	-0.06	-0.02	0
55	SLE QP 2	0	0	1040	-0.07	-0.02	0
55	SLD 1	-1	8	1042	-7.06	3.75	-0.14
55	SLD 2	-1	8	1042	-7.06	3.75	-0.14
55	SLD 3	-2	-15	1062	12.87	2.13	-0.1
55	SLD 4	-2	-15	1062	12.87	2.13	-0.1
55	SLD 5	1	38	1010	-32.4	3.56	-0.1
55	SLD 6	1	38	1010	-32.4	3.56	-0.1
55	SLD 7	-3	-40	1078	34.04	-1.82	0.03
55	SLD 8	-3	-40	1078	34.04	-1.82	0.03
55	SLD 9	3	41	1003	-34.18	1.79	-0.03
55	SLD 10	3	41	1003	-34.18	1.79	-0.03
55	SLD 11	-2	-38	1071	32.25	-3.59	0.1
55	SLD 12	-2	-38	1071	32.25	-3.59	0.1
55	SLD 13	2	16	1019	-13.01	-2.17	0.1
55	SLD 14	2	16	1019	-13.01	-2.17	0.1
55	SLD 15	1	-7	1039	6.92	-3.78	0.14
55	SLD 16	1	-7	1039	6.92	-3.78	0.14
55	SLV 1	-3	21	1043	-18	9.56	-0.36
55	SLV 2	-3	21	1043	-18	9.56	-0.36
55	SLV 3	-6	-40	1095	33.13	5.42	-0.26
55	SLV 4	-6	-40	1095	33.13	5.42	-0.26
55	SLV 5	4	98	963	-83	9.13	-0.26
55	SLV 6	4	98	963	-83	9.13	-0.26
55	SLV 7	-6	-103	1135	87.43	-4.65	0.07
55	SLV 8	-6	-103	1135	87.43	-4.65	0.07
55	SLV 9	6	104	946	-87.58	4.62	-0.07
55	SLV 10	6	104	946	-87.58	4.62	-0.07
55	SLV 11	-4	-97	1118	82.85	-9.16	0.26
55	SLV 12	-4	-97	1118	82.85	-9.16	0.26
55	SLV 13	6	41	986	-33.27	-5.45	0.26
55	SLV 14	6	41	986	-33.27	-5.45	0.26
55	SLV 15	3	-20	1038	17.86	-9.59	0.36
55	SLV 16	3	-20	1038	17.86	-9.59	0.36
56	SLU 1	-1	153	2035	-4.95	-0.65	-0.01
56	SLU 2	-1	153	2035	-4.95	-0.65	-0.01
56	SLU 3	-1	153	2035	-4.95	-0.65	-0.01
56	SLU 4	-1	153	2035	-4.95	-0.65	-0.01
56	SLU 5	-1	153	2035	-4.95	-0.65	-0.01
56	SLU 6	-1	153	2035	-4.95	-0.65	-0.01
56	SLU 7	-1	153	2035	-4.95	-0.65	-0.01
56	SLU 8	-1	153	2035	-4.95	-0.65	-0.01
56	SLU 9	-1	153	2035	-4.95	-0.65	-0.01
56	SLU 10	-1	212	2474	-6.89	-0.92	-0.01
56	SLU 11	-1	212	2474	-6.89	-0.92	-0.01
56	SLU 12	-1	212	2474	-6.89	-0.92	-0.01
56	SLU 13	-1	212	2474	-6.89	-0.92	-0.01
56	SLU 14	-1	212	2474	-6.89	-0.92	-0.01
56	SLU 15	-1	212	2474	-6.89	-0.92	-0.01
56	SLU 16	-1	212	2474	-6.89	-0.92	-0.01
56	SLU 17	-1	212	2474	-6.89	-0.92	-0.01
56	SLU 18	-1	238	2662	-7.72	-1.04	-0.02
56	SLU 19	-1	238	2662	-7.72	-1.04	-0.02
56	SLU 20	-1	238	2662	-7.72	-1.04	-0.02
56	SLU 21	-1	238	2662	-7.72	-1.04	-0.02
56	SLU 22	-1	186	2270	-6.01	-0.81	-0.01
56	SLU 23	-1	186	2270	-6.01	-0.81	-0.01
56	SLU 24	-1	186	2270	-6.01	-0.81	-0.01
56	SLU 25	-1	186	2270	-6.01	-0.81	-0.01
56	SLU 26	-1	186	2270	-6.01	-0.81	-0.01
56	SLU 27	-1	186	2270	-6.01	-0.81	-0.01
56	SLU 28	-1	186	2270	-6.01	-0.81	-0.01
56	SLU 29	-1	186	2270	-6.01	-0.81	-0.01
56	SLU 30	-1	186	2270	-6.01	-0.81	-0.01
56	SLU 31	-1	245	2710	-7.95	-1.08	-0.02
56	SLU 32	-1	245	2710	-7.95	-1.08	-0.02
56	SLU 33	-1	245	2710	-7.95	-1.08	-0.02
56	SLU 34	-1	245	2710	-7.95	-1.08	-0.02
56	SLU 35	-1	245	2710	-7.95	-1.08	-0.02
56	SLU 36	-1	245	2710	-7.95	-1.08	-0.02
56	SLU 37	-1	245	2710	-7.95	-1.08	-0.02
56	SLU 38	-1	245	2710	-7.95	-1.08	-0.02
56	SLU 39	-1	270	2898	-8.78	-1.2	-0.02
56	SLU 40	-1	270	2898	-8.78	-1.2	-0.02
56	SLU 41	-1	270	2898	-8.78	-1.2	-0.02
56	SLU 42	-1	270	2898	-8.78	-1.2	-0.02
56	SLU 43	-1	188	2564	-6.07	-0.8	-0.01
56	SLU 44	-1	188	2564	-6.07	-0.8	-0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
56	SLU 45	-1	188	2564	-6.07	-0.8	-0.01
56	SLU 46	-1	188	2564	-6.07	-0.8	-0.01
56	SLU 47	-1	188	2564	-6.07	-0.8	-0.01
56	SLU 48	-1	188	2564	-6.07	-0.8	-0.01
56	SLU 49	-1	188	2564	-6.07	-0.8	-0.01
56	SLU 50	-1	188	2564	-6.07	-0.8	-0.01
56	SLU 51	-1	188	2564	-6.07	-0.8	-0.01
56	SLU 52	-1	247	3003	-8.01	-1.07	-0.02
56	SLU 53	-1	247	3003	-8.01	-1.07	-0.02
56	SLU 54	-1	247	3003	-8.01	-1.07	-0.02
56	SLU 55	-1	247	3003	-8.01	-1.07	-0.02
56	SLU 56	-1	247	3003	-8.01	-1.07	-0.02
56	SLU 57	-1	247	3003	-8.01	-1.07	-0.02
56	SLU 58	-1	247	3003	-8.01	-1.07	-0.02
56	SLU 59	-1	247	3003	-8.01	-1.07	-0.02
56	SLU 60	-1	272	3192	-8.84	-1.18	-0.02
56	SLU 61	-1	272	3192	-8.84	-1.18	-0.02
56	SLU 62	-1	272	3192	-8.84	-1.18	-0.02
56	SLU 63	-1	272	3192	-8.84	-1.18	-0.02
56	SLU 64	-1	221	2800	-7.13	-0.96	-0.02
56	SLU 65	-1	221	2800	-7.13	-0.96	-0.02
56	SLU 66	-1	221	2800	-7.13	-0.96	-0.02
56	SLU 67	-1	221	2800	-7.13	-0.96	-0.02
56	SLU 68	-1	221	2800	-7.13	-0.96	-0.02
56	SLU 69	-1	221	2800	-7.13	-0.96	-0.02
56	SLU 70	-1	221	2800	-7.13	-0.96	-0.02
56	SLU 71	-1	221	2800	-7.13	-0.96	-0.02
56	SLU 72	-1	221	2800	-7.13	-0.96	-0.02
56	SLU 73	-1	280	3239	-9.07	-1.23	-0.02
56	SLU 74	-1	280	3239	-9.07	-1.23	-0.02
56	SLU 75	-1	280	3239	-9.07	-1.23	-0.02
56	SLU 76	-1	280	3239	-9.07	-1.23	-0.02
56	SLU 77	-1	280	3239	-9.07	-1.23	-0.02
56	SLU 78	-1	280	3239	-9.07	-1.23	-0.02
56	SLU 79	-1	280	3239	-9.07	-1.23	-0.02
56	SLU 80	-1	280	3239	-9.07	-1.23	-0.02
56	SLU 81	-1	305	3427	-9.9	-1.34	-0.02
56	SLU 82	-1	305	3427	-9.9	-1.34	-0.02
56	SLU 83	-1	305	3427	-9.9	-1.34	-0.02
56	SLU 84	-1	305	3427	-9.9	-1.34	-0.02
56	SLE RA 1	-1	163	2102	-5.25	-0.7	-0.01
56	SLE RA 2	-1	163	2102	-5.25	-0.7	-0.01
56	SLE RA 3	-1	163	2102	-5.25	-0.7	-0.01
56	SLE RA 4	-1	163	2102	-5.25	-0.7	-0.01
56	SLE RA 5	-1	163	2102	-5.25	-0.7	-0.01
56	SLE RA 6	-1	163	2102	-5.25	-0.7	-0.01
56	SLE RA 7	-1	163	2102	-5.25	-0.7	-0.01
56	SLE RA 8	-1	163	2102	-5.25	-0.7	-0.01
56	SLE RA 9	-1	163	2102	-5.25	-0.7	-0.01
56	SLE RA 10	-1	202	2395	-6.54	-0.88	-0.01
56	SLE RA 11	-1	202	2395	-6.54	-0.88	-0.01
56	SLE RA 12	-1	202	2395	-6.54	-0.88	-0.01
56	SLE RA 13	-1	202	2395	-6.54	-0.88	-0.01
56	SLE RA 14	-1	202	2395	-6.54	-0.88	-0.01
56	SLE RA 15	-1	202	2395	-6.54	-0.88	-0.01
56	SLE RA 16	-1	202	2395	-6.54	-0.88	-0.01
56	SLE RA 17	-1	202	2395	-6.54	-0.88	-0.01
56	SLE RA 18	-1	219	2520	-7.1	-0.96	-0.02
56	SLE RA 19	-1	219	2520	-7.1	-0.96	-0.02
56	SLE RA 20	-1	219	2520	-7.1	-0.96	-0.02
56	SLE RA 21	-1	219	2520	-7.1	-0.96	-0.02
56	SLE FR 1	-1	163	2102	-5.25	-0.7	-0.01
56	SLE FR 2	-1	163	2102	-5.25	-0.7	-0.01
56	SLE FR 3	-1	163	2102	-5.25	-0.7	-0.01
56	SLE FR 4	-1	179	2227	-5.8	-0.78	-0.01
56	SLE FR 5	-1	179	2227	-5.8	-0.78	-0.01
56	SLE FR 6	-1	191	2311	-6.17	-0.83	-0.01
56	SLE QP 1	-1	163	2102	-5.25	-0.7	-0.01
56	SLE QP 2	-1	179	2227	-5.8	-0.78	-0.01
56	SLD 1	-16	173	2106	-5.76	3.39	-0.08
56	SLD 2	-16	173	2106	-5.76	3.39	-0.08
56	SLD 3	0	25	2065	0.37	12.32	-0.02
56	SLD 4	0	25	2065	0.37	12.32	-0.02
56	SLD 5	-30	403	2254	-15.09	-13.07	-0.11
56	SLD 6	-30	403	2254	-15.09	-13.07	-0.11
56	SLD 7	24	-93	2116	5.35	16.7	0.07
56	SLD 8	24	-93	2116	5.35	16.7	0.07
56	SLD 9	-25	451	2339	-16.96	-18.26	-0.09
56	SLD 10	-25	451	2339	-16.96	-18.26	-0.09
56	SLD 11	28	-44	2201	3.48	11.52	0.09
56	SLD 12	28	-44	2201	3.48	11.52	0.09
56	SLD 13	-1	334	2390	-11.98	-13.88	0
56	SLD 14	-1	334	2390	-11.98	-13.88	0
56	SLD 15	15	186	2349	-5.85	-4.95	0.05
56	SLD 16	15	186	2349	-5.85	-4.95	0.05
56	SLV 1	-40	164	1939	-5.68	9	-0.17
56	SLV 2	-40	164	1939	-5.68	9	-0.17
56	SLV 3	1	-185	1840	8.74	31.88	-0.03
56	SLV 4	1	-185	1840	8.74	31.88	-0.03



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
56	SLV 5	-75	705	2290	-27.64	-32.53	-0.27
56	SLV 6	-75	705	2290	-27.64	-32.53	-0.27
56	SLV 7	62	-460	1962	20.43	43.71	0.2
56	SLV 8	62	-460	1962	20.43	43.71	0.2
56	SLV 9	-64	819	2493	-32.04	-45.26	-0.22
56	SLV 10	-64	819	2493	-32.04	-45.26	-0.22
56	SLV 11	73	-346	2165	16.03	30.98	0.25
56	SLV 12	73	-346	2165	16.03	30.98	0.25
56	SLV 13	-3	544	2614	-20.35	-33.43	0
56	SLV 14	-3	544	2614	-20.35	-33.43	0
56	SLV 15	38	195	2516	-5.93	-10.56	0.14
56	SLV 16	38	195	2516	-5.93	-10.56	0.14
57	SLU 1	5	90	2188	-2.93	1.49	-0.02
57	SLU 2	5	90	2188	-2.93	1.49	-0.02
57	SLU 3	5	90	2188	-2.93	1.49	-0.02
57	SLU 4	5	90	2188	-2.93	1.49	-0.02
57	SLU 5	5	90	2188	-2.93	1.49	-0.02
57	SLU 6	5	90	2188	-2.93	1.49	-0.02
57	SLU 7	5	90	2188	-2.93	1.49	-0.02
57	SLU 8	5	90	2188	-2.93	1.49	-0.02
57	SLU 9	5	90	2188	-2.93	1.49	-0.02
57	SLU 10	6	126	2684	-4.08	1.99	-0.02
57	SLU 11	6	126	2684	-4.08	1.99	-0.02
57	SLU 12	6	126	2684	-4.08	1.99	-0.02
57	SLU 13	6	126	2684	-4.08	1.99	-0.02
57	SLU 14	6	126	2684	-4.08	1.99	-0.02
57	SLU 15	6	126	2684	-4.08	1.99	-0.02
57	SLU 16	6	126	2684	-4.08	1.99	-0.02
57	SLU 17	6	126	2684	-4.08	1.99	-0.02
57	SLU 18	7	142	2897	-4.58	2.2	-0.03
57	SLU 19	7	142	2897	-4.58	2.2	-0.03
57	SLU 20	7	142	2897	-4.58	2.2	-0.03
57	SLU 21	7	142	2897	-4.58	2.2	-0.03
57	SLU 22	6	115	2474	-3.71	1.82	-0.02
57	SLU 23	6	115	2474	-3.71	1.82	-0.02
57	SLU 24	6	115	2474	-3.71	1.82	-0.02
57	SLU 25	6	115	2474	-3.71	1.82	-0.02
57	SLU 26	6	115	2474	-3.71	1.82	-0.02
57	SLU 27	6	115	2474	-3.71	1.82	-0.02
57	SLU 28	6	115	2474	-3.71	1.82	-0.02
57	SLU 29	6	115	2474	-3.71	1.82	-0.02
57	SLU 30	6	115	2474	-3.71	1.82	-0.02
57	SLU 31	7	151	2970	-4.86	2.32	-0.03
57	SLU 32	7	151	2970	-4.86	2.32	-0.03
57	SLU 33	7	151	2970	-4.86	2.32	-0.03
57	SLU 34	7	151	2970	-4.86	2.32	-0.03
57	SLU 35	7	151	2970	-4.86	2.32	-0.03
57	SLU 36	7	151	2970	-4.86	2.32	-0.03
57	SLU 37	7	151	2970	-4.86	2.32	-0.03
57	SLU 38	7	151	2970	-4.86	2.32	-0.03
57	SLU 39	8	166	3183	-5.36	2.54	-0.03
57	SLU 40	8	166	3183	-5.36	2.54	-0.03
57	SLU 41	8	166	3183	-5.36	2.54	-0.03
57	SLU 42	8	166	3183	-5.36	2.54	-0.03
57	SLU 43	6	109	2747	-3.54	1.82	-0.02
57	SLU 44	6	109	2747	-3.54	1.82	-0.02
57	SLU 45	6	109	2747	-3.54	1.82	-0.02
57	SLU 46	6	109	2747	-3.54	1.82	-0.02
57	SLU 47	6	109	2747	-3.54	1.82	-0.02
57	SLU 48	6	109	2747	-3.54	1.82	-0.02
57	SLU 49	6	109	2747	-3.54	1.82	-0.02
57	SLU 50	6	109	2747	-3.54	1.82	-0.02
57	SLU 51	6	109	2747	-3.54	1.82	-0.02
57	SLU 52	7	145	3242	-4.69	2.32	-0.03
57	SLU 53	7	145	3242	-4.69	2.32	-0.03
57	SLU 54	7	145	3242	-4.69	2.32	-0.03
57	SLU 55	7	145	3242	-4.69	2.32	-0.03
57	SLU 56	7	145	3242	-4.69	2.32	-0.03
57	SLU 57	7	145	3242	-4.69	2.32	-0.03
57	SLU 58	7	145	3242	-4.69	2.32	-0.03
57	SLU 59	7	145	3242	-4.69	2.32	-0.03
57	SLU 60	8	160	3455	-5.19	2.54	-0.03
57	SLU 61	8	160	3455	-5.19	2.54	-0.03
57	SLU 62	8	160	3455	-5.19	2.54	-0.03
57	SLU 63	8	160	3455	-5.19	2.54	-0.03
57	SLU 64	7	133	3033	-4.33	2.16	-0.03
57	SLU 65	7	133	3033	-4.33	2.16	-0.03
57	SLU 66	7	133	3033	-4.33	2.16	-0.03
57	SLU 67	7	133	3033	-4.33	2.16	-0.03
57	SLU 68	7	133	3033	-4.33	2.16	-0.03
57	SLU 69	7	133	3033	-4.33	2.16	-0.03
57	SLU 70	7	133	3033	-4.33	2.16	-0.03
57	SLU 71	7	133	3033	-4.33	2.16	-0.03
57	SLU 72	7	133	3033	-4.33	2.16	-0.03
57	SLU 73	8	169	3528	-5.48	2.66	-0.03
57	SLU 74	8	169	3528	-5.48	2.66	-0.03
57	SLU 75	8	169	3528	-5.48	2.66	-0.03
57	SLU 76	8	169	3528	-5.48	2.66	-0.03
57	SLU 77	8	169	3528	-5.48	2.66	-0.03



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
57	SLU 78	8	169	3528	-5.48	2.66	-0.03
57	SLU 79	8	169	3528	-5.48	2.66	-0.03
57	SLU 80	8	169	3528	-5.48	2.66	-0.03
57	SLU 81	9	185	3741	-5.97	2.87	-0.03
57	SLU 82	9	185	3741	-5.97	2.87	-0.03
57	SLU 83	9	185	3741	-5.97	2.87	-0.03
57	SLU 84	9	185	3741	-5.97	2.87	-0.03
57	SLE RA 1	5	97	2270	-3.16	1.59	-0.02
57	SLE RA 2	5	97	2270	-3.16	1.59	-0.02
57	SLE RA 3	5	97	2270	-3.16	1.59	-0.02
57	SLE RA 4	5	97	2270	-3.16	1.59	-0.02
57	SLE RA 5	5	97	2270	-3.16	1.59	-0.02
57	SLE RA 6	5	97	2270	-3.16	1.59	-0.02
57	SLE RA 7	5	97	2270	-3.16	1.59	-0.02
57	SLE RA 8	5	97	2270	-3.16	1.59	-0.02
57	SLE RA 9	5	97	2270	-3.16	1.59	-0.02
57	SLE RA 10	6	121	2601	-3.92	1.92	-0.02
57	SLE RA 11	6	121	2601	-3.92	1.92	-0.02
57	SLE RA 12	6	121	2601	-3.92	1.92	-0.02
57	SLE RA 13	6	121	2601	-3.92	1.92	-0.02
57	SLE RA 14	6	121	2601	-3.92	1.92	-0.02
57	SLE RA 15	6	121	2601	-3.92	1.92	-0.02
57	SLE RA 16	6	121	2601	-3.92	1.92	-0.02
57	SLE RA 17	6	121	2601	-3.92	1.92	-0.02
57	SLE RA 18	6	132	2742	-4.25	2.06	-0.02
57	SLE RA 19	6	132	2742	-4.25	2.06	-0.02
57	SLE RA 20	6	132	2742	-4.25	2.06	-0.02
57	SLE RA 21	6	132	2742	-4.25	2.06	-0.02
57	SLE FR 1	5	97	2270	-3.16	1.59	-0.02
57	SLE FR 2	5	97	2270	-3.16	1.59	-0.02
57	SLE FR 3	5	97	2270	-3.16	1.59	-0.02
57	SLE FR 4	5	108	2412	-3.48	1.73	-0.02
57	SLE FR 5	5	108	2412	-3.48	1.73	-0.02
57	SLE FR 6	6	114	2506	-3.7	1.82	-0.02
57	SLE QP 1	5	97	2270	-3.16	1.59	-0.02
57	SLE QP 2	5	108	2412	-3.48	1.73	-0.02
57	SLD 1	1	284	2631	-10.82	7.06	-0.03
57	SLD 2	1	284	2631	-10.82	7.06	-0.03
57	SLD 3	-7	113	2605	-3.7	3.74	-0.04
57	SLD 4	-7	113	2605	-3.7	3.74	-0.04
57	SLD 5	16	420	2517	-16.48	8.36	-0.01
57	SLD 6	16	420	2517	-16.48	8.36	-0.01
57	SLD 7	-10	-150	2430	7.24	-2.7	-0.04
57	SLD 8	-10	-150	2430	7.24	-2.7	-0.04
57	SLD 9	21	366	2393	-14.21	6.15	0
57	SLD 10	21	366	2393	-14.21	6.15	0
57	SLD 11	-5	-205	2306	9.51	-4.9	-0.03
57	SLD 12	-5	-205	2306	9.51	-4.9	-0.03
57	SLD 13	18	102	2218	-3.27	-0.28	0
57	SLD 14	18	102	2218	-3.27	-0.28	0
57	SLD 15	10	-69	2192	3.85	-3.6	-0.01
57	SLD 16	10	-69	2192	3.85	-3.6	-0.01
57	SLV 1	-5	524	2939	-20.73	15.05	-0.05
57	SLV 2	-5	524	2939	-20.73	15.05	-0.05
57	SLV 3	-25	122	2877	-4.03	6.56	-0.07
57	SLV 4	-25	122	2877	-4.03	6.56	-0.07
57	SLV 5	32	842	2665	-33.98	18.6	0.01
57	SLV 6	32	842	2665	-33.98	18.6	0.01
57	SLV 7	-34	-498	2456	21.67	-9.69	-0.08
57	SLV 8	-34	-498	2456	21.67	-9.69	-0.08
57	SLV 9	44	713	2367	-28.64	13.15	0.04
57	SLV 10	44	713	2367	-28.64	13.15	0.04
57	SLV 11	-21	-627	2159	27.01	-15.14	-0.05
57	SLV 12	-21	-627	2159	27.01	-15.14	-0.05
57	SLV 13	35	93	1946	-2.93	-3.11	0.03
57	SLV 14	35	93	1946	-2.93	-3.11	0.03
57	SLV 15	16	-308	1884	13.76	-11.59	0.01
57	SLV 16	16	-308	1884	13.76	-11.59	0.01
58	SLU 1	0	1	936	-0.04	-0.05	0.01
58	SLU 2	0	1	936	-0.04	-0.05	0.01
58	SLU 3	0	1	936	-0.04	-0.05	0.01
58	SLU 4	0	1	936	-0.04	-0.05	0.01
58	SLU 5	0	1	936	-0.04	-0.05	0.01
58	SLU 6	0	1	936	-0.04	-0.05	0.01
58	SLU 7	0	1	936	-0.04	-0.05	0.01
58	SLU 8	0	1	936	-0.04	-0.05	0.01
58	SLU 9	0	1	936	-0.04	-0.05	0.01
58	SLU 10	0	2	1251	-0.08	-0.06	0.02
58	SLU 11	0	2	1251	-0.08	-0.06	0.02
58	SLU 12	0	2	1251	-0.08	-0.06	0.02
58	SLU 13	0	2	1251	-0.08	-0.06	0.02
58	SLU 14	0	2	1251	-0.08	-0.06	0.02
58	SLU 15	0	2	1251	-0.08	-0.06	0.02
58	SLU 16	0	2	1251	-0.08	-0.06	0.02
58	SLU 17	0	2	1251	-0.08	-0.06	0.02
58	SLU 18	0	2	1386	-0.1	-0.07	0.02
58	SLU 19	0	2	1386	-0.1	-0.07	0.02
58	SLU 20	0	2	1386	-0.1	-0.07	0.02
58	SLU 21	0	2	1386	-0.1	-0.07	0.02



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
58	SLU 22	0	1	1124	-0.06	-0.06	0.02
58	SLU 23	0	1	1124	-0.06	-0.06	0.02
58	SLU 24	0	1	1124	-0.06	-0.06	0.02
58	SLU 25	0	1	1124	-0.06	-0.06	0.02
58	SLU 26	0	1	1124	-0.06	-0.06	0.02
58	SLU 27	0	1	1124	-0.06	-0.06	0.02
58	SLU 28	0	1	1124	-0.06	-0.06	0.02
58	SLU 29	0	1	1124	-0.06	-0.06	0.02
58	SLU 30	0	1	1124	-0.06	-0.06	0.02
58	SLU 31	0	2	1439	-0.1	-0.07	0.02
58	SLU 32	0	2	1439	-0.1	-0.07	0.02
58	SLU 33	0	2	1439	-0.1	-0.07	0.02
58	SLU 34	0	2	1439	-0.1	-0.07	0.02
58	SLU 35	0	2	1439	-0.1	-0.07	0.02
58	SLU 36	0	2	1439	-0.1	-0.07	0.02
58	SLU 37	0	2	1439	-0.1	-0.07	0.02
58	SLU 38	0	2	1439	-0.1	-0.07	0.02
58	SLU 39	0	2	1574	-0.11	-0.08	0.02
58	SLU 40	0	2	1574	-0.11	-0.08	0.02
58	SLU 41	0	2	1574	-0.11	-0.08	0.02
58	SLU 42	0	2	1574	-0.11	-0.08	0.02
58	SLU 43	0	1	1152	-0.04	-0.06	0.02
58	SLU 44	0	1	1152	-0.04	-0.06	0.02
58	SLU 45	0	1	1152	-0.04	-0.06	0.02
58	SLU 46	0	1	1152	-0.04	-0.06	0.02
58	SLU 47	0	1	1152	-0.04	-0.06	0.02
58	SLU 48	0	1	1152	-0.04	-0.06	0.02
58	SLU 49	0	1	1152	-0.04	-0.06	0.02
58	SLU 50	0	1	1152	-0.04	-0.06	0.02
58	SLU 51	0	1	1152	-0.04	-0.06	0.02
58	SLU 52	0	2	1467	-0.08	-0.08	0.02
58	SLU 53	0	2	1467	-0.08	-0.08	0.02
58	SLU 54	0	2	1467	-0.08	-0.08	0.02
58	SLU 55	0	2	1467	-0.08	-0.08	0.02
58	SLU 56	0	2	1467	-0.08	-0.08	0.02
58	SLU 57	0	2	1467	-0.08	-0.08	0.02
58	SLU 58	0	2	1467	-0.08	-0.08	0.02
58	SLU 59	0	2	1467	-0.08	-0.08	0.02
58	SLU 60	0	2	1602	-0.1	-0.08	0.02
58	SLU 61	0	2	1602	-0.1	-0.08	0.02
58	SLU 62	0	2	1602	-0.1	-0.08	0.02
58	SLU 63	0	2	1602	-0.1	-0.08	0.02
58	SLU 64	0	2	1340	-0.06	-0.07	0.02
58	SLU 65	0	2	1340	-0.06	-0.07	0.02
58	SLU 66	0	2	1340	-0.06	-0.07	0.02
58	SLU 67	0	2	1340	-0.06	-0.07	0.02
58	SLU 68	0	2	1340	-0.06	-0.07	0.02
58	SLU 69	0	2	1340	-0.06	-0.07	0.02
58	SLU 70	0	2	1340	-0.06	-0.07	0.02
58	SLU 71	0	2	1340	-0.06	-0.07	0.02
58	SLU 72	0	2	1340	-0.06	-0.07	0.02
58	SLU 73	0	2	1655	-0.1	-0.09	0.02
58	SLU 74	0	2	1655	-0.1	-0.09	0.02
58	SLU 75	0	2	1655	-0.1	-0.09	0.02
58	SLU 76	0	2	1655	-0.1	-0.09	0.02
58	SLU 77	0	2	1655	-0.1	-0.09	0.02
58	SLU 78	0	2	1655	-0.1	-0.09	0.02
58	SLU 79	0	2	1655	-0.1	-0.09	0.02
58	SLU 80	0	2	1655	-0.1	-0.09	0.02
58	SLU 81	0	2	1790	-0.12	-0.09	0.02
58	SLU 82	0	2	1790	-0.12	-0.09	0.02
58	SLU 83	0	2	1790	-0.12	-0.09	0.02
58	SLU 84	0	2	1790	-0.12	-0.09	0.02
58	SLE RA 1	0	1	990	-0.04	-0.06	0.01
58	SLE RA 2	0	1	990	-0.04	-0.06	0.01
58	SLE RA 3	0	1	990	-0.04	-0.06	0.01
58	SLE RA 4	0	1	990	-0.04	-0.06	0.01
58	SLE RA 5	0	1	990	-0.04	-0.06	0.01
58	SLE RA 6	0	1	990	-0.04	-0.06	0.01
58	SLE RA 7	0	1	990	-0.04	-0.06	0.01
58	SLE RA 8	0	1	990	-0.04	-0.06	0.01
58	SLE RA 9	0	1	990	-0.04	-0.06	0.01
58	SLE RA 10	0	2	1200	-0.07	-0.06	0.02
58	SLE RA 11	0	2	1200	-0.07	-0.06	0.02
58	SLE RA 12	0	2	1200	-0.07	-0.06	0.02
58	SLE RA 13	0	2	1200	-0.07	-0.06	0.02
58	SLE RA 14	0	2	1200	-0.07	-0.06	0.02
58	SLE RA 15	0	2	1200	-0.07	-0.06	0.02
58	SLE RA 16	0	2	1200	-0.07	-0.06	0.02
58	SLE RA 17	0	2	1200	-0.07	-0.06	0.02
58	SLE RA 18	0	2	1289	-0.08	-0.07	0.02
58	SLE RA 19	0	2	1289	-0.08	-0.07	0.02
58	SLE RA 20	0	2	1289	-0.08	-0.07	0.02
58	SLE RA 21	0	2	1289	-0.08	-0.07	0.02
58	SLE FR 1	0	1	990	-0.04	-0.06	0.01
58	SLE FR 2	0	1	990	-0.04	-0.06	0.01
58	SLE FR 3	0	1	990	-0.04	-0.06	0.01
58	SLE FR 4	0	1	1080	-0.06	-0.06	0.01
58	SLE FR 5	0	1	1080	-0.06	-0.06	0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
58	SLE FR 6	0	1	1140	-0.06	-0.06	0.02
58	SLE QP 1	0	1	990	-0.04	-0.06	0.01
58	SLE QP 2	0	1	1080	-0.06	-0.06	0.01
58	SLD 1	2	-147	1124	-10.41	1.66	-0.07
58	SLD 2	2	-147	1124	-10.41	1.66	-0.07
58	SLD 3	0	283	1080	19.17	0.57	-0.17
58	SLD 4	0	283	1080	19.17	0.57	-0.17
58	SLD 5	3	-695	1160	-48.02	2.12	0.14
58	SLD 6	3	-695	1160	-48.02	2.12	0.14
58	SLD 7	-3	737	1012	50.57	-1.53	-0.19
58	SLD 8	-3	737	1012	50.57	-1.53	-0.19
58	SLD 9	2	-735	1147	-50.68	1.41	0.22
58	SLD 10	2	-735	1147	-50.68	1.41	0.22
58	SLD 11	-4	698	999	47.91	-2.23	-0.11
58	SLD 12	-4	698	999	47.91	-2.23	-0.11
58	SLD 13	-1	-280	1080	-19.28	-0.68	0.2
58	SLD 14	-1	-280	1080	-19.28	-0.68	0.2
58	SLD 15	-2	150	1035	10.3	-1.78	0.1
58	SLD 16	-2	150	1035	10.3	-1.78	0.1
58	SLV 1	5	-380	1190	-26.62	4.32	-0.2
58	SLV 2	5	-380	1190	-26.62	4.32	-0.2
58	SLV 3	1	723	1076	49.26	1.52	-0.45
58	SLV 4	1	723	1076	49.26	1.52	-0.45
58	SLV 5	9	-1785	1285	-123.11	5.51	0.33
58	SLV 6	9	-1785	1285	-123.11	5.51	0.33
58	SLV 7	-7	1890	906	129.82	-3.84	-0.51
58	SLV 8	-7	1890	906	129.82	-3.84	-0.51
58	SLV 9	7	-1887	1253	-129.93	3.72	0.53
58	SLV 10	7	-1887	1253	-129.93	3.72	0.53
58	SLV 11	-9	1787	874	123	-5.62	-0.3
58	SLV 12	-9	1787	874	123	-5.62	-0.3
58	SLV 13	-1	-720	1083	-49.37	-1.63	0.48
58	SLV 14	-1	-720	1083	-49.37	-1.63	0.48
58	SLV 15	-6	382	970	26.51	-4.44	0.23
58	SLV 16	-6	382	970	26.51	-4.44	0.23
59	SLU 1	-5	127	2199	-4.62	-1.5	0.01
59	SLU 2	-5	127	2199	-4.62	-1.5	0.01
59	SLU 3	-5	127	2199	-4.62	-1.5	0.01
59	SLU 4	-5	127	2199	-4.62	-1.5	0.01
59	SLU 5	-5	127	2199	-4.62	-1.5	0.01
59	SLU 6	-5	127	2199	-4.62	-1.5	0.01
59	SLU 7	-5	127	2199	-4.62	-1.5	0.01
59	SLU 8	-5	127	2199	-4.62	-1.5	0.01
59	SLU 9	-5	127	2199	-4.62	-1.5	0.01
59	SLU 10	-7	179	2706	-6.48	-2.09	0.01
59	SLU 11	-7	179	2706	-6.48	-2.09	0.01
59	SLU 12	-7	179	2706	-6.48	-2.09	0.01
59	SLU 13	-7	179	2706	-6.48	-2.09	0.01
59	SLU 14	-7	179	2706	-6.48	-2.09	0.01
59	SLU 15	-7	179	2706	-6.48	-2.09	0.01
59	SLU 16	-7	179	2706	-6.48	-2.09	0.01
59	SLU 17	-7	179	2706	-6.48	-2.09	0.01
59	SLU 18	-7	201	2923	-7.28	-2.34	0.01
59	SLU 19	-7	201	2923	-7.28	-2.34	0.01
59	SLU 20	-7	201	2923	-7.28	-2.34	0.01
59	SLU 21	-7	201	2923	-7.28	-2.34	0.01
59	SLU 22	-6	156	2476	-5.65	-1.85	0.01
59	SLU 23	-6	156	2476	-5.65	-1.85	0.01
59	SLU 24	-6	156	2476	-5.65	-1.85	0.01
59	SLU 25	-6	156	2476	-5.65	-1.85	0.01
59	SLU 26	-6	156	2476	-5.65	-1.85	0.01
59	SLU 27	-6	156	2476	-5.65	-1.85	0.01
59	SLU 28	-6	156	2476	-5.65	-1.85	0.01
59	SLU 29	-6	156	2476	-5.65	-1.85	0.01
59	SLU 30	-6	156	2476	-5.65	-1.85	0.01
59	SLU 31	-8	209	2983	-7.51	-2.44	0.01
59	SLU 32	-8	209	2983	-7.51	-2.44	0.01
59	SLU 33	-8	209	2983	-7.51	-2.44	0.01
59	SLU 34	-8	209	2983	-7.51	-2.44	0.01
59	SLU 35	-8	209	2983	-7.51	-2.44	0.01
59	SLU 36	-8	209	2983	-7.51	-2.44	0.01
59	SLU 37	-8	209	2983	-7.51	-2.44	0.01
59	SLU 38	-8	209	2983	-7.51	-2.44	0.01
59	SLU 39	-8	231	3200	-8.31	-2.69	0.01
59	SLU 40	-8	231	3200	-8.31	-2.69	0.01
59	SLU 41	-8	231	3200	-8.31	-2.69	0.01
59	SLU 42	-8	231	3200	-8.31	-2.69	0.01
59	SLU 43	-6	154	2764	-5.65	-1.83	0.01
59	SLU 44	-6	154	2764	-5.65	-1.83	0.01
59	SLU 45	-6	154	2764	-5.65	-1.83	0.01
59	SLU 46	-6	154	2764	-5.65	-1.83	0.01
59	SLU 47	-6	154	2764	-5.65	-1.83	0.01
59	SLU 48	-6	154	2764	-5.65	-1.83	0.01
59	SLU 49	-6	154	2764	-5.65	-1.83	0.01
59	SLU 50	-6	154	2764	-5.65	-1.83	0.01
59	SLU 51	-6	154	2764	-5.65	-1.83	0.01
59	SLU 52	-8	207	3271	-7.51	-2.42	0.01
59	SLU 53	-8	207	3271	-7.51	-2.42	0.01
59	SLU 54	-8	207	3271	-7.51	-2.42	0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
59	SLU 55	-8	207	3271	-7.51	-2.42	0.01
59	SLU 56	-8	207	3271	-7.51	-2.42	0.01
59	SLU 57	-8	207	3271	-7.51	-2.42	0.01
59	SLU 58	-8	207	3271	-7.51	-2.42	0.01
59	SLU 59	-8	207	3271	-7.51	-2.42	0.01
59	SLU 60	-8	229	3488	-8.31	-2.67	0.01
59	SLU 61	-8	229	3488	-8.31	-2.67	0.01
59	SLU 62	-8	229	3488	-8.31	-2.67	0.01
59	SLU 63	-8	229	3488	-8.31	-2.67	0.01
59	SLU 64	-7	184	3041	-6.68	-2.18	0.01
59	SLU 65	-7	184	3041	-6.68	-2.18	0.01
59	SLU 66	-7	184	3041	-6.68	-2.18	0.01
59	SLU 67	-7	184	3041	-6.68	-2.18	0.01
59	SLU 68	-7	184	3041	-6.68	-2.18	0.01
59	SLU 69	-7	184	3041	-6.68	-2.18	0.01
59	SLU 70	-7	184	3041	-6.68	-2.18	0.01
59	SLU 71	-7	184	3041	-6.68	-2.18	0.01
59	SLU 72	-7	184	3041	-6.68	-2.18	0.01
59	SLU 73	-9	236	3547	-8.54	-2.77	0.02
59	SLU 74	-9	236	3547	-8.54	-2.77	0.02
59	SLU 75	-9	236	3547	-8.54	-2.77	0.02
59	SLU 76	-9	236	3547	-8.54	-2.77	0.02
59	SLU 77	-9	236	3547	-8.54	-2.77	0.02
59	SLU 78	-9	236	3547	-8.54	-2.77	0.02
59	SLU 79	-9	236	3547	-8.54	-2.77	0.02
59	SLU 80	-9	236	3547	-8.54	-2.77	0.02
59	SLU 81	-9	259	3764	-9.34	-3.02	0.02
59	SLU 82	-9	259	3764	-9.34	-3.02	0.02
59	SLU 83	-9	259	3764	-9.34	-3.02	0.02
59	SLU 84	-9	259	3764	-9.34	-3.02	0.02
59	SLE RA 1	-5	135	2278	-4.91	-1.6	0.01
59	SLE RA 2	-5	135	2278	-4.91	-1.6	0.01
59	SLE RA 3	-5	135	2278	-4.91	-1.6	0.01
59	SLE RA 4	-5	135	2278	-4.91	-1.6	0.01
59	SLE RA 5	-5	135	2278	-4.91	-1.6	0.01
59	SLE RA 6	-5	135	2278	-4.91	-1.6	0.01
59	SLE RA 7	-5	135	2278	-4.91	-1.6	0.01
59	SLE RA 8	-5	135	2278	-4.91	-1.6	0.01
59	SLE RA 9	-5	135	2278	-4.91	-1.6	0.01
59	SLE RA 10	-6	170	2616	-6.15	-1.99	0.01
59	SLE RA 11	-6	170	2616	-6.15	-1.99	0.01
59	SLE RA 12	-6	170	2616	-6.15	-1.99	0.01
59	SLE RA 13	-6	170	2616	-6.15	-1.99	0.01
59	SLE RA 14	-6	170	2616	-6.15	-1.99	0.01
59	SLE RA 15	-6	170	2616	-6.15	-1.99	0.01
59	SLE RA 16	-6	170	2616	-6.15	-1.99	0.01
59	SLE RA 17	-6	170	2616	-6.15	-1.99	0.01
59	SLE RA 18	-7	185	2761	-6.69	-2.16	0.01
59	SLE RA 19	-7	185	2761	-6.69	-2.16	0.01
59	SLE RA 20	-7	185	2761	-6.69	-2.16	0.01
59	SLE RA 21	-7	185	2761	-6.69	-2.16	0.01
59	SLE FR 1	-5	135	2278	-4.91	-1.6	0.01
59	SLE FR 2	-5	135	2278	-4.91	-1.6	0.01
59	SLE FR 3	-5	135	2278	-4.91	-1.6	0.01
59	SLE FR 4	-6	150	2423	-5.45	-1.77	0.01
59	SLE FR 5	-6	150	2423	-5.45	-1.77	0.01
59	SLE FR 6	-6	160	2520	-5.8	-1.88	0.01
59	SLE QP 1	-5	135	2278	-4.91	-1.6	0.01
59	SLE QP 2	-6	150	2423	-5.45	-1.77	0.01
59	SLD 1	-22	141	2227	-5.15	-1.43	-0.04
59	SLD 2	-22	141	2227	-5.15	-1.43	-0.04
59	SLD 3	-10	-6	2194	0.85	4.1	0
59	SLD 4	-10	-6	2194	0.85	4.1	0
59	SLD 5	-28	369	2414	-14.45	-10.05	-0.06
59	SLD 6	-28	369	2414	-14.45	-10.05	-0.06
59	SLD 7	11	-119	2305	5.53	8.38	0.06
59	SLD 8	11	-119	2305	5.53	8.38	0.06
59	SLD 9	-22	419	2541	-16.43	-11.91	-0.04
59	SLD 10	-22	419	2541	-16.43	-11.91	-0.04
59	SLD 11	17	-69	2433	3.56	6.51	0.08
59	SLD 12	17	-69	2433	3.56	6.51	0.08
59	SLD 13	-1	306	2652	-11.74	-7.64	0.02
59	SLD 14	-1	306	2652	-11.74	-7.64	0.02
59	SLD 15	11	159	2619	-5.74	-2.11	0.06
59	SLD 16	11	159	2619	-5.74	-2.11	0.06
59	SLV 1	-46	127	1957	-4.72	-1.19	-0.12
59	SLV 2	-46	127	1957	-4.72	-1.19	-0.12
59	SLV 3	-15	-216	1879	9.35	12.97	-0.03
59	SLV 4	-15	-216	1879	9.35	12.97	-0.03
59	SLV 5	-64	664	2401	-26.58	-23.08	-0.18
59	SLV 6	-64	664	2401	-26.58	-23.08	-0.18
59	SLV 7	38	-481	2142	20.34	24.14	0.15
59	SLV 8	38	-481	2142	20.34	24.14	0.15
59	SLV 9	-49	781	2704	-31.23	-27.67	-0.13
59	SLV 10	-49	781	2704	-31.23	-27.67	-0.13
59	SLV 11	53	-364	2445	15.69	19.54	0.2
59	SLV 12	53	-364	2445	15.69	19.54	0.2
59	SLV 13	4	516	2967	-20.24	-16.51	0.04
59	SLV 14	4	516	2967	-20.24	-16.51	0.04



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
59	SLV 15	35	173	2889	-6.17	-2.35	0.14
59	SLV 16	35	173	2889	-6.17	-2.35	0.14
60	SLU 1	390	4	3266	-0.26	14.84	0
60	SLU 2	390	4	3266	-0.26	14.84	0
60	SLU 3	390	4	3266	-0.26	14.84	0
60	SLU 4	390	4	3266	-0.26	14.84	0
60	SLU 5	390	4	3266	-0.26	14.84	0
60	SLU 6	390	4	3266	-0.26	14.84	0
60	SLU 7	390	4	3266	-0.26	14.84	0
60	SLU 8	390	4	3266	-0.26	14.84	0
60	SLU 9	390	4	3266	-0.26	14.84	0
60	SLU 10	515	6	4062	-0.37	19.88	0
60	SLU 11	515	6	4062	-0.37	19.88	0
60	SLU 12	515	6	4062	-0.37	19.88	0
60	SLU 13	515	6	4062	-0.37	19.88	0
60	SLU 14	515	6	4062	-0.37	19.88	0
60	SLU 15	515	6	4062	-0.37	19.88	0
60	SLU 16	515	6	4062	-0.37	19.88	0
60	SLU 17	515	6	4062	-0.37	19.88	0
60	SLU 18	568	8	4403	-0.42	22.04	0
60	SLU 19	568	8	4403	-0.42	22.04	0
60	SLU 20	568	8	4403	-0.42	22.04	0
60	SLU 21	568	8	4403	-0.42	22.04	0
60	SLU 22	472	5	3740	-0.33	18.18	0
60	SLU 23	472	5	3740	-0.33	18.18	0
60	SLU 24	472	5	3740	-0.33	18.18	0
60	SLU 25	472	5	3740	-0.33	18.18	0
60	SLU 26	472	5	3740	-0.33	18.18	0
60	SLU 27	472	5	3740	-0.33	18.18	0
60	SLU 28	472	5	3740	-0.33	18.18	0
60	SLU 29	472	5	3740	-0.33	18.18	0
60	SLU 30	472	5	3740	-0.33	18.18	0
60	SLU 31	596	8	4536	-0.44	23.22	0
60	SLU 32	596	8	4536	-0.44	23.22	0
60	SLU 33	596	8	4536	-0.44	23.22	0
60	SLU 34	596	8	4536	-0.44	23.22	0
60	SLU 35	596	8	4536	-0.44	23.22	0
60	SLU 36	596	8	4536	-0.44	23.22	0
60	SLU 37	596	8	4536	-0.44	23.22	0
60	SLU 38	596	8	4536	-0.44	23.22	0
60	SLU 39	650	9	4877	-0.49	25.38	0
60	SLU 40	650	9	4877	-0.49	25.38	0
60	SLU 41	650	9	4877	-0.49	25.38	0
60	SLU 42	650	9	4877	-0.49	25.38	0
60	SLU 43	479	5	4083	-0.32	18.14	0
60	SLU 44	479	5	4083	-0.32	18.14	0
60	SLU 45	479	5	4083	-0.32	18.14	0
60	SLU 46	479	5	4083	-0.32	18.14	0
60	SLU 47	479	5	4083	-0.32	18.14	0
60	SLU 48	479	5	4083	-0.32	18.14	0
60	SLU 49	479	5	4083	-0.32	18.14	0
60	SLU 50	479	5	4083	-0.32	18.14	0
60	SLU 51	479	5	4083	-0.32	18.14	0
60	SLU 52	603	7	4879	-0.43	23.18	0
60	SLU 53	603	7	4879	-0.43	23.18	0
60	SLU 54	603	7	4879	-0.43	23.18	0
60	SLU 55	603	7	4879	-0.43	23.18	0
60	SLU 56	603	7	4879	-0.43	23.18	0
60	SLU 57	603	7	4879	-0.43	23.18	0
60	SLU 58	603	7	4879	-0.43	23.18	0
60	SLU 59	603	7	4879	-0.43	23.18	0
60	SLU 60	657	8	5220	-0.48	25.34	0
60	SLU 61	657	8	5220	-0.48	25.34	0
60	SLU 62	657	8	5220	-0.48	25.34	0
60	SLU 63	657	8	5220	-0.48	25.34	0
60	SLU 64	561	6	4557	-0.39	21.49	0
60	SLU 65	561	6	4557	-0.39	21.49	0
60	SLU 66	561	6	4557	-0.39	21.49	0
60	SLU 67	561	6	4557	-0.39	21.49	0
60	SLU 68	561	6	4557	-0.39	21.49	0
60	SLU 69	561	6	4557	-0.39	21.49	0
60	SLU 70	561	6	4557	-0.39	21.49	0
60	SLU 71	561	6	4557	-0.39	21.49	0
60	SLU 72	561	6	4557	-0.39	21.49	0
60	SLU 73	685	9	5353	-0.5	26.53	0
60	SLU 74	685	9	5353	-0.5	26.53	0
60	SLU 75	685	9	5353	-0.5	26.53	0
60	SLU 76	685	9	5353	-0.5	26.53	0
60	SLU 77	685	9	5353	-0.5	26.53	0
60	SLU 78	685	9	5353	-0.5	26.53	0
60	SLU 79	685	9	5353	-0.5	26.53	0
60	SLU 80	685	9	5353	-0.5	26.53	0
60	SLU 81	739	10	5695	-0.55	28.68	0
60	SLU 82	739	10	5695	-0.55	28.68	0
60	SLU 83	739	10	5695	-0.55	28.68	0
60	SLU 84	739	10	5695	-0.55	28.68	0
60	SLE RA 1	413	4	3401	-0.28	15.79	0
60	SLE RA 2	413	4	3401	-0.28	15.79	0
60	SLE RA 3	413	4	3401	-0.28	15.79	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
60	SLE RA 4	413	4	3401	-0.28	15.79	0
60	SLE RA 5	413	4	3401	-0.28	15.79	0
60	SLE RA 6	413	4	3401	-0.28	15.79	0
60	SLE RA 7	413	4	3401	-0.28	15.79	0
60	SLE RA 8	413	4	3401	-0.28	15.79	0
60	SLE RA 9	413	4	3401	-0.28	15.79	0
60	SLE RA 10	496	6	3932	-0.36	19.15	0
60	SLE RA 11	496	6	3932	-0.36	19.15	0
60	SLE RA 12	496	6	3932	-0.36	19.15	0
60	SLE RA 13	496	6	3932	-0.36	19.15	0
60	SLE RA 14	496	6	3932	-0.36	19.15	0
60	SLE RA 15	496	6	3932	-0.36	19.15	0
60	SLE RA 16	496	6	3932	-0.36	19.15	0
60	SLE RA 17	496	6	3932	-0.36	19.15	0
60	SLE RA 18	532	7	4160	-0.39	20.59	0
60	SLE RA 19	532	7	4160	-0.39	20.59	0
60	SLE RA 20	532	7	4160	-0.39	20.59	0
60	SLE RA 21	532	7	4160	-0.39	20.59	0
60	SLE FR 1	413	4	3401	-0.28	15.79	0
60	SLE FR 2	413	4	3401	-0.28	15.79	0
60	SLE FR 3	413	4	3401	-0.28	15.79	0
60	SLE FR 4	449	5	3629	-0.32	17.23	0
60	SLE FR 5	449	5	3629	-0.32	17.23	0
60	SLE FR 6	473	5	3780	-0.34	18.19	0
60	SLE QP 1	413	4	3401	-0.28	15.79	0
60	SLE QP 2	449	5	3629	-0.32	17.23	0
60	SLD 1	575	3	4091	-0.24	23.12	0
60	SLD 2	575	3	4091	-0.24	23.12	0
60	SLD 3	592	-170	4038	7.01	23.91	-0.02
60	SLD 4	592	-170	4038	7.01	23.91	-0.02
60	SLD 5	461	267	3847	-11.29	17.81	0.03
60	SLD 6	461	267	3847	-11.29	17.81	0.03
60	SLD 7	517	-310	3672	12.88	20.43	-0.04
60	SLD 8	517	-310	3672	12.88	20.43	-0.04
60	SLD 9	381	319	3585	-13.51	14.04	0.04
60	SLD 10	381	319	3585	-13.51	14.04	0.04
60	SLD 11	436	-257	3411	10.66	16.66	-0.04
60	SLD 12	436	-257	3411	10.66	16.66	-0.04
60	SLD 13	306	179	3219	-7.64	10.56	0.02
60	SLD 14	306	179	3219	-7.64	10.56	0.02
60	SLD 15	323	7	3166	-0.39	11.34	-0.01
60	SLD 16	323	7	3166	-0.39	11.34	-0.01
60	SLV 1	747	0	4737	-0.1	31.14	0.01
60	SLV 2	747	0	4737	-0.1	31.14	0.01
60	SLV 3	787	-406	4612	16.94	33	-0.05
60	SLV 4	787	-406	4612	16.94	33	-0.05
60	SLV 5	479	619	4150	-26.09	18.58	0.09
60	SLV 6	479	619	4150	-26.09	18.58	0.09
60	SLV 7	610	-733	3735	30.7	24.78	-0.11
60	SLV 8	610	-733	3735	30.7	24.78	-0.11
60	SLV 9	288	743	3522	-31.33	9.68	0.1
60	SLV 10	288	743	3522	-31.33	9.68	0.1
60	SLV 11	419	-609	3107	25.46	15.88	-0.09
60	SLV 12	419	-609	3107	25.46	15.88	-0.09
60	SLV 13	111	416	2645	-17.57	1.47	0.05
60	SLV 14	111	416	2645	-17.57	1.47	0.05
60	SLV 15	150	10	2520	-0.53	3.33	-0.01
60	SLV 16	150	10	2520	-0.53	3.33	-0.01
61	SLU 1	471	0	1507	0	20.47	0
61	SLU 2	471	0	1507	0	20.47	0
61	SLU 3	471	0	1507	0	20.47	0
61	SLU 4	471	0	1507	0	20.47	0
61	SLU 5	471	0	1507	0	20.47	0
61	SLU 6	471	0	1507	0	20.47	0
61	SLU 7	471	0	1507	0	20.47	0
61	SLU 8	471	0	1507	0	20.47	0
61	SLU 9	471	0	1507	0	20.47	0
61	SLU 10	638	0	1874	0	27.69	0
61	SLU 11	638	0	1874	0	27.69	0
61	SLU 12	638	0	1874	0	27.69	0
61	SLU 13	638	0	1874	0	27.69	0
61	SLU 14	638	0	1874	0	27.69	0
61	SLU 15	638	0	1874	0	27.69	0
61	SLU 16	638	0	1874	0	27.69	0
61	SLU 17	638	0	1874	0	27.69	0
61	SLU 18	709	0	2032	0	30.78	0
61	SLU 19	709	0	2032	0	30.78	0
61	SLU 20	709	0	2032	0	30.78	0
61	SLU 21	709	0	2032	0	30.78	0
61	SLU 22	586	0	1739	0	25.38	0
61	SLU 23	586	0	1739	0	25.38	0
61	SLU 24	586	0	1739	0	25.38	0
61	SLU 25	586	0	1739	0	25.38	0
61	SLU 26	586	0	1739	0	25.38	0
61	SLU 27	586	0	1739	0	25.38	0
61	SLU 28	586	0	1739	0	25.38	0
61	SLU 29	586	0	1739	0	25.38	0
61	SLU 30	586	0	1739	0	25.38	0
61	SLU 31	753	0	2106	0	32.59	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
61	SLU 32	753	0	2106	0	32.59	0
61	SLU 33	753	0	2106	0	32.59	0
61	SLU 34	753	0	2106	0	32.59	0
61	SLU 35	753	0	2106	0	32.59	0
61	SLU 36	753	0	2106	0	32.59	0
61	SLU 37	753	0	2106	0	32.59	0
61	SLU 38	753	0	2106	0	32.59	0
61	SLU 39	824	0	2264	0	35.68	0
61	SLU 40	824	0	2264	0	35.68	0
61	SLU 41	824	0	2264	0	35.68	0
61	SLU 42	824	0	2264	0	35.68	0
61	SLU 43	573	0	1880	0	24.93	0
61	SLU 44	573	0	1880	0	24.93	0
61	SLU 45	573	0	1880	0	24.93	0
61	SLU 46	573	0	1880	0	24.93	0
61	SLU 47	573	0	1880	0	24.93	0
61	SLU 48	573	0	1880	0	24.93	0
61	SLU 49	573	0	1880	0	24.93	0
61	SLU 50	573	0	1880	0	24.93	0
61	SLU 51	573	0	1880	0	24.93	0
61	SLU 52	740	0	2247	0	32.15	0
61	SLU 53	740	0	2247	0	32.15	0
61	SLU 54	740	0	2247	0	32.15	0
61	SLU 55	740	0	2247	0	32.15	0
61	SLU 56	740	0	2247	0	32.15	0
61	SLU 57	740	0	2247	0	32.15	0
61	SLU 58	740	0	2247	0	32.15	0
61	SLU 59	740	0	2247	0	32.15	0
61	SLU 60	811	0	2404	0	35.24	0
61	SLU 61	811	0	2404	0	35.24	0
61	SLU 62	811	0	2404	0	35.24	0
61	SLU 63	811	0	2404	0	35.24	0
61	SLU 64	688	0	2112	0	29.84	0
61	SLU 65	688	0	2112	0	29.84	0
61	SLU 66	688	0	2112	0	29.84	0
61	SLU 67	688	0	2112	0	29.84	0
61	SLU 68	688	0	2112	0	29.84	0
61	SLU 69	688	0	2112	0	29.84	0
61	SLU 70	688	0	2112	0	29.84	0
61	SLU 71	688	0	2112	0	29.84	0
61	SLU 72	688	0	2112	0	29.84	0
61	SLU 73	855	0	2479	0	37.05	0
61	SLU 74	855	0	2479	0	37.05	0
61	SLU 75	855	0	2479	0	37.05	0
61	SLU 76	855	0	2479	0	37.05	0
61	SLU 77	855	0	2479	0	37.05	0
61	SLU 78	855	0	2479	0	37.05	0
61	SLU 79	855	0	2479	0	37.05	0
61	SLU 80	855	0	2479	0	37.05	0
61	SLU 81	926	0	2636	0	40.14	0
61	SLU 82	926	0	2636	0	40.14	0
61	SLU 83	926	0	2636	0	40.14	0
61	SLU 84	926	0	2636	0	40.14	0
61	SLE RA 1	504	0	1574	0	21.87	0
61	SLE RA 2	504	0	1574	0	21.87	0
61	SLE RA 3	504	0	1574	0	21.87	0
61	SLE RA 4	504	0	1574	0	21.87	0
61	SLE RA 5	504	0	1574	0	21.87	0
61	SLE RA 6	504	0	1574	0	21.87	0
61	SLE RA 7	504	0	1574	0	21.87	0
61	SLE RA 8	504	0	1574	0	21.87	0
61	SLE RA 9	504	0	1574	0	21.87	0
61	SLE RA 10	615	0	1818	0	26.68	0
61	SLE RA 11	615	0	1818	0	26.68	0
61	SLE RA 12	615	0	1818	0	26.68	0
61	SLE RA 13	615	0	1818	0	26.68	0
61	SLE RA 14	615	0	1818	0	26.68	0
61	SLE RA 15	615	0	1818	0	26.68	0
61	SLE RA 16	615	0	1818	0	26.68	0
61	SLE RA 17	615	0	1818	0	26.68	0
61	SLE RA 18	663	0	1923	0	28.74	0
61	SLE RA 19	663	0	1923	0	28.74	0
61	SLE RA 20	663	0	1923	0	28.74	0
61	SLE RA 21	663	0	1923	0	28.74	0
61	SLE FR 1	504	0	1574	0	21.87	0
61	SLE FR 2	504	0	1574	0	21.87	0
61	SLE FR 3	504	0	1574	0	21.87	0
61	SLE FR 4	552	0	1679	0	23.93	0
61	SLE FR 5	552	0	1679	0	23.93	0
61	SLE FR 6	583	0	1748	0	25.31	0
61	SLE QP 1	504	0	1574	0	21.87	0
61	SLE QP 2	552	0	1679	0	23.93	0
61	SLD 1	760	-1	1823	-1.53	34.74	-0.22
61	SLD 2	760	-1	1823	-1.53	34.74	-0.22
61	SLD 3	789	6	1806	-0.19	36.17	0.1
61	SLD 4	789	6	1806	-0.19	36.17	0.1
61	SLD 5	570	-11	1747	-2.5	25.01	-0.54
61	SLD 6	570	-11	1747	-2.5	25.01	-0.54
61	SLD 7	667	12	1691	1.98	29.77	0.5



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
61	SLD 8	667	12	1691	1.98	29.77	0.5
61	SLD 9	437	-12	1666	-1.99	18.1	-0.5
61	SLD 10	437	-12	1666	-1.99	18.1	-0.5
61	SLD 11	533	11	1610	2.5	22.86	0.54
61	SLD 12	533	11	1610	2.5	22.86	0.54
61	SLD 13	314	-6	1551	0.18	11.7	-0.1
61	SLD 14	314	-6	1551	0.18	11.7	-0.1
61	SLD 15	343	1	1534	1.53	13.13	0.22
61	SLD 16	343	1	1534	1.53	13.13	0.22
61	SLV 1	1046	-3	2026	-3.87	49.83	-0.55
61	SLV 2	1046	-3	2026	-3.87	49.83	-0.55
61	SLV 3	1115	15	1986	-0.44	53.26	0.25
61	SLV 4	1115	15	1986	-0.44	53.26	0.25
61	SLV 5	596	-28	1843	-6.37	26.52	-1.38
61	SLV 6	596	-28	1843	-6.37	26.52	-1.38
61	SLV 7	825	31	1710	5.07	37.92	1.29
61	SLV 8	825	31	1710	5.07	37.92	1.29
61	SLV 9	278	-31	1647	-5.07	9.95	-1.29
61	SLV 10	278	-31	1647	-5.07	9.95	-1.29
61	SLV 11	507	28	1514	6.36	21.35	1.38
61	SLV 12	507	28	1514	6.36	21.35	1.38
61	SLV 13	-12	-15	1371	0.44	-5.39	-0.25
61	SLV 14	-12	-15	1371	0.44	-5.39	-0.25
61	SLV 15	57	3	1331	3.87	-1.96	0.55
61	SLV 16	57	3	1331	3.87	-1.96	0.55
62	SLU 1	387	0	1573	0	13.63	0
62	SLU 2	387	0	1573	0	13.63	0
62	SLU 3	387	0	1573	0	13.63	0
62	SLU 4	387	0	1573	0	13.63	0
62	SLU 5	387	0	1573	0	13.63	0
62	SLU 6	387	0	1573	0	13.63	0
62	SLU 7	387	0	1573	0	13.63	0
62	SLU 8	387	0	1573	0	13.63	0
62	SLU 9	387	0	1573	0	13.63	0
62	SLU 10	538	0	1961	0	19.08	0
62	SLU 11	538	0	1961	0	19.08	0
62	SLU 12	538	0	1961	0	19.08	0
62	SLU 13	538	0	1961	0	19.08	0
62	SLU 14	538	0	1961	0	19.08	0
62	SLU 15	538	0	1961	0	19.08	0
62	SLU 16	538	0	1961	0	19.08	0
62	SLU 17	538	0	1961	0	19.08	0
62	SLU 18	603	0	2128	0.01	21.42	0
62	SLU 19	603	0	2128	0.01	21.42	0
62	SLU 20	603	0	2128	0.01	21.42	0
62	SLU 21	603	0	2128	0.01	21.42	0
62	SLU 22	489	0	1830	0	17.26	0
62	SLU 23	489	0	1830	0	17.26	0
62	SLU 24	489	0	1830	0	17.26	0
62	SLU 25	489	0	1830	0	17.26	0
62	SLU 26	489	0	1830	0	17.26	0
62	SLU 27	489	0	1830	0	17.26	0
62	SLU 28	489	0	1830	0	17.26	0
62	SLU 29	489	0	1830	0	17.26	0
62	SLU 30	489	0	1830	0	17.26	0
62	SLU 31	640	0	2219	0.01	22.71	0
62	SLU 32	640	0	2219	0.01	22.71	0
62	SLU 33	640	0	2219	0.01	22.71	0
62	SLU 34	640	0	2219	0.01	22.71	0
62	SLU 35	640	0	2219	0.01	22.71	0
62	SLU 36	640	0	2219	0.01	22.71	0
62	SLU 37	640	0	2219	0.01	22.71	0
62	SLU 38	640	0	2219	0.01	22.71	0
62	SLU 39	705	0	2386	0.01	25.05	0
62	SLU 40	705	0	2386	0.01	25.05	0
62	SLU 41	705	0	2386	0.01	25.05	0
62	SLU 42	705	0	2386	0.01	25.05	0
62	SLU 43	468	0	1956	0	16.47	0
62	SLU 44	468	0	1956	0	16.47	0
62	SLU 45	468	0	1956	0	16.47	0
62	SLU 46	468	0	1956	0	16.47	0
62	SLU 47	468	0	1956	0	16.47	0
62	SLU 48	468	0	1956	0	16.47	0
62	SLU 49	468	0	1956	0	16.47	0
62	SLU 50	468	0	1956	0	16.47	0
62	SLU 51	468	0	1956	0	16.47	0
62	SLU 52	619	0	2345	0	21.93	0
62	SLU 53	619	0	2345	0	21.93	0
62	SLU 54	619	0	2345	0	21.93	0
62	SLU 55	619	0	2345	0	21.93	0
62	SLU 56	619	0	2345	0	21.93	0
62	SLU 57	619	0	2345	0	21.93	0
62	SLU 58	619	0	2345	0	21.93	0
62	SLU 59	619	0	2345	0	21.93	0
62	SLU 60	684	0	2511	0.01	24.27	0
62	SLU 61	684	0	2511	0.01	24.27	0
62	SLU 62	684	0	2511	0.01	24.27	0
62	SLU 63	684	0	2511	0.01	24.27	0
62	SLU 64	570	0	2214	0	20.1	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
62	SLU 65	570	0	2214	0	20.1	0
62	SLU 66	570	0	2214	0	20.1	0
62	SLU 67	570	0	2214	0	20.1	0
62	SLU 68	570	0	2214	0	20.1	0
62	SLU 69	570	0	2214	0	20.1	0
62	SLU 70	570	0	2214	0	20.1	0
62	SLU 71	570	0	2214	0	20.1	0
62	SLU 72	570	0	2214	0	20.1	0
62	SLU 73	721	0	2603	0	25.56	0
62	SLU 74	721	0	2603	0	25.56	0
62	SLU 75	721	0	2603	0	25.56	0
62	SLU 76	721	0	2603	0	25.56	0
62	SLU 77	721	0	2603	0	25.56	0
62	SLU 78	721	0	2603	0	25.56	0
62	SLU 79	721	0	2603	0	25.56	0
62	SLU 80	721	0	2603	0	25.56	0
62	SLU 81	786	0	2769	0.01	27.89	0
62	SLU 82	786	0	2769	0.01	27.89	0
62	SLU 83	786	0	2769	0.01	27.89	0
62	SLU 84	786	0	2769	0.01	27.89	0
62	SLE RA 1	416	0	1646	0	14.66	0
62	SLE RA 2	416	0	1646	0	14.66	0
62	SLE RA 3	416	0	1646	0	14.66	0
62	SLE RA 4	416	0	1646	0	14.66	0
62	SLE RA 5	416	0	1646	0	14.66	0
62	SLE RA 6	416	0	1646	0	14.66	0
62	SLE RA 7	416	0	1646	0	14.66	0
62	SLE RA 8	416	0	1646	0	14.66	0
62	SLE RA 9	416	0	1646	0	14.66	0
62	SLE RA 10	517	0	1905	0	18.3	0
62	SLE RA 11	517	0	1905	0	18.3	0
62	SLE RA 12	517	0	1905	0	18.3	0
62	SLE RA 13	517	0	1905	0	18.3	0
62	SLE RA 14	517	0	1905	0	18.3	0
62	SLE RA 15	517	0	1905	0	18.3	0
62	SLE RA 16	517	0	1905	0	18.3	0
62	SLE RA 17	517	0	1905	0	18.3	0
62	SLE RA 18	560	0	2017	0	19.86	0
62	SLE RA 19	560	0	2017	0	19.86	0
62	SLE RA 20	560	0	2017	0	19.86	0
62	SLE RA 21	560	0	2017	0	19.86	0
62	SLE FR 1	416	0	1646	0	14.66	0
62	SLE FR 2	416	0	1646	0	14.66	0
62	SLE FR 3	416	0	1646	0	14.66	0
62	SLE FR 4	459	0	1757	0	16.22	0
62	SLE FR 5	459	0	1757	0	16.22	0
62	SLE FR 6	488	0	1831	0	17.26	0
62	SLE QP 1	416	0	1646	0	14.66	0
62	SLE QP 2	459	0	1757	0	16.22	0
62	SLD 1	678	0	1853	-3.79	24.12	0.01
62	SLD 2	678	0	1853	-3.79	24.12	0.01
62	SLD 3	707	6	1841	0.84	25.17	0.08
62	SLD 4	707	6	1841	0.84	25.17	0.08
62	SLD 5	480	-10	1805	-8.15	17	-0.11
62	SLD 6	480	-10	1805	-8.15	17	-0.11
62	SLD 7	578	12	1764	7.27	20.5	0.14
62	SLD 8	578	12	1764	7.27	20.5	0.14
62	SLD 9	340	-12	1751	-7.27	11.94	-0.14
62	SLD 10	340	-12	1751	-7.27	11.94	-0.14
62	SLD 11	438	10	1710	8.15	15.45	0.11
62	SLD 12	438	10	1710	8.15	15.45	0.11
62	SLD 13	211	-6	1674	-0.84	7.27	-0.08
62	SLD 14	211	-6	1674	-0.84	7.27	-0.08
62	SLD 15	240	0	1662	3.79	8.32	-0.01
62	SLD 16	240	0	1662	3.79	8.32	-0.01
62	SLV 1	976	-1	1991	-9.65	34.84	0.02
62	SLV 2	976	-1	1991	-9.65	34.84	0.02
62	SLV 3	1046	16	1962	2.18	37.32	0.21
62	SLV 4	1046	16	1962	2.18	37.32	0.21
62	SLV 5	508	-26	1871	-20.83	18.04	-0.29
62	SLV 6	508	-26	1871	-20.83	18.04	-0.29
62	SLV 7	741	31	1775	18.59	26.32	0.35
62	SLV 8	741	31	1775	18.59	26.32	0.35
62	SLV 9	177	-31	1740	-18.59	6.13	-0.35
62	SLV 10	177	-31	1740	-18.59	6.13	-0.35
62	SLV 11	410	26	1643	20.83	14.4	0.29
62	SLV 12	410	26	1643	20.83	14.4	0.29
62	SLV 13	-128	-16	1553	-2.18	-4.88	-0.21
62	SLV 14	-128	-16	1553	-2.18	-4.88	-0.21
62	SLV 15	-58	1	1524	9.65	-2.4	-0.02
62	SLV 16	-58	1	1524	9.65	-2.4	-0.02
63	SLU 1	312	0	1658	0	9.66	0
63	SLU 2	312	0	1658	0	9.66	0
63	SLU 3	312	0	1658	0	9.66	0
63	SLU 4	312	0	1658	0	9.66	0
63	SLU 5	312	0	1658	0	9.66	0
63	SLU 6	312	0	1658	0	9.66	0
63	SLU 7	312	0	1658	0	9.66	0
63	SLU 8	312	0	1658	0	9.66	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
63	SLU 9	312	0	1658	0	9.66	0
63	SLU 10	442	0	2078	0.01	13.6	0
63	SLU 11	442	0	2078	0.01	13.6	0
63	SLU 12	442	0	2078	0.01	13.6	0
63	SLU 13	442	0	2078	0.01	13.6	0
63	SLU 14	442	0	2078	0.01	13.6	0
63	SLU 15	442	0	2078	0.01	13.6	0
63	SLU 16	442	0	2078	0.01	13.6	0
63	SLU 17	442	0	2078	0.01	13.6	0
63	SLU 18	497	0	2257	0.01	15.29	0
63	SLU 19	497	0	2257	0.01	15.29	0
63	SLU 20	497	0	2257	0.01	15.29	0
63	SLU 21	497	0	2257	0.01	15.29	0
63	SLU 22	399	0	1945	0	12.32	0
63	SLU 23	399	0	1945	0	12.32	0
63	SLU 24	399	0	1945	0	12.32	0
63	SLU 25	399	0	1945	0	12.32	0
63	SLU 26	399	0	1945	0	12.32	0
63	SLU 27	399	0	1945	0	12.32	0
63	SLU 28	399	0	1945	0	12.32	0
63	SLU 29	399	0	1945	0	12.32	0
63	SLU 30	399	0	1945	0	12.32	0
63	SLU 31	529	0	2365	0.01	16.26	0
63	SLU 32	529	0	2365	0.01	16.26	0
63	SLU 33	529	0	2365	0.01	16.26	0
63	SLU 34	529	0	2365	0.01	16.26	0
63	SLU 35	529	0	2365	0.01	16.26	0
63	SLU 36	529	0	2365	0.01	16.26	0
63	SLU 37	529	0	2365	0.01	16.26	0
63	SLU 38	529	0	2365	0.01	16.26	0
63	SLU 39	584	0	2545	0.01	17.95	0
63	SLU 40	584	0	2545	0.01	17.95	0
63	SLU 41	584	0	2545	0.01	17.95	0
63	SLU 42	584	0	2545	0.01	17.95	0
63	SLU 43	376	0	2057	0	11.65	0
63	SLU 44	376	0	2057	0	11.65	0
63	SLU 45	376	0	2057	0	11.65	0
63	SLU 46	376	0	2057	0	11.65	0
63	SLU 47	376	0	2057	0	11.65	0
63	SLU 48	376	0	2057	0	11.65	0
63	SLU 49	376	0	2057	0	11.65	0
63	SLU 50	376	0	2057	0	11.65	0
63	SLU 51	376	0	2057	0	11.65	0
63	SLU 52	506	0	2477	0.01	15.59	0
63	SLU 53	506	0	2477	0.01	15.59	0
63	SLU 54	506	0	2477	0.01	15.59	0
63	SLU 55	506	0	2477	0.01	15.59	0
63	SLU 56	506	0	2477	0.01	15.59	0
63	SLU 57	506	0	2477	0.01	15.59	0
63	SLU 58	506	0	2477	0.01	15.59	0
63	SLU 59	506	0	2477	0.01	15.59	0
63	SLU 60	561	0	2656	0.01	17.28	0
63	SLU 61	561	0	2656	0.01	17.28	0
63	SLU 62	561	0	2656	0.01	17.28	0
63	SLU 63	561	0	2656	0.01	17.28	0
63	SLU 64	463	0	2344	0	14.31	0
63	SLU 65	463	0	2344	0	14.31	0
63	SLU 66	463	0	2344	0	14.31	0
63	SLU 67	463	0	2344	0	14.31	0
63	SLU 68	463	0	2344	0	14.31	0
63	SLU 69	463	0	2344	0	14.31	0
63	SLU 70	463	0	2344	0	14.31	0
63	SLU 71	463	0	2344	0	14.31	0
63	SLU 72	463	0	2344	0	14.31	0
63	SLU 73	593	0	2764	0.01	18.25	0
63	SLU 74	593	0	2764	0.01	18.25	0
63	SLU 75	593	0	2764	0.01	18.25	0
63	SLU 76	593	0	2764	0.01	18.25	0
63	SLU 77	593	0	2764	0.01	18.25	0
63	SLU 78	593	0	2764	0.01	18.25	0
63	SLU 79	593	0	2764	0.01	18.25	0
63	SLU 80	593	0	2764	0.01	18.25	0
63	SLU 81	648	0	2944	0.01	19.94	0
63	SLU 82	648	0	2944	0.01	19.94	0
63	SLU 83	648	0	2944	0.01	19.94	0
63	SLU 84	648	0	2944	0.01	19.94	0
63	SLE RA 1	337	0	1740	0	10.42	0
63	SLE RA 2	337	0	1740	0	10.42	0
63	SLE RA 3	337	0	1740	0	10.42	0
63	SLE RA 4	337	0	1740	0	10.42	0
63	SLE RA 5	337	0	1740	0	10.42	0
63	SLE RA 6	337	0	1740	0	10.42	0
63	SLE RA 7	337	0	1740	0	10.42	0
63	SLE RA 8	337	0	1740	0	10.42	0
63	SLE RA 9	337	0	1740	0	10.42	0
63	SLE RA 10	424	0	2020	0	13.05	0
63	SLE RA 11	424	0	2020	0	13.05	0
63	SLE RA 12	424	0	2020	0	13.05	0
63	SLE RA 13	424	0	2020	0	13.05	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
63	SLE RA 14	424	0	2020	0	13.05	0
63	SLE RA 15	424	0	2020	0	13.05	0
63	SLE RA 16	424	0	2020	0	13.05	0
63	SLE RA 17	424	0	2020	0	13.05	0
63	SLE RA 18	461	0	2140	0.01	14.18	0
63	SLE RA 19	461	0	2140	0.01	14.18	0
63	SLE RA 20	461	0	2140	0.01	14.18	0
63	SLE RA 21	461	0	2140	0.01	14.18	0
63	SLE FR 1	337	0	1740	0	10.42	0
63	SLE FR 2	337	0	1740	0	10.42	0
63	SLE FR 3	337	0	1740	0	10.42	0
63	SLE FR 4	374	0	1860	0	11.55	0
63	SLE FR 5	374	0	1860	0	11.55	0
63	SLE FR 6	399	0	1940	0	12.3	0
63	SLE QP 1	337	0	1740	0	10.42	0
63	SLE QP 2	374	0	1860	0	11.55	0
63	SLD 1	598	0	1932	-7.24	19.09	0.06
63	SLD 2	598	0	1932	-7.24	19.09	0.06
63	SLD 3	628	5	1923	2.99	20.12	0
63	SLD 4	628	5	1923	2.99	20.12	0
63	SLD 5	395	-8	1896	-17.69	12.25	0.11
63	SLD 6	395	-8	1896	-17.69	12.25	0.11
63	SLD 7	496	9	1864	16.42	15.68	-0.09
63	SLD 8	496	9	1864	16.42	15.68	-0.09
63	SLD 9	252	-9	1855	-16.41	7.42	0.09
63	SLD 10	252	-9	1855	-16.41	7.42	0.09
63	SLD 11	353	8	1824	17.69	10.85	-0.11
63	SLD 12	353	8	1824	17.69	10.85	-0.11
63	SLD 13	121	-5	1797	-2.99	2.98	0
63	SLD 14	121	-5	1797	-2.99	2.98	0
63	SLD 15	151	0	1787	7.24	4.01	-0.06
63	SLD 16	151	0	1787	7.24	4.01	-0.06
63	SLV 1	905	0	2037	-18.51	29.6	0.14
63	SLV 2	905	0	2037	-18.51	29.6	0.14
63	SLV 3	976	13	2014	7.68	32.06	-0.01
63	SLV 4	976	13	2014	7.68	32.06	-0.01
63	SLV 5	425	-19	1948	-45.28	13.23	0.27
63	SLV 6	425	-19	1948	-45.28	13.23	0.27
63	SLV 7	663	23	1871	42.03	21.44	-0.23
63	SLV 8	663	23	1871	42.03	21.44	-0.23
63	SLV 9	85	-23	1849	-42.03	1.66	0.23
63	SLV 10	85	-23	1849	-42.03	1.66	0.23
63	SLV 11	324	19	1772	45.28	9.87	-0.27
63	SLV 12	324	19	1772	45.28	9.87	-0.27
63	SLV 13	-228	-13	1706	-7.68	-8.96	0.01
63	SLV 14	-228	-13	1706	-7.68	-8.96	0.01
63	SLV 15	-156	0	1683	18.52	-6.5	-0.14
63	SLV 16	-156	0	1683	18.52	-6.5	-0.14
64	SLU 1	256	0	1726	0	7.67	0
64	SLU 2	256	0	1726	0	7.67	0
64	SLU 3	256	0	1726	0	7.67	0
64	SLU 4	256	0	1726	0	7.67	0
64	SLU 5	256	0	1726	0	7.67	0
64	SLU 6	256	0	1726	0	7.67	0
64	SLU 7	256	0	1726	0	7.67	0
64	SLU 8	256	0	1726	0	7.67	0
64	SLU 9	256	0	1726	0	7.67	0
64	SLU 10	374	0	2173	0.01	11.28	0
64	SLU 11	374	0	2173	0.01	11.28	0
64	SLU 12	374	0	2173	0.01	11.28	0
64	SLU 13	374	0	2173	0.01	11.28	0
64	SLU 14	374	0	2173	0.01	11.28	0
64	SLU 15	374	0	2173	0.01	11.28	0
64	SLU 16	374	0	2173	0.01	11.28	0
64	SLU 17	374	0	2173	0.01	11.28	0
64	SLU 18	424	0	2364	0.01	12.83	0
64	SLU 19	424	0	2364	0.01	12.83	0
64	SLU 20	424	0	2364	0.01	12.83	0
64	SLU 21	424	0	2364	0.01	12.83	0
64	SLU 22	331	0	2037	0	9.91	0
64	SLU 23	331	0	2037	0	9.91	0
64	SLU 24	331	0	2037	0	9.91	0
64	SLU 25	331	0	2037	0	9.91	0
64	SLU 26	331	0	2037	0	9.91	0
64	SLU 27	331	0	2037	0	9.91	0
64	SLU 28	331	0	2037	0	9.91	0
64	SLU 29	331	0	2037	0	9.91	0
64	SLU 30	331	0	2037	0	9.91	0
64	SLU 31	448	0	2484	0.01	13.53	0
64	SLU 32	448	0	2484	0.01	13.53	0
64	SLU 33	448	0	2484	0.01	13.53	0
64	SLU 34	448	0	2484	0.01	13.53	0
64	SLU 35	448	0	2484	0.01	13.53	0
64	SLU 36	448	0	2484	0.01	13.53	0
64	SLU 37	448	0	2484	0.01	13.53	0
64	SLU 38	448	0	2484	0.01	13.53	0
64	SLU 39	499	0	2675	0.01	15.07	0
64	SLU 40	499	0	2675	0.01	15.07	0
64	SLU 41	499	0	2675	0.01	15.07	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
64	SLU 42	499	0	2675	0.01	15.07	0
64	SLU 43	307	0	2138	0	9.2	0
64	SLU 44	307	0	2138	0	9.2	0
64	SLU 45	307	0	2138	0	9.2	0
64	SLU 46	307	0	2138	0	9.2	0
64	SLU 47	307	0	2138	0	9.2	0
64	SLU 48	307	0	2138	0	9.2	0
64	SLU 49	307	0	2138	0	9.2	0
64	SLU 50	307	0	2138	0	9.2	0
64	SLU 51	307	0	2138	0	9.2	0
64	SLU 52	425	0	2584	0.01	12.81	0
64	SLU 53	425	0	2584	0.01	12.81	0
64	SLU 54	425	0	2584	0.01	12.81	0
64	SLU 55	425	0	2584	0.01	12.81	0
64	SLU 56	425	0	2584	0.01	12.81	0
64	SLU 57	425	0	2584	0.01	12.81	0
64	SLU 58	425	0	2584	0.01	12.81	0
64	SLU 59	425	0	2584	0.01	12.81	0
64	SLU 60	475	0	2776	0.01	14.36	0
64	SLU 61	475	0	2776	0.01	14.36	0
64	SLU 62	475	0	2776	0.01	14.36	0
64	SLU 63	475	0	2776	0.01	14.36	0
64	SLU 64	382	0	2449	0	11.44	0
64	SLU 65	382	0	2449	0	11.44	0
64	SLU 66	382	0	2449	0	11.44	0
64	SLU 67	382	0	2449	0	11.44	0
64	SLU 68	382	0	2449	0	11.44	0
64	SLU 69	382	0	2449	0	11.44	0
64	SLU 70	382	0	2449	0	11.44	0
64	SLU 71	382	0	2449	0	11.44	0
64	SLU 72	382	0	2449	0	11.44	0
64	SLU 73	500	0	2895	0.01	15.06	0
64	SLU 74	500	0	2895	0.01	15.06	0
64	SLU 75	500	0	2895	0.01	15.06	0
64	SLU 76	500	0	2895	0.01	15.06	0
64	SLU 77	500	0	2895	0.01	15.06	0
64	SLU 78	500	0	2895	0.01	15.06	0
64	SLU 79	500	0	2895	0.01	15.06	0
64	SLU 80	500	0	2895	0.01	15.06	0
64	SLU 81	550	0	3087	0.01	16.61	0
64	SLU 82	550	0	3087	0.01	16.61	0
64	SLU 83	550	0	3087	0.01	16.61	0
64	SLU 84	550	0	3087	0.01	16.61	0
64	SLE RA 1	278	0	1815	0	8.31	0
64	SLE RA 2	278	0	1815	0	8.31	0
64	SLE RA 3	278	0	1815	0	8.31	0
64	SLE RA 4	278	0	1815	0	8.31	0
64	SLE RA 5	278	0	1815	0	8.31	0
64	SLE RA 6	278	0	1815	0	8.31	0
64	SLE RA 7	278	0	1815	0	8.31	0
64	SLE RA 8	278	0	1815	0	8.31	0
64	SLE RA 9	278	0	1815	0	8.31	0
64	SLE RA 10	356	0	2113	0.01	10.72	0
64	SLE RA 11	356	0	2113	0.01	10.72	0
64	SLE RA 12	356	0	2113	0.01	10.72	0
64	SLE RA 13	356	0	2113	0.01	10.72	0
64	SLE RA 14	356	0	2113	0.01	10.72	0
64	SLE RA 15	356	0	2113	0.01	10.72	0
64	SLE RA 16	356	0	2113	0.01	10.72	0
64	SLE RA 17	356	0	2113	0.01	10.72	0
64	SLE RA 18	389	0	2241	0.01	11.75	0
64	SLE RA 19	389	0	2241	0.01	11.75	0
64	SLE RA 20	389	0	2241	0.01	11.75	0
64	SLE RA 21	389	0	2241	0.01	11.75	0
64	SLE FR 1	278	0	1815	0	8.31	0
64	SLE FR 2	278	0	1815	0	8.31	0
64	SLE FR 3	278	0	1815	0	8.31	0
64	SLE FR 4	311	0	1943	0	9.34	0
64	SLE FR 5	311	0	1943	0	9.34	0
64	SLE FR 6	333	0	2028	0	10.03	0
64	SLE QP 1	278	0	1815	0	8.31	0
64	SLE QP 2	311	0	1943	0	9.34	0
64	SLD 1	527	9	2000	-10.79	15.91	0.06
64	SLD 2	527	9	2000	-10.79	15.91	0.06
64	SLD 3	556	-3	1993	5.24	16.77	-0.02
64	SLD 4	556	-3	1993	5.24	16.77	-0.02
64	SLD 5	332	21	1972	-27.55	10.01	0.15
64	SLD 6	332	21	1972	-27.55	10.01	0.15
64	SLD 7	429	-19	1946	25.89	12.88	-0.13
64	SLD 8	429	-19	1946	25.89	12.88	-0.13
64	SLD 9	194	19	1939	-25.89	5.81	0.13
64	SLD 10	194	19	1939	-25.89	5.81	0.13
64	SLD 11	290	-21	1914	27.56	8.68	-0.15
64	SLD 12	290	-21	1914	27.56	8.68	-0.15
64	SLD 13	66	3	1893	-5.24	1.91	0.02
64	SLD 14	66	3	1893	-5.24	1.91	0.02
64	SLD 15	95	-9	1885	10.79	2.77	-0.06
64	SLD 16	95	-9	1885	10.79	2.77	-0.06
64	SLV 1	821	23	2084	-27.64	24.81	0.16



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
64	SLV 2	821	23	2084	-27.64	24.81	0.16
64	SLV 3	890	-8	2065	13.42	26.84	-0.05
64	SLV 4	890	-8	2065	13.42	26.84	-0.05
64	SLV 5	360	53	2013	-70.57	10.91	0.37
64	SLV 6	360	53	2013	-70.57	10.91	0.37
64	SLV 7	589	-49	1951	66.31	17.67	-0.34
64	SLV 8	589	-49	1951	66.31	17.67	-0.34
64	SLV 9	34	49	1934	-66.3	1.01	0.34
64	SLV 10	34	49	1934	-66.3	1.01	0.34
64	SLV 11	262	-53	1872	70.58	7.78	-0.37
64	SLV 12	262	-53	1872	70.58	7.78	-0.37
64	SLV 13	-267	8	1820	-13.42	-8.16	0.05
64	SLV 14	-267	8	1820	-13.42	-8.16	0.05
64	SLV 15	-199	-23	1802	27.65	-6.13	-0.16
64	SLV 16	-199	-23	1802	27.65	-6.13	-0.16
65	SLU 1	204	0	1781	0	6	0
65	SLU 2	204	0	1781	0	6	0
65	SLU 3	204	0	1781	0	6	0
65	SLU 4	204	0	1781	0	6	0
65	SLU 5	204	0	1781	0	6	0
65	SLU 6	204	0	1781	0	6	0
65	SLU 7	204	0	1781	0	6	0
65	SLU 8	204	0	1781	0	6	0
65	SLU 9	204	0	1781	0	6	0
65	SLU 10	304	0	2252	0.01	8.85	0
65	SLU 11	304	0	2252	0.01	8.85	0
65	SLU 12	304	0	2252	0.01	8.85	0
65	SLU 13	304	0	2252	0.01	8.85	0
65	SLU 14	304	0	2252	0.01	8.85	0
65	SLU 15	304	0	2252	0.01	8.85	0
65	SLU 16	304	0	2252	0.01	8.85	0
65	SLU 17	304	0	2252	0.01	8.85	0
65	SLU 18	347	0	2454	0.01	10.07	0
65	SLU 19	347	0	2454	0.01	10.07	0
65	SLU 20	347	0	2454	0.01	10.07	0
65	SLU 21	347	0	2454	0.01	10.07	0
65	SLU 22	266	0	2112	0	7.8	0
65	SLU 23	266	0	2112	0	7.8	0
65	SLU 24	266	0	2112	0	7.8	0
65	SLU 25	266	0	2112	0	7.8	0
65	SLU 26	266	0	2112	0	7.8	0
65	SLU 27	266	0	2112	0	7.8	0
65	SLU 28	266	0	2112	0	7.8	0
65	SLU 29	266	0	2112	0	7.8	0
65	SLU 30	266	0	2112	0	7.8	0
65	SLU 31	366	0	2583	0.01	10.65	0
65	SLU 32	366	0	2583	0.01	10.65	0
65	SLU 33	366	0	2583	0.01	10.65	0
65	SLU 34	366	0	2583	0.01	10.65	0
65	SLU 35	366	0	2583	0.01	10.65	0
65	SLU 36	366	0	2583	0.01	10.65	0
65	SLU 37	366	0	2583	0.01	10.65	0
65	SLU 38	366	0	2583	0.01	10.65	0
65	SLU 39	409	0	2785	0.01	11.87	0
65	SLU 40	409	0	2785	0.01	11.87	0
65	SLU 41	409	0	2785	0.01	11.87	0
65	SLU 42	409	0	2785	0.01	11.87	0
65	SLU 43	244	0	2202	0	7.18	0
65	SLU 44	244	0	2202	0	7.18	0
65	SLU 45	244	0	2202	0	7.18	0
65	SLU 46	244	0	2202	0	7.18	0
65	SLU 47	244	0	2202	0	7.18	0
65	SLU 48	244	0	2202	0	7.18	0
65	SLU 49	244	0	2202	0	7.18	0
65	SLU 50	244	0	2202	0	7.18	0
65	SLU 51	244	0	2202	0	7.18	0
65	SLU 52	344	0	2673	0.01	10.03	0
65	SLU 53	344	0	2673	0.01	10.03	0
65	SLU 54	344	0	2673	0.01	10.03	0
65	SLU 55	344	0	2673	0.01	10.03	0
65	SLU 56	344	0	2673	0.01	10.03	0
65	SLU 57	344	0	2673	0.01	10.03	0
65	SLU 58	344	0	2673	0.01	10.03	0
65	SLU 59	344	0	2673	0.01	10.03	0
65	SLU 60	387	0	2875	0.01	11.25	0
65	SLU 61	387	0	2875	0.01	11.25	0
65	SLU 62	387	0	2875	0.01	11.25	0
65	SLU 63	387	0	2875	0.01	11.25	0
65	SLU 64	306	0	2533	0	8.98	0
65	SLU 65	306	0	2533	0	8.98	0
65	SLU 66	306	0	2533	0	8.98	0
65	SLU 67	306	0	2533	0	8.98	0
65	SLU 68	306	0	2533	0	8.98	0
65	SLU 69	306	0	2533	0	8.98	0
65	SLU 70	306	0	2533	0	8.98	0
65	SLU 71	306	0	2533	0	8.98	0
65	SLU 72	306	0	2533	0	8.98	0
65	SLU 73	406	0	3004	0.01	11.83	0
65	SLU 74	406	0	3004	0.01	11.83	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
65	SLU 75	406	0	3004	0.01	11.83	0
65	SLU 76	406	0	3004	0.01	11.83	0
65	SLU 77	406	0	3004	0.01	11.83	0
65	SLU 78	406	0	3004	0.01	11.83	0
65	SLU 79	406	0	3004	0.01	11.83	0
65	SLU 80	406	0	3004	0.01	11.83	0
65	SLU 81	449	0	3206	0.01	13.05	0
65	SLU 82	449	0	3206	0.01	13.05	0
65	SLU 83	449	0	3206	0.01	13.05	0
65	SLU 84	449	0	3206	0.01	13.05	0
65	SLE RA 1	222	0	1876	0	6.51	0
65	SLE RA 2	222	0	1876	0	6.51	0
65	SLE RA 3	222	0	1876	0	6.51	0
65	SLE RA 4	222	0	1876	0	6.51	0
65	SLE RA 5	222	0	1876	0	6.51	0
65	SLE RA 6	222	0	1876	0	6.51	0
65	SLE RA 7	222	0	1876	0	6.51	0
65	SLE RA 8	222	0	1876	0	6.51	0
65	SLE RA 9	222	0	1876	0	6.51	0
65	SLE RA 10	288	0	2190	0.01	8.41	0
65	SLE RA 11	288	0	2190	0.01	8.41	0
65	SLE RA 12	288	0	2190	0.01	8.41	0
65	SLE RA 13	288	0	2190	0.01	8.41	0
65	SLE RA 14	288	0	2190	0.01	8.41	0
65	SLE RA 15	288	0	2190	0.01	8.41	0
65	SLE RA 16	288	0	2190	0.01	8.41	0
65	SLE RA 17	288	0	2190	0.01	8.41	0
65	SLE RA 18	317	0	2324	0.01	9.23	0
65	SLE RA 19	317	0	2324	0.01	9.23	0
65	SLE RA 20	317	0	2324	0.01	9.23	0
65	SLE RA 21	317	0	2324	0.01	9.23	0
65	SLE FR 1	222	0	1876	0	6.51	0
65	SLE FR 2	222	0	1876	0	6.51	0
65	SLE FR 3	222	0	1876	0	6.51	0
65	SLE FR 4	250	0	2010	0	7.33	0
65	SLE FR 5	250	0	2010	0	7.33	0
65	SLE FR 6	269	0	2100	0.01	7.87	0
65	SLE QP 1	222	0	1876	0	6.51	0
65	SLE QP 2	250	0	2010	0	7.33	0
65	SLD 1	473	13	2052	-13.72	14.49	0.06
65	SLD 2	473	13	2052	-13.72	14.49	0.06
65	SLD 3	503	-5	2046	7.09	15.44	-0.02
65	SLD 4	503	-5	2046	7.09	15.44	-0.02
65	SLD 5	272	31	2031	-35.69	8.03	0.15
65	SLD 6	272	31	2031	-35.69	8.03	0.15
65	SLD 7	371	-29	2012	33.7	11.21	-0.13
65	SLD 8	371	-29	2012	33.7	11.21	-0.13
65	SLD 9	129	29	2008	-33.69	3.45	0.13
65	SLD 10	129	29	2008	-33.69	3.45	0.13
65	SLD 11	228	-31	1989	35.7	6.63	-0.15
65	SLD 12	228	-31	1989	35.7	6.63	-0.15
65	SLD 13	-2	5	1974	-7.08	-0.79	0.02
65	SLD 14	-2	5	1974	-7.08	-0.79	0.02
65	SLD 15	27	-13	1968	13.73	0.17	-0.06
65	SLD 16	27	-13	1968	13.73	0.17	-0.06
65	SLV 1	779	32	2113	-35.2	24.46	0.16
65	SLV 2	779	32	2113	-35.2	24.46	0.16
65	SLV 3	850	-14	2099	18.13	26.74	-0.05
65	SLV 4	850	-14	2099	18.13	26.74	-0.05
65	SLV 5	302	79	2062	-91.44	9.01	0.37
65	SLV 6	302	79	2062	-91.44	9.01	0.37
65	SLV 7	537	-74	2016	86.33	16.61	-0.34
65	SLV 8	537	-74	2016	86.33	16.61	-0.34
65	SLV 9	-36	74	2005	-86.32	-1.96	0.34
65	SLV 10	-36	74	2005	-86.32	-1.96	0.34
65	SLV 11	198	-79	1958	91.45	5.65	-0.37
65	SLV 12	198	-79	1958	91.45	5.65	-0.37
65	SLV 13	-349	14	1922	-18.12	-12.09	0.05
65	SLV 14	-349	14	1922	-18.12	-12.09	0.05
65	SLV 15	-279	-32	1908	35.21	-9.81	-0.16
65	SLV 16	-279	-32	1908	35.21	-9.81	-0.16
66	SLU 1	158	0	1821	0	4.65	0
66	SLU 2	158	0	1821	0	4.65	0
66	SLU 3	158	0	1821	0	4.65	0
66	SLU 4	158	0	1821	0	4.65	0
66	SLU 5	158	0	1821	0	4.65	0
66	SLU 6	158	0	1821	0	4.65	0
66	SLU 7	158	0	1821	0	4.65	0
66	SLU 8	158	0	1821	0	4.65	0
66	SLU 9	158	0	1821	0	4.65	0
66	SLU 10	248	0	2314	0.01	7.4	0
66	SLU 11	248	0	2314	0.01	7.4	0
66	SLU 12	248	0	2314	0.01	7.4	0
66	SLU 13	248	0	2314	0.01	7.4	0
66	SLU 14	248	0	2314	0.01	7.4	0
66	SLU 15	248	0	2314	0.01	7.4	0
66	SLU 16	248	0	2314	0.01	7.4	0
66	SLU 17	248	0	2314	0.01	7.4	0
66	SLU 18	287	0	2525	0.01	8.58	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
66	SLU 19	287	0	2525	0.01	8.58	0
66	SLU 20	287	0	2525	0.01	8.58	0
66	SLU 21	287	0	2525	0.01	8.58	0
66	SLU 22	210	0	2168	0.01	6.18	0
66	SLU 23	210	0	2168	0.01	6.18	0
66	SLU 24	210	0	2168	0.01	6.18	0
66	SLU 25	210	0	2168	0.01	6.18	0
66	SLU 26	210	0	2168	0.01	6.18	0
66	SLU 27	210	0	2168	0.01	6.18	0
66	SLU 28	210	0	2168	0.01	6.18	0
66	SLU 29	210	0	2168	0.01	6.18	0
66	SLU 30	210	0	2168	0.01	6.18	0
66	SLU 31	300	0	2660	0.01	8.93	0
66	SLU 32	300	0	2660	0.01	8.93	0
66	SLU 33	300	0	2660	0.01	8.93	0
66	SLU 34	300	0	2660	0.01	8.93	0
66	SLU 35	300	0	2660	0.01	8.93	0
66	SLU 36	300	0	2660	0.01	8.93	0
66	SLU 37	300	0	2660	0.01	8.93	0
66	SLU 38	300	0	2660	0.01	8.93	0
66	SLU 39	339	0	2871	0.01	10.11	0
66	SLU 40	339	0	2871	0.01	10.11	0
66	SLU 41	339	0	2871	0.01	10.11	0
66	SLU 42	339	0	2871	0.01	10.11	0
66	SLU 43	188	0	2249	0	5.52	0
66	SLU 44	188	0	2249	0	5.52	0
66	SLU 45	188	0	2249	0	5.52	0
66	SLU 46	188	0	2249	0	5.52	0
66	SLU 47	188	0	2249	0	5.52	0
66	SLU 48	188	0	2249	0	5.52	0
66	SLU 49	188	0	2249	0	5.52	0
66	SLU 50	188	0	2249	0	5.52	0
66	SLU 51	188	0	2249	0	5.52	0
66	SLU 52	278	0	2741	0.01	8.27	0
66	SLU 53	278	0	2741	0.01	8.27	0
66	SLU 54	278	0	2741	0.01	8.27	0
66	SLU 55	278	0	2741	0.01	8.27	0
66	SLU 56	278	0	2741	0.01	8.27	0
66	SLU 57	278	0	2741	0.01	8.27	0
66	SLU 58	278	0	2741	0.01	8.27	0
66	SLU 59	278	0	2741	0.01	8.27	0
66	SLU 60	317	0	2952	0.01	9.45	0
66	SLU 61	317	0	2952	0.01	9.45	0
66	SLU 62	317	0	2952	0.01	9.45	0
66	SLU 63	317	0	2952	0.01	9.45	0
66	SLU 64	239	0	2595	0.01	7.05	0
66	SLU 65	239	0	2595	0.01	7.05	0
66	SLU 66	239	0	2595	0.01	7.05	0
66	SLU 67	239	0	2595	0.01	7.05	0
66	SLU 68	239	0	2595	0.01	7.05	0
66	SLU 69	239	0	2595	0.01	7.05	0
66	SLU 70	239	0	2595	0.01	7.05	0
66	SLU 71	239	0	2595	0.01	7.05	0
66	SLU 72	239	0	2595	0.01	7.05	0
66	SLU 73	330	0	3088	0.01	9.8	0
66	SLU 74	330	0	3088	0.01	9.8	0
66	SLU 75	330	0	3088	0.01	9.8	0
66	SLU 76	330	0	3088	0.01	9.8	0
66	SLU 77	330	0	3088	0.01	9.8	0
66	SLU 78	330	0	3088	0.01	9.8	0
66	SLU 79	330	0	3088	0.01	9.8	0
66	SLU 80	330	0	3088	0.01	9.8	0
66	SLU 81	369	0	3299	0.02	10.98	0
66	SLU 82	369	0	3299	0.02	10.98	0
66	SLU 83	369	0	3299	0.02	10.98	0
66	SLU 84	369	0	3299	0.02	10.98	0
66	SLE RA 1	173	0	1920	0	5.09	0
66	SLE RA 2	173	0	1920	0	5.09	0
66	SLE RA 3	173	0	1920	0	5.09	0
66	SLE RA 4	173	0	1920	0	5.09	0
66	SLE RA 5	173	0	1920	0	5.09	0
66	SLE RA 6	173	0	1920	0	5.09	0
66	SLE RA 7	173	0	1920	0	5.09	0
66	SLE RA 8	173	0	1920	0	5.09	0
66	SLE RA 9	173	0	1920	0	5.09	0
66	SLE RA 10	233	0	2248	0.01	6.92	0
66	SLE RA 11	233	0	2248	0.01	6.92	0
66	SLE RA 12	233	0	2248	0.01	6.92	0
66	SLE RA 13	233	0	2248	0.01	6.92	0
66	SLE RA 14	233	0	2248	0.01	6.92	0
66	SLE RA 15	233	0	2248	0.01	6.92	0
66	SLE RA 16	233	0	2248	0.01	6.92	0
66	SLE RA 17	233	0	2248	0.01	6.92	0
66	SLE RA 18	259	0	2389	0.01	7.71	0
66	SLE RA 19	259	0	2389	0.01	7.71	0
66	SLE RA 20	259	0	2389	0.01	7.71	0
66	SLE RA 21	259	0	2389	0.01	7.71	0
66	SLE FR 1	173	0	1920	0	5.09	0
66	SLE FR 2	173	0	1920	0	5.09	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
66	SLE FR 3	173	0	1920	0	5.09	0
66	SLE FR 4	199	0	2061	0.01	5.87	0
66	SLE FR 5	199	0	2061	0.01	5.87	0
66	SLE FR 6	216	0	2155	0.01	6.4	0
66	SLE QP 1	173	0	1920	0	5.09	0
66	SLE QP 2	199	0	2061	0.01	5.87	0
66	SLD 1	415	15	2090	-15.61	12.27	0.05
66	SLD 2	415	15	2090	-15.61	12.27	0.05
66	SLD 3	444	-7	2086	8.32	13.13	-0.02
66	SLD 4	444	-7	2086	8.32	13.13	-0.02
66	SLD 5	220	37	2076	-40.97	6.49	0.13
66	SLD 6	220	37	2076	-40.97	6.49	0.13
66	SLD 7	315	-35	2062	38.79	9.35	-0.12
66	SLD 8	315	-35	2062	38.79	9.35	-0.12
66	SLD 9	82	35	2059	-38.78	2.4	0.12
66	SLD 10	82	35	2059	-38.78	2.4	0.12
66	SLD 11	177	-37	2046	40.98	5.25	-0.13
66	SLD 12	177	-37	2046	40.98	5.25	-0.13
66	SLD 13	-46	7	2036	-8.31	-1.38	0.02
66	SLD 14	-46	7	2036	-8.31	-1.38	0.02
66	SLD 15	-18	-15	2032	15.62	-0.53	-0.05
66	SLD 16	-18	-15	2032	15.62	-0.53	-0.05
66	SLV 1	710	38	2133	-40.06	20.95	0.14
66	SLV 2	710	38	2133	-40.06	20.95	0.14
66	SLV 3	777	-17	2123	21.25	22.96	-0.06
66	SLV 4	777	-17	2123	21.25	22.96	-0.06
66	SLV 5	250	94	2097	-105	7.34	0.34
66	SLV 6	250	94	2097	-105	7.34	0.34
66	SLV 7	475	-88	2065	99.36	14.05	-0.32
66	SLV 8	475	-88	2065	99.36	14.05	-0.32
66	SLV 9	-77	88	2057	-99.35	-2.31	0.32
66	SLV 10	-77	88	2057	-99.35	-2.31	0.32
66	SLV 11	148	-94	2024	105.01	4.41	-0.34
66	SLV 12	148	-94	2024	105.01	4.41	-0.34
66	SLV 13	-380	17	1998	-21.23	-11.22	0.06
66	SLV 14	-380	17	1998	-21.23	-11.22	0.06
66	SLV 15	-313	-38	1989	40.07	-9.2	-0.14
66	SLV 16	-313	-38	1989	40.07	-9.2	-0.14
67	SLU 1	117	0	1851	0.01	3.39	0
67	SLU 2	117	0	1851	0.01	3.39	0
67	SLU 3	117	0	1851	0.01	3.39	0
67	SLU 4	117	0	1851	0.01	3.39	0
67	SLU 5	117	0	1851	0.01	3.39	0
67	SLU 6	117	0	1851	0.01	3.39	0
67	SLU 7	117	0	1851	0.01	3.39	0
67	SLU 8	117	0	1851	0.01	3.39	0
67	SLU 9	117	0	1851	0.01	3.39	0
67	SLU 10	194	0	2364	0.01	5.53	0
67	SLU 11	194	0	2364	0.01	5.53	0
67	SLU 12	194	0	2364	0.01	5.53	0
67	SLU 13	194	0	2364	0.01	5.53	0
67	SLU 14	194	0	2364	0.01	5.53	0
67	SLU 15	194	0	2364	0.01	5.53	0
67	SLU 16	194	0	2364	0.01	5.53	0
67	SLU 17	194	0	2364	0.01	5.53	0
67	SLU 18	227	0	2583	0.01	6.45	0
67	SLU 19	227	0	2583	0.01	6.45	0
67	SLU 20	227	0	2583	0.01	6.45	0
67	SLU 21	227	0	2583	0.01	6.45	0
67	SLU 22	158	0	2211	0.01	4.58	0
67	SLU 23	158	0	2211	0.01	4.58	0
67	SLU 24	158	0	2211	0.01	4.58	0
67	SLU 25	158	0	2211	0.01	4.58	0
67	SLU 26	158	0	2211	0.01	4.58	0
67	SLU 27	158	0	2211	0.01	4.58	0
67	SLU 28	158	0	2211	0.01	4.58	0
67	SLU 29	158	0	2211	0.01	4.58	0
67	SLU 30	158	0	2211	0.01	4.58	0
67	SLU 31	235	0	2723	0.01	6.72	0
67	SLU 32	235	0	2723	0.01	6.72	0
67	SLU 33	235	0	2723	0.01	6.72	0
67	SLU 34	235	0	2723	0.01	6.72	0
67	SLU 35	235	0	2723	0.01	6.72	0
67	SLU 36	235	0	2723	0.01	6.72	0
67	SLU 37	235	0	2723	0.01	6.72	0
67	SLU 38	235	0	2723	0.01	6.72	0
67	SLU 39	269	0	2943	0.02	7.64	0
67	SLU 40	269	0	2943	0.02	7.64	0
67	SLU 41	269	0	2943	0.02	7.64	0
67	SLU 42	269	0	2943	0.02	7.64	0
67	SLU 43	137	0	2283	0.01	4	0
67	SLU 44	137	0	2283	0.01	4	0
67	SLU 45	137	0	2283	0.01	4	0
67	SLU 46	137	0	2283	0.01	4	0
67	SLU 47	137	0	2283	0.01	4	0
67	SLU 48	137	0	2283	0.01	4	0
67	SLU 49	137	0	2283	0.01	4	0
67	SLU 50	137	0	2283	0.01	4	0
67	SLU 51	137	0	2283	0.01	4	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
67	SLU 52	214	0	2796	0.01	6.14	0
67	SLU 53	214	0	2796	0.01	6.14	0
67	SLU 54	214	0	2796	0.01	6.14	0
67	SLU 55	214	0	2796	0.01	6.14	0
67	SLU 56	214	0	2796	0.01	6.14	0
67	SLU 57	214	0	2796	0.01	6.14	0
67	SLU 58	214	0	2796	0.01	6.14	0
67	SLU 59	214	0	2796	0.01	6.14	0
67	SLU 60	247	0	3015	0.01	7.06	0
67	SLU 61	247	0	3015	0.01	7.06	0
67	SLU 62	247	0	3015	0.01	7.06	0
67	SLU 63	247	0	3015	0.01	7.06	0
67	SLU 64	179	0	2643	0.01	5.19	0
67	SLU 65	179	0	2643	0.01	5.19	0
67	SLU 66	179	0	2643	0.01	5.19	0
67	SLU 67	179	0	2643	0.01	5.19	0
67	SLU 68	179	0	2643	0.01	5.19	0
67	SLU 69	179	0	2643	0.01	5.19	0
67	SLU 70	179	0	2643	0.01	5.19	0
67	SLU 71	179	0	2643	0.01	5.19	0
67	SLU 72	179	0	2643	0.01	5.19	0
67	SLU 73	256	0	3155	0.01	7.33	0
67	SLU 74	256	0	3155	0.01	7.33	0
67	SLU 75	256	0	3155	0.01	7.33	0
67	SLU 76	256	0	3155	0.01	7.33	0
67	SLU 77	256	0	3155	0.01	7.33	0
67	SLU 78	256	0	3155	0.01	7.33	0
67	SLU 79	256	0	3155	0.01	7.33	0
67	SLU 80	256	0	3155	0.01	7.33	0
67	SLU 81	289	0	3375	0.02	8.25	0
67	SLU 82	289	0	3375	0.02	8.25	0
67	SLU 83	289	0	3375	0.02	8.25	0
67	SLU 84	289	0	3375	0.02	8.25	0
67	SLE RA 1	129	0	1954	0.01	3.73	0
67	SLE RA 2	129	0	1954	0.01	3.73	0
67	SLE RA 3	129	0	1954	0.01	3.73	0
67	SLE RA 4	129	0	1954	0.01	3.73	0
67	SLE RA 5	129	0	1954	0.01	3.73	0
67	SLE RA 6	129	0	1954	0.01	3.73	0
67	SLE RA 7	129	0	1954	0.01	3.73	0
67	SLE RA 8	129	0	1954	0.01	3.73	0
67	SLE RA 9	129	0	1954	0.01	3.73	0
67	SLE RA 10	180	0	2296	0.01	5.16	0
67	SLE RA 11	180	0	2296	0.01	5.16	0
67	SLE RA 12	180	0	2296	0.01	5.16	0
67	SLE RA 13	180	0	2296	0.01	5.16	0
67	SLE RA 14	180	0	2296	0.01	5.16	0
67	SLE RA 15	180	0	2296	0.01	5.16	0
67	SLE RA 16	180	0	2296	0.01	5.16	0
67	SLE RA 17	180	0	2296	0.01	5.16	0
67	SLE RA 18	202	0	2442	0.01	5.77	0
67	SLE RA 19	202	0	2442	0.01	5.77	0
67	SLE RA 20	202	0	2442	0.01	5.77	0
67	SLE RA 21	202	0	2442	0.01	5.77	0
67	SLE FR 1	129	0	1954	0.01	3.73	0
67	SLE FR 2	129	0	1954	0.01	3.73	0
67	SLE FR 3	129	0	1954	0.01	3.73	0
67	SLE FR 4	151	0	2100	0.01	4.34	0
67	SLE FR 5	151	0	2100	0.01	4.34	0
67	SLE FR 6	165	0	2198	0.01	4.75	0
67	SLE QP 1	129	0	1954	0.01	3.73	0
67	SLE QP 2	151	0	2100	0.01	4.34	0
67	SLD 1	372	15	2120	-16.3	11.25	0.04
67	SLD 2	372	15	2120	-16.3	11.25	0.04
67	SLD 3	402	-7	2117	8.84	12.18	-0.02
67	SLD 4	402	-7	2117	8.84	12.18	-0.02
67	SLD 5	173	38	2111	-43.02	5.01	0.11
67	SLD 6	173	38	2111	-43.02	5.01	0.11
67	SLD 7	271	-36	2101	40.79	8.1	-0.1
67	SLD 8	271	-36	2101	40.79	8.1	-0.1
67	SLD 9	31	36	2100	-40.77	0.59	0.1
67	SLD 10	31	36	2100	-40.77	0.59	0.1
67	SLD 11	129	-38	2090	43.03	3.67	-0.11
67	SLD 12	129	-38	2090	43.03	3.67	-0.11
67	SLD 13	-101	7	2084	-8.82	-3.5	0.02
67	SLD 14	-101	7	2084	-8.82	-3.5	0.02
67	SLD 15	-71	-15	2081	16.32	-2.57	-0.04
67	SLD 16	-71	-15	2081	16.32	-2.57	-0.04
67	SLV 1	677	39	2148	-41.86	20.84	0.11
67	SLV 2	677	39	2148	-41.86	20.84	0.11
67	SLV 3	746	-18	2141	22.56	23.05	-0.05
67	SLV 4	746	-18	2141	22.56	23.05	-0.05
67	SLV 5	203	98	2126	-110.25	5.95	0.27
67	SLV 6	203	98	2126	-110.25	5.95	0.27
67	SLV 7	435	-91	2101	104.47	13.29	-0.26
67	SLV 8	435	-91	2101	104.47	13.29	-0.26
67	SLV 9	-134	91	2099	-104.45	-4.61	0.26
67	SLV 10	-134	91	2099	-104.45	-4.61	0.26
67	SLV 11	98	-98	2075	110.27	2.73	-0.27



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
67	SLV 12	98	-98	2075	110.27	2.73	-0.27
67	SLV 13	-445	18	2060	-22.54	-14.36	0.05
67	SLV 14	-445	18	2060	-22.54	-14.36	0.05
67	SLV 15	-376	-39	2053	41.88	-12.16	-0.11
67	SLV 16	-376	-39	2053	41.88	-12.16	-0.11
68	SLU 1	79	0	1875	0.01	2.29	0
68	SLU 2	79	0	1875	0.01	2.29	0
68	SLU 3	79	0	1875	0.01	2.29	0
68	SLU 4	79	0	1875	0.01	2.29	0
68	SLU 5	79	0	1875	0.01	2.29	0
68	SLU 6	79	0	1875	0.01	2.29	0
68	SLU 7	79	0	1875	0.01	2.29	0
68	SLU 8	79	0	1875	0.01	2.29	0
68	SLU 9	79	0	1875	0.01	2.29	0
68	SLU 10	149	0	2408	0.01	4.41	0
68	SLU 11	149	0	2408	0.01	4.41	0
68	SLU 12	149	0	2408	0.01	4.41	0
68	SLU 13	149	0	2408	0.01	4.41	0
68	SLU 14	149	0	2408	0.01	4.41	0
68	SLU 15	149	0	2408	0.01	4.41	0
68	SLU 16	149	0	2408	0.01	4.41	0
68	SLU 17	149	0	2408	0.01	4.41	0
68	SLU 18	179	0	2636	0.01	5.32	0
68	SLU 19	179	0	2636	0.01	5.32	0
68	SLU 20	179	0	2636	0.01	5.32	0
68	SLU 21	179	0	2636	0.01	5.32	0
68	SLU 22	113	0	2246	0.01	3.29	0
68	SLU 23	113	0	2246	0.01	3.29	0
68	SLU 24	113	0	2246	0.01	3.29	0
68	SLU 25	113	0	2246	0.01	3.29	0
68	SLU 26	113	0	2246	0.01	3.29	0
68	SLU 27	113	0	2246	0.01	3.29	0
68	SLU 28	113	0	2246	0.01	3.29	0
68	SLU 29	113	0	2246	0.01	3.29	0
68	SLU 30	113	0	2246	0.01	3.29	0
68	SLU 31	183	0	2779	0.02	5.41	0
68	SLU 32	183	0	2779	0.02	5.41	0
68	SLU 33	183	0	2779	0.02	5.41	0
68	SLU 34	183	0	2779	0.02	5.41	0
68	SLU 35	183	0	2779	0.02	5.41	0
68	SLU 36	183	0	2779	0.02	5.41	0
68	SLU 37	183	0	2779	0.02	5.41	0
68	SLU 38	183	0	2779	0.02	5.41	0
68	SLU 39	213	0	3007	0.02	6.31	0
68	SLU 40	213	0	3007	0.02	6.31	0
68	SLU 41	213	0	3007	0.02	6.31	0
68	SLU 42	213	0	3007	0.02	6.31	0
68	SLU 43	91	0	2310	0.01	2.64	0
68	SLU 44	91	0	2310	0.01	2.64	0
68	SLU 45	91	0	2310	0.01	2.64	0
68	SLU 46	91	0	2310	0.01	2.64	0
68	SLU 47	91	0	2310	0.01	2.64	0
68	SLU 48	91	0	2310	0.01	2.64	0
68	SLU 49	91	0	2310	0.01	2.64	0
68	SLU 50	91	0	2310	0.01	2.64	0
68	SLU 51	91	0	2310	0.01	2.64	0
68	SLU 52	161	0	2843	0.01	4.76	0
68	SLU 53	161	0	2843	0.01	4.76	0
68	SLU 54	161	0	2843	0.01	4.76	0
68	SLU 55	161	0	2843	0.01	4.76	0
68	SLU 56	161	0	2843	0.01	4.76	0
68	SLU 57	161	0	2843	0.01	4.76	0
68	SLU 58	161	0	2843	0.01	4.76	0
68	SLU 59	161	0	2843	0.01	4.76	0
68	SLU 60	191	0	3071	0.02	5.66	0
68	SLU 61	191	0	3071	0.02	5.66	0
68	SLU 62	191	0	3071	0.02	5.66	0
68	SLU 63	191	0	3071	0.02	5.66	0
68	SLU 64	125	0	2681	0.01	3.64	0
68	SLU 65	125	0	2681	0.01	3.64	0
68	SLU 66	125	0	2681	0.01	3.64	0
68	SLU 67	125	0	2681	0.01	3.64	0
68	SLU 68	125	0	2681	0.01	3.64	0
68	SLU 69	125	0	2681	0.01	3.64	0
68	SLU 70	125	0	2681	0.01	3.64	0
68	SLU 71	125	0	2681	0.01	3.64	0
68	SLU 72	125	0	2681	0.01	3.64	0
68	SLU 73	195	0	3214	0.02	5.75	0
68	SLU 74	195	0	3214	0.02	5.75	0
68	SLU 75	195	0	3214	0.02	5.75	0
68	SLU 76	195	0	3214	0.02	5.75	0
68	SLU 77	195	0	3214	0.02	5.75	0
68	SLU 78	195	0	3214	0.02	5.75	0
68	SLU 79	195	0	3214	0.02	5.75	0
68	SLU 80	195	0	3214	0.02	5.75	0
68	SLU 81	225	0	3443	0.02	6.66	0
68	SLU 82	225	0	3443	0.02	6.66	0
68	SLU 83	225	0	3443	0.02	6.66	0
68	SLU 84	225	0	3443	0.02	6.66	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
68	SLE RA 1	89	0	1981	0.01	2.58	0
68	SLE RA 2	89	0	1981	0.01	2.58	0
68	SLE RA 3	89	0	1981	0.01	2.58	0
68	SLE RA 4	89	0	1981	0.01	2.58	0
68	SLE RA 5	89	0	1981	0.01	2.58	0
68	SLE RA 6	89	0	1981	0.01	2.58	0
68	SLE RA 7	89	0	1981	0.01	2.58	0
68	SLE RA 8	89	0	1981	0.01	2.58	0
68	SLE RA 9	89	0	1981	0.01	2.58	0
68	SLE RA 10	135	0	2336	0.01	3.99	0
68	SLE RA 11	135	0	2336	0.01	3.99	0
68	SLE RA 12	135	0	2336	0.01	3.99	0
68	SLE RA 13	135	0	2336	0.01	3.99	0
68	SLE RA 14	135	0	2336	0.01	3.99	0
68	SLE RA 15	135	0	2336	0.01	3.99	0
68	SLE RA 16	135	0	2336	0.01	3.99	0
68	SLE RA 17	135	0	2336	0.01	3.99	0
68	SLE RA 18	156	0	2488	0.01	4.59	0
68	SLE RA 19	156	0	2488	0.01	4.59	0
68	SLE RA 20	156	0	2488	0.01	4.59	0
68	SLE RA 21	156	0	2488	0.01	4.59	0
68	SLE FR 1	89	0	1981	0.01	2.58	0
68	SLE FR 2	89	0	1981	0.01	2.58	0
68	SLE FR 3	89	0	1981	0.01	2.58	0
68	SLE FR 4	109	0	2133	0.01	3.18	0
68	SLE FR 5	109	0	2133	0.01	3.18	0
68	SLE FR 6	122	0	2235	0.01	3.59	0
68	SLE QP 1	89	0	1981	0.01	2.58	0
68	SLE QP 2	109	0	2133	0.01	3.18	0
68	SLD 1	324	14	2155	-15.99	9.58	0.03
68	SLD 2	324	14	2155	-15.99	9.58	0.03
68	SLD 3	353	-6	2152	8.69	10.43	-0.01
68	SLD 4	353	-6	2152	8.69	10.43	-0.01
68	SLD 5	130	35	2145	-42.23	3.82	0.07
68	SLD 6	130	35	2145	-42.23	3.82	0.07
68	SLD 7	225	-33	2133	40.06	6.64	-0.07
68	SLD 8	225	-33	2133	40.06	6.64	-0.07
68	SLD 9	-8	33	2133	-40.04	-0.27	0.07
68	SLD 10	-8	33	2133	-40.04	-0.27	0.07
68	SLD 11	87	-35	2121	42.25	2.55	-0.07
68	SLD 12	87	-35	2121	42.25	2.55	-0.07
68	SLD 13	-136	6	2115	-8.67	-4.06	0.01
68	SLD 14	-136	6	2115	-8.67	-4.06	0.01
68	SLD 15	-107	-14	2111	16.01	-3.21	-0.03
68	SLD 16	-107	-14	2111	16.01	-3.21	-0.03
68	SLV 1	619	36	2187	-41.08	18.27	0.08
68	SLV 2	619	36	2187	-41.08	18.27	0.08
68	SLV 3	686	-16	2177	22.18	20.26	-0.03
68	SLV 4	686	-16	2177	22.18	20.26	-0.03
68	SLV 5	159	90	2164	-108.25	4.69	0.19
68	SLV 6	159	90	2164	-108.25	4.69	0.19
68	SLV 7	384	-84	2132	102.59	11.33	-0.17
68	SLV 8	384	-84	2132	102.59	11.33	-0.17
68	SLV 9	-167	84	2134	-102.57	-4.96	0.17
68	SLV 10	-167	84	2134	-102.57	-4.96	0.17
68	SLV 11	58	-90	2103	108.27	1.68	-0.19
68	SLV 12	58	-90	2103	108.27	1.68	-0.19
68	SLV 13	-469	16	2089	-22.16	-13.89	0.03
68	SLV 14	-469	16	2089	-22.16	-13.89	0.03
68	SLV 15	-401	-36	2079	41.1	-11.9	-0.08
68	SLV 16	-401	-36	2079	41.1	-11.9	-0.08
69	SLU 1	40	0	1896	0.01	1.13	0
69	SLU 2	40	0	1896	0.01	1.13	0
69	SLU 3	40	0	1896	0.01	1.13	0
69	SLU 4	40	0	1896	0.01	1.13	0
69	SLU 5	40	0	1896	0.01	1.13	0
69	SLU 6	40	0	1896	0.01	1.13	0
69	SLU 7	40	0	1896	0.01	1.13	0
69	SLU 8	40	0	1896	0.01	1.13	0
69	SLU 9	40	0	1896	0.01	1.13	0
69	SLU 10	98	0	2453	0.01	2.74	0
69	SLU 11	98	0	2453	0.01	2.74	0
69	SLU 12	98	0	2453	0.01	2.74	0
69	SLU 13	98	0	2453	0.01	2.74	0
69	SLU 14	98	0	2453	0.01	2.74	0
69	SLU 15	98	0	2453	0.01	2.74	0
69	SLU 16	98	0	2453	0.01	2.74	0
69	SLU 17	98	0	2453	0.01	2.74	0
69	SLU 18	123	0	2691	0.02	3.43	0
69	SLU 19	123	0	2691	0.02	3.43	0
69	SLU 20	123	0	2691	0.02	3.43	0
69	SLU 21	123	0	2691	0.02	3.43	0
69	SLU 22	65	0	2279	0.01	1.84	0
69	SLU 23	65	0	2279	0.01	1.84	0
69	SLU 24	65	0	2279	0.01	1.84	0
69	SLU 25	65	0	2279	0.01	1.84	0
69	SLU 26	65	0	2279	0.01	1.84	0
69	SLU 27	65	0	2279	0.01	1.84	0
69	SLU 28	65	0	2279	0.01	1.84	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
69	SLU 29	65	0	2279	0.01	1.84	0
69	SLU 30	65	0	2279	0.01	1.84	0
69	SLU 31	123	0	2836	0.02	3.44	0
69	SLU 32	123	0	2836	0.02	3.44	0
69	SLU 33	123	0	2836	0.02	3.44	0
69	SLU 34	123	0	2836	0.02	3.44	0
69	SLU 35	123	0	2836	0.02	3.44	0
69	SLU 36	123	0	2836	0.02	3.44	0
69	SLU 37	123	0	2836	0.02	3.44	0
69	SLU 38	123	0	2836	0.02	3.44	0
69	SLU 39	149	0	3074	0.02	4.13	0
69	SLU 40	149	0	3074	0.02	4.13	0
69	SLU 41	149	0	3074	0.02	4.13	0
69	SLU 42	149	0	3074	0.02	4.13	0
69	SLU 43	43	0	2333	0.01	1.23	0
69	SLU 44	43	0	2333	0.01	1.23	0
69	SLU 45	43	0	2333	0.01	1.23	0
69	SLU 46	43	0	2333	0.01	1.23	0
69	SLU 47	43	0	2333	0.01	1.23	0
69	SLU 48	43	0	2333	0.01	1.23	0
69	SLU 49	43	0	2333	0.01	1.23	0
69	SLU 50	43	0	2333	0.01	1.23	0
69	SLU 51	43	0	2333	0.01	1.23	0
69	SLU 52	102	0	2890	0.02	2.84	0
69	SLU 53	102	0	2890	0.02	2.84	0
69	SLU 54	102	0	2890	0.02	2.84	0
69	SLU 55	102	0	2890	0.02	2.84	0
69	SLU 56	102	0	2890	0.02	2.84	0
69	SLU 57	102	0	2890	0.02	2.84	0
69	SLU 58	102	0	2890	0.02	2.84	0
69	SLU 59	102	0	2890	0.02	2.84	0
69	SLU 60	127	0	3129	0.02	3.53	0
69	SLU 61	127	0	3129	0.02	3.53	0
69	SLU 62	127	0	3129	0.02	3.53	0
69	SLU 63	127	0	3129	0.02	3.53	0
69	SLU 64	68	0	2717	0.02	1.94	0
69	SLU 65	68	0	2717	0.02	1.94	0
69	SLU 66	68	0	2717	0.02	1.94	0
69	SLU 67	68	0	2717	0.02	1.94	0
69	SLU 68	68	0	2717	0.02	1.94	0
69	SLU 69	68	0	2717	0.02	1.94	0
69	SLU 70	68	0	2717	0.02	1.94	0
69	SLU 71	68	0	2717	0.02	1.94	0
69	SLU 72	68	0	2717	0.02	1.94	0
69	SLU 73	127	0	3273	0.02	3.54	0
69	SLU 74	127	0	3273	0.02	3.54	0
69	SLU 75	127	0	3273	0.02	3.54	0
69	SLU 76	127	0	3273	0.02	3.54	0
69	SLU 77	127	0	3273	0.02	3.54	0
69	SLU 78	127	0	3273	0.02	3.54	0
69	SLU 79	127	0	3273	0.02	3.54	0
69	SLU 80	127	0	3273	0.02	3.54	0
69	SLU 81	152	0	3512	0.02	4.23	0
69	SLU 82	152	0	3512	0.02	4.23	0
69	SLU 83	152	0	3512	0.02	4.23	0
69	SLU 84	152	0	3512	0.02	4.23	0
69	SLE RA 1	47	0	2005	0.01	1.34	0
69	SLE RA 2	47	0	2005	0.01	1.34	0
69	SLE RA 3	47	0	2005	0.01	1.34	0
69	SLE RA 4	47	0	2005	0.01	1.34	0
69	SLE RA 5	47	0	2005	0.01	1.34	0
69	SLE RA 6	47	0	2005	0.01	1.34	0
69	SLE RA 7	47	0	2005	0.01	1.34	0
69	SLE RA 8	47	0	2005	0.01	1.34	0
69	SLE RA 9	47	0	2005	0.01	1.34	0
69	SLE RA 10	86	0	2376	0.01	2.41	0
69	SLE RA 11	86	0	2376	0.01	2.41	0
69	SLE RA 12	86	0	2376	0.01	2.41	0
69	SLE RA 13	86	0	2376	0.01	2.41	0
69	SLE RA 14	86	0	2376	0.01	2.41	0
69	SLE RA 15	86	0	2376	0.01	2.41	0
69	SLE RA 16	86	0	2376	0.01	2.41	0
69	SLE RA 17	86	0	2376	0.01	2.41	0
69	SLE RA 18	103	0	2536	0.01	2.87	0
69	SLE RA 19	103	0	2536	0.01	2.87	0
69	SLE RA 20	103	0	2536	0.01	2.87	0
69	SLE RA 21	103	0	2536	0.01	2.87	0
69	SLE FR 1	47	0	2005	0.01	1.34	0
69	SLE FR 2	47	0	2005	0.01	1.34	0
69	SLE FR 3	47	0	2005	0.01	1.34	0
69	SLE FR 4	64	0	2164	0.01	1.79	0
69	SLE FR 5	64	0	2164	0.01	1.79	0
69	SLE FR 6	75	0	2270	0.01	2.1	0
69	SLE QP 1	47	0	2005	0.01	1.34	0
69	SLE QP 2	64	0	2164	0.01	1.79	0
69	SLD 1	309	12	2130	-15.24	8.54	0
69	SLD 2	309	12	2130	-15.24	8.54	0
69	SLD 3	281	-5	2124	8.08	9.45	0.01
69	SLD 4	281	-5	2124	8.08	9.45	0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
69	SLD 5	181	30	2164	-39.94	2.43	-0.02
69	SLD 6	181	30	2164	-39.94	2.43	-0.02
69	SLD 7	85	-28	2142	37.81	5.48	0.02
69	SLD 8	85	-28	2142	37.81	5.48	0.02
69	SLD 9	42	28	2187	-37.79	-1.89	-0.02
69	SLD 10	42	28	2187	-37.79	-1.89	-0.02
69	SLD 11	-54	-30	2165	39.97	1.16	0.02
69	SLD 12	-54	-30	2165	39.97	1.16	0.02
69	SLD 13	-153	5	2205	-8.06	-5.86	-0.01
69	SLD 14	-153	5	2205	-8.06	-5.86	-0.01
69	SLD 15	-182	-12	2199	15.27	-4.95	0
69	SLD 16	-182	-12	2199	15.27	-4.95	0
69	SLV 1	646	32	2084	-39.15	17.85	0
69	SLV 2	646	32	2084	-39.15	17.85	0
69	SLV 3	578	-12	2067	20.63	20.02	0.02
69	SLV 4	578	-12	2067	20.63	20.02	0.02
69	SLV 5	342	76	2165	-102.4	3.32	-0.04
69	SLV 6	342	76	2165	-102.4	3.32	-0.04
69	SLV 7	115	-71	2110	96.86	10.55	0.05
69	SLV 8	115	-71	2110	96.86	10.55	0.05
69	SLV 9	13	71	2219	-96.84	-6.96	-0.05
69	SLV 10	13	71	2219	-96.84	-6.96	-0.05
69	SLV 11	-214	-76	2163	102.43	0.27	0.04
69	SLV 12	-214	-76	2163	102.43	0.27	0.04
69	SLV 13	-450	12	2262	-20.61	-16.43	-0.02
69	SLV 14	-450	12	2262	-20.61	-16.43	-0.02
69	SLV 15	-518	-32	2245	39.17	-14.27	0
69	SLV 16	-518	-32	2245	39.17	-14.27	0
70	SLU 1	-8	0	1917	0.01	-0.24	0
70	SLU 2	-8	0	1917	0.01	-0.24	0
70	SLU 3	-8	0	1917	0.01	-0.24	0
70	SLU 4	-8	0	1917	0.01	-0.24	0
70	SLU 5	-8	0	1917	0.01	-0.24	0
70	SLU 6	-8	0	1917	0.01	-0.24	0
70	SLU 7	-8	0	1917	0.01	-0.24	0
70	SLU 8	-8	0	1917	0.01	-0.24	0
70	SLU 9	-8	0	1917	0.01	-0.24	0
70	SLU 10	39	0	2499	0.02	1.15	0
70	SLU 11	39	0	2499	0.02	1.15	0
70	SLU 12	39	0	2499	0.02	1.15	0
70	SLU 13	39	0	2499	0.02	1.15	0
70	SLU 14	39	0	2499	0.02	1.15	0
70	SLU 15	39	0	2499	0.02	1.15	0
70	SLU 16	39	0	2499	0.02	1.15	0
70	SLU 17	39	0	2499	0.02	1.15	0
70	SLU 18	59	0	2749	0.02	1.74	0
70	SLU 19	59	0	2749	0.02	1.74	0
70	SLU 20	59	0	2749	0.02	1.74	0
70	SLU 21	59	0	2749	0.02	1.74	0
70	SLU 22	7	0	2312	0.02	0.19	0
70	SLU 23	7	0	2312	0.02	0.19	0
70	SLU 24	7	0	2312	0.02	0.19	0
70	SLU 25	7	0	2312	0.02	0.19	0
70	SLU 26	7	0	2312	0.02	0.19	0
70	SLU 27	7	0	2312	0.02	0.19	0
70	SLU 28	7	0	2312	0.02	0.19	0
70	SLU 29	7	0	2312	0.02	0.19	0
70	SLU 30	7	0	2312	0.02	0.19	0
70	SLU 31	54	0	2895	0.02	1.57	0
70	SLU 32	54	0	2895	0.02	1.57	0
70	SLU 33	54	0	2895	0.02	1.57	0
70	SLU 34	54	0	2895	0.02	1.57	0
70	SLU 35	54	0	2895	0.02	1.57	0
70	SLU 36	54	0	2895	0.02	1.57	0
70	SLU 37	54	0	2895	0.02	1.57	0
70	SLU 38	54	0	2895	0.02	1.57	0
70	SLU 39	74	0	3145	0.02	2.17	0
70	SLU 40	74	0	3145	0.02	2.17	0
70	SLU 41	74	0	3145	0.02	2.17	0
70	SLU 42	74	0	3145	0.02	2.17	0
70	SLU 43	-15	0	2356	0.02	-0.46	0
70	SLU 44	-15	0	2356	0.02	-0.46	0
70	SLU 45	-15	0	2356	0.02	-0.46	0
70	SLU 46	-15	0	2356	0.02	-0.46	0
70	SLU 47	-15	0	2356	0.02	-0.46	0
70	SLU 48	-15	0	2356	0.02	-0.46	0
70	SLU 49	-15	0	2356	0.02	-0.46	0
70	SLU 50	-15	0	2356	0.02	-0.46	0
70	SLU 51	-15	0	2356	0.02	-0.46	0
70	SLU 52	32	0	2939	0.02	0.93	0
70	SLU 53	32	0	2939	0.02	0.93	0
70	SLU 54	32	0	2939	0.02	0.93	0
70	SLU 55	32	0	2939	0.02	0.93	0
70	SLU 56	32	0	2939	0.02	0.93	0
70	SLU 57	32	0	2939	0.02	0.93	0
70	SLU 58	32	0	2939	0.02	0.93	0
70	SLU 59	32	0	2939	0.02	0.93	0
70	SLU 60	51	0	3189	0.02	1.52	0
70	SLU 61	51	0	3189	0.02	1.52	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
70	SLU 62	51	0	3189	0.02	1.52	0
70	SLU 63	51	0	3189	0.02	1.52	0
70	SLU 64	0	0	2751	0.02	-0.03	0
70	SLU 65	0	0	2751	0.02	-0.03	0
70	SLU 66	0	0	2751	0.02	-0.03	0
70	SLU 67	0	0	2751	0.02	-0.03	0
70	SLU 68	0	0	2751	0.02	-0.03	0
70	SLU 69	0	0	2751	0.02	-0.03	0
70	SLU 70	0	0	2751	0.02	-0.03	0
70	SLU 71	0	0	2751	0.02	-0.03	0
70	SLU 72	0	0	2751	0.02	-0.03	0
70	SLU 73	46	0	3334	0.02	1.35	0
70	SLU 74	46	0	3334	0.02	1.35	0
70	SLU 75	46	0	3334	0.02	1.35	0
70	SLU 76	46	0	3334	0.02	1.35	0
70	SLU 77	46	0	3334	0.02	1.35	0
70	SLU 78	46	0	3334	0.02	1.35	0
70	SLU 79	46	0	3334	0.02	1.35	0
70	SLU 80	46	0	3334	0.02	1.35	0
70	SLU 81	66	0	3584	0.02	1.95	0
70	SLU 82	66	0	3584	0.02	1.95	0
70	SLU 83	66	0	3584	0.02	1.95	0
70	SLU 84	66	0	3584	0.02	1.95	0
70	SLE RA 1	-3	0	2030	0.01	-0.12	0
70	SLE RA 2	-3	0	2030	0.01	-0.12	0
70	SLE RA 3	-3	0	2030	0.01	-0.12	0
70	SLE RA 4	-3	0	2030	0.01	-0.12	0
70	SLE RA 5	-3	0	2030	0.01	-0.12	0
70	SLE RA 6	-3	0	2030	0.01	-0.12	0
70	SLE RA 7	-3	0	2030	0.01	-0.12	0
70	SLE RA 8	-3	0	2030	0.01	-0.12	0
70	SLE RA 9	-3	0	2030	0.01	-0.12	0
70	SLE RA 10	28	0	2418	0.02	0.81	0
70	SLE RA 11	28	0	2418	0.02	0.81	0
70	SLE RA 12	28	0	2418	0.02	0.81	0
70	SLE RA 13	28	0	2418	0.02	0.81	0
70	SLE RA 14	28	0	2418	0.02	0.81	0
70	SLE RA 15	28	0	2418	0.02	0.81	0
70	SLE RA 16	28	0	2418	0.02	0.81	0
70	SLE RA 17	28	0	2418	0.02	0.81	0
70	SLE RA 18	41	0	2585	0.02	1.2	0
70	SLE RA 19	41	0	2585	0.02	1.2	0
70	SLE RA 20	41	0	2585	0.02	1.2	0
70	SLE RA 21	41	0	2585	0.02	1.2	0
70	SLE FR 1	-3	0	2030	0.01	-0.12	0
70	SLE FR 2	-3	0	2030	0.01	-0.12	0
70	SLE FR 3	-3	0	2030	0.01	-0.12	0
70	SLE FR 4	10	0	2196	0.01	0.28	0
70	SLE FR 5	10	0	2196	0.01	0.28	0
70	SLE FR 6	19	0	2307	0.02	0.54	0
70	SLE QP 1	-3	0	2030	0.01	-0.12	0
70	SLE QP 2	10	0	2196	0.01	0.28	0
70	SLD 1	244	12	2134	-15.04	7.48	-0.05
70	SLD 2	244	12	2134	-15.04	7.48	-0.05
70	SLD 3	216	-3	2123	7.53	6.63	0.02
70	SLD 4	216	-3	2123	7.53	6.63	0.02
70	SLD 5	122	27	2194	-38.73	3.73	-0.11
70	SLD 6	122	27	2194	-38.73	3.73	-0.11
70	SLD 7	30	-24	2157	36.5	0.89	0.1
70	SLD 8	30	-24	2157	36.5	0.89	0.1
70	SLD 9	-10	24	2235	-36.47	-0.33	-0.1
70	SLD 10	-10	24	2235	-36.47	-0.33	-0.1
70	SLD 11	-102	-27	2198	38.76	-3.18	0.11
70	SLD 12	-102	-27	2198	38.76	-3.18	0.11
70	SLD 13	-196	3	2269	-7.5	-6.07	-0.02
70	SLD 14	-196	3	2269	-7.5	-6.07	-0.02
70	SLD 15	-224	-12	2258	15.07	-6.93	0.05
70	SLD 16	-224	-12	2258	15.07	-6.93	0.05
70	SLV 1	563	31	2050	-38.62	17.29	-0.12
70	SLV 2	563	31	2050	-38.62	17.29	-0.12
70	SLV 3	498	-8	2023	19.25	15.27	0.04
70	SLV 4	498	-8	2023	19.25	15.27	0.04
70	SLV 5	276	68	2193	-99.34	8.44	-0.28
70	SLV 6	276	68	2193	-99.34	8.44	-0.28
70	SLV 7	57	-61	2103	93.55	1.72	0.26
70	SLV 8	57	-61	2103	93.55	1.72	0.26
70	SLV 9	-37	61	2289	-93.52	-1.16	-0.26
70	SLV 10	-37	61	2289	-93.52	-1.16	-0.26
70	SLV 11	-256	-68	2199	99.37	-7.88	0.28
70	SLV 12	-256	-68	2199	99.37	-7.88	0.28
70	SLV 13	-478	8	2369	-19.22	-14.72	-0.04
70	SLV 14	-478	8	2369	-19.22	-14.72	-0.04
70	SLV 15	-543	-31	2342	38.65	-16.73	0.12
70	SLV 16	-543	-31	2342	38.65	-16.73	0.12
71	SLU 1	-83	0	1932	0.02	-2.68	0
71	SLU 2	-83	0	1932	0.02	-2.68	0
71	SLU 3	-83	0	1932	0.02	-2.68	0
71	SLU 4	-83	0	1932	0.02	-2.68	0
71	SLU 5	-83	0	1932	0.02	-2.68	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
71	SLU 6	-83	0	1932	0.02	-2.68	0
71	SLU 7	-83	0	1932	0.02	-2.68	0
71	SLU 8	-83	0	1932	0.02	-2.68	0
71	SLU 9	-83	0	1932	0.02	-2.68	0
71	SLU 10	-63	0	2542	0.02	-2.03	0
71	SLU 11	-63	0	2542	0.02	-2.03	0
71	SLU 12	-63	0	2542	0.02	-2.03	0
71	SLU 13	-63	0	2542	0.02	-2.03	0
71	SLU 14	-63	0	2542	0.02	-2.03	0
71	SLU 15	-63	0	2542	0.02	-2.03	0
71	SLU 16	-63	0	2542	0.02	-2.03	0
71	SLU 17	-63	0	2542	0.02	-2.03	0
71	SLU 18	-55	0	2804	0.02	-1.76	0
71	SLU 19	-55	0	2804	0.02	-1.76	0
71	SLU 20	-55	0	2804	0.02	-1.76	0
71	SLU 21	-55	0	2804	0.02	-1.76	0
71	SLU 22	-86	0	2339	0.02	-2.76	0
71	SLU 23	-86	0	2339	0.02	-2.76	0
71	SLU 24	-86	0	2339	0.02	-2.76	0
71	SLU 25	-86	0	2339	0.02	-2.76	0
71	SLU 26	-86	0	2339	0.02	-2.76	0
71	SLU 27	-86	0	2339	0.02	-2.76	0
71	SLU 28	-86	0	2339	0.02	-2.76	0
71	SLU 29	-86	0	2339	0.02	-2.76	0
71	SLU 30	-86	0	2339	0.02	-2.76	0
71	SLU 31	-66	0	2949	0.02	-2.12	0
71	SLU 32	-66	0	2949	0.02	-2.12	0
71	SLU 33	-66	0	2949	0.02	-2.12	0
71	SLU 34	-66	0	2949	0.02	-2.12	0
71	SLU 35	-66	0	2949	0.02	-2.12	0
71	SLU 36	-66	0	2949	0.02	-2.12	0
71	SLU 37	-66	0	2949	0.02	-2.12	0
71	SLU 38	-66	0	2949	0.02	-2.12	0
71	SLU 39	-58	0	3211	0.02	-1.84	0
71	SLU 40	-58	0	3211	0.02	-1.84	0
71	SLU 41	-58	0	3211	0.02	-1.84	0
71	SLU 42	-58	0	3211	0.02	-1.84	0
71	SLU 43	-108	0	2372	0.02	-3.45	0
71	SLU 44	-108	0	2372	0.02	-3.45	0
71	SLU 45	-108	0	2372	0.02	-3.45	0
71	SLU 46	-108	0	2372	0.02	-3.45	0
71	SLU 47	-108	0	2372	0.02	-3.45	0
71	SLU 48	-108	0	2372	0.02	-3.45	0
71	SLU 49	-108	0	2372	0.02	-3.45	0
71	SLU 50	-108	0	2372	0.02	-3.45	0
71	SLU 51	-108	0	2372	0.02	-3.45	0
71	SLU 52	-88	0	2982	0.02	-2.81	0
71	SLU 53	-88	0	2982	0.02	-2.81	0
71	SLU 54	-88	0	2982	0.02	-2.81	0
71	SLU 55	-88	0	2982	0.02	-2.81	0
71	SLU 56	-88	0	2982	0.02	-2.81	0
71	SLU 57	-88	0	2982	0.02	-2.81	0
71	SLU 58	-88	0	2982	0.02	-2.81	0
71	SLU 59	-88	0	2982	0.02	-2.81	0
71	SLU 60	-79	0	3244	0.02	-2.53	0
71	SLU 61	-79	0	3244	0.02	-2.53	0
71	SLU 62	-79	0	3244	0.02	-2.53	0
71	SLU 63	-79	0	3244	0.02	-2.53	0
71	SLU 64	-110	0	2779	0.02	-3.54	0
71	SLU 65	-110	0	2779	0.02	-3.54	0
71	SLU 66	-110	0	2779	0.02	-3.54	0
71	SLU 67	-110	0	2779	0.02	-3.54	0
71	SLU 68	-110	0	2779	0.02	-3.54	0
71	SLU 69	-110	0	2779	0.02	-3.54	0
71	SLU 70	-110	0	2779	0.02	-3.54	0
71	SLU 71	-110	0	2779	0.02	-3.54	0
71	SLU 72	-110	0	2779	0.02	-3.54	0
71	SLU 73	-90	0	3389	0.02	-2.89	0
71	SLU 74	-90	0	3389	0.02	-2.89	0
71	SLU 75	-90	0	3389	0.02	-2.89	0
71	SLU 76	-90	0	3389	0.02	-2.89	0
71	SLU 77	-90	0	3389	0.02	-2.89	0
71	SLU 78	-90	0	3389	0.02	-2.89	0
71	SLU 79	-90	0	3389	0.02	-2.89	0
71	SLU 80	-90	0	3389	0.02	-2.89	0
71	SLU 81	-82	0	3651	0.02	-2.62	0
71	SLU 82	-82	0	3651	0.02	-2.62	0
71	SLU 83	-82	0	3651	0.02	-2.62	0
71	SLU 84	-82	0	3651	0.02	-2.62	0
71	SLE RA 1	-84	0	2048	0.02	-2.7	0
71	SLE RA 2	-84	0	2048	0.02	-2.7	0
71	SLE RA 3	-84	0	2048	0.02	-2.7	0
71	SLE RA 4	-84	0	2048	0.02	-2.7	0
71	SLE RA 5	-84	0	2048	0.02	-2.7	0
71	SLE RA 6	-84	0	2048	0.02	-2.7	0
71	SLE RA 7	-84	0	2048	0.02	-2.7	0
71	SLE RA 8	-84	0	2048	0.02	-2.7	0
71	SLE RA 9	-84	0	2048	0.02	-2.7	0
71	SLE RA 10	-71	0	2455	0.02	-2.27	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
71	SLE RA 11	-71	0	2455	0.02	-2.27	0
71	SLE RA 12	-71	0	2455	0.02	-2.27	0
71	SLE RA 13	-71	0	2455	0.02	-2.27	0
71	SLE RA 14	-71	0	2455	0.02	-2.27	0
71	SLE RA 15	-71	0	2455	0.02	-2.27	0
71	SLE RA 16	-71	0	2455	0.02	-2.27	0
71	SLE RA 17	-71	0	2455	0.02	-2.27	0
71	SLE RA 18	-65	0	2630	0.02	-2.09	0
71	SLE RA 19	-65	0	2630	0.02	-2.09	0
71	SLE RA 20	-65	0	2630	0.02	-2.09	0
71	SLE RA 21	-65	0	2630	0.02	-2.09	0
71	SLE FR 1	-84	0	2048	0.02	-2.7	0
71	SLE FR 2	-84	0	2048	0.02	-2.7	0
71	SLE FR 3	-84	0	2048	0.02	-2.7	0
71	SLE FR 4	-79	0	2223	0.02	-2.52	0
71	SLE FR 5	-79	0	2223	0.02	-2.52	0
71	SLE FR 6	-75	0	2339	0.02	-2.4	0
71	SLE QP 1	-84	0	2048	0.02	-2.7	0
71	SLE QP 2	-79	0	2223	0.02	-2.52	0
71	SLD 1	148	11	2108	-16.97	5.38	-0.43
71	SLD 2	148	11	2108	-16.97	5.38	-0.43
71	SLD 3	121	0	2089	8.22	4.45	0.2
71	SLD 4	121	0	2089	8.22	4.45	0.2
71	SLD 5	30	21	2217	-43.28	1.27	-1.09
71	SLD 6	30	21	2217	-43.28	1.27	-1.09
71	SLD 7	-59	-18	2154	40.68	-1.85	1.02
71	SLD 8	-59	-18	2154	40.68	-1.85	1.02
71	SLD 9	-98	18	2291	-40.65	-3.19	-1.02
71	SLD 10	-98	18	2291	-40.65	-3.19	-1.02
71	SLD 11	-187	-21	2228	43.32	-6.31	1.09
71	SLD 12	-187	-21	2228	43.32	-6.31	1.09
71	SLD 13	-278	0	2356	-8.19	-9.49	-0.2
71	SLD 14	-278	0	2356	-8.19	-9.49	-0.2
71	SLD 15	-305	-11	2337	17	-10.42	0.43
71	SLD 16	-305	-11	2337	17	-10.42	0.43
71	SLV 1	458	29	1953	-43.55	16.25	-1.1
71	SLV 2	458	29	1953	-43.55	16.25	-1.1
71	SLV 3	395	-1	1907	21.06	14.04	0.52
71	SLV 4	395	-1	1907	21.06	14.04	0.52
71	SLV 5	178	55	2211	-111.04	6.47	-2.8
71	SLV 6	178	55	2211	-111.04	6.47	-2.8
71	SLV 7	-32	-46	2058	104.32	-0.91	2.62
71	SLV 8	-32	-46	2058	104.32	-0.91	2.62
71	SLV 9	-125	46	2387	-104.29	-4.13	-2.62
71	SLV 10	-125	46	2387	-104.29	-4.13	-2.62
71	SLV 11	-335	-55	2234	111.08	-11.51	2.8
71	SLV 12	-335	-55	2234	111.08	-11.51	2.8
71	SLV 13	-552	1	2538	-21.03	-19.07	-0.52
71	SLV 14	-552	1	2538	-21.03	-19.07	-0.52
71	SLV 15	-615	-29	2493	43.58	-21.29	1.1
71	SLV 16	-615	-29	2493	43.58	-21.29	1.1
72	SLU 1	-195	0	1991	0.03	-8.79	0
72	SLU 2	-195	0	1991	0.03	-8.79	0
72	SLU 3	-195	0	1991	0.03	-8.79	0
72	SLU 4	-195	0	1991	0.03	-8.79	0
72	SLU 5	-195	0	1991	0.03	-8.79	0
72	SLU 6	-195	0	1991	0.03	-8.79	0
72	SLU 7	-195	0	1991	0.03	-8.79	0
72	SLU 8	-195	0	1991	0.03	-8.79	0
72	SLU 9	-195	0	1991	0.03	-8.79	0
72	SLU 10	-222	0	2628	0.03	-10.06	0
72	SLU 11	-222	0	2628	0.03	-10.06	0
72	SLU 12	-222	0	2628	0.03	-10.06	0
72	SLU 13	-222	0	2628	0.03	-10.06	0
72	SLU 14	-222	0	2628	0.03	-10.06	0
72	SLU 15	-222	0	2628	0.03	-10.06	0
72	SLU 16	-222	0	2628	0.03	-10.06	0
72	SLU 17	-222	0	2628	0.03	-10.06	0
72	SLU 18	-233	0	2901	0.02	-10.6	0
72	SLU 19	-233	0	2901	0.02	-10.6	0
72	SLU 20	-233	0	2901	0.02	-10.6	0
72	SLU 21	-233	0	2901	0.02	-10.6	0
72	SLU 22	-225	0	2414	0.03	-10.23	0
72	SLU 23	-225	0	2414	0.03	-10.23	0
72	SLU 24	-225	0	2414	0.03	-10.23	0
72	SLU 25	-225	0	2414	0.03	-10.23	0
72	SLU 26	-225	0	2414	0.03	-10.23	0
72	SLU 27	-225	0	2414	0.03	-10.23	0
72	SLU 28	-225	0	2414	0.03	-10.23	0
72	SLU 29	-225	0	2414	0.03	-10.23	0
72	SLU 30	-225	0	2414	0.03	-10.23	0
72	SLU 31	-252	0	3051	0.03	-11.49	0
72	SLU 32	-252	0	3051	0.03	-11.49	0
72	SLU 33	-252	0	3051	0.03	-11.49	0
72	SLU 34	-252	0	3051	0.03	-11.49	0
72	SLU 35	-252	0	3051	0.03	-11.49	0
72	SLU 36	-252	0	3051	0.03	-11.49	0
72	SLU 37	-252	0	3051	0.03	-11.49	0
72	SLU 38	-252	0	3051	0.03	-11.49	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
72	SLU 39	-264	0	3324	0.03	-12.04	0
72	SLU 40	-264	0	3324	0.03	-12.04	0
72	SLU 41	-264	0	3324	0.03	-12.04	0
72	SLU 42	-264	0	3324	0.03	-12.04	0
72	SLU 43	-242	0	2443	0.04	-10.93	0
72	SLU 44	-242	0	2443	0.04	-10.93	0
72	SLU 45	-242	0	2443	0.04	-10.93	0
72	SLU 46	-242	0	2443	0.04	-10.93	0
72	SLU 47	-242	0	2443	0.04	-10.93	0
72	SLU 48	-242	0	2443	0.04	-10.93	0
72	SLU 49	-242	0	2443	0.04	-10.93	0
72	SLU 50	-242	0	2443	0.04	-10.93	0
72	SLU 51	-242	0	2443	0.04	-10.93	0
72	SLU 52	-269	0	3080	0.03	-12.2	0
72	SLU 53	-269	0	3080	0.03	-12.2	0
72	SLU 54	-269	0	3080	0.03	-12.2	0
72	SLU 55	-269	0	3080	0.03	-12.2	0
72	SLU 56	-269	0	3080	0.03	-12.2	0
72	SLU 57	-269	0	3080	0.03	-12.2	0
72	SLU 58	-269	0	3080	0.03	-12.2	0
72	SLU 59	-269	0	3080	0.03	-12.2	0
72	SLU 60	-281	0	3353	0.03	-12.74	0
72	SLU 61	-281	0	3353	0.03	-12.74	0
72	SLU 62	-281	0	3353	0.03	-12.74	0
72	SLU 63	-281	0	3353	0.03	-12.74	0
72	SLU 64	-273	0	2866	0.04	-12.37	0
72	SLU 65	-273	0	2866	0.04	-12.37	0
72	SLU 66	-273	0	2866	0.04	-12.37	0
72	SLU 67	-273	0	2866	0.04	-12.37	0
72	SLU 68	-273	0	2866	0.04	-12.37	0
72	SLU 69	-273	0	2866	0.04	-12.37	0
72	SLU 70	-273	0	2866	0.04	-12.37	0
72	SLU 71	-273	0	2866	0.04	-12.37	0
72	SLU 72	-273	0	2866	0.04	-12.37	0
72	SLU 73	-300	0	3503	0.04	-13.64	0
72	SLU 74	-300	0	3503	0.04	-13.64	0
72	SLU 75	-300	0	3503	0.04	-13.64	0
72	SLU 76	-300	0	3503	0.04	-13.64	0
72	SLU 77	-300	0	3503	0.04	-13.64	0
72	SLU 78	-300	0	3503	0.04	-13.64	0
72	SLU 79	-300	0	3503	0.04	-13.64	0
72	SLU 80	-300	0	3503	0.04	-13.64	0
72	SLU 81	-312	0	3776	0.03	-14.18	0
72	SLU 82	-312	0	3776	0.03	-14.18	0
72	SLU 83	-312	0	3776	0.03	-14.18	0
72	SLU 84	-312	0	3776	0.03	-14.18	0
72	SLE RA 1	-203	0	2112	0.03	-9.2	0
72	SLE RA 2	-203	0	2112	0.03	-9.2	0
72	SLE RA 3	-203	0	2112	0.03	-9.2	0
72	SLE RA 4	-203	0	2112	0.03	-9.2	0
72	SLE RA 5	-203	0	2112	0.03	-9.2	0
72	SLE RA 6	-203	0	2112	0.03	-9.2	0
72	SLE RA 7	-203	0	2112	0.03	-9.2	0
72	SLE RA 8	-203	0	2112	0.03	-9.2	0
72	SLE RA 9	-203	0	2112	0.03	-9.2	0
72	SLE RA 10	-221	0	2536	0.03	-10.04	0
72	SLE RA 11	-221	0	2536	0.03	-10.04	0
72	SLE RA 12	-221	0	2536	0.03	-10.04	0
72	SLE RA 13	-221	0	2536	0.03	-10.04	0
72	SLE RA 14	-221	0	2536	0.03	-10.04	0
72	SLE RA 15	-221	0	2536	0.03	-10.04	0
72	SLE RA 16	-221	0	2536	0.03	-10.04	0
72	SLE RA 17	-221	0	2536	0.03	-10.04	0
72	SLE RA 18	-229	0	2718	0.03	-10.41	0
72	SLE RA 19	-229	0	2718	0.03	-10.41	0
72	SLE RA 20	-229	0	2718	0.03	-10.41	0
72	SLE RA 21	-229	0	2718	0.03	-10.41	0
72	SLE FR 1	-203	0	2112	0.03	-9.2	0
72	SLE FR 2	-203	0	2112	0.03	-9.2	0
72	SLE FR 3	-203	0	2112	0.03	-9.2	0
72	SLE FR 4	-211	0	2294	0.03	-9.56	0
72	SLE FR 5	-211	0	2294	0.03	-9.56	0
72	SLE FR 6	-216	0	2415	0.03	-9.8	0
72	SLE QP 1	-203	0	2112	0.03	-9.2	0
72	SLE QP 2	-211	0	2294	0.03	-9.56	0
72	SLD 1	-54	38	2049	-16.2	-0.72	-0.26
72	SLD 2	-54	38	2049	-16.2	-0.72	-0.26
72	SLD 3	-32	-77	2015	31.45	0.47	0.56
72	SLD 4	-32	-77	2015	31.45	0.47	0.56
72	SLD 5	-197	185	2272	-77.1	-8.71	-1.31
72	SLD 6	-197	185	2272	-77.1	-8.71	-1.31
72	SLD 7	-124	-197	2158	81.71	-4.75	1.41
72	SLD 8	-124	-197	2158	81.71	-4.75	1.41
72	SLD 9	-298	197	2429	-81.65	-14.37	-1.4
72	SLD 10	-298	197	2429	-81.65	-14.37	-1.4
72	SLD 11	-225	-185	2315	77.16	-10.41	1.32
72	SLD 12	-225	-185	2315	77.16	-10.41	1.32
72	SLD 13	-390	77	2573	-31.39	-19.59	-0.56
72	SLD 14	-390	77	2573	-31.39	-19.59	-0.56



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
72	SLD 15	-368	-38	2538	16.26	-18.4	0.26
72	SLD 16	-368	-38	2538	16.26	-18.4	0.26
72	SLV 1	161	97	1715	-41.61	11.36	-0.66
72	SLV 2	161	97	1715	-41.61	11.36	-0.66
72	SLV 3	212	-197	1634	80.62	14.18	1.43
72	SLV 4	212	-197	1634	80.62	14.18	1.43
72	SLV 5	-178	474	2244	-197.84	-7.56	-3.37
72	SLV 6	-178	474	2244	-197.84	-7.56	-3.37
72	SLV 7	-6	-504	1972	209.58	1.83	3.6
72	SLV 8	-6	-504	1972	209.58	1.83	3.6
72	SLV 9	-416	504	2615	-209.52	-20.96	-3.6
72	SLV 10	-416	504	2615	-209.52	-20.96	-3.6
72	SLV 11	-245	-474	2344	197.9	-11.56	3.37
72	SLV 12	-245	-474	2344	197.9	-11.56	3.37
72	SLV 13	-634	197	2954	-80.56	-33.3	-1.43
72	SLV 14	-634	197	2954	-80.56	-33.3	-1.43
72	SLV 15	-583	-97	2872	41.67	-30.48	0.67
72	SLV 16	-583	-97	2872	41.67	-30.48	0.67
73	SLU 1	-283	0	2356	0.03	-110.83	-0.02
73	SLU 2	-283	0	2356	0.03	-110.83	-0.02
73	SLU 3	-283	0	2356	0.03	-110.83	-0.02
73	SLU 4	-283	0	2356	0.03	-110.83	-0.02
73	SLU 5	-283	0	2356	0.03	-110.83	-0.02
73	SLU 6	-283	0	2356	0.03	-110.83	-0.02
73	SLU 7	-283	0	2356	0.03	-110.83	-0.02
73	SLU 8	-283	0	2356	0.03	-110.83	-0.02
73	SLU 9	-283	0	2356	0.03	-110.83	-0.02
73	SLU 10	-359	0	3110	-0.01	-144.83	-0.01
73	SLU 11	-359	0	3110	-0.01	-144.83	-0.01
73	SLU 12	-359	0	3110	-0.01	-144.83	-0.01
73	SLU 13	-359	0	3110	-0.01	-144.83	-0.01
73	SLU 14	-359	0	3110	-0.01	-144.83	-0.01
73	SLU 15	-359	0	3110	-0.01	-144.83	-0.01
73	SLU 16	-359	0	3110	-0.01	-144.83	-0.01
73	SLU 17	-359	0	3110	-0.01	-144.83	-0.01
73	SLU 18	-391	0	3434	-0.02	-159.4	-0.01
73	SLU 19	-391	0	3434	-0.02	-159.4	-0.01
73	SLU 20	-391	0	3434	-0.02	-159.4	-0.01
73	SLU 21	-391	0	3434	-0.02	-159.4	-0.01
73	SLU 22	-339	0	2858	0.02	-133.99	-0.02
73	SLU 23	-339	0	2858	0.02	-133.99	-0.02
73	SLU 24	-339	0	2858	0.02	-133.99	-0.02
73	SLU 25	-339	0	2858	0.02	-133.99	-0.02
73	SLU 26	-339	0	2858	0.02	-133.99	-0.02
73	SLU 27	-339	0	2858	0.02	-133.99	-0.02
73	SLU 28	-339	0	2858	0.02	-133.99	-0.02
73	SLU 29	-339	0	2858	0.02	-133.99	-0.02
73	SLU 30	-339	0	2858	0.02	-133.99	-0.02
73	SLU 31	-414	0	3613	-0.02	-167.99	-0.01
73	SLU 32	-414	0	3613	-0.02	-167.99	-0.01
73	SLU 33	-414	0	3613	-0.02	-167.99	-0.01
73	SLU 34	-414	0	3613	-0.02	-167.99	-0.01
73	SLU 35	-414	0	3613	-0.02	-167.99	-0.01
73	SLU 36	-414	0	3613	-0.02	-167.99	-0.01
73	SLU 37	-414	0	3613	-0.02	-167.99	-0.01
73	SLU 38	-414	0	3613	-0.02	-167.99	-0.01
73	SLU 39	-447	0	3936	-0.04	-182.56	-0.01
73	SLU 40	-447	0	3936	-0.04	-182.56	-0.01
73	SLU 41	-447	0	3936	-0.04	-182.56	-0.01
73	SLU 42	-447	0	3936	-0.04	-182.56	-0.01
73	SLU 43	-349	0	2890	0.05	-136.13	-0.02
73	SLU 44	-349	0	2890	0.05	-136.13	-0.02
73	SLU 45	-349	0	2890	0.05	-136.13	-0.02
73	SLU 46	-349	0	2890	0.05	-136.13	-0.02
73	SLU 47	-349	0	2890	0.05	-136.13	-0.02
73	SLU 48	-349	0	2890	0.05	-136.13	-0.02
73	SLU 49	-349	0	2890	0.05	-136.13	-0.02
73	SLU 50	-349	0	2890	0.05	-136.13	-0.02
73	SLU 51	-349	0	2890	0.05	-136.13	-0.02
73	SLU 52	-424	0	3645	0.01	-170.13	-0.02
73	SLU 53	-424	0	3645	0.01	-170.13	-0.02
73	SLU 54	-424	0	3645	0.01	-170.13	-0.02
73	SLU 55	-424	0	3645	0.01	-170.13	-0.02
73	SLU 56	-424	0	3645	0.01	-170.13	-0.02
73	SLU 57	-424	0	3645	0.01	-170.13	-0.02
73	SLU 58	-424	0	3645	0.01	-170.13	-0.02
73	SLU 59	-424	0	3645	0.01	-170.13	-0.02
73	SLU 60	-457	0	3968	-0.01	-184.7	-0.02
73	SLU 61	-457	0	3968	-0.01	-184.7	-0.02
73	SLU 62	-457	0	3968	-0.01	-184.7	-0.02
73	SLU 63	-457	0	3968	-0.01	-184.7	-0.02
73	SLU 64	-405	0	3393	0.04	-159.3	-0.02
73	SLU 65	-405	0	3393	0.04	-159.3	-0.02
73	SLU 66	-405	0	3393	0.04	-159.3	-0.02
73	SLU 67	-405	0	3393	0.04	-159.3	-0.02
73	SLU 68	-405	0	3393	0.04	-159.3	-0.02
73	SLU 69	-405	0	3393	0.04	-159.3	-0.02
73	SLU 70	-405	0	3393	0.04	-159.3	-0.02
73	SLU 71	-405	0	3393	0.04	-159.3	-0.02



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
73	SLU 72	-405	0	3393	0.04	-159.3	-0.02
73	SLU 73	-480	0	4147	0	-193.3	-0.02
73	SLU 74	-480	0	4147	0	-193.3	-0.02
73	SLU 75	-480	0	4147	0	-193.3	-0.02
73	SLU 76	-480	0	4147	0	-193.3	-0.02
73	SLU 77	-480	0	4147	0	-193.3	-0.02
73	SLU 78	-480	0	4147	0	-193.3	-0.02
73	SLU 79	-480	0	4147	0	-193.3	-0.02
73	SLU 80	-480	0	4147	0	-193.3	-0.02
73	SLU 81	-513	0	4471	-0.02	-207.87	-0.02
73	SLU 82	-513	0	4471	-0.02	-207.87	-0.02
73	SLU 83	-513	0	4471	-0.02	-207.87	-0.02
73	SLU 84	-513	0	4471	-0.02	-207.87	-0.02
73	SLE RA 1	-299	0	2500	0.03	-117.44	-0.02
73	SLE RA 2	-299	0	2500	0.03	-117.44	-0.02
73	SLE RA 3	-299	0	2500	0.03	-117.44	-0.02
73	SLE RA 4	-299	0	2500	0.03	-117.44	-0.02
73	SLE RA 5	-299	0	2500	0.03	-117.44	-0.02
73	SLE RA 6	-299	0	2500	0.03	-117.44	-0.02
73	SLE RA 7	-299	0	2500	0.03	-117.44	-0.02
73	SLE RA 8	-299	0	2500	0.03	-117.44	-0.02
73	SLE RA 9	-299	0	2500	0.03	-117.44	-0.02
73	SLE RA 10	-349	0	3002	0	-140.11	-0.02
73	SLE RA 11	-349	0	3002	0	-140.11	-0.02
73	SLE RA 12	-349	0	3002	0	-140.11	-0.02
73	SLE RA 13	-349	0	3002	0	-140.11	-0.02
73	SLE RA 14	-349	0	3002	0	-140.11	-0.02
73	SLE RA 15	-349	0	3002	0	-140.11	-0.02
73	SLE RA 16	-349	0	3002	0	-140.11	-0.02
73	SLE RA 17	-349	0	3002	0	-140.11	-0.02
73	SLE RA 18	-371	0	3218	-0.01	-149.82	-0.01
73	SLE RA 19	-371	0	3218	-0.01	-149.82	-0.01
73	SLE RA 20	-371	0	3218	-0.01	-149.82	-0.01
73	SLE RA 21	-371	0	3218	-0.01	-149.82	-0.01
73	SLE FR 1	-299	0	2500	0.03	-117.44	-0.02
73	SLE FR 2	-299	0	2500	0.03	-117.44	-0.02
73	SLE FR 3	-299	0	2500	0.03	-117.44	-0.02
73	SLE FR 4	-321	0	2715	0.02	-127.16	-0.02
73	SLE FR 5	-321	0	2715	0.02	-127.16	-0.02
73	SLE FR 6	-335	0	2859	0.01	-133.63	-0.02
73	SLE QP 1	-299	0	2500	0.03	-117.44	-0.02
73	SLE QP 2	-321	0	2715	0.02	-127.16	-0.02
73	SLD 1	-209	109	2280	-41.93	-101.72	8.66
73	SLD 2	-209	109	2280	-41.93	-101.72	8.66
73	SLD 3	-194	-206	2222	78.59	-98.31	-16.36
73	SLD 4	-194	-206	2222	78.59	-98.31	-16.36
73	SLD 5	-310	511	2672	-195.36	-124.71	40.54
73	SLD 6	-310	511	2672	-195.36	-124.71	40.54
73	SLD 7	-260	-541	2479	206.38	-113.32	-42.88
73	SLD 8	-260	-541	2479	206.38	-113.32	-42.88
73	SLD 9	-381	540	2951	-206.34	-140.99	42.84
73	SLD 10	-381	540	2951	-206.34	-140.99	42.84
73	SLD 11	-332	-512	2758	195.39	-129.61	-40.58
73	SLD 12	-332	-512	2758	195.39	-129.61	-40.58
73	SLD 13	-448	206	3208	-78.55	-156.01	16.33
73	SLD 14	-448	206	3208	-78.55	-156.01	16.33
73	SLD 15	-433	-110	3150	41.97	-152.6	-8.7
73	SLD 16	-433	-110	3150	41.97	-152.6	-8.7
73	SLV 1	-55	281	1685	-107.61	-66.93	22.25
73	SLV 2	-55	281	1685	-107.61	-66.93	22.25
73	SLV 3	-20	-529	1548	201.59	-58.85	-41.95
73	SLV 4	-20	-529	1548	201.59	-58.85	-41.95
73	SLV 5	-295	1312	2614	-501.22	-121.35	104.04
73	SLV 6	-295	1312	2614	-501.22	-121.35	104.04
73	SLV 7	-177	-1387	2157	529.43	-94.41	-109.97
73	SLV 8	-177	-1387	2157	529.43	-94.41	-109.97
73	SLV 9	-465	1386	3273	-529.4	-159.91	109.94
73	SLV 10	-465	1386	3273	-529.4	-159.91	109.94
73	SLV 11	-347	-1312	2816	501.25	-132.97	-104.07
73	SLV 12	-347	-1312	2816	501.25	-132.97	-104.07
73	SLV 13	-621	528	3882	-201.55	-195.47	41.92
73	SLV 14	-621	528	3882	-201.55	-195.47	41.92
73	SLV 15	-586	-281	3745	107.65	-187.39	-22.29
73	SLV 16	-586	-281	3745	107.65	-187.39	-22.29
75	SLU 1	298	0	1256	0.01	6.14	0
75	SLU 2	298	0	1256	0.01	6.14	0
75	SLU 3	298	0	1256	0.01	6.14	0
75	SLU 4	298	0	1256	0.01	6.14	0
75	SLU 5	298	0	1256	0.01	6.14	0
75	SLU 6	298	0	1256	0.01	6.14	0
75	SLU 7	298	0	1256	0.01	6.14	0
75	SLU 8	298	0	1256	0.01	6.14	0
75	SLU 9	298	0	1256	0.01	6.14	0
75	SLU 10	381	0	1643	0.01	7.46	0
75	SLU 11	381	0	1643	0.01	7.46	0
75	SLU 12	381	0	1643	0.01	7.46	0
75	SLU 13	381	0	1643	0.01	7.46	0
75	SLU 14	381	0	1643	0.01	7.46	0
75	SLU 15	381	0	1643	0.01	7.46	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
75	SLU 16	381	0	1643	0.01	7.46	0
75	SLU 17	381	0	1643	0.01	7.46	0
75	SLU 18	416	0	1808	0.01	8.02	0
75	SLU 19	416	0	1808	0.01	8.02	0
75	SLU 20	416	0	1808	0.01	8.02	0
75	SLU 21	416	0	1808	0.01	8.02	0
75	SLU 22	355	0	1511	0.01	7.14	0
75	SLU 23	355	0	1511	0.01	7.14	0
75	SLU 24	355	0	1511	0.01	7.14	0
75	SLU 25	355	0	1511	0.01	7.14	0
75	SLU 26	355	0	1511	0.01	7.14	0
75	SLU 27	355	0	1511	0.01	7.14	0
75	SLU 28	355	0	1511	0.01	7.14	0
75	SLU 29	355	0	1511	0.01	7.14	0
75	SLU 30	355	0	1511	0.01	7.14	0
75	SLU 31	437	0	1897	0.01	8.46	0
75	SLU 32	437	0	1897	0.01	8.46	0
75	SLU 33	437	0	1897	0.01	8.46	0
75	SLU 34	437	0	1897	0.01	8.46	0
75	SLU 35	437	0	1897	0.01	8.46	0
75	SLU 36	437	0	1897	0.01	8.46	0
75	SLU 37	437	0	1897	0.01	8.46	0
75	SLU 38	437	0	1897	0.01	8.46	0
75	SLU 39	473	0	2063	0.01	9.03	0
75	SLU 40	473	0	2063	0.01	9.03	0
75	SLU 41	473	0	2063	0.01	9.03	0
75	SLU 42	473	0	2063	0.01	9.03	0
75	SLU 43	368	0	1545	0.01	7.63	0
75	SLU 44	368	0	1545	0.01	7.63	0
75	SLU 45	368	0	1545	0.01	7.63	0
75	SLU 46	368	0	1545	0.01	7.63	0
75	SLU 47	368	0	1545	0.01	7.63	0
75	SLU 48	368	0	1545	0.01	7.63	0
75	SLU 49	368	0	1545	0.01	7.63	0
75	SLU 50	368	0	1545	0.01	7.63	0
75	SLU 51	368	0	1545	0.01	7.63	0
75	SLU 52	451	0	1932	0.01	8.95	0
75	SLU 53	451	0	1932	0.01	8.95	0
75	SLU 54	451	0	1932	0.01	8.95	0
75	SLU 55	451	0	1932	0.01	8.95	0
75	SLU 56	451	0	1932	0.01	8.95	0
75	SLU 57	451	0	1932	0.01	8.95	0
75	SLU 58	451	0	1932	0.01	8.95	0
75	SLU 59	451	0	1932	0.01	8.95	0
75	SLU 60	487	0	2098	0.01	9.52	0
75	SLU 61	487	0	2098	0.01	9.52	0
75	SLU 62	487	0	2098	0.01	9.52	0
75	SLU 63	487	0	2098	0.01	9.52	0
75	SLU 64	425	0	1800	0.01	8.64	0
75	SLU 65	425	0	1800	0.01	8.64	0
75	SLU 66	425	0	1800	0.01	8.64	0
75	SLU 67	425	0	1800	0.01	8.64	0
75	SLU 68	425	0	1800	0.01	8.64	0
75	SLU 69	425	0	1800	0.01	8.64	0
75	SLU 70	425	0	1800	0.01	8.64	0
75	SLU 71	425	0	1800	0.01	8.64	0
75	SLU 72	425	0	1800	0.01	8.64	0
75	SLU 73	508	0	2187	0.01	9.96	0
75	SLU 74	508	0	2187	0.01	9.96	0
75	SLU 75	508	0	2187	0.01	9.96	0
75	SLU 76	508	0	2187	0.01	9.96	0
75	SLU 77	508	0	2187	0.01	9.96	0
75	SLU 78	508	0	2187	0.01	9.96	0
75	SLU 79	508	0	2187	0.01	9.96	0
75	SLU 80	508	0	2187	0.01	9.96	0
75	SLU 81	543	0	2352	0.01	10.53	0
75	SLU 82	543	0	2352	0.01	10.53	0
75	SLU 83	543	0	2352	0.01	10.53	0
75	SLU 84	543	0	2352	0.01	10.53	0
75	SLE RA 1	314	0	1329	0.01	6.42	0
75	SLE RA 2	314	0	1329	0.01	6.42	0
75	SLE RA 3	314	0	1329	0.01	6.42	0
75	SLE RA 4	314	0	1329	0.01	6.42	0
75	SLE RA 5	314	0	1329	0.01	6.42	0
75	SLE RA 6	314	0	1329	0.01	6.42	0
75	SLE RA 7	314	0	1329	0.01	6.42	0
75	SLE RA 8	314	0	1329	0.01	6.42	0
75	SLE RA 9	314	0	1329	0.01	6.42	0
75	SLE RA 10	370	0	1586	0.01	7.3	0
75	SLE RA 11	370	0	1586	0.01	7.3	0
75	SLE RA 12	370	0	1586	0.01	7.3	0
75	SLE RA 13	370	0	1586	0.01	7.3	0
75	SLE RA 14	370	0	1586	0.01	7.3	0
75	SLE RA 15	370	0	1586	0.01	7.3	0
75	SLE RA 16	370	0	1586	0.01	7.3	0
75	SLE RA 17	370	0	1586	0.01	7.3	0
75	SLE RA 18	393	0	1697	0.01	7.68	0
75	SLE RA 19	393	0	1697	0.01	7.68	0
75	SLE RA 20	393	0	1697	0.01	7.68	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
75	SLE RA 21	393	0	1697	0.01	7.68	0
75	SLE FR 1	314	0	1329	0.01	6.42	0
75	SLE FR 2	314	0	1329	0.01	6.42	0
75	SLE FR 3	314	0	1329	0.01	6.42	0
75	SLE FR 4	338	0	1439	0.01	6.8	0
75	SLE FR 5	338	0	1439	0.01	6.8	0
75	SLE FR 6	354	0	1513	0.01	7.05	0
75	SLE QP 1	314	0	1329	0.01	6.42	0
75	SLE QP 2	338	0	1439	0.01	6.8	0
75	SLD 1	459	8	1779	-6.18	11.18	0.93
75	SLD 2	459	8	1779	-6.18	11.18	0.93
75	SLD 3	476	-18	1827	10.66	11.79	-1.69
75	SLD 4	476	-18	1827	10.66	11.79	-1.69
75	SLD 5	348	43	1467	-27.39	7.18	4.25
75	SLD 6	348	43	1467	-27.39	7.18	4.25
75	SLD 7	406	-46	1629	28.74	9.23	-4.48
75	SLD 8	406	-46	1629	28.74	9.23	-4.48
75	SLD 9	271	46	1249	-28.73	4.37	4.48
75	SLD 10	271	46	1249	-28.73	4.37	4.48
75	SLD 11	328	-43	1411	27.4	6.42	-4.25
75	SLD 12	328	-43	1411	27.4	6.42	-4.25
75	SLD 13	200	18	1051	-10.65	1.81	1.69
75	SLD 14	200	18	1051	-10.65	1.81	1.69
75	SLD 15	217	-8	1099	6.19	2.42	-0.93
75	SLD 16	217	-8	1099	6.19	2.42	-0.93
75	SLV 1	624	21	2244	-15.88	17.17	2.39
75	SLV 2	624	21	2244	-15.88	17.17	2.39
75	SLV 3	665	-47	2359	27.26	18.62	-4.32
75	SLV 4	665	-47	2359	27.26	18.62	-4.32
75	SLV 5	362	110	1507	-70.2	7.71	10.9
75	SLV 6	362	110	1507	-70.2	7.71	10.9
75	SLV 7	498	-118	1889	73.62	12.54	-11.48
75	SLV 8	498	-118	1889	73.62	12.54	-11.48
75	SLV 9	178	118	989	-73.61	1.06	11.47
75	SLV 10	178	118	989	-73.61	1.06	11.47
75	SLV 11	314	-110	1372	70.21	5.89	-10.9
75	SLV 12	314	-110	1372	70.21	5.89	-10.9
75	SLV 13	11	47	519	-27.25	-5.02	4.32
75	SLV 14	11	47	519	-27.25	-5.02	4.32
75	SLV 15	52	-22	634	15.9	-3.57	-2.39
75	SLV 16	52	-22	634	15.9	-3.57	-2.39
76	SLU 1	132	0	2219	0.01	6.71	0
76	SLU 2	132	0	2219	0.01	6.71	0
76	SLU 3	132	0	2219	0.01	6.71	0
76	SLU 4	132	0	2219	0.01	6.71	0
76	SLU 5	132	0	2219	0.01	6.71	0
76	SLU 6	132	0	2219	0.01	6.71	0
76	SLU 7	132	0	2219	0.01	6.71	0
76	SLU 8	132	0	2219	0.01	6.71	0
76	SLU 9	132	0	2219	0.01	6.71	0
76	SLU 10	143	0	2935	0.01	7.38	0
76	SLU 11	143	0	2935	0.01	7.38	0
76	SLU 12	143	0	2935	0.01	7.38	0
76	SLU 13	143	0	2935	0.01	7.38	0
76	SLU 14	143	0	2935	0.01	7.38	0
76	SLU 15	143	0	2935	0.01	7.38	0
76	SLU 16	143	0	2935	0.01	7.38	0
76	SLU 17	143	0	2935	0.01	7.38	0
76	SLU 18	147	0	3243	0.01	7.66	0
76	SLU 19	147	0	3243	0.01	7.66	0
76	SLU 20	147	0	3243	0.01	7.66	0
76	SLU 21	147	0	3243	0.01	7.66	0
76	SLU 22	145	0	2680	0.01	7.47	0
76	SLU 23	145	0	2680	0.01	7.47	0
76	SLU 24	145	0	2680	0.01	7.47	0
76	SLU 25	145	0	2680	0.01	7.47	0
76	SLU 26	145	0	2680	0.01	7.47	0
76	SLU 27	145	0	2680	0.01	7.47	0
76	SLU 28	145	0	2680	0.01	7.47	0
76	SLU 29	145	0	2680	0.01	7.47	0
76	SLU 30	145	0	2680	0.01	7.47	0
76	SLU 31	156	0	3396	0.01	8.13	0
76	SLU 32	156	0	3396	0.01	8.13	0
76	SLU 33	156	0	3396	0.01	8.13	0
76	SLU 34	156	0	3396	0.01	8.13	0
76	SLU 35	156	0	3396	0.01	8.13	0
76	SLU 36	156	0	3396	0.01	8.13	0
76	SLU 37	156	0	3396	0.01	8.13	0
76	SLU 38	156	0	3396	0.01	8.13	0
76	SLU 39	160	0	3703	0.01	8.41	0
76	SLU 40	160	0	3703	0.01	8.41	0
76	SLU 41	160	0	3703	0.01	8.41	0
76	SLU 42	160	0	3703	0.01	8.41	0
76	SLU 43	168	0	2727	0.01	8.47	0
76	SLU 44	168	0	2727	0.01	8.47	0
76	SLU 45	168	0	2727	0.01	8.47	0
76	SLU 46	168	0	2727	0.01	8.47	0
76	SLU 47	168	0	2727	0.01	8.47	0
76	SLU 48	168	0	2727	0.01	8.47	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
76	SLU 49	168	0	2727	0.01	8.47	0
76	SLU 50	168	0	2727	0.01	8.47	0
76	SLU 51	168	0	2727	0.01	8.47	0
76	SLU 52	178	0	3443	0.01	9.13	0
76	SLU 53	178	0	3443	0.01	9.13	0
76	SLU 54	178	0	3443	0.01	9.13	0
76	SLU 55	178	0	3443	0.01	9.13	0
76	SLU 56	178	0	3443	0.01	9.13	0
76	SLU 57	178	0	3443	0.01	9.13	0
76	SLU 58	178	0	3443	0.01	9.13	0
76	SLU 59	178	0	3443	0.01	9.13	0
76	SLU 60	182	0	3750	0.01	9.42	0
76	SLU 61	182	0	3750	0.01	9.42	0
76	SLU 62	182	0	3750	0.01	9.42	0
76	SLU 63	182	0	3750	0.01	9.42	0
76	SLU 64	181	0	3188	0.01	9.22	0
76	SLU 65	181	0	3188	0.01	9.22	0
76	SLU 66	181	0	3188	0.01	9.22	0
76	SLU 67	181	0	3188	0.01	9.22	0
76	SLU 68	181	0	3188	0.01	9.22	0
76	SLU 69	181	0	3188	0.01	9.22	0
76	SLU 70	181	0	3188	0.01	9.22	0
76	SLU 71	181	0	3188	0.01	9.22	0
76	SLU 72	181	0	3188	0.01	9.22	0
76	SLU 73	191	0	3904	0.01	9.88	0
76	SLU 74	191	0	3904	0.01	9.88	0
76	SLU 75	191	0	3904	0.01	9.88	0
76	SLU 76	191	0	3904	0.01	9.88	0
76	SLU 77	191	0	3904	0.01	9.88	0
76	SLU 78	191	0	3904	0.01	9.88	0
76	SLU 79	191	0	3904	0.01	9.88	0
76	SLU 80	191	0	3904	0.01	9.88	0
76	SLU 81	195	0	4211	0.01	10.17	0
76	SLU 82	195	0	4211	0.01	10.17	0
76	SLU 83	195	0	4211	0.01	10.17	0
76	SLU 84	195	0	4211	0.01	10.17	0
76	SLE RA 1	136	0	2351	0.01	6.93	0
76	SLE RA 2	136	0	2351	0.01	6.93	0
76	SLE RA 3	136	0	2351	0.01	6.93	0
76	SLE RA 4	136	0	2351	0.01	6.93	0
76	SLE RA 5	136	0	2351	0.01	6.93	0
76	SLE RA 6	136	0	2351	0.01	6.93	0
76	SLE RA 7	136	0	2351	0.01	6.93	0
76	SLE RA 8	136	0	2351	0.01	6.93	0
76	SLE RA 9	136	0	2351	0.01	6.93	0
76	SLE RA 10	143	0	2828	0.01	7.37	0
76	SLE RA 11	143	0	2828	0.01	7.37	0
76	SLE RA 12	143	0	2828	0.01	7.37	0
76	SLE RA 13	143	0	2828	0.01	7.37	0
76	SLE RA 14	143	0	2828	0.01	7.37	0
76	SLE RA 15	143	0	2828	0.01	7.37	0
76	SLE RA 16	143	0	2828	0.01	7.37	0
76	SLE RA 17	143	0	2828	0.01	7.37	0
76	SLE RA 18	146	0	3033	0.01	7.56	0
76	SLE RA 19	146	0	3033	0.01	7.56	0
76	SLE RA 20	146	0	3033	0.01	7.56	0
76	SLE RA 21	146	0	3033	0.01	7.56	0
76	SLE FR 1	136	0	2351	0.01	6.93	0
76	SLE FR 2	136	0	2351	0.01	6.93	0
76	SLE FR 3	136	0	2351	0.01	6.93	0
76	SLE FR 4	139	0	2555	0.01	7.12	0
76	SLE FR 5	139	0	2555	0.01	7.12	0
76	SLE FR 6	141	0	2692	0.01	7.24	0
76	SLE QP 1	136	0	2351	0.01	6.93	0
76	SLE QP 2	139	0	2555	0.01	7.12	0
76	SLD 1	318	17	2906	-16.3	16.56	-0.11
76	SLD 2	318	17	2906	-16.3	16.56	-0.11
76	SLD 3	296	-29	2957	25.57	15.4	0.17
76	SLD 4	296	-29	2957	25.57	15.4	0.17
76	SLD 5	226	76	2584	-68.39	11.71	-0.45
76	SLD 6	226	76	2584	-68.39	11.71	-0.45
76	SLD 7	153	-80	2753	71.19	7.85	0.47
76	SLD 8	153	-80	2753	71.19	7.85	0.47
76	SLD 9	125	80	2358	-71.17	6.39	-0.47
76	SLD 10	125	80	2358	-71.17	6.39	-0.47
76	SLD 11	52	-76	2527	68.41	2.52	0.45
76	SLD 12	52	-76	2527	68.41	2.52	0.45
76	SLD 13	-18	29	2154	-25.56	-1.17	-0.17
76	SLD 14	-18	29	2154	-25.56	-1.17	-0.17
76	SLD 15	-40	-18	2204	16.32	-2.33	0.11
76	SLD 16	-40	-18	2204	16.32	-2.33	0.11
76	SLV 1	564	45	3387	-41.87	29.5	-0.27
76	SLV 2	564	45	3387	-41.87	29.5	-0.27
76	SLV 3	512	-75	3507	65.47	26.76	0.43
76	SLV 4	512	-75	3507	65.47	26.76	0.43
76	SLV 5	345	195	2623	-175.37	17.99	-1.15
76	SLV 6	345	195	2623	-175.37	17.99	-1.15
76	SLV 7	172	-204	3023	182.46	8.86	1.2
76	SLV 8	172	-204	3023	182.46	8.86	1.2



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
76	SLV 9	106	204	2088	-182.44	5.38	-1.2
76	SLV 10	106	204	2088	-182.44	5.38	-1.2
76	SLV 11	-67	-195	2488	175.39	-3.75	1.15
76	SLV 12	-67	-195	2488	175.39	-3.75	1.15
76	SLV 13	-234	75	1603	-65.46	-12.53	-0.43
76	SLV 14	-234	75	1603	-65.46	-12.53	-0.43
76	SLV 15	-286	-45	1723	41.89	-15.27	0.27
76	SLV 16	-286	-45	1723	41.89	-15.27	0.27
77	SLU 1	-16	0	2163	0.01	-0.6	0
77	SLU 2	-16	0	2163	0.01	-0.6	0
77	SLU 3	-16	0	2163	0.01	-0.6	0
77	SLU 4	-16	0	2163	0.01	-0.6	0
77	SLU 5	-16	0	2163	0.01	-0.6	0
77	SLU 6	-16	0	2163	0.01	-0.6	0
77	SLU 7	-16	0	2163	0.01	-0.6	0
77	SLU 8	-16	0	2163	0.01	-0.6	0
77	SLU 9	-16	0	2163	0.01	-0.6	0
77	SLU 10	-69	0	2871	0	-2.72	0
77	SLU 11	-69	0	2871	0	-2.72	0
77	SLU 12	-69	0	2871	0	-2.72	0
77	SLU 13	-69	0	2871	0	-2.72	0
77	SLU 14	-69	0	2871	0	-2.72	0
77	SLU 15	-69	0	2871	0	-2.72	0
77	SLU 16	-69	0	2871	0	-2.72	0
77	SLU 17	-69	0	2871	0	-2.72	0
77	SLU 18	-91	0	3175	0	-3.63	0
77	SLU 19	-91	0	3175	0	-3.63	0
77	SLU 20	-91	0	3175	0	-3.63	0
77	SLU 21	-91	0	3175	0	-3.63	0
77	SLU 22	-41	0	2612	0.01	-1.57	0
77	SLU 23	-41	0	2612	0.01	-1.57	0
77	SLU 24	-41	0	2612	0.01	-1.57	0
77	SLU 25	-41	0	2612	0.01	-1.57	0
77	SLU 26	-41	0	2612	0.01	-1.57	0
77	SLU 27	-41	0	2612	0.01	-1.57	0
77	SLU 28	-41	0	2612	0.01	-1.57	0
77	SLU 29	-41	0	2612	0.01	-1.57	0
77	SLU 30	-41	0	2612	0.01	-1.57	0
77	SLU 31	-93	0	3320	0	-3.69	0
77	SLU 32	-93	0	3320	0	-3.69	0
77	SLU 33	-93	0	3320	0	-3.69	0
77	SLU 34	-93	0	3320	0	-3.69	0
77	SLU 35	-93	0	3320	0	-3.69	0
77	SLU 36	-93	0	3320	0	-3.69	0
77	SLU 37	-93	0	3320	0	-3.69	0
77	SLU 38	-93	0	3320	0	-3.69	0
77	SLU 39	-116	0	3624	0	-4.6	0
77	SLU 40	-116	0	3624	0	-4.6	0
77	SLU 41	-116	0	3624	0	-4.6	0
77	SLU 42	-116	0	3624	0	-4.6	0
77	SLU 43	-13	0	2659	0.01	-0.45	0
77	SLU 44	-13	0	2659	0.01	-0.45	0
77	SLU 45	-13	0	2659	0.01	-0.45	0
77	SLU 46	-13	0	2659	0.01	-0.45	0
77	SLU 47	-13	0	2659	0.01	-0.45	0
77	SLU 48	-13	0	2659	0.01	-0.45	0
77	SLU 49	-13	0	2659	0.01	-0.45	0
77	SLU 50	-13	0	2659	0.01	-0.45	0
77	SLU 51	-13	0	2659	0.01	-0.45	0
77	SLU 52	-65	0	3366	0.01	-2.57	0
77	SLU 53	-65	0	3366	0.01	-2.57	0
77	SLU 54	-65	0	3366	0.01	-2.57	0
77	SLU 55	-65	0	3366	0.01	-2.57	0
77	SLU 56	-65	0	3366	0.01	-2.57	0
77	SLU 57	-65	0	3366	0.01	-2.57	0
77	SLU 58	-65	0	3366	0.01	-2.57	0
77	SLU 59	-65	0	3366	0.01	-2.57	0
77	SLU 60	-88	0	3670	0.01	-3.48	0
77	SLU 61	-88	0	3670	0.01	-3.48	0
77	SLU 62	-88	0	3670	0.01	-3.48	0
77	SLU 63	-88	0	3670	0.01	-3.48	0
77	SLU 64	-37	0	3107	0.01	-1.41	0
77	SLU 65	-37	0	3107	0.01	-1.41	0
77	SLU 66	-37	0	3107	0.01	-1.41	0
77	SLU 67	-37	0	3107	0.01	-1.41	0
77	SLU 68	-37	0	3107	0.01	-1.41	0
77	SLU 69	-37	0	3107	0.01	-1.41	0
77	SLU 70	-37	0	3107	0.01	-1.41	0
77	SLU 71	-37	0	3107	0.01	-1.41	0
77	SLU 72	-37	0	3107	0.01	-1.41	0
77	SLU 73	-90	0	3815	0.01	-3.53	0
77	SLU 74	-90	0	3815	0.01	-3.53	0
77	SLU 75	-90	0	3815	0.01	-3.53	0
77	SLU 76	-90	0	3815	0.01	-3.53	0
77	SLU 77	-90	0	3815	0.01	-3.53	0
77	SLU 78	-90	0	3815	0.01	-3.53	0
77	SLU 79	-90	0	3815	0.01	-3.53	0
77	SLU 80	-90	0	3815	0.01	-3.53	0
77	SLU 81	-112	0	4119	0.01	-4.44	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
77	SLU 82	-112	0	4119	0.01	-4.44	0
77	SLU 83	-112	0	4119	0.01	-4.44	0
77	SLU 84	-112	0	4119	0.01	-4.44	0
77	SLE RA 1	-23	0	2292	0.01	-0.88	0
77	SLE RA 2	-23	0	2292	0.01	-0.88	0
77	SLE RA 3	-23	0	2292	0.01	-0.88	0
77	SLE RA 4	-23	0	2292	0.01	-0.88	0
77	SLE RA 5	-23	0	2292	0.01	-0.88	0
77	SLE RA 6	-23	0	2292	0.01	-0.88	0
77	SLE RA 7	-23	0	2292	0.01	-0.88	0
77	SLE RA 8	-23	0	2292	0.01	-0.88	0
77	SLE RA 9	-23	0	2292	0.01	-0.88	0
77	SLE RA 10	-58	0	2764	0	-2.29	0
77	SLE RA 11	-58	0	2764	0	-2.29	0
77	SLE RA 12	-58	0	2764	0	-2.29	0
77	SLE RA 13	-58	0	2764	0	-2.29	0
77	SLE RA 14	-58	0	2764	0	-2.29	0
77	SLE RA 15	-58	0	2764	0	-2.29	0
77	SLE RA 16	-58	0	2764	0	-2.29	0
77	SLE RA 17	-58	0	2764	0	-2.29	0
77	SLE RA 18	-73	0	2966	0	-2.9	0
77	SLE RA 19	-73	0	2966	0	-2.9	0
77	SLE RA 20	-73	0	2966	0	-2.9	0
77	SLE RA 21	-73	0	2966	0	-2.9	0
77	SLE FR 1	-23	0	2292	0.01	-0.88	0
77	SLE FR 2	-23	0	2292	0.01	-0.88	0
77	SLE FR 3	-23	0	2292	0.01	-0.88	0
77	SLE FR 4	-38	0	2494	0.01	-1.48	0
77	SLE FR 5	-38	0	2494	0.01	-1.48	0
77	SLE FR 6	-48	0	2629	0.01	-1.89	0
77	SLE QP 1	-23	0	2292	0.01	-0.88	0
77	SLE QP 2	-38	0	2494	0.01	-1.48	0
77	SLD 1	155	17	2660	-18.02	6.97	-0.11
77	SLD 2	155	17	2660	-18.02	6.97	-0.11
77	SLD 3	182	-28	2685	27.26	8.16	0.18
77	SLD 4	182	-28	2685	27.26	8.16	0.18
77	SLD 5	-21	74	2506	-74.09	-0.74	-0.48
77	SLD 6	-21	74	2506	-74.09	-0.74	-0.48
77	SLD 7	69	-77	2589	76.87	3.21	0.5
77	SLD 8	69	-77	2589	76.87	3.21	0.5
77	SLD 9	-146	77	2399	-76.86	-6.17	-0.5
77	SLD 10	-146	77	2399	-76.86	-6.17	-0.5
77	SLD 11	-55	-74	2482	74.1	-2.22	0.48
77	SLD 12	-55	-74	2482	74.1	-2.22	0.48
77	SLD 13	-259	28	2303	-27.25	-11.12	-0.18
77	SLD 14	-259	28	2303	-27.25	-11.12	-0.18
77	SLD 15	-232	-17	2328	18.04	-9.94	0.11
77	SLD 16	-232	-17	2328	18.04	-9.94	0.11
77	SLV 1	420	45	2889	-46.27	18.53	-0.29
77	SLV 2	420	45	2889	-46.27	18.53	-0.29
77	SLV 3	484	-71	2947	69.84	21.33	0.46
77	SLV 4	484	-71	2947	69.84	21.33	0.46
77	SLV 5	2	189	2524	-189.99	0.28	-1.23
77	SLV 6	2	189	2524	-189.99	0.28	-1.23
77	SLV 7	216	-196	2719	197.07	9.61	1.28
77	SLV 8	216	-196	2719	197.07	9.61	1.28
77	SLV 9	-292	196	2269	-197.06	-12.57	-1.28
77	SLV 10	-292	196	2269	-197.06	-12.57	-1.28
77	SLV 11	-79	-189	2464	190	-3.24	1.23
77	SLV 12	-79	-189	2464	190	-3.24	1.23
77	SLV 13	-561	71	2041	-69.83	-24.3	-0.46
77	SLV 14	-561	71	2041	-69.83	-24.3	-0.46
77	SLV 15	-497	-45	2099	46.29	-21.5	0.29
77	SLV 16	-497	-45	2099	46.29	-21.5	0.29
78	SLU 1	-126	0	2110	0	-4.74	0
78	SLU 2	-126	0	2110	0	-4.74	0
78	SLU 3	-126	0	2110	0	-4.74	0
78	SLU 4	-126	0	2110	0	-4.74	0
78	SLU 5	-126	0	2110	0	-4.74	0
78	SLU 6	-126	0	2110	0	-4.74	0
78	SLU 7	-126	0	2110	0	-4.74	0
78	SLU 8	-126	0	2110	0	-4.74	0
78	SLU 9	-126	0	2110	0	-4.74	0
78	SLU 10	-223	0	2790	0	-8.49	0
78	SLU 11	-223	0	2790	0	-8.49	0
78	SLU 12	-223	0	2790	0	-8.49	0
78	SLU 13	-223	0	2790	0	-8.49	0
78	SLU 14	-223	0	2790	0	-8.49	0
78	SLU 15	-223	0	2790	0	-8.49	0
78	SLU 16	-223	0	2790	0	-8.49	0
78	SLU 17	-223	0	2790	0	-8.49	0
78	SLU 18	-265	0	3081	0	-10.09	0
78	SLU 19	-265	0	3081	0	-10.09	0
78	SLU 20	-265	0	3081	0	-10.09	0
78	SLU 21	-265	0	3081	0	-10.09	0
78	SLU 22	-178	0	2539	0	-6.73	0
78	SLU 23	-178	0	2539	0	-6.73	0
78	SLU 24	-178	0	2539	0	-6.73	0
78	SLU 25	-178	0	2539	0	-6.73	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
78	SLU 26	-178	0	2539	0	-6.73	0
78	SLU 27	-178	0	2539	0	-6.73	0
78	SLU 28	-178	0	2539	0	-6.73	0
78	SLU 29	-178	0	2539	0	-6.73	0
78	SLU 30	-178	0	2539	0	-6.73	0
78	SLU 31	-275	0	3219	0	-10.48	0
78	SLU 32	-275	0	3219	0	-10.48	0
78	SLU 33	-275	0	3219	0	-10.48	0
78	SLU 34	-275	0	3219	0	-10.48	0
78	SLU 35	-275	0	3219	0	-10.48	0
78	SLU 36	-275	0	3219	0	-10.48	0
78	SLU 37	-275	0	3219	0	-10.48	0
78	SLU 38	-275	0	3219	0	-10.48	0
78	SLU 39	-317	0	3511	0	-12.08	0
78	SLU 40	-317	0	3511	0	-12.08	0
78	SLU 41	-317	0	3511	0	-12.08	0
78	SLU 42	-317	0	3511	0	-12.08	0
78	SLU 43	-147	0	2596	0	-5.49	0
78	SLU 44	-147	0	2596	0	-5.49	0
78	SLU 45	-147	0	2596	0	-5.49	0
78	SLU 46	-147	0	2596	0	-5.49	0
78	SLU 47	-147	0	2596	0	-5.49	0
78	SLU 48	-147	0	2596	0	-5.49	0
78	SLU 49	-147	0	2596	0	-5.49	0
78	SLU 50	-147	0	2596	0	-5.49	0
78	SLU 51	-147	0	2596	0	-5.49	0
78	SLU 52	-243	0	3276	0	-9.23	0
78	SLU 53	-243	0	3276	0	-9.23	0
78	SLU 54	-243	0	3276	0	-9.23	0
78	SLU 55	-243	0	3276	0	-9.23	0
78	SLU 56	-243	0	3276	0	-9.23	0
78	SLU 57	-243	0	3276	0	-9.23	0
78	SLU 58	-243	0	3276	0	-9.23	0
78	SLU 59	-243	0	3276	0	-9.23	0
78	SLU 60	-285	0	3567	0	-10.83	0
78	SLU 61	-285	0	3567	0	-10.83	0
78	SLU 62	-285	0	3567	0	-10.83	0
78	SLU 63	-285	0	3567	0	-10.83	0
78	SLU 64	-199	0	3025	0	-7.47	0
78	SLU 65	-199	0	3025	0	-7.47	0
78	SLU 66	-199	0	3025	0	-7.47	0
78	SLU 67	-199	0	3025	0	-7.47	0
78	SLU 68	-199	0	3025	0	-7.47	0
78	SLU 69	-199	0	3025	0	-7.47	0
78	SLU 70	-199	0	3025	0	-7.47	0
78	SLU 71	-199	0	3025	0	-7.47	0
78	SLU 72	-199	0	3025	0	-7.47	0
78	SLU 73	-295	0	3705	0	-11.22	0
78	SLU 74	-295	0	3705	0	-11.22	0
78	SLU 75	-295	0	3705	0	-11.22	0
78	SLU 76	-295	0	3705	0	-11.22	0
78	SLU 77	-295	0	3705	0	-11.22	0
78	SLU 78	-295	0	3705	0	-11.22	0
78	SLU 79	-295	0	3705	0	-11.22	0
78	SLU 80	-295	0	3705	0	-11.22	0
78	SLU 81	-337	0	3996	0	-12.82	0
78	SLU 82	-337	0	3996	0	-12.82	0
78	SLU 83	-337	0	3996	0	-12.82	0
78	SLU 84	-337	0	3996	0	-12.82	0
78	SLE RA 1	-141	0	2233	0	-5.31	0
78	SLE RA 2	-141	0	2233	0	-5.31	0
78	SLE RA 3	-141	0	2233	0	-5.31	0
78	SLE RA 4	-141	0	2233	0	-5.31	0
78	SLE RA 5	-141	0	2233	0	-5.31	0
78	SLE RA 6	-141	0	2233	0	-5.31	0
78	SLE RA 7	-141	0	2233	0	-5.31	0
78	SLE RA 8	-141	0	2233	0	-5.31	0
78	SLE RA 9	-141	0	2233	0	-5.31	0
78	SLE RA 10	-206	0	2686	0	-7.81	0
78	SLE RA 11	-206	0	2686	0	-7.81	0
78	SLE RA 12	-206	0	2686	0	-7.81	0
78	SLE RA 13	-206	0	2686	0	-7.81	0
78	SLE RA 14	-206	0	2686	0	-7.81	0
78	SLE RA 15	-206	0	2686	0	-7.81	0
78	SLE RA 16	-206	0	2686	0	-7.81	0
78	SLE RA 17	-206	0	2686	0	-7.81	0
78	SLE RA 18	-233	0	2880	0	-8.88	0
78	SLE RA 19	-233	0	2880	0	-8.88	0
78	SLE RA 20	-233	0	2880	0	-8.88	0
78	SLE RA 21	-233	0	2880	0	-8.88	0
78	SLE FR 1	-141	0	2233	0	-5.31	0
78	SLE FR 2	-141	0	2233	0	-5.31	0
78	SLE FR 3	-141	0	2233	0	-5.31	0
78	SLE FR 4	-169	0	2427	0	-6.38	0
78	SLE FR 5	-169	0	2427	0	-6.38	0
78	SLE FR 6	-187	0	2556	0	-7.1	0
78	SLE QP 1	-141	0	2233	0	-5.31	0
78	SLE QP 2	-169	0	2427	0	-6.38	0
78	SLD 1	78	16	2526	-17.32	4.09	-0.1



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
78	SLD 2	78	16	2526	-17.32	4.09	-0.1
78	SLD 3	47	-26	2513	26.12	2.8	0.16
78	SLD 4	47	-26	2513	26.12	2.8	0.16
78	SLD 5	-49	68	2477	-71.09	-1.28	-0.41
78	SLD 6	-49	68	2477	-71.09	-1.28	-0.41
78	SLD 7	-150	-71	2433	73.73	-5.58	0.43
78	SLD 8	-150	-71	2433	73.73	-5.58	0.43
78	SLD 9	-188	71	2421	-73.72	-7.18	-0.43
78	SLD 10	-188	71	2421	-73.72	-7.18	-0.43
78	SLD 11	-289	-68	2377	71.09	-11.48	0.41
78	SLD 12	-289	-68	2377	71.09	-11.48	0.41
78	SLD 13	-385	26	2341	-26.12	-15.57	-0.16
78	SLD 14	-385	26	2341	-26.12	-15.57	-0.16
78	SLD 15	-416	-16	2327	17.33	-16.86	0.1
78	SLD 16	-416	-16	2327	17.33	-16.86	0.1
78	SLV 1	415	41	2663	-44.47	18.43	-0.25
78	SLV 2	415	41	2663	-44.47	18.43	-0.25
78	SLV 3	344	-66	2632	66.93	15.39	0.41
78	SLV 4	344	-66	2632	66.93	15.39	0.41
78	SLV 5	115	176	2545	-182.28	5.69	-1.06
78	SLV 6	115	176	2545	-182.28	5.69	-1.06
78	SLV 7	-124	-183	2441	189.03	-4.48	1.11
78	SLV 8	-124	-183	2441	189.03	-4.48	1.11
78	SLV 9	-214	183	2413	-189.02	-8.29	-1.11
78	SLV 10	-214	183	2413	-189.02	-8.29	-1.11
78	SLV 11	-453	-176	2308	182.29	-18.45	1.06
78	SLV 12	-453	-176	2308	182.29	-18.45	1.06
78	SLV 13	-682	66	2222	-66.92	-28.15	-0.41
78	SLV 14	-682	66	2222	-66.92	-28.15	-0.41
78	SLV 15	-753	-41	2191	44.47	-31.2	0.25
78	SLV 16	-753	-41	2191	44.47	-31.2	0.25
79	SLU 1	-210	0	2027	0	-8.26	0
79	SLU 2	-210	0	2027	0	-8.26	0
79	SLU 3	-210	0	2027	0	-8.26	0
79	SLU 4	-210	0	2027	0	-8.26	0
79	SLU 5	-210	0	2027	0	-8.26	0
79	SLU 6	-210	0	2027	0	-8.26	0
79	SLU 7	-210	0	2027	0	-8.26	0
79	SLU 8	-210	0	2027	0	-8.26	0
79	SLU 9	-210	0	2027	0	-8.26	0
79	SLU 10	-338	0	2662	0	-13.29	0
79	SLU 11	-338	0	2662	0	-13.29	0
79	SLU 12	-338	0	2662	0	-13.29	0
79	SLU 13	-338	0	2662	0	-13.29	0
79	SLU 14	-338	0	2662	0	-13.29	0
79	SLU 15	-338	0	2662	0	-13.29	0
79	SLU 16	-338	0	2662	0	-13.29	0
79	SLU 17	-338	0	2662	0	-13.29	0
79	SLU 18	-393	0	2934	0	-15.45	0
79	SLU 19	-393	0	2934	0	-15.45	0
79	SLU 20	-393	0	2934	0	-15.45	0
79	SLU 21	-393	0	2934	0	-15.45	0
79	SLU 22	-282	0	2426	0	-11.08	0
79	SLU 23	-282	0	2426	0	-11.08	0
79	SLU 24	-282	0	2426	0	-11.08	0
79	SLU 25	-282	0	2426	0	-11.08	0
79	SLU 26	-282	0	2426	0	-11.08	0
79	SLU 27	-282	0	2426	0	-11.08	0
79	SLU 28	-282	0	2426	0	-11.08	0
79	SLU 29	-282	0	2426	0	-11.08	0
79	SLU 30	-282	0	2426	0	-11.08	0
79	SLU 31	-410	0	3062	0	-16.12	0
79	SLU 32	-410	0	3062	0	-16.12	0
79	SLU 33	-410	0	3062	0	-16.12	0
79	SLU 34	-410	0	3062	0	-16.12	0
79	SLU 35	-410	0	3062	0	-16.12	0
79	SLU 36	-410	0	3062	0	-16.12	0
79	SLU 37	-410	0	3062	0	-16.12	0
79	SLU 38	-410	0	3062	0	-16.12	0
79	SLU 39	-465	0	3334	0	-18.27	0
79	SLU 40	-465	0	3334	0	-18.27	0
79	SLU 41	-465	0	3334	0	-18.27	0
79	SLU 42	-465	0	3334	0	-18.27	0
79	SLU 43	-248	0	2498	0	-9.76	0
79	SLU 44	-248	0	2498	0	-9.76	0
79	SLU 45	-248	0	2498	0	-9.76	0
79	SLU 46	-248	0	2498	0	-9.76	0
79	SLU 47	-248	0	2498	0	-9.76	0
79	SLU 48	-248	0	2498	0	-9.76	0
79	SLU 49	-248	0	2498	0	-9.76	0
79	SLU 50	-248	0	2498	0	-9.76	0
79	SLU 51	-248	0	2498	0	-9.76	0
79	SLU 52	-376	0	3133	0	-14.8	0
79	SLU 53	-376	0	3133	0	-14.8	0
79	SLU 54	-376	0	3133	0	-14.8	0
79	SLU 55	-376	0	3133	0	-14.8	0
79	SLU 56	-376	0	3133	0	-14.8	0
79	SLU 57	-376	0	3133	0	-14.8	0
79	SLU 58	-376	0	3133	0	-14.8	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
79	SLU 59	-376	0	3133	0	-14.8	0
79	SLU 60	-431	0	3405	0	-16.96	0
79	SLU 61	-431	0	3405	0	-16.96	0
79	SLU 62	-431	0	3405	0	-16.96	0
79	SLU 63	-431	0	3405	0	-16.96	0
79	SLU 64	-321	0	2897	0	-12.59	0
79	SLU 65	-321	0	2897	0	-12.59	0
79	SLU 66	-321	0	2897	0	-12.59	0
79	SLU 67	-321	0	2897	0	-12.59	0
79	SLU 68	-321	0	2897	0	-12.59	0
79	SLU 69	-321	0	2897	0	-12.59	0
79	SLU 70	-321	0	2897	0	-12.59	0
79	SLU 71	-321	0	2897	0	-12.59	0
79	SLU 72	-321	0	2897	0	-12.59	0
79	SLU 73	-449	0	3532	0	-17.62	0
79	SLU 74	-449	0	3532	0	-17.62	0
79	SLU 75	-449	0	3532	0	-17.62	0
79	SLU 76	-449	0	3532	0	-17.62	0
79	SLU 77	-449	0	3532	0	-17.62	0
79	SLU 78	-449	0	3532	0	-17.62	0
79	SLU 79	-449	0	3532	0	-17.62	0
79	SLU 80	-449	0	3532	0	-17.62	0
79	SLU 81	-503	0	3805	0	-19.78	0
79	SLU 82	-503	0	3805	0	-19.78	0
79	SLU 83	-503	0	3805	0	-19.78	0
79	SLU 84	-503	0	3805	0	-19.78	0
79	SLE RA 1	-231	0	2141	0	-9.06	0
79	SLE RA 2	-231	0	2141	0	-9.06	0
79	SLE RA 3	-231	0	2141	0	-9.06	0
79	SLE RA 4	-231	0	2141	0	-9.06	0
79	SLE RA 5	-231	0	2141	0	-9.06	0
79	SLE RA 6	-231	0	2141	0	-9.06	0
79	SLE RA 7	-231	0	2141	0	-9.06	0
79	SLE RA 8	-231	0	2141	0	-9.06	0
79	SLE RA 9	-231	0	2141	0	-9.06	0
79	SLE RA 10	-316	0	2564	0	-12.42	0
79	SLE RA 11	-316	0	2564	0	-12.42	0
79	SLE RA 12	-316	0	2564	0	-12.42	0
79	SLE RA 13	-316	0	2564	0	-12.42	0
79	SLE RA 14	-316	0	2564	0	-12.42	0
79	SLE RA 15	-316	0	2564	0	-12.42	0
79	SLE RA 16	-316	0	2564	0	-12.42	0
79	SLE RA 17	-316	0	2564	0	-12.42	0
79	SLE RA 18	-353	0	2746	0	-13.86	0
79	SLE RA 19	-353	0	2746	0	-13.86	0
79	SLE RA 20	-353	0	2746	0	-13.86	0
79	SLE RA 21	-353	0	2746	0	-13.86	0
79	SLE FR 1	-231	0	2141	0	-9.06	0
79	SLE FR 2	-231	0	2141	0	-9.06	0
79	SLE FR 3	-231	0	2141	0	-9.06	0
79	SLE FR 4	-267	0	2322	0	-10.5	0
79	SLE FR 5	-267	0	2322	0	-10.5	0
79	SLE FR 6	-292	0	2443	0	-11.46	0
79	SLE QP 1	-231	0	2141	0	-9.06	0
79	SLE QP 2	-267	0	2322	0	-10.5	0
79	SLD 1	-6	13	2369	-15.06	-1.03	-0.04
79	SLD 2	-6	13	2369	-15.06	-1.03	-0.04
79	SLD 3	-38	-22	2362	22.95	0.32	0.08
79	SLD 4	-38	-22	2362	22.95	0.32	0.08
79	SLD 5	-140	57	2346	-62.16	-9.71	-0.19
79	SLD 6	-140	57	2346	-62.16	-9.71	-0.19
79	SLD 7	-247	-60	2325	64.53	-5.21	0.21
79	SLD 8	-247	-60	2325	64.53	-5.21	0.21
79	SLD 9	-287	60	2320	-64.53	-15.8	-0.21
79	SLD 10	-287	60	2320	-64.53	-15.8	-0.21
79	SLD 11	-394	-57	2299	62.16	-11.29	0.19
79	SLD 12	-394	-57	2299	62.16	-11.29	0.19
79	SLD 13	-496	22	2282	-22.95	-21.32	-0.08
79	SLD 14	-496	22	2282	-22.95	-21.32	-0.08
79	SLD 15	-528	-13	2276	15.06	-19.97	0.04
79	SLD 16	-528	-13	2276	15.06	-19.97	0.04
79	SLV 1	350	34	2433	-38.65	11.9	-0.1
79	SLV 2	350	34	2433	-38.65	11.9	-0.1
79	SLV 3	274	-56	2418	58.79	15.09	0.21
79	SLV 4	274	-56	2418	58.79	15.09	0.21
79	SLV 5	33	146	2379	-159.39	-8.61	-0.5
79	SLV 6	33	146	2379	-159.39	-8.61	-0.5
79	SLV 7	-220	-153	2328	165.43	2	0.53
79	SLV 8	-220	-153	2328	165.43	2	0.53
79	SLV 9	-315	153	2317	-165.43	-23.01	-0.53
79	SLV 10	-315	153	2317	-165.43	-23.01	-0.53
79	SLV 11	-567	-146	2266	159.39	-12.39	0.5
79	SLV 12	-567	-146	2266	159.39	-12.39	0.5
79	SLV 13	-809	56	2227	-58.79	-36.09	-0.21
79	SLV 14	-809	56	2227	-58.79	-36.09	-0.21
79	SLV 15	-885	-34	2212	38.65	-32.91	0.1
79	SLV 16	-885	-34	2212	38.65	-32.91	0.1
80	SLU 1	-276	0	1926	0	-10.69	0
80	SLU 2	-276	0	1926	0	-10.69	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
80	SLU 3	-276	0	1926	0	-10.69	0
80	SLU 4	-276	0	1926	0	-10.69	0
80	SLU 5	-276	0	1926	0	-10.69	0
80	SLU 6	-276	0	1926	0	-10.69	0
80	SLU 7	-276	0	1926	0	-10.69	0
80	SLU 8	-276	0	1926	0	-10.69	0
80	SLU 9	-276	0	1926	0	-10.69	0
80	SLU 10	-427	0	2509	0	-16.57	0
80	SLU 11	-427	0	2509	0	-16.57	0
80	SLU 12	-427	0	2509	0	-16.57	0
80	SLU 13	-427	0	2509	0	-16.57	0
80	SLU 14	-427	0	2509	0	-16.57	0
80	SLU 15	-427	0	2509	0	-16.57	0
80	SLU 16	-427	0	2509	0	-16.57	0
80	SLU 17	-427	0	2509	0	-16.57	0
80	SLU 18	-492	0	2758	0	-19.09	0
80	SLU 19	-492	0	2758	0	-19.09	0
80	SLU 20	-492	0	2758	0	-19.09	0
80	SLU 21	-492	0	2758	0	-19.09	0
80	SLU 22	-364	0	2291	0	-14.11	0
80	SLU 23	-364	0	2291	0	-14.11	0
80	SLU 24	-364	0	2291	0	-14.11	0
80	SLU 25	-364	0	2291	0	-14.11	0
80	SLU 26	-364	0	2291	0	-14.11	0
80	SLU 27	-364	0	2291	0	-14.11	0
80	SLU 28	-364	0	2291	0	-14.11	0
80	SLU 29	-364	0	2291	0	-14.11	0
80	SLU 30	-364	0	2291	0	-14.11	0
80	SLU 31	-515	0	2873	0	-19.99	0
80	SLU 32	-515	0	2873	0	-19.99	0
80	SLU 33	-515	0	2873	0	-19.99	0
80	SLU 34	-515	0	2873	0	-19.99	0
80	SLU 35	-515	0	2873	0	-19.99	0
80	SLU 36	-515	0	2873	0	-19.99	0
80	SLU 37	-515	0	2873	0	-19.99	0
80	SLU 38	-515	0	2873	0	-19.99	0
80	SLU 39	-580	0	3123	0	-22.51	0
80	SLU 40	-580	0	3123	0	-22.51	0
80	SLU 41	-580	0	3123	0	-22.51	0
80	SLU 42	-580	0	3123	0	-22.51	0
80	SLU 43	-329	0	2379	0	-12.73	0
80	SLU 44	-329	0	2379	0	-12.73	0
80	SLU 45	-329	0	2379	0	-12.73	0
80	SLU 46	-329	0	2379	0	-12.73	0
80	SLU 47	-329	0	2379	0	-12.73	0
80	SLU 48	-329	0	2379	0	-12.73	0
80	SLU 49	-329	0	2379	0	-12.73	0
80	SLU 50	-329	0	2379	0	-12.73	0
80	SLU 51	-329	0	2379	0	-12.73	0
80	SLU 52	-480	0	2962	0	-18.61	0
80	SLU 53	-480	0	2962	0	-18.61	0
80	SLU 54	-480	0	2962	0	-18.61	0
80	SLU 55	-480	0	2962	0	-18.61	0
80	SLU 56	-480	0	2962	0	-18.61	0
80	SLU 57	-480	0	2962	0	-18.61	0
80	SLU 58	-480	0	2962	0	-18.61	0
80	SLU 59	-480	0	2962	0	-18.61	0
80	SLU 60	-544	0	3211	0	-21.13	0
80	SLU 61	-544	0	3211	0	-21.13	0
80	SLU 62	-544	0	3211	0	-21.13	0
80	SLU 63	-544	0	3211	0	-21.13	0
80	SLU 64	-417	0	2744	0	-16.15	0
80	SLU 65	-417	0	2744	0	-16.15	0
80	SLU 66	-417	0	2744	0	-16.15	0
80	SLU 67	-417	0	2744	0	-16.15	0
80	SLU 68	-417	0	2744	0	-16.15	0
80	SLU 69	-417	0	2744	0	-16.15	0
80	SLU 70	-417	0	2744	0	-16.15	0
80	SLU 71	-417	0	2744	0	-16.15	0
80	SLU 72	-417	0	2744	0	-16.15	0
80	SLU 73	-568	0	3326	0	-22.02	0
80	SLU 74	-568	0	3326	0	-22.02	0
80	SLU 75	-568	0	3326	0	-22.02	0
80	SLU 76	-568	0	3326	0	-22.02	0
80	SLU 77	-568	0	3326	0	-22.02	0
80	SLU 78	-568	0	3326	0	-22.02	0
80	SLU 79	-568	0	3326	0	-22.02	0
80	SLU 80	-568	0	3326	0	-22.02	0
80	SLU 81	-633	0	3576	0	-24.54	0
80	SLU 82	-633	0	3576	0	-24.54	0
80	SLU 83	-633	0	3576	0	-24.54	0
80	SLU 84	-633	0	3576	0	-24.54	0
80	SLE RA 1	-301	0	2031	0	-11.67	0
80	SLE RA 2	-301	0	2031	0	-11.67	0
80	SLE RA 3	-301	0	2031	0	-11.67	0
80	SLE RA 4	-301	0	2031	0	-11.67	0
80	SLE RA 5	-301	0	2031	0	-11.67	0
80	SLE RA 6	-301	0	2031	0	-11.67	0
80	SLE RA 7	-301	0	2031	0	-11.67	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
80	SLE RA 8	-301	0	2031	0	-11.67	0
80	SLE RA 9	-301	0	2031	0	-11.67	0
80	SLE RA 10	-402	0	2419	0	-15.59	0
80	SLE RA 11	-402	0	2419	0	-15.59	0
80	SLE RA 12	-402	0	2419	0	-15.59	0
80	SLE RA 13	-402	0	2419	0	-15.59	0
80	SLE RA 14	-402	0	2419	0	-15.59	0
80	SLE RA 15	-402	0	2419	0	-15.59	0
80	SLE RA 16	-402	0	2419	0	-15.59	0
80	SLE RA 17	-402	0	2419	0	-15.59	0
80	SLE RA 18	-445	0	2585	0	-17.27	0
80	SLE RA 19	-445	0	2585	0	-17.27	0
80	SLE RA 20	-445	0	2585	0	-17.27	0
80	SLE RA 21	-445	0	2585	0	-17.27	0
80	SLE FR 1	-301	0	2031	0	-11.67	0
80	SLE FR 2	-301	0	2031	0	-11.67	0
80	SLE FR 3	-301	0	2031	0	-11.67	0
80	SLE FR 4	-345	0	2197	0	-13.35	0
80	SLE FR 5	-345	0	2197	0	-13.35	0
80	SLE FR 6	-373	0	2308	0	-14.47	0
80	SLE QP 1	-301	0	2031	0	-11.67	0
80	SLE QP 2	-345	0	2197	0	-13.35	0
80	SLD 1	-72	16	2181	-11.56	-1.98	-0.01
80	SLD 2	-72	16	2181	-11.56	-1.98	-0.01
80	SLD 3	-106	-8	2178	18.03	-3.38	0.02
80	SLD 4	-106	-8	2178	18.03	-3.38	0.02
80	SLD 5	-212	41	2197	-48.35	-7.81	-0.04
80	SLD 6	-212	41	2197	-48.35	-7.81	-0.04
80	SLD 7	-324	-39	2187	50.29	-12.48	0.04
80	SLD 8	-324	-39	2187	50.29	-12.48	0.04
80	SLD 9	-365	39	2207	-50.29	-14.22	-0.04
80	SLD 10	-365	39	2207	-50.29	-14.22	-0.04
80	SLD 11	-477	-41	2197	48.34	-18.88	0.04
80	SLD 12	-477	-41	2197	48.34	-18.88	0.04
80	SLD 13	-583	8	2216	-18.03	-23.32	-0.02
80	SLD 14	-583	8	2216	-18.03	-23.32	-0.02
80	SLD 15	-617	-16	2213	11.56	-24.72	0.01
80	SLD 16	-617	-16	2213	11.56	-24.72	0.01
80	SLV 1	300	40	2157	-29.69	13.58	-0.02
80	SLV 2	300	40	2157	-29.69	13.58	-0.02
80	SLV 3	221	-22	2150	46.17	10.27	0.04
80	SLV 4	221	-22	2150	46.17	10.27	0.04
80	SLV 5	-31	106	2196	-123.95	-0.26	-0.09
80	SLV 6	-31	106	2196	-123.95	-0.26	-0.09
80	SLV 7	-294	-100	2172	128.89	-11.28	0.1
80	SLV 8	-294	-100	2172	128.89	-11.28	0.1
80	SLV 9	-395	100	2222	-128.9	-15.42	-0.1
80	SLV 10	-395	100	2222	-128.9	-15.42	-0.1
80	SLV 11	-658	-106	2198	123.95	-26.44	0.09
80	SLV 12	-658	-106	2198	123.95	-26.44	0.09
80	SLV 13	-910	22	2244	-46.17	-36.97	-0.04
80	SLV 14	-910	22	2244	-46.17	-36.97	-0.04
80	SLV 15	-989	-40	2236	29.68	-40.27	0.02
80	SLV 16	-989	-40	2236	29.68	-40.27	0.02
81	SLU 1	-341	0	1814	0	-13.48	0
81	SLU 2	-341	0	1814	0	-13.48	0
81	SLU 3	-341	0	1814	0	-13.48	0
81	SLU 4	-341	0	1814	0	-13.48	0
81	SLU 5	-341	0	1814	0	-13.48	0
81	SLU 6	-341	0	1814	0	-13.48	0
81	SLU 7	-341	0	1814	0	-13.48	0
81	SLU 8	-341	0	1814	0	-13.48	0
81	SLU 9	-341	0	1814	0	-13.48	0
81	SLU 10	-512	0	2339	0	-20.21	0
81	SLU 11	-512	0	2339	0	-20.21	0
81	SLU 12	-512	0	2339	0	-20.21	0
81	SLU 13	-512	0	2339	0	-20.21	0
81	SLU 14	-512	0	2339	0	-20.21	0
81	SLU 15	-512	0	2339	0	-20.21	0
81	SLU 16	-512	0	2339	0	-20.21	0
81	SLU 17	-512	0	2339	0	-20.21	0
81	SLU 18	-586	0	2563	0	-23.09	0
81	SLU 19	-586	0	2563	0	-23.09	0
81	SLU 20	-586	0	2563	0	-23.09	0
81	SLU 21	-586	0	2563	0	-23.09	0
81	SLU 22	-444	0	2139	0	-17.49	0
81	SLU 23	-444	0	2139	0	-17.49	0
81	SLU 24	-444	0	2139	0	-17.49	0
81	SLU 25	-444	0	2139	0	-17.49	0
81	SLU 26	-444	0	2139	0	-17.49	0
81	SLU 27	-444	0	2139	0	-17.49	0
81	SLU 28	-444	0	2139	0	-17.49	0
81	SLU 29	-444	0	2139	0	-17.49	0
81	SLU 30	-444	0	2139	0	-17.49	0
81	SLU 31	-615	0	2664	0	-24.21	0
81	SLU 32	-615	0	2664	0	-24.21	0
81	SLU 33	-615	0	2664	0	-24.21	0
81	SLU 34	-615	0	2664	0	-24.21	0
81	SLU 35	-615	0	2664	0	-24.21	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
81	SLU 36	-615	0	2664	0	-24.21	0
81	SLU 37	-615	0	2664	0	-24.21	0
81	SLU 38	-615	0	2664	0	-24.21	0
81	SLU 39	-688	0	2888	0	-27.1	0
81	SLU 40	-688	0	2888	0	-27.1	0
81	SLU 41	-688	0	2888	0	-27.1	0
81	SLU 42	-688	0	2888	0	-27.1	0
81	SLU 43	-409	0	2247	0	-16.16	0
81	SLU 44	-409	0	2247	0	-16.16	0
81	SLU 45	-409	0	2247	0	-16.16	0
81	SLU 46	-409	0	2247	0	-16.16	0
81	SLU 47	-409	0	2247	0	-16.16	0
81	SLU 48	-409	0	2247	0	-16.16	0
81	SLU 49	-409	0	2247	0	-16.16	0
81	SLU 50	-409	0	2247	0	-16.16	0
81	SLU 51	-409	0	2247	0	-16.16	0
81	SLU 52	-580	0	2772	0	-22.88	0
81	SLU 53	-580	0	2772	0	-22.88	0
81	SLU 54	-580	0	2772	0	-22.88	0
81	SLU 55	-580	0	2772	0	-22.88	0
81	SLU 56	-580	0	2772	0	-22.88	0
81	SLU 57	-580	0	2772	0	-22.88	0
81	SLU 58	-580	0	2772	0	-22.88	0
81	SLU 59	-580	0	2772	0	-22.88	0
81	SLU 60	-653	0	2996	0	-25.76	0
81	SLU 61	-653	0	2996	0	-25.76	0
81	SLU 62	-653	0	2996	0	-25.76	0
81	SLU 63	-653	0	2996	0	-25.76	0
81	SLU 64	-511	0	2572	0	-20.16	0
81	SLU 65	-511	0	2572	0	-20.16	0
81	SLU 66	-511	0	2572	0	-20.16	0
81	SLU 67	-511	0	2572	0	-20.16	0
81	SLU 68	-511	0	2572	0	-20.16	0
81	SLU 69	-511	0	2572	0	-20.16	0
81	SLU 70	-511	0	2572	0	-20.16	0
81	SLU 71	-511	0	2572	0	-20.16	0
81	SLU 72	-511	0	2572	0	-20.16	0
81	SLU 73	-682	0	3097	0	-26.89	0
81	SLU 74	-682	0	3097	0	-26.89	0
81	SLU 75	-682	0	3097	0	-26.89	0
81	SLU 76	-682	0	3097	0	-26.89	0
81	SLU 77	-682	0	3097	0	-26.89	0
81	SLU 78	-682	0	3097	0	-26.89	0
81	SLU 79	-682	0	3097	0	-26.89	0
81	SLU 80	-682	0	3097	0	-26.89	0
81	SLU 81	-755	0	3321	0	-29.77	0
81	SLU 82	-755	0	3321	0	-29.77	0
81	SLU 83	-755	0	3321	0	-29.77	0
81	SLU 84	-755	0	3321	0	-29.77	0
81	SLE RA 1	-371	0	1907	0	-14.63	0
81	SLE RA 2	-371	0	1907	0	-14.63	0
81	SLE RA 3	-371	0	1907	0	-14.63	0
81	SLE RA 4	-371	0	1907	0	-14.63	0
81	SLE RA 5	-371	0	1907	0	-14.63	0
81	SLE RA 6	-371	0	1907	0	-14.63	0
81	SLE RA 7	-371	0	1907	0	-14.63	0
81	SLE RA 8	-371	0	1907	0	-14.63	0
81	SLE RA 9	-371	0	1907	0	-14.63	0
81	SLE RA 10	-485	0	2257	0	-19.11	0
81	SLE RA 11	-485	0	2257	0	-19.11	0
81	SLE RA 12	-485	0	2257	0	-19.11	0
81	SLE RA 13	-485	0	2257	0	-19.11	0
81	SLE RA 14	-485	0	2257	0	-19.11	0
81	SLE RA 15	-485	0	2257	0	-19.11	0
81	SLE RA 16	-485	0	2257	0	-19.11	0
81	SLE RA 17	-485	0	2257	0	-19.11	0
81	SLE RA 18	-533	0	2407	0	-21.03	0
81	SLE RA 19	-533	0	2407	0	-21.03	0
81	SLE RA 20	-533	0	2407	0	-21.03	0
81	SLE RA 21	-533	0	2407	0	-21.03	0
81	SLE FR 1	-371	0	1907	0	-14.63	0
81	SLE FR 2	-371	0	1907	0	-14.63	0
81	SLE FR 3	-371	0	1907	0	-14.63	0
81	SLE FR 4	-420	0	2057	0	-16.55	0
81	SLE FR 5	-420	0	2057	0	-16.55	0
81	SLE FR 6	-452	0	2157	0	-17.83	0
81	SLE QP 1	-371	0	1907	0	-14.63	0
81	SLE QP 2	-420	0	2057	0	-16.55	0
81	SLD 1	-146	8	2031	-12.03	-5.33	0
81	SLD 2	-146	8	2031	-12.03	-5.33	0
81	SLD 3	-180	-2	2026	7.36	-6.71	0.01
81	SLD 4	-180	-2	2026	7.36	-6.71	0.01
81	SLD 5	-287	18	2056	-33.02	-11.09	-0.01
81	SLD 6	-287	18	2056	-33.02	-11.09	-0.01
81	SLD 7	-398	-16	2041	31.62	-15.69	0.02
81	SLD 8	-398	-16	2041	31.62	-15.69	0.02
81	SLD 9	-441	16	2073	-31.62	-17.41	-0.02
81	SLD 10	-441	16	2073	-31.62	-17.41	-0.02
81	SLD 11	-552	-18	2058	33.02	-22.01	0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
81	SLD 12	-552	-18	2058	33.02	-22.01	0.01
81	SLD 13	-659	2	2088	-7.37	-26.39	-0.01
81	SLD 14	-659	2	2088	-7.37	-26.39	-0.01
81	SLD 15	-693	-8	2083	12.03	-27.77	0
81	SLD 16	-693	-8	2083	12.03	-27.77	0
81	SLV 1	226	19	1994	-30.78	9.99	0
81	SLV 2	226	19	1994	-30.78	9.99	0
81	SLV 3	148	-6	1983	18.92	6.73	0.02
81	SLV 4	148	-6	1983	18.92	6.73	0.02
81	SLV 5	-106	45	2054	-84.61	-3.65	-0.03
81	SLV 6	-106	45	2054	-84.61	-3.65	-0.03
81	SLV 7	-369	-41	2019	81.05	-14.5	0.04
81	SLV 8	-369	-41	2019	81.05	-14.5	0.04
81	SLV 9	-470	41	2096	-81.05	-18.6	-0.04
81	SLV 10	-470	41	2096	-81.05	-18.6	-0.04
81	SLV 11	-733	-45	2060	84.61	-29.45	0.03
81	SLV 12	-733	-45	2060	84.61	-29.45	0.03
81	SLV 13	-987	6	2131	-18.92	-39.83	-0.02
81	SLV 14	-987	6	2131	-18.92	-39.83	-0.02
81	SLV 15	-1065	-19	2121	30.78	-43.09	0
81	SLV 16	-1065	-19	2121	30.78	-43.09	0
82	SLU 1	-409	0	1694	0	-15.85	0
82	SLU 2	-409	0	1694	0	-15.85	0
82	SLU 3	-409	0	1694	0	-15.85	0
82	SLU 4	-409	0	1694	0	-15.85	0
82	SLU 5	-409	0	1694	0	-15.85	0
82	SLU 6	-409	0	1694	0	-15.85	0
82	SLU 7	-409	0	1694	0	-15.85	0
82	SLU 8	-409	0	1694	0	-15.85	0
82	SLU 9	-409	0	1694	0	-15.85	0
82	SLU 10	-598	0	2158	0	-23.21	0
82	SLU 11	-598	0	2158	0	-23.21	0
82	SLU 12	-598	0	2158	0	-23.21	0
82	SLU 13	-598	0	2158	0	-23.21	0
82	SLU 14	-598	0	2158	0	-23.21	0
82	SLU 15	-598	0	2158	0	-23.21	0
82	SLU 16	-598	0	2158	0	-23.21	0
82	SLU 17	-598	0	2158	0	-23.21	0
82	SLU 18	-679	0	2357	0	-26.36	0
82	SLU 19	-679	0	2357	0	-26.36	0
82	SLU 20	-679	0	2357	0	-26.36	0
82	SLU 21	-679	0	2357	0	-26.36	0
82	SLU 22	-524	0	1976	0	-20.3	0
82	SLU 23	-524	0	1976	0	-20.3	0
82	SLU 24	-524	0	1976	0	-20.3	0
82	SLU 25	-524	0	1976	0	-20.3	0
82	SLU 26	-524	0	1976	0	-20.3	0
82	SLU 27	-524	0	1976	0	-20.3	0
82	SLU 28	-524	0	1976	0	-20.3	0
82	SLU 29	-524	0	1976	0	-20.3	0
82	SLU 30	-524	0	1976	0	-20.3	0
82	SLU 31	-713	0	2441	0	-27.66	0
82	SLU 32	-713	0	2441	0	-27.66	0
82	SLU 33	-713	0	2441	0	-27.66	0
82	SLU 34	-713	0	2441	0	-27.66	0
82	SLU 35	-713	0	2441	0	-27.66	0
82	SLU 36	-713	0	2441	0	-27.66	0
82	SLU 37	-713	0	2441	0	-27.66	0
82	SLU 38	-713	0	2441	0	-27.66	0
82	SLU 39	-794	0	2640	0	-30.82	0
82	SLU 40	-794	0	2640	0	-30.82	0
82	SLU 41	-794	0	2640	0	-30.82	0
82	SLU 42	-794	0	2640	0	-30.82	0
82	SLU 43	-492	0	2105	0	-19.08	0
82	SLU 44	-492	0	2105	0	-19.08	0
82	SLU 45	-492	0	2105	0	-19.08	0
82	SLU 46	-492	0	2105	0	-19.08	0
82	SLU 47	-492	0	2105	0	-19.08	0
82	SLU 48	-492	0	2105	0	-19.08	0
82	SLU 49	-492	0	2105	0	-19.08	0
82	SLU 50	-492	0	2105	0	-19.08	0
82	SLU 51	-492	0	2105	0	-19.08	0
82	SLU 52	-681	0	2569	0	-26.43	0
82	SLU 53	-681	0	2569	0	-26.43	0
82	SLU 54	-681	0	2569	0	-26.43	0
82	SLU 55	-681	0	2569	0	-26.43	0
82	SLU 56	-681	0	2569	0	-26.43	0
82	SLU 57	-681	0	2569	0	-26.43	0
82	SLU 58	-681	0	2569	0	-26.43	0
82	SLU 59	-681	0	2569	0	-26.43	0
82	SLU 60	-762	0	2768	0	-29.59	0
82	SLU 61	-762	0	2768	0	-29.59	0
82	SLU 62	-762	0	2768	0	-29.59	0
82	SLU 63	-762	0	2768	0	-29.59	0
82	SLU 64	-607	0	2387	0	-23.53	0
82	SLU 65	-607	0	2387	0	-23.53	0
82	SLU 66	-607	0	2387	0	-23.53	0
82	SLU 67	-607	0	2387	0	-23.53	0
82	SLU 68	-607	0	2387	0	-23.53	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
82	SLU 69	-607	0	2387	0	-23.53	0
82	SLU 70	-607	0	2387	0	-23.53	0
82	SLU 71	-607	0	2387	0	-23.53	0
82	SLU 72	-607	0	2387	0	-23.53	0
82	SLU 73	-796	0	2852	0	-30.89	0
82	SLU 74	-796	0	2852	0	-30.89	0
82	SLU 75	-796	0	2852	0	-30.89	0
82	SLU 76	-796	0	2852	0	-30.89	0
82	SLU 77	-796	0	2852	0	-30.89	0
82	SLU 78	-796	0	2852	0	-30.89	0
82	SLU 79	-796	0	2852	0	-30.89	0
82	SLU 80	-796	0	2852	0	-30.89	0
82	SLU 81	-877	0	3051	-0.01	-34.04	0
82	SLU 82	-877	0	3051	-0.01	-34.04	0
82	SLU 83	-877	0	3051	-0.01	-34.04	0
82	SLU 84	-877	0	3051	-0.01	-34.04	0
82	SLE RA 1	-442	0	1774	0	-17.12	0
82	SLE RA 2	-442	0	1774	0	-17.12	0
82	SLE RA 3	-442	0	1774	0	-17.12	0
82	SLE RA 4	-442	0	1774	0	-17.12	0
82	SLE RA 5	-442	0	1774	0	-17.12	0
82	SLE RA 6	-442	0	1774	0	-17.12	0
82	SLE RA 7	-442	0	1774	0	-17.12	0
82	SLE RA 8	-442	0	1774	0	-17.12	0
82	SLE RA 9	-442	0	1774	0	-17.12	0
82	SLE RA 10	-568	0	2084	0	-22.03	0
82	SLE RA 11	-568	0	2084	0	-22.03	0
82	SLE RA 12	-568	0	2084	0	-22.03	0
82	SLE RA 13	-568	0	2084	0	-22.03	0
82	SLE RA 14	-568	0	2084	0	-22.03	0
82	SLE RA 15	-568	0	2084	0	-22.03	0
82	SLE RA 16	-568	0	2084	0	-22.03	0
82	SLE RA 17	-568	0	2084	0	-22.03	0
82	SLE RA 18	-622	0	2217	0	-24.13	0
82	SLE RA 19	-622	0	2217	0	-24.13	0
82	SLE RA 20	-622	0	2217	0	-24.13	0
82	SLE RA 21	-622	0	2217	0	-24.13	0
82	SLE FR 1	-442	0	1774	0	-17.12	0
82	SLE FR 2	-442	0	1774	0	-17.12	0
82	SLE FR 3	-442	0	1774	0	-17.12	0
82	SLE FR 4	-496	0	1907	0	-19.22	0
82	SLE FR 5	-496	0	1907	0	-19.22	0
82	SLE FR 6	-532	0	1996	0	-20.63	0
82	SLE QP 1	-442	0	1774	0	-17.12	0
82	SLE QP 2	-496	0	1907	0	-19.22	0
82	SLD 1	-223	-1	1850	-6.26	-7.86	-0.01
82	SLD 2	-223	-1	1850	-6.26	-7.86	-0.01
82	SLD 3	-256	6	1842	3.38	-9.24	0.03
82	SLD 4	-256	6	1842	3.38	-9.24	0.03
82	SLD 5	-363	-11	1903	-16.51	-13.73	-0.06
82	SLD 6	-363	-11	1903	-16.51	-13.73	-0.06
82	SLD 7	-475	13	1874	15.64	-18.32	0.07
82	SLD 8	-475	13	1874	15.64	-18.32	0.07
82	SLD 9	-517	-13	1940	-15.64	-20.13	-0.07
82	SLD 10	-517	-13	1940	-15.64	-20.13	-0.07
82	SLD 11	-628	11	1911	16.5	-24.72	0.06
82	SLD 12	-628	11	1911	16.5	-24.72	0.06
82	SLD 13	-735	-6	1972	-3.38	-29.21	-0.03
82	SLD 14	-735	-6	1972	-3.38	-29.21	-0.03
82	SLD 15	-768	1	1964	6.26	-30.59	0.01
82	SLD 16	-768	1	1964	6.26	-30.59	0.01
82	SLV 1	150	-4	1772	-16	7.67	-0.02
82	SLV 2	150	-4	1772	-16	7.67	-0.02
82	SLV 3	71	15	1751	8.69	4.42	0.08
82	SLV 4	71	15	1751	8.69	4.42	0.08
82	SLV 5	-182	-29	1898	-42.26	-6.23	-0.16
82	SLV 6	-182	-29	1898	-42.26	-6.23	-0.16
82	SLV 7	-446	33	1829	40.07	-17.06	0.17
82	SLV 8	-446	33	1829	40.07	-17.06	0.17
82	SLV 9	-546	-33	1985	-40.07	-21.39	-0.17
82	SLV 10	-546	-33	1985	-40.07	-21.39	-0.17
82	SLV 11	-809	29	1916	42.26	-32.22	0.16
82	SLV 12	-809	29	1916	42.26	-32.22	0.16
82	SLV 13	-1062	-15	2063	-8.7	-42.87	-0.08
82	SLV 14	-1062	-15	2063	-8.7	-42.87	-0.08
82	SLV 15	-1141	4	2042	16	-46.12	0.02
82	SLV 16	-1141	4	2042	16	-46.12	0.02
83	SLU 1	-494	0	1596	0	-20.18	0
83	SLU 2	-494	0	1596	0	-20.18	0
83	SLU 3	-494	0	1596	0	-20.18	0
83	SLU 4	-494	0	1596	0	-20.18	0
83	SLU 5	-494	0	1596	0	-20.18	0
83	SLU 6	-494	0	1596	0	-20.18	0
83	SLU 7	-494	0	1596	0	-20.18	0
83	SLU 8	-494	0	1596	0	-20.18	0
83	SLU 9	-494	0	1596	0	-20.18	0
83	SLU 10	-703	0	2012	-0.01	-28.63	0
83	SLU 11	-703	0	2012	-0.01	-28.63	0
83	SLU 12	-703	0	2012	-0.01	-28.63	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
83	SLU 13	-703	0	2012	-0.01	-28.63	0
83	SLU 14	-703	0	2012	-0.01	-28.63	0
83	SLU 15	-703	0	2012	-0.01	-28.63	0
83	SLU 16	-703	0	2012	-0.01	-28.63	0
83	SLU 17	-703	0	2012	-0.01	-28.63	0
83	SLU 18	-793	0	2191	-0.01	-32.25	0
83	SLU 19	-793	0	2191	-0.01	-32.25	0
83	SLU 20	-793	0	2191	-0.01	-32.25	0
83	SLU 21	-793	0	2191	-0.01	-32.25	0
83	SLU 22	-622	0	1841	-0.01	-25.31	0
83	SLU 23	-622	0	1841	-0.01	-25.31	0
83	SLU 24	-622	0	1841	-0.01	-25.31	0
83	SLU 25	-622	0	1841	-0.01	-25.31	0
83	SLU 26	-622	0	1841	-0.01	-25.31	0
83	SLU 27	-622	0	1841	-0.01	-25.31	0
83	SLU 28	-622	0	1841	-0.01	-25.31	0
83	SLU 29	-622	0	1841	-0.01	-25.31	0
83	SLU 30	-622	0	1841	-0.01	-25.31	0
83	SLU 31	-831	0	2257	-0.01	-33.76	0
83	SLU 32	-831	0	2257	-0.01	-33.76	0
83	SLU 33	-831	0	2257	-0.01	-33.76	0
83	SLU 34	-831	0	2257	-0.01	-33.76	0
83	SLU 35	-831	0	2257	-0.01	-33.76	0
83	SLU 36	-831	0	2257	-0.01	-33.76	0
83	SLU 37	-831	0	2257	-0.01	-33.76	0
83	SLU 38	-831	0	2257	-0.01	-33.76	0
83	SLU 39	-921	0	2436	-0.01	-37.38	0
83	SLU 40	-921	0	2436	-0.01	-37.38	0
83	SLU 41	-921	0	2436	-0.01	-37.38	0
83	SLU 42	-921	0	2436	-0.01	-37.38	0
83	SLU 43	-599	0	1991	-0.01	-24.48	0
83	SLU 44	-599	0	1991	-0.01	-24.48	0
83	SLU 45	-599	0	1991	-0.01	-24.48	0
83	SLU 46	-599	0	1991	-0.01	-24.48	0
83	SLU 47	-599	0	1991	-0.01	-24.48	0
83	SLU 48	-599	0	1991	-0.01	-24.48	0
83	SLU 49	-599	0	1991	-0.01	-24.48	0
83	SLU 50	-599	0	1991	-0.01	-24.48	0
83	SLU 51	-599	0	1991	-0.01	-24.48	0
83	SLU 52	-808	0	2407	-0.01	-32.93	0
83	SLU 53	-808	0	2407	-0.01	-32.93	0
83	SLU 54	-808	0	2407	-0.01	-32.93	0
83	SLU 55	-808	0	2407	-0.01	-32.93	0
83	SLU 56	-808	0	2407	-0.01	-32.93	0
83	SLU 57	-808	0	2407	-0.01	-32.93	0
83	SLU 58	-808	0	2407	-0.01	-32.93	0
83	SLU 59	-808	0	2407	-0.01	-32.93	0
83	SLU 60	-897	0	2585	-0.01	-36.55	0
83	SLU 61	-897	0	2585	-0.01	-36.55	0
83	SLU 62	-897	0	2585	-0.01	-36.55	0
83	SLU 63	-897	0	2585	-0.01	-36.55	0
83	SLU 64	-727	0	2236	-0.01	-29.61	0
83	SLU 65	-727	0	2236	-0.01	-29.61	0
83	SLU 66	-727	0	2236	-0.01	-29.61	0
83	SLU 67	-727	0	2236	-0.01	-29.61	0
83	SLU 68	-727	0	2236	-0.01	-29.61	0
83	SLU 69	-727	0	2236	-0.01	-29.61	0
83	SLU 70	-727	0	2236	-0.01	-29.61	0
83	SLU 71	-727	0	2236	-0.01	-29.61	0
83	SLU 72	-727	0	2236	-0.01	-29.61	0
83	SLU 73	-936	0	2652	-0.01	-38.06	0
83	SLU 74	-936	0	2652	-0.01	-38.06	0
83	SLU 75	-936	0	2652	-0.01	-38.06	0
83	SLU 76	-936	0	2652	-0.01	-38.06	0
83	SLU 77	-936	0	2652	-0.01	-38.06	0
83	SLU 78	-936	0	2652	-0.01	-38.06	0
83	SLU 79	-936	0	2652	-0.01	-38.06	0
83	SLU 80	-936	0	2652	-0.01	-38.06	0
83	SLU 81	-1025	0	2830	-0.01	-41.68	0
83	SLU 82	-1025	0	2830	-0.01	-41.68	0
83	SLU 83	-1025	0	2830	-0.01	-41.68	0
83	SLU 84	-1025	0	2830	-0.01	-41.68	0
83	SLE RA 1	-531	0	1666	0	-21.65	0
83	SLE RA 2	-531	0	1666	0	-21.65	0
83	SLE RA 3	-531	0	1666	0	-21.65	0
83	SLE RA 4	-531	0	1666	0	-21.65	0
83	SLE RA 5	-531	0	1666	0	-21.65	0
83	SLE RA 6	-531	0	1666	0	-21.65	0
83	SLE RA 7	-531	0	1666	0	-21.65	0
83	SLE RA 8	-531	0	1666	0	-21.65	0
83	SLE RA 9	-531	0	1666	0	-21.65	0
83	SLE RA 10	-670	0	1943	-0.01	-27.28	0
83	SLE RA 11	-670	0	1943	-0.01	-27.28	0
83	SLE RA 12	-670	0	1943	-0.01	-27.28	0
83	SLE RA 13	-670	0	1943	-0.01	-27.28	0
83	SLE RA 14	-670	0	1943	-0.01	-27.28	0
83	SLE RA 15	-670	0	1943	-0.01	-27.28	0
83	SLE RA 16	-670	0	1943	-0.01	-27.28	0
83	SLE RA 17	-670	0	1943	-0.01	-27.28	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
83	SLE RA 18	-730	0	2062	-0.01	-29.69	0
83	SLE RA 19	-730	0	2062	-0.01	-29.69	0
83	SLE RA 20	-730	0	2062	-0.01	-29.69	0
83	SLE RA 21	-730	0	2062	-0.01	-29.69	0
83	SLE FR 1	-531	0	1666	0	-21.65	0
83	SLE FR 2	-531	0	1666	0	-21.65	0
83	SLE FR 3	-531	0	1666	0	-21.65	0
83	SLE FR 4	-591	0	1785	-0.01	-24.06	0
83	SLE FR 5	-591	0	1785	-0.01	-24.06	0
83	SLE FR 6	-630	0	1864	-0.01	-25.67	0
83	SLE QP 1	-531	0	1666	0	-21.65	0
83	SLE QP 2	-591	0	1785	-0.01	-24.06	0
83	SLD 1	-328	-3	1671	-2.18	-12.96	0
83	SLD 2	-328	-3	1671	-2.18	-12.96	0
83	SLD 3	-360	7	1654	0.75	-14.32	0.01
83	SLD 4	-360	7	1654	0.75	-14.32	0.01
83	SLD 5	-463	-18	1776	-5.11	-18.68	-0.01
83	SLD 6	-463	-18	1776	-5.11	-18.68	-0.01
83	SLD 7	-570	19	1721	4.68	-23.19	0.01
83	SLD 8	-570	19	1721	4.68	-23.19	0.01
83	SLD 9	-611	-19	1849	-4.69	-24.93	-0.01
83	SLD 10	-611	-19	1849	-4.69	-24.93	-0.01
83	SLD 11	-718	18	1794	5.1	-29.44	0.01
83	SLD 12	-718	18	1794	5.1	-29.44	0.01
83	SLD 13	-821	-7	1916	-0.76	-33.81	-0.01
83	SLD 14	-821	-7	1916	-0.76	-33.81	-0.01
83	SLD 15	-853	3	1899	2.17	-35.16	0
83	SLD 16	-853	3	1899	2.17	-35.16	0
83	SLV 1	29	-9	1513	-5.55	2.17	0
83	SLV 2	29	-9	1513	-5.55	2.17	0
83	SLV 3	-46	19	1474	1.96	-1.03	0.02
83	SLV 4	-46	19	1474	1.96	-1.03	0.02
83	SLV 5	-290	-45	1763	-13.07	-11.35	-0.03
83	SLV 6	-290	-45	1763	-13.07	-11.35	-0.03
83	SLV 7	-542	48	1632	11.98	-21.99	0.04
83	SLV 8	-542	48	1632	11.98	-21.99	0.04
83	SLV 9	-639	-48	1938	-11.99	-26.13	-0.04
83	SLV 10	-639	-48	1938	-11.99	-26.13	-0.04
83	SLV 11	-892	45	1807	13.06	-36.77	0.03
83	SLV 12	-892	45	1807	13.06	-36.77	0.03
83	SLV 13	-1135	-19	2096	-1.97	-47.1	-0.02
83	SLV 14	-1135	-19	2096	-1.97	-47.1	-0.02
83	SLV 15	-1211	9	2056	5.54	-50.29	0
83	SLV 16	-1211	9	2056	5.54	-50.29	0
84	SLU 1	-402	9	3361	-0.13	-14.03	0
84	SLU 2	-402	9	3361	-0.13	-14.03	0
84	SLU 3	-402	9	3361	-0.13	-14.03	0
84	SLU 4	-402	9	3361	-0.13	-14.03	0
84	SLU 5	-402	9	3361	-0.13	-14.03	0
84	SLU 6	-402	9	3361	-0.13	-14.03	0
84	SLU 7	-402	9	3361	-0.13	-14.03	0
84	SLU 8	-402	9	3361	-0.13	-14.03	0
84	SLU 9	-402	9	3361	-0.13	-14.03	0
84	SLU 10	-546	12	4206	-0.19	-19.48	0
84	SLU 11	-546	12	4206	-0.19	-19.48	0
84	SLU 12	-546	12	4206	-0.19	-19.48	0
84	SLU 13	-546	12	4206	-0.19	-19.48	0
84	SLU 14	-546	12	4206	-0.19	-19.48	0
84	SLU 15	-546	12	4206	-0.19	-19.48	0
84	SLU 16	-546	12	4206	-0.19	-19.48	0
84	SLU 17	-546	12	4206	-0.19	-19.48	0
84	SLU 18	-608	13	4568	-0.21	-21.82	0
84	SLU 19	-608	13	4568	-0.21	-21.82	0
84	SLU 20	-608	13	4568	-0.21	-21.82	0
84	SLU 21	-608	13	4568	-0.21	-21.82	0
84	SLU 22	-489	10	3836	-0.15	-17.32	0
84	SLU 23	-489	10	3836	-0.15	-17.32	0
84	SLU 24	-489	10	3836	-0.15	-17.32	0
84	SLU 25	-489	10	3836	-0.15	-17.32	0
84	SLU 26	-489	10	3836	-0.15	-17.32	0
84	SLU 27	-489	10	3836	-0.15	-17.32	0
84	SLU 28	-489	10	3836	-0.15	-17.32	0
84	SLU 29	-489	10	3836	-0.15	-17.32	0
84	SLU 30	-489	10	3836	-0.15	-17.32	0
84	SLU 31	-633	13	4681	-0.2	-22.77	0
84	SLU 32	-633	13	4681	-0.2	-22.77	0
84	SLU 33	-633	13	4681	-0.2	-22.77	0
84	SLU 34	-633	13	4681	-0.2	-22.77	0
84	SLU 35	-633	13	4681	-0.2	-22.77	0
84	SLU 36	-633	13	4681	-0.2	-22.77	0
84	SLU 37	-633	13	4681	-0.2	-22.77	0
84	SLU 38	-633	13	4681	-0.2	-22.77	0
84	SLU 39	-695	14	5043	-0.22	-25.11	0
84	SLU 40	-695	14	5043	-0.22	-25.11	0
84	SLU 41	-695	14	5043	-0.22	-25.11	0
84	SLU 42	-695	14	5043	-0.22	-25.11	0
84	SLU 43	-493	11	4207	-0.17	-17.11	0
84	SLU 44	-493	11	4207	-0.17	-17.11	0
84	SLU 45	-493	11	4207	-0.17	-17.11	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
84	SLU 46	-493	11	4207	-0.17	-17.11	0
84	SLU 47	-493	11	4207	-0.17	-17.11	0
84	SLU 48	-493	11	4207	-0.17	-17.11	0
84	SLU 49	-493	11	4207	-0.17	-17.11	0
84	SLU 50	-493	11	4207	-0.17	-17.11	0
84	SLU 51	-493	11	4207	-0.17	-17.11	0
84	SLU 52	-637	14	5051	-0.22	-22.56	0
84	SLU 53	-637	14	5051	-0.22	-22.56	0
84	SLU 54	-637	14	5051	-0.22	-22.56	0
84	SLU 55	-637	14	5051	-0.22	-22.56	0
84	SLU 56	-637	14	5051	-0.22	-22.56	0
84	SLU 57	-637	14	5051	-0.22	-22.56	0
84	SLU 58	-637	14	5051	-0.22	-22.56	0
84	SLU 59	-637	14	5051	-0.22	-22.56	0
84	SLU 60	-699	16	5414	-0.25	-24.9	0
84	SLU 61	-699	16	5414	-0.25	-24.9	0
84	SLU 62	-699	16	5414	-0.25	-24.9	0
84	SLU 63	-699	16	5414	-0.25	-24.9	0
84	SLU 64	-580	12	4681	-0.18	-20.4	0
84	SLU 65	-580	12	4681	-0.18	-20.4	0
84	SLU 66	-580	12	4681	-0.18	-20.4	0
84	SLU 67	-580	12	4681	-0.18	-20.4	0
84	SLU 68	-580	12	4681	-0.18	-20.4	0
84	SLU 69	-580	12	4681	-0.18	-20.4	0
84	SLU 70	-580	12	4681	-0.18	-20.4	0
84	SLU 71	-580	12	4681	-0.18	-20.4	0
84	SLU 72	-580	12	4681	-0.18	-20.4	0
84	SLU 73	-724	15	5526	-0.24	-25.85	0
84	SLU 74	-724	15	5526	-0.24	-25.85	0
84	SLU 75	-724	15	5526	-0.24	-25.85	0
84	SLU 76	-724	15	5526	-0.24	-25.85	0
84	SLU 77	-724	15	5526	-0.24	-25.85	0
84	SLU 78	-724	15	5526	-0.24	-25.85	0
84	SLU 79	-724	15	5526	-0.24	-25.85	0
84	SLU 80	-724	15	5526	-0.24	-25.85	0
84	SLU 81	-786	17	5888	-0.26	-28.19	0
84	SLU 82	-786	17	5888	-0.26	-28.19	0
84	SLU 83	-786	17	5888	-0.26	-28.19	0
84	SLU 84	-786	17	5888	-0.26	-28.19	0
84	SLE RA 1	-427	9	3497	-0.14	-14.97	0
84	SLE RA 2	-427	9	3497	-0.14	-14.97	0
84	SLE RA 3	-427	9	3497	-0.14	-14.97	0
84	SLE RA 4	-427	9	3497	-0.14	-14.97	0
84	SLE RA 5	-427	9	3497	-0.14	-14.97	0
84	SLE RA 6	-427	9	3497	-0.14	-14.97	0
84	SLE RA 7	-427	9	3497	-0.14	-14.97	0
84	SLE RA 8	-427	9	3497	-0.14	-14.97	0
84	SLE RA 9	-427	9	3497	-0.14	-14.97	0
84	SLE RA 10	-523	11	4060	-0.17	-18.6	0
84	SLE RA 11	-523	11	4060	-0.17	-18.6	0
84	SLE RA 12	-523	11	4060	-0.17	-18.6	0
84	SLE RA 13	-523	11	4060	-0.17	-18.6	0
84	SLE RA 14	-523	11	4060	-0.17	-18.6	0
84	SLE RA 15	-523	11	4060	-0.17	-18.6	0
84	SLE RA 16	-523	11	4060	-0.17	-18.6	0
84	SLE RA 17	-523	11	4060	-0.17	-18.6	0
84	SLE RA 18	-564	12	4301	-0.19	-20.16	0
84	SLE RA 19	-564	12	4301	-0.19	-20.16	0
84	SLE RA 20	-564	12	4301	-0.19	-20.16	0
84	SLE RA 21	-564	12	4301	-0.19	-20.16	0
84	SLE FR 1	-427	9	3497	-0.14	-14.97	0
84	SLE FR 2	-427	9	3497	-0.14	-14.97	0
84	SLE FR 3	-427	9	3497	-0.14	-14.97	0
84	SLE FR 4	-468	10	3738	-0.15	-16.52	0
84	SLE FR 5	-468	10	3738	-0.15	-16.52	0
84	SLE FR 6	-496	11	3899	-0.16	-17.56	0
84	SLE QP 1	-427	9	3497	-0.14	-14.97	0
84	SLE QP 2	-468	10	3738	-0.15	-16.52	0
84	SLD 1	-336	164	3318	-6.61	-9.68	-0.01
84	SLD 2	-336	164	3318	-6.61	-9.68	-0.01
84	SLD 3	-317	9	3258	-0.03	-10.51	0
84	SLD 4	-317	9	3258	-0.03	-10.51	0
84	SLD 5	-457	291	3703	-12.06	-13.22	-0.02
84	SLD 6	-457	291	3703	-12.06	-13.22	-0.02
84	SLD 7	-395	-225	3503	9.85	-15.97	0.02
84	SLD 8	-395	-225	3503	9.85	-15.97	0.02
84	SLD 9	-542	245	3973	-10.16	-17.08	-0.01
84	SLD 10	-542	245	3973	-10.16	-17.08	-0.01
84	SLD 11	-480	-271	3773	11.76	-19.83	0.02
84	SLD 12	-480	-271	3773	11.76	-19.83	0.02
84	SLD 13	-619	11	4218	-0.27	-22.54	0
84	SLD 14	-619	11	4218	-0.27	-22.54	0
84	SLD 15	-600	-144	4158	6.3	-23.37	0.01
84	SLD 16	-600	-144	4158	6.3	-23.37	0.01
84	SLV 1	-155	372	2742	-15.33	-0.35	-0.03
84	SLV 2	-155	372	2742	-15.33	-0.35	-0.03
84	SLV 3	-111	8	2599	0.14	-2.29	0
84	SLV 4	-111	8	2599	0.14	-2.29	0
84	SLV 5	-441	670	3655	-28.17	-8.72	-0.04



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
84	SLV 6	-441	670	3655	-28.17	-8.72	-0.04
84	SLV 7	-294	-542	3180	23.4	-15.21	0.04
84	SLV 8	-294	-542	3180	23.4	-15.21	0.04
84	SLV 9	-642	562	4296	-23.71	-17.84	-0.03
84	SLV 10	-642	562	4296	-23.71	-17.84	-0.03
84	SLV 11	-495	-650	3821	27.87	-24.33	0.04
84	SLV 12	-495	-650	3821	27.87	-24.33	0.04
84	SLV 13	-825	12	4877	-0.45	-30.76	0
84	SLV 14	-825	12	4877	-0.45	-30.76	0
84	SLV 15	-781	-352	4734	15.03	-32.7	0.03
84	SLV 16	-781	-352	4734	15.03	-32.7	0.03
85	SLU 1	0	-1	977	-0.01	-0.05	-0.02
85	SLU 2	0	-1	977	-0.01	-0.05	-0.02
85	SLU 3	0	-1	977	-0.01	-0.05	-0.02
85	SLU 4	0	-1	977	-0.01	-0.05	-0.02
85	SLU 5	0	-1	977	-0.01	-0.05	-0.02
85	SLU 6	0	-1	977	-0.01	-0.05	-0.02
85	SLU 7	0	-1	977	-0.01	-0.05	-0.02
85	SLU 8	0	-1	977	-0.01	-0.05	-0.02
85	SLU 9	0	-1	977	-0.01	-0.05	-0.02
85	SLU 10	0	-1	1308	-0.04	-0.06	-0.02
85	SLU 11	0	-1	1308	-0.04	-0.06	-0.02
85	SLU 12	0	-1	1308	-0.04	-0.06	-0.02
85	SLU 13	0	-1	1308	-0.04	-0.06	-0.02
85	SLU 14	0	-1	1308	-0.04	-0.06	-0.02
85	SLU 15	0	-1	1308	-0.04	-0.06	-0.02
85	SLU 16	0	-1	1308	-0.04	-0.06	-0.02
85	SLU 17	0	-1	1308	-0.04	-0.06	-0.02
85	SLU 18	0	-2	1450	-0.05	-0.06	-0.02
85	SLU 19	0	-2	1450	-0.05	-0.06	-0.02
85	SLU 20	0	-2	1450	-0.05	-0.06	-0.02
85	SLU 21	0	-2	1450	-0.05	-0.06	-0.02
85	SLU 22	0	-1	1174	-0.03	-0.06	-0.02
85	SLU 23	0	-1	1174	-0.03	-0.06	-0.02
85	SLU 24	0	-1	1174	-0.03	-0.06	-0.02
85	SLU 25	0	-1	1174	-0.03	-0.06	-0.02
85	SLU 26	0	-1	1174	-0.03	-0.06	-0.02
85	SLU 27	0	-1	1174	-0.03	-0.06	-0.02
85	SLU 28	0	-1	1174	-0.03	-0.06	-0.02
85	SLU 29	0	-1	1174	-0.03	-0.06	-0.02
85	SLU 30	0	-1	1174	-0.03	-0.06	-0.02
85	SLU 31	0	-2	1504	-0.06	-0.07	-0.02
85	SLU 32	0	-2	1504	-0.06	-0.07	-0.02
85	SLU 33	0	-2	1504	-0.06	-0.07	-0.02
85	SLU 34	0	-2	1504	-0.06	-0.07	-0.02
85	SLU 35	0	-2	1504	-0.06	-0.07	-0.02
85	SLU 36	0	-2	1504	-0.06	-0.07	-0.02
85	SLU 37	0	-2	1504	-0.06	-0.07	-0.02
85	SLU 38	0	-2	1504	-0.06	-0.07	-0.02
85	SLU 39	0	-2	1646	-0.07	-0.07	-0.03
85	SLU 40	0	-2	1646	-0.07	-0.07	-0.03
85	SLU 41	0	-2	1646	-0.07	-0.07	-0.03
85	SLU 42	0	-2	1646	-0.07	-0.07	-0.03
85	SLU 43	0	-1	1203	0	-0.06	-0.02
85	SLU 44	0	-1	1203	0	-0.06	-0.02
85	SLU 45	0	-1	1203	0	-0.06	-0.02
85	SLU 46	0	-1	1203	0	-0.06	-0.02
85	SLU 47	0	-1	1203	0	-0.06	-0.02
85	SLU 48	0	-1	1203	0	-0.06	-0.02
85	SLU 49	0	-1	1203	0	-0.06	-0.02
85	SLU 50	0	-1	1203	0	-0.06	-0.02
85	SLU 51	0	-1	1203	0	-0.06	-0.02
85	SLU 52	0	-1	1534	-0.03	-0.07	-0.02
85	SLU 53	0	-1	1534	-0.03	-0.07	-0.02
85	SLU 54	0	-1	1534	-0.03	-0.07	-0.02
85	SLU 55	0	-1	1534	-0.03	-0.07	-0.02
85	SLU 56	0	-1	1534	-0.03	-0.07	-0.02
85	SLU 57	0	-1	1534	-0.03	-0.07	-0.02
85	SLU 58	0	-1	1534	-0.03	-0.07	-0.02
85	SLU 59	0	-1	1534	-0.03	-0.07	-0.02
85	SLU 60	0	-2	1675	-0.04	-0.08	-0.03
85	SLU 61	0	-2	1675	-0.04	-0.08	-0.03
85	SLU 62	0	-2	1675	-0.04	-0.08	-0.03
85	SLU 63	0	-2	1675	-0.04	-0.08	-0.03
85	SLU 64	0	-1	1399	-0.02	-0.07	-0.02
85	SLU 65	0	-1	1399	-0.02	-0.07	-0.02
85	SLU 66	0	-1	1399	-0.02	-0.07	-0.02
85	SLU 67	0	-1	1399	-0.02	-0.07	-0.02
85	SLU 68	0	-1	1399	-0.02	-0.07	-0.02
85	SLU 69	0	-1	1399	-0.02	-0.07	-0.02
85	SLU 70	0	-1	1399	-0.02	-0.07	-0.02
85	SLU 71	0	-1	1399	-0.02	-0.07	-0.02
85	SLU 72	0	-1	1399	-0.02	-0.07	-0.02
85	SLU 73	0	-2	1730	-0.05	-0.08	-0.03
85	SLU 74	0	-2	1730	-0.05	-0.08	-0.03
85	SLU 75	0	-2	1730	-0.05	-0.08	-0.03
85	SLU 76	0	-2	1730	-0.05	-0.08	-0.03
85	SLU 77	0	-2	1730	-0.05	-0.08	-0.03
85	SLU 78	0	-2	1730	-0.05	-0.08	-0.03



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
85	SLU 79	0	-2	1730	-0.05	-0.08	-0.03
85	SLU 80	0	-2	1730	-0.05	-0.08	-0.03
85	SLU 81	0	-2	1872	-0.06	-0.09	-0.03
85	SLU 82	0	-2	1872	-0.06	-0.09	-0.03
85	SLU 83	0	-2	1872	-0.06	-0.09	-0.03
85	SLU 84	0	-2	1872	-0.06	-0.09	-0.03
85	SLE RA 1	0	-1	1033	-0.01	-0.05	-0.02
85	SLE RA 2	0	-1	1033	-0.01	-0.05	-0.02
85	SLE RA 3	0	-1	1033	-0.01	-0.05	-0.02
85	SLE RA 4	0	-1	1033	-0.01	-0.05	-0.02
85	SLE RA 5	0	-1	1033	-0.01	-0.05	-0.02
85	SLE RA 6	0	-1	1033	-0.01	-0.05	-0.02
85	SLE RA 7	0	-1	1033	-0.01	-0.05	-0.02
85	SLE RA 8	0	-1	1033	-0.01	-0.05	-0.02
85	SLE RA 9	0	-1	1033	-0.01	-0.05	-0.02
85	SLE RA 10	0	-1	1254	-0.03	-0.06	-0.02
85	SLE RA 11	0	-1	1254	-0.03	-0.06	-0.02
85	SLE RA 12	0	-1	1254	-0.03	-0.06	-0.02
85	SLE RA 13	0	-1	1254	-0.03	-0.06	-0.02
85	SLE RA 14	0	-1	1254	-0.03	-0.06	-0.02
85	SLE RA 15	0	-1	1254	-0.03	-0.06	-0.02
85	SLE RA 16	0	-1	1254	-0.03	-0.06	-0.02
85	SLE RA 17	0	-1	1254	-0.03	-0.06	-0.02
85	SLE RA 18	0	-1	1348	-0.04	-0.06	-0.02
85	SLE RA 19	0	-1	1348	-0.04	-0.06	-0.02
85	SLE RA 20	0	-1	1348	-0.04	-0.06	-0.02
85	SLE RA 21	0	-1	1348	-0.04	-0.06	-0.02
85	SLE FR 1	0	-1	1033	-0.01	-0.05	-0.02
85	SLE FR 2	0	-1	1033	-0.01	-0.05	-0.02
85	SLE FR 3	0	-1	1033	-0.01	-0.05	-0.02
85	SLE FR 4	0	-1	1128	-0.02	-0.05	-0.02
85	SLE FR 5	0	-1	1128	-0.02	-0.05	-0.02
85	SLE FR 6	0	-1	1191	-0.03	-0.06	-0.02
85	SLE QP 1	0	-1	1033	-0.01	-0.05	-0.02
85	SLE QP 2	0	-1	1128	-0.02	-0.05	-0.02
85	SLD 1	-2	-29	1123	-20.02	0.17	0
85	SLD 2	-2	-29	1123	-20.02	0.17	0
85	SLD 3	0	52	1186	37.12	1.32	0.03
85	SLD 4	0	52	1186	37.12	1.32	0.03
85	SLD 5	-3	-132	1031	-92.69	-1.72	-0.06
85	SLD 6	-3	-132	1031	-92.69	-1.72	-0.06
85	SLD 7	2	138	1241	97.79	2.09	0.04
85	SLD 8	2	138	1241	97.79	2.09	0.04
85	SLD 9	-3	-140	1015	-97.83	-2.2	-0.08
85	SLD 10	-3	-140	1015	-97.83	-2.2	-0.08
85	SLD 11	3	131	1225	92.65	1.61	0.02
85	SLD 12	3	131	1225	92.65	1.61	0.02
85	SLD 13	0	-54	1070	-37.16	-1.43	-0.07
85	SLD 14	0	-54	1070	-37.16	-1.43	-0.07
85	SLD 15	1	27	1132	19.98	-0.28	-0.03
85	SLD 16	1	27	1132	19.98	-0.28	-0.03
85	SLV 1	-4	-73	1111	-51.34	0.47	0.02
85	SLV 2	-4	-73	1111	-51.34	0.47	0.02
85	SLV 3	0	135	1272	95.27	3.4	0.1
85	SLV 4	0	135	1272	95.27	3.4	0.1
85	SLV 5	-8	-338	878	-237.77	-4.34	-0.13
85	SLV 6	-8	-338	878	-237.77	-4.34	-0.13
85	SLV 7	7	355	1416	250.92	5.42	0.13
85	SLV 8	7	355	1416	250.92	5.42	0.13
85	SLV 9	-7	-357	840	-250.96	-5.53	-0.17
85	SLV 10	-7	-357	840	-250.96	-5.53	-0.17
85	SLV 11	8	336	1378	237.73	4.23	0.09
85	SLV 12	8	336	1378	237.73	4.23	0.09
85	SLV 13	0	-137	983	-95.31	-3.5	-0.13
85	SLV 14	0	-137	983	-95.31	-3.5	-0.13
85	SLV 15	4	71	1145	51.3	-0.57	-0.06
85	SLV 16	4	71	1145	51.3	-0.57	-0.06
86	SLU 1	5	-86	2284	2.8	1.51	0.02
86	SLU 2	5	-86	2284	2.8	1.51	0.02
86	SLU 3	5	-86	2284	2.8	1.51	0.02
86	SLU 4	5	-86	2284	2.8	1.51	0.02
86	SLU 5	5	-86	2284	2.8	1.51	0.02
86	SLU 6	5	-86	2284	2.8	1.51	0.02
86	SLU 7	5	-86	2284	2.8	1.51	0.02
86	SLU 8	5	-86	2284	2.8	1.51	0.02
86	SLU 9	5	-86	2284	2.8	1.51	0.02
86	SLU 10	6	-117	2818	3.85	2.04	0.02
86	SLU 11	6	-117	2818	3.85	2.04	0.02
86	SLU 12	6	-117	2818	3.85	2.04	0.02
86	SLU 13	6	-117	2818	3.85	2.04	0.02
86	SLU 14	6	-117	2818	3.85	2.04	0.02
86	SLU 15	6	-117	2818	3.85	2.04	0.02
86	SLU 16	6	-117	2818	3.85	2.04	0.02
86	SLU 17	6	-117	2818	3.85	2.04	0.02
86	SLU 18	7	-131	3046	4.3	2.27	0.03
86	SLU 19	7	-131	3046	4.3	2.27	0.03
86	SLU 20	7	-131	3046	4.3	2.27	0.03
86	SLU 21	7	-131	3046	4.3	2.27	0.03
86	SLU 22	6	-108	2587	3.52	1.85	0.02



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
86	SLU 23	6	-108	2587	3.52	1.85	0.02
86	SLU 24	6	-108	2587	3.52	1.85	0.02
86	SLU 25	6	-108	2587	3.52	1.85	0.02
86	SLU 26	6	-108	2587	3.52	1.85	0.02
86	SLU 27	6	-108	2587	3.52	1.85	0.02
86	SLU 28	6	-108	2587	3.52	1.85	0.02
86	SLU 29	6	-108	2587	3.52	1.85	0.02
86	SLU 30	6	-108	2587	3.52	1.85	0.02
86	SLU 31	7	-139	3121	4.56	2.38	0.03
86	SLU 32	7	-139	3121	4.56	2.38	0.03
86	SLU 33	7	-139	3121	4.56	2.38	0.03
86	SLU 34	7	-139	3121	4.56	2.38	0.03
86	SLU 35	7	-139	3121	4.56	2.38	0.03
86	SLU 36	7	-139	3121	4.56	2.38	0.03
86	SLU 37	7	-139	3121	4.56	2.38	0.03
86	SLU 38	7	-139	3121	4.56	2.38	0.03
86	SLU 39	8	-153	3350	5.01	2.61	0.03
86	SLU 40	8	-153	3350	5.01	2.61	0.03
86	SLU 41	8	-153	3350	5.01	2.61	0.03
86	SLU 42	8	-153	3350	5.01	2.61	0.03
86	SLU 43	6	-104	2865	3.4	1.84	0.02
86	SLU 44	6	-104	2865	3.4	1.84	0.02
86	SLU 45	6	-104	2865	3.4	1.84	0.02
86	SLU 46	6	-104	2865	3.4	1.84	0.02
86	SLU 47	6	-104	2865	3.4	1.84	0.02
86	SLU 48	6	-104	2865	3.4	1.84	0.02
86	SLU 49	6	-104	2865	3.4	1.84	0.02
86	SLU 50	6	-104	2865	3.4	1.84	0.02
86	SLU 51	6	-104	2865	3.4	1.84	0.02
86	SLU 52	7	-135	3399	4.44	2.37	0.03
86	SLU 53	7	-135	3399	4.44	2.37	0.03
86	SLU 54	7	-135	3399	4.44	2.37	0.03
86	SLU 55	7	-135	3399	4.44	2.37	0.03
86	SLU 56	7	-135	3399	4.44	2.37	0.03
86	SLU 57	7	-135	3399	4.44	2.37	0.03
86	SLU 58	7	-135	3399	4.44	2.37	0.03
86	SLU 59	7	-135	3399	4.44	2.37	0.03
86	SLU 60	8	-149	3628	4.89	2.6	0.03
86	SLU 61	8	-149	3628	4.89	2.6	0.03
86	SLU 62	8	-149	3628	4.89	2.6	0.03
86	SLU 63	8	-149	3628	4.89	2.6	0.03
86	SLU 64	7	-126	3169	4.11	2.18	0.03
86	SLU 65	7	-126	3169	4.11	2.18	0.03
86	SLU 66	7	-126	3169	4.11	2.18	0.03
86	SLU 67	7	-126	3169	4.11	2.18	0.03
86	SLU 68	7	-126	3169	4.11	2.18	0.03
86	SLU 69	7	-126	3169	4.11	2.18	0.03
86	SLU 70	7	-126	3169	4.11	2.18	0.03
86	SLU 71	7	-126	3169	4.11	2.18	0.03
86	SLU 72	7	-126	3169	4.11	2.18	0.03
86	SLU 73	8	-158	3702	5.16	2.71	0.03
86	SLU 74	8	-158	3702	5.16	2.71	0.03
86	SLU 75	8	-158	3702	5.16	2.71	0.03
86	SLU 76	8	-158	3702	5.16	2.71	0.03
86	SLU 77	8	-158	3702	5.16	2.71	0.03
86	SLU 78	8	-158	3702	5.16	2.71	0.03
86	SLU 79	8	-158	3702	5.16	2.71	0.03
86	SLU 80	8	-158	3702	5.16	2.71	0.03
86	SLU 81	9	-171	3931	5.61	2.94	0.03
86	SLU 82	9	-171	3931	5.61	2.94	0.03
86	SLU 83	9	-171	3931	5.61	2.94	0.03
86	SLU 84	9	-171	3931	5.61	2.94	0.03
86	SLE RA 1	5	-92	2371	3.01	1.6	0.02
86	SLE RA 2	5	-92	2371	3.01	1.6	0.02
86	SLE RA 3	5	-92	2371	3.01	1.6	0.02
86	SLE RA 4	5	-92	2371	3.01	1.6	0.02
86	SLE RA 5	5	-92	2371	3.01	1.6	0.02
86	SLE RA 6	5	-92	2371	3.01	1.6	0.02
86	SLE RA 7	5	-92	2371	3.01	1.6	0.02
86	SLE RA 8	5	-92	2371	3.01	1.6	0.02
86	SLE RA 9	5	-92	2371	3.01	1.6	0.02
86	SLE RA 10	6	-113	2726	3.7	1.96	0.02
86	SLE RA 11	6	-113	2726	3.7	1.96	0.02
86	SLE RA 12	6	-113	2726	3.7	1.96	0.02
86	SLE RA 13	6	-113	2726	3.7	1.96	0.02
86	SLE RA 14	6	-113	2726	3.7	1.96	0.02
86	SLE RA 15	6	-113	2726	3.7	1.96	0.02
86	SLE RA 16	6	-113	2726	3.7	1.96	0.02
86	SLE RA 17	6	-113	2726	3.7	1.96	0.02
86	SLE RA 18	6	-122	2879	4	2.11	0.02
86	SLE RA 19	6	-122	2879	4	2.11	0.02
86	SLE RA 20	6	-122	2879	4	2.11	0.02
86	SLE RA 21	6	-122	2879	4	2.11	0.02
86	SLE FR 1	5	-92	2371	3.01	1.6	0.02
86	SLE FR 2	5	-92	2371	3.01	1.6	0.02
86	SLE FR 3	5	-92	2371	3.01	1.6	0.02
86	SLE FR 4	5	-101	2523	3.31	1.76	0.02
86	SLE FR 5	5	-101	2523	3.31	1.76	0.02
86	SLE FR 6	6	-107	2625	3.5	1.86	0.02



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
86	SLE QP 1	5	-92	2371	3.01	1.6	0.02
86	SLE QP 2	5	-101	2523	3.31	1.76	0.02
86	SLD 1	-7	-117	2780	3.77	3.91	0.04
86	SLD 2	-7	-117	2780	3.77	3.91	0.04
86	SLD 3	0	-291	2744	10.87	7.48	0.03
86	SLD 4	0	-291	2744	10.87	7.48	0.03
86	SLD 5	-10	158	2655	-7.32	-3.01	0.04
86	SLD 6	-10	158	2655	-7.32	-3.01	0.04
86	SLD 7	15	-422	2535	16.34	8.89	0.01
86	SLD 8	15	-422	2535	16.34	8.89	0.01
86	SLD 9	-4	220	2511	-9.73	-5.38	0.03
86	SLD 10	-4	220	2511	-9.73	-5.38	0.03
86	SLD 11	21	-361	2392	13.93	6.53	0
86	SLD 12	21	-361	2392	13.93	6.53	0
86	SLD 13	11	89	2302	-4.26	-3.97	0.01
86	SLD 14	11	89	2302	-4.26	-3.97	0.01
86	SLD 15	18	-85	2266	2.84	-0.4	0
86	SLD 16	18	-85	2266	2.84	-0.4	0
86	SLV 1	-26	-139	3152	4.46	6.86	0.08
86	SLV 2	-26	-139	3152	4.46	6.86	0.08
86	SLV 3	-7	-548	3064	21.11	16.01	0.05
86	SLV 4	-7	-548	3064	21.11	16.01	0.05
86	SLV 5	-33	507	2845	-21.61	-10.58	0.08
86	SLV 6	-33	507	2845	-21.61	-10.58	0.08
86	SLV 7	31	-855	2552	33.9	19.9	-0.01
86	SLV 8	31	-855	2552	33.9	19.9	-0.01
86	SLV 9	-20	653	2495	-27.29	-16.38	0.05
86	SLV 10	-20	653	2495	-27.29	-16.38	0.05
86	SLV 11	44	-709	2201	28.22	14.09	-0.04
86	SLV 12	44	-709	2201	28.22	14.09	-0.04
86	SLV 13	18	346	1983	-14.5	-12.49	-0.01
86	SLV 14	18	346	1983	-14.5	-12.49	-0.01
86	SLV 15	37	-63	1895	2.15	-3.35	-0.04
86	SLV 16	37	-63	1895	2.15	-3.35	-0.04
87	SLU 1	-5	-92	2355	2.56	-1.53	-0.02
87	SLU 2	-5	-92	2355	2.56	-1.53	-0.02
87	SLU 3	-5	-92	2355	2.56	-1.53	-0.02
87	SLU 4	-5	-92	2355	2.56	-1.53	-0.02
87	SLU 5	-5	-92	2355	2.56	-1.53	-0.02
87	SLU 6	-5	-92	2355	2.56	-1.53	-0.02
87	SLU 7	-5	-92	2355	2.56	-1.53	-0.02
87	SLU 8	-5	-92	2355	2.56	-1.53	-0.02
87	SLU 9	-5	-92	2355	2.56	-1.53	-0.02
87	SLU 10	-6	-132	2896	3.71	-2.12	-0.03
87	SLU 11	-6	-132	2896	3.71	-2.12	-0.03
87	SLU 12	-6	-132	2896	3.71	-2.12	-0.03
87	SLU 13	-6	-132	2896	3.71	-2.12	-0.03
87	SLU 14	-6	-132	2896	3.71	-2.12	-0.03
87	SLU 15	-6	-132	2896	3.71	-2.12	-0.03
87	SLU 16	-6	-132	2896	3.71	-2.12	-0.03
87	SLU 17	-6	-132	2896	3.71	-2.12	-0.03
87	SLU 18	-7	-150	3128	4.2	-2.38	-0.03
87	SLU 19	-7	-150	3128	4.2	-2.38	-0.03
87	SLU 20	-7	-150	3128	4.2	-2.38	-0.03
87	SLU 21	-7	-150	3128	4.2	-2.38	-0.03
87	SLU 22	-6	-117	2650	3.3	-1.88	-0.02
87	SLU 23	-6	-117	2650	3.3	-1.88	-0.02
87	SLU 24	-6	-117	2650	3.3	-1.88	-0.02
87	SLU 25	-6	-117	2650	3.3	-1.88	-0.02
87	SLU 26	-6	-117	2650	3.3	-1.88	-0.02
87	SLU 27	-6	-117	2650	3.3	-1.88	-0.02
87	SLU 28	-6	-117	2650	3.3	-1.88	-0.02
87	SLU 29	-6	-117	2650	3.3	-1.88	-0.02
87	SLU 30	-6	-117	2650	3.3	-1.88	-0.02
87	SLU 31	-7	-158	3191	4.45	-2.48	-0.03
87	SLU 32	-7	-158	3191	4.45	-2.48	-0.03
87	SLU 33	-7	-158	3191	4.45	-2.48	-0.03
87	SLU 34	-7	-158	3191	4.45	-2.48	-0.03
87	SLU 35	-7	-158	3191	4.45	-2.48	-0.03
87	SLU 36	-7	-158	3191	4.45	-2.48	-0.03
87	SLU 37	-7	-158	3191	4.45	-2.48	-0.03
87	SLU 38	-7	-158	3191	4.45	-2.48	-0.03
87	SLU 39	-8	-175	3424	4.95	-2.73	-0.04
87	SLU 40	-8	-175	3424	4.95	-2.73	-0.04
87	SLU 41	-8	-175	3424	4.95	-2.73	-0.04
87	SLU 42	-8	-175	3424	4.95	-2.73	-0.04
87	SLU 43	-6	-111	2960	3.07	-1.86	-0.03
87	SLU 44	-6	-111	2960	3.07	-1.86	-0.03
87	SLU 45	-6	-111	2960	3.07	-1.86	-0.03
87	SLU 46	-6	-111	2960	3.07	-1.86	-0.03
87	SLU 47	-6	-111	2960	3.07	-1.86	-0.03
87	SLU 48	-6	-111	2960	3.07	-1.86	-0.03
87	SLU 49	-6	-111	2960	3.07	-1.86	-0.03
87	SLU 50	-6	-111	2960	3.07	-1.86	-0.03
87	SLU 51	-6	-111	2960	3.07	-1.86	-0.03
87	SLU 52	-7	-151	3502	4.22	-2.46	-0.03
87	SLU 53	-7	-151	3502	4.22	-2.46	-0.03
87	SLU 54	-7	-151	3502	4.22	-2.46	-0.03
87	SLU 55	-7	-151	3502	4.22	-2.46	-0.03



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
87	SLU 56	-7	-151	3502	4.22	-2.46	-0.03
87	SLU 57	-7	-151	3502	4.22	-2.46	-0.03
87	SLU 58	-7	-151	3502	4.22	-2.46	-0.03
87	SLU 59	-7	-151	3502	4.22	-2.46	-0.03
87	SLU 60	-8	-168	3734	4.71	-2.71	-0.04
87	SLU 61	-8	-168	3734	4.71	-2.71	-0.04
87	SLU 62	-8	-168	3734	4.71	-2.71	-0.04
87	SLU 63	-8	-168	3734	4.71	-2.71	-0.04
87	SLU 64	-7	-136	3255	3.81	-2.22	-0.03
87	SLU 65	-7	-136	3255	3.81	-2.22	-0.03
87	SLU 66	-7	-136	3255	3.81	-2.22	-0.03
87	SLU 67	-7	-136	3255	3.81	-2.22	-0.03
87	SLU 68	-7	-136	3255	3.81	-2.22	-0.03
87	SLU 69	-7	-136	3255	3.81	-2.22	-0.03
87	SLU 70	-7	-136	3255	3.81	-2.22	-0.03
87	SLU 71	-7	-136	3255	3.81	-2.22	-0.03
87	SLU 72	-7	-136	3255	3.81	-2.22	-0.03
87	SLU 73	-9	-176	3797	4.96	-2.82	-0.04
87	SLU 74	-9	-176	3797	4.96	-2.82	-0.04
87	SLU 75	-9	-176	3797	4.96	-2.82	-0.04
87	SLU 76	-9	-176	3797	4.96	-2.82	-0.04
87	SLU 77	-9	-176	3797	4.96	-2.82	-0.04
87	SLU 78	-9	-176	3797	4.96	-2.82	-0.04
87	SLU 79	-9	-176	3797	4.96	-2.82	-0.04
87	SLU 80	-9	-176	3797	4.96	-2.82	-0.04
87	SLU 81	-9	-194	4029	5.46	-3.07	-0.04
87	SLU 82	-9	-194	4029	5.46	-3.07	-0.04
87	SLU 83	-9	-194	4029	5.46	-3.07	-0.04
87	SLU 84	-9	-194	4029	5.46	-3.07	-0.04
87	SLE RA 1	-5	-99	2439	2.77	-1.63	-0.02
87	SLE RA 2	-5	-99	2439	2.77	-1.63	-0.02
87	SLE RA 3	-5	-99	2439	2.77	-1.63	-0.02
87	SLE RA 4	-5	-99	2439	2.77	-1.63	-0.02
87	SLE RA 5	-5	-99	2439	2.77	-1.63	-0.02
87	SLE RA 6	-5	-99	2439	2.77	-1.63	-0.02
87	SLE RA 7	-5	-99	2439	2.77	-1.63	-0.02
87	SLE RA 8	-5	-99	2439	2.77	-1.63	-0.02
87	SLE RA 9	-5	-99	2439	2.77	-1.63	-0.02
87	SLE RA 10	-6	-126	2800	3.54	-2.03	-0.03
87	SLE RA 11	-6	-126	2800	3.54	-2.03	-0.03
87	SLE RA 12	-6	-126	2800	3.54	-2.03	-0.03
87	SLE RA 13	-6	-126	2800	3.54	-2.03	-0.03
87	SLE RA 14	-6	-126	2800	3.54	-2.03	-0.03
87	SLE RA 15	-6	-126	2800	3.54	-2.03	-0.03
87	SLE RA 16	-6	-126	2800	3.54	-2.03	-0.03
87	SLE RA 17	-6	-126	2800	3.54	-2.03	-0.03
87	SLE RA 18	-7	-138	2955	3.87	-2.2	-0.03
87	SLE RA 19	-7	-138	2955	3.87	-2.2	-0.03
87	SLE RA 20	-7	-138	2955	3.87	-2.2	-0.03
87	SLE RA 21	-7	-138	2955	3.87	-2.2	-0.03
87	SLE FR 1	-5	-99	2439	2.77	-1.63	-0.02
87	SLE FR 2	-5	-99	2439	2.77	-1.63	-0.02
87	SLE FR 3	-5	-99	2439	2.77	-1.63	-0.02
87	SLE FR 4	-5	-111	2594	3.1	-1.8	-0.02
87	SLE FR 5	-5	-111	2594	3.1	-1.8	-0.02
87	SLE FR 6	-6	-118	2697	3.32	-1.91	-0.03
87	SLE QP 1	-5	-99	2439	2.77	-1.63	-0.02
87	SLE QP 2	-5	-111	2594	3.1	-1.8	-0.02
87	SLD 1	-12	61	2356	-3.7	4.34	-0.01
87	SLD 2	-12	61	2356	-3.7	4.34	-0.01
87	SLD 3	-25	-100	2393	2.89	-1.87	0
87	SLD 4	-25	-100	2393	2.89	-1.87	0
87	SLD 5	13	186	2468	-8.95	9.46	-0.04
87	SLD 6	13	186	2468	-8.95	9.46	-0.04
87	SLD 7	-31	-352	2589	13.04	-11.23	0.01
87	SLD 8	-31	-352	2589	13.04	-11.23	0.01
87	SLD 9	20	131	2599	-6.85	7.64	-0.06
87	SLD 10	20	131	2599	-6.85	7.64	-0.06
87	SLD 11	-24	-407	2720	15.15	-13.06	0
87	SLD 12	-24	-407	2720	15.15	-13.06	0
87	SLD 13	14	-121	2795	3.3	-1.73	-0.05
87	SLD 14	14	-121	2795	3.3	-1.73	-0.05
87	SLD 15	1	-283	2831	9.9	-7.94	-0.04
87	SLD 16	1	-283	2831	9.9	-7.94	-0.04
87	SLV 1	-20	294	2030	-12.88	13.65	0.01
87	SLV 2	-20	294	2030	-12.88	13.65	0.01
87	SLV 3	-54	-85	2116	2.61	-2.26	0.05
87	SLV 4	-54	-85	2116	2.61	-2.26	0.05
87	SLV 5	41	585	2295	-25.19	26.95	-0.07
87	SLV 6	41	585	2295	-25.19	26.95	-0.07
87	SLV 7	-71	-678	2581	26.45	-26.06	0.06
87	SLV 8	-71	-678	2581	26.45	-26.06	0.06
87	SLV 9	60	456	2607	-20.25	22.46	-0.1
87	SLV 10	60	456	2607	-20.25	22.46	-0.1
87	SLV 11	-52	-807	2893	31.39	-30.55	0.03
87	SLV 12	-52	-807	2893	31.39	-30.55	0.03
87	SLV 13	43	-136	3072	3.58	-1.34	-0.09
87	SLV 14	43	-136	3072	3.58	-1.34	-0.09
87	SLV 15	9	-515	3158	19.08	-17.24	-0.06



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
87	SLV 16	9	-515	3158	19.08	-17.24	-0.06
88	SLU 1	0	1	919	0.01	-0.02	0
88	SLU 2	0	1	919	0.01	-0.02	0
88	SLU 3	0	1	919	0.01	-0.02	0
88	SLU 4	0	1	919	0.01	-0.02	0
88	SLU 5	0	1	919	0.01	-0.02	0
88	SLU 6	0	1	919	0.01	-0.02	0
88	SLU 7	0	1	919	0.01	-0.02	0
88	SLU 8	0	1	919	0.01	-0.02	0
88	SLU 9	0	1	919	0.01	-0.02	0
88	SLU 10	0	2	1265	0	-0.02	0
88	SLU 11	0	2	1265	0	-0.02	0
88	SLU 12	0	2	1265	0	-0.02	0
88	SLU 13	0	2	1265	0	-0.02	0
88	SLU 14	0	2	1265	0	-0.02	0
88	SLU 15	0	2	1265	0	-0.02	0
88	SLU 16	0	2	1265	0	-0.02	0
88	SLU 17	0	2	1265	0	-0.02	0
88	SLU 18	0	2	1414	-0.01	-0.02	0
88	SLU 19	0	2	1414	-0.01	-0.02	0
88	SLU 20	0	2	1414	-0.01	-0.02	0
88	SLU 21	0	2	1414	-0.01	-0.02	0
88	SLU 22	0	1	1106	-0.01	-0.02	0
88	SLU 23	0	1	1106	-0.01	-0.02	0
88	SLU 24	0	1	1106	-0.01	-0.02	0
88	SLU 25	0	1	1106	-0.01	-0.02	0
88	SLU 26	0	1	1106	-0.01	-0.02	0
88	SLU 27	0	1	1106	-0.01	-0.02	0
88	SLU 28	0	1	1106	-0.01	-0.02	0
88	SLU 29	0	1	1106	-0.01	-0.02	0
88	SLU 30	0	1	1106	-0.01	-0.02	0
88	SLU 31	0	2	1452	-0.01	-0.02	0
88	SLU 32	0	2	1452	-0.01	-0.02	0
88	SLU 33	0	2	1452	-0.01	-0.02	0
88	SLU 34	0	2	1452	-0.01	-0.02	0
88	SLU 35	0	2	1452	-0.01	-0.02	0
88	SLU 36	0	2	1452	-0.01	-0.02	0
88	SLU 37	0	2	1452	-0.01	-0.02	0
88	SLU 38	0	2	1452	-0.01	-0.02	0
88	SLU 39	0	3	1600	-0.02	-0.02	0
88	SLU 40	0	3	1600	-0.02	-0.02	0
88	SLU 41	0	3	1600	-0.02	-0.02	0
88	SLU 42	0	3	1600	-0.02	-0.02	0
88	SLU 43	0	1	1131	0.01	-0.02	0
88	SLU 44	0	1	1131	0.01	-0.02	0
88	SLU 45	0	1	1131	0.01	-0.02	0
88	SLU 46	0	1	1131	0.01	-0.02	0
88	SLU 47	0	1	1131	0.01	-0.02	0
88	SLU 48	0	1	1131	0.01	-0.02	0
88	SLU 49	0	1	1131	0.01	-0.02	0
88	SLU 50	0	1	1131	0.01	-0.02	0
88	SLU 51	0	1	1131	0.01	-0.02	0
88	SLU 52	0	2	1477	0	-0.02	0
88	SLU 53	0	2	1477	0	-0.02	0
88	SLU 54	0	2	1477	0	-0.02	0
88	SLU 55	0	2	1477	0	-0.02	0
88	SLU 56	0	2	1477	0	-0.02	0
88	SLU 57	0	2	1477	0	-0.02	0
88	SLU 58	0	2	1477	0	-0.02	0
88	SLU 59	0	2	1477	0	-0.02	0
88	SLU 60	0	2	1625	0	-0.03	0
88	SLU 61	0	2	1625	0	-0.03	0
88	SLU 62	0	2	1625	0	-0.03	0
88	SLU 63	0	2	1625	0	-0.03	0
88	SLU 64	0	1	1318	0	-0.02	0
88	SLU 65	0	1	1318	0	-0.02	0
88	SLU 66	0	1	1318	0	-0.02	0
88	SLU 67	0	1	1318	0	-0.02	0
88	SLU 68	0	1	1318	0	-0.02	0
88	SLU 69	0	1	1318	0	-0.02	0
88	SLU 70	0	1	1318	0	-0.02	0
88	SLU 71	0	1	1318	0	-0.02	0
88	SLU 72	0	1	1318	0	-0.02	0
88	SLU 73	0	2	1664	-0.01	-0.03	0
88	SLU 74	0	2	1664	-0.01	-0.03	0
88	SLU 75	0	2	1664	-0.01	-0.03	0
88	SLU 76	0	2	1664	-0.01	-0.03	0
88	SLU 77	0	2	1664	-0.01	-0.03	0
88	SLU 78	0	2	1664	-0.01	-0.03	0
88	SLU 79	0	2	1664	-0.01	-0.03	0
88	SLU 80	0	2	1664	-0.01	-0.03	0
88	SLU 81	0	3	1812	-0.01	-0.03	0
88	SLU 82	0	3	1812	-0.01	-0.03	0
88	SLU 83	0	3	1812	-0.01	-0.03	0
88	SLU 84	0	3	1812	-0.01	-0.03	0
88	SLE RA 1	0	1	973	0	-0.02	0
88	SLE RA 2	0	1	973	0	-0.02	0
88	SLE RA 3	0	1	973	0	-0.02	0
88	SLE RA 4	0	1	973	0	-0.02	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
88	SLE RA 5	0	1	973	0	-0.02	0
88	SLE RA 6	0	1	973	0	-0.02	0
88	SLE RA 7	0	1	973	0	-0.02	0
88	SLE RA 8	0	1	973	0	-0.02	0
88	SLE RA 9	0	1	973	0	-0.02	0
88	SLE RA 10	0	2	1203	0	-0.02	0
88	SLE RA 11	0	2	1203	0	-0.02	0
88	SLE RA 12	0	2	1203	0	-0.02	0
88	SLE RA 13	0	2	1203	0	-0.02	0
88	SLE RA 14	0	2	1203	0	-0.02	0
88	SLE RA 15	0	2	1203	0	-0.02	0
88	SLE RA 16	0	2	1203	0	-0.02	0
88	SLE RA 17	0	2	1203	0	-0.02	0
88	SLE RA 18	0	2	1302	0	-0.02	0
88	SLE RA 19	0	2	1302	0	-0.02	0
88	SLE RA 20	0	2	1302	0	-0.02	0
88	SLE RA 21	0	2	1302	0	-0.02	0
88	SLE FR 1	0	1	973	0	-0.02	0
88	SLE FR 2	0	1	973	0	-0.02	0
88	SLE FR 3	0	1	973	0	-0.02	0
88	SLE FR 4	0	1	1072	0	-0.02	0
88	SLE FR 5	0	1	1072	0	-0.02	0
88	SLE FR 6	0	1	1138	0	-0.02	0
88	SLE QP 1	0	1	973	0	-0.02	0
88	SLE QP 2	0	1	1072	0	-0.02	0
88	SLD 1	-3	-23	1074	-8.05	1.07	-0.08
88	SLD 2	-3	-23	1074	-8.05	1.07	-0.08
88	SLD 3	-1	47	1112	14.89	2.87	-0.13
88	SLD 4	-1	47	1112	14.89	2.87	-0.13
88	SLD 5	-3	-111	1015	-37.22	-2.41	0.06
88	SLD 6	-3	-111	1015	-37.22	-2.41	0.06
88	SLD 7	2	120	1141	39.27	3.57	-0.12
88	SLD 8	2	120	1141	39.27	3.57	-0.12
88	SLD 9	-2	-118	1002	-39.27	-3.61	0.12
88	SLD 10	-2	-118	1002	-39.27	-3.61	0.12
88	SLD 11	3	114	1128	37.22	2.38	-0.05
88	SLD 12	3	114	1128	37.22	2.38	-0.05
88	SLD 13	1	-44	1031	-14.89	-2.91	0.13
88	SLD 14	1	-44	1031	-14.89	-2.91	0.13
88	SLD 15	3	25	1069	8.06	-1.11	0.08
88	SLD 16	3	25	1069	8.06	-1.11	0.08
88	SLV 1	-7	-60	1075	-20.66	2.63	-0.19
88	SLV 2	-7	-60	1075	-20.66	2.63	-0.19
88	SLV 3	-3	118	1172	38.21	7.24	-0.32
88	SLV 4	-3	118	1172	38.21	7.24	-0.32
88	SLV 5	-8	-288	926	-95.49	-6.21	0.15
88	SLV 6	-8	-288	926	-95.49	-6.21	0.15
88	SLV 7	5	307	1249	100.76	9.14	-0.3
88	SLV 8	5	307	1249	100.76	9.14	-0.3
88	SLV 9	-5	-304	895	-100.76	-9.18	0.3
88	SLV 10	-5	-304	895	-100.76	-9.18	0.3
88	SLV 11	8	290	1218	95.49	6.17	-0.14
88	SLV 12	8	290	1218	95.49	6.17	-0.14
88	SLV 13	3	-116	972	-38.21	-7.28	0.33
88	SLV 14	3	-116	972	-38.21	-7.28	0.33
88	SLV 15	7	63	1068	20.67	-2.67	0.19
88	SLV 16	7	63	1068	20.67	-2.67	0.19
89	SLU 1	1	-85	2169	2.94	0.64	-0.01
89	SLU 2	1	-85	2169	2.94	0.64	-0.01
89	SLU 3	1	-85	2169	2.94	0.64	-0.01
89	SLU 4	1	-85	2169	2.94	0.64	-0.01
89	SLU 5	1	-85	2169	2.94	0.64	-0.01
89	SLU 6	1	-85	2169	2.94	0.64	-0.01
89	SLU 7	1	-85	2169	2.94	0.64	-0.01
89	SLU 8	1	-85	2169	2.94	0.64	-0.01
89	SLU 9	1	-85	2169	2.94	0.64	-0.01
89	SLU 10	1	-116	2666	4.03	0.9	-0.01
89	SLU 11	1	-116	2666	4.03	0.9	-0.01
89	SLU 12	1	-116	2666	4.03	0.9	-0.01
89	SLU 13	1	-116	2666	4.03	0.9	-0.01
89	SLU 14	1	-116	2666	4.03	0.9	-0.01
89	SLU 15	1	-116	2666	4.03	0.9	-0.01
89	SLU 16	1	-116	2666	4.03	0.9	-0.01
89	SLU 17	1	-116	2666	4.03	0.9	-0.01
89	SLU 18	1	-129	2879	4.5	1.02	-0.01
89	SLU 19	1	-129	2879	4.5	1.02	-0.01
89	SLU 20	1	-129	2879	4.5	1.02	-0.01
89	SLU 21	1	-129	2879	4.5	1.02	-0.01
89	SLU 22	1	-106	2441	3.66	0.8	-0.01
89	SLU 23	1	-106	2441	3.66	0.8	-0.01
89	SLU 24	1	-106	2441	3.66	0.8	-0.01
89	SLU 25	1	-106	2441	3.66	0.8	-0.01
89	SLU 26	1	-106	2441	3.66	0.8	-0.01
89	SLU 27	1	-106	2441	3.66	0.8	-0.01
89	SLU 28	1	-106	2441	3.66	0.8	-0.01
89	SLU 29	1	-106	2441	3.66	0.8	-0.01
89	SLU 30	1	-106	2441	3.66	0.8	-0.01
89	SLU 31	1	-137	2938	4.75	1.06	-0.01
89	SLU 32	1	-137	2938	4.75	1.06	-0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
89	SLU 33	1	-137	2938	4.75	1.06	-0.01
89	SLU 34	1	-137	2938	4.75	1.06	-0.01
89	SLU 35	1	-137	2938	4.75	1.06	-0.01
89	SLU 36	1	-137	2938	4.75	1.06	-0.01
89	SLU 37	1	-137	2938	4.75	1.06	-0.01
89	SLU 38	1	-137	2938	4.75	1.06	-0.01
89	SLU 39	1	-150	3151	5.22	1.18	-0.01
89	SLU 40	1	-150	3151	5.22	1.18	-0.01
89	SLU 41	1	-150	3151	5.22	1.18	-0.01
89	SLU 42	1	-150	3151	5.22	1.18	-0.01
89	SLU 43	1	-103	2726	3.57	0.78	-0.01
89	SLU 44	1	-103	2726	3.57	0.78	-0.01
89	SLU 45	1	-103	2726	3.57	0.78	-0.01
89	SLU 46	1	-103	2726	3.57	0.78	-0.01
89	SLU 47	1	-103	2726	3.57	0.78	-0.01
89	SLU 48	1	-103	2726	3.57	0.78	-0.01
89	SLU 49	1	-103	2726	3.57	0.78	-0.01
89	SLU 50	1	-103	2726	3.57	0.78	-0.01
89	SLU 51	1	-103	2726	3.57	0.78	-0.01
89	SLU 52	1	-134	3223	4.67	1.04	-0.01
89	SLU 53	1	-134	3223	4.67	1.04	-0.01
89	SLU 54	1	-134	3223	4.67	1.04	-0.01
89	SLU 55	1	-134	3223	4.67	1.04	-0.01
89	SLU 56	1	-134	3223	4.67	1.04	-0.01
89	SLU 57	1	-134	3223	4.67	1.04	-0.01
89	SLU 58	1	-134	3223	4.67	1.04	-0.01
89	SLU 59	1	-134	3223	4.67	1.04	-0.01
89	SLU 60	1	-147	3436	5.14	1.16	-0.01
89	SLU 61	1	-147	3436	5.14	1.16	-0.01
89	SLU 62	1	-147	3436	5.14	1.16	-0.01
89	SLU 63	1	-147	3436	5.14	1.16	-0.01
89	SLU 64	1	-124	2999	4.29	0.94	-0.01
89	SLU 65	1	-124	2999	4.29	0.94	-0.01
89	SLU 66	1	-124	2999	4.29	0.94	-0.01
89	SLU 67	1	-124	2999	4.29	0.94	-0.01
89	SLU 68	1	-124	2999	4.29	0.94	-0.01
89	SLU 69	1	-124	2999	4.29	0.94	-0.01
89	SLU 70	1	-124	2999	4.29	0.94	-0.01
89	SLU 71	1	-124	2999	4.29	0.94	-0.01
89	SLU 72	1	-124	2999	4.29	0.94	-0.01
89	SLU 73	1	-155	3496	5.39	1.2	-0.01
89	SLU 74	1	-155	3496	5.39	1.2	-0.01
89	SLU 75	1	-155	3496	5.39	1.2	-0.01
89	SLU 76	1	-155	3496	5.39	1.2	-0.01
89	SLU 77	1	-155	3496	5.39	1.2	-0.01
89	SLU 78	1	-155	3496	5.39	1.2	-0.01
89	SLU 79	1	-155	3496	5.39	1.2	-0.01
89	SLU 80	1	-155	3496	5.39	1.2	-0.01
89	SLU 81	1	-168	3709	5.86	1.32	-0.01
89	SLU 82	1	-168	3709	5.86	1.32	-0.01
89	SLU 83	1	-168	3709	5.86	1.32	-0.01
89	SLU 84	1	-168	3709	5.86	1.32	-0.01
89	SLE RA 1	1	-91	2247	3.14	0.69	-0.01
89	SLE RA 2	1	-91	2247	3.14	0.69	-0.01
89	SLE RA 3	1	-91	2247	3.14	0.69	-0.01
89	SLE RA 4	1	-91	2247	3.14	0.69	-0.01
89	SLE RA 5	1	-91	2247	3.14	0.69	-0.01
89	SLE RA 6	1	-91	2247	3.14	0.69	-0.01
89	SLE RA 7	1	-91	2247	3.14	0.69	-0.01
89	SLE RA 8	1	-91	2247	3.14	0.69	-0.01
89	SLE RA 9	1	-91	2247	3.14	0.69	-0.01
89	SLE RA 10	1	-111	2578	3.87	0.86	-0.01
89	SLE RA 11	1	-111	2578	3.87	0.86	-0.01
89	SLE RA 12	1	-111	2578	3.87	0.86	-0.01
89	SLE RA 13	1	-111	2578	3.87	0.86	-0.01
89	SLE RA 14	1	-111	2578	3.87	0.86	-0.01
89	SLE RA 15	1	-111	2578	3.87	0.86	-0.01
89	SLE RA 16	1	-111	2578	3.87	0.86	-0.01
89	SLE RA 17	1	-111	2578	3.87	0.86	-0.01
89	SLE RA 18	1	-120	2720	4.19	0.94	-0.01
89	SLE RA 19	1	-120	2720	4.19	0.94	-0.01
89	SLE RA 20	1	-120	2720	4.19	0.94	-0.01
89	SLE RA 21	1	-120	2720	4.19	0.94	-0.01
89	SLE FR 1	1	-91	2247	3.14	0.69	-0.01
89	SLE FR 2	1	-91	2247	3.14	0.69	-0.01
89	SLE FR 3	1	-91	2247	3.14	0.69	-0.01
89	SLE FR 4	1	-100	2389	3.46	0.76	-0.01
89	SLE FR 5	1	-100	2389	3.46	0.76	-0.01
89	SLE FR 6	1	-106	2483	3.67	0.81	-0.01
89	SLE QP 1	1	-91	2247	3.14	0.69	-0.01
89	SLE QP 2	1	-100	2389	3.46	0.76	-0.01
89	SLD 1	-15	-110	2619	3.77	6.45	-0.03
89	SLD 2	-15	-110	2619	3.77	6.45	-0.03
89	SLD 3	-5	-285	2571	10.85	12.2	-0.03
89	SLD 4	-5	-285	2571	10.85	12.2	-0.03
89	SLD 5	-20	162	2531	-7.18	-6.25	-0.02
89	SLD 6	-20	162	2531	-7.18	-6.25	-0.02
89	SLD 7	14	-420	2370	16.41	12.91	-0.01
89	SLD 8	14	-420	2370	16.41	12.91	-0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
89	SLD 9	-13	221	2407	-9.5	-11.39	-0.01
89	SLD 10	-13	221	2407	-9.5	-11.39	-0.01
89	SLD 11	21	-361	2246	14.1	7.77	0
89	SLD 12	21	-361	2246	14.1	7.77	0
89	SLD 13	6	86	2206	-3.94	-10.68	0.01
89	SLD 14	6	86	2206	-3.94	-10.68	0.01
89	SLD 15	17	-89	2158	3.14	-4.93	0.02
89	SLD 16	17	-89	2158	3.14	-4.93	0.02
89	SLV 1	-39	-126	2965	4.23	14.13	-0.07
89	SLV 2	-39	-126	2965	4.23	14.13	-0.07
89	SLV 3	-13	-536	2846	20.86	28.84	-0.06
89	SLV 4	-13	-536	2846	20.86	28.84	-0.06
89	SLV 5	-51	515	2743	-21.54	-17.53	-0.04
89	SLV 6	-51	515	2743	-21.54	-17.53	-0.04
89	SLV 7	36	-853	2344	33.9	31.49	-0.01
89	SLV 8	36	-853	2344	33.9	31.49	-0.01
89	SLV 9	-35	653	2433	-26.99	-29.97	-0.01
89	SLV 10	-35	653	2433	-26.99	-29.97	-0.01
89	SLV 11	52	-714	2035	28.45	19.05	0.02
89	SLV 12	52	-714	2035	28.45	19.05	0.02
89	SLV 13	14	337	1932	-13.95	-27.31	0.04
89	SLV 14	14	337	1932	-13.95	-27.31	0.04
89	SLV 15	41	-74	1812	2.69	-12.61	0.05
89	SLV 16	41	-74	1812	2.69	-12.61	0.05
90	SLU 1	0	-129	2207	4.91	-0.63	0.01
90	SLU 2	0	-129	2207	4.91	-0.63	0.01
90	SLU 3	0	-129	2207	4.91	-0.63	0.01
90	SLU 4	0	-129	2207	4.91	-0.63	0.01
90	SLU 5	0	-129	2207	4.91	-0.63	0.01
90	SLU 6	0	-129	2207	4.91	-0.63	0.01
90	SLU 7	0	-129	2207	4.91	-0.63	0.01
90	SLU 8	0	-129	2207	4.91	-0.63	0.01
90	SLU 9	0	-129	2207	4.91	-0.63	0.01
90	SLU 10	-1	-181	2685	6.84	-0.89	0.01
90	SLU 11	-1	-181	2685	6.84	-0.89	0.01
90	SLU 12	-1	-181	2685	6.84	-0.89	0.01
90	SLU 13	-1	-181	2685	6.84	-0.89	0.01
90	SLU 14	-1	-181	2685	6.84	-0.89	0.01
90	SLU 15	-1	-181	2685	6.84	-0.89	0.01
90	SLU 16	-1	-181	2685	6.84	-0.89	0.01
90	SLU 17	-1	-181	2685	6.84	-0.89	0.01
90	SLU 18	-1	-203	2890	7.66	-1	0.01
90	SLU 19	-1	-203	2890	7.66	-1	0.01
90	SLU 20	-1	-203	2890	7.66	-1	0.01
90	SLU 21	-1	-203	2890	7.66	-1	0.01
90	SLU 22	-1	-159	2462	6	-0.79	0.01
90	SLU 23	-1	-159	2462	6	-0.79	0.01
90	SLU 24	-1	-159	2462	6	-0.79	0.01
90	SLU 25	-1	-159	2462	6	-0.79	0.01
90	SLU 26	-1	-159	2462	6	-0.79	0.01
90	SLU 27	-1	-159	2462	6	-0.79	0.01
90	SLU 28	-1	-159	2462	6	-0.79	0.01
90	SLU 29	-1	-159	2462	6	-0.79	0.01
90	SLU 30	-1	-159	2462	6	-0.79	0.01
90	SLU 31	-1	-210	2941	7.92	-1.05	0.01
90	SLU 32	-1	-210	2941	7.92	-1.05	0.01
90	SLU 33	-1	-210	2941	7.92	-1.05	0.01
90	SLU 34	-1	-210	2941	7.92	-1.05	0.01
90	SLU 35	-1	-210	2941	7.92	-1.05	0.01
90	SLU 36	-1	-210	2941	7.92	-1.05	0.01
90	SLU 37	-1	-210	2941	7.92	-1.05	0.01
90	SLU 38	-1	-210	2941	7.92	-1.05	0.01
90	SLU 39	-1	-232	3146	8.75	-1.16	0.01
90	SLU 40	-1	-232	3146	8.75	-1.16	0.01
90	SLU 41	-1	-232	3146	8.75	-1.16	0.01
90	SLU 42	-1	-232	3146	8.75	-1.16	0.01
90	SLU 43	-1	-158	2781	6.01	-0.77	0.01
90	SLU 44	-1	-158	2781	6.01	-0.77	0.01
90	SLU 45	-1	-158	2781	6.01	-0.77	0.01
90	SLU 46	-1	-158	2781	6.01	-0.77	0.01
90	SLU 47	-1	-158	2781	6.01	-0.77	0.01
90	SLU 48	-1	-158	2781	6.01	-0.77	0.01
90	SLU 49	-1	-158	2781	6.01	-0.77	0.01
90	SLU 50	-1	-158	2781	6.01	-0.77	0.01
90	SLU 51	-1	-158	2781	6.01	-0.77	0.01
90	SLU 52	-1	-209	3260	7.94	-1.03	0.01
90	SLU 53	-1	-209	3260	7.94	-1.03	0.01
90	SLU 54	-1	-209	3260	7.94	-1.03	0.01
90	SLU 55	-1	-209	3260	7.94	-1.03	0.01
90	SLU 56	-1	-209	3260	7.94	-1.03	0.01
90	SLU 57	-1	-209	3260	7.94	-1.03	0.01
90	SLU 58	-1	-209	3260	7.94	-1.03	0.01
90	SLU 59	-1	-209	3260	7.94	-1.03	0.01
90	SLU 60	-1	-231	3465	8.76	-1.14	0.01
90	SLU 61	-1	-231	3465	8.76	-1.14	0.01
90	SLU 62	-1	-231	3465	8.76	-1.14	0.01
90	SLU 63	-1	-231	3465	8.76	-1.14	0.01
90	SLU 64	-1	-188	3037	7.1	-0.92	0.01
90	SLU 65	-1	-188	3037	7.1	-0.92	0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
90	SLU 66	-1	-188	3037	7.1	-0.92	0.01
90	SLU 67	-1	-188	3037	7.1	-0.92	0.01
90	SLU 68	-1	-188	3037	7.1	-0.92	0.01
90	SLU 69	-1	-188	3037	7.1	-0.92	0.01
90	SLU 70	-1	-188	3037	7.1	-0.92	0.01
90	SLU 71	-1	-188	3037	7.1	-0.92	0.01
90	SLU 72	-1	-188	3037	7.1	-0.92	0.01
90	SLU 73	-1	-239	3515	9.02	-1.18	0.01
90	SLU 74	-1	-239	3515	9.02	-1.18	0.01
90	SLU 75	-1	-239	3515	9.02	-1.18	0.01
90	SLU 76	-1	-239	3515	9.02	-1.18	0.01
90	SLU 77	-1	-239	3515	9.02	-1.18	0.01
90	SLU 78	-1	-239	3515	9.02	-1.18	0.01
90	SLU 79	-1	-239	3515	9.02	-1.18	0.01
90	SLU 80	-1	-239	3515	9.02	-1.18	0.01
90	SLU 81	-1	-261	3720	9.85	-1.29	0.01
90	SLU 82	-1	-261	3720	9.85	-1.29	0.01
90	SLU 83	-1	-261	3720	9.85	-1.29	0.01
90	SLU 84	-1	-261	3720	9.85	-1.29	0.01
90	SLE RA 1	-1	-138	2280	5.22	-0.68	0.01
90	SLE RA 2	-1	-138	2280	5.22	-0.68	0.01
90	SLE RA 3	-1	-138	2280	5.22	-0.68	0.01
90	SLE RA 4	-1	-138	2280	5.22	-0.68	0.01
90	SLE RA 5	-1	-138	2280	5.22	-0.68	0.01
90	SLE RA 6	-1	-138	2280	5.22	-0.68	0.01
90	SLE RA 7	-1	-138	2280	5.22	-0.68	0.01
90	SLE RA 8	-1	-138	2280	5.22	-0.68	0.01
90	SLE RA 9	-1	-138	2280	5.22	-0.68	0.01
90	SLE RA 10	-1	-172	2599	6.51	-0.85	0.01
90	SLE RA 11	-1	-172	2599	6.51	-0.85	0.01
90	SLE RA 12	-1	-172	2599	6.51	-0.85	0.01
90	SLE RA 13	-1	-172	2599	6.51	-0.85	0.01
90	SLE RA 14	-1	-172	2599	6.51	-0.85	0.01
90	SLE RA 15	-1	-172	2599	6.51	-0.85	0.01
90	SLE RA 16	-1	-172	2599	6.51	-0.85	0.01
90	SLE RA 17	-1	-172	2599	6.51	-0.85	0.01
90	SLE RA 18	-1	-187	2736	7.06	-0.92	0.01
90	SLE RA 19	-1	-187	2736	7.06	-0.92	0.01
90	SLE RA 20	-1	-187	2736	7.06	-0.92	0.01
90	SLE RA 21	-1	-187	2736	7.06	-0.92	0.01
90	SLE FR 1	-1	-138	2280	5.22	-0.68	0.01
90	SLE FR 2	-1	-138	2280	5.22	-0.68	0.01
90	SLE FR 3	-1	-138	2280	5.22	-0.68	0.01
90	SLE FR 4	-1	-152	2417	5.77	-0.75	0.01
90	SLE FR 5	-1	-152	2417	5.77	-0.75	0.01
90	SLE FR 6	-1	-162	2508	6.14	-0.8	0.01
90	SLE QP 1	-1	-138	2280	5.22	-0.68	0.01
90	SLE QP 2	-1	-152	2417	5.77	-0.75	0.01
90	SLD 1	-3	13	2253	-0.88	12.12	-0.01
90	SLD 2	-3	13	2253	-0.88	12.12	-0.01
90	SLD 3	-20	-147	2297	5.65	2.33	-0.02
90	SLD 4	-20	-147	2297	5.65	2.33	-0.02
90	SLD 5	25	139	2301	-6.12	17.96	0.02
90	SLD 6	25	139	2301	-6.12	17.96	0.02
90	SLD 7	-33	-393	2447	15.63	-14.67	-0.02
90	SLD 8	-33	-393	2447	15.63	-14.67	-0.02
90	SLD 9	32	88	2386	-4.09	13.17	0.03
90	SLD 10	32	88	2386	-4.09	13.17	0.03
90	SLD 11	-26	-444	2532	17.67	-19.45	0
90	SLD 12	-26	-444	2532	17.67	-19.45	0
90	SLD 13	19	-158	2536	5.9	-3.83	0.04
90	SLD 14	19	-158	2536	5.9	-3.83	0.04
90	SLD 15	2	-318	2580	12.42	-13.62	0.03
90	SLD 16	2	-318	2580	12.42	-13.62	0.03
90	SLV 1	-6	236	2028	-9.87	31.29	-0.04
90	SLV 2	-6	236	2028	-9.87	31.29	-0.04
90	SLV 3	-51	-139	2131	5.49	6.21	-0.07
90	SLV 4	-51	-139	2131	5.49	6.21	-0.07
90	SLV 5	65	533	2144	-22.21	46.89	0.03
90	SLV 6	65	533	2144	-22.21	46.89	0.03
90	SLV 7	-83	-717	2487	28.98	-36.69	-0.05
90	SLV 8	-83	-717	2487	28.98	-36.69	-0.05
90	SLV 9	82	412	2346	-17.44	35.19	0.07
90	SLV 10	82	412	2346	-17.44	35.19	0.07
90	SLV 11	-67	-838	2689	33.76	-48.39	-0.02
90	SLV 12	-67	-838	2689	33.76	-48.39	-0.02
90	SLV 13	49	-166	2702	6.05	-7.71	0.08
90	SLV 14	49	-166	2702	6.05	-7.71	0.08
90	SLV 15	5	-541	2805	21.41	-32.79	0.06
90	SLV 16	5	-541	2805	21.41	-32.79	0.06
91	SLU 1	0	1	993	0.02	0	0
91	SLU 2	0	1	993	0.02	0	0
91	SLU 3	0	1	993	0.02	0	0
91	SLU 4	0	1	993	0.02	0	0
91	SLU 5	0	1	993	0.02	0	0
91	SLU 6	0	1	993	0.02	0	0
91	SLU 7	0	1	993	0.02	0	0
91	SLU 8	0	1	993	0.02	0	0
91	SLU 9	0	1	993	0.02	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
91	SLU 10	0	1	1452	0.01	0	0
91	SLU 11	0	1	1452	0.01	0	0
91	SLU 12	0	1	1452	0.01	0	0
91	SLU 13	0	1	1452	0.01	0	0
91	SLU 14	0	1	1452	0.01	0	0
91	SLU 15	0	1	1452	0.01	0	0
91	SLU 16	0	1	1452	0.01	0	0
91	SLU 17	0	1	1452	0.01	0	0
91	SLU 18	0	1	1649	0.01	0	0
91	SLU 19	0	1	1649	0.01	0	0
91	SLU 20	0	1	1649	0.01	0	0
91	SLU 21	0	1	1649	0.01	0	0
91	SLU 22	0	1	1215	0.01	0	0
91	SLU 23	0	1	1215	0.01	0	0
91	SLU 24	0	1	1215	0.01	0	0
91	SLU 25	0	1	1215	0.01	0	0
91	SLU 26	0	1	1215	0.01	0	0
91	SLU 27	0	1	1215	0.01	0	0
91	SLU 28	0	1	1215	0.01	0	0
91	SLU 29	0	1	1215	0.01	0	0
91	SLU 30	0	1	1215	0.01	0	0
91	SLU 31	0	1	1674	0.01	0	0
91	SLU 32	0	1	1674	0.01	0	0
91	SLU 33	0	1	1674	0.01	0	0
91	SLU 34	0	1	1674	0.01	0	0
91	SLU 35	0	1	1674	0.01	0	0
91	SLU 36	0	1	1674	0.01	0	0
91	SLU 37	0	1	1674	0.01	0	0
91	SLU 38	0	1	1674	0.01	0	0
91	SLU 39	0	1	1871	0.01	0	0
91	SLU 40	0	1	1871	0.01	0	0
91	SLU 41	0	1	1871	0.01	0	0
91	SLU 42	0	1	1871	0.01	0	0
91	SLU 43	0	1	1214	0.02	0	0
91	SLU 44	0	1	1214	0.02	0	0
91	SLU 45	0	1	1214	0.02	0	0
91	SLU 46	0	1	1214	0.02	0	0
91	SLU 47	0	1	1214	0.02	0	0
91	SLU 48	0	1	1214	0.02	0	0
91	SLU 49	0	1	1214	0.02	0	0
91	SLU 50	0	1	1214	0.02	0	0
91	SLU 51	0	1	1214	0.02	0	0
91	SLU 52	0	1	1674	0.02	0	0
91	SLU 53	0	1	1674	0.02	0	0
91	SLU 54	0	1	1674	0.02	0	0
91	SLU 55	0	1	1674	0.02	0	0
91	SLU 56	0	1	1674	0.02	0	0
91	SLU 57	0	1	1674	0.02	0	0
91	SLU 58	0	1	1674	0.02	0	0
91	SLU 59	0	1	1674	0.02	0	0
91	SLU 60	0	1	1870	0.02	0	0
91	SLU 61	0	1	1870	0.02	0	0
91	SLU 62	0	1	1870	0.02	0	0
91	SLU 63	0	1	1870	0.02	0	0
91	SLU 64	0	1	1437	0.02	0	0
91	SLU 65	0	1	1437	0.02	0	0
91	SLU 66	0	1	1437	0.02	0	0
91	SLU 67	0	1	1437	0.02	0	0
91	SLU 68	0	1	1437	0.02	0	0
91	SLU 69	0	1	1437	0.02	0	0
91	SLU 70	0	1	1437	0.02	0	0
91	SLU 71	0	1	1437	0.02	0	0
91	SLU 72	0	1	1437	0.02	0	0
91	SLU 73	0	1	1896	0.02	0	0
91	SLU 74	0	1	1896	0.02	0	0
91	SLU 75	0	1	1896	0.02	0	0
91	SLU 76	0	1	1896	0.02	0	0
91	SLU 77	0	1	1896	0.02	0	0
91	SLU 78	0	1	1896	0.02	0	0
91	SLU 79	0	1	1896	0.02	0	0
91	SLU 80	0	1	1896	0.02	0	0
91	SLU 81	0	2	2092	0.01	0	0
91	SLU 82	0	2	2092	0.01	0	0
91	SLU 83	0	2	2092	0.01	0	0
91	SLU 84	0	2	2092	0.01	0	0
91	SLE RA 1	0	1	1056	0.02	0	0
91	SLE RA 2	0	1	1056	0.02	0	0
91	SLE RA 3	0	1	1056	0.02	0	0
91	SLE RA 4	0	1	1056	0.02	0	0
91	SLE RA 5	0	1	1056	0.02	0	0
91	SLE RA 6	0	1	1056	0.02	0	0
91	SLE RA 7	0	1	1056	0.02	0	0
91	SLE RA 8	0	1	1056	0.02	0	0
91	SLE RA 9	0	1	1056	0.02	0	0
91	SLE RA 10	0	1	1362	0.01	0	0
91	SLE RA 11	0	1	1362	0.01	0	0
91	SLE RA 12	0	1	1362	0.01	0	0
91	SLE RA 13	0	1	1362	0.01	0	0
91	SLE RA 14	0	1	1362	0.01	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
91	SLE RA 15	0	1	1362	0.01	0	0
91	SLE RA 16	0	1	1362	0.01	0	0
91	SLE RA 17	0	1	1362	0.01	0	0
91	SLE RA 18	0	1	1493	0.01	0	0
91	SLE RA 19	0	1	1493	0.01	0	0
91	SLE RA 20	0	1	1493	0.01	0	0
91	SLE RA 21	0	1	1493	0.01	0	0
91	SLE FR 1	0	1	1056	0.02	0	0
91	SLE FR 2	0	1	1056	0.02	0	0
91	SLE FR 3	0	1	1056	0.02	0	0
91	SLE FR 4	0	1	1187	0.01	0	0
91	SLE FR 5	0	1	1187	0.01	0	0
91	SLE FR 6	0	1	1275	0.01	0	0
91	SLE QP 1	0	1	1056	0.02	0	0
91	SLE QP 2	0	1	1187	0.01	0	0
91	SLD 1	-3	-15	1230	-4.74	2.34	0.06
91	SLD 2	-3	-15	1230	-4.74	2.34	0.06
91	SLD 3	-2	33	1173	8.8	4.89	0.03
91	SLD 4	-2	33	1173	8.8	4.89	0.03
91	SLD 5	-3	-76	1287	-21.95	-3.17	0.06
91	SLD 6	-3	-76	1287	-21.95	-3.17	0.06
91	SLD 7	1	83	1097	23.19	5.33	-0.03
91	SLD 8	1	83	1097	23.19	5.33	-0.03
91	SLD 9	-1	-81	1278	-23.16	-5.34	0.03
91	SLD 10	-1	-81	1278	-23.16	-5.34	0.03
91	SLD 11	3	78	1088	21.98	3.16	-0.06
91	SLD 12	3	78	1088	21.98	3.16	-0.06
91	SLD 13	2	-32	1202	-8.78	-4.9	-0.03
91	SLD 14	2	-32	1202	-8.78	-4.9	-0.03
91	SLD 15	3	16	1145	4.76	-2.35	-0.06
91	SLD 16	3	16	1145	4.76	-2.35	-0.06
91	SLV 1	-8	-39	1296	-12.17	5.8	0.15
91	SLV 2	-8	-39	1296	-12.17	5.8	0.15
91	SLV 3	-5	83	1150	22.56	12.34	0.08
91	SLV 4	-5	83	1150	22.56	12.34	0.08
91	SLV 5	-7	-197	1441	-56.33	-8.18	0.15
91	SLV 6	-7	-197	1441	-56.33	-8.18	0.15
91	SLV 7	4	211	955	59.46	13.62	-0.08
91	SLV 8	4	211	955	59.46	13.62	-0.08
91	SLV 9	-4	-210	1420	-59.43	-13.62	0.08
91	SLV 10	-4	-210	1420	-59.43	-13.62	0.08
91	SLV 11	7	199	934	56.35	8.17	-0.15
91	SLV 12	7	199	934	56.35	8.17	-0.15
91	SLV 13	5	-82	1225	-22.54	-12.35	-0.07
91	SLV 14	5	-82	1225	-22.54	-12.35	-0.07
91	SLV 15	8	41	1079	12.2	-5.81	-0.14
91	SLV 16	8	41	1079	12.2	-5.81	-0.14
92	SLU 1	0	-101	2122	3.99	0.32	0
92	SLU 2	0	-101	2122	3.99	0.32	0
92	SLU 3	0	-101	2122	3.99	0.32	0
92	SLU 4	0	-101	2122	3.99	0.32	0
92	SLU 5	0	-101	2122	3.99	0.32	0
92	SLU 6	0	-101	2122	3.99	0.32	0
92	SLU 7	0	-101	2122	3.99	0.32	0
92	SLU 8	0	-101	2122	3.99	0.32	0
92	SLU 9	0	-101	2122	3.99	0.32	0
92	SLU 10	0	-136	2610	5.4	0.5	0
92	SLU 11	0	-136	2610	5.4	0.5	0
92	SLU 12	0	-136	2610	5.4	0.5	0
92	SLU 13	0	-136	2610	5.4	0.5	0
92	SLU 14	0	-136	2610	5.4	0.5	0
92	SLU 15	0	-136	2610	5.4	0.5	0
92	SLU 16	0	-136	2610	5.4	0.5	0
92	SLU 17	0	-136	2610	5.4	0.5	0
92	SLU 18	0	-151	2818	6.01	0.58	0
92	SLU 19	0	-151	2818	6.01	0.58	0
92	SLU 20	0	-151	2818	6.01	0.58	0
92	SLU 21	0	-151	2818	6.01	0.58	0
92	SLU 22	0	-123	2382	4.85	0.41	0
92	SLU 23	0	-123	2382	4.85	0.41	0
92	SLU 24	0	-123	2382	4.85	0.41	0
92	SLU 25	0	-123	2382	4.85	0.41	0
92	SLU 26	0	-123	2382	4.85	0.41	0
92	SLU 27	0	-123	2382	4.85	0.41	0
92	SLU 28	0	-123	2382	4.85	0.41	0
92	SLU 29	0	-123	2382	4.85	0.41	0
92	SLU 30	0	-123	2382	4.85	0.41	0
92	SLU 31	0	-158	2869	6.27	0.59	0
92	SLU 32	0	-158	2869	6.27	0.59	0
92	SLU 33	0	-158	2869	6.27	0.59	0
92	SLU 34	0	-158	2869	6.27	0.59	0
92	SLU 35	0	-158	2869	6.27	0.59	0
92	SLU 36	0	-158	2869	6.27	0.59	0
92	SLU 37	0	-158	2869	6.27	0.59	0
92	SLU 38	0	-158	2869	6.27	0.59	0
92	SLU 39	0	-173	3078	6.87	0.67	0
92	SLU 40	0	-173	3078	6.87	0.67	0
92	SLU 41	0	-173	3078	6.87	0.67	0
92	SLU 42	0	-173	3078	6.87	0.67	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
92	SLU 43	0	-124	2670	4.89	0.39	0
92	SLU 44	0	-124	2670	4.89	0.39	0
92	SLU 45	0	-124	2670	4.89	0.39	0
92	SLU 46	0	-124	2670	4.89	0.39	0
92	SLU 47	0	-124	2670	4.89	0.39	0
92	SLU 48	0	-124	2670	4.89	0.39	0
92	SLU 49	0	-124	2670	4.89	0.39	0
92	SLU 50	0	-124	2670	4.89	0.39	0
92	SLU 51	0	-124	2670	4.89	0.39	0
92	SLU 52	0	-159	3157	6.3	0.57	0
92	SLU 53	0	-159	3157	6.3	0.57	0
92	SLU 54	0	-159	3157	6.3	0.57	0
92	SLU 55	0	-159	3157	6.3	0.57	0
92	SLU 56	0	-159	3157	6.3	0.57	0
92	SLU 57	0	-159	3157	6.3	0.57	0
92	SLU 58	0	-159	3157	6.3	0.57	0
92	SLU 59	0	-159	3157	6.3	0.57	0
92	SLU 60	0	-174	3366	6.91	0.64	0
92	SLU 61	0	-174	3366	6.91	0.64	0
92	SLU 62	0	-174	3366	6.91	0.64	0
92	SLU 63	0	-174	3366	6.91	0.64	0
92	SLU 64	0	-146	2930	5.75	0.48	0
92	SLU 65	0	-146	2930	5.75	0.48	0
92	SLU 66	0	-146	2930	5.75	0.48	0
92	SLU 67	0	-146	2930	5.75	0.48	0
92	SLU 68	0	-146	2930	5.75	0.48	0
92	SLU 69	0	-146	2930	5.75	0.48	0
92	SLU 70	0	-146	2930	5.75	0.48	0
92	SLU 71	0	-146	2930	5.75	0.48	0
92	SLU 72	0	-146	2930	5.75	0.48	0
92	SLU 73	0	-181	3417	7.17	0.66	0
92	SLU 74	0	-181	3417	7.17	0.66	0
92	SLU 75	0	-181	3417	7.17	0.66	0
92	SLU 76	0	-181	3417	7.17	0.66	0
92	SLU 77	0	-181	3417	7.17	0.66	0
92	SLU 78	0	-181	3417	7.17	0.66	0
92	SLU 79	0	-181	3417	7.17	0.66	0
92	SLU 80	0	-181	3417	7.17	0.66	0
92	SLU 81	0	-196	3626	7.77	0.73	0
92	SLU 82	0	-196	3626	7.77	0.73	0
92	SLU 83	0	-196	3626	7.77	0.73	0
92	SLU 84	0	-196	3626	7.77	0.73	0
92	SLE RA 1	0	-107	2197	4.24	0.35	0
92	SLE RA 2	0	-107	2197	4.24	0.35	0
92	SLE RA 3	0	-107	2197	4.24	0.35	0
92	SLE RA 4	0	-107	2197	4.24	0.35	0
92	SLE RA 5	0	-107	2197	4.24	0.35	0
92	SLE RA 6	0	-107	2197	4.24	0.35	0
92	SLE RA 7	0	-107	2197	4.24	0.35	0
92	SLE RA 8	0	-107	2197	4.24	0.35	0
92	SLE RA 9	0	-107	2197	4.24	0.35	0
92	SLE RA 10	0	-131	2521	5.18	0.47	0
92	SLE RA 11	0	-131	2521	5.18	0.47	0
92	SLE RA 12	0	-131	2521	5.18	0.47	0
92	SLE RA 13	0	-131	2521	5.18	0.47	0
92	SLE RA 14	0	-131	2521	5.18	0.47	0
92	SLE RA 15	0	-131	2521	5.18	0.47	0
92	SLE RA 16	0	-131	2521	5.18	0.47	0
92	SLE RA 17	0	-131	2521	5.18	0.47	0
92	SLE RA 18	0	-141	2661	5.58	0.52	0
92	SLE RA 19	0	-141	2661	5.58	0.52	0
92	SLE RA 20	0	-141	2661	5.58	0.52	0
92	SLE RA 21	0	-141	2661	5.58	0.52	0
92	SLE FR 1	0	-107	2197	4.24	0.35	0
92	SLE FR 2	0	-107	2197	4.24	0.35	0
92	SLE FR 3	0	-107	2197	4.24	0.35	0
92	SLE FR 4	0	-117	2336	4.64	0.4	0
92	SLE FR 5	0	-117	2336	4.64	0.4	0
92	SLE FR 6	0	-124	2429	4.91	0.43	0
92	SLE QP 1	0	-107	2197	4.24	0.35	0
92	SLE QP 2	0	-117	2336	4.64	0.4	0
92	SLD 1	-22	-124	2592	4.91	11.28	-0.03
92	SLD 2	-22	-124	2592	4.91	11.28	-0.03
92	SLD 3	-12	-299	2525	11.86	17.69	-0.02
92	SLD 4	-12	-299	2525	11.86	17.69	-0.02
92	SLD 5	-21	145	2514	-5.83	-6.06	-0.01
92	SLD 6	-21	145	2514	-5.83	-6.06	-0.01
92	SLD 7	11	-437	2291	17.36	15.31	0
92	SLD 8	11	-437	2291	17.36	15.31	0
92	SLD 9	-11	202	2381	-8.08	-14.51	0
92	SLD 10	-11	202	2381	-8.08	-14.51	0
92	SLD 11	21	-380	2157	15.11	6.86	0.01
92	SLD 12	21	-380	2157	15.11	6.86	0.01
92	SLD 13	13	64	2146	-2.58	-16.89	0.02
92	SLD 14	13	64	2146	-2.58	-16.89	0.02
92	SLD 15	22	-111	2079	4.37	-10.48	0.02
92	SLD 16	22	-111	2079	4.37	-10.48	0.02
92	SLV 1	-53	-135	2984	5.3	25.96	-0.06
92	SLV 2	-53	-135	2984	5.3	25.96	-0.06



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
92	SLV 3	-28	-544	2817	21.63	42.35	-0.05
92	SLV 4	-28	-544	2817	21.63	42.35	-0.05
92	SLV 5	-52	499	2782	-19.92	-16.79	-0.03
92	SLV 6	-52	499	2782	-19.92	-16.79	-0.03
92	SLV 7	29	-867	2228	34.5	37.85	0
92	SLV 8	29	-867	2228	34.5	37.85	0
92	SLV 9	-28	632	2444	-25.22	-37.05	0
92	SLV 10	-28	632	2444	-25.22	-37.05	0
92	SLV 11	53	-734	1889	29.2	17.59	0.03
92	SLV 12	53	-734	1889	29.2	17.59	0.03
92	SLV 13	29	310	1854	-12.35	-41.55	0.05
92	SLV 14	29	310	1854	-12.35	-41.55	0.05
92	SLV 15	53	-100	1688	3.98	-25.16	0.06
92	SLV 16	53	-100	1688	3.98	-25.16	0.06
93	SLU 1	0	-179	2077	6.16	-0.31	0
93	SLU 2	0	-179	2077	6.16	-0.31	0
93	SLU 3	0	-179	2077	6.16	-0.31	0
93	SLU 4	0	-179	2077	6.16	-0.31	0
93	SLU 5	0	-179	2077	6.16	-0.31	0
93	SLU 6	0	-179	2077	6.16	-0.31	0
93	SLU 7	0	-179	2077	6.16	-0.31	0
93	SLU 8	0	-179	2077	6.16	-0.31	0
93	SLU 9	0	-179	2077	6.16	-0.31	0
93	SLU 10	0	-246	2510	8.51	-0.45	0
93	SLU 11	0	-246	2510	8.51	-0.45	0
93	SLU 12	0	-246	2510	8.51	-0.45	0
93	SLU 13	0	-246	2510	8.51	-0.45	0
93	SLU 14	0	-246	2510	8.51	-0.45	0
93	SLU 15	0	-246	2510	8.51	-0.45	0
93	SLU 16	0	-246	2510	8.51	-0.45	0
93	SLU 17	0	-246	2510	8.51	-0.45	0
93	SLU 18	0	-274	2696	9.51	-0.5	0
93	SLU 19	0	-274	2696	9.51	-0.5	0
93	SLU 20	0	-274	2696	9.51	-0.5	0
93	SLU 21	0	-274	2696	9.51	-0.5	0
93	SLU 22	0	-215	2306	7.44	-0.39	0
93	SLU 23	0	-215	2306	7.44	-0.39	0
93	SLU 24	0	-215	2306	7.44	-0.39	0
93	SLU 25	0	-215	2306	7.44	-0.39	0
93	SLU 26	0	-215	2306	7.44	-0.39	0
93	SLU 27	0	-215	2306	7.44	-0.39	0
93	SLU 28	0	-215	2306	7.44	-0.39	0
93	SLU 29	0	-215	2306	7.44	-0.39	0
93	SLU 30	0	-215	2306	7.44	-0.39	0
93	SLU 31	0	-282	2739	9.79	-0.52	0
93	SLU 32	0	-282	2739	9.79	-0.52	0
93	SLU 33	0	-282	2739	9.79	-0.52	0
93	SLU 34	0	-282	2739	9.79	-0.52	0
93	SLU 35	0	-282	2739	9.79	-0.52	0
93	SLU 36	0	-282	2739	9.79	-0.52	0
93	SLU 37	0	-282	2739	9.79	-0.52	0
93	SLU 38	0	-282	2739	9.79	-0.52	0
93	SLU 39	0	-310	2925	10.79	-0.58	0
93	SLU 40	0	-310	2925	10.79	-0.58	0
93	SLU 41	0	-310	2925	10.79	-0.58	0
93	SLU 42	0	-310	2925	10.79	-0.58	0
93	SLU 43	0	-221	2622	7.57	-0.38	0
93	SLU 44	0	-221	2622	7.57	-0.38	0
93	SLU 45	0	-221	2622	7.57	-0.38	0
93	SLU 46	0	-221	2622	7.57	-0.38	0
93	SLU 47	0	-221	2622	7.57	-0.38	0
93	SLU 48	0	-221	2622	7.57	-0.38	0
93	SLU 49	0	-221	2622	7.57	-0.38	0
93	SLU 50	0	-221	2622	7.57	-0.38	0
93	SLU 51	0	-221	2622	7.57	-0.38	0
93	SLU 52	0	-287	3055	9.92	-0.51	0
93	SLU 53	0	-287	3055	9.92	-0.51	0
93	SLU 54	0	-287	3055	9.92	-0.51	0
93	SLU 55	0	-287	3055	9.92	-0.51	0
93	SLU 56	0	-287	3055	9.92	-0.51	0
93	SLU 57	0	-287	3055	9.92	-0.51	0
93	SLU 58	0	-287	3055	9.92	-0.51	0
93	SLU 59	0	-287	3055	9.92	-0.51	0
93	SLU 60	0	-315	3241	10.92	-0.57	0
93	SLU 61	0	-315	3241	10.92	-0.57	0
93	SLU 62	0	-315	3241	10.92	-0.57	0
93	SLU 63	0	-315	3241	10.92	-0.57	0
93	SLU 64	0	-257	2851	8.85	-0.46	0
93	SLU 65	0	-257	2851	8.85	-0.46	0
93	SLU 66	0	-257	2851	8.85	-0.46	0
93	SLU 67	0	-257	2851	8.85	-0.46	0
93	SLU 68	0	-257	2851	8.85	-0.46	0
93	SLU 69	0	-257	2851	8.85	-0.46	0
93	SLU 70	0	-257	2851	8.85	-0.46	0
93	SLU 71	0	-257	2851	8.85	-0.46	0
93	SLU 72	0	-257	2851	8.85	-0.46	0
93	SLU 73	0	-323	3284	11.2	-0.59	0
93	SLU 74	0	-323	3284	11.2	-0.59	0
93	SLU 75	0	-323	3284	11.2	-0.59	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
93	SLU 76	0	-323	3284	11.2	-0.59	0
93	SLU 77	0	-323	3284	11.2	-0.59	0
93	SLU 78	0	-323	3284	11.2	-0.59	0
93	SLU 79	0	-323	3284	11.2	-0.59	0
93	SLU 80	0	-323	3284	11.2	-0.59	0
93	SLU 81	0	-351	3470	12.2	-0.65	0
93	SLU 82	0	-351	3470	12.2	-0.65	0
93	SLU 83	0	-351	3470	12.2	-0.65	0
93	SLU 84	0	-351	3470	12.2	-0.65	0
93	SLE RA 1	0	-190	2143	6.53	-0.34	0
93	SLE RA 2	0	-190	2143	6.53	-0.34	0
93	SLE RA 3	0	-190	2143	6.53	-0.34	0
93	SLE RA 4	0	-190	2143	6.53	-0.34	0
93	SLE RA 5	0	-190	2143	6.53	-0.34	0
93	SLE RA 6	0	-190	2143	6.53	-0.34	0
93	SLE RA 7	0	-190	2143	6.53	-0.34	0
93	SLE RA 8	0	-190	2143	6.53	-0.34	0
93	SLE RA 9	0	-190	2143	6.53	-0.34	0
93	SLE RA 10	0	-234	2431	8.09	-0.42	0
93	SLE RA 11	0	-234	2431	8.09	-0.42	0
93	SLE RA 12	0	-234	2431	8.09	-0.42	0
93	SLE RA 13	0	-234	2431	8.09	-0.42	0
93	SLE RA 14	0	-234	2431	8.09	-0.42	0
93	SLE RA 15	0	-234	2431	8.09	-0.42	0
93	SLE RA 16	0	-234	2431	8.09	-0.42	0
93	SLE RA 17	0	-234	2431	8.09	-0.42	0
93	SLE RA 18	0	-253	2555	8.76	-0.46	0
93	SLE RA 19	0	-253	2555	8.76	-0.46	0
93	SLE RA 20	0	-253	2555	8.76	-0.46	0
93	SLE RA 21	0	-253	2555	8.76	-0.46	0
93	SLE FR 1	0	-190	2143	6.53	-0.34	0
93	SLE FR 2	0	-190	2143	6.53	-0.34	0
93	SLE FR 3	0	-190	2143	6.53	-0.34	0
93	SLE FR 4	0	-209	2266	7.2	-0.37	0
93	SLE FR 5	0	-209	2266	7.2	-0.37	0
93	SLE FR 6	0	-221	2349	7.64	-0.4	0
93	SLE QP 1	0	-190	2143	6.53	-0.34	0
93	SLE QP 2	0	-209	2266	7.2	-0.37	0
93	SLD 1	21	-43	2129	0.43	20.87	-0.01
93	SLD 2	21	-43	2129	0.43	20.87	-0.01
93	SLD 3	6	-205	2186	7.09	10.19	-0.02
93	SLD 4	6	-205	2186	7.09	10.19	-0.02
93	SLD 5	30	87	2138	-4.93	22.19	0.01
93	SLD 6	30	87	2138	-4.93	22.19	0.01
93	SLD 7	-22	-453	2329	17.26	-13.4	-0.02
93	SLD 8	-22	-453	2329	17.26	-13.4	-0.02
93	SLD 9	21	36	2204	-2.87	12.65	0.02
93	SLD 10	21	36	2204	-2.87	12.65	0.02
93	SLD 11	-30	-504	2394	19.32	-22.94	-0.01
93	SLD 12	-30	-504	2394	19.32	-22.94	-0.01
93	SLD 13	-6	-212	2347	7.31	-10.94	0.02
93	SLD 14	-6	-212	2347	7.31	-10.94	0.02
93	SLD 15	-22	-374	2404	13.96	-21.62	0.01
93	SLD 16	-22	-374	2404	13.96	-21.62	0.01
93	SLV 1	52	181	1940	-8.69	52.28	-0.03
93	SLV 2	52	181	1940	-8.69	52.28	-0.03
93	SLV 3	13	-200	2075	6.95	24.94	-0.06
93	SLV 4	13	-200	2075	6.95	24.94	-0.06
93	SLV 5	75	487	1964	-21.29	56.89	0.03
93	SLV 6	75	487	1964	-21.29	56.89	0.03
93	SLV 7	-56	-784	2414	30.84	-34.25	-0.06
93	SLV 8	-56	-784	2414	30.84	-34.25	-0.06
93	SLV 9	56	367	2119	-16.45	33.5	0.06
93	SLV 10	56	367	2119	-16.45	33.5	0.06
93	SLV 11	-76	-904	2569	35.69	-57.64	-0.03
93	SLV 12	-76	-904	2569	35.69	-57.64	-0.03
93	SLV 13	-13	-217	2457	7.45	-25.69	0.06
93	SLV 14	-13	-217	2457	7.45	-25.69	0.06
93	SLV 15	-53	-598	2592	23.09	-53.03	0.03
93	SLV 16	-53	-598	2592	23.09	-53.03	0.03
94	SLU 1	0	0	1233	0.03	0	0
94	SLU 2	0	0	1233	0.03	0	0
94	SLU 3	0	0	1233	0.03	0	0
94	SLU 4	0	0	1233	0.03	0	0
94	SLU 5	0	0	1233	0.03	0	0
94	SLU 6	0	0	1233	0.03	0	0
94	SLU 7	0	0	1233	0.03	0	0
94	SLU 8	0	0	1233	0.03	0	0
94	SLU 9	0	0	1233	0.03	0	0
94	SLU 10	0	-1	1868	0.02	0	0
94	SLU 11	0	-1	1868	0.02	0	0
94	SLU 12	0	-1	1868	0.02	0	0
94	SLU 13	0	-1	1868	0.02	0	0
94	SLU 14	0	-1	1868	0.02	0	0
94	SLU 15	0	-1	1868	0.02	0	0
94	SLU 16	0	-1	1868	0.02	0	0
94	SLU 17	0	-1	1868	0.02	0	0
94	SLU 18	0	-1	2140	0.02	0	0
94	SLU 19	0	-1	2140	0.02	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
94	SLU 20	0	-1	2140	0.02	0	0
94	SLU 21	0	-1	2140	0.02	0	0
94	SLU 22	0	-1	1532	0.02	0	0
94	SLU 23	0	-1	1532	0.02	0	0
94	SLU 24	0	-1	1532	0.02	0	0
94	SLU 25	0	-1	1532	0.02	0	0
94	SLU 26	0	-1	1532	0.02	0	0
94	SLU 27	0	-1	1532	0.02	0	0
94	SLU 28	0	-1	1532	0.02	0	0
94	SLU 29	0	-1	1532	0.02	0	0
94	SLU 30	0	-1	1532	0.02	0	0
94	SLU 31	0	-1	2168	0.01	0	0
94	SLU 32	0	-1	2168	0.01	0	0
94	SLU 33	0	-1	2168	0.01	0	0
94	SLU 34	0	-1	2168	0.01	0	0
94	SLU 35	0	-1	2168	0.01	0	0
94	SLU 36	0	-1	2168	0.01	0	0
94	SLU 37	0	-1	2168	0.01	0	0
94	SLU 38	0	-1	2168	0.01	0	0
94	SLU 39	0	-1	2440	0.01	0	0
94	SLU 40	0	-1	2440	0.01	0	0
94	SLU 41	0	-1	2440	0.01	0	0
94	SLU 42	0	-1	2440	0.01	0	0
94	SLU 43	0	0	1500	0.04	0	0
94	SLU 44	0	0	1500	0.04	0	0
94	SLU 45	0	0	1500	0.04	0	0
94	SLU 46	0	0	1500	0.04	0	0
94	SLU 47	0	0	1500	0.04	0	0
94	SLU 48	0	0	1500	0.04	0	0
94	SLU 49	0	0	1500	0.04	0	0
94	SLU 50	0	0	1500	0.04	0	0
94	SLU 51	0	0	1500	0.04	0	0
94	SLU 52	0	-1	2135	0.03	0	0
94	SLU 53	0	-1	2135	0.03	0	0
94	SLU 54	0	-1	2135	0.03	0	0
94	SLU 55	0	-1	2135	0.03	0	0
94	SLU 56	0	-1	2135	0.03	0	0
94	SLU 57	0	-1	2135	0.03	0	0
94	SLU 58	0	-1	2135	0.03	0	0
94	SLU 59	0	-1	2135	0.03	0	0
94	SLU 60	0	-1	2408	0.03	0	0
94	SLU 61	0	-1	2408	0.03	0	0
94	SLU 62	0	-1	2408	0.03	0	0
94	SLU 63	0	-1	2408	0.03	0	0
94	SLU 64	0	-1	1800	0.03	0	0
94	SLU 65	0	-1	1800	0.03	0	0
94	SLU 66	0	-1	1800	0.03	0	0
94	SLU 67	0	-1	1800	0.03	0	0
94	SLU 68	0	-1	1800	0.03	0	0
94	SLU 69	0	-1	1800	0.03	0	0
94	SLU 70	0	-1	1800	0.03	0	0
94	SLU 71	0	-1	1800	0.03	0	0
94	SLU 72	0	-1	1800	0.03	0	0
94	SLU 73	0	-1	2435	0.02	0	0
94	SLU 74	0	-1	2435	0.02	0	0
94	SLU 75	0	-1	2435	0.02	0	0
94	SLU 76	0	-1	2435	0.02	0	0
94	SLU 77	0	-1	2435	0.02	0	0
94	SLU 78	0	-1	2435	0.02	0	0
94	SLU 79	0	-1	2435	0.02	0	0
94	SLU 80	0	-1	2435	0.02	0	0
94	SLU 81	0	-1	2707	0.02	0	0
94	SLU 82	0	-1	2707	0.02	0	0
94	SLU 83	0	-1	2707	0.02	0	0
94	SLU 84	0	-1	2707	0.02	0	0
94	SLE RA 1	0	0	1318	0.03	0	0
94	SLE RA 2	0	0	1318	0.03	0	0
94	SLE RA 3	0	0	1318	0.03	0	0
94	SLE RA 4	0	0	1318	0.03	0	0
94	SLE RA 5	0	0	1318	0.03	0	0
94	SLE RA 6	0	0	1318	0.03	0	0
94	SLE RA 7	0	0	1318	0.03	0	0
94	SLE RA 8	0	0	1318	0.03	0	0
94	SLE RA 9	0	0	1318	0.03	0	0
94	SLE RA 10	0	-1	1742	0.02	0	0
94	SLE RA 11	0	-1	1742	0.02	0	0
94	SLE RA 12	0	-1	1742	0.02	0	0
94	SLE RA 13	0	-1	1742	0.02	0	0
94	SLE RA 14	0	-1	1742	0.02	0	0
94	SLE RA 15	0	-1	1742	0.02	0	0
94	SLE RA 16	0	-1	1742	0.02	0	0
94	SLE RA 17	0	-1	1742	0.02	0	0
94	SLE RA 18	0	-1	1923	0.02	0	0
94	SLE RA 19	0	-1	1923	0.02	0	0
94	SLE RA 20	0	-1	1923	0.02	0	0
94	SLE RA 21	0	-1	1923	0.02	0	0
94	SLE FR 1	0	0	1318	0.03	0	0
94	SLE FR 2	0	0	1318	0.03	0	0
94	SLE FR 3	0	0	1318	0.03	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
94	SLE FR 4	0	-1	1500	0.02	0	0
94	SLE FR 5	0	-1	1500	0.02	0	0
94	SLE FR 6	0	-1	1621	0.02	0	0
94	SLE QP 1	0	0	1318	0.03	0	0
94	SLE QP 2	0	-1	1500	0.02	0	0
94	SLD 1	-5	-31	1561	-4.14	7.17	-0.1
94	SLD 2	-5	-31	1561	-4.14	7.17	-0.1
94	SLD 3	-3	57	1476	7.76	3.79	-0.16
94	SLD 4	-3	57	1476	7.76	3.79	-0.16
94	SLD 5	-4	-142	1648	-19.28	7.27	0.05
94	SLD 6	-4	-142	1648	-19.28	7.27	0.05
94	SLD 7	2	149	1363	20.39	-3.98	-0.13
94	SLD 8	2	149	1363	20.39	-3.98	-0.13
94	SLD 9	-2	-151	1637	-20.35	3.98	0.13
94	SLD 10	-2	-151	1637	-20.35	3.98	0.13
94	SLD 11	4	141	1352	19.32	-7.27	-0.05
94	SLD 12	4	141	1352	19.32	-7.27	-0.05
94	SLD 13	3	-58	1524	-7.71	-3.79	0.16
94	SLD 14	3	-58	1524	-7.71	-3.79	0.16
94	SLD 15	5	30	1439	4.19	-7.16	0.1
94	SLD 16	5	30	1439	4.19	-7.16	0.1
94	SLV 1	-13	-78	1655	-10.66	18.12	-0.25
94	SLV 2	-13	-78	1655	-10.66	18.12	-0.25
94	SLV 3	-8	146	1437	19.87	9.47	-0.39
94	SLV 4	-8	146	1437	19.87	9.47	-0.39
94	SLV 5	-11	-364	1878	-49.49	18.56	0.14
94	SLV 6	-11	-364	1878	-49.49	18.56	0.14
94	SLV 7	5	384	1149	52.28	-10.28	-0.33
94	SLV 8	5	384	1149	52.28	-10.28	-0.33
94	SLV 9	-5	-385	1850	-52.24	10.28	0.33
94	SLV 10	-5	-385	1850	-52.24	10.28	0.33
94	SLV 11	11	363	1122	49.53	-18.56	-0.14
94	SLV 12	11	363	1122	49.53	-18.56	-0.14
94	SLV 13	8	-148	1563	-19.82	-9.47	0.39
94	SLV 14	8	-148	1563	-19.82	-9.47	0.39
94	SLV 15	13	77	1345	10.71	-18.12	0.25
94	SLV 16	13	77	1345	10.71	-18.12	0.25
95	SLU 1	0	-117	2093	4.35	0.19	0
95	SLU 2	0	-117	2093	4.35	0.19	0
95	SLU 3	0	-117	2093	4.35	0.19	0
95	SLU 4	0	-117	2093	4.35	0.19	0
95	SLU 5	0	-117	2093	4.35	0.19	0
95	SLU 6	0	-117	2093	4.35	0.19	0
95	SLU 7	0	-117	2093	4.35	0.19	0
95	SLU 8	0	-117	2093	4.35	0.19	0
95	SLU 9	0	-117	2093	4.35	0.19	0
95	SLU 10	0	-156	2579	5.84	0.34	0
95	SLU 11	0	-156	2579	5.84	0.34	0
95	SLU 12	0	-156	2579	5.84	0.34	0
95	SLU 13	0	-156	2579	5.84	0.34	0
95	SLU 14	0	-156	2579	5.84	0.34	0
95	SLU 15	0	-156	2579	5.84	0.34	0
95	SLU 16	0	-156	2579	5.84	0.34	0
95	SLU 17	0	-156	2579	5.84	0.34	0
95	SLU 18	0	-173	2787	6.48	0.4	0
95	SLU 19	0	-173	2787	6.48	0.4	0
95	SLU 20	0	-173	2787	6.48	0.4	0
95	SLU 21	0	-173	2787	6.48	0.4	0
95	SLU 22	0	-140	2346	5.2	0.25	0
95	SLU 23	0	-140	2346	5.2	0.25	0
95	SLU 24	0	-140	2346	5.2	0.25	0
95	SLU 25	0	-140	2346	5.2	0.25	0
95	SLU 26	0	-140	2346	5.2	0.25	0
95	SLU 27	0	-140	2346	5.2	0.25	0
95	SLU 28	0	-140	2346	5.2	0.25	0
95	SLU 29	0	-140	2346	5.2	0.25	0
95	SLU 30	0	-140	2346	5.2	0.25	0
95	SLU 31	0	-179	2832	6.69	0.4	0
95	SLU 32	0	-179	2832	6.69	0.4	0
95	SLU 33	0	-179	2832	6.69	0.4	0
95	SLU 34	0	-179	2832	6.69	0.4	0
95	SLU 35	0	-179	2832	6.69	0.4	0
95	SLU 36	0	-179	2832	6.69	0.4	0
95	SLU 37	0	-179	2832	6.69	0.4	0
95	SLU 38	0	-179	2832	6.69	0.4	0
95	SLU 39	0	-196	3040	7.33	0.47	0
95	SLU 40	0	-196	3040	7.33	0.47	0
95	SLU 41	0	-196	3040	7.33	0.47	0
95	SLU 42	0	-196	3040	7.33	0.47	0
95	SLU 43	0	-145	2634	5.36	0.22	0
95	SLU 44	0	-145	2634	5.36	0.22	0
95	SLU 45	0	-145	2634	5.36	0.22	0
95	SLU 46	0	-145	2634	5.36	0.22	0
95	SLU 47	0	-145	2634	5.36	0.22	0
95	SLU 48	0	-145	2634	5.36	0.22	0
95	SLU 49	0	-145	2634	5.36	0.22	0
95	SLU 50	0	-145	2634	5.36	0.22	0
95	SLU 51	0	-145	2634	5.36	0.22	0
95	SLU 52	0	-184	3120	6.85	0.37	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
95	SLU 53	0	-184	3120	6.85	0.37	0
95	SLU 54	0	-184	3120	6.85	0.37	0
95	SLU 55	0	-184	3120	6.85	0.37	0
95	SLU 56	0	-184	3120	6.85	0.37	0
95	SLU 57	0	-184	3120	6.85	0.37	0
95	SLU 58	0	-184	3120	6.85	0.37	0
95	SLU 59	0	-184	3120	6.85	0.37	0
95	SLU 60	0	-200	3328	7.49	0.44	0
95	SLU 61	0	-200	3328	7.49	0.44	0
95	SLU 62	0	-200	3328	7.49	0.44	0
95	SLU 63	0	-200	3328	7.49	0.44	0
95	SLU 64	0	-168	2887	6.21	0.28	0
95	SLU 65	0	-168	2887	6.21	0.28	0
95	SLU 66	0	-168	2887	6.21	0.28	0
95	SLU 67	0	-168	2887	6.21	0.28	0
95	SLU 68	0	-168	2887	6.21	0.28	0
95	SLU 69	0	-168	2887	6.21	0.28	0
95	SLU 70	0	-168	2887	6.21	0.28	0
95	SLU 71	0	-168	2887	6.21	0.28	0
95	SLU 72	0	-168	2887	6.21	0.28	0
95	SLU 73	0	-207	3373	7.7	0.44	0
95	SLU 74	0	-207	3373	7.7	0.44	0
95	SLU 75	0	-207	3373	7.7	0.44	0
95	SLU 76	0	-207	3373	7.7	0.44	0
95	SLU 77	0	-207	3373	7.7	0.44	0
95	SLU 78	0	-207	3373	7.7	0.44	0
95	SLU 79	0	-207	3373	7.7	0.44	0
95	SLU 80	0	-207	3373	7.7	0.44	0
95	SLU 81	0	-223	3581	8.34	0.5	0
95	SLU 82	0	-223	3581	8.34	0.5	0
95	SLU 83	0	-223	3581	8.34	0.5	0
95	SLU 84	0	-223	3581	8.34	0.5	0
95	SLE RA 1	0	-124	2165	4.59	0.2	0
95	SLE RA 2	0	-124	2165	4.59	0.2	0
95	SLE RA 3	0	-124	2165	4.59	0.2	0
95	SLE RA 4	0	-124	2165	4.59	0.2	0
95	SLE RA 5	0	-124	2165	4.59	0.2	0
95	SLE RA 6	0	-124	2165	4.59	0.2	0
95	SLE RA 7	0	-124	2165	4.59	0.2	0
95	SLE RA 8	0	-124	2165	4.59	0.2	0
95	SLE RA 9	0	-124	2165	4.59	0.2	0
95	SLE RA 10	0	-150	2489	5.59	0.31	0
95	SLE RA 11	0	-150	2489	5.59	0.31	0
95	SLE RA 12	0	-150	2489	5.59	0.31	0
95	SLE RA 13	0	-150	2489	5.59	0.31	0
95	SLE RA 14	0	-150	2489	5.59	0.31	0
95	SLE RA 15	0	-150	2489	5.59	0.31	0
95	SLE RA 16	0	-150	2489	5.59	0.31	0
95	SLE RA 17	0	-150	2489	5.59	0.31	0
95	SLE RA 18	0	-161	2628	6.01	0.35	0
95	SLE RA 19	0	-161	2628	6.01	0.35	0
95	SLE RA 20	0	-161	2628	6.01	0.35	0
95	SLE RA 21	0	-161	2628	6.01	0.35	0
95	SLE FR 1	0	-124	2165	4.59	0.2	0
95	SLE FR 2	0	-124	2165	4.59	0.2	0
95	SLE FR 3	0	-124	2165	4.59	0.2	0
95	SLE FR 4	0	-135	2304	5.02	0.25	0
95	SLE FR 5	0	-135	2304	5.02	0.25	0
95	SLE FR 6	0	-142	2397	5.3	0.28	0
95	SLE QP 1	0	-124	2165	4.59	0.2	0
95	SLE QP 2	0	-135	2304	5.02	0.25	0
95	SLD 1	21	-140	2609	5.15	15.96	-0.02
95	SLD 2	21	-140	2609	5.15	15.96	-0.02
95	SLD 3	29	-315	2520	12.09	22.07	-0.02
95	SLD 4	29	-315	2520	12.09	22.07	-0.02
95	SLD 5	-6	129	2531	-5.47	-4.32	-0.01
95	SLD 6	-6	129	2531	-5.47	-4.32	-0.01
95	SLD 7	20	-454	2233	17.66	16.08	0
95	SLD 8	20	-454	2233	17.66	16.08	0
95	SLD 9	-20	184	2375	-7.63	-15.58	0
95	SLD 10	-20	184	2375	-7.63	-15.58	0
95	SLD 11	6	-399	2077	15.5	4.82	0.01
95	SLD 12	6	-399	2077	15.5	4.82	0.01
95	SLD 13	-28	45	2088	-2.05	-21.58	0.01
95	SLD 14	-28	45	2088	-2.05	-21.58	0.01
95	SLD 15	-21	-130	1999	4.89	-15.46	0.02
95	SLD 16	-21	-130	1999	4.89	-15.46	0.02
95	SLV 1	48	-148	3078	5.34	37.35	-0.04
95	SLV 2	48	-148	3078	5.34	37.35	-0.04
95	SLV 3	68	-559	2856	21.65	52.95	-0.04
95	SLV 4	68	-559	2856	21.65	52.95	-0.04
95	SLV 5	-16	485	2873	-19.62	-12.3	-0.02
95	SLV 6	-16	485	2873	-19.62	-12.3	-0.02
95	SLV 7	50	-886	2134	34.74	39.73	0
95	SLV 8	50	-886	2134	34.74	39.73	0
95	SLV 9	-50	616	2475	-24.7	-39.24	0
95	SLV 10	-50	616	2475	-24.7	-39.24	0
95	SLV 11	16	-755	1736	29.65	12.79	0.02
95	SLV 12	16	-755	1736	29.65	12.79	0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
95	SLV 13	-68	289	1752	-11.62	-52.46	0.04
95	SLV 14	-68	289	1752	-11.62	-52.46	0.04
95	SLV 15	-48	-122	1530	4.69	-36.85	0.04
95	SLV 16	-48	-122	1530	4.69	-36.85	0.04
96	SLU 1	0	-230	1899	8.51	-0.18	0
96	SLU 2	0	-230	1899	8.51	-0.18	0
96	SLU 3	0	-230	1899	8.51	-0.18	0
96	SLU 4	0	-230	1899	8.51	-0.18	0
96	SLU 5	0	-230	1899	8.51	-0.18	0
96	SLU 6	0	-230	1899	8.51	-0.18	0
96	SLU 7	0	-230	1899	8.51	-0.18	0
96	SLU 8	0	-230	1899	8.51	-0.18	0
96	SLU 9	0	-230	1899	8.51	-0.18	0
96	SLU 10	0	-312	2277	11.56	-0.26	0
96	SLU 11	0	-312	2277	11.56	-0.26	0
96	SLU 12	0	-312	2277	11.56	-0.26	0
96	SLU 13	0	-312	2277	11.56	-0.26	0
96	SLU 14	0	-312	2277	11.56	-0.26	0
96	SLU 15	0	-312	2277	11.56	-0.26	0
96	SLU 16	0	-312	2277	11.56	-0.26	0
96	SLU 17	0	-312	2277	11.56	-0.26	0
96	SLU 18	0	-347	2438	12.87	-0.29	0
96	SLU 19	0	-347	2438	12.87	-0.29	0
96	SLU 20	0	-347	2438	12.87	-0.29	0
96	SLU 21	0	-347	2438	12.87	-0.29	0
96	SLU 22	0	-272	2098	10.07	-0.23	0
96	SLU 23	0	-272	2098	10.07	-0.23	0
96	SLU 24	0	-272	2098	10.07	-0.23	0
96	SLU 25	0	-272	2098	10.07	-0.23	0
96	SLU 26	0	-272	2098	10.07	-0.23	0
96	SLU 27	0	-272	2098	10.07	-0.23	0
96	SLU 28	0	-272	2098	10.07	-0.23	0
96	SLU 29	0	-272	2098	10.07	-0.23	0
96	SLU 30	0	-272	2098	10.07	-0.23	0
96	SLU 31	0	-354	2475	13.12	-0.3	0
96	SLU 32	0	-354	2475	13.12	-0.3	0
96	SLU 33	0	-354	2475	13.12	-0.3	0
96	SLU 34	0	-354	2475	13.12	-0.3	0
96	SLU 35	0	-354	2475	13.12	-0.3	0
96	SLU 36	0	-354	2475	13.12	-0.3	0
96	SLU 37	0	-354	2475	13.12	-0.3	0
96	SLU 38	0	-354	2475	13.12	-0.3	0
96	SLU 39	0	-390	2637	14.42	-0.33	0
96	SLU 40	0	-390	2637	14.42	-0.33	0
96	SLU 41	0	-390	2637	14.42	-0.33	0
96	SLU 42	0	-390	2637	14.42	-0.33	0
96	SLU 43	0	-284	2401	10.53	-0.22	0
96	SLU 44	0	-284	2401	10.53	-0.22	0
96	SLU 45	0	-284	2401	10.53	-0.22	0
96	SLU 46	0	-284	2401	10.53	-0.22	0
96	SLU 47	0	-284	2401	10.53	-0.22	0
96	SLU 48	0	-284	2401	10.53	-0.22	0
96	SLU 49	0	-284	2401	10.53	-0.22	0
96	SLU 50	0	-284	2401	10.53	-0.22	0
96	SLU 51	0	-284	2401	10.53	-0.22	0
96	SLU 52	0	-366	2778	13.58	-0.3	0
96	SLU 53	0	-366	2778	13.58	-0.3	0
96	SLU 54	0	-366	2778	13.58	-0.3	0
96	SLU 55	0	-366	2778	13.58	-0.3	0
96	SLU 56	0	-366	2778	13.58	-0.3	0
96	SLU 57	0	-366	2778	13.58	-0.3	0
96	SLU 58	0	-366	2778	13.58	-0.3	0
96	SLU 59	0	-366	2778	13.58	-0.3	0
96	SLU 60	0	-402	2940	14.89	-0.33	0
96	SLU 61	0	-402	2940	14.89	-0.33	0
96	SLU 62	0	-402	2940	14.89	-0.33	0
96	SLU 63	0	-402	2940	14.89	-0.33	0
96	SLU 64	0	-326	2599	12.09	-0.27	0
96	SLU 65	0	-326	2599	12.09	-0.27	0
96	SLU 66	0	-326	2599	12.09	-0.27	0
96	SLU 67	0	-326	2599	12.09	-0.27	0
96	SLU 68	0	-326	2599	12.09	-0.27	0
96	SLU 69	0	-326	2599	12.09	-0.27	0
96	SLU 70	0	-326	2599	12.09	-0.27	0
96	SLU 71	0	-326	2599	12.09	-0.27	0
96	SLU 72	0	-326	2599	12.09	-0.27	0
96	SLU 73	0	-409	2977	15.14	-0.34	0
96	SLU 74	0	-409	2977	15.14	-0.34	0
96	SLU 75	0	-409	2977	15.14	-0.34	0
96	SLU 76	0	-409	2977	15.14	-0.34	0
96	SLU 77	0	-409	2977	15.14	-0.34	0
96	SLU 78	0	-409	2977	15.14	-0.34	0
96	SLU 79	0	-409	2977	15.14	-0.34	0
96	SLU 80	0	-409	2977	15.14	-0.34	0
96	SLU 81	0	-444	3139	16.44	-0.37	0
96	SLU 82	0	-444	3139	16.44	-0.37	0
96	SLU 83	0	-444	3139	16.44	-0.37	0
96	SLU 84	0	-444	3139	16.44	-0.37	0
96	SLE RA 1	0	-242	1956	8.96	-0.2	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
96	SLE RA 2	0	-242	1956	8.96	-0.2	0
96	SLE RA 3	0	-242	1956	8.96	-0.2	0
96	SLE RA 4	0	-242	1956	8.96	-0.2	0
96	SLE RA 5	0	-242	1956	8.96	-0.2	0
96	SLE RA 6	0	-242	1956	8.96	-0.2	0
96	SLE RA 7	0	-242	1956	8.96	-0.2	0
96	SLE RA 8	0	-242	1956	8.96	-0.2	0
96	SLE RA 9	0	-242	1956	8.96	-0.2	0
96	SLE RA 10	0	-297	2207	10.99	-0.25	0
96	SLE RA 11	0	-297	2207	10.99	-0.25	0
96	SLE RA 12	0	-297	2207	10.99	-0.25	0
96	SLE RA 13	0	-297	2207	10.99	-0.25	0
96	SLE RA 14	0	-297	2207	10.99	-0.25	0
96	SLE RA 15	0	-297	2207	10.99	-0.25	0
96	SLE RA 16	0	-297	2207	10.99	-0.25	0
96	SLE RA 17	0	-297	2207	10.99	-0.25	0
96	SLE RA 18	0	-320	2315	11.86	-0.27	0
96	SLE RA 19	0	-320	2315	11.86	-0.27	0
96	SLE RA 20	0	-320	2315	11.86	-0.27	0
96	SLE RA 21	0	-320	2315	11.86	-0.27	0
96	SLE FR 1	0	-242	1956	8.96	-0.2	0
96	SLE FR 2	0	-242	1956	8.96	-0.2	0
96	SLE FR 3	0	-242	1956	8.96	-0.2	0
96	SLE FR 4	0	-265	2064	9.83	-0.22	0
96	SLE FR 5	0	-265	2064	9.83	-0.22	0
96	SLE FR 6	0	-281	2136	10.41	-0.23	0
96	SLE QP 1	0	-242	1956	8.96	-0.2	0
96	SLE QP 2	0	-265	2064	9.83	-0.22	0
96	SLD 1	31	-97	1943	3.29	19.09	-0.01
96	SLD 2	31	-97	1943	3.29	19.09	-0.01
96	SLD 3	19	-263	2007	9.78	29.15	-0.02
96	SLD 4	19	-263	2007	9.78	29.15	-0.02
96	SLD 5	27	38	1930	-1.97	-9.68	0.01
96	SLD 6	27	38	1930	-1.97	-9.68	0.01
96	SLD 7	-12	-518	2144	19.65	23.85	-0.02
96	SLD 8	-12	-518	2144	19.65	23.85	-0.02
96	SLD 9	12	-13	1983	0	-24.28	0.02
96	SLD 10	12	-13	1983	0	-24.28	0.02
96	SLD 11	-27	-569	2198	21.63	9.24	-0.01
96	SLD 12	-27	-569	2198	21.63	9.24	-0.01
96	SLD 13	-19	-267	2120	9.88	-29.59	0.02
96	SLD 14	-19	-267	2120	9.88	-29.59	0.02
96	SLD 15	-31	-434	2184	16.36	-19.53	0.01
96	SLD 16	-31	-434	2184	16.36	-19.53	0.01
96	SLV 1	75	131	1778	-5.54	46.82	-0.03
96	SLV 2	75	131	1778	-5.54	46.82	-0.03
96	SLV 3	45	-261	1930	9.73	72.56	-0.06
96	SLV 4	45	-261	1930	9.73	72.56	-0.06
96	SLV 5	68	449	1748	-17.94	-25.15	0.03
96	SLV 6	68	449	1748	-17.94	-25.15	0.03
96	SLV 7	-33	-859	2254	32.96	60.66	-0.05
96	SLV 8	-33	-859	2254	32.96	60.66	-0.05
96	SLV 9	33	329	1874	-13.3	-61.09	0.05
96	SLV 10	33	329	1874	-13.3	-61.09	0.05
96	SLV 11	-69	-979	2380	37.59	24.71	-0.03
96	SLV 12	-69	-979	2380	37.59	24.71	-0.03
96	SLV 13	-45	-269	2198	9.93	-73	0.06
96	SLV 14	-45	-269	2198	9.93	-73	0.06
96	SLV 15	-75	-662	2349	25.19	-47.26	0.03
96	SLV 16	-75	-662	2349	25.19	-47.26	0.03
97	SLU 1	0	0	1316	0.03	0	0
97	SLU 2	0	0	1316	0.03	0	0
97	SLU 3	0	0	1316	0.03	0	0
97	SLU 4	0	0	1316	0.03	0	0
97	SLU 5	0	0	1316	0.03	0	0
97	SLU 6	0	0	1316	0.03	0	0
97	SLU 7	0	0	1316	0.03	0	0
97	SLU 8	0	0	1316	0.03	0	0
97	SLU 9	0	0	1316	0.03	0	0
97	SLU 10	0	1	1988	0.01	0	0
97	SLU 11	0	1	1988	0.01	0	0
97	SLU 12	0	1	1988	0.01	0	0
97	SLU 13	0	1	1988	0.01	0	0
97	SLU 14	0	1	1988	0.01	0	0
97	SLU 15	0	1	1988	0.01	0	0
97	SLU 16	0	1	1988	0.01	0	0
97	SLU 17	0	1	1988	0.01	0	0
97	SLU 18	0	1	2276	0	0	0
97	SLU 19	0	1	2276	0	0	0
97	SLU 20	0	1	2276	0	0	0
97	SLU 21	0	1	2276	0	0	0
97	SLU 22	0	1	1635	0.02	0	0
97	SLU 23	0	1	1635	0.02	0	0
97	SLU 24	0	1	1635	0.02	0	0
97	SLU 25	0	1	1635	0.02	0	0
97	SLU 26	0	1	1635	0.02	0	0
97	SLU 27	0	1	1635	0.02	0	0
97	SLU 28	0	1	1635	0.02	0	0
97	SLU 29	0	1	1635	0.02	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
97	SLU 30	0	1	1635	0.02	0	0
97	SLU 31	0	1	2307	0	0	0
97	SLU 32	0	1	2307	0	0	0
97	SLU 33	0	1	2307	0	0	0
97	SLU 34	0	1	2307	0	0	0
97	SLU 35	0	1	2307	0	0	0
97	SLU 36	0	1	2307	0	0	0
97	SLU 37	0	1	2307	0	0	0
97	SLU 38	0	1	2307	0	0	0
97	SLU 39	0	1	2596	-0.01	0	0
97	SLU 40	0	1	2596	-0.01	0	0
97	SLU 41	0	1	2596	-0.01	0	0
97	SLU 42	0	1	2596	-0.01	0	0
97	SLU 43	0	1	1601	0.05	0	0
97	SLU 44	0	1	1601	0.05	0	0
97	SLU 45	0	1	1601	0.05	0	0
97	SLU 46	0	1	1601	0.05	0	0
97	SLU 47	0	1	1601	0.05	0	0
97	SLU 48	0	1	1601	0.05	0	0
97	SLU 49	0	1	1601	0.05	0	0
97	SLU 50	0	1	1601	0.05	0	0
97	SLU 51	0	1	1601	0.05	0	0
97	SLU 52	0	1	2273	0.03	0	0
97	SLU 53	0	1	2273	0.03	0	0
97	SLU 54	0	1	2273	0.03	0	0
97	SLU 55	0	1	2273	0.03	0	0
97	SLU 56	0	1	2273	0.03	0	0
97	SLU 57	0	1	2273	0.03	0	0
97	SLU 58	0	1	2273	0.03	0	0
97	SLU 59	0	1	2273	0.03	0	0
97	SLU 60	0	1	2561	0.02	0	0
97	SLU 61	0	1	2561	0.02	0	0
97	SLU 62	0	1	2561	0.02	0	0
97	SLU 63	0	1	2561	0.02	0	0
97	SLU 64	0	1	1920	0.03	0	0
97	SLU 65	0	1	1920	0.03	0	0
97	SLU 66	0	1	1920	0.03	0	0
97	SLU 67	0	1	1920	0.03	0	0
97	SLU 68	0	1	1920	0.03	0	0
97	SLU 69	0	1	1920	0.03	0	0
97	SLU 70	0	1	1920	0.03	0	0
97	SLU 71	0	1	1920	0.03	0	0
97	SLU 72	0	1	1920	0.03	0	0
97	SLU 73	0	1	2593	0.01	0	0
97	SLU 74	0	1	2593	0.01	0	0
97	SLU 75	0	1	2593	0.01	0	0
97	SLU 76	0	1	2593	0.01	0	0
97	SLU 77	0	1	2593	0.01	0	0
97	SLU 78	0	1	2593	0.01	0	0
97	SLU 79	0	1	2593	0.01	0	0
97	SLU 80	0	1	2593	0.01	0	0
97	SLU 81	0	1	2881	0.01	0	0
97	SLU 82	0	1	2881	0.01	0	0
97	SLU 83	0	1	2881	0.01	0	0
97	SLU 84	0	1	2881	0.01	0	0
97	SLE RA 1	0	1	1407	0.03	0	0
97	SLE RA 2	0	1	1407	0.03	0	0
97	SLE RA 3	0	1	1407	0.03	0	0
97	SLE RA 4	0	1	1407	0.03	0	0
97	SLE RA 5	0	1	1407	0.03	0	0
97	SLE RA 6	0	1	1407	0.03	0	0
97	SLE RA 7	0	1	1407	0.03	0	0
97	SLE RA 8	0	1	1407	0.03	0	0
97	SLE RA 9	0	1	1407	0.03	0	0
97	SLE RA 10	0	1	1855	0.02	0	0
97	SLE RA 11	0	1	1855	0.02	0	0
97	SLE RA 12	0	1	1855	0.02	0	0
97	SLE RA 13	0	1	1855	0.02	0	0
97	SLE RA 14	0	1	1855	0.02	0	0
97	SLE RA 15	0	1	1855	0.02	0	0
97	SLE RA 16	0	1	1855	0.02	0	0
97	SLE RA 17	0	1	1855	0.02	0	0
97	SLE RA 18	0	1	2047	0.01	0	0
97	SLE RA 19	0	1	2047	0.01	0	0
97	SLE RA 20	0	1	2047	0.01	0	0
97	SLE RA 21	0	1	2047	0.01	0	0
97	SLE FR 1	0	1	1407	0.03	0	0
97	SLE FR 2	0	1	1407	0.03	0	0
97	SLE FR 3	0	1	1407	0.03	0	0
97	SLE FR 4	0	1	1599	0.02	0	0
97	SLE FR 5	0	1	1599	0.02	0	0
97	SLE FR 6	0	1	1727	0.02	0	0
97	SLE QP 1	0	1	1407	0.03	0	0
97	SLE QP 2	0	1	1599	0.02	0	0
97	SLD 1	-4	-22	1647	-4.05	8.73	0.04
97	SLD 2	-4	-22	1647	-4.05	8.73	0.04
97	SLD 3	-7	44	1582	7.64	4.83	0.03
97	SLD 4	-7	44	1582	7.64	4.83	0.03
97	SLD 5	2	-106	1711	-18.93	8.54	0.03



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
97	SLD 6	2	-106	1711	-18.93	8.54	0.03
97	SLD 7	-5	114	1497	20.04	-4.47	-0.01
97	SLD 8	-5	114	1497	20.04	-4.47	-0.01
97	SLD 9	5	-112	1702	-19.99	4.48	0.01
97	SLD 10	5	-112	1702	-19.99	4.48	0.01
97	SLD 11	-2	107	1487	18.97	-8.54	-0.03
97	SLD 12	-2	107	1487	18.97	-8.54	-0.03
97	SLD 13	7	-43	1616	-7.6	-4.83	-0.03
97	SLD 14	7	-43	1616	-7.6	-4.83	-0.03
97	SLD 15	4	23	1551	4.09	-8.73	-0.04
97	SLD 16	4	23	1551	4.09	-8.73	-0.04
97	SLV 1	-11	-57	1720	-10.42	22.14	0.1
97	SLV 2	-11	-57	1720	-10.42	22.14	0.1
97	SLV 3	-16	112	1556	19.57	12.13	0.07
97	SLV 4	-16	112	1556	19.57	12.13	0.07
97	SLV 5	6	-273	1885	-48.59	21.83	0.07
97	SLV 6	6	-273	1885	-48.59	21.83	0.07
97	SLV 7	-14	291	1336	51.37	-11.55	-0.03
97	SLV 8	-14	291	1336	51.37	-11.55	-0.03
97	SLV 9	14	-289	1862	-51.33	11.55	0.03
97	SLV 10	14	-289	1862	-51.33	11.55	0.03
97	SLV 11	-6	275	1313	48.64	-21.83	-0.07
97	SLV 12	-6	275	1313	48.64	-21.83	-0.07
97	SLV 13	16	-110	1643	-19.53	-12.13	-0.07
97	SLV 14	16	-110	1643	-19.53	-12.13	-0.07
97	SLV 15	11	59	1478	10.46	-22.14	-0.1
97	SLV 16	11	59	1478	10.46	-22.14	-0.1
98	SLU 1	0	-147	2072	5.82	0.12	0
98	SLU 2	0	-147	2072	5.82	0.12	0
98	SLU 3	0	-147	2072	5.82	0.12	0
98	SLU 4	0	-147	2072	5.82	0.12	0
98	SLU 5	0	-147	2072	5.82	0.12	0
98	SLU 6	0	-147	2072	5.82	0.12	0
98	SLU 7	0	-147	2072	5.82	0.12	0
98	SLU 8	0	-147	2072	5.82	0.12	0
98	SLU 9	0	-147	2072	5.82	0.12	0
98	SLU 10	0	-194	2561	7.73	0.27	0
98	SLU 11	0	-194	2561	7.73	0.27	0
98	SLU 12	0	-194	2561	7.73	0.27	0
98	SLU 13	0	-194	2561	7.73	0.27	0
98	SLU 14	0	-194	2561	7.73	0.27	0
98	SLU 15	0	-194	2561	7.73	0.27	0
98	SLU 16	0	-194	2561	7.73	0.27	0
98	SLU 17	0	-194	2561	7.73	0.27	0
98	SLU 18	0	-214	2770	8.54	0.34	0
98	SLU 19	0	-214	2770	8.54	0.34	0
98	SLU 20	0	-214	2770	8.54	0.34	0
98	SLU 21	0	-214	2770	8.54	0.34	0
98	SLU 22	0	-173	2322	6.84	0.17	0
98	SLU 23	0	-173	2322	6.84	0.17	0
98	SLU 24	0	-173	2322	6.84	0.17	0
98	SLU 25	0	-173	2322	6.84	0.17	0
98	SLU 26	0	-173	2322	6.84	0.17	0
98	SLU 27	0	-173	2322	6.84	0.17	0
98	SLU 28	0	-173	2322	6.84	0.17	0
98	SLU 29	0	-173	2322	6.84	0.17	0
98	SLU 30	0	-173	2322	6.84	0.17	0
98	SLU 31	0	-220	2811	8.75	0.32	0
98	SLU 32	0	-220	2811	8.75	0.32	0
98	SLU 33	0	-220	2811	8.75	0.32	0
98	SLU 34	0	-220	2811	8.75	0.32	0
98	SLU 35	0	-220	2811	8.75	0.32	0
98	SLU 36	0	-220	2811	8.75	0.32	0
98	SLU 37	0	-220	2811	8.75	0.32	0
98	SLU 38	0	-220	2811	8.75	0.32	0
98	SLU 39	0	-240	3020	9.56	0.39	0
98	SLU 40	0	-240	3020	9.56	0.39	0
98	SLU 41	0	-240	3020	9.56	0.39	0
98	SLU 42	0	-240	3020	9.56	0.39	0
98	SLU 43	0	-183	2608	7.22	0.14	0
98	SLU 44	0	-183	2608	7.22	0.14	0
98	SLU 45	0	-183	2608	7.22	0.14	0
98	SLU 46	0	-183	2608	7.22	0.14	0
98	SLU 47	0	-183	2608	7.22	0.14	0
98	SLU 48	0	-183	2608	7.22	0.14	0
98	SLU 49	0	-183	2608	7.22	0.14	0
98	SLU 50	0	-183	2608	7.22	0.14	0
98	SLU 51	0	-183	2608	7.22	0.14	0
98	SLU 52	0	-230	3096	9.12	0.29	0
98	SLU 53	0	-230	3096	9.12	0.29	0
98	SLU 54	0	-230	3096	9.12	0.29	0
98	SLU 55	0	-230	3096	9.12	0.29	0
98	SLU 56	0	-230	3096	9.12	0.29	0
98	SLU 57	0	-230	3096	9.12	0.29	0
98	SLU 58	0	-230	3096	9.12	0.29	0
98	SLU 59	0	-230	3096	9.12	0.29	0
98	SLU 60	0	-250	3306	9.94	0.35	0
98	SLU 61	0	-250	3306	9.94	0.35	0
98	SLU 62	0	-250	3306	9.94	0.35	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
98	SLU 63	0	-250	3306	9.94	0.35	0
98	SLU 64	0	-208	2858	8.24	0.19	0
98	SLU 65	0	-208	2858	8.24	0.19	0
98	SLU 66	0	-208	2858	8.24	0.19	0
98	SLU 67	0	-208	2858	8.24	0.19	0
98	SLU 68	0	-208	2858	8.24	0.19	0
98	SLU 69	0	-208	2858	8.24	0.19	0
98	SLU 70	0	-208	2858	8.24	0.19	0
98	SLU 71	0	-208	2858	8.24	0.19	0
98	SLU 72	0	-208	2858	8.24	0.19	0
98	SLU 73	0	-255	3346	10.14	0.34	0
98	SLU 74	0	-255	3346	10.14	0.34	0
98	SLU 75	0	-255	3346	10.14	0.34	0
98	SLU 76	0	-255	3346	10.14	0.34	0
98	SLU 77	0	-255	3346	10.14	0.34	0
98	SLU 78	0	-255	3346	10.14	0.34	0
98	SLU 79	0	-255	3346	10.14	0.34	0
98	SLU 80	0	-255	3346	10.14	0.34	0
98	SLU 81	0	-276	3556	10.96	0.41	0
98	SLU 82	0	-276	3556	10.96	0.41	0
98	SLU 83	0	-276	3556	10.96	0.41	0
98	SLU 84	0	-276	3556	10.96	0.41	0
98	SLE RA 1	0	-155	2143	6.11	0.14	0
98	SLE RA 2	0	-155	2143	6.11	0.14	0
98	SLE RA 3	0	-155	2143	6.11	0.14	0
98	SLE RA 4	0	-155	2143	6.11	0.14	0
98	SLE RA 5	0	-155	2143	6.11	0.14	0
98	SLE RA 6	0	-155	2143	6.11	0.14	0
98	SLE RA 7	0	-155	2143	6.11	0.14	0
98	SLE RA 8	0	-155	2143	6.11	0.14	0
98	SLE RA 9	0	-155	2143	6.11	0.14	0
98	SLE RA 10	0	-186	2469	7.38	0.24	0
98	SLE RA 11	0	-186	2469	7.38	0.24	0
98	SLE RA 12	0	-186	2469	7.38	0.24	0
98	SLE RA 13	0	-186	2469	7.38	0.24	0
98	SLE RA 14	0	-186	2469	7.38	0.24	0
98	SLE RA 15	0	-186	2469	7.38	0.24	0
98	SLE RA 16	0	-186	2469	7.38	0.24	0
98	SLE RA 17	0	-186	2469	7.38	0.24	0
98	SLE RA 18	0	-199	2609	7.93	0.28	0
98	SLE RA 19	0	-199	2609	7.93	0.28	0
98	SLE RA 20	0	-199	2609	7.93	0.28	0
98	SLE RA 21	0	-199	2609	7.93	0.28	0
98	SLE FR 1	0	-155	2143	6.11	0.14	0
98	SLE FR 2	0	-155	2143	6.11	0.14	0
98	SLE FR 3	0	-155	2143	6.11	0.14	0
98	SLE FR 4	0	-168	2283	6.66	0.18	0
98	SLE FR 5	0	-168	2283	6.66	0.18	0
98	SLE FR 6	0	-177	2376	7.02	0.21	0
98	SLE QP 1	0	-155	2143	6.11	0.14	0
98	SLE QP 2	0	-168	2283	6.66	0.18	0
98	SLD 1	25	-172	2652	6.78	18.55	-0.01
98	SLD 2	25	-172	2652	6.78	18.55	-0.01
98	SLD 3	31	-347	2537	13.61	23.9	-0.01
98	SLD 4	31	-347	2537	13.61	23.9	-0.01
98	SLD 5	-2	96	2569	-3.67	-2.42	0
98	SLD 6	-2	96	2569	-3.67	-2.42	0
98	SLD 7	19	-487	2184	19.11	15.41	-0.01
98	SLD 8	19	-487	2184	19.11	15.41	-0.01
98	SLD 9	-19	151	2382	-5.8	-15.05	0.01
98	SLD 10	-19	151	2382	-5.8	-15.05	0.01
98	SLD 11	2	-432	1997	16.99	2.78	0
98	SLD 12	2	-432	1997	16.99	2.78	0
98	SLD 13	-31	11	2029	-0.3	-23.54	0.01
98	SLD 14	-31	11	2029	-0.3	-23.54	0.01
98	SLD 15	-25	-164	1914	6.54	-18.19	0.01
98	SLD 16	-25	-164	1914	6.54	-18.19	0.01
98	SLV 1	59	-179	3221	6.98	43.76	-0.02
98	SLV 2	59	-179	3221	6.98	43.76	-0.02
98	SLV 3	74	-590	2934	23.02	57.38	-0.03
98	SLV 4	74	-590	2934	23.02	57.38	-0.03
98	SLV 5	-6	452	2998	-17.57	-7.39	0
98	SLV 6	-6	452	2998	-17.57	-7.39	0
98	SLV 7	46	-918	2044	35.89	37.98	-0.02
98	SLV 8	46	-918	2044	35.89	37.98	-0.02
98	SLV 9	-46	582	2522	-22.57	-37.62	0.02
98	SLV 10	-46	582	2522	-22.57	-37.62	0.02
98	SLV 11	6	-788	1568	30.89	7.75	0
98	SLV 12	6	-788	1568	30.89	7.75	0
98	SLV 13	-74	254	1631	-9.7	-57.02	0.03
98	SLV 14	-74	254	1631	-9.7	-57.02	0.03
98	SLV 15	-59	-157	1345	6.34	-43.41	0.02
98	SLV 16	-59	-157	1345	6.34	-43.41	0.02
99	SLU 1	0	-216	1709	8.16	-0.12	0
99	SLU 2	0	-216	1709	8.16	-0.12	0
99	SLU 3	0	-216	1709	8.16	-0.12	0
99	SLU 4	0	-216	1709	8.16	-0.12	0
99	SLU 5	0	-216	1709	8.16	-0.12	0
99	SLU 6	0	-216	1709	8.16	-0.12	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
99	SLU 7	0	-216	1709	8.16	-0.12	0
99	SLU 8	0	-216	1709	8.16	-0.12	0
99	SLU 9	0	-216	1709	8.16	-0.12	0
99	SLU 10	0	-299	2025	11.32	-0.16	0
99	SLU 11	0	-299	2025	11.32	-0.16	0
99	SLU 12	0	-299	2025	11.32	-0.16	0
99	SLU 13	0	-299	2025	11.32	-0.16	0
99	SLU 14	0	-299	2025	11.32	-0.16	0
99	SLU 15	0	-299	2025	11.32	-0.16	0
99	SLU 16	0	-299	2025	11.32	-0.16	0
99	SLU 17	0	-299	2025	11.32	-0.16	0
99	SLU 18	0	-334	2161	12.67	-0.18	0
99	SLU 19	0	-334	2161	12.67	-0.18	0
99	SLU 20	0	-334	2161	12.67	-0.18	0
99	SLU 21	0	-334	2161	12.67	-0.18	0
99	SLU 22	0	-257	1876	9.72	-0.14	0
99	SLU 23	0	-257	1876	9.72	-0.14	0
99	SLU 24	0	-257	1876	9.72	-0.14	0
99	SLU 25	0	-257	1876	9.72	-0.14	0
99	SLU 26	0	-257	1876	9.72	-0.14	0
99	SLU 27	0	-257	1876	9.72	-0.14	0
99	SLU 28	0	-257	1876	9.72	-0.14	0
99	SLU 29	0	-257	1876	9.72	-0.14	0
99	SLU 30	0	-257	1876	9.72	-0.14	0
99	SLU 31	0	-340	2192	12.88	-0.18	0
99	SLU 32	0	-340	2192	12.88	-0.18	0
99	SLU 33	0	-340	2192	12.88	-0.18	0
99	SLU 34	0	-340	2192	12.88	-0.18	0
99	SLU 35	0	-340	2192	12.88	-0.18	0
99	SLU 36	0	-340	2192	12.88	-0.18	0
99	SLU 37	0	-340	2192	12.88	-0.18	0
99	SLU 38	0	-340	2192	12.88	-0.18	0
99	SLU 39	0	-375	2328	14.23	-0.2	0
99	SLU 40	0	-375	2328	14.23	-0.2	0
99	SLU 41	0	-375	2328	14.23	-0.2	0
99	SLU 42	0	-375	2328	14.23	-0.2	0
99	SLU 43	0	-266	2164	10.08	-0.15	0
99	SLU 44	0	-266	2164	10.08	-0.15	0
99	SLU 45	0	-266	2164	10.08	-0.15	0
99	SLU 46	0	-266	2164	10.08	-0.15	0
99	SLU 47	0	-266	2164	10.08	-0.15	0
99	SLU 48	0	-266	2164	10.08	-0.15	0
99	SLU 49	0	-266	2164	10.08	-0.15	0
99	SLU 50	0	-266	2164	10.08	-0.15	0
99	SLU 51	0	-266	2164	10.08	-0.15	0
99	SLU 52	0	-349	2480	13.24	-0.19	0
99	SLU 53	0	-349	2480	13.24	-0.19	0
99	SLU 54	0	-349	2480	13.24	-0.19	0
99	SLU 55	0	-349	2480	13.24	-0.19	0
99	SLU 56	0	-349	2480	13.24	-0.19	0
99	SLU 57	0	-349	2480	13.24	-0.19	0
99	SLU 58	0	-349	2480	13.24	-0.19	0
99	SLU 59	0	-349	2480	13.24	-0.19	0
99	SLU 60	0	-385	2616	14.59	-0.2	0
99	SLU 61	0	-385	2616	14.59	-0.2	0
99	SLU 62	0	-385	2616	14.59	-0.2	0
99	SLU 63	0	-385	2616	14.59	-0.2	0
99	SLU 64	0	-307	2331	11.64	-0.17	0
99	SLU 65	0	-307	2331	11.64	-0.17	0
99	SLU 66	0	-307	2331	11.64	-0.17	0
99	SLU 67	0	-307	2331	11.64	-0.17	0
99	SLU 68	0	-307	2331	11.64	-0.17	0
99	SLU 69	0	-307	2331	11.64	-0.17	0
99	SLU 70	0	-307	2331	11.64	-0.17	0
99	SLU 71	0	-307	2331	11.64	-0.17	0
99	SLU 72	0	-307	2331	11.64	-0.17	0
99	SLU 73	0	-390	2647	14.79	-0.21	0
99	SLU 74	0	-390	2647	14.79	-0.21	0
99	SLU 75	0	-390	2647	14.79	-0.21	0
99	SLU 76	0	-390	2647	14.79	-0.21	0
99	SLU 77	0	-390	2647	14.79	-0.21	0
99	SLU 78	0	-390	2647	14.79	-0.21	0
99	SLU 79	0	-390	2647	14.79	-0.21	0
99	SLU 80	0	-390	2647	14.79	-0.21	0
99	SLU 81	0	-426	2783	16.14	-0.23	0
99	SLU 82	0	-426	2783	16.14	-0.23	0
99	SLU 83	0	-426	2783	16.14	-0.23	0
99	SLU 84	0	-426	2783	16.14	-0.23	0
99	SLE RA 1	0	-227	1756	8.61	-0.13	0
99	SLE RA 2	0	-227	1756	8.61	-0.13	0
99	SLE RA 3	0	-227	1756	8.61	-0.13	0
99	SLE RA 4	0	-227	1756	8.61	-0.13	0
99	SLE RA 5	0	-227	1756	8.61	-0.13	0
99	SLE RA 6	0	-227	1756	8.61	-0.13	0
99	SLE RA 7	0	-227	1756	8.61	-0.13	0
99	SLE RA 8	0	-227	1756	8.61	-0.13	0
99	SLE RA 9	0	-227	1756	8.61	-0.13	0
99	SLE RA 10	0	-283	1967	10.71	-0.15	0
99	SLE RA 11	0	-283	1967	10.71	-0.15	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
99	SLE RA 12	0	-283	1967	10.71	-0.15	0
99	SLE RA 13	0	-283	1967	10.71	-0.15	0
99	SLE RA 14	0	-283	1967	10.71	-0.15	0
99	SLE RA 15	0	-283	1967	10.71	-0.15	0
99	SLE RA 16	0	-283	1967	10.71	-0.15	0
99	SLE RA 17	0	-283	1967	10.71	-0.15	0
99	SLE RA 18	0	-306	2058	11.61	-0.16	0
99	SLE RA 19	0	-306	2058	11.61	-0.16	0
99	SLE RA 20	0	-306	2058	11.61	-0.16	0
99	SLE RA 21	0	-306	2058	11.61	-0.16	0
99	SLE FR 1	0	-227	1756	8.61	-0.13	0
99	SLE FR 2	0	-227	1756	8.61	-0.13	0
99	SLE FR 3	0	-227	1756	8.61	-0.13	0
99	SLE FR 4	0	-251	1847	9.51	-0.14	0
99	SLE FR 5	0	-251	1847	9.51	-0.14	0
99	SLE FR 6	0	-267	1907	10.11	-0.15	0
99	SLE QP 1	0	-227	1756	8.61	-0.13	0
99	SLE QP 2	0	-251	1847	9.51	-0.14	0
99	SLD 1	30	-71	1749	2.31	26.41	-0.02
99	SLD 2	30	-71	1749	2.31	26.41	-0.02
99	SLD 3	39	-251	1802	9.48	35.39	-0.02
99	SLD 4	39	-251	1802	9.48	35.39	-0.02
99	SLD 5	-5	76	1737	-3.53	-5.8	0
99	SLD 6	-5	76	1737	-3.53	-5.8	0
99	SLD 7	25	-524	1914	20.38	24.14	-0.01
99	SLD 8	25	-524	1914	20.38	24.14	-0.01
99	SLD 9	-25	22	1779	-1.36	-24.42	0.01
99	SLD 10	-25	22	1779	-1.36	-24.42	0.01
99	SLD 11	5	-579	1957	22.55	5.52	0
99	SLD 12	5	-579	1957	22.55	5.52	0
99	SLD 13	-39	-251	1891	9.54	-35.66	0.02
99	SLD 14	-39	-251	1891	9.54	-35.66	0.02
99	SLD 15	-30	-431	1944	16.71	-26.68	0.02
99	SLD 16	-30	-431	1944	16.71	-26.68	0.02
99	SLV 1	72	173	1616	-7.42	64.98	-0.04
99	SLV 2	72	173	1616	-7.42	64.98	-0.04
99	SLV 3	95	-252	1741	9.46	87.96	-0.05
99	SLV 4	95	-252	1741	9.46	87.96	-0.05
99	SLV 5	-13	519	1587	-21.16	-15.45	0.01
99	SLV 6	-13	519	1587	-21.16	-15.45	0.01
99	SLV 7	63	-894	2005	35.08	61.14	-0.03
99	SLV 8	63	-894	2005	35.08	61.14	-0.03
99	SLV 9	-63	392	1688	-16.06	-61.42	0.04
99	SLV 10	-63	392	1688	-16.06	-61.42	0.04
99	SLV 11	13	-1021	2106	40.18	15.18	-0.01
99	SLV 12	13	-1021	2106	40.18	15.18	-0.01
99	SLV 13	-95	-251	1952	9.56	-88.24	0.05
99	SLV 14	-95	-251	1952	9.56	-88.24	0.05
99	SLV 15	-72	-675	2077	26.44	-65.26	0.04
99	SLV 16	-72	-675	2077	26.44	-65.26	0.04
100	SLU 1	0	0	1279	0.03	0	0
100	SLU 2	0	0	1279	0.03	0	0
100	SLU 3	0	0	1279	0.03	0	0
100	SLU 4	0	0	1279	0.03	0	0
100	SLU 5	0	0	1279	0.03	0	0
100	SLU 6	0	0	1279	0.03	0	0
100	SLU 7	0	0	1279	0.03	0	0
100	SLU 8	0	0	1279	0.03	0	0
100	SLU 9	0	0	1279	0.03	0	0
100	SLU 10	0	-1	1903	0	0	0
100	SLU 11	0	-1	1903	0	0	0
100	SLU 12	0	-1	1903	0	0	0
100	SLU 13	0	-1	1903	0	0	0
100	SLU 14	0	-1	1903	0	0	0
100	SLU 15	0	-1	1903	0	0	0
100	SLU 16	0	-1	1903	0	0	0
100	SLU 17	0	-1	1903	0	0	0
100	SLU 18	0	-1	2170	-0.01	0	0
100	SLU 19	0	-1	2170	-0.01	0	0
100	SLU 20	0	-1	2170	-0.01	0	0
100	SLU 21	0	-1	2170	-0.01	0	0
100	SLU 22	0	-1	1579	0.02	0	0
100	SLU 23	0	-1	1579	0.02	0	0
100	SLU 24	0	-1	1579	0.02	0	0
100	SLU 25	0	-1	1579	0.02	0	0
100	SLU 26	0	-1	1579	0.02	0	0
100	SLU 27	0	-1	1579	0.02	0	0
100	SLU 28	0	-1	1579	0.02	0	0
100	SLU 29	0	-1	1579	0.02	0	0
100	SLU 30	0	-1	1579	0.02	0	0
100	SLU 31	0	-1	2202	-0.01	0	0
100	SLU 32	0	-1	2202	-0.01	0	0
100	SLU 33	0	-1	2202	-0.01	0	0
100	SLU 34	0	-1	2202	-0.01	0	0
100	SLU 35	0	-1	2202	-0.01	0	0
100	SLU 36	0	-1	2202	-0.01	0	0
100	SLU 37	0	-1	2202	-0.01	0	0
100	SLU 38	0	-1	2202	-0.01	0	0
100	SLU 39	0	-2	2469	-0.02	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
100	SLU 40	0	-2	2469	-0.02	0	0
100	SLU 41	0	-2	2469	-0.02	0	0
100	SLU 42	0	-2	2469	-0.02	0	0
100	SLU 43	0	0	1561	0.04	0	0
100	SLU 44	0	0	1561	0.04	0	0
100	SLU 45	0	0	1561	0.04	0	0
100	SLU 46	0	0	1561	0.04	0	0
100	SLU 47	0	0	1561	0.04	0	0
100	SLU 48	0	0	1561	0.04	0	0
100	SLU 49	0	0	1561	0.04	0	0
100	SLU 50	0	0	1561	0.04	0	0
100	SLU 51	0	0	1561	0.04	0	0
100	SLU 52	0	-1	2184	0.01	0	0
100	SLU 53	0	-1	2184	0.01	0	0
100	SLU 54	0	-1	2184	0.01	0	0
100	SLU 55	0	-1	2184	0.01	0	0
100	SLU 56	0	-1	2184	0.01	0	0
100	SLU 57	0	-1	2184	0.01	0	0
100	SLU 58	0	-1	2184	0.01	0	0
100	SLU 59	0	-1	2184	0.01	0	0
100	SLU 60	0	-1	2451	0	0	0
100	SLU 61	0	-1	2451	0	0	0
100	SLU 62	0	-1	2451	0	0	0
100	SLU 63	0	-1	2451	0	0	0
100	SLU 64	0	-1	1860	0.03	0	0
100	SLU 65	0	-1	1860	0.03	0	0
100	SLU 66	0	-1	1860	0.03	0	0
100	SLU 67	0	-1	1860	0.03	0	0
100	SLU 68	0	-1	1860	0.03	0	0
100	SLU 69	0	-1	1860	0.03	0	0
100	SLU 70	0	-1	1860	0.03	0	0
100	SLU 71	0	-1	1860	0.03	0	0
100	SLU 72	0	-1	1860	0.03	0	0
100	SLU 73	0	-1	2483	0	0	0
100	SLU 74	0	-1	2483	0	0	0
100	SLU 75	0	-1	2483	0	0	0
100	SLU 76	0	-1	2483	0	0	0
100	SLU 77	0	-1	2483	0	0	0
100	SLU 78	0	-1	2483	0	0	0
100	SLU 79	0	-1	2483	0	0	0
100	SLU 80	0	-1	2483	0	0	0
100	SLU 81	0	-2	2750	-0.01	0	0
100	SLU 82	0	-2	2750	-0.01	0	0
100	SLU 83	0	-2	2750	-0.01	0	0
100	SLU 84	0	-2	2750	-0.01	0	0
100	SLE RA 1	0	0	1365	0.03	0	0
100	SLE RA 2	0	0	1365	0.03	0	0
100	SLE RA 3	0	0	1365	0.03	0	0
100	SLE RA 4	0	0	1365	0.03	0	0
100	SLE RA 5	0	0	1365	0.03	0	0
100	SLE RA 6	0	0	1365	0.03	0	0
100	SLE RA 7	0	0	1365	0.03	0	0
100	SLE RA 8	0	0	1365	0.03	0	0
100	SLE RA 9	0	0	1365	0.03	0	0
100	SLE RA 10	0	-1	1780	0.01	0	0
100	SLE RA 11	0	-1	1780	0.01	0	0
100	SLE RA 12	0	-1	1780	0.01	0	0
100	SLE RA 13	0	-1	1780	0.01	0	0
100	SLE RA 14	0	-1	1780	0.01	0	0
100	SLE RA 15	0	-1	1780	0.01	0	0
100	SLE RA 16	0	-1	1780	0.01	0	0
100	SLE RA 17	0	-1	1780	0.01	0	0
100	SLE RA 18	0	-1	1959	0	0	0
100	SLE RA 19	0	-1	1959	0	0	0
100	SLE RA 20	0	-1	1959	0	0	0
100	SLE RA 21	0	-1	1959	0	0	0
100	SLE FR 1	0	0	1365	0.03	0	0
100	SLE FR 2	0	0	1365	0.03	0	0
100	SLE FR 3	0	0	1365	0.03	0	0
100	SLE FR 4	0	-1	1543	0.02	0	0
100	SLE FR 5	0	-1	1543	0.02	0	0
100	SLE FR 6	0	-1	1662	0.01	0	0
100	SLE QP 1	0	0	1365	0.03	0	0
100	SLE QP 2	0	-1	1543	0.02	0	0
100	SLD 1	-5	-37	1583	-4.06	9.67	-0.16
100	SLD 2	-5	-37	1583	-4.06	9.67	-0.16
100	SLD 3	-7	71	1528	7.69	5.52	-0.23
100	SLD 4	-7	71	1528	7.69	5.52	-0.23
100	SLD 5	2	-176	1639	-19.03	9.19	0.06
100	SLD 6	2	-176	1639	-19.03	9.19	0.06
100	SLD 7	-6	185	1455	20.14	-4.63	-0.18
100	SLD 8	-6	185	1455	20.14	-4.63	-0.18
100	SLD 9	6	-186	1631	-20.11	4.64	0.18
100	SLD 10	6	-186	1631	-20.11	4.64	0.18
100	SLD 11	-2	174	1447	19.06	-9.19	-0.06
100	SLD 12	-2	174	1447	19.06	-9.19	-0.06
100	SLD 13	7	-72	1558	-7.66	-5.52	0.23
100	SLD 14	7	-72	1558	-7.66	-5.52	0.23
100	SLD 15	5	36	1503	4.09	-9.67	0.16



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
100	SLD 16	5	36	1503	4.09	-9.67	0.16
100	SLV 1	-11	-95	1645	-10.44	24.57	-0.39
100	SLV 2	-11	-95	1645	-10.44	24.57	-0.39
100	SLV 3	-18	182	1504	19.71	13.93	-0.57
100	SLV 4	-18	182	1504	19.71	13.93	-0.57
100	SLV 5	6	-450	1788	-48.84	23.5	0.16
100	SLV 6	6	-450	1788	-48.84	23.5	0.16
100	SLV 7	-15	475	1317	51.65	-11.95	-0.45
100	SLV 8	-15	475	1317	51.65	-11.95	-0.45
100	SLV 9	15	-476	1769	-51.62	11.95	0.45
100	SLV 10	15	-476	1769	-51.62	11.95	0.45
100	SLV 11	-6	448	1298	48.88	-23.5	-0.16
100	SLV 12	-6	448	1298	48.88	-23.5	-0.16
100	SLV 13	18	-183	1582	-19.68	-13.93	0.57
100	SLV 14	18	-183	1582	-19.68	-13.93	0.57
100	SLV 15	11	94	1441	10.47	-24.56	0.39
100	SLV 16	11	94	1441	10.47	-24.56	0.39
101	SLU 1	0	-181	2054	6.63	0.11	0
101	SLU 2	0	-181	2054	6.63	0.11	0
101	SLU 3	0	-181	2054	6.63	0.11	0
101	SLU 4	0	-181	2054	6.63	0.11	0
101	SLU 5	0	-181	2054	6.63	0.11	0
101	SLU 6	0	-181	2054	6.63	0.11	0
101	SLU 7	0	-181	2054	6.63	0.11	0
101	SLU 8	0	-181	2054	6.63	0.11	0
101	SLU 9	0	-181	2054	6.63	0.11	0
101	SLU 10	0	-236	2550	8.73	0.27	0
101	SLU 11	0	-236	2550	8.73	0.27	0
101	SLU 12	0	-236	2550	8.73	0.27	0
101	SLU 13	0	-236	2550	8.73	0.27	0
101	SLU 14	0	-236	2550	8.73	0.27	0
101	SLU 15	0	-236	2550	8.73	0.27	0
101	SLU 16	0	-236	2550	8.73	0.27	0
101	SLU 17	0	-236	2550	8.73	0.27	0
101	SLU 18	0	-260	2762	9.63	0.34	0
101	SLU 19	0	-260	2762	9.63	0.34	0
101	SLU 20	0	-260	2762	9.63	0.34	0
101	SLU 21	0	-260	2762	9.63	0.34	0
101	SLU 22	0	-209	2304	7.7	0.16	0
101	SLU 23	0	-209	2304	7.7	0.16	0
101	SLU 24	0	-209	2304	7.7	0.16	0
101	SLU 25	0	-209	2304	7.7	0.16	0
101	SLU 26	0	-209	2304	7.7	0.16	0
101	SLU 27	0	-209	2304	7.7	0.16	0
101	SLU 28	0	-209	2304	7.7	0.16	0
101	SLU 29	0	-209	2304	7.7	0.16	0
101	SLU 30	0	-209	2304	7.7	0.16	0
101	SLU 31	0	-265	2799	9.79	0.32	0
101	SLU 32	0	-265	2799	9.79	0.32	0
101	SLU 33	0	-265	2799	9.79	0.32	0
101	SLU 34	0	-265	2799	9.79	0.32	0
101	SLU 35	0	-265	2799	9.79	0.32	0
101	SLU 36	0	-265	2799	9.79	0.32	0
101	SLU 37	0	-265	2799	9.79	0.32	0
101	SLU 38	0	-265	2799	9.79	0.32	0
101	SLU 39	0	-289	3012	10.69	0.39	0
101	SLU 40	0	-289	3012	10.69	0.39	0
101	SLU 41	0	-289	3012	10.69	0.39	0
101	SLU 42	0	-289	3012	10.69	0.39	0
101	SLU 43	0	-225	2585	8.25	0.13	0
101	SLU 44	0	-225	2585	8.25	0.13	0
101	SLU 45	0	-225	2585	8.25	0.13	0
101	SLU 46	0	-225	2585	8.25	0.13	0
101	SLU 47	0	-225	2585	8.25	0.13	0
101	SLU 48	0	-225	2585	8.25	0.13	0
101	SLU 49	0	-225	2585	8.25	0.13	0
101	SLU 50	0	-225	2585	8.25	0.13	0
101	SLU 51	0	-225	2585	8.25	0.13	0
101	SLU 52	0	-280	3080	10.35	0.29	0
101	SLU 53	0	-280	3080	10.35	0.29	0
101	SLU 54	0	-280	3080	10.35	0.29	0
101	SLU 55	0	-280	3080	10.35	0.29	0
101	SLU 56	0	-280	3080	10.35	0.29	0
101	SLU 57	0	-280	3080	10.35	0.29	0
101	SLU 58	0	-280	3080	10.35	0.29	0
101	SLU 59	0	-280	3080	10.35	0.29	0
101	SLU 60	0	-304	3292	11.25	0.36	0
101	SLU 61	0	-304	3292	11.25	0.36	0
101	SLU 62	0	-304	3292	11.25	0.36	0
101	SLU 63	0	-304	3292	11.25	0.36	0
101	SLU 64	0	-254	2835	9.32	0.17	0
101	SLU 65	0	-254	2835	9.32	0.17	0
101	SLU 66	0	-254	2835	9.32	0.17	0
101	SLU 67	0	-254	2835	9.32	0.17	0
101	SLU 68	0	-254	2835	9.32	0.17	0
101	SLU 69	0	-254	2835	9.32	0.17	0
101	SLU 70	0	-254	2835	9.32	0.17	0
101	SLU 71	0	-254	2835	9.32	0.17	0
101	SLU 72	0	-254	2835	9.32	0.17	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
101	SLU 73	0	-309	3330	11.42	0.34	0
101	SLU 74	0	-309	3330	11.42	0.34	0
101	SLU 75	0	-309	3330	11.42	0.34	0
101	SLU 76	0	-309	3330	11.42	0.34	0
101	SLU 77	0	-309	3330	11.42	0.34	0
101	SLU 78	0	-309	3330	11.42	0.34	0
101	SLU 79	0	-309	3330	11.42	0.34	0
101	SLU 80	0	-309	3330	11.42	0.34	0
101	SLU 81	0	-333	3542	12.32	0.41	0
101	SLU 82	0	-333	3542	12.32	0.41	0
101	SLU 83	0	-333	3542	12.32	0.41	0
101	SLU 84	0	-333	3542	12.32	0.41	0
101	SLE RA 1	0	-189	2125	6.93	0.12	0
101	SLE RA 2	0	-189	2125	6.93	0.12	0
101	SLE RA 3	0	-189	2125	6.93	0.12	0
101	SLE RA 4	0	-189	2125	6.93	0.12	0
101	SLE RA 5	0	-189	2125	6.93	0.12	0
101	SLE RA 6	0	-189	2125	6.93	0.12	0
101	SLE RA 7	0	-189	2125	6.93	0.12	0
101	SLE RA 8	0	-189	2125	6.93	0.12	0
101	SLE RA 9	0	-189	2125	6.93	0.12	0
101	SLE RA 10	0	-226	2456	8.33	0.23	0
101	SLE RA 11	0	-226	2456	8.33	0.23	0
101	SLE RA 12	0	-226	2456	8.33	0.23	0
101	SLE RA 13	0	-226	2456	8.33	0.23	0
101	SLE RA 14	0	-226	2456	8.33	0.23	0
101	SLE RA 15	0	-226	2456	8.33	0.23	0
101	SLE RA 16	0	-226	2456	8.33	0.23	0
101	SLE RA 17	0	-226	2456	8.33	0.23	0
101	SLE RA 18	0	-242	2597	8.93	0.28	0
101	SLE RA 19	0	-242	2597	8.93	0.28	0
101	SLE RA 20	0	-242	2597	8.93	0.28	0
101	SLE RA 21	0	-242	2597	8.93	0.28	0
101	SLE FR 1	0	-189	2125	6.93	0.12	0
101	SLE FR 2	0	-189	2125	6.93	0.12	0
101	SLE FR 3	0	-189	2125	6.93	0.12	0
101	SLE FR 4	0	-205	2267	7.53	0.17	0
101	SLE FR 5	0	-205	2267	7.53	0.17	0
101	SLE FR 6	0	-215	2361	7.93	0.2	0
101	SLE QP 1	0	-189	2125	6.93	0.12	0
101	SLE QP 2	0	-205	2267	7.53	0.17	0
101	SLD 1	24	-25	2715	7.57	18.18	0.01
101	SLD 2	24	-25	2715	7.57	18.18	0.01
101	SLD 3	29	-201	2568	14.42	22.56	0.01
101	SLD 4	29	-201	2568	14.42	22.56	0.01
101	SLD 5	0	116	2623	-2.84	-1.06	0.01
101	SLD 6	0	116	2623	-2.84	-1.06	0.01
101	SLD 7	16	-471	2136	19.98	13.52	0
101	SLD 8	16	-471	2136	19.98	13.52	0
101	SLD 9	-16	61	2398	-4.91	-13.18	0
101	SLD 10	-16	61	2398	-4.91	-13.18	0
101	SLD 11	0	-526	1911	17.9	1.4	-0.01
101	SLD 12	0	-526	1911	17.9	1.4	-0.01
101	SLD 13	-29	-208	1966	0.65	-22.22	-0.01
101	SLD 14	-29	-208	1966	0.65	-22.22	-0.01
101	SLD 15	-24	-384	1820	7.49	-17.84	-0.01
101	SLD 16	-24	-384	1820	7.49	-17.84	-0.01
101	SLV 1	57	219	3402	7.66	43.04	0.02
101	SLV 2	57	219	3402	7.66	43.04	0.02
101	SLV 3	68	-195	3040	23.73	54.15	0.01
101	SLV 4	68	-195	3040	23.73	54.15	0.01
101	SLV 5	-1	549	3157	-16.81	-3.81	0.01
101	SLV 6	-1	549	3157	-16.81	-3.81	0.01
101	SLV 7	39	-829	1950	36.77	33.21	0
101	SLV 8	39	-829	1950	36.77	33.21	0
101	SLV 9	-39	419	2584	-21.71	-32.87	0
101	SLV 10	-39	419	2584	-21.71	-32.87	0
101	SLV 11	1	-959	1377	31.88	4.15	-0.01
101	SLV 12	1	-959	1377	31.88	4.15	-0.01
101	SLV 13	-69	-215	1494	-8.67	-53.81	-0.01
101	SLV 14	-69	-215	1494	-8.67	-53.81	-0.01
101	SLV 15	-57	-628	1132	7.41	-42.7	-0.02
101	SLV 16	-57	-628	1132	7.41	-42.7	-0.02
102	SLU 1	0	-143	1612	5.45	-0.09	0
102	SLU 2	0	-143	1612	5.45	-0.09	0
102	SLU 3	0	-143	1612	5.45	-0.09	0
102	SLU 4	0	-143	1612	5.45	-0.09	0
102	SLU 5	0	-143	1612	5.45	-0.09	0
102	SLU 6	0	-143	1612	5.45	-0.09	0
102	SLU 7	0	-143	1612	5.45	-0.09	0
102	SLU 8	0	-143	1612	5.45	-0.09	0
102	SLU 9	0	-143	1612	5.45	-0.09	0
102	SLU 10	0	-208	1890	7.92	-0.11	0
102	SLU 11	0	-208	1890	7.92	-0.11	0
102	SLU 12	0	-208	1890	7.92	-0.11	0
102	SLU 13	0	-208	1890	7.92	-0.11	0
102	SLU 14	0	-208	1890	7.92	-0.11	0
102	SLU 15	0	-208	1890	7.92	-0.11	0
102	SLU 16	0	-208	1890	7.92	-0.11	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
102	SLU 17	0	-208	1890	7.92	-0.11	0
102	SLU 18	0	-237	2009	8.97	-0.12	0
102	SLU 19	0	-237	2009	8.97	-0.12	0
102	SLU 20	0	-237	2009	8.97	-0.12	0
102	SLU 21	0	-237	2009	8.97	-0.12	0
102	SLU 22	0	-173	1760	6.6	-0.11	0
102	SLU 23	0	-173	1760	6.6	-0.11	0
102	SLU 24	0	-173	1760	6.6	-0.11	0
102	SLU 25	0	-173	1760	6.6	-0.11	0
102	SLU 26	0	-173	1760	6.6	-0.11	0
102	SLU 27	0	-173	1760	6.6	-0.11	0
102	SLU 28	0	-173	1760	6.6	-0.11	0
102	SLU 29	0	-173	1760	6.6	-0.11	0
102	SLU 30	0	-173	1760	6.6	-0.11	0
102	SLU 31	0	-239	2038	9.07	-0.13	0
102	SLU 32	0	-239	2038	9.07	-0.13	0
102	SLU 33	0	-239	2038	9.07	-0.13	0
102	SLU 34	0	-239	2038	9.07	-0.13	0
102	SLU 35	0	-239	2038	9.07	-0.13	0
102	SLU 36	0	-239	2038	9.07	-0.13	0
102	SLU 37	0	-239	2038	9.07	-0.13	0
102	SLU 38	0	-239	2038	9.07	-0.13	0
102	SLU 39	0	-267	2157	10.13	-0.14	0
102	SLU 40	0	-267	2157	10.13	-0.14	0
102	SLU 41	0	-267	2157	10.13	-0.14	0
102	SLU 42	0	-267	2157	10.13	-0.14	0
102	SLU 43	0	-175	2045	6.69	-0.12	0
102	SLU 44	0	-175	2045	6.69	-0.12	0
102	SLU 45	0	-175	2045	6.69	-0.12	0
102	SLU 46	0	-175	2045	6.69	-0.12	0
102	SLU 47	0	-175	2045	6.69	-0.12	0
102	SLU 48	0	-175	2045	6.69	-0.12	0
102	SLU 49	0	-175	2045	6.69	-0.12	0
102	SLU 50	0	-175	2045	6.69	-0.12	0
102	SLU 51	0	-175	2045	6.69	-0.12	0
102	SLU 52	0	-241	2323	9.16	-0.14	0
102	SLU 53	0	-241	2323	9.16	-0.14	0
102	SLU 54	0	-241	2323	9.16	-0.14	0
102	SLU 55	0	-241	2323	9.16	-0.14	0
102	SLU 56	0	-241	2323	9.16	-0.14	0
102	SLU 57	0	-241	2323	9.16	-0.14	0
102	SLU 58	0	-241	2323	9.16	-0.14	0
102	SLU 59	0	-241	2323	9.16	-0.14	0
102	SLU 60	0	-269	2442	10.21	-0.15	0
102	SLU 61	0	-269	2442	10.21	-0.15	0
102	SLU 62	0	-269	2442	10.21	-0.15	0
102	SLU 63	0	-269	2442	10.21	-0.15	0
102	SLU 64	0	-206	2193	7.84	-0.13	0
102	SLU 65	0	-206	2193	7.84	-0.13	0
102	SLU 66	0	-206	2193	7.84	-0.13	0
102	SLU 67	0	-206	2193	7.84	-0.13	0
102	SLU 68	0	-206	2193	7.84	-0.13	0
102	SLU 69	0	-206	2193	7.84	-0.13	0
102	SLU 70	0	-206	2193	7.84	-0.13	0
102	SLU 71	0	-206	2193	7.84	-0.13	0
102	SLU 72	0	-206	2193	7.84	-0.13	0
102	SLU 73	0	-271	2471	10.31	-0.15	0
102	SLU 74	0	-271	2471	10.31	-0.15	0
102	SLU 75	0	-271	2471	10.31	-0.15	0
102	SLU 76	0	-271	2471	10.31	-0.15	0
102	SLU 77	0	-271	2471	10.31	-0.15	0
102	SLU 78	0	-271	2471	10.31	-0.15	0
102	SLU 79	0	-271	2471	10.31	-0.15	0
102	SLU 80	0	-271	2471	10.31	-0.15	0
102	SLU 81	0	-300	2590	11.37	-0.16	0
102	SLU 82	0	-300	2590	11.37	-0.16	0
102	SLU 83	0	-300	2590	11.37	-0.16	0
102	SLU 84	0	-300	2590	11.37	-0.16	0
102	SLE RA 1	0	-152	1655	5.78	-0.1	0
102	SLE RA 2	0	-152	1655	5.78	-0.1	0
102	SLE RA 3	0	-152	1655	5.78	-0.1	0
102	SLE RA 4	0	-152	1655	5.78	-0.1	0
102	SLE RA 5	0	-152	1655	5.78	-0.1	0
102	SLE RA 6	0	-152	1655	5.78	-0.1	0
102	SLE RA 7	0	-152	1655	5.78	-0.1	0
102	SLE RA 8	0	-152	1655	5.78	-0.1	0
102	SLE RA 9	0	-152	1655	5.78	-0.1	0
102	SLE RA 10	0	-195	1840	7.42	-0.11	0
102	SLE RA 11	0	-195	1840	7.42	-0.11	0
102	SLE RA 12	0	-195	1840	7.42	-0.11	0
102	SLE RA 13	0	-195	1840	7.42	-0.11	0
102	SLE RA 14	0	-195	1840	7.42	-0.11	0
102	SLE RA 15	0	-195	1840	7.42	-0.11	0
102	SLE RA 16	0	-195	1840	7.42	-0.11	0
102	SLE RA 17	0	-195	1840	7.42	-0.11	0
102	SLE RA 18	0	-214	1919	8.13	-0.12	0
102	SLE RA 19	0	-214	1919	8.13	-0.12	0
102	SLE RA 20	0	-214	1919	8.13	-0.12	0
102	SLE RA 21	0	-214	1919	8.13	-0.12	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
102	SLE FR 1	0	-152	1655	5.78	-0.1	0
102	SLE FR 2	0	-152	1655	5.78	-0.1	0
102	SLE FR 3	0	-152	1655	5.78	-0.1	0
102	SLE FR 4	0	-170	1734	6.48	-0.1	0
102	SLE FR 5	0	-170	1734	6.48	-0.1	0
102	SLE FR 6	0	-183	1787	6.95	-0.11	0
102	SLE QP 1	0	-152	1655	5.78	-0.1	0
102	SLE QP 2	0	-170	1734	6.48	-0.1	0
102	SLD 1	35	8	1654	-0.35	30.36	0.01
102	SLD 2	35	8	1654	-0.35	30.36	0.01
102	SLD 3	43	-171	1686	6.51	38.46	0.01
102	SLD 4	43	-171	1686	6.51	38.46	0.01
102	SLD 5	0	154	1662	-5.97	-3.25	0
102	SLD 6	0	154	1662	-5.97	-3.25	0
102	SLD 7	24	-441	1768	16.9	23.75	0.01
102	SLD 8	24	-441	1768	16.9	23.75	0.01
102	SLD 9	-24	101	1700	-3.93	-23.95	-0.01
102	SLD 10	-24	101	1700	-3.93	-23.95	-0.01
102	SLD 11	1	-495	1807	18.94	3.04	0
102	SLD 12	1	-495	1807	18.94	3.04	0
102	SLD 13	-43	-170	1782	6.45	-38.66	-0.01
102	SLD 14	-43	-170	1782	6.45	-38.66	-0.01
102	SLD 15	-35	-349	1814	13.32	-30.57	-0.01
102	SLD 16	-35	-349	1814	13.32	-30.57	-0.01
102	SLV 1	86	249	1545	-9.58	74.9	0.02
102	SLV 2	86	249	1545	-9.58	74.9	0.02
102	SLV 3	105	-171	1620	6.57	95.6	0.02
102	SLV 4	105	-171	1620	6.57	95.6	0.02
102	SLV 5	-2	593	1563	-22.83	-9.01	0
102	SLV 6	-2	593	1563	-22.83	-9.01	0
102	SLV 7	60	-808	1814	31	60.01	0.02
102	SLV 8	60	-808	1814	31	60.01	0.02
102	SLV 9	-60	468	1654	-18.03	-60.22	-0.02
102	SLV 10	-60	468	1654	-18.03	-60.22	-0.02
102	SLV 11	2	-934	1905	35.8	8.8	0
102	SLV 12	2	-934	1905	35.8	8.8	0
102	SLV 13	-105	-169	1848	6.4	-95.81	-0.02
102	SLV 14	-105	-169	1848	6.4	-95.81	-0.02
102	SLV 15	-86	-590	1923	22.55	-75.1	-0.02
102	SLV 16	-86	-590	1923	22.55	-75.1	-0.02
103	SLU 1	0	0	1251	0.03	0	0
103	SLU 2	0	0	1251	0.03	0	0
103	SLU 3	0	0	1251	0.03	0	0
103	SLU 4	0	0	1251	0.03	0	0
103	SLU 5	0	0	1251	0.03	0	0
103	SLU 6	0	0	1251	0.03	0	0
103	SLU 7	0	0	1251	0.03	0	0
103	SLU 8	0	0	1251	0.03	0	0
103	SLU 9	0	0	1251	0.03	0	0
103	SLU 10	0	0	1829	-0.01	0	0
103	SLU 11	0	0	1829	-0.01	0	0
103	SLU 12	0	0	1829	-0.01	0	0
103	SLU 13	0	0	1829	-0.01	0	0
103	SLU 14	0	0	1829	-0.01	0	0
103	SLU 15	0	0	1829	-0.01	0	0
103	SLU 16	0	0	1829	-0.01	0	0
103	SLU 17	0	0	1829	-0.01	0	0
103	SLU 18	0	1	2077	-0.03	0	0
103	SLU 19	0	1	2077	-0.03	0	0
103	SLU 20	0	1	2077	-0.03	0	0
103	SLU 21	0	1	2077	-0.03	0	0
103	SLU 22	0	0	1531	0.02	0	0
103	SLU 23	0	0	1531	0.02	0	0
103	SLU 24	0	0	1531	0.02	0	0
103	SLU 25	0	0	1531	0.02	0	0
103	SLU 26	0	0	1531	0.02	0	0
103	SLU 27	0	0	1531	0.02	0	0
103	SLU 28	0	0	1531	0.02	0	0
103	SLU 29	0	0	1531	0.02	0	0
103	SLU 30	0	0	1531	0.02	0	0
103	SLU 31	0	1	2110	-0.03	0	0
103	SLU 32	0	1	2110	-0.03	0	0
103	SLU 33	0	1	2110	-0.03	0	0
103	SLU 34	0	1	2110	-0.03	0	0
103	SLU 35	0	1	2110	-0.03	0	0
103	SLU 36	0	1	2110	-0.03	0	0
103	SLU 37	0	1	2110	-0.03	0	0
103	SLU 38	0	1	2110	-0.03	0	0
103	SLU 39	0	1	2358	-0.05	0	0
103	SLU 40	0	1	2358	-0.05	0	0
103	SLU 41	0	1	2358	-0.05	0	0
103	SLU 42	0	1	2358	-0.05	0	0
103	SLU 43	0	0	1530	0.05	0	0
103	SLU 44	0	0	1530	0.05	0	0
103	SLU 45	0	0	1530	0.05	0	0
103	SLU 46	0	0	1530	0.05	0	0
103	SLU 47	0	0	1530	0.05	0	0
103	SLU 48	0	0	1530	0.05	0	0
103	SLU 49	0	0	1530	0.05	0	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
103	SLU 50	0	0	1530	0.05	0	0
103	SLU 51	0	0	1530	0.05	0	0
103	SLU 52	0	1	2108	0	0	0
103	SLU 53	0	1	2108	0	0	0
103	SLU 54	0	1	2108	0	0	0
103	SLU 55	0	1	2108	0	0	0
103	SLU 56	0	1	2108	0	0	0
103	SLU 57	0	1	2108	0	0	0
103	SLU 58	0	1	2108	0	0	0
103	SLU 59	0	1	2108	0	0	0
103	SLU 60	0	1	2356	-0.02	0	0
103	SLU 61	0	1	2356	-0.02	0	0
103	SLU 62	0	1	2356	-0.02	0	0
103	SLU 63	0	1	2356	-0.02	0	0
103	SLU 64	0	0	1810	0.03	0	0
103	SLU 65	0	0	1810	0.03	0	0
103	SLU 66	0	0	1810	0.03	0	0
103	SLU 67	0	0	1810	0.03	0	0
103	SLU 68	0	0	1810	0.03	0	0
103	SLU 69	0	0	1810	0.03	0	0
103	SLU 70	0	0	1810	0.03	0	0
103	SLU 71	0	0	1810	0.03	0	0
103	SLU 72	0	0	1810	0.03	0	0
103	SLU 73	0	1	2389	-0.01	0	0
103	SLU 74	0	1	2389	-0.01	0	0
103	SLU 75	0	1	2389	-0.01	0	0
103	SLU 76	0	1	2389	-0.01	0	0
103	SLU 77	0	1	2389	-0.01	0	0
103	SLU 78	0	1	2389	-0.01	0	0
103	SLU 79	0	1	2389	-0.01	0	0
103	SLU 80	0	1	2389	-0.01	0	0
103	SLU 81	0	1	2637	-0.03	0	0
103	SLU 82	0	1	2637	-0.03	0	0
103	SLU 83	0	1	2637	-0.03	0	0
103	SLU 84	0	1	2637	-0.03	0	0
103	SLE RA 1	0	0	1331	0.03	0	0
103	SLE RA 2	0	0	1331	0.03	0	0
103	SLE RA 3	0	0	1331	0.03	0	0
103	SLE RA 4	0	0	1331	0.03	0	0
103	SLE RA 5	0	0	1331	0.03	0	0
103	SLE RA 6	0	0	1331	0.03	0	0
103	SLE RA 7	0	0	1331	0.03	0	0
103	SLE RA 8	0	0	1331	0.03	0	0
103	SLE RA 9	0	0	1331	0.03	0	0
103	SLE RA 10	0	0	1717	0	0	0
103	SLE RA 11	0	0	1717	0	0	0
103	SLE RA 12	0	0	1717	0	0	0
103	SLE RA 13	0	0	1717	0	0	0
103	SLE RA 14	0	0	1717	0	0	0
103	SLE RA 15	0	0	1717	0	0	0
103	SLE RA 16	0	0	1717	0	0	0
103	SLE RA 17	0	0	1717	0	0	0
103	SLE RA 18	0	0	1882	-0.01	0	0
103	SLE RA 19	0	0	1882	-0.01	0	0
103	SLE RA 20	0	0	1882	-0.01	0	0
103	SLE RA 21	0	0	1882	-0.01	0	0
103	SLE FR 1	0	0	1331	0.03	0	0
103	SLE FR 2	0	0	1331	0.03	0	0
103	SLE FR 3	0	0	1331	0.03	0	0
103	SLE FR 4	0	0	1496	0.02	0	0
103	SLE FR 5	0	0	1496	0.02	0	0
103	SLE FR 6	0	0	1606	0.01	0	0
103	SLE QP 1	0	0	1331	0.03	0	0
103	SLE QP 2	0	0	1496	0.02	0	0
103	SLD 1	-5	-20	1535	-5.67	9.72	0.04
103	SLD 2	-5	-20	1535	-5.67	9.72	0.04
103	SLD 3	-8	40	1480	10.81	5.69	0.05
103	SLD 4	-8	40	1480	10.81	5.69	0.05
103	SLD 5	3	-96	1590	-26.69	9.03	-0.01
103	SLD 6	3	-96	1590	-26.69	9.03	-0.01
103	SLD 7	-7	102	1409	28.25	-4.4	0.04
103	SLD 8	-7	102	1409	28.25	-4.4	0.04
103	SLD 9	7	-102	1583	-28.22	4.41	-0.04
103	SLD 10	7	-102	1583	-28.22	4.41	-0.04
103	SLD 11	-3	97	1402	26.72	-9.02	0.01
103	SLD 12	-3	97	1402	26.72	-9.02	0.01
103	SLD 13	8	-39	1512	-10.78	-5.68	-0.05
103	SLD 14	8	-39	1512	-10.78	-5.68	-0.05
103	SLD 15	5	20	1458	5.7	-9.71	-0.04
103	SLD 16	5	20	1458	5.7	-9.71	-0.04
103	SLV 1	-13	-51	1594	-14.58	24.72	0.09
103	SLV 2	-13	-51	1594	-14.58	24.72	0.09
103	SLV 3	-20	101	1455	27.71	14.39	0.12
103	SLV 4	-20	101	1455	27.71	14.39	0.12
103	SLV 5	7	-246	1737	-68.49	23.08	-0.03
103	SLV 6	7	-246	1737	-68.49	23.08	-0.03
103	SLV 7	-17	262	1273	72.45	-11.35	0.09
103	SLV 8	-17	262	1273	72.45	-11.35	0.09
103	SLV 9	17	-261	1720	-72.42	11.35	-0.09



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
103	SLV 10	17	-261	1720	-72.42	11.35	-0.09
103	SLV 11	-7	247	1256	68.52	-23.08	0.03
103	SLV 12	-7	247	1256	68.52	-23.08	0.03
103	SLV 13	20	-101	1537	-27.67	-14.39	-0.13
103	SLV 14	20	-101	1537	-27.67	-14.39	-0.13
103	SLV 15	13	52	1398	14.61	-24.72	-0.09
103	SLV 16	13	52	1398	14.61	-24.72	-0.09
104	SLU 1	0	-242	2030	9.34	0.17	0
104	SLU 2	0	-242	2030	9.34	0.17	0
104	SLU 3	0	-242	2030	9.34	0.17	0
104	SLU 4	0	-242	2030	9.34	0.17	0
104	SLU 5	0	-242	2030	9.34	0.17	0
104	SLU 6	0	-242	2030	9.34	0.17	0
104	SLU 7	0	-242	2030	9.34	0.17	0
104	SLU 8	0	-242	2030	9.34	0.17	0
104	SLU 9	0	-242	2030	9.34	0.17	0
104	SLU 10	0	-314	2533	12.21	0.36	0
104	SLU 11	0	-314	2533	12.21	0.36	0
104	SLU 12	0	-314	2533	12.21	0.36	0
104	SLU 13	0	-314	2533	12.21	0.36	0
104	SLU 14	0	-314	2533	12.21	0.36	0
104	SLU 15	0	-314	2533	12.21	0.36	0
104	SLU 16	0	-314	2533	12.21	0.36	0
104	SLU 17	0	-314	2533	12.21	0.36	0
104	SLU 18	0	-345	2748	13.44	0.44	0
104	SLU 19	0	-345	2748	13.44	0.44	0
104	SLU 20	0	-345	2748	13.44	0.44	0
104	SLU 21	0	-345	2748	13.44	0.44	0
104	SLU 22	0	-278	2280	10.77	0.23	0
104	SLU 23	0	-278	2280	10.77	0.23	0
104	SLU 24	0	-278	2280	10.77	0.23	0
104	SLU 25	0	-278	2280	10.77	0.23	0
104	SLU 26	0	-278	2280	10.77	0.23	0
104	SLU 27	0	-278	2280	10.77	0.23	0
104	SLU 28	0	-278	2280	10.77	0.23	0
104	SLU 29	0	-278	2280	10.77	0.23	0
104	SLU 30	0	-278	2280	10.77	0.23	0
104	SLU 31	0	-351	2783	13.64	0.42	0
104	SLU 32	0	-351	2783	13.64	0.42	0
104	SLU 33	0	-351	2783	13.64	0.42	0
104	SLU 34	0	-351	2783	13.64	0.42	0
104	SLU 35	0	-351	2783	13.64	0.42	0
104	SLU 36	0	-351	2783	13.64	0.42	0
104	SLU 37	0	-351	2783	13.64	0.42	0
104	SLU 38	0	-351	2783	13.64	0.42	0
104	SLU 39	0	-382	2999	14.87	0.5	0
104	SLU 40	0	-382	2999	14.87	0.5	0
104	SLU 41	0	-382	2999	14.87	0.5	0
104	SLU 42	0	-382	2999	14.87	0.5	0
104	SLU 43	0	-302	2553	11.65	0.2	0
104	SLU 44	0	-302	2553	11.65	0.2	0
104	SLU 45	0	-302	2553	11.65	0.2	0
104	SLU 46	0	-302	2553	11.65	0.2	0
104	SLU 47	0	-302	2553	11.65	0.2	0
104	SLU 48	0	-302	2553	11.65	0.2	0
104	SLU 49	0	-302	2553	11.65	0.2	0
104	SLU 50	0	-302	2553	11.65	0.2	0
104	SLU 51	0	-302	2553	11.65	0.2	0
104	SLU 52	0	-374	3056	14.52	0.39	0
104	SLU 53	0	-374	3056	14.52	0.39	0
104	SLU 54	0	-374	3056	14.52	0.39	0
104	SLU 55	0	-374	3056	14.52	0.39	0
104	SLU 56	0	-374	3056	14.52	0.39	0
104	SLU 57	0	-374	3056	14.52	0.39	0
104	SLU 58	0	-374	3056	14.52	0.39	0
104	SLU 59	0	-374	3056	14.52	0.39	0
104	SLU 60	0	-405	3271	15.75	0.48	0
104	SLU 61	0	-405	3271	15.75	0.48	0
104	SLU 62	0	-405	3271	15.75	0.48	0
104	SLU 63	0	-405	3271	15.75	0.48	0
104	SLU 64	0	-338	2803	13.08	0.26	0
104	SLU 65	0	-338	2803	13.08	0.26	0
104	SLU 66	0	-338	2803	13.08	0.26	0
104	SLU 67	0	-338	2803	13.08	0.26	0
104	SLU 68	0	-338	2803	13.08	0.26	0
104	SLU 69	0	-338	2803	13.08	0.26	0
104	SLU 70	0	-338	2803	13.08	0.26	0
104	SLU 71	0	-338	2803	13.08	0.26	0
104	SLU 72	0	-338	2803	13.08	0.26	0
104	SLU 73	0	-411	3306	15.95	0.45	0
104	SLU 74	0	-411	3306	15.95	0.45	0
104	SLU 75	0	-411	3306	15.95	0.45	0
104	SLU 76	0	-411	3306	15.95	0.45	0
104	SLU 77	0	-411	3306	15.95	0.45	0
104	SLU 78	0	-411	3306	15.95	0.45	0
104	SLU 79	0	-411	3306	15.95	0.45	0
104	SLU 80	0	-411	3306	15.95	0.45	0
104	SLU 81	0	-442	3522	17.18	0.53	0
104	SLU 82	0	-442	3522	17.18	0.53	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
104	SLU 83	0	-442	3522	17.18	0.53	0
104	SLU 84	0	-442	3522	17.18	0.53	0
104	SLE RA 1	0	-252	2101	9.75	0.19	0
104	SLE RA 2	0	-252	2101	9.75	0.19	0
104	SLE RA 3	0	-252	2101	9.75	0.19	0
104	SLE RA 4	0	-252	2101	9.75	0.19	0
104	SLE RA 5	0	-252	2101	9.75	0.19	0
104	SLE RA 6	0	-252	2101	9.75	0.19	0
104	SLE RA 7	0	-252	2101	9.75	0.19	0
104	SLE RA 8	0	-252	2101	9.75	0.19	0
104	SLE RA 9	0	-252	2101	9.75	0.19	0
104	SLE RA 10	0	-301	2437	11.66	0.31	0
104	SLE RA 11	0	-301	2437	11.66	0.31	0
104	SLE RA 12	0	-301	2437	11.66	0.31	0
104	SLE RA 13	0	-301	2437	11.66	0.31	0
104	SLE RA 14	0	-301	2437	11.66	0.31	0
104	SLE RA 15	0	-301	2437	11.66	0.31	0
104	SLE RA 16	0	-301	2437	11.66	0.31	0
104	SLE RA 17	0	-301	2437	11.66	0.31	0
104	SLE RA 18	0	-321	2580	12.48	0.37	0
104	SLE RA 19	0	-321	2580	12.48	0.37	0
104	SLE RA 20	0	-321	2580	12.48	0.37	0
104	SLE RA 21	0	-321	2580	12.48	0.37	0
104	SLE FR 1	0	-252	2101	9.75	0.19	0
104	SLE FR 2	0	-252	2101	9.75	0.19	0
104	SLE FR 3	0	-252	2101	9.75	0.19	0
104	SLE FR 4	0	-273	2245	10.57	0.24	0
104	SLE FR 5	0	-273	2245	10.57	0.24	0
104	SLE FR 6	0	-287	2341	11.11	0.28	0
104	SLE QP 1	0	-252	2101	9.75	0.19	0
104	SLE QP 2	0	-273	2245	10.57	0.24	0
104	SLD 1	18	-95	2786	10.65	15.04	0.01
104	SLD 2	18	-95	2786	10.65	15.04	0.01
104	SLD 3	22	-272	2602	17.39	18.37	0.01
104	SLD 4	22	-272	2602	17.39	18.37	0.01
104	SLD 5	0	49	2686	0.38	-0.36	0.01
104	SLD 6	0	49	2686	0.38	-0.36	0.01
104	SLD 7	12	-541	2073	22.83	10.73	0
104	SLD 8	12	-541	2073	22.83	10.73	0
104	SLD 9	-12	-5	2417	-1.69	-10.24	0.01
104	SLD 10	-12	-5	2417	-1.69	-10.24	0.01
104	SLD 11	0	-595	1804	20.76	0.85	-0.01
104	SLD 12	0	-595	1804	20.76	0.85	-0.01
104	SLD 13	-22	-274	1888	3.75	-17.89	0
104	SLD 14	-22	-274	1888	3.75	-17.89	0
104	SLD 15	-18	-451	1704	10.49	-14.56	-0.01
104	SLD 16	-18	-451	1704	10.49	-14.56	-0.01
104	SLV 1	42	146	3617	10.78	35.54	0.02
104	SLV 2	42	146	3617	10.78	35.54	0.02
104	SLV 3	52	-270	3161	26.58	43.99	0.02
104	SLV 4	52	-270	3161	26.58	43.99	0.02
104	SLV 5	-2	483	3348	-13.34	-1.97	0.02
104	SLV 6	-2	483	3348	-13.34	-1.97	0.02
104	SLV 7	30	-903	1829	39.34	26.17	-0.01
104	SLV 8	30	-903	1829	39.34	26.17	-0.01
104	SLV 9	-30	356	2661	-18.2	-25.69	0.01
104	SLV 10	-30	356	2661	-18.2	-25.69	0.01
104	SLV 11	2	-1029	1143	34.47	2.46	-0.02
104	SLV 12	2	-1029	1143	34.47	2.46	-0.02
104	SLV 13	-52	-276	1329	-5.44	-43.5	-0.01
104	SLV 14	-52	-276	1329	-5.44	-43.5	-0.01
104	SLV 15	-42	-692	873	10.36	-35.06	-0.02
104	SLV 16	-42	-692	873	10.36	-35.06	-0.02
105	SLU 1	0	-73	1665	3.23	-0.09	0
105	SLU 2	0	-73	1665	3.23	-0.09	0
105	SLU 3	0	-73	1665	3.23	-0.09	0
105	SLU 4	0	-73	1665	3.23	-0.09	0
105	SLU 5	0	-73	1665	3.23	-0.09	0
105	SLU 6	0	-73	1665	3.23	-0.09	0
105	SLU 7	0	-73	1665	3.23	-0.09	0
105	SLU 8	0	-73	1665	3.23	-0.09	0
105	SLU 9	0	-73	1665	3.23	-0.09	0
105	SLU 10	0	-120	1944	5.16	-0.11	0
105	SLU 11	0	-120	1944	5.16	-0.11	0
105	SLU 12	0	-120	1944	5.16	-0.11	0
105	SLU 13	0	-120	1944	5.16	-0.11	0
105	SLU 14	0	-120	1944	5.16	-0.11	0
105	SLU 15	0	-120	1944	5.16	-0.11	0
105	SLU 16	0	-120	1944	5.16	-0.11	0
105	SLU 17	0	-120	1944	5.16	-0.11	0
105	SLU 18	0	-140	2064	5.99	-0.11	0
105	SLU 19	0	-140	2064	5.99	-0.11	0
105	SLU 20	0	-140	2064	5.99	-0.11	0
105	SLU 21	0	-140	2064	5.99	-0.11	0
105	SLU 22	0	-93	1815	4.07	-0.11	0
105	SLU 23	0	-93	1815	4.07	-0.11	0
105	SLU 24	0	-93	1815	4.07	-0.11	0
105	SLU 25	0	-93	1815	4.07	-0.11	0
105	SLU 26	0	-93	1815	4.07	-0.11	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
105	SLU 27	0	-93	1815	4.07	-0.11	0
105	SLU 28	0	-93	1815	4.07	-0.11	0
105	SLU 29	0	-93	1815	4.07	-0.11	0
105	SLU 30	0	-93	1815	4.07	-0.11	0
105	SLU 31	0	-140	2094	6	-0.12	0
105	SLU 32	0	-140	2094	6	-0.12	0
105	SLU 33	0	-140	2094	6	-0.12	0
105	SLU 34	0	-140	2094	6	-0.12	0
105	SLU 35	0	-140	2094	6	-0.12	0
105	SLU 36	0	-140	2094	6	-0.12	0
105	SLU 37	0	-140	2094	6	-0.12	0
105	SLU 38	0	-140	2094	6	-0.12	0
105	SLU 39	0	-161	2213	6.83	-0.13	0
105	SLU 40	0	-161	2213	6.83	-0.13	0
105	SLU 41	0	-161	2213	6.83	-0.13	0
105	SLU 42	0	-161	2213	6.83	-0.13	0
105	SLU 43	0	-88	2113	3.91	-0.12	0
105	SLU 44	0	-88	2113	3.91	-0.12	0
105	SLU 45	0	-88	2113	3.91	-0.12	0
105	SLU 46	0	-88	2113	3.91	-0.12	0
105	SLU 47	0	-88	2113	3.91	-0.12	0
105	SLU 48	0	-88	2113	3.91	-0.12	0
105	SLU 49	0	-88	2113	3.91	-0.12	0
105	SLU 50	0	-88	2113	3.91	-0.12	0
105	SLU 51	0	-88	2113	3.91	-0.12	0
105	SLU 52	0	-135	2392	5.84	-0.13	0
105	SLU 53	0	-135	2392	5.84	-0.13	0
105	SLU 54	0	-135	2392	5.84	-0.13	0
105	SLU 55	0	-135	2392	5.84	-0.13	0
105	SLU 56	0	-135	2392	5.84	-0.13	0
105	SLU 57	0	-135	2392	5.84	-0.13	0
105	SLU 58	0	-135	2392	5.84	-0.13	0
105	SLU 59	0	-135	2392	5.84	-0.13	0
105	SLU 60	0	-156	2512	6.67	-0.14	0
105	SLU 61	0	-156	2512	6.67	-0.14	0
105	SLU 62	0	-156	2512	6.67	-0.14	0
105	SLU 63	0	-156	2512	6.67	-0.14	0
105	SLU 64	0	-108	2263	4.75	-0.13	0
105	SLU 65	0	-108	2263	4.75	-0.13	0
105	SLU 66	0	-108	2263	4.75	-0.13	0
105	SLU 67	0	-108	2263	4.75	-0.13	0
105	SLU 68	0	-108	2263	4.75	-0.13	0
105	SLU 69	0	-108	2263	4.75	-0.13	0
105	SLU 70	0	-108	2263	4.75	-0.13	0
105	SLU 71	0	-108	2263	4.75	-0.13	0
105	SLU 72	0	-108	2263	4.75	-0.13	0
105	SLU 73	0	-155	2542	6.68	-0.14	0
105	SLU 74	0	-155	2542	6.68	-0.14	0
105	SLU 75	0	-155	2542	6.68	-0.14	0
105	SLU 76	0	-155	2542	6.68	-0.14	0
105	SLU 77	0	-155	2542	6.68	-0.14	0
105	SLU 78	0	-155	2542	6.68	-0.14	0
105	SLU 79	0	-155	2542	6.68	-0.14	0
105	SLU 80	0	-155	2542	6.68	-0.14	0
105	SLU 81	0	-176	2662	7.51	-0.15	0
105	SLU 82	0	-176	2662	7.51	-0.15	0
105	SLU 83	0	-176	2662	7.51	-0.15	0
105	SLU 84	0	-176	2662	7.51	-0.15	0
105	SLE RA 1	0	-79	1708	3.47	-0.1	0
105	SLE RA 2	0	-79	1708	3.47	-0.1	0
105	SLE RA 3	0	-79	1708	3.47	-0.1	0
105	SLE RA 4	0	-79	1708	3.47	-0.1	0
105	SLE RA 5	0	-79	1708	3.47	-0.1	0
105	SLE RA 6	0	-79	1708	3.47	-0.1	0
105	SLE RA 7	0	-79	1708	3.47	-0.1	0
105	SLE RA 8	0	-79	1708	3.47	-0.1	0
105	SLE RA 9	0	-79	1708	3.47	-0.1	0
105	SLE RA 10	0	-110	1894	4.76	-0.11	0
105	SLE RA 11	0	-110	1894	4.76	-0.11	0
105	SLE RA 12	0	-110	1894	4.76	-0.11	0
105	SLE RA 13	0	-110	1894	4.76	-0.11	0
105	SLE RA 14	0	-110	1894	4.76	-0.11	0
105	SLE RA 15	0	-110	1894	4.76	-0.11	0
105	SLE RA 16	0	-110	1894	4.76	-0.11	0
105	SLE RA 17	0	-110	1894	4.76	-0.11	0
105	SLE RA 18	0	-124	1974	5.31	-0.11	0
105	SLE RA 19	0	-124	1974	5.31	-0.11	0
105	SLE RA 20	0	-124	1974	5.31	-0.11	0
105	SLE RA 21	0	-124	1974	5.31	-0.11	0
105	SLE FR 1	0	-79	1708	3.47	-0.1	0
105	SLE FR 2	0	-79	1708	3.47	-0.1	0
105	SLE FR 3	0	-79	1708	3.47	-0.1	0
105	SLE FR 4	0	-92	1788	4.02	-0.1	0
105	SLE FR 5	0	-92	1788	4.02	-0.1	0
105	SLE FR 6	0	-101	1841	4.39	-0.1	0
105	SLE QP 1	0	-79	1708	3.47	-0.1	0
105	SLE QP 2	0	-92	1788	4.02	-0.1	0
105	SLD 1	35	81	1722	-2.91	30.21	0.03
105	SLD 2	35	81	1722	-2.91	30.21	0.03



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
105	SLD 3	42	-92	1698	4.04	37.88	0.02
105	SLD 4	42	-92	1698	4.04	37.88	0.02
105	SLD 5	0	223	1805	-8.61	-2.65	0.02
105	SLD 6	0	223	1805	-8.61	-2.65	0.02
105	SLD 7	24	-356	1723	14.57	22.93	0
105	SLD 8	24	-356	1723	14.57	22.93	0
105	SLD 9	-23	171	1852	-6.53	-23.13	0
105	SLD 10	-23	171	1852	-6.53	-23.13	0
105	SLD 11	0	-408	1770	16.65	2.44	-0.02
105	SLD 12	0	-408	1770	16.65	2.44	-0.02
105	SLD 13	-42	-93	1878	4	-38.09	-0.02
105	SLD 14	-42	-93	1878	4	-38.09	-0.02
105	SLD 15	-35	-266	1853	10.96	-30.41	-0.03
105	SLD 16	-35	-266	1853	10.96	-30.41	-0.03
105	SLV 1	85	316	1632	-12.27	74.64	0.07
105	SLV 2	85	316	1632	-12.27	74.64	0.07
105	SLV 3	103	-92	1574	4.08	94.24	0.05
105	SLV 4	103	-92	1574	4.08	94.24	0.05
105	SLV 5	-2	649	1829	-25.67	-7.4	0.04
105	SLV 6	-2	649	1829	-25.67	-7.4	0.04
105	SLV 7	59	-711	1635	28.84	57.92	-0.01
105	SLV 8	59	-711	1635	28.84	57.92	-0.01
105	SLV 9	-59	526	1940	-20.8	-58.13	0.01
105	SLV 10	-59	526	1940	-20.8	-58.13	0.01
105	SLV 11	2	-834	1746	33.71	7.2	-0.04
105	SLV 12	2	-834	1746	33.71	7.2	-0.04
105	SLV 13	-103	-93	2001	3.96	-94.44	-0.05
105	SLV 14	-103	-93	2001	3.96	-94.44	-0.05
105	SLV 15	-85	-501	1943	20.31	-74.85	-0.07
105	SLV 16	-85	-501	1943	20.31	-74.85	-0.07
106	SLU 1	0	0	1213	0.03	0	0
106	SLU 2	0	0	1213	0.03	0	0
106	SLU 3	0	0	1213	0.03	0	0
106	SLU 4	0	0	1213	0.03	0	0
106	SLU 5	0	0	1213	0.03	0	0
106	SLU 6	0	0	1213	0.03	0	0
106	SLU 7	0	0	1213	0.03	0	0
106	SLU 8	0	0	1213	0.03	0	0
106	SLU 9	0	0	1213	0.03	0	0
106	SLU 10	0	0	1738	0	0.01	0
106	SLU 11	0	0	1738	0	0.01	0
106	SLU 12	0	0	1738	0	0.01	0
106	SLU 13	0	0	1738	0	0.01	0
106	SLU 14	0	0	1738	0	0.01	0
106	SLU 15	0	0	1738	0	0.01	0
106	SLU 16	0	0	1738	0	0.01	0
106	SLU 17	0	0	1738	0	0.01	0
106	SLU 18	0	0	1963	-0.02	0.01	0
106	SLU 19	0	0	1963	-0.02	0.01	0
106	SLU 20	0	0	1963	-0.02	0.01	0
106	SLU 21	0	0	1963	-0.02	0.01	0
106	SLU 22	0	0	1471	0.02	0.01	0
106	SLU 23	0	0	1471	0.02	0.01	0
106	SLU 24	0	0	1471	0.02	0.01	0
106	SLU 25	0	0	1471	0.02	0.01	0
106	SLU 26	0	0	1471	0.02	0.01	0
106	SLU 27	0	0	1471	0.02	0.01	0
106	SLU 28	0	0	1471	0.02	0.01	0
106	SLU 29	0	0	1471	0.02	0.01	0
106	SLU 30	0	0	1471	0.02	0.01	0
106	SLU 31	0	0	1996	-0.01	0.01	0
106	SLU 32	0	0	1996	-0.01	0.01	0
106	SLU 33	0	0	1996	-0.01	0.01	0
106	SLU 34	0	0	1996	-0.01	0.01	0
106	SLU 35	0	0	1996	-0.01	0.01	0
106	SLU 36	0	0	1996	-0.01	0.01	0
106	SLU 37	0	0	1996	-0.01	0.01	0
106	SLU 38	0	0	1996	-0.01	0.01	0
106	SLU 39	0	0	2221	-0.03	0.01	0
106	SLU 40	0	0	2221	-0.03	0.01	0
106	SLU 41	0	0	2221	-0.03	0.01	0
106	SLU 42	0	0	2221	-0.03	0.01	0
106	SLU 43	0	0	1488	0.05	0	0
106	SLU 44	0	0	1488	0.05	0	0
106	SLU 45	0	0	1488	0.05	0	0
106	SLU 46	0	0	1488	0.05	0	0
106	SLU 47	0	0	1488	0.05	0	0
106	SLU 48	0	0	1488	0.05	0	0
106	SLU 49	0	0	1488	0.05	0	0
106	SLU 50	0	0	1488	0.05	0	0
106	SLU 51	0	0	1488	0.05	0	0
106	SLU 52	0	0	2013	0.01	0.01	0
106	SLU 53	0	0	2013	0.01	0.01	0
106	SLU 54	0	0	2013	0.01	0.01	0
106	SLU 55	0	0	2013	0.01	0.01	0
106	SLU 56	0	0	2013	0.01	0.01	0
106	SLU 57	0	0	2013	0.01	0.01	0
106	SLU 58	0	0	2013	0.01	0.01	0
106	SLU 59	0	0	2013	0.01	0.01	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
106	SLU 60	0	0	2238	0	0.01	0
106	SLU 61	0	0	2238	0	0.01	0
106	SLU 62	0	0	2238	0	0.01	0
106	SLU 63	0	0	2238	0	0.01	0
106	SLU 64	0	0	1747	0.04	0.01	0
106	SLU 65	0	0	1747	0.04	0.01	0
106	SLU 66	0	0	1747	0.04	0.01	0
106	SLU 67	0	0	1747	0.04	0.01	0
106	SLU 68	0	0	1747	0.04	0.01	0
106	SLU 69	0	0	1747	0.04	0.01	0
106	SLU 70	0	0	1747	0.04	0.01	0
106	SLU 71	0	0	1747	0.04	0.01	0
106	SLU 72	0	0	1747	0.04	0.01	0
106	SLU 73	0	0	2272	0	0.01	0
106	SLU 74	0	0	2272	0	0.01	0
106	SLU 75	0	0	2272	0	0.01	0
106	SLU 76	0	0	2272	0	0.01	0
106	SLU 77	0	0	2272	0	0.01	0
106	SLU 78	0	0	2272	0	0.01	0
106	SLU 79	0	0	2272	0	0.01	0
106	SLU 80	0	0	2272	0	0.01	0
106	SLU 81	0	0	2497	-0.01	0.01	0
106	SLU 82	0	0	2497	-0.01	0.01	0
106	SLU 83	0	0	2497	-0.01	0.01	0
106	SLU 84	0	0	2497	-0.01	0.01	0
106	SLE RA 1	0	0	1287	0.03	0	0
106	SLE RA 2	0	0	1287	0.03	0	0
106	SLE RA 3	0	0	1287	0.03	0	0
106	SLE RA 4	0	0	1287	0.03	0	0
106	SLE RA 5	0	0	1287	0.03	0	0
106	SLE RA 6	0	0	1287	0.03	0	0
106	SLE RA 7	0	0	1287	0.03	0	0
106	SLE RA 8	0	0	1287	0.03	0	0
106	SLE RA 9	0	0	1287	0.03	0	0
106	SLE RA 10	0	0	1637	0.01	0.01	0
106	SLE RA 11	0	0	1637	0.01	0.01	0
106	SLE RA 12	0	0	1637	0.01	0.01	0
106	SLE RA 13	0	0	1637	0.01	0.01	0
106	SLE RA 14	0	0	1637	0.01	0.01	0
106	SLE RA 15	0	0	1637	0.01	0.01	0
106	SLE RA 16	0	0	1637	0.01	0.01	0
106	SLE RA 17	0	0	1637	0.01	0.01	0
106	SLE RA 18	0	0	1787	0	0.01	0
106	SLE RA 19	0	0	1787	0	0.01	0
106	SLE RA 20	0	0	1787	0	0.01	0
106	SLE RA 21	0	0	1787	0	0.01	0
106	SLE FR 1	0	0	1287	0.03	0	0
106	SLE FR 2	0	0	1287	0.03	0	0
106	SLE FR 3	0	0	1287	0.03	0	0
106	SLE FR 4	0	0	1437	0.02	0	0
106	SLE FR 5	0	0	1437	0.02	0	0
106	SLE FR 6	0	0	1537	0.01	0.01	0
106	SLE QP 1	0	0	1287	0.03	0	0
106	SLE QP 2	0	0	1437	0.02	0	0
106	SLD 1	-4	0	1476	-6.41	8.74	-0.03
106	SLD 2	-4	0	1476	-6.41	8.74	-0.03
106	SLD 3	-7	2	1420	12.28	5.23	-0.05
106	SLD 4	-7	2	1420	12.28	5.23	-0.05
106	SLD 5	2	-2	1534	-30.26	7.96	0.02
106	SLD 6	2	-2	1534	-30.26	7.96	0.02
106	SLD 7	-6	2	1347	32.05	-3.76	-0.05
106	SLD 8	-6	2	1347	32.05	-3.76	-0.05
106	SLD 9	6	-2	1527	-32	3.77	0.05
106	SLD 10	6	-2	1527	-32	3.77	0.05
106	SLD 11	-2	2	1340	30.3	-7.95	-0.02
106	SLD 12	-2	2	1340	30.3	-7.95	-0.02
106	SLD 13	7	-2	1454	-12.24	-5.22	0.05
106	SLD 14	7	-2	1454	-12.24	-5.22	0.05
106	SLD 15	4	0	1398	6.45	-8.73	0.03
106	SLD 16	4	0	1398	6.45	-8.73	0.03
106	SLV 1	-11	1	1537	-16.48	22.27	-0.07
106	SLV 2	-11	1	1537	-16.48	22.27	-0.07
106	SLV 3	-17	4	1393	31.47	13.26	-0.13
106	SLV 4	-17	4	1393	31.47	13.26	-0.13
106	SLV 5	6	-4	1685	-77.66	20.35	0.06
106	SLV 6	6	-4	1685	-77.66	20.35	0.06
106	SLV 7	-15	6	1205	82.18	-9.68	-0.12
106	SLV 8	-15	6	1205	82.18	-9.68	-0.12
106	SLV 9	15	-6	1669	-82.14	9.69	0.12
106	SLV 10	15	-6	1669	-82.14	9.69	0.12
106	SLV 11	-6	4	1189	77.7	-20.34	-0.06
106	SLV 12	-6	4	1189	77.7	-20.34	-0.06
106	SLV 13	17	-4	1481	-31.42	-13.25	0.13
106	SLV 14	17	-4	1481	-31.42	-13.25	0.13
106	SLV 15	11	-1	1337	16.53	-22.26	0.07
106	SLV 16	11	-1	1337	16.53	-22.26	0.07
107	SLU 1	0	-317	1987	11.3	0.48	0.01
107	SLU 2	0	-317	1987	11.3	0.48	0.01
107	SLU 3	0	-317	1987	11.3	0.48	0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
107	SLU 4	0	-317	1987	11.3	0.48	0.01
107	SLU 5	0	-317	1987	11.3	0.48	0.01
107	SLU 6	0	-317	1987	11.3	0.48	0.01
107	SLU 7	0	-317	1987	11.3	0.48	0.01
107	SLU 8	0	-317	1987	11.3	0.48	0.01
107	SLU 9	0	-317	1987	11.3	0.48	0.01
107	SLU 10	0	-409	2496	14.68	0.74	0.01
107	SLU 11	0	-409	2496	14.68	0.74	0.01
107	SLU 12	0	-409	2496	14.68	0.74	0.01
107	SLU 13	0	-409	2496	14.68	0.74	0.01
107	SLU 14	0	-409	2496	14.68	0.74	0.01
107	SLU 15	0	-409	2496	14.68	0.74	0.01
107	SLU 16	0	-409	2496	14.68	0.74	0.01
107	SLU 17	0	-409	2496	14.68	0.74	0.01
107	SLU 18	0	-449	2714	16.13	0.86	0.01
107	SLU 19	0	-449	2714	16.13	0.86	0.01
107	SLU 20	0	-449	2714	16.13	0.86	0.01
107	SLU 21	0	-449	2714	16.13	0.86	0.01
107	SLU 22	0	-362	2237	12.95	0.57	0.01
107	SLU 23	0	-362	2237	12.95	0.57	0.01
107	SLU 24	0	-362	2237	12.95	0.57	0.01
107	SLU 25	0	-362	2237	12.95	0.57	0.01
107	SLU 26	0	-362	2237	12.95	0.57	0.01
107	SLU 27	0	-362	2237	12.95	0.57	0.01
107	SLU 28	0	-362	2237	12.95	0.57	0.01
107	SLU 29	0	-362	2237	12.95	0.57	0.01
107	SLU 30	0	-362	2237	12.95	0.57	0.01
107	SLU 31	0	-455	2746	16.33	0.84	0.01
107	SLU 32	0	-455	2746	16.33	0.84	0.01
107	SLU 33	0	-455	2746	16.33	0.84	0.01
107	SLU 34	0	-455	2746	16.33	0.84	0.01
107	SLU 35	0	-455	2746	16.33	0.84	0.01
107	SLU 36	0	-455	2746	16.33	0.84	0.01
107	SLU 37	0	-455	2746	16.33	0.84	0.01
107	SLU 38	0	-455	2746	16.33	0.84	0.01
107	SLU 39	0	-495	2964	17.79	0.95	0.01
107	SLU 40	0	-495	2964	17.79	0.95	0.01
107	SLU 41	0	-495	2964	17.79	0.95	0.01
107	SLU 42	0	-495	2964	17.79	0.95	0.01
107	SLU 43	0	-396	2497	14.12	0.59	0.01
107	SLU 44	0	-396	2497	14.12	0.59	0.01
107	SLU 45	0	-396	2497	14.12	0.59	0.01
107	SLU 46	0	-396	2497	14.12	0.59	0.01
107	SLU 47	0	-396	2497	14.12	0.59	0.01
107	SLU 48	0	-396	2497	14.12	0.59	0.01
107	SLU 49	0	-396	2497	14.12	0.59	0.01
107	SLU 50	0	-396	2497	14.12	0.59	0.01
107	SLU 51	0	-396	2497	14.12	0.59	0.01
107	SLU 52	0	-488	3006	17.51	0.85	0.02
107	SLU 53	0	-488	3006	17.51	0.85	0.02
107	SLU 54	0	-488	3006	17.51	0.85	0.02
107	SLU 55	0	-488	3006	17.51	0.85	0.02
107	SLU 56	0	-488	3006	17.51	0.85	0.02
107	SLU 57	0	-488	3006	17.51	0.85	0.02
107	SLU 58	0	-488	3006	17.51	0.85	0.02
107	SLU 59	0	-488	3006	17.51	0.85	0.02
107	SLU 60	0	-528	3224	18.96	0.97	0.02
107	SLU 61	0	-528	3224	18.96	0.97	0.02
107	SLU 62	0	-528	3224	18.96	0.97	0.02
107	SLU 63	0	-528	3224	18.96	0.97	0.02
107	SLU 64	0	-442	2747	15.77	0.68	0.01
107	SLU 65	0	-442	2747	15.77	0.68	0.01
107	SLU 66	0	-442	2747	15.77	0.68	0.01
107	SLU 67	0	-442	2747	15.77	0.68	0.01
107	SLU 68	0	-442	2747	15.77	0.68	0.01
107	SLU 69	0	-442	2747	15.77	0.68	0.01
107	SLU 70	0	-442	2747	15.77	0.68	0.01
107	SLU 71	0	-442	2747	15.77	0.68	0.01
107	SLU 72	0	-442	2747	15.77	0.68	0.01
107	SLU 73	0	-534	3256	19.16	0.95	0.02
107	SLU 74	0	-534	3256	19.16	0.95	0.02
107	SLU 75	0	-534	3256	19.16	0.95	0.02
107	SLU 76	0	-534	3256	19.16	0.95	0.02
107	SLU 77	0	-534	3256	19.16	0.95	0.02
107	SLU 78	0	-534	3256	19.16	0.95	0.02
107	SLU 79	0	-534	3256	19.16	0.95	0.02
107	SLU 80	0	-534	3256	19.16	0.95	0.02
107	SLU 81	0	-574	3474	20.61	1.06	0.02
107	SLU 82	0	-574	3474	20.61	1.06	0.02
107	SLU 83	0	-574	3474	20.61	1.06	0.02
107	SLU 84	0	-574	3474	20.61	1.06	0.02
107	SLE RA 1	0	-330	2058	11.77	0.5	0.01
107	SLE RA 2	0	-330	2058	11.77	0.5	0.01
107	SLE RA 3	0	-330	2058	11.77	0.5	0.01
107	SLE RA 4	0	-330	2058	11.77	0.5	0.01
107	SLE RA 5	0	-330	2058	11.77	0.5	0.01
107	SLE RA 6	0	-330	2058	11.77	0.5	0.01
107	SLE RA 7	0	-330	2058	11.77	0.5	0.01
107	SLE RA 8	0	-330	2058	11.77	0.5	0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
107	SLE RA 9	0	-330	2058	11.77	0.5	0.01
107	SLE RA 10	0	-391	2398	14.03	0.68	0.01
107	SLE RA 11	0	-391	2398	14.03	0.68	0.01
107	SLE RA 12	0	-391	2398	14.03	0.68	0.01
107	SLE RA 13	0	-391	2398	14.03	0.68	0.01
107	SLE RA 14	0	-391	2398	14.03	0.68	0.01
107	SLE RA 15	0	-391	2398	14.03	0.68	0.01
107	SLE RA 16	0	-391	2398	14.03	0.68	0.01
107	SLE RA 17	0	-391	2398	14.03	0.68	0.01
107	SLE RA 18	0	-418	2543	14.99	0.76	0.01
107	SLE RA 19	0	-418	2543	14.99	0.76	0.01
107	SLE RA 20	0	-418	2543	14.99	0.76	0.01
107	SLE RA 21	0	-418	2543	14.99	0.76	0.01
107	SLE FR 1	0	-330	2058	11.77	0.5	0.01
107	SLE FR 2	0	-330	2058	11.77	0.5	0.01
107	SLE FR 3	0	-330	2058	11.77	0.5	0.01
107	SLE FR 4	0	-356	2204	12.74	0.58	0.01
107	SLE FR 5	0	-356	2204	12.74	0.58	0.01
107	SLE FR 6	0	-374	2301	13.38	0.63	0.01
107	SLE QP 1	0	-330	2058	11.77	0.5	0.01
107	SLE QP 2	0	-356	2204	12.74	0.58	0.01
107	SLD 1	9	-174	2871	12.72	10.4	0.03
107	SLD 2	9	-174	2871	12.72	10.4	0.03
107	SLD 3	12	-355	2636	19.6	12.65	0.02
107	SLD 4	12	-355	2636	19.6	12.65	0.02
107	SLD 5	-2	-27	2760	2.3	0.11	0.02
107	SLD 6	-2	-27	2760	2.3	0.11	0.02
107	SLD 7	9	-630	1977	25.23	7.61	0.01
107	SLD 8	9	-630	1977	25.23	7.61	0.01
107	SLD 9	-8	-82	2431	0.25	-6.45	0.02
107	SLD 10	-8	-82	2431	0.25	-6.45	0.02
107	SLD 11	3	-685	1647	23.17	1.04	0
107	SLD 12	3	-685	1647	23.17	1.04	0
107	SLD 13	-12	-358	1772	5.87	-11.49	0
107	SLD 14	-12	-358	1772	5.87	-11.49	0
107	SLD 15	-8	-538	1537	12.75	-9.24	-0.01
107	SLD 16	-8	-538	1537	12.75	-9.24	-0.01
107	SLV 1	20	72	3891	12.7	24.05	0.05
107	SLV 2	20	72	3891	12.7	24.05	0.05
107	SLV 3	28	-352	3308	28.85	29.76	0.04
107	SLV 4	28	-352	3308	28.85	29.76	0.04
107	SLV 5	-7	417	3594	-11.76	-1.03	0.05
107	SLV 6	-7	417	3594	-11.76	-1.03	0.05
107	SLV 7	21	-999	1650	42.06	17.99	0
107	SLV 8	21	-999	1650	42.06	17.99	0
107	SLV 9	-21	287	2757	-16.59	-16.83	0.02
107	SLV 10	-21	287	2757	-16.59	-16.83	0.02
107	SLV 11	7	-1129	813	37.24	2.19	-0.02
107	SLV 12	7	-1129	813	37.24	2.19	-0.02
107	SLV 13	-28	-360	1100	-3.37	-28.6	-0.02
107	SLV 14	-28	-360	1100	-3.37	-28.6	-0.02
107	SLV 15	-20	-785	517	12.77	-22.89	-0.03
107	SLV 16	-20	-785	517	12.77	-22.89	-0.03
108	SLU 1	0	-56	1830	2.58	-0.13	0
108	SLU 2	0	-56	1830	2.58	-0.13	0
108	SLU 3	0	-56	1830	2.58	-0.13	0
108	SLU 4	0	-56	1830	2.58	-0.13	0
108	SLU 5	0	-56	1830	2.58	-0.13	0
108	SLU 6	0	-56	1830	2.58	-0.13	0
108	SLU 7	0	-56	1830	2.58	-0.13	0
108	SLU 8	0	-56	1830	2.58	-0.13	0
108	SLU 9	0	-56	1830	2.58	-0.13	0
108	SLU 10	0	-94	2144	4.11	-0.15	0
108	SLU 11	0	-94	2144	4.11	-0.15	0
108	SLU 12	0	-94	2144	4.11	-0.15	0
108	SLU 13	0	-94	2144	4.11	-0.15	0
108	SLU 14	0	-94	2144	4.11	-0.15	0
108	SLU 15	0	-94	2144	4.11	-0.15	0
108	SLU 16	0	-94	2144	4.11	-0.15	0
108	SLU 17	0	-94	2144	4.11	-0.15	0
108	SLU 18	0	-110	2279	4.76	-0.15	0
108	SLU 19	0	-110	2279	4.76	-0.15	0
108	SLU 20	0	-110	2279	4.76	-0.15	0
108	SLU 21	0	-110	2279	4.76	-0.15	0
108	SLU 22	0	-70	1999	3.17	-0.14	0
108	SLU 23	0	-70	1999	3.17	-0.14	0
108	SLU 24	0	-70	1999	3.17	-0.14	0
108	SLU 25	0	-70	1999	3.17	-0.14	0
108	SLU 26	0	-70	1999	3.17	-0.14	0
108	SLU 27	0	-70	1999	3.17	-0.14	0
108	SLU 28	0	-70	1999	3.17	-0.14	0
108	SLU 29	0	-70	1999	3.17	-0.14	0
108	SLU 30	0	-70	1999	3.17	-0.14	0
108	SLU 31	0	-108	2313	4.7	-0.16	0
108	SLU 32	0	-108	2313	4.7	-0.16	0
108	SLU 33	0	-108	2313	4.7	-0.16	0
108	SLU 34	0	-108	2313	4.7	-0.16	0
108	SLU 35	0	-108	2313	4.7	-0.16	0
108	SLU 36	0	-108	2313	4.7	-0.16	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
108	SLU 37	0	-108	2313	4.7	-0.16	0
108	SLU 38	0	-108	2313	4.7	-0.16	0
108	SLU 39	0	-124	2448	5.35	-0.17	0
108	SLU 40	0	-124	2448	5.35	-0.17	0
108	SLU 41	0	-124	2448	5.35	-0.17	0
108	SLU 42	0	-124	2448	5.35	-0.17	0
108	SLU 43	0	-68	2320	3.15	-0.16	0
108	SLU 44	0	-68	2320	3.15	-0.16	0
108	SLU 45	0	-68	2320	3.15	-0.16	0
108	SLU 46	0	-68	2320	3.15	-0.16	0
108	SLU 47	0	-68	2320	3.15	-0.16	0
108	SLU 48	0	-68	2320	3.15	-0.16	0
108	SLU 49	0	-68	2320	3.15	-0.16	0
108	SLU 50	0	-68	2320	3.15	-0.16	0
108	SLU 51	0	-68	2320	3.15	-0.16	0
108	SLU 52	0	-106	2635	4.68	-0.18	0
108	SLU 53	0	-106	2635	4.68	-0.18	0
108	SLU 54	0	-106	2635	4.68	-0.18	0
108	SLU 55	0	-106	2635	4.68	-0.18	0
108	SLU 56	0	-106	2635	4.68	-0.18	0
108	SLU 57	0	-106	2635	4.68	-0.18	0
108	SLU 58	0	-106	2635	4.68	-0.18	0
108	SLU 59	0	-106	2635	4.68	-0.18	0
108	SLU 60	0	-122	2770	5.33	-0.19	0
108	SLU 61	0	-122	2770	5.33	-0.19	0
108	SLU 62	0	-122	2770	5.33	-0.19	0
108	SLU 63	0	-122	2770	5.33	-0.19	0
108	SLU 64	0	-82	2490	3.74	-0.18	0
108	SLU 65	0	-82	2490	3.74	-0.18	0
108	SLU 66	0	-82	2490	3.74	-0.18	0
108	SLU 67	0	-82	2490	3.74	-0.18	0
108	SLU 68	0	-82	2490	3.74	-0.18	0
108	SLU 69	0	-82	2490	3.74	-0.18	0
108	SLU 70	0	-82	2490	3.74	-0.18	0
108	SLU 71	0	-82	2490	3.74	-0.18	0
108	SLU 72	0	-82	2490	3.74	-0.18	0
108	SLU 73	0	-120	2804	5.27	-0.19	0
108	SLU 74	0	-120	2804	5.27	-0.19	0
108	SLU 75	0	-120	2804	5.27	-0.19	0
108	SLU 76	0	-120	2804	5.27	-0.19	0
108	SLU 77	0	-120	2804	5.27	-0.19	0
108	SLU 78	0	-120	2804	5.27	-0.19	0
108	SLU 79	0	-120	2804	5.27	-0.19	0
108	SLU 80	0	-120	2804	5.27	-0.19	0
108	SLU 81	0	-136	2939	5.92	-0.2	0
108	SLU 82	0	-136	2939	5.92	-0.2	0
108	SLU 83	0	-136	2939	5.92	-0.2	0
108	SLU 84	0	-136	2939	5.92	-0.2	0
108	SLE RA 1	0	-60	1878	2.75	-0.13	0
108	SLE RA 2	0	-60	1878	2.75	-0.13	0
108	SLE RA 3	0	-60	1878	2.75	-0.13	0
108	SLE RA 4	0	-60	1878	2.75	-0.13	0
108	SLE RA 5	0	-60	1878	2.75	-0.13	0
108	SLE RA 6	0	-60	1878	2.75	-0.13	0
108	SLE RA 7	0	-60	1878	2.75	-0.13	0
108	SLE RA 8	0	-60	1878	2.75	-0.13	0
108	SLE RA 9	0	-60	1878	2.75	-0.13	0
108	SLE RA 10	0	-85	2088	3.77	-0.14	0
108	SLE RA 11	0	-85	2088	3.77	-0.14	0
108	SLE RA 12	0	-85	2088	3.77	-0.14	0
108	SLE RA 13	0	-85	2088	3.77	-0.14	0
108	SLE RA 14	0	-85	2088	3.77	-0.14	0
108	SLE RA 15	0	-85	2088	3.77	-0.14	0
108	SLE RA 16	0	-85	2088	3.77	-0.14	0
108	SLE RA 17	0	-85	2088	3.77	-0.14	0
108	SLE RA 18	0	-96	2178	4.2	-0.15	0
108	SLE RA 19	0	-96	2178	4.2	-0.15	0
108	SLE RA 20	0	-96	2178	4.2	-0.15	0
108	SLE RA 21	0	-96	2178	4.2	-0.15	0
108	SLE FR 1	0	-60	1878	2.75	-0.13	0
108	SLE FR 2	0	-60	1878	2.75	-0.13	0
108	SLE FR 3	0	-60	1878	2.75	-0.13	0
108	SLE FR 4	0	-71	1968	3.18	-0.14	0
108	SLE FR 5	0	-71	1968	3.18	-0.14	0
108	SLE FR 6	0	-78	2028	3.47	-0.14	0
108	SLE QP 1	0	-60	1878	2.75	-0.13	0
108	SLE QP 2	0	-71	1968	3.18	-0.14	0
108	SLD 1	28	87	1848	-3.01	26.13	0.02
108	SLD 2	28	87	1848	-3.01	26.13	0.02
108	SLD 3	37	-68	1880	3.06	33.78	0.01
108	SLD 4	37	-68	1880	3.06	33.78	0.01
108	SLD 5	-4	212	1883	-7.88	-3.86	0.02
108	SLD 6	-4	212	1883	-7.88	-3.86	0.02
108	SLD 7	24	-305	1990	12.35	21.64	-0.01
108	SLD 8	24	-305	1990	12.35	21.64	-0.01
108	SLD 9	-24	163	1945	-5.98	-21.92	0.01
108	SLD 10	-24	163	1945	-5.98	-21.92	0.01
108	SLD 11	4	-354	2053	14.25	3.59	-0.02
108	SLD 12	4	-354	2053	14.25	3.59	-0.02



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
108	SLD 13	-37	-74	2056	3.31	-34.06	-0.01
108	SLD 14	-37	-74	2056	3.31	-34.06	-0.01
108	SLD 15	-28	-229	2088	9.38	-26.4	-0.02
108	SLD 16	-28	-229	2088	9.38	-26.4	-0.02
108	SLV 1	69	301	1683	-11.39	64.65	0.04
108	SLV 2	69	301	1683	-11.39	64.65	0.04
108	SLV 3	91	-64	1759	2.89	84.18	0.03
108	SLV 4	91	-64	1759	2.89	84.18	0.03
108	SLV 5	-12	593	1767	-22.83	-10.33	0.04
108	SLV 6	-12	593	1767	-22.83	-10.33	0.04
108	SLV 7	60	-622	2021	24.74	54.79	-0.02
108	SLV 8	60	-622	2021	24.74	54.79	-0.02
108	SLV 9	-60	480	1915	-18.37	-55.06	0.02
108	SLV 10	-60	480	1915	-18.37	-55.06	0.02
108	SLV 11	12	-735	2169	29.2	10.06	-0.04
108	SLV 12	12	-735	2169	29.2	10.06	-0.04
108	SLV 13	-91	-78	2177	3.48	-84.46	-0.03
108	SLV 14	-91	-78	2177	3.48	-84.46	-0.03
108	SLV 15	-69	-443	2253	17.75	-64.92	-0.04
108	SLV 16	-69	-443	2253	17.75	-64.92	-0.04
109	SLU 1	0	0	1175	0.05	0	0
109	SLU 2	0	0	1175	0.05	0	0
109	SLU 3	0	0	1175	0.05	0	0
109	SLU 4	0	0	1175	0.05	0	0
109	SLU 5	0	0	1175	0.05	0	0
109	SLU 6	0	0	1175	0.05	0	0
109	SLU 7	0	0	1175	0.05	0	0
109	SLU 8	0	0	1175	0.05	0	0
109	SLU 9	0	0	1175	0.05	0	0
109	SLU 10	0	0	1643	0.03	0.01	0
109	SLU 11	0	0	1643	0.03	0.01	0
109	SLU 12	0	0	1643	0.03	0.01	0
109	SLU 13	0	0	1643	0.03	0.01	0
109	SLU 14	0	0	1643	0.03	0.01	0
109	SLU 15	0	0	1643	0.03	0.01	0
109	SLU 16	0	0	1643	0.03	0.01	0
109	SLU 17	0	0	1643	0.03	0.01	0
109	SLU 18	0	0	1844	0.02	0.01	0
109	SLU 19	0	0	1844	0.02	0.01	0
109	SLU 20	0	0	1844	0.02	0.01	0
109	SLU 21	0	0	1844	0.02	0.01	0
109	SLU 22	0	0	1411	0.05	0.01	0
109	SLU 23	0	0	1411	0.05	0.01	0
109	SLU 24	0	0	1411	0.05	0.01	0
109	SLU 25	0	0	1411	0.05	0.01	0
109	SLU 26	0	0	1411	0.05	0.01	0
109	SLU 27	0	0	1411	0.05	0.01	0
109	SLU 28	0	0	1411	0.05	0.01	0
109	SLU 29	0	0	1411	0.05	0.01	0
109	SLU 30	0	0	1411	0.05	0.01	0
109	SLU 31	0	0	1879	0.02	0.01	0
109	SLU 32	0	0	1879	0.02	0.01	0
109	SLU 33	0	0	1879	0.02	0.01	0
109	SLU 34	0	0	1879	0.02	0.01	0
109	SLU 35	0	0	1879	0.02	0.01	0
109	SLU 36	0	0	1879	0.02	0.01	0
109	SLU 37	0	0	1879	0.02	0.01	0
109	SLU 38	0	0	1879	0.02	0.01	0
109	SLU 39	0	0	2079	0.01	0.01	0
109	SLU 40	0	0	2079	0.01	0.01	0
109	SLU 41	0	0	2079	0.01	0.01	0
109	SLU 42	0	0	2079	0.01	0.01	0
109	SLU 43	0	0	1447	0.07	0.01	0
109	SLU 44	0	0	1447	0.07	0.01	0
109	SLU 45	0	0	1447	0.07	0.01	0
109	SLU 46	0	0	1447	0.07	0.01	0
109	SLU 47	0	0	1447	0.07	0.01	0
109	SLU 48	0	0	1447	0.07	0.01	0
109	SLU 49	0	0	1447	0.07	0.01	0
109	SLU 50	0	0	1447	0.07	0.01	0
109	SLU 51	0	0	1447	0.07	0.01	0
109	SLU 52	0	0	1915	0.04	0.01	0
109	SLU 53	0	0	1915	0.04	0.01	0
109	SLU 54	0	0	1915	0.04	0.01	0
109	SLU 55	0	0	1915	0.04	0.01	0
109	SLU 56	0	0	1915	0.04	0.01	0
109	SLU 57	0	0	1915	0.04	0.01	0
109	SLU 58	0	0	1915	0.04	0.01	0
109	SLU 59	0	0	1915	0.04	0.01	0
109	SLU 60	0	0	2116	0.03	0.01	0
109	SLU 61	0	0	2116	0.03	0.01	0
109	SLU 62	0	0	2116	0.03	0.01	0
109	SLU 63	0	0	2116	0.03	0.01	0
109	SLU 64	0	0	1683	0.07	0.01	0
109	SLU 65	0	0	1683	0.07	0.01	0
109	SLU 66	0	0	1683	0.07	0.01	0
109	SLU 67	0	0	1683	0.07	0.01	0
109	SLU 68	0	0	1683	0.07	0.01	0
109	SLU 69	0	0	1683	0.07	0.01	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
109	SLU 70	0	0	1683	0.07	0.01	0
109	SLU 71	0	0	1683	0.07	0.01	0
109	SLU 72	0	0	1683	0.07	0.01	0
109	SLU 73	0	0	2151	0.04	0.01	0
109	SLU 74	0	0	2151	0.04	0.01	0
109	SLU 75	0	0	2151	0.04	0.01	0
109	SLU 76	0	0	2151	0.04	0.01	0
109	SLU 77	0	0	2151	0.04	0.01	0
109	SLU 78	0	0	2151	0.04	0.01	0
109	SLU 79	0	0	2151	0.04	0.01	0
109	SLU 80	0	0	2151	0.04	0.01	0
109	SLU 81	0	0	2351	0.03	0.01	0
109	SLU 82	0	0	2351	0.03	0.01	0
109	SLU 83	0	0	2351	0.03	0.01	0
109	SLU 84	0	0	2351	0.03	0.01	0
109	SLE RA 1	0	0	1243	0.05	0.01	0
109	SLE RA 2	0	0	1243	0.05	0.01	0
109	SLE RA 3	0	0	1243	0.05	0.01	0
109	SLE RA 4	0	0	1243	0.05	0.01	0
109	SLE RA 5	0	0	1243	0.05	0.01	0
109	SLE RA 6	0	0	1243	0.05	0.01	0
109	SLE RA 7	0	0	1243	0.05	0.01	0
109	SLE RA 8	0	0	1243	0.05	0.01	0
109	SLE RA 9	0	0	1243	0.05	0.01	0
109	SLE RA 10	0	0	1555	0.03	0.01	0
109	SLE RA 11	0	0	1555	0.03	0.01	0
109	SLE RA 12	0	0	1555	0.03	0.01	0
109	SLE RA 13	0	0	1555	0.03	0.01	0
109	SLE RA 14	0	0	1555	0.03	0.01	0
109	SLE RA 15	0	0	1555	0.03	0.01	0
109	SLE RA 16	0	0	1555	0.03	0.01	0
109	SLE RA 17	0	0	1555	0.03	0.01	0
109	SLE RA 18	0	0	1688	0.03	0.01	0
109	SLE RA 19	0	0	1688	0.03	0.01	0
109	SLE RA 20	0	0	1688	0.03	0.01	0
109	SLE RA 21	0	0	1688	0.03	0.01	0
109	SLE FR 1	0	0	1243	0.05	0.01	0
109	SLE FR 2	0	0	1243	0.05	0.01	0
109	SLE FR 3	0	0	1243	0.05	0.01	0
109	SLE FR 4	0	0	1376	0.04	0.01	0
109	SLE FR 5	0	0	1376	0.04	0.01	0
109	SLE FR 6	0	0	1465	0.04	0.01	0
109	SLE QP 1	0	0	1243	0.05	0.01	0
109	SLE QP 2	0	0	1376	0.04	0.01	0
109	SLD 1	-4	1	1394	-9.54	7.06	-0.01
109	SLD 2	-4	1	1394	-9.54	7.06	-0.01
109	SLD 3	-6	-3	1336	18.35	4.3	-0.02
109	SLD 4	-6	-3	1336	18.35	4.3	-0.02
109	SLD 5	2	6	1470	-45.14	6.32	0.02
109	SLD 6	2	6	1470	-45.14	6.32	0.02
109	SLD 7	-5	-6	1276	47.84	-2.9	-0.03
109	SLD 8	-5	-6	1276	47.84	-2.9	-0.03
109	SLD 9	5	6	1477	-47.75	2.92	0.03
109	SLD 10	5	6	1477	-47.75	2.92	0.03
109	SLD 11	-2	-6	1283	45.23	-6.31	-0.02
109	SLD 12	-2	-6	1283	45.23	-6.31	-0.02
109	SLD 13	6	2	1417	-18.26	-4.28	0.02
109	SLD 14	6	2	1417	-18.26	-4.28	0.02
109	SLD 15	4	-1	1359	9.63	-7.05	0.01
109	SLD 16	4	-1	1359	9.63	-7.05	0.01
109	SLV 1	-9	3	1422	-24.56	17.99	-0.02
109	SLV 2	-9	3	1422	-24.56	17.99	-0.02
109	SLV 3	-14	-6	1273	47.01	10.9	-0.05
109	SLV 4	-14	-6	1273	47.01	10.9	-0.05
109	SLV 5	5	16	1616	-115.87	16.16	0.05
109	SLV 6	5	16	1616	-115.87	16.16	0.05
109	SLV 7	-12	-17	1119	122.67	-7.48	-0.07
109	SLV 8	-12	-17	1119	122.67	-7.48	-0.07
109	SLV 9	12	17	1633	-122.58	7.5	0.07
109	SLV 10	12	17	1633	-122.58	7.5	0.07
109	SLV 11	-5	-16	1137	115.96	-16.14	-0.05
109	SLV 12	-5	-16	1137	115.96	-16.14	-0.05
109	SLV 13	14	6	1480	-46.92	-10.88	0.05
109	SLV 14	14	6	1480	-46.92	-10.88	0.05
109	SLV 15	9	-3	1331	24.65	-17.98	0.02
109	SLV 16	9	-3	1331	24.65	-17.98	0.02
110	SLU 1	6	-418	1987	16.58	1.59	-0.03
110	SLU 2	6	-418	1987	16.58	1.59	-0.03
110	SLU 3	6	-418	1987	16.58	1.59	-0.03
110	SLU 4	6	-418	1987	16.58	1.59	-0.03
110	SLU 5	6	-418	1987	16.58	1.59	-0.03
110	SLU 6	6	-418	1987	16.58	1.59	-0.03
110	SLU 7	6	-418	1987	16.58	1.59	-0.03
110	SLU 8	6	-418	1987	16.58	1.59	-0.03
110	SLU 9	6	-418	1987	16.58	1.59	-0.03
110	SLU 10	7	-540	2518	21.51	2.12	-0.04
110	SLU 11	7	-540	2518	21.51	2.12	-0.04
110	SLU 12	7	-540	2518	21.51	2.12	-0.04
110	SLU 13	7	-540	2518	21.51	2.12	-0.04



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
110	SLU 14	7	-540	2518	21.51	2.12	-0.04
110	SLU 15	7	-540	2518	21.51	2.12	-0.04
110	SLU 16	7	-540	2518	21.51	2.12	-0.04
110	SLU 17	7	-540	2518	21.51	2.12	-0.04
110	SLU 18	8	-592	2745	23.62	2.36	-0.04
110	SLU 19	8	-592	2745	23.62	2.36	-0.04
110	SLU 20	8	-592	2745	23.62	2.36	-0.04
110	SLU 21	8	-592	2745	23.62	2.36	-0.04
110	SLU 22	6	-478	2244	18.98	1.82	-0.03
110	SLU 23	6	-478	2244	18.98	1.82	-0.03
110	SLU 24	6	-478	2244	18.98	1.82	-0.03
110	SLU 25	6	-478	2244	18.98	1.82	-0.03
110	SLU 26	6	-478	2244	18.98	1.82	-0.03
110	SLU 27	6	-478	2244	18.98	1.82	-0.03
110	SLU 28	6	-478	2244	18.98	1.82	-0.03
110	SLU 29	6	-478	2244	18.98	1.82	-0.03
110	SLU 30	6	-478	2244	18.98	1.82	-0.03
110	SLU 31	8	-600	2774	23.92	2.36	-0.04
110	SLU 32	8	-600	2774	23.92	2.36	-0.04
110	SLU 33	8	-600	2774	23.92	2.36	-0.04
110	SLU 34	8	-600	2774	23.92	2.36	-0.04
110	SLU 35	8	-600	2774	23.92	2.36	-0.04
110	SLU 36	8	-600	2774	23.92	2.36	-0.04
110	SLU 37	8	-600	2774	23.92	2.36	-0.04
110	SLU 38	8	-600	2774	23.92	2.36	-0.04
110	SLU 39	9	-652	3001	26.03	2.59	-0.04
110	SLU 40	9	-652	3001	26.03	2.59	-0.04
110	SLU 41	9	-652	3001	26.03	2.59	-0.04
110	SLU 42	9	-652	3001	26.03	2.59	-0.04
110	SLU 43	7	-523	2496	20.73	1.98	-0.04
110	SLU 44	7	-523	2496	20.73	1.98	-0.04
110	SLU 45	7	-523	2496	20.73	1.98	-0.04
110	SLU 46	7	-523	2496	20.73	1.98	-0.04
110	SLU 47	7	-523	2496	20.73	1.98	-0.04
110	SLU 48	7	-523	2496	20.73	1.98	-0.04
110	SLU 49	7	-523	2496	20.73	1.98	-0.04
110	SLU 50	7	-523	2496	20.73	1.98	-0.04
110	SLU 51	7	-523	2496	20.73	1.98	-0.04
110	SLU 52	9	-645	3026	25.66	2.52	-0.04
110	SLU 53	9	-645	3026	25.66	2.52	-0.04
110	SLU 54	9	-645	3026	25.66	2.52	-0.04
110	SLU 55	9	-645	3026	25.66	2.52	-0.04
110	SLU 56	9	-645	3026	25.66	2.52	-0.04
110	SLU 57	9	-645	3026	25.66	2.52	-0.04
110	SLU 58	9	-645	3026	25.66	2.52	-0.04
110	SLU 59	9	-645	3026	25.66	2.52	-0.04
110	SLU 60	9	-697	3253	27.77	2.75	-0.05
110	SLU 61	9	-697	3253	27.77	2.75	-0.05
110	SLU 62	9	-697	3253	27.77	2.75	-0.05
110	SLU 63	9	-697	3253	27.77	2.75	-0.05
110	SLU 64	8	-583	2752	23.13	2.22	-0.04
110	SLU 65	8	-583	2752	23.13	2.22	-0.04
110	SLU 66	8	-583	2752	23.13	2.22	-0.04
110	SLU 67	8	-583	2752	23.13	2.22	-0.04
110	SLU 68	8	-583	2752	23.13	2.22	-0.04
110	SLU 69	8	-583	2752	23.13	2.22	-0.04
110	SLU 70	8	-583	2752	23.13	2.22	-0.04
110	SLU 71	8	-583	2752	23.13	2.22	-0.04
110	SLU 72	8	-583	2752	23.13	2.22	-0.04
110	SLU 73	9	-704	3283	28.07	2.76	-0.05
110	SLU 74	9	-704	3283	28.07	2.76	-0.05
110	SLU 75	9	-704	3283	28.07	2.76	-0.05
110	SLU 76	9	-704	3283	28.07	2.76	-0.05
110	SLU 77	9	-704	3283	28.07	2.76	-0.05
110	SLU 78	9	-704	3283	28.07	2.76	-0.05
110	SLU 79	9	-704	3283	28.07	2.76	-0.05
110	SLU 80	9	-704	3283	28.07	2.76	-0.05
110	SLU 81	10	-757	3510	30.18	2.99	-0.05
110	SLU 82	10	-757	3510	30.18	2.99	-0.05
110	SLU 83	10	-757	3510	30.18	2.99	-0.05
110	SLU 84	10	-757	3510	30.18	2.99	-0.05
110	SLE RA 1	6	-435	2061	17.27	1.65	-0.03
110	SLE RA 2	6	-435	2061	17.27	1.65	-0.03
110	SLE RA 3	6	-435	2061	17.27	1.65	-0.03
110	SLE RA 4	6	-435	2061	17.27	1.65	-0.03
110	SLE RA 5	6	-435	2061	17.27	1.65	-0.03
110	SLE RA 6	6	-435	2061	17.27	1.65	-0.03
110	SLE RA 7	6	-435	2061	17.27	1.65	-0.03
110	SLE RA 8	6	-435	2061	17.27	1.65	-0.03
110	SLE RA 9	6	-435	2061	17.27	1.65	-0.03
110	SLE RA 10	7	-516	2414	20.55	2.01	-0.04
110	SLE RA 11	7	-516	2414	20.55	2.01	-0.04
110	SLE RA 12	7	-516	2414	20.55	2.01	-0.04
110	SLE RA 13	7	-516	2414	20.55	2.01	-0.04
110	SLE RA 14	7	-516	2414	20.55	2.01	-0.04
110	SLE RA 15	7	-516	2414	20.55	2.01	-0.04
110	SLE RA 16	7	-516	2414	20.55	2.01	-0.04
110	SLE RA 17	7	-516	2414	20.55	2.01	-0.04
110	SLE RA 18	7	-551	2566	21.96	2.17	-0.04



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
110	SLE RA 19	7	-551	2566	21.96	2.17	-0.04
110	SLE RA 20	7	-551	2566	21.96	2.17	-0.04
110	SLE RA 21	7	-551	2566	21.96	2.17	-0.04
110	SLE FR 1	6	-435	2061	17.27	1.65	-0.03
110	SLE FR 2	6	-435	2061	17.27	1.65	-0.03
110	SLE FR 3	6	-435	2061	17.27	1.65	-0.03
110	SLE FR 4	6	-470	2212	18.68	1.81	-0.03
110	SLE FR 5	6	-470	2212	18.68	1.81	-0.03
110	SLE FR 6	7	-493	2313	19.61	1.91	-0.03
110	SLE QP 1	6	-435	2061	17.27	1.65	-0.03
110	SLE QP 2	6	-470	2212	18.68	1.81	-0.03
110	SLD 1	8	-282	3134	18.82	6.87	-0.05
110	SLD 2	8	-282	3134	18.82	6.87	-0.05
110	SLD 3	10	-468	2799	25.63	7.94	-0.04
110	SLD 4	10	-468	2799	25.63	7.94	-0.04
110	SLD 5	4	-132	2997	8.39	1.71	-0.05
110	SLD 6	4	-132	2997	8.39	1.71	-0.05
110	SLD 7	11	-750	1880	31.09	5.27	-0.03
110	SLD 8	11	-750	1880	31.09	5.27	-0.03
110	SLD 9	2	-189	2545	6.26	-1.65	-0.04
110	SLD 10	2	-189	2545	6.26	-1.65	-0.04
110	SLD 11	9	-807	1427	28.96	1.91	-0.02
110	SLD 12	9	-807	1427	28.96	1.91	-0.02
110	SLD 13	2	-472	1625	11.72	-4.33	-0.02
110	SLD 14	2	-472	1625	11.72	-4.33	-0.02
110	SLD 15	4	-657	1290	18.53	-3.26	-0.01
110	SLD 16	4	-657	1290	18.53	-3.26	-0.01
110	SLV 1	11	-29	4534	19.09	14.04	-0.08
110	SLV 2	11	-29	4534	19.09	14.04	-0.08
110	SLV 3	16	-465	3700	35.06	16.73	-0.06
110	SLV 4	16	-465	3700	35.06	16.73	-0.06
110	SLV 5	0	323	4175	-5.43	1.4	-0.07
110	SLV 6	0	323	4175	-5.43	1.4	-0.07
110	SLV 7	17	-1129	1393	47.82	10.36	-0.02
110	SLV 8	17	-1129	1393	47.82	10.36	-0.02
110	SLV 9	-5	189	3032	-10.47	-6.75	-0.05
110	SLV 10	-5	189	3032	-10.47	-6.75	-0.05
110	SLV 11	13	-1262	250	42.78	2.21	0
110	SLV 12	13	-1262	250	42.78	2.21	0
110	SLV 13	-4	-475	725	2.29	-13.11	0
110	SLV 14	-4	-475	725	2.29	-13.11	0
110	SLV 15	1	-910	-110	18.26	-10.43	0.01
110	SLV 16	1	-910	-110	18.26	-10.43	0.01
111	SLU 1	0	-125	2006	6.21	-0.21	0
111	SLU 2	0	-125	2006	6.21	-0.21	0
111	SLU 3	0	-125	2006	6.21	-0.21	0
111	SLU 4	0	-125	2006	6.21	-0.21	0
111	SLU 5	0	-125	2006	6.21	-0.21	0
111	SLU 6	0	-125	2006	6.21	-0.21	0
111	SLU 7	0	-125	2006	6.21	-0.21	0
111	SLU 8	0	-125	2006	6.21	-0.21	0
111	SLU 9	0	-125	2006	6.21	-0.21	0
111	SLU 10	0	-175	2367	8.57	-0.25	0
111	SLU 11	0	-175	2367	8.57	-0.25	0
111	SLU 12	0	-175	2367	8.57	-0.25	0
111	SLU 13	0	-175	2367	8.57	-0.25	0
111	SLU 14	0	-175	2367	8.57	-0.25	0
111	SLU 15	0	-175	2367	8.57	-0.25	0
111	SLU 16	0	-175	2367	8.57	-0.25	0
111	SLU 17	0	-175	2367	8.57	-0.25	0
111	SLU 18	0	-196	2521	9.59	-0.26	0
111	SLU 19	0	-196	2521	9.59	-0.26	0
111	SLU 20	0	-196	2521	9.59	-0.26	0
111	SLU 21	0	-196	2521	9.59	-0.26	0
111	SLU 22	0	-144	2201	7.17	-0.24	0
111	SLU 23	0	-144	2201	7.17	-0.24	0
111	SLU 24	0	-144	2201	7.17	-0.24	0
111	SLU 25	0	-144	2201	7.17	-0.24	0
111	SLU 26	0	-144	2201	7.17	-0.24	0
111	SLU 27	0	-144	2201	7.17	-0.24	0
111	SLU 28	0	-144	2201	7.17	-0.24	0
111	SLU 29	0	-144	2201	7.17	-0.24	0
111	SLU 30	0	-144	2201	7.17	-0.24	0
111	SLU 31	0	-194	2562	9.54	-0.27	0
111	SLU 32	0	-194	2562	9.54	-0.27	0
111	SLU 33	0	-194	2562	9.54	-0.27	0
111	SLU 34	0	-194	2562	9.54	-0.27	0
111	SLU 35	0	-194	2562	9.54	-0.27	0
111	SLU 36	0	-194	2562	9.54	-0.27	0
111	SLU 37	0	-194	2562	9.54	-0.27	0
111	SLU 38	0	-194	2562	9.54	-0.27	0
111	SLU 39	0	-216	2716	10.55	-0.28	0
111	SLU 40	0	-216	2716	10.55	-0.28	0
111	SLU 41	0	-216	2716	10.55	-0.28	0
111	SLU 42	0	-216	2716	10.55	-0.28	0
111	SLU 43	0	-155	2541	7.74	-0.27	0
111	SLU 44	0	-155	2541	7.74	-0.27	0
111	SLU 45	0	-155	2541	7.74	-0.27	0
111	SLU 46	0	-155	2541	7.74	-0.27	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
111	SLU 47	0	-155	2541	7.74	-0.27	0
111	SLU 48	0	-155	2541	7.74	-0.27	0
111	SLU 49	0	-155	2541	7.74	-0.27	0
111	SLU 50	0	-155	2541	7.74	-0.27	0
111	SLU 51	0	-155	2541	7.74	-0.27	0
111	SLU 52	0	-206	2902	10.1	-0.3	0
111	SLU 53	0	-206	2902	10.1	-0.3	0
111	SLU 54	0	-206	2902	10.1	-0.3	0
111	SLU 55	0	-206	2902	10.1	-0.3	0
111	SLU 56	0	-206	2902	10.1	-0.3	0
111	SLU 57	0	-206	2902	10.1	-0.3	0
111	SLU 58	0	-206	2902	10.1	-0.3	0
111	SLU 59	0	-206	2902	10.1	-0.3	0
111	SLU 60	0	-227	3056	11.12	-0.32	0
111	SLU 61	0	-227	3056	11.12	-0.32	0
111	SLU 62	0	-227	3056	11.12	-0.32	0
111	SLU 63	0	-227	3056	11.12	-0.32	0
111	SLU 64	0	-175	2735	8.7	-0.29	0
111	SLU 65	0	-175	2735	8.7	-0.29	0
111	SLU 66	0	-175	2735	8.7	-0.29	0
111	SLU 67	0	-175	2735	8.7	-0.29	0
111	SLU 68	0	-175	2735	8.7	-0.29	0
111	SLU 69	0	-175	2735	8.7	-0.29	0
111	SLU 70	0	-175	2735	8.7	-0.29	0
111	SLU 71	0	-175	2735	8.7	-0.29	0
111	SLU 72	0	-175	2735	8.7	-0.29	0
111	SLU 73	0	-225	3096	11.07	-0.32	0
111	SLU 74	0	-225	3096	11.07	-0.32	0
111	SLU 75	0	-225	3096	11.07	-0.32	0
111	SLU 76	0	-225	3096	11.07	-0.32	0
111	SLU 77	0	-225	3096	11.07	-0.32	0
111	SLU 78	0	-225	3096	11.07	-0.32	0
111	SLU 79	0	-225	3096	11.07	-0.32	0
111	SLU 80	0	-225	3096	11.07	-0.32	0
111	SLU 81	0	-246	3251	12.08	-0.34	0
111	SLU 82	0	-246	3251	12.08	-0.34	0
111	SLU 83	0	-246	3251	12.08	-0.34	0
111	SLU 84	0	-246	3251	12.08	-0.34	0
111	SLE RA 1	0	-130	2061	6.48	-0.22	0
111	SLE RA 2	0	-130	2061	6.48	-0.22	0
111	SLE RA 3	0	-130	2061	6.48	-0.22	0
111	SLE RA 4	0	-130	2061	6.48	-0.22	0
111	SLE RA 5	0	-130	2061	6.48	-0.22	0
111	SLE RA 6	0	-130	2061	6.48	-0.22	0
111	SLE RA 7	0	-130	2061	6.48	-0.22	0
111	SLE RA 8	0	-130	2061	6.48	-0.22	0
111	SLE RA 9	0	-130	2061	6.48	-0.22	0
111	SLE RA 10	0	-164	2302	8.06	-0.24	0
111	SLE RA 11	0	-164	2302	8.06	-0.24	0
111	SLE RA 12	0	-164	2302	8.06	-0.24	0
111	SLE RA 13	0	-164	2302	8.06	-0.24	0
111	SLE RA 14	0	-164	2302	8.06	-0.24	0
111	SLE RA 15	0	-164	2302	8.06	-0.24	0
111	SLE RA 16	0	-164	2302	8.06	-0.24	0
111	SLE RA 17	0	-164	2302	8.06	-0.24	0
111	SLE RA 18	0	-178	2405	8.74	-0.25	0
111	SLE RA 19	0	-178	2405	8.74	-0.25	0
111	SLE RA 20	0	-178	2405	8.74	-0.25	0
111	SLE RA 21	0	-178	2405	8.74	-0.25	0
111	SLE FR 1	0	-130	2061	6.48	-0.22	0
111	SLE FR 2	0	-130	2061	6.48	-0.22	0
111	SLE FR 3	0	-130	2061	6.48	-0.22	0
111	SLE FR 4	0	-145	2164	7.16	-0.23	0
111	SLE FR 5	0	-145	2164	7.16	-0.23	0
111	SLE FR 6	0	-154	2233	7.61	-0.23	0
111	SLE QP 1	0	-130	2061	6.48	-0.22	0
111	SLE QP 2	0	-145	2164	7.16	-0.23	0
111	SLD 1	18	-152	1993	7.32	19.18	0.02
111	SLD 2	18	-152	1993	7.32	19.18	0.02
111	SLD 3	28	-299	2047	13.52	26.8	0.01
111	SLD 4	28	-299	2047	13.52	26.8	0.01
111	SLD 5	-11	76	2031	-2.21	-5.96	0.01
111	SLD 6	-11	76	2031	-2.21	-5.96	0.01
111	SLD 7	24	-414	2211	18.48	19.44	-0.01
111	SLD 8	24	-414	2211	18.48	19.44	-0.01
111	SLD 9	-25	125	2118	-4.17	-19.9	0.01
111	SLD 10	-25	125	2118	-4.17	-19.9	0.01
111	SLD 11	11	-365	2298	16.53	5.51	-0.02
111	SLD 12	11	-365	2298	16.53	5.51	-0.02
111	SLD 13	-28	10	2282	0.79	-27.26	-0.01
111	SLD 14	-28	10	2282	0.79	-27.26	-0.01
111	SLD 15	-18	-137	2336	7	-19.64	-0.02
111	SLD 16	-18	-137	2336	7	-19.64	-0.02
111	SLV 1	43	-163	1758	7.53	47.61	0.04
111	SLV 2	43	-163	1758	7.53	47.61	0.04
111	SLV 3	70	-508	1886	22.12	67.06	0.02
111	SLV 4	70	-508	1886	22.12	67.06	0.02
111	SLV 5	-28	374	1849	-14.85	-15.39	0.04
111	SLV 6	-28	374	1849	-14.85	-15.39	0.04



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
111	SLV 7	62	-778	2274	33.76	49.47	-0.02
111	SLV 8	62	-778	2274	33.76	49.47	-0.02
111	SLV 9	-62	489	2055	-19.45	-49.93	0.02
111	SLV 10	-62	489	2055	-19.45	-49.93	0.02
111	SLV 11	28	-663	2480	29.16	14.93	-0.04
111	SLV 12	28	-663	2480	29.16	14.93	-0.04
111	SLV 13	-70	219	2443	-7.8	-67.52	-0.02
111	SLV 14	-70	219	2443	-7.8	-67.52	-0.02
111	SLV 15	-43	-126	2571	6.78	-48.06	-0.04
111	SLV 16	-43	-126	2571	6.78	-48.06	-0.04
112	SLU 1	0	0	1125	0.08	0	0
112	SLU 2	0	0	1125	0.08	0	0
112	SLU 3	0	0	1125	0.08	0	0
112	SLU 4	0	0	1125	0.08	0	0
112	SLU 5	0	0	1125	0.08	0	0
112	SLU 6	0	0	1125	0.08	0	0
112	SLU 7	0	0	1125	0.08	0	0
112	SLU 8	0	0	1125	0.08	0	0
112	SLU 9	0	0	1125	0.08	0	0
112	SLU 10	0	0	1528	0.07	0.01	0
112	SLU 11	0	0	1528	0.07	0.01	0
112	SLU 12	0	0	1528	0.07	0.01	0
112	SLU 13	0	0	1528	0.07	0.01	0
112	SLU 14	0	0	1528	0.07	0.01	0
112	SLU 15	0	0	1528	0.07	0.01	0
112	SLU 16	0	0	1528	0.07	0.01	0
112	SLU 17	0	0	1528	0.07	0.01	0
112	SLU 18	0	0	1700	0.07	0.01	0
112	SLU 19	0	0	1700	0.07	0.01	0
112	SLU 20	0	0	1700	0.07	0.01	0
112	SLU 21	0	0	1700	0.07	0.01	0
112	SLU 22	0	0	1334	0.09	0.01	0
112	SLU 23	0	0	1334	0.09	0.01	0
112	SLU 24	0	0	1334	0.09	0.01	0
112	SLU 25	0	0	1334	0.09	0.01	0
112	SLU 26	0	0	1334	0.09	0.01	0
112	SLU 27	0	0	1334	0.09	0.01	0
112	SLU 28	0	0	1334	0.09	0.01	0
112	SLU 29	0	0	1334	0.09	0.01	0
112	SLU 30	0	0	1334	0.09	0.01	0
112	SLU 31	0	0	1736	0.08	0.01	0
112	SLU 32	0	0	1736	0.08	0.01	0
112	SLU 33	0	0	1736	0.08	0.01	0
112	SLU 34	0	0	1736	0.08	0.01	0
112	SLU 35	0	0	1736	0.08	0.01	0
112	SLU 36	0	0	1736	0.08	0.01	0
112	SLU 37	0	0	1736	0.08	0.01	0
112	SLU 38	0	0	1736	0.08	0.01	0
112	SLU 39	0	0	1908	0.08	0.01	0
112	SLU 40	0	0	1908	0.08	0.01	0
112	SLU 41	0	0	1908	0.08	0.01	0
112	SLU 42	0	0	1908	0.08	0.01	0
112	SLU 43	0	0	1391	0.1	0	0
112	SLU 44	0	0	1391	0.1	0	0
112	SLU 45	0	0	1391	0.1	0	0
112	SLU 46	0	0	1391	0.1	0	0
112	SLU 47	0	0	1391	0.1	0	0
112	SLU 48	0	0	1391	0.1	0	0
112	SLU 49	0	0	1391	0.1	0	0
112	SLU 50	0	0	1391	0.1	0	0
112	SLU 51	0	0	1391	0.1	0	0
112	SLU 52	0	0	1794	0.1	0.01	0
112	SLU 53	0	0	1794	0.1	0.01	0
112	SLU 54	0	0	1794	0.1	0.01	0
112	SLU 55	0	0	1794	0.1	0.01	0
112	SLU 56	0	0	1794	0.1	0.01	0
112	SLU 57	0	0	1794	0.1	0.01	0
112	SLU 58	0	0	1794	0.1	0.01	0
112	SLU 59	0	0	1794	0.1	0.01	0
112	SLU 60	0	0	1966	0.09	0.01	0
112	SLU 61	0	0	1966	0.09	0.01	0
112	SLU 62	0	0	1966	0.09	0.01	0
112	SLU 63	0	0	1966	0.09	0.01	0
112	SLU 64	0	0	1600	0.11	0.01	0
112	SLU 65	0	0	1600	0.11	0.01	0
112	SLU 66	0	0	1600	0.11	0.01	0
112	SLU 67	0	0	1600	0.11	0.01	0
112	SLU 68	0	0	1600	0.11	0.01	0
112	SLU 69	0	0	1600	0.11	0.01	0
112	SLU 70	0	0	1600	0.11	0.01	0
112	SLU 71	0	0	1600	0.11	0.01	0
112	SLU 72	0	0	1600	0.11	0.01	0
112	SLU 73	0	0	2002	0.1	0.01	0
112	SLU 74	0	0	2002	0.1	0.01	0
112	SLU 75	0	0	2002	0.1	0.01	0
112	SLU 76	0	0	2002	0.1	0.01	0
112	SLU 77	0	0	2002	0.1	0.01	0
112	SLU 78	0	0	2002	0.1	0.01	0
112	SLU 79	0	0	2002	0.1	0.01	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
112	SLU 80	0	0	2002	0.1	0.01	0
112	SLU 81	0	0	2174	0.1	0.01	0
112	SLU 82	0	0	2174	0.1	0.01	0
112	SLU 83	0	0	2174	0.1	0.01	0
112	SLU 84	0	0	2174	0.1	0.01	0
112	SLE RA 1	0	0	1185	0.08	0	0
112	SLE RA 2	0	0	1185	0.08	0	0
112	SLE RA 3	0	0	1185	0.08	0	0
112	SLE RA 4	0	0	1185	0.08	0	0
112	SLE RA 5	0	0	1185	0.08	0	0
112	SLE RA 6	0	0	1185	0.08	0	0
112	SLE RA 7	0	0	1185	0.08	0	0
112	SLE RA 8	0	0	1185	0.08	0	0
112	SLE RA 9	0	0	1185	0.08	0	0
112	SLE RA 10	0	0	1453	0.08	0.01	0
112	SLE RA 11	0	0	1453	0.08	0.01	0
112	SLE RA 12	0	0	1453	0.08	0.01	0
112	SLE RA 13	0	0	1453	0.08	0.01	0
112	SLE RA 14	0	0	1453	0.08	0.01	0
112	SLE RA 15	0	0	1453	0.08	0.01	0
112	SLE RA 16	0	0	1453	0.08	0.01	0
112	SLE RA 17	0	0	1453	0.08	0.01	0
112	SLE RA 18	0	0	1568	0.08	0.01	0
112	SLE RA 19	0	0	1568	0.08	0.01	0
112	SLE RA 20	0	0	1568	0.08	0.01	0
112	SLE RA 21	0	0	1568	0.08	0.01	0
112	SLE FR 1	0	0	1185	0.08	0	0
112	SLE FR 2	0	0	1185	0.08	0	0
112	SLE FR 3	0	0	1185	0.08	0	0
112	SLE FR 4	0	0	1300	0.08	0	0
112	SLE FR 5	0	0	1300	0.08	0	0
112	SLE FR 6	0	0	1376	0.08	0.01	0
112	SLE QP 1	0	0	1185	0.08	0	0
112	SLE QP 2	0	0	1300	0.08	0	0
112	SLD 1	-3	0	1325	-15.38	5.04	0
112	SLD 2	-3	0	1325	-15.38	5.04	0
112	SLD 3	-4	-1	1245	29.59	3.02	-0.03
112	SLD 4	-4	-1	1245	29.59	3.02	-0.03
112	SLD 5	2	2	1428	-72.76	4.59	0.05
112	SLD 6	2	2	1428	-72.76	4.59	0.05
112	SLD 7	-4	-3	1163	77.14	-2.16	-0.05
112	SLD 8	-4	-3	1163	77.14	-2.16	-0.05
112	SLD 9	4	3	1437	-76.98	2.17	0.05
112	SLD 10	4	3	1437	-76.98	2.17	0.05
112	SLD 11	-2	-2	1171	72.92	-4.58	-0.05
112	SLD 12	-2	-2	1171	72.92	-4.58	-0.05
112	SLD 13	4	1	1354	-29.43	-3.01	0.03
112	SLD 14	4	1	1354	-29.43	-3.01	0.03
112	SLD 15	3	0	1274	15.54	-5.03	0
112	SLD 16	3	0	1274	15.54	-5.03	0
112	SLV 1	-6	0	1365	-39.58	12.83	0.01
112	SLV 2	-6	0	1365	-39.58	12.83	0.01
112	SLV 3	-11	-4	1161	75.79	7.65	-0.07
112	SLV 4	-11	-4	1161	75.79	7.65	-0.07
112	SLV 5	5	5	1629	-186.79	11.72	0.12
112	SLV 6	5	5	1629	-186.79	11.72	0.12
112	SLV 7	-10	-7	949	197.77	-5.57	-0.14
112	SLV 8	-10	-7	949	197.77	-5.57	-0.14
112	SLV 9	10	6	1651	-197.61	5.58	0.14
112	SLV 10	10	6	1651	-197.61	5.58	0.14
112	SLV 11	-5	-6	971	186.95	-11.71	-0.12
112	SLV 12	-5	-6	971	186.95	-11.71	-0.12
112	SLV 13	11	3	1438	-75.63	-7.64	0.07
112	SLV 14	11	3	1438	-75.63	-7.64	0.07
112	SLV 15	6	0	1234	39.74	-12.82	-0.01
112	SLV 16	6	0	1234	39.74	-12.82	-0.01
113	SLU 1	145	-245	2316	8.77	4.8	-0.03
113	SLU 2	145	-245	2316	8.77	4.8	-0.03
113	SLU 3	145	-245	2316	8.77	4.8	-0.03
113	SLU 4	145	-245	2316	8.77	4.8	-0.03
113	SLU 5	145	-245	2316	8.77	4.8	-0.03
113	SLU 6	145	-245	2316	8.77	4.8	-0.03
113	SLU 7	145	-245	2316	8.77	4.8	-0.03
113	SLU 8	145	-245	2316	8.77	4.8	-0.03
113	SLU 9	145	-245	2316	8.77	4.8	-0.03
113	SLU 10	178	-325	2938	11.51	6.06	-0.04
113	SLU 11	178	-325	2938	11.51	6.06	-0.04
113	SLU 12	178	-325	2938	11.51	6.06	-0.04
113	SLU 13	178	-325	2938	11.51	6.06	-0.04
113	SLU 14	178	-325	2938	11.51	6.06	-0.04
113	SLU 15	178	-325	2938	11.51	6.06	-0.04
113	SLU 16	178	-325	2938	11.51	6.06	-0.04
113	SLU 17	178	-325	2938	11.51	6.06	-0.04
113	SLU 18	192	-360	3205	12.68	6.6	-0.05
113	SLU 19	192	-360	3205	12.68	6.6	-0.05
113	SLU 20	192	-360	3205	12.68	6.6	-0.05
113	SLU 21	192	-360	3205	12.68	6.6	-0.05
113	SLU 22	162	-282	2619	10.07	5.42	-0.04
113	SLU 23	162	-282	2619	10.07	5.42	-0.04



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
113	SLU 24	162	-282	2619	10.07	5.42	-0.04
113	SLU 25	162	-282	2619	10.07	5.42	-0.04
113	SLU 26	162	-282	2619	10.07	5.42	-0.04
113	SLU 27	162	-282	2619	10.07	5.42	-0.04
113	SLU 28	162	-282	2619	10.07	5.42	-0.04
113	SLU 29	162	-282	2619	10.07	5.42	-0.04
113	SLU 30	162	-282	2619	10.07	5.42	-0.04
113	SLU 31	195	-362	3241	12.81	6.68	-0.05
113	SLU 32	195	-362	3241	12.81	6.68	-0.05
113	SLU 33	195	-362	3241	12.81	6.68	-0.05
113	SLU 34	195	-362	3241	12.81	6.68	-0.05
113	SLU 35	195	-362	3241	12.81	6.68	-0.05
113	SLU 36	195	-362	3241	12.81	6.68	-0.05
113	SLU 37	195	-362	3241	12.81	6.68	-0.05
113	SLU 38	195	-362	3241	12.81	6.68	-0.05
113	SLU 39	209	-397	3508	13.98	7.23	-0.05
113	SLU 40	209	-397	3508	13.98	7.23	-0.05
113	SLU 41	209	-397	3508	13.98	7.23	-0.05
113	SLU 42	209	-397	3508	13.98	7.23	-0.05
113	SLU 43	182	-306	2907	10.96	6.02	-0.04
113	SLU 44	182	-306	2907	10.96	6.02	-0.04
113	SLU 45	182	-306	2907	10.96	6.02	-0.04
113	SLU 46	182	-306	2907	10.96	6.02	-0.04
113	SLU 47	182	-306	2907	10.96	6.02	-0.04
113	SLU 48	182	-306	2907	10.96	6.02	-0.04
113	SLU 49	182	-306	2907	10.96	6.02	-0.04
113	SLU 50	182	-306	2907	10.96	6.02	-0.04
113	SLU 51	182	-306	2907	10.96	6.02	-0.04
113	SLU 52	215	-386	3529	13.7	7.29	-0.05
113	SLU 53	215	-386	3529	13.7	7.29	-0.05
113	SLU 54	215	-386	3529	13.7	7.29	-0.05
113	SLU 55	215	-386	3529	13.7	7.29	-0.05
113	SLU 56	215	-386	3529	13.7	7.29	-0.05
113	SLU 57	215	-386	3529	13.7	7.29	-0.05
113	SLU 58	215	-386	3529	13.7	7.29	-0.05
113	SLU 59	215	-386	3529	13.7	7.29	-0.05
113	SLU 60	229	-421	3796	14.87	7.83	-0.06
113	SLU 61	229	-421	3796	14.87	7.83	-0.06
113	SLU 62	229	-421	3796	14.87	7.83	-0.06
113	SLU 63	229	-421	3796	14.87	7.83	-0.06
113	SLU 64	200	-343	3210	12.25	6.65	-0.05
113	SLU 65	200	-343	3210	12.25	6.65	-0.05
113	SLU 66	200	-343	3210	12.25	6.65	-0.05
113	SLU 67	200	-343	3210	12.25	6.65	-0.05
113	SLU 68	200	-343	3210	12.25	6.65	-0.05
113	SLU 69	200	-343	3210	12.25	6.65	-0.05
113	SLU 70	200	-343	3210	12.25	6.65	-0.05
113	SLU 71	200	-343	3210	12.25	6.65	-0.05
113	SLU 72	200	-343	3210	12.25	6.65	-0.05
113	SLU 73	233	-423	3832	14.99	7.91	-0.06
113	SLU 74	233	-423	3832	14.99	7.91	-0.06
113	SLU 75	233	-423	3832	14.99	7.91	-0.06
113	SLU 76	233	-423	3832	14.99	7.91	-0.06
113	SLU 77	233	-423	3832	14.99	7.91	-0.06
113	SLU 78	233	-423	3832	14.99	7.91	-0.06
113	SLU 79	233	-423	3832	14.99	7.91	-0.06
113	SLU 80	233	-423	3832	14.99	7.91	-0.06
113	SLU 81	247	-457	4099	16.17	8.45	-0.06
113	SLU 82	247	-457	4099	16.17	8.45	-0.06
113	SLU 83	247	-457	4099	16.17	8.45	-0.06
113	SLU 84	247	-457	4099	16.17	8.45	-0.06
113	SLE RA 1	150	-256	2403	9.14	4.98	-0.03
113	SLE RA 2	150	-256	2403	9.14	4.98	-0.03
113	SLE RA 3	150	-256	2403	9.14	4.98	-0.03
113	SLE RA 4	150	-256	2403	9.14	4.98	-0.03
113	SLE RA 5	150	-256	2403	9.14	4.98	-0.03
113	SLE RA 6	150	-256	2403	9.14	4.98	-0.03
113	SLE RA 7	150	-256	2403	9.14	4.98	-0.03
113	SLE RA 8	150	-256	2403	9.14	4.98	-0.03
113	SLE RA 9	150	-256	2403	9.14	4.98	-0.03
113	SLE RA 10	172	-309	2817	10.97	5.82	-0.04
113	SLE RA 11	172	-309	2817	10.97	5.82	-0.04
113	SLE RA 12	172	-309	2817	10.97	5.82	-0.04
113	SLE RA 13	172	-309	2817	10.97	5.82	-0.04
113	SLE RA 14	172	-309	2817	10.97	5.82	-0.04
113	SLE RA 15	172	-309	2817	10.97	5.82	-0.04
113	SLE RA 16	172	-309	2817	10.97	5.82	-0.04
113	SLE RA 17	172	-309	2817	10.97	5.82	-0.04
113	SLE RA 18	181	-332	2995	11.75	6.18	-0.04
113	SLE RA 19	181	-332	2995	11.75	6.18	-0.04
113	SLE RA 20	181	-332	2995	11.75	6.18	-0.04
113	SLE RA 21	181	-332	2995	11.75	6.18	-0.04
113	SLE FR 1	150	-256	2403	9.14	4.98	-0.03
113	SLE FR 2	150	-256	2403	9.14	4.98	-0.03
113	SLE FR 3	150	-256	2403	9.14	4.98	-0.03
113	SLE FR 4	159	-279	2580	9.92	5.34	-0.04
113	SLE FR 5	159	-279	2580	9.92	5.34	-0.04
113	SLE FR 6	166	-294	2699	10.45	5.58	-0.04
113	SLE QP 1	150	-256	2403	9.14	4.98	-0.03



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
113	SLE QP 2	159	-279	2580	9.92	5.34	-0.04
113	SLD 1	384	-45	3922	0.41	15.42	0.02
113	SLD 2	384	-45	3922	0.41	15.42	0.02
113	SLD 3	285	-221	3428	7.2	11.15	-0.01
113	SLD 4	285	-221	3428	7.2	11.15	-0.01
113	SLD 5	377	58	3732	-3.22	14.84	0.02
113	SLD 6	377	58	3732	-3.22	14.84	0.02
113	SLD 7	47	-527	2086	19.4	0.6	-0.08
113	SLD 8	47	-527	2086	19.4	0.6	-0.08
113	SLD 9	272	-30	3075	0.45	10.07	0
113	SLD 10	272	-30	3075	0.45	10.07	0
113	SLD 11	-58	-615	1429	23.07	-4.17	-0.1
113	SLD 12	-58	-615	1429	23.07	-4.17	-0.1
113	SLD 13	34	-337	1732	12.65	-0.48	-0.06
113	SLD 14	34	-337	1732	12.65	-0.48	-0.06
113	SLD 15	-65	-512	1239	19.44	-4.75	-0.09
113	SLD 16	-65	-512	1239	19.44	-4.75	-0.09
113	SLV 1	713	279	5942	-12.95	30.27	0.09
113	SLV 2	713	279	5942	-12.95	30.27	0.09
113	SLV 3	470	-137	4709	3.15	19.73	0.02
113	SLV 4	470	-137	4709	3.15	19.73	0.02
113	SLV 5	694	520	5459	-21.35	28.8	0.11
113	SLV 6	694	520	5459	-21.35	28.8	0.11
113	SLV 7	-116	-867	1349	32.3	-6.33	-0.13
113	SLV 8	-116	-867	1349	32.3	-6.33	-0.13
113	SLV 9	434	310	3812	-12.45	17.01	0.05
113	SLV 10	434	310	3812	-12.45	17.01	0.05
113	SLV 11	-375	-1077	-298	41.2	-18.13	-0.18
113	SLV 12	-375	-1077	-298	41.2	-18.13	-0.18
113	SLV 13	-152	-420	452	16.7	-9.05	-0.1
113	SLV 14	-152	-420	452	16.7	-9.05	-0.1
113	SLV 15	-395	-836	-781	32.79	-19.59	-0.17
113	SLV 16	-395	-836	-781	32.79	-19.59	-0.17
114	SLU 1	0	-212	2150	8.84	-0.43	0
114	SLU 2	0	-212	2150	8.84	-0.43	0
114	SLU 3	0	-212	2150	8.84	-0.43	0
114	SLU 4	0	-212	2150	8.84	-0.43	0
114	SLU 5	0	-212	2150	8.84	-0.43	0
114	SLU 6	0	-212	2150	8.84	-0.43	0
114	SLU 7	0	-212	2150	8.84	-0.43	0
114	SLU 8	0	-212	2150	8.84	-0.43	0
114	SLU 9	0	-212	2150	8.84	-0.43	0
114	SLU 10	0	-279	2555	11.61	-0.51	-0.01
114	SLU 11	0	-279	2555	11.61	-0.51	-0.01
114	SLU 12	0	-279	2555	11.61	-0.51	-0.01
114	SLU 13	0	-279	2555	11.61	-0.51	-0.01
114	SLU 14	0	-279	2555	11.61	-0.51	-0.01
114	SLU 15	0	-279	2555	11.61	-0.51	-0.01
114	SLU 16	0	-279	2555	11.61	-0.51	-0.01
114	SLU 17	0	-279	2555	11.61	-0.51	-0.01
114	SLU 18	0	-307	2729	12.81	-0.55	-0.01
114	SLU 19	0	-307	2729	12.81	-0.55	-0.01
114	SLU 20	0	-307	2729	12.81	-0.55	-0.01
114	SLU 21	0	-307	2729	12.81	-0.55	-0.01
114	SLU 22	0	-239	2370	9.98	-0.48	-0.01
114	SLU 23	0	-239	2370	9.98	-0.48	-0.01
114	SLU 24	0	-239	2370	9.98	-0.48	-0.01
114	SLU 25	0	-239	2370	9.98	-0.48	-0.01
114	SLU 26	0	-239	2370	9.98	-0.48	-0.01
114	SLU 27	0	-239	2370	9.98	-0.48	-0.01
114	SLU 28	0	-239	2370	9.98	-0.48	-0.01
114	SLU 29	0	-239	2370	9.98	-0.48	-0.01
114	SLU 30	0	-239	2370	9.98	-0.48	-0.01
114	SLU 31	0	-305	2776	12.76	-0.56	-0.01
114	SLU 32	0	-305	2776	12.76	-0.56	-0.01
114	SLU 33	0	-305	2776	12.76	-0.56	-0.01
114	SLU 34	0	-305	2776	12.76	-0.56	-0.01
114	SLU 35	0	-305	2776	12.76	-0.56	-0.01
114	SLU 36	0	-305	2776	12.76	-0.56	-0.01
114	SLU 37	0	-305	2776	12.76	-0.56	-0.01
114	SLU 38	0	-305	2776	12.76	-0.56	-0.01
114	SLU 39	0	-334	2950	13.95	-0.6	-0.01
114	SLU 40	0	-334	2950	13.95	-0.6	-0.01
114	SLU 41	0	-334	2950	13.95	-0.6	-0.01
114	SLU 42	0	-334	2950	13.95	-0.6	-0.01
114	SLU 43	0	-267	2719	11.09	-0.54	-0.01
114	SLU 44	0	-267	2719	11.09	-0.54	-0.01
114	SLU 45	0	-267	2719	11.09	-0.54	-0.01
114	SLU 46	0	-267	2719	11.09	-0.54	-0.01
114	SLU 47	0	-267	2719	11.09	-0.54	-0.01
114	SLU 48	0	-267	2719	11.09	-0.54	-0.01
114	SLU 49	0	-267	2719	11.09	-0.54	-0.01
114	SLU 50	0	-267	2719	11.09	-0.54	-0.01
114	SLU 51	0	-267	2719	11.09	-0.54	-0.01
114	SLU 52	0	-333	3125	13.87	-0.62	-0.01
114	SLU 53	0	-333	3125	13.87	-0.62	-0.01
114	SLU 54	0	-333	3125	13.87	-0.62	-0.01
114	SLU 55	0	-333	3125	13.87	-0.62	-0.01
114	SLU 56	0	-333	3125	13.87	-0.62	-0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
114	SLU 57	0	-333	3125	13.87	-0.62	-0.01
114	SLU 58	0	-333	3125	13.87	-0.62	-0.01
114	SLU 59	0	-333	3125	13.87	-0.62	-0.01
114	SLU 60	0	-362	3298	15.06	-0.66	-0.01
114	SLU 61	0	-362	3298	15.06	-0.66	-0.01
114	SLU 62	0	-362	3298	15.06	-0.66	-0.01
114	SLU 63	0	-362	3298	15.06	-0.66	-0.01
114	SLU 64	0	-294	2940	12.24	-0.59	-0.01
114	SLU 65	0	-294	2940	12.24	-0.59	-0.01
114	SLU 66	0	-294	2940	12.24	-0.59	-0.01
114	SLU 67	0	-294	2940	12.24	-0.59	-0.01
114	SLU 68	0	-294	2940	12.24	-0.59	-0.01
114	SLU 69	0	-294	2940	12.24	-0.59	-0.01
114	SLU 70	0	-294	2940	12.24	-0.59	-0.01
114	SLU 71	0	-294	2940	12.24	-0.59	-0.01
114	SLU 72	0	-294	2940	12.24	-0.59	-0.01
114	SLU 73	0	-360	3345	15.02	-0.67	-0.01
114	SLU 74	0	-360	3345	15.02	-0.67	-0.01
114	SLU 75	0	-360	3345	15.02	-0.67	-0.01
114	SLU 76	0	-360	3345	15.02	-0.67	-0.01
114	SLU 77	0	-360	3345	15.02	-0.67	-0.01
114	SLU 78	0	-360	3345	15.02	-0.67	-0.01
114	SLU 79	0	-360	3345	15.02	-0.67	-0.01
114	SLU 80	0	-360	3345	15.02	-0.67	-0.01
114	SLU 81	0	-388	3519	16.21	-0.71	-0.01
114	SLU 82	0	-388	3519	16.21	-0.71	-0.01
114	SLU 83	0	-388	3519	16.21	-0.71	-0.01
114	SLU 84	0	-388	3519	16.21	-0.71	-0.01
114	SLE RA 1	0	-220	2213	9.16	-0.44	-0.01
114	SLE RA 2	0	-220	2213	9.16	-0.44	-0.01
114	SLE RA 3	0	-220	2213	9.16	-0.44	-0.01
114	SLE RA 4	0	-220	2213	9.16	-0.44	-0.01
114	SLE RA 5	0	-220	2213	9.16	-0.44	-0.01
114	SLE RA 6	0	-220	2213	9.16	-0.44	-0.01
114	SLE RA 7	0	-220	2213	9.16	-0.44	-0.01
114	SLE RA 8	0	-220	2213	9.16	-0.44	-0.01
114	SLE RA 9	0	-220	2213	9.16	-0.44	-0.01
114	SLE RA 10	0	-264	2483	11.02	-0.5	-0.01
114	SLE RA 11	0	-264	2483	11.02	-0.5	-0.01
114	SLE RA 12	0	-264	2483	11.02	-0.5	-0.01
114	SLE RA 13	0	-264	2483	11.02	-0.5	-0.01
114	SLE RA 14	0	-264	2483	11.02	-0.5	-0.01
114	SLE RA 15	0	-264	2483	11.02	-0.5	-0.01
114	SLE RA 16	0	-264	2483	11.02	-0.5	-0.01
114	SLE RA 17	0	-264	2483	11.02	-0.5	-0.01
114	SLE RA 18	0	-283	2599	11.81	-0.52	-0.01
114	SLE RA 19	0	-283	2599	11.81	-0.52	-0.01
114	SLE RA 20	0	-283	2599	11.81	-0.52	-0.01
114	SLE RA 21	0	-283	2599	11.81	-0.52	-0.01
114	SLE FR 1	0	-220	2213	9.16	-0.44	-0.01
114	SLE FR 2	0	-220	2213	9.16	-0.44	-0.01
114	SLE FR 3	0	-220	2213	9.16	-0.44	-0.01
114	SLE FR 4	0	-239	2329	9.96	-0.47	-0.01
114	SLE FR 5	0	-239	2329	9.96	-0.47	-0.01
114	SLE FR 6	0	-252	2406	10.49	-0.48	-0.01
114	SLE QP 1	0	-220	2213	9.16	-0.44	-0.01
114	SLE QP 2	0	-239	2329	9.96	-0.47	-0.01
114	SLD 1	7	-253	2074	3.7	11.1	0.02
114	SLD 2	7	-253	2074	3.7	11.1	0.02
114	SLD 3	18	-392	2171	9.5	17.88	0.01
114	SLD 4	18	-392	2171	9.5	17.88	0.01
114	SLD 5	-16	-33	2104	-0.72	-7.28	0.01
114	SLD 6	-16	-33	2104	-0.72	-7.28	0.01
114	SLD 7	23	-495	2429	18.62	15.33	-0.01
114	SLD 8	23	-495	2429	18.62	15.33	-0.01
114	SLD 9	-24	17	2228	1.3	-16.26	0
114	SLD 10	-24	17	2228	1.3	-16.26	0
114	SLD 11	15	-445	2553	20.63	6.35	-0.02
114	SLD 12	15	-445	2553	20.63	6.35	-0.02
114	SLD 13	-19	-86	2486	10.42	-18.82	-0.02
114	SLD 14	-19	-86	2486	10.42	-18.82	-0.02
114	SLD 15	-7	-225	2583	16.22	-12.03	-0.03
114	SLD 16	-7	-225	2583	16.22	-12.03	-0.03
114	SLV 1	16	-273	1725	-4.76	28.01	0.05
114	SLV 2	16	-273	1725	-4.76	28.01	0.05
114	SLV 3	46	-598	1954	8.86	45.32	0.03
114	SLV 4	46	-598	1954	8.86	45.32	0.03
114	SLV 5	-41	245	1799	-15.13	-18.19	0.04
114	SLV 6	-41	245	1799	-15.13	-18.19	0.04
114	SLV 7	59	-840	2564	30.3	39.53	-0.02
114	SLV 8	59	-840	2564	30.3	39.53	-0.02
114	SLV 9	-60	362	2093	-10.38	-40.46	0.01
114	SLV 10	-60	362	2093	-10.38	-40.46	0.01
114	SLV 11	40	-722	2858	35.04	17.25	-0.05
114	SLV 12	40	-722	2858	35.04	17.25	-0.05
114	SLV 13	-46	120	2703	11.05	-46.25	-0.04
114	SLV 14	-46	120	2703	11.05	-46.25	-0.04
114	SLV 15	-16	-205	2933	24.68	-28.94	-0.06
114	SLV 16	-16	-205	2933	24.68	-28.94	-0.06



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
115	SLU 1	0	0	1088	0.11	-0.01	0
115	SLU 2	0	0	1088	0.11	-0.01	0
115	SLU 3	0	0	1088	0.11	-0.01	0
115	SLU 4	0	0	1088	0.11	-0.01	0
115	SLU 5	0	0	1088	0.11	-0.01	0
115	SLU 6	0	0	1088	0.11	-0.01	0
115	SLU 7	0	0	1088	0.11	-0.01	0
115	SLU 8	0	0	1088	0.11	-0.01	0
115	SLU 9	0	0	1088	0.11	-0.01	0
115	SLU 10	0	0	1419	0.12	0	0
115	SLU 11	0	0	1419	0.12	0	0
115	SLU 12	0	0	1419	0.12	0	0
115	SLU 13	0	0	1419	0.12	0	0
115	SLU 14	0	0	1419	0.12	0	0
115	SLU 15	0	0	1419	0.12	0	0
115	SLU 16	0	0	1419	0.12	0	0
115	SLU 17	0	0	1419	0.12	0	0
115	SLU 18	0	0	1561	0.13	0	0
115	SLU 19	0	0	1561	0.13	0	0
115	SLU 20	0	0	1561	0.13	0	0
115	SLU 21	0	0	1561	0.13	0	0
115	SLU 22	0	0	1270	0.13	0	0
115	SLU 23	0	0	1270	0.13	0	0
115	SLU 24	0	0	1270	0.13	0	0
115	SLU 25	0	0	1270	0.13	0	0
115	SLU 26	0	0	1270	0.13	0	0
115	SLU 27	0	0	1270	0.13	0	0
115	SLU 28	0	0	1270	0.13	0	0
115	SLU 29	0	0	1270	0.13	0	0
115	SLU 30	0	0	1270	0.13	0	0
115	SLU 31	0	0	1601	0.14	0	0
115	SLU 32	0	0	1601	0.14	0	0
115	SLU 33	0	0	1601	0.14	0	0
115	SLU 34	0	0	1601	0.14	0	0
115	SLU 35	0	0	1601	0.14	0	0
115	SLU 36	0	0	1601	0.14	0	0
115	SLU 37	0	0	1601	0.14	0	0
115	SLU 38	0	0	1601	0.14	0	0
115	SLU 39	0	0	1743	0.14	0	0
115	SLU 40	0	0	1743	0.14	0	0
115	SLU 41	0	0	1743	0.14	0	0
115	SLU 42	0	0	1743	0.14	0	0
115	SLU 43	0	0	1352	0.14	-0.01	0
115	SLU 44	0	0	1352	0.14	-0.01	0
115	SLU 45	0	0	1352	0.14	-0.01	0
115	SLU 46	0	0	1352	0.14	-0.01	0
115	SLU 47	0	0	1352	0.14	-0.01	0
115	SLU 48	0	0	1352	0.14	-0.01	0
115	SLU 49	0	0	1352	0.14	-0.01	0
115	SLU 50	0	0	1352	0.14	-0.01	0
115	SLU 51	0	0	1352	0.14	-0.01	0
115	SLU 52	0	0	1684	0.15	0	0
115	SLU 53	0	0	1684	0.15	0	0
115	SLU 54	0	0	1684	0.15	0	0
115	SLU 55	0	0	1684	0.15	0	0
115	SLU 56	0	0	1684	0.15	0	0
115	SLU 57	0	0	1684	0.15	0	0
115	SLU 58	0	0	1684	0.15	0	0
115	SLU 59	0	0	1684	0.15	0	0
115	SLU 60	0	0	1826	0.15	0	0
115	SLU 61	0	0	1826	0.15	0	0
115	SLU 62	0	0	1826	0.15	0	0
115	SLU 63	0	0	1826	0.15	0	0
115	SLU 64	0	0	1534	0.16	-0.01	0
115	SLU 65	0	0	1534	0.16	-0.01	0
115	SLU 66	0	0	1534	0.16	-0.01	0
115	SLU 67	0	0	1534	0.16	-0.01	0
115	SLU 68	0	0	1534	0.16	-0.01	0
115	SLU 69	0	0	1534	0.16	-0.01	0
115	SLU 70	0	0	1534	0.16	-0.01	0
115	SLU 71	0	0	1534	0.16	-0.01	0
115	SLU 72	0	0	1534	0.16	-0.01	0
115	SLU 73	0	0	1865	0.17	0	0
115	SLU 74	0	0	1865	0.17	0	0
115	SLU 75	0	0	1865	0.17	0	0
115	SLU 76	0	0	1865	0.17	0	0
115	SLU 77	0	0	1865	0.17	0	0
115	SLU 78	0	0	1865	0.17	0	0
115	SLU 79	0	0	1865	0.17	0	0
115	SLU 80	0	0	1865	0.17	0	0
115	SLU 81	0	0	2007	0.17	0	0
115	SLU 82	0	0	2007	0.17	0	0
115	SLU 83	0	0	2007	0.17	0	0
115	SLU 84	0	0	2007	0.17	0	0
115	SLE RA 1	0	0	1140	0.12	-0.01	0
115	SLE RA 2	0	0	1140	0.12	-0.01	0
115	SLE RA 3	0	0	1140	0.12	-0.01	0
115	SLE RA 4	0	0	1140	0.12	-0.01	0
115	SLE RA 5	0	0	1140	0.12	-0.01	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
115	SLE RA 6	0	0	1140	0.12	-0.01	0
115	SLE RA 7	0	0	1140	0.12	-0.01	0
115	SLE RA 8	0	0	1140	0.12	-0.01	0
115	SLE RA 9	0	0	1140	0.12	-0.01	0
115	SLE RA 10	0	0	1361	0.12	0	0
115	SLE RA 11	0	0	1361	0.12	0	0
115	SLE RA 12	0	0	1361	0.12	0	0
115	SLE RA 13	0	0	1361	0.12	0	0
115	SLE RA 14	0	0	1361	0.12	0	0
115	SLE RA 15	0	0	1361	0.12	0	0
115	SLE RA 16	0	0	1361	0.12	0	0
115	SLE RA 17	0	0	1361	0.12	0	0
115	SLE RA 18	0	0	1455	0.13	0	0
115	SLE RA 19	0	0	1455	0.13	0	0
115	SLE RA 20	0	0	1455	0.13	0	0
115	SLE RA 21	0	0	1455	0.13	0	0
115	SLE FR 1	0	0	1140	0.12	-0.01	0
115	SLE FR 2	0	0	1140	0.12	-0.01	0
115	SLE FR 3	0	0	1140	0.12	-0.01	0
115	SLE FR 4	0	0	1235	0.12	0	0
115	SLE FR 5	0	0	1235	0.12	0	0
115	SLE FR 6	0	0	1298	0.12	0	0
115	SLE QP 1	0	0	1140	0.12	-0.01	0
115	SLE QP 2	0	0	1235	0.12	0	0
115	SLD 1	0	-6	1264	-24.83	3.14	0.02
115	SLD 2	0	-6	1264	-24.83	3.14	0.02
115	SLD 3	-4	13	1171	47.73	1.37	-0.06
115	SLD 4	-4	13	1171	47.73	1.37	-0.06
115	SLD 5	5	-31	1385	-117.4	3.62	0.13
115	SLD 6	5	-31	1385	-117.4	3.62	0.13
115	SLD 7	-6	33	1074	124.44	-2.27	-0.15
115	SLD 8	-6	33	1074	124.44	-2.27	-0.15
115	SLD 9	6	-33	1395	-124.2	2.26	0.15
115	SLD 10	6	-33	1395	-124.2	2.26	0.15
115	SLD 11	-5	31	1085	117.65	-3.63	-0.14
115	SLD 12	-5	31	1085	117.65	-3.63	-0.14
115	SLD 13	4	-13	1298	-47.49	-1.38	0.06
115	SLD 14	4	-13	1298	-47.49	-1.38	0.06
115	SLD 15	0	6	1205	25.07	-3.15	-0.02
115	SLD 16	0	6	1205	25.07	-3.15	-0.02
115	SLV 1	-1	-16	1311	-63.88	8	0.06
115	SLV 2	-1	-16	1311	-63.88	8	0.06
115	SLV 3	-9	33	1072	122.25	3.47	-0.16
115	SLV 4	-9	33	1072	122.25	3.47	-0.16
115	SLV 5	12	-80	1620	-301.39	9.27	0.34
115	SLV 6	12	-80	1620	-301.39	9.27	0.34
115	SLV 7	-15	85	823	319.07	-5.84	-0.38
115	SLV 8	-15	85	823	319.07	-5.84	-0.38
115	SLV 9	15	-85	1646	-318.83	5.83	0.38
115	SLV 10	15	-85	1646	-318.83	5.83	0.38
115	SLV 11	-12	80	850	301.63	-9.28	-0.35
115	SLV 12	-12	80	850	301.63	-9.28	-0.35
115	SLV 13	9	-34	1398	-122.01	-3.48	0.16
115	SLV 14	9	-34	1398	-122.01	-3.48	0.16
115	SLV 15	1	16	1159	64.13	-8.01	-0.06
115	SLV 16	1	16	1159	64.13	-8.01	-0.06
116	SLU 1	44	40	1992	-1.34	4.17	0.06
116	SLU 2	44	40	1992	-1.34	4.17	0.06
116	SLU 3	44	40	1992	-1.34	4.17	0.06
116	SLU 4	44	40	1992	-1.34	4.17	0.06
116	SLU 5	44	40	1992	-1.34	4.17	0.06
116	SLU 6	44	40	1992	-1.34	4.17	0.06
116	SLU 7	44	40	1992	-1.34	4.17	0.06
116	SLU 8	44	40	1992	-1.34	4.17	0.06
116	SLU 9	44	40	1992	-1.34	4.17	0.06
116	SLU 10	42	36	2438	-1.47	5.09	0.08
116	SLU 11	42	36	2438	-1.47	5.09	0.08
116	SLU 12	42	36	2438	-1.47	5.09	0.08
116	SLU 13	42	36	2438	-1.47	5.09	0.08
116	SLU 14	42	36	2438	-1.47	5.09	0.08
116	SLU 15	42	36	2438	-1.47	5.09	0.08
116	SLU 16	42	36	2438	-1.47	5.09	0.08
116	SLU 17	42	36	2438	-1.47	5.09	0.08
116	SLU 18	41	34	2629	-1.53	5.49	0.08
116	SLU 19	41	34	2629	-1.53	5.49	0.08
116	SLU 20	41	34	2629	-1.53	5.49	0.08
116	SLU 21	41	34	2629	-1.53	5.49	0.08
116	SLU 22	47	42	2234	-1.45	4.68	0.07
116	SLU 23	47	42	2234	-1.45	4.68	0.07
116	SLU 24	47	42	2234	-1.45	4.68	0.07
116	SLU 25	47	42	2234	-1.45	4.68	0.07
116	SLU 26	47	42	2234	-1.45	4.68	0.07
116	SLU 27	47	42	2234	-1.45	4.68	0.07
116	SLU 28	47	42	2234	-1.45	4.68	0.07
116	SLU 29	47	42	2234	-1.45	4.68	0.07
116	SLU 30	47	42	2234	-1.45	4.68	0.07
116	SLU 31	45	38	2680	-1.59	5.61	0.08
116	SLU 32	45	38	2680	-1.59	5.61	0.08
116	SLU 33	45	38	2680	-1.59	5.61	0.08



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
116	SLU 34	45	38	2680	-1.59	5.61	0.08
116	SLU 35	45	38	2680	-1.59	5.61	0.08
116	SLU 36	45	38	2680	-1.59	5.61	0.08
116	SLU 37	45	38	2680	-1.59	5.61	0.08
116	SLU 38	45	38	2680	-1.59	5.61	0.08
116	SLU 39	44	36	2871	-1.65	6	0.09
116	SLU 40	44	36	2871	-1.65	6	0.09
116	SLU 41	44	36	2871	-1.65	6	0.09
116	SLU 42	44	36	2871	-1.65	6	0.09
116	SLU 43	56	51	2506	-1.7	5.24	0.08
116	SLU 44	56	51	2506	-1.7	5.24	0.08
116	SLU 45	56	51	2506	-1.7	5.24	0.08
116	SLU 46	56	51	2506	-1.7	5.24	0.08
116	SLU 47	56	51	2506	-1.7	5.24	0.08
116	SLU 48	56	51	2506	-1.7	5.24	0.08
116	SLU 49	56	51	2506	-1.7	5.24	0.08
116	SLU 50	56	51	2506	-1.7	5.24	0.08
116	SLU 51	56	51	2506	-1.7	5.24	0.08
116	SLU 52	54	47	2952	-1.83	6.16	0.09
116	SLU 53	54	47	2952	-1.83	6.16	0.09
116	SLU 54	54	47	2952	-1.83	6.16	0.09
116	SLU 55	54	47	2952	-1.83	6.16	0.09
116	SLU 56	54	47	2952	-1.83	6.16	0.09
116	SLU 57	54	47	2952	-1.83	6.16	0.09
116	SLU 58	54	47	2952	-1.83	6.16	0.09
116	SLU 59	54	47	2952	-1.83	6.16	0.09
116	SLU 60	54	45	3143	-1.89	6.56	0.1
116	SLU 61	54	45	3143	-1.89	6.56	0.1
116	SLU 62	54	45	3143	-1.89	6.56	0.1
116	SLU 63	54	45	3143	-1.89	6.56	0.1
116	SLU 64	59	53	2749	-1.81	5.75	0.08
116	SLU 65	59	53	2749	-1.81	5.75	0.08
116	SLU 66	59	53	2749	-1.81	5.75	0.08
116	SLU 67	59	53	2749	-1.81	5.75	0.08
116	SLU 68	59	53	2749	-1.81	5.75	0.08
116	SLU 69	59	53	2749	-1.81	5.75	0.08
116	SLU 70	59	53	2749	-1.81	5.75	0.08
116	SLU 71	59	53	2749	-1.81	5.75	0.08
116	SLU 72	59	53	2749	-1.81	5.75	0.08
116	SLU 73	57	49	3195	-1.95	6.68	0.1
116	SLU 74	57	49	3195	-1.95	6.68	0.1
116	SLU 75	57	49	3195	-1.95	6.68	0.1
116	SLU 76	57	49	3195	-1.95	6.68	0.1
116	SLU 77	57	49	3195	-1.95	6.68	0.1
116	SLU 78	57	49	3195	-1.95	6.68	0.1
116	SLU 79	57	49	3195	-1.95	6.68	0.1
116	SLU 80	57	49	3195	-1.95	6.68	0.1
116	SLU 81	57	47	3386	-2.01	7.08	0.1
116	SLU 82	57	47	3386	-2.01	7.08	0.1
116	SLU 83	57	47	3386	-2.01	7.08	0.1
116	SLU 84	57	47	3386	-2.01	7.08	0.1
116	SLE RA 1	45	40	2061	-1.37	4.31	0.06
116	SLE RA 2	45	40	2061	-1.37	4.31	0.06
116	SLE RA 3	45	40	2061	-1.37	4.31	0.06
116	SLE RA 4	45	40	2061	-1.37	4.31	0.06
116	SLE RA 5	45	40	2061	-1.37	4.31	0.06
116	SLE RA 6	45	40	2061	-1.37	4.31	0.06
116	SLE RA 7	45	40	2061	-1.37	4.31	0.06
116	SLE RA 8	45	40	2061	-1.37	4.31	0.06
116	SLE RA 9	45	40	2061	-1.37	4.31	0.06
116	SLE RA 10	43	38	2358	-1.46	4.93	0.07
116	SLE RA 11	43	38	2358	-1.46	4.93	0.07
116	SLE RA 12	43	38	2358	-1.46	4.93	0.07
116	SLE RA 13	43	38	2358	-1.46	4.93	0.07
116	SLE RA 14	43	38	2358	-1.46	4.93	0.07
116	SLE RA 15	43	38	2358	-1.46	4.93	0.07
116	SLE RA 16	43	38	2358	-1.46	4.93	0.07
116	SLE RA 17	43	38	2358	-1.46	4.93	0.07
116	SLE RA 18	43	36	2486	-1.5	5.19	0.08
116	SLE RA 19	43	36	2486	-1.5	5.19	0.08
116	SLE RA 20	43	36	2486	-1.5	5.19	0.08
116	SLE RA 21	43	36	2486	-1.5	5.19	0.08
116	SLE FR 1	45	40	2061	-1.37	4.31	0.06
116	SLE FR 2	45	40	2061	-1.37	4.31	0.06
116	SLE FR 3	45	40	2061	-1.37	4.31	0.06
116	SLE FR 4	44	39	2189	-1.41	4.58	0.07
116	SLE FR 5	44	39	2189	-1.41	4.58	0.07
116	SLE FR 6	44	38	2273	-1.43	4.75	0.07
116	SLE QP 1	45	40	2061	-1.37	4.31	0.06
116	SLE QP 2	44	39	2189	-1.41	4.58	0.07
116	SLD 1	336	361	2744	-14.75	17.6	0.11
116	SLD 2	336	361	2744	-14.75	17.6	0.11
116	SLD 3	188	202	2545	-8.98	10.88	0.08
116	SLD 4	188	202	2545	-8.98	10.88	0.08
116	SLD 5	356	377	2657	-14.16	18.67	0.12
116	SLD 6	356	377	2657	-14.16	18.67	0.12
116	SLD 7	-137	-153	1993	5.07	-3.72	0.03
116	SLD 8	-137	-153	1993	5.07	-3.72	0.03
116	SLD 9	225	231	2384	-7.88	12.88	0.1



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
116	SLD 10	225	231	2384	-7.88	12.88	0.1
116	SLD 11	-268	-299	1720	11.34	-9.52	0.02
116	SLD 12	-268	-299	1720	11.34	-9.52	0.02
116	SLD 13	-100	-124	1833	6.17	-1.73	0.05
116	SLD 14	-100	-124	1833	6.17	-1.73	0.05
116	SLD 15	-248	-283	1633	11.93	-8.45	0.03
116	SLD 16	-248	-283	1633	11.93	-8.45	0.03
116	SLV 1	754	821	3561	-34	36.55	0.17
116	SLV 2	754	821	3561	-34	36.55	0.17
116	SLV 3	397	438	3072	-20.18	19.96	0.11
116	SLV 4	397	438	3072	-20.18	19.96	0.11
116	SLV 5	800	855	3341	-32.15	39.33	0.19
116	SLV 6	800	855	3341	-32.15	39.33	0.19
116	SLV 7	-393	-422	1713	13.92	-15.97	-0.01
116	SLV 8	-393	-422	1713	13.92	-15.97	-0.01
116	SLV 9	481	500	2664	-16.74	25.12	0.15
116	SLV 10	481	500	2664	-16.74	25.12	0.15
116	SLV 11	-712	-777	1036	29.33	-30.17	-0.06
116	SLV 12	-712	-777	1036	29.33	-30.17	-0.06
116	SLV 13	-308	-360	1305	17.36	-10.8	0.03
116	SLV 14	-308	-360	1305	17.36	-10.8	0.03
116	SLV 15	-666	-743	816	31.18	-27.39	-0.03
116	SLV 16	-666	-743	816	31.18	-27.39	-0.03
117	SLU 1	-3	-331	2370	15.72	-1.03	0.01
117	SLU 2	-3	-331	2370	15.72	-1.03	0.01
117	SLU 3	-3	-331	2370	15.72	-1.03	0.01
117	SLU 4	-3	-331	2370	15.72	-1.03	0.01
117	SLU 5	-3	-331	2370	15.72	-1.03	0.01
117	SLU 6	-3	-331	2370	15.72	-1.03	0.01
117	SLU 7	-3	-331	2370	15.72	-1.03	0.01
117	SLU 8	-3	-331	2370	15.72	-1.03	0.01
117	SLU 9	-3	-331	2370	15.72	-1.03	0.01
117	SLU 10	-4	-421	2844	20	-1.25	0.02
117	SLU 11	-4	-421	2844	20	-1.25	0.02
117	SLU 12	-4	-421	2844	20	-1.25	0.02
117	SLU 13	-4	-421	2844	20	-1.25	0.02
117	SLU 14	-4	-421	2844	20	-1.25	0.02
117	SLU 15	-4	-421	2844	20	-1.25	0.02
117	SLU 16	-4	-421	2844	20	-1.25	0.02
117	SLU 17	-4	-421	2844	20	-1.25	0.02
117	SLU 18	-4	-459	3047	21.83	-1.34	0.02
117	SLU 19	-4	-459	3047	21.83	-1.34	0.02
117	SLU 20	-4	-459	3047	21.83	-1.34	0.02
117	SLU 21	-4	-459	3047	21.83	-1.34	0.02
117	SLU 22	-4	-369	2631	17.63	-1.17	0.02
117	SLU 23	-4	-369	2631	17.63	-1.17	0.02
117	SLU 24	-4	-369	2631	17.63	-1.17	0.02
117	SLU 25	-4	-369	2631	17.63	-1.17	0.02
117	SLU 26	-4	-369	2631	17.63	-1.17	0.02
117	SLU 27	-4	-369	2631	17.63	-1.17	0.02
117	SLU 28	-4	-369	2631	17.63	-1.17	0.02
117	SLU 29	-4	-369	2631	17.63	-1.17	0.02
117	SLU 30	-4	-369	2631	17.63	-1.17	0.02
117	SLU 31	-4	-459	3105	21.91	-1.38	0.02
117	SLU 32	-4	-459	3105	21.91	-1.38	0.02
117	SLU 33	-4	-459	3105	21.91	-1.38	0.02
117	SLU 34	-4	-459	3105	21.91	-1.38	0.02
117	SLU 35	-4	-459	3105	21.91	-1.38	0.02
117	SLU 36	-4	-459	3105	21.91	-1.38	0.02
117	SLU 37	-4	-459	3105	21.91	-1.38	0.02
117	SLU 38	-4	-459	3105	21.91	-1.38	0.02
117	SLU 39	-5	-497	3308	23.75	-1.47	0.02
117	SLU 40	-5	-497	3308	23.75	-1.47	0.02
117	SLU 41	-5	-497	3308	23.75	-1.47	0.02
117	SLU 42	-5	-497	3308	23.75	-1.47	0.02
117	SLU 43	-4	-417	2992	19.78	-1.3	0.02
117	SLU 44	-4	-417	2992	19.78	-1.3	0.02
117	SLU 45	-4	-417	2992	19.78	-1.3	0.02
117	SLU 46	-4	-417	2992	19.78	-1.3	0.02
117	SLU 47	-4	-417	2992	19.78	-1.3	0.02
117	SLU 48	-4	-417	2992	19.78	-1.3	0.02
117	SLU 49	-4	-417	2992	19.78	-1.3	0.02
117	SLU 50	-4	-417	2992	19.78	-1.3	0.02
117	SLU 51	-4	-417	2992	19.78	-1.3	0.02
117	SLU 52	-5	-507	3466	24.06	-1.51	0.02
117	SLU 53	-5	-507	3466	24.06	-1.51	0.02
117	SLU 54	-5	-507	3466	24.06	-1.51	0.02
117	SLU 55	-5	-507	3466	24.06	-1.51	0.02
117	SLU 56	-5	-507	3466	24.06	-1.51	0.02
117	SLU 57	-5	-507	3466	24.06	-1.51	0.02
117	SLU 58	-5	-507	3466	24.06	-1.51	0.02
117	SLU 59	-5	-507	3466	24.06	-1.51	0.02
117	SLU 60	-5	-545	3669	25.89	-1.6	0.02
117	SLU 61	-5	-545	3669	25.89	-1.6	0.02
117	SLU 62	-5	-545	3669	25.89	-1.6	0.02
117	SLU 63	-5	-545	3669	25.89	-1.6	0.02
117	SLU 64	-4	-455	3253	21.7	-1.43	0.02
117	SLU 65	-4	-455	3253	21.7	-1.43	0.02
117	SLU 66	-4	-455	3253	21.7	-1.43	0.02



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
117	SLU 67	-4	-455	3253	21.7	-1.43	0.02
117	SLU 68	-4	-455	3253	21.7	-1.43	0.02
117	SLU 69	-4	-455	3253	21.7	-1.43	0.02
117	SLU 70	-4	-455	3253	21.7	-1.43	0.02
117	SLU 71	-4	-455	3253	21.7	-1.43	0.02
117	SLU 72	-4	-455	3253	21.7	-1.43	0.02
117	SLU 73	-5	-545	3727	25.97	-1.64	0.02
117	SLU 74	-5	-545	3727	25.97	-1.64	0.02
117	SLU 75	-5	-545	3727	25.97	-1.64	0.02
117	SLU 76	-5	-545	3727	25.97	-1.64	0.02
117	SLU 77	-5	-545	3727	25.97	-1.64	0.02
117	SLU 78	-5	-545	3727	25.97	-1.64	0.02
117	SLU 79	-5	-545	3727	25.97	-1.64	0.02
117	SLU 80	-5	-545	3727	25.97	-1.64	0.02
117	SLU 81	-5	-583	3930	27.81	-1.74	0.03
117	SLU 82	-5	-583	3930	27.81	-1.74	0.03
117	SLU 83	-5	-583	3930	27.81	-1.74	0.03
117	SLU 84	-5	-583	3930	27.81	-1.74	0.03
117	SLE RA 1	-3	-342	2445	16.27	-1.07	0.02
117	SLE RA 2	-3	-342	2445	16.27	-1.07	0.02
117	SLE RA 3	-3	-342	2445	16.27	-1.07	0.02
117	SLE RA 4	-3	-342	2445	16.27	-1.07	0.02
117	SLE RA 5	-3	-342	2445	16.27	-1.07	0.02
117	SLE RA 6	-3	-342	2445	16.27	-1.07	0.02
117	SLE RA 7	-3	-342	2445	16.27	-1.07	0.02
117	SLE RA 8	-3	-342	2445	16.27	-1.07	0.02
117	SLE RA 9	-3	-342	2445	16.27	-1.07	0.02
117	SLE RA 10	-4	-402	2761	19.12	-1.21	0.02
117	SLE RA 11	-4	-402	2761	19.12	-1.21	0.02
117	SLE RA 12	-4	-402	2761	19.12	-1.21	0.02
117	SLE RA 13	-4	-402	2761	19.12	-1.21	0.02
117	SLE RA 14	-4	-402	2761	19.12	-1.21	0.02
117	SLE RA 15	-4	-402	2761	19.12	-1.21	0.02
117	SLE RA 16	-4	-402	2761	19.12	-1.21	0.02
117	SLE RA 17	-4	-402	2761	19.12	-1.21	0.02
117	SLE RA 18	-4	-427	2896	20.34	-1.28	0.02
117	SLE RA 19	-4	-427	2896	20.34	-1.28	0.02
117	SLE RA 20	-4	-427	2896	20.34	-1.28	0.02
117	SLE RA 21	-4	-427	2896	20.34	-1.28	0.02
117	SLE FR 1	-3	-342	2445	16.27	-1.07	0.02
117	SLE FR 2	-3	-342	2445	16.27	-1.07	0.02
117	SLE FR 3	-3	-342	2445	16.27	-1.07	0.02
117	SLE FR 4	-3	-367	2580	17.49	-1.13	0.02
117	SLE FR 5	-3	-367	2580	17.49	-1.13	0.02
117	SLE FR 6	-4	-384	2670	18.31	-1.17	0.02
117	SLE QP 1	-3	-342	2445	16.27	-1.07	0.02
117	SLE QP 2	-3	-367	2580	17.49	-1.13	0.02
117	SLD 1	-2	-388	2168	17.91	3.73	0
117	SLD 2	-2	-388	2168	17.91	3.73	0
117	SLD 3	7	-524	2345	24.02	8	0.01
117	SLD 4	7	-524	2345	24.02	8	0.01
117	SLD 5	-17	-168	2189	8.35	-6.14	0
117	SLD 6	-17	-168	2189	8.35	-6.14	0
117	SLD 7	14	-620	2777	28.72	8.07	0.03
117	SLD 8	14	-620	2777	28.72	8.07	0.03
117	SLD 9	-20	-115	2383	6.26	-10.33	0.01
117	SLD 10	-20	-115	2383	6.26	-10.33	0.01
117	SLD 11	10	-566	2971	26.63	3.87	0.04
117	SLD 12	10	-566	2971	26.63	3.87	0.04
117	SLD 13	-14	-211	2815	10.96	-10.26	0.03
117	SLD 14	-14	-211	2815	10.96	-10.26	0.03
117	SLD 15	-5	-346	2992	17.07	-6	0.04
117	SLD 16	-5	-346	2992	17.07	-6	0.04
117	SLV 1	0	-417	1605	18.49	10.84	-0.03
117	SLV 2	0	-417	1605	18.49	10.84	-0.03
117	SLV 3	24	-735	2021	32.84	21.71	-0.01
117	SLV 4	24	-735	2021	32.84	21.71	-0.01
117	SLV 5	-37	100	1657	-3.98	-14.03	-0.03
117	SLV 6	-37	100	1657	-3.98	-14.03	-0.03
117	SLV 7	40	-960	3043	43.87	22.21	0.05
117	SLV 8	40	-960	3043	43.87	22.21	0.05
117	SLV 9	-47	225	2117	-8.89	-24.47	-0.01
117	SLV 10	-47	225	2117	-8.89	-24.47	-0.01
117	SLV 11	30	-835	3503	38.96	11.76	0.07
117	SLV 12	30	-835	3503	38.96	11.76	0.07
117	SLV 13	-30	0	3139	2.14	-23.98	0.04
117	SLV 14	-30	0	3139	2.14	-23.98	0.04
117	SLV 15	-7	-318	3555	16.49	-13.1	0.07
117	SLV 16	-7	-318	3555	16.49	-13.1	0.07
118	SLU 1	0	0	1068	0.12	-0.03	0.01
118	SLU 2	0	0	1068	0.12	-0.03	0.01
118	SLU 3	0	0	1068	0.12	-0.03	0.01
118	SLU 4	0	0	1068	0.12	-0.03	0.01
118	SLU 5	0	0	1068	0.12	-0.03	0.01
118	SLU 6	0	0	1068	0.12	-0.03	0.01
118	SLU 7	0	0	1068	0.12	-0.03	0.01
118	SLU 8	0	0	1068	0.12	-0.03	0.01
118	SLU 9	0	0	1068	0.12	-0.03	0.01
118	SLU 10	0	-1	1338	0.11	-0.04	0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
118	SLU 11	0	-1	1338	0.11	-0.04	0.01
118	SLU 12	0	-1	1338	0.11	-0.04	0.01
118	SLU 13	0	-1	1338	0.11	-0.04	0.01
118	SLU 14	0	-1	1338	0.11	-0.04	0.01
118	SLU 15	0	-1	1338	0.11	-0.04	0.01
118	SLU 16	0	-1	1338	0.11	-0.04	0.01
118	SLU 17	0	-1	1338	0.11	-0.04	0.01
118	SLU 18	0	-1	1454	0.11	-0.04	0.01
118	SLU 19	0	-1	1454	0.11	-0.04	0.01
118	SLU 20	0	-1	1454	0.11	-0.04	0.01
118	SLU 21	0	-1	1454	0.11	-0.04	0.01
118	SLU 22	0	0	1228	0.13	-0.04	0.01
118	SLU 23	0	0	1228	0.13	-0.04	0.01
118	SLU 24	0	0	1228	0.13	-0.04	0.01
118	SLU 25	0	0	1228	0.13	-0.04	0.01
118	SLU 26	0	0	1228	0.13	-0.04	0.01
118	SLU 27	0	0	1228	0.13	-0.04	0.01
118	SLU 28	0	0	1228	0.13	-0.04	0.01
118	SLU 29	0	0	1228	0.13	-0.04	0.01
118	SLU 30	0	0	1228	0.13	-0.04	0.01
118	SLU 31	0	-1	1498	0.12	-0.04	0.01
118	SLU 32	0	-1	1498	0.12	-0.04	0.01
118	SLU 33	0	-1	1498	0.12	-0.04	0.01
118	SLU 34	0	-1	1498	0.12	-0.04	0.01
118	SLU 35	0	-1	1498	0.12	-0.04	0.01
118	SLU 36	0	-1	1498	0.12	-0.04	0.01
118	SLU 37	0	-1	1498	0.12	-0.04	0.01
118	SLU 38	0	-1	1498	0.12	-0.04	0.01
118	SLU 39	0	-1	1614	0.12	-0.04	0.01
118	SLU 40	0	-1	1614	0.12	-0.04	0.01
118	SLU 41	0	-1	1614	0.12	-0.04	0.01
118	SLU 42	0	-1	1614	0.12	-0.04	0.01
118	SLU 43	0	0	1334	0.15	-0.04	0.01
118	SLU 44	0	0	1334	0.15	-0.04	0.01
118	SLU 45	0	0	1334	0.15	-0.04	0.01
118	SLU 46	0	0	1334	0.15	-0.04	0.01
118	SLU 47	0	0	1334	0.15	-0.04	0.01
118	SLU 48	0	0	1334	0.15	-0.04	0.01
118	SLU 49	0	0	1334	0.15	-0.04	0.01
118	SLU 50	0	0	1334	0.15	-0.04	0.01
118	SLU 51	0	0	1334	0.15	-0.04	0.01
118	SLU 52	0	-1	1604	0.14	-0.05	0.01
118	SLU 53	0	-1	1604	0.14	-0.05	0.01
118	SLU 54	0	-1	1604	0.14	-0.05	0.01
118	SLU 55	0	-1	1604	0.14	-0.05	0.01
118	SLU 56	0	-1	1604	0.14	-0.05	0.01
118	SLU 57	0	-1	1604	0.14	-0.05	0.01
118	SLU 58	0	-1	1604	0.14	-0.05	0.01
118	SLU 59	0	-1	1604	0.14	-0.05	0.01
118	SLU 60	0	-1	1720	0.14	-0.05	0.01
118	SLU 61	0	-1	1720	0.14	-0.05	0.01
118	SLU 62	0	-1	1720	0.14	-0.05	0.01
118	SLU 63	0	-1	1720	0.14	-0.05	0.01
118	SLU 64	0	0	1494	0.16	-0.05	0.01
118	SLU 65	0	0	1494	0.16	-0.05	0.01
118	SLU 66	0	0	1494	0.16	-0.05	0.01
118	SLU 67	0	0	1494	0.16	-0.05	0.01
118	SLU 68	0	0	1494	0.16	-0.05	0.01
118	SLU 69	0	0	1494	0.16	-0.05	0.01
118	SLU 70	0	0	1494	0.16	-0.05	0.01
118	SLU 71	0	0	1494	0.16	-0.05	0.01
118	SLU 72	0	0	1494	0.16	-0.05	0.01
118	SLU 73	0	-1	1764	0.16	-0.05	0.01
118	SLU 74	0	-1	1764	0.16	-0.05	0.01
118	SLU 75	0	-1	1764	0.16	-0.05	0.01
118	SLU 76	0	-1	1764	0.16	-0.05	0.01
118	SLU 77	0	-1	1764	0.16	-0.05	0.01
118	SLU 78	0	-1	1764	0.16	-0.05	0.01
118	SLU 79	0	-1	1764	0.16	-0.05	0.01
118	SLU 80	0	-1	1764	0.16	-0.05	0.01
118	SLU 81	0	-1	1880	0.15	-0.05	0.02
118	SLU 82	0	-1	1880	0.15	-0.05	0.02
118	SLU 83	0	-1	1880	0.15	-0.05	0.02
118	SLU 84	0	-1	1880	0.15	-0.05	0.02
118	SLE RA 1	0	0	1114	0.12	-0.04	0.01
118	SLE RA 2	0	0	1114	0.12	-0.04	0.01
118	SLE RA 3	0	0	1114	0.12	-0.04	0.01
118	SLE RA 4	0	0	1114	0.12	-0.04	0.01
118	SLE RA 5	0	0	1114	0.12	-0.04	0.01
118	SLE RA 6	0	0	1114	0.12	-0.04	0.01
118	SLE RA 7	0	0	1114	0.12	-0.04	0.01
118	SLE RA 8	0	0	1114	0.12	-0.04	0.01
118	SLE RA 9	0	0	1114	0.12	-0.04	0.01
118	SLE RA 10	0	0	1294	0.12	-0.04	0.01
118	SLE RA 11	0	0	1294	0.12	-0.04	0.01
118	SLE RA 12	0	0	1294	0.12	-0.04	0.01
118	SLE RA 13	0	0	1294	0.12	-0.04	0.01
118	SLE RA 14	0	0	1294	0.12	-0.04	0.01
118	SLE RA 15	0	0	1294	0.12	-0.04	0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
118	SLE RA 16	0	0	1294	0.12	-0.04	0.01
118	SLE RA 17	0	0	1294	0.12	-0.04	0.01
118	SLE RA 18	0	-1	1371	0.12	-0.04	0.01
118	SLE RA 19	0	-1	1371	0.12	-0.04	0.01
118	SLE RA 20	0	-1	1371	0.12	-0.04	0.01
118	SLE RA 21	0	-1	1371	0.12	-0.04	0.01
118	SLE FR 1	0	0	1114	0.12	-0.04	0.01
118	SLE FR 2	0	0	1114	0.12	-0.04	0.01
118	SLE FR 3	0	0	1114	0.12	-0.04	0.01
118	SLE FR 4	0	0	1191	0.12	-0.04	0.01
118	SLE FR 5	0	0	1191	0.12	-0.04	0.01
118	SLE FR 6	0	0	1243	0.12	-0.04	0.01
118	SLE QP 1	0	0	1114	0.12	-0.04	0.01
118	SLE QP 2	0	0	1191	0.12	-0.04	0.01
118	SLD 1	3	-73	1192	-36.97	2.14	-0.18
118	SLD 2	3	-73	1192	-36.97	2.14	-0.18
118	SLD 3	-7	140	1130	70.79	-0.21	0.08
118	SLD 4	-7	140	1130	70.79	-0.21	0.08
118	SLD 5	16	-346	1285	-174.45	4.19	-0.44
118	SLD 6	16	-346	1285	-174.45	4.19	-0.44
118	SLD 7	-18	366	1080	184.76	-3.67	0.42
118	SLD 8	-18	366	1080	184.76	-3.67	0.42
118	SLD 9	17	-366	1303	-184.52	3.59	-0.4
118	SLD 10	17	-366	1303	-184.52	3.59	-0.4
118	SLD 11	-16	346	1098	174.69	-4.27	0.46
118	SLD 12	-16	346	1098	174.69	-4.27	0.46
118	SLD 13	7	-141	1252	-70.55	0.14	-0.06
118	SLD 14	7	-141	1252	-70.55	0.14	-0.06
118	SLD 15	-3	73	1190	37.22	-2.22	0.2
118	SLD 16	-3	73	1190	37.22	-2.22	0.2
118	SLV 1	8	-187	1198	-95.05	5.53	-0.48
118	SLV 2	8	-187	1198	-95.05	5.53	-0.48
118	SLV 3	-18	361	1041	181.42	-0.51	0.18
118	SLV 4	-18	361	1041	181.42	-0.51	0.18
118	SLV 5	42	-887	1432	-447.74	10.81	-1.13
118	SLV 6	42	-887	1432	-447.74	10.81	-1.13
118	SLV 7	-45	939	907	473.82	-9.35	1.06
118	SLV 8	-45	939	907	473.82	-9.35	1.06
118	SLV 9	44	-940	1475	-473.58	9.28	-1.04
118	SLV 10	44	-940	1475	-473.58	9.28	-1.04
118	SLV 11	-42	887	950	447.98	-10.88	1.15
118	SLV 12	-42	887	950	447.98	-10.88	1.15
118	SLV 13	17	-361	1342	-181.18	0.44	-0.16
118	SLV 14	17	-361	1342	-181.18	0.44	-0.16
118	SLV 15	-8	187	1184	95.29	-5.61	0.5
118	SLV 16	-8	187	1184	95.29	-5.61	0.5
119	SLU 1	-27	-37	2082	4.14	-0.92	-0.02
119	SLU 2	-27	-37	2082	4.14	-0.92	-0.02
119	SLU 3	-27	-37	2082	4.14	-0.92	-0.02
119	SLU 4	-27	-37	2082	4.14	-0.92	-0.02
119	SLU 5	-27	-37	2082	4.14	-0.92	-0.02
119	SLU 6	-27	-37	2082	4.14	-0.92	-0.02
119	SLU 7	-27	-37	2082	4.14	-0.92	-0.02
119	SLU 8	-27	-37	2082	4.14	-0.92	-0.02
119	SLU 9	-27	-37	2082	4.14	-0.92	-0.02
119	SLU 10	-38	-52	2443	4.98	-1.12	-0.03
119	SLU 11	-38	-52	2443	4.98	-1.12	-0.03
119	SLU 12	-38	-52	2443	4.98	-1.12	-0.03
119	SLU 13	-38	-52	2443	4.98	-1.12	-0.03
119	SLU 14	-38	-52	2443	4.98	-1.12	-0.03
119	SLU 15	-38	-52	2443	4.98	-1.12	-0.03
119	SLU 16	-38	-52	2443	4.98	-1.12	-0.03
119	SLU 17	-38	-52	2443	4.98	-1.12	-0.03
119	SLU 18	-44	-58	2598	5.34	-1.21	-0.03
119	SLU 19	-44	-58	2598	5.34	-1.21	-0.03
119	SLU 20	-44	-58	2598	5.34	-1.21	-0.03
119	SLU 21	-44	-58	2598	5.34	-1.21	-0.03
119	SLU 22	-30	-42	2320	4.65	-1.02	-0.03
119	SLU 23	-30	-42	2320	4.65	-1.02	-0.03
119	SLU 24	-30	-42	2320	4.65	-1.02	-0.03
119	SLU 25	-30	-42	2320	4.65	-1.02	-0.03
119	SLU 26	-30	-42	2320	4.65	-1.02	-0.03
119	SLU 27	-30	-42	2320	4.65	-1.02	-0.03
119	SLU 28	-30	-42	2320	4.65	-1.02	-0.03
119	SLU 29	-30	-42	2320	4.65	-1.02	-0.03
119	SLU 30	-30	-42	2320	4.65	-1.02	-0.03
119	SLU 31	-42	-57	2682	5.49	-1.22	-0.03
119	SLU 32	-42	-57	2682	5.49	-1.22	-0.03
119	SLU 33	-42	-57	2682	5.49	-1.22	-0.03
119	SLU 34	-42	-57	2682	5.49	-1.22	-0.03
119	SLU 35	-42	-57	2682	5.49	-1.22	-0.03
119	SLU 36	-42	-57	2682	5.49	-1.22	-0.03
119	SLU 37	-42	-57	2682	5.49	-1.22	-0.03
119	SLU 38	-42	-57	2682	5.49	-1.22	-0.03
119	SLU 39	-47	-63	2836	5.85	-1.3	-0.03
119	SLU 40	-47	-63	2836	5.85	-1.3	-0.03
119	SLU 41	-47	-63	2836	5.85	-1.3	-0.03
119	SLU 42	-47	-63	2836	5.85	-1.3	-0.03
119	SLU 43	-33	-47	2625	5.21	-1.17	-0.03



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
119	SLU 44	-33	-47	2625	5.21	-1.17	-0.03
119	SLU 45	-33	-47	2625	5.21	-1.17	-0.03
119	SLU 46	-33	-47	2625	5.21	-1.17	-0.03
119	SLU 47	-33	-47	2625	5.21	-1.17	-0.03
119	SLU 48	-33	-47	2625	5.21	-1.17	-0.03
119	SLU 49	-33	-47	2625	5.21	-1.17	-0.03
119	SLU 50	-33	-47	2625	5.21	-1.17	-0.03
119	SLU 51	-33	-47	2625	5.21	-1.17	-0.03
119	SLU 52	-45	-61	2986	6.05	-1.37	-0.03
119	SLU 53	-45	-61	2986	6.05	-1.37	-0.03
119	SLU 54	-45	-61	2986	6.05	-1.37	-0.03
119	SLU 55	-45	-61	2986	6.05	-1.37	-0.03
119	SLU 56	-45	-61	2986	6.05	-1.37	-0.03
119	SLU 57	-45	-61	2986	6.05	-1.37	-0.03
119	SLU 58	-45	-61	2986	6.05	-1.37	-0.03
119	SLU 59	-45	-61	2986	6.05	-1.37	-0.03
119	SLU 60	-50	-68	3141	6.41	-1.45	-0.04
119	SLU 61	-50	-68	3141	6.41	-1.45	-0.04
119	SLU 62	-50	-68	3141	6.41	-1.45	-0.04
119	SLU 63	-50	-68	3141	6.41	-1.45	-0.04
119	SLU 64	-37	-52	2863	5.72	-1.26	-0.03
119	SLU 65	-37	-52	2863	5.72	-1.26	-0.03
119	SLU 66	-37	-52	2863	5.72	-1.26	-0.03
119	SLU 67	-37	-52	2863	5.72	-1.26	-0.03
119	SLU 68	-37	-52	2863	5.72	-1.26	-0.03
119	SLU 69	-37	-52	2863	5.72	-1.26	-0.03
119	SLU 70	-37	-52	2863	5.72	-1.26	-0.03
119	SLU 71	-37	-52	2863	5.72	-1.26	-0.03
119	SLU 72	-37	-52	2863	5.72	-1.26	-0.03
119	SLU 73	-49	-66	3224	6.56	-1.46	-0.04
119	SLU 74	-49	-66	3224	6.56	-1.46	-0.04
119	SLU 75	-49	-66	3224	6.56	-1.46	-0.04
119	SLU 76	-49	-66	3224	6.56	-1.46	-0.04
119	SLU 77	-49	-66	3224	6.56	-1.46	-0.04
119	SLU 78	-49	-66	3224	6.56	-1.46	-0.04
119	SLU 79	-49	-66	3224	6.56	-1.46	-0.04
119	SLU 80	-49	-66	3224	6.56	-1.46	-0.04
119	SLU 81	-54	-73	3379	6.92	-1.55	-0.04
119	SLU 82	-54	-73	3379	6.92	-1.55	-0.04
119	SLU 83	-54	-73	3379	6.92	-1.55	-0.04
119	SLU 84	-54	-73	3379	6.92	-1.55	-0.04
119	SLE RA 1	-28	-39	2150	4.29	-0.95	-0.02
119	SLE RA 2	-28	-39	2150	4.29	-0.95	-0.02
119	SLE RA 3	-28	-39	2150	4.29	-0.95	-0.02
119	SLE RA 4	-28	-39	2150	4.29	-0.95	-0.02
119	SLE RA 5	-28	-39	2150	4.29	-0.95	-0.02
119	SLE RA 6	-28	-39	2150	4.29	-0.95	-0.02
119	SLE RA 7	-28	-39	2150	4.29	-0.95	-0.02
119	SLE RA 8	-28	-39	2150	4.29	-0.95	-0.02
119	SLE RA 9	-28	-39	2150	4.29	-0.95	-0.02
119	SLE RA 10	-36	-48	2391	4.85	-1.08	-0.03
119	SLE RA 11	-36	-48	2391	4.85	-1.08	-0.03
119	SLE RA 12	-36	-48	2391	4.85	-1.08	-0.03
119	SLE RA 13	-36	-48	2391	4.85	-1.08	-0.03
119	SLE RA 14	-36	-48	2391	4.85	-1.08	-0.03
119	SLE RA 15	-36	-48	2391	4.85	-1.08	-0.03
119	SLE RA 16	-36	-48	2391	4.85	-1.08	-0.03
119	SLE RA 17	-36	-48	2391	4.85	-1.08	-0.03
119	SLE RA 18	-39	-53	2494	5.09	-1.14	-0.03
119	SLE RA 19	-39	-53	2494	5.09	-1.14	-0.03
119	SLE RA 20	-39	-53	2494	5.09	-1.14	-0.03
119	SLE RA 21	-39	-53	2494	5.09	-1.14	-0.03
119	SLE FR 1	-28	-39	2150	4.29	-0.95	-0.02
119	SLE FR 2	-28	-39	2150	4.29	-0.95	-0.02
119	SLE FR 3	-28	-39	2150	4.29	-0.95	-0.02
119	SLE FR 4	-31	-43	2253	4.53	-1.01	-0.02
119	SLE FR 5	-31	-43	2253	4.53	-1.01	-0.02
119	SLE FR 6	-33	-46	2322	4.69	-1.05	-0.03
119	SLE QP 1	-28	-39	2150	4.29	-0.95	-0.02
119	SLE QP 2	-31	-43	2253	4.53	-1.01	-0.02
119	SLD 1	280	303	2517	-11.71	13.15	-0.04
119	SLD 2	280	303	2517	-11.71	13.15	-0.04
119	SLD 3	132	144	2731	-4.76	5.76	-0.07
119	SLD 4	132	144	2731	-4.76	5.76	-0.07
119	SLD 5	286	302	2008	-10.88	14.45	0.02
119	SLD 6	286	302	2008	-10.88	14.45	0.02
119	SLD 7	-206	-227	2722	12.27	-10.19	-0.09
119	SLD 8	-206	-227	2722	12.27	-10.19	-0.09
119	SLD 9	144	142	1785	-3.22	8.18	0.04
119	SLD 10	144	142	1785	-3.22	8.18	0.04
119	SLD 11	-348	-387	2499	19.93	-16.47	-0.07
119	SLD 12	-348	-387	2499	19.93	-16.47	-0.07
119	SLD 13	-194	-230	1775	13.82	-7.78	0.02
119	SLD 14	-194	-230	1775	13.82	-7.78	0.02
119	SLD 15	-342	-389	1990	20.76	-15.17	-0.01
119	SLD 16	-342	-389	1990	20.76	-15.17	-0.01
119	SLV 1	725	799	2900	-35.34	33.72	-0.07
119	SLV 2	725	799	2900	-35.34	33.72	-0.07
119	SLV 3	366	415	3425	-18.59	15.48	-0.15



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
119	SLV 4	366	415	3425	-18.59	15.48	-0.15
119	SLV 5	740	791	1652	-32.85	37.07	0.08
119	SLV 6	740	791	1652	-32.85	37.07	0.08
119	SLV 7	-455	-487	3400	23	-23.72	-0.18
119	SLV 8	-455	-487	3400	23	-23.72	-0.18
119	SLV 9	393	401	1107	-13.95	21.71	0.13
119	SLV 10	393	401	1107	-13.95	21.71	0.13
119	SLV 11	-801	-877	2855	41.9	-39.09	-0.13
119	SLV 12	-801	-877	2855	41.9	-39.09	-0.13
119	SLV 13	-428	-501	1082	27.64	-17.5	0.1
119	SLV 14	-428	-501	1082	27.64	-17.5	0.1
119	SLV 15	-787	-884	1606	44.4	-35.74	0.02
119	SLV 16	-787	-884	1606	44.4	-35.74	0.02
120	SLU 1	431	-170	2660	4.9	12.08	0.02
120	SLU 2	431	-170	2660	4.9	12.08	0.02
120	SLU 3	431	-170	2660	4.9	12.08	0.02
120	SLU 4	431	-170	2660	4.9	12.08	0.02
120	SLU 5	431	-170	2660	4.9	12.08	0.02
120	SLU 6	431	-170	2660	4.9	12.08	0.02
120	SLU 7	431	-170	2660	4.9	12.08	0.02
120	SLU 8	431	-170	2660	4.9	12.08	0.02
120	SLU 9	431	-170	2660	4.9	12.08	0.02
120	SLU 10	501	-198	3056	5.64	14.32	0.02
120	SLU 11	501	-198	3056	5.64	14.32	0.02
120	SLU 12	501	-198	3056	5.64	14.32	0.02
120	SLU 13	501	-198	3056	5.64	14.32	0.02
120	SLU 14	501	-198	3056	5.64	14.32	0.02
120	SLU 15	501	-198	3056	5.64	14.32	0.02
120	SLU 16	501	-198	3056	5.64	14.32	0.02
120	SLU 17	501	-198	3056	5.64	14.32	0.02
120	SLU 18	531	-210	3226	5.95	15.28	0.02
120	SLU 19	531	-210	3226	5.95	15.28	0.02
120	SLU 20	531	-210	3226	5.95	15.28	0.02
120	SLU 21	531	-210	3226	5.95	15.28	0.02
120	SLU 22	485	-190	2964	5.46	13.7	0.02
120	SLU 23	485	-190	2964	5.46	13.7	0.02
120	SLU 24	485	-190	2964	5.46	13.7	0.02
120	SLU 25	485	-190	2964	5.46	13.7	0.02
120	SLU 26	485	-190	2964	5.46	13.7	0.02
120	SLU 27	485	-190	2964	5.46	13.7	0.02
120	SLU 28	485	-190	2964	5.46	13.7	0.02
120	SLU 29	485	-190	2964	5.46	13.7	0.02
120	SLU 30	485	-190	2964	5.46	13.7	0.02
120	SLU 31	555	-217	3360	6.2	15.95	0.02
120	SLU 32	555	-217	3360	6.2	15.95	0.02
120	SLU 33	555	-217	3360	6.2	15.95	0.02
120	SLU 34	555	-217	3360	6.2	15.95	0.02
120	SLU 35	555	-217	3360	6.2	15.95	0.02
120	SLU 36	555	-217	3360	6.2	15.95	0.02
120	SLU 37	555	-217	3360	6.2	15.95	0.02
120	SLU 38	555	-217	3360	6.2	15.95	0.02
120	SLU 39	585	-229	3530	6.51	16.91	0.02
120	SLU 40	585	-229	3530	6.51	16.91	0.02
120	SLU 41	585	-229	3530	6.51	16.91	0.02
120	SLU 42	585	-229	3530	6.51	16.91	0.02
120	SLU 43	541	-215	3354	6.18	15.15	0.02
120	SLU 44	541	-215	3354	6.18	15.15	0.02
120	SLU 45	541	-215	3354	6.18	15.15	0.02
120	SLU 46	541	-215	3354	6.18	15.15	0.02
120	SLU 47	541	-215	3354	6.18	15.15	0.02
120	SLU 48	541	-215	3354	6.18	15.15	0.02
120	SLU 49	541	-215	3354	6.18	15.15	0.02
120	SLU 50	541	-215	3354	6.18	15.15	0.02
120	SLU 51	541	-215	3354	6.18	15.15	0.02
120	SLU 52	611	-243	3750	6.92	17.39	0.02
120	SLU 53	611	-243	3750	6.92	17.39	0.02
120	SLU 54	611	-243	3750	6.92	17.39	0.02
120	SLU 55	611	-243	3750	6.92	17.39	0.02
120	SLU 56	611	-243	3750	6.92	17.39	0.02
120	SLU 57	611	-243	3750	6.92	17.39	0.02
120	SLU 58	611	-243	3750	6.92	17.39	0.02
120	SLU 59	611	-243	3750	6.92	17.39	0.02
120	SLU 60	641	-255	3920	7.23	18.35	0.02
120	SLU 61	641	-255	3920	7.23	18.35	0.02
120	SLU 62	641	-255	3920	7.23	18.35	0.02
120	SLU 63	641	-255	3920	7.23	18.35	0.02
120	SLU 64	596	-234	3658	6.74	16.77	0.02
120	SLU 65	596	-234	3658	6.74	16.77	0.02
120	SLU 66	596	-234	3658	6.74	16.77	0.02
120	SLU 67	596	-234	3658	6.74	16.77	0.02
120	SLU 68	596	-234	3658	6.74	16.77	0.02
120	SLU 69	596	-234	3658	6.74	16.77	0.02
120	SLU 70	596	-234	3658	6.74	16.77	0.02
120	SLU 71	596	-234	3658	6.74	16.77	0.02
120	SLU 72	596	-234	3658	6.74	16.77	0.02
120	SLU 73	666	-262	4054	7.48	19.01	0.02
120	SLU 74	666	-262	4054	7.48	19.01	0.02
120	SLU 75	666	-262	4054	7.48	19.01	0.02
120	SLU 76	666	-262	4054	7.48	19.01	0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
120	SLU 77	666	-262	4054	7.48	19.01	0.02
120	SLU 78	666	-262	4054	7.48	19.01	0.02
120	SLU 79	666	-262	4054	7.48	19.01	0.02
120	SLU 80	666	-262	4054	7.48	19.01	0.02
120	SLU 81	696	-274	4224	7.79	19.97	0.02
120	SLU 82	696	-274	4224	7.79	19.97	0.02
120	SLU 83	696	-274	4224	7.79	19.97	0.02
120	SLU 84	696	-274	4224	7.79	19.97	0.02
120	SLE RA 1	446	-176	2747	5.06	12.54	0.02
120	SLE RA 2	446	-176	2747	5.06	12.54	0.02
120	SLE RA 3	446	-176	2747	5.06	12.54	0.02
120	SLE RA 4	446	-176	2747	5.06	12.54	0.02
120	SLE RA 5	446	-176	2747	5.06	12.54	0.02
120	SLE RA 6	446	-176	2747	5.06	12.54	0.02
120	SLE RA 7	446	-176	2747	5.06	12.54	0.02
120	SLE RA 8	446	-176	2747	5.06	12.54	0.02
120	SLE RA 9	446	-176	2747	5.06	12.54	0.02
120	SLE RA 10	493	-194	3011	5.55	14.04	0.02
120	SLE RA 11	493	-194	3011	5.55	14.04	0.02
120	SLE RA 12	493	-194	3011	5.55	14.04	0.02
120	SLE RA 13	493	-194	3011	5.55	14.04	0.02
120	SLE RA 14	493	-194	3011	5.55	14.04	0.02
120	SLE RA 15	493	-194	3011	5.55	14.04	0.02
120	SLE RA 16	493	-194	3011	5.55	14.04	0.02
120	SLE RA 17	493	-194	3011	5.55	14.04	0.02
120	SLE RA 18	513	-202	3124	5.76	14.68	0.02
120	SLE RA 19	513	-202	3124	5.76	14.68	0.02
120	SLE RA 20	513	-202	3124	5.76	14.68	0.02
120	SLE RA 21	513	-202	3124	5.76	14.68	0.02
120	SLE FR 1	446	-176	2747	5.06	12.54	0.02
120	SLE FR 2	446	-176	2747	5.06	12.54	0.02
120	SLE FR 3	446	-176	2747	5.06	12.54	0.02
120	SLE FR 4	466	-184	2860	5.27	13.18	0.02
120	SLE FR 5	466	-184	2860	5.27	13.18	0.02
120	SLE FR 6	480	-189	2936	5.41	13.61	0.02
120	SLE QP 1	446	-176	2747	5.06	12.54	0.02
120	SLE QP 2	466	-184	2860	5.27	13.18	0.02
120	SLD 1	697	32	1493	-2.91	24.29	0.07
120	SLD 2	697	32	1493	-2.91	24.29	0.07
120	SLD 3	740	-70	2093	0.66	21.98	0.28
120	SLD 4	740	-70	2093	0.66	21.98	0.28
120	SLD 5	470	36	1540	-2.6	20.02	-0.29
120	SLD 6	470	36	1540	-2.6	20.02	-0.29
120	SLD 7	614	-305	3539	9.3	12.32	0.42
120	SLD 8	614	-305	3539	9.3	12.32	0.42
120	SLD 9	318	-63	2181	1.24	14.05	-0.39
120	SLD 10	318	-63	2181	1.24	14.05	-0.39
120	SLD 11	463	-404	4180	13.14	6.35	0.33
120	SLD 12	463	-404	4180	13.14	6.35	0.33
120	SLD 13	192	-297	3627	9.89	4.39	-0.25
120	SLD 14	192	-297	3627	9.89	4.39	-0.25
120	SLD 15	235	-400	4227	13.46	2.08	-0.03
120	SLD 16	235	-400	4227	13.46	2.08	-0.03
120	SLV 1	1009	349	-557	-14.95	39.39	0.14
120	SLV 2	1009	349	-557	-14.95	39.39	0.14
120	SLV 3	1112	99	930	-6.28	33.91	0.68
120	SLV 4	1112	99	930	-6.28	33.91	0.68
120	SLV 5	473	355	-420	-13.94	29.36	-0.77
120	SLV 6	473	355	-420	-13.94	29.36	-0.77
120	SLV 7	816	-477	4536	14.95	11.09	1.04
120	SLV 8	816	-477	4536	14.95	11.09	1.04
120	SLV 9	116	110	1184	-4.41	15.28	-1
120	SLV 10	116	110	1184	-4.41	15.28	-1
120	SLV 11	459	-722	6140	24.48	-2.99	0.8
120	SLV 12	459	-722	6140	24.48	-2.99	0.8
120	SLV 13	-180	-467	4791	16.82	-7.54	-0.64
120	SLV 14	-180	-467	4791	16.82	-7.54	-0.64
120	SLV 15	-77	-717	6278	25.49	-13.02	-0.1
120	SLV 16	-77	-717	6278	25.49	-13.02	-0.1
121	SLU 1	386	-5	2187	1.63	25.04	0.35
121	SLU 2	386	-5	2187	1.63	25.04	0.35
121	SLU 3	386	-5	2187	1.63	25.04	0.35
121	SLU 4	386	-5	2187	1.63	25.04	0.35
121	SLU 5	386	-5	2187	1.63	25.04	0.35
121	SLU 6	386	-5	2187	1.63	25.04	0.35
121	SLU 7	386	-5	2187	1.63	25.04	0.35
121	SLU 8	386	-5	2187	1.63	25.04	0.35
121	SLU 9	386	-5	2187	1.63	25.04	0.35
121	SLU 10	465	-6	2493	1.82	29.79	0.41
121	SLU 11	465	-6	2493	1.82	29.79	0.41
121	SLU 12	465	-6	2493	1.82	29.79	0.41
121	SLU 13	465	-6	2493	1.82	29.79	0.41
121	SLU 14	465	-6	2493	1.82	29.79	0.41
121	SLU 15	465	-6	2493	1.82	29.79	0.41
121	SLU 16	465	-6	2493	1.82	29.79	0.41
121	SLU 17	465	-6	2493	1.82	29.79	0.41
121	SLU 18	498	-6	2625	1.91	31.82	0.44
121	SLU 19	498	-6	2625	1.91	31.82	0.44
121	SLU 20	498	-6	2625	1.91	31.82	0.44



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
121	SLU 21	498	-6	2625	1.91	31.82	0.44
121	SLU 22	439	-6	2428	1.82	28.4	0.4
121	SLU 23	439	-6	2428	1.82	28.4	0.4
121	SLU 24	439	-6	2428	1.82	28.4	0.4
121	SLU 25	439	-6	2428	1.82	28.4	0.4
121	SLU 26	439	-6	2428	1.82	28.4	0.4
121	SLU 27	439	-6	2428	1.82	28.4	0.4
121	SLU 28	439	-6	2428	1.82	28.4	0.4
121	SLU 29	439	-6	2428	1.82	28.4	0.4
121	SLU 30	439	-6	2428	1.82	28.4	0.4
121	SLU 31	518	-7	2735	2.02	33.15	0.45
121	SLU 32	518	-7	2735	2.02	33.15	0.45
121	SLU 33	518	-7	2735	2.02	33.15	0.45
121	SLU 34	518	-7	2735	2.02	33.15	0.45
121	SLU 35	518	-7	2735	2.02	33.15	0.45
121	SLU 36	518	-7	2735	2.02	33.15	0.45
121	SLU 37	518	-7	2735	2.02	33.15	0.45
121	SLU 38	518	-7	2735	2.02	33.15	0.45
121	SLU 39	551	-7	2866	2.1	35.18	0.48
121	SLU 40	551	-7	2866	2.1	35.18	0.48
121	SLU 41	551	-7	2866	2.1	35.18	0.48
121	SLU 42	551	-7	2866	2.1	35.18	0.48
121	SLU 43	484	-7	2760	2.05	31.4	0.44
121	SLU 44	484	-7	2760	2.05	31.4	0.44
121	SLU 45	484	-7	2760	2.05	31.4	0.44
121	SLU 46	484	-7	2760	2.05	31.4	0.44
121	SLU 47	484	-7	2760	2.05	31.4	0.44
121	SLU 48	484	-7	2760	2.05	31.4	0.44
121	SLU 49	484	-7	2760	2.05	31.4	0.44
121	SLU 50	484	-7	2760	2.05	31.4	0.44
121	SLU 51	484	-7	2760	2.05	31.4	0.44
121	SLU 52	562	-7	3066	2.25	36.15	0.5
121	SLU 53	562	-7	3066	2.25	36.15	0.5
121	SLU 54	562	-7	3066	2.25	36.15	0.5
121	SLU 55	562	-7	3066	2.25	36.15	0.5
121	SLU 56	562	-7	3066	2.25	36.15	0.5
121	SLU 57	562	-7	3066	2.25	36.15	0.5
121	SLU 58	562	-7	3066	2.25	36.15	0.5
121	SLU 59	562	-7	3066	2.25	36.15	0.5
121	SLU 60	596	-8	3198	2.33	38.18	0.53
121	SLU 61	596	-8	3198	2.33	38.18	0.53
121	SLU 62	596	-8	3198	2.33	38.18	0.53
121	SLU 63	596	-8	3198	2.33	38.18	0.53
121	SLU 64	537	-7	3001	2.24	34.76	0.49
121	SLU 65	537	-7	3001	2.24	34.76	0.49
121	SLU 66	537	-7	3001	2.24	34.76	0.49
121	SLU 67	537	-7	3001	2.24	34.76	0.49
121	SLU 68	537	-7	3001	2.24	34.76	0.49
121	SLU 69	537	-7	3001	2.24	34.76	0.49
121	SLU 70	537	-7	3001	2.24	34.76	0.49
121	SLU 71	537	-7	3001	2.24	34.76	0.49
121	SLU 72	537	-7	3001	2.24	34.76	0.49
121	SLU 73	615	-8	3308	2.44	39.51	0.55
121	SLU 74	615	-8	3308	2.44	39.51	0.55
121	SLU 75	615	-8	3308	2.44	39.51	0.55
121	SLU 76	615	-8	3308	2.44	39.51	0.55
121	SLU 77	615	-8	3308	2.44	39.51	0.55
121	SLU 78	615	-8	3308	2.44	39.51	0.55
121	SLU 79	615	-8	3308	2.44	39.51	0.55
121	SLU 80	615	-8	3308	2.44	39.51	0.55
121	SLU 81	649	-8	3439	2.52	41.54	0.57
121	SLU 82	649	-8	3439	2.52	41.54	0.57
121	SLU 83	649	-8	3439	2.52	41.54	0.57
121	SLU 84	649	-8	3439	2.52	41.54	0.57
121	SLE RA 1	401	-6	2256	1.68	26	0.36
121	SLE RA 2	401	-6	2256	1.68	26	0.36
121	SLE RA 3	401	-6	2256	1.68	26	0.36
121	SLE RA 4	401	-6	2256	1.68	26	0.36
121	SLE RA 5	401	-6	2256	1.68	26	0.36
121	SLE RA 6	401	-6	2256	1.68	26	0.36
121	SLE RA 7	401	-6	2256	1.68	26	0.36
121	SLE RA 8	401	-6	2256	1.68	26	0.36
121	SLE RA 9	401	-6	2256	1.68	26	0.36
121	SLE RA 10	454	-6	2460	1.81	29.16	0.4
121	SLE RA 11	454	-6	2460	1.81	29.16	0.4
121	SLE RA 12	454	-6	2460	1.81	29.16	0.4
121	SLE RA 13	454	-6	2460	1.81	29.16	0.4
121	SLE RA 14	454	-6	2460	1.81	29.16	0.4
121	SLE RA 15	454	-6	2460	1.81	29.16	0.4
121	SLE RA 16	454	-6	2460	1.81	29.16	0.4
121	SLE RA 17	454	-6	2460	1.81	29.16	0.4
121	SLE RA 18	476	-6	2548	1.87	30.52	0.42
121	SLE RA 19	476	-6	2548	1.87	30.52	0.42
121	SLE RA 20	476	-6	2548	1.87	30.52	0.42
121	SLE RA 21	476	-6	2548	1.87	30.52	0.42
121	SLE FR 1	401	-6	2256	1.68	26	0.36
121	SLE FR 2	401	-6	2256	1.68	26	0.36
121	SLE FR 3	401	-6	2256	1.68	26	0.36
121	SLE FR 4	424	-6	2343	1.74	27.35	0.38



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
121	SLE FR 5	424	-6	2343	1.74	27.35	0.38
121	SLE FR 6	439	-6	2402	1.78	28.26	0.39
121	SLE QP 1	401	-6	2256	1.68	26	0.36
121	SLE QP 2	424	-6	2343	1.74	27.35	0.38
121	SLD 1	745	-5	1494	2.32	41.82	0.15
121	SLD 2	745	-5	1494	2.32	41.82	0.15
121	SLD 3	665	0	1836	6.91	43.82	0.27
121	SLD 4	665	0	1836	6.91	43.82	0.27
121	SLD 5	641	-13	1570	-5.06	28.66	0.12
121	SLD 6	641	-13	1570	-5.06	28.66	0.12
121	SLD 7	375	4	2710	10.26	35.33	0.54
121	SLD 8	375	4	2710	10.26	35.33	0.54
121	SLD 9	472	-15	1976	-6.79	19.38	0.22
121	SLD 10	472	-15	1976	-6.79	19.38	0.22
121	SLD 11	206	2	3117	8.53	26.05	0.64
121	SLD 12	206	2	3117	8.53	26.05	0.64
121	SLD 13	182	-12	2850	-3.44	10.89	0.49
121	SLD 14	182	-12	2850	-3.44	10.89	0.49
121	SLD 15	102	-7	3192	1.16	12.89	0.62
121	SLD 16	102	-7	3192	1.16	12.89	0.62
121	SLV 1	1187	-4	207	3.17	61.36	-0.21
121	SLV 2	1187	-4	207	3.17	61.36	-0.21
121	SLV 3	995	9	1062	14.73	66.17	0.1
121	SLV 4	995	9	1062	14.73	66.17	0.1
121	SLV 5	943	-25	406	-15.35	30.25	-0.27
121	SLV 6	943	-25	406	-15.35	30.25	-0.27
121	SLV 7	305	18	3256	23.16	46.31	0.77
121	SLV 8	305	18	3256	23.16	46.31	0.77
121	SLV 9	543	-30	1431	-19.68	8.4	-0.01
121	SLV 10	543	-30	1431	-19.68	8.4	-0.01
121	SLV 11	-96	14	4281	18.83	24.46	1.03
121	SLV 12	-96	14	4281	18.83	24.46	1.03
121	SLV 13	-148	-20	3625	-11.25	-11.46	0.66
121	SLV 14	-148	-20	3625	-11.25	-11.46	0.66
121	SLV 15	-339	-7	4480	0.3	-6.65	0.97
121	SLV 16	-339	-7	4480	0.3	-6.65	0.97
122	SLU 1	323	0	2224	0.6	16.52	-0.03
122	SLU 2	323	0	2224	0.6	16.52	-0.03
122	SLU 3	323	0	2224	0.6	16.52	-0.03
122	SLU 4	323	0	2224	0.6	16.52	-0.03
122	SLU 5	323	0	2224	0.6	16.52	-0.03
122	SLU 6	323	0	2224	0.6	16.52	-0.03
122	SLU 7	323	0	2224	0.6	16.52	-0.03
122	SLU 8	323	0	2224	0.6	16.52	-0.03
122	SLU 9	323	0	2224	0.6	16.52	-0.03
122	SLU 10	394	0	2548	0.63	20.03	-0.03
122	SLU 11	394	0	2548	0.63	20.03	-0.03
122	SLU 12	394	0	2548	0.63	20.03	-0.03
122	SLU 13	394	0	2548	0.63	20.03	-0.03
122	SLU 14	394	0	2548	0.63	20.03	-0.03
122	SLU 15	394	0	2548	0.63	20.03	-0.03
122	SLU 16	394	0	2548	0.63	20.03	-0.03
122	SLU 17	394	0	2548	0.63	20.03	-0.03
122	SLU 18	425	0	2687	0.64	21.53	-0.03
122	SLU 19	425	0	2687	0.64	21.53	-0.03
122	SLU 20	425	0	2687	0.64	21.53	-0.03
122	SLU 21	425	0	2687	0.64	21.53	-0.03
122	SLU 22	371	-1	2473	0.67	18.92	-0.03
122	SLU 23	371	-1	2473	0.67	18.92	-0.03
122	SLU 24	371	-1	2473	0.67	18.92	-0.03
122	SLU 25	371	-1	2473	0.67	18.92	-0.03
122	SLU 26	371	-1	2473	0.67	18.92	-0.03
122	SLU 27	371	-1	2473	0.67	18.92	-0.03
122	SLU 28	371	-1	2473	0.67	18.92	-0.03
122	SLU 29	371	-1	2473	0.67	18.92	-0.03
122	SLU 30	371	-1	2473	0.67	18.92	-0.03
122	SLU 31	442	0	2797	0.69	22.43	-0.04
122	SLU 32	442	0	2797	0.69	22.43	-0.04
122	SLU 33	442	0	2797	0.69	22.43	-0.04
122	SLU 34	442	0	2797	0.69	22.43	-0.04
122	SLU 35	442	0	2797	0.69	22.43	-0.04
122	SLU 36	442	0	2797	0.69	22.43	-0.04
122	SLU 37	442	0	2797	0.69	22.43	-0.04
122	SLU 38	442	0	2797	0.69	22.43	-0.04
122	SLU 39	472	0	2936	0.7	23.93	-0.04
122	SLU 40	472	0	2936	0.7	23.93	-0.04
122	SLU 41	472	0	2936	0.7	23.93	-0.04
122	SLU 42	472	0	2936	0.7	23.93	-0.04
122	SLU 43	404	-1	2806	0.76	20.66	-0.03
122	SLU 44	404	-1	2806	0.76	20.66	-0.03
122	SLU 45	404	-1	2806	0.76	20.66	-0.03
122	SLU 46	404	-1	2806	0.76	20.66	-0.03
122	SLU 47	404	-1	2806	0.76	20.66	-0.03
122	SLU 48	404	-1	2806	0.76	20.66	-0.03
122	SLU 49	404	-1	2806	0.76	20.66	-0.03
122	SLU 50	404	-1	2806	0.76	20.66	-0.03
122	SLU 51	404	-1	2806	0.76	20.66	-0.03
122	SLU 52	475	-1	3130	0.78	24.16	-0.04
122	SLU 53	475	-1	3130	0.78	24.16	-0.04



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
122	SLU 54	475	-1	3130	0.78	24.16	-0.04
122	SLU 55	475	-1	3130	0.78	24.16	-0.04
122	SLU 56	475	-1	3130	0.78	24.16	-0.04
122	SLU 57	475	-1	3130	0.78	24.16	-0.04
122	SLU 58	475	-1	3130	0.78	24.16	-0.04
122	SLU 59	475	-1	3130	0.78	24.16	-0.04
122	SLU 60	505	-1	3269	0.79	25.67	-0.04
122	SLU 61	505	-1	3269	0.79	25.67	-0.04
122	SLU 62	505	-1	3269	0.79	25.67	-0.04
122	SLU 63	505	-1	3269	0.79	25.67	-0.04
122	SLU 64	451	-1	3055	0.83	23.05	-0.04
122	SLU 65	451	-1	3055	0.83	23.05	-0.04
122	SLU 66	451	-1	3055	0.83	23.05	-0.04
122	SLU 67	451	-1	3055	0.83	23.05	-0.04
122	SLU 68	451	-1	3055	0.83	23.05	-0.04
122	SLU 69	451	-1	3055	0.83	23.05	-0.04
122	SLU 70	451	-1	3055	0.83	23.05	-0.04
122	SLU 71	451	-1	3055	0.83	23.05	-0.04
122	SLU 72	451	-1	3055	0.83	23.05	-0.04
122	SLU 73	522	-1	3379	0.85	26.56	-0.04
122	SLU 74	522	-1	3379	0.85	26.56	-0.04
122	SLU 75	522	-1	3379	0.85	26.56	-0.04
122	SLU 76	522	-1	3379	0.85	26.56	-0.04
122	SLU 77	522	-1	3379	0.85	26.56	-0.04
122	SLU 78	522	-1	3379	0.85	26.56	-0.04
122	SLU 79	522	-1	3379	0.85	26.56	-0.04
122	SLU 80	522	-1	3379	0.85	26.56	-0.04
122	SLU 81	553	-1	3518	0.86	28.06	-0.04
122	SLU 82	553	-1	3518	0.86	28.06	-0.04
122	SLU 83	553	-1	3518	0.86	28.06	-0.04
122	SLU 84	553	-1	3518	0.86	28.06	-0.04
122	SLE RA 1	337	0	2295	0.62	17.21	-0.03
122	SLE RA 2	337	0	2295	0.62	17.21	-0.03
122	SLE RA 3	337	0	2295	0.62	17.21	-0.03
122	SLE RA 4	337	0	2295	0.62	17.21	-0.03
122	SLE RA 5	337	0	2295	0.62	17.21	-0.03
122	SLE RA 6	337	0	2295	0.62	17.21	-0.03
122	SLE RA 7	337	0	2295	0.62	17.21	-0.03
122	SLE RA 8	337	0	2295	0.62	17.21	-0.03
122	SLE RA 9	337	0	2295	0.62	17.21	-0.03
122	SLE RA 10	384	0	2511	0.64	19.54	-0.03
122	SLE RA 11	384	0	2511	0.64	19.54	-0.03
122	SLE RA 12	384	0	2511	0.64	19.54	-0.03
122	SLE RA 13	384	0	2511	0.64	19.54	-0.03
122	SLE RA 14	384	0	2511	0.64	19.54	-0.03
122	SLE RA 15	384	0	2511	0.64	19.54	-0.03
122	SLE RA 16	384	0	2511	0.64	19.54	-0.03
122	SLE RA 17	384	0	2511	0.64	19.54	-0.03
122	SLE RA 18	404	0	2604	0.64	20.55	-0.03
122	SLE RA 19	404	0	2604	0.64	20.55	-0.03
122	SLE RA 20	404	0	2604	0.64	20.55	-0.03
122	SLE RA 21	404	0	2604	0.64	20.55	-0.03
122	SLE FR 1	337	0	2295	0.62	17.21	-0.03
122	SLE FR 2	337	0	2295	0.62	17.21	-0.03
122	SLE FR 3	337	0	2295	0.62	17.21	-0.03
122	SLE FR 4	357	0	2388	0.63	18.21	-0.03
122	SLE FR 5	357	0	2388	0.63	18.21	-0.03
122	SLE FR 6	371	0	2449	0.63	18.88	-0.03
122	SLE QP 1	337	0	2295	0.62	17.21	-0.03
122	SLE QP 2	357	0	2388	0.63	18.21	-0.03
122	SLD 1	632	-9	1727	1.33	32.07	-0.05
122	SLD 2	632	-9	1727	1.33	32.07	-0.05
122	SLD 3	672	-1	1977	9.98	33.94	-0.36
122	SLD 4	672	-1	1977	9.98	33.94	-0.36
122	SLD 5	379	-14	1811	-12.28	19.53	0.42
122	SLD 6	379	-14	1811	-12.28	19.53	0.42
122	SLD 7	512	11	2643	16.55	25.77	-0.59
122	SLD 8	512	11	2643	16.55	25.77	-0.59
122	SLD 9	202	-11	2132	-15.29	10.65	0.53
122	SLD 10	202	-11	2132	-15.29	10.65	0.53
122	SLD 11	335	13	2964	13.53	16.89	-0.48
122	SLD 12	335	13	2964	13.53	16.89	-0.48
122	SLD 13	42	0	2799	-8.72	2.48	0.3
122	SLD 14	42	0	2799	-8.72	2.48	0.3
122	SLD 15	82	8	3048	-0.08	4.35	-0.01
122	SLD 16	82	8	3048	-0.08	4.35	-0.01
122	SLV 1	1004	-21	719	2.38	50.81	-0.08
122	SLV 2	1004	-21	719	2.38	50.81	-0.08
122	SLV 3	1099	-2	1346	24.18	55.26	-0.85
122	SLV 4	1099	-2	1346	24.18	55.26	-0.85
122	SLV 5	408	-34	936	-31.92	21.25	1.11
122	SLV 6	408	-34	936	-31.92	21.25	1.11
122	SLV 7	722	27	3026	40.77	36.06	-1.43
122	SLV 8	722	27	3026	40.77	36.06	-1.43
122	SLV 9	-8	-28	1749	-39.51	0.36	1.37
122	SLV 10	-8	-28	1749	-39.51	0.36	1.37
122	SLV 11	306	33	3839	33.17	15.17	-1.17
122	SLV 12	306	33	3839	33.17	15.17	-1.17
122	SLV 13	-385	1	3429	-22.93	-18.84	0.79



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
122	SLV 14	-385	1	3429	-22.93	-18.84	0.79
122	SLV 15	-290	20	4056	-1.12	-14.4	0.03
122	SLV 16	-290	20	4056	-1.12	-14.4	0.03
123	SLU 1	267	0	2261	0.35	12.63	0
123	SLU 2	267	0	2261	0.35	12.63	0
123	SLU 3	267	0	2261	0.35	12.63	0
123	SLU 4	267	0	2261	0.35	12.63	0
123	SLU 5	267	0	2261	0.35	12.63	0
123	SLU 6	267	0	2261	0.35	12.63	0
123	SLU 7	267	0	2261	0.35	12.63	0
123	SLU 8	267	0	2261	0.35	12.63	0
123	SLU 9	267	0	2261	0.35	12.63	0
123	SLU 10	330	0	2603	0.34	15.51	-0.01
123	SLU 11	330	0	2603	0.34	15.51	-0.01
123	SLU 12	330	0	2603	0.34	15.51	-0.01
123	SLU 13	330	0	2603	0.34	15.51	-0.01
123	SLU 14	330	0	2603	0.34	15.51	-0.01
123	SLU 15	330	0	2603	0.34	15.51	-0.01
123	SLU 16	330	0	2603	0.34	15.51	-0.01
123	SLU 17	330	0	2603	0.34	15.51	-0.01
123	SLU 18	357	0	2749	0.34	16.75	-0.01
123	SLU 19	357	0	2749	0.34	16.75	-0.01
123	SLU 20	357	0	2749	0.34	16.75	-0.01
123	SLU 21	357	0	2749	0.34	16.75	-0.01
123	SLU 22	309	0	2517	0.39	14.55	-0.01
123	SLU 23	309	0	2517	0.39	14.55	-0.01
123	SLU 24	309	0	2517	0.39	14.55	-0.01
123	SLU 25	309	0	2517	0.39	14.55	-0.01
123	SLU 26	309	0	2517	0.39	14.55	-0.01
123	SLU 27	309	0	2517	0.39	14.55	-0.01
123	SLU 28	309	0	2517	0.39	14.55	-0.01
123	SLU 29	309	0	2517	0.39	14.55	-0.01
123	SLU 30	309	0	2517	0.39	14.55	-0.01
123	SLU 31	372	0	2859	0.39	17.44	-0.01
123	SLU 32	372	0	2859	0.39	17.44	-0.01
123	SLU 33	372	0	2859	0.39	17.44	-0.01
123	SLU 34	372	0	2859	0.39	17.44	-0.01
123	SLU 35	372	0	2859	0.39	17.44	-0.01
123	SLU 36	372	0	2859	0.39	17.44	-0.01
123	SLU 37	372	0	2859	0.39	17.44	-0.01
123	SLU 38	372	0	2859	0.39	17.44	-0.01
123	SLU 39	399	0	3006	0.38	18.68	-0.01
123	SLU 40	399	0	3006	0.38	18.68	-0.01
123	SLU 41	399	0	3006	0.38	18.68	-0.01
123	SLU 42	399	0	3006	0.38	18.68	-0.01
123	SLU 43	333	0	2851	0.44	15.75	-0.01
123	SLU 44	333	0	2851	0.44	15.75	-0.01
123	SLU 45	333	0	2851	0.44	15.75	-0.01
123	SLU 46	333	0	2851	0.44	15.75	-0.01
123	SLU 47	333	0	2851	0.44	15.75	-0.01
123	SLU 48	333	0	2851	0.44	15.75	-0.01
123	SLU 49	333	0	2851	0.44	15.75	-0.01
123	SLU 50	333	0	2851	0.44	15.75	-0.01
123	SLU 51	333	0	2851	0.44	15.75	-0.01
123	SLU 52	396	0	3193	0.44	18.64	-0.01
123	SLU 53	396	0	3193	0.44	18.64	-0.01
123	SLU 54	396	0	3193	0.44	18.64	-0.01
123	SLU 55	396	0	3193	0.44	18.64	-0.01
123	SLU 56	396	0	3193	0.44	18.64	-0.01
123	SLU 57	396	0	3193	0.44	18.64	-0.01
123	SLU 58	396	0	3193	0.44	18.64	-0.01
123	SLU 59	396	0	3193	0.44	18.64	-0.01
123	SLU 60	423	0	3339	0.43	19.87	-0.01
123	SLU 61	423	0	3339	0.43	19.87	-0.01
123	SLU 62	423	0	3339	0.43	19.87	-0.01
123	SLU 63	423	0	3339	0.43	19.87	-0.01
123	SLU 64	374	0	3108	0.48	17.68	-0.01
123	SLU 65	374	0	3108	0.48	17.68	-0.01
123	SLU 66	374	0	3108	0.48	17.68	-0.01
123	SLU 67	374	0	3108	0.48	17.68	-0.01
123	SLU 68	374	0	3108	0.48	17.68	-0.01
123	SLU 69	374	0	3108	0.48	17.68	-0.01
123	SLU 70	374	0	3108	0.48	17.68	-0.01
123	SLU 71	374	0	3108	0.48	17.68	-0.01
123	SLU 72	374	0	3108	0.48	17.68	-0.01
123	SLU 73	438	0	3449	0.48	20.57	-0.01
123	SLU 74	438	0	3449	0.48	20.57	-0.01
123	SLU 75	438	0	3449	0.48	20.57	-0.01
123	SLU 76	438	0	3449	0.48	20.57	-0.01
123	SLU 77	438	0	3449	0.48	20.57	-0.01
123	SLU 78	438	0	3449	0.48	20.57	-0.01
123	SLU 79	438	0	3449	0.48	20.57	-0.01
123	SLU 80	438	0	3449	0.48	20.57	-0.01
123	SLU 81	465	0	3596	0.48	21.8	-0.01
123	SLU 82	465	0	3596	0.48	21.8	-0.01
123	SLU 83	465	0	3596	0.48	21.8	-0.01
123	SLU 84	465	0	3596	0.48	21.8	-0.01
123	SLE RA 1	279	0	2334	0.36	13.18	0
123	SLE RA 2	279	0	2334	0.36	13.18	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
123	SLE RA 3	279	0	2334	0.36	13.18	0
123	SLE RA 4	279	0	2334	0.36	13.18	0
123	SLE RA 5	279	0	2334	0.36	13.18	0
123	SLE RA 6	279	0	2334	0.36	13.18	0
123	SLE RA 7	279	0	2334	0.36	13.18	0
123	SLE RA 8	279	0	2334	0.36	13.18	0
123	SLE RA 9	279	0	2334	0.36	13.18	0
123	SLE RA 10	321	0	2562	0.36	15.1	-0.01
123	SLE RA 11	321	0	2562	0.36	15.1	-0.01
123	SLE RA 12	321	0	2562	0.36	15.1	-0.01
123	SLE RA 13	321	0	2562	0.36	15.1	-0.01
123	SLE RA 14	321	0	2562	0.36	15.1	-0.01
123	SLE RA 15	321	0	2562	0.36	15.1	-0.01
123	SLE RA 16	321	0	2562	0.36	15.1	-0.01
123	SLE RA 17	321	0	2562	0.36	15.1	-0.01
123	SLE RA 18	339	0	2660	0.36	15.92	-0.01
123	SLE RA 19	339	0	2660	0.36	15.92	-0.01
123	SLE RA 20	339	0	2660	0.36	15.92	-0.01
123	SLE RA 21	339	0	2660	0.36	15.92	-0.01
123	SLE FR 1	279	0	2334	0.36	13.18	0
123	SLE FR 2	279	0	2334	0.36	13.18	0
123	SLE FR 3	279	0	2334	0.36	13.18	0
123	SLE FR 4	297	0	2432	0.36	14	-0.01
123	SLE FR 5	297	0	2432	0.36	14	-0.01
123	SLE FR 6	309	0	2497	0.36	14.55	-0.01
123	SLE QP 1	279	0	2334	0.36	13.18	0
123	SLE QP 2	297	0	2432	0.36	14	-0.01
123	SLD 1	573	-2	1899	0.95	27.22	-0.01
123	SLD 2	573	-2	1899	0.95	27.22	-0.01
123	SLD 3	611	-15	2095	16.3	29.04	-0.39
123	SLD 4	611	-15	2095	16.3	29.04	-0.39
123	SLD 5	323	19	1975	-22.75	15.21	0.56
123	SLD 6	323	19	1975	-22.75	15.21	0.56
123	SLD 7	448	-24	2628	28.43	21.27	-0.69
123	SLD 8	448	-24	2628	28.43	21.27	-0.69
123	SLD 9	146	24	2236	-27.71	6.73	0.68
123	SLD 10	146	24	2236	-27.71	6.73	0.68
123	SLD 11	271	-19	2888	23.48	12.79	-0.57
123	SLD 12	271	-19	2888	23.48	12.79	-0.57
123	SLD 13	-17	15	2768	-15.58	-1.04	0.37
123	SLD 14	-17	15	2768	-15.58	-1.04	0.37
123	SLD 15	21	2	2964	-0.22	0.78	0
123	SLD 16	21	2	2964	-0.22	0.78	0
123	SLV 1	948	-5	1082	1.78	45.1	-0.01
123	SLV 2	948	-5	1082	1.78	45.1	-0.01
123	SLV 3	1038	-37	1577	40.65	49.46	-0.96
123	SLV 4	1038	-37	1577	40.65	49.46	-0.96
123	SLV 5	356	47	1277	-58.16	16.72	1.44
123	SLV 6	356	47	1277	-58.16	16.72	1.44
123	SLV 7	655	-60	2925	71.4	31.24	-1.74
123	SLV 8	655	-60	2925	71.4	31.24	-1.74
123	SLV 9	-61	59	1939	-70.67	-3.24	1.73
123	SLV 10	-61	59	1939	-70.67	-3.24	1.73
123	SLV 11	238	-47	3586	58.88	11.28	-1.45
123	SLV 12	238	-47	3586	58.88	11.28	-1.45
123	SLV 13	-444	37	3287	-39.92	-21.46	0.95
123	SLV 14	-444	37	3287	-39.92	-21.46	0.95
123	SLV 15	-354	5	3781	-1.06	-17.1	0
123	SLV 16	-354	5	3781	-1.06	-17.1	0
124	SLU 1	210	0	2309	0.26	9.42	0
124	SLU 2	210	0	2309	0.26	9.42	0
124	SLU 3	210	0	2309	0.26	9.42	0
124	SLU 4	210	0	2309	0.26	9.42	0
124	SLU 5	210	0	2309	0.26	9.42	0
124	SLU 6	210	0	2309	0.26	9.42	0
124	SLU 7	210	0	2309	0.26	9.42	0
124	SLU 8	210	0	2309	0.26	9.42	0
124	SLU 9	210	0	2309	0.26	9.42	0
124	SLU 10	264	0	2672	0.26	11.77	0
124	SLU 11	264	0	2672	0.26	11.77	0
124	SLU 12	264	0	2672	0.26	11.77	0
124	SLU 13	264	0	2672	0.26	11.77	0
124	SLU 14	264	0	2672	0.26	11.77	0
124	SLU 15	264	0	2672	0.26	11.77	0
124	SLU 16	264	0	2672	0.26	11.77	0
124	SLU 17	264	0	2672	0.26	11.77	0
124	SLU 18	287	0	2828	0.26	12.78	0
124	SLU 19	287	0	2828	0.26	12.78	0
124	SLU 20	287	0	2828	0.26	12.78	0
124	SLU 21	287	0	2828	0.26	12.78	0
124	SLU 22	245	0	2576	0.29	10.96	0
124	SLU 23	245	0	2576	0.29	10.96	0
124	SLU 24	245	0	2576	0.29	10.96	0
124	SLU 25	245	0	2576	0.29	10.96	0
124	SLU 26	245	0	2576	0.29	10.96	0
124	SLU 27	245	0	2576	0.29	10.96	0
124	SLU 28	245	0	2576	0.29	10.96	0
124	SLU 29	245	0	2576	0.29	10.96	0
124	SLU 30	245	0	2576	0.29	10.96	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
124	SLU 31	299	0	2939	0.3	13.31	0
124	SLU 32	299	0	2939	0.3	13.31	0
124	SLU 33	299	0	2939	0.3	13.31	0
124	SLU 34	299	0	2939	0.3	13.31	0
124	SLU 35	299	0	2939	0.3	13.31	0
124	SLU 36	299	0	2939	0.3	13.31	0
124	SLU 37	299	0	2939	0.3	13.31	0
124	SLU 38	299	0	2939	0.3	13.31	0
124	SLU 39	322	0	3095	0.3	14.32	0
124	SLU 40	322	0	3095	0.3	14.32	0
124	SLU 41	322	0	3095	0.3	14.32	0
124	SLU 42	322	0	3095	0.3	14.32	0
124	SLU 43	261	0	2911	0.32	11.72	0
124	SLU 44	261	0	2911	0.32	11.72	0
124	SLU 45	261	0	2911	0.32	11.72	0
124	SLU 46	261	0	2911	0.32	11.72	0
124	SLU 47	261	0	2911	0.32	11.72	0
124	SLU 48	261	0	2911	0.32	11.72	0
124	SLU 49	261	0	2911	0.32	11.72	0
124	SLU 50	261	0	2911	0.32	11.72	0
124	SLU 51	261	0	2911	0.32	11.72	0
124	SLU 52	315	0	3274	0.32	14.07	0
124	SLU 53	315	0	3274	0.32	14.07	0
124	SLU 54	315	0	3274	0.32	14.07	0
124	SLU 55	315	0	3274	0.32	14.07	0
124	SLU 56	315	0	3274	0.32	14.07	0
124	SLU 57	315	0	3274	0.32	14.07	0
124	SLU 58	315	0	3274	0.32	14.07	0
124	SLU 59	315	0	3274	0.32	14.07	0
124	SLU 60	338	0	3429	0.32	15.08	0
124	SLU 61	338	0	3429	0.32	15.08	0
124	SLU 62	338	0	3429	0.32	15.08	0
124	SLU 63	338	0	3429	0.32	15.08	0
124	SLU 64	296	0	3177	0.36	13.26	0
124	SLU 65	296	0	3177	0.36	13.26	0
124	SLU 66	296	0	3177	0.36	13.26	0
124	SLU 67	296	0	3177	0.36	13.26	0
124	SLU 68	296	0	3177	0.36	13.26	0
124	SLU 69	296	0	3177	0.36	13.26	0
124	SLU 70	296	0	3177	0.36	13.26	0
124	SLU 71	296	0	3177	0.36	13.26	0
124	SLU 72	296	0	3177	0.36	13.26	0
124	SLU 73	350	0	3540	0.36	15.61	0
124	SLU 74	350	0	3540	0.36	15.61	0
124	SLU 75	350	0	3540	0.36	15.61	0
124	SLU 76	350	0	3540	0.36	15.61	0
124	SLU 77	350	0	3540	0.36	15.61	0
124	SLU 78	350	0	3540	0.36	15.61	0
124	SLU 79	350	0	3540	0.36	15.61	0
124	SLU 80	350	0	3540	0.36	15.61	0
124	SLU 81	373	0	3696	0.36	16.62	0
124	SLU 82	373	0	3696	0.36	16.62	0
124	SLU 83	373	0	3696	0.36	16.62	0
124	SLU 84	373	0	3696	0.36	16.62	0
124	SLE RA 1	220	0	2386	0.27	9.86	0
124	SLE RA 2	220	0	2386	0.27	9.86	0
124	SLE RA 3	220	0	2386	0.27	9.86	0
124	SLE RA 4	220	0	2386	0.27	9.86	0
124	SLE RA 5	220	0	2386	0.27	9.86	0
124	SLE RA 6	220	0	2386	0.27	9.86	0
124	SLE RA 7	220	0	2386	0.27	9.86	0
124	SLE RA 8	220	0	2386	0.27	9.86	0
124	SLE RA 9	220	0	2386	0.27	9.86	0
124	SLE RA 10	256	0	2627	0.27	11.43	0
124	SLE RA 11	256	0	2627	0.27	11.43	0
124	SLE RA 12	256	0	2627	0.27	11.43	0
124	SLE RA 13	256	0	2627	0.27	11.43	0
124	SLE RA 14	256	0	2627	0.27	11.43	0
124	SLE RA 15	256	0	2627	0.27	11.43	0
124	SLE RA 16	256	0	2627	0.27	11.43	0
124	SLE RA 17	256	0	2627	0.27	11.43	0
124	SLE RA 18	271	0	2731	0.27	12.1	0
124	SLE RA 19	271	0	2731	0.27	12.1	0
124	SLE RA 20	271	0	2731	0.27	12.1	0
124	SLE RA 21	271	0	2731	0.27	12.1	0
124	SLE FR 1	220	0	2386	0.27	9.86	0
124	SLE FR 2	220	0	2386	0.27	9.86	0
124	SLE FR 3	220	0	2386	0.27	9.86	0
124	SLE FR 4	235	0	2489	0.27	10.53	0
124	SLE FR 5	235	0	2489	0.27	10.53	0
124	SLE FR 6	246	0	2558	0.27	10.98	0
124	SLE QP 1	220	0	2386	0.27	9.86	0
124	SLE QP 2	235	0	2489	0.27	10.53	0
124	SLD 1	510	-3	2050	0.22	23.12	-0.01
124	SLD 2	510	-3	2050	0.22	23.12	-0.01
124	SLD 3	549	-21	2213	22.04	24.92	-0.35
124	SLD 4	549	-21	2213	22.04	24.92	-0.35
124	SLD 5	259	27	2109	-32.84	11.59	0.52
124	SLD 6	259	27	2109	-32.84	11.59	0.52



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
124	SLD 7	388	-34	2655	39.89	17.57	-0.63
124	SLD 8	388	-34	2655	39.89	17.57	-0.63
124	SLD 9	82	34	2323	-39.36	3.5	0.63
124	SLD 10	82	34	2323	-39.36	3.5	0.63
124	SLD 11	212	-27	2870	33.38	9.47	-0.53
124	SLD 12	212	-27	2870	33.38	9.47	-0.53
124	SLD 13	-78	21	2765	-21.51	-3.85	0.35
124	SLD 14	-78	21	2765	-21.51	-3.85	0.35
124	SLD 15	-39	3	2929	0.32	-2.06	0.01
124	SLD 16	-39	3	2929	0.32	-2.06	0.01
124	SLV 1	882	-7	1372	0.03	40.15	-0.01
124	SLV 2	882	-7	1372	0.03	40.15	-0.01
124	SLV 3	976	-53	1787	55.43	44.48	-0.89
124	SLV 4	976	-53	1787	55.43	44.48	-0.89
124	SLV 5	287	67	1524	-83.82	12.85	1.33
124	SLV 6	287	67	1524	-83.82	12.85	1.33
124	SLV 7	600	-85	2908	100.83	27.29	-1.6
124	SLV 8	600	-85	2908	100.83	27.29	-1.6
124	SLV 9	-130	85	2070	-100.29	-6.23	1.6
124	SLV 10	-130	85	2070	-100.29	-6.23	1.6
124	SLV 11	184	-67	3454	84.35	8.22	-1.33
124	SLV 12	184	-67	3454	84.35	8.22	-1.33
124	SLV 13	-506	53	3191	-54.89	-23.42	0.89
124	SLV 14	-506	53	3191	-54.89	-23.42	0.89
124	SLV 15	-412	7	3607	0.5	-19.09	0.01
124	SLV 16	-412	7	3607	0.5	-19.09	0.01
125	SLU 1	151	0	2360	0.21	6.13	0
125	SLU 2	151	0	2360	0.21	6.13	0
125	SLU 3	151	0	2360	0.21	6.13	0
125	SLU 4	151	0	2360	0.21	6.13	0
125	SLU 5	151	0	2360	0.21	6.13	0
125	SLU 6	151	0	2360	0.21	6.13	0
125	SLU 7	151	0	2360	0.21	6.13	0
125	SLU 8	151	0	2360	0.21	6.13	0
125	SLU 9	151	0	2360	0.21	6.13	0
125	SLU 10	194	0	2746	0.24	7.84	0
125	SLU 11	194	0	2746	0.24	7.84	0
125	SLU 12	194	0	2746	0.24	7.84	0
125	SLU 13	194	0	2746	0.24	7.84	0
125	SLU 14	194	0	2746	0.24	7.84	0
125	SLU 15	194	0	2746	0.24	7.84	0
125	SLU 16	194	0	2746	0.24	7.84	0
125	SLU 17	194	0	2746	0.24	7.84	0
125	SLU 18	213	0	2912	0.25	8.58	0
125	SLU 19	213	0	2912	0.25	8.58	0
125	SLU 20	213	0	2912	0.25	8.58	0
125	SLU 21	213	0	2912	0.25	8.58	0
125	SLU 22	178	0	2638	0.25	7.22	0
125	SLU 23	178	0	2638	0.25	7.22	0
125	SLU 24	178	0	2638	0.25	7.22	0
125	SLU 25	178	0	2638	0.25	7.22	0
125	SLU 26	178	0	2638	0.25	7.22	0
125	SLU 27	178	0	2638	0.25	7.22	0
125	SLU 28	178	0	2638	0.25	7.22	0
125	SLU 29	178	0	2638	0.25	7.22	0
125	SLU 30	178	0	2638	0.25	7.22	0
125	SLU 31	222	0	3024	0.27	8.93	0
125	SLU 32	222	0	3024	0.27	8.93	0
125	SLU 33	222	0	3024	0.27	8.93	0
125	SLU 34	222	0	3024	0.27	8.93	0
125	SLU 35	222	0	3024	0.27	8.93	0
125	SLU 36	222	0	3024	0.27	8.93	0
125	SLU 37	222	0	3024	0.27	8.93	0
125	SLU 38	222	0	3024	0.27	8.93	0
125	SLU 39	240	0	3190	0.29	9.67	0
125	SLU 40	240	0	3190	0.29	9.67	0
125	SLU 41	240	0	3190	0.29	9.67	0
125	SLU 42	240	0	3190	0.29	9.67	0
125	SLU 43	187	0	2972	0.26	7.6	0
125	SLU 44	187	0	2972	0.26	7.6	0
125	SLU 45	187	0	2972	0.26	7.6	0
125	SLU 46	187	0	2972	0.26	7.6	0
125	SLU 47	187	0	2972	0.26	7.6	0
125	SLU 48	187	0	2972	0.26	7.6	0
125	SLU 49	187	0	2972	0.26	7.6	0
125	SLU 50	187	0	2972	0.26	7.6	0
125	SLU 51	187	0	2972	0.26	7.6	0
125	SLU 52	230	0	3359	0.29	9.31	0
125	SLU 53	230	0	3359	0.29	9.31	0
125	SLU 54	230	0	3359	0.29	9.31	0
125	SLU 55	230	0	3359	0.29	9.31	0
125	SLU 56	230	0	3359	0.29	9.31	0
125	SLU 57	230	0	3359	0.29	9.31	0
125	SLU 58	230	0	3359	0.29	9.31	0
125	SLU 59	230	0	3359	0.29	9.31	0
125	SLU 60	249	0	3524	0.3	10.04	0
125	SLU 61	249	0	3524	0.3	10.04	0
125	SLU 62	249	0	3524	0.3	10.04	0
125	SLU 63	249	0	3524	0.3	10.04	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
125	SLU 64	214	0	3251	0.3	8.69	0
125	SLU 65	214	0	3251	0.3	8.69	0
125	SLU 66	214	0	3251	0.3	8.69	0
125	SLU 67	214	0	3251	0.3	8.69	0
125	SLU 68	214	0	3251	0.3	8.69	0
125	SLU 69	214	0	3251	0.3	8.69	0
125	SLU 70	214	0	3251	0.3	8.69	0
125	SLU 71	214	0	3251	0.3	8.69	0
125	SLU 72	214	0	3251	0.3	8.69	0
125	SLU 73	257	0	3637	0.32	10.4	0
125	SLU 74	257	0	3637	0.32	10.4	0
125	SLU 75	257	0	3637	0.32	10.4	0
125	SLU 76	257	0	3637	0.32	10.4	0
125	SLU 77	257	0	3637	0.32	10.4	0
125	SLU 78	257	0	3637	0.32	10.4	0
125	SLU 79	257	0	3637	0.32	10.4	0
125	SLU 80	257	0	3637	0.32	10.4	0
125	SLU 81	276	0	3803	0.34	11.13	0
125	SLU 82	276	0	3803	0.34	11.13	0
125	SLU 83	276	0	3803	0.34	11.13	0
125	SLU 84	276	0	3803	0.34	11.13	0
125	SLE RA 1	158	0	2439	0.22	6.44	0
125	SLE RA 2	158	0	2439	0.22	6.44	0
125	SLE RA 3	158	0	2439	0.22	6.44	0
125	SLE RA 4	158	0	2439	0.22	6.44	0
125	SLE RA 5	158	0	2439	0.22	6.44	0
125	SLE RA 6	158	0	2439	0.22	6.44	0
125	SLE RA 7	158	0	2439	0.22	6.44	0
125	SLE RA 8	158	0	2439	0.22	6.44	0
125	SLE RA 9	158	0	2439	0.22	6.44	0
125	SLE RA 10	188	0	2697	0.24	7.58	0
125	SLE RA 11	188	0	2697	0.24	7.58	0
125	SLE RA 12	188	0	2697	0.24	7.58	0
125	SLE RA 13	188	0	2697	0.24	7.58	0
125	SLE RA 14	188	0	2697	0.24	7.58	0
125	SLE RA 15	188	0	2697	0.24	7.58	0
125	SLE RA 16	188	0	2697	0.24	7.58	0
125	SLE RA 17	188	0	2697	0.24	7.58	0
125	SLE RA 18	200	0	2807	0.25	8.07	0
125	SLE RA 19	200	0	2807	0.25	8.07	0
125	SLE RA 20	200	0	2807	0.25	8.07	0
125	SLE RA 21	200	0	2807	0.25	8.07	0
125	SLE FR 1	158	0	2439	0.22	6.44	0
125	SLE FR 2	158	0	2439	0.22	6.44	0
125	SLE FR 3	158	0	2439	0.22	6.44	0
125	SLE FR 4	171	0	2550	0.23	6.93	0
125	SLE FR 5	171	0	2550	0.23	6.93	0
125	SLE FR 6	179	0	2623	0.23	7.26	0
125	SLE QP 1	158	0	2439	0.22	6.44	0
125	SLE QP 2	171	0	2550	0.23	6.93	0
125	SLD 1	443	-3	2189	-1.32	18.34	-0.01
125	SLD 2	443	-3	2189	-1.32	18.34	-0.01
125	SLD 3	484	-24	2333	26.79	20.04	-0.3
125	SLD 4	484	-24	2333	26.79	20.04	-0.3
125	SLD 5	190	32	2224	-42.87	7.77	0.44
125	SLD 6	190	32	2224	-42.87	7.77	0.44
125	SLD 7	327	-40	2702	50.83	13.45	-0.53
125	SLD 8	327	-40	2702	50.83	13.45	-0.53
125	SLD 9	15	40	2397	-50.37	0.42	0.53
125	SLD 10	15	40	2397	-50.37	0.42	0.53
125	SLD 11	152	-32	2875	43.32	6.09	-0.44
125	SLD 12	152	-32	2875	43.32	6.09	-0.44
125	SLD 13	-142	24	2767	-26.33	-6.18	0.3
125	SLD 14	-142	24	2767	-26.33	-6.18	0.3
125	SLD 15	-101	2	2910	1.78	-4.48	0.01
125	SLD 16	-101	2	2910	1.78	-4.48	0.01
125	SLV 1	812	-7	1632	-3.87	33.76	-0.02
125	SLV 2	812	-7	1632	-3.87	33.76	-0.02
125	SLV 3	912	-60	1996	67.68	37.91	-0.75
125	SLV 4	912	-60	1996	67.68	37.91	-0.75
125	SLV 5	211	79	1722	-109.53	8.69	1.1
125	SLV 6	211	79	1722	-109.53	8.69	1.1
125	SLV 7	545	-100	2936	129	22.51	-1.34
125	SLV 8	545	-100	2936	129	22.51	-1.34
125	SLV 9	-203	99	2163	-128.54	-8.65	1.33
125	SLV 10	-203	99	2163	-128.54	-8.65	1.33
125	SLV 11	131	-79	3378	109.99	5.17	-1.11
125	SLV 12	131	-79	3378	109.99	5.17	-1.11
125	SLV 13	-570	60	3104	-67.23	-24.05	0.75
125	SLV 14	-570	60	3104	-67.23	-24.05	0.75
125	SLV 15	-470	6	3468	4.33	-19.9	0.02
125	SLV 16	-470	6	3468	4.33	-19.9	0.02
126	SLU 1	116	0	2408	0.18	4.18	0
126	SLU 2	116	0	2408	0.18	4.18	0
126	SLU 3	116	0	2408	0.18	4.18	0
126	SLU 4	116	0	2408	0.18	4.18	0
126	SLU 5	116	0	2408	0.18	4.18	0
126	SLU 6	116	0	2408	0.18	4.18	0
126	SLU 7	116	0	2408	0.18	4.18	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
126	SLU 8	116	0	2408	0.18	4.18	0
126	SLU 9	116	0	2408	0.18	4.18	0
126	SLU 10	155	0	2816	0.22	5.58	0
126	SLU 11	155	0	2816	0.22	5.58	0
126	SLU 12	155	0	2816	0.22	5.58	0
126	SLU 13	155	0	2816	0.22	5.58	0
126	SLU 14	155	0	2816	0.22	5.58	0
126	SLU 15	155	0	2816	0.22	5.58	0
126	SLU 16	155	0	2816	0.22	5.58	0
126	SLU 17	155	0	2816	0.22	5.58	0
126	SLU 18	172	0	2991	0.24	6.19	0
126	SLU 19	172	0	2991	0.24	6.19	0
126	SLU 20	172	0	2991	0.24	6.19	0
126	SLU 21	172	0	2991	0.24	6.19	0
126	SLU 22	140	0	2696	0.22	5.04	0
126	SLU 23	140	0	2696	0.22	5.04	0
126	SLU 24	140	0	2696	0.22	5.04	0
126	SLU 25	140	0	2696	0.22	5.04	0
126	SLU 26	140	0	2696	0.22	5.04	0
126	SLU 27	140	0	2696	0.22	5.04	0
126	SLU 28	140	0	2696	0.22	5.04	0
126	SLU 29	140	0	2696	0.22	5.04	0
126	SLU 30	140	0	2696	0.22	5.04	0
126	SLU 31	178	0	3104	0.26	6.44	0
126	SLU 32	178	0	3104	0.26	6.44	0
126	SLU 33	178	0	3104	0.26	6.44	0
126	SLU 34	178	0	3104	0.26	6.44	0
126	SLU 35	178	0	3104	0.26	6.44	0
126	SLU 36	178	0	3104	0.26	6.44	0
126	SLU 37	178	0	3104	0.26	6.44	0
126	SLU 38	178	0	3104	0.26	6.44	0
126	SLU 39	195	0	3279	0.28	7.04	0
126	SLU 40	195	0	3279	0.28	7.04	0
126	SLU 41	195	0	3279	0.28	7.04	0
126	SLU 42	195	0	3279	0.28	7.04	0
126	SLU 43	143	0	3031	0.22	5.14	0
126	SLU 44	143	0	3031	0.22	5.14	0
126	SLU 45	143	0	3031	0.22	5.14	0
126	SLU 46	143	0	3031	0.22	5.14	0
126	SLU 47	143	0	3031	0.22	5.14	0
126	SLU 48	143	0	3031	0.22	5.14	0
126	SLU 49	143	0	3031	0.22	5.14	0
126	SLU 50	143	0	3031	0.22	5.14	0
126	SLU 51	143	0	3031	0.22	5.14	0
126	SLU 52	182	0	3439	0.26	6.54	0
126	SLU 53	182	0	3439	0.26	6.54	0
126	SLU 54	182	0	3439	0.26	6.54	0
126	SLU 55	182	0	3439	0.26	6.54	0
126	SLU 56	182	0	3439	0.26	6.54	0
126	SLU 57	182	0	3439	0.26	6.54	0
126	SLU 58	182	0	3439	0.26	6.54	0
126	SLU 59	182	0	3439	0.26	6.54	0
126	SLU 60	198	0	3614	0.28	7.15	0
126	SLU 61	198	0	3614	0.28	7.15	0
126	SLU 62	198	0	3614	0.28	7.15	0
126	SLU 63	198	0	3614	0.28	7.15	0
126	SLU 64	166	0	3320	0.26	6	0
126	SLU 65	166	0	3320	0.26	6	0
126	SLU 66	166	0	3320	0.26	6	0
126	SLU 67	166	0	3320	0.26	6	0
126	SLU 68	166	0	3320	0.26	6	0
126	SLU 69	166	0	3320	0.26	6	0
126	SLU 70	166	0	3320	0.26	6	0
126	SLU 71	166	0	3320	0.26	6	0
126	SLU 72	166	0	3320	0.26	6	0
126	SLU 73	205	0	3728	0.3	7.4	0
126	SLU 74	205	0	3728	0.3	7.4	0
126	SLU 75	205	0	3728	0.3	7.4	0
126	SLU 76	205	0	3728	0.3	7.4	0
126	SLU 77	205	0	3728	0.3	7.4	0
126	SLU 78	205	0	3728	0.3	7.4	0
126	SLU 79	205	0	3728	0.3	7.4	0
126	SLU 80	205	0	3728	0.3	7.4	0
126	SLU 81	222	0	3903	0.32	8	0
126	SLU 82	222	0	3903	0.32	8	0
126	SLU 83	222	0	3903	0.32	8	0
126	SLU 84	222	0	3903	0.32	8	0
126	SLE RA 1	123	0	2490	0.19	4.43	0
126	SLE RA 2	123	0	2490	0.19	4.43	0
126	SLE RA 3	123	0	2490	0.19	4.43	0
126	SLE RA 4	123	0	2490	0.19	4.43	0
126	SLE RA 5	123	0	2490	0.19	4.43	0
126	SLE RA 6	123	0	2490	0.19	4.43	0
126	SLE RA 7	123	0	2490	0.19	4.43	0
126	SLE RA 8	123	0	2490	0.19	4.43	0
126	SLE RA 9	123	0	2490	0.19	4.43	0
126	SLE RA 10	149	0	2762	0.22	5.36	0
126	SLE RA 11	149	0	2762	0.22	5.36	0
126	SLE RA 12	149	0	2762	0.22	5.36	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
126	SLE RA 13	149	0	2762	0.22	5.36	0
126	SLE RA 14	149	0	2762	0.22	5.36	0
126	SLE RA 15	149	0	2762	0.22	5.36	0
126	SLE RA 16	149	0	2762	0.22	5.36	0
126	SLE RA 17	149	0	2762	0.22	5.36	0
126	SLE RA 18	160	0	2879	0.23	5.76	0
126	SLE RA 19	160	0	2879	0.23	5.76	0
126	SLE RA 20	160	0	2879	0.23	5.76	0
126	SLE RA 21	160	0	2879	0.23	5.76	0
126	SLE FR 1	123	0	2490	0.19	4.43	0
126	SLE FR 2	123	0	2490	0.19	4.43	0
126	SLE FR 3	123	0	2490	0.19	4.43	0
126	SLE FR 4	134	0	2607	0.2	4.83	0
126	SLE FR 5	134	0	2607	0.2	4.83	0
126	SLE FR 6	141	0	2684	0.21	5.09	0
126	SLE QP 1	123	0	2490	0.19	4.43	0
126	SLE QP 2	134	0	2607	0.2	4.83	0
126	SLD 1	399	-3	2308	-4.13	16.62	-0.1
126	SLD 2	399	-3	2308	-4.13	16.62	-0.1
126	SLD 3	441	-26	2441	30.76	18.53	0.51
126	SLD 4	441	-26	2441	30.76	18.53	0.51
126	SLD 5	149	32	2315	-54.01	5.47	-0.95
126	SLD 6	149	32	2315	-54.01	5.47	-0.95
126	SLD 7	290	-41	2759	62.29	11.83	1.07
126	SLD 8	290	-41	2759	62.29	11.83	1.07
126	SLD 9	-23	41	2454	-61.88	-2.17	-1.07
126	SLD 10	-23	41	2454	-61.88	-2.17	-1.07
126	SLD 11	119	-33	2898	54.42	4.18	0.95
126	SLD 12	119	-33	2898	54.42	4.18	0.95
126	SLD 13	-173	25	2772	-30.35	-8.87	-0.51
126	SLD 14	-173	25	2772	-30.35	-8.87	-0.51
126	SLD 15	-131	3	2905	4.54	-6.97	0.1
126	SLD 16	-131	3	2905	4.54	-6.97	0.1
126	SLV 1	757	-9	1844	-11.03	32.54	-0.26
126	SLV 2	757	-9	1844	-11.03	32.54	-0.26
126	SLV 3	861	-64	2183	78.04	37.22	1.28
126	SLV 4	861	-64	2183	78.04	37.22	1.28
126	SLV 5	163	81	1863	-138.26	6.05	-2.42
126	SLV 6	163	81	1863	-138.26	6.05	-2.42
126	SLV 7	510	-103	2995	158.64	21.64	2.72
126	SLV 8	510	-103	2995	158.64	21.64	2.72
126	SLV 9	-242	102	2219	-158.24	-11.99	-2.72
126	SLV 10	-242	102	2219	-158.24	-11.99	-2.72
126	SLV 11	104	-81	3350	138.66	3.61	2.42
126	SLV 12	104	-81	3350	138.66	3.61	2.42
126	SLV 13	-593	64	3030	-77.63	-27.57	-1.28
126	SLV 14	-593	64	3030	-77.63	-27.57	-1.28
126	SLV 15	-490	9	3369	11.44	-22.89	0.26
126	SLV 16	-490	9	3369	11.44	-22.89	0.26
127	SLU 1	22	0	2457	0.15	1.16	0
127	SLU 2	22	0	2457	0.15	1.16	0
127	SLU 3	22	0	2457	0.15	1.16	0
127	SLU 4	22	0	2457	0.15	1.16	0
127	SLU 5	22	0	2457	0.15	1.16	0
127	SLU 6	22	0	2457	0.15	1.16	0
127	SLU 7	22	0	2457	0.15	1.16	0
127	SLU 8	22	0	2457	0.15	1.16	0
127	SLU 9	22	0	2457	0.15	1.16	0
127	SLU 10	42	0	2891	0.2	2.02	0
127	SLU 11	42	0	2891	0.2	2.02	0
127	SLU 12	42	0	2891	0.2	2.02	0
127	SLU 13	42	0	2891	0.2	2.02	0
127	SLU 14	42	0	2891	0.2	2.02	0
127	SLU 15	42	0	2891	0.2	2.02	0
127	SLU 16	42	0	2891	0.2	2.02	0
127	SLU 17	42	0	2891	0.2	2.02	0
127	SLU 18	50	0	3076	0.22	2.39	0
127	SLU 19	50	0	3076	0.22	2.39	0
127	SLU 20	50	0	3076	0.22	2.39	0
127	SLU 21	50	0	3076	0.22	2.39	0
127	SLU 22	32	0	2758	0.19	1.65	0
127	SLU 23	32	0	2758	0.19	1.65	0
127	SLU 24	32	0	2758	0.19	1.65	0
127	SLU 25	32	0	2758	0.19	1.65	0
127	SLU 26	32	0	2758	0.19	1.65	0
127	SLU 27	32	0	2758	0.19	1.65	0
127	SLU 28	32	0	2758	0.19	1.65	0
127	SLU 29	32	0	2758	0.19	1.65	0
127	SLU 30	32	0	2758	0.19	1.65	0
127	SLU 31	52	0	3191	0.24	2.5	0
127	SLU 32	52	0	3191	0.24	2.5	0
127	SLU 33	52	0	3191	0.24	2.5	0
127	SLU 34	52	0	3191	0.24	2.5	0
127	SLU 35	52	0	3191	0.24	2.5	0
127	SLU 36	52	0	3191	0.24	2.5	0
127	SLU 37	52	0	3191	0.24	2.5	0
127	SLU 38	52	0	3191	0.24	2.5	0
127	SLU 39	61	0	3377	0.26	2.87	0
127	SLU 40	61	0	3377	0.26	2.87	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
127	SLU 41	61	0	3377	0.26	2.87	0
127	SLU 42	61	0	3377	0.26	2.87	0
127	SLU 43	25	0	3091	0.19	1.35	0
127	SLU 44	25	0	3091	0.19	1.35	0
127	SLU 45	25	0	3091	0.19	1.35	0
127	SLU 46	25	0	3091	0.19	1.35	0
127	SLU 47	25	0	3091	0.19	1.35	0
127	SLU 48	25	0	3091	0.19	1.35	0
127	SLU 49	25	0	3091	0.19	1.35	0
127	SLU 50	25	0	3091	0.19	1.35	0
127	SLU 51	25	0	3091	0.19	1.35	0
127	SLU 52	45	0	3525	0.24	2.21	0
127	SLU 53	45	0	3525	0.24	2.21	0
127	SLU 54	45	0	3525	0.24	2.21	0
127	SLU 55	45	0	3525	0.24	2.21	0
127	SLU 56	45	0	3525	0.24	2.21	0
127	SLU 57	45	0	3525	0.24	2.21	0
127	SLU 58	45	0	3525	0.24	2.21	0
127	SLU 59	45	0	3525	0.24	2.21	0
127	SLU 60	53	0	3710	0.26	2.57	0
127	SLU 61	53	0	3710	0.26	2.57	0
127	SLU 62	53	0	3710	0.26	2.57	0
127	SLU 63	53	0	3710	0.26	2.57	0
127	SLU 64	35	0	3392	0.22	1.83	0
127	SLU 65	35	0	3392	0.22	1.83	0
127	SLU 66	35	0	3392	0.22	1.83	0
127	SLU 67	35	0	3392	0.22	1.83	0
127	SLU 68	35	0	3392	0.22	1.83	0
127	SLU 69	35	0	3392	0.22	1.83	0
127	SLU 70	35	0	3392	0.22	1.83	0
127	SLU 71	35	0	3392	0.22	1.83	0
127	SLU 72	35	0	3392	0.22	1.83	0
127	SLU 73	55	0	3825	0.27	2.69	0
127	SLU 74	55	0	3825	0.27	2.69	0
127	SLU 75	55	0	3825	0.27	2.69	0
127	SLU 76	55	0	3825	0.27	2.69	0
127	SLU 77	55	0	3825	0.27	2.69	0
127	SLU 78	55	0	3825	0.27	2.69	0
127	SLU 79	55	0	3825	0.27	2.69	0
127	SLU 80	55	0	3825	0.27	2.69	0
127	SLU 81	64	0	4011	0.29	3.06	0
127	SLU 82	64	0	4011	0.29	3.06	0
127	SLU 83	64	0	4011	0.29	3.06	0
127	SLU 84	64	0	4011	0.29	3.06	0
127	SLE RA 1	25	0	2543	0.16	1.3	0
127	SLE RA 2	25	0	2543	0.16	1.3	0
127	SLE RA 3	25	0	2543	0.16	1.3	0
127	SLE RA 4	25	0	2543	0.16	1.3	0
127	SLE RA 5	25	0	2543	0.16	1.3	0
127	SLE RA 6	25	0	2543	0.16	1.3	0
127	SLE RA 7	25	0	2543	0.16	1.3	0
127	SLE RA 8	25	0	2543	0.16	1.3	0
127	SLE RA 9	25	0	2543	0.16	1.3	0
127	SLE RA 10	38	0	2832	0.2	1.87	0
127	SLE RA 11	38	0	2832	0.2	1.87	0
127	SLE RA 12	38	0	2832	0.2	1.87	0
127	SLE RA 13	38	0	2832	0.2	1.87	0
127	SLE RA 14	38	0	2832	0.2	1.87	0
127	SLE RA 15	38	0	2832	0.2	1.87	0
127	SLE RA 16	38	0	2832	0.2	1.87	0
127	SLE RA 17	38	0	2832	0.2	1.87	0
127	SLE RA 18	44	0	2956	0.21	2.12	0
127	SLE RA 19	44	0	2956	0.21	2.12	0
127	SLE RA 20	44	0	2956	0.21	2.12	0
127	SLE RA 21	44	0	2956	0.21	2.12	0
127	SLE FR 1	25	0	2543	0.16	1.3	0
127	SLE FR 2	25	0	2543	0.16	1.3	0
127	SLE FR 3	25	0	2543	0.16	1.3	0
127	SLE FR 4	31	0	2667	0.18	1.55	0
127	SLE FR 5	31	0	2667	0.18	1.55	0
127	SLE FR 6	34	0	2749	0.19	1.71	0
127	SLE QP 1	25	0	2543	0.16	1.3	0
127	SLE QP 2	31	0	2667	0.18	1.55	0
127	SLD 1	277	-3	2418	-7.44	13.1	-0.06
127	SLD 2	277	-3	2418	-7.44	13.1	-0.06
127	SLD 3	320	-22	2547	33.22	15	-0.28
127	SLD 4	320	-22	2547	33.22	15	-0.28
127	SLD 5	40	28	2397	-63.78	2.13	0.32
127	SLD 6	40	28	2397	-63.78	2.13	0.32
127	SLD 7	182	-36	2826	71.76	8.47	-0.42
127	SLD 8	182	-36	2826	71.76	8.47	-0.42
127	SLD 9	-121	35	2508	-71.41	-5.37	0.42
127	SLD 10	-121	35	2508	-71.41	-5.37	0.42
127	SLD 11	21	-28	2937	64.14	0.96	-0.32
127	SLD 12	21	-28	2937	64.14	0.96	-0.32
127	SLD 13	-259	22	2787	-32.87	-11.9	0.28
127	SLD 14	-259	22	2787	-32.87	-11.9	0.28
127	SLD 15	-216	3	2916	7.8	-10	0.06
127	SLD 16	-216	3	2916	7.8	-10	0.06



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
127	SLV 1	610	-9	2034	-19.45	28.69	-0.14
127	SLV 2	610	-9	2034	-19.45	28.69	-0.14
127	SLV 3	716	-56	2363	84.56	33.36	-0.69
127	SLV 4	716	-56	2363	84.56	33.36	-0.69
127	SLV 5	45	69	1979	-163.46	2.61	0.78
127	SLV 6	45	69	1979	-163.46	2.61	0.78
127	SLV 7	396	-88	3074	183.25	18.18	-1.03
127	SLV 8	396	-88	3074	183.25	18.18	-1.03
127	SLV 9	-335	88	2260	-182.89	-15.08	1.03
127	SLV 10	-335	88	2260	-182.89	-15.08	1.03
127	SLV 11	16	-69	3355	163.82	0.49	-0.79
127	SLV 12	16	-69	3355	163.82	0.49	-0.79
127	SLV 13	-655	56	2971	-84.2	-30.27	0.69
127	SLV 14	-655	56	2971	-84.2	-30.27	0.69
127	SLV 15	-549	9	3299	19.81	-25.6	0.14
127	SLV 16	-549	9	3299	19.81	-25.6	0.14
128	SLU 1	-32	0	2513	0.11	-2.6	0
128	SLU 2	-32	0	2513	0.11	-2.6	0
128	SLU 3	-32	0	2513	0.11	-2.6	0
128	SLU 4	-32	0	2513	0.11	-2.6	0
128	SLU 5	-32	0	2513	0.11	-2.6	0
128	SLU 6	-32	0	2513	0.11	-2.6	0
128	SLU 7	-32	0	2513	0.11	-2.6	0
128	SLU 8	-32	0	2513	0.11	-2.6	0
128	SLU 9	-32	0	2513	0.11	-2.6	0
128	SLU 10	-22	0	2972	0.14	-2.58	0
128	SLU 11	-22	0	2972	0.14	-2.58	0
128	SLU 12	-22	0	2972	0.14	-2.58	0
128	SLU 13	-22	0	2972	0.14	-2.58	0
128	SLU 14	-22	0	2972	0.14	-2.58	0
128	SLU 15	-22	0	2972	0.14	-2.58	0
128	SLU 16	-22	0	2972	0.14	-2.58	0
128	SLU 17	-22	0	2972	0.14	-2.58	0
128	SLU 18	-18	0	3169	0.15	-2.57	0
128	SLU 19	-18	0	3169	0.15	-2.57	0
128	SLU 20	-18	0	3169	0.15	-2.57	0
128	SLU 21	-18	0	3169	0.15	-2.57	0
128	SLU 22	-28	0	2826	0.14	-2.67	0
128	SLU 23	-28	0	2826	0.14	-2.67	0
128	SLU 24	-28	0	2826	0.14	-2.67	0
128	SLU 25	-28	0	2826	0.14	-2.67	0
128	SLU 26	-28	0	2826	0.14	-2.67	0
128	SLU 27	-28	0	2826	0.14	-2.67	0
128	SLU 28	-28	0	2826	0.14	-2.67	0
128	SLU 29	-28	0	2826	0.14	-2.67	0
128	SLU 30	-28	0	2826	0.14	-2.67	0
128	SLU 31	-19	0	3286	0.16	-2.65	0
128	SLU 32	-19	0	3286	0.16	-2.65	0
128	SLU 33	-19	0	3286	0.16	-2.65	0
128	SLU 34	-19	0	3286	0.16	-2.65	0
128	SLU 35	-19	0	3286	0.16	-2.65	0
128	SLU 36	-19	0	3286	0.16	-2.65	0
128	SLU 37	-19	0	3286	0.16	-2.65	0
128	SLU 38	-19	0	3286	0.16	-2.65	0
128	SLU 39	-15	0	3483	0.18	-2.63	0
128	SLU 40	-15	0	3483	0.18	-2.63	0
128	SLU 41	-15	0	3483	0.18	-2.63	0
128	SLU 42	-15	0	3483	0.18	-2.63	0
128	SLU 43	-42	0	3159	0.14	-3.36	0
128	SLU 44	-42	0	3159	0.14	-3.36	0
128	SLU 45	-42	0	3159	0.14	-3.36	0
128	SLU 46	-42	0	3159	0.14	-3.36	0
128	SLU 47	-42	0	3159	0.14	-3.36	0
128	SLU 48	-42	0	3159	0.14	-3.36	0
128	SLU 49	-42	0	3159	0.14	-3.36	0
128	SLU 50	-42	0	3159	0.14	-3.36	0
128	SLU 51	-42	0	3159	0.14	-3.36	0
128	SLU 52	-33	0	3619	0.17	-3.34	0
128	SLU 53	-33	0	3619	0.17	-3.34	0
128	SLU 54	-33	0	3619	0.17	-3.34	0
128	SLU 55	-33	0	3619	0.17	-3.34	0
128	SLU 56	-33	0	3619	0.17	-3.34	0
128	SLU 57	-33	0	3619	0.17	-3.34	0
128	SLU 58	-33	0	3619	0.17	-3.34	0
128	SLU 59	-33	0	3619	0.17	-3.34	0
128	SLU 60	-29	0	3816	0.18	-3.33	0
128	SLU 61	-29	0	3816	0.18	-3.33	0
128	SLU 62	-29	0	3816	0.18	-3.33	0
128	SLU 63	-29	0	3816	0.18	-3.33	0
128	SLU 64	-39	0	3473	0.16	-3.43	0
128	SLU 65	-39	0	3473	0.16	-3.43	0
128	SLU 66	-39	0	3473	0.16	-3.43	0
128	SLU 67	-39	0	3473	0.16	-3.43	0
128	SLU 68	-39	0	3473	0.16	-3.43	0
128	SLU 69	-39	0	3473	0.16	-3.43	0
128	SLU 70	-39	0	3473	0.16	-3.43	0
128	SLU 71	-39	0	3473	0.16	-3.43	0
128	SLU 72	-39	0	3473	0.16	-3.43	0
128	SLU 73	-30	0	3932	0.19	-3.4	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
128	SLU 74	-30	0	3932	0.19	-3.4	0
128	SLU 75	-30	0	3932	0.19	-3.4	0
128	SLU 76	-30	0	3932	0.19	-3.4	0
128	SLU 77	-30	0	3932	0.19	-3.4	0
128	SLU 78	-30	0	3932	0.19	-3.4	0
128	SLU 79	-30	0	3932	0.19	-3.4	0
128	SLU 80	-30	0	3932	0.19	-3.4	0
128	SLU 81	-26	0	4129	0.2	-3.39	0
128	SLU 82	-26	0	4129	0.2	-3.39	0
128	SLU 83	-26	0	4129	0.2	-3.39	0
128	SLU 84	-26	0	4129	0.2	-3.39	0
128	SLE RA 1	-31	0	2602	0.12	-2.62	0
128	SLE RA 2	-31	0	2602	0.12	-2.62	0
128	SLE RA 3	-31	0	2602	0.12	-2.62	0
128	SLE RA 4	-31	0	2602	0.12	-2.62	0
128	SLE RA 5	-31	0	2602	0.12	-2.62	0
128	SLE RA 6	-31	0	2602	0.12	-2.62	0
128	SLE RA 7	-31	0	2602	0.12	-2.62	0
128	SLE RA 8	-31	0	2602	0.12	-2.62	0
128	SLE RA 9	-31	0	2602	0.12	-2.62	0
128	SLE RA 10	-24	0	2909	0.14	-2.61	0
128	SLE RA 11	-24	0	2909	0.14	-2.61	0
128	SLE RA 12	-24	0	2909	0.14	-2.61	0
128	SLE RA 13	-24	0	2909	0.14	-2.61	0
128	SLE RA 14	-24	0	2909	0.14	-2.61	0
128	SLE RA 15	-24	0	2909	0.14	-2.61	0
128	SLE RA 16	-24	0	2909	0.14	-2.61	0
128	SLE RA 17	-24	0	2909	0.14	-2.61	0
128	SLE RA 18	-22	0	3040	0.15	-2.6	0
128	SLE RA 19	-22	0	3040	0.15	-2.6	0
128	SLE RA 20	-22	0	3040	0.15	-2.6	0
128	SLE RA 21	-22	0	3040	0.15	-2.6	0
128	SLE FR 1	-31	0	2602	0.12	-2.62	0
128	SLE FR 2	-31	0	2602	0.12	-2.62	0
128	SLE FR 3	-31	0	2602	0.12	-2.62	0
128	SLE FR 4	-28	0	2734	0.13	-2.61	0
128	SLE FR 5	-28	0	2734	0.13	-2.61	0
128	SLE FR 6	-26	0	2821	0.13	-2.61	0
128	SLE QP 1	-31	0	2602	0.12	-2.62	0
128	SLE QP 2	-28	0	2734	0.13	-2.61	0
128	SLD 1	208	-4	2479	-15	7.87	-0.6
128	SLD 2	208	-4	2479	-15	7.87	-0.6
128	SLD 3	249	-17	2610	39.18	9.6	1.24
128	SLD 4	249	-17	2610	39.18	9.6	1.24
128	SLD 5	-20	18	2460	-86.57	-2.09	-2.98
128	SLD 6	-20	18	2460	-86.57	-2.09	-2.98
128	SLD 7	117	-24	2894	94	3.67	3.17
128	SLD 8	117	-24	2894	94	3.67	3.17
128	SLD 9	-173	24	2573	-93.75	-8.9	-3.17
128	SLD 10	-173	24	2573	-93.75	-8.9	-3.17
128	SLD 11	-37	-18	3008	86.82	-3.14	2.97
128	SLD 12	-37	-18	3008	86.82	-3.14	2.97
128	SLD 13	-305	16	2858	-38.92	-14.83	-1.25
128	SLD 14	-305	16	2858	-38.92	-14.83	-1.25
128	SLD 15	-264	4	2988	15.25	-13.1	0.6
128	SLD 16	-264	4	2988	15.25	-13.1	0.6
128	SLV 1	526	-10	2102	-38.72	22.02	-1.54
128	SLV 2	526	-10	2102	-38.72	22.02	-1.54
128	SLV 3	628	-42	2435	100.14	26.28	3.19
128	SLV 4	628	-42	2435	100.14	26.28	3.19
128	SLV 5	-16	45	2039	-222.13	-1.68	-7.63
128	SLV 6	-16	45	2039	-222.13	-1.68	-7.63
128	SLV 7	323	-60	3149	240.73	12.5	8.12
128	SLV 8	323	-60	3149	240.73	12.5	8.12
128	SLV 9	-379	60	2318	-240.48	-17.73	-8.13
128	SLV 10	-379	60	2318	-240.48	-17.73	-8.13
128	SLV 11	-41	-45	3428	222.39	-3.55	7.63
128	SLV 12	-41	-45	3428	222.39	-3.55	7.63
128	SLV 13	-684	41	3032	-99.88	-31.51	-3.19
128	SLV 14	-684	41	3032	-99.88	-31.51	-3.19
128	SLV 15	-582	10	3365	38.98	-27.25	1.54
128	SLV 16	-582	10	3365	38.98	-27.25	1.54
129	SLU 1	-146	0	2502	0.08	-12.67	0
129	SLU 2	-146	0	2502	0.08	-12.67	0
129	SLU 3	-146	0	2502	0.08	-12.67	0
129	SLU 4	-146	0	2502	0.08	-12.67	0
129	SLU 5	-146	0	2502	0.08	-12.67	0
129	SLU 6	-146	0	2502	0.08	-12.67	0
129	SLU 7	-146	0	2502	0.08	-12.67	0
129	SLU 8	-146	0	2502	0.08	-12.67	0
129	SLU 9	-146	0	2502	0.08	-12.67	0
129	SLU 10	-159	0	2970	0.02	-14.42	0.01
129	SLU 11	-159	0	2970	0.02	-14.42	0.01
129	SLU 12	-159	0	2970	0.02	-14.42	0.01
129	SLU 13	-159	0	2970	0.02	-14.42	0.01
129	SLU 14	-159	0	2970	0.02	-14.42	0.01
129	SLU 15	-159	0	2970	0.02	-14.42	0.01
129	SLU 16	-159	0	2970	0.02	-14.42	0.01
129	SLU 17	-159	0	2970	0.02	-14.42	0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
129	SLU 18	-165	0	3170	-0.01	-15.17	0.01
129	SLU 19	-165	0	3170	-0.01	-15.17	0.01
129	SLU 20	-165	0	3170	-0.01	-15.17	0.01
129	SLU 21	-165	0	3170	-0.01	-15.17	0.01
129	SLU 22	-158	0	2817	0.07	-13.97	0.01
129	SLU 23	-158	0	2817	0.07	-13.97	0.01
129	SLU 24	-158	0	2817	0.07	-13.97	0.01
129	SLU 25	-158	0	2817	0.07	-13.97	0.01
129	SLU 26	-158	0	2817	0.07	-13.97	0.01
129	SLU 27	-158	0	2817	0.07	-13.97	0.01
129	SLU 28	-158	0	2817	0.07	-13.97	0.01
129	SLU 29	-158	0	2817	0.07	-13.97	0.01
129	SLU 30	-158	0	2817	0.07	-13.97	0.01
129	SLU 31	-171	0	3284	0.01	-15.72	0.01
129	SLU 32	-171	0	3284	0.01	-15.72	0.01
129	SLU 33	-171	0	3284	0.01	-15.72	0.01
129	SLU 34	-171	0	3284	0.01	-15.72	0.01
129	SLU 35	-171	0	3284	0.01	-15.72	0.01
129	SLU 36	-171	0	3284	0.01	-15.72	0.01
129	SLU 37	-171	0	3284	0.01	-15.72	0.01
129	SLU 38	-171	0	3284	0.01	-15.72	0.01
129	SLU 39	-177	0	3484	-0.02	-16.47	0.02
129	SLU 40	-177	0	3484	-0.02	-16.47	0.02
129	SLU 41	-177	0	3484	-0.02	-16.47	0.02
129	SLU 42	-177	0	3484	-0.02	-16.47	0.02
129	SLU 43	-186	0	3145	0.11	-16.02	0
129	SLU 44	-186	0	3145	0.11	-16.02	0
129	SLU 45	-186	0	3145	0.11	-16.02	0
129	SLU 46	-186	0	3145	0.11	-16.02	0
129	SLU 47	-186	0	3145	0.11	-16.02	0
129	SLU 48	-186	0	3145	0.11	-16.02	0
129	SLU 49	-186	0	3145	0.11	-16.02	0
129	SLU 50	-186	0	3145	0.11	-16.02	0
129	SLU 51	-186	0	3145	0.11	-16.02	0
129	SLU 52	-199	0	3612	0.04	-17.77	0.01
129	SLU 53	-199	0	3612	0.04	-17.77	0.01
129	SLU 54	-199	0	3612	0.04	-17.77	0.01
129	SLU 55	-199	0	3612	0.04	-17.77	0.01
129	SLU 56	-199	0	3612	0.04	-17.77	0.01
129	SLU 57	-199	0	3612	0.04	-17.77	0.01
129	SLU 58	-199	0	3612	0.04	-17.77	0.01
129	SLU 59	-199	0	3612	0.04	-17.77	0.01
129	SLU 60	-205	0	3813	0.02	-18.52	0.01
129	SLU 61	-205	0	3813	0.02	-18.52	0.01
129	SLU 62	-205	0	3813	0.02	-18.52	0.01
129	SLU 63	-205	0	3813	0.02	-18.52	0.01
129	SLU 64	-198	0	3460	0.1	-17.32	0
129	SLU 65	-198	0	3460	0.1	-17.32	0
129	SLU 66	-198	0	3460	0.1	-17.32	0
129	SLU 67	-198	0	3460	0.1	-17.32	0
129	SLU 68	-198	0	3460	0.1	-17.32	0
129	SLU 69	-198	0	3460	0.1	-17.32	0
129	SLU 70	-198	0	3460	0.1	-17.32	0
129	SLU 71	-198	0	3460	0.1	-17.32	0
129	SLU 72	-198	0	3460	0.1	-17.32	0
129	SLU 73	-211	0	3927	0.03	-19.07	0.01
129	SLU 74	-211	0	3927	0.03	-19.07	0.01
129	SLU 75	-211	0	3927	0.03	-19.07	0.01
129	SLU 76	-211	0	3927	0.03	-19.07	0.01
129	SLU 77	-211	0	3927	0.03	-19.07	0.01
129	SLU 78	-211	0	3927	0.03	-19.07	0.01
129	SLU 79	-211	0	3927	0.03	-19.07	0.01
129	SLU 80	-211	0	3927	0.03	-19.07	0.01
129	SLU 81	-217	0	4127	0.01	-19.82	0.02
129	SLU 82	-217	0	4127	0.01	-19.82	0.02
129	SLU 83	-217	0	4127	0.01	-19.82	0.02
129	SLU 84	-217	0	4127	0.01	-19.82	0.02
129	SLE RA 1	-150	0	2592	0.08	-13.04	0
129	SLE RA 2	-150	0	2592	0.08	-13.04	0
129	SLE RA 3	-150	0	2592	0.08	-13.04	0
129	SLE RA 4	-150	0	2592	0.08	-13.04	0
129	SLE RA 5	-150	0	2592	0.08	-13.04	0
129	SLE RA 6	-150	0	2592	0.08	-13.04	0
129	SLE RA 7	-150	0	2592	0.08	-13.04	0
129	SLE RA 8	-150	0	2592	0.08	-13.04	0
129	SLE RA 9	-150	0	2592	0.08	-13.04	0
129	SLE RA 10	-158	0	2904	0.04	-14.21	0.01
129	SLE RA 11	-158	0	2904	0.04	-14.21	0.01
129	SLE RA 12	-158	0	2904	0.04	-14.21	0.01
129	SLE RA 13	-158	0	2904	0.04	-14.21	0.01
129	SLE RA 14	-158	0	2904	0.04	-14.21	0.01
129	SLE RA 15	-158	0	2904	0.04	-14.21	0.01
129	SLE RA 16	-158	0	2904	0.04	-14.21	0.01
129	SLE RA 17	-158	0	2904	0.04	-14.21	0.01
129	SLE RA 18	-162	0	3037	0.02	-14.71	0.01
129	SLE RA 19	-162	0	3037	0.02	-14.71	0.01
129	SLE RA 20	-162	0	3037	0.02	-14.71	0.01
129	SLE RA 21	-162	0	3037	0.02	-14.71	0.01
129	SLE FR 1	-150	0	2592	0.08	-13.04	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
129	SLE FR 2	-150	0	2592	0.08	-13.04	0
129	SLE FR 3	-150	0	2592	0.08	-13.04	0
129	SLE FR 4	-153	0	2726	0.06	-13.54	0.01
129	SLE FR 5	-153	0	2726	0.06	-13.54	0.01
129	SLE FR 6	-156	0	2815	0.05	-13.87	0.01
129	SLE QP 1	-150	0	2592	0.08	-13.04	0
129	SLE QP 2	-153	0	2726	0.06	-13.54	0.01
129	SLD 1	-7	67	2366	-49.49	-0.59	2.16
129	SLD 2	-7	67	2366	-49.49	-0.59	2.16
129	SLD 3	19	-128	2496	96.71	1.25	-1.02
129	SLD 4	19	-128	2496	96.71	1.25	-1.02
129	SLD 5	-149	315	2421	-236.54	-12.44	5.48
129	SLD 6	-149	315	2421	-236.54	-12.44	5.48
129	SLD 7	-62	-333	2854	250.79	-6.31	-5.13
129	SLD 8	-62	-333	2854	250.79	-6.31	-5.13
129	SLD 9	-245	333	2598	-250.67	-20.77	5.14
129	SLD 10	-245	333	2598	-250.67	-20.77	5.14
129	SLD 11	-158	-315	3030	236.66	-14.63	-5.47
129	SLD 12	-158	-315	3030	236.66	-14.63	-5.47
129	SLD 13	-326	128	2955	-96.59	-28.33	1.03
129	SLD 14	-326	128	2955	-96.59	-28.33	1.03
129	SLD 15	-300	-67	3085	49.61	-26.49	-2.15
129	SLD 16	-300	-67	3085	49.61	-26.49	-2.15
129	SLV 1	192	172	1860	-127.07	16.94	5.52
129	SLV 2	192	172	1860	-127.07	16.94	5.52
129	SLV 3	256	-327	2190	247.97	21.4	-2.63
129	SLV 4	256	-327	2190	247.97	21.4	-2.63
129	SLV 5	-147	809	1965	-606.9	-11.15	14.03
129	SLV 6	-147	809	1965	-606.9	-11.15	14.03
129	SLV 7	67	-855	3066	643.26	3.7	-13.16
129	SLV 8	67	-855	3066	643.26	3.7	-13.16
129	SLV 9	-374	855	2385	-643.14	-30.77	13.17
129	SLV 10	-374	855	2385	-643.14	-30.77	13.17
129	SLV 11	-160	-808	3487	607.02	-15.93	-14.02
129	SLV 12	-160	-808	3487	607.02	-15.93	-14.02
129	SLV 13	-563	327	3261	-247.85	-48.48	2.64
129	SLV 14	-563	327	3261	-247.85	-48.48	2.64
129	SLV 15	-499	-172	3591	127.19	-44.02	-5.51
129	SLV 16	-499	-172	3591	127.19	-44.02	-5.51
130	SLU 1	-517	0	2056	0.09	-48.24	0.01
130	SLU 2	-517	0	2056	0.09	-48.24	0.01
130	SLU 3	-517	0	2056	0.09	-48.24	0.01
130	SLU 4	-517	0	2056	0.09	-48.24	0.01
130	SLU 5	-517	0	2056	0.09	-48.24	0.01
130	SLU 6	-517	0	2056	0.09	-48.24	0.01
130	SLU 7	-517	0	2056	0.09	-48.24	0.01
130	SLU 8	-517	0	2056	0.09	-48.24	0.01
130	SLU 9	-517	0	2056	0.09	-48.24	0.01
130	SLU 10	-614	1	2454	-0.05	-57.45	0.01
130	SLU 11	-614	1	2454	-0.05	-57.45	0.01
130	SLU 12	-614	1	2454	-0.05	-57.45	0.01
130	SLU 13	-614	1	2454	-0.05	-57.45	0.01
130	SLU 14	-614	1	2454	-0.05	-57.45	0.01
130	SLU 15	-614	1	2454	-0.05	-57.45	0.01
130	SLU 16	-614	1	2454	-0.05	-57.45	0.01
130	SLU 17	-614	1	2454	-0.05	-57.45	0.01
130	SLU 18	-656	1	2625	-0.11	-61.4	0.01
130	SLU 19	-656	1	2625	-0.11	-61.4	0.01
130	SLU 20	-656	1	2625	-0.11	-61.4	0.01
130	SLU 21	-656	1	2625	-0.11	-61.4	0.01
130	SLU 22	-582	0	2320	0.06	-54.38	0.01
130	SLU 23	-582	0	2320	0.06	-54.38	0.01
130	SLU 24	-582	0	2320	0.06	-54.38	0.01
130	SLU 25	-582	0	2320	0.06	-54.38	0.01
130	SLU 26	-582	0	2320	0.06	-54.38	0.01
130	SLU 27	-582	0	2320	0.06	-54.38	0.01
130	SLU 28	-582	0	2320	0.06	-54.38	0.01
130	SLU 29	-582	0	2320	0.06	-54.38	0.01
130	SLU 30	-582	0	2320	0.06	-54.38	0.01
130	SLU 31	-679	1	2719	-0.08	-63.59	0.01
130	SLU 32	-679	1	2719	-0.08	-63.59	0.01
130	SLU 33	-679	1	2719	-0.08	-63.59	0.01
130	SLU 34	-679	1	2719	-0.08	-63.59	0.01
130	SLU 35	-679	1	2719	-0.08	-63.59	0.01
130	SLU 36	-679	1	2719	-0.08	-63.59	0.01
130	SLU 37	-679	1	2719	-0.08	-63.59	0.01
130	SLU 38	-679	1	2719	-0.08	-63.59	0.01
130	SLU 39	-721	1	2890	-0.14	-67.54	0.01
130	SLU 40	-721	1	2890	-0.14	-67.54	0.01
130	SLU 41	-721	1	2890	-0.14	-67.54	0.01
130	SLU 42	-721	1	2890	-0.14	-67.54	0.01
130	SLU 43	-649	0	2582	0.13	-60.61	0.01
130	SLU 44	-649	0	2582	0.13	-60.61	0.01
130	SLU 45	-649	0	2582	0.13	-60.61	0.01
130	SLU 46	-649	0	2582	0.13	-60.61	0.01
130	SLU 47	-649	0	2582	0.13	-60.61	0.01
130	SLU 48	-649	0	2582	0.13	-60.61	0.01
130	SLU 49	-649	0	2582	0.13	-60.61	0.01
130	SLU 50	-649	0	2582	0.13	-60.61	0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
130	SLU 51	-649	0	2582	0.13	-60.61	0.01
130	SLU 52	-747	1	2980	-0.01	-69.82	0.01
130	SLU 53	-747	1	2980	-0.01	-69.82	0.01
130	SLU 54	-747	1	2980	-0.01	-69.82	0.01
130	SLU 55	-747	1	2980	-0.01	-69.82	0.01
130	SLU 56	-747	1	2980	-0.01	-69.82	0.01
130	SLU 57	-747	1	2980	-0.01	-69.82	0.01
130	SLU 58	-747	1	2980	-0.01	-69.82	0.01
130	SLU 59	-747	1	2980	-0.01	-69.82	0.01
130	SLU 60	-789	1	3151	-0.07	-73.76	0.01
130	SLU 61	-789	1	3151	-0.07	-73.76	0.01
130	SLU 62	-789	1	3151	-0.07	-73.76	0.01
130	SLU 63	-789	1	3151	-0.07	-73.76	0.01
130	SLU 64	-714	0	2846	0.1	-66.75	0.01
130	SLU 65	-714	0	2846	0.1	-66.75	0.01
130	SLU 66	-714	0	2846	0.1	-66.75	0.01
130	SLU 67	-714	0	2846	0.1	-66.75	0.01
130	SLU 68	-714	0	2846	0.1	-66.75	0.01
130	SLU 69	-714	0	2846	0.1	-66.75	0.01
130	SLU 70	-714	0	2846	0.1	-66.75	0.01
130	SLU 71	-714	0	2846	0.1	-66.75	0.01
130	SLU 72	-714	0	2846	0.1	-66.75	0.01
130	SLU 73	-812	1	3245	-0.04	-75.96	0.01
130	SLU 74	-812	1	3245	-0.04	-75.96	0.01
130	SLU 75	-812	1	3245	-0.04	-75.96	0.01
130	SLU 76	-812	1	3245	-0.04	-75.96	0.01
130	SLU 77	-812	1	3245	-0.04	-75.96	0.01
130	SLU 78	-812	1	3245	-0.04	-75.96	0.01
130	SLU 79	-812	1	3245	-0.04	-75.96	0.01
130	SLU 80	-812	1	3245	-0.04	-75.96	0.01
130	SLU 81	-854	1	3416	-0.1	-79.9	0.01
130	SLU 82	-854	1	3416	-0.1	-79.9	0.01
130	SLU 83	-854	1	3416	-0.1	-79.9	0.01
130	SLU 84	-854	1	3416	-0.1	-79.9	0.01
130	SLE RA 1	-535	0	2131	0.08	-50	0.01
130	SLE RA 2	-535	0	2131	0.08	-50	0.01
130	SLE RA 3	-535	0	2131	0.08	-50	0.01
130	SLE RA 4	-535	0	2131	0.08	-50	0.01
130	SLE RA 5	-535	0	2131	0.08	-50	0.01
130	SLE RA 6	-535	0	2131	0.08	-50	0.01
130	SLE RA 7	-535	0	2131	0.08	-50	0.01
130	SLE RA 8	-535	0	2131	0.08	-50	0.01
130	SLE RA 9	-535	0	2131	0.08	-50	0.01
130	SLE RA 10	-600	0	2397	-0.01	-56.14	0.01
130	SLE RA 11	-600	0	2397	-0.01	-56.14	0.01
130	SLE RA 12	-600	0	2397	-0.01	-56.14	0.01
130	SLE RA 13	-600	0	2397	-0.01	-56.14	0.01
130	SLE RA 14	-600	0	2397	-0.01	-56.14	0.01
130	SLE RA 15	-600	0	2397	-0.01	-56.14	0.01
130	SLE RA 16	-600	0	2397	-0.01	-56.14	0.01
130	SLE RA 17	-600	0	2397	-0.01	-56.14	0.01
130	SLE RA 18	-628	1	2511	-0.05	-58.77	0.01
130	SLE RA 19	-628	1	2511	-0.05	-58.77	0.01
130	SLE RA 20	-628	1	2511	-0.05	-58.77	0.01
130	SLE RA 21	-628	1	2511	-0.05	-58.77	0.01
130	SLE FR 1	-535	0	2131	0.08	-50	0.01
130	SLE FR 2	-535	0	2131	0.08	-50	0.01
130	SLE FR 3	-535	0	2131	0.08	-50	0.01
130	SLE FR 4	-563	0	2245	0.04	-52.63	0.01
130	SLE FR 5	-563	0	2245	0.04	-52.63	0.01
130	SLE FR 6	-582	0	2321	0.02	-54.38	0.01
130	SLE QP 1	-535	0	2131	0.08	-50	0.01
130	SLE QP 2	-563	0	2245	0.04	-52.63	0.01
130	SLD 1	-329	280	1653	-87.1	-34.91	-1.9
130	SLD 2	-329	280	1653	-87.1	-34.91	-1.9
130	SLD 3	-358	-528	1753	165.28	-37.69	0.94
130	SLD 4	-358	-528	1753	165.28	-37.69	0.94
130	SLD 5	-449	1311	1917	-408.88	-43.1	-4.87
130	SLD 6	-449	1311	1917	-408.88	-43.1	-4.87
130	SLD 7	-546	-1385	2248	432.4	-52.36	4.59
130	SLD 8	-546	-1385	2248	432.4	-52.36	4.59
130	SLD 9	-581	1385	2242	-432.31	-52.9	-4.57
130	SLD 10	-581	1385	2242	-432.31	-52.9	-4.57
130	SLD 11	-678	-1310	2573	408.97	-62.15	4.88
130	SLD 12	-678	-1310	2573	408.97	-62.15	4.88
130	SLD 13	-769	529	2737	-165.2	-67.56	-0.92
130	SLD 14	-769	529	2737	-165.2	-67.56	-0.92
130	SLD 15	-798	-280	2837	87.19	-70.34	1.91
130	SLD 16	-798	-280	2837	87.19	-70.34	1.91
130	SLV 1	-10	719	844	-223.54	-10.72	-4.88
130	SLV 2	-10	719	844	-223.54	-10.72	-4.88
130	SLV 3	-80	-1355	1090	423.95	-17.57	2.4
130	SLV 4	-80	-1355	1090	423.95	-17.57	2.4
130	SLV 5	-291	3362	1452	-1049.05	-29.67	-12.49
130	SLV 6	-291	3362	1452	-1049.05	-29.67	-12.49
130	SLV 7	-524	-3552	2272	1109.23	-52.5	11.76
130	SLV 8	-524	-3552	2272	1109.23	-52.5	11.76
130	SLV 9	-602	3553	2218	-1109.15	-52.76	-11.75
130	SLV 10	-602	3553	2218	-1109.15	-52.76	-11.75



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
130	SLV 11	-835	-3361	3038	1049.14	-75.59	12.51
130	SLV 12	-835	-3361	3038	1049.14	-75.59	12.51
130	SLV 13	-1047	1356	3400	-423.86	-87.69	-2.39
130	SLV 14	-1047	1356	3400	-423.86	-87.69	-2.39
130	SLV 15	-1116	-718	3646	223.62	-94.53	4.89
130	SLV 16	-1116	-718	3646	223.62	-94.53	4.89
132	SLU 1	476	0	1396	0.03	7.88	-0.01
132	SLU 2	476	0	1396	0.03	7.88	-0.01
132	SLU 3	476	0	1396	0.03	7.88	-0.01
132	SLU 4	476	0	1396	0.03	7.88	-0.01
132	SLU 5	476	0	1396	0.03	7.88	-0.01
132	SLU 6	476	0	1396	0.03	7.88	-0.01
132	SLU 7	476	0	1396	0.03	7.88	-0.01
132	SLU 8	476	0	1396	0.03	7.88	-0.01
132	SLU 9	476	0	1396	0.03	7.88	-0.01
132	SLU 10	556	0	1636	0.08	9.13	-0.02
132	SLU 11	556	0	1636	0.08	9.13	-0.02
132	SLU 12	556	0	1636	0.08	9.13	-0.02
132	SLU 13	556	0	1636	0.08	9.13	-0.02
132	SLU 14	556	0	1636	0.08	9.13	-0.02
132	SLU 15	556	0	1636	0.08	9.13	-0.02
132	SLU 16	556	0	1636	0.08	9.13	-0.02
132	SLU 17	556	0	1636	0.08	9.13	-0.02
132	SLU 18	591	0	1739	0.1	9.66	-0.02
132	SLU 19	591	0	1739	0.1	9.66	-0.02
132	SLU 20	591	0	1739	0.1	9.66	-0.02
132	SLU 21	591	0	1739	0.1	9.66	-0.02
132	SLU 22	534	0	1567	0.05	8.81	-0.01
132	SLU 23	534	0	1567	0.05	8.81	-0.01
132	SLU 24	534	0	1567	0.05	8.81	-0.01
132	SLU 25	534	0	1567	0.05	8.81	-0.01
132	SLU 26	534	0	1567	0.05	8.81	-0.01
132	SLU 27	534	0	1567	0.05	8.81	-0.01
132	SLU 28	534	0	1567	0.05	8.81	-0.01
132	SLU 29	534	0	1567	0.05	8.81	-0.01
132	SLU 30	534	0	1567	0.05	8.81	-0.01
132	SLU 31	614	0	1807	0.09	10.05	-0.02
132	SLU 32	614	0	1807	0.09	10.05	-0.02
132	SLU 33	614	0	1807	0.09	10.05	-0.02
132	SLU 34	614	0	1807	0.09	10.05	-0.02
132	SLU 35	614	0	1807	0.09	10.05	-0.02
132	SLU 36	614	0	1807	0.09	10.05	-0.02
132	SLU 37	614	0	1807	0.09	10.05	-0.02
132	SLU 38	614	0	1807	0.09	10.05	-0.02
132	SLU 39	649	0	1910	0.11	10.59	-0.02
132	SLU 40	649	0	1910	0.11	10.59	-0.02
132	SLU 41	649	0	1910	0.11	10.59	-0.02
132	SLU 42	649	0	1910	0.11	10.59	-0.02
132	SLU 43	599	0	1756	0.04	9.93	-0.01
132	SLU 44	599	0	1756	0.04	9.93	-0.01
132	SLU 45	599	0	1756	0.04	9.93	-0.01
132	SLU 46	599	0	1756	0.04	9.93	-0.01
132	SLU 47	599	0	1756	0.04	9.93	-0.01
132	SLU 48	599	0	1756	0.04	9.93	-0.01
132	SLU 49	599	0	1756	0.04	9.93	-0.01
132	SLU 50	599	0	1756	0.04	9.93	-0.01
132	SLU 51	599	0	1756	0.04	9.93	-0.01
132	SLU 52	679	0	1996	0.08	11.18	-0.02
132	SLU 53	679	0	1996	0.08	11.18	-0.02
132	SLU 54	679	0	1996	0.08	11.18	-0.02
132	SLU 55	679	0	1996	0.08	11.18	-0.02
132	SLU 56	679	0	1996	0.08	11.18	-0.02
132	SLU 57	679	0	1996	0.08	11.18	-0.02
132	SLU 58	679	0	1996	0.08	11.18	-0.02
132	SLU 59	679	0	1996	0.08	11.18	-0.02
132	SLU 60	714	0	2099	0.1	11.71	-0.02
132	SLU 61	714	0	2099	0.1	11.71	-0.02
132	SLU 62	714	0	2099	0.1	11.71	-0.02
132	SLU 63	714	0	2099	0.1	11.71	-0.02
132	SLU 64	657	0	1927	0.06	10.85	-0.01
132	SLU 65	657	0	1927	0.06	10.85	-0.01
132	SLU 66	657	0	1927	0.06	10.85	-0.01
132	SLU 67	657	0	1927	0.06	10.85	-0.01
132	SLU 68	657	0	1927	0.06	10.85	-0.01
132	SLU 69	657	0	1927	0.06	10.85	-0.01
132	SLU 70	657	0	1927	0.06	10.85	-0.01
132	SLU 71	657	0	1927	0.06	10.85	-0.01
132	SLU 72	657	0	1927	0.06	10.85	-0.01
132	SLU 73	737	0	2167	0.1	12.1	-0.02
132	SLU 74	737	0	2167	0.1	12.1	-0.02
132	SLU 75	737	0	2167	0.1	12.1	-0.02
132	SLU 76	737	0	2167	0.1	12.1	-0.02
132	SLU 77	737	0	2167	0.1	12.1	-0.02
132	SLU 78	737	0	2167	0.1	12.1	-0.02
132	SLU 79	737	0	2167	0.1	12.1	-0.02
132	SLU 80	737	0	2167	0.1	12.1	-0.02
132	SLU 81	772	0	2270	0.12	12.64	-0.02
132	SLU 82	772	0	2270	0.12	12.64	-0.02
132	SLU 83	772	0	2270	0.12	12.64	-0.02



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
132	SLU 84	772	0	2270	0.12	12.64	-0.02
132	SLE RA 1	493	0	1445	0.04	8.14	-0.01
132	SLE RA 2	493	0	1445	0.04	8.14	-0.01
132	SLE RA 3	493	0	1445	0.04	8.14	-0.01
132	SLE RA 4	493	0	1445	0.04	8.14	-0.01
132	SLE RA 5	493	0	1445	0.04	8.14	-0.01
132	SLE RA 6	493	0	1445	0.04	8.14	-0.01
132	SLE RA 7	493	0	1445	0.04	8.14	-0.01
132	SLE RA 8	493	0	1445	0.04	8.14	-0.01
132	SLE RA 9	493	0	1445	0.04	8.14	-0.01
132	SLE RA 10	546	0	1605	0.07	8.98	-0.01
132	SLE RA 11	546	0	1605	0.07	8.98	-0.01
132	SLE RA 12	546	0	1605	0.07	8.98	-0.01
132	SLE RA 13	546	0	1605	0.07	8.98	-0.01
132	SLE RA 14	546	0	1605	0.07	8.98	-0.01
132	SLE RA 15	546	0	1605	0.07	8.98	-0.01
132	SLE RA 16	546	0	1605	0.07	8.98	-0.01
132	SLE RA 17	546	0	1605	0.07	8.98	-0.01
132	SLE RA 18	569	0	1673	0.08	9.33	-0.02
132	SLE RA 19	569	0	1673	0.08	9.33	-0.02
132	SLE RA 20	569	0	1673	0.08	9.33	-0.02
132	SLE RA 21	569	0	1673	0.08	9.33	-0.02
132	SLE FR 1	493	0	1445	0.04	8.14	-0.01
132	SLE FR 2	493	0	1445	0.04	8.14	-0.01
132	SLE FR 3	493	0	1445	0.04	8.14	-0.01
132	SLE FR 4	516	0	1513	0.05	8.5	-0.01
132	SLE FR 5	516	0	1513	0.05	8.5	-0.01
132	SLE FR 6	531	0	1559	0.06	8.74	-0.01
132	SLE QP 1	493	0	1445	0.04	8.14	-0.01
132	SLE QP 2	516	0	1513	0.05	8.5	-0.01
132	SLD 1	723	28	1944	-18.96	13.7	3.54
132	SLD 2	723	28	1944	-18.96	13.7	3.54
132	SLD 3	752	7	2012	7.84	14.37	-1.53
132	SLD 4	752	7	2012	7.84	14.37	-1.53
132	SLD 5	534	40	1539	-46.31	9.05	8.74
132	SLD 6	534	40	1539	-46.31	9.05	8.74
132	SLD 7	631	-29	1766	43.05	11.27	-8.15
132	SLD 8	631	-29	1766	43.05	11.27	-8.15
132	SLD 9	401	30	1260	-42.94	5.73	8.13
132	SLD 10	401	30	1260	-42.94	5.73	8.13
132	SLD 11	498	-40	1487	46.41	7.95	-8.76
132	SLD 12	498	-40	1487	46.41	7.95	-8.76
132	SLD 13	279	-7	1014	-7.74	2.63	1.51
132	SLD 14	279	-7	1014	-7.74	2.63	1.51
132	SLD 15	308	-27	1083	19.07	3.3	-3.56
132	SLD 16	308	-27	1083	19.07	3.3	-3.56
132	SLV 1	1003	70	2526	-48.45	20.75	9.06
132	SLV 2	1003	70	2526	-48.45	20.75	9.06
132	SLV 3	1074	18	2694	20.26	22.36	-3.93
132	SLV 4	1074	18	2694	20.26	22.36	-3.93
132	SLV 5	554	102	1562	-118.71	9.72	22.42
132	SLV 6	554	102	1562	-118.71	9.72	22.42
132	SLV 7	791	-75	2122	110.32	15.11	-20.89
132	SLV 8	791	-75	2122	110.32	15.11	-20.89
132	SLV 9	240	75	904	-110.22	1.89	20.87
132	SLV 10	240	75	904	-110.22	1.89	20.87
132	SLV 11	477	-101	1464	118.81	7.28	-22.44
132	SLV 12	477	-101	1464	118.81	7.28	-22.44
132	SLV 13	-43	-17	333	-20.15	-5.36	3.91
132	SLV 14	-43	-17	333	-20.15	-5.36	3.91
132	SLV 15	28	-70	501	48.56	-3.74	-9.08
132	SLV 16	28	-70	501	48.56	-3.74	-9.08
133	SLU 1	136	0	2282	0.12	10.32	0
133	SLU 2	136	0	2282	0.12	10.32	0
133	SLU 3	136	0	2282	0.12	10.32	0
133	SLU 4	136	0	2282	0.12	10.32	0
133	SLU 5	136	0	2282	0.12	10.32	0
133	SLU 6	136	0	2282	0.12	10.32	0
133	SLU 7	136	0	2282	0.12	10.32	0
133	SLU 8	136	0	2282	0.12	10.32	0
133	SLU 9	136	0	2282	0.12	10.32	0
133	SLU 10	155	0	2685	0.24	11.71	0
133	SLU 11	155	0	2685	0.24	11.71	0
133	SLU 12	155	0	2685	0.24	11.71	0
133	SLU 13	155	0	2685	0.24	11.71	0
133	SLU 14	155	0	2685	0.24	11.71	0
133	SLU 15	155	0	2685	0.24	11.71	0
133	SLU 16	155	0	2685	0.24	11.71	0
133	SLU 17	155	0	2685	0.24	11.71	0
133	SLU 18	164	0	2858	0.3	12.3	0
133	SLU 19	164	0	2858	0.3	12.3	0
133	SLU 20	164	0	2858	0.3	12.3	0
133	SLU 21	164	0	2858	0.3	12.3	0
133	SLU 22	150	0	2561	0.17	11.41	0
133	SLU 23	150	0	2561	0.17	11.41	0
133	SLU 24	150	0	2561	0.17	11.41	0
133	SLU 25	150	0	2561	0.17	11.41	0
133	SLU 26	150	0	2561	0.17	11.41	0
133	SLU 27	150	0	2561	0.17	11.41	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
133	SLU 28	150	0	2561	0.17	11.41	0
133	SLU 29	150	0	2561	0.17	11.41	0
133	SLU 30	150	0	2561	0.17	11.41	0
133	SLU 31	169	0	2965	0.3	12.79	0
133	SLU 32	169	0	2965	0.3	12.79	0
133	SLU 33	169	0	2965	0.3	12.79	0
133	SLU 34	169	0	2965	0.3	12.79	0
133	SLU 35	169	0	2965	0.3	12.79	0
133	SLU 36	169	0	2965	0.3	12.79	0
133	SLU 37	169	0	2965	0.3	12.79	0
133	SLU 38	169	0	2965	0.3	12.79	0
133	SLU 39	177	0	3137	0.35	13.38	0
133	SLU 40	177	0	3137	0.35	13.38	0
133	SLU 41	177	0	3137	0.35	13.38	0
133	SLU 42	177	0	3137	0.35	13.38	0
133	SLU 43	172	0	2871	0.13	13.05	0
133	SLU 44	172	0	2871	0.13	13.05	0
133	SLU 45	172	0	2871	0.13	13.05	0
133	SLU 46	172	0	2871	0.13	13.05	0
133	SLU 47	172	0	2871	0.13	13.05	0
133	SLU 48	172	0	2871	0.13	13.05	0
133	SLU 49	172	0	2871	0.13	13.05	0
133	SLU 50	172	0	2871	0.13	13.05	0
133	SLU 51	172	0	2871	0.13	13.05	0
133	SLU 52	192	0	3274	0.26	14.43	0
133	SLU 53	192	0	3274	0.26	14.43	0
133	SLU 54	192	0	3274	0.26	14.43	0
133	SLU 55	192	0	3274	0.26	14.43	0
133	SLU 56	192	0	3274	0.26	14.43	0
133	SLU 57	192	0	3274	0.26	14.43	0
133	SLU 58	192	0	3274	0.26	14.43	0
133	SLU 59	192	0	3274	0.26	14.43	0
133	SLU 60	200	0	3447	0.32	15.02	0
133	SLU 61	200	0	3447	0.32	15.02	0
133	SLU 62	200	0	3447	0.32	15.02	0
133	SLU 63	200	0	3447	0.32	15.02	0
133	SLU 64	186	0	3150	0.19	14.13	0
133	SLU 65	186	0	3150	0.19	14.13	0
133	SLU 66	186	0	3150	0.19	14.13	0
133	SLU 67	186	0	3150	0.19	14.13	0
133	SLU 68	186	0	3150	0.19	14.13	0
133	SLU 69	186	0	3150	0.19	14.13	0
133	SLU 70	186	0	3150	0.19	14.13	0
133	SLU 71	186	0	3150	0.19	14.13	0
133	SLU 72	186	0	3150	0.19	14.13	0
133	SLU 73	205	0	3553	0.31	15.51	0
133	SLU 74	205	0	3553	0.31	15.51	0
133	SLU 75	205	0	3553	0.31	15.51	0
133	SLU 76	205	0	3553	0.31	15.51	0
133	SLU 77	205	0	3553	0.31	15.51	0
133	SLU 78	205	0	3553	0.31	15.51	0
133	SLU 79	205	0	3553	0.31	15.51	0
133	SLU 80	205	0	3553	0.31	15.51	0
133	SLU 81	213	0	3726	0.37	16.11	0
133	SLU 82	213	0	3726	0.37	16.11	0
133	SLU 83	213	0	3726	0.37	16.11	0
133	SLU 84	213	0	3726	0.37	16.11	0
133	SLE RA 1	140	0	2362	0.13	10.63	0
133	SLE RA 2	140	0	2362	0.13	10.63	0
133	SLE RA 3	140	0	2362	0.13	10.63	0
133	SLE RA 4	140	0	2362	0.13	10.63	0
133	SLE RA 5	140	0	2362	0.13	10.63	0
133	SLE RA 6	140	0	2362	0.13	10.63	0
133	SLE RA 7	140	0	2362	0.13	10.63	0
133	SLE RA 8	140	0	2362	0.13	10.63	0
133	SLE RA 9	140	0	2362	0.13	10.63	0
133	SLE RA 10	153	0	2631	0.22	11.55	0
133	SLE RA 11	153	0	2631	0.22	11.55	0
133	SLE RA 12	153	0	2631	0.22	11.55	0
133	SLE RA 13	153	0	2631	0.22	11.55	0
133	SLE RA 14	153	0	2631	0.22	11.55	0
133	SLE RA 15	153	0	2631	0.22	11.55	0
133	SLE RA 16	153	0	2631	0.22	11.55	0
133	SLE RA 17	153	0	2631	0.22	11.55	0
133	SLE RA 18	158	0	2746	0.25	11.95	0
133	SLE RA 19	158	0	2746	0.25	11.95	0
133	SLE RA 20	158	0	2746	0.25	11.95	0
133	SLE RA 21	158	0	2746	0.25	11.95	0
133	SLE FR 1	140	0	2362	0.13	10.63	0
133	SLE FR 2	140	0	2362	0.13	10.63	0
133	SLE FR 3	140	0	2362	0.13	10.63	0
133	SLE FR 4	145	0	2477	0.17	11.03	0
133	SLE FR 5	145	0	2477	0.17	11.03	0
133	SLE FR 6	149	0	2554	0.19	11.29	0
133	SLE QP 1	140	0	2362	0.13	10.63	0
133	SLE QP 2	145	0	2477	0.17	11.03	0
133	SLD 1	243	54	2761	-40.56	21.78	-2.55
133	SLD 2	243	54	2761	-40.56	21.78	-2.55
133	SLD 3	256	-16	2834	13.08	23.11	0.82



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
133	SLD 4	256	-16	2834	13.08	23.11	0.82
133	SLD 5	156	122	2452	-93.41	12.23	-5.87
133	SLD 6	156	122	2452	-93.41	12.23	-5.87
133	SLD 7	197	-111	2695	85.4	16.67	5.35
133	SLD 8	197	-111	2695	85.4	16.67	5.35
133	SLD 9	94	111	2259	-85.07	5.38	-5.35
133	SLD 10	94	111	2259	-85.07	5.38	-5.35
133	SLD 11	135	-122	2503	93.75	9.82	5.87
133	SLD 12	135	-122	2503	93.75	9.82	5.87
133	SLD 13	35	16	2120	-12.75	-1.05	-0.82
133	SLD 14	35	16	2120	-12.75	-1.05	-0.82
133	SLD 15	48	-54	2193	40.9	0.28	2.55
133	SLD 16	48	-54	2193	40.9	0.28	2.55
133	SLV 1	376	137	3142	-103.51	36.34	-6.52
133	SLV 2	376	137	3142	-103.51	36.34	-6.52
133	SLV 3	405	-42	3326	33.96	39.54	2.1
133	SLV 4	405	-42	3326	33.96	39.54	2.1
133	SLV 5	170	312	2398	-239.44	13.76	-15.03
133	SLV 6	170	312	2398	-239.44	13.76	-15.03
133	SLV 7	268	-284	3010	218.81	24.44	13.71
133	SLV 8	268	-284	3010	218.81	24.44	13.71
133	SLV 9	23	284	1944	-218.47	-2.38	-13.71
133	SLV 10	23	284	1944	-218.47	-2.38	-13.71
133	SLV 11	121	-312	2557	239.77	8.29	15.03
133	SLV 12	121	-312	2557	239.77	8.29	15.03
133	SLV 13	-114	42	1629	-33.63	-17.49	-2.11
133	SLV 14	-114	42	1629	-33.63	-17.49	-2.11
133	SLV 15	-85	-137	1813	103.85	-14.29	6.52
133	SLV 16	-85	-137	1813	103.85	-14.29	6.52
134	SLU 1	-10	0	2324	0.14	1.47	0
134	SLU 2	-10	0	2324	0.14	1.47	0
134	SLU 3	-10	0	2324	0.14	1.47	0
134	SLU 4	-10	0	2324	0.14	1.47	0
134	SLU 5	-10	0	2324	0.14	1.47	0
134	SLU 6	-10	0	2324	0.14	1.47	0
134	SLU 7	-10	0	2324	0.14	1.47	0
134	SLU 8	-10	0	2324	0.14	1.47	0
134	SLU 9	-10	0	2324	0.14	1.47	0
134	SLU 10	-25	0	2744	0.28	1.2	0
134	SLU 11	-25	0	2744	0.28	1.2	0
134	SLU 12	-25	0	2744	0.28	1.2	0
134	SLU 13	-25	0	2744	0.28	1.2	0
134	SLU 14	-25	0	2744	0.28	1.2	0
134	SLU 15	-25	0	2744	0.28	1.2	0
134	SLU 16	-25	0	2744	0.28	1.2	0
134	SLU 17	-25	0	2744	0.28	1.2	0
134	SLU 18	-32	0	2923	0.35	1.08	0
134	SLU 19	-32	0	2923	0.35	1.08	0
134	SLU 20	-32	0	2923	0.35	1.08	0
134	SLU 21	-32	0	2923	0.35	1.08	0
134	SLU 22	-18	0	2609	0.2	1.41	0
134	SLU 23	-18	0	2609	0.2	1.41	0
134	SLU 24	-18	0	2609	0.2	1.41	0
134	SLU 25	-18	0	2609	0.2	1.41	0
134	SLU 26	-18	0	2609	0.2	1.41	0
134	SLU 27	-18	0	2609	0.2	1.41	0
134	SLU 28	-18	0	2609	0.2	1.41	0
134	SLU 29	-18	0	2609	0.2	1.41	0
134	SLU 30	-18	0	2609	0.2	1.41	0
134	SLU 31	-33	0	3029	0.35	1.14	0
134	SLU 32	-33	0	3029	0.35	1.14	0
134	SLU 33	-33	0	3029	0.35	1.14	0
134	SLU 34	-33	0	3029	0.35	1.14	0
134	SLU 35	-33	0	3029	0.35	1.14	0
134	SLU 36	-33	0	3029	0.35	1.14	0
134	SLU 37	-33	0	3029	0.35	1.14	0
134	SLU 38	-33	0	3029	0.35	1.14	0
134	SLU 39	-40	0	3209	0.41	1.02	0
134	SLU 40	-40	0	3209	0.41	1.02	0
134	SLU 41	-40	0	3209	0.41	1.02	0
134	SLU 42	-40	0	3209	0.41	1.02	0
134	SLU 43	-10	0	2923	0.16	1.93	0
134	SLU 44	-10	0	2923	0.16	1.93	0
134	SLU 45	-10	0	2923	0.16	1.93	0
134	SLU 46	-10	0	2923	0.16	1.93	0
134	SLU 47	-10	0	2923	0.16	1.93	0
134	SLU 48	-10	0	2923	0.16	1.93	0
134	SLU 49	-10	0	2923	0.16	1.93	0
134	SLU 50	-10	0	2923	0.16	1.93	0
134	SLU 51	-10	0	2923	0.16	1.93	0
134	SLU 52	-25	0	3343	0.31	1.66	0
134	SLU 53	-25	0	3343	0.31	1.66	0
134	SLU 54	-25	0	3343	0.31	1.66	0
134	SLU 55	-25	0	3343	0.31	1.66	0
134	SLU 56	-25	0	3343	0.31	1.66	0
134	SLU 57	-25	0	3343	0.31	1.66	0
134	SLU 58	-25	0	3343	0.31	1.66	0
134	SLU 59	-25	0	3343	0.31	1.66	0
134	SLU 60	-32	0	3523	0.37	1.54	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
134	SLU 61	-32	0	3523	0.37	1.54	0
134	SLU 62	-32	0	3523	0.37	1.54	0
134	SLU 63	-32	0	3523	0.37	1.54	0
134	SLU 64	-18	0	3209	0.22	1.87	0
134	SLU 65	-18	0	3209	0.22	1.87	0
134	SLU 66	-18	0	3209	0.22	1.87	0
134	SLU 67	-18	0	3209	0.22	1.87	0
134	SLU 68	-18	0	3209	0.22	1.87	0
134	SLU 69	-18	0	3209	0.22	1.87	0
134	SLU 70	-18	0	3209	0.22	1.87	0
134	SLU 71	-18	0	3209	0.22	1.87	0
134	SLU 72	-18	0	3209	0.22	1.87	0
134	SLU 73	-33	0	3628	0.37	1.6	0
134	SLU 74	-33	0	3628	0.37	1.6	0
134	SLU 75	-33	0	3628	0.37	1.6	0
134	SLU 76	-33	0	3628	0.37	1.6	0
134	SLU 77	-33	0	3628	0.37	1.6	0
134	SLU 78	-33	0	3628	0.37	1.6	0
134	SLU 79	-33	0	3628	0.37	1.6	0
134	SLU 80	-33	0	3628	0.37	1.6	0
134	SLU 81	-40	0	3808	0.43	1.48	0
134	SLU 82	-40	0	3808	0.43	1.48	0
134	SLU 83	-40	0	3808	0.43	1.48	0
134	SLU 84	-40	0	3808	0.43	1.48	0
134	SLE RA 1	-12	0	2405	0.16	1.45	0
134	SLE RA 2	-12	0	2405	0.16	1.45	0
134	SLE RA 3	-12	0	2405	0.16	1.45	0
134	SLE RA 4	-12	0	2405	0.16	1.45	0
134	SLE RA 5	-12	0	2405	0.16	1.45	0
134	SLE RA 6	-12	0	2405	0.16	1.45	0
134	SLE RA 7	-12	0	2405	0.16	1.45	0
134	SLE RA 8	-12	0	2405	0.16	1.45	0
134	SLE RA 9	-12	0	2405	0.16	1.45	0
134	SLE RA 10	-22	0	2685	0.25	1.27	0
134	SLE RA 11	-22	0	2685	0.25	1.27	0
134	SLE RA 12	-22	0	2685	0.25	1.27	0
134	SLE RA 13	-22	0	2685	0.25	1.27	0
134	SLE RA 14	-22	0	2685	0.25	1.27	0
134	SLE RA 15	-22	0	2685	0.25	1.27	0
134	SLE RA 16	-22	0	2685	0.25	1.27	0
134	SLE RA 17	-22	0	2685	0.25	1.27	0
134	SLE RA 18	-27	0	2805	0.3	1.19	0
134	SLE RA 19	-27	0	2805	0.3	1.19	0
134	SLE RA 20	-27	0	2805	0.3	1.19	0
134	SLE RA 21	-27	0	2805	0.3	1.19	0
134	SLE FR 1	-12	0	2405	0.16	1.45	0
134	SLE FR 2	-12	0	2405	0.16	1.45	0
134	SLE FR 3	-12	0	2405	0.16	1.45	0
134	SLE FR 4	-16	0	2525	0.2	1.37	0
134	SLE FR 5	-16	0	2525	0.2	1.37	0
134	SLE FR 6	-19	0	2605	0.23	1.32	0
134	SLE QP 1	-12	0	2405	0.16	1.45	0
134	SLE QP 2	-16	0	2525	0.2	1.37	0
134	SLD 1	203	33	2647	-37.72	11.19	1.3
134	SLD 2	203	33	2647	-37.72	11.19	1.3
134	SLD 3	230	-2	2708	8.2	12.38	-0.42
134	SLD 4	230	-2	2708	8.2	12.38	-0.42
134	SLD 5	9	63	2469	-80.83	2.51	2.99
134	SLD 6	9	63	2469	-80.83	2.51	2.99
134	SLD 7	98	-54	2674	72.25	6.49	-2.73
134	SLD 8	98	-54	2674	72.25	6.49	-2.73
134	SLD 9	-131	54	2377	-71.85	-3.74	2.73
134	SLD 10	-131	54	2377	-71.85	-3.74	2.73
134	SLD 11	-42	-63	2582	81.22	0.24	-2.99
134	SLD 12	-42	-63	2582	81.22	0.24	-2.99
134	SLD 13	-262	2	2343	-7.81	-9.64	0.42
134	SLD 14	-262	2	2343	-7.81	-9.64	0.42
134	SLD 15	-236	-33	2404	38.12	-8.45	-1.3
134	SLD 16	-236	-33	2404	38.12	-8.45	-1.3
134	SLV 1	500	83	2807	-96.27	24.5	3.3
134	SLV 2	500	83	2807	-96.27	24.5	3.3
134	SLV 3	564	-7	2962	21.4	27.36	-1.1
134	SLV 4	564	-7	2962	21.4	27.36	-1.1
134	SLV 5	41	161	2375	-207.2	3.97	7.65
134	SLV 6	41	161	2375	-207.2	3.97	7.65
134	SLV 7	255	-138	2892	185.02	13.51	-6.99
134	SLV 8	255	-138	2892	185.02	13.51	-6.99
134	SLV 9	-288	138	2159	-184.62	-10.76	6.99
134	SLV 10	-288	138	2159	-184.62	-10.76	6.99
134	SLV 11	-74	-161	2676	207.59	-1.22	-7.65
134	SLV 12	-74	-161	2676	207.59	-1.22	-7.65
134	SLV 13	-597	7	2089	-21	-24.61	1.1
134	SLV 14	-597	7	2089	-21	-24.61	1.1
134	SLV 15	-533	-83	2244	96.66	-21.75	-3.3
134	SLV 16	-533	-83	2244	96.66	-21.75	-3.3
135	SLU 1	-32	0	2284	0.15	-2.14	0
135	SLU 2	-32	0	2284	0.15	-2.14	0
135	SLU 3	-32	0	2284	0.15	-2.14	0
135	SLU 4	-32	0	2284	0.15	-2.14	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
135	SLU 5	-32	0	2284	0.15	-2.14	0
135	SLU 6	-32	0	2284	0.15	-2.14	0
135	SLU 7	-32	0	2284	0.15	-2.14	0
135	SLU 8	-32	0	2284	0.15	-2.14	0
135	SLU 9	-32	0	2284	0.15	-2.14	0
135	SLU 10	-51	0	2697	0.3	-3.14	0
135	SLU 11	-51	0	2697	0.3	-3.14	0
135	SLU 12	-51	0	2697	0.3	-3.14	0
135	SLU 13	-51	0	2697	0.3	-3.14	0
135	SLU 14	-51	0	2697	0.3	-3.14	0
135	SLU 15	-51	0	2697	0.3	-3.14	0
135	SLU 16	-51	0	2697	0.3	-3.14	0
135	SLU 17	-51	0	2697	0.3	-3.14	0
135	SLU 18	-59	0	2874	0.36	-3.57	0
135	SLU 19	-59	0	2874	0.36	-3.57	0
135	SLU 20	-59	0	2874	0.36	-3.57	0
135	SLU 21	-59	0	2874	0.36	-3.57	0
135	SLU 22	-42	0	2562	0.21	-2.7	0
135	SLU 23	-42	0	2562	0.21	-2.7	0
135	SLU 24	-42	0	2562	0.21	-2.7	0
135	SLU 25	-42	0	2562	0.21	-2.7	0
135	SLU 26	-42	0	2562	0.21	-2.7	0
135	SLU 27	-42	0	2562	0.21	-2.7	0
135	SLU 28	-42	0	2562	0.21	-2.7	0
135	SLU 29	-42	0	2562	0.21	-2.7	0
135	SLU 30	-42	0	2562	0.21	-2.7	0
135	SLU 31	-61	0	2976	0.36	-3.7	0
135	SLU 32	-61	0	2976	0.36	-3.7	0
135	SLU 33	-61	0	2976	0.36	-3.7	0
135	SLU 34	-61	0	2976	0.36	-3.7	0
135	SLU 35	-61	0	2976	0.36	-3.7	0
135	SLU 36	-61	0	2976	0.36	-3.7	0
135	SLU 37	-61	0	2976	0.36	-3.7	0
135	SLU 38	-61	0	2976	0.36	-3.7	0
135	SLU 39	-70	0	3153	0.42	-4.13	0
135	SLU 40	-70	0	3153	0.42	-4.13	0
135	SLU 41	-70	0	3153	0.42	-4.13	0
135	SLU 42	-70	0	3153	0.42	-4.13	0
135	SLU 43	-38	0	2873	0.17	-2.58	0
135	SLU 44	-38	0	2873	0.17	-2.58	0
135	SLU 45	-38	0	2873	0.17	-2.58	0
135	SLU 46	-38	0	2873	0.17	-2.58	0
135	SLU 47	-38	0	2873	0.17	-2.58	0
135	SLU 48	-38	0	2873	0.17	-2.58	0
135	SLU 49	-38	0	2873	0.17	-2.58	0
135	SLU 50	-38	0	2873	0.17	-2.58	0
135	SLU 51	-38	0	2873	0.17	-2.58	0
135	SLU 52	-57	0	3287	0.32	-3.58	0
135	SLU 53	-57	0	3287	0.32	-3.58	0
135	SLU 54	-57	0	3287	0.32	-3.58	0
135	SLU 55	-57	0	3287	0.32	-3.58	0
135	SLU 56	-57	0	3287	0.32	-3.58	0
135	SLU 57	-57	0	3287	0.32	-3.58	0
135	SLU 58	-57	0	3287	0.32	-3.58	0
135	SLU 59	-57	0	3287	0.32	-3.58	0
135	SLU 60	-65	0	3464	0.38	-4.01	0
135	SLU 61	-65	0	3464	0.38	-4.01	0
135	SLU 62	-65	0	3464	0.38	-4.01	0
135	SLU 63	-65	0	3464	0.38	-4.01	0
135	SLU 64	-48	0	3152	0.24	-3.15	0
135	SLU 65	-48	0	3152	0.24	-3.15	0
135	SLU 66	-48	0	3152	0.24	-3.15	0
135	SLU 67	-48	0	3152	0.24	-3.15	0
135	SLU 68	-48	0	3152	0.24	-3.15	0
135	SLU 69	-48	0	3152	0.24	-3.15	0
135	SLU 70	-48	0	3152	0.24	-3.15	0
135	SLU 71	-48	0	3152	0.24	-3.15	0
135	SLU 72	-48	0	3152	0.24	-3.15	0
135	SLU 73	-67	0	3565	0.38	-4.15	0
135	SLU 74	-67	0	3565	0.38	-4.15	0
135	SLU 75	-67	0	3565	0.38	-4.15	0
135	SLU 76	-67	0	3565	0.38	-4.15	0
135	SLU 77	-67	0	3565	0.38	-4.15	0
135	SLU 78	-67	0	3565	0.38	-4.15	0
135	SLU 79	-67	0	3565	0.38	-4.15	0
135	SLU 80	-67	0	3565	0.38	-4.15	0
135	SLU 81	-76	0	3743	0.44	-4.58	0.01
135	SLU 82	-76	0	3743	0.44	-4.58	0.01
135	SLU 83	-76	0	3743	0.44	-4.58	0.01
135	SLU 84	-76	0	3743	0.44	-4.58	0.01
135	SLE RA 1	-35	0	2363	0.17	-2.3	0
135	SLE RA 2	-35	0	2363	0.17	-2.3	0
135	SLE RA 3	-35	0	2363	0.17	-2.3	0
135	SLE RA 4	-35	0	2363	0.17	-2.3	0
135	SLE RA 5	-35	0	2363	0.17	-2.3	0
135	SLE RA 6	-35	0	2363	0.17	-2.3	0
135	SLE RA 7	-35	0	2363	0.17	-2.3	0
135	SLE RA 8	-35	0	2363	0.17	-2.3	0
135	SLE RA 9	-35	0	2363	0.17	-2.3	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
135	SLE RA 10	-48	0	2639	0.26	-2.97	0
135	SLE RA 11	-48	0	2639	0.26	-2.97	0
135	SLE RA 12	-48	0	2639	0.26	-2.97	0
135	SLE RA 13	-48	0	2639	0.26	-2.97	0
135	SLE RA 14	-48	0	2639	0.26	-2.97	0
135	SLE RA 15	-48	0	2639	0.26	-2.97	0
135	SLE RA 16	-48	0	2639	0.26	-2.97	0
135	SLE RA 17	-48	0	2639	0.26	-2.97	0
135	SLE RA 18	-53	0	2757	0.31	-3.25	0
135	SLE RA 19	-53	0	2757	0.31	-3.25	0
135	SLE RA 20	-53	0	2757	0.31	-3.25	0
135	SLE RA 21	-53	0	2757	0.31	-3.25	0
135	SLE FR 1	-35	0	2363	0.17	-2.3	0
135	SLE FR 2	-35	0	2363	0.17	-2.3	0
135	SLE FR 3	-35	0	2363	0.17	-2.3	0
135	SLE FR 4	-40	0	2481	0.21	-2.58	0
135	SLE FR 5	-40	0	2481	0.21	-2.58	0
135	SLE FR 6	-44	0	2560	0.24	-2.77	0
135	SLE QP 1	-35	0	2363	0.17	-2.3	0
135	SLE QP 2	-40	0	2481	0.21	-2.58	0
135	SLD 1	189	-5	2527	-2.89	7.94	0.08
135	SLD 2	189	-5	2527	-2.89	7.94	0.08
135	SLD 3	217	-30	2583	35.25	9.23	0.55
135	SLD 4	217	-30	2583	35.25	9.23	0.55
135	SLD 5	-14	37	2410	-58.58	-1.39	-0.69
135	SLD 6	-14	37	2410	-58.58	-1.39	-0.69
135	SLD 7	79	-47	2597	68.58	2.92	0.88
135	SLD 8	79	-47	2597	68.58	2.92	0.88
135	SLD 9	-160	47	2366	-68.16	-8.09	-0.87
135	SLD 10	-160	47	2366	-68.16	-8.09	-0.87
135	SLD 11	-67	-37	2552	59	-3.78	0.69
135	SLD 12	-67	-37	2552	59	-3.78	0.69
135	SLD 13	-298	30	2379	-34.83	-14.4	-0.55
135	SLD 14	-298	30	2379	-34.83	-14.4	-0.55
135	SLD 15	-270	5	2435	3.31	-13.11	-0.08
135	SLD 16	-270	5	2435	3.31	-13.11	-0.08
135	SLV 1	500	-12	2586	-8.36	22.19	0.2
135	SLV 2	500	-12	2586	-8.36	22.19	0.2
135	SLV 3	567	-76	2725	89.31	25.29	1.38
135	SLV 4	567	-76	2725	89.31	25.29	1.38
135	SLV 5	20	94	2301	-150.5	0.15	-1.74
135	SLV 6	20	94	2301	-150.5	0.15	-1.74
135	SLV 7	244	-120	2766	175.08	10.48	2.22
135	SLV 8	244	-120	2766	175.08	10.48	2.22
135	SLV 9	-324	120	2197	-174.66	-15.65	-2.21
135	SLV 10	-324	120	2197	-174.66	-15.65	-2.21
135	SLV 11	-101	-94	2661	150.92	-5.31	1.75
135	SLV 12	-101	-94	2661	150.92	-5.31	1.75
135	SLV 13	-648	76	2238	-88.89	-30.46	-1.38
135	SLV 14	-648	76	2238	-88.89	-30.46	-1.38
135	SLV 15	-581	12	2377	8.78	-27.36	-0.19
135	SLV 16	-581	12	2377	8.78	-27.36	-0.19
136	SLU 1	-129	0	2248	0.16	-4.98	0
136	SLU 2	-129	0	2248	0.16	-4.98	0
136	SLU 3	-129	0	2248	0.16	-4.98	0
136	SLU 4	-129	0	2248	0.16	-4.98	0
136	SLU 5	-129	0	2248	0.16	-4.98	0
136	SLU 6	-129	0	2248	0.16	-4.98	0
136	SLU 7	-129	0	2248	0.16	-4.98	0
136	SLU 8	-129	0	2248	0.16	-4.98	0
136	SLU 9	-129	0	2248	0.16	-4.98	0
136	SLU 10	-167	0	2656	0.3	-6.51	0
136	SLU 11	-167	0	2656	0.3	-6.51	0
136	SLU 12	-167	0	2656	0.3	-6.51	0
136	SLU 13	-167	0	2656	0.3	-6.51	0
136	SLU 14	-167	0	2656	0.3	-6.51	0
136	SLU 15	-167	0	2656	0.3	-6.51	0
136	SLU 16	-167	0	2656	0.3	-6.51	0
136	SLU 17	-167	0	2656	0.3	-6.51	0
136	SLU 18	-183	0	2830	0.35	-7.16	0
136	SLU 19	-183	0	2830	0.35	-7.16	0
136	SLU 20	-183	0	2830	0.35	-7.16	0
136	SLU 21	-183	0	2830	0.35	-7.16	0
136	SLU 22	-154	0	2518	0.21	-5.93	0
136	SLU 23	-154	0	2518	0.21	-5.93	0
136	SLU 24	-154	0	2518	0.21	-5.93	0
136	SLU 25	-154	0	2518	0.21	-5.93	0
136	SLU 26	-154	0	2518	0.21	-5.93	0
136	SLU 27	-154	0	2518	0.21	-5.93	0
136	SLU 28	-154	0	2518	0.21	-5.93	0
136	SLU 29	-154	0	2518	0.21	-5.93	0
136	SLU 30	-154	0	2518	0.21	-5.93	0
136	SLU 31	-191	0	2926	0.35	-7.46	0
136	SLU 32	-191	0	2926	0.35	-7.46	0
136	SLU 33	-191	0	2926	0.35	-7.46	0
136	SLU 34	-191	0	2926	0.35	-7.46	0
136	SLU 35	-191	0	2926	0.35	-7.46	0
136	SLU 36	-191	0	2926	0.35	-7.46	0
136	SLU 37	-191	0	2926	0.35	-7.46	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
136	SLU 38	-191	0	2926	0.35	-7.46	0
136	SLU 39	-207	0	3101	0.41	-8.11	0
136	SLU 40	-207	0	3101	0.41	-8.11	0
136	SLU 41	-207	0	3101	0.41	-8.11	0
136	SLU 42	-207	0	3101	0.41	-8.11	0
136	SLU 43	-160	0	2829	0.18	-6.15	0
136	SLU 44	-160	0	2829	0.18	-6.15	0
136	SLU 45	-160	0	2829	0.18	-6.15	0
136	SLU 46	-160	0	2829	0.18	-6.15	0
136	SLU 47	-160	0	2829	0.18	-6.15	0
136	SLU 48	-160	0	2829	0.18	-6.15	0
136	SLU 49	-160	0	2829	0.18	-6.15	0
136	SLU 50	-160	0	2829	0.18	-6.15	0
136	SLU 51	-160	0	2829	0.18	-6.15	0
136	SLU 52	-197	0	3237	0.32	-7.68	0
136	SLU 53	-197	0	3237	0.32	-7.68	0
136	SLU 54	-197	0	3237	0.32	-7.68	0
136	SLU 55	-197	0	3237	0.32	-7.68	0
136	SLU 56	-197	0	3237	0.32	-7.68	0
136	SLU 57	-197	0	3237	0.32	-7.68	0
136	SLU 58	-197	0	3237	0.32	-7.68	0
136	SLU 59	-197	0	3237	0.32	-7.68	0
136	SLU 60	-213	0	3412	0.38	-8.33	0
136	SLU 61	-213	0	3412	0.38	-8.33	0
136	SLU 62	-213	0	3412	0.38	-8.33	0
136	SLU 63	-213	0	3412	0.38	-8.33	0
136	SLU 64	-184	0	3100	0.24	-7.1	0
136	SLU 65	-184	0	3100	0.24	-7.1	0
136	SLU 66	-184	0	3100	0.24	-7.1	0
136	SLU 67	-184	0	3100	0.24	-7.1	0
136	SLU 68	-184	0	3100	0.24	-7.1	0
136	SLU 69	-184	0	3100	0.24	-7.1	0
136	SLU 70	-184	0	3100	0.24	-7.1	0
136	SLU 71	-184	0	3100	0.24	-7.1	0
136	SLU 72	-184	0	3100	0.24	-7.1	0
136	SLU 73	-222	0	3508	0.38	-8.63	0
136	SLU 74	-222	0	3508	0.38	-8.63	0
136	SLU 75	-222	0	3508	0.38	-8.63	0
136	SLU 76	-222	0	3508	0.38	-8.63	0
136	SLU 77	-222	0	3508	0.38	-8.63	0
136	SLU 78	-222	0	3508	0.38	-8.63	0
136	SLU 79	-222	0	3508	0.38	-8.63	0
136	SLU 80	-222	0	3508	0.38	-8.63	0
136	SLU 81	-238	0	3683	0.44	-9.28	0
136	SLU 82	-238	0	3683	0.44	-9.28	0
136	SLU 83	-238	0	3683	0.44	-9.28	0
136	SLU 84	-238	0	3683	0.44	-9.28	0
136	SLE RA 1	-136	0	2325	0.17	-5.25	0
136	SLE RA 2	-136	0	2325	0.17	-5.25	0
136	SLE RA 3	-136	0	2325	0.17	-5.25	0
136	SLE RA 4	-136	0	2325	0.17	-5.25	0
136	SLE RA 5	-136	0	2325	0.17	-5.25	0
136	SLE RA 6	-136	0	2325	0.17	-5.25	0
136	SLE RA 7	-136	0	2325	0.17	-5.25	0
136	SLE RA 8	-136	0	2325	0.17	-5.25	0
136	SLE RA 9	-136	0	2325	0.17	-5.25	0
136	SLE RA 10	-161	0	2597	0.27	-6.27	0
136	SLE RA 11	-161	0	2597	0.27	-6.27	0
136	SLE RA 12	-161	0	2597	0.27	-6.27	0
136	SLE RA 13	-161	0	2597	0.27	-6.27	0
136	SLE RA 14	-161	0	2597	0.27	-6.27	0
136	SLE RA 15	-161	0	2597	0.27	-6.27	0
136	SLE RA 16	-161	0	2597	0.27	-6.27	0
136	SLE RA 17	-161	0	2597	0.27	-6.27	0
136	SLE RA 18	-172	0	2714	0.3	-6.71	0
136	SLE RA 19	-172	0	2714	0.3	-6.71	0
136	SLE RA 20	-172	0	2714	0.3	-6.71	0
136	SLE RA 21	-172	0	2714	0.3	-6.71	0
136	SLE FR 1	-136	0	2325	0.17	-5.25	0
136	SLE FR 2	-136	0	2325	0.17	-5.25	0
136	SLE FR 3	-136	0	2325	0.17	-5.25	0
136	SLE FR 4	-147	0	2442	0.21	-5.69	0
136	SLE FR 5	-147	0	2442	0.21	-5.69	0
136	SLE FR 6	-154	0	2519	0.24	-5.98	0
136	SLE QP 1	-136	0	2325	0.17	-5.25	0
136	SLE QP 2	-147	0	2442	0.21	-5.69	0
136	SLD 1	96	-6	2384	-0.67	5.8	-0.28
136	SLD 2	96	-6	2384	-0.67	5.8	-0.28
136	SLD 3	126	-28	2439	32.48	7.2	-0.08
136	SLD 4	126	-28	2439	32.48	7.2	-0.08
136	SLD 5	-119	31	2339	-50.33	-4.38	-0.39
136	SLD 6	-119	31	2339	-50.33	-4.38	-0.39
136	SLD 7	-20	-41	2526	60.18	0.31	0.28
136	SLD 8	-20	-41	2526	60.18	0.31	0.28
136	SLD 9	-274	41	2357	-59.75	-11.69	-0.28
136	SLD 10	-274	41	2357	-59.75	-11.69	-0.28
136	SLD 11	-175	-31	2544	50.76	-7	0.39
136	SLD 12	-175	-31	2544	50.76	-7	0.39
136	SLD 13	-420	27	2444	-32.06	-18.58	0.08



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
136	SLD 14	-420	27	2444	-32.06	-18.58	0.08
136	SLD 15	-391	6	2500	1.09	-17.18	0.28
136	SLD 16	-391	6	2500	1.09	-17.18	0.28
136	SLV 1	426	-14	2302	-2.56	21.36	-0.71
136	SLV 2	426	-14	2302	-2.56	21.36	-0.71
136	SLV 3	498	-69	2439	82.26	24.74	-0.21
136	SLV 4	498	-69	2439	82.26	24.74	-0.21
136	SLV 5	-84	79	2193	-129.27	-2.7	-0.98
136	SLV 6	-84	79	2193	-129.27	-2.7	-0.98
136	SLV 7	155	-104	2647	153.48	8.56	0.7
136	SLV 8	155	-104	2647	153.48	8.56	0.7
136	SLV 9	-450	104	2236	-153.05	-19.94	-0.7
136	SLV 10	-450	104	2236	-153.05	-19.94	-0.7
136	SLV 11	-210	-79	2690	129.7	-8.69	0.98
136	SLV 12	-210	-79	2690	129.7	-8.69	0.98
136	SLV 13	-792	69	2444	-81.84	-36.12	0.2
136	SLV 14	-792	69	2444	-81.84	-36.12	0.2
136	SLV 15	-720	14	2581	2.99	-32.74	0.71
136	SLV 16	-720	14	2581	2.99	-32.74	0.71
137	SLU 1	-172	0	2210	0.17	-6.69	0
137	SLU 2	-172	0	2210	0.17	-6.69	0
137	SLU 3	-172	0	2210	0.17	-6.69	0
137	SLU 4	-172	0	2210	0.17	-6.69	0
137	SLU 5	-172	0	2210	0.17	-6.69	0
137	SLU 6	-172	0	2210	0.17	-6.69	0
137	SLU 7	-172	0	2210	0.17	-6.69	0
137	SLU 8	-172	0	2210	0.17	-6.69	0
137	SLU 9	-172	0	2210	0.17	-6.69	0
137	SLU 10	-216	0	2613	0.3	-8.43	0
137	SLU 11	-216	0	2613	0.3	-8.43	0
137	SLU 12	-216	0	2613	0.3	-8.43	0
137	SLU 13	-216	0	2613	0.3	-8.43	0
137	SLU 14	-216	0	2613	0.3	-8.43	0
137	SLU 15	-216	0	2613	0.3	-8.43	0
137	SLU 16	-216	0	2613	0.3	-8.43	0
137	SLU 17	-216	0	2613	0.3	-8.43	0
137	SLU 18	-235	0	2786	0.35	-9.17	0
137	SLU 19	-235	0	2786	0.35	-9.17	0
137	SLU 20	-235	0	2786	0.35	-9.17	0
137	SLU 21	-235	0	2786	0.35	-9.17	0
137	SLU 22	-202	0	2474	0.22	-7.82	0
137	SLU 23	-202	0	2474	0.22	-7.82	0
137	SLU 24	-202	0	2474	0.22	-7.82	0
137	SLU 25	-202	0	2474	0.22	-7.82	0
137	SLU 26	-202	0	2474	0.22	-7.82	0
137	SLU 27	-202	0	2474	0.22	-7.82	0
137	SLU 28	-202	0	2474	0.22	-7.82	0
137	SLU 29	-202	0	2474	0.22	-7.82	0
137	SLU 30	-202	0	2474	0.22	-7.82	0
137	SLU 31	-245	0	2877	0.35	-9.56	0
137	SLU 32	-245	0	2877	0.35	-9.56	0
137	SLU 33	-245	0	2877	0.35	-9.56	0
137	SLU 34	-245	0	2877	0.35	-9.56	0
137	SLU 35	-245	0	2877	0.35	-9.56	0
137	SLU 36	-245	0	2877	0.35	-9.56	0
137	SLU 37	-245	0	2877	0.35	-9.56	0
137	SLU 38	-245	0	2877	0.35	-9.56	0
137	SLU 39	-264	0	3050	0.4	-10.31	0
137	SLU 40	-264	0	3050	0.4	-10.31	0
137	SLU 41	-264	0	3050	0.4	-10.31	0
137	SLU 42	-264	0	3050	0.4	-10.31	0
137	SLU 43	-214	0	2782	0.2	-8.3	0
137	SLU 44	-214	0	2782	0.2	-8.3	0
137	SLU 45	-214	0	2782	0.2	-8.3	0
137	SLU 46	-214	0	2782	0.2	-8.3	0
137	SLU 47	-214	0	2782	0.2	-8.3	0
137	SLU 48	-214	0	2782	0.2	-8.3	0
137	SLU 49	-214	0	2782	0.2	-8.3	0
137	SLU 50	-214	0	2782	0.2	-8.3	0
137	SLU 51	-214	0	2782	0.2	-8.3	0
137	SLU 52	-258	0	3186	0.33	-10.05	0
137	SLU 53	-258	0	3186	0.33	-10.05	0
137	SLU 54	-258	0	3186	0.33	-10.05	0
137	SLU 55	-258	0	3186	0.33	-10.05	0
137	SLU 56	-258	0	3186	0.33	-10.05	0
137	SLU 57	-258	0	3186	0.33	-10.05	0
137	SLU 58	-258	0	3186	0.33	-10.05	0
137	SLU 59	-258	0	3186	0.33	-10.05	0
137	SLU 60	-276	0	3359	0.38	-10.79	0
137	SLU 61	-276	0	3359	0.38	-10.79	0
137	SLU 62	-276	0	3359	0.38	-10.79	0
137	SLU 63	-276	0	3359	0.38	-10.79	0
137	SLU 64	-243	0	3046	0.26	-9.44	0
137	SLU 65	-243	0	3046	0.26	-9.44	0
137	SLU 66	-243	0	3046	0.26	-9.44	0
137	SLU 67	-243	0	3046	0.26	-9.44	0
137	SLU 68	-243	0	3046	0.26	-9.44	0
137	SLU 69	-243	0	3046	0.26	-9.44	0
137	SLU 70	-243	0	3046	0.26	-9.44	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
137	SLU 71	-243	0	3046	0.26	-9.44	0
137	SLU 72	-243	0	3046	0.26	-9.44	0
137	SLU 73	-287	0	3450	0.38	-11.18	0
137	SLU 74	-287	0	3450	0.38	-11.18	0
137	SLU 75	-287	0	3450	0.38	-11.18	0
137	SLU 76	-287	0	3450	0.38	-11.18	0
137	SLU 77	-287	0	3450	0.38	-11.18	0
137	SLU 78	-287	0	3450	0.38	-11.18	0
137	SLU 79	-287	0	3450	0.38	-11.18	0
137	SLU 80	-287	0	3450	0.38	-11.18	0
137	SLU 81	-306	0	3623	0.44	-11.93	0
137	SLU 82	-306	0	3623	0.44	-11.93	0
137	SLU 83	-306	0	3623	0.44	-11.93	0
137	SLU 84	-306	0	3623	0.44	-11.93	0
137	SLE RA 1	-181	0	2285	0.18	-7.01	0
137	SLE RA 2	-181	0	2285	0.18	-7.01	0
137	SLE RA 3	-181	0	2285	0.18	-7.01	0
137	SLE RA 4	-181	0	2285	0.18	-7.01	0
137	SLE RA 5	-181	0	2285	0.18	-7.01	0
137	SLE RA 6	-181	0	2285	0.18	-7.01	0
137	SLE RA 7	-181	0	2285	0.18	-7.01	0
137	SLE RA 8	-181	0	2285	0.18	-7.01	0
137	SLE RA 9	-181	0	2285	0.18	-7.01	0
137	SLE RA 10	-210	0	2554	0.27	-8.17	0
137	SLE RA 11	-210	0	2554	0.27	-8.17	0
137	SLE RA 12	-210	0	2554	0.27	-8.17	0
137	SLE RA 13	-210	0	2554	0.27	-8.17	0
137	SLE RA 14	-210	0	2554	0.27	-8.17	0
137	SLE RA 15	-210	0	2554	0.27	-8.17	0
137	SLE RA 16	-210	0	2554	0.27	-8.17	0
137	SLE RA 17	-210	0	2554	0.27	-8.17	0
137	SLE RA 18	-222	0	2670	0.31	-8.67	0
137	SLE RA 19	-222	0	2670	0.31	-8.67	0
137	SLE RA 20	-222	0	2670	0.31	-8.67	0
137	SLE RA 21	-222	0	2670	0.31	-8.67	0
137	SLE FR 1	-181	0	2285	0.18	-7.01	0
137	SLE FR 2	-181	0	2285	0.18	-7.01	0
137	SLE FR 3	-181	0	2285	0.18	-7.01	0
137	SLE FR 4	-193	0	2400	0.22	-7.51	0
137	SLE FR 5	-193	0	2400	0.22	-7.51	0
137	SLE FR 6	-201	0	2477	0.25	-7.84	0
137	SLE QP 1	-181	0	2285	0.18	-7.01	0
137	SLE QP 2	-193	0	2400	0.22	-7.51	0
137	SLD 1	60	-5	2317	1.14	3.05	-0.24
137	SLD 2	60	-5	2317	1.14	3.05	-0.24
137	SLD 3	91	-26	2379	28.4	4.34	-0.06
137	SLD 4	91	-26	2379	28.4	4.34	-0.06
137	SLD 5	-164	30	2282	-40.84	-6.29	-0.35
137	SLD 6	-164	30	2282	-40.84	-6.29	-0.35
137	SLD 7	-61	-39	2487	50.01	-2	0.26
137	SLD 8	-61	-39	2487	50.01	-2	0.26
137	SLD 9	-325	39	2313	-49.57	-13.02	-0.26
137	SLD 10	-325	39	2313	-49.57	-13.02	-0.26
137	SLD 11	-222	-30	2519	41.28	-8.73	0.35
137	SLD 12	-222	-30	2519	41.28	-8.73	0.35
137	SLD 13	-477	26	2422	-27.96	-19.36	0.06
137	SLD 14	-477	26	2422	-27.96	-19.36	0.06
137	SLD 15	-446	5	2483	-0.7	-18.07	0.24
137	SLD 16	-446	5	2483	-0.7	-18.07	0.24
137	SLV 1	402	-12	2202	2.21	17.37	-0.61
137	SLV 2	402	-12	2202	2.21	17.37	-0.61
137	SLV 3	477	-65	2350	71.87	20.46	-0.15
137	SLV 4	477	-65	2350	71.87	20.46	-0.15
137	SLV 5	-127	76	2118	-104.83	-4.73	-0.89
137	SLV 6	-127	76	2118	-104.83	-4.73	-0.89
137	SLV 7	121	-99	2609	127.37	5.57	0.66
137	SLV 8	121	-99	2609	127.37	5.57	0.66
137	SLV 9	-507	99	2192	-126.93	-20.59	-0.66
137	SLV 10	-507	99	2192	-126.93	-20.59	-0.66
137	SLV 11	-259	-76	2683	105.28	-10.29	0.89
137	SLV 12	-259	-76	2683	105.28	-10.29	0.89
137	SLV 13	-863	65	2451	-71.43	-35.48	0.15
137	SLV 14	-863	65	2451	-71.43	-35.48	0.15
137	SLV 15	-788	12	2598	-1.77	-32.39	0.61
137	SLV 16	-788	12	2598	-1.77	-32.39	0.61
138	SLU 1	-211	0	2175	0.2	-8.28	0
138	SLU 2	-211	0	2175	0.2	-8.28	0
138	SLU 3	-211	0	2175	0.2	-8.28	0
138	SLU 4	-211	0	2175	0.2	-8.28	0
138	SLU 5	-211	0	2175	0.2	-8.28	0
138	SLU 6	-211	0	2175	0.2	-8.28	0
138	SLU 7	-211	0	2175	0.2	-8.28	0
138	SLU 8	-211	0	2175	0.2	-8.28	0
138	SLU 9	-211	0	2175	0.2	-8.28	0
138	SLU 10	-261	0	2576	0.31	-10.25	0
138	SLU 11	-261	0	2576	0.31	-10.25	0
138	SLU 12	-261	0	2576	0.31	-10.25	0
138	SLU 13	-261	0	2576	0.31	-10.25	0
138	SLU 14	-261	0	2576	0.31	-10.25	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
138	SLU 15	-261	0	2576	0.31	-10.25	0
138	SLU 16	-261	0	2576	0.31	-10.25	0
138	SLU 17	-261	0	2576	0.31	-10.25	0
138	SLU 18	-282	0	2749	0.36	-11.09	0
138	SLU 19	-282	0	2749	0.36	-11.09	0
138	SLU 20	-282	0	2749	0.36	-11.09	0
138	SLU 21	-282	0	2749	0.36	-11.09	0
138	SLU 22	-246	0	2432	0.25	-9.61	0
138	SLU 23	-246	0	2432	0.25	-9.61	0
138	SLU 24	-246	0	2432	0.25	-9.61	0
138	SLU 25	-246	0	2432	0.25	-9.61	0
138	SLU 26	-246	0	2432	0.25	-9.61	0
138	SLU 27	-246	0	2432	0.25	-9.61	0
138	SLU 28	-246	0	2432	0.25	-9.61	0
138	SLU 29	-246	0	2432	0.25	-9.61	0
138	SLU 30	-246	0	2432	0.25	-9.61	0
138	SLU 31	-295	0	2834	0.36	-11.58	0
138	SLU 32	-295	0	2834	0.36	-11.58	0
138	SLU 33	-295	0	2834	0.36	-11.58	0
138	SLU 34	-295	0	2834	0.36	-11.58	0
138	SLU 35	-295	0	2834	0.36	-11.58	0
138	SLU 36	-295	0	2834	0.36	-11.58	0
138	SLU 37	-295	0	2834	0.36	-11.58	0
138	SLU 38	-295	0	2834	0.36	-11.58	0
138	SLU 39	-316	0	3006	0.41	-12.42	0
138	SLU 40	-316	0	3006	0.41	-12.42	0
138	SLU 41	-316	0	3006	0.41	-12.42	0
138	SLU 42	-316	0	3006	0.41	-12.42	0
138	SLU 43	-263	0	2740	0.24	-10.31	0
138	SLU 44	-263	0	2740	0.24	-10.31	0
138	SLU 45	-263	0	2740	0.24	-10.31	0
138	SLU 46	-263	0	2740	0.24	-10.31	0
138	SLU 47	-263	0	2740	0.24	-10.31	0
138	SLU 48	-263	0	2740	0.24	-10.31	0
138	SLU 49	-263	0	2740	0.24	-10.31	0
138	SLU 50	-263	0	2740	0.24	-10.31	0
138	SLU 51	-263	0	2740	0.24	-10.31	0
138	SLU 52	-312	0	3141	0.36	-12.28	0
138	SLU 53	-312	0	3141	0.36	-12.28	0
138	SLU 54	-312	0	3141	0.36	-12.28	0
138	SLU 55	-312	0	3141	0.36	-12.28	0
138	SLU 56	-312	0	3141	0.36	-12.28	0
138	SLU 57	-312	0	3141	0.36	-12.28	0
138	SLU 58	-312	0	3141	0.36	-12.28	0
138	SLU 59	-312	0	3141	0.36	-12.28	0
138	SLU 60	-333	0	3313	0.41	-13.12	0
138	SLU 61	-333	0	3313	0.41	-13.12	0
138	SLU 62	-333	0	3313	0.41	-13.12	0
138	SLU 63	-333	0	3313	0.41	-13.12	0
138	SLU 64	-297	0	2997	0.29	-11.64	0
138	SLU 65	-297	0	2997	0.29	-11.64	0
138	SLU 66	-297	0	2997	0.29	-11.64	0
138	SLU 67	-297	0	2997	0.29	-11.64	0
138	SLU 68	-297	0	2997	0.29	-11.64	0
138	SLU 69	-297	0	2997	0.29	-11.64	0
138	SLU 70	-297	0	2997	0.29	-11.64	0
138	SLU 71	-297	0	2997	0.29	-11.64	0
138	SLU 72	-297	0	2997	0.29	-11.64	0
138	SLU 73	-347	0	3398	0.41	-13.61	0
138	SLU 74	-347	0	3398	0.41	-13.61	0
138	SLU 75	-347	0	3398	0.41	-13.61	0
138	SLU 76	-347	0	3398	0.41	-13.61	0
138	SLU 77	-347	0	3398	0.41	-13.61	0
138	SLU 78	-347	0	3398	0.41	-13.61	0
138	SLU 79	-347	0	3398	0.41	-13.61	0
138	SLU 80	-347	0	3398	0.41	-13.61	0
138	SLU 81	-368	0	3570	0.46	-14.45	0
138	SLU 82	-368	0	3570	0.46	-14.45	0
138	SLU 83	-368	0	3570	0.46	-14.45	0
138	SLU 84	-368	0	3570	0.46	-14.45	0
138	SLE RA 1	-221	0	2249	0.21	-8.66	0
138	SLE RA 2	-221	0	2249	0.21	-8.66	0
138	SLE RA 3	-221	0	2249	0.21	-8.66	0
138	SLE RA 4	-221	0	2249	0.21	-8.66	0
138	SLE RA 5	-221	0	2249	0.21	-8.66	0
138	SLE RA 6	-221	0	2249	0.21	-8.66	0
138	SLE RA 7	-221	0	2249	0.21	-8.66	0
138	SLE RA 8	-221	0	2249	0.21	-8.66	0
138	SLE RA 9	-221	0	2249	0.21	-8.66	0
138	SLE RA 10	-254	0	2516	0.29	-9.97	0
138	SLE RA 11	-254	0	2516	0.29	-9.97	0
138	SLE RA 12	-254	0	2516	0.29	-9.97	0
138	SLE RA 13	-254	0	2516	0.29	-9.97	0
138	SLE RA 14	-254	0	2516	0.29	-9.97	0
138	SLE RA 15	-254	0	2516	0.29	-9.97	0
138	SLE RA 16	-254	0	2516	0.29	-9.97	0
138	SLE RA 17	-254	0	2516	0.29	-9.97	0
138	SLE RA 18	-268	0	2631	0.32	-10.54	0
138	SLE RA 19	-268	0	2631	0.32	-10.54	0



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
138	SLE RA 20	-268	0	2631	0.32	-10.54	0
138	SLE RA 21	-268	0	2631	0.32	-10.54	0
138	SLE FR 1	-221	0	2249	0.21	-8.66	0
138	SLE FR 2	-221	0	2249	0.21	-8.66	0
138	SLE FR 3	-221	0	2249	0.21	-8.66	0
138	SLE FR 4	-235	0	2363	0.25	-9.22	0
138	SLE FR 5	-235	0	2363	0.25	-9.22	0
138	SLE FR 6	-245	0	2440	0.27	-9.6	0
138	SLE QP 1	-221	0	2249	0.21	-8.66	0
138	SLE QP 2	-235	0	2363	0.25	-9.22	0
138	SLD 1	15	-7	2239	2.67	0.93	-0.31
138	SLD 2	15	-7	2239	2.67	0.93	-0.31
138	SLD 3	47	-21	2312	23.51	2.18	-0.05
138	SLD 4	47	-21	2312	23.51	2.18	-0.05
138	SLD 5	-208	20	2215	-30.64	-8.07	-0.48
138	SLD 6	-208	20	2215	-30.64	-8.07	-0.48
138	SLD 7	-103	-29	2459	38.83	-3.91	0.38
138	SLD 8	-103	-29	2459	38.83	-3.91	0.38
138	SLD 9	-367	29	2268	-38.34	-14.54	-0.38
138	SLD 10	-367	29	2268	-38.34	-14.54	-0.38
138	SLD 11	-263	-21	2512	31.13	-10.38	0.48
138	SLD 12	-263	-21	2512	31.13	-10.38	0.48
138	SLD 13	-517	21	2414	-23.02	-20.63	0.05
138	SLD 14	-517	21	2414	-23.02	-20.63	0.05
138	SLD 15	-486	6	2488	-2.18	-19.38	0.31
138	SLD 16	-486	6	2488	-2.18	-19.38	0.31
138	SLV 1	355	-17	2068	6.23	14.7	-0.77
138	SLV 2	355	-17	2068	6.23	14.7	-0.77
138	SLV 3	430	-54	2241	59.41	17.7	-0.11
138	SLV 4	430	-54	2241	59.41	17.7	-0.11
138	SLV 5	-173	51	2012	-78.61	-6.59	-1.24
138	SLV 6	-173	51	2012	-78.61	-6.59	-1.24
138	SLV 7	79	-73	2590	98.65	3.4	0.97
138	SLV 8	79	-73	2590	98.65	3.4	0.97
138	SLV 9	-549	72	2137	-98.16	-21.85	-0.97
138	SLV 10	-549	72	2137	-98.16	-21.85	-0.97
138	SLV 11	-298	-52	2715	79.1	-11.86	1.24
138	SLV 12	-298	-52	2715	79.1	-11.86	1.24
138	SLV 13	-901	54	2485	-58.92	-36.15	0.11
138	SLV 14	-901	54	2485	-58.92	-36.15	0.11
138	SLV 15	-825	16	2659	-5.74	-33.15	0.77
138	SLV 16	-825	16	2659	-5.74	-33.15	0.77
139	SLU 1	-257	0	2154	0.27	-10.6	0
139	SLU 2	-257	0	2154	0.27	-10.6	0
139	SLU 3	-257	0	2154	0.27	-10.6	0
139	SLU 4	-257	0	2154	0.27	-10.6	0
139	SLU 5	-257	0	2154	0.27	-10.6	0
139	SLU 6	-257	0	2154	0.27	-10.6	0
139	SLU 7	-257	0	2154	0.27	-10.6	0
139	SLU 8	-257	0	2154	0.27	-10.6	0
139	SLU 9	-257	0	2154	0.27	-10.6	0
139	SLU 10	-313	0	2558	0.39	-12.97	0
139	SLU 11	-313	0	2558	0.39	-12.97	0
139	SLU 12	-313	0	2558	0.39	-12.97	0
139	SLU 13	-313	0	2558	0.39	-12.97	0
139	SLU 14	-313	0	2558	0.39	-12.97	0
139	SLU 15	-313	0	2558	0.39	-12.97	0
139	SLU 16	-313	0	2558	0.39	-12.97	0
139	SLU 17	-313	0	2558	0.39	-12.97	0
139	SLU 18	-336	0	2731	0.44	-13.98	0
139	SLU 19	-336	0	2731	0.44	-13.98	0
139	SLU 20	-336	0	2731	0.44	-13.98	0
139	SLU 21	-336	0	2731	0.44	-13.98	0
139	SLU 22	-297	0	2406	0.32	-12.23	0
139	SLU 23	-297	0	2406	0.32	-12.23	0
139	SLU 24	-297	0	2406	0.32	-12.23	0
139	SLU 25	-297	0	2406	0.32	-12.23	0
139	SLU 26	-297	0	2406	0.32	-12.23	0
139	SLU 27	-297	0	2406	0.32	-12.23	0
139	SLU 28	-297	0	2406	0.32	-12.23	0
139	SLU 29	-297	0	2406	0.32	-12.23	0
139	SLU 30	-297	0	2406	0.32	-12.23	0
139	SLU 31	-352	0	2810	0.44	-14.59	0
139	SLU 32	-352	0	2810	0.44	-14.59	0
139	SLU 33	-352	0	2810	0.44	-14.59	0
139	SLU 34	-352	0	2810	0.44	-14.59	0
139	SLU 35	-352	0	2810	0.44	-14.59	0
139	SLU 36	-352	0	2810	0.44	-14.59	0
139	SLU 37	-352	0	2810	0.44	-14.59	0
139	SLU 38	-352	0	2810	0.44	-14.59	0
139	SLU 39	-376	0	2983	0.49	-15.6	0
139	SLU 40	-376	0	2983	0.49	-15.6	0
139	SLU 41	-376	0	2983	0.49	-15.6	0
139	SLU 42	-376	0	2983	0.49	-15.6	0
139	SLU 43	-320	0	2713	0.33	-13.23	0
139	SLU 44	-320	0	2713	0.33	-13.23	0
139	SLU 45	-320	0	2713	0.33	-13.23	0
139	SLU 46	-320	0	2713	0.33	-13.23	0
139	SLU 47	-320	0	2713	0.33	-13.23	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
139	SLU 48	-320	0	2713	0.33	-13.23	0
139	SLU 49	-320	0	2713	0.33	-13.23	0
139	SLU 50	-320	0	2713	0.33	-13.23	0
139	SLU 51	-320	0	2713	0.33	-13.23	0
139	SLU 52	-376	0	3117	0.45	-15.59	0
139	SLU 53	-376	0	3117	0.45	-15.59	0
139	SLU 54	-376	0	3117	0.45	-15.59	0
139	SLU 55	-376	0	3117	0.45	-15.59	0
139	SLU 56	-376	0	3117	0.45	-15.59	0
139	SLU 57	-376	0	3117	0.45	-15.59	0
139	SLU 58	-376	0	3117	0.45	-15.59	0
139	SLU 59	-376	0	3117	0.45	-15.59	0
139	SLU 60	-400	0	3290	0.5	-16.6	0
139	SLU 61	-400	0	3290	0.5	-16.6	0
139	SLU 62	-400	0	3290	0.5	-16.6	0
139	SLU 63	-400	0	3290	0.5	-16.6	0
139	SLU 64	-360	0	2965	0.39	-14.85	0
139	SLU 65	-360	0	2965	0.39	-14.85	0
139	SLU 66	-360	0	2965	0.39	-14.85	0
139	SLU 67	-360	0	2965	0.39	-14.85	0
139	SLU 68	-360	0	2965	0.39	-14.85	0
139	SLU 69	-360	0	2965	0.39	-14.85	0
139	SLU 70	-360	0	2965	0.39	-14.85	0
139	SLU 71	-360	0	2965	0.39	-14.85	0
139	SLU 72	-360	0	2965	0.39	-14.85	0
139	SLU 73	-416	0	3369	0.5	-17.21	0
139	SLU 74	-416	0	3369	0.5	-17.21	0
139	SLU 75	-416	0	3369	0.5	-17.21	0
139	SLU 76	-416	0	3369	0.5	-17.21	0
139	SLU 77	-416	0	3369	0.5	-17.21	0
139	SLU 78	-416	0	3369	0.5	-17.21	0
139	SLU 79	-416	0	3369	0.5	-17.21	0
139	SLU 80	-416	0	3369	0.5	-17.21	0
139	SLU 81	-440	0	3542	0.55	-18.23	0
139	SLU 82	-440	0	3542	0.55	-18.23	0
139	SLU 83	-440	0	3542	0.55	-18.23	0
139	SLU 84	-440	0	3542	0.55	-18.23	0
139	SLE RA 1	-268	0	2226	0.29	-11.07	0
139	SLE RA 2	-268	0	2226	0.29	-11.07	0
139	SLE RA 3	-268	0	2226	0.29	-11.07	0
139	SLE RA 4	-268	0	2226	0.29	-11.07	0
139	SLE RA 5	-268	0	2226	0.29	-11.07	0
139	SLE RA 6	-268	0	2226	0.29	-11.07	0
139	SLE RA 7	-268	0	2226	0.29	-11.07	0
139	SLE RA 8	-268	0	2226	0.29	-11.07	0
139	SLE RA 9	-268	0	2226	0.29	-11.07	0
139	SLE RA 10	-305	0	2495	0.36	-12.64	0
139	SLE RA 11	-305	0	2495	0.36	-12.64	0
139	SLE RA 12	-305	0	2495	0.36	-12.64	0
139	SLE RA 13	-305	0	2495	0.36	-12.64	0
139	SLE RA 14	-305	0	2495	0.36	-12.64	0
139	SLE RA 15	-305	0	2495	0.36	-12.64	0
139	SLE RA 16	-305	0	2495	0.36	-12.64	0
139	SLE RA 17	-305	0	2495	0.36	-12.64	0
139	SLE RA 18	-321	0	2610	0.4	-13.32	0
139	SLE RA 19	-321	0	2610	0.4	-13.32	0
139	SLE RA 20	-321	0	2610	0.4	-13.32	0
139	SLE RA 21	-321	0	2610	0.4	-13.32	0
139	SLE FR 1	-268	0	2226	0.29	-11.07	0
139	SLE FR 2	-268	0	2226	0.29	-11.07	0
139	SLE FR 3	-268	0	2226	0.29	-11.07	0
139	SLE FR 4	-284	0	2341	0.32	-11.74	0
139	SLE FR 5	-284	0	2341	0.32	-11.74	0
139	SLE FR 6	-295	0	2418	0.34	-12.19	0
139	SLE QP 1	-268	0	2226	0.29	-11.07	0
139	SLE QP 2	-284	0	2341	0.32	-11.74	0
139	SLD 1	-39	-9	2163	3.88	-1.49	-0.37
139	SLD 2	-39	-9	2163	3.88	-1.49	-0.37
139	SLD 3	-7	-19	2255	18.45	-0.21	-0.05
139	SLD 4	-7	-19	2255	18.45	-0.21	-0.05
139	SLD 5	-259	12	2147	-20.72	-10.6	-0.59
139	SLD 6	-259	12	2147	-20.72	-10.6	-0.59
139	SLD 7	-153	-20	2456	27.87	-6.35	0.46
139	SLD 8	-153	-20	2456	27.87	-6.35	0.46
139	SLD 9	-416	20	2227	-27.23	-17.13	-0.46
139	SLD 10	-416	20	2227	-27.23	-17.13	-0.46
139	SLD 11	-309	-12	2535	21.36	-12.89	0.59
139	SLD 12	-309	-12	2535	21.36	-12.89	0.59
139	SLD 13	-561	19	2427	-17.81	-23.27	0.05
139	SLD 14	-561	19	2427	-17.81	-23.27	0.05
139	SLD 15	-529	9	2519	-3.24	-22	0.37
139	SLD 16	-529	9	2519	-3.24	-22	0.37
139	SLV 1	293	-23	1918	9.26	12.42	-0.93
139	SLV 2	293	-23	1918	9.26	12.42	-0.93
139	SLV 3	369	-47	2136	46.39	15.48	-0.13
139	SLV 4	369	-47	2136	46.39	15.48	-0.13
139	SLV 5	-227	29	1883	-53.31	-9.13	-1.49
139	SLV 6	-227	29	1883	-53.31	-9.13	-1.49
139	SLV 7	28	-51	2610	70.45	1.06	1.17



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
139	SLV 8	28	-51	2610	70.45	1.06	1.17
139	SLV 9	-596	50	2072	-69.81	-24.54	-1.17
139	SLV 10	-596	50	2072	-69.81	-24.54	-1.17
139	SLV 11	-341	-29	2799	53.95	-14.36	1.49
139	SLV 12	-341	-29	2799	53.95	-14.36	1.49
139	SLV 13	-937	47	2546	-45.75	-38.96	0.13
139	SLV 14	-937	47	2546	-45.75	-38.96	0.13
139	SLV 15	-861	23	2764	-8.62	-35.91	0.93
139	SLV 16	-861	23	2764	-8.62	-35.91	0.93
140	SLU 1	-307	0	2155	0.48	-13.97	0.01
140	SLU 2	-307	0	2155	0.48	-13.97	0.01
140	SLU 3	-307	0	2155	0.48	-13.97	0.01
140	SLU 4	-307	0	2155	0.48	-13.97	0.01
140	SLU 5	-307	0	2155	0.48	-13.97	0.01
140	SLU 6	-307	0	2155	0.48	-13.97	0.01
140	SLU 7	-307	0	2155	0.48	-13.97	0.01
140	SLU 8	-307	0	2155	0.48	-13.97	0.01
140	SLU 9	-307	0	2155	0.48	-13.97	0.01
140	SLU 10	-370	0	2571	0.63	-16.95	0.01
140	SLU 11	-370	0	2571	0.63	-16.95	0.01
140	SLU 12	-370	0	2571	0.63	-16.95	0.01
140	SLU 13	-370	0	2571	0.63	-16.95	0.01
140	SLU 14	-370	0	2571	0.63	-16.95	0.01
140	SLU 15	-370	0	2571	0.63	-16.95	0.01
140	SLU 16	-370	0	2571	0.63	-16.95	0.01
140	SLU 17	-370	0	2571	0.63	-16.95	0.01
140	SLU 18	-397	-1	2749	0.69	-18.22	0.01
140	SLU 19	-397	-1	2749	0.69	-18.22	0.01
140	SLU 20	-397	-1	2749	0.69	-18.22	0.01
140	SLU 21	-397	-1	2749	0.69	-18.22	0.01
140	SLU 22	-353	0	2406	0.55	-16.02	0.01
140	SLU 23	-353	0	2406	0.55	-16.02	0.01
140	SLU 24	-353	0	2406	0.55	-16.02	0.01
140	SLU 25	-353	0	2406	0.55	-16.02	0.01
140	SLU 26	-353	0	2406	0.55	-16.02	0.01
140	SLU 27	-353	0	2406	0.55	-16.02	0.01
140	SLU 28	-353	0	2406	0.55	-16.02	0.01
140	SLU 29	-353	0	2406	0.55	-16.02	0.01
140	SLU 30	-353	0	2406	0.55	-16.02	0.01
140	SLU 31	-416	-1	2822	0.7	-18.99	0.01
140	SLU 32	-416	-1	2822	0.7	-18.99	0.01
140	SLU 33	-416	-1	2822	0.7	-18.99	0.01
140	SLU 34	-416	-1	2822	0.7	-18.99	0.01
140	SLU 35	-416	-1	2822	0.7	-18.99	0.01
140	SLU 36	-416	-1	2822	0.7	-18.99	0.01
140	SLU 37	-416	-1	2822	0.7	-18.99	0.01
140	SLU 38	-416	-1	2822	0.7	-18.99	0.01
140	SLU 39	-443	-1	3000	0.77	-20.27	0.01
140	SLU 40	-443	-1	3000	0.77	-20.27	0.01
140	SLU 41	-443	-1	3000	0.77	-20.27	0.01
140	SLU 42	-443	-1	3000	0.77	-20.27	0.01
140	SLU 43	-384	-1	2716	0.6	-17.46	0.01
140	SLU 44	-384	-1	2716	0.6	-17.46	0.01
140	SLU 45	-384	-1	2716	0.6	-17.46	0.01
140	SLU 46	-384	-1	2716	0.6	-17.46	0.01
140	SLU 47	-384	-1	2716	0.6	-17.46	0.01
140	SLU 48	-384	-1	2716	0.6	-17.46	0.01
140	SLU 49	-384	-1	2716	0.6	-17.46	0.01
140	SLU 50	-384	-1	2716	0.6	-17.46	0.01
140	SLU 51	-384	-1	2716	0.6	-17.46	0.01
140	SLU 52	-447	-1	3131	0.75	-20.44	0.01
140	SLU 53	-447	-1	3131	0.75	-20.44	0.01
140	SLU 54	-447	-1	3131	0.75	-20.44	0.01
140	SLU 55	-447	-1	3131	0.75	-20.44	0.01
140	SLU 56	-447	-1	3131	0.75	-20.44	0.01
140	SLU 57	-447	-1	3131	0.75	-20.44	0.01
140	SLU 58	-447	-1	3131	0.75	-20.44	0.01
140	SLU 59	-447	-1	3131	0.75	-20.44	0.01
140	SLU 60	-473	-1	3309	0.81	-21.71	0.01
140	SLU 61	-473	-1	3309	0.81	-21.71	0.01
140	SLU 62	-473	-1	3309	0.81	-21.71	0.01
140	SLU 63	-473	-1	3309	0.81	-21.71	0.01
140	SLU 64	-430	-1	2967	0.67	-19.51	0.01
140	SLU 65	-430	-1	2967	0.67	-19.51	0.01
140	SLU 66	-430	-1	2967	0.67	-19.51	0.01
140	SLU 67	-430	-1	2967	0.67	-19.51	0.01
140	SLU 68	-430	-1	2967	0.67	-19.51	0.01
140	SLU 69	-430	-1	2967	0.67	-19.51	0.01
140	SLU 70	-430	-1	2967	0.67	-19.51	0.01
140	SLU 71	-430	-1	2967	0.67	-19.51	0.01
140	SLU 72	-430	-1	2967	0.67	-19.51	0.01
140	SLU 73	-492	-1	3382	0.82	-22.48	0.01
140	SLU 74	-492	-1	3382	0.82	-22.48	0.01
140	SLU 75	-492	-1	3382	0.82	-22.48	0.01
140	SLU 76	-492	-1	3382	0.82	-22.48	0.01
140	SLU 77	-492	-1	3382	0.82	-22.48	0.01
140	SLU 78	-492	-1	3382	0.82	-22.48	0.01
140	SLU 79	-492	-1	3382	0.82	-22.48	0.01
140	SLU 80	-492	-1	3382	0.82	-22.48	0.01



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
140	SLU 81	-519	-1	3560	0.89	-23.76	0.02
140	SLU 82	-519	-1	3560	0.89	-23.76	0.02
140	SLU 83	-519	-1	3560	0.89	-23.76	0.02
140	SLU 84	-519	-1	3560	0.89	-23.76	0.02
140	SLE RA 1	-320	0	2227	0.5	-14.56	0.01
140	SLE RA 2	-320	0	2227	0.5	-14.56	0.01
140	SLE RA 3	-320	0	2227	0.5	-14.56	0.01
140	SLE RA 4	-320	0	2227	0.5	-14.56	0.01
140	SLE RA 5	-320	0	2227	0.5	-14.56	0.01
140	SLE RA 6	-320	0	2227	0.5	-14.56	0.01
140	SLE RA 7	-320	0	2227	0.5	-14.56	0.01
140	SLE RA 8	-320	0	2227	0.5	-14.56	0.01
140	SLE RA 9	-320	0	2227	0.5	-14.56	0.01
140	SLE RA 10	-362	0	2504	0.6	-16.54	0.01
140	SLE RA 11	-362	0	2504	0.6	-16.54	0.01
140	SLE RA 12	-362	0	2504	0.6	-16.54	0.01
140	SLE RA 13	-362	0	2504	0.6	-16.54	0.01
140	SLE RA 14	-362	0	2504	0.6	-16.54	0.01
140	SLE RA 15	-362	0	2504	0.6	-16.54	0.01
140	SLE RA 16	-362	0	2504	0.6	-16.54	0.01
140	SLE RA 17	-362	0	2504	0.6	-16.54	0.01
140	SLE RA 18	-380	-1	2623	0.64	-17.39	0.01
140	SLE RA 19	-380	-1	2623	0.64	-17.39	0.01
140	SLE RA 20	-380	-1	2623	0.64	-17.39	0.01
140	SLE RA 21	-380	-1	2623	0.64	-17.39	0.01
140	SLE FR 1	-320	0	2227	0.5	-14.56	0.01
140	SLE FR 2	-320	0	2227	0.5	-14.56	0.01
140	SLE FR 3	-320	0	2227	0.5	-14.56	0.01
140	SLE FR 4	-338	0	2346	0.54	-15.41	0.01
140	SLE FR 5	-338	0	2346	0.54	-15.41	0.01
140	SLE FR 6	-350	0	2425	0.57	-15.97	0.01
140	SLE QP 1	-320	0	2227	0.5	-14.56	0.01
140	SLE QP 2	-338	0	2346	0.54	-15.41	0.01
140	SLD 1	-103	-17	2091	4.61	-4.65	0.08
140	SLD 2	-103	-17	2091	4.61	-4.65	0.08
140	SLD 3	-69	-12	2213	13.32	-3.25	0.5
140	SLD 4	-69	-12	2213	13.32	-3.25	0.5
140	SLD 5	-320	-13	2084	-11.44	-14.29	-0.62
140	SLD 6	-320	-13	2084	-11.44	-14.29	-0.62
140	SLD 7	-206	4	2491	17.58	-9.65	0.81
140	SLD 8	-206	4	2491	17.58	-9.65	0.81
140	SLD 9	-471	-5	2200	-16.49	-21.17	-0.79
140	SLD 10	-471	-5	2200	-16.49	-21.17	-0.79
140	SLD 11	-357	12	2608	12.53	-16.52	0.64
140	SLD 12	-357	12	2608	12.53	-16.52	0.64
140	SLD 13	-608	11	2479	-12.23	-27.56	-0.49
140	SLD 14	-608	11	2479	-12.23	-27.56	-0.49
140	SLD 15	-574	16	2601	-3.52	-26.16	-0.06
140	SLD 16	-574	16	2601	-3.52	-26.16	-0.06
140	SLV 1	216	-42	1741	10.77	9.94	0.18
140	SLV 2	216	-42	1741	10.77	9.94	0.18
140	SLV 3	298	-30	2028	32.9	13.29	1.26
140	SLV 4	298	-30	2028	32.9	13.29	1.26
140	SLV 5	-296	-32	1728	-29.96	-12.87	-1.59
140	SLV 6	-296	-32	1728	-29.96	-12.87	-1.59
140	SLV 7	-24	10	2687	43.82	-1.73	2.03
140	SLV 8	-24	10	2687	43.82	-1.73	2.03
140	SLV 9	-653	-11	2005	-42.73	-29.08	-2.01
140	SLV 10	-653	-11	2005	-42.73	-29.08	-2.01
140	SLV 11	-381	31	2963	31.04	-17.94	1.6
140	SLV 12	-381	31	2963	31.04	-17.94	1.6
140	SLV 13	-975	29	2663	-31.81	-44.1	-1.24
140	SLV 14	-975	29	2663	-31.81	-44.1	-1.24
140	SLV 15	-893	42	2951	-9.68	-40.76	-0.16
140	SLV 16	-893	42	2951	-9.68	-40.76	-0.16
141	SLU 1	-240	-3	2204	1.05	-21.95	-0.07
141	SLU 2	-240	-3	2204	1.05	-21.95	-0.07
141	SLU 3	-240	-3	2204	1.05	-21.95	-0.07
141	SLU 4	-240	-3	2204	1.05	-21.95	-0.07
141	SLU 5	-240	-3	2204	1.05	-21.95	-0.07
141	SLU 6	-240	-3	2204	1.05	-21.95	-0.07
141	SLU 7	-240	-3	2204	1.05	-21.95	-0.07
141	SLU 8	-240	-3	2204	1.05	-21.95	-0.07
141	SLU 9	-240	-3	2204	1.05	-21.95	-0.07
141	SLU 10	-281	-4	2643	1.32	-26.59	-0.09
141	SLU 11	-281	-4	2643	1.32	-26.59	-0.09
141	SLU 12	-281	-4	2643	1.32	-26.59	-0.09
141	SLU 13	-281	-4	2643	1.32	-26.59	-0.09
141	SLU 14	-281	-4	2643	1.32	-26.59	-0.09
141	SLU 15	-281	-4	2643	1.32	-26.59	-0.09
141	SLU 16	-281	-4	2643	1.32	-26.59	-0.09
141	SLU 17	-281	-4	2643	1.32	-26.59	-0.09
141	SLU 18	-298	-5	2831	1.44	-28.58	-0.09
141	SLU 19	-298	-5	2831	1.44	-28.58	-0.09
141	SLU 20	-298	-5	2831	1.44	-28.58	-0.09
141	SLU 21	-298	-5	2831	1.44	-28.58	-0.09
141	SLU 22	-275	-4	2460	1.18	-24.97	-0.08
141	SLU 23	-275	-4	2460	1.18	-24.97	-0.08
141	SLU 24	-275	-4	2460	1.18	-24.97	-0.08



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
141	SLU 25	-275	-4	2460	1.18	-24.97	-0.08
141	SLU 26	-275	-4	2460	1.18	-24.97	-0.08
141	SLU 27	-275	-4	2460	1.18	-24.97	-0.08
141	SLU 28	-275	-4	2460	1.18	-24.97	-0.08
141	SLU 29	-275	-4	2460	1.18	-24.97	-0.08
141	SLU 30	-275	-4	2460	1.18	-24.97	-0.08
141	SLU 31	-316	-5	2899	1.46	-29.61	-0.1
141	SLU 32	-316	-5	2899	1.46	-29.61	-0.1
141	SLU 33	-316	-5	2899	1.46	-29.61	-0.1
141	SLU 34	-316	-5	2899	1.46	-29.61	-0.1
141	SLU 35	-316	-5	2899	1.46	-29.61	-0.1
141	SLU 36	-316	-5	2899	1.46	-29.61	-0.1
141	SLU 37	-316	-5	2899	1.46	-29.61	-0.1
141	SLU 38	-316	-5	2899	1.46	-29.61	-0.1
141	SLU 39	-334	-5	3088	1.58	-31.6	-0.1
141	SLU 40	-334	-5	3088	1.58	-31.6	-0.1
141	SLU 41	-334	-5	3088	1.58	-31.6	-0.1
141	SLU 42	-334	-5	3088	1.58	-31.6	-0.1
141	SLU 43	-300	-4	2777	1.31	-27.5	-0.09
141	SLU 44	-300	-4	2777	1.31	-27.5	-0.09
141	SLU 45	-300	-4	2777	1.31	-27.5	-0.09
141	SLU 46	-300	-4	2777	1.31	-27.5	-0.09
141	SLU 47	-300	-4	2777	1.31	-27.5	-0.09
141	SLU 48	-300	-4	2777	1.31	-27.5	-0.09
141	SLU 49	-300	-4	2777	1.31	-27.5	-0.09
141	SLU 50	-300	-4	2777	1.31	-27.5	-0.09
141	SLU 51	-300	-4	2777	1.31	-27.5	-0.09
141	SLU 52	-340	-5	3216	1.59	-32.14	-0.11
141	SLU 53	-340	-5	3216	1.59	-32.14	-0.11
141	SLU 54	-340	-5	3216	1.59	-32.14	-0.11
141	SLU 55	-340	-5	3216	1.59	-32.14	-0.11
141	SLU 56	-340	-5	3216	1.59	-32.14	-0.11
141	SLU 57	-340	-5	3216	1.59	-32.14	-0.11
141	SLU 58	-340	-5	3216	1.59	-32.14	-0.11
141	SLU 59	-340	-5	3216	1.59	-32.14	-0.11
141	SLU 60	-358	-5	3404	1.71	-34.13	-0.11
141	SLU 61	-358	-5	3404	1.71	-34.13	-0.11
141	SLU 62	-358	-5	3404	1.71	-34.13	-0.11
141	SLU 63	-358	-5	3404	1.71	-34.13	-0.11
141	SLU 64	-335	-5	3033	1.45	-30.52	-0.1
141	SLU 65	-335	-5	3033	1.45	-30.52	-0.1
141	SLU 66	-335	-5	3033	1.45	-30.52	-0.1
141	SLU 67	-335	-5	3033	1.45	-30.52	-0.1
141	SLU 68	-335	-5	3033	1.45	-30.52	-0.1
141	SLU 69	-335	-5	3033	1.45	-30.52	-0.1
141	SLU 70	-335	-5	3033	1.45	-30.52	-0.1
141	SLU 71	-335	-5	3033	1.45	-30.52	-0.1
141	SLU 72	-335	-5	3033	1.45	-30.52	-0.1
141	SLU 73	-376	-6	3473	1.73	-35.16	-0.11
141	SLU 74	-376	-6	3473	1.73	-35.16	-0.11
141	SLU 75	-376	-6	3473	1.73	-35.16	-0.11
141	SLU 76	-376	-6	3473	1.73	-35.16	-0.11
141	SLU 77	-376	-6	3473	1.73	-35.16	-0.11
141	SLU 78	-376	-6	3473	1.73	-35.16	-0.11
141	SLU 79	-376	-6	3473	1.73	-35.16	-0.11
141	SLU 80	-376	-6	3473	1.73	-35.16	-0.11
141	SLU 81	-394	-6	3661	1.85	-37.15	-0.12
141	SLU 82	-394	-6	3661	1.85	-37.15	-0.12
141	SLU 83	-394	-6	3661	1.85	-37.15	-0.12
141	SLU 84	-394	-6	3661	1.85	-37.15	-0.12
141	SLE RA 1	-250	-4	2277	1.08	-22.81	-0.08
141	SLE RA 2	-250	-4	2277	1.08	-22.81	-0.08
141	SLE RA 3	-250	-4	2277	1.08	-22.81	-0.08
141	SLE RA 4	-250	-4	2277	1.08	-22.81	-0.08
141	SLE RA 5	-250	-4	2277	1.08	-22.81	-0.08
141	SLE RA 6	-250	-4	2277	1.08	-22.81	-0.08
141	SLE RA 7	-250	-4	2277	1.08	-22.81	-0.08
141	SLE RA 8	-250	-4	2277	1.08	-22.81	-0.08
141	SLE RA 9	-250	-4	2277	1.08	-22.81	-0.08
141	SLE RA 10	-277	-4	2570	1.27	-25.91	-0.08
141	SLE RA 11	-277	-4	2570	1.27	-25.91	-0.08
141	SLE RA 12	-277	-4	2570	1.27	-25.91	-0.08
141	SLE RA 13	-277	-4	2570	1.27	-25.91	-0.08
141	SLE RA 14	-277	-4	2570	1.27	-25.91	-0.08
141	SLE RA 15	-277	-4	2570	1.27	-25.91	-0.08
141	SLE RA 16	-277	-4	2570	1.27	-25.91	-0.08
141	SLE RA 17	-277	-4	2570	1.27	-25.91	-0.08
141	SLE RA 18	-289	-4	2695	1.35	-27.23	-0.09
141	SLE RA 19	-289	-4	2695	1.35	-27.23	-0.09
141	SLE RA 20	-289	-4	2695	1.35	-27.23	-0.09
141	SLE RA 21	-289	-4	2695	1.35	-27.23	-0.09
141	SLE FR 1	-250	-4	2277	1.08	-22.81	-0.08
141	SLE FR 2	-250	-4	2277	1.08	-22.81	-0.08
141	SLE FR 3	-250	-4	2277	1.08	-22.81	-0.08
141	SLE FR 4	-262	-4	2402	1.16	-24.14	-0.08
141	SLE FR 5	-262	-4	2402	1.16	-24.14	-0.08
141	SLE FR 6	-269	-4	2486	1.22	-25.02	-0.08
141	SLE QP 1	-250	-4	2277	1.08	-22.81	-0.08
141	SLE QP 2	-262	-4	2402	1.16	-24.14	-0.08



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
141	SLD 1	-87	-18	2042	4.49	-12.02	0.41
141	SLD 2	-87	-18	2042	4.49	-12.02	0.41
141	SLD 3	-37	-15	2209	8.8	-10.47	1.11
141	SLD 4	-37	-15	2209	8.8	-10.47	1.11
141	SLD 5	-285	-13	2041	-4.38	-22.87	-0.99
141	SLD 6	-285	-13	2041	-4.38	-22.87	-0.99
141	SLD 7	-119	-2	2597	9.99	-17.67	1.33
141	SLD 8	-119	-2	2597	9.99	-17.67	1.33
141	SLD 9	-405	-6	2208	-7.67	-30.61	-1.49
141	SLD 10	-405	-6	2208	-7.67	-30.61	-1.49
141	SLD 11	-238	5	2764	6.7	-25.41	0.83
141	SLD 12	-238	5	2764	6.7	-25.41	0.83
141	SLD 13	-486	7	2596	-6.47	-37.81	-1.27
141	SLD 14	-486	7	2596	-6.47	-37.81	-1.27
141	SLD 15	-436	10	2763	-2.16	-36.26	-0.57
141	SLD 16	-436	10	2763	-2.16	-36.26	-0.57
141	SLV 1	149	-39	1549	9.5	4.43	1.17
141	SLV 2	149	-39	1549	9.5	4.43	1.17
141	SLV 3	267	-30	1942	20.44	8.16	2.93
141	SLV 4	267	-30	1942	20.44	8.16	2.93
141	SLV 5	-318	-27	1551	-12.93	-21.22	-2.38
141	SLV 6	-318	-27	1551	-12.93	-21.22	-2.38
141	SLV 7	76	1	2860	23.54	-8.8	3.5
141	SLV 8	76	1	2860	23.54	-8.8	3.5
141	SLV 9	-599	-9	1945	-21.21	-39.48	-3.66
141	SLV 10	-599	-9	1945	-21.21	-39.48	-3.66
141	SLV 11	-206	19	3254	15.26	-27.06	2.22
141	SLV 12	-206	19	3254	15.26	-27.06	2.22
141	SLV 13	-791	23	2863	-18.11	-56.44	-3.09
141	SLV 14	-791	23	2863	-18.11	-56.44	-3.09
141	SLV 15	-672	31	3256	-7.17	-52.71	-1.33
141	SLV 16	-672	31	3256	-7.17	-52.71	-1.33
142	SLU 1	-628	-402	3071	11.34	-13.39	-0.01
142	SLU 2	-628	-402	3071	11.34	-13.39	-0.01
142	SLU 3	-628	-402	3071	11.34	-13.39	-0.01
142	SLU 4	-628	-402	3071	11.34	-13.39	-0.01
142	SLU 5	-628	-402	3071	11.34	-13.39	-0.01
142	SLU 6	-628	-402	3071	11.34	-13.39	-0.01
142	SLU 7	-628	-402	3071	11.34	-13.39	-0.01
142	SLU 8	-628	-402	3071	11.34	-13.39	-0.01
142	SLU 9	-628	-402	3071	11.34	-13.39	-0.01
142	SLU 10	-763	-497	3729	14.21	-16.17	-0.01
142	SLU 11	-763	-497	3729	14.21	-16.17	-0.01
142	SLU 12	-763	-497	3729	14.21	-16.17	-0.01
142	SLU 13	-763	-497	3729	14.21	-16.17	-0.01
142	SLU 14	-763	-497	3729	14.21	-16.17	-0.01
142	SLU 15	-763	-497	3729	14.21	-16.17	-0.01
142	SLU 16	-763	-497	3729	14.21	-16.17	-0.01
142	SLU 17	-763	-497	3729	14.21	-16.17	-0.01
142	SLU 18	-820	-538	4012	15.43	-17.36	-0.01
142	SLU 19	-820	-538	4012	15.43	-17.36	-0.01
142	SLU 20	-820	-538	4012	15.43	-17.36	-0.01
142	SLU 21	-820	-538	4012	15.43	-17.36	-0.01
142	SLU 22	-708	-449	3437	12.69	-15.19	-0.01
142	SLU 23	-708	-449	3437	12.69	-15.19	-0.01
142	SLU 24	-708	-449	3437	12.69	-15.19	-0.01
142	SLU 25	-708	-449	3437	12.69	-15.19	-0.01
142	SLU 26	-708	-449	3437	12.69	-15.19	-0.01
142	SLU 27	-708	-449	3437	12.69	-15.19	-0.01
142	SLU 28	-708	-449	3437	12.69	-15.19	-0.01
142	SLU 29	-708	-449	3437	12.69	-15.19	-0.01
142	SLU 30	-708	-449	3437	12.69	-15.19	-0.01
142	SLU 31	-843	-544	4095	15.56	-17.97	-0.02
142	SLU 32	-843	-544	4095	15.56	-17.97	-0.02
142	SLU 33	-843	-544	4095	15.56	-17.97	-0.02
142	SLU 34	-843	-544	4095	15.56	-17.97	-0.02
142	SLU 35	-843	-544	4095	15.56	-17.97	-0.02
142	SLU 36	-843	-544	4095	15.56	-17.97	-0.02
142	SLU 37	-843	-544	4095	15.56	-17.97	-0.02
142	SLU 38	-843	-544	4095	15.56	-17.97	-0.02
142	SLU 39	-900	-585	4377	16.78	-19.16	-0.02
142	SLU 40	-900	-585	4377	16.78	-19.16	-0.02
142	SLU 41	-900	-585	4377	16.78	-19.16	-0.02
142	SLU 42	-900	-585	4377	16.78	-19.16	-0.02
142	SLU 43	-789	-507	3867	14.28	-16.79	-0.01
142	SLU 44	-789	-507	3867	14.28	-16.79	-0.01
142	SLU 45	-789	-507	3867	14.28	-16.79	-0.01
142	SLU 46	-789	-507	3867	14.28	-16.79	-0.01
142	SLU 47	-789	-507	3867	14.28	-16.79	-0.01
142	SLU 48	-789	-507	3867	14.28	-16.79	-0.01
142	SLU 49	-789	-507	3867	14.28	-16.79	-0.01
142	SLU 50	-789	-507	3867	14.28	-16.79	-0.01
142	SLU 51	-789	-507	3867	14.28	-16.79	-0.01
142	SLU 52	-923	-602	4525	17.15	-19.56	-0.02
142	SLU 53	-923	-602	4525	17.15	-19.56	-0.02
142	SLU 54	-923	-602	4525	17.15	-19.56	-0.02
142	SLU 55	-923	-602	4525	17.15	-19.56	-0.02
142	SLU 56	-923	-602	4525	17.15	-19.56	-0.02
142	SLU 57	-923	-602	4525	17.15	-19.56	-0.02



Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
142	SLU 58	-923	-602	4525	17.15	-19.56	-0.02
142	SLU 59	-923	-602	4525	17.15	-19.56	-0.02
142	SLU 60	-981	-643	4808	18.37	-20.75	-0.02
142	SLU 61	-981	-643	4808	18.37	-20.75	-0.02
142	SLU 62	-981	-643	4808	18.37	-20.75	-0.02
142	SLU 63	-981	-643	4808	18.37	-20.75	-0.02
142	SLU 64	-869	-554	4233	15.63	-18.59	-0.02
142	SLU 65	-869	-554	4233	15.63	-18.59	-0.02
142	SLU 66	-869	-554	4233	15.63	-18.59	-0.02
142	SLU 67	-869	-554	4233	15.63	-18.59	-0.02
142	SLU 68	-869	-554	4233	15.63	-18.59	-0.02
142	SLU 69	-869	-554	4233	15.63	-18.59	-0.02
142	SLU 70	-869	-554	4233	15.63	-18.59	-0.02
142	SLU 71	-869	-554	4233	15.63	-18.59	-0.02
142	SLU 72	-869	-554	4233	15.63	-18.59	-0.02
142	SLU 73	-1004	-649	4891	18.5	-21.37	-0.02
142	SLU 74	-1004	-649	4891	18.5	-21.37	-0.02
142	SLU 75	-1004	-649	4891	18.5	-21.37	-0.02
142	SLU 76	-1004	-649	4891	18.5	-21.37	-0.02
142	SLU 77	-1004	-649	4891	18.5	-21.37	-0.02
142	SLU 78	-1004	-649	4891	18.5	-21.37	-0.02
142	SLU 79	-1004	-649	4891	18.5	-21.37	-0.02
142	SLU 80	-1004	-649	4891	18.5	-21.37	-0.02
142	SLU 81	-1061	-689	5173	19.72	-22.56	-0.02
142	SLU 82	-1061	-689	5173	19.72	-22.56	-0.02
142	SLU 83	-1061	-689	5173	19.72	-22.56	-0.02
142	SLU 84	-1061	-689	5173	19.72	-22.56	-0.02
142	SLE RA 1	-651	-416	3176	11.73	-13.9	-0.01
142	SLE RA 2	-651	-416	3176	11.73	-13.9	-0.01
142	SLE RA 3	-651	-416	3176	11.73	-13.9	-0.01
142	SLE RA 4	-651	-416	3176	11.73	-13.9	-0.01
142	SLE RA 5	-651	-416	3176	11.73	-13.9	-0.01
142	SLE RA 6	-651	-416	3176	11.73	-13.9	-0.01
142	SLE RA 7	-651	-416	3176	11.73	-13.9	-0.01
142	SLE RA 8	-651	-416	3176	11.73	-13.9	-0.01
142	SLE RA 9	-651	-416	3176	11.73	-13.9	-0.01
142	SLE RA 10	-741	-479	3615	13.64	-15.75	-0.01
142	SLE RA 11	-741	-479	3615	13.64	-15.75	-0.01
142	SLE RA 12	-741	-479	3615	13.64	-15.75	-0.01
142	SLE RA 13	-741	-479	3615	13.64	-15.75	-0.01
142	SLE RA 14	-741	-479	3615	13.64	-15.75	-0.01
142	SLE RA 15	-741	-479	3615	13.64	-15.75	-0.01
142	SLE RA 16	-741	-479	3615	13.64	-15.75	-0.01
142	SLE RA 17	-741	-479	3615	13.64	-15.75	-0.01
142	SLE RA 18	-779	-506	3803	14.46	-16.55	-0.01
142	SLE RA 19	-779	-506	3803	14.46	-16.55	-0.01
142	SLE RA 20	-779	-506	3803	14.46	-16.55	-0.01
142	SLE RA 21	-779	-506	3803	14.46	-16.55	-0.01
142	SLE FR 1	-651	-416	3176	11.73	-13.9	-0.01
142	SLE FR 2	-651	-416	3176	11.73	-13.9	-0.01
142	SLE FR 3	-651	-416	3176	11.73	-13.9	-0.01
142	SLE FR 4	-689	-443	3364	12.55	-14.7	-0.01
142	SLE FR 5	-689	-443	3364	12.55	-14.7	-0.01
142	SLE FR 6	-715	-461	3489	13.09	-15.23	-0.01
142	SLE QP 1	-651	-416	3176	11.73	-13.9	-0.01
142	SLE QP 2	-689	-443	3364	12.55	-14.7	-0.01
142	SLD 1	-450	-350	2605	9.06	-8.4	-0.31
142	SLD 2	-450	-350	2605	9.06	-8.4	-0.31
142	SLD 3	-498	-439	2939	12.39	-7.28	-0.61
142	SLD 4	-498	-439	2939	12.39	-7.28	-0.61
142	SLD 5	-545	-280	2631	6.46	-14.5	0.35
142	SLD 6	-545	-280	2631	6.46	-14.5	0.35
142	SLD 7	-704	-576	3742	17.55	-10.78	-0.65
142	SLD 8	-704	-576	3742	17.55	-10.78	-0.65
142	SLD 9	-675	-309	2986	7.55	-18.62	0.62
142	SLD 10	-675	-309	2986	7.55	-18.62	0.62
142	SLD 11	-833	-605	4097	18.64	-14.89	-0.38
142	SLD 12	-833	-605	4097	18.64	-14.89	-0.38
142	SLD 13	-881	-446	3789	12.7	-22.12	0.58
142	SLD 14	-881	-446	3789	12.7	-22.12	0.58
142	SLD 15	-929	-535	4122	16.03	-21	0.28
142	SLD 16	-929	-535	4122	16.03	-21	0.28
142	SLV 1	-124	-225	1571	4.34	0.13	-0.76
142	SLV 2	-124	-225	1571	4.34	0.13	-0.76
142	SLV 3	-236	-433	2355	12.15	2.88	-1.52
142	SLV 4	-236	-433	2355	12.15	2.88	-1.52
142	SLV 5	-349	-61	1636	-1.77	-14.42	0.92
142	SLV 6	-349	-61	1636	-1.77	-14.42	0.92
142	SLV 7	-724	-757	4251	24.28	-5.26	-1.62
142	SLV 8	-724	-757	4251	24.28	-5.26	-1.62
142	SLV 9	-654	-129	2477	0.81	-24.14	1.6
142	SLV 10	-654	-129	2477	0.81	-24.14	1.6
142	SLV 11	-1030	-825	5091	26.86	-14.98	-0.95
142	SLV 12	-1030	-825	5091	26.86	-14.98	-0.95
142	SLV 13	-1142	-452	4372	12.94	-32.27	1.49
142	SLV 14	-1142	-452	4372	12.94	-32.27	1.49
142	SLV 15	-1255	-661	5157	20.76	-29.52	0.73
142	SLV 16	-1255	-661	5157	20.76	-29.52	0.73



1.3 Risposta modale

Modo: identificativo del modo di vibrare.

Periodo: periodo. [s]

Massa X: massa partecipante in direzione globale X. Il valore è adimensionale.

Massa Y: massa partecipante in direzione globale Y. Il valore è adimensionale.

Massa Z: massa partecipante in direzione globale Z. Il valore è adimensionale.

Massa rot. X: massa rotazionale partecipante attorno la direzione globale X. Il valore è adimensionale.

Massa rot. Y: massa rotazionale partecipante attorno la direzione globale Y. Il valore è adimensionale.

Massa rot. Z: massa rotazionale partecipante attorno la direzione globale Z. Il valore è adimensionale.

Massa sX: massa partecipante in direzione Sisma X. Il valore è adimensionale.

Massa sY: massa partecipante in direzione Sisma Y. Il valore è adimensionale.

Totale masse partecipanti:

Traslazione X: 0.937007

Traslazione Y: 0.931864

Traslazione Z: 0

Rotazione X: 0.879963

Rotazione Y: 0.902493

Rotazione Z: 0.919148

Modo	Periodo	Massa X	Massa Y	Massa Z	Massa rot. X	Massa rot. Y	Massa rot. Z	Massa sX	Massa sY
1	3.299107677	0.006312172	0.000093017	0	0.000094144	0.015655775	0.000480113	0.006312172	0.000093017
2	2.768233509	0.061829309	0.000001696	0	0.000001631	0.156919073	0.001075187	0.061829309	0.000001696
3	1.731863846	0.000006734	0.047796826	0	0.035220486	0.000032293	0.043728469	0.000006734	0.047796826
4	1.620438128	0.001555659	0.014413384	0	0.007518021	0.003293468	0.0071734	0.001555659	0.014413384
5	1.461561265	0.005700279	0.277914548	0	0.207114724	0.011859643	0.273822458	0.005700279	0.277914548
6	1.435188677	0.005305838	0.033503786	0	0.019613307	0.011831084	0.036927479	0.005305838	0.033503786
7	1.361259022	0.000362573	0.013902231	0	0.011021793	0.001141899	0.018322256	0.000362573	0.013902231
8	1.258819097	0.036727491	0.003657943	0	0.002768363	0.089024106	0.000899437	0.036727491	0.003657943
9	1.195896758	0.0098892	0.001802384	0	0.000855998	0.025083125	0.002787684	0.0098892	0.001802384
10	1.176103922	0.008659251	0.052020851	0	0.055967348	0.007353935	0.045680003	0.008659251	0.052020851
11	1.132557871	0.000729113	0.045133859	0	0.049780514	0.000100836	0.046244808	0.000729113	0.045133859
12	1.09606536	0.008352286	0.009706845	0	0.033207581	0.018220393	0.011600128	0.008352286	0.009706845
13	1.082395246	0.000582352	0.002928254	0	0.009315244	0.009233868	0.0020188	0.000582352	0.002928254
14	1.05605522	0.074712324	0.000319481	0	0.001520352	0.091778172	0.000739355	0.074712324	0.000319481
15	0.940831388	0.000004603	0.001404737	0	0.003051127	0.000046217	0.000853006	0.000004603	0.001404737
16	0.901212097	0.001359676	0.000073858	0	0.000329105	0.008308586	0.000523125	0.001359676	0.000073858
17	0.857060377	0.005421483	0.000180236	0	0.000506361	0.025828719	0.000201593	0.005421483	0.000180236
18	0.7791198	0.001355508	0.003219717	0	0.001797203	0.002127142	0.004434855	0.001355508	0.003219717
19	0.742930135	0.002934398	0.0045775	0	0.00456317	0.004655684	0.001731252	0.002934398	0.0045775
20	0.695696589	0.008282042	0.001675523	0	0.000463773	0.013307536	0.002241333	0.008282042	0.001675523
21	0.688277627	0.004135128	0.00021667	0	0.000001758	0.006281919	0.000231149	0.004135128	0.00021667
22	0.644811497	0.000172588	0.000092773	0	0.000055055	0.000156054	0.000189307	0.000172588	0.000092773
23	0.639385355	0.000672047	0.000000621	0	0.000002373	0.000735519	0.000000095	0.000672047	0.000000621
24	0.629433865	0.000185854	0.006828415	0	0.0008774157	0.000478992	0.006356793	0.000185854	0.006828415
25	0.625873145	0.002826338	0.000816286	0	0.000578924	0.002553129	0.000844409	0.002826338	0.000816286
26	0.605558984	0.005205954	0.000804561	0	0.000910454	0.000077068	0.002191964	0.005205954	0.000804561
27	0.593504601	0.003502403	0.00015043	0	0.00015359	0.000081007	0.000275506	0.003502403	0.00015043
28	0.579891992	0.00172621	0.00313937	0	0.0002761421	0.002704581	0.001795094	0.00172621	0.00313937
29	0.570533393	0.006024606	0.005397077	0	0.002454243	0.002993267	0.006907974	0.006024606	0.005397077
30	0.548665804	0.002047583	0.014751193	0	0.001252387	0.000494018	0.01388993	0.002047583	0.014751193
31	0.534185856	0.011759926	0.0000224	0	0.000528252	0.004813239	0.000582572	0.011759926	0.0000224
32	0.511495018	0.001802401	0.000991837	0	0.002794915	0.000484171	0.001416041	0.001802401	0.000991837
33	0.483828487	0.013685539	0.000039489	0	0.000875334	0.003006069	0.000396897	0.013685539	0.000039489
34	0.474090516	0.000046099	0.009271194	0	0.003200711	0.000015798	0.008212756	0.000046099	0.009271194
35	0.459073334	0.014705563	0.000011989	0	0.000076045	0.004704514	0.000448625	0.014705563	0.000011989
36	0.43903978	0.000800672	0.000883867	0	0.000388102	0.000264651	0.000589643	0.000800672	0.000883867
37	0.398280962	0.000425984	0.000648669	0	0.000452593	0.000653618	0.000176009	0.000425984	0.000648669
38	0.377635306	0.001144138	0.000228438	0	0.000027089	0.002448817	0.000362104	0.001144138	0.000228438
39	0.336304404	0.010903861	0.000003029	0	0.00031579	0.003090409	0.000381869	0.010903861	0.000003029
40	0.32332217	0.000252992	0.003503144	0	0.000419512	0.000062162	0.003820114	0.000252992	0.003503144
41	0.295953111	0.014591655	0.000591686	0	0.000003321	0.00281755	0.001708563	0.014591655	0.000591686
42	0.277987828	0.002270641	0.006421273	0	0.002402651	0.000697539	0.005044671	0.002270641	0.006421273
43	0.254346643	0.016834527	0.000898362	0	0.000989402	0.017947279	0.002226213	0.016834527	0.000898362
44	0.240955777	0.003708597	0.009495234	0	0.006648674	0.005169905	0.007346833	0.003708597	0.009495234
45	0.198432656	0.01094146	0.000785001	0	0.000139807	0.003994633	0.001947423	0.01094146	0.000785001
46	0.193192156	0.001182453	0.009158063	0	0.005625625	0.000079133	0.007617353	0.001182453	0.009158063
47	0.1454171	0.021077689	0.002865781	0	0.001059454	0.011812365	0.005409163	0.021077689	0.002865781
48	0.139286019	0.002427372	0.017490558	0	0.000126607	0.000703807	0.015295786	0.002427372	0.017490558
49	0.090738945	0.040166152	0.002769914	0	0.001044623	0.030636505	0.006867863	0.040166152	0.002769914
50	0.082653846	0.002749516	0.030717671	0	0.029613348	0.001713892	0.027308925	0.002749516	0.030717671
51	0.048380226	0.075332691	0.063482853	0	0.085333452	0.042705805	0.082959551	0.075332691	0.063482853
52	0.044718563	0.049745071	0.220589971	0	0.270267501	0.029852402	0.179950452	0.049745071	0.220589971
53	0.040179041	0.373514929	0.004427262	0	0.004509445	0.22176748	0.024863793	0.373514929	0.004427262
54	0.015951572	0.00021178	0.000004027	0	0.000134834	0.000230259	0.000000213	0.00021178	0.000004027
55	0.013186762	0.000019335	0.000024135	0	0.000019629	0.000018113	0.000009202	0.000019335	0.000024135
56	0.012272427	0.000055233	0.000000102	0	0.000632538	0.000003483	0.000006848	0.000055233	0.000000102
57	0.011001525	0.000042143	0.000002372	0	0.000170803	0.000144268	0.000003752	0.000042143	0.000002372
58	0.010579522	0.000000724	0.000004603	0	0.000144129	0.000065272	0.00002331	0.000000724	0.000004603
59	0.009190349	0.000008728	0.000001233	0	0.000000002	0.000145511	0.000000227	0.000008728	0.000001233
60	0.008011747	0.000018411	0.000005362	0	0.00041403	0.000086911	0.000003926	0.000018411	0.000005362



1.4 Equilibrio globale forze

Contributo: Nome attribuito al sistema risultante.

Fx: Componente X di forza del sistema risultante. [daN]

Fy: Componente Y di forza del sistema risultante. [daN]

Fz: Componente Z di forza del sistema risultante. [daN]

Mx: Componente di momento attorno l'asse X del sistema risultante. [daN*m]

My: Componente di momento attorno l'asse Y del sistema risultante. [daN*m]

Mz: Componente di momento attorno l'asse Z del sistema risultante. [daN*m]

Bilancio in condizione di carico: Pesi strutturali

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	0	-225489.54	-1036837.42	6907855.33	0
Reazioni	0	0	225489.54	1036837.42	-6907855.33	0
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

Bilancio in condizione di carico: Permanenti portati

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	0	-51430.53	-241718.95	1572291.71	0
Reazioni	0	0	51430.53	241718.95	-1572291.71	0
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

Bilancio in condizione di carico: Variabile A

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	0	-58257.151	-270810.36	1784297.1	0
Reazioni	0	0	58257.151	270810.36	-1784297.1	0
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

Bilancio in condizione di carico: Sisma X SLV

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	72292.619	0	0	0	287211.93	-337018.89
Reazioni	-72292.619	0	0	0	-287211.93	337018.89
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

Bilancio in condizione di carico: Sisma Y SLV

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	32909.046	0	-130744.62	0	1007598.83
Reazioni	0	-32909.046	0	130744.62	0	-1007598.83
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

Bilancio in condizione di carico: Sisma X SLD

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	30675.666	0	0	0	121871.6	-143006.01
Reazioni	-30675.666	0	0	0	-121871.6	143006.01
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

Bilancio in condizione di carico: Sisma Y SLD

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	12827.635	0	-50963.01	0	392752.48
Reazioni	0	-12827.635	0	50963.01	0	-392752.48
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

Bilancio in condizione di carico: Rig Ux

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	0	0	0	0	0
Reazioni	0	0	0	0	0	0
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

Bilancio in condizione di carico: Rig Uy

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	0	0	0	0	0
Reazioni	0	0	0	0	0	0
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

Bilancio in condizione di carico: Rig Rz

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	0	0	0	0	0
Reazioni	0	0	0	0	0	0
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0



1.5 Risposta di spettro

Spettro: condizione elementare corrispondente allo spettro.
N.b.: nome breve della condizione elementare.
Fx: componente della forza lungo l'asse X. [daN]
Fy: componente della forza lungo l'asse Y. [daN]
Fz: componente della forza lungo l'asse Z. [daN]
Mx: componente della coppia attorno all'asse X. [daN*m]
My: componente della coppia attorno all'asse Y. [daN*m]
Mz: componente della coppia attorno all'asse Z. [daN*m]
Max X: massima reazione lungo l'asse X.
Valore: valore massimo della reazione. [daN]
Angolo: angolo d'ingresso del sisma che provoca il valore massimo della reazione. [deg]
Max Y: massima reazione lungo l'asse Y.
Valore: valore massimo della reazione. [daN]
Angolo: angolo d'ingresso del sisma che provoca il valore massimo della reazione. [deg]
Max Z: massima reazione lungo l'asse Z.
Valore: valore massimo della reazione. [daN]
Angolo: angolo d'ingresso del sisma che provoca il valore massimo della reazione. [deg]

Spettro N.b.	Fx	Fy	Fz	Mx	My	Mz	Max X		Max Y		Max Z	
							Valore	Angolo	Valore	Angolo	Valore	Angolo
SLV X	32423.11	5764.95	0	2.130E04	85383.991	2.387E05	32423.11	0	24142.89	85	0	0
SLV Y	5764.95	24072.02	0	8.392E04	15460.385	7.307E05	32423.11	0	24142.89	85	0	0
X SLD	13722.55	2447.36	0	9046.6894	3.602E04	1.013E05	13722.55	0	10029.53	85	0	0
Y SLD	2447.36	9996.07	0	3.509E04	6532.9241	3.031E05	13722.55	0	10029.53	85	0	0

1.6 Annotazioni solutore

Informazioni: informazioni fornite dal solutore al termine del calcolo del modello.

Informazioni

1.7 Statistiche soluzione

Tipo di equazioni	Lineari
Tecnica di soluzione	Intel MKL PARDISO
Numero equazioni	14610
Elemento min. diagonale	1254.68396072
Elemento max diagonale	587038963.146967
Rapporto max/min	467877.95295624
Elementi non nulli	394123

TABULATI DI CALCOLO – VERIFICHE
CIVICO 35
STATO DI FATTO



Sommario

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1 Verifiche

1.1 Verifica regolarità strutturale

Le unità di misura elencate nel capitolo sono in [m, daN] ove non espressamente specificato.

Livello:

Descr: descrizione livello.

Quota: quota livello. [m]

Q: quota livello. [m]

Qinf: quota livello precedente. [m]

Comb: combinazione.

A1: a1 (Distribuzione masse).

A1n: a1 numeratore (distanza tra centro massa vs. centro rigidezza [se presente] o centro dell'ingombro del piano). [m]

A1d: a1 denominatore (ingombro del piano nella medesima direzione [x o y globale]). [m]

A1r: a1 rapporto (distanza centro massa/rigidezza su ingombro del piano).

A2: a2 (Distribuzione rigidezze).

A2n: a2 numeratore (rigidezza max [x o y globale]).

A2d: a2 denominatore (rigidezza min [x o y globale]).

A2r: a2 rapporto (rigidezza max/min).

A3: a3 (Forma compatta).

A3n: a3 numeratore (area convessa). [m²]

A3d: a3 denominatore (area piano). [m²]

A3r: a3 rapporto (area convessa/area piano).

B: b (Rapporto lati).

Bn: b numeratore (lato max [x o y globale]). [m]

Bd: b denominatore (lato min [x o y globale]). [m]

Br: b rapporto (lato max/min).

C: c (Rapporto rigidezze piano).

Cn: c numeratore (rigidezza elementi verticali).

Cd: c denominatore (rigidezza piano).

Cr: c rapporto (rigidezza elementi verticali/rigidezza piano).

E1: e1 (Variazione masse).

E1n: e1 numeratore (massa max). [daN]

E1d: e1 denominatore (massa min). [daN]

E1r: e1 rapporto (massa max/min).

E2: e2 (Riduzione rigidezze).

E2n: e2 numeratore (rigidezza relativa alla traslazione KUmax). [daN/m]

E2d: e2 denominatore (rigidezza relativa alla traslazione KUmin). [daN/m]

E2r: e2 rapporto (variazione massima in decremento Kmax/Kmin).

E3: e3 (Incremento rigidezze).

E3n: e3 numeratore (rigidezza relativa alla traslazione KUmax). [daN/m]

E3d: e3 denominatore (rigidezza relativa alla traslazione KUmin). [daN/m]

E3r: e3 rapporto (variazione massima in incremento Kmax/Kmin).

F: f (Rapporto Capacità/Domanda).

Fn: f numeratore (rapporto capacità/domanda massimo [c/d max]). [daN]

Fd: f denominatore (rapporto capacità/domanda minimo [c/d min]). [daN]

Fr: f rapporto (variazione massima [rapporto (c/d max)/(c/d min)]).

G1: g1 (Rastremazione di piano).

G1n: g1 numeratore (L1). [m]

G1d: g1 denominatore (L2). [m]

G1r: g1 rapporto (L1/L2).

G2: g2 (Rastremazione totale).

G2n: g2 numeratore (L0). [m]

G2d: g2 denominatore (Li). [m]

G2r: g2 rapporto (L0/Li).

Capacità/Domanda in X:

VrdX: taglio resistente complessivo in direzione X. [daN]

VedX: taglio agente complessivo in direzione X. [daN]

|Rd/Ed|: |Rd/Ed| (rapporto capacità/domanda in termini di resistenza a taglio).

Capacità/Domanda in Y:

VrdY: taglio resistente complessivo in direzione Y. [daN]

VedY: taglio agente complessivo in direzione Y. [daN]

Verifica regolarità strutturale

Controllo regolarità edificio secondo D.M. 17-01-18 (N.T.C.) §7.2.1 - §C7.2.1

Avvertenze

La seguente procedura valuta la regolarità della costruzione secondo quanto indicato nelle NTC 2018 §7.2.1.

Tali valutazioni sono a carattere puramente informativo e vengono condotte sulla base del modello e delle verifiche presenti alla sua generazione, con le limitazioni



indicate nella manualistica.

In ogni caso l'impostazione di regolarità della costruzione, in pianta ed elevazione, va indicata nelle preferenze di analisi dall'utente utilizzatore del software.

Sintesi dei risultati

Orizzontamenti considerati nella valutazione

Nessun livello di fondazione trovato

Livelli di elevazione considerati: Rialzato(L2), Primo(L3),

Regolarità in pianta - NO

L'edificio risulta NON regolare in pianta, in base alle condizioni indicate in NTC 2018 §7.2.1

Ok - Criterio A1 (Distribuzione masse) rispettato, con rapporto massimo 0 (limite=0,2) al livello Primo

N.V. - Criterio A2 (Distribuzione rigidezze) non valutabile al livello Rialzato

Ok - Criterio A3 (Forma compatta) rispettato, con rapporto massimo 1 (limite=1,05) al livello Rialzato

Ok - Criterio B (Rapporto lati) rispettato, con rapporto massimo 1 (limite=4) al livello Rialzato

No - Criterio C (Rapporto rigidezze piano) NON rispettato, con rapporto massimo > 999 (limite=0) al livello Rialzato

Regolarità in altezza - NO

L'edificio risulta NON regolare in altezza, in base alle condizioni indicate in NTC 2018 §7.2.1

Ok - Criterio D (Altezza elementi sismoresistenti) rispettato, con rapporto massimo 1 (limite=1,01)

Ok - Criterio E1 (Variazione masse) rispettato, con rapporto massimo 1,04 (limite=1,25) tra il livello Primo ed il precedente

N.V. - Criterio E2 (Riduzione rigidezze) non valutabile tra il livello Primo ed il precedente

N.V. - Criterio E3 (Incremento rigidezze) non valutabile tra il livello Primo ed il precedente

No - Criterio F (Rapporto Capacità/Domanda) NON rispettato, con rapporto massimo 60.2/7.4=8.2 (limite=1,3) tra il livello Primo ed il precedente

Ok - Criterio G1 (Rastremazione di piano) rispettato, con rapporto massimo 0,01 (limite=0,1) tra il livello Primo ed il precedente

Ok - Criterio G2 (Rastremazione totale) rispettato, con rapporto massimo 0,01 (limite=0,3) tra il livello Primo ed il precedente

Valori per piano

Verifiche di regolarità in pianta

Livello		A1			A2			A3			B			C		
Descr	Quota	A1n	A1d	A1r	A2n	A2d	A2r	A3n	A3d	A3r	Bn	Bd	Br	Cn	Cd	Cr
Rialzato	1.67	0.02	10.08	0				101.4919	101.4919	1	10.12	10.08	1	9999		9999
Primo	5.52	0.03	10.08	0				100.704	100.704	1	10.08	10.05	1	9999		9999

Verifiche di regolarità in elevazione

Rapporto di regolarità per la condizione D (Altezza elementi sismoresistenti): 3.85/3.85=0.01.

Livello			E1			E2			E3			F			G1			G2		
Descr	Q	Qinf	E1n	E1d	E1r	E2n	E2d	E2r	E3n	E3d	E3r	Fn	Fd	Fr	G1n	G1d	G1r	G2n	G2d	G2r
Primo	5.52	1.67	70694	67695	1.04							60.2	7.4	8.16	0.08	10.12	0.01	0.08	10.12	0.01

Dettaglio delle resistenze di piano a taglio (per valutazione punto F)

Livello			Capacità/Domanda in X			Capacità/Domanda in Y		
Descr	Q	Comb	VrdX	VedX	Rd/Ed	VrdY	VedY	Rd/Ed
Rialzato	1.67	SLV 1	100973	-32307	3.1	76873	-10237	7.5
Rialzato	1.67	SLV 2	100973	-32307	3.1	76873	-10237	7.5
Rialzato	1.67	SLV 3	100978	-31746	3.2	77721	9131	8.5
Rialzato	1.67	SLV 4	100978	-31746	3.2	77721	9131	8.5
Rialzato	1.67	SLV 5	101805	-10543	9.7	77096	-32446	2.4
Rialzato	1.67	SLV 6	101805	-10543	9.7	77096	-32446	2.4
Rialzato	1.67	SLV 7	101824	-8673	11.7	76502	32115	2.4
Rialzato	1.67	SLV 8	101824	-8673	11.7	76502	32115	2.4
Rialzato	1.67	SLV 9	102525	8673	11.8	77781	-32115	2.4
Rialzato	1.67	SLV 10	102525	8673	11.8	77781	-32115	2.4
Rialzato	1.67	SLV 11	102543	10543	9.7	75505	32446	2.3
Rialzato	1.67	SLV 12	102543	10543	9.7	75505	32446	2.3
Rialzato	1.67	SLV 13	103370	31746	3.3	76636	-9131	8.4
Rialzato	1.67	SLV 14	103370	31746	3.3	76636	-9131	8.4
Rialzato	1.67	SLV 15	103376	32307	3.2	75548	10237	7.4
Rialzato	1.67	SLV 16	103376	32307	3.2	75548	10237	7.4
Primo	5.52	SLV 1	54941	-5887	9.3	61926	-1032	60
Primo	5.52	SLV 2	54941	-5887	9.3	61926	-1032	60
Primo	5.52	SLV 3	55100	-5967	9.2	61889	3525	17.6
Primo	5.52	SLV 4	55100	-5967	9.2	61889	3525	17.6
Primo	5.52	SLV 5	54127	-1646	32.9	62113	-7221	8.6
Primo	5.52	SLV 6	54127	-1646	32.9	62113	-7221	8.6
Primo	5.52	SLV 7	52762	-1911	27.6	62013	7969	7.8
Primo	5.52	SLV 8	52762	-1911	27.6	62013	7969	7.8
Primo	5.52	SLV 9	50521	1911	26.4	62245	-7969	7.8
Primo	5.52	SLV 10	50521	1911	26.4	62245	-7969	7.8
Primo	5.52	SLV 11	50133	1646	30.5	62009	7221	8.6
Primo	5.52	SLV 12	50133	1646	30.5	62009	7221	8.6
Primo	5.52	SLV 13	44092	5967	7.4	62238	-3525	17.7
Primo	5.52	SLV 14	44092	5967	7.4	62238	-3525	17.7
Primo	5.52	SLV 15	44561	5887	7.6	62170	1032	60.2
Primo	5.52	SLV 16	44561	5887	7.6	62170	1032	60.2

1.2 Verifica sismica globale

Desc.: descrizione.

Stato limite: (muratura) V=Taglio; PF=Pressoflessione; PFFP=Pressoflessione fuori piano; R=Ribaltamento.



Molt.: moltiplicatore minimo della azione sismica che produce lo stato limite.

Comb.: combinazione.

PGA: accelerazione al suolo.

iPGA (ZE): indicatore di rischio sismico in termini di PGA ovvero rapporto tra l'azione sismica massima sopportabile dall'elemento e l'azione sismica massima che si utilizzerebbe nel progetto nuovo (§C8.3).

TR: tempo di ritorno.

(TR/TRrif)^.41: indicatore di rischio sismico in termini di periodo di ritorno.

fa: fattore di accelerazione.

Stato limite: (muratura) V=Taglio; PF=Presso flessione; PFFP=Pressoflessione fuori piano; R=Ribaltamento.

Coeff.s.: coefficiente minimo prodotto dallo stato limite.

Verifica: stato di verifica.

Maschio: maschio.

Stato limite: (maschio muratura) V=Taglio; PF=Presso flessione; PFFP=Presso flessione fuori piano; R=Ribaltamento.

Trave: trave di collegamento in muratura.

Stato limite: (trave muratura) V=Taglio; F=Flessione.

S. L.: stato limite di riferimento.

TR,C: periodo di ritorno di capacità.

PGA,C: accelerazione di aggancio di capacità.

TR,Rif: periodo di ritorno di riferimento.

PGA,Rif: accelerazione di aggancio di riferimento.

Tipo rottura: tipo di rottura che fornisce il valore minimo degli elementi considerati.

PAM: perdita media annua attesa.

Classe PAM: classe di rischio PAM.

IS-V: indice di sicurezza.

Classe IS-V: classe di rischio IS-V.

Verifica di elementi dotati di indicatori di rischio sismico mediante analisi con fattore q

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.) § C8.7.1

Accelerazioni e tempi di ritorno

Accelerazione di aggancio SLO (ag/g_SLO*S*ST) PGA,SLOrif = 0.081

Accelerazione di aggancio SLD (ag/g_SLD*S*ST) PGA,SLDrif = 0.101

Accelerazione di aggancio SLV (ag/g_SLV*S*ST) PGA,SLVrif = 0.244

Tr,SLOrif = 30 anni

Tr,SLDrif = 50 anni

Tr,SLVrif = 475 anni

Moltiplicatori minimi delle condizioni sismiche

(Il valore di ZE corrisponde al valore di I.R. PGA secondo quanto riportato nella Circolare 7 21-01-19 §C8.3)

Rottura a taglio

Moltiplicatore: 0

Trave di accoppiamento 3

Lunghezza: 1; altezza: 1.39; spessore: 0.45; distanza: 0

Combinazione SLV 1 V = -1882 V orto = 0 Vp = 4419 Vt = 5213

Tempo di ritorno 0 anni

Indicatore iTr = (Tr/Tr,SLVrif)^.41 = 0

PGA 0

Indicatore iPGA = PGA/PGA,SLVrif = 0

Fattore di accelerazione fa = 0

Rottura a flessione

Moltiplicatore: 0.032

Maschio 17

Lunghezza: 0.13; altezza: 3.85; spessore: 0.3 sezione a quota 3.67

Combinazione SLV 1 N = -136 M = 8.6 σ0 = 3478 fd = 143750 Mu = 8.63

Tempo di ritorno 0 anni

Indicatore iTr = (Tr/Tr,SLVrif)^.41 = 0

PGA 0

Indicatore iPGA = PGA/PGA,SLVrif = 0

Fattore di accelerazione fa = 0

Rottura a pressoflessione nel piano ortogonale

Moltiplicatore: 0.052

Maschio 17

Lunghezza: 0.13; altezza: 3.85; spessore: 0.3; sezione a quota: 3.595

Combinazione SLV 1 fd = 143750 Ta = 0.08 Wa = 540 N = -9 M = 1.11 Mc = 1.35

Tempo di ritorno 0 anni

Indicatore iTr = (Tr/Tr,SLVrif)^.41 = 0

PGA 0

Indicatore iPGA = PGA/PGA,SLVrif = 0

Fattore di accelerazione fa = 0



Rottura per meccanismi locali di collasso

Moltiplicatore: 0.05

Maschio 17

Lunghezza: 0.13; altezza: 3.85; spessore: 0.3 f.agg.= 0 a.lim.= 3.145145

Combinazione SLV 1 N top= -66 N base= -731 T orto= 6 α_0 = 0.033 M*= 31 e*= 0.901 a0*= 0.2677

Tempo di ritorno 0 anni

Indicatore iTr=(Tr/Tr,SLVrif)^.41 = 0

PGA 0

Indicatore iPGA=PGA/PGA,SLVrif = 0

Fattore di accelerazione fa = 0

Indicatori minimi riferiti al solo materiale muratura

Desc.	Stato limite	Molt.	Comb.	PGA	iPGA (ZE)	TR	(TR/Trrif)^.41	fa
Maschio 17	PF	0.032	SLV 1	0	0	0	0	0
Maschio 17	V	0.032	SLV 1	0	0	0	0	0
Maschio 17	PFFP	0.052	SLV 1	0	0	0	0	0
Maschio 17	R	0.05	SLV 1	0	0	0	0	0
Trave di accoppiamento 2	PF	0.999	SLV 15	0.244	0.9987	473	0.9983	0.9984
Trave di accoppiamento 3	V	0	SLV 1	0	0	0	0	0

Coefficienti di sicurezza riferiti al solo materiale muratura

Desc.	Stato limite	Coeff.s.	Comb.	Verifica
Maschio 1	PF SLU	16.627	SLU 39	Si
Maschio 1	V SLU	542.147	SLU 81	Si
Maschio 1	PF	3.59	SLV 15	Si
Maschio 1	V	2.725	SLV 7	Si
Maschio 1	PFFP	9.521	SLV 15	Si
Maschio 1	R	0.127	SLV 1	No
Maschio 2	PF SLU	1.642	SLU 81	Si
Maschio 2	V SLU	3.438	SLU 81	Si
Maschio 2	PF	0	SLV 1	No
Maschio 2	V	0	SLV 1	No
Maschio 2	PFFP	2.778	SLV 9	Si
Maschio 2	R	0	SLV 16	No
Maschio 3	PF SLU	4.478	SLU 81	Si
Maschio 3	V SLU	13.666	SLU 81	Si
Maschio 3	PF	0.904	SLV 1	No
Maschio 3	V	0	SLV 1	No
Maschio 3	PFFP	9.145	SLV 9	Si
Maschio 3	R	0	SLV 16	No
Maschio 4	PF SLU	5.215	SLU 81	Si
Maschio 4	V SLU	10.585	SLU 81	Si
Maschio 4	PF	4.324	SLV 7	Si
Maschio 4	V	2.468	SLV 3	Si
Maschio 4	PFFP	12.48	SLV 11	Si
Maschio 4	R	0.14	SLV 13	No
Maschio 5	PF SLU	123.342	SLU 39	Si
Maschio 5	V SLU	166.226	SLU 81	Si
Maschio 5	PF	14.005	SLV 15	Si
Maschio 5	V	2.585	SLV 15	Si
Maschio 5	PFFP	13.79	SLV 7	Si
Maschio 5	R	0	SLV 5	No
Maschio 6	PF SLU	4.957	SLU 81	Si
Maschio 6	V SLU	10.59	SLU 81	Si
Maschio 6	PF	3.559	SLV 3	Si
Maschio 6	V	2.522	SLV 15	Si
Maschio 6	PFFP	12.776	SLV 7	Si
Maschio 6	R	0.136	SLV 13	No
Maschio 7	PF SLU	10.951	SLU 39	Si
Maschio 7	V SLU	3.306	SLU 81	Si
Maschio 7	PF	5.304	SLV 13	Si
Maschio 7	V	1.861	SLV 3	Si
Maschio 7	PFFP	13.973	SLV 11	Si
Maschio 7	R	0	SLV 5	No
Maschio 8	PF SLU	5.729	SLU 81	Si
Maschio 8	V SLU	2.447	SLU 81	Si
Maschio 8	PF	4.18	SLV 3	Si
Maschio 8	V	1.728	SLV 13	Si
Maschio 8	PFFP	15.044	SLV 11	Si
Maschio 8	R	0.009	SLV 7	No
Maschio 10	PF SLU	21.28	SLU 39	Si
Maschio 10	V SLU	6.286	SLU 81	Si
Maschio 10	PF	4.435	SLV 1	Si
Maschio 10	V	2.043	SLV 1	Si
Maschio 10	PFFP	11.206	SLV 5	Si
Maschio 10	R	0	SLV 5	No
Maschio 11	PF SLU	32.447	SLU 64	Si
Maschio 11	V SLU	5.922	SLU 81	Si
Maschio 11	PF	5.036	SLV 1	Si
Maschio 11	V	2.495	SLV 13	Si
Maschio 11	PFFP	14.61	SLV 5	Si
Maschio 11	R	0.1	SLV 1	No
Maschio 12	PF SLU	6.725	SLU 81	Si
Maschio 12	V SLU	9.738	SLU 81	Si
Maschio 12	PF	4.281	SLV 7	Si
Maschio 12	V	2.587	SLV 5	Si
Maschio 12	PFFP	11.451	SLV 3	Si
Maschio 12	R	0.145	SLV 13	No
Maschio 13	PF SLU	150.213	SLU 81	Si



Desc.	Stato limite	Coeff.s.	Comb.	Verifica
Maschio 13	V SLU	328.404	SLU 39	Si
Maschio 13	PF	11.2	SLV 5	Si
Maschio 13	V	2.654	SLV 7	Si
Maschio 13	PFFP	13.112	SLV 1	Si
Maschio 13	R	0.133	SLV 13	No
Maschio 14	PF SLU	6.88	SLU 81	Si
Maschio 14	V SLU	10.279	SLU 81	Si
Maschio 14	PF	4.793	SLV 5	Si
Maschio 14	V	2.632	SLV 7	Si
Maschio 14	PFFP	11.47	SLV 1	Si
Maschio 14	R	0.136	SLV 15	No
Maschio 15	PF SLU	13.991	SLU 39	Si
Maschio 15	V SLU	1000	SLU 1	Si
Maschio 15	PF	2.512	SLV 15	Si
Maschio 15	V	2.979	SLV 7	Si
Maschio 15	PFFP	1.497	SLV 1	Si
Maschio 15	R	0.068	SLV 13	No
Maschio 16	PF SLU	9.806	SLU 43	Si
Maschio 16	V SLU	37.388	SLU 64	Si
Maschio 16	PF	0	SLV 16	No
Maschio 16	V	0	SLV 1	No
Maschio 16	PFFP	0	SLV 16	No
Maschio 16	R	0	SLV 10	No
Maschio 17	PF SLU	4.414	SLU 39	Si
Maschio 17	V SLU	20.063	SLU 81	Si
Maschio 17	PF	0	SLV 16	No
Maschio 17	V	0	SLV 1	No
Maschio 17	PFFP	0	SLV 10	No
Maschio 17	R	0	SLV 16	No
Maschio 18	PF SLU	2.098	SLU 39	Si
Maschio 18	V SLU	1.857	SLU 39	Si
Maschio 18	PF	1.242	SLV 13	Si
Maschio 18	V	2.041	SLV 3	Si
Maschio 18	PFFP	0	SLV 5	No
Maschio 18	R	0	SLV 16	No
Maschio 19	PF SLU	8.73	SLU 43	Si
Maschio 19	V SLU	12.565	SLU 39	Si
Maschio 19	PF	4.165	SLV 1	Si
Maschio 19	V	5.29	SLV 13	Si
Maschio 19	PFFP	1.031	SLV 11	Si
Maschio 19	R	0.002	SLV 3	No
Maschio 20	PF SLU	2.44	SLU 43	Si
Maschio 20	V SLU	11.441	SLU 39	Si
Maschio 20	PF	1.551	SLV 15	Si
Maschio 20	V	3.276	SLV 15	Si
Maschio 20	PFFP	1.148	SLV 15	Si
Maschio 20	R	0.015	SLV 7	No
Maschio 21	PF SLU	7.364	SLU 39	Si
Maschio 21	V SLU	15.122	SLU 39	Si
Maschio 21	PF	5.852	SLV 13	Si
Maschio 21	V	5.944	SLV 13	Si
Maschio 21	PFFP	1.389	SLV 11	Si
Maschio 21	R	0.083	SLV 13	No
Maschio 22	PF SLU	6.971	SLU 43	Si
Maschio 22	V SLU	8.952	SLU 39	Si
Maschio 22	PF	3.313	SLV 13	Si
Maschio 22	V	5.023	SLV 1	Si
Maschio 22	PFFP	1.012	SLV 7	Si
Maschio 22	R	0	SLV 1	No
Maschio 23	PF SLU	4.226	SLU 81	Si
Maschio 23	V SLU	4.98	SLU 81	Si
Maschio 23	PF	1.9	SLV 7	Si
Maschio 23	V	1.502	SLV 9	Si
Maschio 23	PFFP	1.594	SLV 11	Si
Maschio 23	R	0.068	SLV 5	No
Maschio 24	PF SLU	10.058	SLU 81	Si
Maschio 24	V SLU	19.462	SLU 43	Si
Maschio 24	PF	4.094	SLV 9	Si
Maschio 24	V	1.744	SLV 5	Si
Maschio 24	PFFP	1.935	SLV 3	Si
Maschio 24	R	0.059	SLV 5	No
Maschio 25	PF SLU	3.988	SLU 81	Si
Maschio 25	V SLU	5.358	SLU 39	Si
Maschio 25	PF	2.191	SLV 5	Si
Maschio 25	V	1.678	SLV 7	Si
Maschio 25	PFFP	1.702	SLV 9	Si
Maschio 25	R	0.022	SLV 9	No
Maschio 26	PF SLU	32.541	SLU 43	Si
Maschio 26	V SLU	1000	SLU 1	Si
Maschio 26	PF	2.262	SLV 1	Si
Maschio 26	V	2.911	SLV 1	Si
Maschio 26	PFFP	0	SLV 13	No
Maschio 26	R	0.087	SLV 3	No
Maschio 27	PF SLU	1.753	SLU 60	Si
Maschio 27	V SLU	2.319	SLU 81	Si
Maschio 27	PF	1.057	SLV 15	Si
Maschio 27	V	0.517	SLV 15	No
Maschio 27	PFFP	0	SLV 1	No
Maschio 27	R	0.108	SLV 7	No
Maschio 28	PF SLU	3.7	SLU 81	Si
Maschio 28	V SLU	6.028	SLU 39	Si



Desc.	Stato limite	Coeff.s.	Comb.	Verifica
Maschio 28	PF	2.753	SLV 9	Si
Maschio 28	V	2.882	SLV 5	Si
Maschio 28	PFFP	1.72	SLV 3	Si
Maschio 28	R	0	SLV 5	No
Maschio 29	PF SLU	155.362	SLU 39	Si
Maschio 29	V SLU	259.876	SLU 64	Si
Maschio 29	PF	4.89	SLV 7	Si
Maschio 29	V	3.181	SLV 7	Si
Maschio 29	PFFP	2.031	SLV 1	Si
Maschio 29	R	0.028	SLV 13	No
Maschio 30	PF SLU	3.694	SLU 81	Si
Maschio 30	V SLU	6.247	SLU 39	Si
Maschio 30	PF	3.058	SLV 11	Si
Maschio 30	V	2.589	SLV 7	Si
Maschio 30	PFFP	1.632	SLV 1	Si
Maschio 30	R	0	SLV 5	No

Verifica maschi in muratura

Maschio	Stato limite	Molt.	Comb.	PGA	iPGA (ZE)	TR	(TR/TRrif)^.41	Verifica
1	PF	1.995	SLV 15	0.362	1.483	1618	1.653	Si
	V	2.002	SLV 15	0.362	1.483	1618	1.653	Si
	PFFP	2.383	SLV 15	0.362	1.483	1618	1.653	Si
	R	0.145	SLV 1	0.031	0.127	3	0.125	No
2	PF	0.183	SLV 11	0.051	0.21	10	0.205	No
	V	0.178	SLV 15	0.041	0.169	6	0.167	No
	PFFP	1.146	SLV 9	0.276	1.129	683	1.161	Si
	R	0.132	SLV 13	0.026	0.107	2	0.106	No
3	PF	0.892	SLV 1	0.217	0.888	346	0.878	No
	V	0.589	SLV 1	0.141	0.578	120	0.569	No
	PFFP	2.84	SLV 9	0.362	1.483	1618	1.653	Si
	R	0.143	SLV 1	0.031	0.127	3	0.125	No
4	PF	3.902	SLV 11	0.362	1.483	1618	1.653	Si
	V	2.612	SLV 3	0.362	1.483	1618	1.653	Si
	PFFP	3.685	SLV 11	0.362	1.483	1618	1.653	Si
	R	0.146	SLV 1	0.031	0.127	3	0.125	No
5	PF	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	2.527	SLV 3	0.362	1.483	1618	1.653	Si
	PFFP	3.84	SLV 7	0.362	1.483	1618	1.653	Si
	R	0.126	SLV 13	0.026	0.107	2	0.106	No
6	PF	3.555	SLV 7	0.362	1.483	1618	1.653	Si
	V	2.433	SLV 3	0.362	1.483	1618	1.653	Si
	PFFP	3.515	SLV 7	0.362	1.483	1618	1.653	Si
	R	0.145	SLV 13	0.031	0.127	3	0.125	No
7	PF	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	2.125	SLV 3	0.362	1.483	1618	1.653	Si
	PFFP	1000	SLV 1	0.362	1.483	1618	1.653	Si
	R	0.076	SLV 1	0	0	0	0	No
8	PF	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	2	SLV 13	0.362	1.483	1618	1.653	Si
	PFFP	1000	SLV 1	0.362	1.483	1618	1.653	Si
	R	0.076	SLV 1	0	0	0	0	No
10	PF	1.89	SLV 5	0.362	1.483	1618	1.653	Si
	V	1.696	SLV 1	0.362	1.483	1618	1.653	Si
	PFFP	2.281	SLV 5	0.362	1.483	1618	1.653	Si
	R	0.137	SLV 3	0.031	0.127	3	0.125	No
11	PF	4.032	SLV 5	0.362	1.483	1618	1.653	Si
	V	2.539	SLV 13	0.362	1.483	1618	1.653	Si
	PFFP	1000	SLV 1	0.362	1.483	1618	1.653	Si
	R	0.137	SLV 15	0.031	0.127	3	0.125	No
12	PF	3.559	SLV 3	0.362	1.483	1618	1.653	Si
	V	2.453	SLV 7	0.362	1.483	1618	1.653	Si
	PFFP	3.305	SLV 3	0.362	1.483	1618	1.653	Si
	R	0.151	SLV 13	0.035	0.143	4	0.141	No
13	PF	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	2.616	SLV 5	0.362	1.483	1618	1.653	Si
	PFFP	1000	SLV 1	0.362	1.483	1618	1.653	Si
	R	0.146	SLV 13	0.031	0.127	3	0.125	No
14	PF	3.611	SLV 1	0.362	1.483	1618	1.653	Si
	V	2.712	SLV 5	0.362	1.483	1618	1.653	Si
	PFFP	3.34	SLV 1	0.362	1.483	1618	1.653	Si
	R	0.149	SLV 15	0.031	0.127	3	0.125	No
15	PF	1.659	SLV 15	0.362	1.483	1618	1.653	Si
	V	1.676	SLV 15	0.362	1.483	1618	1.653	Si
	PFFP	1.36	SLV 1	0.331	1.354	1197	1.461	Si
	R	0.087	SLV 3	0.02	0.08	1	0.08	No
16	PF	0.038	SLV 15	0	0	0	0	No
	V	0.039	SLV 15	0	0	0	0	No
	PFFP	0.066	SLV 15	0	0	0	0	No
	R	0.07	SLV 5	0.02	0.08	1	0.08	No
17	PF	0.032	SLV 1	0	0	0	0	No
	V	0.032	SLV 1	0	0	0	0	No
	PFFP	0.052	SLV 1	0	0	0	0	No
	R	0.05	SLV 1	0	0	0	0	No
18	PF	1.196	SLV 13	0.291	1.192	802	1.24	Si
	V	1.2	SLV 13	0.292	1.196	810	1.245	Si
	PFFP	0.671	SLV 13	0.162	0.661	164	0.647	No
	R	0.091	SLV 5	0.026	0.107	2	0.106	No
19	PF	2.781	SLV 15	0.362	1.483	1618	1.653	Si
	V	2.571	SLV 15	0.362	1.483	1618	1.653	Si
	PFFP	1.025	SLV 11	0.25	1.022	507	1.027	Si
	R	0.096	SLV 1	0.02	0.08	1	0.08	No



Maschio	Stato limite	Molt.	Comb.	PGA	IPGA (ZE)	TR	(TR/TRrif)^.41	Verifica
20	PF	1.282	SLV 1	0.312	1.277	987	1.35	Si
	V	1.237	SLV 1	0.301	1.232	887	1.292	Si
	PFFP	1.127	SLV 11	0.272	1.112	653	1.139	Si
	R	0.1	SLV 3	0.02	0.08	1	0.08	No
21	PF	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	3.636	SLV 13	0.362	1.483	1618	1.653	Si
	PFFP	1.371	SLV 11	0.323	1.32	1103	1.413	Si
	R	0.103	SLV 3	0.02	0.08	1	0.08	No
22	PF	2.28	SLV 7	0.362	1.483	1618	1.653	Si
	V	2.199	SLV 3	0.362	1.483	1618	1.653	Si
	PFFP	1.009	SLV 7	0.246	1.008	486	1.009	Si
	R	0.096	SLV 1	0.02	0.08	1	0.08	No
23	PF	2.034	SLV 11	0.362	1.483	1618	1.653	Si
	V	1.287	SLV 7	0.305	1.25	926	1.315	Si
	PFFP	1.49	SLV 11	0.346	1.418	1394	1.555	Si
	R	0.078	SLV 5	0.02	0.08	1	0.08	No
24	PF	2.708	SLV 13	0.362	1.483	1618	1.653	Si
	V	1.727	SLV 7	0.362	1.483	1618	1.653	Si
	PFFP	1.637	SLV 3	0.362	1.483	1618	1.653	Si
	R	0.082	SLV 5	0.02	0.08	1	0.08	No
25	PF	2.485	SLV 9	0.362	1.483	1618	1.653	Si
	V	1.465	SLV 9	0.341	1.398	1330	1.525	Si
	PFFP	1.618	SLV 9	0.362	1.483	1618	1.653	Si
	R	0.075	SLV 7	0.02	0.08	1	0.08	No
26	PF	1.467	SLV 1	0.357	1.459	1533	1.617	Si
	V	1.329	SLV 1	0.323	1.323	1110	1.416	Si
	PFFP	0.877	SLV 15	0.213	0.873	331	0.862	No
	R	0.104	SLV 3	0.02	0.08	1	0.08	No
27	PF	1.123	SLV 15	0.274	1.121	668	1.15	Si
	V	0.873	SLV 15	0.212	0.868	326	0.857	No
	PFFP	0.945	SLV 5	0.232	0.95	415	0.946	No
	R	0.114	SLV 5	0.031	0.127	3	0.125	No
28	PF	3.324	SLV 7	0.362	1.483	1618	1.653	Si
	V	2.685	SLV 5	0.362	1.483	1618	1.653	Si
	PFFP	1.55	SLV 3	0.362	1.483	1618	1.653	Si
	R	0.087	SLV 3	0.02	0.08	1	0.08	No
29	PF	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	2.521	SLV 5	0.362	1.483	1618	1.653	Si
	PFFP	1.894	SLV 1	0.362	1.483	1618	1.653	Si
	R	0.084	SLV 1	0	0	0	0	No
30	PF	3.624	SLV 5	0.362	1.483	1618	1.653	Si
	V	2.547	SLV 7	0.362	1.483	1618	1.653	Si
	PFFP	1.449	SLV 1	0.352	1.441	1473	1.59	Si
	R	0.085	SLV 1	0.02	0.08	1	0.08	No

Verifica travi di collegamento in muratura

Trave	Stato limite	Molt.	Comb.	PGA	IPGA (ZE)	TR	(TR/TRrif)^.41	Verifica
1	F	1.455	SLV 11	0.339	1.389	1304	1.513	Si
	V	0.104	SLV 11	0.031	0.127	3	0.125	No
2	F	0.999	SLV 15	0.244	0.999	473	0.998	No
	V	0.024	SLV 15	0	0	0	0	No
3	F	3.149	SLV 1	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
4	F	2.782	SLV 1	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
5	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
6	F	4.042	SLV 13	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
7	F	2.063	SLV 3	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
8	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
9	F	3.135	SLV 5	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
10	F	2.833	SLV 9	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
11	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
12	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
13	F	1.101	SLV 15	0.269	1.099	630	1.123	Si
	V	0.056	SLV 15	0	0	0	0	No
14	F	2.733	SLV 3	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
15	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0.483	SLV 1	0.115	0.471	73	0.464	No
16	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0.9	SLV 1	0.219	0.896	355	0.887	No
17	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0.295	SLV 1	0.069	0.281	21	0.278	No
18	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	1.697	SLV 1	0.362	1.483	1618	1.653	Si
19	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0.127	SLV 13	0.026	0.107	2	0.106	No
20	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0.941	SLV 13	0.229	0.938	401	0.933	No
21	F	1.781	SLV 11	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
22	F	1.647	SLV 5	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No



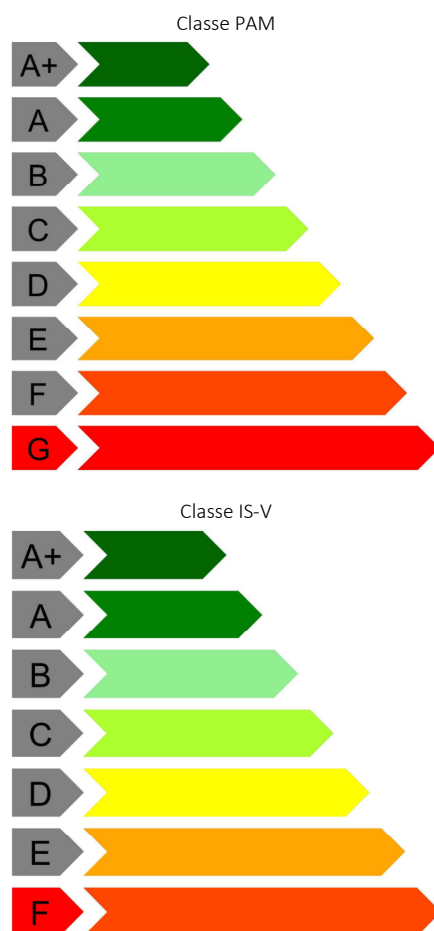
Trave	Stato limite	Molt.	Comb.	PGA	IPGA (ZE)	TR	(TR/TRrif)^.41	Verifica
23	F	3.607	SLV 9	0.362	1.483	1618	1.653	Si
	V	0.074	SLV 9	0.02	0.08	1	0.08	No
24	F	3.581	SLV 7	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
25	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
26	F	3.583	SLV 7	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No

Periodi di ritorno e accelerazioni di aggancio per gli Stati Limite

S. L.	TR,C	PGA,C	TR,Rif	PGA,Rif	Tipo rottura
Stato limite di salvaguardia della vita	0	0	475	0.244	taglio maschio muratura

Coefficienti relativi alle Linee guida per la classificazione del rischio sismico delle costruzioni secondo il D.M. 24 09/01/2020

TR,C	TR,Rif	PAM	Classe PAM	IS-V	Classe IS-V	Tipo rottura
0	475	8.22	G	0	F	taglio maschio muratura



1.3 Verifiche maschi in muratura

Le unità di misura elencate nel capitolo sono in [m, daN, s] ove non espressamente specificato.

X ini.: coordinate del punto iniziale del maschio. [m]

Y ini.: coordinate del punto iniziale del maschio. [m]

X fin.: coordinate del punto finale del maschio. [m]

Y fin.: coordinate del punto finale del maschio. [m]

Quota i.: livello o falda inferiore.

Quota s.: livello o falda superiore.

l: lunghezza del maschio. [m]

Sp.: spessore. [m]

h netta: altezza netta (a filo solai). [m]

h ini.: altezza nel modello al punto iniziale. [m]

h fin.: altezza nel modello al punto finale. [m]

a: distanza tra irrigidimenti laterali. [m]



a.s.,sx: lunghezza di appoggio del solaio di sinistra. [m]

a.s.,dx: lunghezza di appoggio del solaio di destra. [m]

fb: resistenza normalizzata a compressione verticale dei blocchi. [daN/m²]

fk: resistenza caratteristica a compressione della muratura utilizzata. [daN/m²]

fvk0: resistenza caratteristica a taglio in assenza di carichi verticali. [daN/m²]

fmedio: resistenza media a compressione della muratura utilizzata. [daN/m²]

t0: resistenza media a taglio in assenza di azioni normali [C8.7.1.16]. [daN/m²]

fv0: resistenza media a taglio in assenza di azioni normali [C8.7.1.17]. [daN/m²]

μ: coefficiente di attrito [C8.7.1.17].

φ: coefficiente di ammortamento o ingranamento secondo Circolare 7 21-01-19 §C8.7.1.3.1.1.

fv,lim: valore massimo della resistenza a taglio che può essere impiegata nel calcolo. [daN/m²]

E: modulo di elasticità longitudinale della muratura utilizzato. [daN/m²]

G: modulo di elasticità tangenziale della muratura utilizzato. [daN/m²]

FC: fattore di confidenza della muratura.

Comb.: combinazione.

Quota: quota della sezione di verifica. [m]

N: sforzo normale. [daN]

M: momento flettente nel piano. [daN*m]

σ0: tensione media di compressione. [daN/m²]

Mu: momento flettente ultimo. [daN*m]

c.s.: coefficiente di sicurezza.

Verifica: stato di verifica.

V par: taglio nel piano. [daN]

σN: tensione media di compressione sulla parte reagente. [daN/m²]

l': lunghezza della parte compressa della parete. [m]

fvd: resistenza a taglio di calcolo. [daN/m²]

Vt scorr.: taglio ultimo per verifica a scorrimento. [daN]

Vt fess.diag.: taglio ultimo per verifica a fessurazione diagonale regolare [C8.7.1.17]. [daN]

Vt,lim: taglio limite [C8.7.1.18]. [daN]

c.s.: coefficiente di sicurezza a taglio.

fd: resistenza a compressione di calcolo. [daN/m²]

Sa: accelerazione massima, adimensionalizzata rispetto a g, che l'elemento strutturale subisce durante il sisma.

M: momento flettente fuori piano. [daN*m]

Mc: momento di collasso per azioni perpendicolari al piano. [daN*m]

Coeff.s.: coefficiente di sicurezza.

N top: sforzo normale in sommità. [daN]

N base: sforzo normale al piede. [daN]

V orto: taglio fuori piano. [daN]

α0: moltiplicatore secondo [C8.7.1.1].

M*: massa partecipante al cinematisimo. [daN/(m/s²)]

e*: frazione di massa partecipante della muratura [C8.7.1.5].

α0*: accelerazione spettrale di attivazione del meccanismo [C8.7.1.8]. [m/s²]

αLim: accelerazione limite [C7.2.11]. [m/s²]

Stato limite: pF_SLV=Presso flessione per azioni non sismiche; V_SLV=Taglio per azioni non sismiche; PF_SLV=Presso flessione per azioni sismiche; V_SLV=Taglio per azioni sismiche; PFPF_SLV=Presso flessione fuori piano per azioni sismiche; R_SLV=Ribaltamento per azioni sismiche.

Maschio 1

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
25.794	-0.169	25.794	8.566	L1	L2	8.735	0.45	2.65	2.65	2.65			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	t0	fv0	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 82	-0.98	-77376	2384.36	19685	256275.06	107.482	Si
SLU 82	1.67	-49806	10260.06	12671	183691.24	17.904	Si
SLU 20	-0.98	-60080	2385.28	15285	213164.44	89.367	Si
SLU 20	1.67	-39163	8470.66	9963	150124.65	17.723	Si
SLU 39	-0.98	-65438	3257.69	16648	227390.4	69.801	Si
SLU 39	1.67	-43677	9908.16	11112	164738.97	16.627	Si
SLU 18	-0.98	-60080	2385.28	15285	213164.44	89.367	Si
SLU 18	1.67	-39163	8470.66	9963	150124.65	17.723	Si
SLU 40	-0.98	-65438	3257.69	16648	227390.4	69.801	Si
SLU 40	1.67	-43677	9908.16	11112	164738.97	16.627	Si
SLU 41	-0.98	-65438	3257.69	16648	227390.4	69.801	Si
SLU 41	1.67	-43677	9908.16	11112	164738.97	16.627	Si
SLU 42	-0.98	-65438	3257.69	16648	227390.4	69.801	Si
SLU 42	1.67	-43677	9908.16	11112	164738.97	16.627	Si
SLU 21	-0.98	-60080	2385.28	15285	213164.44	89.367	Si
SLU 21	1.67	-39163	8470.66	9963	150124.65	17.723	Si
SLU 81	-0.98	-77376	2384.36	19685	256275.06	107.482	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 81	1.67	-49806	10260.06	12671	183691.24	17.904	Si
SLU 19	-0.98	-60080	2385.28	15285	213164.44	89.367	Si
SLU 19	1.67	-39163	8470.66	9963	150124.65	17.723	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 6	-0.98	-63579	10765.31	16175	240923.6	22.38	Si
SLV 6	1.67	-34790	16928.77	8851	140939.15	8.325	Si
SLV 14	-0.98	-37644	-17459.85	9577	151525.34	8.679	Si
SLV 14	1.67	-22753	-21866	5788	94665.9	4.329	Si
SLV 2	-0.98	-68150	19468.58	17338	255412.19	13.119	Si
SLV 2	1.67	-38164	33170.5	9709	153436.41	4.626	Si
SLV 5	-0.98	-63579	10765.31	16175	240923.6	22.38	Si
SLV 5	1.67	-34790	16928.77	8851	140939.15	8.325	Si
SLV 16	-0.98	-32411	-21078.43	8245	132001.16	6.262	Si
SLV 16	1.67	-21022	-24455.46	5348	87793.34	3.59	Si
SLV 1	-0.98	-68150	19468.58	17338	255412.19	13.119	Si
SLV 1	1.67	-38164	33170.5	9709	153436.41	4.626	Si
SLV 3	-0.98	-62917	15850	16006	238791.75	15.066	Si
SLV 3	1.67	-36433	30581.04	9269	147049.11	4.809	Si
SLV 13	-0.98	-37644	-17459.85	9577	151525.34	8.679	Si
SLV 13	1.67	-22753	-21866	5788	94665.9	4.329	Si
SLV 4	-0.98	-62917	15850	16006	238791.75	15.066	Si
SLV 4	1.67	-36433	30581.04	9269	147049.11	4.809	Si
SLV 15	-0.98	-32411	-21078.43	8245	132001.16	6.262	Si
SLV 15	1.67	-21022	-24455.46	5348	87793.34	3.59	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 82	-0.98	-77376	-59	2384.36		19685	8.735	8180	32154			542.15	Si
SLU 82	1.67	-49806	-12	10260.06		12671	8.735	7245	28478			1000	Si
SLU 81	-0.98	-77376	-59	2384.36		19685	8.735	8180	32154			542.15	Si
SLU 81	1.67	-49806	-12	10260.06		12671	8.735	7245	28478			1000	Si
SLU 60	-0.98	-72019	-54	1511.95		18322	8.735	7998	31440			582.12	Si
SLU 60	1.67	-45292	-10	8822.56		11522	8.735	7092	27876			1000	Si
SLU 39	-0.98	-65438	-53	3257.69		16648	8.735	7775	30563			576.83	Si
SLU 39	1.67	-43677	-12	9908.16		11112	8.735	7037	27661			1000	Si
SLU 61	-0.98	-72019	-54	1511.95		18322	8.735	7998	31440			582.12	Si
SLU 61	1.67	-45292	-10	8822.56		11522	8.735	7092	27876			1000	Si
SLU 83	-0.98	-77376	-59	2384.36		19685	8.735	8180	32154			542.15	Si
SLU 83	1.67	-49806	-12	10260.06		12671	8.735	7245	28478			1000	Si
SLU 84	-0.98	-77376	-59	2384.36		19685	8.735	8180	32154			542.15	Si
SLU 84	1.67	-49806	-12	10260.06		12671	8.735	7245	28478			1000	Si
SLU 42	-0.98	-65438	-53	3257.69		16648	8.735	7775	30563			576.83	Si
SLU 42	1.67	-43677	-12	9908.16		11112	8.735	7037	27661			1000	Si
SLU 41	-0.98	-65438	-53	3257.69		16648	8.735	7775	30563			576.83	Si
SLU 41	1.67	-43677	-12	9908.16		11112	8.735	7037	27661			1000	Si
SLU 40	-0.98	-65438	-53	3257.69		16648	8.735	7775	30563			576.83	Si
SLU 40	1.67	-43677	-12	9908.16		11112	8.735	7037	27661			1000	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 6	-0.98	-63579	-14318	10765.31		16175	8.735	11568	45472			3.18	Si
SLV 6	1.67	-34790	-8924	16928.77		8851	8.735	10103	39714			4.45	Si
SLV 11	-0.98	-36982	14253	-12375.16		9408	8.735	10215	40153			2.82	Si
SLV 11	1.67	-24395	8917	-8213.72		6206	8.735	9575	37635			4.22	Si
SLV 12	-0.98	-36982	14253	-12375.16		9408	8.735	10215	40153			2.82	Si
SLV 12	1.67	-24395	8917	-8213.72		6206	8.735	9575	37635			4.22	Si
SLV 8	-0.98	-46134	15407	-1296.63		11737	8.735	10681	41983			2.72	Si
SLV 8	1.67	-29019	10138	8297.23		7383	8.735	9810	38560			3.8	Si
SLV 10	-0.98	-54427	-15473	-313.22		13847	8.735	11103	43642			2.82	Si
SLV 10	1.67	-30167	-10145	417.82		7675	8.735	9868	38790			3.82	Si
SLV 7	-0.98	-46134	15407	-1296.63		11737	8.735	10681	41983			2.72	Si
SLV 7	1.67	-29019	10138	8297.23		7383	8.735	9810	38560			3.8	Si
SLV 14	-0.98	-37644	-6416	-17459.85		9577	8.735	10249	40285			6.28	Si
SLV 14	1.67	-22753	-4898	-21866		5788	8.735	9491	37307			7.62	Si
SLV 5	-0.98	-63579	-14318	10765.31		16175	8.735	11568	45472			3.18	Si
SLV 5	1.67	-34790	-8924	16928.77		8851	8.735	10103	39714			4.45	Si
SLV 13	-0.98	-37644	-6416	-17459.85		9577	8.735	10249	40285			6.28	Si
SLV 13	1.67	-22753	-4898	-21866		5788	8.735	9491	37307			7.62	Si
SLV 9	-0.98	-54427	-15473	-313.22		13847	8.735	11103	43642			2.82	Si
SLV 9	1.67	-30167	-10145	417.82		7675	8.735	9868	38790			3.82	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.345 Wa 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 16	143750	0.27	6475	-25452	569.61	5423.13	9.52	Si
SLV 15	143750	0.27	6475	-25452	569.61	5423.13	9.52	Si
SLV 14	143750	0.27	7444	-29262	569.61	6182.85	10.85	Si
SLV 13	143750	0.27	7444	-29262	569.61	6182.85	10.85	Si
SLV 12	143750	0.27	7495	-29459	569.61	6221.77	10.92	Si
SLV 11	143750	0.27	7495	-29459	569.61	6221.77	10.92	Si
SLV 7	143750	0.27	9338	-36705	569.61	7627.5	13.39	Si
SLV 8	143750	0.27	9338	-36705	569.61	7627.5	13.39	Si
SLV 10	143750	0.27	10726	-42161	569.61	8653.58	15.19	Si
SLV 9	143750	0.27	10726	-42161	569.61	8653.58	15.19	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 0.345 Wa = 0.08 Ta = 0.0261



Comb.	N top	N base	V orto	$\alpha 0$	M*	e*	a0*	aLim	Verifica
SLV 2	-38164	-68150	-558	0.09	5376	0.927	1.41017	11.13714	No
SLV 1	-38164	-68150	-558	0.09	5376	0.927	1.41017	11.13714	No
SLV 4	-36433	-62917	-519	0.091	5201.7	0.925	1.42941	11.13714	No
SLV 3	-36433	-62917	-519	0.091	5201.7	0.925	1.42941	11.13714	No
SLV 15	-21022	-32411	566	0.092	3663.5	0.904	1.48748	11.13714	No
SLV 16	-21022	-32411	566	0.092	3663.5	0.904	1.48748	11.13714	No
SLV 14	-22753	-37644	527	0.093	3834.4	0.906	1.4959	11.13714	No
SLV 13	-22753	-37644	527	0.093	3834.4	0.906	1.4959	11.13714	No
SLV 6	-34790	-63579	-224	0.098	5036.6	0.923	1.54116	2.73586	No
SLV 5	-34790	-63579	-224	0.098	5036.6	0.923	1.54116	2.73586	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	16.627	SLU 39	Si
V_SLU	542.147	SLU 81	Si
PF_SLV	3.59	SLV 15	Si
V_SLV	2.725	SLV 7	Si
PFFP_SLV	9.521	SLV 15	Si
R_SLV	0.127	SLV 1	No

Maschio 2

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.sx	a.s.dx
25.794	8.566	25.882	8.663	L1	L2	0.13	0.45	2.65	2.65	2.65			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _k	f _{vk0}	f _{medio}	$\tau 0$	f _{v0}	μ	ϕ	f _{v,lim}	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma 0$	Mu	c.s.	Verifica
SLU 75	0.41	-1589	40.72	27063	69.23	1.7	Si
SLU 75	0.81	-1534	-16.47	26127	67.99	4.129	Si
SLU 80	0.41	-1589	40.72	27063	69.23	1.7	Si
SLU 80	0.81	-1534	-16.47	26127	67.99	4.129	Si
SLU 84	0.41	-1719	43.75	29280	71.85	1.642	Si
SLU 84	0.81	-1664	-17.65	28344	70.8	4.012	Si
SLU 76	0.41	-1589	40.72	27063	69.23	1.7	Si
SLU 76	0.81	-1534	-16.47	26127	67.99	4.129	Si
SLU 78	0.41	-1589	40.72	27063	69.23	1.7	Si
SLU 78	0.81	-1534	-16.47	26127	67.99	4.129	Si
SLU 83	0.41	-1719	43.75	29280	71.85	1.642	Si
SLU 83	0.81	-1664	-17.65	28344	70.8	4.012	Si
SLU 77	0.41	-1589	40.72	27063	69.23	1.7	Si
SLU 77	0.81	-1534	-16.47	26127	67.99	4.129	Si
SLU 79	0.41	-1589	40.72	27063	69.23	1.7	Si
SLU 79	0.81	-1534	-16.47	26127	67.99	4.129	Si
SLU 82	0.41	-1719	43.75	29280	71.85	1.642	Si
SLU 82	0.81	-1664	-17.65	28344	70.8	4.012	Si
SLU 81	0.41	-1719	43.75	29280	71.85	1.642	Si
SLU 81	0.81	-1664	-17.65	28344	70.8	4.012	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma 0$	Mu	c.s.	Verifica
SLV 1	0.41	-1342	-124.99	0	0	0	No, $e > l/2$
SLV 1	0.81	-1353	142.8	0	0	0	No, $e > l/2$
SLV 5	0.41	-1115	-138	0	0	0	No, $e > l/2$
SLV 5	0.81	-1143	153.41	0	0	0	No, $e > l/2$
SLV 8	0.41	-1153	124.65	0	0	0	No, $e > l/2$
SLV 8	0.81	-1061	-106.68	0	0	0	No, $e > l/2$
SLV 2	0.41	-1342	-124.99	0	0	0	No, $e > l/2$
SLV 2	0.81	-1353	142.8	0	0	0	No, $e > l/2$
SLV 10	0.41	-931	-70.36	0	0	0	No, $e > l/2$
SLV 10	0.81	-939	84.49	0	0	0	No, $e > l/2$
SLV 9	0.41	-931	-70.36	0	0	0	No, $e > l/2$
SLV 9	0.81	-939	84.49	0	0	0	No, $e > l/2$
SLV 11	0.41	-970	192.3	0	0	0	No, $e > l/2$
SLV 11	0.81	-857	-175.61	0	0	0	No, $e > l/2$
SLV 7	0.41	-1153	124.65	0	0	0	No, $e > l/2$
SLV 7	0.81	-1061	-106.68	0	0	0	No, $e > l/2$
SLV 6	0.41	-1115	-138	0	0	0	No, $e > l/2$
SLV 6	0.81	-1143	153.41	0	0	0	No, $e > l/2$
SLV 12	0.41	-970	192.3	0	0	0	No, $e > l/2$
SLV 12	0.81	-857	-175.61	0	0	0	No, $e > l/2$

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma 0$	σN	I'	f _{vd}	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLU 84	0.41	-1719	153	43.75		32004	0.1194	9823	528			3.44	Si
SLU 84	0.81	-1664	153	-17.65		28344	0.1305	9335	548			3.57	Si
SLU 81	0.41	-1719	153	43.75		32004	0.1194	9823	528			3.44	Si
SLU 81	0.81	-1664	153	-17.65		28344	0.1305	9335	548			3.57	Si
SLU 63	0.41	-1568	142	40.35		29394	0.1185	9475	505			3.55	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 63	0.81	-1513	142	-16.56		25762	0.1305	8990	528			3.71	Si
SLU 62	0.41	-1568	142	40.35		29394	0.1185	9475	505			3.55	Si
SLU 62	0.81	-1513	142	-16.56		25762	0.1305	8990	528			3.71	Si
SLU 61	0.41	-1568	142	40.35		29394	0.1185	9475	505			3.55	Si
SLU 61	0.81	-1513	142	-16.56		25762	0.1305	8990	528			3.71	Si
SLU 60	0.41	-1568	142	40.35		29394	0.1185	9475	505			3.55	Si
SLU 60	0.81	-1513	142	-16.56		25762	0.1305	8990	528			3.71	Si
SLU 75	0.41	-1589	143	40.72		29711	0.1189	9517	509			3.56	Si
SLU 75	0.81	-1534	143	-16.47		26127	0.1305	9039	531			3.71	Si
SLU 82	0.41	-1719	153	43.75		32004	0.1194	9823	528			3.44	Si
SLU 82	0.81	-1664	153	-17.65		28344	0.1305	9335	548			3.57	Si
SLU 83	0.41	-1719	153	43.75		32004	0.1194	9823	528			3.44	Si
SLU 83	0.81	-1664	153	-17.65		28344	0.1305	9335	548			3.57	Si
SLU 74	0.41	-1589	143	40.72		29711	0.1189	9517	509			3.56	Si
SLU 74	0.81	-1534	143	-16.47		26127	0.1305	9039	531			3.71	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 1	0.41	-1342	-622	-124.99		0	0	8333	0			0	No, Vu<V
SLV 1	0.81	-1353	-709	142.8		0	0	8333	0			0	No, Vu<V
SLV 5	0.41	-1115	-583	-138		0	0	8333	0			0	No, Vu<V
SLV 5	0.81	-1143	-770	153.41		0	0	8333	0			0	No, Vu<V
SLV 2	0.41	-1342	-622	-124.99		0	0	8333	0			0	No, Vu<V
SLV 2	0.81	-1353	-709	142.8		0	0	8333	0			0	No, Vu<V
SLV 12	0.41	-970	775	192.3		0	0	8333	0			0	No, Vu<V
SLV 12	0.81	-857	961	-175.61		0	0	8333	0			0	No, Vu<V
SLV 10	0.41	-931	-244	-70.36		0	0	8333	0			0	No, Vu<V
SLV 10	0.81	-939	-410	84.49		0	0	8333	0			0	No, Vu<V
SLV 9	0.41	-931	-244	-70.36		0	0	8333	0			0	No, Vu<V
SLV 9	0.81	-939	-410	84.49		0	0	8333	0			0	No, Vu<V
SLV 7	0.41	-1153	436	124.65		0	0	8333	0			0	No, Vu<V
SLV 7	0.81	-1061	601	-106.68		0	0	8333	0			0	No, Vu<V
SLV 8	0.41	-1153	436	124.65		0	0	8333	0			0	No, Vu<V
SLV 8	0.81	-1061	601	-106.68		0	0	8333	0			0	No, Vu<V
SLV 6	0.41	-1115	-583	-138		0	0	8333	0			0	No, Vu<V
SLV 6	0.81	-1143	-770	153.41		0	0	8333	0			0	No, Vu<V
SLV 11	0.41	-970	775	192.3		0	0	8333	0			0	No, Vu<V
SLV 11	0.81	-857	961	-175.61		0	0	8333	0			0	No, Vu<V

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.345 Wa 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 9	143750	0.27	1790	-105	8.39	23.3	2.78	Si
SLV 10	143750	0.27	1790	-105	8.39	23.3	2.78	Si
SLV 13	143750	0.27	2938	-173	8.39	37.89	4.52	Si
SLV 14	143750	0.27	2938	-173	8.39	37.89	4.52	Si
SLV 6	143750	0.27	4350	-255	8.39	55.43	6.61	Si
SLV 5	143750	0.27	4350	-255	8.39	55.43	6.61	Si
SLV 16	143750	0.27	6483	-381	8.39	81.11	9.67	Si
SLV 15	143750	0.27	6483	-381	8.39	81.11	9.67	Si
SLV 1	143750	0.27	11473	-674	8.39	137.34	16.38	Si
SLV 2	143750	0.27	11473	-674	8.39	137.34	16.38	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 0.345 Wa = 0.08 Ta = 0.0261

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 1	560	-1499	8	0	0	0	0	11.13714	No, Trazione
SLV 9	-109	-1037	124	0	35.3	0.89	0	2.73586	No
SLV 4	338	-1192	-62	0	0	0	0	11.13714	No, Trazione
SLV 7	-421	-392	-124	0	65.3	0.914	0	2.73586	No
SLV 10	-109	-1037	124	0	35.3	0.89	0	2.73586	No
SLV 2	560	-1499	8	0	0	0	0	11.13714	No, Trazione
SLV 5	320	-1416	108	0	0	0	0	2.73586	No, Trazione
SLV 6	320	-1416	108	0	0	0	0	2.73586	No, Trazione
SLV 3	338	-1192	-62	0	0	0	0	11.13714	No, Trazione
SLV 8	-421	-392	-124	0	65.3	0.914	0	2.73586	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	1.642	SLU 81	Si
V_SLU	3.438	SLU 81	Si
PF_SLV	0	SLV 1	No
V_SLV	0	SLV 1	No
PFFP_SLV	2.778	SLV 9	Si
R_SLV	0	SLV 16	No

Maschio 3

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
26.284	9.108	26.639	9.502	L1	L2	0.53	0.45	2.65	2.65	2.65			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

Sismicad 12.19 - Licenza assegnata a Sidel ingegneria Srl - Via Isonzo, 13 - Villanova di Castenaso (BO)



fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 42	0.41	-4140	-188.07	17343	864.32	4.596	Si
SLU 42	0.81	-3968	-140.51	16623	837.74	5.962	Si
SLU 62	0.41	-4441	-196.27	18604	908.92	4.631	Si
SLU 62	0.81	-4218	-143.08	17668	876.04	6.123	Si
SLU 81	0.41	-4849	-215.61	20312	965.41	4.478	Si
SLU 81	0.81	-4625	-158.74	19376	935.02	5.89	Si
SLU 82	0.41	-4849	-215.61	20312	965.41	4.478	Si
SLU 82	0.81	-4625	-158.74	19376	935.02	5.89	Si
SLU 40	0.41	-4140	-188.07	17343	864.32	4.596	Si
SLU 40	0.81	-3968	-140.51	16623	837.74	5.962	Si
SLU 83	0.41	-4849	-215.61	20312	965.41	4.478	Si
SLU 83	0.81	-4625	-158.74	19376	935.02	5.89	Si
SLU 39	0.41	-4140	-188.07	17343	864.32	4.596	Si
SLU 39	0.81	-3968	-140.51	16623	837.74	5.962	Si
SLU 41	0.41	-4140	-188.07	17343	864.32	4.596	Si
SLU 41	0.81	-3968	-140.51	16623	837.74	5.962	Si
SLU 84	0.41	-4849	-215.61	20312	965.41	4.478	Si
SLU 84	0.81	-4625	-158.74	19376	935.02	5.89	Si
SLU 63	0.41	-4441	-196.27	18604	908.92	4.631	Si
SLU 63	0.81	-4218	-143.08	17668	876.04	6.123	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 2	0.41	-2874	-760.4	12037	687.09	0.904	No, M>Mu
SLV 2	0.81	-2710	445.96	11351	651.94	1.462	Si
SLV 1	0.41	-2874	-760.4	12037	687.09	0.904	No, M>Mu
SLV 1	0.81	-2710	445.96	11351	651.94	1.462	Si
SLV 16	0.41	-3378	499.6	14151	792.25	1.586	Si
SLV 16	0.81	-3198	-630.71	13398	755.3	1.198	Si
SLV 11	0.41	-3487	435.63	14605	814.23	1.869	Si
SLV 11	0.81	-3351	-606.33	14039	786.8	1.298	Si
SLV 15	0.41	-3378	499.6	14151	792.25	1.586	Si
SLV 15	0.81	-3198	-630.71	13398	755.3	1.198	Si
SLV 12	0.41	-3487	435.63	14605	814.23	1.869	Si
SLV 12	0.81	-3351	-606.33	14039	786.8	1.298	Si
SLV 6	0.41	-2765	-696.44	11583	663.9	0.953	No, M>Mu
SLV 6	0.81	-2556	421.57	10709	618.65	1.467	Si
SLV 3	0.41	-3061	-511.8	12825	726.79	1.42	Si
SLV 3	0.81	-2923	213.58	12246	697.68	3.267	Si
SLV 4	0.41	-3061	-511.8	12825	726.79	1.42	Si
SLV 4	0.81	-2923	213.58	12246	697.68	3.267	Si
SLV 5	0.41	-2765	-696.44	11583	663.9	0.953	No, M>Mu
SLV 5	0.81	-2556	421.57	10709	618.65	1.467	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 81	0.41	-4849	-142	-215.61		20312	0.5305	8264	1973			13.88	Si
SLU 81	0.81	-4625	-142	-158.74		19376	0.5305	8139	1943			13.67	Si
SLU 78	0.41	-4578	-136	-199.17		19176	0.5305	8112	1937			14.27	Si
SLU 78	0.81	-4354	-136	-144.89		18240	0.5305	7988	1907			14.05	Si
SLU 79	0.41	-4578	-136	-199.17		19176	0.5305	8112	1937			14.27	Si
SLU 79	0.81	-4354	-136	-144.89		18240	0.5305	7988	1907			14.05	Si
SLU 80	0.41	-4578	-136	-199.17		19176	0.5305	8112	1937			14.27	Si
SLU 80	0.81	-4354	-136	-144.89		18240	0.5305	7988	1907			14.05	Si
SLU 77	0.41	-4578	-136	-199.17		19176	0.5305	8112	1937			14.27	Si
SLU 77	0.81	-4354	-136	-144.89		18240	0.5305	7988	1907			14.05	Si
SLU 82	0.41	-4849	-142	-215.61		20312	0.5305	8264	1973			13.88	Si
SLU 82	0.81	-4625	-142	-158.74		19376	0.5305	8139	1943			13.67	Si
SLU 76	0.41	-4578	-136	-199.17		19176	0.5305	8112	1937			14.27	Si
SLU 76	0.81	-4354	-136	-144.89		18240	0.5305	7988	1907			14.05	Si
SLU 84	0.41	-4849	-142	-215.61		20312	0.5305	8264	1973			13.88	Si
SLU 84	0.81	-4625	-142	-158.74		19376	0.5305	8139	1943			13.67	Si
SLU 83	0.41	-4849	-142	-215.61		20312	0.5305	8264	1973			13.88	Si
SLU 83	0.81	-4625	-142	-158.74		19376	0.5305	8139	1943			13.67	Si
SLU 75	0.41	-4578	-136	-199.17		19176	0.5305	8112	1937			14.27	Si
SLU 75	0.81	-4354	-136	-144.89		18240	0.5305	7988	1907			14.05	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 12	0.41	-3487	2480	435.63		18409	0.4209	12015	2276			0.92	No, Vu<V
SLV 12	0.81	-3351	2477	-606.33		29440	0.253	14221	1619			0.65	No, Vu<V
SLV 3	0.41	-3061	-1632	-511.8		23125	0.2942	12958	1716			1.05	Si
SLV 3	0.81	-2923	-1631	213.58		12246	0.5305	10783	2574			1.58	Si
SLV 11	0.41	-3487	2480	435.63		18409	0.4209	12015	2276			0.92	No, Vu<V
SLV 11	0.81	-3351	2477	-606.33		29440	0.253	14221	1619			0.65	No, Vu<V
SLV 2	0.41	-2874	-2795	-760.4		0	0	8333	0			0	No, Vu<V
SLV 2	0.81	-2710	-2793	445.96		19940	0.302	12321	1674			0.6	No, Vu<V
SLV 4	0.41	-3061	-1632	-511.8		23125	0.2942	12958	1716			1.05	Si
SLV 4	0.81	-2923	-1631	213.58		12246	0.5305	10783	2574			1.58	Si
SLV 5	0.41	-2765	-2670	-696.44		153117	0.0401	16250	293			0.11	No, Vu<V
SLV 5	0.81	-2556	-2667	421.57		18873	0.301	12108	1640			0.61	No, Vu<V
SLV 6	0.41	-2765	-2670	-696.44		153117	0.0401	16250	293			0.11	No, Vu<V
SLV 6	0.81	-2556	-2667	421.57		18873	0.301	12108	1640			0.61	No, Vu<V
SLV 1	0.41	-2874	-2795	-760.4		0	0	8333	0			0	No, Vu<V
SLV 1	0.81	-2710	-2793	445.96		19940	0.302	12321	1674			0.6	No, Vu<V



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 15	0.41	-3378	2605	499.6		21324	0.352	12598	1996			0.77	No, Vu<V
SLV 15	0.81	-3198	2603	-630.71		34821	0.2041	15297	1405			0.54	No, Vu<V
SLV 16	0.41	-3378	2605	499.6		21324	0.352	12598	1996			0.77	No, Vu<V
SLV 16	0.81	-3198	2603	-630.71		34821	0.2041	15297	1405			0.54	No, Vu<V

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.345 Wa 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 9	143750	0.27	6111	-1459	34.1	311.81	9.15	Si
SLV 10	143750	0.27	6111	-1459	34.1	311.81	9.15	Si
SLV 5	143750	0.27	6426	-1534	34.1	327.01	9.59	Si
SLV 6	143750	0.27	6426	-1534	34.1	327.01	9.59	Si
SLV 14	143750	0.27	7260	-1733	34.1	366.77	10.76	Si
SLV 13	143750	0.27	7260	-1733	34.1	366.77	10.76	Si
SLV 2	143750	0.27	8311	-1984	34.1	416.03	12.2	Si
SLV 1	143750	0.27	8311	-1984	34.1	416.03	12.2	Si
SLV 16	143750	0.27	8560	-2043	34.1	427.57	12.54	Si
SLV 15	143750	0.27	8560	-2043	34.1	427.57	12.54	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 0.345 Wa = 0.08 Ta = 0.0261

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 10	-2132	-1600	279	0	307.8	0.923	0	2.73586	No
SLV 14	1903	-3136	88	0	0	0	0	11.13714	No, Trazione
SLV 9	-2132	-1600	279	0	307.8	0.923	0	2.73586	No
SLV 8	-116	-4537	-278	0	119.5	0.934	0	2.73586	No
SLV 16	3166	-4118	-78	0	0	0	0	11.13714	No, Trazione
SLV 11	2079	-4872	-276	0	0	0	0	2.73586	No, Trazione
SLV 15	3166	-4118	-78	0	0	0	0	11.13714	No, Trazione
SLV 12	2079	-4872	-276	0	0	0	0	2.73586	No, Trazione
SLV 13	1903	-3136	88	0	0	0	0	11.13714	No, Trazione
SLV 7	-116	-4537	-278	0	119.5	0.934	0	2.73586	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	4.478	SLU 81	Si
V_SLU	13.666	SLU 81	Si
PF_SLV	0.904	SLV 1	No
V_SLV	0	SLV 1	No
PFFP_SLV	9.145	SLV 9	Si
R_SLV	0	SLV 16	No

Maschio 4

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
27.92	-0.169	25.794	-0.169	L1	L2	2.125	0.45	2.65	2.65	2.65			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 79	0.41	-16397	-2301.49	17144	13758.36	5.978	Si
SLU 79	0.81	-15580	-2509.6	16289	13246.42	5.278	Si
SLU 81	0.41	-17337	-2431.41	18126	14324.36	5.891	Si
SLU 81	0.81	-16517	-2652.48	17269	13832.01	5.215	Si
SLU 74	0.41	-16397	-2301.49	17144	13758.36	5.978	Si
SLU 74	0.81	-15580	-2509.6	16289	13246.42	5.278	Si
SLU 76	0.41	-16397	-2301.49	17144	13758.36	5.978	Si
SLU 76	0.81	-15580	-2509.6	16289	13246.42	5.278	Si
SLU 83	0.41	-17337	-2431.41	18126	14324.36	5.891	Si
SLU 83	0.81	-16517	-2652.48	17269	13832.01	5.215	Si
SLU 78	0.41	-16397	-2301.49	17144	13758.36	5.978	Si
SLU 78	0.81	-15580	-2509.6	16289	13246.42	5.278	Si
SLU 75	0.41	-16397	-2301.49	17144	13758.36	5.978	Si
SLU 75	0.81	-15580	-2509.6	16289	13246.42	5.278	Si
SLU 84	0.41	-17337	-2431.41	18126	14324.36	5.891	Si
SLU 84	0.81	-16517	-2652.48	17269	13832.01	5.215	Si
SLU 82	0.41	-17337	-2431.41	18126	14324.36	5.891	Si
SLU 82	0.81	-16517	-2652.48	17269	13832.01	5.215	Si
SLU 73	0.41	-16397	-2301.49	17144	13758.36	5.978	Si
SLU 73	0.81	-15580	-2509.6	16289	13246.42	5.278	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 1	0.41	-11949	-1113.19	12493	11400.32	10.241	Si
SLV 1	0.81	-11682	-2226.83	12213	11173.43	5.018	Si
SLV 16	0.41	-10555	-2039.32	11035	10203.88	5.004	Si
SLV 16	0.81	-9570	-1206.51	10006	9337.73	7.739	Si
SLV 12	0.41	-9129	-1960.05	9545	8944.15	4.563	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 12	0.81	-8627	-1694.5	9019	8490.97	5.011	Si
SLV 7	0.41	-9169	-1730.64	9587	8979.83	5.189	Si
SLV 7	0.81	-8927	-2026.49	9334	8762.4	4.324	Si
SLV 11	0.41	-9129	-1960.05	9545	8944.15	4.563	Si
SLV 11	0.81	-8627	-1694.5	9019	8490.97	5.011	Si
SLV 15	0.41	-10555	-2039.32	11035	10203.88	5.004	Si
SLV 15	0.81	-9570	-1206.51	10006	9337.73	7.739	Si
SLV 3	0.41	-10688	-1274.64	11174	10319.25	8.096	Si
SLV 3	0.81	-10572	-2313.12	11053	10218.9	4.418	Si
SLV 2	0.41	-11949	-1113.19	12493	11400.32	10.241	Si
SLV 2	0.81	-11682	-2226.83	12213	11173.43	5.018	Si
SLV 4	0.41	-10688	-1274.64	11174	10319.25	8.096	Si
SLV 4	0.81	-10572	-2313.12	11053	10218.9	4.418	Si
SLV 8	0.41	-9169	-1730.64	9587	8979.83	5.189	Si
SLV 8	0.81	-8927	-2026.49	9334	8762.4	4.324	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 83	0.41	-17337	710	-2431.41		18126	2.1255	7972	7625			10.74	Si
SLU 83	0.81	-16517	710	-2652.48		17269	2.1255	7858	7516			10.59	Si
SLU 76	0.41	-16397	683	-2301.49		17144	2.1255	7841	7500			10.98	Si
SLU 76	0.81	-15580	683	-2509.6		16289	2.1255	7727	7391			10.81	Si
SLU 84	0.41	-17337	710	-2431.41		18126	2.1255	7972	7625			10.74	Si
SLU 84	0.81	-16517	710	-2652.48		17269	2.1255	7858	7516			10.59	Si
SLU 77	0.41	-16397	683	-2301.49		17144	2.1255	7841	7500			10.98	Si
SLU 77	0.81	-15580	683	-2509.6		16289	2.1255	7727	7391			10.81	Si
SLU 75	0.41	-16397	683	-2301.49		17144	2.1255	7841	7500			10.98	Si
SLU 75	0.81	-15580	683	-2509.6		16289	2.1255	7727	7391			10.81	Si
SLU 80	0.41	-16397	683	-2301.49		17144	2.1255	7841	7500			10.98	Si
SLU 80	0.81	-15580	683	-2509.6		16289	2.1255	7727	7391			10.81	Si
SLU 81	0.41	-17337	710	-2431.41		18126	2.1255	7972	7625			10.74	Si
SLU 81	0.81	-16517	710	-2652.48		17269	2.1255	7858	7516			10.59	Si
SLU 78	0.41	-16397	683	-2301.49		17144	2.1255	7841	7500			10.98	Si
SLU 78	0.81	-15580	683	-2509.6		16289	2.1255	7727	7391			10.81	Si
SLU 79	0.41	-16397	683	-2301.49		17144	2.1255	7841	7500			10.98	Si
SLU 79	0.81	-15580	683	-2509.6		16289	2.1255	7727	7391			10.81	Si
SLU 82	0.41	-17337	710	-2431.41		18126	2.1255	7972	7625			10.74	Si
SLU 82	0.81	-16517	710	-2652.48		17269	2.1255	7858	7516			10.59	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 4	0.41	-10688	4096	-1274.64		11174	2.1255	10568	10108			2.47	Si
SLV 4	0.81	-10572	3772	-2313.12		11053	2.1255	10544	10085			2.67	Si
SLV 15	0.41	-10555	-2793	-2039.32		11035	2.1255	10540	10081			3.61	Si
SLV 15	0.81	-9570	-2555	-1206.51		10006	2.1255	10335	9885			3.87	Si
SLV 2	0.41	-11949	3753	-1113.19		12493	2.1255	10832	10360			2.76	Si
SLV 2	0.81	-11682	3514	-2226.83		12213	2.1255	10776	10307			2.93	Si
SLV 1	0.41	-11949	3753	-1113.19		12493	2.1255	10832	10360			2.76	Si
SLV 1	0.81	-11682	3514	-2226.83		12213	2.1255	10776	10307			2.93	Si
SLV 7	0.41	-9169	2085	-1730.64		9587	2.1255	10251	9804			4.7	Si
SLV 7	0.81	-8927	1858	-2026.49		9334	2.1255	10200	9756			5.25	Si
SLV 3	0.41	-10688	4096	-1274.64		11174	2.1255	10568	10108			2.47	Si
SLV 3	0.81	-10572	3772	-2313.12		11053	2.1255	10544	10085			2.67	Si
SLV 14	0.41	-11816	-3136	-1877.87		12354	2.1255	10804	10334			3.29	Si
SLV 14	0.81	-10680	-2812	-1120.21		11166	2.1255	10567	10106			3.59	Si
SLV 8	0.41	-9169	2085	-1730.64		9587	2.1255	10251	9804			4.7	Si
SLV 8	0.81	-8927	1858	-2026.49		9334	2.1255	10200	9756			5.25	Si
SLV 16	0.41	-10555	-2793	-2039.32		11035	2.1255	10540	10081			3.61	Si
SLV 16	0.81	-9570	-2555	-1206.51		10006	2.1255	10335	9885			3.87	Si
SLV 13	0.41	-11816	-3136	-1877.87		12354	2.1255	10804	10334			3.29	Si
SLV 13	0.81	-10680	-2812	-1120.21		11166	2.1255	10567	10106			3.59	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.345 Wa 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 11	143750	0.27	8515	-8145	136.61	1704.81	12.48	Si
SLV 12	143750	0.27	8515	-8145	136.61	1704.81	12.48	Si
SLV 7	143750	0.27	8839	-8454	136.61	1764.58	12.92	Si
SLV 8	143750	0.27	8839	-8454	136.61	1764.58	12.92	Si
SLV 15	143750	0.27	9622	-9203	136.61	1907.6	13.96	Si
SLV 16	143750	0.27	9622	-9203	136.61	1907.6	13.96	Si
SLV 3	143750	0.27	10701	-10235	136.61	2101.19	15.38	Si
SLV 4	143750	0.27	10701	-10235	136.61	2101.19	15.38	Si
SLV 14	143750	0.27	10894	-10420	136.61	2135.42	15.63	Si
SLV 13	143750	0.27	10894	-10420	136.61	2135.42	15.63	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 0.345 Wa = 0.08 Ta = 0.0261

Comb.	N top	N base	V orto	α_0	M*	e*	α_0^*	aLim	Verifica
SLV 14	-8144	-11905	47	0.099	1193.3	0.921	1.56071	11.13714	No
SLV 13	-8144	-11905	47	0.099	1193.3	0.921	1.56071	11.13714	No
SLV 2	-8345	-14592	41	0.099	1213.5	0.922	1.56496	11.13714	No
SLV 1	-8345	-14592	41	0.099	1213.5	0.922	1.56496	11.13714	No
SLV 4	-7524	-12897	-48	0.1	1131.1	0.918	1.57983	11.13714	No
SLV 3	-7524	-12897	-48	0.1	1131.1	0.918	1.57983	11.13714	No
SLV 16	-7323	-10209	-41	0.101	1110.9	0.917	1.59793	11.13714	No
SLV 15	-7323	-10209	-41	0.101	1110.9	0.917	1.59793	11.13714	No
SLV 9	-9173	-14823	148	0.089	1296.7	0.926	1.39486	2.73586	No
SLV 10	-9173	-14823	148	0.089	1296.7	0.926	1.39486	2.73586	No



Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	5.215	SLU 81	Si
V_SLU	10.585	SLU 81	Si
PF_SLV	4.324	SLV 7	Si
V_SLV	2.468	SLV 3	Si
PFFP_SLV	12.48	SLV 11	Si
R_SLV	0.14	SLV 13	No

Maschio 5

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
32.569	-0.169	28.92	-0.169	L1	L2	3.649	0.45	2.65	2.65	2.65			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ0	fv0	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 18	0.41	-25886	-300.27	15763	38092.91	126.863	Si
SLU 18	0.81	-24729	-278.27	15059	36780.57	132.177	Si
SLU 20	0.41	-25886	-300.27	15763	38092.91	126.863	Si
SLU 20	0.81	-24729	-278.27	15059	36780.57	132.177	Si
SLU 84	0.41	-33531	-367.94	20419	45846.23	124.601	Si
SLU 84	0.81	-32020	-340.54	19498	44440.18	130.498	Si
SLU 83	0.41	-33531	-367.94	20419	45846.23	124.601	Si
SLU 83	0.81	-32020	-340.54	19498	44440.18	130.498	Si
SLU 82	0.41	-33531	-367.94	20419	45846.23	124.601	Si
SLU 82	0.81	-32020	-340.54	19498	44440.18	130.498	Si
SLU 81	0.41	-33531	-367.94	20419	45846.23	124.601	Si
SLU 81	0.81	-32020	-340.54	19498	44440.18	130.498	Si
SLU 39	0.41	-28744	-333.86	17504	41178.39	123.342	Si
SLU 39	0.81	-27575	-310.56	16792	39942.73	128.616	Si
SLU 40	0.41	-28744	-333.86	17504	41178.39	123.342	Si
SLU 40	0.81	-27575	-310.56	16792	39942.73	128.616	Si
SLU 41	0.41	-28744	-333.86	17504	41178.39	123.342	Si
SLU 41	0.81	-27575	-310.56	16792	39942.73	128.616	Si
SLU 42	0.41	-28744	-333.86	17504	41178.39	123.342	Si
SLU 42	0.81	-27575	-310.56	16792	39942.73	128.616	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γM = 2

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLV 1	0.41	-22608	1977.48	13767	36604.16	18.511	Si
SLV 1	0.81	-21465	-595.93	13071	34975.95	58.692	Si
SLV 4	0.41	-20024	2037.15	12194	32890.67	16.145	Si
SLV 4	0.81	-18856	-529.97	11482	31172.9	58.82	Si
SLV 2	0.41	-22608	1977.48	13767	36604.16	18.511	Si
SLV 2	0.81	-21465	-595.93	13071	34975.95	58.692	Si
SLV 11	0.41	-17081	-751.37	10401	28513.47	37.949	Si
SLV 11	0.81	-15883	52.14	9672	26687.21	511.885	Si
SLV 3	0.41	-20024	2037.15	12194	32890.67	16.145	Si
SLV 3	0.81	-18856	-529.97	11482	31172.9	58.82	Si
SLV 14	0.41	-22719	-2419.67	13834	36760.13	15.192	Si
SLV 14	0.81	-21572	181.24	13136	35130.35	193.834	Si
SLV 12	0.41	-17081	-751.37	10401	28513.47	37.949	Si
SLV 12	0.81	-15883	52.14	9672	26687.21	511.885	Si
SLV 13	0.41	-22719	-2419.67	13834	36760.13	15.192	Si
SLV 13	0.81	-21572	181.24	13136	35130.35	193.834	Si
SLV 16	0.41	-20134	-2360	12261	33051.83	14.005	Si
SLV 16	0.81	-18964	247.19	11548	31332.42	126.752	Si
SLV 15	0.41	-20134	-2360	12261	33051.83	14.005	Si
SLV 15	0.81	-18964	247.19	11548	31332.42	126.752	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, γM = 3

Comb.	Quota	N	V par	M	σ0	σN	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 81	0.41	-33531	-81	-367.94		20419	3.6493	8278	13594			168.73	Si
SLU 81	0.81	-32020	-81	-340.54		19498	3.6493	8155	13393			166.23	Si
SLU 61	0.41	-30673	-77	-334.36		18678	3.6493	8046	13213			171.72	Si
SLU 61	0.81	-29174	-77	-308.25		17766	3.6493	7924	13013			169.12	Si
SLU 84	0.41	-33531	-81	-367.94		20419	3.6493	8278	13594			168.73	Si
SLU 84	0.81	-32020	-81	-340.54		19498	3.6493	8155	13393			166.23	Si
SLU 62	0.41	-30673	-77	-334.36		18678	3.6493	8046	13213			171.72	Si
SLU 62	0.81	-29174	-77	-308.25		17766	3.6493	7924	13013			169.12	Si
SLU 74	0.41	-31532	-75	-323.47		19201	3.6493	8116	13327			176.9	Si
SLU 74	0.81	-30022	-75	-298.12		18282	3.6493	7993	13126			174.22	Si
SLU 75	0.41	-31532	-75	-323.47		19201	3.6493	8116	13327			176.9	Si
SLU 75	0.81	-30022	-75	-298.12		18282	3.6493	7993	13126			174.22	Si
SLU 82	0.41	-33531	-81	-367.94		20419	3.6493	8278	13594			168.73	Si
SLU 82	0.81	-32020	-81	-340.54		19498	3.6493	8155	13393			166.23	Si
SLU 63	0.41	-30673	-77	-334.36		18678	3.6493	8046	13213			171.72	Si
SLU 63	0.81	-29174	-77	-308.25		17766	3.6493	7924	13013			169.12	Si
SLU 60	0.41	-30673	-77	-334.36		18678	3.6493	8046	13213			171.72	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 60	0.81	-29174	-77	-308.25		17766	3.6493	7924	13013			169.12	Si
SLU 83	0.41	-33531	-81	-367.94		20419	3.6493	8278	13594			168.73	Si
SLU 83	0.81	-32020	-81	-340.54		19498	3.6493	8155	13393			166.23	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 13	0.41	-22719	-6907	-2419.67		13834	3.6493	11100	18229			2.64	Si
SLV 13	0.81	-21572	-6437	181.24		13136	3.6493	10961	17999			2.8	Si
SLV 2	0.41	-22608	6749	1977.48		13767	3.6493	11087	18207			2.7	Si
SLV 2	0.81	-21465	6264	-595.93		13071	3.6493	10948	17978			2.87	Si
SLV 1	0.41	-22608	6749	1977.48		13767	3.6493	11087	18207			2.7	Si
SLV 1	0.81	-21465	6264	-595.93		13071	3.6493	10948	17978			2.87	Si
SLV 3	0.41	-20024	6805	2037.15		12194	3.6493	10772	17690			2.6	Si
SLV 3	0.81	-18856	6335	-529.97		11482	3.6493	10630	17456			2.76	Si
SLV 8	0.41	-17048	2090	567.78		10381	3.6493	10410	17094			8.18	Si
SLV 8	0.81	-15851	1972	-181.01		9652	3.6493	10264	16855			8.55	Si
SLV 4	0.41	-20024	6805	2037.15		12194	3.6493	10772	17690			2.6	Si
SLV 4	0.81	-18856	6335	-529.97		11482	3.6493	10630	17456			2.76	Si
SLV 15	0.41	-20134	-6851	-2360		12261	3.6493	10785	17712			2.59	Si
SLV 15	0.81	-18964	-6367	247.19		11548	3.6493	10643	17478			2.75	Si
SLV 7	0.41	-17048	2090	567.78		10381	3.6493	10410	17094			8.18	Si
SLV 7	0.81	-15851	1972	-181.01		9652	3.6493	10264	16855			8.55	Si
SLV 16	0.41	-20134	-6851	-2360		12261	3.6493	10785	17712			2.59	Si
SLV 16	0.81	-18964	-6367	247.19		11548	3.6493	10643	17478			2.75	Si
SLV 14	0.41	-22719	-6907	-2419.67		13834	3.6493	11100	18229			2.64	Si
SLV 14	0.81	-21572	-6437	181.24		13136	3.6493	10961	17999			2.8	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.345 Wa 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 7	143750	0.27	9491	-15586	234.55	3234.47	13.79	Si
SLV 8	143750	0.27	9491	-15586	234.55	3234.47	13.79	Si
SLV 12	143750	0.27	9513	-15622	234.55	3241.26	13.82	Si
SLV 11	143750	0.27	9513	-15622	234.55	3241.26	13.82	Si
SLV 3	143750	0.27	11184	-18365	234.55	3754	16.01	Si
SLV 4	143750	0.27	11184	-18365	234.55	3754	16.01	Si
SLV 16	143750	0.27	11256	-18484	234.55	3775.88	16.1	Si
SLV 15	143750	0.27	11256	-18484	234.55	3775.88	16.1	Si
SLV 2	143750	0.27	12656	-20783	234.55	4191.89	17.87	Si
SLV 1	143750	0.27	12656	-20783	234.55	4191.89	17.87	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 0.345 Wa = 0.08 Ta = 0.0261

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 12	-10767	-18048	-3994	0	1727.2	0.911	0	2.73586	No
SLV 6	-18887	-24878	4164	0	2542.9	0.934	0	2.73586	No
SLV 8	-10765	-18010	-4047	0	1726.9	0.911	0	2.73586	No
SLV 5	-18887	-24878	4164	0	2542.9	0.934	0	2.73586	No
SLV 9	-18890	-24916	4217	0	2543.2	0.934	0	2.73586	No
SLV 11	-10767	-18048	-3994	0	1727.2	0.911	0	2.73586	No
SLV 10	-18890	-24916	4217	0	2543.2	0.934	0	2.73586	No
SLV 7	-10765	-18010	-4047	0	1726.9	0.911	0	2.73586	No
SLV 14	-16050	-22556	1405	0.031	2256.7	0.927	0.48876	11.13714	No
SLV 13	-16050	-22556	1405	0.031	2256.7	0.927	0.48876	11.13714	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	123.342	SLU 39	Si
V_SLU	166.226	SLU 81	Si
PF_SLV	14.005	SLV 15	Si
V_SLV	2.585	SLV 15	Si
PFFP_SLV	13.79	SLV 7	Si
R_SLV	0	SLV 5	No

Maschio 6

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
35.424	-0.169	33.569	-0.169	L1	L2	1.855	0.45	2.65	2.65	2.65			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 79	0.41	-15015	1890.17	17986	10853.25	5.742	Si
SLU 79	0.81	-14300	2090.44	17129	10475.73	5.011	Si
SLU 76	0.41	-15015	1890.17	17986	10853.25	5.742	Si
SLU 76	0.81	-14300	2090.44	17129	10475.73	5.011	Si
SLU 78	0.41	-15015	1890.17	17986	10853.25	5.742	Si
SLU 78	0.81	-14300	2090.44	17129	10475.73	5.011	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 75	0.41	-15015	1890.17	17986	10853.25	5.742	Si
SLU 75	0.81	-14300	2090.44	17129	10475.73	5.011	Si
SLU 83	0.41	-15952	1998.42	19107	11326.37	5.668	Si
SLU 83	0.81	-15231	2212	18244	10964.52	4.957	Si
SLU 81	0.41	-15952	1998.42	19107	11326.37	5.668	Si
SLU 81	0.81	-15231	2212	18244	10964.52	4.957	Si
SLU 77	0.41	-15015	1890.17	17986	10853.25	5.742	Si
SLU 77	0.81	-14300	2090.44	17129	10475.73	5.011	Si
SLU 80	0.41	-15015	1890.17	17986	10853.25	5.742	Si
SLU 80	0.81	-14300	2090.44	17129	10475.73	5.011	Si
SLU 84	0.41	-15952	1998.42	19107	11326.37	5.668	Si
SLU 84	0.81	-15231	2212	18244	10964.52	4.957	Si
SLU 82	0.41	-15952	1998.42	19107	11326.37	5.668	Si
SLU 82	0.81	-15231	2212	18244	10964.52	4.957	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 2	0.41	-9826	2041.41	11769	8236.68	4.035	Si
SLV 2	0.81	-8869	1397.41	10624	7512.16	5.376	Si
SLV 11	0.41	-8629	1119.02	10336	7327.29	6.548	Si
SLV 11	0.81	-8364	1462.44	10018	7122.43	4.87	Si
SLV 1	0.41	-9826	2041.41	11769	8236.68	4.035	Si
SLV 1	0.81	-8869	1397.41	10624	7512.16	5.376	Si
SLV 16	0.41	-10602	543.26	12699	8812.2	16.221	Si
SLV 16	0.81	-10469	1455.52	12539	8714.37	5.987	Si
SLV 4	0.41	-8704	2075.3	10426	7385.24	3.559	Si
SLV 4	0.81	-7851	1415.38	9404	6722.09	4.749	Si
SLV 3	0.41	-8704	2075.3	10426	7385.24	3.559	Si
SLV 3	0.81	-7851	1415.38	9404	6722.09	4.749	Si
SLV 8	0.41	-8060	1578.63	9654	6885.66	4.362	Si
SLV 8	0.81	-7579	1450.4	9078	6507.77	4.487	Si
SLV 7	0.41	-8060	1578.63	9654	6885.66	4.362	Si
SLV 7	0.81	-7579	1450.4	9078	6507.77	4.487	Si
SLV 12	0.41	-8629	1119.02	10336	7327.29	6.548	Si
SLV 12	0.81	-8364	1462.44	10018	7122.43	4.87	Si
SLV 15	0.41	-10602	543.26	12699	8812.2	16.221	Si
SLV 15	0.81	-10469	1455.52	12539	8714.37	5.987	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 81	0.41	-15952	-629	1998.42		19107	1.8552	8103	6765			10.75	Si
SLU 81	0.81	-15231	-630	2212		18244	1.8552	7988	6669			10.59	Si
SLU 80	0.41	-15015	-608	1890.17		17986	1.8552	7954	6640			10.92	Si
SLU 80	0.81	-14300	-608	2090.44		17129	1.8552	7839	6545			10.76	Si
SLU 79	0.41	-15015	-608	1890.17		17986	1.8552	7954	6640			10.92	Si
SLU 79	0.81	-14300	-608	2090.44		17129	1.8552	7839	6545			10.76	Si
SLU 83	0.41	-15952	-629	1998.42		19107	1.8552	8103	6765			10.75	Si
SLU 83	0.81	-15231	-630	2212		18244	1.8552	7988	6669			10.59	Si
SLU 78	0.41	-15015	-608	1890.17		17986	1.8552	7954	6640			10.92	Si
SLU 78	0.81	-14300	-608	2090.44		17129	1.8552	7839	6545			10.76	Si
SLU 75	0.41	-15015	-608	1890.17		17986	1.8552	7954	6640			10.92	Si
SLU 75	0.81	-14300	-608	2090.44		17129	1.8552	7839	6545			10.76	Si
SLU 84	0.41	-15952	-629	1998.42		19107	1.8552	8103	6765			10.75	Si
SLU 84	0.81	-15231	-630	2212		18244	1.8552	7988	6669			10.59	Si
SLU 76	0.41	-15015	-608	1890.17		17986	1.8552	7954	6640			10.92	Si
SLU 76	0.81	-14300	-608	2090.44		17129	1.8552	7839	6545			10.76	Si
SLU 77	0.41	-15015	-608	1890.17		17986	1.8552	7954	6640			10.92	Si
SLU 77	0.81	-14300	-608	2090.44		17129	1.8552	7839	6545			10.76	Si
SLU 82	0.41	-15952	-629	1998.42		19107	1.8552	8103	6765			10.75	Si
SLU 82	0.81	-15231	-630	2212		18244	1.8552	7988	6669			10.59	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 11	0.41	-8629	-2030	1119.02		10336	1.8552	10400	8683			4.28	Si
SLV 11	0.81	-8364	-1756	1462.44		10018	1.8552	10337	8630			4.91	Si
SLV 2	0.41	-9826	2742	2041.41		11769	1.8552	10687	8922			3.25	Si
SLV 2	0.81	-8869	2435	1397.41		10624	1.8552	10458	8731			3.59	Si
SLV 16	0.41	-10602	-3599	543.26		12699	1.8552	10873	9077			2.52	Si
SLV 16	0.81	-10469	-3293	1455.52		12539	1.8552	10841	9051			2.75	Si
SLV 12	0.41	-8629	-2030	1119.02		10336	1.8552	10400	8683			4.28	Si
SLV 12	0.81	-8364	-1756	1462.44		10018	1.8552	10337	8630			4.91	Si
SLV 3	0.41	-8704	2313	2075.3		10426	1.8552	10419	8698			3.76	Si
SLV 3	0.81	-7851	2126	1415.38		9404	1.8552	10214	8527			4.01	Si
SLV 1	0.41	-9826	2742	2041.41		11769	1.8552	10687	8922			3.25	Si
SLV 1	0.81	-8869	2435	1397.41		10624	1.8552	10458	8731			3.59	Si
SLV 4	0.41	-8704	2313	2075.3		10426	1.8552	10419	8698			3.76	Si
SLV 4	0.81	-7851	2126	1415.38		9404	1.8552	10214	8527			4.01	Si
SLV 14	0.41	-11723	-3170	509.36		14042	1.8552	11142	9302			2.93	Si
SLV 14	0.81	-11487	-2984	1437.54		13760	1.8552	11085	9255			3.1	Si
SLV 13	0.41	-11723	-3170	509.36		14042	1.8552	11142	9302			2.93	Si
SLV 13	0.81	-11487	-2984	1437.54		13760	1.8552	11085	9255			3.1	Si
SLV 15	0.41	-10602	-3599	543.26		12699	1.8552	10873	9077			2.52	Si
SLV 15	0.81	-10469	-3293	1455.52		12539	1.8552	10841	9051			2.75	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.345 Wa 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 7	143750	0.27	8735	-7292	119.24	1523.46	12.78	Si
SLV 8	143750	0.27	8735	-7292	119.24	1523.46	12.78	Si



Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 4	143750	0.27	9092	-7591	119.24	1580.84	13.26	Si
SLV 3	143750	0.27	9092	-7591	119.24	1580.84	13.26	Si
SLV 11	143750	0.27	9684	-8085	119.24	1674.96	14.05	Si
SLV 12	143750	0.27	9684	-8085	119.24	1674.96	14.05	Si
SLV 2	143750	0.27	10349	-8640	119.24	1779.27	14.92	Si
SLV 1	143750	0.27	10349	-8640	119.24	1779.27	14.92	Si
SLV 16	143750	0.27	12258	-10234	119.24	2071.56	17.37	Si
SLV 15	143750	0.27	12258	-10234	119.24	2071.56	17.37	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 0.345 $W_a = 0.08$ $T_a = 0.0261$

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 13	-8194	-13679	52	0.096	1150.8	0.927	1.51083	11.13714	No
SLV 14	-8194	-13679	52	0.096	1150.8	0.927	1.51083	11.13714	No
SLV 16	-7443	-12305	-22	0.101	1075.2	0.923	1.58228	11.13714	No
SLV 15	-7443	-12305	-22	0.101	1075.2	0.923	1.58228	11.13714	No
SLV 3	-5666	-8427	-52	0.1	897.2	0.912	1.59566	11.13714	No
SLV 4	-5666	-8427	-52	0.1	897.2	0.912	1.59566	11.13714	No
SLV 2	-6417	-9801	22	0.102	972.2	0.917	1.62295	11.13714	No
SLV 1	-6417	-9801	22	0.102	972.2	0.917	1.62295	11.13714	No
SLV 10	-8449	-13925	128	0.089	1176.4	0.928	1.39073	2.73586	No
SLV 9	-8449	-13925	128	0.089	1176.4	0.928	1.39073	2.73586	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	4.957	SLU 81	Si
V_SLU	10.59	SLU 81	Si
PF_SLV	3.559	SLV 3	Si
V_SLV	2.522	SLV 15	Si
PFFP_SLV	12.776	SLV 7	Si
R_SLV	0.136	SLV 13	No

Maschio 7

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
25.794	4.507	30.808	4.507	L1	L2	5.014	0.3	2.65	2.65	2.65			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 42	-0.98	-37586	5964.74	24988	65321.07	10.951	Si
SLU 42	1.19	-32877	4482.11	21858	60305.53	13.455	Si
SLU 81	-0.98	-43132	6385.42	28675	70065.13	10.973	Si
SLU 81	1.19	-36833	4675.16	24487	64579.77	13.813	Si
SLU 83	-0.98	-43132	6385.42	28675	70065.13	10.973	Si
SLU 83	1.19	-36833	4675.16	24487	64579.77	13.813	Si
SLU 38	-0.98	-34744	5299.88	23099	62402.54	11.774	Si
SLU 38	1.19	-29930	3843.57	19898	56703.54	14.753	Si
SLU 39	-0.98	-37586	5964.74	24988	65321.07	10.951	Si
SLU 39	1.19	-32877	4482.11	21858	60305.53	13.455	Si
SLU 37	-0.98	-34744	5299.88	23099	62402.54	11.774	Si
SLU 37	1.19	-29930	3843.57	19898	56703.54	14.753	Si
SLU 84	-0.98	-43132	6385.42	28675	70065.13	10.973	Si
SLU 84	1.19	-36833	4675.16	24487	64579.77	13.813	Si
SLU 40	-0.98	-37586	5964.74	24988	65321.07	10.951	Si
SLU 40	1.19	-32877	4482.11	21858	60305.53	13.455	Si
SLU 41	-0.98	-37586	5964.74	24988	65321.07	10.951	Si
SLU 41	1.19	-32877	4482.11	21858	60305.53	13.455	Si
SLU 82	-0.98	-43132	6385.42	28675	70065.13	10.973	Si
SLU 82	1.19	-36833	4675.16	24487	64579.77	13.813	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 13	-0.98	-27038	10899.21	17976	57810.97	5.304	Si
SLV 13	1.19	-20572	3822.25	13677	45800.41	11.983	Si
SLV 4	-0.98	-26560	-4079.82	17657	56961.27	13.962	Si
SLV 4	1.19	-22883	596.35	15213	50223.12	84.218	Si
SLV 9	-0.98	-27474	6601.16	18265	58579.74	8.874	Si
SLV 9	1.19	-21039	2483.48	13987	46705.58	18.806	Si
SLV 15	-0.98	-26640	10276.38	17711	57104.85	5.557	Si
SLV 15	1.19	-20798	3960.51	13827	46238.38	11.675	Si
SLV 11	-0.98	-26148	4525.08	17384	56225	12.425	Si
SLV 11	1.19	-21790	2944.36	14487	48150.5	16.353	Si
SLV 14	-0.98	-27038	10899.21	17976	57810.97	5.304	Si
SLV 14	1.19	-20572	3822.25	13677	45800.41	11.983	Si
SLV 16	-0.98	-26640	10276.38	17711	57104.85	5.557	Si
SLV 16	1.19	-20798	3960.51	13827	46238.38	11.675	Si
SLV 10	-0.98	-27474	6601.16	18265	58579.74	8.874	Si
SLV 10	1.19	-21039	2483.48	13987	46705.58	18.806	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 3	-0.98	-26560	-4079.82	17657	56961.27	13.962	Si
SLV 3	1.19	-22883	596.35	15213	50223.12	84.218	Si
SLV 12	-0.98	-26148	4525.08	17384	56225	12.425	Si
SLV 12	1.19	-21790	2944.36	14487	48150.5	16.353	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLU 81	-0.98	-43132	-4268	6385.42		28675	5.0139	9379	14107			3.31	Si
SLU 81	1.19	-36833	-3556	4675.16		24487	5.0139	8821	13267			3.73	Si
SLU 83	-0.98	-43132	-4268	6385.42		28675	5.0139	9379	14107			3.31	Si
SLU 83	1.19	-36833	-3556	4675.16		24487	5.0139	8821	13267			3.73	Si
SLU 39	-0.98	-37586	-3923	5964.74		24988	5.0139	8887	13368			3.41	Si
SLU 39	1.19	-32877	-3289	4482.11		21858	5.0139	8470	12740			3.87	Si
SLU 41	-0.98	-37586	-3923	5964.74		24988	5.0139	8887	13368			3.41	Si
SLU 41	1.19	-32877	-3289	4482.11		21858	5.0139	8470	12740			3.87	Si
SLU 42	-0.98	-37586	-3923	5964.74		24988	5.0139	8887	13368			3.41	Si
SLU 42	1.19	-32877	-3289	4482.11		21858	5.0139	8470	12740			3.87	Si
SLU 84	-0.98	-43132	-4268	6385.42		28675	5.0139	9379	14107			3.31	Si
SLU 84	1.19	-36833	-3556	4675.16		24487	5.0139	8821	13267			3.73	Si
SLU 40	-0.98	-37586	-3923	5964.74		24988	5.0139	8887	13368			3.41	Si
SLU 40	1.19	-32877	-3289	4482.11		21858	5.0139	8470	12740			3.87	Si
SLU 77	-0.98	-40290	-3819	5720.56		26786	5.0139	9127	13728			3.59	Si
SLU 77	1.19	-33885	-3164	4036.63		22527	5.0139	8559	12874			4.07	Si
SLU 82	-0.98	-43132	-4268	6385.42		28675	5.0139	9379	14107			3.31	Si
SLU 82	1.19	-36833	-3556	4675.16		24487	5.0139	8821	13267			3.73	Si
SLU 75	-0.98	-40290	-3819	5720.56		26786	5.0139	9127	13728			3.59	Si
SLU 75	1.19	-33885	-3164	4036.63		22527	5.0139	8559	12874			4.07	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLV 4	-0.98	-26560	-9588	-4079.82		17657	5.0139	11865	17847			1.86	Si
SLV 4	1.19	-22883	-7856	596.35		15213	5.0139	11376	17111			2.18	Si
SLV 16	-0.98	-26640	4359	10276.38		17711	5.0139	11876	17863			4.1	Si
SLV 16	1.19	-20798	3725	3960.51		13827	5.0139	11099	16694			4.48	Si
SLV 1	-0.98	-26957	-8961	-3457		17922	5.0139	11918	17926			2	Si
SLV 1	1.19	-22657	-7483	458.08		15063	5.0139	11346	17066			2.28	Si
SLV 15	-0.98	-26640	4359	10276.38		17711	5.0139	11876	17863			4.1	Si
SLV 15	1.19	-20798	3725	3960.51		13827	5.0139	11099	16694			4.48	Si
SLV 7	-0.98	-26124	-5437	218.22		17368	5.0139	11807	17759			3.27	Si
SLV 7	1.19	-22416	-4238	1935.11		14903	5.0139	11314	17018			4.02	Si
SLV 3	-0.98	-26560	-9588	-4079.82		17657	5.0139	11865	17847			1.86	Si
SLV 3	1.19	-22883	-7856	596.35		15213	5.0139	11376	17111			2.18	Si
SLV 14	-0.98	-27038	4985	10899.21		17976	5.0139	11928	17942			3.6	Si
SLV 14	1.19	-20572	4098	3822.25		13677	5.0139	11069	16649			4.06	Si
SLV 2	-0.98	-26957	-8961	-3457		17922	5.0139	11918	17926			2	Si
SLV 2	1.19	-22657	-7483	458.08		15063	5.0139	11346	17066			2.28	Si
SLV 13	-0.98	-27038	4985	10899.21		17976	5.0139	11928	17942			3.6	Si
SLV 13	1.19	-20572	4098	3822.25		13677	5.0139	11069	16649			4.06	Si
SLV 8	-0.98	-26124	-5437	218.22		17368	5.0139	11807	17759			3.27	Si
SLV 8	1.19	-22416	-4238	1935.11		14903	5.0139	11314	17018			4.02	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.345 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 11	143750	0.27	15714	-23637	221.11	3089.54	13.97	Si
SLV 12	143750	0.27	15714	-23637	221.11	3089.54	13.97	Si
SLV 16	143750	0.27	15776	-23730	221.11	3099.93	14.02	Si
SLV 15	143750	0.27	15776	-23730	221.11	3099.93	14.02	Si
SLV 7	143750	0.27	15841	-23828	221.11	3110.79	14.07	Si
SLV 8	143750	0.27	15841	-23828	221.11	3110.79	14.07	Si
SLV 13	143750	0.27	15956	-24001	221.11	3130.02	14.16	Si
SLV 14	143750	0.27	15956	-24001	221.11	3130.02	14.16	Si
SLV 4	143750	0.27	16200	-24367	221.11	3170.44	14.34	Si
SLV 3	143750	0.27	16200	-24367	221.11	3170.44	14.34	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 0.345 Wa = 0.05 Ta = 0.0391

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 6	-19731	-27450	-2312	0	2575.1	0.939	0	2.83646	No
SLV 9	-19149	-27474	-2333	0	2516.2	0.938	0	2.83646	No
SLV 10	-19149	-27474	-2333	0	2516.2	0.938	0	2.83646	No
SLV 5	-19731	-27450	-2312	0	2575.1	0.939	0	2.83646	No
SLV 7	-20549	-26124	2333	0	2658	0.94	0	2.83646	No
SLV 12	-19967	-26148	2312	0	2599	0.939	0	2.83646	No
SLV 11	-19967	-26148	2312	0	2599	0.939	0	2.83646	No
SLV 8	-20549	-26124	2333	0	2658	0.94	0	2.83646	No
SLV 13	-18756	-27038	-732	0.033	2476.4	0.937	0.51071	12.73267	No
SLV 14	-18756	-27038	-732	0.033	2476.4	0.937	0.51071	12.73267	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	10.951	SLU 39	Si
V_SLV	3.306	SLU 81	Si
PF_SLV	5.304	SLV 13	Si
V_SLV	1.861	SLV 3	Si
PFFP_SLV	13.973	SLV 11	Si
R_SLV	0	SLV 5	No



Maschio 8

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
31.808	4.507	35.424	4.507	L1	L2	3.616	0.3	2.65	2.65	2.65			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _k	f _{vk0}	f _{medio}	τ ₀	f _{v0}	μ	φ	f _{v,lim}	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γ_M = 3

Comb.	Quota	N	M	σ ₀	Mu	c.s.	Verifica
SLU 78	-0.98	-30737	-3879.24	28334	36244.46	9.343	Si
SLU 78	1.19	-26444	-5494.87	24376	33505.03	6.098	Si
SLU 40	-0.98	-28867	-3922.4	26609	35143.43	8.96	Si
SLU 40	1.19	-25906	-5668.76	23880	33108.4	5.841	Si
SLU 42	-0.98	-28867	-3922.4	26609	35143.43	8.96	Si
SLU 42	1.19	-25906	-5668.76	23880	33108.4	5.841	Si
SLU 82	-0.98	-33051	-4271.27	30466	37407.86	8.758	Si
SLU 82	1.19	-28926	-6140.94	26664	35180.55	5.729	Si
SLU 83	-0.98	-33051	-4271.27	30466	37407.86	8.758	Si
SLU 83	1.19	-28926	-6140.94	26664	35180.55	5.729	Si
SLU 39	-0.98	-28867	-3922.4	26609	35143.43	8.96	Si
SLU 39	1.19	-25906	-5668.76	23880	33108.4	5.841	Si
SLU 77	-0.98	-30737	-3879.24	28334	36244.46	9.343	Si
SLU 77	1.19	-26444	-5494.87	24376	33505.03	6.098	Si
SLU 84	-0.98	-33051	-4271.27	30466	37407.86	8.758	Si
SLU 84	1.19	-28926	-6140.94	26664	35180.55	5.729	Si
SLU 41	-0.98	-28867	-3922.4	26609	35143.43	8.96	Si
SLU 41	1.19	-25906	-5668.76	23880	33108.4	5.841	Si
SLU 81	-0.98	-33051	-4271.27	30466	37407.86	8.758	Si
SLU 81	1.19	-28926	-6140.94	26664	35180.55	5.729	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γ_M = 2

Comb.	Quota	N	M	σ ₀	Mu	c.s.	Verifica
SLV 3	-0.98	-21719	-7856.23	20021	32835.27	4.18	Si
SLV 3	1.19	-16187	-2531.37	14921	25693.3	10.15	Si
SLV 2	-0.98	-21815	-7190.95	20109	32951.67	4.582	Si
SLV 2	1.19	-16329	-2283.76	15052	25886.44	11.335	Si
SLV 7	-0.98	-20577	-5040.81	18968	31428.85	6.235	Si
SLV 7	1.19	-16378	-3444.12	15097	25952.97	7.535	Si
SLV 16	-0.98	-18775	2405.46	17307	29137.97	12.113	Si
SLV 16	1.19	-17203	-4313.87	15858	27067.27	6.274	Si
SLV 11	-0.98	-19694	-1962.3	18153	30316.97	15.45	Si
SLV 11	1.19	-16682	-3978.87	15378	26366.53	6.627	Si
SLV 15	-0.98	-18775	2405.46	17307	29137.97	12.113	Si
SLV 15	1.19	-17203	-4313.87	15858	27067.27	6.274	Si
SLV 4	-0.98	-21719	-7856.23	20021	32835.27	4.18	Si
SLV 4	1.19	-16187	-2531.37	14921	25693.3	10.15	Si
SLV 8	-0.98	-20577	-5040.81	18968	31428.85	6.235	Si
SLV 8	1.19	-16378	-3444.12	15097	25952.97	7.535	Si
SLV 1	-0.98	-21815	-7190.95	20109	32951.67	4.582	Si
SLV 1	1.19	-16329	-2283.76	15052	25886.44	11.335	Si
SLV 12	-0.98	-19694	-1962.3	18153	30316.97	15.45	Si
SLV 12	1.19	-16682	-3978.87	15378	26366.53	6.627	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, γ_M = 3

Comb.	Quota	N	V par	M	σ ₀	σ _N	I'	f _{vd}	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLU 75	-0.98	-30737	3817	-3879.24		28334	3.6161	9333	10125			2.65	Si
SLU 75	1.19	-26444	3319	-5494.87		24376	3.6161	8806	9553			2.88	Si
SLU 82	-0.98	-33051	4264	-4271.27		30466	3.6161	9618	10434			2.45	Si
SLU 82	1.19	-28926	3711	-6140.94		26664	3.6161	9111	9884			2.66	Si
SLU 39	-0.98	-28867	3920	-3922.4		26609	3.6161	9103	9876			2.52	Si
SLU 39	1.19	-25906	3415	-5668.76		23880	3.6161	8740	9481			2.78	Si
SLU 40	-0.98	-28867	3920	-3922.4		26609	3.6161	9103	9876			2.52	Si
SLU 40	1.19	-25906	3415	-5668.76		23880	3.6161	8740	9481			2.78	Si
SLU 83	-0.98	-33051	4264	-4271.27		30466	3.6161	9618	10434			2.45	Si
SLU 83	1.19	-28926	3711	-6140.94		26664	3.6161	9111	9884			2.66	Si
SLU 77	-0.98	-30737	3817	-3879.24		28334	3.6161	9333	10125			2.65	Si
SLU 77	1.19	-26444	3319	-5494.87		24376	3.6161	8806	9553			2.88	Si
SLU 41	-0.98	-28867	3920	-3922.4		26609	3.6161	9103	9876			2.52	Si
SLU 41	1.19	-25906	3415	-5668.76		23880	3.6161	8740	9481			2.78	Si
SLU 42	-0.98	-28867	3920	-3922.4		26609	3.6161	9103	9876			2.52	Si
SLU 42	1.19	-25906	3415	-5668.76		23880	3.6161	8740	9481			2.78	Si
SLU 81	-0.98	-33051	4264	-4271.27		30466	3.6161	9618	10434			2.45	Si
SLU 81	1.19	-28926	3711	-6140.94		26664	3.6161	9111	9884			2.66	Si
SLU 84	-0.98	-33051	4264	-4271.27		30466	3.6161	9618	10434			2.45	Si
SLU 84	1.19	-28926	3711	-6140.94		26664	3.6161	9111	9884			2.66	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, γ_M = 2

Comb.	Quota	N	V par	M	σ ₀	σ _N	I'	f _{vd}	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLV 16	-0.98	-18775	7295	2405.46		17307	3.6161	11795	12795			1.75	Si
SLV 16	1.19	-17203	6335	-4313.87		15858	3.6161	11505	12481			1.97	Si
SLV 14	-0.98	-18871	7414	3070.74		17395	3.6161	11812	12814			1.73	Si
SLV 14	1.19	-17344	6108	-4066.26		15988	3.6161	11531	12509			2.05	Si
SLV 11	-0.98	-19694	3617	-1962.3		18153	3.6161	11964	12979			3.59	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 11	1.19	-16682	3641	-3978.87		15378	3.6161	11409	12377			3.4	Si
SLV 4	-0.98	-21719	-2814	-7856.23		20021	3.6161	12337	13384			4.76	Si
SLV 4	1.19	-16187	-2116	-2531.37		14921	3.6161	11318	12278			5.8	Si
SLV 13	-0.98	-18871	7414	3070.74		17395	3.6161	11812	12814			1.73	Si
SLV 13	1.19	-17344	6108	-4066.26		15988	3.6161	11531	12509			2.05	Si
SLV 10	-0.98	-20013	4015	255.32		18448	3.6161	12023	13043			3.25	Si
SLV 10	1.19	-17154	2887	-3153.5		15813	3.6161	11496	12471			4.32	Si
SLV 12	-0.98	-19694	3617	-1962.3		18153	3.6161	11964	12979			3.59	Si
SLV 12	1.19	-16682	3641	-3978.87		15378	3.6161	11409	12377			3.4	Si
SLV 9	-0.98	-20013	4015	255.32		18448	3.6161	12023	13043			3.25	Si
SLV 9	1.19	-17154	2887	-3153.5		15813	3.6161	11496	12471			4.32	Si
SLV 3	-0.98	-21719	-2814	-7856.23		20021	3.6161	12337	13384			4.76	Si
SLV 3	1.19	-16187	-2116	-2531.37		14921	3.6161	11318	12278			5.8	Si
SLV 15	-0.98	-18775	7295	2405.46		17307	3.6161	11795	12795			1.75	Si
SLV 15	1.19	-17203	6335	-4313.87		15858	3.6161	11505	12481			1.97	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.345 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 11	143750	0.27	17150	-18605	159.47	2399.03	15.04	Si
SLV 12	143750	0.27	17150	-18605	159.47	2399.03	15.04	Si
SLV 7	143750	0.27	17221	-18682	159.47	2407.36	15.1	Si
SLV 8	143750	0.27	17221	-18682	159.47	2407.36	15.1	Si
SLV 15	143750	0.27	17267	-18732	159.47	2412.76	15.13	Si
SLV 16	143750	0.27	17267	-18732	159.47	2412.76	15.13	Si
SLV 13	143750	0.27	17439	-18919	159.47	2432.8	15.26	Si
SLV 14	143750	0.27	17439	-18919	159.47	2432.8	15.26	Si
SLV 4	143750	0.27	17505	-18990	159.47	2440.41	15.3	Si
SLV 3	143750	0.27	17505	-18990	159.47	2440.41	15.3	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 0.345 Wa = 0.05 Ta = 0.0391

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 8	-15285	-20577	1129	0.002	1964	0.942	0.0249	2.83646	No
SLV 7	-15285	-20577	1129	0.002	1964	0.942	0.0249	2.83646	No
SLV 10	-15642	-20013	-1129	0.003	2000.2	0.943	0.04148	2.83646	No
SLV 9	-15642	-20013	-1129	0.003	2000.2	0.943	0.04148	2.83646	No
SLV 6	-15386	-20896	-1113	0.003	1974.3	0.942	0.04365	2.83646	No
SLV 5	-15386	-20896	-1113	0.003	1974.3	0.942	0.04365	2.83646	No
SLV 12	-15541	-19694	1113	0.003	1990	0.942	0.05073	2.83646	No
SLV 11	-15541	-19694	1113	0.003	1990	0.942	0.05073	2.83646	No
SLV 4	-15022	-21719	364	0.044	1937.3	0.941	0.68383	12.73267	No
SLV 3	-15022	-21719	364	0.044	1937.3	0.941	0.68383	12.73267	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	5.729	SLU 81	Si
V_SLU	2.447	SLU 81	Si
PF_SLV	4.18	SLV 3	Si
V_SLV	1.728	SLV 13	Si
PFFP_SLV	15.044	SLV 11	Si
R_SLV	0.009	SLV 7	No

Maschio 10

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
26.639	9.502	30.644	9.502	L1	L2	4.005	0.45	2.65	2.65	2.65			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	t0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 81	-0.98	-39033	2644.4	21660	57374.53	21.697	Si
SLU 81	1.22	-28584	1683.44	15862	46090	27.378	Si
SLU 18	-0.98	-29898	2107.45	16591	47672.85	22.621	Si
SLU 18	1.22	-21930	1361.05	12169	37351.1	27.443	Si
SLU 40	-0.98	-32759	2394.58	18178	50955.52	21.28	Si
SLU 40	1.22	-24585	1579.42	13643	40982.69	25.948	Si
SLU 82	-0.98	-39033	2644.4	21660	57374.53	21.697	Si
SLU 82	1.22	-28584	1683.44	15862	46090	27.378	Si
SLU 42	-0.98	-32759	2394.58	18178	50955.52	21.28	Si
SLU 42	1.22	-24585	1579.42	13643	40982.69	25.948	Si
SLU 84	-0.98	-39033	2644.4	21660	57374.53	21.697	Si
SLU 84	1.22	-28584	1683.44	15862	46090	27.378	Si
SLU 41	-0.98	-32759	2394.58	18178	50955.52	21.28	Si
SLU 41	1.22	-24585	1579.42	13643	40982.69	25.948	Si
SLU 39	-0.98	-32759	2394.58	18178	50955.52	21.28	Si
SLU 39	1.22	-24585	1579.42	13643	40982.69	25.948	Si
SLU 83	-0.98	-39033	2644.4	21660	57374.53	21.697	Si
SLU 83	1.22	-28584	1683.44	15862	46090	27.378	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 20	-0.98	-29898	2107.45	16591	47672.85	22.621	Si
SLU 20	1.22	-21930	1361.05	12169	37351.1	27.443	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 4	-0.98	-20836	2593.72	11562	37772.31	14.563	Si
SLV 4	1.22	-15546	5204.22	8627	28930.43	5.559	Si
SLV 1	-0.98	-15683	5074.63	8703	29165.36	5.747	Si
SLV 1	1.22	-12290	5238.81	6820	23234.22	4.435	Si
SLV 9	-0.98	-19920	4846.52	11054	36278.34	7.485	Si
SLV 9	1.22	-14105	-453.66	7827	26433.27	58.267	Si
SLV 5	-0.98	-15190	6287.68	8429	28316.6	4.504	Si
SLV 5	1.22	-11514	2192.26	6389	21848.33	9.966	Si
SLV 13	-0.98	-31451	270.78	17453	53980.35	199.355	Si
SLV 13	1.22	-20927	-3580.92	11613	37920.52	10.59	Si
SLV 6	-0.98	-15190	6287.68	8429	28316.6	4.504	Si
SLV 6	1.22	-11514	2192.26	6389	21848.33	9.966	Si
SLV 10	-0.98	-19920	4846.52	11054	36278.34	7.485	Si
SLV 10	1.22	-14105	-453.66	7827	26433.27	58.267	Si
SLV 2	-0.98	-15683	5074.63	8703	29165.36	5.747	Si
SLV 2	1.22	-12290	5238.81	6820	23234.22	4.435	Si
SLV 3	-0.98	-20836	2593.72	11562	37772.31	14.563	Si
SLV 3	1.22	-15546	5204.22	8627	28930.43	5.559	Si
SLV 14	-0.98	-31451	270.78	17453	53980.35	199.355	Si
SLV 14	1.22	-20927	-3580.92	11613	37920.52	10.59	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 75	-0.98	-37319	-2266	2360.44	20709	4.0046	8317	14987				6.61	Si
SLU 75	1.22	-26915	-1666	1454.02	14935	4.0046	7547	13600				8.16	Si
SLU 73	-0.98	-37319	-2266	2360.44	20709	4.0046	8317	14987				6.61	Si
SLU 73	1.22	-26915	-1666	1454.02	14935	4.0046	7547	13600				8.16	Si
SLU 81	-0.98	-39033	-2421	2644.4	21660	4.0046	8444	15216				6.29	Si
SLU 81	1.22	-28584	-1796	1683.44	15862	4.0046	7670	13823				7.69	Si
SLU 82	-0.98	-39033	-2421	2644.4	21660	4.0046	8444	15216				6.29	Si
SLU 82	1.22	-28584	-1796	1683.44	15862	4.0046	7670	13823				7.69	Si
SLU 84	-0.98	-39033	-2421	2644.4	21660	4.0046	8444	15216				6.29	Si
SLU 84	1.22	-28584	-1796	1683.44	15862	4.0046	7670	13823				7.69	Si
SLU 83	-0.98	-39033	-2421	2644.4	21660	4.0046	8444	15216				6.29	Si
SLU 83	1.22	-28584	-1796	1683.44	15862	4.0046	7670	13823				7.69	Si
SLU 74	-0.98	-37319	-2266	2360.44	20709	4.0046	8317	14987				6.61	Si
SLU 74	1.22	-26915	-1666	1454.02	14935	4.0046	7547	13600				8.16	Si
SLU 79	-0.98	-37319	-2266	2360.44	20709	4.0046	8317	14987				6.61	Si
SLU 79	1.22	-26915	-1666	1454.02	14935	4.0046	7547	13600				8.16	Si
SLU 78	-0.98	-37319	-2266	2360.44	20709	4.0046	8317	14987				6.61	Si
SLU 78	1.22	-26915	-1666	1454.02	14935	4.0046	7547	13600				8.16	Si
SLU 76	-0.98	-37319	-2266	2360.44	20709	4.0046	8317	14987				6.61	Si
SLU 76	1.22	-26915	-1666	1454.02	14935	4.0046	7547	13600				8.16	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 13	-0.98	-31451	6341	270.78	17453	4.0046	11824	21308				3.36	Si
SLV 13	1.22	-20927	4289	-3580.92	11613	4.0046	10656	19203				4.48	Si
SLV 4	-0.98	-20836	-9376	2593.72	11562	4.0046	10646	19185				2.05	Si
SLV 4	1.22	-15546	-6481	5204.22	8627	4.0046	10059	18127				2.8	Si
SLV 15	-0.98	-36605	5849	-2210.14	20312	4.0046	12396	22338				3.82	Si
SLV 15	1.22	-24184	4031	-3615.51	13420	4.0046	11017	19854				4.93	Si
SLV 7	-0.98	-32367	-4621	-1982.03	17961	4.0046	11926	21491				4.65	Si
SLV 7	1.22	-22369	-3102	2076.96	12413	4.0046	10816	19491				6.28	Si
SLV 2	-0.98	-15683	-8884	5074.63	8703	4.0046	10074	18154				2.04	Si
SLV 2	1.22	-12290	-6223	5238.81	6820	4.0046	9697	17475				2.81	Si
SLV 8	-0.98	-32367	-4621	-1982.03	17961	4.0046	11926	21491				4.65	Si
SLV 8	1.22	-22369	-3102	2076.96	12413	4.0046	10816	19491				6.28	Si
SLV 1	-0.98	-15683	-8884	5074.63	8703	4.0046	10074	18154				2.04	Si
SLV 1	1.22	-12290	-6223	5238.81	6820	4.0046	9697	17475				2.81	Si
SLV 3	-0.98	-20836	-9376	2593.72	11562	4.0046	10646	19185				2.05	Si
SLV 3	1.22	-15546	-6481	5204.22	8627	4.0046	10059	18127				2.8	Si
SLV 16	-0.98	-36605	5849	-2210.14	20312	4.0046	12396	22338				3.82	Si
SLV 16	1.22	-24184	4031	-3615.51	13420	4.0046	11017	19854				4.93	Si
SLV 14	-0.98	-31451	6341	270.78	17453	4.0046	11824	21308				3.36	Si
SLV 14	1.22	-20927	4289	-3580.92	11613	4.0046	10656	19203				4.48	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.345 Wa 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 5	143750	0.27	7703	-13882	261.14	2926.5	11.21	Si
SLV 6	143750	0.27	7703	-13882	261.14	2926.5	11.21	Si
SLV 2	143750	0.27	8792	-15844	261.14	3308.42	12.67	Si
SLV 1	143750	0.27	8792	-15844	261.14	3308.42	12.67	Si
SLV 9	143750	0.27	9224	-16622	261.14	3457.7	13.24	Si
SLV 10	143750	0.27	9224	-16622	261.14	3457.7	13.24	Si
SLV 4	143750	0.27	11246	-20267	261.14	4140.32	15.85	Si
SLV 3	143750	0.27	11246	-20267	261.14	4140.32	15.85	Si
SLV 14	143750	0.27	13861	-24979	261.14	4982.76	19.08	Si
SLV 13	143750	0.27	13861	-24979	261.14	4982.76	19.08	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 0.345 Wa = 0.08 Ta = 0.0261



Comb.	N top	N base	V orto	$\alpha 0$	M*	e*	a0*	aLim	Verifica
SLV 6	-9307	-15190	-1670	0	1647	0.902	0	2.73586	No
SLV 5	-9307	-15190	-1670	0	1647	0.902	0	2.73586	No
SLV 9	-12566	-19920	-1729	0.004	1970.1	0.913	0.06366	2.73586	No
SLV 10	-12566	-19920	-1729	0.004	1970.1	0.913	0.06366	2.73586	No
SLV 4	-13643	-20836	632	0.07	2077.8	0.917	1.11003	11.13714	No
SLV 3	-13643	-20836	632	0.07	2077.8	0.917	1.11003	11.13714	No
SLV 14	-20749	-31451	-595	0.076	2792.8	0.934	1.17837	11.13714	No
SLV 13	-20749	-31451	-595	0.076	2792.8	0.934	1.17837	11.13714	No
SLV 15	-24505	-36605	435	0.082	3172.8	0.94	1.27446	11.13714	No
SLV 16	-24505	-36605	435	0.082	3172.8	0.94	1.27446	11.13714	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	21.28	SLU 39	Si
V_SLU	6.286	SLU 81	Si
PF_SLV	4.435	SLV 1	Si
V_SLV	2.043	SLV 1	Si
PFFP_SLV	11.206	SLV 5	Si
R_SLV	0	SLV 5	No

Maschio 11

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s,sx	a.s,dx
31.644	9.502	35.424	9.502	L1	L2	3.78	0.45	2.65	2.65	2.65			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _k	f _{vk0}	f _{medio}	$\tau 0$	f _{v0}	μ	ϕ	f _{v,lim}	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	$\alpha 0$	Mu	c.s.	Verifica
SLU 72	-0.98	-31712	-44.41	18642	46224.55	1000	Si
SLU 72	1.22	-20996	-1037.78	12342	33672.76	32.447	Si
SLU 69	-0.98	-31712	-44.41	18642	46224.55	1000	Si
SLU 69	1.22	-20996	-1037.78	12342	33672.76	32.447	Si
SLU 66	-0.98	-31712	-44.41	18642	46224.55	1000	Si
SLU 66	1.22	-20996	-1037.78	12342	33672.76	32.447	Si
SLU 68	-0.98	-31712	-44.41	18642	46224.55	1000	Si
SLU 68	1.22	-20996	-1037.78	12342	33672.76	32.447	Si
SLU 26	-0.98	-25753	-56.05	15138	39631.55	707.027	Si
SLU 26	1.22	-17368	-865.58	10209	28713.91	33.173	Si
SLU 64	-0.98	-31712	-44.41	18642	46224.55	1000	Si
SLU 64	1.22	-20996	-1037.78	12342	33672.76	32.447	Si
SLU 71	-0.98	-31712	-44.41	18642	46224.55	1000	Si
SLU 71	1.22	-20996	-1037.78	12342	33672.76	32.447	Si
SLU 70	-0.98	-31712	-44.41	18642	46224.55	1000	Si
SLU 70	1.22	-20996	-1037.78	12342	33672.76	32.447	Si
SLU 67	-0.98	-31712	-44.41	18642	46224.55	1000	Si
SLU 67	1.22	-20996	-1037.78	12342	33672.76	32.447	Si
SLU 65	-0.98	-31712	-44.41	18642	46224.55	1000	Si
SLU 65	1.22	-20996	-1037.78	12342	33672.76	32.447	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	$\alpha 0$	Mu	c.s.	Verifica
SLV 6	-0.98	-20823	-3618.35	12240	35416.1	9.788	Si
SLV 6	1.22	-13948	-997.48	8199	24595.47	24.658	Si
SLV 2	-0.98	-23473	-7815.27	13798	39358.63	5.036	Si
SLV 2	1.22	-14666	-784.17	8621	25765.38	32.857	Si
SLV 5	-0.98	-20823	-3618.35	12240	35416.1	9.788	Si
SLV 5	1.22	-13948	-997.48	8199	24595.47	24.658	Si
SLV 15	-0.98	-26557	7907.36	15611	43784.93	5.537	Si
SLV 15	1.22	-18786	-776.35	11043	32300.34	41.606	Si
SLV 1	-0.98	-23473	-7815.27	13798	39358.63	5.036	Si
SLV 1	1.22	-14666	-784.17	8621	25765.38	32.857	Si
SLV 13	-0.98	-24098	7046.26	14166	40269.11	5.715	Si
SLV 13	1.22	-17362	-918.8	10206	30076.64	32.735	Si
SLV 3	-0.98	-25933	-6954.17	15244	42902.39	6.169	Si
SLV 3	1.22	-16090	-641.72	9458	28058.92	43.725	Si
SLV 4	-0.98	-25933	-6954.17	15244	42902.39	6.169	Si
SLV 4	1.22	-16090	-641.72	9458	28058.92	43.725	Si
SLV 16	-0.98	-26557	7907.36	15611	43784.93	5.537	Si
SLV 16	1.22	-18786	-776.35	11043	32300.34	41.606	Si
SLV 14	-0.98	-24098	7046.26	14166	40269.11	5.715	Si
SLV 14	1.22	-17362	-918.8	10206	30076.64	32.735	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\alpha 0$	αN	I'	f _{vd}	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLU 79	-0.98	-36001	2294	202.26		21163	3.7804	8377	14251			6.21	Si
SLU 79	1.22	-24904	1568	-1079.34		14639	3.7804	7507	12771			8.15	Si
SLU 75	-0.98	-36001	2294	202.26		21163	3.7804	8377	14251			6.21	Si
SLU 75	1.22	-24904	1568	-1079.34		14639	3.7804	7507	12771			8.15	Si
SLU 84	-0.98	-37839	2448	307.98		22243	3.7804	8521	14496			5.92	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 84	1.22	-26579	1664	-1097.15		15624	3.7804	7639	12995			7.81	Si
SLU 73	-0.98	-36001	2294	202.26		21163	3.7804	8377	14251			6.21	Si
SLU 73	1.22	-24904	1568	-1079.34		14639	3.7804	7507	12771			8.15	Si
SLU 81	-0.98	-37839	2448	307.98		22243	3.7804	8521	14496			5.92	Si
SLU 81	1.22	-26579	1664	-1097.15		15624	3.7804	7639	12995			7.81	Si
SLU 78	-0.98	-36001	2294	202.26		21163	3.7804	8377	14251			6.21	Si
SLU 78	1.22	-24904	1568	-1079.34		14639	3.7804	7507	12771			8.15	Si
SLU 83	-0.98	-37839	2448	307.98		22243	3.7804	8521	14496			5.92	Si
SLU 83	1.22	-26579	1664	-1097.15		15624	3.7804	7639	12995			7.81	Si
SLU 76	-0.98	-36001	2294	202.26		21163	3.7804	8377	14251			6.21	Si
SLU 76	1.22	-24904	1568	-1079.34		14639	3.7804	7507	12771			8.15	Si
SLU 82	-0.98	-37839	2448	307.98		22243	3.7804	8521	14496			5.92	Si
SLU 82	1.22	-26579	1664	-1097.15		15624	3.7804	7639	12995			7.81	Si
SLU 74	-0.98	-36001	2294	202.26		21163	3.7804	8377	14251			6.21	Si
SLU 74	1.22	-24904	1568	-1079.34		14639	3.7804	7507	12771			8.15	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 15	-0.98	-26557	7355	7907.36		15611	3.7804	11456	19488			2.65	Si
SLV 15	1.22	-18786	4701	-776.35		11043	3.7804	10542	17934			3.81	Si
SLV 10	-0.98	-21010	3752	840.11		12350	3.7804	10803	18378			4.9	Si
SLV 10	1.22	-14757	3278	-1037.87		8675	3.7804	10068	17128			5.22	Si
SLV 3	-0.98	-25933	-4533	-6954.17		15244	3.7804	11382	19363			4.27	Si
SLV 3	1.22	-16090	-3197	-641.72		9458	3.7804	10225	17394			5.44	Si
SLV 13	-0.98	-24098	7613	7046.26		14166	3.7804	11166	18996			2.5	Si
SLV 13	1.22	-17362	5320	-918.8		10206	3.7804	10375	17649			3.32	Si
SLV 14	-0.98	-24098	7613	7046.26		14166	3.7804	11166	18996			2.5	Si
SLV 14	1.22	-17362	5320	-918.8		10206	3.7804	10375	17649			3.32	Si
SLV 2	-0.98	-23473	-4275	-7815.27		13798	3.7804	11093	18871			4.41	Si
SLV 2	1.22	-14666	-2578	-784.17		8621	3.7804	10058	17110			6.64	Si
SLV 9	-0.98	-21010	3752	840.11		12350	3.7804	10803	18378			4.9	Si
SLV 9	1.22	-14757	3278	-1037.87		8675	3.7804	10068	17128			5.22	Si
SLV 4	-0.98	-25933	-4533	-6954.17		15244	3.7804	11382	19363			4.27	Si
SLV 4	1.22	-16090	-3197	-641.72		9458	3.7804	10225	17394			5.44	Si
SLV 1	-0.98	-23473	-4275	-7815.27		13798	3.7804	11093	18871			4.41	Si
SLV 1	1.22	-14666	-2578	-784.17		8621	3.7804	10058	17110			6.64	Si
SLV 16	-0.98	-26557	7355	7907.36		15611	3.7804	11456	19488			2.65	Si
SLV 16	1.22	-18786	4701	-776.35		11043	3.7804	10542	17934			3.81	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.345 Wa 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 6	143750	0.27	10273	-17477	246.52	3601.66	14.61	Si
SLV 5	143750	0.27	10273	-17477	246.52	3601.66	14.61	Si
SLV 9	143750	0.27	10746	-18281	246.52	3751.39	15.22	Si
SLV 10	143750	0.27	10746	-18281	246.52	3751.39	15.22	Si
SLV 2	143750	0.27	11035	-18772	246.52	3842.21	15.59	Si
SLV 1	143750	0.27	11035	-18772	246.52	3842.21	15.59	Si
SLV 4	143750	0.27	12160	-20685	246.52	4191.06	17	Si
SLV 3	143750	0.27	12160	-20685	246.52	4191.06	17	Si
SLV 13	143750	0.27	12610	-21451	246.52	4328.37	17.56	Si
SLV 14	143750	0.27	12610	-21451	246.52	4328.37	17.56	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 0.345 Wa = 0.08 Ta = 0.0261

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 2	-13617	-23473	-602	0.07	2035.3	0.919	1.11274	11.13714	No
SLV 1	-13617	-23473	-602	0.07	2035.3	0.919	1.11274	11.13714	No
SLV 15	-17565	-26557	605	0.073	2432.3	0.929	1.13929	11.13714	No
SLV 16	-17565	-26557	605	0.073	2432.3	0.929	1.13929	11.13714	No
SLV 13	-16407	-24098	168	0.094	2315.6	0.926	1.46769	11.13714	No
SLV 14	-16407	-24098	168	0.094	2315.6	0.926	1.46769	11.13714	No
SLV 3	-14775	-25933	-164	0.094	2151.4	0.922	1.4893	11.13714	No
SLV 4	-14775	-25933	-164	0.094	2151.4	0.922	1.4893	11.13714	No
SLV 6	-13242	-20823	-843	0.056	1997.7	0.918	0.88799	2.73586	No
SLV 5	-13242	-20823	-843	0.056	1997.7	0.918	0.88799	2.73586	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	32.447	SLU 64	Si
V_SLU	5.922	SLU 81	Si
PF_SLV	5.036	SLV 1	Si
V_SLV	2.495	SLV 13	Si
PFFP_SLV	14.61	SLV 5	Si
R_SLV	0.1	SLV 1	No

Maschio 12

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s,sx	a.s,dx
35.424	1.847	35.424	-0.169	L1	L2	2.016	0.45	2.65	2.65	2.65			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

Sismicad 12.19 - Licenza assegnata a Sidel ingegneria Srl - Via Isonzo, 13 - Villanova di Castenaso (BO)



fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 81	0.41	-15259	-1417.92	16823	12202.59	8.606	Si
SLU 81	0.81	-14395	-1736.91	15870	11680.86	6.725	Si
SLU 75	0.41	-14362	-1342.26	15834	11660.84	8.687	Si
SLU 75	0.81	-13492	-1624.58	14875	11114.68	6.842	Si
SLU 74	0.41	-14362	-1342.26	15834	11660.84	8.687	Si
SLU 74	0.81	-13492	-1624.58	14875	11114.68	6.842	Si
SLU 84	0.41	-15259	-1417.92	16823	12202.59	8.606	Si
SLU 84	0.81	-14395	-1736.91	15870	11680.86	6.725	Si
SLU 60	0.41	-14194	-1340.26	15649	11557.02	8.623	Si
SLU 60	0.81	-13341	-1620.55	14709	11017.83	6.799	Si
SLU 62	0.41	-14194	-1340.26	15649	11557.02	8.623	Si
SLU 62	0.81	-13341	-1620.55	14709	11017.83	6.799	Si
SLU 63	0.41	-14194	-1340.26	15649	11557.02	8.623	Si
SLU 63	0.81	-13341	-1620.55	14709	11017.83	6.799	Si
SLU 83	0.41	-15259	-1417.92	16823	12202.59	8.606	Si
SLU 83	0.81	-14395	-1736.91	15870	11680.86	6.725	Si
SLU 82	0.41	-15259	-1417.92	16823	12202.59	8.606	Si
SLU 82	0.81	-14395	-1736.91	15870	11680.86	6.725	Si
SLU 61	0.41	-14194	-1340.26	15649	11557.02	8.623	Si
SLU 61	0.81	-13341	-1620.55	14709	11017.83	6.799	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 8	0.41	-8223	-1791.94	9065	7672.15	4.281	Si
SLV 8	0.81	-7253	-1102.72	7997	6831.59	6.195	Si
SLV 13	0.41	-11998	-640.19	13227	10782.63	16.843	Si
SLV 13	0.81	-11237	-1257.2	12389	10176.89	8.095	Si
SLV 11	0.41	-9359	-1771.29	10318	8635.36	4.875	Si
SLV 11	0.81	-8272	-1209.15	9120	7714.69	6.38	Si
SLV 14	0.41	-11998	-640.19	13227	10782.63	16.843	Si
SLV 14	0.81	-11237	-1257.2	12389	10176.89	8.095	Si
SLV 4	0.41	-7605	-1219.97	8384	7138.45	5.851	Si
SLV 4	0.81	-7021	-937.56	7740	6627.52	7.069	Si
SLV 16	0.41	-11391	-1151.11	12559	10300.45	8.948	Si
SLV 16	0.81	-10417	-1292.34	11485	9512.12	7.36	Si
SLV 15	0.41	-11391	-1151.11	12559	10300.45	8.948	Si
SLV 15	0.81	-10417	-1292.34	11485	9512.12	7.36	Si
SLV 12	0.41	-9359	-1771.29	10318	8635.36	4.875	Si
SLV 12	0.81	-8272	-1209.15	9120	7714.69	6.38	Si
SLV 7	0.41	-8223	-1791.94	9065	7672.15	4.281	Si
SLV 7	0.81	-7253	-1102.72	7997	6831.59	6.195	Si
SLV 3	0.41	-7605	-1219.97	8384	7138.45	5.851	Si
SLV 3	0.81	-7021	-937.56	7740	6627.52	7.069	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 82	0.41	-15259	714	-1417.92		16823	2.0156	7799	7074			9.9	Si
SLU 82	0.81	-14395	715	-1736.91		15870	2.0156	7672	6958			9.74	Si
SLU 42	0.41	-12955	670	-1187.3		14282	2.0156	7460	6766			10.1	Si
SLU 42	0.81	-12288	670	-1480.02		13547	2.0156	7362	6677			9.96	Si
SLU 40	0.41	-12955	670	-1187.3		14282	2.0156	7460	6766			10.1	Si
SLU 40	0.81	-12288	670	-1480.02		13547	2.0156	7362	6677			9.96	Si
SLU 41	0.41	-12955	670	-1187.3		14282	2.0156	7460	6766			10.1	Si
SLU 41	0.81	-12288	670	-1480.02		13547	2.0156	7362	6677			9.96	Si
SLU 84	0.41	-15259	714	-1417.92		16823	2.0156	7799	7074			9.9	Si
SLU 84	0.81	-14395	715	-1736.91		15870	2.0156	7672	6958			9.74	Si
SLU 83	0.41	-15259	714	-1417.92		16823	2.0156	7799	7074			9.9	Si
SLU 83	0.81	-14395	715	-1736.91		15870	2.0156	7672	6958			9.74	Si
SLU 63	0.41	-14194	633	-1340.26		15649	2.0156	7642	6932			10.95	Si
SLU 63	0.81	-13341	634	-1620.55		14709	2.0156	7517	6818			10.76	Si
SLU 39	0.41	-12955	670	-1187.3		14282	2.0156	7460	6766			10.1	Si
SLU 39	0.81	-12288	670	-1480.02		13547	2.0156	7362	6677			9.96	Si
SLU 81	0.41	-15259	714	-1417.92		16823	2.0156	7799	7074			9.9	Si
SLU 81	0.81	-14395	715	-1736.91		15870	2.0156	7672	6958			9.74	Si
SLU 62	0.41	-14194	633	-1340.26		15649	2.0156	7642	6932			10.95	Si
SLU 62	0.81	-13341	634	-1620.55		14709	2.0156	7517	6818			10.76	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 5	0.41	-10244	3684	-88.88		11294	2.0156	10592	9607			2.61	Si
SLV 5	0.81	-9986	3694	-985.61		11009	2.0156	10535	9556			2.59	Si
SLV 9	0.41	-11380	3220	-68.22		12546	2.0156	10843	9835			3.05	Si
SLV 9	0.81	-11005	2965	-1092.04		12133	2.0156	10760	9760			3.29	Si
SLV 1	0.41	-8211	2042	-709.05		9053	2.0156	10144	9201			4.51	Si
SLV 1	0.81	-7841	2448	-902.43		8644	2.0156	10062	9127			3.73	Si
SLV 12	0.41	-9359	-3017	-1771.29		10318	2.0156	10397	9430			3.13	Si
SLV 12	0.81	-8272	-3027	-1209.15		9120	2.0156	10157	9213			3.04	Si
SLV 11	0.41	-9359	-3017	-1771.29		10318	2.0156	10397	9430			3.13	Si
SLV 11	0.81	-8272	-3027	-1209.15		9120	2.0156	10157	9213			3.04	Si
SLV 6	0.41	-10244	3684	-88.88		11294	2.0156	10592	9607			2.61	Si
SLV 6	0.81	-9986	3694	-985.61		11009	2.0156	10535	9556			2.59	Si
SLV 2	0.41	-8211	2042	-709.05		9053	2.0156	10144	9201			4.51	Si
SLV 2	0.81	-7841	2448	-902.43		8644	2.0156	10062	9127			3.73	Si
SLV 7	0.41	-8223	-2553	-1791.94		9065	2.0156	10146	9203			3.6	Si
SLV 7	0.81	-7253	-2298	-1102.72		7997	2.0156	9933	9009			3.92	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 8	0.41	-8223	-2553	-1791.94		9065	2.0156	10146	9203			3.6	Si
SLV 8	0.81	-7253	-2298	-1102.72		7997	2.0156	9933	9009			3.92	Si
SLV 10	0.41	-11380	3220	-68.22		12546	2.0156	10843	9835			3.05	Si
SLV 10	0.81	-11005	2965	-1092.04		12133	2.0156	10760	9760			3.29	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.345 Wa 0.08 denominatore $8 \gamma M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 3	143750	0.27	7762	-7041	129.55	1483.52	11.45	Si
SLV 4	143750	0.27	7762	-7041	129.55	1483.52	11.45	Si
SLV 7	143750	0.27	8108	-7354	129.55	1544.95	11.93	Si
SLV 8	143750	0.27	8108	-7354	129.55	1544.95	11.93	Si
SLV 2	143750	0.27	8661	-7855	129.55	1642.2	12.68	Si
SLV 1	143750	0.27	8661	-7855	129.55	1642.2	12.68	Si
SLV 11	143750	0.27	9303	-8438	129.55	1754.06	13.54	Si
SLV 12	143750	0.27	9303	-8438	129.55	1754.06	13.54	Si
SLV 6	143750	0.27	11103	-10070	129.55	2059.97	15.9	Si
SLV 5	143750	0.27	11103	-10070	129.55	2059.97	15.9	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 0.345 Wa = 0.08 Ta = 0.0261

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 13	-7757	-14216	-9	0.103	1135	0.921	1.6167	11.13714	No
SLV 14	-7757	-14216	-9	0.103	1135	0.921	1.6167	11.13714	No
SLV 15	-7274	-13073	-13	0.103	1086.5	0.919	1.62943	11.13714	No
SLV 16	-7274	-13073	-13	0.103	1086.5	0.919	1.62943	11.13714	No
SLV 1	-5385	-9394	12	0.108	898.2	0.907	1.72366	11.13714	No
SLV 2	-5385	-9394	12	0.108	898.2	0.907	1.72366	11.13714	No
SLV 3	-4902	-8251	9	0.11	850.4	0.904	1.76315	11.13714	No
SLV 4	-4902	-8251	9	0.11	850.4	0.904	1.76315	11.13714	No
SLV 10	-7490	-13862	3	0.104	1108.2	0.92	1.63745	2.73586	No
SLV 9	-7490	-13862	3	0.104	1108.2	0.92	1.63745	2.73586	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	6.725	SLU 81	Si
V_SLU	9.738	SLU 81	Si
PF_SLV	4.281	SLV 7	Si
V_SLV	2.587	SLV 5	Si
PFFP_SLV	11.451	SLV 3	Si
R_SLV	0.145	SLV 13	No

Maschio 13

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s,sx	a.s,dx
35.424	6.497	35.424	2.847	L1	L2	3.65	0.45	2.65	2.65	2.65			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	f _{v0}	μ	ϕ	f _{v,lim}	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 84	0.41	-30798	288.05	18751	43268.77	150.213	Si
SLU 84	0.81	-28753	208.67	17506	41197.29	197.427	Si
SLU 78	0.41	-28755	272.14	17507	41199.61	151.391	Si
SLU 78	0.81	-26763	200.02	16294	39072.25	195.342	Si
SLU 83	0.41	-30798	288.05	18751	43268.77	150.213	Si
SLU 83	0.81	-28753	208.67	17506	41197.29	197.427	Si
SLU 76	0.41	-28755	272.14	17507	41199.61	151.391	Si
SLU 76	0.81	-26763	200.02	16294	39072.25	195.342	Si
SLU 81	0.41	-30798	288.05	18751	43268.77	150.213	Si
SLU 81	0.81	-28753	208.67	17506	41197.29	197.427	Si
SLU 82	0.41	-30798	288.05	18751	43268.77	150.213	Si
SLU 82	0.81	-28753	208.67	17506	41197.29	197.427	Si
SLU 79	0.41	-28755	272.14	17507	41199.61	151.391	Si
SLU 79	0.81	-26763	200.02	16294	39072.25	195.342	Si
SLU 80	0.41	-28755	272.14	17507	41199.61	151.391	Si
SLU 80	0.81	-26763	200.02	16294	39072.25	195.342	Si
SLU 75	0.41	-28755	272.14	17507	41199.61	151.391	Si
SLU 75	0.81	-26763	200.02	16294	39072.25	195.342	Si
SLU 77	0.41	-28755	272.14	17507	41199.61	151.391	Si
SLU 77	0.81	-26763	200.02	16294	39072.25	195.342	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 9	0.41	-20064	2794.18	12216	32956.68	11.795	Si
SLV 9	0.81	-18547	234.09	11292	30720.61	131.234	Si
SLV 7	0.41	-18492	-2425.97	11259	30638.61	12.629	Si
SLV 7	0.81	-17106	43.89	10414	28557.19	650.703	Si
SLV 14	0.41	-22214	1098.08	13525	36053.9	32.834	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 14	0.81	-20489	134.86	12474	33574.52	248.951	Si
SLV 5	0.41	-18284	2707.83	11132	30328.26	11.2	Si
SLV 5	0.81	-16935	255.62	10310	28297.77	110.702	Si
SLV 8	0.41	-18492	-2425.97	11259	30638.61	12.629	Si
SLV 8	0.81	-17106	43.89	10414	28557.19	650.703	Si
SLV 10	0.41	-20064	2794.18	12216	32956.68	11.795	Si
SLV 10	0.81	-18547	234.09	11292	30720.61	131.234	Si
SLV 12	0.41	-20273	-2339.62	12343	33260.28	14.216	Si
SLV 12	0.81	-18718	22.36	11396	30975.01	1000	Si
SLV 13	0.41	-22214	1098.08	13525	36053.9	32.834	Si
SLV 13	0.81	-20489	134.86	12474	33574.52	248.951	Si
SLV 11	0.41	-20273	-2339.62	12343	33260.28	14.216	Si
SLV 11	0.81	-18718	22.36	11396	30975.01	1000	Si
SLV 6	0.41	-18284	2707.83	11132	30328.26	11.2	Si
SLV 6	0.81	-16935	255.62	10310	28297.77	110.702	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 84	0.41	-30798	-39	288.05		18751	3.65	8056	13231			339.83	Si
SLU 84	0.81	-28753	-39	208.67		17506	3.65	7890	12959			332.74	Si
SLU 83	0.41	-30798	-39	288.05		18751	3.65	8056	13231			339.83	Si
SLU 83	0.81	-28753	-39	208.67		17506	3.65	7890	12959			332.74	Si
SLU 81	0.41	-30798	-39	288.05		18751	3.65	8056	13231			339.83	Si
SLU 81	0.81	-28753	-39	208.67		17506	3.65	7890	12959			332.74	Si
SLU 41	0.41	-26468	-38	250.21		16115	3.65	7704	12654			334.32	Si
SLU 41	0.81	-24807	-38	178.67		15103	3.65	7569	12433			328.4	Si
SLU 42	0.41	-26468	-38	250.21		16115	3.65	7704	12654			334.32	Si
SLU 42	0.81	-24807	-38	178.67		15103	3.65	7569	12433			328.4	Si
SLU 82	0.41	-30798	-39	288.05		18751	3.65	8056	13231			339.83	Si
SLU 82	0.81	-28753	-39	208.67		17506	3.65	7890	12959			332.74	Si
SLU 40	0.41	-26468	-38	250.21		16115	3.65	7704	12654			334.32	Si
SLU 40	0.81	-24807	-38	178.67		15103	3.65	7569	12433			328.4	Si
SLU 38	0.41	-24425	-34	234.31		14871	3.65	7538	12382			363.43	Si
SLU 38	0.81	-22817	-34	170.02		13891	3.65	7408	12167			357.05	Si
SLU 37	0.41	-24425	-34	234.31		14871	3.65	7538	12382			363.43	Si
SLU 37	0.81	-22817	-34	170.02		13891	3.65	7408	12167			357.05	Si
SLU 39	0.41	-26468	-38	250.21		16115	3.65	7704	12654			334.32	Si
SLU 39	0.81	-24807	-38	178.67		15103	3.65	7569	12433			328.4	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 11	0.41	-20273	-6536	-2339.62		12343	3.65	10802	17742			2.71	Si
SLV 11	0.81	-18718	-6106	22.36		11396	3.65	10613	17431			2.85	Si
SLV 12	0.41	-20273	-6536	-2339.62		12343	3.65	10802	17742			2.71	Si
SLV 12	0.81	-18718	-6106	22.36		11396	3.65	10613	17431			2.85	Si
SLV 8	0.41	-18492	-6550	-2425.97		11259	3.65	10585	17386			2.65	Si
SLV 8	0.81	-17106	-5943	43.89		10414	3.65	10416	17109			2.88	Si
SLV 6	0.41	-18284	6495	2707.83		11132	3.65	10560	17344			2.67	Si
SLV 6	0.81	-16935	6065	255.62		10310	3.65	10395	17074			2.82	Si
SLV 9	0.41	-20064	6509	2794.18		12216	3.65	10776	17700			2.72	Si
SLV 9	0.81	-18547	5902	234.09		11292	3.65	10592	17397			2.95	Si
SLV 2	0.41	-16280	1912	810.27		9912	3.65	10316	16943			8.86	Si
SLV 2	0.81	-15113	2052	206.63		9201	3.65	10174	16710			8.14	Si
SLV 1	0.41	-16280	1912	810.27		9912	3.65	10316	16943			8.86	Si
SLV 1	0.81	-15113	2052	206.63		9201	3.65	10174	16710			8.14	Si
SLV 5	0.41	-18284	6495	2707.83		11132	3.65	10560	17344			2.67	Si
SLV 5	0.81	-16935	6065	255.62		10310	3.65	10395	17074			2.82	Si
SLV 10	0.41	-20064	6509	2794.18		12216	3.65	10776	17700			2.72	Si
SLV 10	0.81	-18547	5902	234.09		11292	3.65	10592	17397			2.95	Si
SLV 7	0.41	-18492	-6550	-2425.97		11259	3.65	10585	17386			2.65	Si
SLV 7	0.81	-17106	-5943	43.89		10414	3.65	10416	17109			2.88	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.345 Wa 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 1	143750	0.27	8984	-14756	234.59	3075.95	13.11	Si
SLV 2	143750	0.27	8984	-14756	234.59	3075.95	13.11	Si
SLV 4	143750	0.27	9019	-14814	234.59	3087.11	13.16	Si
SLV 3	143750	0.27	9019	-14814	234.59	3087.11	13.16	Si
SLV 5	143750	0.27	10088	-16569	234.59	3420.31	14.58	Si
SLV 6	143750	0.27	10088	-16569	234.59	3420.31	14.58	Si
SLV 8	143750	0.27	10206	-16763	234.59	3456.69	14.73	Si
SLV 7	143750	0.27	10206	-16763	234.59	3456.69	14.73	Si
SLV 10	143750	0.27	11070	-18182	234.59	3720.33	15.86	Si
SLV 9	143750	0.27	11070	-18182	234.59	3720.33	15.86	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 0.345 Wa = 0.08 Ta = 0.0261

Comb.	N top	N base	V orto	α_0	M*	e*	α_0^*	aLim	Verifica
SLV 14	-14397	-24317	165	0.094	2090.5	0.922	1.48204	11.13714	No
SLV 13	-14397	-24317	165	0.094	2090.5	0.922	1.48204	11.13714	No
SLV 15	-14435	-24435	161	0.094	2094.3	0.923	1.48451	11.13714	No
SLV 16	-14435	-24435	161	0.094	2094.3	0.923	1.48451	11.13714	No
SLV 3	-10980	-17351	-161	0.096	1748.5	0.912	1.53679	11.13714	No
SLV 4	-10980	-17351	-161	0.096	1748.5	0.912	1.53679	11.13714	No
SLV 2	-10943	-17233	-158	0.097	1744.7	0.912	1.54115	11.13714	No
SLV 1	-10943	-17233	-158	0.097	1744.7	0.912	1.54115	11.13714	No
SLV 9	-13144	-21701	56	0.101	1964.7	0.919	1.59969	2.73586	No
SLV 10	-13144	-21701	56	0.101	1964.7	0.919	1.59969	2.73586	No



Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	150.213	SLU 81	Si
V_SLU	328.404	SLU 39	Si
PF_SLV	11.2	SLV 5	Si
V_SLV	2.654	SLV 7	Si
PFFP_SLV	13.112	SLV 1	Si
R_SLV	0.133	SLV 13	No

Maschio 14

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
35.424	9.502	35.424	7.497	L1	L2	2.005	0.45	2.65	2.65	2.65			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ0	fv0	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 81	0.41	-15398	1404.69	17063	12204.52	8.688	Si
SLU 81	0.81	-14549	1700.69	16122	11700.12	6.88	Si
SLU 82	0.41	-15398	1404.69	17063	12204.52	8.688	Si
SLU 82	0.81	-14549	1700.69	16122	11700.12	6.88	Si
SLU 83	0.41	-15398	1404.69	17063	12204.52	8.688	Si
SLU 83	0.81	-14549	1700.69	16122	11700.12	6.88	Si
SLU 75	0.41	-14478	1332.54	16044	11657.23	8.748	Si
SLU 75	0.81	-13625	1592.48	15099	11128.83	6.988	Si
SLU 60	0.41	-14283	1336.22	15828	11538.37	8.635	Si
SLU 60	0.81	-13447	1596.11	14902	11016.3	6.902	Si
SLU 84	0.41	-15398	1404.69	17063	12204.52	8.688	Si
SLU 84	0.81	-14549	1700.69	16122	11700.12	6.88	Si
SLU 61	0.41	-14283	1336.22	15828	11538.37	8.635	Si
SLU 61	0.81	-13447	1596.11	14902	11016.3	6.902	Si
SLU 74	0.41	-14478	1332.54	16044	11657.23	8.748	Si
SLU 74	0.81	-13625	1592.48	15099	11128.83	6.988	Si
SLU 63	0.41	-14283	1336.22	15828	11538.37	8.635	Si
SLU 63	0.81	-13447	1596.11	14902	11016.3	6.902	Si
SLU 62	0.41	-14283	1336.22	15828	11538.37	8.635	Si
SLU 62	0.81	-13447	1596.11	14902	11016.3	6.902	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γM = 2

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLV 6	0.41	-8544	1648.97	9468	7902.97	4.793	Si
SLV 6	0.81	-7959	561.58	8820	7403.89	13.184	Si
SLV 3	0.41	-8164	847.69	9048	7579.91	8.942	Si
SLV 3	0.81	-7700	1224.67	8533	7181.42	5.864	Si
SLV 9	0.41	-9691	1574.53	10739	8862.58	5.629	Si
SLV 9	0.81	-8987	567.49	9959	8276.06	14.584	Si
SLV 2	0.41	-7722	1257.6	8558	7200.43	5.726	Si
SLV 2	0.81	-7266	915.44	8052	6805.26	7.434	Si
SLV 7	0.41	-10018	282.61	11102	9132.05	32.313	Si
SLV 7	0.81	-9406	1592.34	10423	8626.2	5.417	Si
SLV 8	0.41	-10018	282.61	11102	9132.05	32.313	Si
SLV 8	0.81	-9406	1592.34	10423	8626.2	5.417	Si
SLV 1	0.41	-7722	1257.6	8558	7200.43	5.726	Si
SLV 1	0.81	-7266	915.44	8052	6805.26	7.434	Si
SLV 5	0.41	-8544	1648.97	9468	7902.97	4.793	Si
SLV 5	0.81	-7959	561.58	8820	7403.89	13.184	Si
SLV 4	0.41	-8164	847.69	9048	7579.91	8.942	Si
SLV 4	0.81	-7700	1224.67	8533	7181.42	5.864	Si
SLV 10	0.41	-9691	1574.53	10739	8862.58	5.629	Si
SLV 10	0.81	-8987	567.49	9959	8276.06	14.584	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, γM = 3

Comb.	Quota	N	V par	M	σ0	σN	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 40	0.41	-13103	-633	1169.9		14520	2.0053	7492	6760			10.69	Si
SLU 40	0.81	-12447	-633	1443.17		13793	2.0053	7395	6673			10.54	Si
SLU 81	0.41	-15398	-676	1404.69		17063	2.0053	7831	7066			10.45	Si
SLU 81	0.81	-14549	-676	1700.69		16122	2.0053	7705	6953			10.28	Si
SLU 83	0.41	-15398	-676	1404.69		17063	2.0053	7831	7066			10.45	Si
SLU 83	0.81	-14549	-676	1700.69		16122	2.0053	7705	6953			10.28	Si
SLU 41	0.41	-13103	-633	1169.9		14520	2.0053	7492	6760			10.69	Si
SLU 41	0.81	-12447	-633	1443.17		13793	2.0053	7395	6673			10.54	Si
SLU 42	0.41	-13103	-633	1169.9		14520	2.0053	7492	6760			10.69	Si
SLU 42	0.81	-12447	-633	1443.17		13793	2.0053	7395	6673			10.54	Si
SLU 84	0.41	-15398	-676	1404.69		17063	2.0053	7831	7066			10.45	Si
SLU 84	0.81	-14549	-676	1700.69		16122	2.0053	7705	6953			10.28	Si
SLU 82	0.41	-15398	-676	1404.69		17063	2.0053	7831	7066			10.45	Si
SLU 82	0.81	-14549	-676	1700.69		16122	2.0053	7705	6953			10.28	Si
SLU 39	0.41	-13103	-633	1169.9		14520	2.0053	7492	6760			10.69	Si
SLU 39	0.81	-12447	-633	1443.17		13793	2.0053	7395	6673			10.54	Si
SLU 62	0.41	-14283	-605	1336.22		15828	2.0053	7666	6918			11.43	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 62	0.81	-13447	-605	1596.11		14902	2.0053	7542	6806			11.24	Si
SLU 63	0.41	-14283	-605	1336.22		15828	2.0053	7666	6918			11.43	Si
SLU 63	0.81	-13447	-605	1596.11		14902	2.0053	7542	6806			11.24	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 3	0.41	-8164	-2010	847.69		9048	2.0053	10143	9153			4.55	Si
SLV 3	0.81	-7700	-1957	1224.67		8533	2.0053	10040	9060			4.63	Si
SLV 7	0.41	-10018	-3618	282.61		11102	2.0053	10554	9524			2.63	Si
SLV 7	0.81	-9406	-3361	1592.34		10423	2.0053	10418	9401			2.8	Si
SLV 8	0.41	-10018	-3618	282.61		11102	2.0053	10554	9524			2.63	Si
SLV 8	0.81	-9406	-3361	1592.34		10423	2.0053	10418	9401			2.8	Si
SLV 5	0.41	-8544	2526	1648.97		9468	2.0053	10227	9229			3.65	Si
SLV 5	0.81	-7959	2253	561.58		8820	2.0053	10097	9112			4.04	Si
SLV 4	0.41	-8164	-2010	847.69		9048	2.0053	10143	9153			4.55	Si
SLV 4	0.81	-7700	-1957	1224.67		8533	2.0053	10040	9060			4.63	Si
SLV 6	0.41	-8544	2526	1648.97		9468	2.0053	10227	9229			3.65	Si
SLV 6	0.81	-7959	2253	561.58		8820	2.0053	10097	9112			4.04	Si
SLV 11	0.41	-11165	-3153	208.17		12373	2.0053	10808	9753			3.09	Si
SLV 11	0.81	-10434	-2880	1598.26		11562	2.0053	10646	9607			3.34	Si
SLV 12	0.41	-11165	-3153	208.17		12373	2.0053	10808	9753			3.09	Si
SLV 12	0.81	-10434	-2880	1598.26		11562	2.0053	10646	9607			3.34	Si
SLV 10	0.41	-9691	2991	1574.53		10739	2.0053	10481	9458			3.16	Si
SLV 10	0.81	-8987	2734	567.49		9959	2.0053	10325	9317			3.41	Si
SLV 9	0.41	-9691	2991	1574.53		10739	2.0053	10481	9458			3.16	Si
SLV 9	0.81	-8987	2734	567.49		9959	2.0053	10325	9317			3.41	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.345 Wa 0.08 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 1	143750	0.27	7776	-7017	128.88	1478.32	11.47	Si
SLV 2	143750	0.27	7776	-7017	128.88	1478.32	11.47	Si
SLV 5	143750	0.27	8341	-7526	128.88	1577.86	12.24	Si
SLV 6	143750	0.27	8341	-7526	128.88	1577.86	12.24	Si
SLV 4	143750	0.27	8511	-7680	128.88	1607.65	12.47	Si
SLV 3	143750	0.27	8511	-7680	128.88	1607.65	12.47	Si
SLV 9	143750	0.27	9560	-8626	128.88	1789.1	13.88	Si
SLV 10	143750	0.27	9560	-8626	128.88	1789.1	13.88	Si
SLV 8	143750	0.27	10790	-9737	128.88	1997.38	15.5	Si
SLV 7	143750	0.27	10790	-9737	128.88	1997.38	15.5	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 0.345 Wa = 0.08 Ta = 0.0261

Comb.	N top	N base	V orto	α_0	M*	e*	α_0^*	aLim	Verifica
SLV 16	-7572	-14256	74	0.096	1114.6	0.921	1.51632	11.13714	No
SLV 15	-7572	-14256	74	0.096	1114.6	0.921	1.51632	11.13714	No
SLV 2	-5206	-8152	-74	0.1	878.6	0.906	1.59768	11.13714	No
SLV 1	-5206	-8152	-74	0.1	878.6	0.906	1.59768	11.13714	No
SLV 13	-7387	-13223	-19	0.102	1096	0.92	1.61244	11.13714	No
SLV 14	-7387	-13223	-19	0.102	1096	0.92	1.61244	11.13714	No
SLV 4	-5392	-9186	19	0.107	897	0.907	1.7069	11.13714	No
SLV 3	-5392	-9186	19	0.107	897	0.907	1.7069	11.13714	No
SLV 12	-7026	-13687	164	0.087	1059.8	0.918	1.37659	2.73586	No
SLV 11	-7026	-13687	164	0.087	1059.8	0.918	1.37659	2.73586	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	6.88	SLU 81	Si
V_SLU	10.279	SLU 81	Si
PF_SLV	4.793	SLV 5	Si
V_SLV	2.632	SLV 7	Si
PFFP_SLV	11.47	SLV 1	Si
R_SLV	0.136	SLV 15	No

Maschio 15

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
25.794	-0.169	25.794	8.566	L2	L3	8.735	0.3	3.85	3.85	3.85			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 41	1.67	-43024	10723.75	16418	150034.04	13.991	Si
SLU 41	5.52	-23600	956.11	9006	91675.85	95.884	Si
SLU 21	1.67	-38695	9212.21	14766	138363.86	15.02	Si
SLU 21	5.52	-19725	805.13	7527	78189.71	97.114	Si
SLU 83	1.67	-49115	11228.37	18743	165154.76	14.709	Si
SLU 83	5.52	-24051	986.55	9178	93206.2	94.477	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 82	1.67	-49115	11228.37	18743	165154.76	14.709	Si
SLU 82	5.52	-24051	986.55	9178	93206.2	94.477	Si
SLU 42	1.67	-43024	10723.75	16418	150034.04	13.991	Si
SLU 42	5.52	-23600	956.11	9006	91675.85	95.884	Si
SLU 84	1.67	-49115	11228.37	18743	165154.76	14.709	Si
SLU 84	5.52	-24051	986.55	9178	93206.2	94.477	Si
SLU 40	1.67	-43024	10723.75	16418	150034.04	13.991	Si
SLU 40	5.52	-23600	956.11	9006	91675.85	95.884	Si
SLU 81	1.67	-49115	11228.37	18743	165154.76	14.709	Si
SLU 81	5.52	-24051	986.55	9178	93206.2	94.477	Si
SLU 20	1.67	-38695	9212.21	14766	138363.86	15.02	Si
SLU 20	5.52	-19725	805.13	7527	78189.71	97.114	Si
SLU 39	1.67	-43024	10723.75	16418	150034.04	13.991	Si
SLU 39	5.52	-23600	956.11	9006	91675.85	95.884	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 15	1.67	-19786	-32272.1	7550	81073.59	2.512	Si
SLV 15	5.52	-10369	-375.35	3957	43820.78	116.746	Si
SLV 16	1.67	-19786	-32272.1	7550	81073.59	2.512	Si
SLV 16	5.52	-10369	-375.35	3957	43820.78	116.746	Si
SLV 1	1.67	-38571	42276.01	14719	148165.08	3.505	Si
SLV 1	5.52	-9225	1222.09	3520	39128.39	32.018	Si
SLV 6	1.67	-35359	20054.92	13493	137377.15	6.85	Si
SLV 6	5.52	-9907	1085.75	3781	41931.71	38.62	Si
SLV 2	1.67	-38571	42276.01	14719	148165.08	3.505	Si
SLV 2	5.52	-9225	1222.09	3520	39128.39	32.018	Si
SLV 3	1.67	-36353	39723.87	13873	140746.3	3.543	Si
SLV 3	5.52	-9039	943.35	3449	38362.36	40.666	Si
SLV 13	1.67	-22003	-29719.96	8397	89494.64	3.011	Si
SLV 13	5.52	-10555	-96.61	4028	44580.05	461.454	Si
SLV 4	1.67	-36353	39723.87	13873	140746.3	3.543	Si
SLV 4	5.52	-9039	943.35	3449	38362.36	40.666	Si
SLV 14	1.67	-22003	-29719.96	8397	89494.64	3.011	Si
SLV 14	5.52	-10555	-96.61	4028	44580.05	461.454	Si
SLV 5	1.67	-35359	20054.92	13493	137377.15	6.85	Si
SLV 5	5.52	-9907	1085.75	3781	41931.71	38.62	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 60	1.67	-44786	-7	9716.84		17091	8.735	7834	20530			1000	Si
SLU 60	5.52	-20176	-2	835.57		7699	8.735	6582	17249			1000	Si
SLU 55	1.67	-40753	-6	7976.04		15552	8.735	7629	19992			1000	Si
SLU 55	5.52	-16038	-2	676.23		6120	8.735	6372	16697			1000	Si
SLU 59	1.67	-40753	-6	7976.04		15552	8.735	7629	19992			1000	Si
SLU 59	5.52	-16038	-2	676.23		6120	8.735	6372	16697			1000	Si
SLU 54	1.67	-40753	-6	7976.04		15552	8.735	7629	19992			1000	Si
SLU 54	5.52	-16038	-2	676.23		6120	8.735	6372	16697			1000	Si
SLU 53	1.67	-40753	-6	7976.04		15552	8.735	7629	19992			1000	Si
SLU 53	5.52	-16038	-2	676.23		6120	8.735	6372	16697			1000	Si
SLU 56	1.67	-40753	-6	7976.04		15552	8.735	7629	19992			1000	Si
SLU 56	5.52	-16038	-2	676.23		6120	8.735	6372	16697			1000	Si
SLU 58	1.67	-40753	-6	7976.04		15552	8.735	7629	19992			1000	Si
SLU 58	5.52	-16038	-2	676.23		6120	8.735	6372	16697			1000	Si
SLU 1	1.67	-25253	-1	3409.56		9637	8.735	6840	17925			1000	Si
SLU 1	5.52	-5931	0	274.01		2263	8.735	5857	15349			1000	Si
SLU 61	1.67	-44786	-7	9716.84		17091	8.735	7834	20530			1000	Si
SLU 61	5.52	-20176	-2	835.57		7699	8.735	6582	17249			1000	Si
SLU 57	1.67	-40753	-6	7976.04		15552	8.735	7629	19992			1000	Si
SLU 57	5.52	-16038	-2	676.23		6120	8.735	6372	16697			1000	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 10	1.67	-30389	-9215	-1543.87		11597	8.735	10653	27915			3.03	Si
SLV 10	5.52	-10307	-1973	690.14		3933	8.735	9120	23899			12.11	Si
SLV 11	1.67	-22997	8107	-10051.01		8776	8.735	10089	26437			3.26	Si
SLV 11	5.52	-9687	1495	-239.01		3696	8.735	9073	23775			15.9	Si
SLV 13	1.67	-22003	-4440	-29719.96		8397	8.735	10013	26238			5.91	Si
SLV 13	5.52	-10555	-1315	-96.61		4028	8.735	9139	23949			18.21	Si
SLV 7	1.67	-27967	9209	11547.78		10673	8.735	10468	27431			2.98	Si
SLV 7	5.52	-9287	1971	156.6		3544	8.735	9042	23695			12.02	Si
SLV 14	1.67	-22003	-4440	-29719.96		8397	8.735	10013	26238			5.91	Si
SLV 14	5.52	-10555	-1315	-96.61		4028	8.735	9139	23949			18.21	Si
SLV 6	1.67	-35359	-8113	20054.92		13493	8.735	11032	28909			3.56	Si
SLV 6	5.52	-9907	-1497	1085.75		3781	8.735	9089	23819			15.92	Si
SLV 8	1.67	-27967	9209	11547.78		10673	8.735	10468	27431			2.98	Si
SLV 8	5.52	-9287	1971	156.6		3544	8.735	9042	23695			12.02	Si
SLV 5	1.67	-35359	-8113	20054.92		13493	8.735	11032	28909			3.56	Si
SLV 5	5.52	-9907	-1497	1085.75		3781	8.735	9089	23819			15.92	Si
SLV 12	1.67	-22997	8107	-10051.01		8776	8.735	10089	26437			3.26	Si
SLV 12	5.52	-9687	1495	-239.01		3696	8.735	9073	23775			15.9	Si
SLV 9	1.67	-30389	-9215	-1543.87		11597	8.735	10653	27915			3.03	Si
SLV 9	5.52	-10307	-1973	690.14		3933	8.735	9120	23899			12.11	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.595 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 1	143750	0.48	5880	-15409	1469.57	2200.16	1.5	Si
SLV 2	143750	0.48	5880	-15409	1469.57	2200.16	1.5	Si



Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 5	143750	0.48	6196	-16238	1469.57	2312.13	1.57	Si
SLV 6	143750	0.48	6196	-16238	1469.57	2312.13	1.57	Si
SLV 3	143750	0.48	6396	-16762	1469.57	2382.62	1.62	Si
SLV 4	143750	0.48	6396	-16762	1469.57	2382.62	1.62	Si
SLV 10	143750	0.48	6983	-18300	1469.57	2588.11	1.76	Si
SLV 9	143750	0.48	6983	-18300	1469.57	2588.11	1.76	Si
SLV 7	143750	0.48	7917	-20745	1469.57	2910.17	1.98	Si
SLV 8	143750	0.48	7917	-20745	1469.57	2910.17	1.98	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 3.595 $W_a = 0.05$ $T_a = 0.0825$

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 13	-10555	-22003	254	0.044	2603.5	0.889	0.71981	10.57293	No
SLV 14	-10555	-22003	254	0.044	2603.5	0.889	0.71981	10.57293	No
SLV 3	-9039	-36353	-254	0.044	2464.5	0.889	0.72691	10.57293	No
SLV 4	-9039	-36353	-254	0.044	2464.5	0.889	0.72691	10.57293	No
SLV 15	-10369	-19786	125	0.051	2586.3	0.889	0.82925	10.57293	No
SLV 16	-10369	-19786	125	0.051	2586.3	0.889	0.82925	10.57293	No
SLV 2	-9225	-38571	-125	0.051	2481.4	0.889	0.84139	10.57293	No
SLV 1	-9225	-38571	-125	0.051	2481.4	0.889	0.84139	10.57293	No
SLV 10	-10307	-30389	272	0.043	2580.5	0.889	0.7057	4.97545	No
SLV 9	-10307	-30389	272	0.043	2580.5	0.889	0.7057	4.97545	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	13.991	SLU 39	Si
V_SLU	1000	SLU 1	Si
PF_SLV	2.512	SLV 15	Si
V_SLV	2.979	SLV 7	Si
PFFP_SLV	1.497	SLV 1	Si
R_SLV	0.068	SLV 13	No

Maschio 16

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
25.794	8.566	25.882	8.663	L2	L3	0.13	0.3	3.85	3.85	3.85			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 44	1.67	-540	0.08	13795	29.26	350.94	Si
SLU 44	3.67	-446	2.55	11391	25.02	9.806	Si
SLU 47	1.67	-540	0.08	13795	29.26	350.94	Si
SLU 47	3.67	-446	2.55	11391	25.02	9.806	Si
SLU 50	1.67	-540	0.08	13795	29.26	350.94	Si
SLU 50	3.67	-446	2.55	11391	25.02	9.806	Si
SLU 45	1.67	-540	0.08	13795	29.26	350.94	Si
SLU 45	3.67	-446	2.55	11391	25.02	9.806	Si
SLU 1	1.67	-438	0.1	11177	24.63	253.036	Si
SLU 1	3.67	-367	2.01	9366	21.17	10.551	Si
SLU 46	1.67	-540	0.08	13795	29.26	350.94	Si
SLU 46	3.67	-446	2.55	11391	25.02	9.806	Si
SLU 51	1.67	-540	0.08	13795	29.26	350.94	Si
SLU 51	3.67	-446	2.55	11391	25.02	9.806	Si
SLU 48	1.67	-540	0.08	13795	29.26	350.94	Si
SLU 48	3.67	-446	2.55	11391	25.02	9.806	Si
SLU 49	1.67	-540	0.08	13795	29.26	350.94	Si
SLU 49	3.67	-446	2.55	11391	25.02	9.806	Si
SLU 43	1.67	-540	0.08	13795	29.26	350.94	Si
SLU 43	3.67	-446	2.55	11391	25.02	9.806	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 8	1.67	-1940	79.96	49564	75.23	0.941	No, M>Mu
SLV 8	3.67	924	-76.12	0	0	0	No, Trazione
SLV 3	1.67	3878	-259.8	0	0	0	No, Trazione
SLV 3	3.67	-5211	263.39	133112	0	0	No, Rottura per schiacciamento
SLV 4	1.67	3878	-259.8	0	0	0	No, Trazione
SLV 4	3.67	-5211	263.39	133112	0	0	No, Rottura per schiacciamento
SLV 6	1.67	4081	-266.56	0	0	0	No, Trazione
SLV 6	3.67	-5236	267.98	133770	0	0	No, Rottura per schiacciamento
SLV 7	1.67	-1940	79.96	49564	75.23	0.941	No, M>Mu
SLV 7	3.67	924	-76.12	0	0	0	No, Trazione
SLV 10	1.67	900	-79.3	0	0	0	No, Trazione
SLV 10	3.67	-1826	80.2	46648	73.65	0.918	No, M>Mu
SLV 1	1.67	5684	-363.75	0	0	0	No, Trazione



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 1	3.67	-7059	366.62	180327	0	0	No, Rottura per schiacciamento
SLV 5	1.67	4081	-266.56	0	0	0	No, Trazione
SLV 5	3.67	-5236	267.98	133770	0	0	No, Rottura per schiacciamento
SLV 9	1.67	900	-79.3	0	0	0	No, Trazione
SLV 9	3.67	-1826	80.2	46648	73.65	0.918	No, M>Mu
SLV 2	1.67	5684	-363.75	0	0	0	No, Trazione
SLV 2	3.67	-7059	366.62	180327	0	0	No, Rottura per schiacciamento

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 66	1.67	-624	-2	0.21		15938	0.1305	7681	301			177.89	Si
SLU 66	3.67	-536	-8	2.72		13680	0.1305	7380	289			37.39	Si
SLU 72	1.67	-624	-2	0.21		15938	0.1305	7681	301			177.89	Si
SLU 72	3.67	-536	-8	2.72		13680	0.1305	7380	289			37.39	Si
SLU 65	1.67	-624	-2	0.21		15938	0.1305	7681	301			177.89	Si
SLU 65	3.67	-536	-8	2.72		13680	0.1305	7380	289			37.39	Si
SLU 67	1.67	-624	-2	0.21		15938	0.1305	7681	301			177.89	Si
SLU 67	3.67	-536	-8	2.72		13680	0.1305	7380	289			37.39	Si
SLU 71	1.67	-624	-2	0.21		15938	0.1305	7681	301			177.89	Si
SLU 71	3.67	-536	-8	2.72		13680	0.1305	7380	289			37.39	Si
SLU 70	1.67	-624	-2	0.21		15938	0.1305	7681	301			177.89	Si
SLU 70	3.67	-536	-8	2.72		13680	0.1305	7380	289			37.39	Si
SLU 68	1.67	-624	-2	0.21		15938	0.1305	7681	301			177.89	Si
SLU 68	3.67	-536	-8	2.72		13680	0.1305	7380	289			37.39	Si
SLU 64	1.67	-624	-2	0.21		15938	0.1305	7681	301			177.89	Si
SLU 64	3.67	-536	-8	2.72		13680	0.1305	7380	289			37.39	Si
SLU 69	1.67	-624	-2	0.21		15938	0.1305	7681	301			177.89	Si
SLU 69	3.67	-536	-8	2.72		13680	0.1305	7380	289			37.39	Si
SLU 43	1.67	-540	-2	0.08		13795	0.1305	7395	289			165.56	Si
SLU 43	3.67	-446	-7	2.55		11391	0.1305	7074	277			39.02	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 4	1.67	3878	-592	-259.8		0	0	8333	0			0	No, Vu<V
SLV 4	3.67	-5211	-538	263.39		394050	0.0441	16250	215			0.4	No, Vu<V
SLV 2	1.67	5684	-829	-363.75		0	0	8333	0			0	No, Vu<V
SLV 2	3.67	-7059	-750	366.62		589553	0.0399	16250	195			0.26	No, Vu<V
SLV 10	1.67	900	-182	-79.3		0	0	8333	0			0	No, Vu<V
SLV 10	3.67	-1826	-167	80.2		95151	0.064	16250	312			1.87	Si
SLV 7	1.67	-1940	180	79.96		89721	0.0721	16250	351			1.95	Si
SLV 7	3.67	924	155	-76.12		0	0	8333	0			0	No, Vu<V
SLV 8	1.67	-1940	180	79.96		89721	0.0721	16250	351			1.95	Si
SLV 8	3.67	924	155	-76.12		0	0	8333	0			0	No, Vu<V
SLV 9	1.67	900	-182	-79.3		0	0	8333	0			0	No, Vu<V
SLV 9	3.67	-1826	-167	80.2		95151	0.064	16250	312			1.87	Si
SLV 6	1.67	4081	-608	-266.56		0	0	8333	0			0	No, Vu<V
SLV 6	3.67	-5236	-550	267.98		413659	0.0422	16250	206			0.37	No, Vu<V
SLV 3	1.67	3878	-592	-259.8		0	0	8333	0			0	No, Vu<V
SLV 3	3.67	-5211	-538	263.39		394050	0.0441	16250	215			0.4	No, Vu<V
SLV 5	1.67	4081	-608	-266.56		0	0	8333	0			0	No, Vu<V
SLV 5	3.67	-5236	-550	267.98		413659	0.0422	16250	206			0.37	No, Vu<V
SLV 1	1.67	5684	-829	-363.75		0	0	8333	0			0	No, Vu<V
SLV 1	3.67	-7059	-750	366.62		589553	0.0399	16250	195			0.26	No, Vu<V

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.595 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 12	143750	0.48	0	4335	21.49	0	0	No, Trazione
SLV 1	143750	0.48	180327	-7059	21.49	0	0	No, Rottura per schiacciamento
SLV 5	143750	0.48	133770	-5236	21.49	0	0	No, Rottura per schiacciamento
SLV 4	143750	0.48	133112	-5211	21.49	0	0	No, Rottura per schiacciamento
SLV 2	143750	0.48	180327	-7059	21.49	0	0	No, Rottura per schiacciamento
SLV 7	143750	0.48	0	924	21.49	0	0	No, Trazione
SLV 8	143750	0.48	0	924	21.49	0	0	No, Trazione
SLV 6	143750	0.48	133770	-5236	21.49	0	0	No, Rottura per schiacciamento
SLV 11	143750	0.48	0	4335	21.49	0	0	No, Trazione
SLV 3	143750	0.48	133112	-5211	21.49	0	0	No, Rottura per schiacciamento

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 3.595 Wa = 0.05 Ta = 0.0825

Comb.	N top	N base	V orto	α_0	M*	e*	α_0^*	aLim	Verifica
SLV 5	-149	4081	136	0	0	0	0	4.97545	No, Trazione
SLV 8	-104	-1940	-136	0	34.1	0.891	0	4.97545	No
SLV 6	-149	4081	136	0	0	0	0	4.97545	No, Trazione
SLV 1	-158	5684	41	0	0	0	0	10.57293	No, Trazione
SLV 3	-144	3878	-41	0	0	0	0	10.57293	No, Trazione
SLV 7	-104	-1940	-136	0	34.1	0.891	0	4.97545	No
SLV 4	-144	3878	-41	0	0	0	0	10.57293	No, Trazione
SLV 10	-129	900	136	0	0	0	0	4.97545	No, Trazione
SLV 9	-129	900	136	0	0	0	0	4.97545	No, Trazione
SLV 2	-158	5684	41	0	0	0	0	10.57293	No, Trazione



Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	9.806	SLU 43	Si
V_SLU	37.388	SLU 64	Si
PF_SLV	0	SLV 16	No
V_SLV	0	SLV 1	No
PFFP_SLV	0	SLV 16	No
R_SLV	0	SLV 10	No

Maschio 17

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
26.552	9.405	26.639	9.502	L2	L3	0.13	0.3	3.85	3.85	3.85			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ0	fν0	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 39	1.67	-473	2.53	12072	26.26	10.387	Si
SLU 39	3.67	-507	-6.3	12940	27.8	4.414	Si
SLU 21	1.67	-446	2.11	11404	25.05	11.875	Si
SLU 21	3.67	-458	-5.48	11710	25.61	4.673	Si
SLU 40	1.67	-473	2.53	12072	26.26	10.387	Si
SLU 40	3.67	-507	-6.3	12940	27.8	4.414	Si
SLU 42	1.67	-473	2.53	12072	26.26	10.387	Si
SLU 42	3.67	-507	-6.3	12940	27.8	4.414	Si
SLU 84	1.67	-584	2.4	14912	31.11	12.963	Si
SLU 84	3.67	-581	-6.64	14835	30.99	4.667	Si
SLU 41	1.67	-473	2.53	12072	26.26	10.387	Si
SLU 41	3.67	-507	-6.3	12940	27.8	4.414	Si
SLU 81	1.67	-584	2.4	14912	31.11	12.963	Si
SLU 81	3.67	-581	-6.64	14835	30.99	4.667	Si
SLU 82	1.67	-584	2.4	14912	31.11	12.963	Si
SLU 82	3.67	-581	-6.64	14835	30.99	4.667	Si
SLU 83	1.67	-584	2.4	14912	31.11	12.963	Si
SLU 83	3.67	-581	-6.64	14835	30.99	4.667	Si
SLU 20	1.67	-446	2.11	11404	25.05	11.875	Si
SLU 20	3.67	-458	-5.48	11710	25.61	4.673	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γM = 2

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLV 7	1.67	1025	84.19	0	0	0	No, Trazione
SLV 7	3.67	-1722	-77.3	43991	71.9	0.93	No, M>Mu
SLV 3	1.67	-4883	-258.51	124734	0	0	No, Rottura per schiacciamento
SLV 3	3.67	4352	255.64	0	0	0	No, Trazione
SLV 10	1.67	-1860	-83.03	47507	74.15	0.893	No, M>Mu
SLV 10	3.67	1028	71.32	0	0	0	No, Trazione
SLV 6	1.67	-5089	-270.4	130012	0	0	No, Rottura per schiacciamento
SLV 6	3.67	4398	256.55	0	0	0	No, Trazione
SLV 5	1.67	-5089	-270.4	130012	0	0	No, Rottura per schiacciamento
SLV 5	3.67	4398	256.55	0	0	0	No, Trazione
SLV 8	1.67	1025	84.19	0	0	0	No, Trazione
SLV 8	3.67	-1722	-77.3	43991	71.9	0.93	No, M>Mu
SLV 2	1.67	-6717	-364.89	171596	0	0	No, Rottura per schiacciamento
SLV 2	3.67	6188	355.79	0	0	0	No, Trazione
SLV 9	1.67	-1860	-83.03	47507	74.15	0.893	No, M>Mu
SLV 9	3.67	1028	71.32	0	0	0	No, Trazione
SLV 4	1.67	-4883	-258.51	124734	0	0	No, Rottura per schiacciamento
SLV 4	3.67	4352	255.64	0	0	0	No, Trazione
SLV 1	1.67	-6717	-364.89	171596	0	0	No, Rottura per schiacciamento
SLV 1	3.67	6188	355.79	0	0	0	No, Trazione

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, γM = 3

Comb.	Quota	N	V par	M	σ0	σN	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 62	1.67	-558	7	1.98		14244	0.1305	7455	292			43.21	Si
SLU 62	3.67	-533	13	-5.82		13604	0.1305	7369	288			22.35	Si
SLU 42	1.67	-473	8	2.53		12072	0.1305	7165	280			34.19	Si
SLU 42	3.67	-507	14	-6.3		12940	0.1305	7281	285			20.35	Si
SLU 63	1.67	-558	7	1.98		14244	0.1305	7455	292			43.21	Si
SLU 63	3.67	-533	13	-5.82		13604	0.1305	7369	288			22.35	Si
SLU 83	1.67	-584	8	2.4		14912	0.1305	7544	295			36.73	Si
SLU 83	3.67	-581	15	-6.64		14835	0.1305	7533	295			20.06	Si
SLU 81	1.67	-584	8	2.4		14912	0.1305	7544	295			36.73	Si
SLU 81	3.67	-581	15	-6.64		14835	0.1305	7533	295			20.06	Si
SLU 82	1.67	-584	8	2.4		14912	0.1305	7544	295			36.73	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 82	3.67	-581	15	-6.64		14835	0.1305	7533	295			20.06	Si
SLU 39	1.67	-473	8	2.53		12072	0.1305	7165	280			34.19	Si
SLU 39	3.67	-507	14	-6.3		12940	0.1305	7281	285			20.35	Si
SLU 41	1.67	-473	8	2.53		12072	0.1305	7165	280			34.19	Si
SLU 41	3.67	-507	14	-6.3		12940	0.1305	7281	285			20.35	Si
SLU 84	1.67	-584	8	2.4		14912	0.1305	7544	295			36.73	Si
SLU 84	3.67	-581	15	-6.64		14835	0.1305	7533	295			20.06	Si
SLU 40	1.67	-473	8	2.53		12072	0.1305	7165	280			34.19	Si
SLU 40	3.67	-507	14	-6.3		12940	0.1305	7281	285			20.35	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 6	1.67	-5089	-616	-270.4		466915	0.0363	16250	177			0.29	No, Vu<V
SLV 6	3.67	4398	-530	256.55		0	0	8333	0			0	No, Vu<V
SLV 7	1.67	1025	198	84.19		0	0	8333	0			0	No, Vu<V
SLV 7	3.67	-1722	160	-77.3		94024	0.061	16250	298			1.86	Si
SLV 9	1.67	-1860	-193	-83.03		100328	0.0618	16250	301			1.56	Si
SLV 9	3.67	1028	-147	71.32		0	0	8333	0			0	No, Vu<V
SLV 2	1.67	-6717	-825	-364.89		683539	0.0328	16250	160			0.19	No, Vu<V
SLV 2	3.67	6188	-734	355.79		0	0	8333	0			0	No, Vu<V
SLV 10	1.67	-1860	-193	-83.03		100328	0.0618	16250	301			1.56	Si
SLV 10	3.67	1028	-147	71.32		0	0	8333	0			0	No, Vu<V
SLV 5	1.67	-5089	-616	-270.4		466915	0.0363	16250	177			0.29	No, Vu<V
SLV 5	3.67	4398	-530	256.55		0	0	8333	0			0	No, Vu<V
SLV 1	1.67	-6717	-825	-364.89		683539	0.0328	16250	160			0.19	No, Vu<V
SLV 1	3.67	6188	-734	355.79		0	0	8333	0			0	No, Vu<V
SLV 8	1.67	1025	198	84.19		0	0	8333	0			0	No, Vu<V
SLV 8	3.67	-1722	160	-77.3		94024	0.061	16250	298			1.86	Si
SLV 4	1.67	-4883	-580	-258.51		441199	0.0369	16250	180			0.31	No, Vu<V
SLV 4	3.67	4352	-527	255.64		0	0	8333	0			0	No, Vu<V
SLV 3	1.67	-4883	-580	-258.51		441199	0.0369	16250	180			0.31	No, Vu<V
SLV 3	3.67	4352	-527	255.64		0	0	8333	0			0	No, Vu<V

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.595 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 11	143750	0.48	130085	-5092	21.49	0	0	No, Rottura per schiacciamento
SLV 12	143750	0.48	130085	-5092	21.49	0	0	No, Rottura per schiacciamento
SLV 9	143750	0.48	0	1028	21.49	0	0	No, Trazione
SLV 5	143750	0.48	0	4398	21.49	0	0	No, Trazione
SLV 1	143750	0.48	0	6188	21.49	0	0	No, Trazione
SLV 10	143750	0.48	0	1028	21.49	0	0	No, Trazione
SLV 4	143750	0.48	0	4352	21.49	0	0	No, Trazione
SLV 3	143750	0.48	0	4352	21.49	0	0	No, Trazione
SLV 2	143750	0.48	0	6188	21.49	0	0	No, Trazione
SLV 6	143750	0.48	0	4398	21.49	0	0	No, Trazione

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.595 Wa = 0.05 Ta = 0.0825

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 2	-52	-6717	130	0	30	0.909	0	10.57293	No
SLV 9	-64	-1860	-39	0	30.8	0.902	0	4.97545	No
SLV 1	-52	-6717	130	0	30	0.909	0	10.57293	No
SLV 4	-56	-4883	130	0	30.2	0.906	0	10.57293	No
SLV 5	-57	-5089	38	0	30.3	0.906	0	4.97545	No
SLV 6	-57	-5089	38	0	30.3	0.906	0	4.97545	No
SLV 7	-69	1025	39	0	0	0	0	4.97545	No, Trazione
SLV 8	-69	1025	39	0	0	0	0	4.97545	No, Trazione
SLV 10	-64	-1860	-39	0	30.8	0.902	0	4.97545	No
SLV 3	-56	-4883	130	0	30.2	0.906	0	10.57293	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	4.414	SLU 39	Si
V_SLU	20.063	SLU 81	Si
PF_SLV	0	SLV 16	No
V_SLV	0	SLV 1	No
PFFP_SLV	0	SLV 10	No
R_SLV	0	SLV 16	No

Maschio 18

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
25.944	4.507	29.728	4.507	L2	L3	3.784	0.18	3.85	3.85	3.85			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	t0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2



Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 18	1.67	-8302	611.79	12189	13356.83	21.832	Si
SLU 18	3.71	-5761	4388.7	8459	9767.96	2.226	Si
SLU 20	1.67	-8302	611.79	12189	13356.83	21.832	Si
SLU 20	3.71	-5761	4388.7	8459	9767.96	2.226	Si
SLU 82	1.67	-10706	646.8	15719	16347	25.274	Si
SLU 82	3.71	-7322	5399.17	10751	12025.01	2.227	Si
SLU 39	1.67	-9105	616.11	13368	14398.6	23.37	Si
SLU 39	3.71	-6441	5134.24	9456	10770.77	2.098	Si
SLU 21	1.67	-8302	611.79	12189	13356.83	21.832	Si
SLU 21	3.71	-5761	4388.7	8459	9767.96	2.226	Si
SLU 19	1.67	-8302	611.79	12189	13356.83	21.832	Si
SLU 19	3.71	-5761	4388.7	8459	9767.96	2.226	Si
SLU 41	1.67	-9105	616.11	13368	14398.6	23.37	Si
SLU 41	3.71	-6441	5134.24	9456	10770.77	2.098	Si
SLU 42	1.67	-9105	616.11	13368	14398.6	23.37	Si
SLU 42	3.71	-6441	5134.24	9456	10770.77	2.098	Si
SLU 40	1.67	-9105	616.11	13368	14398.6	23.37	Si
SLU 40	3.71	-6441	5134.24	9456	10770.77	2.098	Si
SLU 81	1.67	-10706	646.8	15719	16347	25.274	Si
SLU 81	3.71	-7322	5399.17	10751	12025.01	2.227	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 10	1.67	-5751	1589.54	8444	10128.64	6.372	Si
SLV 10	3.71	-3196	2915.35	4692	5813.61	1.994	Si
SLV 16	1.67	-5660	3608.72	8310	9979.7	2.765	Si
SLV 16	3.71	-2836	3582.98	4164	5182.91	1.447	Si
SLV 9	1.67	-5751	1589.54	8444	10128.64	6.372	Si
SLV 9	3.71	-3196	2915.35	4692	5813.61	1.994	Si
SLV 11	1.67	-7170	928.32	10527	12396.32	13.353	Si
SLV 11	3.71	-4440	2722.24	6519	7952.47	2.921	Si
SLV 13	1.67	-5234	3807.09	7685	9279.78	2.438	Si
SLV 13	3.71	-2463	3640.92	3616	4521.42	1.242	Si
SLV 14	1.67	-5234	3807.09	7685	9279.78	2.438	Si
SLV 14	3.71	-2463	3640.92	3616	4521.42	1.242	Si
SLV 15	1.67	-5660	3608.72	8310	9979.7	2.765	Si
SLV 15	3.71	-2836	3582.98	4164	5182.91	1.447	Si
SLV 12	1.67	-7170	928.32	10527	12396.32	13.353	Si
SLV 12	3.71	-4440	2722.24	6519	7952.47	2.921	Si
SLV 6	1.67	-6620	-509.58	9719	11527.91	22.622	Si
SLV 6	3.71	-4197	2235.5	6162	7540.17	3.373	Si
SLV 5	1.67	-6620	-509.58	9719	11527.91	22.622	Si
SLV 5	3.71	-4197	2235.5	6162	7540.17	3.373	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 83	1.67	-10706	-2351	646.8		15719	3.7839	7651	5211			2.22	Si
SLU 83	3.71	-7322	-2351	5399.17		11744	3.4637	7121	4440			1.89	Si
SLU 41	1.67	-9105	-2231	616.11		13368	3.7839	7338	4998			2.24	Si
SLU 41	3.71	-6441	-2231	5134.24		10895	3.2843	7008	4143			1.86	Si
SLU 39	1.67	-9105	-2231	616.11		13368	3.7839	7338	4998			2.24	Si
SLU 39	3.71	-6441	-2231	5134.24		10895	3.2843	7008	4143			1.86	Si
SLU 37	1.67	-8491	-1915	464.74		12466	3.7839	7218	4916			2.57	Si
SLU 37	3.71	-5827	-1915	4338.17		9404	3.4423	6809	4219			2.2	Si
SLU 82	1.67	-10706	-2351	646.8		15719	3.7839	7651	5211			2.22	Si
SLU 82	3.71	-7322	-2351	5399.17		11744	3.4637	7121	4440			1.89	Si
SLU 84	1.67	-10706	-2351	646.8		15719	3.7839	7651	5211			2.22	Si
SLU 84	3.71	-7322	-2351	5399.17		11744	3.4637	7121	4440			1.89	Si
SLU 38	1.67	-8491	-1915	464.74		12466	3.7839	7218	4916			2.57	Si
SLU 38	3.71	-5827	-1915	4338.17		9404	3.4423	6809	4219			2.2	Si
SLU 81	1.67	-10706	-2351	646.8		15719	3.7839	7651	5211			2.22	Si
SLU 81	3.71	-7322	-2351	5399.17		11744	3.4637	7121	4440			1.89	Si
SLU 40	1.67	-9105	-2231	616.11		13368	3.7839	7338	4998			2.24	Si
SLU 40	3.71	-6441	-2231	5134.24		10895	3.2843	7008	4143			1.86	Si
SLU 42	1.67	-9105	-2231	616.11		13368	3.7839	7338	4998			2.24	Si
SLU 42	3.71	-6441	-2231	5134.24		10895	3.2843	7008	4143			1.86	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 5	1.67	-6620	-1721	-509.58		9719	3.7839	10277	7000			4.07	Si
SLV 5	3.71	-4197	-1307	2235.5		6162	3.7839	9566	6515			4.99	Si
SLV 8	1.67	-8039	-2005	-1170.8		11802	3.7839	10694	7284			3.63	Si
SLV 8	3.71	-5442	-1655	2042.4		7990	3.7839	9931	6764			4.09	Si
SLV 7	1.67	-8039	-2005	-1170.8		11802	3.7839	10694	7284			3.63	Si
SLV 7	3.71	-5442	-1655	2042.4		7990	3.7839	9931	6764			4.09	Si
SLV 14	1.67	-5234	1361	3807.09		8323	3.4937	9998	6287			4.62	Si
SLV 14	3.71	-2463	97	3640.92		11029	1.2406	10539	2353			24.23	Si
SLV 1	1.67	-8130	-3534	-3189.98		11936	3.7839	10721	7302			2.07	Si
SLV 1	3.71	-5801	-2250	1374.76		8517	3.7839	10037	6836			3.04	Si
SLV 13	1.67	-5234	1361	3807.09		8323	3.4937	9998	6287			4.62	Si
SLV 13	3.71	-2463	97	3640.92		11029	1.2406	10539	2353			24.23	Si
SLV 2	1.67	-8130	-3534	-3189.98		11936	3.7839	10721	7302			2.07	Si
SLV 2	3.71	-5801	-2250	1374.76		8517	3.7839	10037	6836			3.04	Si
SLV 4	1.67	-8556	-3619	-3388.34		12561	3.7839	10846	7387			2.04	Si
SLV 4	3.71	-6175	-2355	1316.83		9066	3.7839	10146	6911			2.93	Si
SLV 6	1.67	-6620	-1721	-509.58		9719	3.7839	10277	7000			4.07	Si
SLV 6	3.71	-4197	-1307	2235.5		6162	3.7839	9566	6515			4.99	Si
SLV 3	1.67	-8556	-3619	-3388.34		12561	3.7839	10846	7387			2.04	Si



Comb.	Quota	N	V par	M	σ_0	σN	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 3	3.71	-6175	-2355	1316.83		9066	3.7839	10146	6911			2.93	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.595 Wa 0.03 denominatore 8 $\gamma M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 5	143750	0.48	0	-4196	392.79	0	0	No, $e > t/2$
SLV 6	143750	0.48	0	-4196	392.79	0	0	No, $e > t/2$
SLV 14	143750	0.48	0	-2410	392.79	0	0	No, $e > t/2$
SLV 13	143750	0.48	0	-2410	392.79	0	0	No, $e > t/2$
SLV 16	143750	0.48	0	-2810	392.79	0	0	No, $e > t/2$
SLV 10	143750	0.48	0	-3156	392.79	0	0	No, $e > t/2$
SLV 9	143750	0.48	0	-3156	392.79	0	0	No, $e > t/2$
SLV 15	143750	0.48	0	-2810	392.79	0	0	No, $e > t/2$
SLV 12	143750	0.48	6593	-4490	392.79	382.32	0.97	No, $M > M_u$
SLV 11	143750	0.48	6593	-4490	392.79	382.32	0.97	No, $M > M_u$

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.595 Wa = 0.03 Ta = 0.1375

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 12	-12	-7170	-270	0	481.2	0.997	0	5.79734	No
SLV 11	-12	-7170	-270	0	481.2	0.997	0	5.79734	No
SLV 5	-186	-6620	270	0	483.7	0.967	0	5.79734	No
SLV 2	-956	-8130	134	0	524.8	0.907	0	2.39674	No
SLV 1	-956	-8130	134	0	524.8	0.907	0	2.39674	No
SLV 10	362	-5751	235	0	0	0	0	5.79734	No, Trazione
SLV 7	-560	-8039	-235	0	499.5	0.928	0	5.79734	No
SLV 9	362	-5751	235	0	0	0	0	5.79734	No, Trazione
SLV 8	-560	-8039	-235	0	499.5	0.928	0	5.79734	No
SLV 6	-186	-6620	270	0	483.7	0.967	0	5.79734	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	2.098	SLU 39	Si
V_SLU	1.857	SLU 39	Si
PF_SLV	1.242	SLV 13	Si
V_SLV	2.041	SLV 3	Si
PFFP_SLV	0	SLV 5	No
R_SLV	0	SLV 16	No

Maschio 19

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
27.92	-0.169	25.794	-0.169	L2	L3	2.125	0.3	3.85	3.85	3.85			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 46	2.67	-4679	-252.08	7337	4524.19	17.947	Si
SLU 46	4.57	-1769	-208.02	2774	1816.03	8.73	Si
SLU 43	2.67	-4679	-252.08	7337	4524.19	17.947	Si
SLU 43	4.57	-1769	-208.02	2774	1816.03	8.73	Si
SLU 47	2.67	-4679	-252.08	7337	4524.19	17.947	Si
SLU 47	4.57	-1769	-208.02	2774	1816.03	8.73	Si
SLU 48	2.67	-4679	-252.08	7337	4524.19	17.947	Si
SLU 48	4.57	-1769	-208.02	2774	1816.03	8.73	Si
SLU 51	2.67	-4679	-252.08	7337	4524.19	17.947	Si
SLU 51	4.57	-1769	-208.02	2774	1816.03	8.73	Si
SLU 44	2.67	-4679	-252.08	7337	4524.19	17.947	Si
SLU 44	4.57	-1769	-208.02	2774	1816.03	8.73	Si
SLU 45	2.67	-4679	-252.08	7337	4524.19	17.947	Si
SLU 45	4.57	-1769	-208.02	2774	1816.03	8.73	Si
SLU 1	2.67	-3677	-174.56	5766	3630.84	20.8	Si
SLU 1	4.57	-1403	-146.64	2201	1451.02	9.895	Si
SLU 49	2.67	-4679	-252.08	7337	4524.19	17.947	Si
SLU 49	4.57	-1769	-208.02	2774	1816.03	8.73	Si
SLU 50	2.67	-4679	-252.08	7337	4524.19	17.947	Si
SLU 50	4.57	-1769	-208.02	2774	1816.03	8.73	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 2	2.67	-3800	231.69	5959	3841.23	16.579	Si
SLV 2	4.57	-1800	-448.77	2824	1869.11	4.165	Si
SLV 3	2.67	-3212	233.91	5037	3272.73	13.991	Si
SLV 3	4.57	-1603	-395.98	2515	1668.94	4.215	Si
SLV 16	2.67	-4093	-452.19	6420	4121.55	9.115	Si
SLV 16	4.57	-1297	260.71	2035	1355.78	5.2	Si
SLV 13	2.67	-4681	-454.42	7341	4675.93	10.29	Si
SLV 13	4.57	-1494	207.92	2344	1557.59	7.491	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 6	2.67	-4794	-11.04	7519	4781.36	433.015	Si
SLV 6	4.57	-1923	-280.5	3016	1993.23	7.106	Si
SLV 15	2.67	-4093	-452.19	6420	4121.55	9.115	Si
SLV 15	4.57	-1297	260.71	2035	1355.78	5.2	Si
SLV 5	2.67	-4794	-11.04	7519	4781.36	433.015	Si
SLV 5	4.57	-1923	-280.5	3016	1993.23	7.106	Si
SLV 1	2.67	-3800	231.69	5959	3841.23	16.579	Si
SLV 1	4.57	-1800	-448.77	2824	1869.11	4.165	Si
SLV 4	2.67	-3212	233.91	5037	3272.73	13.991	Si
SLV 4	4.57	-1603	-395.98	2515	1668.94	4.215	Si
SLV 14	2.67	-4681	-454.42	7341	4675.93	10.29	Si
SLV 14	4.57	-1494	207.92	2344	1557.59	7.491	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 39	2.67	-4899	-304	115.53		7683	2.1255	6580	4196			13.79	Si
SLU 39	4.57	-2062	-304	94.67		3234	2.1255	5987	3817			12.57	Si
SLU 41	2.67	-4899	-304	115.53		7683	2.1255	6580	4196			13.79	Si
SLU 41	4.57	-2062	-304	94.67		3234	2.1255	5987	3817			12.57	Si
SLU 40	2.67	-4899	-304	115.53		7683	2.1255	6580	4196			13.79	Si
SLU 40	4.57	-2062	-304	94.67		3234	2.1255	5987	3817			12.57	Si
SLU 83	2.67	-5901	-299	38		9254	2.1255	6789	4329			14.49	Si
SLU 83	4.57	-2428	-298	33.29		3808	2.1255	6063	3866			12.96	Si
SLU 19	2.67	-4604	-259	42.15		7220	2.1255	6518	4156			16.04	Si
SLU 19	4.57	-1901	-259	43.96		2982	2.1255	5953	3796			14.66	Si
SLU 81	2.67	-5901	-299	38		9254	2.1255	6789	4329			14.49	Si
SLU 81	4.57	-2428	-298	33.29		3808	2.1255	6063	3866			12.96	Si
SLU 42	2.67	-4899	-304	115.53		7683	2.1255	6580	4196			13.79	Si
SLU 42	4.57	-2062	-304	94.67		3234	2.1255	5987	3817			12.57	Si
SLU 82	2.67	-5901	-299	38		9254	2.1255	6789	4329			14.49	Si
SLU 82	4.57	-2428	-298	33.29		3808	2.1255	6063	3866			12.96	Si
SLU 18	2.67	-4604	-259	42.15		7220	2.1255	6518	4156			16.04	Si
SLU 18	4.57	-1901	-259	43.96		2982	2.1255	5953	3796			14.66	Si
SLU 84	2.67	-5901	-299	38		9254	2.1255	6789	4329			14.49	Si
SLU 84	4.57	-2428	-298	33.29		3808	2.1255	6063	3866			12.96	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 2	2.67	-3800	865	231.69		5959	2.1255	9525	6074			7.02	Si
SLV 2	4.57	-1800	399	-448.77		2824	2.1255	8898	5674			14.22	Si
SLV 3	2.67	-3212	999	233.91		5037	2.1255	9341	5956			5.96	Si
SLV 3	4.57	-1603	729	-395.98		2515	2.1255	8836	5634			7.73	Si
SLV 15	2.67	-4093	-1048	-452.19		6420	2.1255	9617	6132			5.85	Si
SLV 15	4.57	-1297	-581	260.71		2035	2.1255	8740	5573			9.59	Si
SLV 13	2.67	-4681	-1181	-454.42		7341	2.1255	9802	6250			5.29	Si
SLV 13	4.57	-1494	-911	207.92		2344	2.1255	8802	5613			6.16	Si
SLV 4	2.67	-3212	999	233.91		5037	2.1255	9341	5956			5.96	Si
SLV 4	4.57	-1603	729	-395.98		2515	2.1255	8836	5634			7.73	Si
SLV 10	2.67	-5059	-621	-216.87		7933	2.1255	9920	6325			10.18	Si
SLV 10	4.57	-1831	-837	-83.5		2872	2.1255	8908	5680			6.78	Si
SLV 9	2.67	-5059	-621	-216.87		7933	2.1255	9920	6325			10.18	Si
SLV 9	4.57	-1831	-837	-83.5		2872	2.1255	8908	5680			6.78	Si
SLV 1	2.67	-3800	865	231.69		5959	2.1255	9525	6074			7.02	Si
SLV 1	4.57	-1800	399	-448.77		2824	2.1255	8898	5674			14.22	Si
SLV 14	2.67	-4681	-1181	-454.42		7341	2.1255	9802	6250			5.29	Si
SLV 14	4.57	-1494	-911	207.92		2344	2.1255	8802	5613			6.16	Si
SLV 16	2.67	-4093	-1048	-452.19		6420	2.1255	9617	6132			5.85	Si
SLV 16	4.57	-1297	-581	260.71		2035	2.1255	8740	5573			9.59	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.595 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 12	143750	0.48	3896	-2484	349.98	360.76	1.03	Si
SLV 11	143750	0.48	3896	-2484	349.98	360.76	1.03	Si
SLV 8	143750	0.48	3927	-2504	349.98	363.5	1.04	Si
SLV 7	143750	0.48	3927	-2504	349.98	363.5	1.04	Si
SLV 15	143750	0.48	4440	-2831	349.98	409.26	1.17	Si
SLV 16	143750	0.48	4440	-2831	349.98	409.26	1.17	Si
SLV 3	143750	0.48	4542	-2896	349.98	418.3	1.2	Si
SLV 4	143750	0.48	4542	-2896	349.98	418.3	1.2	Si
SLV 13	143750	0.48	4937	-3148	349.98	453.16	1.29	Si
SLV 14	143750	0.48	4937	-3148	349.98	453.16	1.29	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 3.595 Wa = 0.05 Ta = 0.0825

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 3	-46	-4455	171	0.001	450.6	0.99	0.02201	10.57293	No
SLV 4	-46	-4455	171	0.001	450.6	0.99	0.02201	10.57293	No
SLV 13	-224	-5279	-171	0.004	454.3	0.96	0.06387	10.57293	No
SLV 14	-224	-5279	-171	0.004	454.3	0.96	0.06387	10.57293	No
SLV 1	-96	-5150	164	0.005	451.2	0.98	0.07847	10.57293	No
SLV 2	-96	-5150	164	0.005	451.2	0.98	0.07847	10.57293	No
SLV 16	-173	-4585	-164	0.006	452.8	0.967	0.09561	10.57293	No
SLV 15	-173	-4585	-164	0.006	452.8	0.967	0.09561	10.57293	No
SLV 8	-32	-3691	62	0.05	450.5	0.993	0.73033	4.97545	No
SLV 7	-32	-3691	62	0.05	450.5	0.993	0.73033	4.97545	No



Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	8.73	SLU 43	Si
V_SLU	12.565	SLU 39	Si
PF_SLV	4.165	SLV 1	Si
V_SLV	5.29	SLV 13	Si
PFFP_SLV	1.031	SLV 11	Si
R_SLV	0.002	SLV 3	No

Maschio 20

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
29.469	-0.169	28.92	-0.169	L2	L3	0.549	0.3	3.85	3.85	3.85			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	$\tau 0$	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma M = 3$

Comb.	Quota	N	M	$\sigma 0$	Mu	c.s.	Verifica
SLU 47	3.67	-1310	-40.57	7949	324.88	8.009	Si
SLU 47	4.57	-716	76.3	4341	186.15	2.44	Si
SLU 1	3.67	-1026	-29.65	6223	260.34	8.781	Si
SLU 1	4.57	-554	58.23	3362	145.99	2.507	Si
SLU 43	3.67	-1310	-40.57	7949	324.88	8.009	Si
SLU 43	4.57	-716	76.3	4341	186.15	2.44	Si
SLU 50	3.67	-1310	-40.57	7949	324.88	8.009	Si
SLU 50	4.57	-716	76.3	4341	186.15	2.44	Si
SLU 46	3.67	-1310	-40.57	7949	324.88	8.009	Si
SLU 46	4.57	-716	76.3	4341	186.15	2.44	Si
SLU 49	3.67	-1310	-40.57	7949	324.88	8.009	Si
SLU 49	4.57	-716	76.3	4341	186.15	2.44	Si
SLU 44	3.67	-1310	-40.57	7949	324.88	8.009	Si
SLU 44	4.57	-716	76.3	4341	186.15	2.44	Si
SLU 48	3.67	-1310	-40.57	7949	324.88	8.009	Si
SLU 48	4.57	-716	76.3	4341	186.15	2.44	Si
SLU 51	3.67	-1310	-40.57	7949	324.88	8.009	Si
SLU 51	4.57	-716	76.3	4341	186.15	2.44	Si
SLU 45	3.67	-1310	-40.57	7949	324.88	8.009	Si
SLU 45	4.57	-716	76.3	4341	186.15	2.44	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma M = 2$

Comb.	Quota	N	M	$\sigma 0$	Mu	c.s.	Verifica
SLV 15	3.67	-1191	-97	7225	307.89	3.174	Si
SLV 15	4.57	-843	143.11	5115	221.95	1.551	Si
SLV 14	3.67	-1187	-75.18	7201	306.91	4.083	Si
SLV 14	4.57	-799	118.54	4846	210.79	1.778	Si
SLV 13	3.67	-1187	-75.18	7201	306.91	4.083	Si
SLV 13	4.57	-799	118.54	4846	210.79	1.778	Si
SLV 2	3.67	-984	50.66	5966	257.03	5.074	Si
SLV 2	4.57	-286	-31.66	1734	77.43	2.446	Si
SLV 8	3.67	-1064	-40.68	6451	276.77	6.804	Si
SLV 8	4.57	-561	74.15	3405	149.92	2.022	Si
SLV 12	3.67	-1125	-78.43	6822	291.72	3.72	Si
SLV 12	4.57	-715	119.21	4339	189.52	1.59	Si
SLV 11	3.67	-1125	-78.43	6822	291.72	3.72	Si
SLV 11	4.57	-715	119.21	4339	189.52	1.59	Si
SLV 16	3.67	-1191	-97	7225	307.89	3.174	Si
SLV 16	4.57	-843	143.11	5115	221.95	1.551	Si
SLV 1	3.67	-984	50.66	5966	257.03	5.074	Si
SLV 1	4.57	-286	-31.66	1734	77.43	2.446	Si
SLV 7	3.67	-1064	-40.68	6451	276.77	6.804	Si
SLV 7	4.57	-561	74.15	3405	149.92	2.022	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma M = 3$

Comb.	Quota	N	V par	M	$\sigma 0$	σN	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 81	3.67	-1588	75	-10.71		9632	0.5495	6840	1128			14.97	Si
SLU 81	4.57	-761	35	64.5		4617	0.5495	6171	1017			29.4	Si
SLU 39	3.67	-1304	95	0.21		7907	0.5495	6610	1090			11.44	Si
SLU 39	4.57	-600	52	46.43		3638	0.5495	6041	996			18.98	Si
SLU 42	3.67	-1304	95	0.21		7907	0.5495	6610	1090			11.44	Si
SLU 42	4.57	-600	52	46.43		3638	0.5495	6041	996			18.98	Si
SLU 41	3.67	-1304	95	0.21		7907	0.5495	6610	1090			11.44	Si
SLU 41	4.57	-600	52	46.43		3638	0.5495	6041	996			18.98	Si
SLU 82	3.67	-1588	75	-10.71		9632	0.5495	6840	1128			14.97	Si
SLU 82	4.57	-761	35	64.5		4617	0.5495	6171	1017			29.4	Si
SLU 84	3.67	-1588	75	-10.71		9632	0.5495	6840	1128			14.97	Si
SLU 84	4.57	-761	35	64.5		4617	0.5495	6171	1017			29.4	Si
SLU 83	3.67	-1588	75	-10.71		9632	0.5495	6840	1128			14.97	Si
SLU 83	4.57	-761	35	64.5		4617	0.5495	6171	1017			29.4	Si
SLU 40	3.67	-1304	95	0.21		7907	0.5495	6610	1090			11.44	Si
SLU 40	4.57	-600	52	46.43		3638	0.5495	6041	996			18.98	Si
SLU 21	3.67	-1235	68	-5.69		7494	0.5495	6555	1081			15.96	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 21	4.57	-586	35	48.17		3553	0.5495	6029	994			28.14	Si
SLU 20	3.67	-1235	68	-5.69		7494	0.5495	6555	1081			15.96	Si
SLU 20	4.57	-586	35	48.17		3553	0.5495	6029	994			28.14	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 14	3.67	-1187	-174	-75.18		7201	0.5495	9773	1611			9.28	Si
SLV 14	4.57	-799	-192	118.54		7024	0.3791	9738	1108			5.76	Si
SLV 11	3.67	-1125	-149	-78.43		6822	0.5495	9698	1599			10.7	Si
SLV 11	4.57	-715	-253	119.21		7353	0.3242	9804	954			3.78	Si
SLV 6	3.67	-1050	136	32.08		6370	0.5495	9607	1584			11.61	Si
SLV 6	4.57	-414	213	-7.76		2510	0.5495	8835	1457			6.85	Si
SLV 13	3.67	-1187	-174	-75.18		7201	0.5495	9773	1611			9.28	Si
SLV 13	4.57	-799	-192	118.54		7024	0.3791	9738	1108			5.76	Si
SLV 2	3.67	-984	212	50.66		5966	0.5495	9527	1570			7.42	Si
SLV 2	4.57	-286	252	-31.66		1937	0.492	8721	1287			5.11	Si
SLV 12	3.67	-1125	-149	-78.43		6822	0.5495	9698	1599			10.7	Si
SLV 12	4.57	-715	-253	119.21		7353	0.3242	9804	954			3.78	Si
SLV 15	3.67	-1191	-225	-97		7225	0.5495	9778	1612			7.17	Si
SLV 15	4.57	-843	-292	143.11		8921	0.315	10117	956			3.28	Si
SLV 16	3.67	-1191	-225	-97		7225	0.5495	9778	1612			7.17	Si
SLV 16	4.57	-843	-292	143.11		8921	0.315	10117	956			3.28	Si
SLV 1	3.67	-984	212	50.66		5966	0.5495	9527	1570			7.42	Si
SLV 1	4.57	-286	252	-31.66		1937	0.492	8721	1287			5.11	Si
SLV 5	3.67	-1050	136	32.08		6370	0.5495	9607	1584			11.61	Si
SLV 5	4.57	-414	213	-7.76		2510	0.5495	8835	1457			6.85	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.595 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 16	143750	0.48	4356	-718	90.48	103.88	1.15	Si
SLV 15	143750	0.48	4356	-718	90.48	103.88	1.15	Si
SLV 11	143750	0.48	4358	-718	90.48	103.93	1.15	Si
SLV 12	143750	0.48	4358	-718	90.48	103.93	1.15	Si
SLV 14	143750	0.48	4647	-766	90.48	110.53	1.22	Si
SLV 13	143750	0.48	4647	-766	90.48	110.53	1.22	Si
SLV 7	143750	0.48	4650	-767	90.48	110.61	1.22	Si
SLV 8	143750	0.48	4650	-767	90.48	110.61	1.22	Si
SLV 10	143750	0.48	5326	-878	90.48	125.96	1.39	Si
SLV 9	143750	0.48	5326	-878	90.48	125.96	1.39	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 3.595 Wa = 0.05 Ta = 0.0825

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 8	-28	-968	43	0.005	116.7	0.978	0.07434	4.97545	No
SLV 7	-28	-968	43	0.005	116.7	0.978	0.07434	4.97545	No
SLV 9	-33	-1191	-43	0.005	116.8	0.975	0.07616	4.97545	No
SLV 10	-33	-1191	-43	0.005	116.8	0.975	0.07616	4.97545	No
SLV 14	-28	-941	-25	0.034	116.7	0.978	0.50045	10.57293	No
SLV 13	-28	-941	-25	0.034	116.7	0.978	0.50045	10.57293	No
SLV 4	-34	-1218	25	0.034	116.8	0.974	0.50614	10.57293	No
SLV 3	-34	-1218	25	0.034	116.8	0.974	0.50614	10.57293	No
SLV 12	-26	-855	34	0.019	116.7	0.98	0.27783	4.97545	No
SLV 11	-26	-855	34	0.019	116.7	0.98	0.27783	4.97545	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	2.44	SLU 43	Si
V_SLU	11.441	SLU 39	Si
PF_SLV	1.551	SLV 15	Si
V_SLV	3.276	SLV 15	Si
PFFP_SLV	1.148	SLV 15	Si
R_SLV	0.015	SLV 7	No

Maschio 21

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s,sx	a.s,dx
32.569	-0.169	29.969	-0.169	L2	L3	2.6	0.3	3.85	3.85	3.85			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 41	3.67	-6312	1003.49	8093	7389.6	7.364	Si
SLU 41	4.57	-3498	483.87	4485	4296.98	8.881	Si
SLU 42	3.67	-6312	1003.49	8093	7389.6	7.364	Si
SLU 42	4.57	-3498	483.87	4485	4296.98	8.881	Si
SLU 39	3.67	-6312	1003.49	8093	7389.6	7.364	Si
SLU 39	4.57	-3498	483.87	4485	4296.98	8.881	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 21	3.67	-5764	841.77	7390	6812.37	8.093	Si
SLU 21	4.57	-3162	374.45	4054	3905.38	10.43	Si
SLU 81	3.67	-7312	1036.6	9375	8411.15	8.114	Si
SLU 81	4.57	-3999	443.48	5127	4870.9	10.983	Si
SLU 40	3.67	-6312	1003.49	8093	7389.6	7.364	Si
SLU 40	4.57	-3498	483.87	4485	4296.98	8.881	Si
SLU 18	3.67	-5764	841.77	7390	6812.37	8.093	Si
SLU 18	4.57	-3162	374.45	4054	3905.38	10.43	Si
SLU 20	3.67	-5764	841.77	7390	6812.37	8.093	Si
SLU 20	4.57	-3162	374.45	4054	3905.38	10.43	Si
SLU 19	3.67	-5764	841.77	7390	6812.37	8.093	Si
SLU 19	4.57	-3162	374.45	4054	3905.38	10.43	Si
SLU 82	3.67	-7312	1036.6	9375	8411.15	8.114	Si
SLU 82	4.57	-3999	443.48	5127	4870.9	10.983	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 13	3.67	-4451	-16.07	5706	5515.25	343.295	Si
SLV 13	4.57	-2171	471.32	2784	2758.06	5.852	Si
SLV 2	3.67	-4623	914.34	5927	5717.36	6.253	Si
SLV 2	4.57	-2577	-205.07	3304	3259.32	15.893	Si
SLV 3	3.67	-4506	917.49	5777	5580.43	6.082	Si
SLV 3	4.57	-2571	-274.34	3296	3251.78	11.853	Si
SLV 15	3.67	-4334	-12.92	5557	5377.77	416.274	Si
SLV 15	4.57	-2165	402.05	2776	2750.45	6.841	Si
SLV 8	3.67	-4310	595.52	5526	5349.15	8.982	Si
SLV 8	4.57	-2422	-118.41	3105	3067.99	25.91	Si
SLV 7	3.67	-4310	595.52	5526	5349.15	8.982	Si
SLV 7	4.57	-2422	-118.41	3105	3067.99	25.91	Si
SLV 1	3.67	-4623	914.34	5927	5717.36	6.253	Si
SLV 1	4.57	-2577	-205.07	3304	3259.32	15.893	Si
SLV 4	3.67	-4506	917.49	5777	5580.43	6.082	Si
SLV 4	4.57	-2571	-274.34	3296	3251.78	11.853	Si
SLV 16	3.67	-4334	-12.92	5557	5377.77	416.274	Si
SLV 16	4.57	-2165	402.05	2776	2750.45	6.841	Si
SLV 14	3.67	-4451	-16.07	5706	5515.25	343.295	Si
SLV 14	4.57	-2171	471.32	2784	2758.06	5.852	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 40	3.67	-6312	-164	1003.49		8093	2.5998	6635	5175			31.63	Si
SLU 40	4.57	-3498	-317	483.87		4485	2.5998	6154	4799			15.12	Si
SLU 81	3.67	-7312	-142	1036.6		9375	2.5998	6806	5308			37.5	Si
SLU 81	4.57	-3999	-294	443.48		5127	2.5998	6239	4866			16.52	Si
SLU 83	3.67	-7312	-142	1036.6		9375	2.5998	6806	5308			37.5	Si
SLU 83	4.57	-3999	-294	443.48		5127	2.5998	6239	4866			16.52	Si
SLU 42	3.67	-6312	-164	1003.49		8093	2.5998	6635	5175			31.63	Si
SLU 42	4.57	-3498	-317	483.87		4485	2.5998	6154	4799			15.12	Si
SLU 82	3.67	-7312	-142	1036.6		9375	2.5998	6806	5308			37.5	Si
SLU 82	4.57	-3999	-294	443.48		5127	2.5998	6239	4866			16.52	Si
SLU 20	3.67	-5764	-125	841.77		7390	2.5998	6541	5101			40.69	Si
SLU 20	4.57	-3162	-254	374.45		4054	2.5998	6096	4755			18.72	Si
SLU 41	3.67	-6312	-164	1003.49		8093	2.5998	6635	5175			31.63	Si
SLU 41	4.57	-3498	-317	483.87		4485	2.5998	6154	4799			15.12	Si
SLU 21	3.67	-5764	-125	841.77		7390	2.5998	6541	5101			40.69	Si
SLU 21	4.57	-3162	-254	374.45		4054	2.5998	6096	4755			18.72	Si
SLU 39	3.67	-6312	-164	1003.49		8093	2.5998	6635	5175			31.63	Si
SLU 39	4.57	-3498	-317	483.87		4485	2.5998	6154	4799			15.12	Si
SLU 84	3.67	-7312	-142	1036.6		9375	2.5998	6806	5308			37.5	Si
SLU 84	4.57	-3999	-294	443.48		5127	2.5998	6239	4866			16.52	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 16	3.67	-4334	-1052	-12.92		5557	2.5998	9445	7366			7	Si
SLV 16	4.57	-2165	-698	402.05		2776	2.5998	8889	6933			9.94	Si
SLV 4	3.67	-4506	1219	917.49		5777	2.5998	9489	7401			6.07	Si
SLV 4	4.57	-2571	863	-274.34		3296	2.5998	8993	7014			8.12	Si
SLV 14	3.67	-4451	-1243	-16.07		5706	2.5998	9475	7390			5.94	Si
SLV 14	4.57	-2171	-995	471.32		2784	2.5998	8890	6934			6.97	Si
SLV 15	3.67	-4334	-1052	-12.92		5557	2.5998	9445	7366			7	Si
SLV 15	4.57	-2165	-698	402.05		2776	2.5998	8889	6933			9.94	Si
SLV 9	3.67	-4647	-671	305.9		5958	2.5998	9525	7429			11.07	Si
SLV 9	4.57	-2320	-796	315.39		2975	2.5998	8928	6964			8.75	Si
SLV 1	3.67	-4623	1028	914.34		5927	2.5998	9519	7424			7.22	Si
SLV 1	4.57	-2577	566	-205.07		3304	2.5998	8994	7015			12.39	Si
SLV 3	3.67	-4506	1219	917.49		5777	2.5998	9489	7401			6.07	Si
SLV 3	4.57	-2571	863	-274.34		3296	2.5998	8993	7014			8.12	Si
SLV 2	3.67	-4623	1028	914.34		5927	2.5998	9519	7424			7.22	Si
SLV 2	4.57	-2577	566	-205.07		3304	2.5998	8994	7015			12.39	Si
SLV 13	3.67	-4451	-1243	-16.07		5706	2.5998	9475	7390			5.94	Si
SLV 13	4.57	-2171	-995	471.32		2784	2.5998	8890	6934			6.97	Si
SLV 10	3.67	-4647	-671	305.9		5958	2.5998	9525	7429			11.07	Si
SLV 10	4.57	-2320	-796	315.39		2975	2.5998	8928	6964			8.75	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.595 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 12	143750	0.48	5312	-4143	428.08	594.43	1.39	Si
SLV 11	143750	0.48	5312	-4143	428.08	594.43	1.39	Si



Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 8	143750	0.48	5317	-4147	428.08	595	1.39	Si
SLV 7	143750	0.48	5317	-4147	428.08	595	1.39	Si
SLV 16	143750	0.48	5438	-4242	428.08	607.93	1.42	Si
SLV 15	143750	0.48	5438	-4242	428.08	607.93	1.42	Si
SLV 4	143750	0.48	5456	-4255	428.08	609.8	1.42	Si
SLV 3	143750	0.48	5456	-4255	428.08	609.8	1.42	Si
SLV 13	143750	0.48	5552	-4330	428.08	620.04	1.45	Si
SLV 14	143750	0.48	5552	-4330	428.08	620.04	1.45	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 3.595 $W_a = 0.05$ $T_a = 0.0825$

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 14	-323	-7251	49	0.058	557.3	0.954	0.87793	10.57293	No
SLV 13	-323	-7251	49	0.058	557.3	0.954	0.87793	10.57293	No
SLV 3	-312	-7000	-49	0.058	556.9	0.956	0.8789	10.57293	No
SLV 4	-312	-7000	-49	0.058	556.9	0.956	0.8789	10.57293	No
SLV 15	-314	-7557	31	0.063	557	0.955	0.96574	10.57293	No
SLV 16	-314	-7557	31	0.063	557	0.955	0.96574	10.57293	No
SLV 1	-321	-6694	-31	0.063	557.3	0.955	0.96663	10.57293	No
SLV 2	-321	-6694	-31	0.063	557.3	0.955	0.96663	10.57293	No
SLV 10	-334	-6700	41	0.06	557.7	0.953	0.9162	4.97545	No
SLV 9	-334	-6700	41	0.06	557.7	0.953	0.9162	4.97545	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	7.364	SLU 39	Si
V_SLU	15.122	SLU 39	Si
PF_SLV	5.852	SLV 13	Si
V_SLV	5.944	SLV 13	Si
PFFP_SLV	1.389	SLV 11	Si
R_SLV	0.083	SLV 13	No

Maschio 22

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
35.424	-0.169	33.569	-0.169	L2	L3	1.855	0.3	3.85	3.85	3.85			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 48	2.67	-4145	178.14	7447	3493.42	19.611	Si
SLU 48	4.57	-1532	196.99	2753	1373.26	6.971	Si
SLU 47	2.67	-4145	178.14	7447	3493.42	19.611	Si
SLU 47	4.57	-1532	196.99	2753	1373.26	6.971	Si
SLU 51	2.67	-4145	178.14	7447	3493.42	19.611	Si
SLU 51	4.57	-1532	196.99	2753	1373.26	6.971	Si
SLU 45	2.67	-4145	178.14	7447	3493.42	19.611	Si
SLU 45	4.57	-1532	196.99	2753	1373.26	6.971	Si
SLU 49	2.67	-4145	178.14	7447	3493.42	19.611	Si
SLU 49	4.57	-1532	196.99	2753	1373.26	6.971	Si
SLU 44	2.67	-4145	178.14	7447	3493.42	19.611	Si
SLU 44	4.57	-1532	196.99	2753	1373.26	6.971	Si
SLU 1	2.67	-3265	125.7	5866	2810.65	22.36	Si
SLU 1	4.57	-1215	143.12	2182	1096.43	7.661	Si
SLU 46	2.67	-4145	178.14	7447	3493.42	19.611	Si
SLU 46	4.57	-1532	196.99	2753	1373.26	6.971	Si
SLU 50	2.67	-4145	178.14	7447	3493.42	19.611	Si
SLU 50	4.57	-1532	196.99	2753	1373.26	6.971	Si
SLU 43	2.67	-4145	178.14	7447	3493.42	19.611	Si
SLU 43	4.57	-1532	196.99	2753	1373.26	6.971	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 15	2.67	-3106	-338.02	5581	2749.97	8.135	Si
SLV 15	4.57	-1390	373.91	2498	1263.2	3.378	Si
SLV 10	2.67	-4559	-43.97	8192	3945.85	89.749	Si
SLV 10	4.57	-1762	310.18	3167	1592.48	5.134	Si
SLV 13	2.67	-3736	-340.93	6712	3275.16	9.607	Si
SLV 13	4.57	-1614	441.1	2900	1461.52	3.313	Si
SLV 1	2.67	-3990	517.23	7170	3484.38	6.737	Si
SLV 1	4.57	-1293	-156.92	2323	1176.32	7.496	Si
SLV 2	2.67	-3990	517.23	7170	3484.38	6.737	Si
SLV 2	4.57	-1293	-156.92	2323	1176.32	7.496	Si
SLV 9	2.67	-4559	-43.97	8192	3945.85	89.749	Si
SLV 9	4.57	-1762	310.18	3167	1592.48	5.134	Si
SLV 14	2.67	-3736	-340.93	6712	3275.16	9.607	Si
SLV 14	4.57	-1614	441.1	2900	1461.52	3.313	Si
SLV 16	2.67	-3106	-338.02	5581	2749.97	8.135	Si
SLV 16	4.57	-1390	373.91	2498	1263.2	3.378	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 3	2.67	-3361	520.14	6039	2963.57	5.698	Si
SLV 3	4.57	-1069	-224.11	1921	976.04	4.355	Si
SLV 4	2.67	-3361	520.14	6039	2963.57	5.698	Si
SLV 4	4.57	-1069	-224.11	1921	976.04	4.355	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLU 41	2.67	-4557	372	-36.37		8188	1.8552	6647	3700			9.94	Si
SLU 41	4.57	-1791	372	-16.33		3217	1.8552	5985	3331			8.95	Si
SLU 19	2.67	-4266	317	6.6		7666	1.8552	6578	3661			11.56	Si
SLU 19	4.57	-1655	316	15.56		2973	1.8552	5952	3313			10.47	Si
SLU 18	2.67	-4266	317	6.6		7666	1.8552	6578	3661			11.56	Si
SLU 18	4.57	-1655	316	15.56		2973	1.8552	5952	3313			10.47	Si
SLU 82	2.67	-5437	365	16.07		9769	1.8552	6858	3817			10.47	Si
SLU 82	4.57	-2108	365	37.54		3788	1.8552	6061	3373			9.25	Si
SLU 39	2.67	-4557	372	-36.37		8188	1.8552	6647	3700			9.94	Si
SLU 39	4.57	-1791	372	-16.33		3217	1.8552	5985	3331			8.95	Si
SLU 42	2.67	-4557	372	-36.37		8188	1.8552	6647	3700			9.94	Si
SLU 42	4.57	-1791	372	-16.33		3217	1.8552	5985	3331			8.95	Si
SLU 84	2.67	-5437	365	16.07		9769	1.8552	6858	3817			10.47	Si
SLU 84	4.57	-2108	365	37.54		3788	1.8552	6061	3373			9.25	Si
SLU 40	2.67	-4557	372	-36.37		8188	1.8552	6647	3700			9.94	Si
SLU 40	4.57	-1791	372	-16.33		3217	1.8552	5985	3331			8.95	Si
SLU 83	2.67	-5437	365	16.07		9769	1.8552	6858	3817			10.47	Si
SLU 83	4.57	-2108	365	37.54		3788	1.8552	6061	3373			9.25	Si
SLU 81	2.67	-5437	365	16.07		9769	1.8552	6858	3817			10.47	Si
SLU 81	4.57	-2108	365	37.54		3788	1.8552	6061	3373			9.25	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLV 6	2.67	-4636	577	213.48		8329	1.8552	9999	5565			9.64	Si
SLV 6	4.57	-1666	820	130.77		2993	1.8552	8932	4971			6.06	Si
SLV 4	2.67	-3361	966	520.14		6039	1.8552	9541	5310			5.49	Si
SLV 4	4.57	-1069	428	-224.11		1921	1.8552	8717	4852			11.35	Si
SLV 5	2.67	-4636	577	213.48		8329	1.8552	9999	5565			9.64	Si
SLV 5	4.57	-1666	820	130.77		2993	1.8552	8932	4971			6.06	Si
SLV 2	2.67	-3990	1082	517.23		7170	1.8552	9767	5436			5.02	Si
SLV 2	4.57	-1293	766	-156.92		2323	1.8552	8798	4897			6.39	Si
SLV 3	2.67	-3361	966	520.14		6039	1.8552	9541	5310			5.49	Si
SLV 3	4.57	-1069	428	-224.11		1921	1.8552	8717	4852			11.35	Si
SLV 13	2.67	-3736	-747	-340.93		6712	1.8552	9676	5385			7.21	Si
SLV 13	4.57	-1614	-208	441.1		2900	1.8552	8913	4961			23.85	Si
SLV 14	2.67	-3736	-747	-340.93		6712	1.8552	9676	5385			7.21	Si
SLV 14	4.57	-1614	-208	441.1		2900	1.8552	8913	4961			23.85	Si
SLV 16	2.67	-3106	-862	-338.02		5581	1.8552	9450	5259			6.1	Si
SLV 16	4.57	-1390	-547	373.91		2498	1.8552	8833	4916			9	Si
SLV 15	2.67	-3106	-862	-338.02		5581	1.8552	9450	5259			6.1	Si
SLV 15	4.57	-1390	-547	373.91		2498	1.8552	8833	4916			9	Si
SLV 1	2.67	-3990	1082	517.23		7170	1.8552	9767	5436			5.02	Si
SLV 1	4.57	-1293	766	-156.92		2323	1.8552	8798	4897			6.39	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.595 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 8	143750	0.48	3824	-2128	305.48	309.24	1.01	Si
SLV 7	143750	0.48	3824	-2128	305.48	309.24	1.01	Si
SLV 11	143750	0.48	3833	-2133	305.48	309.96	1.01	Si
SLV 12	143750	0.48	3833	-2133	305.48	309.96	1.01	Si
SLV 4	143750	0.48	4445	-2474	305.48	357.63	1.17	Si
SLV 3	143750	0.48	4445	-2474	305.48	357.63	1.17	Si
SLV 16	143750	0.48	4476	-2491	305.48	359.97	1.18	Si
SLV 15	143750	0.48	4476	-2491	305.48	359.97	1.18	Si
SLV 1	143750	0.48	4987	-2776	305.48	399.38	1.31	Si
SLV 2	143750	0.48	4987	-2776	305.48	399.38	1.31	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.595 Wa = 0.05 Ta = 0.0825

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 1	-186	-4258	-167	0	396.2	0.961	0	10.57293	No
SLV 15	-55	-4460	167	0	393.5	0.987	0	10.57293	No
SLV 16	-55	-4460	167	0	393.5	0.987	0	10.57293	No
SLV 14	-105	-5120	159	0	394.2	0.976	0	10.57293	No
SLV 2	-186	-4258	-167	0	396.2	0.961	0	10.57293	No
SLV 3	-136	-3597	-160	0	394.9	0.97	0	10.57293	No
SLV 4	-136	-3597	-160	0	394.9	0.97	0	10.57293	No
SLV 13	-105	-5120	159	0	394.2	0.976	0	10.57293	No
SLV 12	-24	-3387	61	0.046	393.2	0.994	0.67507	4.97545	No
SLV 11	-24	-3387	61	0.046	393.2	0.994	0.67507	4.97545	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	6.971	SLU 43	Si
V_SLU	8.952	SLU 39	Si
PF_SLV	3.313	SLV 13	Si
V_SLV	5.023	SLV 1	Si
PFFP_SLV	1.012	SLV 7	Si
R_SLV	0	SLV 1	No



Maschio 23

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
30.718	3.536	30.718	-0.169	L2	L3	3.705	0.18	3.85	3.85	3.85			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _k	f _{vk0}	f _{medio}	τ ₀	f _{v0}	μ	φ	f _{v,lim}	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γ_M = 3

Comb.	Quota	N	M	σ ₀	Mu	c.s.	Verifica
SLU 42	1.67	-17465	-5191.9	26189	21952.62	4.228	Si
SLU 42	3.77	-16843	-3935.66	25256	21527.93	5.47	Si
SLU 82	1.67	-19165	-5437.84	28737	22977.93	4.226	Si
SLU 82	3.77	-17887	-4126.48	26821	22225.46	5.386	Si
SLU 20	1.67	-15229	-4381.04	22836	20303.19	4.634	Si
SLU 20	3.77	-14412	-3292.71	21611	19615.43	5.957	Si
SLU 84	1.67	-19165	-5437.84	28737	22977.93	4.226	Si
SLU 84	3.77	-17887	-4126.48	26821	22225.46	5.386	Si
SLU 41	1.67	-17465	-5191.9	26189	21952.62	4.228	Si
SLU 41	3.77	-16843	-3935.66	25256	21527.93	5.47	Si
SLU 21	1.67	-15229	-4381.04	22836	20303.19	4.634	Si
SLU 21	3.77	-14412	-3292.71	21611	19615.43	5.957	Si
SLU 40	1.67	-17465	-5191.9	26189	21952.62	4.228	Si
SLU 40	3.77	-16843	-3935.66	25256	21527.93	5.47	Si
SLU 39	1.67	-17465	-5191.9	26189	21952.62	4.228	Si
SLU 39	3.77	-16843	-3935.66	25256	21527.93	5.47	Si
SLU 83	1.67	-19165	-5437.84	28737	22977.93	4.226	Si
SLU 83	3.77	-17887	-4126.48	26821	22225.46	5.386	Si
SLU 81	1.67	-19165	-5437.84	28737	22977.93	4.226	Si
SLU 81	3.77	-17887	-4126.48	26821	22225.46	5.386	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γ_M = 2

Comb.	Quota	N	M	σ ₀	Mu	c.s.	Verifica
SLV 10	1.67	-11000	3189.52	16494	17626.27	5.526	Si
SLV 10	3.77	-9239	-2713.61	13854	15175.29	5.592	Si
SLV 11	1.67	-9193	-7907.76	13785	15109.05	1.911	Si
SLV 11	3.77	-7515	-1158.05	11269	12637.85	10.913	Si
SLV 15	1.67	-9442	-3683.11	14159	15465.05	4.199	Si
SLV 15	3.77	-7637	-1695.22	11452	12821.9	7.564	Si
SLV 16	1.67	-9442	-3683.11	14159	15465.05	4.199	Si
SLV 16	3.77	-7637	-1695.22	11452	12821.9	7.564	Si
SLV 7	1.67	-9522	-8199.7	14277	15577.66	1.9	Si
SLV 7	3.77	-7928	-1164.28	11888	13257.44	11.387	Si
SLV 9	1.67	-11000	3189.52	16494	17626.27	5.526	Si
SLV 9	3.77	-9239	-2713.61	13854	15175.29	5.592	Si
SLV 4	1.67	-10537	-4656.25	15800	16995.64	3.65	Si
SLV 4	3.77	-9013	-1716	13514	14849.46	8.654	Si
SLV 8	1.67	-9522	-8199.7	14277	15577.66	1.9	Si
SLV 8	3.77	-7928	-1164.28	11888	13257.44	11.387	Si
SLV 3	1.67	-10537	-4656.25	15800	16995.64	3.65	Si
SLV 3	3.77	-9013	-1716	13514	14849.46	8.654	Si
SLV 12	1.67	-9193	-7907.76	13785	15109.05	1.911	Si
SLV 12	3.77	-7515	-1158.05	11269	12637.85	10.913	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, γ_M = 3

Comb.	Quota	N	V par	M	σ ₀	σ _N	I'	f _{vd}	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLU 63	1.67	-16928	1042	-4626.99	25384	3.705	8940	5962				5.72	Si
SLU 63	3.77	-15456	1026	-3483.53	23176	3.705	8646	5766				5.62	Si
SLU 41	1.67	-17465	1211	-5191.9	26189	3.705	9047	6034				4.98	Si
SLU 41	3.77	-16843	1192	-3935.66	25256	3.705	8923	5951				4.99	Si
SLU 39	1.67	-17465	1211	-5191.9	26189	3.705	9047	6034				4.98	Si
SLU 39	3.77	-16843	1192	-3935.66	25256	3.705	8923	5951				4.99	Si
SLU 83	1.67	-19165	1242	-5437.84	28737	3.705	9387	6260				5.04	Si
SLU 83	3.77	-17887	1223	-4126.48	26821	3.705	9132	6090				4.98	Si
SLU 62	1.67	-16928	1042	-4626.99	25384	3.705	8940	5962				5.72	Si
SLU 62	3.77	-15456	1026	-3483.53	23176	3.705	8646	5766				5.62	Si
SLU 82	1.67	-19165	1242	-5437.84	28737	3.705	9387	6260				5.04	Si
SLU 82	3.77	-17887	1223	-4126.48	26821	3.705	9132	6090				4.98	Si
SLU 84	1.67	-19165	1242	-5437.84	28737	3.705	9387	6260				5.04	Si
SLU 84	3.77	-17887	1223	-4126.48	26821	3.705	9132	6090				4.98	Si
SLU 81	1.67	-19165	1242	-5437.84	28737	3.705	9387	6260				5.04	Si
SLU 81	3.77	-17887	1223	-4126.48	26821	3.705	9132	6090				4.98	Si
SLU 40	1.67	-17465	1211	-5191.9	26189	3.705	9047	6034				4.98	Si
SLU 40	3.77	-16843	1192	-3935.66	25256	3.705	8923	5951				4.99	Si
SLU 42	1.67	-17465	1211	-5191.9	26189	3.705	9047	6034				4.98	Si
SLU 42	3.77	-16843	1192	-3935.66	25256	3.705	8923	5951				4.99	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, γ_M = 2

Comb.	Quota	N	V par	M	σ ₀	σ _N	I'	f _{vd}	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLV 10	1.67	-11000	5164	3189.52	16494	3.705	11632	7757				1.5	Si
SLV 10	3.77	-9239	3142	-2713.61	13854	3.705	11104	7405				2.36	Si
SLV 11	1.67	-9193	-3917	-7907.76	17156	2.977	11765	6304				1.61	Si
SLV 11	3.77	-7515	-1983	-1158.05	11269	3.705	10587	7061				3.56	Si
SLV 13	1.67	-9984	2212	-353.93	14971	3.705	11328	7554				3.41	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 13	3.77	-8154	1490	-2161.89		12227	3.705	10779	7188			4.82	Si
SLV 6	1.67	-11328	4970	2897.58		16986	3.705	11731	7823			1.57	Si
SLV 6	3.77	-9652	3020	-2719.84		14473	3.705	11228	7488			2.48	Si
SLV 5	1.67	-11328	4970	2897.58		16986	3.705	11731	7823			1.57	Si
SLV 5	3.77	-9652	3020	-2719.84		14473	3.705	11228	7488			2.48	Si
SLV 9	1.67	-11000	5164	3189.52		16494	3.705	11632	7757			1.5	Si
SLV 9	3.77	-9239	3142	-2713.61		13854	3.705	11104	7405			2.36	Si
SLV 12	1.67	-9193	-3917	-7907.76		17156	2.977	11765	6304			1.61	Si
SLV 12	3.77	-7515	-1983	-1158.05		11269	3.705	10587	7061			3.56	Si
SLV 14	1.67	-9984	2212	-353.93		14971	3.705	11328	7554			3.41	Si
SLV 14	3.77	-8154	1490	-2161.89		12227	3.705	10779	7188			4.82	Si
SLV 8	1.67	-9522	-4111	-8199.7		17787	2.974	11891	6365			1.55	Si
SLV 8	3.77	-7928	-2105	-1164.28		11888	3.705	10711	7143			3.39	Si
SLV 7	1.67	-9522	-4111	-8199.7		17787	2.974	11891	6365			1.55	Si
SLV 7	3.77	-7928	-2105	-1164.28		11888	3.705	10711	7143			3.39	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.595 Wa 0.03 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 11	143750	0.48	11250	-7503	384.6	613.07	1.59	Si
SLV 12	143750	0.48	11250	-7503	384.6	613.07	1.59	Si
SLV 15	143750	0.48	11452	-7638	384.6	622.95	1.62	Si
SLV 16	143750	0.48	11452	-7638	384.6	622.95	1.62	Si
SLV 8	143750	0.48	11883	-7925	384.6	643.87	1.67	Si
SLV 7	143750	0.48	11883	-7925	384.6	643.87	1.67	Si
SLV 14	143750	0.48	12259	-8175	384.6	661.96	1.72	Si
SLV 13	143750	0.48	12259	-8175	384.6	661.96	1.72	Si
SLV 3	143750	0.48	13563	-9045	384.6	723.68	1.88	Si
SLV 4	143750	0.48	13563	-9045	384.6	723.68	1.88	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.595 Wa = 0.03 Ta = 0.1375

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 5	-7270	-11328	-40	0.025	1110.6	0.916	0.39416	5.79734	No
SLV 6	-7270	-11328	-40	0.025	1110.6	0.916	0.39416	5.79734	No
SLV 12	-7199	-9193	40	0.025	1103.4	0.916	0.39452	5.79734	No
SLV 11	-7199	-9193	40	0.025	1103.4	0.916	0.39452	5.79734	No
SLV 7	-7239	-9522	-23	0.027	1107.5	0.916	0.42303	5.79734	No
SLV 8	-7239	-9522	-23	0.027	1107.5	0.916	0.42303	5.79734	No
SLV 9	-7230	-11000	23	0.027	1106.6	0.916	0.42311	5.79734	No
SLV 10	-7230	-11000	23	0.027	1106.6	0.916	0.42311	5.79734	No
SLV 16	-7163	-9442	107	0.018	1099.8	0.916	0.28253	2.39674	No
SLV 15	-7163	-9442	107	0.018	1099.8	0.916	0.28253	2.39674	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	4.226	SLU 81	Si
V_SLU	4.98	SLU 81	Si
PF_SLV	1.9	SLV 7	Si
V_SLV	1.502	SLV 9	Si
PFFP_SLV	1.594	SLV 11	Si
R_SLV	0.068	SLV 5	No

Maschio 24

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
30.718	4.834	30.718	4.336	L2	L3	0.497	0.18	3.85	3.85	3.85			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	t0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 41	1.67	-4165	-3.74	46521	444.18	118.843	Si
SLU 41	3.77	-3817	41.36	42633	452.35	10.936	Si
SLU 82	1.67	-4577	-5.7	51125	423.81	74.386	Si
SLU 82	3.77	-4002	44.64	44707	449.02	10.058	Si
SLU 83	1.67	-4577	-5.7	51125	423.81	74.386	Si
SLU 83	3.77	-4002	44.64	44707	449.02	10.058	Si
SLU 40	1.67	-4165	-3.74	46521	444.18	118.843	Si
SLU 40	3.77	-3817	41.36	42633	452.35	10.936	Si
SLU 39	1.67	-4165	-3.74	46521	444.18	118.843	Si
SLU 39	3.77	-3817	41.36	42633	452.35	10.936	Si
SLU 42	1.67	-4165	-3.74	46521	444.18	118.843	Si
SLU 42	3.77	-3817	41.36	42633	452.35	10.936	Si
SLU 77	1.67	-4093	-7.54	45719	446.54	59.202	Si
SLU 77	3.77	-3390	39.59	37872	451.11	11.396	Si
SLU 84	1.67	-4577	-5.7	51125	423.81	74.386	Si
SLU 84	3.77	-4002	44.64	44707	449.02	10.058	Si
SLU 81	1.67	-4577	-5.7	51125	423.81	74.386	Si
SLU 81	3.77	-4002	44.64	44707	449.02	10.058	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 75	1.67	-4093	-7.54	45719	446.54	59.202	Si
SLU 75	3.77	-3390	39.59	37872	451.11	11.396	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 8	1.67	-2647	95.82	29564	498.89	5.207	Si
SLV 8	3.77	-1642	52.68	18344	347.05	6.588	Si
SLV 9	1.67	-2316	-110.9	25876	454.05	4.094	Si
SLV 9	3.77	-1956	-5.97	21844	399.35	66.878	Si
SLV 10	1.67	-2316	-110.9	25876	454.05	4.094	Si
SLV 10	3.77	-1956	-5.97	21844	399.35	66.878	Si
SLV 13	1.67	-1811	-62.11	20232	375.82	6.051	Si
SLV 13	3.77	-2148	25.39	23996	429.28	16.908	Si
SLV 11	1.67	-2237	80.28	24992	442.55	5.513	Si
SLV 11	3.77	-1842	59.82	20571	380.84	6.366	Si
SLV 12	1.67	-2237	80.28	24992	442.55	5.513	Si
SLV 12	3.77	-1842	59.82	20571	380.84	6.366	Si
SLV 7	1.67	-2647	95.82	29564	498.89	5.207	Si
SLV 7	3.77	-1642	52.68	18344	347.05	6.588	Si
SLV 5	1.67	-2726	-95.36	30448	508.91	5.337	Si
SLV 5	3.77	-1756	-13.11	19618	366.6	27.955	Si
SLV 14	1.67	-1811	-62.11	20232	375.82	6.051	Si
SLV 14	3.77	-2148	25.39	23996	429.28	16.908	Si
SLV 6	1.67	-2726	-95.36	30448	508.91	5.337	Si
SLV 6	3.77	-1756	-13.11	19618	366.6	27.955	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 48	1.67	-2414	-35	-10.28		26967	0.4973	9151	819			23.2	Si
SLU 48	3.77	-1422	-35	21.45		15886	0.4973	7674	687			19.46	Si
SLU 45	1.67	-2414	-35	-10.28		26967	0.4973	9151	819			23.2	Si
SLU 45	3.77	-1422	-35	21.45		15886	0.4973	7674	687			19.46	Si
SLU 47	1.67	-2414	-35	-10.28		26967	0.4973	9151	819			23.2	Si
SLU 47	3.77	-1422	-35	21.45		15886	0.4973	7674	687			19.46	Si
SLU 51	1.67	-2414	-35	-10.28		26967	0.4973	9151	819			23.2	Si
SLU 51	3.77	-1422	-35	21.45		15886	0.4973	7674	687			19.46	Si
SLU 50	1.67	-2414	-35	-10.28		26967	0.4973	9151	819			23.2	Si
SLU 50	3.77	-1422	-35	21.45		15886	0.4973	7674	687			19.46	Si
SLU 43	1.67	-2414	-35	-10.28		26967	0.4973	9151	819			23.2	Si
SLU 43	3.77	-1422	-35	21.45		15886	0.4973	7674	687			19.46	Si
SLU 67	1.67	-2963	-39	-11.85		33104	0.4973	9969	892			22.94	Si
SLU 67	3.77	-1963	-39	27.79		21923	0.4973	8479	759			19.51	Si
SLU 44	1.67	-2414	-35	-10.28		26967	0.4973	9151	819			23.2	Si
SLU 44	3.77	-1422	-35	21.45		15886	0.4973	7674	687			19.46	Si
SLU 46	1.67	-2414	-35	-10.28		26967	0.4973	9151	819			23.2	Si
SLU 46	3.77	-1422	-35	21.45		15886	0.4973	7674	687			19.46	Si
SLU 49	1.67	-2414	-35	-10.28		26967	0.4973	9151	819			23.2	Si
SLU 49	3.77	-1422	-35	21.45		15886	0.4973	7674	687			19.46	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 14	1.67	-1811	92	-62.11		20232	0.4973	12380	1108			11.98	Si
SLV 14	3.77	-2148	-248	25.39		23996	0.4973	13133	1176			4.75	Si
SLV 10	1.67	-2316	-13	-110.9		25876	0.4973	13509	1209			92.06	Si
SLV 10	3.77	-1956	-651	-5.97		21844	0.4973	12702	1137			1.75	Si
SLV 13	1.67	-1811	92	-62.11		20232	0.4973	12380	1108			11.98	Si
SLV 13	3.77	-2148	-248	25.39		23996	0.4973	13133	1176			4.75	Si
SLV 5	1.67	-2726	-89	-95.36		30448	0.4973	14423	1291			14.48	Si
SLV 5	3.77	-1756	-629	-13.11		19618	0.4973	12257	1097			1.74	Si
SLV 8	1.67	-2647	-41	95.82		29564	0.4973	14246	1275			31.22	Si
SLV 8	3.77	-1642	597	52.68		18344	0.4973	12002	1074			1.8	Si
SLV 9	1.67	-2316	-13	-110.9		25876	0.4973	13509	1209			92.06	Si
SLV 9	3.77	-1956	-651	-5.97		21844	0.4973	12702	1137			1.75	Si
SLV 6	1.67	-2726	-89	-95.36		30448	0.4973	14423	1291			14.48	Si
SLV 6	3.77	-1756	-629	-13.11		19618	0.4973	12257	1097			1.74	Si
SLV 7	1.67	-2647	-41	95.82		29564	0.4973	14246	1275			31.22	Si
SLV 7	3.77	-1642	597	52.68		18344	0.4973	12002	1074			1.8	Si
SLV 12	1.67	-2237	35	80.28		24992	0.4973	13332	1193			33.92	Si
SLV 12	3.77	-1842	575	59.82		20571	0.4973	12447	1114			1.94	Si
SLV 11	1.67	-2237	35	80.28		24992	0.4973	13332	1193			33.92	Si
SLV 11	3.77	-1842	575	59.82		20571	0.4973	12447	1114			1.94	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.595 Wa 0.03 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 4	143750	0.48	14007	-1254	51.63	99.92	1.94	Si
SLV 3	143750	0.48	14007	-1254	51.63	99.92	1.94	Si
SLV 2	143750	0.48	14594	-1306	51.63	103.54	2.01	Si
SLV 1	143750	0.48	14594	-1306	51.63	103.54	2.01	Si
SLV 8	143750	0.48	15762	-1411	51.63	110.61	2.14	Si
SLV 7	143750	0.48	15762	-1411	51.63	110.61	2.14	Si
SLV 6	143750	0.48	17719	-1586	51.63	122.06	2.36	Si
SLV 5	143750	0.48	17719	-1586	51.63	122.06	2.36	Si
SLV 12	143750	0.48	17854	-1598	51.63	122.83	2.38	Si
SLV 11	143750	0.48	17854	-1598	51.63	122.83	2.38	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.595 Wa = 0.03 Ta = 0.1375



Comb.	N top	N base	V orto	$\alpha 0$	M*	e*	a0*	aLim	Verifica
SLV 6	-668	-2726	-9	0.021	118.5	0.902	0.34312	5.79734	No
SLV 5	-668	-2726	-9	0.021	118.5	0.902	0.34312	5.79734	No
SLV 11	-614	-2237	8	0.023	113.2	0.9	0.36375	5.79734	No
SLV 12	-614	-2237	8	0.023	113.2	0.9	0.36375	5.79734	No
SLV 15	-550	-1787	19	0.01	106.9	0.897	0.16562	2.39674	No
SLV 16	-550	-1787	19	0.01	106.9	0.897	0.16562	2.39674	No
SLV 1	-732	-3176	-20	0.011	124.8	0.905	0.18203	2.39674	No
SLV 2	-732	-3176	-20	0.011	124.8	0.905	0.18203	2.39674	No
SLV 7	-668	-2647	-3	0.028	118.5	0.902	0.4483	5.79734	No
SLV 8	-668	-2647	-3	0.028	118.5	0.902	0.4483	5.79734	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	10.058	SLU 81	Si
V_SLU	19.462	SLU 43	Si
PF_SLV	4.094	SLV 9	Si
V_SLV	1.744	SLV 5	Si
PFFP_SLV	1.935	SLV 3	Si
R_SLV	0.059	SLV 5	No

Maschio 25

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.sx	a.s.dx
30.718	9.502	30.718	5.634	L2	L3	3.869	0.18	3.85	3.85	3.85			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _k	f _{vk0}	f _{medio}	$\tau 0$	f _{v0}	μ	ϕ	f _{v,lim}	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma 0$	Mu	c.s.	Verifica
SLU 82	1.67	-20723	6378.73	29759	25440.15	3.988	Si
SLU 82	3.77	-19106	5212.5	27438	24509.03	4.702	Si
SLU 21	1.67	-16461	5157.08	23639	22600.75	4.382	Si
SLU 21	3.77	-15394	4166.28	22106	21695.49	5.207	Si
SLU 42	1.67	-18905	6102.85	27149	24380.79	3.995	Si
SLU 42	3.77	-18004	4955.13	25855	23771.91	4.797	Si
SLU 39	1.67	-18905	6102.85	27149	24380.79	3.995	Si
SLU 39	3.77	-18004	4955.13	25855	23771.91	4.797	Si
SLU 83	1.67	-20723	6378.73	29759	25440.15	3.988	Si
SLU 83	3.77	-19106	5212.5	27438	24509.03	4.702	Si
SLU 20	1.67	-16461	5157.08	23639	22600.75	4.382	Si
SLU 20	3.77	-15394	4166.28	22106	21695.49	5.207	Si
SLU 84	1.67	-20723	6378.73	29759	25440.15	3.988	Si
SLU 84	3.77	-19106	5212.5	27438	24509.03	4.702	Si
SLU 81	1.67	-20723	6378.73	29759	25440.15	3.988	Si
SLU 81	3.77	-19106	5212.5	27438	24509.03	4.702	Si
SLU 40	1.67	-18905	6102.85	27149	24380.79	3.995	Si
SLU 40	3.77	-18004	4955.13	25855	23771.91	4.797	Si
SLU 41	1.67	-18905	6102.85	27149	24380.79	3.995	Si
SLU 41	3.77	-18004	4955.13	25855	23771.91	4.797	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma 0$	Mu	c.s.	Verifica
SLV 14	1.67	-10340	3946.53	14849	17570.18	4.452	Si
SLV 14	3.77	-8729	1791.89	12535	15152.26	8.456	Si
SLV 1	1.67	-11300	4861.91	16228	18955.09	3.899	Si
SLV 1	3.77	-9155	2730.15	13147	15803.12	5.788	Si
SLV 8	1.67	-12052	-1968.04	17307	20009.61	10.167	Si
SLV 8	3.77	-9909	3290.78	14230	16935	5.146	Si
SLV 10	1.67	-10091	7772.07	14491	17203.47	2.214	Si
SLV 10	3.77	-8392	1641.58	12051	14631.18	8.913	Si
SLV 2	1.67	-11300	4861.91	16228	18955.09	3.899	Si
SLV 2	3.77	-9155	2730.15	13147	15803.12	5.788	Si
SLV 9	1.67	-10091	7772.07	14491	17203.47	2.214	Si
SLV 9	3.77	-8392	1641.58	12051	14631.18	8.913	Si
SLV 13	1.67	-10340	3946.53	14849	17570.18	4.452	Si
SLV 13	3.77	-8729	1791.89	12535	15152.26	8.456	Si
SLV 6	1.67	-10379	8046.68	14904	17626.61	2.191	Si
SLV 6	3.77	-8519	1923.06	12235	14829.26	7.711	Si
SLV 5	1.67	-10379	8046.68	14904	17626.61	2.191	Si
SLV 5	3.77	-8519	1923.06	12235	14829.26	7.711	Si
SLV 7	1.67	-12052	-1968.04	17307	20009.61	10.167	Si
SLV 7	3.77	-9909	3290.78	14230	16935	5.146	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma 0$	σN	l'	f _{vd}	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLU 81	1.67	-20723	-1211	6378.73		29759	3.8686	9523	6632			5.47	Si
SLU 81	3.77	-19106	-1194	5212.5		27438	3.8686	9214	6416			5.37	Si
SLU 20	1.67	-16461	-991	5157.08		23639	3.8686	8707	6063			6.12	Si
SLU 20	3.77	-15394	-976	4166.28		22106	3.8686	8503	5921			6.06	Si
SLU 40	1.67	-18905	-1187	6102.85		27149	3.8686	9175	6389			5.38	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 40	3.77	-18004	-1170	4955.13		25855	3.8686	9003	6269			5.36	Si
SLU 41	1.67	-18905	-1187	6102.85		27149	3.8686	9175	6389			5.38	Si
SLU 41	3.77	-18004	-1170	4955.13		25855	3.8686	9003	6269			5.36	Si
SLU 18	1.67	-16461	-991	5157.08		23639	3.8686	8707	6063			6.12	Si
SLU 18	3.77	-15394	-976	4166.28		22106	3.8686	8503	5921			6.06	Si
SLU 39	1.67	-18905	-1187	6102.85		27149	3.8686	9175	6389			5.38	Si
SLU 39	3.77	-18004	-1170	4955.13		25855	3.8686	9003	6269			5.36	Si
SLU 83	1.67	-20723	-1211	6378.73		29759	3.8686	9523	6632			5.47	Si
SLU 83	3.77	-19106	-1194	5212.5		27438	3.8686	9214	6416			5.37	Si
SLU 42	1.67	-18905	-1187	6102.85		27149	3.8686	9175	6389			5.38	Si
SLU 42	3.77	-18004	-1170	4955.13		25855	3.8686	9003	6269			5.36	Si
SLU 82	1.67	-20723	-1211	6378.73		29759	3.8686	9523	6632			5.47	Si
SLU 82	3.77	-19106	-1194	5212.5		27438	3.8686	9214	6416			5.37	Si
SLU 84	1.67	-20723	-1211	6378.73		29759	3.8686	9523	6632			5.47	Si
SLU 84	3.77	-19106	-1194	5212.5		27438	3.8686	9214	6416			5.37	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 4	1.67	-11802	-2245	1857.5		16949	3.8686	11723	8163			3.64	Si
SLV 4	3.77	-9572	-891	3140.47		13746	3.8686	11082	7717			8.66	Si
SLV 12	1.67	-11764	-4613	-2242.66		16893	3.8686	11712	8156			1.77	Si
SLV 12	3.77	-9781	-2869	3009.3		14047	3.8686	11143	7759			2.7	Si
SLV 10	1.67	-10091	3898	7772.07		16052	3.4922	11544	7256			1.86	Si
SLV 10	3.77	-8392	1715	1641.58		12051	3.8686	10744	7481			4.36	Si
SLV 7	1.67	-12052	-4895	-1968.04		17307	3.8686	11795	8213			1.68	Si
SLV 7	3.77	-9909	-2697	3290.78		14230	3.8686	11179	7785			2.89	Si
SLV 11	1.67	-11764	-4613	-2242.66		16893	3.8686	11712	8156			1.77	Si
SLV 11	3.77	-9781	-2869	3009.3		14047	3.8686	11143	7759			2.7	Si
SLV 9	1.67	-10091	3898	7772.07		16052	3.4922	11544	7256			1.86	Si
SLV 9	3.77	-8392	1715	1641.58		12051	3.8686	10744	7481			4.36	Si
SLV 6	1.67	-10379	3616	8046.68		16583	3.477	11650	7291			2.02	Si
SLV 6	3.77	-8519	1887	1923.06		12235	3.8686	10780	7507			3.98	Si
SLV 5	1.67	-10379	3616	8046.68		16583	3.477	11650	7291			2.02	Si
SLV 5	3.77	-8519	1887	1923.06		12235	3.8686	10780	7507			3.98	Si
SLV 8	1.67	-12052	-4895	-1968.04		17307	3.8686	11795	8213			1.68	Si
SLV 8	3.77	-9909	-2697	3290.78		14230	3.8686	11179	7785			2.89	Si
SLV 3	1.67	-11802	-2245	1857.5		16949	3.8686	11723	8163			3.64	Si
SLV 3	3.77	-9572	-891	3140.47		13746	3.8686	11082	7717			8.66	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.595 Wa 0.03 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 10	143750	0.48	12106	-8430	401.59	683.55	1.7	Si
SLV 9	143750	0.48	12106	-8430	401.59	683.55	1.7	Si
SLV 6	143750	0.48	12216	-8507	401.59	689.05	1.72	Si
SLV 5	143750	0.48	12216	-8507	401.59	689.05	1.72	Si
SLV 14	143750	0.48	12693	-8839	401.59	712.84	1.78	Si
SLV 13	143750	0.48	12693	-8839	401.59	712.84	1.78	Si
SLV 1	143750	0.48	13058	-9093	401.59	730.9	1.82	Si
SLV 2	143750	0.48	13058	-9093	401.59	730.9	1.82	Si
SLV 15	143750	0.48	13305	-9265	401.59	743.05	1.85	Si
SLV 16	143750	0.48	13305	-9265	401.59	743.05	1.85	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.595 Wa = 0.03 Ta = 0.1375

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 9	-7469	-10091	209	0.008	1147.4	0.916	0.12667	5.79734	No
SLV 10	-7469	-10091	209	0.008	1147.4	0.916	0.12667	5.79734	No
SLV 8	-7516	-12052	-209	0.008	1152.1	0.916	0.1278	5.79734	No
SLV 7	-7516	-12052	-209	0.008	1152.1	0.916	0.1278	5.79734	No
SLV 13	-7452	-10340	220	0.007	1145.7	0.915	0.1084	2.39674	No
SLV 14	-7452	-10340	220	0.007	1145.7	0.915	0.1084	2.39674	No
SLV 4	-7532	-11802	-220	0.007	1153.7	0.916	0.11047	2.39674	No
SLV 3	-7532	-11802	-220	0.007	1153.7	0.916	0.11047	2.39674	No
SLV 5	-7490	-10379	105	0.018	1149.5	0.916	0.29319	5.79734	No
SLV 6	-7490	-10379	105	0.018	1149.5	0.916	0.29319	5.79734	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	3.988	SLU 81	Si
V_SLU	5.358	SLU 39	Si
PF_SLV	2.191	SLV 5	Si
V_SLV	1.678	SLV 7	Si
PFFP_SLV	1.702	SLV 9	Si
R_SLV	0.022	SLV 9	No

Maschio 26

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s,sx	a.s,dx
26.639	9.502	35.424	9.502	L2	L3	8.785	0.3	3.85	3.85	3.85			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

Sismicad 12.19 - Licenza assegnata a Sidel ingegneria Srl - Via Isonzo, 13 - Villanova di Castenaso (BO)



fb	fk	fvk0	fmedio	τ_0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 50	1.67	-26723	-3158.16	10139	102768.26	32.541	Si
SLU 50	5.52	-336	-26.03	128	1474.57	56.648	Si
SLU 48	1.67	-26723	-3158.16	10139	102768.26	32.541	Si
SLU 48	5.52	-336	-26.03	128	1474.57	56.648	Si
SLU 51	1.67	-26723	-3158.16	10139	102768.26	32.541	Si
SLU 51	5.52	-336	-26.03	128	1474.57	56.648	Si
SLU 46	1.67	-26723	-3158.16	10139	102768.26	32.541	Si
SLU 46	5.52	-336	-26.03	128	1474.57	56.648	Si
SLU 44	1.67	-26723	-3158.16	10139	102768.26	32.541	Si
SLU 44	5.52	-336	-26.03	128	1474.57	56.648	Si
SLU 47	1.67	-26723	-3158.16	10139	102768.26	32.541	Si
SLU 47	5.52	-336	-26.03	128	1474.57	56.648	Si
SLU 65	1.67	-28529	-3205.38	10825	108660.92	33.9	Si
SLU 65	5.52	-546	0.02	207	2392.36	1000	Si
SLU 43	1.67	-26723	-3158.16	10139	102768.26	32.541	Si
SLU 43	5.52	-336	-26.03	128	1474.57	56.648	Si
SLU 45	1.67	-26723	-3158.16	10139	102768.26	32.541	Si
SLU 45	5.52	-336	-26.03	128	1474.57	56.648	Si
SLU 49	1.67	-26723	-3158.16	10139	102768.26	32.541	Si
SLU 49	5.52	-336	-26.03	128	1474.57	56.648	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 14	1.67	-28053	-20406.18	10644	112490.01	5.513	Si
SLV 14	5.52	-458	-611.08	174	2008.81	3.287	Si
SLV 15	1.67	-32068	-28749.63	12168	126830.51	4.412	Si
SLV 15	5.52	-545	-555.45	207	2389.85	4.303	Si
SLV 2	1.67	-13005	24228.41	4934	54816.21	2.262	Si
SLV 2	5.52	-466	586.5	177	2042.24	3.482	Si
SLV 5	1.67	-13589	18340.33	5156	57168.89	3.117	Si
SLV 5	5.52	-361	102.45	137	1585.75	15.478	Si
SLV 4	1.67	-17019	15884.96	6458	70804.7	4.457	Si
SLV 4	5.52	-553	642.12	210	2423.26	3.774	Si
SLV 3	1.67	-17019	15884.96	6458	70804.7	4.457	Si
SLV 3	5.52	-553	642.12	210	2423.26	3.774	Si
SLV 16	1.67	-32068	-28749.63	12168	126830.51	4.412	Si
SLV 16	5.52	-545	-555.45	207	2389.85	4.303	Si
SLV 1	1.67	-13005	24228.41	4934	54816.21	2.262	Si
SLV 1	5.52	-466	586.5	177	2042.24	3.482	Si
SLV 6	1.67	-13589	18340.33	5156	57168.89	3.117	Si
SLV 6	5.52	-361	102.45	137	1585.75	15.478	Si
SLV 13	1.67	-28053	-20406.18	10644	112490.01	5.513	Si
SLV 13	5.52	-458	-611.08	174	2008.81	3.287	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 1	1.67	-21032	2	-2441.81		7980	8.785	6620	17446			1000	Si
SLU 1	5.52	-314	0	-13.15		119	8.785	5571	14684			1000	Si
SLU 53	1.67	-30180	0	-2476.75		11451	8.785	7082	18666			1000	Si
SLU 53	5.52	-796	-1	48.28		302	8.785	5596	14748			1000	Si
SLU 54	1.67	-30180	0	-2476.75		11451	8.785	7082	18666			1000	Si
SLU 54	5.52	-796	-1	48.28		302	8.785	5596	14748			1000	Si
SLU 61	1.67	-31662	-1	-2184.72		12014	8.785	7157	18863			1000	Si
SLU 61	5.52	-993	-2	80.13		377	8.785	5606	14774			1000	Si
SLU 58	1.67	-30180	0	-2476.75		11451	8.785	7082	18666			1000	Si
SLU 58	5.52	-796	-1	48.28		302	8.785	5596	14748			1000	Si
SLU 56	1.67	-30180	0	-2476.75		11451	8.785	7082	18666			1000	Si
SLU 56	5.52	-796	-1	48.28		302	8.785	5596	14748			1000	Si
SLU 57	1.67	-30180	0	-2476.75		11451	8.785	7082	18666			1000	Si
SLU 57	5.52	-796	-1	48.28		302	8.785	5596	14748			1000	Si
SLU 55	1.67	-30180	0	-2476.75		11451	8.785	7082	18666			1000	Si
SLU 55	5.52	-796	-1	48.28		302	8.785	5596	14748			1000	Si
SLU 60	1.67	-31662	-1	-2184.72		12014	8.785	7157	18863			1000	Si
SLU 60	5.52	-993	-2	80.13		377	8.785	5606	14774			1000	Si
SLU 59	1.67	-30180	0	-2476.75		11451	8.785	7082	18666			1000	Si
SLU 59	5.52	-796	-1	48.28		302	8.785	5596	14748			1000	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 9	1.67	-18103	2514	4949.95		6869	8.785	9707	25583			10.18	Si
SLV 9	5.52	-359	622	-256.82		136	8.785	8361	22034			35.42	Si
SLV 14	1.67	-28053	7572	-20406.18		10644	8.785	10462	27573			3.64	Si
SLV 14	5.52	-458	1133	-611.08		174	8.785	8368	22054			19.46	Si
SLV 15	1.67	-32068	7413	-28749.63		12168	8.785	10767	28376			3.83	Si
SLV 15	5.52	-545	947	-555.45		207	8.785	8375	22071			23.31	Si
SLV 16	1.67	-32068	7413	-28749.63		12168	8.785	10767	28376			3.83	Si
SLV 16	5.52	-545	947	-555.45		207	8.785	8375	22071			23.31	Si
SLV 4	1.67	-17019	-7569	15884.96		6458	8.785	9625	25366			3.35	Si
SLV 4	5.52	-553	-1134	642.12		210	8.785	8375	22073			19.46	Si
SLV 1	1.67	-13005	-7410	24228.41		5713	7.5883	9476	21572			2.91	Si
SLV 1	5.52	-466	-948	586.5		177	8.785	8369	22056			23.26	Si
SLV 13	1.67	-28053	7572	-20406.18		10644	8.785	10462	27573			3.64	Si
SLV 13	5.52	-458	1133	-611.08		174	8.785	8368	22054			19.46	Si
SLV 2	1.67	-13005	-7410	24228.41		5713	7.5883	9476	21572			2.91	Si
SLV 2	5.52	-466	-948	586.5		177	8.785	8369	22056			23.26	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 10	1.67	-18103	2514	4949.95		6869	8.785	9707	25583			10.18	Si
SLV 10	5.52	-359	622	-256.82		136	8.785	8361	22034			35.42	Si
SLV 3	1.67	-17019	-7569	15884.96		6458	8.785	9625	25366			3.35	Si
SLV 3	5.52	-553	-1134	642.12		210	8.785	8375	22073			19.46	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.595 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 13	143750	0.48	0	-8934	1477.98	0	0	No, $e > t/2$
SLV 16	143750	0.48	0	-8471	1477.98	0	0	No, $e > t/2$
SLV 15	143750	0.48	0	-8471	1477.98	0	0	No, $e > t/2$
SLV 14	143750	0.48	0	-8934	1477.98	0	0	No, $e > t/2$
SLV 12	143750	0.48	3885	-10240	1477.98	1487.19	1.01	Si
SLV 11	143750	0.48	3885	-10240	1477.98	1487.19	1.01	Si
SLV 9	143750	0.48	4472	-11786	1477.98	1703.18	1.15	Si
SLV 10	143750	0.48	4472	-11786	1477.98	1703.18	1.15	Si
SLV 8	143750	0.48	4637	-12221	1477.98	1763.54	1.19	Si
SLV 7	143750	0.48	4637	-12221	1477.98	1763.54	1.19	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.595 Wa = 0.05 Ta = 0.0825

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 3	-553	-17019	-136	0.062	1867.9	0.974	0.91956	10.57293	No
SLV 4	-553	-17019	-136	0.062	1867.9	0.974	0.91956	10.57293	No
SLV 13	-458	-28053	136	0.062	1866	0.978	0.91975	10.57293	No
SLV 14	-458	-28053	136	0.062	1866	0.978	0.91975	10.57293	No
SLV 1	-466	-13005	-97	0.066	1866.2	0.977	0.97987	10.57293	No
SLV 2	-466	-13005	-97	0.066	1866.2	0.977	0.97987	10.57293	No
SLV 16	-545	-32068	97	0.066	1867.7	0.974	0.98051	10.57293	No
SLV 15	-545	-32068	97	0.066	1867.7	0.974	0.98051	10.57293	No
SLV 7	-651	-26969	-100	0.065	1870.1	0.97	0.97492	4.97545	No
SLV 8	-651	-26969	-100	0.065	1870.1	0.97	0.97492	4.97545	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	32.541	SLU 43	Si
V_SLU	1000	SLU 1	Si
PF_SLV	2.262	SLV 1	Si
V_SLV	2.911	SLV 1	Si
PFFP_SLV	0	SLV 13	No
R_SLV	0.087	SLV 3	No

Maschio 27

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
30.718	4.507	35.424	4.507	L2	L3	4.706	0.18	3.85	3.85	3.85			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ_0	fvt0	μ	ϕ	fvl,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 62	1.67	-12331	-554.93	14557	23831.26	42.944	Si
SLU 62	5.52	-1092	-1442.07	1289	2528.61	1.753	Si
SLU 61	1.67	-12331	-554.93	14557	23831.26	42.944	Si
SLU 61	5.52	-1092	-1442.07	1289	2528.61	1.753	Si
SLU 60	1.67	-12331	-554.93	14557	23831.26	42.944	Si
SLU 60	5.52	-1092	-1442.07	1289	2528.61	1.753	Si
SLU 19	1.67	-10625	-751.39	12542	21151.01	28.149	Si
SLU 19	5.52	-1065	-1407.2	1258	2468.26	1.754	Si
SLU 84	1.67	-13325	-789.08	15730	25300.31	32.063	Si
SLU 84	5.52	-1304	-1713.03	1540	3011.13	1.758	Si
SLU 20	1.67	-10625	-751.39	12542	21151.01	28.149	Si
SLU 20	5.52	-1065	-1407.2	1258	2468.26	1.754	Si
SLU 18	1.67	-10625	-751.39	12542	21151.01	28.149	Si
SLU 18	5.52	-1065	-1407.2	1258	2468.26	1.754	Si
SLU 63	1.67	-12331	-554.93	14557	23831.26	42.944	Si
SLU 63	5.52	-1092	-1442.07	1289	2528.61	1.753	Si
SLU 21	1.67	-10625	-751.39	12542	21151.01	28.149	Si
SLU 21	5.52	-1065	-1407.2	1258	2468.26	1.754	Si
SLU 82	1.67	-13325	-789.08	15730	25300.31	32.063	Si
SLU 82	5.52	-1304	-1713.03	1540	3011.13	1.758	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 8	1.67	-8039	-1098.85	9490	17447.59	15.878	Si
SLV 8	5.52	-557	-662.48	658	1304.12	1.969	Si
SLV 7	1.67	-8039	-1098.85	9490	17447.59	15.878	Si
SLV 7	5.52	-557	-662.48	658	1304.12	1.969	Si
SLV 14	1.67	-7904	1556.25	9331	17178.61	11.038	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 14	5.52	-488	-1043.42	576	1143.47	1.096	Si
SLV 11	1.67	-8096	-369.5	9557	17560.04	47.523	Si
SLV 11	5.52	-528	-881.87	623	1235.38	1.401	Si
SLV 12	1.67	-8096	-369.5	9557	17560.04	47.523	Si
SLV 12	5.52	-528	-881.87	623	1235.38	1.401	Si
SLV 16	1.67	-8023	1060.17	9471	17415.49	16.427	Si
SLV 16	5.52	-491	-1086.99	579	1148.85	1.057	Si
SLV 10	1.67	-7699	1284.12	9089	16769.25	13.059	Si
SLV 10	5.52	-520	-736.64	614	1217.45	1.653	Si
SLV 13	1.67	-7904	1556.25	9331	17178.61	11.038	Si
SLV 13	5.52	-488	-1043.42	576	1143.47	1.096	Si
SLV 15	1.67	-8023	1060.17	9471	17415.49	16.427	Si
SLV 15	5.52	-491	-1086.99	579	1148.85	1.057	Si
SLV 9	1.67	-7699	1284.12	9089	16769.25	13.059	Si
SLV 9	5.52	-520	-736.64	614	1217.45	1.653	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 84	1.67	-13325	2349	-789.08		15730	4.7061	7653	6483			2.76	Si
SLU 84	5.52	-1304	1420	-1713.03		2323	3.1191	5865	3293			2.32	Si
SLU 82	1.67	-13325	2349	-789.08		15730	4.7061	7653	6483			2.76	Si
SLU 82	5.52	-1304	1420	-1713.03		2323	3.1191	5865	3293			2.32	Si
SLU 39	1.67	-11618	2229	-985.54		13716	4.7061	7384	6255			2.81	Si
SLU 39	5.52	-1278	1377	-1678.17		2276	3.1193	5859	3290			2.39	Si
SLU 83	1.67	-13325	2349	-789.08		15730	4.7061	7653	6483			2.76	Si
SLU 83	5.52	-1304	1420	-1713.03		2323	3.1191	5865	3293			2.32	Si
SLU 81	1.67	-13325	2349	-789.08		15730	4.7061	7653	6483			2.76	Si
SLU 81	5.52	-1304	1420	-1713.03		2323	3.1191	5865	3293			2.32	Si
SLU 41	1.67	-11618	2229	-985.54		13716	4.7061	7384	6255			2.81	Si
SLU 41	5.52	-1278	1377	-1678.17		2276	3.1193	5859	3290			2.39	Si
SLU 62	1.67	-12331	1987	-554.93		14557	4.7061	7497	6350			3.2	Si
SLU 62	5.52	-1092	1202	-1442.07		1959	3.097	5817	3243			2.7	Si
SLU 63	1.67	-12331	1987	-554.93		14557	4.7061	7497	6350			3.2	Si
SLU 63	5.52	-1092	1202	-1442.07		1959	3.097	5817	3243			2.7	Si
SLU 42	1.67	-11618	2229	-985.54		13716	4.7061	7384	6255			2.81	Si
SLU 42	5.52	-1278	1377	-1678.17		2276	3.1193	5859	3290			2.39	Si
SLU 40	1.67	-11618	2229	-985.54		13716	4.7061	7384	6255			2.81	Si
SLU 40	5.52	-1278	1377	-1678.17		2276	3.1193	5859	3290			2.39	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 4	1.67	-7834	-1979	-1370.98		9248	4.7061	10183	8626			4.36	Si
SLV 4	5.52	-589	-68	-355.7		695	4.7061	8472	7177			105.59	Si
SLV 12	1.67	-8096	2518	-369.5		9557	4.7061	10245	8678			3.45	Si
SLV 12	5.52	-528	995	-881.87		1433	2.0457	8620	3174			3.19	Si
SLV 2	1.67	-7715	-2231	-874.9		9108	4.7061	10155	8602			3.86	Si
SLV 2	5.52	-587	-169	-312.14		693	4.7061	8472	7177			42.36	Si
SLV 16	1.67	-8023	4488	1060.17		9471	4.7061	10228	8664			1.93	Si
SLV 16	5.52	-491	1386	-1086.99		6619	0.4118	9657	716			0.52	No, Vu<V
SLV 11	1.67	-8096	2518	-369.5		9557	4.7061	10245	8678			3.45	Si
SLV 11	5.52	-528	995	-881.87		1433	2.0457	8620	3174			3.19	Si
SLV 13	1.67	-7904	4237	1556.25		9331	4.7061	10199	8640			2.04	Si
SLV 13	5.52	-488	1284	-1043.42		4186	0.648	9171	1070			0.83	No, Vu<V
SLV 14	1.67	-7904	4237	1556.25		9331	4.7061	10199	8640			2.04	Si
SLV 14	5.52	-488	1284	-1043.42		4186	0.648	9171	1070			0.83	No, Vu<V
SLV 1	1.67	-7715	-2231	-874.9		9108	4.7061	10155	8602			3.86	Si
SLV 1	5.52	-587	-169	-312.14		693	4.7061	8472	7177			42.36	Si
SLV 3	1.67	-7834	-1979	-1370.98		9248	4.7061	10183	8626			4.36	Si
SLV 3	5.52	-589	-68	-355.7		695	4.7061	8472	7177			105.59	Si
SLV 15	1.67	-8023	4488	1060.17		9471	4.7061	10228	8664			1.93	Si
SLV 15	5.52	-491	1386	-1086.99		6619	0.4118	9657	716			0.52	No, Vu<V

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.595 Wa 0.03 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 6	143750	0.48	0	-5393	488.53	0	0	No, e>t/2
SLV 2	143750	0.48	0	-5420	488.53	0	0	No, e>t/2
SLV 5	143750	0.48	0	-5393	488.53	0	0	No, e>t/2
SLV 1	143750	0.48	0	-5420	488.53	0	0	No, e>t/2
SLV 9	143750	0.48	6514	-5518	488.53	470.16	0.96	No, M>Mu
SLV 10	143750	0.48	6514	-5518	488.53	470.16	0.96	No, M>Mu
SLV 3	143750	0.48	6574	-5569	488.53	474.25	0.97	No, M>Mu
SLV 4	143750	0.48	6574	-5569	488.53	474.25	0.97	No, M>Mu
SLV 13	143750	0.48	6891	-5837	488.53	495.74	1.01	Si
SLV 14	143750	0.48	6891	-5837	488.53	495.74	1.01	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.595 Wa = 0.03 Ta = 0.1375

Comb.	N top	N base	V orto	α_0	M*	e*	α_0^*	aLim	Verifica
SLV 7	-557	-8039	9	0.04	614	0.937	0.62639	5.79734	No
SLV 8	-557	-8039	9	0.04	614	0.937	0.62639	5.79734	No
SLV 5	-550	-7643	-9	0.04	613.7	0.938	0.62644	5.79734	No
SLV 6	-550	-7643	-9	0.04	613.7	0.938	0.62644	5.79734	No
SLV 12	-528	-8096	9	0.041	612.6	0.939	0.62705	5.79734	No
SLV 11	-528	-8096	9	0.041	612.6	0.939	0.62705	5.79734	No
SLV 10	-520	-7699	-9	0.041	612.3	0.94	0.62736	5.79734	No
SLV 9	-520	-7699	-9	0.041	612.3	0.94	0.62736	5.79734	No
SLV 1	-587	-7715	-3	0.042	615.5	0.935	0.6537	2.39674	No
SLV 2	-587	-7715	-3	0.042	615.5	0.935	0.6537	2.39674	No



Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	1.753	SLU 60	Si
V_SLU	2.319	SLU 81	Si
PF_SLV	1.057	SLV 15	Si
V_SLV	0.517	SLV 15	No
PFFP_SLV	0	SLV 1	No
R_SLV	0.108	SLV 7	No

Maschio 28

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
35.424	1.847	35.424	-0.169	L2	L3	2.016	0.3	3.85	3.85	3.85			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	τ0	fν0	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 81	2.67	-9552	-1166.97	15797	7760.12	6.65	Si
SLU 81	4.57	-7524	-1736.29	12443	6424.94	3.7	Si
SLU 40	2.67	-8459	-1069.06	13990	7061.47	6.605	Si
SLU 40	4.57	-7075	-1642.75	11701	6106.4	3.717	Si
SLU 41	2.67	-8459	-1069.06	13990	7061.47	6.605	Si
SLU 41	4.57	-7075	-1642.75	11701	6106.4	3.717	Si
SLU 84	2.67	-9552	-1166.97	15797	7760.12	6.65	Si
SLU 84	4.57	-7524	-1736.29	12443	6424.94	3.7	Si
SLU 82	2.67	-9552	-1166.97	15797	7760.12	6.65	Si
SLU 82	4.57	-7524	-1736.29	12443	6424.94	3.7	Si
SLU 63	2.67	-8654	-1031.71	14312	7189.67	6.969	Si
SLU 63	4.57	-6533	-1498.6	10804	5711.09	3.811	Si
SLU 62	2.67	-8654	-1031.71	14312	7189.67	6.969	Si
SLU 62	4.57	-6533	-1498.6	10804	5711.09	3.811	Si
SLU 83	2.67	-9552	-1166.97	15797	7760.12	6.65	Si
SLU 83	4.57	-7524	-1736.29	12443	6424.94	3.7	Si
SLU 42	2.67	-8459	-1069.06	13990	7061.47	6.605	Si
SLU 42	4.57	-7075	-1642.75	11701	6106.4	3.717	Si
SLU 39	2.67	-8459	-1069.06	13990	7061.47	6.605	Si
SLU 39	4.57	-7075	-1642.75	11701	6106.4	3.717	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γM = 2

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLV 8	2.67	-5356	-1428.01	8857	5006.2	3.506	Si
SLV 8	4.57	-2937	-158.12	4857	2842.38	17.977	Si
SLV 13	2.67	-6490	-478.99	10733	5966.64	12.457	Si
SLV 13	4.57	-4179	-1323.19	6911	3973.63	3.003	Si
SLV 9	2.67	-5653	207.65	9348	5260.95	25.335	Si
SLV 9	4.57	-4271	-1473.26	7064	4055.84	2.753	Si
SLV 10	2.67	-5653	207.65	9348	5260.95	25.335	Si
SLV 10	4.57	-4271	-1473.26	7064	4055.84	2.753	Si
SLV 7	2.67	-5356	-1428.01	8857	5006.2	3.506	Si
SLV 7	4.57	-2937	-158.12	4857	2842.38	17.977	Si
SLV 6	2.67	-5032	282.92	8321	4725.57	16.703	Si
SLV 6	4.57	-4024	-1268.71	6655	3834.71	3.023	Si
SLV 5	2.67	-5032	282.92	8321	4725.57	16.703	Si
SLV 5	4.57	-4024	-1268.71	6655	3834.71	3.023	Si
SLV 12	2.67	-5977	-1503.28	9884	5536.09	3.683	Si
SLV 12	4.57	-3184	-362.66	5266	3070.84	8.468	Si
SLV 14	2.67	-6490	-478.99	10733	5966.64	12.457	Si
SLV 14	4.57	-4179	-1323.19	6911	3973.63	3.003	Si
SLV 11	2.67	-5977	-1503.28	9884	5536.09	3.683	Si
SLV 11	4.57	-3184	-362.66	5266	3070.84	8.468	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, γM = 3

Comb.	Quota	N	V par	M	σ0	σN	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 84	2.67	-9552	704	-1166.97		15797	2.0156	7662	4633			6.59	Si
SLU 84	4.57	-7524	703	-1736.29		12443	2.0156	7215	4363			6.2	Si
SLU 81	2.67	-9552	704	-1166.97		15797	2.0156	7662	4633			6.59	Si
SLU 81	4.57	-7524	703	-1736.29		12443	2.0156	7215	4363			6.2	Si
SLU 19	2.67	-7562	594	-933.8		12505	2.0156	7223	4368			7.35	Si
SLU 19	4.57	-6084	594	-1405.06		10061	2.0156	6897	4171			7.02	Si
SLU 42	2.67	-8459	714	-1069.06		13990	2.0156	7421	4487			6.28	Si
SLU 42	4.57	-7075	714	-1642.75		11701	2.0156	7116	4303			6.03	Si
SLU 18	2.67	-7562	594	-933.8		12505	2.0156	7223	4368			7.35	Si
SLU 18	4.57	-6084	594	-1405.06		10061	2.0156	6897	4171			7.02	Si
SLU 82	2.67	-9552	704	-1166.97		15797	2.0156	7662	4633			6.59	Si
SLU 82	4.57	-7524	703	-1736.29		12443	2.0156	7215	4363			6.2	Si
SLU 40	2.67	-8459	714	-1069.06		13990	2.0156	7421	4487			6.28	Si
SLU 40	4.57	-7075	714	-1642.75		11701	2.0156	7116	4303			6.03	Si
SLU 83	2.67	-9552	704	-1166.97		15797	2.0156	7662	4633			6.59	Si
SLU 83	4.57	-7524	703	-1736.29		12443	2.0156	7215	4363			6.2	Si
SLU 41	2.67	-8459	714	-1069.06		13990	2.0156	7421	4487			6.28	Si



Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 41	4.57	-7075	714	-1642.75		11701	2.0156	7116	4303			6.03	Si
SLU 39	2.67	-8459	714	-1069.06		13990	2.0156	7421	4487			6.28	Si
SLU 39	4.57	-7075	714	-1642.75		11701	2.0156	7116	4303			6.03	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 5	2.67	-5032	2097	282.92		8321	2.0156	9997	6045			2.88	Si
SLV 5	4.57	-4024	1284	-1268.71		6655	2.0156	9664	5844			4.55	Si
SLV 7	2.67	-5356	-1115	-1428.01		8857	2.0156	10105	6110			5.48	Si
SLV 7	4.57	-2937	-666	-158.12		4857	2.0156	9305	5627			8.44	Si
SLV 2	2.67	-4420	1571	-228.09		7310	2.0156	9795	5923			3.77	Si
SLV 2	4.57	-3355	773	-641.36		5549	2.0156	9443	5710			7.38	Si
SLV 12	2.67	-5977	-1628	-1503.28		9884	2.0156	10310	6234			3.83	Si
SLV 12	4.57	-3184	-814	-362.66		5266	2.0156	9387	5676			6.97	Si
SLV 6	2.67	-5032	2097	282.92		8321	2.0156	9997	6045			2.88	Si
SLV 6	4.57	-4024	1284	-1268.71		6655	2.0156	9664	5844			4.55	Si
SLV 1	2.67	-4420	1571	-228.09		7310	2.0156	9795	5923			3.77	Si
SLV 1	4.57	-3355	773	-641.36		5549	2.0156	9443	5710			7.38	Si
SLV 10	2.67	-5653	1585	207.65		9348	2.0156	10203	6170			3.89	Si
SLV 10	4.57	-4271	1136	-1473.26		7159	1.9887	9765	5826			5.13	Si
SLV 9	2.67	-5653	1585	207.65		9348	2.0156	10203	6170			3.89	Si
SLV 9	4.57	-4271	1136	-1473.26		7159	1.9887	9765	5826			5.13	Si
SLV 8	2.67	-5356	-1115	-1428.01		8857	2.0156	10105	6110			5.48	Si
SLV 8	4.57	-2937	-666	-158.12		4857	2.0156	9305	5627			8.44	Si
SLV 11	2.67	-5977	-1628	-1503.28		9884	2.0156	10310	6234			3.83	Si
SLV 11	4.57	-3184	-814	-362.66		5266	2.0156	9387	5676			6.97	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.595 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 3	143750	0.48	6654	-4024	331.9	570.7	1.72	Si
SLV 4	143750	0.48	6654	-4024	331.9	570.7	1.72	Si
SLV 8	143750	0.48	6999	-4232	331.9	598.45	1.8	Si
SLV 7	143750	0.48	6999	-4232	331.9	598.45	1.8	Si
SLV 1	143750	0.48	7004	-4236	331.9	598.91	1.8	Si
SLV 2	143750	0.48	7004	-4236	331.9	598.91	1.8	Si
SLV 12	143750	0.48	7644	-4622	331.9	649.98	1.96	Si
SLV 11	143750	0.48	7644	-4622	331.9	649.98	1.96	Si
SLV 6	143750	0.48	8166	-4938	331.9	691.19	2.08	Si
SLV 5	143750	0.48	8166	-4938	331.9	691.19	2.08	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 3.595 Wa = 0.05 Ta = 0.0825

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 8	-2054	-5295	-256	0	565.8	0.889	0	4.97545	No
SLV 7	-2054	-5295	-256	0	565.8	0.889	0	4.97545	No
SLV 6	-2063	-6362	244	0	566.6	0.889	0	4.97545	No
SLV 10	-2191	-6893	256	0	578.2	0.889	0	4.97545	No
SLV 9	-2191	-6893	256	0	578.2	0.889	0	4.97545	No
SLV 5	-2063	-6362	244	0	566.6	0.889	0	4.97545	No
SLV 12	-2182	-5826	-244	0.001	577.4	0.889	0.01571	4.97545	No
SLV 11	-2182	-5826	-244	0.001	577.4	0.889	0.01571	4.97545	No
SLV 3	-1908	-5049	-95	0.036	552.7	0.889	0.58375	10.57293	No
SLV 4	-1908	-5049	-95	0.036	552.7	0.889	0.58375	10.57293	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	3.7	SLU 81	Si
V_SLU	6.028	SLU 39	Si
PF_SLV	2.753	SLV 9	Si
V_SLV	2.882	SLV 5	Si
PFFP_SLV	1.72	SLV 3	Si
R_SLV	0	SLV 5	No

Maschio 29

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
35.424	6.497	35.424	2.847	L2	L3	3.65	0.3	3.85	3.85	3.85			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	t0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 41	2.67	-17729	-166.87	16191	25924.89	155.362	Si
SLU 41	4.57	-14011	-79.38	12796	21553.74	271.512	Si
SLU 40	2.67	-17729	-166.87	16191	25924.89	155.362	Si
SLU 40	4.57	-14011	-79.38	12796	21553.74	271.512	Si
SLU 82	2.67	-19794	-165.28	18077	28107.65	170.062	Si
SLU 82	4.57	-14905	-78.72	13612	22656.57	287.816	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 83	2.67	-19794	-165.28	18077	28107.65	170.062	Si
SLU 83	4.57	-14905	-78.72	13612	22656.57	287.816	Si
SLU 42	2.67	-17729	-166.87	16191	25924.89	155.362	Si
SLU 42	4.57	-14011	-79.38	12796	21553.74	271.512	Si
SLU 84	2.67	-19794	-165.28	18077	28107.65	170.062	Si
SLU 84	4.57	-14905	-78.72	13612	22656.57	287.816	Si
SLU 39	2.67	-17729	-166.87	16191	25924.89	155.362	Si
SLU 39	4.57	-14011	-79.38	12796	21553.74	271.512	Si
SLU 81	2.67	-19794	-165.28	18077	28107.65	170.062	Si
SLU 81	4.57	-14905	-78.72	13612	22656.57	287.816	Si
SLU 21	2.67	-15700	-136.78	14338	23608.83	172.601	Si
SLU 21	4.57	-12054	-63.13	11008	19025.83	301.388	Si
SLU 20	2.67	-15700	-136.78	14338	23608.83	172.601	Si
SLU 20	4.57	-12054	-63.13	11008	19025.83	301.388	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 7	2.67	-10709	-3677.2	9780	17980.03	4.89	Si
SLV 7	4.57	-7229	1813.55	6602	12480.25	6.882	Si
SLV 12	2.67	-11697	-3582.43	10682	19480.72	5.438	Si
SLV 12	4.57	-7132	1656.7	6513	12321.8	7.438	Si
SLV 5	2.67	-10465	3463.99	9557	17605.37	5.082	Si
SLV 5	4.57	-7156	-1717.42	6535	12360.58	7.197	Si
SLV 11	2.67	-11697	-3582.43	10682	19480.72	5.438	Si
SLV 11	4.57	-7132	1656.7	6513	12321.8	7.438	Si
SLV 6	2.67	-10465	3463.99	9557	17605.37	5.082	Si
SLV 6	4.57	-7156	-1717.42	6535	12360.58	7.197	Si
SLV 9	2.67	-11453	3558.76	10459	19112.63	5.371	Si
SLV 9	4.57	-7058	-1874.27	6446	12201.94	6.51	Si
SLV 4	2.67	-9472	-1288.36	8650	16061.96	12.467	Si
SLV 4	4.57	-7317	760.7	6682	12622.99	16.594	Si
SLV 3	2.67	-9472	-1288.36	8650	16061.96	12.467	Si
SLV 3	4.57	-7317	760.7	6682	12622.99	16.594	Si
SLV 10	2.67	-11453	3558.76	10459	19112.63	5.371	Si
SLV 10	4.57	-7058	-1874.27	6446	12201.94	6.51	Si
SLV 8	2.67	-10709	-3677.2	9780	17980.03	4.89	Si
SLV 8	4.57	-7229	1813.55	6602	12480.25	6.882	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 65	2.67	-13296	-28	-57.58		12142	3.65	7175	7856			285.2	Si
SLU 65	4.57	-8068	-28	-31.95		7368	3.65	6538	7159			259.88	Si
SLU 72	2.67	-13296	-28	-57.58		12142	3.65	7175	7856			285.2	Si
SLU 72	4.57	-8068	-28	-31.95		7368	3.65	6538	7159			259.88	Si
SLU 70	2.67	-13296	-28	-57.58		12142	3.65	7175	7856			285.2	Si
SLU 70	4.57	-8068	-28	-31.95		7368	3.65	6538	7159			259.88	Si
SLU 69	2.67	-13296	-28	-57.58		12142	3.65	7175	7856			285.2	Si
SLU 69	4.57	-8068	-28	-31.95		7368	3.65	6538	7159			259.88	Si
SLU 68	2.67	-13296	-28	-57.58		12142	3.65	7175	7856			285.2	Si
SLU 68	4.57	-8068	-28	-31.95		7368	3.65	6538	7159			259.88	Si
SLU 71	2.67	-13296	-28	-57.58		12142	3.65	7175	7856			285.2	Si
SLU 71	4.57	-8068	-28	-31.95		7368	3.65	6538	7159			259.88	Si
SLU 77	2.67	-17845	-29	-132.97		16296	3.65	7728	8463			288.07	Si
SLU 77	4.57	-12854	-29	-64.69		11739	3.65	7121	7797			265.39	Si
SLU 64	2.67	-13296	-28	-57.58		12142	3.65	7175	7856			285.2	Si
SLU 64	4.57	-8068	-28	-31.95		7368	3.65	6538	7159			259.88	Si
SLU 66	2.67	-13296	-28	-57.58		12142	3.65	7175	7856			285.2	Si
SLU 66	4.57	-8068	-28	-31.95		7368	3.65	6538	7159			259.88	Si
SLU 67	2.67	-13296	-28	-57.58		12142	3.65	7175	7856			285.2	Si
SLU 67	4.57	-8068	-28	-31.95		7368	3.65	6538	7159			259.88	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 4	2.67	-9472	-1206	-1288.36		8650	3.65	10063	11019			9.14	Si
SLV 4	4.57	-7317	-841	760.7		6682	3.65	9670	10588			12.59	Si
SLV 11	2.67	-11697	-3457	-3582.43		10682	3.65	10470	11464			3.32	Si
SLV 11	4.57	-7132	-2807	1656.7		6513	3.65	9636	10551			3.76	Si
SLV 7	2.67	-10709	-3542	-3677.2		9780	3.65	10289	11267			3.18	Si
SLV 7	4.57	-7229	-2799	1813.55		6602	3.65	9654	10571			3.78	Si
SLV 12	2.67	-11697	-3457	-3582.43		10682	3.65	10470	11464			3.32	Si
SLV 12	4.57	-7132	-2807	1656.7		6513	3.65	9636	10551			3.76	Si
SLV 8	2.67	-10709	-3542	-3677.2		9780	3.65	10289	11267			3.18	Si
SLV 8	4.57	-7229	-2799	1813.55		6602	3.65	9654	10571			3.78	Si
SLV 6	2.67	-10465	3418	3463.99		9557	3.65	10245	11218			3.28	Si
SLV 6	4.57	-7156	2767	-1717.42		6535	3.65	9640	10556			3.81	Si
SLV 9	2.67	-11453	3503	3558.76		10459	3.65	10425	11416			3.26	Si
SLV 9	4.57	-7058	2759	-1874.27		6446	3.65	9623	10537			3.82	Si
SLV 5	2.67	-10465	3418	3463.99		9557	3.65	10245	11218			3.28	Si
SLV 5	4.57	-7156	2767	-1717.42		6535	3.65	9640	10556			3.81	Si
SLV 3	2.67	-9472	-1206	-1288.36		8650	3.65	10063	11019			9.14	Si
SLV 3	4.57	-7317	-841	760.7		6682	3.65	9670	10588			12.59	Si
SLV 10	2.67	-11453	3503	3558.76		10459	3.65	10425	11416			3.26	Si
SLV 10	4.57	-7058	2759	-1874.27		6446	3.65	9623	10537			3.82	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.595 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 1	143750	0.48	7948	-8703	601.01	1220.51	2.03	Si
SLV 2	143750	0.48	7948	-8703	601.01	1220.51	2.03	Si



Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 4	143750	0.48	7969	-8726	601.01	1223.57	2.04	Si
SLV 3	143750	0.48	7969	-8726	601.01	1223.57	2.04	Si
SLV 5	143750	0.48	8362	-9157	601.01	1279.48	2.13	Si
SLV 6	143750	0.48	8362	-9157	601.01	1279.48	2.13	Si
SLV 8	143750	0.48	8434	-9235	601.01	1289.62	2.15	Si
SLV 7	143750	0.48	8434	-9235	601.01	1289.62	2.15	Si
SLV 9	143750	0.48	8739	-9569	601.01	1332.69	2.22	Si
SLV 10	143750	0.48	8739	-9569	601.01	1332.69	2.22	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.595 $W_a = 0.05$ $T_a = 0.0825$

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 13	-3979	-13536	310	0.018	1048.2	0.889	0.295	10.57293	No
SLV 14	-3979	-13536	310	0.018	1048.2	0.889	0.295	10.57293	No
SLV 3	-4141	-10721	-310	0.018	1063	0.889	0.30225	10.57293	No
SLV 4	-4141	-10721	-310	0.018	1063	0.889	0.30225	10.57293	No
SLV 15	-3998	-13621	305	0.019	1049.9	0.889	0.30653	10.57293	No
SLV 16	-3998	-13621	305	0.019	1049.9	0.889	0.30653	10.57293	No
SLV 1	-4122	-10635	-305	0.019	1061.3	0.889	0.31199	10.57293	No
SLV 2	-4122	-10635	-305	0.019	1061.3	0.889	0.31199	10.57293	No
SLV 8	-4113	-11836	-101	0.045	1060.5	0.889	0.73418	4.97545	No
SLV 7	-4113	-11836	-101	0.045	1060.5	0.889	0.73418	4.97545	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	155.362	SLU 39	Si
V_SLU	259.876	SLU 64	Si
PF_SLV	4.89	SLV 7	Si
V_SLV	3.181	SLV 7	Si
PFFP_SLV	2.031	SLV 1	Si
R_SLV	0.028	SLV 13	No

Maschio 30

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
35.424	9.502	35.424	7.497	L2	L3	2.005	0.3	3.85	3.85	3.85			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fk	fvk0	fmedio	t0	fv0	μ	ϕ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLU 40	2.67	-8441	1113.29	14032	7005.87	6.293	Si
SLU 40	4.57	-7073	1638.96	11758	6068.43	3.703	Si
SLU 83	2.67	-9522	1218.48	15828	7692.31	6.313	Si
SLU 83	4.57	-7523	1728.33	12504	6384.67	3.694	Si
SLU 82	2.67	-9522	1218.48	15828	7692.31	6.313	Si
SLU 82	4.57	-7523	1728.33	12504	6384.67	3.694	Si
SLU 42	2.67	-8441	1113.29	14032	7005.87	6.293	Si
SLU 42	4.57	-7073	1638.96	11758	6068.43	3.703	Si
SLU 41	2.67	-8441	1113.29	14032	7005.87	6.293	Si
SLU 41	4.57	-7073	1638.96	11758	6068.43	3.703	Si
SLU 39	2.67	-8441	1113.29	14032	7005.87	6.293	Si
SLU 39	4.57	-7073	1638.96	11758	6068.43	3.703	Si
SLU 61	2.67	-8612	1079.23	14316	7117.68	6.595	Si
SLU 61	4.57	-6531	1490.22	10856	5675.43	3.808	Si
SLU 84	2.67	-9522	1218.48	15828	7692.31	6.313	Si
SLU 84	4.57	-7523	1728.33	12504	6384.67	3.694	Si
SLU 60	2.67	-8612	1079.23	14316	7117.68	6.595	Si
SLU 60	4.57	-6531	1490.22	10856	5675.43	3.808	Si
SLU 81	2.67	-9522	1218.48	15828	7692.31	6.313	Si
SLU 81	4.57	-7523	1728.33	12504	6384.67	3.694	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 12	2.67	-5411	31.13	8994	5025.95	161.428	Si
SLV 12	4.57	-4295	1325.91	7140	4055.08	3.058	Si
SLV 9	2.67	-6095	1368.94	10132	5604.51	4.094	Si
SLV 9	4.57	-3171	364.03	5271	3042.22	8.357	Si
SLV 16	2.67	-6287	633.83	10450	5764.39	9.095	Si
SLV 16	4.57	-4203	1084.34	6986	3972.76	3.664	Si
SLV 3	2.67	-4468	249.65	7428	4207.95	16.855	Si
SLV 3	4.57	-3343	812.66	5558	3199.75	3.937	Si
SLV 10	2.67	-6095	1368.94	10132	5604.51	4.094	Si
SLV 10	4.57	-3171	364.03	5271	3042.22	8.357	Si
SLV 7	2.67	-4865	-84.12	8088	4555.46	54.154	Si
SLV 7	4.57	-4038	1244.41	6712	3825.94	3.075	Si
SLV 8	2.67	-4865	-84.12	8088	4555.46	54.154	Si
SLV 8	4.57	-4038	1244.41	6712	3825.94	3.075	Si
SLV 11	2.67	-5411	31.13	8994	5025.95	161.428	Si
SLV 11	4.57	-4295	1325.91	7140	4055.08	3.058	Si



Comb.	Quota	N	M	σ_0	Mu	c.s.	Verifica
SLV 4	2.67	-4468	249.65	7428	4207.95	16.855	Si
SLV 4	4.57	-3343	812.66	5558	3199.75	3.937	Si
SLV 15	2.67	-6287	633.83	10450	5764.39	9.095	Si
SLV 15	4.57	-4203	1084.34	6986	3972.76	3.664	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLU 83	2.67	-9522	-674	1218.48		15828	2.0053	7666	4612			6.85	Si
SLU 83	4.57	-7523	-673	1728.33		12504	2.0053	7223	4345			6.45	Si
SLU 39	2.67	-8441	-686	1113.29		14032	2.0053	7426	4468			6.51	Si
SLU 39	4.57	-7073	-686	1638.96		11758	2.0053	7123	4285			6.25	Si
SLU 19	2.67	-7532	-575	974.04		12520	2.0053	7225	4346			7.56	Si
SLU 19	4.57	-6082	-574	1400.85		10109	2.0053	6903	4153			7.23	Si
SLU 41	2.67	-8441	-686	1113.29		14032	2.0053	7426	4468			6.51	Si
SLU 41	4.57	-7073	-686	1638.96		11758	2.0053	7123	4285			6.25	Si
SLU 42	2.67	-8441	-686	1113.29		14032	2.0053	7426	4468			6.51	Si
SLU 42	4.57	-7073	-686	1638.96		11758	2.0053	7123	4285			6.25	Si
SLU 40	2.67	-8441	-686	1113.29		14032	2.0053	7426	4468			6.51	Si
SLU 40	4.57	-7073	-686	1638.96		11758	2.0053	7123	4285			6.25	Si
SLU 84	2.67	-9522	-674	1218.48		15828	2.0053	7666	4612			6.85	Si
SLU 84	4.57	-7523	-673	1728.33		12504	2.0053	7223	4345			6.45	Si
SLU 18	2.67	-7532	-575	974.04		12520	2.0053	7225	4346			7.56	Si
SLU 18	4.57	-6082	-574	1400.85		10109	2.0053	6903	4153			7.23	Si
SLU 82	2.67	-9522	-674	1218.48		15828	2.0053	7666	4612			6.85	Si
SLU 82	4.57	-7523	-673	1728.33		12504	2.0053	7223	4345			6.45	Si
SLU 81	2.67	-9522	-674	1218.48		15828	2.0053	7666	4612			6.85	Si
SLU 81	4.57	-7523	-673	1728.33		12504	2.0053	7223	4345			6.45	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	V par	M	σ_0	σ_N	I'	fvd	Vt scorr.	Vt fess.diag.	Vt _{lim}	c.s.	Verifica
SLV 6	2.67	-5550	1071	1253.69		9225	2.0053	10178	6123			5.72	Si
SLV 6	4.57	-2913	1329	282.53		4843	2.0053	9302	5596			4.21	Si
SLV 9	2.67	-6095	1537	1368.94		10132	2.0053	10360	6232			4.06	Si
SLV 9	4.57	-3171	1818	364.03		5271	2.0053	9388	5647			3.11	Si
SLV 8	2.67	-4865	-1967	-84.12		8088	2.0053	9951	5986			3.04	Si
SLV 8	4.57	-4038	-2248	1244.41		6712	2.0053	9676	5821			2.59	Si
SLV 5	2.67	-5550	1071	1253.69		9225	2.0053	10178	6123			5.72	Si
SLV 5	4.57	-2913	1329	282.53		4843	2.0053	9302	5596			4.21	Si
SLV 10	2.67	-6095	1537	1368.94		10132	2.0053	10360	6232			4.06	Si
SLV 10	4.57	-3171	1818	364.03		5271	2.0053	9388	5647			3.11	Si
SLV 4	2.67	-4468	-1447	249.65		7428	2.0053	9819	5907			4.08	Si
SLV 4	4.57	-3343	-1567	812.66		5558	2.0053	9445	5682			3.63	Si
SLV 12	2.67	-5411	-1501	31.13		8994	2.0053	10132	6095			4.06	Si
SLV 12	4.57	-4295	-1759	1325.91		7140	2.0053	9761	5872			3.34	Si
SLV 7	2.67	-4865	-1967	-84.12		8088	2.0053	9951	5986			3.04	Si
SLV 7	4.57	-4038	-2248	1244.41		6712	2.0053	9676	5821			2.59	Si
SLV 11	2.67	-5411	-1501	31.13		8994	2.0053	10132	6095			4.06	Si
SLV 11	4.57	-4295	-1759	1325.91		7140	2.0053	9761	5872			3.34	Si
SLV 3	2.67	-4468	-1447	249.65		7428	2.0053	9819	5907			4.08	Si
SLV 3	4.57	-3343	-1567	812.66		5558	2.0053	9445	5682			3.63	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.595 Wa 0.05 denominatore 8 $\gamma_M = 2$

Comb.	fd	Sa	σ_0	N	M	Mc	Coeff.s.	Verifica
SLV 2	143750	0.48	6295	-3787	330.19	538.82	1.63	Si
SLV 1	143750	0.48	6295	-3787	330.19	538.82	1.63	Si
SLV 3	143750	0.48	6632	-3990	330.19	565.98	1.71	Si
SLV 4	143750	0.48	6632	-3990	330.19	565.98	1.71	Si
SLV 5	143750	0.48	6935	-4172	330.19	590.26	1.79	Si
SLV 6	143750	0.48	6935	-4172	330.19	590.26	1.79	Si
SLV 10	143750	0.48	7819	-4704	330.19	660.44	2	Si
SLV 9	143750	0.48	7819	-4704	330.19	660.44	2	Si
SLV 7	143750	0.48	8057	-4847	330.19	679.08	2.06	Si
SLV 8	143750	0.48	8057	-4847	330.19	679.08	2.06	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.595 Wa = 0.05 Ta = 0.0825

Comb.	N top	N base	V orto	α_0	M*	e*	a0*	aLim	Verifica
SLV 11	-2261	-6807	277	0	582.7	0.889	0	4.97545	No
SLV 5	-2030	-5403	-277	0	561.7	0.889	0	4.97545	No
SLV 12	-2261	-6807	277	0	582.7	0.889	0	4.97545	No
SLV 6	-2030	-5403	-277	0	561.7	0.889	0	4.97545	No
SLV 10	-2141	-5947	-243	0.001	571.8	0.889	0.01252	4.97545	No
SLV 9	-2141	-5947	-243	0.001	571.8	0.889	0.01252	4.97545	No
SLV 8	-2150	-6263	243	0.001	572.6	0.889	0.01395	4.97545	No
SLV 7	-2150	-6263	243	0.001	572.6	0.889	0.01395	4.97545	No
SLV 2	-1941	-5069	-136	0.025	553.8	0.889	0.41595	10.57293	No
SLV 1	-1941	-5069	-136	0.025	553.8	0.889	0.41595	10.57293	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	3.694	SLU 81	Si
V_SLU	6.247	SLU 39	Si
PF_SLV	3.058	SLV 11	Si
V_SLV	2.589	SLV 7	Si
PFFP_SLV	1.632	SLV 1	Si
R_SLV	0	SLV 5	No



1.4 Verifiche travi di accoppiamento in muratura

Le unità di misura elencate nel capitolo sono in [m, daN] ove non espressamente specificato.

X ini.: coordinata punto iniziale. [m]

Y ini.: coordinata punto iniziale. [m]

Z ini.inf.: coordinata punto iniziale. [m]

Z ini.sup.: coordinata punto iniziale. [m]

H ini.: altezza della sezione iniziale. [m]

X fin.: coordinata punto finale. [m]

Y fin.: coordinata punto finale. [m]

Z fin.inf.: coordinata punto finale. [m]

Z fin.sup.: coordinata punto finale. [m]

H fin.: altezza della sezione finale. [m]

Luce: lunghezza della trave. [m]

Spessore: spessore. [m]

R. Trazione: resistenza a trazione dell'elemento teso disposto orizzontalmente. [daN]

fb₋: resistenza normalizzata a compressione in direzione orizzontale dei blocchi. [daN/m²]

f_{hk}: resistenza caratteristica a compressione della muratura utilizzata in direzione orizzontale. [daN/m²]

fvk0: resistenza caratteristica a taglio in assenza di carichi verticali. [daN/m²]

f_{hmedio}: resistenza media a compressione della muratura utilizzata in direzione orizzontale. [daN/m²]

τ0: resistenza media a taglio in assenza di azioni normali [C8.7.1.16]. [daN/m²]

fv0: resistenza media a taglio in assenza di azioni normali [C8.7.1.17]. [daN/m²]

μ: coefficiente di attrito [C8.7.1.17].

φ: coefficiente di ammorsamento o ingranamento secondo Circolare 7 21-01-19 §C8.7.1.3.1.1.

fvk,lim: valore caratteristico massimo della resistenza a taglio che può essere impiegata nel calcolo (§11.10.3.3). [daN/m²]

E: modulo di elasticità longitudinale della muratura utilizzato. [daN/m²]

G: modulo di elasticità tangenziale della muratura utilizzato. [daN/m²]

FC: fattore di confidenza della muratura.

Sezione: sezione di verifica.

γM: fattore parziale di sicurezza del materiale.

N: sforzo normale. [daN]

M: momento flettente nel piano. [daN*m]

Mu: momento ultimo. [daN*m]

Comb.: combinazione.

c.s.: coefficiente di sicurezza.

Verifica: stato di verifica.

M: momento flettente. [daN*m]

V: taglio nel piano. [daN]

Vt: resistenza a taglio secondo [7.8.4]. [daN]

Vp: resistenza a taglio secondo [7.8.6]. [daN]

Vt fess. diag.: resistenza a taglio per fessurazione diagonale secondo §C8.7.1.3.1.1 formule [C8.7.1.16] ovvero [C8.7.1.17]. [daN]

Vt,lim: taglio limite [C8.1.7.18]. [daN]

Stato limite: pF_SLV=Presso flessione per azioni sismiche; V_SLV=Taglio per azioni sismiche.

Coeff.s.: coefficiente di sicurezza.

Trave di accoppiamento 1

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
25.882	8.663	-0.98	0.41	1.39	26.284	9.108	-0.98	0.41	1.39	0.6	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb ₋	f _{hk}	fvk0	f _{hmedio}	τ0	fv0	μ	φ	fvk,lim	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-552	-163.1	2098.31	SLU 83	12.87	Si
fin.	3	-624	-387.82	2098.31	SLU 83	5.41	Si
ini.	3	-518	-152.21	2098.31	SLU 76	13.79	Si
fin.	3	-593	-363.63	2098.31	SLU 76	5.77	Si
ini.	3	-552	-163.1	2098.31	SLU 82	12.87	Si
fin.	3	-624	-387.82	2098.31	SLU 82	5.41	Si
ini.	3	-518	-152.21	2098.31	SLU 75	13.79	Si
fin.	3	-593	-363.63	2098.31	SLU 75	5.77	Si
ini.	3	-518	-152.21	2098.31	SLU 73	13.79	Si
fin.	3	-593	-363.63	2098.31	SLU 73	5.77	Si
ini.	3	-552	-163.1	2098.31	SLU 84	12.87	Si
fin.	3	-624	-387.82	2098.31	SLU 84	5.41	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-552	-163.1	2098.31	SLU 81	12.87	Si
fin.	3	-624	-387.82	2098.31	SLU 81	5.41	Si
ini.	3	-518	-152.21	2098.31	SLU 74	13.79	Si
fin.	3	-593	-363.63	2098.31	SLU 74	5.77	Si
ini.	3	-518	-152.21	2098.31	SLU 79	13.79	Si
fin.	3	-593	-363.63	2098.31	SLU 79	5.77	Si
ini.	3	-518	-152.21	2098.31	SLU 78	13.79	Si
fin.	3	-593	-363.63	2098.31	SLU 78	5.77	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt _{lim}	Comb.	c.s.	Verifica
ini.	3	0	-163.1	-1402			2409	907	SLU 82	0.65	No
fin.	3	0	-387.82	801			2409	907	SLU 82	1.13	Si
ini.	3	0	-163.1	-1402			2409	907	SLU 84	0.65	No
fin.	3	0	-387.82	801			2409	907	SLU 84	1.13	Si
ini.	3	0	-152.21	-1279			2409	907	SLU 74	0.71	No
fin.	3	0	-363.63	733			2409	907	SLU 74	1.24	Si
ini.	3	0	-163.1	-1402			2409	907	SLU 83	0.65	No
fin.	3	0	-387.82	801			2409	907	SLU 83	1.13	Si
ini.	3	0	-152.21	-1279			2409	907	SLU 75	0.71	No
fin.	3	0	-363.63	733			2409	907	SLU 75	1.24	Si
ini.	3	0	-152.21	-1279			2409	907	SLU 78	0.71	No
fin.	3	0	-363.63	733			2409	907	SLU 78	1.24	Si
ini.	3	0	-163.1	-1402			2409	907	SLU 81	0.65	No
fin.	3	0	-387.82	801			2409	907	SLU 81	1.13	Si
ini.	3	0	-152.21	-1279			2409	907	SLU 73	0.71	No
fin.	3	0	-363.63	733			2409	907	SLU 73	1.24	Si
ini.	3	0	-152.21	-1279			2409	907	SLU 79	0.71	No
fin.	3	0	-363.63	733			2409	907	SLU 79	1.24	Si
ini.	3	0	-152.21	-1279			2409	907	SLU 76	0.71	No
fin.	3	0	-363.63	733			2409	907	SLU 76	1.24	Si

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-364	676.45	2209.71	SLV 16	3.27	Si
fin.	2	592	-1466.8	2209.71	SLV 16	1.51	Si
ini.	2	-339	-879.3	2209.71	SLV 1	2.51	Si
fin.	2	-1413	976.29	2209.71	SLV 1	2.26	Si
ini.	2	-515	575.99	2209.71	SLV 11	3.84	Si
fin.	2	539	-1594.87	2209.71	SLV 11	1.39	Si
ini.	2	-188	-778.84	2209.71	SLV 5	2.84	Si
fin.	2	-1360	1104.36	2209.71	SLV 5	2	Si
ini.	2	-539	197.1	2209.71	SLV 8	11.21	Si
fin.	2	66	-1056.41	2209.71	SLV 8	2.09	Si
ini.	2	-364	676.45	2209.71	SLV 15	3.27	Si
fin.	2	592	-1466.8	2209.71	SLV 15	1.51	Si
ini.	2	-539	197.1	2209.71	SLV 7	11.21	Si
fin.	2	66	-1056.41	2209.71	SLV 7	2.09	Si
ini.	2	-188	-778.84	2209.71	SLV 6	2.84	Si
fin.	2	-1360	1104.36	2209.71	SLV 6	2	Si
ini.	2	-515	575.99	2209.71	SLV 12	3.84	Si
fin.	2	539	-1594.87	2209.71	SLV 12	1.39	Si
ini.	2	-339	-879.3	2209.71	SLV 2	2.51	Si
fin.	2	-1413	976.29	2209.71	SLV 2	2.26	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt _{lim}	Comb.	c.s.	Verifica
ini.	2	0	-879.3	3041			3613	1360	SLV 2	0.45	No
fin.	2	0	976.29	6054			3613	1360	SLV 2	0.22	No
ini.	2	0	-778.84	4442			3613	1360	SLV 6	0.31	No
fin.	2	0	1104.36	5862			3613	1360	SLV 6	0.23	No
ini.	2	0	197.1	-4565			3613	1360	SLV 8	0.3	No
fin.	2	0	-1056.41	-2310			3613	1360	SLV 8	0.59	No
ini.	2	0	575.99	-6066			3613	1360	SLV 11	0.22	No
fin.	2	0	-1594.87	-4926			3613	1360	SLV 11	0.28	No
ini.	2	0	-879.3	3041			3613	1360	SLV 1	0.45	No
fin.	2	0	976.29	6054			3613	1360	SLV 1	0.22	No
ini.	2	0	676.45	-4664			3613	1360	SLV 15	0.29	No
fin.	2	0	-1466.8	-5118			3613	1360	SLV 15	0.27	No
ini.	2	0	-778.84	4442			3613	1360	SLV 5	0.31	No
fin.	2	0	1104.36	5862			3613	1360	SLV 5	0.23	No
ini.	2	0	575.99	-6066			3613	1360	SLV 12	0.22	No
fin.	2	0	-1594.87	-4926			3613	1360	SLV 12	0.28	No
ini.	2	0	676.45	-4664			3613	1360	SLV 16	0.29	No
fin.	2	0	-1466.8	-5118			3613	1360	SLV 16	0.27	No
ini.	2	0	197.1	-4565			3613	1360	SLV 7	0.3	No
fin.	2	0	-1056.41	-2310			3613	1360	SLV 7	0.59	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.386	SLV 11	Si
V_SLV	0.224	SLV 11	No
PF_SLU	5.41	SLU 81	Si
V_SLU	0.646	SLU 81	No



Trave di accoppiamento 2

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
25.882	8.663	0.81	1.67	0.86	26.284	9.108	0.81	1.67	0.86	0.6	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	149	84.91	1170.81	SLU 73	13.79	Si
fin.	3	149	-231.83	1170.81	SLU 73	5.05	Si
ini.	3	147	81.86	1170.81	SLU 62	14.3	Si
fin.	3	147	-232.5	1170.81	SLU 62	5.04	Si
ini.	3	147	81.86	1170.81	SLU 61	14.3	Si
fin.	3	147	-232.5	1170.81	SLU 61	5.04	Si
ini.	3	149	84.91	1170.81	SLU 74	13.79	Si
fin.	3	149	-231.83	1170.81	SLU 74	5.05	Si
ini.	3	159	90.68	1170.81	SLU 84	12.91	Si
fin.	3	159	-249.93	1170.81	SLU 84	4.68	Si
ini.	3	159	90.68	1170.81	SLU 81	12.91	Si
fin.	3	159	-249.93	1170.81	SLU 81	4.68	Si
ini.	3	159	90.68	1170.81	SLU 82	12.91	Si
fin.	3	159	-249.93	1170.81	SLU 82	4.68	Si
ini.	3	147	81.86	1170.81	SLU 63	14.3	Si
fin.	3	147	-232.5	1170.81	SLU 63	5.04	Si
ini.	3	147	81.86	1170.81	SLU 60	14.3	Si
fin.	3	147	-232.5	1170.81	SLU 60	5.04	Si
ini.	3	159	90.68	1170.81	SLU 83	12.91	Si
fin.	3	159	-249.93	1170.81	SLU 83	4.68	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	90.68	75			1490	561	SLU 83	7.49	Si
fin.	3	0	-249.93	-1167			1490	561	SLU 83	0.48	No
ini.	3	0	84.91	92			1490	561	SLU 77	6.1	Si
fin.	3	0	-231.83	-1099			1490	561	SLU 77	0.51	No
ini.	3	0	90.68	75			1490	561	SLU 84	7.49	Si
fin.	3	0	-249.93	-1167			1490	561	SLU 84	0.48	No
ini.	3	0	84.91	92			1490	561	SLU 78	6.1	Si
fin.	3	0	-231.83	-1099			1490	561	SLU 78	0.51	No
ini.	3	0	84.91	92			1490	561	SLU 79	6.1	Si
fin.	3	0	-231.83	-1099			1490	561	SLU 79	0.51	No
ini.	3	0	84.91	92			1490	561	SLU 75	6.1	Si
fin.	3	0	-231.83	-1099			1490	561	SLU 75	0.51	No
ini.	3	0	90.68	75			1490	561	SLU 82	7.49	Si
fin.	3	0	-249.93	-1167			1490	561	SLU 82	0.48	No
ini.	3	0	84.91	92			1490	561	SLU 80	6.1	Si
fin.	3	0	-231.83	-1099			1490	561	SLU 80	0.51	No
ini.	3	0	90.68	75			1490	561	SLU 81	7.49	Si
fin.	3	0	-249.93	-1167			1490	561	SLU 81	0.48	No
ini.	3	0	84.91	92			1490	561	SLU 76	6.1	Si
fin.	3	0	-231.83	-1099			1490	561	SLU 76	0.51	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-430	902.23	1282.21	SLV 14	1.42	Si
fin.	2	-620	-741.4	1282.21	SLV 14	1.73	Si
ini.	2	-430	902.23	1282.21	SLV 13	1.42	Si
fin.	2	-620	-741.4	1282.21	SLV 13	1.73	Si
ini.	2	434	-888.26	1282.21	SLV 6	1.44	Si
fin.	2	627	823.98	1282.21	SLV 6	1.56	Si
ini.	2	728	-1169.14	1282.21	SLV 2	1.1	Si
fin.	2	992	874.64	1282.21	SLV 2	1.47	Si
ini.	2	-525	1282.88	1282.21	SLV 15	1	No
fin.	2	-790	-1182.79	1282.21	SLV 15	1.08	Si
ini.	2	434	-888.26	1282.21	SLV 5	1.44	Si
fin.	2	627	823.98	1282.21	SLV 5	1.56	Si
ini.	2	-231	1001.99	1282.21	SLV 11	1.28	Si
fin.	2	-424	-1132.13	1282.21	SLV 11	1.13	Si
ini.	2	728	-1169.14	1282.21	SLV 1	1.1	Si
fin.	2	992	874.64	1282.21	SLV 1	1.47	Si
ini.	2	-231	1001.99	1282.21	SLV 12	1.28	Si
fin.	2	-424	-1132.13	1282.21	SLV 12	1.13	Si
ini.	2	-525	1282.88	1282.21	SLV 16	1	No
fin.	2	-790	-1182.79	1282.21	SLV 16	1.08	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-888.26	3390			2236	841	SLV 5	0.25	No
fin.	2	0	823.98	2536			2236	841	SLV 5	0.33	No
ini.	2	0	902.23	-2361			2236	841	SLV 13	0.36	No
fin.	2	0	-741.4	-3192			2236	841	SLV 13	0.26	No
ini.	2	0	-888.26	3390			2236	841	SLV 6	0.25	No



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
fin.	2	0	823.98	2536			2236	841	SLV 6	0.33	No
ini.	2	0	1001.99	-3208			2236	841	SLV 11	0.26	No
fin.	2	0	-1132.13	-4032			2236	841	SLV 11	0.21	No
ini.	2	0	1001.99	-3208			2236	841	SLV 12	0.26	No
fin.	2	0	-1132.13	-4032			2236	841	SLV 12	0.21	No
ini.	2	0	1282.88	-3772			2236	841	SLV 16	0.22	No
fin.	2	0	-1182.79	-4596			2236	841	SLV 16	0.18	No
ini.	2	0	-1169.14	3954			2236	841	SLV 1	0.21	No
fin.	2	0	874.64	3099			2236	841	SLV 1	0.27	No
ini.	2	0	1282.88	-3772			2236	841	SLV 15	0.22	No
fin.	2	0	-1182.79	-4596			2236	841	SLV 15	0.18	No
ini.	2	0	-1169.14	3954			2236	841	SLV 2	0.21	No
fin.	2	0	874.64	3099			2236	841	SLV 2	0.27	No
ini.	2	0	902.23	-2361			2236	841	SLV 14	0.36	No
fin.	2	0	-741.4	-3192			2236	841	SLV 14	0.26	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	0.999	SLV 15	No
V_SLV	0.183	SLV 15	No
PF_SLU	4.685	SLU 81	Si
V_SLU	0.48	SLU 81	No

Trave di accoppiamento 3

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
28.92	-0.169	-0.98	0.41	1.39	27.92	-0.169	-0.98	0.41	1.39	1	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-2101	246.21	2098.31	SLU 75	8.52	Si
fin.	3	-1627	-122.44	2098.31	SLU 75	17.14	Si
ini.	3	-2101	246.21	2098.31	SLU 78	8.52	Si
fin.	3	-1627	-122.44	2098.31	SLU 78	17.14	Si
ini.	3	-2101	246.21	2098.31	SLU 79	8.52	Si
fin.	3	-1627	-122.44	2098.31	SLU 79	17.14	Si
ini.	3	-2101	246.21	2098.31	SLU 73	8.52	Si
fin.	3	-1627	-122.44	2098.31	SLU 73	17.14	Si
ini.	3	-2221	265.13	2098.31	SLU 82	7.91	Si
fin.	3	-1716	-126.37	2098.31	SLU 82	16.6	Si
ini.	3	-2101	246.21	2098.31	SLU 74	8.52	Si
fin.	3	-1627	-122.44	2098.31	SLU 74	17.14	Si
ini.	3	-2221	265.13	2098.31	SLU 83	7.91	Si
fin.	3	-1716	-126.37	2098.31	SLU 83	16.6	Si
ini.	3	-2221	265.13	2098.31	SLU 81	7.91	Si
fin.	3	-1716	-126.37	2098.31	SLU 81	16.6	Si
ini.	3	-2221	265.13	2098.31	SLU 84	7.91	Si
fin.	3	-1716	-126.37	2098.31	SLU 84	16.6	Si
ini.	3	-2101	246.21	2098.31	SLU 76	8.52	Si
fin.	3	-1627	-122.44	2098.31	SLU 76	17.14	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	246.21	-2786			2409	907	SLU 75	0.33	No
fin.	3	0	-122.44	1009			2409	907	SLU 75	0.9	No
ini.	3	0	265.13	-2966			2409	907	SLU 84	0.31	No
fin.	3	0	-126.37	1079			2409	907	SLU 84	0.84	No
ini.	3	0	265.13	-2966			2409	907	SLU 81	0.31	No
fin.	3	0	-126.37	1079			2409	907	SLU 81	0.84	No
ini.	3	0	246.21	-2786			2409	907	SLU 78	0.33	No
fin.	3	0	-122.44	1009			2409	907	SLU 78	0.9	No
ini.	3	0	246.21	-2786			2409	907	SLU 74	0.33	No
fin.	3	0	-122.44	1009			2409	907	SLU 74	0.9	No
ini.	3	0	265.13	-2966			2409	907	SLU 82	0.31	No
fin.	3	0	-126.37	1079			2409	907	SLU 82	0.84	No
ini.	3	0	246.21	-2786			2409	907	SLU 79	0.33	No
fin.	3	0	-122.44	1009			2409	907	SLU 79	0.9	No
ini.	3	0	265.13	-2966			2409	907	SLU 83	0.31	No
fin.	3	0	-126.37	1079			2409	907	SLU 83	0.84	No
ini.	3	0	246.21	-2786			2409	907	SLU 76	0.33	No
fin.	3	0	-122.44	1009			2409	907	SLU 76	0.9	No
ini.	3	0	246.21	-2786			2409	907	SLU 73	0.33	No
fin.	3	0	-122.44	1009			2409	907	SLU 73	0.9	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-774	-350.89	2209.71	SLV 14	6.3	Si
fin.	2	-1800	585.11	2209.71	SLV 14	3.78	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-602	-432.95	2209.71	SLV 16	5.1	Si
fin.	2	-1509	585.76	2209.71	SLV 16	3.77	Si
ini.	2	-2284	758.41	2209.71	SLV 1	2.91	Si
fin.	2	-739	-761.73	2209.71	SLV 1	2.9	Si
ini.	2	-774	-350.89	2209.71	SLV 13	6.3	Si
fin.	2	-1800	585.11	2209.71	SLV 13	3.78	Si
ini.	2	-1956	465.89	2209.71	SLV 5	4.74	Si
fin.	2	-1449	-291.1	2209.71	SLV 5	7.59	Si
ini.	2	-2284	758.41	2209.71	SLV 2	2.91	Si
fin.	2	-739	-761.73	2209.71	SLV 2	2.9	Si
ini.	2	-2112	676.35	2209.71	SLV 4	3.27	Si
fin.	2	-449	-761.08	2209.71	SLV 4	2.9	Si
ini.	2	-2112	676.35	2209.71	SLV 3	3.27	Si
fin.	2	-449	-761.08	2209.71	SLV 3	2.9	Si
ini.	2	-1956	465.89	2209.71	SLV 6	4.74	Si
fin.	2	-1449	-291.1	2209.71	SLV 6	7.59	Si
ini.	2	-602	-432.95	2209.71	SLV 15	5.1	Si
fin.	2	-1509	585.76	2209.71	SLV 15	3.77	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	465.89	-3039			3613	1360	SLV 6	0.45	No
fin.	2	0	-291.1	101			3613	1360	SLV 6	13.48	Si
ini.	2	0	676.35	-4007			3613	1360	SLV 3	0.34	No
fin.	2	0	-761.08	-1510			3613	1360	SLV 3	0.9	No
ini.	2	0	758.41	-4293			3613	1360	SLV 1	0.32	No
fin.	2	0	-761.73	-1465			3613	1360	SLV 1	0.93	No
ini.	2	0	-432.95	530			3613	1360	SLV 16	2.57	Si
fin.	2	0	585.76	2813			3613	1360	SLV 16	0.48	No
ini.	2	0	-350.89	244			3613	1360	SLV 14	5.58	Si
fin.	2	0	585.11	2858			3613	1360	SLV 14	0.48	No
ini.	2	0	676.35	-4007			3613	1360	SLV 4	0.34	No
fin.	2	0	-761.08	-1510			3613	1360	SLV 4	0.9	No
ini.	2	0	-432.95	530			3613	1360	SLV 15	2.57	Si
fin.	2	0	585.76	2813			3613	1360	SLV 15	0.48	No
ini.	2	0	465.89	-3039			3613	1360	SLV 5	0.45	No
fin.	2	0	-291.1	101			3613	1360	SLV 5	13.48	Si
ini.	2	0	758.41	-4293			3613	1360	SLV 2	0.32	No
fin.	2	0	-761.73	-1465			3613	1360	SLV 2	0.93	No
ini.	2	0	-350.89	244			3613	1360	SLV 13	5.58	Si
fin.	2	0	585.11	2858			3613	1360	SLV 13	0.48	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	2.901	SLV 1	Si
V_SLV	0.317	SLV 1	No
PF_SLU	7.914	SLU 81	Si
V_SLU	0.306	SLU 81	No

Trave di accoppiamento 4

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
28.92	-0.169	0.81	1.67	0.86	27.92	-0.169	0.81	1.67	0.86	1	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb _m	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{vd}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-504	-151.32	1170.81	SLU 84	7.74	Si
fin.	3	-621	-224.46	1170.81	SLU 84	5.22	Si
ini.	3	-458	-142.98	1170.81	SLU 75	8.19	Si
fin.	3	-558	-209.82	1170.81	SLU 75	5.58	Si
ini.	3	-458	-142.98	1170.81	SLU 74	8.19	Si
fin.	3	-558	-209.82	1170.81	SLU 74	5.58	Si
ini.	3	-504	-151.32	1170.81	SLU 83	7.74	Si
fin.	3	-621	-224.46	1170.81	SLU 83	5.22	Si
ini.	3	-504	-151.32	1170.81	SLU 82	7.74	Si
fin.	3	-621	-224.46	1170.81	SLU 82	5.22	Si
ini.	3	-458	-142.98	1170.81	SLU 73	8.19	Si
fin.	3	-558	-209.82	1170.81	SLU 73	5.58	Si
ini.	3	-458	-142.98	1170.81	SLU 78	8.19	Si
fin.	3	-558	-209.82	1170.81	SLU 78	5.58	Si
ini.	3	-504	-151.32	1170.81	SLU 81	7.74	Si
fin.	3	-621	-224.46	1170.81	SLU 81	5.22	Si
ini.	3	-458	-142.98	1170.81	SLU 79	8.19	Si
fin.	3	-558	-209.82	1170.81	SLU 79	5.58	Si
ini.	3	-458	-142.98	1170.81	SLU 76	8.19	Si
fin.	3	-558	-209.82	1170.81	SLU 76	5.58	Si



Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-142.98	2051			1282	482	SLU 80	0.24	No
fin.	3	0	-209.82	-1982			1282	482	SLU 80	0.24	No
ini.	3	0	-142.98	2051			1282	482	SLU 78	0.24	No
fin.	3	0	-209.82	-1982			1282	482	SLU 78	0.24	No
ini.	3	0	-142.98	2051			1282	482	SLU 77	0.24	No
fin.	3	0	-209.82	-1982			1282	482	SLU 77	0.24	No
ini.	3	0	-142.98	2051			1282	482	SLU 76	0.24	No
fin.	3	0	-209.82	-1982			1282	482	SLU 76	0.24	No
ini.	3	0	-142.98	2051			1282	482	SLU 79	0.24	No
fin.	3	0	-209.82	-1982			1282	482	SLU 79	0.24	No
ini.	3	0	-151.32	2160			1282	482	SLU 81	0.22	No
fin.	3	0	-224.46	-2098			1282	482	SLU 81	0.23	No
ini.	3	0	-151.32	2160			1282	482	SLU 83	0.22	No
fin.	3	0	-224.46	-2098			1282	482	SLU 83	0.23	No
ini.	3	0	-151.32	2160			1282	482	SLU 84	0.22	No
fin.	3	0	-224.46	-2098			1282	482	SLU 84	0.23	No
ini.	3	0	-142.98	2051			1282	482	SLU 75	0.24	No
fin.	3	0	-209.82	-1982			1282	482	SLU 75	0.24	No
ini.	3	0	-151.32	2160			1282	482	SLU 82	0.22	No
fin.	3	0	-224.46	-2098			1282	482	SLU 82	0.23	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	511	228.57	1282.21	SLV 1	5.61	Si
fin.	2	-864	-550.72	1282.21	SLV 1	2.33	Si
ini.	2	3	48.77	1282.21	SLV 6	26.29	Si
fin.	2	-603	-342.35	1282.21	SLV 6	3.75	Si
ini.	2	-1050	-391.7	1282.21	SLV 13	3.27	Si
fin.	2	114	217.91	1282.21	SLV 13	5.88	Si
ini.	2	-1084	-423.67	1282.21	SLV 16	3.03	Si
fin.	2	184	269.91	1282.21	SLV 16	4.75	Si
ini.	2	3	48.77	1282.21	SLV 5	26.29	Si
fin.	2	-603	-342.35	1282.21	SLV 5	3.75	Si
ini.	2	511	228.57	1282.21	SLV 2	5.61	Si
fin.	2	-864	-550.72	1282.21	SLV 2	2.33	Si
ini.	2	-1084	-423.67	1282.21	SLV 15	3.03	Si
fin.	2	184	269.91	1282.21	SLV 15	4.75	Si
ini.	2	478	196.6	1282.21	SLV 4	6.52	Si
fin.	2	-794	-498.73	1282.21	SLV 4	2.57	Si
ini.	2	478	196.6	1282.21	SLV 3	6.52	Si
fin.	2	-794	-498.73	1282.21	SLV 3	2.57	Si
ini.	2	-1050	-391.7	1282.21	SLV 14	3.27	Si
fin.	2	114	217.91	1282.21	SLV 14	5.88	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-137.31	1876			1923	724	SLV 10	0.39	No
fin.	2	0	-111.76	-1138			1923	724	SLV 10	0.64	No
ini.	2	0	-391.7	2609			1923	724	SLV 14	0.28	No
fin.	2	0	217.91	-189			1923	724	SLV 14	3.82	Si
ini.	2	0	228.57	290			1923	724	SLV 1	2.49	Si
fin.	2	0	-550.72	-2611			1923	724	SLV 1	0.28	No
ini.	2	0	-423.67	2541			1923	724	SLV 16	0.28	No
fin.	2	0	269.91	-102			1923	724	SLV 16	7.08	Si
ini.	2	0	196.6	223			1923	724	SLV 4	3.25	Si
fin.	2	0	-498.73	-2524			1923	724	SLV 4	0.29	No
ini.	2	0	196.6	223			1923	724	SLV 3	3.25	Si
fin.	2	0	-498.73	-2524			1923	724	SLV 3	0.29	No
ini.	2	0	-423.67	2541			1923	724	SLV 15	0.28	No
fin.	2	0	269.91	-102			1923	724	SLV 15	7.08	Si
ini.	2	0	228.57	290			1923	724	SLV 2	2.49	Si
fin.	2	0	-550.72	-2611			1923	724	SLV 2	0.28	No
ini.	2	0	-137.31	1876			1923	724	SLV 9	0.39	No
fin.	2	0	-111.76	-1138			1923	724	SLV 9	0.64	No
ini.	2	0	-391.7	2609			1923	724	SLV 13	0.28	No
fin.	2	0	217.91	-189			1923	724	SLV 13	3.82	Si

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	2.328	SLV 1	Si
V_SLV	0.277	SLV 1	No
PF_SLU	5.216	SLU 81	Si
V_SLU	0.223	SLU 81	No

Trave di accoppiamento 5

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
33.569	-0.169	-0.98	0.41	1.39	32.569	-0.169	-0.98	0.41	1.39	1	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti



fb	fthk	fvk0	fthmedio	τ0	fv0	μ	φ	fvk,lim	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-1452	-91.64	2098.31	SLU 76	22.9	Si
fin.	3	-2222	129.65	2098.31	SLU 76	16.18	Si
ini.	3	-1452	-91.64	2098.31	SLU 75	22.9	Si
fin.	3	-2222	129.65	2098.31	SLU 75	16.18	Si
ini.	3	-1536	-94.12	2098.31	SLU 82	22.29	Si
fin.	3	-2353	142.41	2098.31	SLU 82	14.73	Si
ini.	3	-1536	-94.12	2098.31	SLU 84	22.29	Si
fin.	3	-2353	142.41	2098.31	SLU 84	14.73	Si
ini.	3	-1536	-94.12	2098.31	SLU 83	22.29	Si
fin.	3	-2353	142.41	2098.31	SLU 83	14.73	Si
ini.	3	-1452	-91.64	2098.31	SLU 78	22.9	Si
fin.	3	-2222	129.65	2098.31	SLU 78	16.18	Si
ini.	3	-1536	-94.12	2098.31	SLU 81	22.29	Si
fin.	3	-2353	142.41	2098.31	SLU 81	14.73	Si
ini.	3	-1452	-91.64	2098.31	SLU 79	22.9	Si
fin.	3	-2222	129.65	2098.31	SLU 79	16.18	Si
ini.	3	-1452	-91.64	2098.31	SLU 74	22.9	Si
fin.	3	-2222	129.65	2098.31	SLU 74	16.18	Si
ini.	3	-1452	-91.64	2098.31	SLU 73	22.9	Si
fin.	3	-2222	129.65	2098.31	SLU 73	16.18	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-91.64	-2598			2409	907	SLU 77	0.35	No
fin.	3	0	129.65	4087			2409	907	SLU 77	0.22	No
ini.	3	0	-91.64	-2598			2409	907	SLU 78	0.35	No
fin.	3	0	129.65	4087			2409	907	SLU 78	0.22	No
ini.	3	0	-94.12	-2744			2409	907	SLU 82	0.33	No
fin.	3	0	142.41	4330			2409	907	SLU 82	0.21	No
ini.	3	0	-91.64	-2598			2409	907	SLU 79	0.35	No
fin.	3	0	129.65	4087			2409	907	SLU 79	0.22	No
ini.	3	0	-91.64	-2598			2409	907	SLU 75	0.35	No
fin.	3	0	129.65	4087			2409	907	SLU 75	0.22	No
ini.	3	0	-94.12	-2744			2409	907	SLU 81	0.33	No
fin.	3	0	142.41	4330			2409	907	SLU 81	0.21	No
ini.	3	0	-94.12	-2744			2409	907	SLU 83	0.33	No
fin.	3	0	142.41	4330			2409	907	SLU 83	0.21	No
ini.	3	0	-91.64	-2598			2409	907	SLU 80	0.35	No
fin.	3	0	129.65	4087			2409	907	SLU 80	0.22	No
ini.	3	0	-91.64	-2598			2409	907	SLU 76	0.35	No
fin.	3	0	129.65	4087			2409	907	SLU 76	0.22	No
ini.	3	0	-94.12	-2744			2409	907	SLU 84	0.33	No
fin.	3	0	142.41	4330			2409	907	SLU 84	0.21	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-1416	-142.05	2209.71	SLV 10	15.56	Si
fin.	2	-2145	291.23	2209.71	SLV 10	7.59	Si
ini.	2	-1416	-142.05	2209.71	SLV 9	15.56	Si
fin.	2	-2145	291.23	2209.71	SLV 9	7.59	Si
ini.	2	-2014	361.53	2209.71	SLV 2	6.11	Si
fin.	2	-630	-291.5	2209.71	SLV 2	7.58	Si
ini.	2	-1617	332.41	2209.71	SLV 3	6.65	Si
fin.	2	-434	-344.91	2209.71	SLV 3	6.41	Si
ini.	2	15	-494.61	2209.71	SLV 15	4.47	Si
fin.	2	-2412	455.75	2209.71	SLV 15	4.85	Si
ini.	2	-1617	332.41	2209.71	SLV 4	6.65	Si
fin.	2	-434	-344.91	2209.71	SLV 4	6.41	Si
ini.	2	15	-494.61	2209.71	SLV 16	4.47	Si
fin.	2	-2412	455.75	2209.71	SLV 16	4.85	Si
ini.	2	-2014	361.53	2209.71	SLV 1	6.11	Si
fin.	2	-630	-291.5	2209.71	SLV 1	7.58	Si
ini.	2	-382	-465.49	2209.71	SLV 14	4.75	Si
fin.	2	-2608	509.16	2209.71	SLV 14	4.34	Si
ini.	2	-382	-465.49	2209.71	SLV 13	4.75	Si
fin.	2	-2608	509.16	2209.71	SLV 13	4.34	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	332.41	-3833			3613	1360	SLV 4	0.35	No
fin.	2	0	-344.91	305			3613	1360	SLV 4	4.46	Si
ini.	2	0	-465.49	253			3613	1360	SLV 14	5.37	Si
fin.	2	0	509.16	5285			3613	1360	SLV 14	0.26	No
ini.	2	0	-494.61	515			3613	1360	SLV 15	2.64	Si
fin.	2	0	455.75	4948			3613	1360	SLV 15	0.27	No
ini.	2	0	-142.05	-1574			3613	1360	SLV 10	0.86	No
fin.	2	0	291.23	4054			3613	1360	SLV 10	0.34	No
ini.	2	0	361.53	-4095			3613	1360	SLV 1	0.33	No
fin.	2	0	-291.5	642			3613	1360	SLV 1	2.12	Si
ini.	2	0	-142.05	-1574			3613	1360	SLV 9	0.86	No
fin.	2	0	291.23	4054			3613	1360	SLV 9	0.34	No
ini.	2	0	361.53	-4095			3613	1360	SLV 2	0.33	No
fin.	2	0	-291.5	642			3613	1360	SLV 2	2.12	Si
ini.	2	0	332.41	-3833			3613	1360	SLV 3	0.35	No
fin.	2	0	-344.91	305			3613	1360	SLV 3	4.46	Si



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-465.49	253			3613	1360	SLV 13	5.37	Si
fin.	2	0	509.16	5285			3613	1360	SLV 13	0.26	No
ini.	2	0	-494.61	515			3613	1360	SLV 16	2.64	Si
fin.	2	0	455.75	4948			3613	1360	SLV 16	0.27	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	4.34	SLV 13	Si
V_SLV	0.257	SLV 13	No
PF_SLU	14.734	SLU 81	Si
V_SLU	0.209	SLU 81	No

Trave di accoppiamento 6

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
33.569	-0.169	0.81	1.67	0.86	32.569	-0.169	0.81	1.67	0.86	1	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	f _{hk}	f _{vk0}	f _{hmedio}	t ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-581	-191.67	1170.81	SLU 76	6.11	Si
fin.	3	-448	-98.1	1170.81	SLU 76	11.93	Si
ini.	3	-581	-191.67	1170.81	SLU 73	6.11	Si
fin.	3	-448	-98.1	1170.81	SLU 73	11.93	Si
ini.	3	-646	-204.95	1170.81	SLU 81	5.71	Si
fin.	3	-495	-104.25	1170.81	SLU 81	11.23	Si
ini.	3	-646	-204.95	1170.81	SLU 84	5.71	Si
fin.	3	-495	-104.25	1170.81	SLU 84	11.23	Si
ini.	3	-581	-191.67	1170.81	SLU 75	6.11	Si
fin.	3	-448	-98.1	1170.81	SLU 75	11.93	Si
ini.	3	-581	-191.67	1170.81	SLU 79	6.11	Si
fin.	3	-448	-98.1	1170.81	SLU 79	11.93	Si
ini.	3	-581	-191.67	1170.81	SLU 74	6.11	Si
fin.	3	-448	-98.1	1170.81	SLU 74	11.93	Si
ini.	3	-646	-204.95	1170.81	SLU 82	5.71	Si
fin.	3	-495	-104.25	1170.81	SLU 82	11.23	Si
ini.	3	-646	-204.95	1170.81	SLU 83	5.71	Si
fin.	3	-495	-104.25	1170.81	SLU 83	11.23	Si
ini.	3	-581	-191.67	1170.81	SLU 78	6.11	Si
fin.	3	-448	-98.1	1170.81	SLU 78	11.93	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-191.67	2884			1282	482	SLU 78	0.17	No
fin.	3	0	-98.1	-2578			1282	482	SLU 78	0.19	No
ini.	3	0	-191.67	2884			1282	482	SLU 74	0.17	No
fin.	3	0	-98.1	-2578			1282	482	SLU 74	0.19	No
ini.	3	0	-204.95	3075			1282	482	SLU 81	0.16	No
fin.	3	0	-104.25	-2742			1282	482	SLU 81	0.18	No
ini.	3	0	-191.67	2884			1282	482	SLU 73	0.17	No
fin.	3	0	-98.1	-2578			1282	482	SLU 73	0.19	No
ini.	3	0	-191.67	2884			1282	482	SLU 76	0.17	No
fin.	3	0	-98.1	-2578			1282	482	SLU 76	0.19	No
ini.	3	0	-191.67	2884			1282	482	SLU 79	0.17	No
fin.	3	0	-98.1	-2578			1282	482	SLU 79	0.19	No
ini.	3	0	-204.95	3075			1282	482	SLU 82	0.16	No
fin.	3	0	-104.25	-2742			1282	482	SLU 82	0.18	No
ini.	3	0	-204.95	3075			1282	482	SLU 83	0.16	No
fin.	3	0	-104.25	-2742			1282	482	SLU 83	0.18	No
ini.	3	0	-191.67	2884			1282	482	SLU 75	0.17	No
fin.	3	0	-98.1	-2578			1282	482	SLU 75	0.19	No
ini.	3	0	-204.95	3075			1282	482	SLU 84	0.16	No
fin.	3	0	-104.25	-2742			1282	482	SLU 84	0.18	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	471	156.68	1282.21	SLV 4	8.18	Si
fin.	2	-1332	-308.65	1282.21	SLV 4	4.15	Si
ini.	2	471	156.68	1282.21	SLV 3	8.18	Si
fin.	2	-1332	-308.65	1282.21	SLV 3	4.15	Si
ini.	2	-697	-314.85	1282.21	SLV 10	4.07	Si
fin.	2	228	31.73	1282.21	SLV 10	40.41	Si
ini.	2	-1116	-347.72	1282.21	SLV 16	3.69	Si
fin.	2	659	158.53	1282.21	SLV 16	8.09	Si
ini.	2	-1179	-414.03	1282.21	SLV 14	3.1	Si
fin.	2	782	175.48	1282.21	SLV 14	7.31	Si
ini.	2	408	90.37	1282.21	SLV 1	14.19	Si
fin.	2	-1209	-291.7	1282.21	SLV 1	4.4	Si
ini.	2	-697	-314.85	1282.21	SLV 9	4.07	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
fin.	2	228	31.73	1282.21	SLV 9	40.41	Si
ini.	2	408	90.37	1282.21	SLV 2	14.19	Si
fin.	2	-1209	-291.7	1282.21	SLV 2	4.4	Si
ini.	2	-1116	-347.72	1282.21	SLV 15	3.69	Si
fin.	2	659	158.53	1282.21	SLV 15	8.09	Si
ini.	2	-1179	-414.03	1282.21	SLV 13	3.1	Si
fin.	2	782	175.48	1282.21	SLV 13	7.31	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-314.85	2522			1923	724	SLV 9	0.29	No
fin.	2	0	31.73	-1602			1923	724	SLV 9	0.45	No
ini.	2	0	-414.03	3243			1923	724	SLV 13	0.22	No
fin.	2	0	175.48	-666			1923	724	SLV 13	1.09	Si
ini.	2	0	156.68	642			1923	724	SLV 3	1.13	Si
fin.	2	0	-308.65	-2817			1923	724	SLV 3	0.26	No
ini.	2	0	156.68	642			1923	724	SLV 4	1.13	Si
fin.	2	0	-308.65	-2817			1923	724	SLV 4	0.26	No
ini.	2	0	-347.72	3119			1923	724	SLV 16	0.23	No
fin.	2	0	158.53	-546			1923	724	SLV 16	1.33	Si
ini.	2	0	-347.72	3119			1923	724	SLV 15	0.23	No
fin.	2	0	158.53	-546			1923	724	SLV 15	1.33	Si
ini.	2	0	-414.03	3243			1923	724	SLV 14	0.22	No
fin.	2	0	175.48	-666			1923	724	SLV 14	1.09	Si
ini.	2	0	90.37	767			1923	724	SLV 1	0.94	No
fin.	2	0	-291.7	-2937			1923	724	SLV 1	0.25	No
ini.	2	0	-314.85	2522			1923	724	SLV 10	0.29	No
fin.	2	0	31.73	-1602			1923	724	SLV 10	0.45	No
ini.	2	0	90.37	767			1923	724	SLV 2	0.94	No
fin.	2	0	-291.7	-2937			1923	724	SLV 2	0.25	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	3.097	SLV 13	Si
V_SLV	0.223	SLV 13	No
PF_SLU	5.713	SLU 81	Si
V_SLU	0.157	SLU 81	No

Trave di accoppiamento 7

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
30.808	4.507	1.19	1.67	0.48	31.808	4.507	1.19	1.67	0.48	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-880	-277.47	350.68	SLU 79	1.26	Si
fin.	3	-225	-105.86	350.68	SLU 79	3.31	Si
ini.	3	-880	-277.47	350.68	SLU 77	1.26	Si
fin.	3	-225	-105.86	350.68	SLU 77	3.31	Si
ini.	3	-934	-302.29	350.68	SLU 81	1.16	Si
fin.	3	-236	-119.45	350.68	SLU 81	2.94	Si
ini.	3	-934	-302.29	350.68	SLU 84	1.16	Si
fin.	3	-236	-119.45	350.68	SLU 84	2.94	Si
ini.	3	-880	-277.47	350.68	SLU 78	1.26	Si
fin.	3	-225	-105.86	350.68	SLU 78	3.31	Si
ini.	3	-934	-302.29	350.68	SLU 83	1.16	Si
fin.	3	-236	-119.45	350.68	SLU 83	2.94	Si
ini.	3	-880	-277.47	350.68	SLU 80	1.26	Si
fin.	3	-225	-105.86	350.68	SLU 80	3.31	Si
ini.	3	-880	-277.47	350.68	SLU 76	1.26	Si
fin.	3	-225	-105.86	350.68	SLU 76	3.31	Si
ini.	3	-934	-302.29	350.68	SLU 82	1.16	Si
fin.	3	-236	-119.45	350.68	SLU 82	2.94	Si
ini.	3	-880	-277.47	350.68	SLU 75	1.26	Si
fin.	3	-225	-105.86	350.68	SLU 75	3.31	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-277.47	2016			370	139	SLU 76	0.07	No
fin.	3	0	-105.86	-628			370	139	SLU 76	0.22	No
ini.	3	0	-277.47	2016			370	139	SLU 79	0.07	No
fin.	3	0	-105.86	-628			370	139	SLU 79	0.22	No
ini.	3	0	-302.29	2206			370	139	SLU 82	0.06	No
fin.	3	0	-119.45	-707			370	139	SLU 82	0.2	No
ini.	3	0	-277.47	2016			370	139	SLU 77	0.07	No
fin.	3	0	-105.86	-628			370	139	SLU 77	0.22	No
ini.	3	0	-277.47	2016			370	139	SLU 80	0.07	No
fin.	3	0	-105.86	-628			370	139	SLU 80	0.22	No



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-277.47	2016			370	139	SLU 75	0.07	No
fin.	3	0	-105.86	-628			370	139	SLU 75	0.22	No
ini.	3	0	-277.47	2016			370	139	SLU 78	0.07	No
fin.	3	0	-105.86	-628			370	139	SLU 78	0.22	No
ini.	3	0	-302.29	2206			370	139	SLU 84	0.06	No
fin.	3	0	-119.45	-707			370	139	SLU 84	0.2	No
ini.	3	0	-302.29	2206			370	139	SLU 81	0.06	No
fin.	3	0	-119.45	-707			370	139	SLU 81	0.2	No
ini.	3	0	-302.29	2206			370	139	SLU 83	0.06	No
fin.	3	0	-119.45	-707			370	139	SLU 83	0.2	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-870	-274.75	505.81	SLV 8	1.84	Si
fin.	2	62	-40.56	505.81	SLV 8	12.47	Si
ini.	2	-1187	-336.3	505.81	SLV 4	1.5	Si
fin.	2	-82	18.58	505.81	SLV 4	27.22	Si
ini.	2	-532	-189	505.81	SLV 11	2.68	Si
fin.	2	58	-89.71	505.81	SLV 11	5.64	Si
ini.	2	-1120	-303.32	505.81	SLV 1	1.67	Si
fin.	2	-209	20.13	505.81	SLV 1	25.13	Si
ini.	2	-870	-274.75	505.81	SLV 7	1.84	Si
fin.	2	62	-40.56	505.81	SLV 7	12.47	Si
ini.	2	-648	-164.8	505.81	SLV 6	3.07	Si
fin.	2	-363	-35.41	505.81	SLV 6	14.28	Si
ini.	2	-1120	-303.32	505.81	SLV 2	1.67	Si
fin.	2	-209	20.13	505.81	SLV 2	25.13	Si
ini.	2	-648	-164.8	505.81	SLV 5	3.07	Si
fin.	2	-363	-35.41	505.81	SLV 5	14.28	Si
ini.	2	-1187	-336.3	505.81	SLV 3	1.5	Si
fin.	2	-82	18.58	505.81	SLV 3	27.22	Si
ini.	2	-532	-189	505.81	SLV 12	2.68	Si
fin.	2	58	-89.71	505.81	SLV 12	5.64	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-274.75	1513			555	209	SLV 7	0.14	No
fin.	2	0	-40.56	-325			555	209	SLV 7	0.64	No
ini.	2	0	-336.3	1912			555	209	SLV 3	0.11	No
fin.	2	0	18.58	-87			555	209	SLV 3	2.39	Si
ini.	2	0	-189	1141			555	209	SLV 12	0.18	No
fin.	2	0	-89.71	-504			555	209	SLV 12	0.41	No
ini.	2	0	-336.3	1912			555	209	SLV 4	0.11	No
fin.	2	0	18.58	-87			555	209	SLV 4	2.39	Si
ini.	2	0	-303.32	1882			555	209	SLV 1	0.11	No
fin.	2	0	20.13	-63			555	209	SLV 1	3.3	Si
ini.	2	0	-164.8	1413			555	209	SLV 5	0.15	No
fin.	2	0	-35.41	-244			555	209	SLV 5	0.85	No
ini.	2	0	-274.75	1513			555	209	SLV 8	0.14	No
fin.	2	0	-40.56	-325			555	209	SLV 8	0.64	No
ini.	2	0	-303.32	1882			555	209	SLV 2	0.11	No
fin.	2	0	20.13	-63			555	209	SLV 2	3.3	Si
ini.	2	0	-164.8	1413			555	209	SLV 6	0.15	No
fin.	2	0	-35.41	-244			555	209	SLV 6	0.85	No
ini.	2	0	-189	1141			555	209	SLV 11	0.18	No
fin.	2	0	-89.71	-504			555	209	SLV 11	0.41	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.504	SLV 3	Si
V_SLV	0.109	SLV 3	No
PF_SLU	1.16	SLU 81	Si
V_SLU	0.063	SLU 81	No

Trave di accoppiamento 8

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
30.644	9.502	1.22	1.67	0.45	31.644	9.502	1.22	1.67	0.45	1	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-372	-22.65	453.31	SLU 81	20.01	Si
fin.	3	-448	-62.43	453.31	SLU 81	7.26	Si
ini.	3	-352	-19.97	453.31	SLU 75	22.7	Si
fin.	3	-416	-57.43	453.31	SLU 75	7.89	Si
ini.	3	-352	-19.97	453.31	SLU 76	22.7	Si
fin.	3	-416	-57.43	453.31	SLU 76	7.89	Si
ini.	3	-352	-19.97	453.31	SLU 74	22.7	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
fin.	3	-416	-57.43	453.31	SLU 74	7.89	Si
ini.	3	-372	-22.65	453.31	SLU 83	20.01	Si
fin.	3	-448	-62.43	453.31	SLU 83	7.26	Si
ini.	3	-352	-19.97	453.31	SLU 73	22.7	Si
fin.	3	-416	-57.43	453.31	SLU 73	7.89	Si
ini.	3	-372	-22.65	453.31	SLU 82	20.01	Si
fin.	3	-448	-62.43	453.31	SLU 82	7.26	Si
ini.	3	-352	-19.97	453.31	SLU 78	22.7	Si
fin.	3	-416	-57.43	453.31	SLU 78	7.89	Si
ini.	3	-372	-22.65	453.31	SLU 84	20.01	Si
fin.	3	-448	-62.43	453.31	SLU 84	7.26	Si
ini.	3	-352	-19.97	453.31	SLU 79	22.7	Si
fin.	3	-416	-57.43	453.31	SLU 79	7.89	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-19.97	1262			520	196	SLU 74	0.16	No
fin.	3	0	-57.43	-1145			520	196	SLU 74	0.17	No
ini.	3	0	-22.65	1359			520	196	SLU 82	0.14	No
fin.	3	0	-62.43	-1228			520	196	SLU 82	0.16	No
ini.	3	0	-22.65	1359			520	196	SLU 81	0.14	No
fin.	3	0	-62.43	-1228			520	196	SLU 81	0.16	No
ini.	3	0	-19.97	1262			520	196	SLU 78	0.16	No
fin.	3	0	-57.43	-1145			520	196	SLU 78	0.17	No
ini.	3	0	-19.97	1262			520	196	SLU 75	0.16	No
fin.	3	0	-57.43	-1145			520	196	SLU 75	0.17	No
ini.	3	0	-19.97	1262			520	196	SLU 79	0.16	No
fin.	3	0	-57.43	-1145			520	196	SLU 79	0.17	No
ini.	3	0	-19.97	1262			520	196	SLU 73	0.16	No
fin.	3	0	-57.43	-1145			520	196	SLU 73	0.17	No
ini.	3	0	-22.65	1359			520	196	SLU 83	0.14	No
fin.	3	0	-62.43	-1228			520	196	SLU 83	0.16	No
ini.	3	0	-22.65	1359			520	196	SLU 84	0.14	No
fin.	3	0	-62.43	-1228			520	196	SLU 84	0.16	No
ini.	3	0	-19.97	1262			520	196	SLU 76	0.16	No
fin.	3	0	-57.43	-1145			520	196	SLU 76	0.17	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-590	18.57	564.71	SLV 11	30.41	Si
fin.	2	-365	-59.51	564.71	SLV 11	9.49	Si
ini.	2	-730	27.92	564.71	SLV 7	20.22	Si
fin.	2	-219	-55.49	564.71	SLV 7	10.18	Si
ini.	2	250	-51.45	564.71	SLV 9	10.98	Si
fin.	2	-329	-18.75	564.71	SLV 9	30.11	Si
ini.	2	250	-51.45	564.71	SLV 10	10.98	Si
fin.	2	-329	-18.75	564.71	SLV 10	30.11	Si
ini.	2	110	-42.09	564.71	SLV 5	13.42	Si
fin.	2	-183	-14.73	564.71	SLV 5	38.35	Si
ini.	2	-132	-16.85	564.71	SLV 16	33.51	Si
fin.	2	-523	-49.95	564.71	SLV 16	11.31	Si
ini.	2	-730	27.92	564.71	SLV 8	20.22	Si
fin.	2	-219	-55.49	564.71	SLV 8	10.18	Si
ini.	2	-132	-16.85	564.71	SLV 15	33.51	Si
fin.	2	-523	-49.95	564.71	SLV 15	11.31	Si
ini.	2	-590	18.57	564.71	SLV 12	30.41	Si
fin.	2	-365	-59.51	564.71	SLV 12	9.49	Si
ini.	2	110	-42.09	564.71	SLV 6	13.42	Si
fin.	2	-183	-14.73	564.71	SLV 6	38.35	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-37.86	74			780	293	SLV 14	3.95	Si
fin.	2	0	-37.72	-1109			780	293	SLV 14	0.26	No
ini.	2	0	-37.86	74			780	293	SLV 13	3.95	Si
fin.	2	0	-37.72	-1109			780	293	SLV 13	0.26	No
ini.	2	0	-16.85	776			780	293	SLV 16	0.38	No
fin.	2	0	-49.95	-1217			780	293	SLV 16	0.24	No
ini.	2	0	27.92	2122			780	293	SLV 7	0.14	No
fin.	2	0	-55.49	-821			780	293	SLV 7	0.36	No
ini.	2	0	14.33	1588			780	293	SLV 3	0.18	No
fin.	2	0	-36.52	-414			780	293	SLV 3	0.71	No
ini.	2	0	-16.85	776			780	293	SLV 15	0.38	No
fin.	2	0	-49.95	-1217			780	293	SLV 15	0.24	No
ini.	2	0	18.57	1878			780	293	SLV 11	0.16	No
fin.	2	0	-59.51	-1062			780	293	SLV 11	0.28	No
ini.	2	0	18.57	1878			780	293	SLV 12	0.16	No
fin.	2	0	-59.51	-1062			780	293	SLV 12	0.28	No
ini.	2	0	14.33	1588			780	293	SLV 4	0.18	No
fin.	2	0	-36.52	-414			780	293	SLV 4	0.71	No
ini.	2	0	27.92	2122			780	293	SLV 8	0.14	No
fin.	2	0	-55.49	-821			780	293	SLV 8	0.36	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	9.489	SLV 11	Si
V_SLV	0.138	SLV 7	No
PF_SLU	7.261	SLU 81	Si
V_SLU	0.144	SLU 81	No



Trave di accoppiamento 9

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
35.424	2.847	-0.98	0.41	1.39	35.424	1.847	-0.98	0.41	1.39	1	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb _m	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-2070	269.22	2098.31	SLU 81	7.79	Si
fin.	3	-1440	-234.15	2098.31	SLU 81	8.96	Si
ini.	3	-1959	245.08	2098.31	SLU 75	8.56	Si
fin.	3	-1386	-208.47	2098.31	SLU 75	10.07	Si
ini.	3	-2070	269.22	2098.31	SLU 84	7.79	Si
fin.	3	-1440	-234.15	2098.31	SLU 84	8.96	Si
ini.	3	-1959	245.08	2098.31	SLU 76	8.56	Si
fin.	3	-1386	-208.47	2098.31	SLU 76	10.07	Si
ini.	3	-1959	245.08	2098.31	SLU 73	8.56	Si
fin.	3	-1386	-208.47	2098.31	SLU 73	10.07	Si
ini.	3	-1959	245.08	2098.31	SLU 74	8.56	Si
fin.	3	-1386	-208.47	2098.31	SLU 74	10.07	Si
ini.	3	-2070	269.22	2098.31	SLU 83	7.79	Si
fin.	3	-1440	-234.15	2098.31	SLU 83	8.96	Si
ini.	3	-1959	245.08	2098.31	SLU 78	8.56	Si
fin.	3	-1386	-208.47	2098.31	SLU 78	10.07	Si
ini.	3	-1959	245.08	2098.31	SLU 79	8.56	Si
fin.	3	-1386	-208.47	2098.31	SLU 79	10.07	Si
ini.	3	-2070	269.22	2098.31	SLU 82	7.79	Si
fin.	3	-1440	-234.15	2098.31	SLU 82	8.96	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	245.08	-2485			2409	907	SLU 76	0.36	No
fin.	3	0	-208.47	436			2409	907	SLU 76	2.08	Si
ini.	3	0	245.08	-2485			2409	907	SLU 78	0.36	No
fin.	3	0	-208.47	436			2409	907	SLU 78	2.08	Si
ini.	3	0	245.08	-2485			2409	907	SLU 73	0.36	No
fin.	3	0	-208.47	436			2409	907	SLU 73	2.08	Si
ini.	3	0	245.08	-2485			2409	907	SLU 79	0.36	No
fin.	3	0	-208.47	436			2409	907	SLU 79	2.08	Si
ini.	3	0	269.22	-2692			2409	907	SLU 82	0.34	No
fin.	3	0	-234.15	456			2409	907	SLU 82	1.99	Si
ini.	3	0	245.08	-2485			2409	907	SLU 74	0.36	No
fin.	3	0	-208.47	436			2409	907	SLU 74	2.08	Si
ini.	3	0	245.08	-2485			2409	907	SLU 75	0.36	No
fin.	3	0	-208.47	436			2409	907	SLU 75	2.08	Si
ini.	3	0	269.22	-2692			2409	907	SLU 81	0.34	No
fin.	3	0	-234.15	456			2409	907	SLU 81	1.99	Si
ini.	3	0	269.22	-2692			2409	907	SLU 84	0.34	No
fin.	3	0	-234.15	456			2409	907	SLU 84	1.99	Si
ini.	3	0	269.22	-2692			2409	907	SLU 83	0.34	No
fin.	3	0	-234.15	456			2409	907	SLU 83	1.99	Si

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-480	-463.14	2209.71	SLV 8	4.77	Si
fin.	2	-1212	466.48	2209.71	SLV 8	4.74	Si
ini.	2	-1871	756.88	2209.71	SLV 6	2.92	Si
fin.	2	-242	-790.47	2209.71	SLV 6	2.8	Si
ini.	2	-979	311.14	2209.71	SLV 2	7.1	Si
fin.	2	26	-435.3	2209.71	SLV 2	5.08	Si
ini.	2	-979	311.14	2209.71	SLV 1	7.1	Si
fin.	2	26	-435.3	2209.71	SLV 1	5.08	Si
ini.	2	-2218	772.93	2209.71	SLV 10	2.86	Si
fin.	2	-763	-717.82	2209.71	SLV 10	3.08	Si
ini.	2	-827	-447.08	2209.71	SLV 12	4.94	Si
fin.	2	-1732	539.13	2209.71	SLV 12	4.1	Si
ini.	2	-2218	772.93	2209.71	SLV 9	2.86	Si
fin.	2	-763	-717.82	2209.71	SLV 9	3.08	Si
ini.	2	-480	-463.14	2209.71	SLV 7	4.77	Si
fin.	2	-1212	466.48	2209.71	SLV 7	4.74	Si
ini.	2	-827	-447.08	2209.71	SLV 11	4.94	Si
fin.	2	-1732	539.13	2209.71	SLV 11	4.1	Si
ini.	2	-1871	756.88	2209.71	SLV 5	2.92	Si
fin.	2	-242	-790.47	2209.71	SLV 5	2.8	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	772.93	-4010			3613	1360	SLV 9	0.34	No
fin.	2	0	-717.82	-1746			3613	1360	SLV 9	0.78	No



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	364.66	-2707			3613	1360	SLV 13	0.5	No
fin.	2	0	-193.13	-100			3613	1360	SLV 13	13.58	Si
ini.	2	0	-463.14	762			3613	1360	SLV 7	1.78	Si
fin.	2	0	466.48	2358			3613	1360	SLV 7	0.58	No
ini.	2	0	756.88	-3768			3613	1360	SLV 5	0.36	No
fin.	2	0	-790.47	-1884			3613	1360	SLV 5	0.72	No
ini.	2	0	-447.08	520			3613	1360	SLV 11	2.62	Si
fin.	2	0	539.13	2496			3613	1360	SLV 11	0.54	No
ini.	2	0	772.93	-4010			3613	1360	SLV 10	0.34	No
fin.	2	0	-717.82	-1746			3613	1360	SLV 10	0.78	No
ini.	2	0	-463.14	762			3613	1360	SLV 8	1.78	Si
fin.	2	0	466.48	2358			3613	1360	SLV 8	0.58	No
ini.	2	0	-447.08	520			3613	1360	SLV 12	2.62	Si
fin.	2	0	539.13	2496			3613	1360	SLV 12	0.54	No
ini.	2	0	364.66	-2707			3613	1360	SLV 14	0.5	No
fin.	2	0	-193.13	-100			3613	1360	SLV 14	13.58	Si
ini.	2	0	756.88	-3768			3613	1360	SLV 6	0.36	No
fin.	2	0	-790.47	-1884			3613	1360	SLV 6	0.72	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	2.795	SLV 5	Si
V_SLV	0.339	SLV 9	No
PF_SLU	7.794	SLU 81	Si
V_SLU	0.337	SLU 81	No

Trave di accoppiamento 10

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
35.424	2.847	0.81	1.67	0.86	35.424	1.847	0.81	1.67	0.86	1	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	93	-35.96	1170.81	SLU 78	32.56	Si
fin.	3	-133	-253.12	1170.81	SLU 78	4.63	Si
ini.	3	93	-35.96	1170.81	SLU 79	32.56	Si
fin.	3	-133	-253.12	1170.81	SLU 79	4.63	Si
ini.	3	93	-35.96	1170.81	SLU 76	32.56	Si
fin.	3	-133	-253.12	1170.81	SLU 76	4.63	Si
ini.	3	133	-31.45	1170.81	SLU 84	37.23	Si
fin.	3	-136	-278.89	1170.81	SLU 84	4.2	Si
ini.	3	93	-35.96	1170.81	SLU 74	32.56	Si
fin.	3	-133	-253.12	1170.81	SLU 74	4.63	Si
ini.	3	133	-31.45	1170.81	SLU 81	37.23	Si
fin.	3	-136	-278.89	1170.81	SLU 81	4.2	Si
ini.	3	93	-35.96	1170.81	SLU 75	32.56	Si
fin.	3	-133	-253.12	1170.81	SLU 75	4.63	Si
ini.	3	93	-35.96	1170.81	SLU 73	32.56	Si
fin.	3	-133	-253.12	1170.81	SLU 73	4.63	Si
ini.	3	133	-31.45	1170.81	SLU 82	37.23	Si
fin.	3	-136	-278.89	1170.81	SLU 82	4.2	Si
ini.	3	133	-31.45	1170.81	SLU 83	37.23	Si
fin.	3	-136	-278.89	1170.81	SLU 83	4.2	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-35.96	1294			1282	482	SLU 80	0.37	No
fin.	3	0	-253.12	-1934			1282	482	SLU 80	0.25	No
ini.	3	0	-35.96	1294			1282	482	SLU 78	0.37	No
fin.	3	0	-253.12	-1934			1282	482	SLU 78	0.25	No
ini.	3	0	-35.96	1294			1282	482	SLU 76	0.37	No
fin.	3	0	-253.12	-1934			1282	482	SLU 76	0.25	No
ini.	3	0	-35.96	1294			1282	482	SLU 75	0.37	No
fin.	3	0	-253.12	-1934			1282	482	SLU 75	0.25	No
ini.	3	0	-31.45	1341			1282	482	SLU 83	0.36	No
fin.	3	0	-278.89	-2068			1282	482	SLU 83	0.23	No
ini.	3	0	-31.45	1341			1282	482	SLU 84	0.36	No
fin.	3	0	-278.89	-2068			1282	482	SLU 84	0.23	No
ini.	3	0	-31.45	1341			1282	482	SLU 82	0.36	No
fin.	3	0	-278.89	-2068			1282	482	SLU 82	0.23	No
ini.	3	0	-31.45	1341			1282	482	SLU 81	0.36	No
fin.	3	0	-278.89	-2068			1282	482	SLU 81	0.23	No
ini.	3	0	-35.96	1294			1282	482	SLU 79	0.37	No
fin.	3	0	-253.12	-1934			1282	482	SLU 79	0.25	No
ini.	3	0	-35.96	1294			1282	482	SLU 77	0.37	No
fin.	3	0	-253.12	-1934			1282	482	SLU 77	0.25	No



Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	508	264.41	1282.21	SLV 6	4.85	Si
fin.	2	-591	-451.11	1282.21	SLV 6	2.84	Si
ini.	2	-471	-331.68	1282.21	SLV 11	3.87	Si
fin.	2	398	132.76	1282.21	SLV 11	9.66	Si
ini.	2	508	264.41	1282.21	SLV 5	4.85	Si
fin.	2	-591	-451.11	1282.21	SLV 5	2.84	Si
ini.	2	570	178.64	1282.21	SLV 13	7.18	Si
fin.	2	-441	-436.32	1282.21	SLV 13	2.94	Si
ini.	2	570	178.64	1282.21	SLV 14	7.18	Si
fin.	2	-441	-436.32	1282.21	SLV 14	2.94	Si
ini.	2	-471	-331.68	1282.21	SLV 12	3.87	Si
fin.	2	398	132.76	1282.21	SLV 12	9.66	Si
ini.	2	-693	-399.3	1282.21	SLV 8	3.21	Si
fin.	2	507	237.11	1282.21	SLV 8	5.41	Si
ini.	2	731	332.04	1282.21	SLV 10	3.86	Si
fin.	2	-699	-555.46	1282.21	SLV 10	2.31	Si
ini.	2	731	332.04	1282.21	SLV 9	3.86	Si
fin.	2	-699	-555.46	1282.21	SLV 9	2.31	Si
ini.	2	-693	-399.3	1282.21	SLV 7	3.21	Si
fin.	2	507	237.11	1282.21	SLV 7	5.41	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-399.3	2029			1923	724	SLV 7	0.36	No
fin.	2	0	237.11	-20			1923	724	SLV 7	36.66	Si
ini.	2	0	264.41	-191			1923	724	SLV 5	3.79	Si
fin.	2	0	-451.11	-2455			1923	724	SLV 5	0.29	No
ini.	2	0	178.64	638			1923	724	SLV 14	1.13	Si
fin.	2	0	-436.32	-1886			1923	724	SLV 14	0.38	No
ini.	2	0	-331.68	2053			1923	724	SLV 11	0.35	No
fin.	2	0	132.76	-150			1923	724	SLV 11	4.81	Si
ini.	2	0	332.04	-167			1923	724	SLV 9	4.33	Si
fin.	2	0	-555.46	-2585			1923	724	SLV 9	0.28	No
ini.	2	0	264.41	-191			1923	724	SLV 6	3.79	Si
fin.	2	0	-451.11	-2455			1923	724	SLV 6	0.29	No
ini.	2	0	-331.68	2053			1923	724	SLV 12	0.35	No
fin.	2	0	132.76	-150			1923	724	SLV 12	4.81	Si
ini.	2	0	-399.3	2029			1923	724	SLV 8	0.36	No
fin.	2	0	237.11	-20			1923	724	SLV 8	36.66	Si
ini.	2	0	178.64	638			1923	724	SLV 13	1.13	Si
fin.	2	0	-436.32	-1886			1923	724	SLV 13	0.38	No
ini.	2	0	332.04	-167			1923	724	SLV 10	4.33	Si
fin.	2	0	-555.46	-2585			1923	724	SLV 10	0.28	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF SLV		2.308	SLV 9
V SLV	0.28		SLV 9
PF SLU		4.198	SLU 81
V SLU	0.233		SLU 81

Trave di accoppiamento 11

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
35.424	7.497	-0.98	0.41	1.39	35.424	6.497	-0.98	0.41	1.39	1	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fhk	fvk0	fhmmedio	τ0	fv0	μ	φ	fvk,lim	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-1129	-139.31	2098.31	SLU 39	15.06	Si
fin.	3	-1932	118.39	2098.31	SLU 39	17.72	Si
ini.	3	-1129	-139.31	2098.31	SLU 40	15.06	Si
fin.	3	-1932	118.39	2098.31	SLU 40	17.72	Si
ini.	3	-1129	-139.31	2098.31	SLU 41	15.06	Si
fin.	3	-1932	118.39	2098.31	SLU 41	17.72	Si
ini.	3	-1300	-138.62	2098.31	SLU 62	15.14	Si
fin.	3	-2109	115.16	2098.31	SLU 62	18.22	Si
ini.	3	-1300	-138.62	2098.31	SLU 63	15.14	Si
fin.	3	-2109	115.16	2098.31	SLU 63	18.22	Si
ini.	3	-1129	-139.31	2098.31	SLU 42	15.06	Si
fin.	3	-1932	118.39	2098.31	SLU 42	17.72	Si
ini.	3	-1374	-154.44	2098.31	SLU 82	13.59	Si
fin.	3	-2276	130.99	2098.31	SLU 82	16.02	Si
ini.	3	-1374	-154.44	2098.31	SLU 83	13.59	Si
fin.	3	-2276	130.99	2098.31	SLU 83	16.02	Si
ini.	3	-1374	-154.44	2098.31	SLU 81	13.59	Si
fin.	3	-2276	130.99	2098.31	SLU 81	16.02	Si
ini.	3	-1374	-154.44	2098.31	SLU 84	13.59	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
fin.	3	-2276	130.99	2098.31	SLU 84	16.02	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-154.44	-2492			2409	907	SLU 83	0.36	No
fin.	3	0	130.99	4239			2409	907	SLU 83	0.21	No
ini.	3	0	-154.44	-2492			2409	907	SLU 84	0.36	No
fin.	3	0	130.99	4239			2409	907	SLU 84	0.21	No
ini.	3	0	-154.44	-2492			2409	907	SLU 82	0.36	No
fin.	3	0	130.99	4239			2409	907	SLU 82	0.21	No
ini.	3	0	-154.44	-2492			2409	907	SLU 81	0.36	No
fin.	3	0	130.99	4239			2409	907	SLU 81	0.21	No
ini.	3	0	-137.94	-2393			2409	907	SLU 78	0.38	No
fin.	3	0	118.26	3964			2409	907	SLU 78	0.23	No
ini.	3	0	-137.94	-2393			2409	907	SLU 80	0.38	No
fin.	3	0	118.26	3964			2409	907	SLU 80	0.23	No
ini.	3	0	-137.94	-2393			2409	907	SLU 79	0.38	No
fin.	3	0	118.26	3964			2409	907	SLU 79	0.23	No
ini.	3	0	-137.94	-2393			2409	907	SLU 75	0.38	No
fin.	3	0	118.26	3964			2409	907	SLU 75	0.23	No
ini.	3	0	-137.94	-2393			2409	907	SLU 77	0.38	No
fin.	3	0	118.26	3964			2409	907	SLU 77	0.23	No
ini.	3	0	-137.94	-2393			2409	907	SLU 76	0.38	No
fin.	3	0	118.26	3964			2409	907	SLU 76	0.23	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-1533	245.47	2209.71	SLV 6	9	Si
fin.	2	-357	-311.03	2209.71	SLV 6	7.1	Si
ini.	2	-1590	-124	2209.71	SLV 15	17.82	Si
fin.	2	-2110	271.64	2209.71	SLV 15	8.13	Si
ini.	2	-2065	284.27	2209.71	SLV 9	7.77	Si
fin.	2	-558	-256.13	2209.71	SLV 9	8.63	Si
ini.	2	-379	-413.49	2209.71	SLV 12	5.34	Si
fin.	2	-2583	457.28	2209.71	SLV 12	4.83	Si
ini.	2	-379	-413.49	2209.71	SLV 11	5.34	Si
fin.	2	-2583	457.28	2209.71	SLV 11	4.83	Si
ini.	2	-1590	-124	2209.71	SLV 16	17.82	Si
fin.	2	-2110	271.64	2209.71	SLV 16	8.13	Si
ini.	2	153	-452.3	2209.71	SLV 7	4.89	Si
fin.	2	-2382	402.37	2209.71	SLV 7	5.49	Si
ini.	2	-2065	284.27	2209.71	SLV 10	7.77	Si
fin.	2	-558	-256.13	2209.71	SLV 10	8.63	Si
ini.	2	-1533	245.47	2209.71	SLV 5	9	Si
fin.	2	-357	-311.03	2209.71	SLV 5	7.1	Si
ini.	2	153	-452.3	2209.71	SLV 8	4.89	Si
fin.	2	-2382	402.37	2209.71	SLV 8	5.49	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	284.27	-3958			3613	1360	SLV 10	0.34	No
fin.	2	0	-256.13	488			3613	1360	SLV 10	2.78	Si
ini.	2	0	-452.3	556			3613	1360	SLV 7	2.45	Si
fin.	2	0	402.37	4847			3613	1360	SLV 7	0.28	No
ini.	2	0	245.47	-3729			3613	1360	SLV 5	0.36	No
fin.	2	0	-311.03	169			3613	1360	SLV 5	8.04	Si
ini.	2	0	-124	-1440			3613	1360	SLV 15	0.94	No
fin.	2	0	271.64	3901			3613	1360	SLV 15	0.35	No
ini.	2	0	-413.49	327			3613	1360	SLV 12	4.16	Si
fin.	2	0	457.28	5166			3613	1360	SLV 12	0.26	No
ini.	2	0	284.27	-3958			3613	1360	SLV 9	0.34	No
fin.	2	0	-256.13	488			3613	1360	SLV 9	2.78	Si
ini.	2	0	-124	-1440			3613	1360	SLV 16	0.94	No
fin.	2	0	271.64	3901			3613	1360	SLV 16	0.35	No
ini.	2	0	-413.49	327			3613	1360	SLV 11	4.16	Si
fin.	2	0	457.28	5166			3613	1360	SLV 11	0.26	No
ini.	2	0	245.47	-3729			3613	1360	SLV 6	0.36	No
fin.	2	0	-311.03	169			3613	1360	SLV 6	8.04	Si
ini.	2	0	-452.3	556			3613	1360	SLV 8	2.45	Si
fin.	2	0	402.37	4847			3613	1360	SLV 8	0.28	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	4.832	SLV 11	Si
V_SLV	0.263	SLV 11	No
PF_SLU	13.587	SLU 81	Si
V_SLU	0.214	SLU 81	No

Trave di accoppiamento 12

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
35.424	7.497	0.81	1.67	0.86	35.424	6.497	0.81	1.67	0.86	1	0.45	3500



Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fhk	fvk0	fhmmedio	τ0	fv0	μ	φ	fvk,lim	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-280	-220.52	1170.81	SLU 78	5.31	Si
fin.	3	137	-79.54	1170.81	SLU 78	14.72	Si
ini.	3	-280	-220.52	1170.81	SLU 74	5.31	Si
fin.	3	137	-79.54	1170.81	SLU 74	14.72	Si
ini.	3	-299	-241.7	1170.81	SLU 82	4.84	Si
fin.	3	191	-82.28	1170.81	SLU 82	14.23	Si
ini.	3	-280	-220.52	1170.81	SLU 75	5.31	Si
fin.	3	137	-79.54	1170.81	SLU 75	14.72	Si
ini.	3	-299	-241.7	1170.81	SLU 83	4.84	Si
fin.	3	191	-82.28	1170.81	SLU 83	14.23	Si
ini.	3	-280	-220.52	1170.81	SLU 76	5.31	Si
fin.	3	137	-79.54	1170.81	SLU 76	14.72	Si
ini.	3	-280	-220.52	1170.81	SLU 73	5.31	Si
fin.	3	137	-79.54	1170.81	SLU 73	14.72	Si
ini.	3	-299	-241.7	1170.81	SLU 84	4.84	Si
fin.	3	191	-82.28	1170.81	SLU 84	14.23	Si
ini.	3	-299	-241.7	1170.81	SLU 81	4.84	Si
fin.	3	191	-82.28	1170.81	SLU 81	14.23	Si
ini.	3	-280	-220.52	1170.81	SLU 79	5.31	Si
fin.	3	137	-79.54	1170.81	SLU 79	14.72	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-220.52	2672			1282	482	SLU 74	0.18	No
fin.	3	0	-79.54	-1955			1282	482	SLU 74	0.25	No
ini.	3	0	-220.52	2672			1282	482	SLU 79	0.18	No
fin.	3	0	-79.54	-1955			1282	482	SLU 79	0.25	No
ini.	3	0	-220.52	2672			1282	482	SLU 78	0.18	No
fin.	3	0	-79.54	-1955			1282	482	SLU 78	0.25	No
ini.	3	0	-220.52	2672			1282	482	SLU 76	0.18	No
fin.	3	0	-79.54	-1955			1282	482	SLU 76	0.25	No
ini.	3	0	-220.52	2672			1282	482	SLU 75	0.18	No
fin.	3	0	-79.54	-1955			1282	482	SLU 75	0.25	No
ini.	3	0	-241.7	2884			1282	482	SLU 83	0.17	No
fin.	3	0	-82.28	-2069			1282	482	SLU 83	0.23	No
ini.	3	0	-241.7	2884			1282	482	SLU 81	0.17	No
fin.	3	0	-82.28	-2069			1282	482	SLU 81	0.23	No
ini.	3	0	-241.7	2884			1282	482	SLU 84	0.17	No
fin.	3	0	-82.28	-2069			1282	482	SLU 84	0.23	No
ini.	3	0	-241.7	2884			1282	482	SLU 82	0.17	No
fin.	3	0	-82.28	-2069			1282	482	SLU 82	0.23	No
ini.	3	0	-220.52	2672			1282	482	SLU 73	0.18	No
fin.	3	0	-79.54	-1955			1282	482	SLU 73	0.25	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-1019	-329.41	1282.21	SLV 8	3.89	Si
fin.	2	858	147.53	1282.21	SLV 8	8.69	Si
ini.	2	-1098	-413.99	1282.21	SLV 12	3.1	Si
fin.	2	1143	163.8	1282.21	SLV 12	7.83	Si
ini.	2	720	133.26	1282.21	SLV 6	9.62	Si
fin.	2	-1074	-277.98	1282.21	SLV 6	4.61	Si
ini.	2	-583	-350.72	1282.21	SLV 15	3.66	Si
fin.	2	799	33.87	1282.21	SLV 15	37.86	Si
ini.	2	640	48.68	1282.21	SLV 10	26.34	Si
fin.	2	-789	-261.7	1282.21	SLV 10	4.9	Si
ini.	2	640	48.68	1282.21	SLV 9	26.34	Si
fin.	2	-789	-261.7	1282.21	SLV 9	4.9	Si
ini.	2	-1019	-329.41	1282.21	SLV 7	3.89	Si
fin.	2	858	147.53	1282.21	SLV 7	8.69	Si
ini.	2	-1098	-413.99	1282.21	SLV 11	3.1	Si
fin.	2	1143	163.8	1282.21	SLV 11	7.83	Si
ini.	2	-583	-350.72	1282.21	SLV 16	3.66	Si
fin.	2	799	33.87	1282.21	SLV 16	37.86	Si
ini.	2	720	133.26	1282.21	SLV 5	9.62	Si
fin.	2	-1074	-277.98	1282.21	SLV 5	4.61	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-350.72	2431			1923	724	SLV 16	0.3	No
fin.	2	0	33.87	-1235			1923	724	SLV 16	0.59	No
ini.	2	0	133.26	454			1923	724	SLV 6	1.6	Si
fin.	2	0	-277.98	-2352			1923	724	SLV 6	0.31	No
ini.	2	0	-413.99	3075			1923	724	SLV 11	0.24	No
fin.	2	0	163.8	-343			1923	724	SLV 11	2.11	Si
ini.	2	0	-329.41	2894			1923	724	SLV 7	0.25	No
fin.	2	0	147.53	-218			1923	724	SLV 7	3.31	Si
ini.	2	0	48.68	634			1923	724	SLV 9	1.14	Si
fin.	2	0	-261.7	-2477			1923	724	SLV 9	0.29	No
ini.	2	0	133.26	454			1923	724	SLV 5	1.6	Si
fin.	2	0	-277.98	-2352			1923	724	SLV 5	0.31	No
ini.	2	0	48.68	634			1923	724	SLV 10	1.14	Si



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
fin.	2	0	-261.7	-2477			1923	724	SLV 10	0.29	No
ini.	2	0	-413.99	3075			1923	724	SLV 12	0.24	No
fin.	2	0	163.8	-343			1923	724	SLV 12	2.11	Si
ini.	2	0	-329.41	2894			1923	724	SLV 8	0.25	No
fin.	2	0	147.53	-218			1923	724	SLV 8	3.31	Si
ini.	2	0	-350.72	2431			1923	724	SLV 15	0.3	No
fin.	2	0	33.87	-1235			1923	724	SLV 15	0.59	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	3.097	SLV 11	Si
V_SLV	0.235	SLV 11	No
PF_SLU	4.844	SLU 81	Si
V_SLU	0.167	SLU 81	No

Trave di accoppiamento 13

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
25.882	8.663	3.67	5.52	1.85	26.552	9.405	3.67	5.52	1.85	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fhk	fvk0	fhmmedio	t0	fv0	μ	φ	fvk,lim	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-8	173.28	2736.22	SLU 83	15.79	Si
fin.	3	-8	165.97	2736.22	SLU 83	16.49	Si
ini.	3	-7	157.3	2736.22	SLU 73	17.39	Si
fin.	3	-7	152.54	2736.22	SLU 73	17.94	Si
ini.	3	-7	158.59	2736.22	SLU 61	17.25	Si
fin.	3	-7	152.4	2736.22	SLU 61	17.95	Si
ini.	3	-8	173.28	2736.22	SLU 84	15.79	Si
fin.	3	-8	165.97	2736.22	SLU 84	16.49	Si
ini.	3	-7	158.59	2736.22	SLU 60	17.25	Si
fin.	3	-7	152.4	2736.22	SLU 60	17.95	Si
ini.	3	-8	173.28	2736.22	SLU 82	15.79	Si
fin.	3	-8	165.97	2736.22	SLU 82	16.49	Si
ini.	3	-7	158.59	2736.22	SLU 63	17.25	Si
fin.	3	-7	152.4	2736.22	SLU 63	17.95	Si
ini.	3	-7	158.59	2736.22	SLU 62	17.25	Si
fin.	3	-7	152.4	2736.22	SLU 62	17.95	Si
ini.	3	-7	157.3	2736.22	SLU 74	17.39	Si
fin.	3	-7	152.54	2736.22	SLU 74	17.94	Si
ini.	3	-8	173.28	2736.22	SLU 81	15.79	Si
fin.	3	-8	165.97	2736.22	SLU 81	16.49	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	158.59	1586			2137	804	SLU 60	0.51	No
fin.	3	0	152.4	-1572			2137	804	SLU 60	0.51	No
ini.	3	0	173.28	1738			2137	804	SLU 83	0.46	No
fin.	3	0	165.97	-1721			2137	804	SLU 83	0.47	No
ini.	3	0	158.59	1586			2137	804	SLU 62	0.51	No
fin.	3	0	152.4	-1572			2137	804	SLU 62	0.51	No
ini.	3	0	157.3	1583			2137	804	SLU 73	0.51	No
fin.	3	0	152.54	-1566			2137	804	SLU 73	0.51	No
ini.	3	0	157.3	1583			2137	804	SLU 74	0.51	No
fin.	3	0	152.54	-1566			2137	804	SLU 74	0.51	No
ini.	3	0	173.28	1738			2137	804	SLU 82	0.46	No
fin.	3	0	165.97	-1721			2137	804	SLU 82	0.47	No
ini.	3	0	158.59	1586			2137	804	SLU 61	0.51	No
fin.	3	0	152.4	-1572			2137	804	SLU 61	0.51	No
ini.	3	0	173.28	1738			2137	804	SLU 84	0.46	No
fin.	3	0	165.97	-1721			2137	804	SLU 84	0.47	No
ini.	3	0	173.28	1738			2137	804	SLU 81	0.46	No
fin.	3	0	165.97	-1721			2137	804	SLU 81	0.47	No
ini.	3	0	158.59	1586			2137	804	SLU 63	0.51	No
fin.	3	0	152.4	-1572			2137	804	SLU 63	0.51	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-516	2643.43	2903.31	SLV 15	1.1	Si
fin.	2	-570	-1178.54	2903.31	SLV 15	2.46	Si
ini.	2	508	-2443.92	2903.31	SLV 2	1.19	Si
fin.	2	562	1376.94	2903.31	SLV 2	2.11	Si
ini.	2	-516	2643.43	2903.31	SLV 16	1.1	Si
fin.	2	-570	-1178.54	2903.31	SLV 16	2.46	Si
ini.	2	-849	2347.91	2903.31	SLV 13	1.24	Si
fin.	2	-693	-572.23	2903.31	SLV 13	5.07	Si
ini.	2	-356	-1111.56	2903.31	SLV 5	2.61	Si
fin.	2	-20	1402.08	2903.31	SLV 5	2.07	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-356	-1111.56	2903.31	SLV 6	2.61	Si
fin.	2	-20	1402.08	2903.31	SLV 6	2.07	Si
ini.	2	-849	2347.91	2903.31	SLV 14	1.24	Si
fin.	2	-693	-572.23	2903.31	SLV 14	5.07	Si
ini.	2	508	-2443.92	2903.31	SLV 1	1.19	Si
fin.	2	562	1376.94	2903.31	SLV 1	2.11	Si
ini.	2	841	-2148.39	2903.31	SLV 3	1.35	Si
fin.	2	685	770.64	2903.31	SLV 3	3.77	Si
ini.	2	841	-2148.39	2903.31	SLV 4	1.35	Si
fin.	2	685	770.64	2903.31	SLV 4	3.77	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-2148.39	3522			3206	1207	SLV 4	0.34	No
fin.	2	0	770.64	1703			3206	1207	SLV 4	0.71	No
ini.	2	0	1311.07	-1343			3206	1207	SLV 12	0.9	No
fin.	2	0	-1203.68	-3637			3206	1207	SLV 12	0.33	No
ini.	2	0	1311.07	-1343			3206	1207	SLV 11	0.9	No
fin.	2	0	-1203.68	-3637			3206	1207	SLV 11	0.33	No
ini.	2	0	-2443.92	4401			3206	1207	SLV 1	0.27	No
fin.	2	0	1376.94	2710			3206	1207	SLV 1	0.45	No
ini.	2	0	2347.91	-1503			3206	1207	SLV 13	0.8	No
fin.	2	0	-572.23	-3697			3206	1207	SLV 13	0.33	No
ini.	2	0	2643.43	-2383			3206	1207	SLV 16	0.51	No
fin.	2	0	-1178.54	-4704			3206	1207	SLV 16	0.26	No
ini.	2	0	-2443.92	4401			3206	1207	SLV 2	0.27	No
fin.	2	0	1376.94	2710			3206	1207	SLV 2	0.45	No
ini.	2	0	2347.91	-1503			3206	1207	SLV 14	0.8	No
fin.	2	0	-572.23	-3697			3206	1207	SLV 14	0.33	No
ini.	2	0	-2148.39	3522			3206	1207	SLV 3	0.34	No
fin.	2	0	770.64	1703			3206	1207	SLV 3	0.71	No
ini.	2	0	2643.43	-2383			3206	1207	SLV 15	0.51	No
fin.	2	0	-1178.54	-4704			3206	1207	SLV 15	0.26	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.098	SLV 15	Si
V_SLV	0.256	SLV 15	No
PF_SLU	15.791	SLU 81	Si
V_SLU	0.463	SLU 81	No

Trave di accoppiamento 14

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
29.728	4.507	3.71	5.52	1.81	30.628	4.507	3.71	5.52	1.81	0.9	0.18	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-2229	-402.58	2332.04	SLU 41	5.79	Si
fin.	3	-2229	2699.52	2332.04	SLU 41	0.86	No
ini.	3	-2229	-402.58	2332.04	SLU 42	5.79	Si
fin.	3	-2229	2699.52	2332.04	SLU 42	0.86	No
ini.	3	-2229	-402.58	2332.04	SLU 39	5.79	Si
fin.	3	-2229	2699.52	2332.04	SLU 39	0.86	No
ini.	3	-2349	-421.54	2332.04	SLU 83	5.53	Si
fin.	3	-2349	2778.74	2332.04	SLU 83	0.84	No
ini.	3	-2229	-402.58	2332.04	SLU 40	5.79	Si
fin.	3	-2229	2699.52	2332.04	SLU 40	0.86	No
ini.	3	-2349	-421.54	2332.04	SLU 84	5.53	Si
fin.	3	-2349	2778.74	2332.04	SLU 84	0.84	No
ini.	3	-2349	-421.54	2332.04	SLU 81	5.53	Si
fin.	3	-2349	2778.74	2332.04	SLU 81	0.84	No
ini.	3	-2349	-421.54	2332.04	SLU 82	5.53	Si
fin.	3	-2349	2778.74	2332.04	SLU 82	0.84	No
ini.	3	-1987	-359.97	2332.04	SLU 62	6.48	Si
fin.	3	-1987	2354.28	2332.04	SLU 62	0.99	No
ini.	3	-1987	-359.97	2332.04	SLU 63	6.48	Si
fin.	3	-1987	2354.28	2332.04	SLU 63	0.99	No

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-359.97	3317			1255	472	SLU 63	0.14	No
fin.	3	0	2354.28	2667			1255	472	SLU 63	0.18	No
ini.	3	0	-402.58	3698			1255	472	SLU 42	0.13	No
fin.	3	0	2699.52	3169			1255	472	SLU 42	0.15	No
ini.	3	0	-402.58	3698			1255	472	SLU 41	0.13	No
fin.	3	0	2699.52	3169			1255	472	SLU 41	0.15	No
ini.	3	0	-421.54	3872			1255	472	SLU 82	0.12	No



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
fin.	3	0	2778.74	3199			1255	472	SLU 82	0.15	No
ini.	3	0	-421.54	3872			1255	472	SLU 83	0.12	No
fin.	3	0	2778.74	3199			1255	472	SLU 83	0.15	No
ini.	3	0	-402.58	3698			1255	472	SLU 40	0.13	No
fin.	3	0	2699.52	3169			1255	472	SLU 40	0.15	No
ini.	3	0	-421.54	3872			1255	472	SLU 81	0.12	No
fin.	3	0	2778.74	3199			1255	472	SLU 81	0.15	No
ini.	3	0	-402.58	3698			1255	472	SLU 39	0.13	No
fin.	3	0	2699.52	3169			1255	472	SLU 39	0.15	No
ini.	3	0	-359.97	3317			1255	472	SLU 62	0.14	No
fin.	3	0	2354.28	2667			1255	472	SLU 62	0.18	No
ini.	3	0	-421.54	3872			1255	472	SLU 84	0.12	No
fin.	3	0	2778.74	3199			1255	472	SLU 84	0.15	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-1262	-314.52	2610.52	SLV 8	8.3	Si
fin.	2	-1103	1528.02	2610.52	SLV 8	1.71	Si
ini.	2	-1132	-189.22	2610.52	SLV 5	13.8	Si
fin.	2	-1147	1099.58	2610.52	SLV 5	2.37	Si
ini.	2	-1132	-189.22	2610.52	SLV 6	13.8	Si
fin.	2	-1147	1099.58	2610.52	SLV 6	2.37	Si
ini.	2	-1337	-371.27	2610.52	SLV 2	7.03	Si
fin.	2	-1124	1572	2610.52	SLV 2	1.66	Si
ini.	2	-1125	-196.07	2610.52	SLV 12	13.31	Si
fin.	2	-1110	1251.62	2610.52	SLV 12	2.09	Si
ini.	2	-1377	-408.86	2610.52	SLV 3	6.38	Si
fin.	2	-1110	1700.53	2610.52	SLV 3	1.54	Si
ini.	2	-1262	-314.52	2610.52	SLV 7	8.3	Si
fin.	2	-1103	1528.02	2610.52	SLV 7	1.71	Si
ini.	2	-1125	-196.07	2610.52	SLV 11	13.31	Si
fin.	2	-1110	1251.62	2610.52	SLV 11	2.09	Si
ini.	2	-1337	-371.27	2610.52	SLV 1	7.03	Si
fin.	2	-1124	1572	2610.52	SLV 1	1.66	Si
ini.	2	-1377	-408.86	2610.52	SLV 4	6.38	Si
fin.	2	-1110	1700.53	2610.52	SLV 4	1.54	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-408.86	2698			1882	708	SLV 4	0.26	No
fin.	2	0	1700.53	2139			1882	708	SLV 4	0.33	No
ini.	2	0	-196.07	1765			1882	708	SLV 11	0.4	No
fin.	2	0	1251.62	1311			1882	708	SLV 11	0.54	No
ini.	2	0	-196.07	1765			1882	708	SLV 12	0.4	No
fin.	2	0	1251.62	1311			1882	708	SLV 12	0.54	No
ini.	2	0	-189.22	1755			1882	708	SLV 6	0.4	No
fin.	2	0	1099.58	1184			1882	708	SLV 6	0.6	No
ini.	2	0	-371.27	2540			1882	708	SLV 2	0.28	No
fin.	2	0	1572	1957			1882	708	SLV 2	0.36	No
ini.	2	0	-314.52	2281			1882	708	SLV 7	0.31	No
fin.	2	0	1528.02	1791			1882	708	SLV 7	0.4	No
ini.	2	0	-314.52	2281			1882	708	SLV 8	0.31	No
fin.	2	0	1528.02	1791			1882	708	SLV 8	0.4	No
ini.	2	0	-408.86	2698			1882	708	SLV 3	0.26	No
fin.	2	0	1700.53	2139			1882	708	SLV 3	0.33	No
ini.	2	0	-189.22	1755			1882	708	SLV 5	0.4	No
fin.	2	0	1099.58	1184			1882	708	SLV 5	0.6	No
ini.	2	0	-371.27	2540			1882	708	SLV 1	0.28	No
fin.	2	0	1572	1957			1882	708	SLV 1	0.36	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.535	SLV 3	Si
V_SLV	0.263	SLV 3	No
PF_SLU	0.839	SLU 81	No
V_SLU	0.122	SLU 81	No

Trave di accoppiamento 15

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
28.92	-0.169	1.67	2.67	1	27.92	-0.169	1.67	2.67	1	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb _m	f _{tk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-505	67.3	1248.72	SLU 82	18.55	Si
fin.	3	-388	17.21	1248.72	SLU 82	72.55	Si
ini.	3	-452	59.82	1248.72	SLU 63	20.88	Si
fin.	3	-353	19.25	1248.72	SLU 63	64.87	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-451	61.68	1248.72	SLU 41	20.25	Si
fin.	3	-340	10.73	1248.72	SLU 41	116.33	Si
ini.	3	-451	61.68	1248.72	SLU 39	20.25	Si
fin.	3	-340	10.73	1248.72	SLU 39	116.33	Si
ini.	3	-451	61.68	1248.72	SLU 42	20.25	Si
fin.	3	-340	10.73	1248.72	SLU 42	116.33	Si
ini.	3	-505	67.3	1248.72	SLU 83	18.55	Si
fin.	3	-388	17.21	1248.72	SLU 83	72.55	Si
ini.	3	-451	61.68	1248.72	SLU 40	20.25	Si
fin.	3	-340	10.73	1248.72	SLU 40	116.33	Si
ini.	3	-505	67.3	1248.72	SLU 81	18.55	Si
fin.	3	-388	17.21	1248.72	SLU 81	72.55	Si
ini.	3	-505	67.3	1248.72	SLU 84	18.55	Si
fin.	3	-388	17.21	1248.72	SLU 84	72.55	Si
ini.	3	-452	59.82	1248.72	SLU 62	20.88	Si
fin.	3	-353	19.25	1248.72	SLU 62	64.87	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	59.82	-405			1155	435	SLU 60	1.07	Si
fin.	3	0	19.25	112			1155	435	SLU 60	3.89	Si
ini.	3	0	59.82	-405			1155	435	SLU 61	1.07	Si
fin.	3	0	19.25	112			1155	435	SLU 61	3.89	Si
ini.	3	0	59.23	-393			1155	435	SLU 74	1.11	Si
fin.	3	0	19.16	103			1155	435	SLU 74	4.21	Si
ini.	3	0	67.3	-431			1155	435	SLU 81	1.01	Si
fin.	3	0	17.21	100			1155	435	SLU 81	4.36	Si
ini.	3	0	67.3	-431			1155	435	SLU 84	1.01	Si
fin.	3	0	17.21	100			1155	435	SLU 84	4.36	Si
ini.	3	0	59.82	-405			1155	435	SLU 63	1.07	Si
fin.	3	0	19.25	112			1155	435	SLU 63	3.89	Si
ini.	3	0	59.82	-405			1155	435	SLU 62	1.07	Si
fin.	3	0	19.25	112			1155	435	SLU 62	3.89	Si
ini.	3	0	67.3	-431			1155	435	SLU 82	1.01	Si
fin.	3	0	17.21	100			1155	435	SLU 82	4.36	Si
ini.	3	0	67.3	-431			1155	435	SLU 83	1.01	Si
fin.	3	0	17.21	100			1155	435	SLU 83	4.36	Si
ini.	3	0	59.23	-393			1155	435	SLU 73	1.11	Si
fin.	3	0	19.16	103			1155	435	SLU 73	4.21	Si

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-1	-123.91	1415.81	SLV 14	11.43	Si
fin.	2	-520	220.19	1415.81	SLV 14	6.43	Si
ini.	2	-390	14.95	1415.81	SLV 12	94.7	Si
fin.	2	-711	115.41	1415.81	SLV 12	12.27	Si
ini.	2	-464	178.24	1415.81	SLV 2	7.94	Si
fin.	2	274	-205.89	1415.81	SLV 2	6.88	Si
ini.	2	-106	-108.63	1415.81	SLV 16	13.03	Si
fin.	2	-736	240.66	1415.81	SLV 16	5.88	Si
ini.	2	-464	178.24	1415.81	SLV 1	7.94	Si
fin.	2	274	-205.89	1415.81	SLV 1	6.88	Si
ini.	2	-390	14.95	1415.81	SLV 11	94.7	Si
fin.	2	-711	115.41	1415.81	SLV 11	12.27	Si
ini.	2	-568	193.52	1415.81	SLV 3	7.32	Si
fin.	2	58	-185.42	1415.81	SLV 3	7.64	Si
ini.	2	-568	193.52	1415.81	SLV 4	7.32	Si
fin.	2	58	-185.42	1415.81	SLV 4	7.64	Si
ini.	2	-1	-123.91	1415.81	SLV 13	11.43	Si
fin.	2	-520	220.19	1415.81	SLV 13	6.43	Si
ini.	2	-106	-108.63	1415.81	SLV 15	13.03	Si
fin.	2	-736	240.66	1415.81	SLV 15	5.88	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	193.52	-968			1733	652	SLV 4	0.67	No
fin.	2	0	-185.42	-708			1733	652	SLV 4	0.92	No
ini.	2	0	-108.63	575			1733	652	SLV 16	1.13	Si
fin.	2	0	240.66	789			1733	652	SLV 16	0.83	No
ini.	2	0	178.24	-1080			1733	652	SLV 1	0.6	No
fin.	2	0	-205.89	-618			1733	652	SLV 1	1.06	Si
ini.	2	0	193.52	-968			1733	652	SLV 3	0.67	No
fin.	2	0	-185.42	-708			1733	652	SLV 3	0.92	No
ini.	2	0	54.66	-670			1733	652	SLV 6	0.97	No
fin.	2	0	-80.64	11			1733	652	SLV 6	58.12	Si
ini.	2	0	-108.63	575			1733	652	SLV 15	1.13	Si
fin.	2	0	240.66	789			1733	652	SLV 15	0.83	No
ini.	2	0	-123.91	463			1733	652	SLV 13	1.41	Si
fin.	2	0	220.19	879			1733	652	SLV 13	0.74	No
ini.	2	0	178.24	-1080			1733	652	SLV 2	0.6	No
fin.	2	0	-205.89	-618			1733	652	SLV 2	1.06	Si
ini.	2	0	-123.91	463			1733	652	SLV 14	1.41	Si
fin.	2	0	220.19	879			1733	652	SLV 14	0.74	No
ini.	2	0	54.66	-670			1733	652	SLV 5	0.97	No
fin.	2	0	-80.64	11			1733	652	SLV 5	58.12	Si

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF, SLV	5.883	SLV 15	Si



Stato limite	Coeff.s.	Comb.	Verifica
V SLV	0.604	SLV 1	No
PF SLU	18.555	SLU 81	Si
V SLU	1.008	SLU 81	Si

Trave di accoppiamento 16

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
28.92	-0.169	4.57	5.52	0.95	27.92	-0.169	4.57	5.52	0.95	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fthk	fvk0	fthmedio	t0	fv0	μ	φ	fvk,lim	E	G	FC
120000				9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	304	-27.25	1161.22	SLU 42	42.62	Si
fin.	3	304	-116.82	1161.22	SLU 42	9.94	Si
ini.	3	299	-29.42	1161.22	SLU 83	39.47	Si
fin.	3	299	-111.12	1161.22	SLU 83	10.45	Si
ini.	3	304	-27.25	1161.22	SLU 39	42.62	Si
fin.	3	304	-116.82	1161.22	SLU 39	9.94	Si
ini.	3	259	-23.99	1161.22	SLU 21	48.4	Si
fin.	3	259	-92.09	1161.22	SLU 21	12.61	Si
ini.	3	304	-27.25	1161.22	SLU 40	42.62	Si
fin.	3	304	-116.82	1161.22	SLU 40	9.94	Si
ini.	3	299	-29.42	1161.22	SLU 81	39.47	Si
fin.	3	299	-111.12	1161.22	SLU 81	10.45	Si
ini.	3	299	-29.42	1161.22	SLU 84	39.47	Si
fin.	3	299	-111.12	1161.22	SLU 84	10.45	Si
ini.	3	259	-23.99	1161.22	SLU 20	48.4	Si
fin.	3	259	-92.09	1161.22	SLU 20	12.61	Si
ini.	3	304	-27.25	1161.22	SLU 41	42.62	Si
fin.	3	304	-116.82	1161.22	SLU 41	9.94	Si
ini.	3	299	-29.42	1161.22	SLU 82	39.47	Si
fin.	3	299	-111.12	1161.22	SLU 82	10.45	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-29.42	182			1043	392	SLU 83	2.15	Si
fin.	3	0	-111.12	-435			1043	392	SLU 83	0.9	No
ini.	3	0	-29.42	182			1043	392	SLU 82	2.15	Si
fin.	3	0	-111.12	-435			1043	392	SLU 82	0.9	No
ini.	3	0	-25.51	203			1043	392	SLU 75	1.93	Si
fin.	3	0	-86.27	-414			1043	392	SLU 75	0.95	No
ini.	3	0	-25.51	203			1043	392	SLU 78	1.93	Si
fin.	3	0	-86.27	-414			1043	392	SLU 78	0.95	No
ini.	3	0	-25.51	203			1043	392	SLU 79	1.93	Si
fin.	3	0	-86.27	-414			1043	392	SLU 79	0.95	No
ini.	3	0	-25.51	203			1043	392	SLU 76	1.93	Si
fin.	3	0	-86.27	-414			1043	392	SLU 76	0.95	No
ini.	3	0	-25.51	203			1043	392	SLU 77	1.93	Si
fin.	3	0	-86.27	-414			1043	392	SLU 77	0.95	No
ini.	3	0	-29.42	182			1043	392	SLU 81	2.15	Si
fin.	3	0	-111.12	-435			1043	392	SLU 81	0.9	No
ini.	3	0	-25.51	203			1043	392	SLU 80	1.93	Si
fin.	3	0	-86.27	-414			1043	392	SLU 80	0.95	No
ini.	3	0	-29.42	182			1043	392	SLU 84	2.15	Si
fin.	3	0	-111.12	-435			1043	392	SLU 84	0.9	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-488	9.71	1328.31	SLV 8	136.83	Si
fin.	2	-446	-100.76	1328.31	SLV 8	13.18	Si
ini.	2	199	-167.43	1328.31	SLV 14	7.93	Si
fin.	2	116	150.19	1328.31	SLV 14	8.84	Si
ini.	2	-16	138.43	1328.31	SLV 3	9.6	Si
fin.	2	66	-215.97	1328.31	SLV 3	6.15	Si
ini.	2	-16	138.43	1328.31	SLV 4	9.6	Si
fin.	2	66	-215.97	1328.31	SLV 4	6.15	Si
ini.	2	344	152.72	1328.31	SLV 2	8.7	Si
fin.	2	415	-207.44	1328.31	SLV 2	6.4	Si
ini.	2	-162	-181.72	1328.31	SLV 16	7.31	Si
fin.	2	-233	141.66	1328.31	SLV 16	9.38	Si
ini.	2	344	152.72	1328.31	SLV 1	8.7	Si
fin.	2	415	-207.44	1328.31	SLV 1	6.4	Si
ini.	2	-162	-181.72	1328.31	SLV 15	7.31	Si
fin.	2	-233	141.66	1328.31	SLV 15	9.38	Si
ini.	2	199	-167.43	1328.31	SLV 13	7.93	Si
fin.	2	116	150.19	1328.31	SLV 13	8.84	Si
ini.	2	-488	9.71	1328.31	SLV 7	136.83	Si
fin.	2	-446	-100.76	1328.31	SLV 7	13.18	Si



Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-167.43	420			1564	589	SLV 13	1.4	Si
fin.	2	0	150.19	-34			1564	589	SLV 13	17.49	Si
ini.	2	0	-181.72	495			1564	589	SLV 15	1.19	Si
fin.	2	0	141.66	42			1564	589	SLV 15	13.97	Si
ini.	2	0	-181.72	495			1564	589	SLV 16	1.19	Si
fin.	2	0	141.66	42			1564	589	SLV 16	13.97	Si
ini.	2	0	138.43	-52			1564	589	SLV 4	11.3	Si
fin.	2	0	-215.97	-546			1564	589	SLV 4	1.08	Si
ini.	2	0	-167.43	420			1564	589	SLV 14	1.4	Si
fin.	2	0	150.19	-34			1564	589	SLV 14	17.49	Si
ini.	2	0	152.72	-127			1564	589	SLV 1	4.63	Si
fin.	2	0	-207.44	-622			1564	589	SLV 1	0.95	No
ini.	2	0	138.43	-52			1564	589	SLV 3	11.3	Si
fin.	2	0	-215.97	-546			1564	589	SLV 3	1.08	Si
ini.	2	0	152.72	-127			1564	589	SLV 2	4.63	Si
fin.	2	0	-207.44	-622			1564	589	SLV 2	0.95	No
ini.	2	0	57.34	-23			1564	589	SLV 6	25.22	Si
fin.	2	0	-72.31	-504			1564	589	SLV 6	1.17	Si
ini.	2	0	57.34	-23			1564	589	SLV 5	25.22	Si
fin.	2	0	-72.31	-504			1564	589	SLV 5	1.17	Si

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	6.15	SLV 3	Si
V_SLV	0.947	SLV 1	No
PF_SLU	9.94	SLU 39	Si
V_SLU	0.902	SLU 81	No

Trave di accoppiamento 17

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
29.969	-0.169	1.67	3.67	2	29.469	-0.169	1.67	3.67	2	0.5	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-259	149.55	2998.72	SLU 75	20.05	Si
fin.	3	-227	-34.18	2998.72	SLU 75	87.74	Si
ini.	3	-289	168.49	2998.72	SLU 81	17.8	Si
fin.	3	-239	-59.78	2998.72	SLU 81	50.17	Si
ini.	3	-259	149.55	2998.72	SLU 77	20.05	Si
fin.	3	-227	-34.18	2998.72	SLU 77	87.74	Si
ini.	3	-253	154.91	2998.72	SLU 42	19.36	Si
fin.	3	-198	-77.24	2998.72	SLU 42	38.83	Si
ini.	3	-289	168.49	2998.72	SLU 84	17.8	Si
fin.	3	-239	-59.78	2998.72	SLU 84	50.17	Si
ini.	3	-289	168.49	2998.72	SLU 83	17.8	Si
fin.	3	-239	-59.78	2998.72	SLU 83	50.17	Si
ini.	3	-253	154.91	2998.72	SLU 41	19.36	Si
fin.	3	-198	-77.24	2998.72	SLU 41	38.83	Si
ini.	3	-253	154.91	2998.72	SLU 39	19.36	Si
fin.	3	-198	-77.24	2998.72	SLU 39	38.83	Si
ini.	3	-289	168.49	2998.72	SLU 82	17.8	Si
fin.	3	-239	-59.78	2998.72	SLU 82	50.17	Si
ini.	3	-253	154.91	2998.72	SLU 40	19.36	Si
fin.	3	-198	-77.24	2998.72	SLU 40	38.83	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	168.49	-1782			2311	870	SLU 82	0.49	No
fin.	3	0	-59.78	875			2311	870	SLU 82	0.99	No
ini.	3	0	154.91	-1637			2311	870	SLU 41	0.53	No
fin.	3	0	-77.24	655			2311	870	SLU 41	1.33	Si
ini.	3	0	168.49	-1782			2311	870	SLU 84	0.49	No
fin.	3	0	-59.78	875			2311	870	SLU 84	0.99	No
ini.	3	0	154.91	-1637			2311	870	SLU 40	0.53	No
fin.	3	0	-77.24	655			2311	870	SLU 40	1.33	Si
ini.	3	0	146.79	-1578			2311	870	SLU 60	0.55	No
fin.	3	0	-36.39	873			2311	870	SLU 60	1	No
ini.	3	0	146.79	-1578			2311	870	SLU 61	0.55	No
fin.	3	0	-36.39	873			2311	870	SLU 61	1	No
ini.	3	0	154.91	-1637			2311	870	SLU 39	0.53	No
fin.	3	0	-77.24	655			2311	870	SLU 39	1.33	Si
ini.	3	0	168.49	-1782			2311	870	SLU 83	0.49	No
fin.	3	0	-59.78	875			2311	870	SLU 83	0.99	No
ini.	3	0	154.91	-1637			2311	870	SLU 42	0.53	No
fin.	3	0	-77.24	655			2311	870	SLU 42	1.33	Si
ini.	3	0	168.49	-1782			2311	870	SLU 81	0.49	No



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
fin.	3	0	-59.78	875			2311	870	SLU 81	0.99	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	198	42.48	3165.81	SLV 14	74.53	Si
fin.	2	-16	64.19	3165.81	SLV 14	49.32	Si
ini.	2	-523	135.33	3165.81	SLV 3	23.39	Si
fin.	2	-301	-48.73	3165.81	SLV 3	64.96	Si
ini.	2	-433	225.2	3165.81	SLV 6	14.06	Si
fin.	2	-209	18.11	3165.81	SLV 6	174.78	Si
ini.	2	-433	225.2	3165.81	SLV 5	14.06	Si
fin.	2	-209	18.11	3165.81	SLV 5	174.78	Si
ini.	2	-612	202.69	3165.81	SLV 2	15.62	Si
fin.	2	-305	-33.69	3165.81	SLV 2	93.96	Si
ini.	2	-612	202.69	3165.81	SLV 1	15.62	Si
fin.	2	-305	-33.69	3165.81	SLV 1	93.96	Si
ini.	2	-189	177.13	3165.81	SLV 10	17.87	Si
fin.	2	-122	47.48	3165.81	SLV 10	66.68	Si
ini.	2	-523	135.33	3165.81	SLV 4	23.39	Si
fin.	2	-301	-48.73	3165.81	SLV 4	64.96	Si
ini.	2	198	42.48	3165.81	SLV 13	74.53	Si
fin.	2	-16	64.19	3165.81	SLV 13	49.32	Si
ini.	2	-189	177.13	3165.81	SLV 9	17.87	Si
fin.	2	-122	47.48	3165.81	SLV 9	66.68	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	225.2	-1906			3466	1304	SLV 5	0.68	No
fin.	2	0	18.11	223			3466	1304	SLV 5	5.85	Si
ini.	2	0	42.48	-1			3466	1304	SLV 13	1174.88	Si
fin.	2	0	64.19	1382			3466	1304	SLV 13	0.94	No
ini.	2	0	225.2	-1906			3466	1304	SLV 6	0.68	No
fin.	2	0	18.11	223			3466	1304	SLV 6	5.85	Si
ini.	2	0	202.69	-2227			3466	1304	SLV 1	0.59	No
fin.	2	0	-33.69	-105			3466	1304	SLV 1	12.39	Si
ini.	2	0	135.33	-1834			3466	1304	SLV 4	0.71	No
fin.	2	0	-48.73	60			3466	1304	SLV 4	21.92	Si
ini.	2	0	135.33	-1834			3466	1304	SLV 3	0.71	No
fin.	2	0	-48.73	60			3466	1304	SLV 3	21.92	Si
ini.	2	0	202.69	-2227			3466	1304	SLV 2	0.59	No
fin.	2	0	-33.69	-105			3466	1304	SLV 2	12.39	Si
ini.	2	0	-24.88	392			3466	1304	SLV 16	3.33	Si
fin.	2	0	49.15	1547			3466	1304	SLV 16	0.84	No
ini.	2	0	42.48	-1			3466	1304	SLV 14	1174.88	Si
fin.	2	0	64.19	1382			3466	1304	SLV 14	0.94	No
ini.	2	0	-24.88	392			3466	1304	SLV 15	3.33	Si
fin.	2	0	49.15	1547			3466	1304	SLV 15	0.84	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV		SLV 5	Si
V_SLV	0.586	SLV 1	No
PF_SLU	17.797	SLU 81	Si
V_SLU	0.488	SLU 81	No

Trave di accoppiamento 18

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
29.969	-0.169	4.47	5.52	1.05	29.469	-0.169	4.47	5.52	1.05	0.5	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fhk	fvk0	fmedlo	t0	fv0	μ	φ	fvk,lim	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	223	131.72	1336.22	SLU 81	10.14	Si
fin.	3	223	-66.91	1336.22	SLU 81	19.97	Si
ini.	3	209	138.22	1336.22	SLU 39	9.67	Si
fin.	3	209	-65.64	1336.22	SLU 39	20.36	Si
ini.	3	209	138.22	1336.22	SLU 41	9.67	Si
fin.	3	209	-65.64	1336.22	SLU 41	20.36	Si
ini.	3	209	138.22	1336.22	SLU 42	9.67	Si
fin.	3	209	-65.64	1336.22	SLU 42	20.36	Si
ini.	3	191	109.9	1336.22	SLU 20	12.16	Si
fin.	3	191	-55.85	1336.22	SLU 20	23.93	Si
ini.	3	209	138.22	1336.22	SLU 40	9.67	Si
fin.	3	209	-65.64	1336.22	SLU 40	20.36	Si
ini.	3	223	131.72	1336.22	SLU 83	10.14	Si
fin.	3	223	-66.91	1336.22	SLU 83	19.97	Si
ini.	3	191	109.9	1336.22	SLU 21	12.16	Si
fin.	3	191	-55.85	1336.22	SLU 21	23.93	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	223	131.72	1336.22	SLU 82	10.14	Si
fin.	3	223	-66.91	1336.22	SLU 82	19.97	Si
ini.	3	223	131.72	1336.22	SLU 84	10.14	Si
fin.	3	223	-66.91	1336.22	SLU 84	19.97	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	131.72	-172			1213	457	SLU 81	2.65	Si
fin.	3	0	-66.91	-590			1213	457	SLU 81	0.77	No
ini.	3	0	131.72	-172			1213	457	SLU 82	2.65	Si
fin.	3	0	-66.91	-590			1213	457	SLU 82	0.77	No
ini.	3	0	138.22	-234			1213	457	SLU 42	1.95	Si
fin.	3	0	-65.64	-557			1213	457	SLU 42	0.82	No
ini.	3	0	138.22	-234			1213	457	SLU 39	1.95	Si
fin.	3	0	-65.64	-557			1213	457	SLU 39	0.82	No
ini.	3	0	103.41	-98			1213	457	SLU 62	4.68	Si
fin.	3	0	-57.12	-512			1213	457	SLU 62	0.89	No
ini.	3	0	131.72	-172			1213	457	SLU 84	2.65	Si
fin.	3	0	-66.91	-590			1213	457	SLU 84	0.77	No
ini.	3	0	138.22	-234			1213	457	SLU 41	1.95	Si
fin.	3	0	-65.64	-557			1213	457	SLU 41	0.82	No
ini.	3	0	131.72	-172			1213	457	SLU 83	2.65	Si
fin.	3	0	-66.91	-590			1213	457	SLU 83	0.77	No
ini.	3	0	103.41	-98			1213	457	SLU 63	4.68	Si
fin.	3	0	-57.12	-512			1213	457	SLU 63	0.89	No
ini.	3	0	138.22	-234			1213	457	SLU 40	1.95	Si
fin.	3	0	-65.64	-557			1213	457	SLU 40	0.82	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	509	101.61	1503.31	SLV 6	14.79	Si
fin.	2	679	-14.51	1503.31	SLV 6	103.58	Si
ini.	2	-24	207.99	1503.31	SLV 4	7.23	Si
fin.	2	-43	114.79	1503.31	SLV 4	13.1	Si
ini.	2	220	-130.71	1503.31	SLV 14	11.5	Si
fin.	2	238	-167.42	1503.31	SLV 14	8.98	Si
ini.	2	-27	-137.4	1503.31	SLV 16	10.94	Si
fin.	2	-105	-150.62	1503.31	SLV 16	9.98	Si
ini.	2	220	-130.71	1503.31	SLV 13	11.5	Si
fin.	2	238	-167.42	1503.31	SLV 13	8.98	Si
ini.	2	-27	-137.4	1503.31	SLV 15	10.94	Si
fin.	2	-105	-150.62	1503.31	SLV 15	9.98	Si
ini.	2	222	214.69	1503.31	SLV 2	7	Si
fin.	2	300	97.98	1503.31	SLV 2	15.34	Si
ini.	2	222	214.69	1503.31	SLV 1	7	Si
fin.	2	300	97.98	1503.31	SLV 1	15.34	Si
ini.	2	-24	207.99	1503.31	SLV 3	7.23	Si
fin.	2	-43	114.79	1503.31	SLV 3	13.1	Si
ini.	2	509	101.61	1503.31	SLV 5	14.79	Si
fin.	2	679	-14.51	1503.31	SLV 5	103.58	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-2	16			1820	685	SLV 10	42.78	Si
fin.	2	0	-94.13	-331			1820	685	SLV 10	2.07	Si
ini.	2	0	101.61	-104			1820	685	SLV 6	6.61	Si
fin.	2	0	-14.51	-454			1820	685	SLV 6	1.51	Si
ini.	2	0	-2	16			1820	685	SLV 9	42.78	Si
fin.	2	0	-94.13	-331			1820	685	SLV 9	2.07	Si
ini.	2	0	101.61	-104			1820	685	SLV 5	6.61	Si
fin.	2	0	-14.51	-454			1820	685	SLV 5	1.51	Si
ini.	2	0	207.99	-131			1820	685	SLV 3	5.25	Si
fin.	2	0	114.79	-448			1820	685	SLV 3	1.53	Si
ini.	2	0	214.69	-182			1820	685	SLV 1	3.75	Si
fin.	2	0	97.98	-517			1820	685	SLV 1	1.32	Si
ini.	2	0	-137.4	268			1820	685	SLV 16	2.56	Si
fin.	2	0	-150.62	-38			1820	685	SLV 16	17.93	Si
ini.	2	0	-137.4	268			1820	685	SLV 15	2.56	Si
fin.	2	0	-150.62	-38			1820	685	SLV 15	17.93	Si
ini.	2	0	214.69	-182			1820	685	SLV 2	3.75	Si
fin.	2	0	97.98	-517			1820	685	SLV 2	1.32	Si
ini.	2	0	207.99	-131			1820	685	SLV 4	5.25	Si
fin.	2	0	114.79	-448			1820	685	SLV 4	1.53	Si

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	7.002	SLV 1	Si
V_SLV	1.323	SLV 1	Si
PF_SLU	9.668	SLU 39	Si
V_SLU	0.774	SLU 81	No

Trave di accoppiamento 19

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)



Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
33.569	-0.169	1.67	2.67	1	32.569	-0.169	1.67	2.67	1	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	f _{hk}	f _{vk0}	f _{hmedio}	t ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-309	88.79	1248.72	SLU 77	14.06	Si
fin.	3	-442	97.49	1248.72	SLU 77	12.81	Si
ini.	3	-348	94.37	1248.72	SLU 82	13.23	Si
fin.	3	-499	108.35	1248.72	SLU 82	11.53	Si
ini.	3	-348	94.37	1248.72	SLU 84	13.23	Si
fin.	3	-499	108.35	1248.72	SLU 84	11.53	Si
ini.	3	-318	80.58	1248.72	SLU 39	15.5	Si
fin.	3	-456	97.64	1248.72	SLU 39	12.79	Si
ini.	3	-318	80.58	1248.72	SLU 42	15.5	Si
fin.	3	-456	97.64	1248.72	SLU 42	12.79	Si
ini.	3	-318	80.58	1248.72	SLU 40	15.5	Si
fin.	3	-456	97.64	1248.72	SLU 40	12.79	Si
ini.	3	-348	94.37	1248.72	SLU 81	13.23	Si
fin.	3	-499	108.35	1248.72	SLU 81	11.53	Si
ini.	3	-309	88.79	1248.72	SLU 78	14.06	Si
fin.	3	-442	97.49	1248.72	SLU 78	12.81	Si
ini.	3	-348	94.37	1248.72	SLU 83	13.23	Si
fin.	3	-499	108.35	1248.72	SLU 83	11.53	Si
ini.	3	-318	80.58	1248.72	SLU 41	15.5	Si
fin.	3	-456	97.64	1248.72	SLU 41	12.79	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	86.88	-659			1155	435	SLU 62	0.66	No
fin.	3	0	96.31	820			1155	435	SLU 62	0.53	No
ini.	3	0	86.88	-659			1155	435	SLU 61	0.66	No
fin.	3	0	96.31	820			1155	435	SLU 61	0.53	No
ini.	3	0	88.79	-643			1155	435	SLU 75	0.68	No
fin.	3	0	97.49	803			1155	435	SLU 75	0.54	No
ini.	3	0	94.37	-668			1155	435	SLU 82	0.65	No
fin.	3	0	108.35	861			1155	435	SLU 82	0.5	No
ini.	3	0	86.88	-659			1155	435	SLU 60	0.66	No
fin.	3	0	96.31	820			1155	435	SLU 60	0.53	No
ini.	3	0	88.79	-643			1155	435	SLU 74	0.68	No
fin.	3	0	97.49	803			1155	435	SLU 74	0.54	No
ini.	3	0	86.88	-659			1155	435	SLU 63	0.66	No
fin.	3	0	96.31	820			1155	435	SLU 63	0.53	No
ini.	3	0	94.37	-668			1155	435	SLU 83	0.65	No
fin.	3	0	108.35	861			1155	435	SLU 83	0.5	No
ini.	3	0	94.37	-668			1155	435	SLU 81	0.65	No
fin.	3	0	108.35	861			1155	435	SLU 81	0.5	No
ini.	3	0	94.37	-668			1155	435	SLU 84	0.65	No
fin.	3	0	108.35	861			1155	435	SLU 84	0.5	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	497	-62.04	1415.81	SLV 13	22.82	Si
fin.	2	-603	185.87	1415.81	SLV 13	7.62	Si
ini.	2	497	-62.04	1415.81	SLV 14	22.82	Si
fin.	2	-603	185.87	1415.81	SLV 14	7.62	Si
ini.	2	279	-54.9	1415.81	SLV 16	25.79	Si
fin.	2	-497	151.94	1415.81	SLV 16	9.32	Si
ini.	2	-648	175.64	1415.81	SLV 2	8.06	Si
fin.	2	-30	-31.74	1415.81	SLV 2	44.6	Si
ini.	2	-867	182.78	1415.81	SLV 4	7.75	Si
fin.	2	77	-65.67	1415.81	SLV 4	21.56	Si
ini.	2	351	12.82	1415.81	SLV 10	110.45	Si
fin.	2	-527	149.28	1415.81	SLV 10	9.48	Si
ini.	2	279	-54.9	1415.81	SLV 15	25.79	Si
fin.	2	-497	151.94	1415.81	SLV 15	9.32	Si
ini.	2	-648	175.64	1415.81	SLV 1	8.06	Si
fin.	2	-30	-31.74	1415.81	SLV 1	44.6	Si
ini.	2	351	12.82	1415.81	SLV 9	110.45	Si
fin.	2	-527	149.28	1415.81	SLV 9	9.48	Si
ini.	2	-867	182.78	1415.81	SLV 3	7.75	Si
fin.	2	77	-65.67	1415.81	SLV 3	21.56	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	182.78	-1029			1733	652	SLV 4	0.63	No
fin.	2	0	-65.67	-321			1733	652	SLV 4	2.03	Si
ini.	2	0	12.82	-565			1733	652	SLV 10	1.15	Si
fin.	2	0	149.28	1089			1733	652	SLV 10	0.6	No
ini.	2	0	-54.9	279			1733	652	SLV 16	2.34	Si
fin.	2	0	151.94	1216			1733	652	SLV 16	0.54	No
ini.	2	0	175.64	-1207			1733	652	SLV 1	0.54	No
fin.	2	0	-31.74	-131			1733	652	SLV 1	4.97	Si
ini.	2	0	-54.9	279			1733	652	SLV 15	2.34	Si



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
fin.	2	0	151.94	1216			1733	652	SLV 15	0.54	No
ini.	2	0	-62.04	100			1733	652	SLV 13	6.5	Si
fin.	2	0	185.87	1405			1733	652	SLV 13	0.46	No
ini.	2	0	-62.04	100			1733	652	SLV 14	6.5	Si
fin.	2	0	185.87	1405			1733	652	SLV 14	0.46	No
ini.	2	0	175.64	-1207			1733	652	SLV 2	0.54	No
fin.	2	0	-31.74	-131			1733	652	SLV 2	4.97	Si
ini.	2	0	12.82	-565			1733	652	SLV 9	1.15	Si
fin.	2	0	149.28	1089			1733	652	SLV 9	0.6	No
ini.	2	0	182.78	-1029			1733	652	SLV 3	0.63	No
fin.	2	0	-65.67	-321			1733	652	SLV 3	2.03	Si

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	7.617	SLV 13	Si
V_SLV	0.464	SLV 13	No
PF_SLU	11.525	SLU 81	Si
V_SLU	0.505	SLU 81	No

Trave di accoppiamento 20

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
33.569	-0.169	4.57	5.52	0.95	32.569	-0.169	4.57	5.52	0.95	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fthk	fvk0	fthmedio	t0	fv0	μ	φ	fvk,lim	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	365	-63.34	1161.22	SLU 83	18.33	Si
fin.	3	365	-23.08	1161.22	SLU 83	50.31	Si
ini.	3	372	-70.73	1161.22	SLU 40	16.42	Si
fin.	3	372	-20.99	1161.22	SLU 40	55.31	Si
ini.	3	372	-70.73	1161.22	SLU 39	16.42	Si
fin.	3	372	-20.99	1161.22	SLU 39	55.31	Si
ini.	3	289	-53.38	1161.22	SLU 37	21.75	Si
fin.	3	289	-18.28	1161.22	SLU 37	63.51	Si
ini.	3	372	-70.73	1161.22	SLU 42	16.42	Si
fin.	3	372	-20.99	1161.22	SLU 42	55.31	Si
ini.	3	365	-63.34	1161.22	SLU 84	18.33	Si
fin.	3	365	-23.08	1161.22	SLU 84	50.31	Si
ini.	3	289	-53.38	1161.22	SLU 33	21.75	Si
fin.	3	289	-18.28	1161.22	SLU 33	63.51	Si
ini.	3	365	-63.34	1161.22	SLU 81	18.33	Si
fin.	3	365	-23.08	1161.22	SLU 81	50.31	Si
ini.	3	372	-70.73	1161.22	SLU 41	16.42	Si
fin.	3	372	-20.99	1161.22	SLU 41	55.31	Si
ini.	3	365	-63.34	1161.22	SLU 82	18.33	Si
fin.	3	365	-23.08	1161.22	SLU 82	50.31	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-63.34	341			1043	392	SLU 83	1.15	Si
fin.	3	0	-23.08	-259			1043	392	SLU 83	1.52	Si
ini.	3	0	-46	326			1043	392	SLU 75	1.2	Si
fin.	3	0	-20.37	-273			1043	392	SLU 75	1.44	Si
ini.	3	0	-46	326			1043	392	SLU 79	1.2	Si
fin.	3	0	-20.37	-273			1043	392	SLU 79	1.44	Si
ini.	3	0	-46	326			1043	392	SLU 78	1.2	Si
fin.	3	0	-20.37	-273			1043	392	SLU 78	1.44	Si
ini.	3	0	-63.34	341			1043	392	SLU 84	1.15	Si
fin.	3	0	-23.08	-259			1043	392	SLU 84	1.52	Si
ini.	3	0	-63.34	341			1043	392	SLU 81	1.15	Si
fin.	3	0	-23.08	-259			1043	392	SLU 81	1.52	Si
ini.	3	0	-46	326			1043	392	SLU 77	1.2	Si
fin.	3	0	-20.37	-273			1043	392	SLU 77	1.44	Si
ini.	3	0	-63.34	341			1043	392	SLU 82	1.15	Si
fin.	3	0	-23.08	-259			1043	392	SLU 82	1.52	Si
ini.	3	0	-46	326			1043	392	SLU 76	1.2	Si
fin.	3	0	-20.37	-273			1043	392	SLU 76	1.44	Si
ini.	3	0	-46	326			1043	392	SLU 80	1.2	Si
fin.	3	0	-20.37	-273			1043	392	SLU 80	1.44	Si

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	197	179.9	1328.31	SLV 1	7.38	Si
fin.	2	80	-211.78	1328.31	SLV 1	6.27	Si
ini.	2	355	-182.77	1328.31	SLV 13	7.27	Si
fin.	2	471	189.3	1328.31	SLV 13	7.02	Si
ini.	2	-419	-101.49	1328.31	SLV 11	13.09	Si
fin.	2	-383	45.2	1328.31	SLV 11	29.38	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-135	158.83	1328.31	SLV 4	8.36	Si
fin.	2	-251	-213.5	1328.31	SLV 4	6.22	Si
ini.	2	23	-203.84	1328.31	SLV 15	6.52	Si
fin.	2	140	187.59	1328.31	SLV 15	7.08	Si
ini.	2	355	-182.77	1328.31	SLV 14	7.27	Si
fin.	2	471	189.3	1328.31	SLV 14	7.02	Si
ini.	2	-419	-101.49	1328.31	SLV 12	13.09	Si
fin.	2	-383	45.2	1328.31	SLV 12	29.38	Si
ini.	2	23	-203.84	1328.31	SLV 16	6.52	Si
fin.	2	140	187.59	1328.31	SLV 16	7.08	Si
ini.	2	197	179.9	1328.31	SLV 2	7.38	Si
fin.	2	80	-211.78	1328.31	SLV 2	6.27	Si
ini.	2	-135	158.83	1328.31	SLV 3	8.36	Si
fin.	2	-251	-213.5	1328.31	SLV 3	6.22	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	179.9	-39			1564	589	SLV 2	15.11	Si
fin.	2	0	-211.78	-509			1564	589	SLV 2	1.16	Si
ini.	2	0	-31.25	514			1564	589	SLV 9	1.14	Si
fin.	2	0	50.93	19			1564	589	SLV 9	30.25	Si
ini.	2	0	-203.84	499			1564	589	SLV 15	1.18	Si
fin.	2	0	187.59	51			1564	589	SLV 15	11.58	Si
ini.	2	0	158.83	-151			1564	589	SLV 3	3.89	Si
fin.	2	0	-213.5	-600			1564	589	SLV 3	0.98	No
ini.	2	0	158.83	-151			1564	589	SLV 4	3.89	Si
fin.	2	0	-213.5	-600			1564	589	SLV 4	0.98	No
ini.	2	0	-203.84	499			1564	589	SLV 16	1.18	Si
fin.	2	0	187.59	51			1564	589	SLV 16	11.58	Si
ini.	2	0	-182.77	611			1564	589	SLV 14	0.96	No
fin.	2	0	189.3	141			1564	589	SLV 14	4.16	Si
ini.	2	0	-31.25	514			1564	589	SLV 10	1.14	Si
fin.	2	0	50.93	19			1564	589	SLV 10	30.25	Si
ini.	2	0	179.9	-39			1564	589	SLV 1	15.11	Si
fin.	2	0	-211.78	-509			1564	589	SLV 1	1.16	Si
ini.	2	0	-182.77	611			1564	589	SLV 13	0.96	No
fin.	2	0	189.3	141			1564	589	SLV 13	4.16	Si

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	6.222	SLV 3	Si
V_SLV	0.963	SLV 13	No
PF_SLU	16.418	SLU 39	Si
V_SLU	1.152	SLU 81	Si

Trave di accoppiamento 21

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
30.718	4.336	3.77	5.52	1.75	30.718	3.536	3.77	5.52	1.75	0.8	0.18	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fhk	fvk0	fhmmedio	τ0	fv0	μ	φ	fvk,lim	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-1226	-919.38	2227.04	SLU 82	2.42	Si
fin.	3	-1226	1073.75	2227.04	SLU 82	2.07	Si
ini.	3	-1028	-781.89	2227.04	SLU 63	2.85	Si
fin.	3	-1028	902.97	2227.04	SLU 63	2.47	Si
ini.	3	-1226	-919.38	2227.04	SLU 81	2.42	Si
fin.	3	-1226	1073.75	2227.04	SLU 81	2.07	Si
ini.	3	-1195	-925.72	2227.04	SLU 42	2.41	Si
fin.	3	-1195	1050.5	2227.04	SLU 42	2.12	Si
ini.	3	-1195	-925.72	2227.04	SLU 41	2.41	Si
fin.	3	-1195	1050.5	2227.04	SLU 41	2.12	Si
ini.	3	-1195	-925.72	2227.04	SLU 40	2.41	Si
fin.	3	-1195	1050.5	2227.04	SLU 40	2.12	Si
ini.	3	-1226	-919.38	2227.04	SLU 84	2.42	Si
fin.	3	-1226	1073.75	2227.04	SLU 84	2.07	Si
ini.	3	-1195	-925.72	2227.04	SLU 39	2.41	Si
fin.	3	-1195	1050.5	2227.04	SLU 39	2.12	Si
ini.	3	-1226	-919.38	2227.04	SLU 83	2.42	Si
fin.	3	-1226	1073.75	2227.04	SLU 83	2.07	Si
ini.	3	-1028	-781.89	2227.04	SLU 62	2.85	Si
fin.	3	-1028	902.97	2227.04	SLU 62	2.47	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	-781.89	4081			1213	457	SLU 63	0.11	No
fin.	3	0	902.97	17			1213	457	SLU 63	26.32	Si
ini.	3	0	-919.38	4779			1213	457	SLU 83	0.1	No



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
fin.	3	0	1073.75	70			1213	457	SLU 83	6.56	Si
ini.	3	0	-925.72	4635			1213	457	SLU 42	0.1	No
fin.	3	0	1050.5	174			1213	457	SLU 42	2.63	Si
ini.	3	0	-781.89	4081			1213	457	SLU 62	0.11	No
fin.	3	0	902.97	17			1213	457	SLU 62	26.32	Si
ini.	3	0	-925.72	4635			1213	457	SLU 39	0.1	No
fin.	3	0	1050.5	174			1213	457	SLU 39	2.63	Si
ini.	3	0	-919.38	4779			1213	457	SLU 82	0.1	No
fin.	3	0	1073.75	70			1213	457	SLU 82	6.56	Si
ini.	3	0	-925.72	4635			1213	457	SLU 40	0.1	No
fin.	3	0	1050.5	174			1213	457	SLU 40	2.63	Si
ini.	3	0	-925.72	4635			1213	457	SLU 41	0.1	No
fin.	3	0	1050.5	174			1213	457	SLU 41	2.63	Si
ini.	3	0	-919.38	4779			1213	457	SLU 81	0.1	No
fin.	3	0	1073.75	70			1213	457	SLU 81	6.56	Si
ini.	3	0	-919.38	4779			1213	457	SLU 84	0.1	No
fin.	3	0	1073.75	70			1213	457	SLU 84	6.56	Si

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	128	-175.36	2505.52	SLV 15	14.29	Si
fin.	2	-150	830.98	2505.52	SLV 15	3.02	Si
ini.	2	-1236	-697.79	2505.52	SLV 5	3.59	Si
fin.	2	-1283	-715.2	2505.52	SLV 5	3.5	Si
ini.	2	-1236	-697.79	2505.52	SLV 6	3.59	Si
fin.	2	-1283	-715.2	2505.52	SLV 6	3.5	Si
ini.	2	-824	-203.33	2505.52	SLV 3	12.32	Si
fin.	2	-459	741.52	2505.52	SLV 3	3.38	Si
ini.	2	128	-175.36	2505.52	SLV 16	14.29	Si
fin.	2	-150	830.98	2505.52	SLV 16	3.02	Si
ini.	2	-89	77.98	2505.52	SLV 7	32.13	Si
fin.	2	151	1574.08	2505.52	SLV 7	1.59	Si
ini.	2	-824	-203.33	2505.52	SLV 4	12.32	Si
fin.	2	-459	741.52	2505.52	SLV 4	3.38	Si
ini.	2	-89	77.98	2505.52	SLV 8	32.13	Si
fin.	2	151	1574.08	2505.52	SLV 8	1.59	Si
ini.	2	197	86.37	2505.52	SLV 11	29.01	Si
fin.	2	243	1600.91	2505.52	SLV 11	1.57	Si
ini.	2	197	86.37	2505.52	SLV 12	29.01	Si
fin.	2	243	1600.91	2505.52	SLV 12	1.57	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-175.36	2368			1820	685	SLV 16	0.29	No
fin.	2	0	830.98	428			1820	685	SLV 16	1.6	Si
ini.	2	0	-436.07	1648			1820	685	SLV 1	0.42	No
fin.	2	0	54.74	-810			1820	685	SLV 1	0.85	No
ini.	2	0	86.37	3254			1820	685	SLV 11	0.21	No
fin.	2	0	1600.91	1036			1820	685	SLV 11	0.66	No
ini.	2	0	-203.33	2398			1820	685	SLV 3	0.29	No
fin.	2	0	741.52	-123			1820	685	SLV 3	5.57	Si
ini.	2	0	86.37	3254			1820	685	SLV 12	0.21	No
fin.	2	0	1600.91	1036			1820	685	SLV 12	0.66	No
ini.	2	0	-436.07	1648			1820	685	SLV 2	0.42	No
fin.	2	0	54.74	-810			1820	685	SLV 2	0.85	No
ini.	2	0	-203.33	2398			1820	685	SLV 4	0.29	No
fin.	2	0	741.52	-123			1820	685	SLV 4	5.57	Si
ini.	2	0	77.98	3263			1820	685	SLV 8	0.21	No
fin.	2	0	1574.08	871			1820	685	SLV 8	0.79	No
ini.	2	0	77.98	3263			1820	685	SLV 7	0.21	No
fin.	2	0	1574.08	871			1820	685	SLV 7	0.79	No
ini.	2	0	-175.36	2368			1820	685	SLV 15	0.29	No
fin.	2	0	830.98	428			1820	685	SLV 15	1.6	Si

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.565	SLV 11	Si
V_SLV	0.21	SLV 7	No
PF_SLU	2.074	SLU 81	Si
V_SLU	0.096	SLU 81	No

Trave di accoppiamento 22

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
30.718	5.634	3.77	5.52	1.75	30.718	4.834	3.77	5.52	1.75	0.8	0.18	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	fhk	fvk0	fhmmedio	t0	fv0	μ	φ	fvk,lim	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2



Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-1004	1182.74	2227.04	SLU 63	1.88	Si
fin.	3	-1004	-243.05	2227.04	SLU 63	9.16	Si
ini.	3	-1174	1382.86	2227.04	SLU 41	1.61	Si
fin.	3	-1174	-304.52	2227.04	SLU 41	7.31	Si
ini.	3	-1198	1408.68	2227.04	SLU 81	1.58	Si
fin.	3	-1198	-280.79	2227.04	SLU 81	7.93	Si
ini.	3	-1174	1382.86	2227.04	SLU 39	1.61	Si
fin.	3	-1174	-304.52	2227.04	SLU 39	7.31	Si
ini.	3	-1174	1382.86	2227.04	SLU 40	1.61	Si
fin.	3	-1174	-304.52	2227.04	SLU 40	7.31	Si
ini.	3	-1174	1382.86	2227.04	SLU 42	1.61	Si
fin.	3	-1174	-304.52	2227.04	SLU 42	7.31	Si
ini.	3	-1198	1408.68	2227.04	SLU 83	1.58	Si
fin.	3	-1198	-280.79	2227.04	SLU 83	7.93	Si
ini.	3	-1004	1182.74	2227.04	SLU 62	1.88	Si
fin.	3	-1004	-243.05	2227.04	SLU 62	9.16	Si
ini.	3	-1198	1408.68	2227.04	SLU 84	1.58	Si
fin.	3	-1198	-280.79	2227.04	SLU 84	7.93	Si
ini.	3	-1198	1408.68	2227.04	SLU 82	1.58	Si
fin.	3	-1198	-280.79	2227.04	SLU 82	7.93	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	1182.74	-462			1213	457	SLU 62	0.99	No
fin.	3	0	-243.05	-4287			1213	457	SLU 62	0.11	No
ini.	3	0	1408.68	-592			1213	457	SLU 84	0.77	No
fin.	3	0	-280.79	-5055			1213	457	SLU 84	0.09	No
ini.	3	0	1182.74	-462			1213	457	SLU 63	0.99	No
fin.	3	0	-243.05	-4287			1213	457	SLU 63	0.11	No
ini.	3	0	1382.86	-682			1213	457	SLU 39	0.67	No
fin.	3	0	-304.52	-4943			1213	457	SLU 39	0.09	No
ini.	3	0	1408.68	-592			1213	457	SLU 81	0.77	No
fin.	3	0	-280.79	-5055			1213	457	SLU 81	0.09	No
ini.	3	0	1382.86	-682			1213	457	SLU 40	0.67	No
fin.	3	0	-304.52	-4943			1213	457	SLU 40	0.09	No
ini.	3	0	1408.68	-592			1213	457	SLU 83	0.77	No
fin.	3	0	-280.79	-5055			1213	457	SLU 83	0.09	No
ini.	3	0	1382.86	-682			1213	457	SLU 42	0.67	No
fin.	3	0	-304.52	-4943			1213	457	SLU 42	0.09	No
ini.	3	0	1382.86	-682			1213	457	SLU 41	0.67	No
fin.	3	0	-304.52	-4943			1213	457	SLU 41	0.09	No
ini.	3	0	1408.68	-592			1213	457	SLU 82	0.77	No
fin.	3	0	-280.79	-5055			1213	457	SLU 82	0.09	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-200	1171.94	2505.52	SLV 2	2.14	Si
fin.	2	-314	368.48	2505.52	SLV 2	6.8	Si
ini.	2	-63	1581.39	2505.52	SLV 10	1.58	Si
fin.	2	-143	379.85	2505.52	SLV 10	6.6	Si
ini.	2	-1012	-602.44	2505.52	SLV 12	4.16	Si
fin.	2	-883	-604.29	2505.52	SLV 12	4.15	Si
ini.	2	-1012	-602.44	2505.52	SLV 11	4.16	Si
fin.	2	-883	-604.29	2505.52	SLV 11	4.15	Si
ini.	2	-63	1581.39	2505.52	SLV 9	1.58	Si
fin.	2	-143	379.85	2505.52	SLV 9	6.6	Si
ini.	2	-501	625.95	2505.52	SLV 13	4	Si
fin.	2	-449	-143.95	2505.52	SLV 13	17.41	Si
ini.	2	27	1745.18	2505.52	SLV 6	1.44	Si
fin.	2	-102	533.57	2505.52	SLV 6	4.7	Si
ini.	2	27	1745.18	2505.52	SLV 5	1.44	Si
fin.	2	-102	533.57	2505.52	SLV 5	4.7	Si
ini.	2	-501	625.95	2505.52	SLV 14	4	Si
fin.	2	-449	-143.95	2505.52	SLV 14	17.41	Si
ini.	2	-200	1171.94	2505.52	SLV 1	2.14	Si
fin.	2	-314	368.48	2505.52	SLV 1	6.8	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	1581.39	-1091			1820	685	SLV 9	0.63	No
fin.	2	0	379.85	-3225			1820	685	SLV 9	0.21	No
ini.	2	0	625.95	-563			1820	685	SLV 14	1.22	Si
fin.	2	0	-143.95	-2459			1820	685	SLV 14	0.28	No
ini.	2	0	625.95	-563			1820	685	SLV 13	1.22	Si
fin.	2	0	-143.95	-2459			1820	685	SLV 13	0.28	No
ini.	2	0	-29.2	33			1820	685	SLV 15	20.99	Si
fin.	2	0	-439.19	-1768			1820	685	SLV 15	0.39	No
ini.	2	0	-29.2	33			1820	685	SLV 16	20.99	Si
fin.	2	0	-439.19	-1768			1820	685	SLV 16	0.39	No
ini.	2	0	1745.18	-948			1820	685	SLV 5	0.72	No
fin.	2	0	533.57	-3191			1820	685	SLV 5	0.21	No
ini.	2	0	1581.39	-1091			1820	685	SLV 10	0.63	No
fin.	2	0	379.85	-3225			1820	685	SLV 10	0.21	No
ini.	2	0	1745.18	-948			1820	685	SLV 6	0.72	No
fin.	2	0	533.57	-3191			1820	685	SLV 6	0.21	No
ini.	2	0	1171.94	-87			1820	685	SLV 2	7.83	Si
fin.	2	0	368.48	-2345			1820	685	SLV 2	0.29	No
ini.	2	0	1171.94	-87			1820	685	SLV 1	7.83	Si



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
fin.	2	0	368.48	-2345			1820	685	SLV 1	0.29	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.436	SLV 5	Si
V_SLV	0.212	SLV 9	No
PF_SLU	1.581	SLU 81	Si
V_SLU	0.09	SLU 81	No

Trave di accoppiamento 23

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
35.424	2.847	1.67	2.67	1	35.424	1.847	1.67	2.67	1	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	f _{hk}	f _{vk0}	f _{hmedio}	t ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-107	90.27	1248.72	SLU 39	13.83	Si
fin.	3	157	-48.98	1248.72	SLU 39	25.49	Si
ini.	3	-107	90.27	1248.72	SLU 41	13.83	Si
fin.	3	157	-48.98	1248.72	SLU 41	25.49	Si
ini.	3	-147	83.06	1248.72	SLU 77	15.03	Si
fin.	3	79	-35.19	1248.72	SLU 77	35.48	Si
ini.	3	-107	90.27	1248.72	SLU 42	13.83	Si
fin.	3	157	-48.98	1248.72	SLU 42	25.49	Si
ini.	3	-143	95.72	1248.72	SLU 82	13.05	Si
fin.	3	126	-45.53	1248.72	SLU 82	27.42	Si
ini.	3	-143	95.72	1248.72	SLU 81	13.05	Si
fin.	3	126	-45.53	1248.72	SLU 81	27.42	Si
ini.	3	-143	95.72	1248.72	SLU 84	13.05	Si
fin.	3	126	-45.53	1248.72	SLU 84	27.42	Si
ini.	3	-147	83.06	1248.72	SLU 75	15.03	Si
fin.	3	79	-35.19	1248.72	SLU 75	35.48	Si
ini.	3	-107	90.27	1248.72	SLU 40	13.83	Si
fin.	3	157	-48.98	1248.72	SLU 40	25.49	Si
ini.	3	-143	95.72	1248.72	SLU 83	13.05	Si
fin.	3	126	-45.53	1248.72	SLU 83	27.42	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	90.27	-1038			1155	435	SLU 42	0.42	No
fin.	3	0	-48.98	312			1155	435	SLU 42	1.39	Si
ini.	3	0	95.72	-1112			1155	435	SLU 83	0.39	No
fin.	3	0	-45.53	338			1155	435	SLU 83	1.29	Si
ini.	3	0	90.27	-1038			1155	435	SLU 40	0.42	No
fin.	3	0	-48.98	312			1155	435	SLU 40	1.39	Si
ini.	3	0	95.72	-1112			1155	435	SLU 84	0.39	No
fin.	3	0	-45.53	338			1155	435	SLU 84	1.29	Si
ini.	3	0	95.72	-1112			1155	435	SLU 82	0.39	No
fin.	3	0	-45.53	338			1155	435	SLU 82	1.29	Si
ini.	3	0	90.27	-1038			1155	435	SLU 41	0.42	No
fin.	3	0	-48.98	312			1155	435	SLU 41	1.39	Si
ini.	3	0	90.27	-1038			1155	435	SLU 39	0.42	No
fin.	3	0	-48.98	312			1155	435	SLU 39	1.39	Si
ini.	3	0	95.72	-1112			1155	435	SLU 81	0.39	No
fin.	3	0	-45.53	338			1155	435	SLU 81	1.29	Si
ini.	3	0	83.06	-972			1155	435	SLU 77	0.45	No
fin.	3	0	-35.19	296			1155	435	SLU 77	1.47	Si
ini.	3	0	83.06	-972			1155	435	SLU 75	0.45	No
fin.	3	0	-35.19	296			1155	435	SLU 75	1.47	Si

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-391	248.44	1415.81	SLV 14	5.7	Si
fin.	2	547	-277.76	1415.81	SLV 14	5.1	Si
ini.	2	-510	313.54	1415.81	SLV 5	4.52	Si
fin.	2	403	-303.81	1415.81	SLV 5	4.66	Si
ini.	2	-596	380.59	1415.81	SLV 9	3.72	Si
fin.	2	638	-401.63	1415.81	SLV 9	3.53	Si
ini.	2	362	-287.52	1415.81	SLV 8	4.92	Si
fin.	2	-642	376.17	1415.81	SLV 8	3.76	Si
ini.	2	-391	248.44	1415.81	SLV 13	5.7	Si
fin.	2	547	-277.76	1415.81	SLV 13	5.1	Si
ini.	2	276	-220.47	1415.81	SLV 11	6.42	Si
fin.	2	-407	278.35	1415.81	SLV 11	5.09	Si
ini.	2	-510	313.54	1415.81	SLV 6	4.52	Si
fin.	2	403	-303.81	1415.81	SLV 6	4.66	Si
ini.	2	362	-287.52	1415.81	SLV 7	4.92	Si
fin.	2	-642	376.17	1415.81	SLV 7	3.76	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	276	-220.47	1415.81	SLV 12	6.42	Si
fin.	2	-407	278.35	1415.81	SLV 12	5.09	Si
ini.	2	-596	380.59	1415.81	SLV 10	3.72	Si
fin.	2	638	-401.63	1415.81	SLV 10	3.53	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	248.44	-1168			1733	652	SLV 14	0.56	No
fin.	2	0	-277.76	39			1733	652	SLV 14	16.58	Si
ini.	2	0	-287.52	741			1733	652	SLV 8	0.88	No
fin.	2	0	376.17	1162			1733	652	SLV 8	0.56	No
ini.	2	0	-220.47	594			1733	652	SLV 11	1.1	Si
fin.	2	0	278.35	1270			1733	652	SLV 11	0.51	No
ini.	2	0	313.54	-1706			1733	652	SLV 6	0.38	No
fin.	2	0	-303.81	-925			1733	652	SLV 6	0.7	No
ini.	2	0	248.44	-1168			1733	652	SLV 13	0.56	No
fin.	2	0	-277.76	39			1733	652	SLV 13	16.58	Si
ini.	2	0	380.59	-1853			1733	652	SLV 9	0.35	No
fin.	2	0	-401.63	-817			1733	652	SLV 9	0.8	No
ini.	2	0	-287.52	741			1733	652	SLV 7	0.88	No
fin.	2	0	376.17	1162			1733	652	SLV 7	0.56	No
ini.	2	0	380.59	-1853			1733	652	SLV 10	0.35	No
fin.	2	0	-401.63	-817			1733	652	SLV 10	0.8	No
ini.	2	0	-220.47	594			1733	652	SLV 12	1.1	Si
fin.	2	0	278.35	1270			1733	652	SLV 12	0.51	No
ini.	2	0	313.54	-1706			1733	652	SLV 5	0.38	No
fin.	2	0	-303.81	-925			1733	652	SLV 5	0.7	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	3.525	SLV 9	Si
V_SLV	0.352	SLV 9	No
PF_SLU	13.045	SLU 81	Si
V_SLU	0.391	SLU 81	No

Trave di accoppiamento 24

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
35.424	2.847	4.57	5.52	0.95	35.424	1.847	4.57	5.52	0.95	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-704	3.41	1161.22	SLU 81	340.93	Si
fin.	3	-704	149.66	1161.22	SLU 81	7.76	Si
ini.	3	-584	0.15	1161.22	SLU 62	7781.28	Si
fin.	3	-584	135.56	1161.22	SLU 62	8.57	Si
ini.	3	-584	0.15	1161.22	SLU 63	7781.28	Si
fin.	3	-584	135.56	1161.22	SLU 63	8.57	Si
ini.	3	-704	3.41	1161.22	SLU 84	340.93	Si
fin.	3	-704	149.66	1161.22	SLU 84	7.76	Si
ini.	3	-714	5	1161.22	SLU 41	232.4	Si
fin.	3	-714	134.84	1161.22	SLU 41	8.61	Si
ini.	3	-584	0.15	1161.22	SLU 60	7781.28	Si
fin.	3	-584	135.56	1161.22	SLU 60	8.57	Si
ini.	3	-584	0.15	1161.22	SLU 61	7781.28	Si
fin.	3	-584	135.56	1161.22	SLU 61	8.57	Si
ini.	3	-704	3.41	1161.22	SLU 82	340.93	Si
fin.	3	-704	149.66	1161.22	SLU 82	7.76	Si
ini.	3	-704	3.41	1161.22	SLU 83	340.93	Si
fin.	3	-704	149.66	1161.22	SLU 83	7.76	Si
ini.	3	-714	5	1161.22	SLU 40	232.4	Si
fin.	3	-714	134.84	1161.22	SLU 40	8.61	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	5	1469			1043	392	SLU 39	0.27	No
fin.	3	0	134.84	-1213			1043	392	SLU 39	0.32	No
ini.	3	0	5	1469			1043	392	SLU 42	0.27	No
fin.	3	0	134.84	-1213			1043	392	SLU 42	0.32	No
ini.	3	0	3.41	1588			1043	392	SLU 83	0.25	No
fin.	3	0	149.66	-1318			1043	392	SLU 83	0.3	No
ini.	3	0	3.41	1588			1043	392	SLU 81	0.25	No
fin.	3	0	149.66	-1318			1043	392	SLU 81	0.3	No
ini.	3	0	5	1469			1043	392	SLU 41	0.27	No
fin.	3	0	134.84	-1213			1043	392	SLU 41	0.32	No
ini.	3	0	0.15	1401			1043	392	SLU 62	0.28	No
fin.	3	0	135.56	-1164			1043	392	SLU 62	0.34	No
ini.	3	0	0.15	1401			1043	392	SLU 63	0.28	No



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
fin.	3	0	135.56	-1164			1043	392	SLU 63	0.34	No
ini.	3	0	3.41	1588			1043	392	SLU 84	0.25	No
fin.	3	0	149.66	-1318			1043	392	SLU 84	0.3	No
ini.	3	0	5	1469			1043	392	SLU 40	0.27	No
fin.	3	0	134.84	-1213			1043	392	SLU 40	0.32	No
ini.	3	0	3.41	1588			1043	392	SLU 82	0.25	No
fin.	3	0	149.66	-1318			1043	392	SLU 82	0.3	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	43	311.3	1328.31	SLV 6	4.27	Si
fin.	2	-385	-264.73	1328.31	SLV 6	5.02	Si
ini.	2	-859	-162.47	1328.31	SLV 4	8.18	Si
fin.	2	-888	189.78	1328.31	SLV 4	7	Si
ini.	2	340	349.34	1328.31	SLV 9	3.8	Si
fin.	2	-1	-267.81	1328.31	SLV 9	4.96	Si
ini.	2	-810	-349.31	1328.31	SLV 7	3.8	Si
fin.	2	-469	428.99	1328.31	SLV 7	3.1	Si
ini.	2	340	349.34	1328.31	SLV 10	3.8	Si
fin.	2	-1	-267.81	1328.31	SLV 10	4.96	Si
ini.	2	-513	-311.27	1328.31	SLV 11	4.27	Si
fin.	2	-85	425.92	1328.31	SLV 11	3.12	Si
ini.	2	43	311.3	1328.31	SLV 5	4.27	Si
fin.	2	-385	-264.73	1328.31	SLV 5	5.02	Si
ini.	2	-810	-349.31	1328.31	SLV 8	3.8	Si
fin.	2	-469	428.99	1328.31	SLV 8	3.1	Si
ini.	2	-513	-311.27	1328.31	SLV 12	4.27	Si
fin.	2	-85	425.92	1328.31	SLV 12	3.12	Si
ini.	2	-859	-162.47	1328.31	SLV 3	8.18	Si
fin.	2	-888	189.78	1328.31	SLV 3	7	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	349.34	-30			1564	589	SLV 9	19.64	Si
fin.	2	0	-267.81	-1507			1564	589	SLV 9	0.39	No
ini.	2	0	-311.27	1453			1564	589	SLV 12	0.4	No
fin.	2	0	425.92	-17			1564	589	SLV 12	35.39	Si
ini.	2	0	349.34	-30			1564	589	SLV 10	19.64	Si
fin.	2	0	-267.81	-1507			1564	589	SLV 10	0.39	No
ini.	2	0	311.3	139			1564	589	SLV 5	4.24	Si
fin.	2	0	-264.73	-1340			1564	589	SLV 5	0.44	No
ini.	2	0	-349.31	1622			1564	589	SLV 8	0.36	No
fin.	2	0	428.99	151			1564	589	SLV 8	3.91	Si
ini.	2	0	-162.47	1300			1564	589	SLV 3	0.45	No
fin.	2	0	189.78	-176			1564	589	SLV 3	3.34	Si
ini.	2	0	-311.27	1453			1564	589	SLV 11	0.4	No
fin.	2	0	425.92	-17			1564	589	SLV 11	35.39	Si
ini.	2	0	-162.47	1300			1564	589	SLV 4	0.45	No
fin.	2	0	189.78	-176			1564	589	SLV 4	3.34	Si
ini.	2	0	311.3	139			1564	589	SLV 6	4.24	Si
fin.	2	0	-264.73	-1340			1564	589	SLV 6	0.44	No
ini.	2	0	-349.31	1622			1564	589	SLV 7	0.36	No
fin.	2	0	428.99	151			1564	589	SLV 7	3.91	Si

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	3.096	SLV 7	Si
V_SLV	0.363	SLV 7	No
PF_SLU	7.759	SLU 81	Si
V_SLU	0.247	SLU 81	No

Trave di accoppiamento 25

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
35.424	7.497	1.67	2.67	1	35.424	6.497	1.67	2.67	1	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

fb	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	297	26.08	1248.72	SLU 83	47.89	Si
fin.	3	-192	79.97	1248.72	SLU 83	15.61	Si
ini.	3	312	15.14	1248.72	SLU 39	82.48	Si
fin.	3	-158	72.13	1248.72	SLU 39	17.31	Si
ini.	3	230	30.52	1248.72	SLU 63	40.91	Si
fin.	3	-183	71.61	1248.72	SLU 63	17.44	Si
ini.	3	230	30.52	1248.72	SLU 62	40.91	Si
fin.	3	-183	71.61	1248.72	SLU 62	17.44	Si
ini.	3	312	15.14	1248.72	SLU 41	82.48	Si
fin.	3	-158	72.13	1248.72	SLU 41	17.31	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	312	15.14	1248.72	SLU 40	82.48	Si
fin.	3	-158	72.13	1248.72	SLU 40	17.31	Si
ini.	3	297	26.08	1248.72	SLU 81	47.89	Si
fin.	3	-192	79.97	1248.72	SLU 81	15.61	Si
ini.	3	312	15.14	1248.72	SLU 42	82.48	Si
fin.	3	-158	72.13	1248.72	SLU 42	17.31	Si
ini.	3	297	26.08	1248.72	SLU 82	47.89	Si
fin.	3	-192	79.97	1248.72	SLU 82	15.61	Si
ini.	3	297	26.08	1248.72	SLU 84	47.89	Si
fin.	3	-192	79.97	1248.72	SLU 84	15.61	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	26.08	-1473			1155	435	SLU 81	0.3	No
fin.	3	0	79.97	2008			1155	435	SLU 81	0.22	No
ini.	3	0	26.08	-1473			1155	435	SLU 83	0.3	No
fin.	3	0	79.97	2008			1155	435	SLU 83	0.22	No
ini.	3	0	15.14	-1283			1155	435	SLU 41	0.34	No
fin.	3	0	72.13	1818			1155	435	SLU 41	0.24	No
ini.	3	0	15.14	-1283			1155	435	SLU 39	0.34	No
fin.	3	0	72.13	1818			1155	435	SLU 39	0.24	No
ini.	3	0	15.14	-1283			1155	435	SLU 42	0.34	No
fin.	3	0	72.13	1818			1155	435	SLU 42	0.24	No
ini.	3	0	26.08	-1473			1155	435	SLU 82	0.3	No
fin.	3	0	79.97	2008			1155	435	SLU 82	0.22	No
ini.	3	0	29.61	-1358			1155	435	SLU 75	0.32	No
fin.	3	0	71.56	1797			1155	435	SLU 75	0.24	No
ini.	3	0	26.08	-1473			1155	435	SLU 84	0.3	No
fin.	3	0	79.97	2008			1155	435	SLU 84	0.22	No
ini.	3	0	15.14	-1283			1155	435	SLU 40	0.34	No
fin.	3	0	72.13	1818			1155	435	SLU 40	0.24	No
ini.	3	0	29.61	-1358			1155	435	SLU 77	0.32	No
fin.	3	0	71.56	1797			1155	435	SLU 77	0.24	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-455	185.59	1415.81	SLV 10	7.63	Si
fin.	2	455	-136.9	1415.81	SLV 10	10.34	Si
ini.	2	-873	243.08	1415.81	SLV 5	5.82	Si
fin.	2	582	-169.06	1415.81	SLV 5	8.37	Si
ini.	2	-873	243.08	1415.81	SLV 6	5.82	Si
fin.	2	582	-169.06	1415.81	SLV 6	8.37	Si
ini.	2	-455	185.59	1415.81	SLV 9	7.63	Si
fin.	2	455	-136.9	1415.81	SLV 9	10.34	Si
ini.	2	1056	-187.6	1415.81	SLV 12	7.55	Si
fin.	2	-846	256.48	1415.81	SLV 12	5.52	Si
ini.	2	-832	179.54	1415.81	SLV 2	7.89	Si
fin.	2	274	-68.9	1415.81	SLV 2	20.55	Si
ini.	2	-832	179.54	1415.81	SLV 1	7.89	Si
fin.	2	274	-68.9	1415.81	SLV 1	20.55	Si
ini.	2	638	-130.1	1415.81	SLV 8	10.88	Si
fin.	2	-719	224.32	1415.81	SLV 8	6.31	Si
ini.	2	638	-130.1	1415.81	SLV 7	10.88	Si
fin.	2	-719	224.32	1415.81	SLV 7	6.31	Si
ini.	2	1056	-187.6	1415.81	SLV 11	7.55	Si
fin.	2	-846	256.48	1415.81	SLV 11	5.52	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	185.59	-2042			1733	652	SLV 10	0.32	No
fin.	2	0	-136.9	-121			1733	652	SLV 10	5.38	Si
ini.	2	0	-130.1	267			1733	652	SLV 7	2.45	Si
fin.	2	0	224.32	2312			1733	652	SLV 7	0.28	No
ini.	2	0	-187.6	102			1733	652	SLV 12	6.41	Si
fin.	2	0	256.48	2499			1733	652	SLV 12	0.26	No
ini.	2	0	-187.6	102			1733	652	SLV 11	6.41	Si
fin.	2	0	256.48	2499			1733	652	SLV 11	0.26	No
ini.	2	0	-124.06	-841			1733	652	SLV 15	0.78	No
fin.	2	0	156.33	1801			1733	652	SLV 15	0.36	No
ini.	2	0	243.08	-1878			1733	652	SLV 5	0.35	No
fin.	2	0	-169.06	-308			1733	652	SLV 5	2.12	Si
ini.	2	0	-130.1	267			1733	652	SLV 8	2.45	Si
fin.	2	0	224.32	2312			1733	652	SLV 8	0.28	No
ini.	2	0	-124.06	-841			1733	652	SLV 16	0.78	No
fin.	2	0	156.33	1801			1733	652	SLV 16	0.36	No
ini.	2	0	185.59	-2042			1733	652	SLV 9	0.32	No
fin.	2	0	-136.9	-121			1733	652	SLV 9	5.38	Si
ini.	2	0	243.08	-1878			1733	652	SLV 6	0.35	No
fin.	2	0	-169.06	-308			1733	652	SLV 6	2.12	Si

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	5.52	SLV 11	Si
V_SLV	0.261	SLV 11	No
PF_SLU	15.614	SLU 81	Si
V_SLU	0.217	SLU 81	No



Trave di accoppiamento 26

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
35.424	7.497	4.57	5.52	0.95	35.424	6.497	4.57	5.52	0.95	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2_Corti

f _b	f _{hk}	f _{vk0}	f _{hmedio}	τ ₀	f _{v0}	μ	φ	f _{vk,lim}	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni non sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	3	-562	118.07	1161.22	SLU 61	9.83	Si
fin.	3	-562	4.98	1161.22	SLU 61	233.08	Si
ini.	3	-562	118.07	1161.22	SLU 60	9.83	Si
fin.	3	-562	4.98	1161.22	SLU 60	233.08	Si
ini.	3	-562	118.07	1161.22	SLU 63	9.83	Si
fin.	3	-562	4.98	1161.22	SLU 63	233.08	Si
ini.	3	-686	117.93	1161.22	SLU 41	9.85	Si
fin.	3	-686	11.19	1161.22	SLU 41	103.75	Si
ini.	3	-674	130.86	1161.22	SLU 84	8.87	Si
fin.	3	-674	9.08	1161.22	SLU 84	127.89	Si
ini.	3	-674	130.86	1161.22	SLU 82	8.87	Si
fin.	3	-674	9.08	1161.22	SLU 82	127.89	Si
ini.	3	-562	118.07	1161.22	SLU 62	9.83	Si
fin.	3	-562	4.98	1161.22	SLU 62	233.08	Si
ini.	3	-686	117.93	1161.22	SLU 40	9.85	Si
fin.	3	-686	11.19	1161.22	SLU 40	103.75	Si
ini.	3	-674	130.86	1161.22	SLU 81	8.87	Si
fin.	3	-674	9.08	1161.22	SLU 81	127.89	Si
ini.	3	-674	130.86	1161.22	SLU 83	8.87	Si
fin.	3	-674	9.08	1161.22	SLU 83	127.89	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni non sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	3	0	117.93	1804			1043	392	SLU 39	0.22	No
fin.	3	0	11.19	-1964			1043	392	SLU 39	0.2	No
ini.	3	0	130.86	1890			1043	392	SLU 83	0.21	No
fin.	3	0	9.08	-2078			1043	392	SLU 83	0.19	No
ini.	3	0	118.07	1622			1043	392	SLU 63	0.24	No
fin.	3	0	4.98	-1801			1043	392	SLU 63	0.22	No
ini.	3	0	118.07	1622			1043	392	SLU 62	0.24	No
fin.	3	0	4.98	-1801			1043	392	SLU 62	0.22	No
ini.	3	0	117.93	1804			1043	392	SLU 41	0.22	No
fin.	3	0	11.19	-1964			1043	392	SLU 41	0.2	No
ini.	3	0	130.86	1890			1043	392	SLU 81	0.21	No
fin.	3	0	9.08	-2078			1043	392	SLU 81	0.19	No
ini.	3	0	130.86	1890			1043	392	SLU 82	0.21	No
fin.	3	0	9.08	-2078			1043	392	SLU 82	0.19	No
ini.	3	0	117.93	1804			1043	392	SLU 42	0.22	No
fin.	3	0	11.19	-1964			1043	392	SLU 42	0.2	No
ini.	3	0	117.93	1804			1043	392	SLU 40	0.22	No
fin.	3	0	11.19	-1964			1043	392	SLU 40	0.2	No
ini.	3	0	130.86	1890			1043	392	SLU 84	0.21	No
fin.	3	0	9.08	-2078			1043	392	SLU 84	0.19	No

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	123	-261.79	1328.31	SLV 12	5.07	Si
fin.	2	391	342.74	1328.31	SLV 12	3.88	Si
ini.	2	-319	-246.3	1328.31	SLV 8	5.39	Si
fin.	2	-20	371.14	1328.31	SLV 8	3.58	Si
ini.	2	-319	-246.3	1328.31	SLV 7	5.39	Si
fin.	2	-20	371.14	1328.31	SLV 7	3.58	Si
ini.	2	-553	403.48	1328.31	SLV 6	3.29	Si
fin.	2	-822	-341.34	1328.31	SLV 6	3.89	Si
ini.	2	-986	194.13	1328.31	SLV 2	6.84	Si
fin.	2	-1020	-58.85	1328.31	SLV 2	22.57	Si
ini.	2	-553	403.48	1328.31	SLV 5	3.29	Si
fin.	2	-822	-341.34	1328.31	SLV 5	3.89	Si
ini.	2	-111	387.99	1328.31	SLV 9	3.42	Si
fin.	2	-411	-369.73	1328.31	SLV 9	3.59	Si
ini.	2	-986	194.13	1328.31	SLV 1	6.84	Si
fin.	2	-1020	-58.85	1328.31	SLV 1	22.57	Si
ini.	2	123	-261.79	1328.31	SLV 11	5.07	Si
fin.	2	391	342.74	1328.31	SLV 11	3.88	Si
ini.	2	-111	387.99	1328.31	SLV 10	3.42	Si
fin.	2	-411	-369.73	1328.31	SLV 10	3.59	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	387.99	181			1564	589	SLV 10	3.25	Si
fin.	2	0	-369.73	-1640			1564	589	SLV 10	0.36	No
ini.	2	0	403.48	-11			1564	589	SLV 6	53.59	Si
fin.	2	0	-341.34	-1857			1564	589	SLV 6	0.32	No
ini.	2	0	403.48	-11			1564	589	SLV 5	53.59	Si



Sezione	γ_M	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
fin.	2	0	-341.34	-1857			1564	589	SLV 5	0.32	No
ini.	2	0	-261.79	1728			1564	589	SLV 11	0.34	No
fin.	2	0	342.74	-92			1564	589	SLV 11	6.4	Si
ini.	2	0	387.99	181			1564	589	SLV 9	3.25	Si
fin.	2	0	-369.73	-1640			1564	589	SLV 9	0.36	No
ini.	2	0	-246.3	1536			1564	589	SLV 7	0.38	No
fin.	2	0	371.14	-309			1564	589	SLV 7	1.91	Si
ini.	2	0	-246.3	1536			1564	589	SLV 8	0.38	No
fin.	2	0	371.14	-309			1564	589	SLV 8	1.91	Si
ini.	2	0	-261.79	1728			1564	589	SLV 12	0.34	No
fin.	2	0	342.74	-92			1564	589	SLV 12	6.4	Si
ini.	2	0	194.13	306			1564	589	SLV 2	1.92	Si
fin.	2	0	-58.85	-1568			1564	589	SLV 2	0.38	No
ini.	2	0	194.13	306			1564	589	SLV 1	1.92	Si
fin.	2	0	-58.85	-1568			1564	589	SLV 1	0.38	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	3.292	SLV 5	Si
V_SLV	0.317	SLV 5	No
PF_SLU	8.874	SLU 81	Si
V_SLU	0.189	SLU 81	No