



azienda casa emilia - romagna  
provincia di bologna

Piazza della Resistenza 4 - 40122  
Bologna - BO  
tel. 051.292111 fax 051.554335  
Codice Fiscale - Partita IVA e Registro  
Imprese di Bologna n. 00322270372  
sito web: www.acerbologna.it  
posta elettronica: info@acerbologna.it

INTERVENTO

**FONDO COMPLEMENTARE AL PIANO NAZIONALE DI RIPRESA E RESILIENZA  
PROGRAMMA "SICURO, VERDE E SOCIALE: RIQUALIFICAZIONE DELL'EDILIZIA RESIDENZIALE PUBBLICA"**

**PROGETTO DI MANUTENZIONE STRAORDINARIA PER IL RESTAURO E RISANAMENTO  
CONSERVATIVO DI DUE CASAMENTI A CORTE SITI IN  
COMUNE DI BOLOGNA LOCALITA' CIRENAICA.  
VIA BENTIVOGLI CIV. 31+59 PER COMPLESSIVI 56 ALLOGGI  
DI ERP CON RELATIVE PERTINENZE E PARTI COMUNI**

LOTTO **3053/PN\_1**

**PROGETTO ESECUTIVO**

TAV.  <b>TAB_01</b>		OGGETTO  TABULATI DI CALCOLO CIVICO 29/2 STATO DI FATTO			DATA  <b>Settembre 2022</b>	
SCALA					N. DISEGNO	
VERSIONE	DESCRIZIONE	DATA	REDATTO	VERIFICATO		APPROVATO
00	PRIMA EMISSIONE	Settembre 2022	F. DALMONTE	N. LEONE		N. LEONE
01						
02						
03						

<b>Il Progettista Architettonico</b>  Arch. Francesca Tovoli Ing. Nicola Leone  SIDEL Ingegneria Srl Via Isonzo, 13 40055 Villanova di Castenaso (BO)	<b>Il Progettista Strutturale</b>  Ing. Nicola Leone  SIDEL Ingegneria Srl Via Isonzo, 13 40055 Villanova di Castenaso (BO)	<b>Il Progettista Impianti Elettrici</b>  Ing. Nicola Leone  SIDEL Ingegneria Srl Via Isonzo, 13 40055 Villanova di Castenaso (BO)	<b>Il Progettista Impianti Meccanici</b>  Ing. Nicola Leone  SIDEL Ingegneria Srl Via Isonzo, 13 40055 Villanova di Castenaso (BO)
<b>Il Coordinatore della Sicurezza in Fase Progettuale</b>  Ing. Nicola Leone  SIDEL Ingegneria Srl Via Isonzo, 13 40055 Villanova di Castenaso (BO)	<b>Il Coordinatore per la progettazione</b>  Ing. Nicola Leone  SIDEL Ingegneria Srl Via Isonzo, 13 40055 Villanova di Castenaso (BO)	<b>Collaboratori Progettisti:</b> Ing. Marco Venturini Ing. Federica DalmonTE Geom. Alessio Breviglieri Arch. Domenico Conaci Geom. Arianna Danieli P. I. Andrea Gamberini Ing. Cesare Orsini	
<b>Responsabile del Procedimento</b>  Ing. Antonio Frighi  ACER Bologna Piazza della Resistenza, 4 40122 Bologna	<b>Il Dirigente Responsabile del Servizio Tecnico</b>  Ing. Antonio Frighi  ACER Bologna Piazza della Resistenza, 4 40122 Bologna	<b>Il Direttore Generale</b>  Avv. Francesco Nitti  ACER Bologna Piazza della Resistenza, 4 40122 Bologna	<b>Il Presidente</b>  Marco Bertuzzi  ACER Bologna Piazza della Resistenza, 4 40122 Bologna

TABULATI DI CALCOLO  
CIVICO 29/2  
STATO DI FATTO



## Sommario

1 Risultati numerici.....	3
1.1 Sollecitazioni.....	3
1.1.1 Sollecitazioni aste.....	3
1.1.1.1 Convenzioni di segno aste.....	3
1.1.1.2 Sollecitazioni estreme aste.....	5
1.1.2 Sollecitazioni gusci.....	6
1.1.2.1 Convenzioni di segno gusci.....	6
1.1.2.2 Sollecitazioni estreme gusci.....	8
1.1.2.3 Sollecitazioni estreme gusci non verticali.....	9
1.1.2.4 Sollecitazioni estreme gusci verticali.....	11
1.1.3 Sollecitazioni gusci armati.....	12
1.1.3.1 Convenzioni di segno gusci.....	12
1.1.4 Sollecitazioni gusci muratura.....	14
1.1.4.1 Convenzioni di segno gusci muratura.....	14
1.1.5 Sollecitazioni aste in muratura.....	16
1.1.5.1 Convenzioni di segno aste.....	16
1.1.6 Sollecitazioni aste in muratura FRCM.....	18
1.1.6.1 Convenzioni di segno aste.....	18
1.1.7 Sollecitazioni aste in muratura armata.....	21
1.1.7.1 Convenzioni di segno aste.....	21
1.2 Reazioni nodali.....	23
1.2.1 Reazioni nodali estreme.....	23
1.2.2 Reazioni nodali in combinazioni di carico.....	24
1.3 Risposta modale.....	281
1.4 Equilibrio globale forze.....	283
1.5 Risposta di spettro.....	284
1.6 Annotazioni solutore.....	284
1.7 Statistiche soluzione.....	284
2 Verifiche.....	284
2.1 Verifica regolarità strutturale.....	284
2.2 Verifica sismica globale.....	286
2.3 Verifiche maschi in muratura.....	292
2.4 Verifiche travi di accoppiamento in muratura.....	352



# 1 Risultati numerici

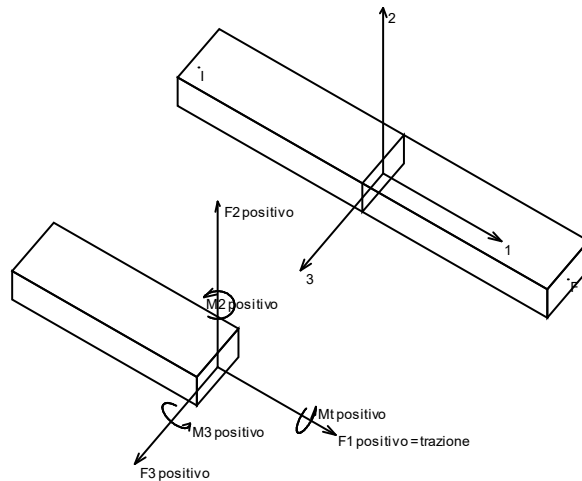
## 1.1 Sollecitazioni

### 1.1.1 Sollecitazioni aste

#### 1.1.1.1 Convenzioni di segno aste

Le abbreviazioni relative alle sollecitazioni sugli elementi aste sono da intendersi:

- $F1$  (N): sforzo normale nell'asta;
- $F2$ : sforzo di taglio agente nella direzione dell'asse locale 2;
- $F3$ : sforzo di taglio agente nella direzione dell'asse locale 3;
- $M1$  ( $M_t$ ): momento attorno all'asse locale 1; equivale al momento torcente;
- $M2$ : momento attorno all'asse locale 2;
- $M3$ : momento attorno all'asse locale 3.



La convenzione sui segni per i parametri di sollecitazione delle aste è la seguente:

presa un'asta con nodo iniziale  $i$  e nodo finale  $f$ , asse 1 che va da  $i$  a  $f$ , assi 2 e 3 presi secondo quanto indicato nei paragrafi successivi relativi al sistema locale delle aste sezionando l'asta in un punto e considerando la sezione sinistra del punto in cui si è effettuato il taglio (sezione da cui esce il versore asse 1) i parametri di sollecitazione sono positivi se hanno verso e direzione concordi con il sistema di riferimento locale dell'asta 1, 2, 3 (per i momenti si adotta la regola della mano destra).

Il sistema è definito diversamente per tre categorie di aste, a seconda che siano originate da:

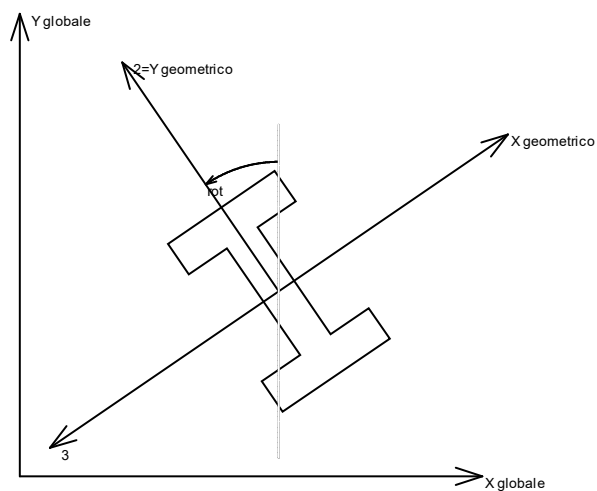
- aste verticali ad esempio pilastri e colonne;
- aste non verticali non di c.a., ad esempio travi di acciaio o legno;
- aste non verticali in c.a.: travi in c.a. di piano, falda o a quota generica.

Nel seguito si indica con 1, 2 e 3 il sistema locale dell'asta che non sempre coincide con gli assi principali della sezione. Si ricorda che per assi principali si intendono gli assi rispetto a cui si ha il raggio di inerzia minimo e massimo. Gli assi 1, 2 e 3 rispettano la regola della mano destra.



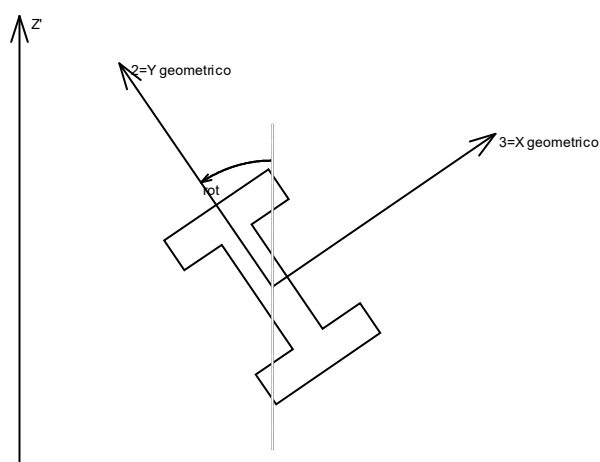


## Sistema locale aste verticali



Nella figura si considera l'asse 1 uscente dal foglio (l'osservatore guarda in direzione opposta a quella dell'asse 1).

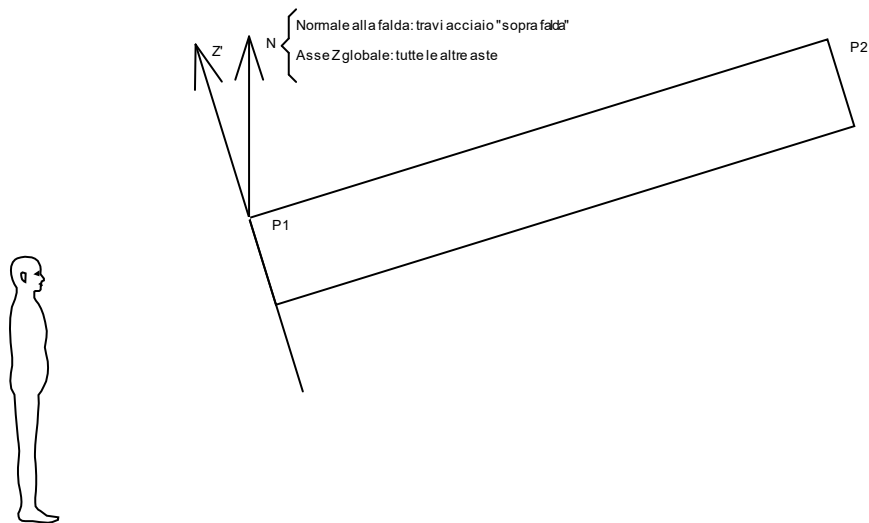
## Sistema locale aste non verticali



Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1).

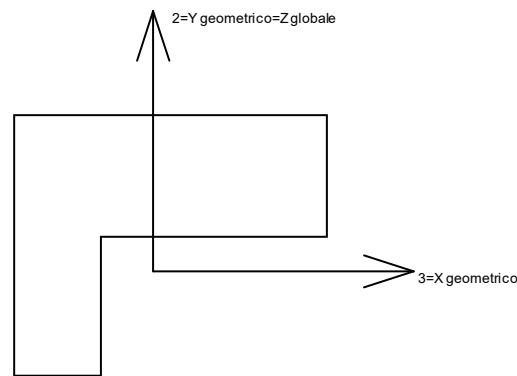
L'asse Z' è illustrato nella figura seguente dove:

- P1 è il punto di inserimento iniziale dell'asta;
- P2 è il punto di inserimento finale dell'asta;
- N è la normale al piano o falda di inserimento;



Z' è quindi l'intersezione tra il piano passante per P1, P2 contenente N e il piano della sezione iniziale dell'asta.

**Sistema locale aste derivanti da travi in c.a.**



Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1). L'asse 2 è sempre verticale e quindi coincidente con l'asse Z globale nonché con l'asse y geometrico. L'asse 3 coincide con l'asse x geometrico. Si sottolinea il fatto che gli assi 2 e 3 non corrispondono agli assi principali della sezione.

#### 1.1.1.2 Sollecitazioni estreme aste

**Asta:** elemento asta a cui si riferiscono le sollecitazioni.

**Ind.:** indice dell'asta.

**Cont.:** contesto a cui si riferisce la sollecitazione

**N.br.:** nome breve della condizione o combinazione di carico.

**Pos.:** numero della sezione all'interno dell'asta (tra 1 e 31, dove 1 corrisponde alla sezione al nodo iniziale, 16 è la sezione in mezzzeria, 31 corrisponde alla sezione al nodo finale).

**Posizione:** posizione a cui si riferisce la sollecitazione dell'asta.

**X:** componente X della posizione a cui si riferisce la sollecitazione dell'asta. [m]

**Y:** componente Y della posizione a cui si riferisce la sollecitazione dell'asta. [m]

**Z:** componente Z della posizione a cui si riferisce la sollecitazione dell'asta. [m]

**Soll.traslazionale:** componente traslazionale della sollecitazione dell'asta.

**F1:** componente F1 della sollecitazione dell'asta. [daN]

**F2:** componente F2 della sollecitazione dell'asta. [daN]

**F3:** componente F3 della sollecitazione dell'asta. [daN]

**Soll.rotazionale:** componente rotazionale della sollecitazione dell'asta.

**M1:** componente M1 della sollecitazione dell'asta. [daN\*m]

**M2:** componente M2 della sollecitazione dell'asta. [daN\*m]

**M3:** componente M3 della sollecitazione dell'asta. [daN\*m]

#### Sollecitazioni con sforzo normale (N) minimo

Vengono mostrate le sole 5 aste più sollecitate.



Asta	Cont.	Pos.	Posizione			Soll.traslazionale			Soll.rotazionale		
Ind.	N.br.		X	Y	Z	F1	F2	F3	M1	M2	M3
9	SLU 81	1	-29.4	2.62	1.39	-22141	-1	9	0.11	443.23	-4.82
5	SLV X	1	-26.39	-0.48	5.15	-2357	-109	-237	0.97	119.74	49.45
6	SLV 13	1	-26.84	-0.48	5.15	-2014	-6338	-62	-3.87	277.95	-8191.95
4	SLV X	1	-25.94	-0.48	5.15	-1926	-68	-163	0.33	109.98	25.34
3	SLV X	1	-25.5	-0.48	5.15	-1545	-56	-168	-0.46	111.25	15.14

#### Sollecitazioni con sforzo normale (N) massimo

Vengono mostrate le sole 5 aste più sollecitate.

Asta	Cont.	Pos.	Posizione			Soll.traslazionale			Soll.rotazionale		
Ind.	N.br.		X	Y	Z	F1	F2	F3	M1	M2	M3
5	SLU 81	1	-26.39	-0.48	5.15	9818	5675	183	145.51	-974.2	-11853.65
4	SLU 81	1	-25.94	-0.48	5.15	9240	4257	215	44.32	-992.23	-3257.1
3	SLU 81	1	-25.5	-0.48	5.15	5334	3082	198	-0.7	-553.55	-380.61
2	SLU 81	1	-25.05	-0.48	5.15	2540	2172	190	-9.88	-261.78	386.02
6	SLV 3	1	-26.84	-0.48	5.15	1741	-6421	6	-4.11	114.05	-8392.39

#### Sollecitazioni con momento M2 minimo

Vengono mostrate le sole 5 aste più sollecitate.

Asta	Cont.	Pos.	Posizione			Soll.traslazionale			Soll.rotazionale		
Ind.	N.br.		X	Y	Z	F1	F2	F3	M1	M2	M3
8	SLV 9	1	-29.4	2.62	5.15	368	-4520	977	9.36	-4732	-4866.16
7	SLV 9	31	-29.4	2.62	5.15	87	4448	-1000	-9.26	-4726.68	-4661.39
9	SLV 15	31	-29.4	2.62	5.15	-8883	123	-386	-14.91	-1403.34	-15.21
4	SLU 81	1	-25.94	-0.48	5.15	9240	4257	215	44.32	-992.23	-3257.1
5	SLU 81	1	-26.39	-0.48	5.15	9818	5675	183	145.51	-974.2	-11853.65

#### Sollecitazioni con momento M2 massimo

Vengono mostrate le sole 5 aste più sollecitate.

Asta	Cont.	Pos.	Posizione			Soll.traslazionale			Soll.rotazionale		
Ind.	N.br.		X	Y	Z	F1	F2	F3	M1	M2	M3
8	SLV 7	1	-29.4	2.62	5.15	-374	-4233	-979	-9.35	4726.18	-3668.53
7	SLV 7	31	-29.4	2.62	5.15	-99	4405	998	9.31	4720.77	-4294.24
9	SLV 1	31	-29.4	2.62	5.15	-8723	-124	392	14.99	1824.28	15.18
6	SLU 82	1	-26.84	-0.48	5.15	-481	-15331	-68	-9.56	472.36	-19920.32
5	SLV Y	1	-26.39	-0.48	5.15	834	-134	-428	0.67	154.77	-30.24

#### Sollecitazioni con momento M3 minimo

Vengono mostrate le sole 5 aste più sollecitate.

Asta	Cont.	Pos.	Posizione			Soll.traslazionale			Soll.rotazionale		
Ind.	N.br.		X	Y	Z	F1	F2	F3	M1	M2	M3
6	SLU 81	1	-26.84	-0.48	5.15	-329	-15339	-67	-9.57	470.71	-19936.56
5	SLU 81	31	-26.84	-0.48	5.15	9818	6469	183	145.51	-892.31	-14567.78
7	SLU 81	31	-29.4	2.62	5.15	-14	10379	-2	0.06	-7.05	-10491.54
8	SLU 82	1	-29.4	2.62	5.15	-100	-10278	-4	0.02	-8.48	-10098.2
4	SLU 81	31	-26.39	-0.48	5.15	9240	5050	215	44.32	-896.23	-5337.33

#### Sollecitazioni con momento M3 massimo

Vengono mostrate le sole 5 aste più sollecitate.

Asta	Cont.	Pos.	Posizione			Soll.traslazionale			Soll.rotazionale		
Ind.	N.br.		X	Y	Z	F1	F2	F3	M1	M2	M3
6	SLU 81	19	-31.24	-0.48	5.15	-329	-79	-67	-9.57	175.27	14036.47
8	SLU 81	20	-32.43	2.62	5.15	-5	105	-3	0.01	-16.74	5378.92
7	SLU 82	12	-26.36	2.62	5.15	-64	-41	-2	0.06	-0.86	5269.64
9	SLV 7	1	-29.4	2.62	1.39	-9900	458	-113	45.67	275.69	1701.79
1	SLU 82	1	-24.6	-0.48	5.15	819	1320	169	-12.98	-99.64	396.47

### 1.1.2 Sollecitazioni gusci

#### 1.1.2.1 Convenzioni di segno gusci

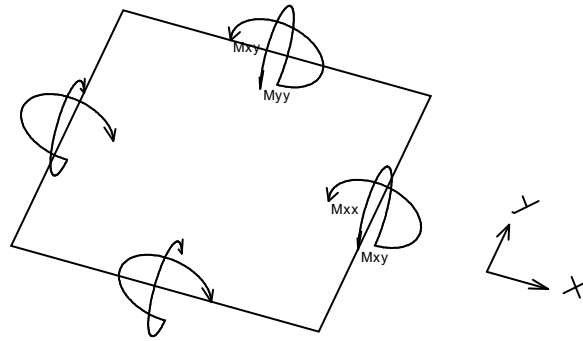
Sono individuate distinte convenzioni di segno in relazione al tipo di elemento strutturale a cui il guscio si riferisce:

- convenzione per gusci non verticali, originati ad esempio da piastre e platee;
- convenzione per gusci verticali, originati ad esempio da pareti e muri.

#### Convenzione di segno per gusci non verticali

Il sistema di riferimento nel quale sono espressi i parametri di sollecitazione è così definito: origine appartenente al piano dell'elemento, asse x e y contenuti nel piano dell'elemento e terzo asse (z) ortogonale al piano dell'elemento a formare una terna destrorsa. In particolare l'asse x ha proiezione in pianta parallela ed equivale all'asse globale X. Nel caso di piastre orizzontali (caso più comune) gli assi x, y e z locali all'elemento sono paralleli ed equivale agli assi X, Y e Z globali. Si sottolinea che non ha alcun interesse collocare esattamente nel piano dell'elemento la posizione dell'origine in quanto i parametri di sollecitazione sono invarianti rispetto a tale posizione.

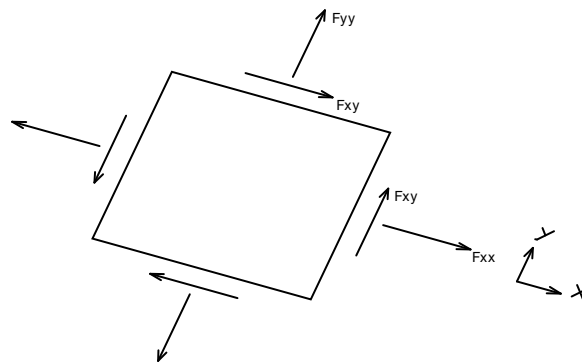
In figura è mostrato un elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione  $M_{xx}$ ,  $M_{yy}$ ,  $M_{xy}$ .



Si definiscono:

- $M_{xx}$ : momento flettente [Forza\*Lunghezza/Lunghezza] agente sul bordo di normale  $x$  (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- $M_{yy}$ : momento flettente [Forza\*Lunghezza/Lunghezza] agente sul bordo di normale  $y$  (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- $M_{xy}$ : momento torcente [Forza\*Lunghezza/Lunghezza] agente sui bordi (verso positivo indicato dalla freccia in figura).

Per quanto riguarda le sollecitazioni estensionali si faccia riferimento alla figura seguente dove per lo stesso elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione  $F_{xx}$ ,  $F_{yy}$ ,  $F_{xy}$ .



Si definiscono:

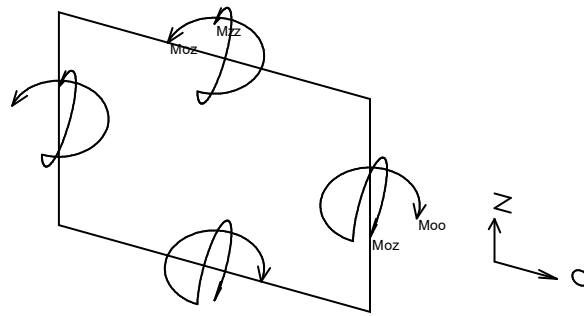
- $F_{xx}$ : sforzo estensionale [Forza/Lunghezza] agente sul bordo di normale  $x$  (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- $F_{yy}$ : sforzo estensionale [Forza/Lunghezza] agente sul bordo di normale all'asse  $y$  (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- $F_{xy}$ : sforzo di taglio [Forza/Lunghezza] agente sui bordi (verso positivo indicato dalla freccia in figura).

Vengono riportati inoltre i tagli fuori dal piano dell'elemento guscio:

- $V_x$ : taglio fuori piano [Forza/Lunghezza] applicato al bordo di normale parallela all'asse  $x$ ;
- $V_y$ : taglio fuori piano [Forza/Lunghezza] applicato al bordo di normale parallela all'asse  $y$ .

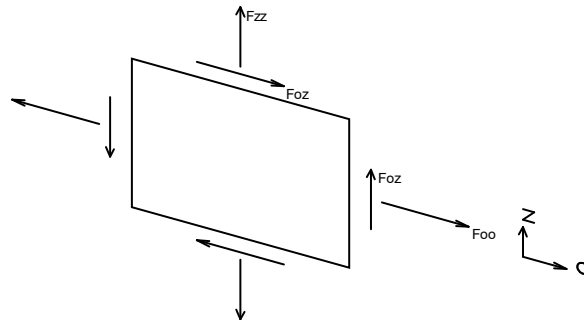
#### Convenzione di segno per gusci verticali

Il sistema di riferimento nel quale sono espressi i parametri di sollecitazione è così definito: origine appartenente al piano dell'elemento, asse  $O$  (ascisse) e  $z$  (ordinate) contenuti nel piano dell'elemento e terzo asse ortogonale al piano dell'elemento a formare una terna destrorsa. In particolare l'asse  $O$  è orizzontale e l'asse  $z$  parallelo ed equiverso con l'asse  $Z$  globale. Si sottolinea che non ha alcun interesse collocare esattamente nel piano dell'elemento la posizione dell'origine in quanto i parametri di sollecitazione sono invarianti rispetto a tale posizione. In figura è mostrato un elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione  $M_{xx}$ ,  $M_{yy}$ ,  $M_{xy}$ ,  $F_{xx}$ ,  $F_{yy}$ ,  $F_{xy}$ .



- Moo: momento flettente distribuito  $[Forza * Lunghezza / Lunghezza]$  applicato al bordo di normale parallela all'asse O (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- Mzz: momento flettente distribuito  $[Forza * Lunghezza / Lunghezza]$  applicato al bordo di normale parallela all'asse z (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- Moz: momento 'torcente' distribuito  $[Forza * Lunghezza / Lunghezza]$  applicato sui bordi (verso positivo indicato dalla freccia in figura).

Per quanto riguarda le sollecitazioni estensionali si faccia riferimento alla figura seguente dove per lo stesso elemento infinitesimo di shell con indicato il sistema di riferimento i parametri di sollecitazione Foo, Fzz, Foz sono rispettivamente:



- Fzz: sforzo tensionale distribuito  $[Forza / Lunghezza]$  applicato al bordo di normale parallela all'asse z (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- Foo: sforzo tensionale distribuito  $[Forza / Lunghezza]$  applicato al bordo di normale parallela all'asse O (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- Foz: sforzo tagliante distribuito  $[Forza / Lunghezza]$  applicato sui bordi (verso positivo indicato dalla freccia in figura).

Vengono riportati inoltre i tagli fuori dal piano dell'elemento guscio:

- Vo: taglio fuori piano applicato al bordo di normale parallela all'asse O;
- Vz: taglio fuori piano applicato al bordo di normale parallela all'asse z.

#### 1.1.2.2 Sollecitazioni estreme gusci

**Shell:** elemento guscio a cui si riferiscono le sollecitazioni.

**Ind:** indice del guscio.

**Cont.:** contesto a cui si riferiscono le sollecitazioni.

**N.br.:** nome breve della condizione o combinazione di carico.

**Nodo:** nodo su cui si basa il guscio a cui si riferisce la sollecitazione.

**Ind:** indice del nodo.

**Sollecitazione:** valori della sollecitazione.

**M11:** componente M11 della sollecitazione del guscio nel nodo indicato.  $[daN * m / m]$

**M12:** componente M12 della sollecitazione del guscio nel nodo indicato.  $[daN * m / m]$

**M22:** componente M22 della sollecitazione del guscio nel nodo indicato.  $[daN * m / m]$

**F11:** componente F11 della sollecitazione del guscio nel nodo indicato.  $[daN / m]$

**F12:** componente F12 della sollecitazione del guscio nel nodo indicato.  $[daN / m]$

**F22:** componente F22 della sollecitazione del guscio nel nodo indicato.  $[daN / m]$

**V13:** componente V13 della sollecitazione del guscio nel nodo indicato.  $[daN / m]$

**V23:** componente V23 della sollecitazione del guscio nel nodo indicato.  $[daN / m]$

#### Sollecitazioni con momento M11 minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione
-------	-------	------	----------------



Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
1603	SLV 15	2342	-1159	-498	-2068	-8446	-4460	-14358	3435	5918
432	SLV 1	1240	-1036	-190	-308	-816	72	-5461	-2082	645
1331	SLV 1	2341	-914	118	-216	5220	-796	-546	-1804	763
425	SLV 1	1240	-908	68	-277	-593	-227	-5427	1807	624
1611	SLV 1	2364	-828	370	-2133	-7510	2965	-11059	-2604	8788

#### Sollecitazioni con momento M11 massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
1603	SLV 1	2342	1265	-19	-402	-200	-1816	-13020	-3029	449
1611	SLV 15	2364	1001	-365	1846	76	-77	-9189	3105	-7864
432	SLV 15	1240	964	181	273	435	-452	-3200	1921	-539
1331	SLV 15	2341	924	-128	253	-905	42	1436	1841	-858
1602	SLV 15	2342	882	26	-1891	-6706	1041	-13027	2103	4713

#### Sollecitazioni con momento M22 minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
1603	SLU 82	2342	14	-656	-3155	-10797	-7495	-32771	812	8227
1602	SLU 82	2342	202	608	-2984	-12455	5693	-30629	-625	6997
1611	SLV 3	2364	-609	302	-2273	-4183	1668	-10713	-1803	9408
1612	SLV 3	2364	-646	-383	-2078	-10984	-2852	-10911	2403	7391
1323	SLV 15	2366	-519	298	-1774	-2454	2088	-8219	-1288	4367

#### Sollecitazioni con momento M22 massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
1611	SLV X	2364	805	-333	2060	2129	-873	762	2454	-8636
1612	SLV X	2364	483	301	1825	4002	719	766	-1792	-6346
1323	SLV 1	2366	555	-254	1548	-3158	695	-6686	1301	-3860
1324	SLV 1	2366	540	254	1533	-5508	-1451	-6805	-1255	-3675
966	SLV 1	1258	322	-251	1415	-8986	4514	-27254	798	-3744

#### Sollecitazioni con sforzo F11 minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
1885	SLU 81	2243	-1	-12	48	-156132	-140927	-223294	-52	-265
1928	SLU 81	2243	-2	9	1	-122700	-129404	-231458	70	226
1936	SLU 81	2231	4	7	-9	-79319	-68521	-61173	-18	26
1892	SLU 82	2192	7	3	-13	-63839	-23662	31901	-32	-88
1891	SLU 81	2192	20	-13	20	-61101	-66740	-22182	173	-54

#### Sollecitazioni con sforzo F11 massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
1928	SLU 81	2334	0	-18	21	155671	102647	129580	35	-79
1885	SLU 81	2337	10	23	25	138781	140328	94873	-151	-62
1892	SLU 81	2338	-3	8	-25	85059	65488	22209	-37	79
1927	SLU 81	2334	1	1	21	67368	2028	44431	-9	-64
1926	SLU 81	2328	0	-1	1	48488	29147	29385	1	-4

#### Sollecitazioni con sforzo F22 minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
1928	SLU 81	2243	-2	9	1	-122700	-129404	-231458	70	226
1885	SLU 81	2243	-1	-12	48	-156132	-140927	-223294	-52	-265
1936	SLU 81	2243	4	6	24	-41201	-4913	-93669	-18	-38
1891	SLU 81	2243	-35	-11	-89	13476	-50212	-72166	174	104
966	SLU 81	1258	8	0	2	-24445	12004	-69870	14	-9

#### Sollecitazioni con sforzo F22 massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	M11	M12	M22	F11	F12	F22	V13	V23
1928	SLU 81	2334	0	-18	21	155671	102647	129580	35	-79
1885	SLU 81	2337	10	23	25	138781	140328	94873	-151	-62
1927	SLU 81	2231	3	-3	-7	32962	58594	82161	-15	-65
1892	SLU 81	2337	10	9	26	17834	41624	62179	-41	-84
1935	SLU 81	2226	0	-1	1	23126	36872	43108	-1	-6

#### 1.1.2.3 Sollecitazioni estreme gusci non verticali

**Shell:** elemento guscio a cui si riferiscono le sollecitazioni.

**Ind:** indice del guscio.

**Cont.:** contesto a cui si riferiscono le sollecitazioni.

**N.br.:** nome breve della condizione o combinazione di carico.

**Nodo:** nodo su cui si basa il guscio a cui si riferisce la sollecitazione.

**Ind:** indice del nodo.



**Sollecitazione:** valori della sollecitazione.

**Mxx:** componente Mxx della sollecitazione del guscio nel nodo indicato. [daN\*m/m]

**Mxy:** componente Mxy della sollecitazione del guscio nel nodo indicato. [daN\*m/m]

**Myy:** componente Myy della sollecitazione del guscio nel nodo indicato. [daN\*m/m]

**Fxx:** componente Fxx della sollecitazione del guscio nel nodo indicato. [daN/m]

**Fxy:** componente Fxy della sollecitazione del guscio nel nodo indicato. [daN/m]

**Fyy:** componente Fyy della sollecitazione del guscio nel nodo indicato. [daN/m]

**Vx:** componente Vo della sollecitazione del guscio nel nodo indicato. [daN/m]

**Vy:** componente Vz della sollecitazione del guscio nel nodo indicato. [daN/m]

#### Sollecitazioni con momento Mxx minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy
1886	SLV 3	2201	-64	12	-16	-4598	-7146	-322	150	-64
1887	SLV 3	2201	-64	3	-16	620	-6023	123	132	26
1911	SLV 7	1793	-49	1	-12	-63	-1218	548	80	22
1884	SLV 3	1402	-41	1	-16	-2403	-7771	-32557	-127	-4
1917	SLV 3	1351	-38	-3	-10	327	-4571	490	151	-16

#### Sollecitazioni con momento Mxx massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy
1886	SLV 13	2201	62	-13	16	-1786	-2023	-925	-150	58
1887	SLV 13	2201	61	-3	15	2113	-2136	555	-134	-26
1919	SLV 13	1351	40	4	10	794	6212	-3373	-173	-32
1917	SLV 13	1351	40	4	10	-265	6476	-1821	-162	18
1911	SLV 9	1793	36	-1	9	-904	1294	393	-30	-19

#### Sollecitazioni con momento Myy minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy
1883	SLV 15	1223	-18	-12	-105	-6214	3674	-14806	36	-351
1884	SLU 82	1222	-17	-9	-69	-6314	-352	-9620	36	-296
1920	SLV 1	1225	-19	-5	-63	-5506	-2004	-12233	-77	-234
1919	SLV 13	1350	-11	-6	-28	2543	6368	4500	-172	117
1886	SLV X	2340	-6	2	-26	-2923	1801	-347	-23	97

#### Sollecitazioni con momento Myy massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy
1920	SLV 15	1225	21	6	67	7235	3204	15788	87	248
1884	SLU 81	1387	34	-9	54	672	-1640	-11190	-147	-297
1883	SLU 81	1387	32	-11	53	162	134	-10589	64	-303
1886	SLV 1	2340	8	-2	33	7657	747	891	29	-115
1919	SLV 13	1226	8	-6	25	3475	3263	4345	-57	117

#### Sollecitazioni con sforzo Fxx minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy
1884	SLV 3	1221	-25	0	-9	-10167	-3977	-30862	-35	-4
1886	SLU 81	2201	-2	-1	0	-7833	-11162	-1460	0	-7
1920	SLV 3	1225	-12	-3	-43	-6915	-2761	-16208	-33	-175
1883	SLU 82	1222	-18	-6	-69	-6581	586	-9876	21	-302
1919	SLV 1	1226	-4	5	-17	-3330	-1707	-4166	8	-71

#### Sollecitazioni con sforzo Fxx massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy
1886	SLU 81	2340	2	-3	10	10581	5563	1550	8	-27
1920	SLV 13	1225	14	4	47	8644	3961	19763	43	189
1884	SLV X	1221	15	-6	4	6259	3437	15132	30	13
1919	SLV 15	1226	3	-5	20	4266	2778	3431	-13	96
1887	SLU 82	2201	0	-1	-1	3371	-9810	1026	-9	-1

#### Sollecitazioni con sforzo Fyy minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy
1884	SLU 81	1402	-28	-9	-20	-617	-3254	-32751	-145	32
1883	SLV 13	1348	8	-11	37	-2341	5641	-19489	-12	-286
1920	SLV 3	1349	4	10	33	-459	-3783	-16764	-14	-175
1913	SLV 13	1693	12	2	6	-1122	5091	-7457	47	-9
1911	SLV 13	1693	12	2	4	-1611	4528	-5574	46	-14

#### Sollecitazioni con sforzo Fyy massimo

Vengono mostrati i soli 5 gusci più sollecitati.



Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Mxx	Mxy	Myy	Fxx	Fxy	Fyy	Vx	Vy
1920	SLV 13	1349	-5	-11	-34	597	5231	20395	26	189
1884	SLV X	1402	24	-7	6	1718	5686	16030	52	13
1883	SLV 3	1348	0	4	-2	2821	-4986	12305	69	-14
1919	SLV 13	1350	-11	-6	-28	2543	6368	4500	-172	117
1913	SLV 3	1693	-11	-1	-5	530	-3416	3483	-11	5

#### 1.1.2.4 Sollecitazioni estreme gusci verticali

**Shell:** elemento guscio a cui si riferiscono le sollecitazioni.

**Ind:** indice del guscio.

**Cont.:** contesto a cui si riferiscono le sollecitazioni.

**N.br.:** nome breve della condizione o combinazione di carico.

**Nodo:** nodo su cui si basa il guscio a cui si riferisce la sollecitazione.

**Ind:** indice del nodo.

**Sollecitazione:** valori della sollecitazione.

**Moo:** componente Moo della sollecitazione del guscio nel nodo indicato. [daN\*m/m]

**Moz:** componente Moz della sollecitazione del guscio nel nodo indicato. [daN\*m/m]

**Mzz:** componente Mzz della sollecitazione del guscio nel nodo indicato. [daN\*m/m]

**Foo:** componente Foo della sollecitazione del guscio nel nodo indicato. [daN/m]

**Foz:** componente Foz della sollecitazione del guscio nel nodo indicato. [daN/m]

**Fzz:** componente Fzz della sollecitazione del guscio nel nodo indicato. [daN/m]

**Vo:** componente Vo della sollecitazione del guscio nel nodo indicato. [daN/m]

**Vz:** componente Vz della sollecitazione del guscio nel nodo indicato. [daN/m]

#### Sollecitazioni con momento Moo minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
1603	SLV 1	2342	-1265	-19	402	-200	1816	-13020	-3029	-449
432	SLV 1	1240	-1036	-190	-308	-816	72	-5461	-2082	645
1611	SLV 15	2364	-1001	-365	-1846	76	77	-9189	3105	7864
1331	SLV 1	2341	-914	118	-216	5220	-796	-546	-1804	763
425	SLV 1	1240	-908	68	-277	-593	-227	-5427	1807	624

#### Sollecitazioni con momento Moo massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
1603	SLV 15	2342	1159	-498	2068	-8446	4460	-14358	3435	-5918
432	SLV 15	1240	964	181	273	435	-452	-3200	1921	-539
1331	SLV 15	2341	924	-128	253	-905	42	1436	1841	-858
425	SLV 15	1240	829	-50	239	162	1283	-3238	-1620	-509
1611	SLV 1	2364	828	370	2133	-7510	-2965	-11059	-2604	-8788

#### Sollecitazioni con momento Mzz minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
1611	SLV X	2364	-805	-333	-2060	2129	873	762	2454	8636
1612	SLV X	2364	-483	301	-1825	4002	-719	766	-1792	6346
1323	SLV 15	2366	-519	298	-1774	-2454	2088	-8219	-1288	4367
1324	SLV 15	2366	-520	-304	-1755	-90	-1550	-7680	1297	4157
966	SLV 15	1258	-316	252	-1416	-13106	6284	-36603	-788	3743

#### Sollecitazioni con momento Mzz massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
1603	SLU 82	2342	-14	-656	3155	-10797	7495	-32771	812	-8227
1602	SLU 82	2342	-202	608	2984	-12455	-5693	-30629	-625	-6997
1611	SLV 3	2364	609	302	2273	-4183	-1668	-10713	-1803	-9408
1612	SLV 3	2364	646	-383	2078	-10984	2852	-10911	2403	-7391
1323	SLV 1	2366	555	-254	1548	-3158	695	-6686	1301	-3860

#### Sollecitazioni con sforzo Foo minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
1885	SLU 81	2243	1	-12	-48	-156132	140927	-223294	-52	265
1928	SLU 81	2243	-2	9	1	-122700	-129404	-231458	70	226
1936	SLU 81	2231	4	7	-9	-79319	-68521	-61173	-18	26
1892	SLU 82	2192	-7	3	13	-63839	23662	31901	-32	88
1891	SLU 81	2192	-20	-13	-20	-61101	66740	-22182	173	54

#### Sollecitazioni con sforzo Foo massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
1928	SLU 81	2334	0	-18	21	155671	102647	129580	35	-79
1885	SLU 81	2337	-10	23	-25	138781	-140328	94873	-151	62





Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
1892	SLU 81	2338	3	8	25	85059	-65488	22209	-37	-79
1927	SLU 81	2334	1	1	21	67368	2028	44431	-9	-64
1926	SLU 81	2328	0	-1	1	48488	29147	29385	1	-4

#### Sollecitazioni con sforzo Fzz minimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
1928	SLU 81	2243	-2	9	1	-122700	-129404	-231458	70	226
1885	SLU 81	2243	1	-12	-48	-156132	140927	-223294	-52	265
1936	SLU 81	2243	4	6	24	-41201	-4913	-93669	-18	-38
1891	SLU 81	2243	35	-11	89	13476	50212	-72166	174	-104
966	SLU 81	1258	8	0	2	-24445	12004	-69870	14	-9

#### Sollecitazioni con sforzo Fzz massimo

Vengono mostrati i soli 5 gusci più sollecitati.

Shell	Cont.	Nodo	Sollecitazione							
Ind	N.br.	Ind	Moo	Moz	Mzz	Foo	Foz	Fzz	Vo	Vz
1928	SLU 81	2334	0	-18	21	155671	102647	129580	35	-79
1885	SLU 81	2337	-10	23	-25	138781	-140328	94873	-151	62
1927	SLU 81	2231	3	-3	-7	32962	58594	82161	-15	-65
1892	SLU 81	2337	-10	9	-26	17834	-41624	62179	-41	84
1935	SLU 81	2226	0	-1	1	23126	36872	43108	-1	-6

### 1.1.3 Sollecitazioni gusci armati

#### 1.1.3.1 Convenzioni di segno gusci

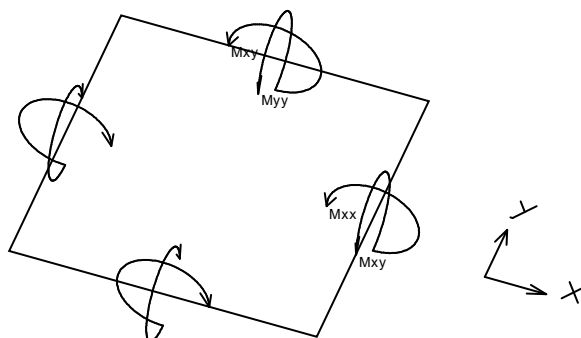
Sono individuate distinte convenzioni di segno in relazione al tipo di elemento strutturale a cui il guscio si riferisce:

- convenzione per gusci non verticali, originati ad esempio da piastre e platee;
- convenzione per gusci verticali, originati ad esempio da pareti e muri.

#### Convenzione di segno per gusci non verticali

Il sistema di riferimento nel quale sono espressi i parametri di sollecitazione è così definito: origine appartenente al piano dell'elemento, asse x e y contenuti nel piano dell'elemento e terzo asse (z) ortogonale al piano dell'elemento a formare una terna destrorsa. In particolare l'asse x ha proiezione in pianta parallela ed equiversa all'asse globale X. Nel caso di piastre orizzontali (caso più comune) gli assi x, y e z locali all'elemento sono paralleli ed equiversi agli assi X, Y e Z globali. Si sottolinea che non ha alcun interesse collocare esattamente nel piano dell'elemento la posizione dell'origine in quanto i parametri di sollecitazione sono invarianti rispetto a tale posizione.

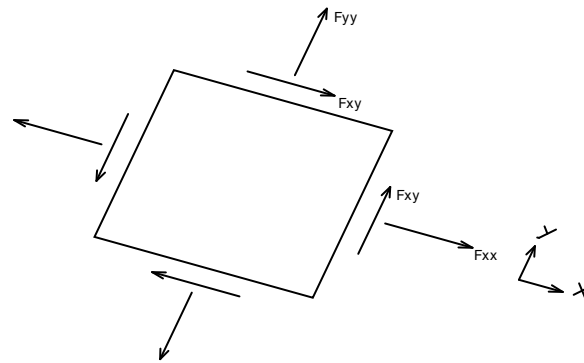
In figura è mostrato un elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione Mxx, Myy, Mxy.



Si definiscono:

- Mxx: momento flettente  $[Forza \cdot Lunghezza / Lunghezza]$  agente sul bordo di normale x (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- Myy: momento flettente  $[Forza \cdot Lunghezza / Lunghezza]$  agente sul bordo di normale y (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- Mxy: momento torcente  $[Forza \cdot Lunghezza / Lunghezza]$  agente sui bordi (verso positivo indicato dalla freccia in figura).

Per quanto riguarda le sollecitazioni estensionali si faccia riferimento alla figura seguente dove per lo stesso elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione Fxx, Fyy, Fxy.



Si definiscono:

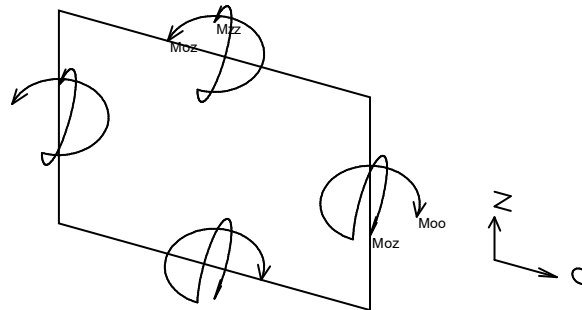
- $F_{xx}$ : sforzo estensionale [Forza/Lunghezza] agente sul bordo di normale  $x$  (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- $F_{yy}$ : sforzo estensionale [Forza/Lunghezza] agente sul bordo di normale all'asse  $y$  (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- $F_{xy}$ : sforzo di taglio [Forza/Lunghezza] agente sui bordi (verso positivo indicato dalla freccia in figura).

Vengono riportati inoltre i tagli fuori dal piano dell'elemento guscio:

- $V_x$ : taglio fuori piano [Forza/Lunghezza] applicato al bordo di normale parallela all'asse  $x$ ;
- $V_y$ : taglio fuori piano [Forza/Lunghezza] applicato al bordo di normale parallela all'asse  $y$ .

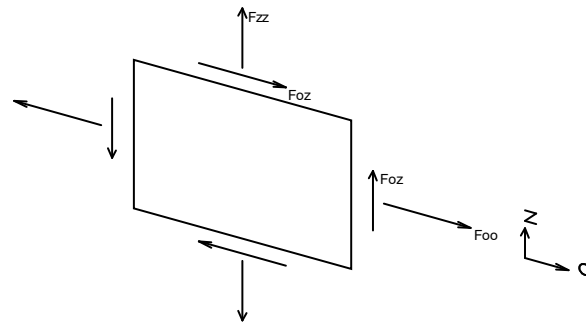
#### Convenzione di segno per gusci verticali

Il sistema di riferimento nel quale sono espressi i parametri di sollecitazione è così definito: origine appartenente al piano dell'elemento, asse  $O$  (ascisse) e  $z$  (ordinate) contenuti nel piano dell'elemento e terzo asse ortogonale al piano dell'elemento a formare una terna destrorsa. In particolare l'asse  $O$  è orizzontale e l'asse  $z$  parallelo ed equiverso con l'asse  $Z$  globale. Si sottolinea che non ha alcun interesse collocare esattamente nel piano dell'elemento la posizione dell'origine in quanto i parametri di sollecitazione sono invarianti rispetto a tale posizione. In figura è mostrato un elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione  $M_{oo}$ ,  $M_{zz}$ ,  $M_{oz}$ .



- $M_{oo}$ : momento flettente distribuito [Forza\*Lunghezza/Lunghezza] applicato al bordo di normale parallela all'asse  $O$  (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- $M_{zz}$ : momento flettente distribuito [Forza\*Lunghezza/Lunghezza] applicato al bordo di normale parallela all'asse  $z$  (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- $M_{oz}$ : momento 'torcente' distribuito [Forza\*Lunghezza/Lunghezza] applicato sui bordi (verso positivo indicato dalla freccia in figura).

Per quanto riguarda le sollecitazioni estensionali si faccia riferimento alla figura seguente dove per lo stesso elemento infinitesimo di shell con indicato il sistema di riferimento i parametri di sollecitazione  $F_{oo}$ ,  $F_{zz}$ ,  $F_{oz}$  sono rispettivamente:



- $F_{zz}$ : sforzo tensionale distribuito [Forza/Lunghezza] applicato al bordo di normale parallela all'asse  $z$  (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- $F_{oo}$ : sforzo tensionale distribuito [Forza/Lunghezza] applicato al bordo di normale parallela all'asse  $O$  (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- $F_{oz}$ : sforzo tagliante distribuito [Forza/Lunghezza] applicato sui bordi (verso positivo indicato dalla freccia in figura).

Vengono riportati inoltre i tagli fuori dal piano dell'elemento guscio:

- $V_o$ : taglio fuori piano applicato al bordo di normale parallela all'asse  $O$ ;
- $V_z$ : taglio fuori piano applicato al bordo di normale parallela all'asse  $z$ .

### 1.1.4 Sollecitazioni gusci muratura

#### 1.1.4.1 Convenzioni di segno gusci muratura

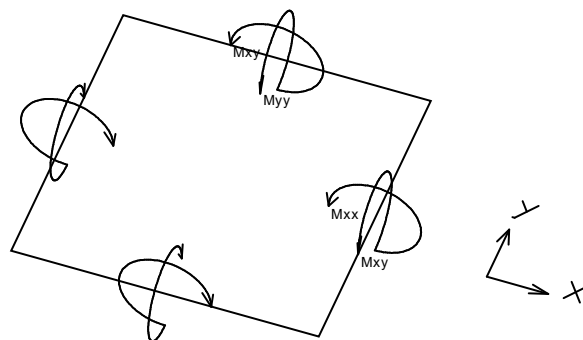
Sono individuate distinte convenzioni di segno in relazione al tipo di elemento strutturale a cui il guscio muratura si riferisce:

- convenzione per gusci non verticali, originati ad esempio da piastre e platee;
- convenzione per gusci verticali, originati ad esempio da pareti e muri.

#### Convenzione di segno per gusci non verticali

Il sistema di riferimento nel quale sono espressi i parametri di sollecitazione è così definito: origine appartenente al piano dell'elemento, asse  $x$  e  $y$  contenuti nel piano dell'elemento e terzo asse ( $z$ ) ortogonale al piano dell'elemento a formare una terna destrorsa. In particolare l'asse  $x$  ha proiezione in pianta parallela ed equiversa all'asse globale  $X$ . Nel caso di piastre orizzontali (caso più comune) gli assi  $x$ ,  $y$  e  $z$  locali all'elemento sono paralleli ed equiversi agli assi  $X$ ,  $Y$  e  $Z$  globali. Si sottolinea che non ha alcun interesse collocare esattamente nel piano dell'elemento la posizione dell'origine in quanto i parametri di sollecitazione sono invarianti rispetto a tale posizione.

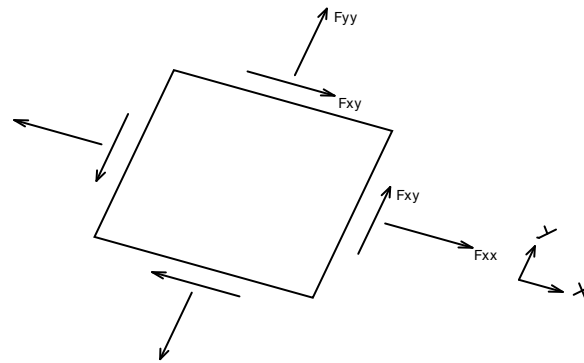
In figura è mostrato un elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione  $M_{xx}$ ,  $M_{yy}$ ,  $M_{xy}$ .



Si definiscono:

- $M_{xx}$ : momento flettente [Forza\*Lunghezza/Lunghezza] agente sul bordo di normale  $x$  (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- $M_{yy}$ : momento flettente [Forza\*Lunghezza/Lunghezza] agente sul bordo di normale  $y$  (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- $M_{xy}$ : momento torcente [Forza\*Lunghezza/Lunghezza] agente sui bordi (verso positivo indicato dalla freccia in figura).

Per quanto riguarda le sollecitazioni estensionali si faccia riferimento alla figura seguente dove per lo stesso elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione  $F_{xx}$ ,  $F_{yy}$ ,  $F_{xy}$ .

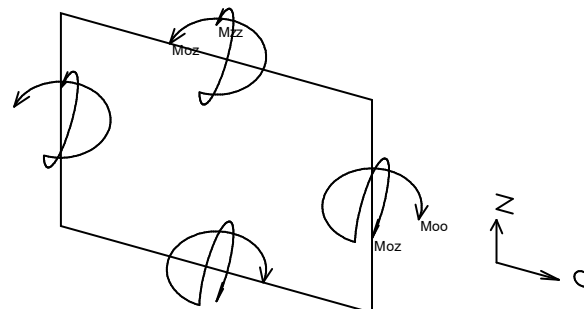


Si definiscono:

- $F_{xx}$ : sforzo tensionale [Forza/Lunghezza] agente sul bordo di normale  $x$  (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- $F_{yy}$ : sforzo tensionale [Forza/Lunghezza] agente sul bordo di normale all'asse  $y$  (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);
- $F_{xy}$ : sforzo tagliante [Forza/Lunghezza] agente sui bordi (verso positivo indicato dalla freccia in figura).

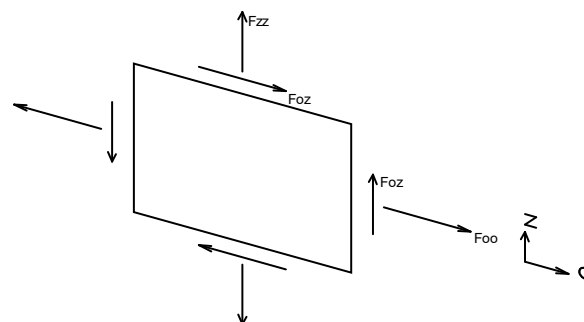
#### Convenzione di segno per gusci verticali

Il sistema di riferimento nel quale sono espressi i parametri di sollecitazione è così definito: origine appartenente al piano dell'elemento, asse  $O$  (ascisse) e  $z$  (ordinate) contenuti nel piano dell'elemento e terzo asse ortogonale al piano dell'elemento a formare una terna destrorsa. In particolare l'asse  $O$  è orizzontale e l'asse  $z$  parallelo ed equiverso con l'asse  $Z$  globale. Si sottolinea che non ha alcun interesse collocare esattamente nel piano dell'elemento la posizione dell'origine in quanto i parametri di sollecitazione sono invarianti rispetto a tale posizione. In figura è mostrato un elemento infinitesimo di shell orizzontale con indicato il sistema di riferimento e i parametri di sollecitazione  $M_{oo}$ ,  $M_{zz}$ ,  $M_{oz}$ .



- $M_{oo}$ : momento flettente distribuito [Forza\*Lunghezza/Lunghezza] applicato al bordo di normale parallela all'asse  $O$  (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- $M_{zz}$ : momento flettente distribuito [Forza\*Lunghezza/Lunghezza] applicato al bordo di normale parallela all'asse  $z$  (verso positivo indicato dalla freccia in figura che tende le fibre inferiori);
- $M_{oz}$ : momento 'torcente' distribuito [Forza\*Lunghezza/Lunghezza] applicato sui bordi (verso positivo indicato dalla freccia in figura).

Per quanto riguarda le sollecitazioni estensionali si faccia riferimento alla figura seguente dove per lo stesso elemento infinitesimo di shell con indicato il sistema di riferimento i parametri di sollecitazione  $F_{oo}$ ,  $F_{zz}$ ,  $F_{oz}$  sono rispettivamente:



- $F_{zz}$ : sforzo tensionale distribuito [Forza/Lunghezza] applicato al bordo di normale parallela all'asse  $z$  (verso positivo indicato dalla freccia in figura che



mette in trazione l'elemento);

- $F_{oo}$ : sforzo tensionale distribuito [Forza/Lunghezza] applicato al bordo di normale parallela all'asse O (verso positivo indicato dalla freccia in figura che mette in trazione l'elemento);

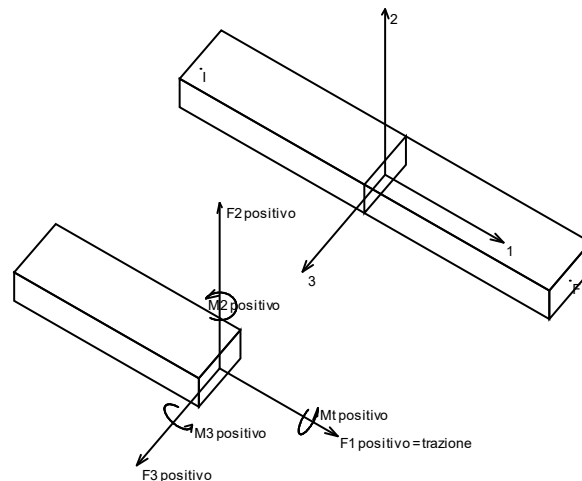
- $F_{oz}$ : sforzo tagliante distribuito [Forza/Lunghezza] applicato sui bordi (verso positivo indicato dalla freccia in figura).

## 1.1.5 Sollecitazioni aste in muratura

### 1.1.5.1 Convenzioni di segno aste

Le abbreviazioni relative alle sollecitazioni sugli elementi aste sono da intendersi:

- $F_1$  (N): sforzo normale nell'asta;
- $F_2$ : sforzo di taglio agente nella direzione dell'asse locale 2;
- $F_3$ : sforzo di taglio agente nella direzione dell'asse locale 3;
- $M_1$  (Mt): momento attorno all'asse locale 1; equivale al momento torcente;
- $M_2$ : momento attorno all'asse locale 2;
- $M_3$ : momento attorno all'asse locale 3.



La convenzione sui segni per i parametri di sollecitazione delle aste è la seguente:

presa un'asta con nodo iniziale  $i$  e nodo finale  $f$ , asse 1 che va da  $i$  a  $f$ , assi 2 e 3 presi secondo quanto indicato nei paragrafi successivi relativi al sistema locale delle aste sezionando l'asta in un punto e considerando la sezione sinistra del punto in cui si è effettuato il taglio (sezione da cui esce il versore asse 1) i parametri di sollecitazione sono positivi se hanno verso e direzione concordi con il sistema di riferimento locale dell'asta 1, 2, 3 (per i momenti si adotta la regola della mano destra).

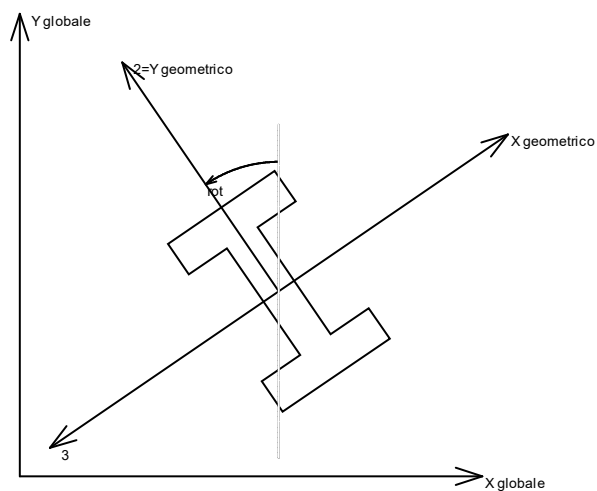
Il sistema è definito diversamente per tre categorie di aste, a seconda che siano originate da:

- aste verticali ad esempio pilastri e colonne;
- aste non verticali non di c.a., ad esempio travi di acciaio o legno;
- aste non verticali in c.a.: travi in c.a. di piano, falda o a quota generica.

Nel seguito si indica con 1, 2 e 3 il sistema locale dell'asta che non sempre coincide con gli assi principali della sezione. Si ricorda che per assi principali si intendono gli assi rispetto a cui si ha il raggio di inerzia minimo e massimo. Gli assi 1, 2 e 3 rispettano la regola della mano destra.

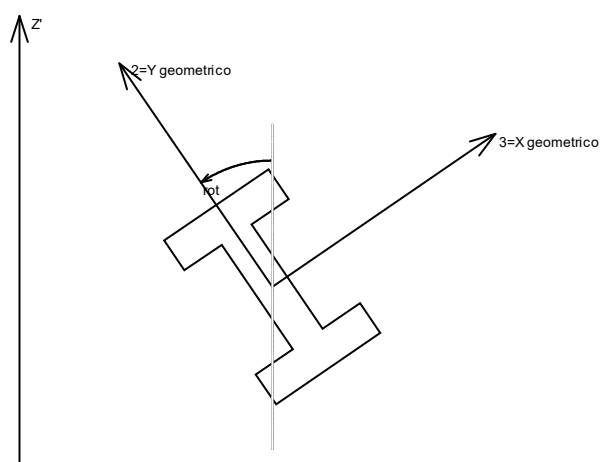


## Sistema locale aste verticali



Nella figura si considera l'asse 1 uscente dal foglio (l'osservatore guarda in direzione opposta a quella dell'asse 1).

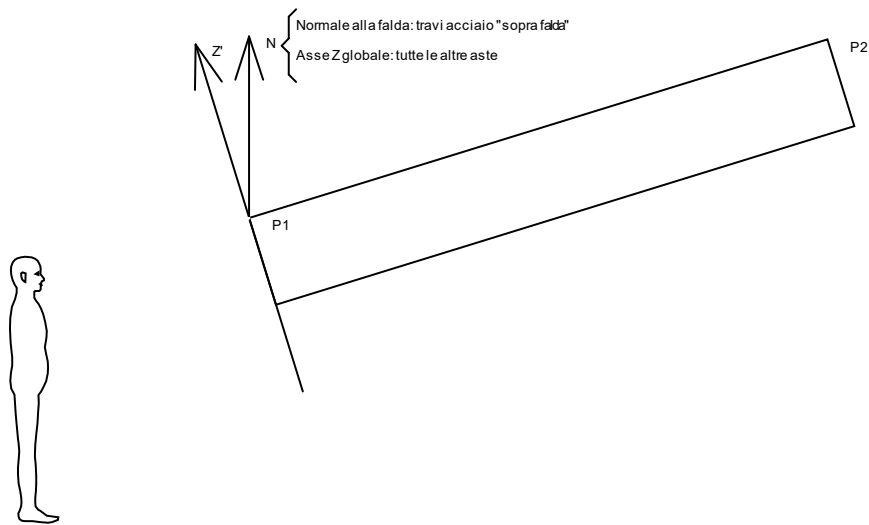
## Sistema locale aste non verticali



Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1).

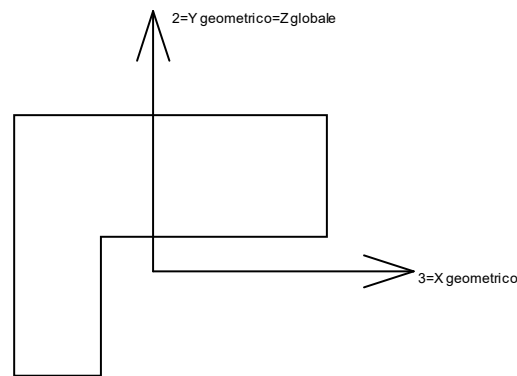
L'asse Z' è illustrato nella figura seguente dove:

- P1 è il punto di inserimento iniziale dell'asta;
- P2 è il punto di inserimento finale dell'asta;
- N è la normale al piano o falda di inserimento;



Z' è quindi l'intersezione tra il piano passante per P1, P2 contenente N e il piano della sezione iniziale dell'asta.

**Sistema locale aste derivanti da travi in c.a.**



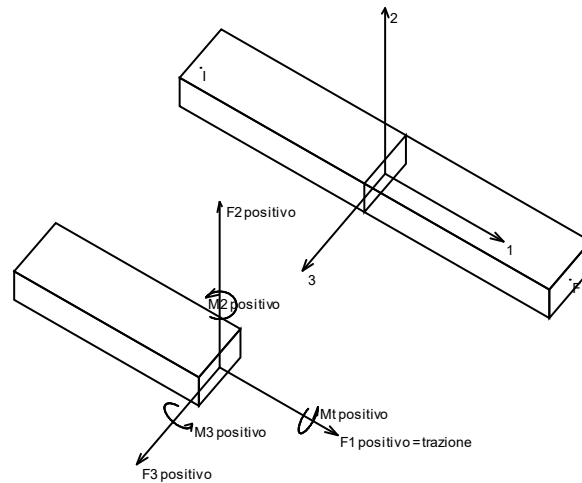
Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1). L'asse 2 è sempre verticale e quindi coincidente con l'asse Z globale nonché con l'asse y geometrico. L'asse 3 coincide con l'asse x geometrico. Si sottolinea il fatto che gli assi 2 e 3 non corrispondono agli assi principali della sezione.

### 1.1.6 Sollecitazioni aste in muratura FRCM

#### 1.1.6.1 Convenzioni di segno aste

Le abbreviazioni relative alle sollecitazioni sugli elementi aste sono da intendersi:

- F1 (N): sforzo normale nell'asta;
- F2: sforzo di taglio agente nella direzione dell'asse locale 2;
- F3: sforzo di taglio agente nella direzione dell'asse locale 3;
- M1 (Mt): momento attorno all'asse locale 1; equivale al momento torcente;
- M2: momento attorno all'asse locale 2;
- M3: momento attorno all'asse locale 3.



La convenzione sui segni per i parametri di sollecitazione delle aste è la seguente:

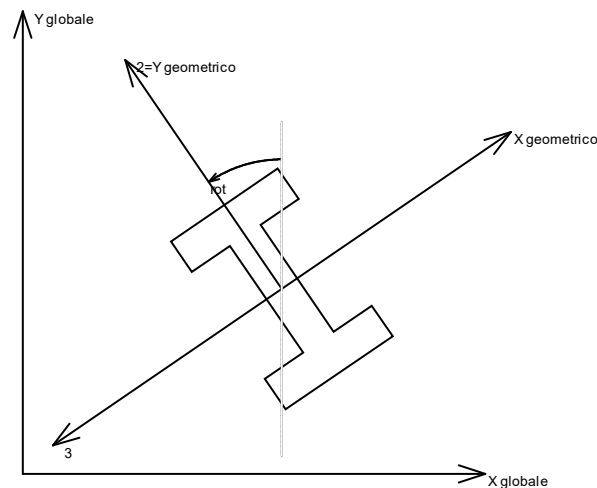
presa un'asta con nodo iniziale  $i$  e nodo finale  $f$ , asse 1 che va da  $i$  a  $f$ , assi 2 e 3 presi secondo quanto indicato nei paragrafi successivi relativi al sistema locale delle aste sezionando l'asta in un punto e considerando la sezione sinistra del punto in cui si è effettuato il taglio (sezione da cui esce il versore asse 1) i parametri di sollecitazione sono positivi se hanno verso e direzione concordi con il sistema di riferimento locale dell'asta 1, 2, 3 (per i momenti si adotta la regola della mano destra).

Il sistema è definito diversamente per tre categorie di aste, a seconda che siano originate da:

- aste verticali ad esempio pilastri e colonne;
- aste non verticali non di c.a., ad esempio travi di acciaio o legno;
- aste non verticali in c.a.: travi in c.a. di piano, falda o a quota generica.

Nel seguito si indica con 1, 2 e 3 il sistema locale dell'asta che non sempre coincide con gli assi principali della sezione. Si ricorda che per assi principali si intendono gli assi rispetto a cui si ha il raggio di inerzia minimo e massimo. Gli assi 1, 2 e 3 rispettano la regola della mano destra.

#### Sistema locale aste verticali

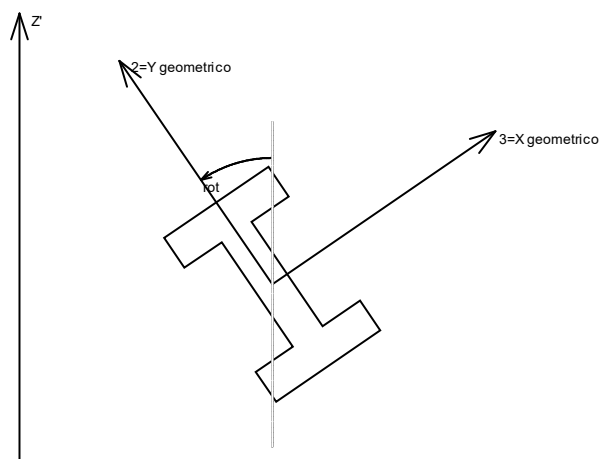


Nella figura si considera l'asse 1 uscente dal foglio (l'osservatore guarda in direzione opposta a quella dell'asse 1).





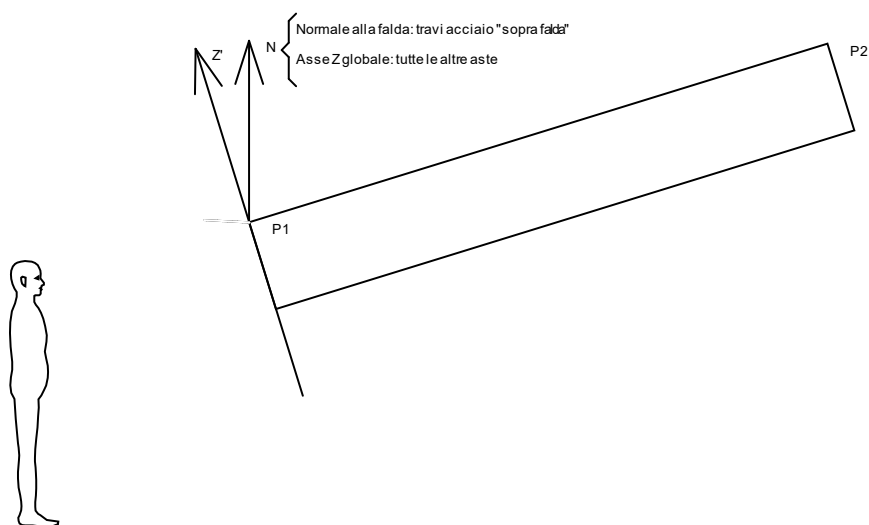
## Sistema locale aste non verticali



Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1).

L'asse  $Z'$  è illustrato nella figura seguente dove:

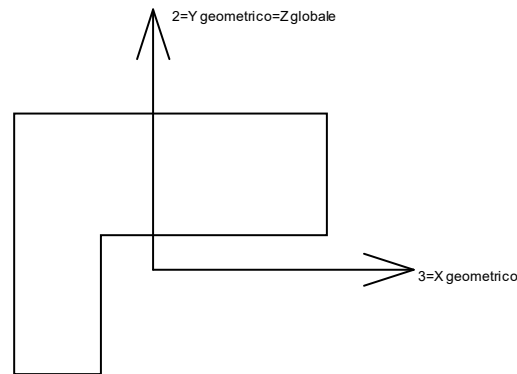
- $P1$  è il punto di inserimento iniziale dell'asta;
- $P2$  è il punto di inserimento finale dell'asta;
- $N$  è la normale al piano o falda di inserimento;



$Z'$  è quindi l'intersezione tra il piano passante per  $P1, P2$  contenente  $N$  e il piano della sezione iniziale dell'asta.



## Sistema locale aste derivanti da travi in c.a.



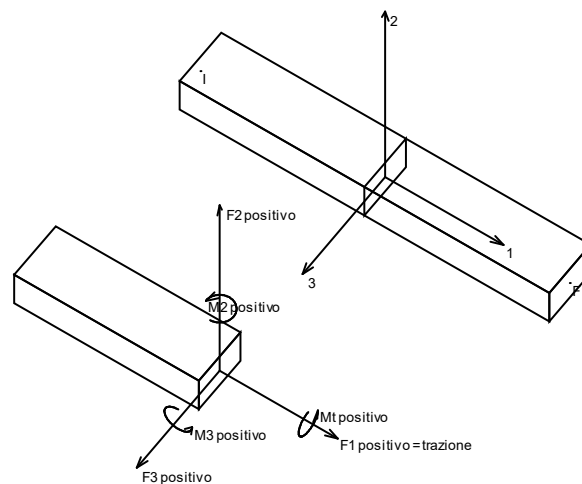
Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1). L'asse 2 è sempre verticale e quindi coincidente con l'asse Z globale nonché con l'asse y geometrico. L'asse 3 coincide con l'asse x geometrico. Si sottolinea il fatto che gli assi 2 e 3 non corrispondono agli assi principali della sezione.

### 1.1.7 Sollecitazioni aste in muratura armata

#### 1.1.7.1 Convenzioni di segno aste

Le abbreviazioni relative alle sollecitazioni sugli elementi aste sono da intendersi:

- F1 (N): sforzo normale nell'asta;
- F2: sforzo di taglio agente nella direzione dell'asse locale 2;
- F3: sforzo di taglio agente nella direzione dell'asse locale 3;
- M1 (Mt): momento attorno all'asse locale 1; equivale al momento torcente;
- M2: momento attorno all'asse locale 2;
- M3: momento attorno all'asse locale 3.



La convenzione sui segni per i parametri di sollecitazione delle aste è la seguente:

presa un'asta con nodo iniziale i e nodo finale f, asse 1 che va da i a f, assi 2 e 3 presi secondo quanto indicato nei paragrafi successivi relativi al sistema locale delle aste sezionando l'asta in un punto e considerando la sezione sinistra del punto in cui si è effettuato il taglio (sezione da cui esce il vettore asse 1) i parametri di sollecitazione sono positivi se hanno verso e direzione concordi con il sistema di riferimento locale dell'asta 1, 2, 3 (per i momenti si adotta la regola della mano destra).

Il sistema è definito diversamente per tre categorie di aste, a seconda che siano originate da:

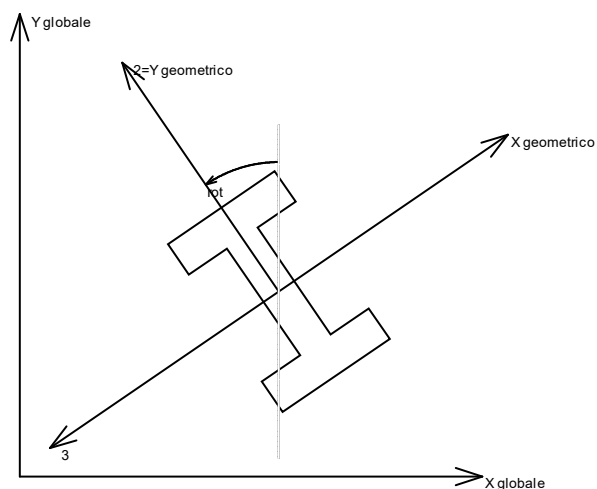
- aste verticali ad esempio pilastri e colonne;
- aste non verticali non di c.a., ad esempio travi di acciaio o legno;
- aste non verticali in c.a.: travi in c.a. di piano, falda o a quota generica.

Nel seguito si indica con 1, 2 e 3 il sistema locale dell'asta che non sempre coincide con gli assi principali della sezione. Si ricorda che per assi principali si intendono gli



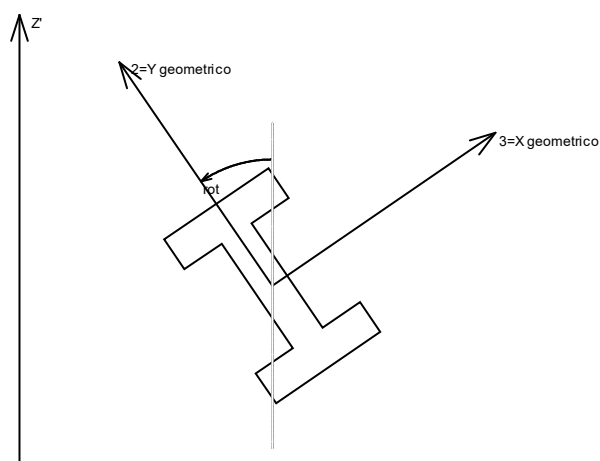
assi rispetto a cui si ha il raggio di inerzia minimo e massimo. Gli assi 1, 2 e 3 rispettano la regola della mano destra.

#### Sistema locale aste verticali



Nella figura si considera l'asse 1 uscente dal foglio (l'osservatore guarda in direzione opposta a quella dell'asse 1).

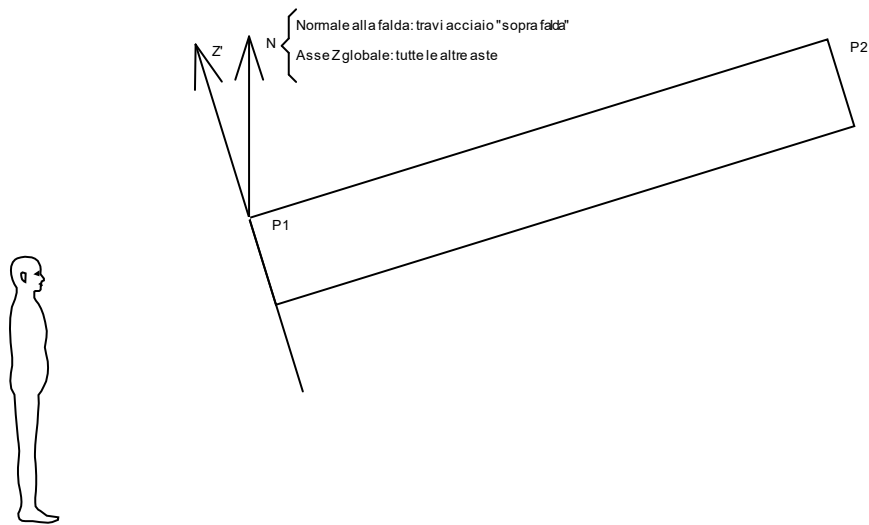
#### Sistema locale aste non verticali



Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1).

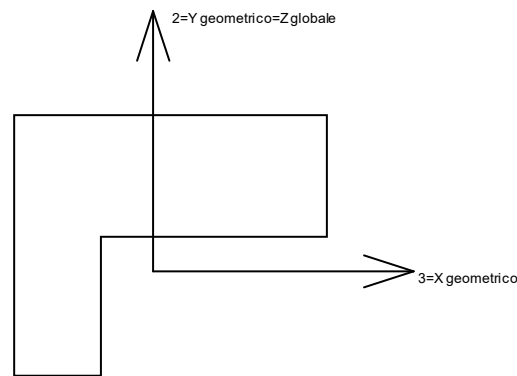
L'asse Z' è illustrato nella figura seguente dove:

- P1 è il punto di inserimento iniziale dell'asta;
- P2 è il punto di inserimento finale dell'asta;
- N è la normale al piano o falda di inserimento;



Z' è quindi l'intersezione tra il piano passante per P1, P2 contenente N e il piano della sezione iniziale dell'asta.

Sistema locale aste derivanti da travi in c.a.



Nella figura si considera l'asse 1 entrante nel foglio (l'osservatore guarda in direzione coincidente a quella dell'asse 1). L'asse 2 è sempre verticale e quindi coincidente con l'asse Z globale nonché con l'asse y geometrico. L'asse 3 coincide con l'asse x geometrico. Si sottolinea il fatto che gli assi 2 e 3 non corrispondono agli assi principali della sezione.

## 1.2 Reazioni nodali

### 1.2.1 Reazioni nodali estreme

**Nodo:** Nodo sollecitato dalla reazione vincolare.

**Ind.:** indice del nodo.

**Cont.:** Contesto a cui si riferisce la reazione vincolare.

**N.br.:** nome breve della condizione o combinazione di carico.

**Reazione a traslazione:** reazione vincolare traslazionale del nodo.

**x:** componente X della reazione vincolare del nodo. [daN]

**y:** componente Y della reazione vincolare del nodo. [daN]

**z:** componente Z della reazione vincolare del nodo. [daN]

**Reazione a rotazione:** reazione vincolare rotazionale del nodo.

**x:** componente X della reazione a rotazione del nodo. [daN\*m]

**y:** componente Y della reazione a rotazione del nodo. [daN\*m]

**z:** componente Z della reazione a rotazione del nodo. [daN\*m]

#### Reazioni Fx minime

Vengono mostrati i soli 5 nodi più sollecitati.

Nodo	Cont.	Reazione a traslazione	Reazione a rotazione
------	-------	------------------------	----------------------



Ind.	N.br.	x	y	z	x	y	z
21	SLV 13	-1103	27	3522	-7.46	-43.94	0.06
77	SLU 82	-1095	-2	5264	1.09	-23.54	0.13
20	SLV 13	-897	252	5344	-9.48	-36.35	0.06
19	SLV 15	-797	-9	2486	11.87	-32.77	0.03
22	SLV 13	-794	259	3733	-12.91	-32.63	-0.08

#### Reazioni Fx massime

Vengono mostrati i soli 5 nodi più sollecitati.

Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
73	SLV 3	1016	-21	2783	12.6	44.78	0.02
74	SLV 3	978	-22	3412	11.32	39.28	0.01
3	SLV 1	943	-13	3358	1.02	43.9	-0.05
72	SLV 3	930	-21	2275	12.59	37.94	0.02
75	SLV 3	910	-24	4256	7.88	40.09	-0.02

#### Reazioni Fy minime

Vengono mostrati i soli 5 nodi più sollecitati.

Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
76	SLU 81	-112	-1370	12313	11.3	-13.55	-0.06
117	SLV 11	-10	-1211	2075	103.38	-17.85	0.01
123	SLV 11	6	-1171	1602	82.17	-6.02	-0.02
129	SLV 11	11	-1123	1542	70.27	0.16	0.02
114	SLV 9	-33	-1122	2543	106.18	-23.53	0.06

#### Reazioni Fy massime

Vengono mostrati i soli 5 nodi più sollecitati.

Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
99	SLV 9	-8	1192	2273	-99.28	-15.79	0.02
87	SLV 9	6	1159	1731	-83.91	-4.93	0
25	SLV 5	-12	1128	440	-48.92	2.84	0.01
29	SLV 5	-9	1116	1145	-57.22	8.35	0
81	SLV 9	18	1115	1384	-74.27	1.65	-0.03

#### Reazioni Fz minime

Vengono mostrati i soli 5 nodi più sollecitati.

Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
20	SLV Y	161	-501	-2808	23.96	6.06	-0.04
30	SLV Y	448	-373	-2711	16.14	16.99	-0.17
34	SLV Y	10	-592	-2206	25.05	5.55	0.03
22	SLV 5	-374	-242	-1878	14.56	-14.54	0.14
76	SLV X	-373	306	-1871	-6.52	-21.93	-0.09

#### Reazioni Fz massime

Vengono mostrati i soli 5 nodi più sollecitati.

Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
76	SLU 81	-112	-1370	12313	11.3	-13.55	-0.06
22	SLV 11	-38	458	6124	-23.64	-3.32	-0.16
20	SLV 9	-606	724	6110	-31.86	-23.95	0.05
75	SLU 81	614	-4	5843	1.76	22.2	-0.01
21	SLV 11	-230	43	5686	-12.6	-12.14	0.11

### 1.2.2 Reazioni nodali in combinazioni di carico

**Nodo:** Nodo sollecitato dalla reazione vincolare.

**Ind.:** indice del nodo.

**Cont.:** Contesto a cui si riferisce la reazione vincolare.

**N.br.:** nome breve della condizione o combinazione di carico.

**Reazione a traslazione:** reazione vincolare traslazionale del nodo.

**x:** componente X della reazione vincolare del nodo. [daN]

**y:** componente Y della reazione vincolare del nodo. [daN]

**z:** componente Z della reazione vincolare del nodo. [daN]

**Reazione a rotazione:** reazione vincolare rotazionale del nodo.

**x:** componente X della reazione a rotazione del nodo. [daN\*m]

**y:** componente Y della reazione a rotazione del nodo. [daN\*m]

**z:** componente Z della reazione a rotazione del nodo. [daN\*m]

Nodo	Cont.	Reazione a traslazione			Reazione a rotazione		
Ind.	N.br.	x	y	z	x	y	z
2	SLU 1	399	336	2606	-8.97	11.62	-0.01
2	SLU 2	394	328	2567	-8.99	11.25	-0.01
2	SLU 3	399	336	2606	-8.97	11.62	-0.01
2	SLU 4	396	331	2583	-8.98	11.4	-0.01
2	SLU 5	394	328	2567	-8.99	11.25	-0.01
2	SLU 6	399	336	2606	-8.97	11.62	-0.01
2	SLU 7	396	331	2583	-8.98	11.4	-0.01
2	SLU 8	399	336	2606	-8.97	11.62	-0.01
2	SLU 9	396	331	2583	-8.98	11.4	-0.01
2	SLU 10	486	399	3122	-10.87	14.13	-0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
2	SLU 11	491	407	3161	-10.85	14.5	-0.02
2	SLU 12	488	402	3138	-10.86	14.28	-0.02
2	SLU 13	486	399	3122	-10.87	14.13	-0.02
2	SLU 14	491	407	3161	-10.85	14.5	-0.02
2	SLU 15	488	402	3138	-10.86	14.28	-0.02
2	SLU 16	491	407	3161	-10.85	14.5	-0.02
2	SLU 17	488	402	3138	-10.86	14.28	-0.02
2	SLU 18	531	437	3399	-11.65	15.73	-0.02
2	SLU 19	528	432	3376	-11.67	15.51	-0.02
2	SLU 20	531	437	3399	-11.65	15.73	-0.02
2	SLU 21	528	432	3376	-11.67	15.51	-0.02
2	SLU 22	443	368	2865	-9.82	13.02	-0.01
2	SLU 23	438	361	2826	-9.84	12.65	-0.01
2	SLU 24	443	368	2865	-9.82	13.02	-0.01
2	SLU 25	440	364	2841	-9.83	12.8	-0.01
2	SLU 26	438	361	2826	-9.84	12.65	-0.01
2	SLU 27	443	368	2865	-9.82	13.02	-0.01
2	SLU 28	440	364	2841	-9.83	12.8	-0.01
2	SLU 29	443	368	2865	-9.82	13.02	-0.01
2	SLU 30	440	364	2841	-9.83	12.8	-0.01
2	SLU 31	531	431	3381	-11.72	15.53	-0.02
2	SLU 32	536	439	3420	-11.7	15.9	-0.02
2	SLU 33	533	434	3397	-11.71	15.68	-0.02
2	SLU 34	531	431	3381	-11.72	15.53	-0.02
2	SLU 35	536	439	3420	-11.7	15.9	-0.02
2	SLU 36	533	434	3397	-11.71	15.68	-0.02
2	SLU 37	536	439	3420	-11.7	15.9	-0.02
2	SLU 38	533	434	3397	-11.71	15.68	-0.02
2	SLU 39	575	469	3658	-12.5	17.13	-0.02
2	SLU 40	572	465	3635	-12.51	16.91	-0.02
2	SLU 41	575	469	3658	-12.5	17.13	-0.02
2	SLU 42	572	465	3635	-12.51	16.91	-0.02
2	SLU 43	503	426	3299	-11.37	14.62	-0.01
2	SLU 44	498	418	3260	-11.39	14.26	-0.01
2	SLU 45	503	426	3299	-11.37	14.62	-0.01
2	SLU 46	500	421	3276	-11.38	14.4	-0.01
2	SLU 47	498	418	3260	-11.39	14.26	-0.01
2	SLU 48	503	426	3299	-11.37	14.62	-0.01
2	SLU 49	500	421	3276	-11.38	14.4	-0.01
2	SLU 50	503	426	3299	-11.37	14.62	-0.01
2	SLU 51	500	421	3276	-11.38	14.4	-0.01
2	SLU 52	590	489	3815	-13.27	17.14	-0.02
2	SLU 53	595	496	3855	-13.25	17.5	-0.02
2	SLU 54	592	492	3831	-13.26	17.28	-0.02
2	SLU 55	590	489	3815	-13.27	17.14	-0.02
2	SLU 56	595	496	3855	-13.25	17.5	-0.02
2	SLU 57	592	492	3831	-13.26	17.28	-0.02
2	SLU 58	595	496	3855	-13.25	17.5	-0.02
2	SLU 59	592	492	3831	-13.26	17.28	-0.02
2	SLU 60	635	527	4093	-14.05	18.74	-0.02
2	SLU 61	632	522	4069	-14.07	18.52	-0.02
2	SLU 62	635	527	4093	-14.05	18.74	-0.02
2	SLU 63	632	522	4069	-14.07	18.52	-0.02
2	SLU 64	547	458	3558	-12.22	16.02	-0.02
2	SLU 65	543	450	3519	-12.24	15.66	-0.02
2	SLU 66	547	458	3558	-12.22	16.02	-0.02
2	SLU 67	545	453	3534	-12.23	15.8	-0.02
2	SLU 68	543	450	3519	-12.24	15.66	-0.02
2	SLU 69	547	458	3558	-12.22	16.02	-0.02
2	SLU 70	545	453	3534	-12.23	15.8	-0.02
2	SLU 71	547	458	3558	-12.22	16.02	-0.02
2	SLU 72	545	453	3534	-12.23	15.8	-0.02
2	SLU 73	635	521	4074	-14.12	18.54	-0.02
2	SLU 74	640	529	4113	-14.1	18.9	-0.02
2	SLU 75	637	524	4090	-14.11	18.68	-0.02
2	SLU 76	635	521	4074	-14.12	18.54	-0.02
2	SLU 77	640	529	4113	-14.1	18.9	-0.02
2	SLU 78	637	524	4090	-14.11	18.68	-0.02
2	SLU 79	640	529	4113	-14.1	18.9	-0.02
2	SLU 80	637	524	4090	-14.11	18.68	-0.02
2	SLU 81	680	559	4351	-14.9	20.14	-0.02
2	SLU 82	677	554	4328	-14.91	19.92	-0.02
2	SLU 83	680	559	4351	-14.9	20.14	-0.02
2	SLU 84	677	554	4328	-14.91	19.92	-0.02
2	SLE RA 1	411	345	2680	-9.21	12.02	-0.01
2	SLE RA 2	408	340	2654	-9.23	11.77	-0.01
2	SLE RA 3	411	345	2680	-9.21	12.02	-0.01
2	SLE RA 4	409	342	2664	-9.22	11.87	-0.01
2	SLE RA 5	408	340	2654	-9.23	11.77	-0.01
2	SLE RA 6	411	345	2680	-9.21	12.02	-0.01
2	SLE RA 7	409	342	2664	-9.22	11.87	-0.01
2	SLE RA 8	411	345	2680	-9.21	12.02	-0.01
2	SLE RA 9	409	342	2664	-9.22	11.87	-0.01
2	SLE RA 10	470	387	3024	-10.48	13.69	-0.01
2	SLE RA 11	473	392	3050	-10.47	13.94	-0.02
2	SLE RA 12	471	389	3035	-10.47	13.79	-0.02
2	SLE RA 13	470	387	3024	-10.48	13.69	-0.01
2	SLE RA 14	473	392	3050	-10.47	13.94	-0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
2	SLE RA 15	471	389	3035	-10.47	13.79	-0.02
2	SLE RA 16	473	392	3050	-10.47	13.94	-0.02
2	SLE RA 17	471	389	3035	-10.47	13.79	-0.02
2	SLE RA 18	499	412	3209	-11	14.76	-0.02
2	SLE RA 19	497	409	3193	-11.01	14.61	-0.02
2	SLE RA 20	499	412	3209	-11	14.76	-0.02
2	SLE RA 21	497	409	3193	-11.01	14.61	-0.02
2	SLE FR 1	411	345	2680	-9.21	12.02	-0.01
2	SLE FR 2	411	344	2675	-9.22	11.97	-0.01
2	SLE FR 3	411	345	2680	-9.21	12.02	-0.01
2	SLE FR 4	437	364	2833	-9.75	12.79	-0.01
2	SLE FR 5	438	365	2839	-9.75	12.84	-0.01
2	SLE FR 6	455	379	2944	-10.11	13.39	-0.01
2	SLE QP 1	411	345	2680	-9.21	12.02	-0.01
2	SLE QP 2	438	365	2839	-9.75	12.84	-0.01
2	SLD 1	594	427	3440	-9.94	18.68	-0.05
2	SLD 2	594	427	3440	-9.94	18.68	-0.05
2	SLD 3	548	369	3183	-7.59	17.18	-0.08
2	SLD 4	548	369	3183	-7.59	17.18	-0.08
2	SLD 5	555	473	3409	-13.37	16.88	0.02
2	SLD 6	555	473	3409	-13.37	16.88	0.02
2	SLD 7	400	277	2552	-5.54	11.86	-0.08
2	SLD 8	400	277	2552	-5.54	11.86	-0.08
2	SLD 9	475	453	3125	-13.96	13.82	0.05
2	SLD 10	475	453	3125	-13.96	13.82	0.05
2	SLD 11	320	258	2269	-6.13	8.8	-0.05
2	SLD 12	320	258	2269	-6.13	8.8	-0.05
2	SLD 13	328	362	2494	-11.91	8.5	0.05
2	SLD 14	328	362	2494	-11.91	8.5	0.05
2	SLD 15	281	303	2237	-9.56	7	0.02
2	SLD 16	281	303	2237	-9.56	7	0.02
2	SLV 1	812	511	4270	-10.22	26.74	-0.09
2	SLV 2	812	511	4270	-10.22	26.74	-0.09
2	SLV 3	694	373	3645	-4.65	23.05	-0.16
2	SLV 4	694	373	3645	-4.65	23.05	-0.16
2	SLV 5	729	619	4217	-18.34	22.61	0.07
2	SLV 6	729	619	4217	-18.34	22.61	0.07
2	SLV 7	335	158	2132	0.22	10.31	-0.17
2	SLV 8	335	158	2132	0.22	10.31	-0.17
2	SLV 9	540	573	3546	-19.72	15.37	0.14
2	SLV 10	540	573	3546	-19.72	15.37	0.14
2	SLV 11	146	112	1460	-1.16	3.07	-0.1
2	SLV 12	146	112	1460	-1.16	3.07	-0.1
2	SLV 13	181	358	2033	-14.85	2.63	0.13
2	SLV 14	181	358	2033	-14.85	2.63	0.13
2	SLV 15	63	219	1407	-9.28	-1.06	0.06
2	SLV 16	63	219	1407	-9.28	-1.06	0.06
3	SLU 1	357	3	2208	-0.73	17	-0.01
3	SLU 2	350	4	2182	-2.23	16.65	-0.01
3	SLU 3	357	3	2208	-0.73	17	-0.01
3	SLU 4	353	4	2192	-1.63	16.79	-0.01
3	SLU 5	350	4	2182	-2.23	16.65	-0.01
3	SLU 6	357	3	2208	-0.73	17	-0.01
3	SLU 7	353	4	2192	-1.63	16.79	-0.01
3	SLU 8	357	3	2208	-0.73	17	-0.01
3	SLU 9	353	4	2192	-1.63	16.79	-0.01
3	SLU 10	441	5	2631	-2.16	20.99	-0.01
3	SLU 11	448	4	2657	-0.66	21.33	-0.02
3	SLU 12	443	5	2641	-1.56	21.13	-0.01
3	SLU 13	441	5	2631	-2.16	20.99	-0.01
3	SLU 14	448	4	2657	-0.66	21.33	-0.02
3	SLU 15	443	5	2641	-1.56	21.13	-0.01
3	SLU 16	448	4	2657	-0.66	21.33	-0.02
3	SLU 17	443	5	2641	-1.56	21.13	-0.01
3	SLU 18	486	4	2850	-0.63	23.19	-0.02
3	SLU 19	482	5	2834	-1.53	22.98	-0.02
3	SLU 20	486	4	2850	-0.63	23.19	-0.02
3	SLU 21	482	5	2834	-1.53	22.98	-0.02
3	SLU 22	402	3	2420	-0.72	19.14	-0.01
3	SLU 23	396	5	2393	-2.21	18.79	-0.01
3	SLU 24	402	3	2420	-0.72	19.14	-0.01
3	SLU 25	398	4	2404	-1.61	18.93	-0.01
3	SLU 26	396	5	2393	-2.21	18.79	-0.01
3	SLU 27	402	3	2420	-0.72	19.14	-0.01
3	SLU 28	398	4	2404	-1.61	18.93	-0.01
3	SLU 29	402	3	2420	-0.72	19.14	-0.01
3	SLU 30	398	4	2404	-1.61	18.93	-0.01
3	SLU 31	486	6	2842	-2.14	23.13	-0.01
3	SLU 32	493	4	2869	-0.65	23.47	-0.02
3	SLU 33	489	5	2853	-1.54	23.26	-0.02
3	SLU 34	486	6	2842	-2.14	23.13	-0.01
3	SLU 35	493	4	2869	-0.65	23.47	-0.02
3	SLU 36	489	5	2853	-1.54	23.26	-0.02
3	SLU 37	493	4	2869	-0.65	23.47	-0.02
3	SLU 38	489	5	2853	-1.54	23.26	-0.02
3	SLU 39	532	4	3061	-0.62	25.33	-0.02
3	SLU 40	527	5	3045	-1.52	25.12	-0.02
3	SLU 41	532	4	3061	-0.62	25.33	-0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
3	SLU 42	527	5	3045	-1.52	25.12	-0.02
3	SLU 43	449	4	2798	-0.95	21.36	-0.02
3	SLU 44	442	5	2772	-2.45	21.02	-0.01
3	SLU 45	449	4	2798	-0.95	21.36	-0.02
3	SLU 46	445	5	2782	-1.85	21.16	-0.01
3	SLU 47	442	5	2772	-2.45	21.02	-0.01
3	SLU 48	449	4	2798	-0.95	21.36	-0.02
3	SLU 49	445	5	2782	-1.85	21.16	-0.01
3	SLU 50	449	4	2798	-0.95	21.36	-0.02
3	SLU 51	445	5	2782	-1.85	21.16	-0.01
3	SLU 52	532	6	3221	-2.38	25.35	-0.02
3	SLU 53	539	5	3247	-0.88	25.7	-0.02
3	SLU 54	535	5	3231	-1.78	25.49	-0.02
3	SLU 55	532	6	3221	-2.38	25.35	-0.02
3	SLU 56	539	5	3247	-0.88	25.7	-0.02
3	SLU 57	535	5	3231	-1.78	25.49	-0.02
3	SLU 58	539	5	3247	-0.88	25.7	-0.02
3	SLU 59	535	5	3231	-1.78	25.49	-0.02
3	SLU 60	578	5	3440	-0.86	27.56	-0.02
3	SLU 61	574	6	3424	-1.75	27.35	-0.02
3	SLU 62	578	5	3440	-0.86	27.56	-0.02
3	SLU 63	574	6	3424	-1.75	27.35	-0.02
3	SLU 64	494	4	3010	-0.94	23.5	-0.02
3	SLU 65	487	6	2983	-2.44	23.16	-0.02
3	SLU 66	494	4	3010	-0.94	23.5	-0.02
3	SLU 67	490	5	2994	-1.84	23.29	-0.02
3	SLU 68	487	6	2983	-2.44	23.16	-0.02
3	SLU 69	494	4	3010	-0.94	23.5	-0.02
3	SLU 70	490	5	2994	-1.84	23.29	-0.02
3	SLU 71	494	4	3010	-0.94	23.5	-0.02
3	SLU 72	490	5	2994	-1.84	23.29	-0.02
3	SLU 73	578	6	3432	-2.37	27.49	-0.02
3	SLU 74	584	5	3459	-0.87	27.84	-0.02
3	SLU 75	580	6	3443	-1.77	27.63	-0.02
3	SLU 76	578	6	3432	-2.37	27.49	-0.02
3	SLU 77	584	5	3459	-0.87	27.84	-0.02
3	SLU 78	580	6	3443	-1.77	27.63	-0.02
3	SLU 79	584	5	3459	-0.87	27.84	-0.02
3	SLU 80	580	6	3443	-1.77	27.63	-0.02
3	SLU 81	623	5	3651	-0.84	29.69	-0.02
3	SLU 82	619	6	3635	-1.74	29.49	-0.02
3	SLU 83	623	5	3651	-0.84	29.69	-0.02
3	SLU 84	619	6	3635	-1.74	29.49	-0.02
3	SLE RA 1	370	3	2269	-0.73	17.61	-0.01
3	SLE RA 2	366	4	2251	-1.72	17.38	-0.01
3	SLE RA 3	370	3	2269	-0.73	17.61	-0.01
3	SLE RA 4	367	4	2258	-1.32	17.47	-0.01
3	SLE RA 5	366	4	2251	-1.72	17.38	-0.01
3	SLE RA 6	370	3	2269	-0.73	17.61	-0.01
3	SLE RA 7	367	4	2258	-1.32	17.47	-0.01
3	SLE RA 8	370	3	2269	-0.73	17.61	-0.01
3	SLE RA 9	367	4	2258	-1.32	17.47	-0.01
3	SLE RA 10	426	5	2550	-1.68	20.27	-0.01
3	SLE RA 11	430	4	2568	-0.68	20.5	-0.02
3	SLE RA 12	428	4	2558	-1.28	20.36	-0.01
3	SLE RA 13	426	5	2550	-1.68	20.27	-0.01
3	SLE RA 14	430	4	2568	-0.68	20.5	-0.02
3	SLE RA 15	428	4	2558	-1.28	20.36	-0.01
3	SLE RA 16	430	4	2568	-0.68	20.5	-0.02
3	SLE RA 17	428	4	2558	-1.28	20.36	-0.01
3	SLE RA 18	456	4	2696	-0.66	21.74	-0.02
3	SLE RA 19	453	4	2686	-1.26	21.6	-0.02
3	SLE RA 20	456	4	2696	-0.66	21.74	-0.02
3	SLE RA 21	453	4	2686	-1.26	21.6	-0.02
3	SLE FR 1	370	3	2269	-0.73	17.61	-0.01
3	SLE FR 2	369	3	2265	-0.93	17.56	-0.01
3	SLE FR 3	370	3	2269	-0.73	17.61	-0.01
3	SLE FR 4	395	4	2394	-0.91	18.8	-0.01
3	SLE FR 5	396	3	2397	-0.71	18.85	-0.01
3	SLE FR 6	413	3	2483	-0.69	19.67	-0.01
3	SLE QP 1	370	3	2269	-0.73	17.61	-0.01
3	SLE QP 2	396	3	2397	-0.71	18.85	-0.01
3	SLD 1	626	-4	2801	0.09	29.35	-0.03
3	SLD 2	626	-4	2801	0.09	29.35	-0.03
3	SLD 3	558	-1	2623	4.61	26.45	-0.02
3	SLD 4	558	-1	2623	4.61	26.45	-0.02
3	SLD 5	567	-3	2788	-7.32	26.39	-0.03
3	SLD 6	567	-3	2788	-7.32	26.39	-0.03
3	SLD 7	343	6	2194	7.74	16.74	0
3	SLD 8	343	6	2194	7.74	16.74	0
3	SLD 9	449	1	2600	-9.15	20.96	-0.03
3	SLD 10	449	1	2600	-9.15	20.96	-0.03
3	SLD 11	225	9	2006	5.91	11.3	0.01
3	SLD 12	225	9	2006	5.91	11.3	0.01
3	SLD 13	233	7	2171	-6.02	11.24	-0.01
3	SLD 14	233	7	2171	-6.02	11.24	-0.01
3	SLD 15	166	10	1993	-1.5	8.34	0
3	SLD 16	166	10	1993	-1.5	8.34	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
3	SLV 1	943	-13	3358	1.02	43.9	-0.05
3	SLV 2	943	-13	3358	1.02	43.9	-0.05
3	SLV 3	777	-6	2924	12.69	36.69	-0.02
3	SLV 4	777	-6	2924	12.69	36.69	-0.02
3	SLV 5	811	-12	3344	-17.89	37.29	-0.07
3	SLV 6	811	-12	3344	-17.89	37.29	-0.07
3	SLV 7	259	11	1896	21.02	13.27	0.03
3	SLV 8	259	11	1896	21.02	13.27	0.03
3	SLV 9	533	-4	2898	-22.43	24.42	-0.05
3	SLV 10	533	-4	2898	-22.43	24.42	-0.05
3	SLV 11	-19	18	1450	16.48	0.4	0.04
3	SLV 12	-19	18	1450	16.48	0.4	0.04
3	SLV 13	14	13	1870	-14.1	1	-0.01
3	SLV 14	14	13	1870	-14.1	1	-0.01
3	SLV 15	-151	20	1436	-2.43	-6.2	0.02
3	SLV 16	-151	20	1436	-2.43	-6.2	0.02
4	SLU 1	293	0	2055	0.01	12.36	0
4	SLU 2	284	3	2039	-2.82	11.93	0.01
4	SLU 3	293	0	2055	0.01	12.36	0
4	SLU 4	288	2	2046	-1.69	12.1	0.01
4	SLU 5	284	3	2039	-2.82	11.93	0.01
4	SLU 6	293	0	2055	0.01	12.36	0
4	SLU 7	288	2	2046	-1.69	12.1	0.01
4	SLU 8	293	0	2055	0.01	12.36	0
4	SLU 9	288	2	2046	-1.69	12.1	0.01
4	SLU 10	364	3	2437	-2.3	15.36	0.01
4	SLU 11	373	0	2453	0.54	15.78	0
4	SLU 12	367	2	2443	-1.16	15.52	0.01
4	SLU 13	364	3	2437	-2.3	15.36	0.01
4	SLU 14	373	0	2453	0.54	15.78	0
4	SLU 15	367	2	2443	-1.16	15.52	0.01
4	SLU 16	373	0	2453	0.54	15.78	0
4	SLU 17	367	2	2443	-1.16	15.52	0.01
4	SLU 18	407	0	2623	0.76	17.24	0
4	SLU 19	401	2	2614	-0.94	16.99	0.01
4	SLU 20	407	0	2623	0.76	17.24	0
4	SLU 21	401	2	2614	-0.94	16.99	0.01
4	SLU 22	333	0	2246	0.22	14.05	0
4	SLU 23	324	3	2230	-2.62	13.63	0.01
4	SLU 24	333	0	2246	0.22	14.05	0
4	SLU 25	328	2	2237	-1.49	13.8	0.01
4	SLU 26	324	3	2230	-2.62	13.63	0.01
4	SLU 27	333	0	2246	0.22	14.05	0
4	SLU 28	328	2	2237	-1.49	13.8	0.01
4	SLU 29	333	0	2246	0.22	14.05	0
4	SLU 30	328	2	2237	-1.49	13.8	0.01
4	SLU 31	404	3	2628	-2.1	17.05	0.01
4	SLU 32	413	0	2644	0.74	17.47	0
4	SLU 33	407	2	2634	-0.96	17.22	0.01
4	SLU 34	404	3	2628	-2.1	17.05	0.01
4	SLU 35	413	0	2644	0.74	17.47	0
4	SLU 36	407	2	2634	-0.96	17.22	0.01
4	SLU 37	413	0	2644	0.74	17.47	0
4	SLU 38	407	2	2634	-0.96	17.22	0.01
4	SLU 39	447	0	2814	0.96	18.94	0
4	SLU 40	441	2	2805	-0.74	18.68	0.01
4	SLU 41	447	0	2814	0.96	18.94	0
4	SLU 42	441	2	2805	-0.74	18.68	0.01
4	SLU 43	368	0	2606	-0.05	15.48	0.01
4	SLU 44	359	3	2590	-2.88	15.06	0.01
4	SLU 45	368	0	2606	-0.05	15.48	0.01
4	SLU 46	362	2	2597	-1.75	15.23	0.01
4	SLU 47	359	3	2590	-2.88	15.06	0.01
4	SLU 48	368	0	2606	-0.05	15.48	0.01
4	SLU 49	362	2	2597	-1.75	15.23	0.01
4	SLU 50	368	0	2606	-0.05	15.48	0.01
4	SLU 51	362	2	2597	-1.75	15.23	0.01
4	SLU 52	438	3	2988	-2.36	18.48	0.01
4	SLU 53	447	0	3004	0.47	18.9	0.01
4	SLU 54	442	2	2994	-1.23	18.65	0.01
4	SLU 55	438	3	2988	-2.36	18.48	0.01
4	SLU 56	447	0	3004	0.47	18.9	0.01
4	SLU 57	442	2	2994	-1.23	18.65	0.01
4	SLU 58	447	0	3004	0.47	18.9	0.01
4	SLU 59	442	2	2994	-1.23	18.65	0.01
4	SLU 60	481	0	3174	0.7	20.37	0.01
4	SLU 61	476	2	3165	-1.01	20.12	0.01
4	SLU 62	481	0	3174	0.7	20.37	0.01
4	SLU 63	476	2	3165	-1.01	20.12	0.01
4	SLU 64	407	0	2797	0.15	17.18	0.01
4	SLU 65	399	3	2781	-2.68	16.75	0.01
4	SLU 66	407	0	2797	0.15	17.18	0.01
4	SLU 67	402	2	2788	-1.55	16.92	0.01
4	SLU 68	399	3	2781	-2.68	16.75	0.01
4	SLU 69	407	0	2797	0.15	17.18	0.01
4	SLU 70	402	2	2788	-1.55	16.92	0.01
4	SLU 71	407	0	2797	0.15	17.18	0.01
4	SLU 72	402	2	2788	-1.55	16.92	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
4	SLU 73	478	3	3179	-2.16	20.18	0.01
4	SLU 74	487	0	3195	0.67	20.6	0.01
4	SLU 75	482	2	3185	-1.03	20.34	0.01
4	SLU 76	478	3	3179	-2.16	20.18	0.01
4	SLU 77	487	0	3195	0.67	20.6	0.01
4	SLU 78	482	2	3185	-1.03	20.34	0.01
4	SLU 79	487	0	3195	0.67	20.6	0.01
4	SLU 80	482	2	3185	-1.03	20.34	0.01
4	SLU 81	521	0	3365	0.9	22.06	0.01
4	SLU 82	516	2	3356	-0.8	21.81	0.01
4	SLU 83	521	0	3365	0.9	22.06	0.01
4	SLU 84	516	2	3356	-0.8	21.81	0.01
4	SLE RA 1	305	0	2110	0.07	12.84	0
4	SLE RA 2	299	2	2099	-1.82	12.56	0.01
4	SLE RA 3	305	0	2110	0.07	12.84	0
4	SLE RA 4	301	1	2103	-1.06	12.67	0
4	SLE RA 5	299	2	2099	-1.82	12.56	0.01
4	SLE RA 6	305	0	2110	0.07	12.84	0
4	SLE RA 7	301	1	2103	-1.06	12.67	0
4	SLE RA 8	305	0	2110	0.07	12.84	0
4	SLE RA 9	301	1	2103	-1.06	12.67	0
4	SLE RA 10	352	2	2364	-1.47	14.84	0.01
4	SLE RA 11	358	0	2375	0.42	15.12	0
4	SLE RA 12	354	1	2368	-0.71	14.95	0
4	SLE RA 13	352	2	2364	-1.47	14.84	0.01
4	SLE RA 14	358	0	2375	0.42	15.12	0
4	SLE RA 15	354	1	2368	-0.71	14.95	0
4	SLE RA 16	358	0	2375	0.42	15.12	0
4	SLE RA 17	354	1	2368	-0.71	14.95	0
4	SLE RA 18	380	0	2489	0.57	16.1	0
4	SLE RA 19	377	1	2482	-0.57	15.93	0
4	SLE RA 20	380	0	2489	0.57	16.1	0
4	SLE RA 21	377	1	2482	-0.57	15.93	0
4	SLE FR 1	305	0	2110	0.07	12.84	0
4	SLE FR 2	303	1	2108	-0.31	12.78	0
4	SLE FR 3	305	0	2110	0.07	12.84	0
4	SLE FR 4	326	1	2221	-0.16	13.76	0
4	SLE FR 5	327	0	2223	0.22	13.82	0
4	SLE FR 6	342	0	2299	0.32	14.47	0
4	SLE QP 1	305	0	2110	0.07	12.84	0
4	SLE QP 2	327	0	2223	0.22	13.82	0
4	SLD 1	566	-9	2496	0.92	24.13	0.02
4	SLD 2	566	-9	2496	0.92	24.13	0.02
4	SLD 3	501	-5	2371	11.2	21.37	0.01
4	SLD 4	501	-5	2371	11.2	21.37	0.01
4	SLD 5	497	-9	2495	-15.15	21.1	0.02
4	SLD 6	497	-9	2495	-15.15	21.1	0.02
4	SLD 7	281	5	2078	19.09	11.89	-0.01
4	SLD 8	281	5	2078	19.09	11.89	-0.01
4	SLD 9	373	-4	2368	-18.65	15.74	0.02
4	SLD 10	373	-4	2368	-18.65	15.74	0.02
4	SLD 11	157	9	1952	15.59	6.54	-0.02
4	SLD 12	157	9	1952	15.59	6.54	-0.02
4	SLD 13	153	6	2075	-10.75	6.27	0
4	SLD 14	153	6	2075	-10.75	6.27	0
4	SLD 15	88	10	1950	-0.48	3.51	-0.01
4	SLD 16	88	10	1950	-0.48	3.51	-0.01
4	SLV 1	896	-23	2873	1.47	38.38	0.04
4	SLV 2	896	-23	2873	1.47	38.38	0.04
4	SLV 3	736	-13	2568	28.04	31.55	0.01
4	SLV 4	736	-13	2568	28.04	31.55	0.01
4	SLV 5	741	-21	2881	-39.7	31.55	0.05
4	SLV 6	741	-21	2881	-39.7	31.55	0.05
4	SLV 7	207	11	1864	48.86	8.78	-0.03
4	SLV 8	207	11	1864	48.86	8.78	-0.03
4	SLV 9	447	-10	2583	-48.42	18.86	0.04
4	SLV 10	447	-10	2583	-48.42	18.86	0.04
4	SLV 11	-86	21	1566	40.14	-3.91	-0.05
4	SLV 12	-86	21	1566	40.14	-3.91	-0.05
4	SLV 13	-82	13	1879	-27.59	-3.92	-0.01
4	SLV 14	-82	13	1879	-27.59	-3.92	-0.01
4	SLV 15	-242	23	1574	-1.03	-10.74	-0.03
4	SLV 16	-242	23	1574	-1.03	-10.74	-0.03
5	SLU 1	233	0	2036	0.43	9.8	0
5	SLU 2	223	3	2026	-3.37	9.39	0
5	SLU 3	233	0	2036	0.43	9.8	0
5	SLU 4	227	2	2030	-1.85	9.55	0
5	SLU 5	223	3	2026	-3.37	9.39	0
5	SLU 6	233	0	2036	0.43	9.8	0
5	SLU 7	227	2	2030	-1.85	9.55	0
5	SLU 8	233	0	2036	0.43	9.8	0
5	SLU 9	227	2	2030	-1.85	9.55	0
5	SLU 10	289	3	2408	-2.46	12.19	0
5	SLU 11	299	-1	2418	1.34	12.61	0
5	SLU 12	293	1	2412	-0.94	12.36	0
5	SLU 13	289	3	2408	-2.46	12.19	0
5	SLU 14	299	-1	2418	1.34	12.61	0
5	SLU 15	293	1	2412	-0.94	12.36	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
5	SLU 16	299	-1	2418	1.34	12.61	0
5	SLU 17	293	1	2412	-0.94	12.36	0
5	SLU 18	327	-1	2582	1.73	13.81	0
5	SLU 19	321	1	2576	-0.55	13.56	0
5	SLU 20	327	-1	2582	1.73	13.81	0
5	SLU 21	321	1	2576	-0.55	13.56	0
5	SLU 22	266	0	2222	0.79	11.18	0
5	SLU 23	256	3	2213	-3.01	10.77	0
5	SLU 24	266	0	2222	0.79	11.18	0
5	SLU 25	260	2	2217	-1.49	10.94	0
5	SLU 26	256	3	2213	-3.01	10.77	0
5	SLU 27	266	0	2222	0.79	11.18	0
5	SLU 28	260	2	2217	-1.49	10.94	0
5	SLU 29	266	0	2222	0.79	11.18	0
5	SLU 30	260	2	2217	-1.49	10.94	0
5	SLU 31	322	3	2595	-2.1	13.58	0
5	SLU 32	332	-1	2605	1.7	13.99	0
5	SLU 33	326	1	2599	-0.58	13.74	0
5	SLU 34	322	3	2595	-2.1	13.58	0
5	SLU 35	332	-1	2605	1.7	13.99	0
5	SLU 36	326	1	2599	-0.58	13.74	0
5	SLU 37	332	-1	2605	1.7	13.99	0
5	SLU 38	326	1	2599	-0.58	13.74	0
5	SLU 39	360	-1	2769	2.08	15.2	0
5	SLU 40	354	1	2763	-0.2	14.95	0
5	SLU 41	360	-1	2769	2.08	15.2	0
5	SLU 42	354	1	2763	-0.2	14.95	0
5	SLU 43	291	0	2582	0.44	12.27	0
5	SLU 44	282	3	2572	-3.36	11.85	0
5	SLU 45	291	0	2582	0.44	12.27	0
5	SLU 46	286	2	2576	-1.84	12.02	0
5	SLU 47	282	3	2572	-3.36	11.85	0
5	SLU 48	291	0	2582	0.44	12.27	0
5	SLU 49	286	2	2576	-1.84	12.02	0
5	SLU 50	291	0	2582	0.44	12.27	0
5	SLU 51	286	2	2576	-1.84	12.02	0
5	SLU 52	348	3	2955	-2.45	14.66	0
5	SLU 53	357	-1	2964	1.35	15.08	0
5	SLU 54	352	1	2959	-0.93	14.83	0
5	SLU 55	348	3	2955	-2.45	14.66	0
5	SLU 56	357	-1	2964	1.35	15.08	0
5	SLU 57	352	1	2959	-0.93	14.83	0
5	SLU 58	357	-1	2964	1.35	15.08	0
5	SLU 59	352	1	2959	-0.93	14.83	0
5	SLU 60	386	-1	3128	1.74	16.28	0
5	SLU 61	380	1	3123	-0.54	16.03	0
5	SLU 62	386	-1	3128	1.74	16.28	0
5	SLU 63	380	1	3123	-0.54	16.03	0
5	SLU 64	324	0	2769	0.8	13.65	0
5	SLU 65	315	3	2759	-3	13.24	0
5	SLU 66	324	0	2769	0.8	13.65	0
5	SLU 67	318	2	2763	-1.48	13.4	0
5	SLU 68	315	3	2759	-3	13.24	0
5	SLU 69	324	0	2769	0.8	13.65	0
5	SLU 70	318	2	2763	-1.48	13.4	0
5	SLU 71	324	0	2769	0.8	13.65	0
5	SLU 72	318	2	2763	-1.48	13.4	0
5	SLU 73	381	3	3142	-2.1	16.04	0
5	SLU 74	390	-1	3151	1.7	16.46	0
5	SLU 75	385	1	3146	-0.58	16.21	0
5	SLU 76	381	3	3142	-2.1	16.04	0
5	SLU 77	390	-1	3151	1.7	16.46	0
5	SLU 78	385	1	3146	-0.58	16.21	0
5	SLU 79	390	-1	3151	1.7	16.46	0
5	SLU 80	385	1	3146	-0.58	16.21	0
5	SLU 81	419	-1	3315	2.09	17.66	0
5	SLU 82	413	1	3309	-0.19	17.41	0
5	SLU 83	419	-1	3315	2.09	17.66	0
5	SLU 84	413	1	3309	-0.19	17.41	0
5	SLE RA 1	242	0	2089	0.54	10.2	0
5	SLE RA 2	236	2	2082	-2	9.92	0
5	SLE RA 3	242	0	2089	0.54	10.2	0
5	SLE RA 4	238	1	2085	-0.98	10.03	0
5	SLE RA 5	236	2	2082	-2	9.92	0
5	SLE RA 6	242	0	2089	0.54	10.2	0
5	SLE RA 7	238	1	2085	-0.98	10.03	0
5	SLE RA 8	242	0	2089	0.54	10.2	0
5	SLE RA 9	238	1	2085	-0.98	10.03	0
5	SLE RA 10	280	2	2337	-1.39	11.79	0
5	SLE RA 11	286	-1	2344	1.14	12.07	0
5	SLE RA 12	282	1	2340	-0.38	11.9	0
5	SLE RA 13	280	2	2337	-1.39	11.79	0
5	SLE RA 14	286	-1	2344	1.14	12.07	0
5	SLE RA 15	282	1	2340	-0.38	11.9	0
5	SLE RA 16	286	-1	2344	1.14	12.07	0
5	SLE RA 17	282	1	2340	-0.38	11.9	0
5	SLE RA 18	305	-1	2453	1.4	12.87	0
5	SLE RA 19	301	1	2449	-0.12	12.7	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
5	SLE RA 20	305	-1	2453	1.4	12.87	0
5	SLE RA 21	301	1	2449	-0.12	12.7	0
5	SLE FR 1	242	0	2089	0.54	10.2	0
5	SLE FR 2	241	0	2088	0.03	10.14	0
5	SLE FR 3	242	0	2089	0.54	10.2	0
5	SLE FR 4	260	0	2197	0.29	10.94	0
5	SLE FR 5	261	0	2198	0.79	11	0
5	SLE FR 6	274	-1	2271	0.97	11.53	0
5	SLE QP 1	242	0	2089	0.54	10.2	0
5	SLE QP 2	261	0	2198	0.79	11	0
5	SLD 1	507	-5	2403	0.64	21.45	0
5	SLD 2	507	-5	2403	0.64	21.45	0
5	SLD 3	443	-14	2307	17.75	18.74	-0.02
5	SLD 4	443	-14	2307	17.75	18.74	-0.02
5	SLD 5	432	13	2405	-25.21	18.24	0.02
5	SLD 6	432	13	2405	-25.21	18.24	0.02
5	SLD 7	218	-19	2086	31.84	9.21	-0.02
5	SLD 8	218	-19	2086	31.84	9.21	-0.02
5	SLD 9	304	18	2311	-30.25	12.78	0.03
5	SLD 10	304	18	2311	-30.25	12.78	0.03
5	SLD 11	90	-14	1991	26.8	3.76	-0.02
5	SLD 12	90	-14	1991	26.8	3.76	-0.02
5	SLD 13	79	13	2089	-16.16	3.26	0.02
5	SLD 14	79	13	2089	-16.16	3.26	0.02
5	SLD 15	15	4	1993	0.95	0.55	0
5	SLD 16	15	4	1993	0.95	0.55	0
5	SLV 1	847	-11	2687	-0.49	35.88	-0.01
5	SLV 2	847	-11	2687	-0.49	35.88	-0.01
5	SLV 3	689	-35	2452	43.85	29.19	-0.04
5	SLV 4	689	-35	2452	43.85	29.19	-0.04
5	SLV 5	676	33	2701	-66.84	28.6	0.05
5	SLV 6	676	33	2701	-66.84	28.6	0.05
5	SLV 7	150	-47	1918	80.96	6.32	-0.06
5	SLV 8	150	-47	1918	80.96	6.32	-0.06
5	SLV 9	372	46	2478	-79.37	15.68	0.06
5	SLV 10	372	46	2478	-79.37	15.68	0.06
5	SLV 11	-154	-34	1696	68.43	-6.6	-0.05
5	SLV 12	-154	-34	1696	68.43	-6.6	-0.05
5	SLV 13	-167	34	1944	-42.26	-7.19	0.04
5	SLV 14	-167	34	1944	-42.26	-7.19	0.04
5	SLV 15	-324	10	1710	2.08	-13.88	0.01
5	SLV 16	-324	10	1710	2.08	-13.88	0.01
6	SLU 1	185	0	2029	0.7	7.74	0
6	SLU 2	175	3	2024	-3.66	7.25	0
6	SLU 3	185	0	2029	0.7	7.74	0
6	SLU 4	179	2	2026	-1.91	7.45	0
6	SLU 5	175	3	2024	-3.66	7.25	0
6	SLU 6	185	0	2029	0.7	7.74	0
6	SLU 7	179	2	2026	-1.91	7.45	0
6	SLU 8	185	0	2029	0.7	7.74	0
6	SLU 9	179	2	2026	-1.91	7.45	0
6	SLU 10	229	2	2396	-2.45	9.59	0
6	SLU 11	240	-1	2401	1.9	10.08	0
6	SLU 12	234	1	2398	-0.71	9.78	0
6	SLU 13	229	2	2396	-2.45	9.59	0
6	SLU 14	240	-1	2401	1.9	10.08	0
6	SLU 15	234	1	2398	-0.71	9.78	0
6	SLU 16	240	-1	2401	1.9	10.08	0
6	SLU 17	234	1	2398	-0.71	9.78	0
6	SLU 18	263	-1	2561	2.41	11.08	0
6	SLU 19	257	1	2558	-0.2	10.79	0
6	SLU 20	263	-1	2561	2.41	11.08	0
6	SLU 21	257	1	2558	-0.2	10.79	0
6	SLU 22	212	-1	2214	1.17	8.86	0
6	SLU 23	201	3	2208	-3.18	8.38	0
6	SLU 24	212	-1	2214	1.17	8.86	0
6	SLU 25	205	1	2210	-1.44	8.57	0
6	SLU 26	201	3	2208	-3.18	8.38	0
6	SLU 27	212	-1	2214	1.17	8.86	0
6	SLU 28	205	1	2210	-1.44	8.57	0
6	SLU 29	212	-1	2214	1.17	8.86	0
6	SLU 30	205	1	2210	-1.44	8.57	0
6	SLU 31	256	2	2581	-1.98	10.71	0
6	SLU 32	267	-1	2586	2.38	11.2	0
6	SLU 33	260	1	2583	-0.24	10.91	0
6	SLU 34	256	2	2581	-1.98	10.71	0
6	SLU 35	267	-1	2586	2.38	11.2	0
6	SLU 36	260	1	2583	-0.24	10.91	0
6	SLU 37	267	-1	2586	2.38	11.2	0
6	SLU 38	260	1	2583	-0.24	10.91	0
6	SLU 39	290	-2	2745	2.89	12.2	0
6	SLU 40	283	0	2742	0.28	11.91	0
6	SLU 41	290	-2	2745	2.89	12.2	0
6	SLU 42	283	0	2742	0.28	11.91	0
6	SLU 43	232	0	2574	0.75	9.68	0
6	SLU 44	221	3	2569	-3.61	9.19	0
6	SLU 45	232	0	2574	0.75	9.68	0
6	SLU 46	225	2	2571	-1.87	9.39	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
6	SLU 47	221	3	2569	-3.61	9.19	0
6	SLU 48	232	0	2574	0.75	9.68	0
6	SLU 49	225	2	2571	-1.87	9.39	0
6	SLU 50	232	0	2574	0.75	9.68	0
6	SLU 51	225	2	2571	-1.87	9.39	0
6	SLU 52	276	2	2941	-2.41	11.53	0
6	SLU 53	287	-1	2946	1.95	12.01	0
6	SLU 54	280	1	2943	-0.67	11.72	0
6	SLU 55	276	2	2941	-2.41	11.53	0
6	SLU 56	287	-1	2946	1.95	12.01	0
6	SLU 57	280	1	2943	-0.67	11.72	0
6	SLU 58	287	-1	2946	1.95	12.01	0
6	SLU 59	280	1	2943	-0.67	11.72	0
6	SLU 60	310	-2	3106	2.46	13.01	0
6	SLU 61	303	1	3103	-0.15	12.72	0
6	SLU 62	310	-2	3106	2.46	13.01	0
6	SLU 63	303	1	3103	-0.15	12.72	0
6	SLU 64	259	-1	2759	1.22	10.8	0
6	SLU 65	248	3	2754	-3.13	10.32	0
6	SLU 66	259	-1	2759	1.22	10.8	0
6	SLU 67	252	1	2756	-1.39	10.51	0
6	SLU 68	248	3	2754	-3.13	10.32	0
6	SLU 69	259	-1	2759	1.22	10.8	0
6	SLU 70	252	1	2756	-1.39	10.51	0
6	SLU 71	259	-1	2759	1.22	10.8	0
6	SLU 72	252	1	2756	-1.39	10.51	0
6	SLU 73	302	2	3126	-1.93	12.65	0
6	SLU 74	313	-2	3131	2.42	13.14	0
6	SLU 75	307	1	3128	-0.19	12.85	0
6	SLU 76	302	2	3126	-1.93	12.65	0
6	SLU 77	313	-2	3131	2.42	13.14	0
6	SLU 78	307	1	3128	-0.19	12.85	0
6	SLU 79	313	-2	3131	2.42	13.14	0
6	SLU 80	307	1	3128	-0.19	12.85	0
6	SLU 81	337	-2	3291	2.94	14.14	0
6	SLU 82	330	0	3288	0.32	13.85	0
6	SLU 83	337	-2	3291	2.94	14.14	0
6	SLU 84	330	0	3288	0.32	13.85	0
6	SLE RA 1	193	-1	2082	0.84	8.06	0
6	SLE RA 2	186	2	2078	-2.07	7.74	0
6	SLE RA 3	193	-1	2082	0.84	8.06	0
6	SLE RA 4	189	1	2080	-0.91	7.87	0
6	SLE RA 5	186	2	2078	-2.07	7.74	0
6	SLE RA 6	193	-1	2082	0.84	8.06	0
6	SLE RA 7	189	1	2080	-0.91	7.87	0
6	SLE RA 8	193	-1	2082	0.84	8.06	0
6	SLE RA 9	189	1	2080	-0.91	7.87	0
6	SLE RA 10	222	1	2326	-1.27	9.29	0
6	SLE RA 11	229	-1	2330	1.64	9.62	0
6	SLE RA 12	225	0	2328	-0.11	9.42	0
6	SLE RA 13	222	1	2326	-1.27	9.29	0
6	SLE RA 14	229	-1	2330	1.64	9.62	0
6	SLE RA 15	225	0	2328	-0.11	9.42	0
6	SLE RA 16	229	-1	2330	1.64	9.62	0
6	SLE RA 17	225	0	2328	-0.11	9.42	0
6	SLE RA 18	245	-1	2436	1.98	10.29	0
6	SLE RA 19	241	0	2434	0.24	10.09	0
6	SLE RA 20	245	-1	2436	1.98	10.29	0
6	SLE RA 21	241	0	2434	0.24	10.09	0
6	SLE FR 1	193	-1	2082	0.84	8.06	0
6	SLE FR 2	192	0	2081	0.25	8	0
6	SLE FR 3	193	-1	2082	0.84	8.06	0
6	SLE FR 4	207	0	2187	0.6	8.66	0
6	SLE FR 5	209	-1	2188	1.18	8.73	0
6	SLE FR 6	219	-1	2259	1.41	9.17	0
6	SLE QP 1	193	-1	2082	0.84	8.06	0
6	SLE QP 2	209	-1	2188	1.18	8.73	0
6	SLD 1	460	-4	2344	-0.34	19.37	0
6	SLD 2	460	-4	2344	-0.34	19.37	0
6	SLD 3	396	-20	2270	23.79	16.67	-0.02
6	SLD 4	396	-20	2270	23.79	16.67	-0.02
6	SLD 5	381	23	2347	-35.86	16.03	0.03
6	SLD 6	381	23	2347	-35.86	16.03	0.03
6	SLD 7	168	-31	2101	44.55	7.01	-0.04
6	SLD 8	168	-31	2101	44.55	7.01	-0.04
6	SLD 9	249	30	2275	-42.19	10.45	0.04
6	SLD 10	249	30	2275	-42.19	10.45	0.04
6	SLD 11	37	-25	2029	38.22	1.43	-0.03
6	SLD 12	37	-25	2029	38.22	1.43	-0.03
6	SLD 13	21	19	2106	-21.43	0.79	0.02
6	SLD 14	21	19	2106	-21.43	0.79	0.02
6	SLD 15	-42	2	2032	2.69	-1.92	0
6	SLD 16	-42	2	2032	2.69	-1.92	0
6	SLV 1	806	-8	2560	-3.99	34.08	0
6	SLV 2	806	-8	2560	-3.99	34.08	0
6	SLV 3	649	-49	2378	58.62	27.4	-0.05
6	SLV 4	649	-49	2378	58.62	27.4	-0.05
6	SLV 5	626	60	2575	-95.33	26.47	0.07



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
6	SLV 6	626	60	2575	-95.33	26.47	0.07
6	SLV 7	102	-78	1970	113.37	4.19	-0.09
6	SLV 8	102	-78	1970	113.37	4.19	-0.09
6	SLV 9	315	77	2406	-111.01	13.26	0.09
6	SLV 10	315	77	2406	-111.01	13.26	0.09
6	SLV 11	-209	-62	1801	97.68	-9.01	-0.07
6	SLV 12	-209	-62	1801	97.68	-9.01	-0.07
6	SLV 13	-232	48	1998	-56.26	-9.94	0.05
6	SLV 14	-232	48	1998	-56.26	-9.94	0.05
6	SLV 15	-389	6	1816	6.35	-16.62	0
6	SLV 16	-389	6	1816	6.35	-16.62	0
7	SLU 1	144	-1	2027	0.87	6.05	0
7	SLU 2	133	3	2025	-3.68	5.57	0
7	SLU 3	144	-1	2027	0.87	6.05	0
7	SLU 4	138	2	2026	-1.86	5.76	0
7	SLU 5	133	3	2025	-3.68	5.57	0
7	SLU 6	144	-1	2027	0.87	6.05	0
7	SLU 7	138	2	2026	-1.86	5.76	0
7	SLU 8	144	-1	2027	0.87	6.05	0
7	SLU 9	138	2	2026	-1.86	5.76	0
7	SLU 10	175	2	2389	-2.28	7.37	0
7	SLU 11	187	-1	2390	2.28	7.85	0
7	SLU 12	180	1	2389	-0.45	7.56	0
7	SLU 13	175	2	2389	-2.28	7.37	0
7	SLU 14	187	-1	2390	2.28	7.85	0
7	SLU 15	180	1	2389	-0.45	7.56	0
7	SLU 16	187	-1	2390	2.28	7.85	0
7	SLU 17	180	1	2389	-0.45	7.56	0
7	SLU 18	205	-2	2546	2.88	8.63	0
7	SLU 19	198	0	2545	0.15	8.33	0
7	SLU 20	205	-2	2546	2.88	8.63	0
7	SLU 21	198	0	2545	0.15	8.33	0
7	SLU 22	164	-1	2209	1.43	6.89	0
7	SLU 23	153	3	2207	-3.12	6.41	0
7	SLU 24	164	-1	2209	1.43	6.89	0
7	SLU 25	158	1	2208	-1.3	6.6	0
7	SLU 26	153	3	2207	-3.12	6.41	0
7	SLU 27	164	-1	2209	1.43	6.89	0
7	SLU 28	158	1	2208	-1.3	6.6	0
7	SLU 29	164	-1	2209	1.43	6.89	0
7	SLU 30	158	1	2208	-1.3	6.6	0
7	SLU 31	195	2	2571	-1.72	8.21	0
7	SLU 32	207	-2	2572	2.84	8.7	0
7	SLU 33	200	0	2571	0.1	8.41	0
7	SLU 34	195	2	2571	-1.72	8.21	0
7	SLU 35	207	-2	2572	2.84	8.7	0
7	SLU 36	200	0	2571	0.1	8.41	0
7	SLU 37	207	-2	2572	2.84	8.7	0
7	SLU 38	200	0	2571	0.1	8.41	0
7	SLU 39	225	-2	2728	3.44	9.47	0
7	SLU 40	218	0	2727	0.71	9.18	0
7	SLU 41	225	-2	2728	3.44	9.47	0
7	SLU 42	218	0	2727	0.71	9.18	0
7	SLU 43	181	-1	2572	0.95	7.58	0
7	SLU 44	169	3	2571	-3.61	7.09	0
7	SLU 45	181	-1	2572	0.95	7.58	0
7	SLU 46	174	1	2571	-1.79	7.28	0
7	SLU 47	169	3	2571	-3.61	7.09	0
7	SLU 48	181	-1	2572	0.95	7.58	0
7	SLU 49	174	1	2571	-1.79	7.28	0
7	SLU 50	181	-1	2572	0.95	7.58	0
7	SLU 51	174	1	2571	-1.79	7.28	0
7	SLU 52	212	2	2934	-2.2	8.89	0
7	SLU 53	223	-1	2936	2.35	9.38	0
7	SLU 54	216	1	2935	-0.38	9.09	0
7	SLU 55	212	2	2934	-2.2	8.89	0
7	SLU 56	223	-1	2936	2.35	9.38	0
7	SLU 57	216	1	2935	-0.38	9.09	0
7	SLU 58	223	-1	2936	2.35	9.38	0
7	SLU 59	216	1	2935	-0.38	9.09	0
7	SLU 60	242	-2	3092	2.95	10.15	0
7	SLU 61	235	0	3091	0.22	9.86	0
7	SLU 62	242	-2	3092	2.95	10.15	0
7	SLU 63	235	0	3091	0.22	9.86	0
7	SLU 64	201	-1	2755	1.5	8.42	0
7	SLU 65	189	3	2753	-3.05	7.93	0
7	SLU 66	201	-1	2755	1.5	8.42	0
7	SLU 67	194	1	2754	-1.23	8.13	0
7	SLU 68	189	3	2753	-3.05	7.93	0
7	SLU 69	201	-1	2755	1.5	8.42	0
7	SLU 70	194	1	2754	-1.23	8.13	0
7	SLU 71	201	-1	2755	1.5	8.42	0
7	SLU 72	194	1	2754	-1.23	8.13	0
7	SLU 73	232	2	3116	-1.65	9.74	0
7	SLU 74	243	-2	3118	2.91	10.22	0
7	SLU 75	236	0	3117	0.18	9.93	0
7	SLU 76	232	2	3116	-1.65	9.74	0
7	SLU 77	243	-2	3118	2.91	10.22	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
7	SLU 78	236	0	3117	0.18	9.93	0
7	SLU 79	243	-2	3118	2.91	10.22	0
7	SLU 80	236	0	3117	0.18	9.93	0
7	SLU 81	262	-2	3274	3.51	11	0
7	SLU 82	255	0	3273	0.78	10.7	0
7	SLU 83	262	-2	3274	3.51	11	0
7	SLU 84	255	0	3273	0.78	10.7	0
7	SLE RA 1	150	-1	2079	1.03	6.29	0
7	SLE RA 2	142	2	2078	-2	5.97	0
7	SLE RA 3	150	-1	2079	1.03	6.29	0
7	SLE RA 4	146	1	2078	-0.79	6.1	0
7	SLE RA 5	142	2	2078	-2	5.97	0
7	SLE RA 6	150	-1	2079	1.03	6.29	0
7	SLE RA 7	146	1	2078	-0.79	6.1	0
7	SLE RA 8	150	-1	2079	1.03	6.29	0
7	SLE RA 9	146	1	2078	-0.79	6.1	0
7	SLE RA 10	171	1	2320	-1.07	7.17	0
7	SLE RA 11	178	-1	2321	1.97	7.49	0
7	SLE RA 12	174	0	2320	0.15	7.3	0
7	SLE RA 13	171	1	2320	-1.07	7.17	0
7	SLE RA 14	178	-1	2321	1.97	7.49	0
7	SLE RA 15	174	0	2320	0.15	7.3	0
7	SLE RA 16	178	-1	2321	1.97	7.49	0
7	SLE RA 17	174	0	2320	0.15	7.3	0
7	SLE RA 18	191	-1	2425	2.37	8.01	0
7	SLE RA 19	186	0	2424	0.55	7.81	0
7	SLE RA 20	191	-1	2425	2.37	8.01	0
7	SLE RA 21	186	0	2424	0.55	7.81	0
7	SLE FR 1	150	-1	2079	1.03	6.29	0
7	SLE FR 2	149	0	2079	0.43	6.23	0
7	SLE FR 3	150	-1	2079	1.03	6.29	0
7	SLE FR 4	161	0	2183	0.83	6.74	0
7	SLE FR 5	162	-1	2183	1.44	6.81	0
7	SLE FR 6	170	-1	2252	1.7	7.15	0
7	SLE QP 1	150	-1	2079	1.03	6.29	0
7	SLE QP 2	162	-1	2183	1.44	6.81	0
7	SLD 1	417	-3	2301	-1.81	17.56	0
7	SLD 2	417	-3	2301	-1.81	17.56	0
7	SLD 3	354	-25	2244	28.7	14.89	-0.03
7	SLD 4	354	-25	2244	28.7	14.89	-0.03
7	SLD 5	334	33	2304	-45.82	14.09	0.04
7	SLD 6	334	33	2304	-45.82	14.09	0.04
7	SLD 7	124	-42	2115	55.89	5.17	-0.05
7	SLD 8	124	-42	2115	55.89	5.17	-0.05
7	SLD 9	200	40	2250	-53.02	8.44	0.04
7	SLD 10	200	40	2250	-53.02	8.44	0.04
7	SLD 11	-10	-34	2061	48.69	-0.48	-0.04
7	SLD 12	-10	-34	2061	48.69	-0.48	-0.04
7	SLD 13	-29	23	2121	-25.83	-1.28	0.02
7	SLD 14	-29	23	2121	-25.83	-1.28	0.02
7	SLD 15	-92	1	2064	4.68	-3.95	0
7	SLD 16	-92	1	2064	4.68	-3.95	0
7	SLV 1	769	-4	2465	-8.53	32.42	0
7	SLV 2	769	-4	2465	-8.53	32.42	0
7	SLV 3	613	-61	2325	70.78	25.81	-0.06
7	SLV 4	613	-61	2325	70.78	25.81	-0.06
7	SLV 5	581	85	2479	-121.83	24.53	0.1
7	SLV 6	581	85	2479	-121.83	24.53	0.1
7	SLV 7	61	-106	2014	142.52	2.47	-0.11
7	SLV 8	61	-106	2014	142.52	2.47	-0.11
7	SLV 9	264	104	2352	-139.65	11.14	0.11
7	SLV 10	264	104	2352	-139.65	11.14	0.11
7	SLV 11	-256	-87	1886	124.71	-10.91	-0.1
7	SLV 12	-256	-87	1886	124.71	-10.91	-0.1
7	SLV 13	-288	59	2040	-67.91	-12.19	0.06
7	SLV 14	-288	59	2040	-67.91	-12.19	0.06
7	SLV 15	-444	2	1901	11.4	-18.81	0
7	SLV 16	-444	2	1901	11.4	-18.81	0
8	SLU 1	107	-1	2023	0.98	4.5	0
8	SLU 2	95	2	2024	-3.51	3.98	0
8	SLU 3	107	-1	2023	0.98	4.5	0
8	SLU 4	100	1	2024	-1.71	4.19	0
8	SLU 5	95	2	2024	-3.51	3.98	0
8	SLU 6	107	-1	2023	0.98	4.5	0
8	SLU 7	100	1	2024	-1.71	4.19	0
8	SLU 8	107	-1	2023	0.98	4.5	0
8	SLU 9	100	1	2024	-1.71	4.19	0
8	SLU 10	126	2	2378	-1.98	5.34	0
8	SLU 11	138	-1	2377	2.5	5.86	0
8	SLU 12	131	0	2377	-0.19	5.55	0
8	SLU 13	126	2	2378	-1.98	5.34	0
8	SLU 14	138	-1	2377	2.5	5.86	0
8	SLU 15	131	0	2377	-0.19	5.55	0
8	SLU 16	138	-1	2377	2.5	5.86	0
8	SLU 17	131	0	2377	-0.19	5.55	0
8	SLU 18	152	-2	2529	3.16	6.45	0
8	SLU 19	144	0	2529	0.47	6.13	0
8	SLU 20	152	-2	2529	3.16	6.45	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
8	SLU 21	144	0	2529	0.47	6.13	0
8	SLU 22	121	-1	2202	1.59	5.11	0
8	SLU 23	109	2	2203	-2.9	4.58	0
8	SLU 24	121	-1	2202	1.59	5.11	0
8	SLU 25	114	1	2202	-1.1	4.79	0
8	SLU 26	109	2	2203	-2.9	4.58	0
8	SLU 27	121	-1	2202	1.59	5.11	0
8	SLU 28	114	1	2202	-1.1	4.79	0
8	SLU 29	121	-1	2202	1.59	5.11	0
8	SLU 30	114	1	2202	-1.1	4.79	0
8	SLU 31	140	1	2557	-1.37	5.94	0
8	SLU 32	152	-2	2556	3.11	6.47	0
8	SLU 33	145	0	2556	0.42	6.15	0
8	SLU 34	140	1	2557	-1.37	5.94	0
8	SLU 35	152	-2	2556	3.11	6.47	0
8	SLU 36	145	0	2556	0.42	6.15	0
8	SLU 37	152	-2	2556	3.11	6.47	0
8	SLU 38	145	0	2556	0.42	6.15	0
8	SLU 39	165	-2	2707	3.77	7.05	0
8	SLU 40	158	0	2708	1.07	6.74	0
8	SLU 41	165	-2	2707	3.77	7.05	0
8	SLU 42	158	0	2708	1.07	6.74	0
8	SLU 43	135	-1	2569	1.07	5.65	0
8	SLU 44	123	2	2570	-3.42	5.13	0
8	SLU 45	135	-1	2569	1.07	5.65	0
8	SLU 46	128	1	2569	-1.62	5.34	0
8	SLU 47	123	2	2570	-3.42	5.13	0
8	SLU 48	135	-1	2569	1.07	5.65	0
8	SLU 49	128	1	2569	-1.62	5.34	0
8	SLU 50	135	-1	2569	1.07	5.65	0
8	SLU 51	128	1	2569	-1.62	5.34	0
8	SLU 52	154	2	2923	-1.89	6.49	0
8	SLU 53	166	-1	2923	2.59	7.01	0
8	SLU 54	159	0	2923	-0.1	6.7	0
8	SLU 55	154	2	2923	-1.89	6.49	0
8	SLU 56	166	-1	2923	2.59	7.01	0
8	SLU 57	159	0	2923	-0.1	6.7	0
8	SLU 58	166	-1	2923	2.59	7.01	0
8	SLU 59	159	0	2923	-0.1	6.7	0
8	SLU 60	179	-2	3074	3.24	7.59	0
8	SLU 61	172	0	3075	0.55	7.28	0
8	SLU 62	179	-2	3074	3.24	7.59	0
8	SLU 63	172	0	3075	0.55	7.28	0
8	SLU 64	149	-1	2748	1.67	6.25	0
8	SLU 65	137	2	2748	-2.81	5.73	0
8	SLU 66	149	-1	2748	1.67	6.25	0
8	SLU 67	141	1	2748	-1.02	5.94	0
8	SLU 68	137	2	2748	-2.81	5.73	0
8	SLU 69	149	-1	2748	1.67	6.25	0
8	SLU 70	141	1	2748	-1.02	5.94	0
8	SLU 71	149	-1	2748	1.67	6.25	0
8	SLU 72	141	1	2748	-1.02	5.94	0
8	SLU 73	167	1	3102	-1.29	7.09	0
8	SLU 74	180	-2	3101	3.2	7.61	0
8	SLU 75	172	0	3102	0.51	7.3	0
8	SLU 76	167	1	3102	-1.29	7.09	0
8	SLU 77	180	-2	3101	3.2	7.61	0
8	SLU 78	172	0	3102	0.51	7.3	0
8	SLU 79	180	-2	3101	3.2	7.61	0
8	SLU 80	172	0	3102	0.51	7.3	0
8	SLU 81	193	-2	3253	3.85	8.19	0
8	SLU 82	186	0	3254	1.16	7.88	0
8	SLU 83	193	-2	3253	3.85	8.19	0
8	SLU 84	186	0	3254	1.16	7.88	0
8	SLE RA 1	111	-1	2074	1.15	4.68	0
8	SLE RA 2	103	1	2075	-1.84	4.33	0
8	SLE RA 3	111	-1	2074	1.15	4.68	0
8	SLE RA 4	106	1	2075	-0.64	4.47	0
8	SLE RA 5	103	1	2075	-1.84	4.33	0
8	SLE RA 6	111	-1	2074	1.15	4.68	0
8	SLE RA 7	106	1	2075	-0.64	4.47	0
8	SLE RA 8	111	-1	2074	1.15	4.68	0
8	SLE RA 9	106	1	2075	-0.64	4.47	0
8	SLE RA 10	124	1	2311	-0.82	5.24	0
8	SLE RA 11	132	-1	2310	2.17	5.58	0
8	SLE RA 12	127	0	2310	0.38	5.37	0
8	SLE RA 13	124	1	2311	-0.82	5.24	0
8	SLE RA 14	132	-1	2310	2.17	5.58	0
8	SLE RA 15	127	0	2310	0.38	5.37	0
8	SLE RA 16	132	-1	2310	2.17	5.58	0
8	SLE RA 17	127	0	2310	0.38	5.37	0
8	SLE RA 18	141	-1	2411	2.61	5.97	0
8	SLE RA 19	136	0	2412	0.81	5.76	0
8	SLE RA 20	141	-1	2411	2.61	5.97	0
8	SLE RA 21	136	0	2412	0.81	5.76	0
8	SLE FR 1	111	-1	2074	1.15	4.68	0
8	SLE FR 2	110	0	2074	0.56	4.61	0
8	SLE FR 3	111	-1	2074	1.15	4.68	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
8	SLE FR 4	119	-1	2176	0.99	5	0
8	SLE FR 5	120	-1	2175	1.59	5.06	0
8	SLE FR 6	126	-1	2243	1.88	5.32	0
8	SLE QP 1	111	-1	2074	1.15	4.68	0
8	SLE QP 2	120	-1	2175	1.59	5.06	0
8	SLD 1	377	-1	2264	-3.61	15.87	0
8	SLD 2	377	-1	2264	-3.61	15.87	0
8	SLD 3	315	-28	2221	32.14	13.24	-0.03
8	SLD 4	315	-28	2221	32.14	13.24	-0.03
8	SLD 5	292	40	2267	-54.2	12.29	0.05
8	SLD 6	292	40	2267	-54.2	12.29	0.05
8	SLD 7	84	-50	2124	64.99	3.53	-0.06
8	SLD 8	84	-50	2124	64.99	3.53	-0.06
8	SLD 9	156	48	2227	-61.81	6.6	0.06
8	SLD 10	156	48	2227	-61.81	6.6	0.06
8	SLD 11	-51	-42	2084	57.38	-2.16	-0.05
8	SLD 12	-51	-42	2084	57.38	-2.16	-0.05
8	SLD 13	-75	26	2130	-28.96	-3.11	0.03
8	SLD 14	-75	26	2130	-28.96	-3.11	0.03
8	SLD 15	-137	-1	2087	6.79	-5.74	0
8	SLD 16	-137	-1	2087	6.79	-5.74	0
8	SLV 1	732	2	2387	-13.57	30.8	0
8	SLV 2	732	2	2387	-13.57	30.8	0
8	SLV 3	578	-68	2280	79.45	24.29	-0.08
8	SLV 4	578	-68	2280	79.45	24.29	-0.08
8	SLV 5	538	106	2400	-144.03	22.67	0.12
8	SLV 6	538	106	2400	-144.03	22.67	0.12
8	SLV 7	24	-127	2046	166.02	0.95	-0.15
8	SLV 8	24	-127	2046	166.02	0.95	-0.15
8	SLV 9	217	125	2305	-162.84	9.18	0.15
8	SLV 10	217	125	2305	-162.84	9.18	0.15
8	SLV 11	-297	-108	1951	147.21	-12.54	-0.12
8	SLV 12	-297	-108	1951	147.21	-12.54	-0.12
8	SLV 13	-338	66	2070	-76.27	-14.16	0.08
8	SLV 14	-338	66	2070	-76.27	-14.16	0.08
8	SLV 15	-492	-4	1964	16.75	-20.68	0
8	SLV 16	-492	-4	1964	16.75	-20.68	0
9	SLU 1	74	-1	2016	1.03	3.13	0
9	SLU 2	62	2	2019	-3.19	2.61	0
9	SLU 3	74	-1	2016	1.03	3.13	0
9	SLU 4	66	1	2018	-1.5	2.82	0
9	SLU 5	62	2	2019	-3.19	2.61	0
9	SLU 6	74	-1	2016	1.03	3.13	0
9	SLU 7	66	1	2018	-1.5	2.82	0
9	SLU 8	74	-1	2016	1.03	3.13	0
9	SLU 9	66	1	2018	-1.5	2.82	0
9	SLU 10	80	1	2361	-1.62	3.45	0
9	SLU 11	93	-1	2358	2.61	3.96	0
9	SLU 12	85	0	2360	0.07	3.65	0
9	SLU 13	80	1	2361	-1.62	3.45	0
9	SLU 14	93	-1	2358	2.61	3.96	0
9	SLU 15	85	0	2360	0.07	3.65	0
9	SLU 16	93	-1	2358	2.61	3.96	0
9	SLU 17	85	0	2360	0.07	3.65	0
9	SLU 18	101	-2	2505	3.28	4.31	0
9	SLU 19	93	0	2506	0.74	4.01	0
9	SLU 20	101	-2	2505	3.28	4.31	0
9	SLU 21	93	0	2506	0.74	4.01	0
9	SLU 22	81	-1	2190	1.66	3.46	0
9	SLU 23	69	2	2192	-2.57	2.95	0
9	SLU 24	81	-1	2190	1.66	3.46	0
9	SLU 25	74	1	2191	-0.88	3.16	0
9	SLU 26	69	2	2192	-2.57	2.95	0
9	SLU 27	81	-1	2190	1.66	3.46	0
9	SLU 28	74	1	2191	-0.88	3.16	0
9	SLU 29	81	-1	2190	1.66	3.46	0
9	SLU 30	74	1	2191	-0.88	3.16	0
9	SLU 31	88	1	2535	-0.99	3.78	0
9	SLU 32	100	-2	2532	3.23	4.3	0
9	SLU 33	93	0	2534	0.7	3.99	0
9	SLU 34	88	1	2535	-0.99	3.78	0
9	SLU 35	100	-2	2532	3.23	4.3	0
9	SLU 36	93	0	2534	0.7	3.99	0
9	SLU 37	100	-2	2532	3.23	4.3	0
9	SLU 38	93	0	2534	0.7	3.99	0
9	SLU 39	108	-2	2679	3.91	4.65	0
9	SLU 40	101	-1	2680	1.37	4.34	0
9	SLU 41	108	-2	2679	3.91	4.65	0
9	SLU 42	101	-1	2680	1.37	4.34	0
9	SLU 43	93	-1	2561	1.13	3.95	0
9	SLU 44	81	2	2564	-3.1	3.44	0
9	SLU 45	93	-1	2561	1.13	3.95	0
9	SLU 46	86	1	2563	-1.41	3.64	0
9	SLU 47	81	2	2564	-3.1	3.44	0
9	SLU 48	93	-1	2561	1.13	3.95	0
9	SLU 49	86	1	2563	-1.41	3.64	0
9	SLU 50	93	-1	2561	1.13	3.95	0
9	SLU 51	86	1	2563	-1.41	3.64	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
9	SLU 52	100	1	2906	-1.53	4.27	0
9	SLU 53	112	-1	2903	2.7	4.78	0
9	SLU 54	105	0	2905	0.16	4.47	0
9	SLU 55	100	1	2906	-1.53	4.27	0
9	SLU 56	112	-1	2903	2.7	4.78	0
9	SLU 57	105	0	2905	0.16	4.47	0
9	SLU 58	112	-1	2903	2.7	4.78	0
9	SLU 59	105	0	2905	0.16	4.47	0
9	SLU 60	120	-2	3050	3.37	5.14	0
9	SLU 61	113	0	3052	0.84	4.83	0
9	SLU 62	120	-2	3050	3.37	5.14	0
9	SLU 63	113	0	3052	0.84	4.83	0
9	SLU 64	101	-1	2735	1.75	4.29	0
9	SLU 65	89	2	2738	-2.47	3.77	0
9	SLU 66	101	-1	2735	1.75	4.29	0
9	SLU 67	94	1	2737	-0.78	3.98	0
9	SLU 68	89	2	2738	-2.47	3.77	0
9	SLU 69	101	-1	2735	1.75	4.29	0
9	SLU 70	94	1	2737	-0.78	3.98	0
9	SLU 71	101	-1	2735	1.75	4.29	0
9	SLU 72	94	1	2737	-0.78	3.98	0
9	SLU 73	108	1	3080	-0.9	4.61	0
9	SLU 74	120	-2	3077	3.33	5.12	0
9	SLU 75	112	0	3079	0.79	4.81	0
9	SLU 76	108	1	3080	-0.9	4.61	0
9	SLU 77	120	-2	3077	3.33	5.12	0
9	SLU 78	112	0	3079	0.79	4.81	0
9	SLU 79	120	-2	3077	3.33	5.12	0
9	SLU 80	112	0	3079	0.79	4.81	0
9	SLU 81	128	-2	3224	4	5.47	0
9	SLU 82	121	-1	3225	1.47	5.17	0
9	SLU 83	128	-2	3224	4	5.47	0
9	SLU 84	121	-1	3225	1.47	5.17	0
9	SLE RA 1	76	-1	2066	1.21	3.22	0
9	SLE RA 2	68	1	2067	-1.61	2.88	0
9	SLE RA 3	76	-1	2066	1.21	3.22	0
9	SLE RA 4	71	0	2067	-0.48	3.02	0
9	SLE RA 5	68	1	2067	-1.61	2.88	0
9	SLE RA 6	76	-1	2066	1.21	3.22	0
9	SLE RA 7	71	0	2067	-0.48	3.02	0
9	SLE RA 8	76	-1	2066	1.21	3.22	0
9	SLE RA 9	71	0	2067	-0.48	3.02	0
9	SLE RA 10	80	0	2296	-0.56	3.44	0
9	SLE RA 11	89	-1	2294	2.26	3.78	0
9	SLE RA 12	84	0	2295	0.57	3.57	0
9	SLE RA 13	80	0	2296	-0.56	3.44	0
9	SLE RA 14	89	-1	2294	2.26	3.78	0
9	SLE RA 15	84	0	2295	0.57	3.57	0
9	SLE RA 16	89	-1	2294	2.26	3.78	0
9	SLE RA 17	84	0	2295	0.57	3.57	0
9	SLE RA 18	94	-1	2392	2.71	4.01	0
9	SLE RA 19	89	0	2393	1.02	3.81	0
9	SLE RA 20	94	-1	2392	2.71	4.01	0
9	SLE RA 21	89	0	2393	1.02	3.81	0
9	SLE FR 1	76	-1	2066	1.21	3.22	0
9	SLE FR 2	74	0	2066	0.65	3.15	0
9	SLE FR 3	76	-1	2066	1.21	3.22	0
9	SLE FR 4	80	-1	2164	1.1	3.39	0
9	SLE FR 5	81	-1	2163	1.66	3.46	0
9	SLE FR 6	85	-1	2229	1.96	3.62	0
9	SLE QP 1	76	-1	2066	1.21	3.22	0
9	SLE QP 2	81	-1	2163	1.66	3.46	0
9	SLD 1	339	2	2229	-5.44	14.31	0
9	SLD 2	339	2	2229	-5.44	14.31	0
9	SLD 3	278	-29	2196	34.05	11.73	-0.04
9	SLD 4	278	-29	2196	34.05	11.73	-0.04
9	SLD 5	251	46	2233	-60.37	10.63	0.07
9	SLD 6	251	46	2233	-60.37	10.63	0.07
9	SLD 7	48	-56	2123	71.28	2.03	-0.08
9	SLD 8	48	-56	2123	71.28	2.03	-0.08
9	SLD 9	115	54	2204	-67.96	4.89	0.08
9	SLD 10	115	54	2204	-67.96	4.89	0.08
9	SLD 11	-89	-48	2094	63.69	-3.71	-0.07
9	SLD 12	-89	-48	2094	63.69	-3.71	-0.07
9	SLD 13	-116	27	2131	-30.73	-4.81	0.04
9	SLD 14	-116	27	2131	-30.73	-4.81	0.04
9	SLD 15	-177	-3	2098	8.76	-7.39	-0.01
9	SLD 16	-177	-3	2098	8.76	-7.39	-0.01
9	SLV 1	696	8	2320	-18.32	29.32	0.01
9	SLV 2	696	8	2320	-18.32	29.32	0.01
9	SLV 3	544	-71	2238	84.47	22.9	-0.1
9	SLV 4	544	-71	2238	84.47	22.9	-0.1
9	SLV 5	496	121	2334	-160.22	20.96	0.17
9	SLV 6	496	121	2334	-160.22	20.96	0.17
9	SLV 7	-10	-141	2062	182.39	-0.45	-0.2
9	SLV 8	-10	-141	2062	182.39	-0.45	-0.2
9	SLV 9	173	139	2265	-179.07	7.37	0.19
9	SLV 10	173	139	2265	-179.07	7.37	0.19



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
9	SLV 11	-334	-123	1993	163.54	-14.04	-0.17
9	SLV 12	-334	-123	1993	163.54	-14.04	-0.17
9	SLV 13	-382	69	2089	-81.14	-15.98	0.09
9	SLV 14	-382	69	2089	-81.14	-15.98	0.09
9	SLV 15	-534	-9	2007	21.64	-22.4	-0.02
9	SLV 16	-534	-9	2007	21.64	-22.4	-0.02
10	SLU 1	43	-1	2005	1.04	1.88	0
10	SLU 2	31	2	2009	-2.79	1.36	0
10	SLU 3	43	-1	2005	1.04	1.88	0
10	SLU 4	36	1	2007	-1.26	1.57	0
10	SLU 5	31	2	2009	-2.79	1.36	0
10	SLU 6	43	-1	2005	1.04	1.88	0
10	SLU 7	36	1	2007	-1.26	1.57	0
10	SLU 8	43	-1	2005	1.04	1.88	0
10	SLU 9	36	1	2007	-1.26	1.57	0
10	SLU 10	39	1	2337	-1.23	1.78	0
10	SLU 11	51	-1	2333	2.61	2.31	0
10	SLU 12	44	0	2335	0.3	1.99	0
10	SLU 13	39	1	2337	-1.23	1.78	0
10	SLU 14	51	-1	2333	2.61	2.31	0
10	SLU 15	44	0	2335	0.3	1.99	0
10	SLU 16	51	-1	2333	2.61	2.31	0
10	SLU 17	44	0	2335	0.3	1.99	0
10	SLU 18	54	-2	2474	3.28	2.49	0
10	SLU 19	47	0	2476	0.97	2.17	0
10	SLU 20	54	-2	2474	3.28	2.49	0
10	SLU 21	47	0	2476	0.97	2.17	0
10	SLU 22	45	-1	2172	1.67	2.01	0
10	SLU 23	33	1	2176	-2.17	1.49	0
10	SLU 24	45	-1	2172	1.67	2.01	0
10	SLU 25	38	0	2175	-0.63	1.7	0
10	SLU 26	33	1	2176	-2.17	1.49	0
10	SLU 27	45	-1	2172	1.67	2.01	0
10	SLU 28	38	0	2175	-0.63	1.7	0
10	SLU 29	45	-1	2172	1.67	2.01	0
10	SLU 30	38	0	2175	-0.63	1.7	0
10	SLU 31	41	0	2504	-0.61	1.91	0
10	SLU 32	53	-2	2500	3.23	2.43	0
10	SLU 33	46	0	2503	0.93	2.12	0
10	SLU 34	41	0	2504	-0.61	1.91	0
10	SLU 35	53	-2	2500	3.23	2.43	0
10	SLU 36	46	0	2503	0.93	2.12	0
10	SLU 37	53	-2	2500	3.23	2.43	0
10	SLU 38	46	0	2503	0.93	2.12	0
10	SLU 39	57	-2	2641	3.9	2.61	0
10	SLU 40	49	-1	2643	1.6	2.3	0
10	SLU 41	57	-2	2641	3.9	2.61	0
10	SLU 42	49	-1	2643	1.6	2.3	0
10	SLU 43	56	-1	2549	1.14	2.41	0
10	SLU 44	43	1	2553	-2.7	1.88	0
10	SLU 45	56	-1	2549	1.14	2.41	0
10	SLU 46	48	1	2552	-1.16	2.09	0
10	SLU 47	43	1	2553	-2.7	1.88	0
10	SLU 48	56	-1	2549	1.14	2.41	0
10	SLU 49	48	1	2552	-1.16	2.09	0
10	SLU 50	56	-1	2549	1.14	2.41	0
10	SLU 51	48	1	2552	-1.16	2.09	0
10	SLU 52	51	1	2881	-1.13	2.3	0
10	SLU 53	63	-1	2877	2.71	2.83	0
10	SLU 54	56	0	2880	0.4	2.51	0
10	SLU 55	51	1	2881	-1.13	2.3	0
10	SLU 56	63	-1	2877	2.71	2.83	0
10	SLU 57	56	0	2880	0.4	2.51	0
10	SLU 58	63	-1	2877	2.71	2.83	0
10	SLU 59	56	0	2880	0.4	2.51	0
10	SLU 60	67	-2	3018	3.38	3.01	0
10	SLU 61	59	0	3020	1.07	2.69	0
10	SLU 62	67	-2	3018	3.38	3.01	0
10	SLU 63	59	0	3020	1.07	2.69	0
10	SLU 64	58	-1	2716	1.77	2.53	0
10	SLU 65	45	1	2721	-2.07	2.01	0
10	SLU 66	58	-1	2716	1.77	2.53	0
10	SLU 67	50	0	2719	-0.54	2.22	0
10	SLU 68	45	1	2721	-2.07	2.01	0
10	SLU 69	58	-1	2716	1.77	2.53	0
10	SLU 70	50	0	2719	-0.54	2.22	0
10	SLU 71	58	-1	2716	1.77	2.53	0
10	SLU 72	50	0	2719	-0.54	2.22	0
10	SLU 73	53	0	3049	-0.51	2.43	0
10	SLU 74	65	-2	3044	3.33	2.95	0
10	SLU 75	58	0	3047	1.03	2.64	0
10	SLU 76	53	0	3049	-0.51	2.43	0
10	SLU 77	65	-2	3044	3.33	2.95	0
10	SLU 78	58	0	3047	1.03	2.64	0
10	SLU 79	65	-2	3044	3.33	2.95	0
10	SLU 80	58	0	3047	1.03	2.64	0
10	SLU 81	69	-2	3185	4	3.14	0
10	SLU 82	61	-1	3188	1.7	2.82	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
10	SLU 83	69	-2	3185	4	3.14	0
10	SLU 84	61	-1	3188	1.7	2.82	0
10	SLE RA 1	44	-1	2053		1.92	0
10	SLE RA 2	36	1	2056	-1.34	1.57	0
10	SLE RA 3	44	-1	2053	1.22	1.92	0
10	SLE RA 4	39	0	2054	-0.31	1.71	0
10	SLE RA 5	36	1	2056	-1.34	1.57	0
10	SLE RA 6	44	-1	2053	1.22	1.92	0
10	SLE RA 7	39	0	2054	-0.31	1.71	0
10	SLE RA 8	44	-1	2053	1.22	1.92	0
10	SLE RA 9	39	0	2054	-0.31	1.71	0
10	SLE RA 10	41	0	2274	-0.29	1.85	0
10	SLE RA 11	49	-1	2271	2.26	2.2	0
10	SLE RA 12	44	0	2273	0.73	1.99	0
10	SLE RA 13	41	0	2274	-0.29	1.85	0
10	SLE RA 14	49	-1	2271	2.26	2.2	0
10	SLE RA 15	44	0	2273	0.73	1.99	0
10	SLE RA 16	49	-1	2271	2.26	2.2	0
10	SLE RA 17	44	0	2273	0.73	1.99	0
10	SLE RA 18	51	-1	2365	2.71	2.32	0
10	SLE RA 19	46	-1	2367	1.18	2.11	0
10	SLE RA 20	51	-1	2365	2.71	2.32	0
10	SLE RA 21	46	-1	2367	1.18	2.11	0
10	SLE FR 1	44	-1	2053	1.22	1.92	0
10	SLE FR 2	42	0	2053	0.71	1.85	0
10	SLE FR 3	44	-1	2053	1.22	1.92	0
10	SLE FR 4	45	-1	2147	1.16	1.97	0
10	SLE FR 5	46	-1	2147	1.67	2.04	0
10	SLE FR 6	48	-1	2209	1.97	2.12	0
10	SLE QP 1	44	-1	2053	1.22	1.92	0
10	SLE QP 2	46	-1	2147	1.67	2.04	0
10	SLD 1	305	4	2199	-6.87	12.9	0.01
10	SLD 2	305	4	2199	-6.87	12.9	0.01
10	SLD 3	245	-29	2170	34.63	10.38	-0.05
10	SLD 4	245	-29	2170	34.63	10.38	-0.05
10	SLD 5	214	50	2207	-63.83	9.12	0.09
10	SLD 6	214	50	2207	-63.83	9.12	0.09
10	SLD 7	16	-58	2109	74.5	0.72	-0.1
10	SLD 8	16	-58	2109	74.5	0.72	-0.1
10	SLD 9	77	57	2184	-71.16	3.36	0.1
10	SLD 10	77	57	2184	-71.16	3.36	0.1
10	SLD 11	-121	-51	2086	67.17	-5.04	-0.09
10	SLD 12	-121	-51	2086	67.17	-5.04	-0.09
10	SLD 13	-153	27	2123	-31.3	-6.3	0.05
10	SLD 14	-153	27	2123	-31.3	-6.3	0.05
10	SLD 15	-212	-5	2094	10.2	-8.82	-0.01
10	SLD 16	-212	-5	2094	10.2	-8.82	-0.01
10	SLV 1	662	12	2272	-21.74	27.95	0.02
10	SLV 2	662	12	2272	-21.74	27.95	0.02
10	SLV 3	514	-71	2201	86.28	21.67	-0.12
10	SLV 4	514	-71	2201	86.28	21.67	-0.12
10	SLV 5	456	129	2292	-169.18	19.34	0.23
10	SLV 6	456	129	2292	-169.18	19.34	0.23
10	SLV 7	-38	-148	2055	190.88	-1.6	-0.26
10	SLV 8	-38	-148	2055	190.88	-1.6	-0.26
10	SLV 9	130	146	2238	-187.55	5.68	0.26
10	SLV 10	130	146	2238	-187.55	5.68	0.26
10	SLV 11	-363	-131	2001	172.52	-15.26	-0.23
10	SLV 12	-363	-131	2001	172.52	-15.26	-0.23
10	SLV 13	-422	69	2092	-82.94	-17.59	0.12
10	SLV 14	-422	69	2092	-82.94	-17.59	0.12
10	SLV 15	-570	-14	2021	25.08	-23.87	-0.03
10	SLV 16	-570	-14	2021	25.08	-23.87	-0.03
11	SLU 1	15	0	2010	1.03	0.71	0
11	SLU 2	3	1	2016	-2.37	0.2	0
11	SLU 3	15	0	2010	1.03	0.71	0
11	SLU 4	8	0	2014	-1.01	0.4	0
11	SLU 5	3	1	2016	-2.37	0.2	0
11	SLU 6	15	0	2010	1.03	0.71	0
11	SLU 7	8	0	2014	-1.01	0.4	0
11	SLU 8	15	0	2010	1.03	0.71	0
11	SLU 9	8	0	2014	-1.01	0.4	0
11	SLU 10	-1	0	2330	-0.85	0.12	0
11	SLU 11	12	-1	2325	2.56	0.63	0
11	SLU 12	4	0	2328	0.52	0.32	0
11	SLU 13	-1	0	2330	-0.85	0.12	0
11	SLU 14	12	-1	2325	2.56	0.63	0
11	SLU 15	4	0	2328	0.52	0.32	0
11	SLU 16	12	-1	2325	2.56	0.63	0
11	SLU 17	4	0	2328	0.52	0.32	0
11	SLU 18	10	-1	2460	3.21	0.6	0
11	SLU 19	3	-1	2463	1.17	0.29	0
11	SLU 20	10	-1	2460	3.21	0.6	0
11	SLU 21	3	-1	2463	1.17	0.29	0
11	SLU 22	12	-1	2171	1.64	0.6	0
11	SLU 23	0	1	2177	-1.76	0.09	0
11	SLU 24	12	-1	2171	1.64	0.6	0
11	SLU 25	5	0	2175	-0.4	0.3	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
11	SLU 26	0	1	2177	-1.76	0.09	0
11	SLU 27	12	-1	2171	1.64	0.6	0
11	SLU 28	5	0	2175	-0.4	0.3	0
11	SLU 29	12	-1	2171	1.64	0.6	0
11	SLU 30	5	0	2175	-0.4	0.3	0
11	SLU 31	-4	0	2491	-0.23	0.02	0
11	SLU 32	8	-1	2486	3.17	0.53	0
11	SLU 33	1	-1	2489	1.13	0.22	0
11	SLU 34	-4	0	2491	-0.23	0.02	0
11	SLU 35	8	-1	2486	3.17	0.53	0
11	SLU 36	1	-1	2489	1.13	0.22	0
11	SLU 37	8	-1	2486	3.17	0.53	0
11	SLU 38	1	-1	2489	1.13	0.22	0
11	SLU 39	7	-2	2621	3.82	0.5	0
11	SLU 40	-1	-1	2624	1.78	0.19	0
11	SLU 41	7	-2	2621	3.82	0.5	0
11	SLU 42	-1	-1	2624	1.78	0.19	0
11	SLU 43	21	-1	2558	1.13	0.95	0
11	SLU 44	9	1	2564	-2.27	0.44	0
11	SLU 45	21	-1	2558	1.13	0.95	0
11	SLU 46	14	0	2561	-0.91	0.65	0
11	SLU 47	9	1	2564	-2.27	0.44	0
11	SLU 48	21	-1	2558	1.13	0.95	0
11	SLU 49	14	0	2561	-0.91	0.65	0
11	SLU 50	21	-1	2558	1.13	0.95	0
11	SLU 51	14	0	2561	-0.91	0.65	0
11	SLU 52	5	0	2878	-0.74	0.37	0
11	SLU 53	17	-1	2873	2.66	0.88	0
11	SLU 54	10	0	2876	0.62	0.57	0
11	SLU 55	5	0	2878	-0.74	0.37	0
11	SLU 56	17	-1	2873	2.66	0.88	0
11	SLU 57	10	0	2876	0.62	0.57	0
11	SLU 58	17	-1	2873	2.66	0.88	0
11	SLU 59	10	0	2876	0.62	0.57	0
11	SLU 60	16	-2	3007	3.31	0.85	0
11	SLU 61	8	-1	3011	1.27	0.54	0
11	SLU 62	16	-2	3007	3.31	0.85	0
11	SLU 63	8	-1	3011	1.27	0.54	0
11	SLU 64	18	-1	2719	1.74	0.85	0
11	SLU 65	5	1	2725	-1.66	0.34	0
11	SLU 66	18	-1	2719	1.74	0.85	0
11	SLU 67	10	0	2722	-0.3	0.55	0
11	SLU 68	5	1	2725	-1.66	0.34	0
11	SLU 69	18	-1	2719	1.74	0.85	0
11	SLU 70	10	0	2722	-0.3	0.55	0
11	SLU 71	18	-1	2719	1.74	0.85	0
11	SLU 72	10	0	2722	-0.3	0.55	0
11	SLU 73	2	0	3039	-0.13	0.27	0
11	SLU 74	14	-2	3034	3.27	0.78	0
11	SLU 75	7	-1	3037	1.23	0.47	0
11	SLU 76	2	0	3039	-0.13	0.27	0
11	SLU 77	14	-2	3034	3.27	0.78	0
11	SLU 78	7	-1	3037	1.23	0.47	0
11	SLU 79	14	-2	3034	3.27	0.78	0
11	SLU 80	7	-1	3037	1.23	0.47	0
11	SLU 81	12	-2	3168	3.92	0.74	0
11	SLU 82	5	-1	3172	1.88	0.44	0
11	SLU 83	12	-2	3168	3.92	0.74	0
11	SLU 84	5	-1	3172	1.88	0.44	0
11	SLE RA 1	14	-1	2056	1.21	0.68	0
11	SLE RA 2	6	1	2060	-1.06	0.34	0
11	SLE RA 3	14	-1	2056	1.21	0.68	0
11	SLE RA 4	9	0	2058	-0.15	0.47	0
11	SLE RA 5	6	1	2060	-1.06	0.34	0
11	SLE RA 6	14	-1	2056	1.21	0.68	0
11	SLE RA 7	9	0	2058	-0.15	0.47	0
11	SLE RA 8	14	-1	2056	1.21	0.68	0
11	SLE RA 9	9	0	2058	-0.15	0.47	0
11	SLE RA 10	4	0	2270	-0.04	0.29	0
11	SLE RA 11	12	-1	2266	2.22	0.63	0
11	SLE RA 12	7	0	2268	0.86	0.42	0
11	SLE RA 13	4	0	2270	-0.04	0.29	0
11	SLE RA 14	12	-1	2266	2.22	0.63	0
11	SLE RA 15	7	0	2268	0.86	0.42	0
11	SLE RA 16	12	-1	2266	2.22	0.63	0
11	SLE RA 17	7	0	2268	0.86	0.42	0
11	SLE RA 18	11	-1	2356	2.66	0.6	0
11	SLE RA 19	6	-1	2358	1.3	0.4	0
11	SLE RA 20	11	-1	2356	2.66	0.6	0
11	SLE RA 21	6	-1	2358	1.3	0.4	0
11	SLE FR 1	14	-1	2056	1.21	0.68	0
11	SLE FR 2	13	0	2057	0.75	0.61	0
11	SLE FR 3	14	-1	2056	1.21	0.68	0
11	SLE FR 4	12	-1	2147	1.19	0.59	0
11	SLE FR 5	13	-1	2146	1.64	0.66	0
11	SLE FR 6	13	-1	2206	1.93	0.64	0
11	SLE QP 1	14	-1	2056	1.21	0.68	0
11	SLE QP 2	13	-1	2146	1.64	0.66	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
11	SLD 1	274	5	2203	-7.53	11.58	0.01
11	SLD 2	274	5	2203	-7.53	11.58	0.01
11	SLD 3	216	-28	2168	34.55	9.11	-0.07
11	SLD 4	216	-28	2168	34.55	9.11	-0.07
11	SLD 5	180	50	2217	-64.93	7.68	0.13
11	SLD 6	180	50	2217	-64.93	7.68	0.13
11	SLD 7	-15	-58	2100	75.33	-0.55	-0.15
11	SLD 8	-15	-58	2100	75.33	-0.55	-0.15
11	SLD 9	41	57	2193	-72.05	1.86	0.15
11	SLD 10	41	57	2193	-72.05	1.86	0.15
11	SLD 11	-154	-52	2076	68.21	-6.36	-0.13
11	SLD 12	-154	-52	2076	68.21	-6.36	-0.13
11	SLD 13	-189	26	2124	-31.26	-7.8	0.07
11	SLD 14	-189	26	2124	-31.26	-7.8	0.07
11	SLD 15	-248	-6	2089	10.82	-10.27	-0.02
11	SLD 16	-248	-6	2089	10.82	-10.27	-0.02
11	SLV 1	636	14	2280	-23.12	26.72	0.04
11	SLV 2	636	14	2280	-23.12	26.72	0.04
11	SLV 3	490	-70	2198	86.41	20.54	-0.18
11	SLV 4	490	-70	2198	86.41	20.54	-0.18
11	SLV 5	421	131	2309	-171.91	17.85	0.34
11	SLV 6	421	131	2309	-171.91	17.85	0.34
11	SLV 7	-65	-148	2039	193.19	-2.75	-0.38
11	SLV 8	-65	-148	2039	193.19	-2.75	-0.38
11	SLV 9	92	147	2254	-189.9	4.06	0.38
11	SLV 10	92	147	2254	-189.9	4.06	0.38
11	SLV 11	-395	-132	1983	175.19	-16.53	-0.34
11	SLV 12	-395	-132	1983	175.19	-16.53	-0.34
11	SLV 13	-463	68	2094	-83.12	-19.23	0.18
11	SLV 14	-463	68	2094	-83.12	-19.23	0.18
11	SLV 15	-609	-16	2013	26.41	-25.41	-0.04
11	SLV 16	-609	-16	2013	26.41	-25.41	-0.04
12	SLU 1	-11	0	2012	1	-0.34	0
12	SLU 2	-23	1	2019	-1.91	-0.85	0
12	SLU 3	-11	0	2012	1	-0.34	0
12	SLU 4	-18	0	2016	-0.75	-0.65	0
12	SLU 5	-23	1	2019	-1.91	-0.85	0
12	SLU 6	-11	0	2012	1	-0.34	0
12	SLU 7	-18	0	2016	-0.75	-0.65	0
12	SLU 8	-11	0	2012	1	-0.34	0
12	SLU 9	-18	0	2016	-0.75	-0.65	0
12	SLU 10	-37	0	2316	-0.46	-1.29	0
12	SLU 11	-25	-1	2310	2.45	-0.78	0
12	SLU 12	-32	0	2314	0.7	-1.09	0
12	SLU 13	-37	0	2316	-0.46	-1.29	0
12	SLU 14	-25	-1	2310	2.45	-0.78	0
12	SLU 15	-32	0	2314	0.7	-1.09	0
12	SLU 16	-25	-1	2310	2.45	-0.78	0
12	SLU 17	-32	0	2314	0.7	-1.09	0
12	SLU 18	-30	-1	2437	3.07	-0.97	0
12	SLU 19	-38	-1	2441	1.32	-1.28	0
12	SLU 20	-30	-1	2437	3.07	-0.97	0
12	SLU 21	-38	-1	2441	1.32	-1.28	0
12	SLU 22	-19	-1	2165	1.58	-0.61	0
12	SLU 23	-31	0	2172	-1.33	-1.12	0
12	SLU 24	-19	-1	2165	1.58	-0.61	0
12	SLU 25	-26	0	2169	-0.17	-0.92	0
12	SLU 26	-31	0	2172	-1.33	-1.12	0
12	SLU 27	-19	-1	2165	1.58	-0.61	0
12	SLU 28	-26	0	2169	-0.17	-0.92	0
12	SLU 29	-19	-1	2165	1.58	-0.61	0
12	SLU 30	-26	0	2169	-0.17	-0.92	0
12	SLU 31	-44	0	2470	0.12	-1.56	0
12	SLU 32	-32	-1	2463	3.03	-1.05	0
12	SLU 33	-40	-1	2467	1.28	-1.36	0
12	SLU 34	-44	0	2470	0.12	-1.56	0
12	SLU 35	-32	-1	2463	3.03	-1.05	0
12	SLU 36	-40	-1	2467	1.28	-1.36	0
12	SLU 37	-32	-1	2463	3.03	-1.05	0
12	SLU 38	-40	-1	2467	1.28	-1.36	0
12	SLU 39	-38	-2	2590	3.65	-1.24	0
12	SLU 40	-45	-1	2594	1.9	-1.54	0
12	SLU 41	-38	-2	2590	3.65	-1.24	0
12	SLU 42	-45	-1	2594	1.9	-1.54	0
12	SLU 43	-12	0	2563	1.1	-0.35	0
12	SLU 44	-24	1	2570	-1.81	-0.86	0
12	SLU 45	-12	0	2563	1.1	-0.35	0
12	SLU 46	-19	0	2567	-0.65	-0.66	0
12	SLU 47	-24	1	2570	-1.81	-0.86	0
12	SLU 48	-12	0	2563	1.1	-0.35	0
12	SLU 49	-19	0	2567	-0.65	-0.66	0
12	SLU 50	-12	0	2563	1.1	-0.35	0
12	SLU 51	-19	0	2567	-0.65	-0.66	0
12	SLU 52	-37	0	2867	-0.36	-1.3	0
12	SLU 53	-25	-1	2861	2.55	-0.79	0
12	SLU 54	-32	0	2865	0.8	-1.1	0
12	SLU 55	-37	0	2867	-0.36	-1.3	0
12	SLU 56	-25	-1	2861	2.55	-0.79	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
12	SLU 57	-32	0	2865	0.8	-1.1	0
12	SLU 58	-25	-1	2861	2.55	-0.79	0
12	SLU 59	-32	0	2865		-1.1	0
12	SLU 60	-31	-1	2988	3.17	-0.98	0
12	SLU 61	-38	-1	2992	1.42	-1.29	0
12	SLU 62	-31	-1	2988	3.17	-0.98	0
12	SLU 63	-38	-1	2992	1.42	-1.29	0
12	SLU 64	-20	-1	2716	1.68	-0.62	0
12	SLU 65	-32	0	2723	-1.23	-1.13	0
12	SLU 66	-20	-1	2716	1.68	-0.62	0
12	SLU 67	-27	0	2720	-0.07	-0.93	0
12	SLU 68	-32	0	2723	-1.23	-1.13	0
12	SLU 69	-20	-1	2716	1.68	-0.62	0
12	SLU 70	-27	0	2720	-0.07	-0.93	0
12	SLU 71	-20	-1	2716	1.68	-0.62	0
12	SLU 72	-27	0	2720	-0.07	-0.93	0
12	SLU 73	-45	0	3021	0.22	-1.57	0
12	SLU 74	-33	-1	3014	3.13	-1.06	0
12	SLU 75	-40	-1	3018	1.38	-1.37	0
12	SLU 76	-45	0	3021	0.22	-1.57	0
12	SLU 77	-33	-1	3014	3.13	-1.06	0
12	SLU 78	-40	-1	3018	1.38	-1.37	0
12	SLU 79	-33	-1	3014	3.13	-1.06	0
12	SLU 80	-40	-1	3018	1.38	-1.37	0
12	SLU 81	-39	-2	3142	3.75	-1.25	0
12	SLU 82	-46	-1	3146	2	-1.55	0
12	SLU 83	-39	-2	3142	3.75	-1.25	0
12	SLU 84	-46	-1	3146	2	-1.55	0
12	SLE RA 1	-13	-1	2056	1.16	-0.42	0
12	SLE RA 2	-21	0	2060	-0.78	-0.76	0
12	SLE RA 3	-13	-1	2056	1.16	-0.42	0
12	SLE RA 4	-18	0	2058	0	-0.62	0
12	SLE RA 5	-21	0	2060	-0.78	-0.76	0
12	SLE RA 6	-13	-1	2056	1.16	-0.42	0
12	SLE RA 7	-18	0	2058	0	-0.62	0
12	SLE RA 8	-13	-1	2056	1.16	-0.42	0
12	SLE RA 9	-18	0	2058	0	-0.62	0
12	SLE RA 10	-30	0	2259	0.19	-1.05	0
12	SLE RA 11	-22	-1	2254	2.13	-0.71	0
12	SLE RA 12	-27	0	2257	0.97	-0.92	0
12	SLE RA 13	-30	0	2259	0.19	-1.05	0
12	SLE RA 14	-22	-1	2254	2.13	-0.71	0
12	SLE RA 15	-27	0	2257	0.97	-0.92	0
12	SLE RA 16	-22	-1	2254	2.13	-0.71	0
12	SLE RA 17	-27	0	2257	0.97	-0.92	0
12	SLE RA 18	-26	-1	2339	2.54	-0.84	0
12	SLE RA 19	-31	-1	2342	1.38	-1.04	0
12	SLE RA 20	-26	-1	2339	2.54	-0.84	0
12	SLE RA 21	-31	-1	2342	1.38	-1.04	0
12	SLE FR 1	-13	-1	2056	1.16	-0.42	0
12	SLE FR 2	-15	0	2057	0.78	-0.49	0
12	SLE FR 3	-13	-1	2056	1.16	-0.42	0
12	SLE FR 4	-19	-1	2142	1.19	-0.61	0
12	SLE FR 5	-17	-1	2141	1.58	-0.55	0
12	SLE FR 6	-20	-1	2198	1.85	-0.63	0
12	SLE QP 1	-13	-1	2056	1.16	-0.42	0
12	SLE QP 2	-17	-1	2141	1.58	-0.55	0
12	SLD 1	245	26	2111	-7.13	10.44	0.05
12	SLD 2	245	26	2111	-7.13	10.44	0.05
12	SLD 3	188	-5	2063	33.65	8.05	-0.01
12	SLD 4	188	-5	2063	33.65	8.05	-0.01
12	SLD 5	148	54	2205	-62.88	6.38	0.1
12	SLD 6	148	54	2205	-62.88	6.38	0.1
12	SLD 7	-42	-49	2044	73.05	-1.6	-0.09
12	SLD 8	-42	-49	2044	73.05	-1.6	-0.09
12	SLD 9	7	48	2238	-69.89	0.51	0.08
12	SLD 10	7	48	2238	-69.89	0.51	0.08
12	SLD 11	-182	-56	2077	66.04	-7.47	-0.1
12	SLD 12	-182	-56	2077	66.04	-7.47	-0.1
12	SLD 13	-223	4	2219	-30.49	-9.14	0
12	SLD 14	-223	4	2219	-30.49	-9.14	0
12	SLD 15	-279	-27	2171	10.29	-11.53	-0.05
12	SLD 16	-279	-27	2171	10.29	-11.53	-0.05
12	SLV 1	609	66	2069	-21.81	25.68	0.12
12	SLV 2	609	66	2069	-21.81	25.68	0.12
12	SLV 3	467	-13	1959	84.32	19.68	-0.02
12	SLV 4	467	-13	1959	84.32	19.68	-0.02
12	SLV 5	386	140	2287	-166.4	16.42	0.25
12	SLV 6	386	140	2287	-166.4	16.42	0.25
12	SLV 7	-88	-126	1918	187.36	-3.57	-0.22
12	SLV 8	-88	-126	1918	187.36	-3.57	-0.22
12	SLV 9	53	124	2363	-184.21	2.48	0.22
12	SLV 10	53	124	2363	-184.21	2.48	0.22
12	SLV 11	-421	-142	1994	169.56	-17.51	-0.25
12	SLV 12	-421	-142	1994	169.56	-17.51	-0.25
12	SLV 13	-501	12	2323	-81.16	-20.77	0.02
12	SLV 14	-501	12	2323	-81.16	-20.77	0.02
12	SLV 15	-643	-68	2212	24.97	-26.77	-0.12



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
12	SLV 16	-643	-68	2212	24.97	-26.77	-0.12
13	SLU 1	-36	0	1991	0.93	-1.41	0
13	SLU 2	-48	0	1998	-1.43	-1.9	0
13	SLU 3	-36	0	1991	0.93	-1.41	0
13	SLU 4	-43	0	1995	-0.48	-1.7	0
13	SLU 5	-48	0	1998	-1.43	-1.9	0
13	SLU 6	-36	0	1991	0.93	-1.41	0
13	SLU 7	-43	0	1995	-0.48	-1.7	0
13	SLU 8	-36	0	1991	0.93	-1.41	0
13	SLU 9	-43	0	1995	-0.48	-1.7	0
13	SLU 10	-71	0	2274	-0.11	-2.76	0
13	SLU 11	-60	-1	2266	2.26	-2.27	0
13	SLU 12	-67	0	2270	0.84	-2.57	0
13	SLU 13	-71	0	2274	-0.11	-2.76	0
13	SLU 14	-60	-1	2266	2.26	-2.27	0
13	SLU 15	-67	0	2270	0.84	-2.57	0
13	SLU 16	-60	-1	2266	2.26	-2.27	0
13	SLU 17	-67	0	2270	0.84	-2.57	0
13	SLU 18	-70	-1	2384	2.82	-2.64	0
13	SLU 19	-77	-1	2388	1.41	-2.94	0
13	SLU 20	-70	-1	2384	2.82	-2.64	0
13	SLU 21	-77	-1	2388	1.41	-2.94	0
13	SLU 22	-48	-1	2134	1.47	-1.86	0
13	SLU 23	-60	0	2141	-0.9	-2.34	0
13	SLU 24	-48	-1	2134	1.47	-1.86	0
13	SLU 25	-55	0	2138	0.05	-2.15	0
13	SLU 26	-60	0	2141	-0.9	-2.34	0
13	SLU 27	-48	-1	2134	1.47	-1.86	0
13	SLU 28	-55	0	2138	0.05	-2.15	0
13	SLU 29	-48	-1	2134	1.47	-1.86	0
13	SLU 30	-55	0	2138	0.05	-2.15	0
13	SLU 31	-83	0	2417	0.43	-3.21	0
13	SLU 32	-72	-1	2409	2.79	-2.72	0
13	SLU 33	-79	-1	2413	1.37	-3.01	0
13	SLU 34	-83	0	2417	0.43	-3.21	0
13	SLU 35	-72	-1	2409	2.79	-2.72	0
13	SLU 36	-79	-1	2413	1.37	-3.01	0
13	SLU 37	-72	-1	2409	2.79	-2.72	0
13	SLU 38	-79	-1	2413	1.37	-3.01	0
13	SLU 39	-82	-1	2527	3.36	-3.09	0
13	SLU 40	-88	-1	2531	1.94	-3.38	0
13	SLU 41	-82	-1	2527	3.36	-3.09	0
13	SLU 42	-88	-1	2531	1.94	-3.38	0
13	SLU 43	-43	0	2539	1.03	-1.68	0
13	SLU 44	-55	0	2546	-1.33	-2.17	0
13	SLU 45	-43	0	2539	1.03	-1.68	0
13	SLU 46	-50	0	2543	-0.39	-1.97	0
13	SLU 47	-55	0	2546	-1.33	-2.17	0
13	SLU 48	-43	0	2539	1.03	-1.68	0
13	SLU 49	-50	0	2543	-0.39	-1.97	0
13	SLU 50	-43	0	2539	1.03	-1.68	0
13	SLU 51	-50	0	2543	-0.39	-1.97	0
13	SLU 52	-78	0	2822	-0.01	-3.03	0
13	SLU 53	-66	-1	2814	2.35	-2.54	0
13	SLU 54	-73	-1	2819	0.94	-2.83	0
13	SLU 55	-78	0	2822	-0.01	-3.03	0
13	SLU 56	-66	-1	2814	2.35	-2.54	0
13	SLU 57	-73	-1	2819	0.94	-2.83	0
13	SLU 58	-66	-1	2814	2.35	-2.54	0
13	SLU 59	-73	-1	2819	0.94	-2.83	0
13	SLU 60	-76	-1	2932	2.92	-2.91	0
13	SLU 61	-83	-1	2937	1.5	-3.2	0
13	SLU 62	-76	-1	2932	2.92	-2.91	0
13	SLU 63	-83	-1	2937	1.5	-3.2	0
13	SLU 64	-55	-1	2682	1.56	-2.13	0
13	SLU 65	-67	0	2689	-0.8	-2.61	0
13	SLU 66	-55	-1	2682	1.56	-2.13	0
13	SLU 67	-62	0	2686	0.15	-2.42	0
13	SLU 68	-67	0	2689	-0.8	-2.61	0
13	SLU 69	-55	-1	2682	1.56	-2.13	0
13	SLU 70	-62	0	2686	0.15	-2.42	0
13	SLU 71	-55	-1	2682	1.56	-2.13	0
13	SLU 72	-62	0	2686	0.15	-2.42	0
13	SLU 73	-90	0	2965	0.52	-3.48	0
13	SLU 74	-78	-1	2957	2.89	-2.99	0
13	SLU 75	-85	-1	2962	1.47	-3.28	0
13	SLU 76	-90	0	2965	0.52	-3.48	0
13	SLU 77	-78	-1	2957	2.89	-2.99	0
13	SLU 78	-85	-1	2962	1.47	-3.28	0
13	SLU 79	-78	-1	2957	2.89	-2.99	0
13	SLU 80	-85	-1	2962	1.47	-3.28	0
13	SLU 81	-88	-1	3075	3.45	-3.36	0
13	SLU 82	-95	-1	3079	2.04	-3.65	0
13	SLU 83	-88	-1	3075	3.45	-3.36	0
13	SLU 84	-95	-1	3079	2.04	-3.65	0
13	SLE RA 1	-40	0	2031	1.09	-1.54	0
13	SLE RA 2	-48	0	2037	-0.49	-1.86	0
13	SLE RA 3	-40	0	2031	1.09	-1.54	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione			
		x	y	z		x	y	z	
13	SLE RA 4	-44	0	2035		0.14	-1.73	0	
13	SLE RA 5	-48	0	2037		-0.49	-1.86	0	
13	SLE RA 6	-40	0	2031		1.09	-1.54	0	
13	SLE RA 7	-44	0	2035		0.14	-1.73	0	
13	SLE RA 8	-40	0	2031		1.09	-1.54	0	
13	SLE RA 9	-44	0	2035		0.14	-1.73	0	
13	SLE RA 10	-63	0	2220		0.39	-2.44	0	
13	SLE RA 11	-55	-1	2215		1.97	-2.11	0	
13	SLE RA 12	-60	-1	2218		1.02	-2.31	0	
13	SLE RA 13	-63	0	2220		0.39	-2.44	0	
13	SLE RA 14	-55	-1	2215		1.97	-2.11	0	
13	SLE RA 15	-60	-1	2218		1.02	-2.31	0	
13	SLE RA 16	-55	-1	2215		1.97	-2.11	0	
13	SLE RA 17	-60	-1	2218		1.02	-2.31	0	
13	SLE RA 18	-62	-1	2294		2.35	-2.36	0	
13	SLE RA 19	-67	-1	2297		1.4	-2.56	0	
13	SLE RA 20	-62	-1	2294		2.35	-2.36	0	
13	SLE RA 21	-67	-1	2297		1.4	-2.56	0	
13	SLE FR 1	-40	0	2031		1.09	-1.54	0	
13	SLE FR 2	-41	0	2032		0.77	-1.6	0	
13	SLE FR 3	-40	0	2031		1.09	-1.54	0	
13	SLE FR 4	-48	-1	2111		1.15	-1.85	0	
13	SLE FR 5	-46	-1	2110		1.46	-1.78	0	
13	SLE FR 6	-51	-1	2162		1.72	-1.95	0	
13	SLE QP 1	-40	0	2031		1.09	-1.54	0	
13	SLE QP 2	-46	-1	2110		1.46	-1.78	0	
13	SLD 1	215	24	2066		-28.65	9.12	0.03	
13	SLD 2	215	24	2066		-28.65	9.12	0.03	
13	SLD 3	161	-3	1999		8.66	6.79	0	
13	SLD 4	161	-3	1999		8.66	6.79	0	
13	SLD 5	114	49	2198		-64.17	5.01	0.06	
13	SLD 6	114	49	2198		-64.17	5.01	0.06	
13	SLD 7	-67	-43	1975		60.22	-2.74	-0.06	
13	SLD 8	-67	-43	1975		60.22	-2.74	-0.06	
13	SLD 9	-26	42	2245		-57.3	-0.83	0.05	
13	SLD 10	-26	42	2245		-57.3	-0.83	0.05	
13	SLD 11	-207	-50	2022		67.1	-8.58	-0.07	
13	SLD 12	-207	-50	2022		67.1	-8.58	-0.07	
13	SLD 13	-253	2	2221		-5.74	-10.36	0	
13	SLD 14	-253	2	2221		-5.74	-10.36	0	
13	SLD 15	-308	-26	2154		31.58	-12.69	-0.03	
13	SLD 16	-308	-26	2154		31.58	-12.69	-0.03	
13	SLV 1	578	63	2005		-76.15	24.24	0.08	
13	SLV 2	578	63	2005		-76.15	24.24	0.08	
13	SLV 3	441	-8	1851		20.93	18.4	-0.01	
13	SLV 4	441	-8	1851		20.93	18.4	-0.01	
13	SLV 5	348	126	2312		-169.06	14.88	0.16	
13	SLV 6	348	126	2312		-169.06	14.88	0.16	
13	SLV 7	-107	-111	1799		154.54	-4.59	-0.14	
13	SLV 8	-107	-111	1799		154.54	-4.59	-0.14	
13	SLV 9	14	109	2421		-151.62	1.02	0.14	
13	SLV 10	14	109	2421		-151.62	1.02	0.14	
13	SLV 11	-441	-127	1908		171.99	-18.45	-0.17	
13	SLV 12	-441	-127	1908		171.99	-18.45	-0.17	
13	SLV 13	-534	7	2369		-18	-21.97	0.01	
13	SLV 14	-534	7	2369		-18	-21.97	0.01	
13	SLV 15	-670	-64	2215		79.08	-27.81	-0.09	
13	SLV 16	-670	-64	2215		79.08	-27.81	-0.09	
14	SLU 1	-60	0	1967		0.85	-2.36	0	
14	SLU 2	-71	0	1976		-0.97	-2.83	0	
14	SLU 3	-60	0	1967		0.85	-2.36	0	
14	SLU 4	-67	0	1973		-0.24	-2.64	0	
14	SLU 5	-71	0	1976		-0.97	-2.83	0	
14	SLU 6	-60	0	1967		0.85	-2.36	0	
14	SLU 7	-67	0	1973		-0.24	-2.64	0	
14	SLU 8	-60	0	1967		0.85	-2.36	0	
14	SLU 9	-67	0	1973		-0.24	-2.64	0	
14	SLU 10	-102	0	2227		0.2	-3.99	0	
14	SLU 11	-91	-1	2218		2.02	-3.51	0	
14	SLU 12	-98	-1	2223		0.93	-3.8	0	
14	SLU 13	-102	0	2227		0.2	-3.99	0	
14	SLU 14	-91	-1	2218		2.02	-3.51	0	
14	SLU 15	-98	-1	2223		0.93	-3.8	0	
14	SLU 16	-91	-1	2218		2.02	-3.51	0	
14	SLU 17	-98	-1	2223		0.93	-3.8	0	
14	SLU 18	-104	-1	2325		2.53	-4.01	0	
14	SLU 19	-111	-1	2331		1.43	-4.29	0	
14	SLU 20	-104	-1	2325		2.53	-4.01	0	
14	SLU 21	-111	-1	2331		1.43	-4.29	0	
14	SLU 22	-75	-1	2099		1.32	-2.92	0	
14	SLU 23	-86	0	2108		-0.5	-3.4	0	
14	SLU 24	-75	-1	2099		1.32	-2.92	0	
14	SLU 25	-82	0	2105		0.23	-3.21	0	
14	SLU 26	-86	0	2108		-0.5	-3.4	0	
14	SLU 27	-75	-1	2099		1.32	-2.92	0	
14	SLU 28	-82	0	2105		0.23	-3.21	0	
14	SLU 29	-75	-1	2099		1.32	-2.92	0	
14	SLU 30	-82	0	2105		0.23	-3.21	0	



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
14	SLU 31	-117	-1	2359	0.68	-4.55	0
14	SLU 32	-106	-1	2350	2.5	-4.08	0
14	SLU 33	-113	-1	2355	1.41	-4.36	0
14	SLU 34	-117	-1	2359	0.68	-4.55	0
14	SLU 35	-106	-1	2350	2.5	-4.08	0
14	SLU 36	-113	-1	2355	1.41	-4.36	0
14	SLU 37	-106	-1	2350	2.5	-4.08	0
14	SLU 38	-113	-1	2355	1.41	-4.36	0
14	SLU 39	-119	-1	2457	3	-4.57	0
14	SLU 40	-126	-1	2462	1.91	-4.86	0
14	SLU 41	-119	-1	2457	3	-4.57	0
14	SLU 42	-126	-1	2462	1.91	-4.86	0
14	SLU 43	-73	0	2512	0.94	-2.87	0
14	SLU 44	-84	0	2521	-0.88	-3.34	0
14	SLU 45	-73	0	2512	0.94	-2.87	0
14	SLU 46	-79	0	2518	-0.15	-3.15	0
14	SLU 47	-84	0	2521	-0.88	-3.34	0
14	SLU 48	-73	0	2512	0.94	-2.87	0
14	SLU 49	-79	0	2518	-0.15	-3.15	0
14	SLU 50	-73	0	2512	0.94	-2.87	0
14	SLU 51	-79	0	2518	-0.15	-3.15	0
14	SLU 52	-115	0	2772	0.3	-4.5	0
14	SLU 53	-104	-1	2763	2.12	-4.02	0
14	SLU 54	-111	-1	2768	1.03	-4.31	0
14	SLU 55	-115	0	2772	0.3	-4.5	0
14	SLU 56	-104	-1	2763	2.12	-4.02	0
14	SLU 57	-111	-1	2768	1.03	-4.31	0
14	SLU 58	-104	-1	2763	2.12	-4.02	0
14	SLU 59	-111	-1	2768	1.03	-4.31	0
14	SLU 60	-117	-1	2870	2.62	-4.52	0
14	SLU 61	-124	-1	2875	1.53	-4.81	0
14	SLU 62	-117	-1	2870	2.62	-4.52	0
14	SLU 63	-124	-1	2875	1.53	-4.81	0
14	SLU 64	-88	-1	2644	1.42	-3.43	0
14	SLU 65	-99	0	2653	-0.4	-3.91	0
14	SLU 66	-88	-1	2644	1.42	-3.43	0
14	SLU 67	-95	0	2649	0.33	-3.72	0
14	SLU 68	-99	0	2653	-0.4	-3.91	0
14	SLU 69	-88	-1	2644	1.42	-3.43	0
14	SLU 70	-95	0	2649	0.33	-3.72	0
14	SLU 71	-88	-1	2644	1.42	-3.43	0
14	SLU 72	-95	0	2649	0.33	-3.72	0
14	SLU 73	-130	-1	2904	0.77	-5.07	0
14	SLU 74	-119	-1	2895	2.59	-4.59	0
14	SLU 75	-126	-1	2900	1.5	-4.88	0
14	SLU 76	-130	-1	2904	0.77	-5.07	0
14	SLU 77	-119	-1	2895	2.59	-4.59	0
14	SLU 78	-126	-1	2900	1.5	-4.88	0
14	SLU 79	-119	-1	2895	2.59	-4.59	0
14	SLU 80	-126	-1	2900	1.5	-4.88	0
14	SLU 81	-132	-1	3002	3.09	-5.09	0
14	SLU 82	-139	-1	3007	2	-5.37	0
14	SLU 83	-132	-1	3002	3.09	-5.09	0
14	SLU 84	-139	-1	3007	2	-5.37	0
14	SLE RA 1	-64	0	2005	0.99	-2.52	0
14	SLE RA 2	-72	0	2011	-0.23	-2.83	0
14	SLE RA 3	-64	0	2005	0.99	-2.52	0
14	SLE RA 4	-69	0	2009	0.26	-2.71	0
14	SLE RA 5	-72	0	2011	-0.23	-2.83	0
14	SLE RA 6	-64	0	2005	0.99	-2.52	0
14	SLE RA 7	-69	0	2009	0.26	-2.71	0
14	SLE RA 8	-64	0	2005	0.99	-2.52	0
14	SLE RA 9	-69	0	2009	0.26	-2.71	0
14	SLE RA 10	-92	0	2178	0.55	-3.61	0
14	SLE RA 11	-85	-1	2172	1.77	-3.29	0
14	SLE RA 12	-89	-1	2176	1.04	-3.48	0
14	SLE RA 13	-92	0	2178	0.55	-3.61	0
14	SLE RA 14	-85	-1	2172	1.77	-3.29	0
14	SLE RA 15	-89	-1	2176	1.04	-3.48	0
14	SLE RA 16	-85	-1	2172	1.77	-3.29	0
14	SLE RA 17	-89	-1	2176	1.04	-3.48	0
14	SLE RA 18	-94	-1	2244	2.1	-3.62	0
14	SLE RA 19	-98	-1	2247	1.38	-3.81	0
14	SLE RA 20	-94	-1	2244	2.1	-3.62	0
14	SLE RA 21	-98	-1	2247	1.38	-3.81	0
14	SLE FR 1	-64	0	2005	0.99	-2.52	0
14	SLE FR 2	-66	0	2006	0.74	-2.58	0
14	SLE FR 3	-64	0	2005	0.99	-2.52	0
14	SLE FR 4	-75	0	2078	1.08	-2.91	0
14	SLE FR 5	-73	-1	2076	1.32	-2.85	0
14	SLE FR 6	-79	-1	2124	1.55	-3.07	0
14	SLE QP 1	-64	0	2005	0.99	-2.52	0
14	SLE QP 2	-73	-1	2076	1.32	-2.85	0
14	SLD 1	187	22	2014	-25.92	8.01	0.02
14	SLD 2	187	22	2014	-25.92	8.01	0.02
14	SLD 3	135	-1	1923	6.49	5.8	0
14	SLD 4	135	-1	1923	6.49	5.8	0
14	SLD 5	84	41	2196	-56	3.76	0.04



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
14	SLD 6	84	41	2196	-56	3.76	0.04
14	SLD 7	-90	-36	1893	52.02	-3.6	-0.04
14	SLD 8	-90	-36	1893	52.02	-3.6	-0.04
14	SLD 9	-56	35	2260	-49.38	-2.09	0.03
14	SLD 10	-56	35	2260	-49.38	-2.09	0.03
14	SLD 11	-230	-42	1957	58.65	-9.45	-0.04
14	SLD 12	-230	-42	1957	58.65	-9.45	-0.04
14	SLD 13	-281	0	2230	-3.84	-11.5	0
14	SLD 14	-281	0	2230	-3.84	-11.5	0
14	SLD 15	-333	-23	2139	28.57	-13.7	-0.02
14	SLD 16	-333	-23	2139	28.57	-13.7	-0.02
14	SLV 1	548	57	1927	-68.65	23.08	0.06
14	SLV 2	548	57	1927	-68.65	23.08	0.06
14	SLV 3	417	-2	1718	15.56	17.54	0
14	SLV 4	417	-2	1718	15.56	17.54	0
14	SLV 5	312	106	2350	-147.4	13.34	0.11
14	SLV 6	312	106	2350	-147.4	13.34	0.11
14	SLV 7	-125	-91	1651	133.32	-5.14	-0.09
14	SLV 8	-125	-91	1651	133.32	-5.14	-0.09
14	SLV 9	-21	90	2502	-130.67	-0.56	0.09
14	SLV 10	-21	90	2502	-130.67	-0.56	0.09
14	SLV 11	-458	-107	1803	150.04	-19.04	-0.11
14	SLV 12	-458	-107	1803	150.04	-19.04	-0.11
14	SLV 13	-563	1	2435	-12.92	-23.23	0
14	SLV 14	-563	1	2435	-12.92	-23.23	0
14	SLV 15	-694	-58	2226	71.3	-28.78	-0.06
14	SLV 16	-694	-58	2226	71.3	-28.78	-0.06
15	SLU 1	-84	0	1942	0.75	-3.35	0
15	SLU 2	-95	0	1953	-0.55	-3.81	0
15	SLU 3	-84	0	1942	0.75	-3.35	0
15	SLU 4	-90	0	1949	-0.03	-3.62	0
15	SLU 5	-95	0	1953	-0.55	-3.81	0
15	SLU 6	-84	0	1942	0.75	-3.35	0
15	SLU 7	-90	0	1949	-0.03	-3.62	0
15	SLU 8	-84	0	1942	0.75	-3.35	0
15	SLU 9	-90	0	1949	-0.03	-3.62	0
15	SLU 10	-132	-1	2177	0.44	-5.24	0
15	SLU 11	-121	-1	2167	1.75	-4.78	0
15	SLU 12	-128	-1	2173	0.97	-5.06	0
15	SLU 13	-132	-1	2177	0.44	-5.24	0
15	SLU 14	-121	-1	2167	1.75	-4.78	0
15	SLU 15	-128	-1	2173	0.97	-5.06	0
15	SLU 16	-121	-1	2167	1.75	-4.78	0
15	SLU 17	-128	-1	2173	0.97	-5.06	0
15	SLU 18	-138	-1	2263	2.18	-5.4	0
15	SLU 19	-144	-1	2269	1.39	-5.67	0
15	SLU 20	-138	-1	2263	2.18	-5.4	0
15	SLU 21	-144	-1	2269	1.39	-5.67	0
15	SLU 22	-101	0	2063	1.16	-4.03	0
15	SLU 23	-112	0	2073	-0.15	-4.48	0
15	SLU 24	-101	0	2063	1.16	-4.03	0
15	SLU 25	-108	0	2069	0.37	-4.3	0
15	SLU 26	-112	0	2073	-0.15	-4.48	0
15	SLU 27	-101	0	2063	1.16	-4.03	0
15	SLU 28	-108	0	2069	0.37	-4.3	0
15	SLU 29	-101	0	2063	1.16	-4.03	0
15	SLU 30	-108	0	2069	0.37	-4.3	0
15	SLU 31	-150	-1	2298	0.85	-5.91	0
15	SLU 32	-139	-1	2288	2.15	-5.46	0
15	SLU 33	-146	-1	2294	1.37	-5.73	0
15	SLU 34	-150	-1	2298	0.85	-5.91	0
15	SLU 35	-139	-1	2288	2.15	-5.46	0
15	SLU 36	-146	-1	2294	1.37	-5.73	0
15	SLU 37	-139	-1	2288	2.15	-5.46	0
15	SLU 38	-146	-1	2294	1.37	-5.73	0
15	SLU 39	-155	-1	2384	2.58	-6.07	0
15	SLU 40	-162	-1	2390	1.8	-6.35	0
15	SLU 41	-155	-1	2384	2.58	-6.07	0
15	SLU 42	-162	-1	2390	1.8	-6.35	0
15	SLU 43	-103	0	2484	0.84	-4.12	0
15	SLU 44	-114	0	2494	-0.47	-4.58	0
15	SLU 45	-103	0	2484	0.84	-4.12	0
15	SLU 46	-109	0	2490	0.06	-4.4	0
15	SLU 47	-114	0	2494	-0.47	-4.58	0
15	SLU 48	-103	0	2484	0.84	-4.12	0
15	SLU 49	-109	0	2490	0.06	-4.4	0
15	SLU 50	-103	0	2484	0.84	-4.12	0
15	SLU 51	-109	0	2490	0.06	-4.4	0
15	SLU 52	-151	-1	2719	0.53	-6.01	0
15	SLU 53	-140	-1	2708	1.84	-5.56	0
15	SLU 54	-147	-1	2715	1.05	-5.83	0
15	SLU 55	-151	-1	2719	0.53	-6.01	0
15	SLU 56	-140	-1	2708	1.84	-5.56	0
15	SLU 57	-147	-1	2715	1.05	-5.83	0
15	SLU 58	-140	-1	2708	1.84	-5.56	0
15	SLU 59	-147	-1	2715	1.05	-5.83	0
15	SLU 60	-157	-1	2805	2.26	-6.17	0
15	SLU 61	-163	-1	2811	1.48	-6.44	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
15	SLU 62	-157	-1	2805	2.26	-6.17	0
15	SLU 63	-163	-1	2811	1.48	-6.44	0
15	SLU 64	-120	-1	2605	1.25	-4.8	0
15	SLU 65	-131	0	2615	-0.06	-5.26	0
15	SLU 66	-120	-1	2605	1.25	-4.8	0
15	SLU 67	-127	-1	2611	0.46	-5.07	0
15	SLU 68	-131	0	2615	-0.06	-5.26	0
15	SLU 69	-120	-1	2605	1.25	-4.8	0
15	SLU 70	-127	-1	2611	0.46	-5.07	0
15	SLU 71	-120	-1	2605	1.25	-4.8	0
15	SLU 72	-127	-1	2611	0.46	-5.07	0
15	SLU 73	-169	-1	2839	0.93	-6.69	0
15	SLU 74	-158	-1	2829	2.24	-6.23	0
15	SLU 75	-165	-1	2835	1.46	-6.51	0
15	SLU 76	-169	-1	2839	0.93	-6.69	0
15	SLU 77	-158	-1	2829	2.24	-6.23	0
15	SLU 78	-165	-1	2835	1.46	-6.51	0
15	SLU 79	-158	-1	2829	2.24	-6.23	0
15	SLU 80	-165	-1	2835	1.46	-6.51	0
15	SLU 81	-174	-1	2925	2.67	-6.85	0
15	SLU 82	-181	-1	2931	1.88	-7.12	0
15	SLU 83	-174	-1	2925	2.67	-6.85	0
15	SLU 84	-181	-1	2931	1.88	-7.12	0
15	SLE RA 1	-89	0	1977	0.87	-3.54	0
15	SLE RA 2	-96	0	1984	0	-3.85	0
15	SLE RA 3	-89	0	1977	0.87	-3.54	0
15	SLE RA 4	-93	0	1981	0.35	-3.73	0
15	SLE RA 5	-96	0	1984	0	-3.85	0
15	SLE RA 6	-89	0	1977	0.87	-3.54	0
15	SLE RA 7	-93	0	1981	0.35	-3.73	0
15	SLE RA 8	-89	0	1977	0.87	-3.54	0
15	SLE RA 9	-93	0	1981	0.35	-3.73	0
15	SLE RA 10	-121	-1	2133	0.66	-4.8	0
15	SLE RA 11	-114	-1	2127	1.53	-4.5	0
15	SLE RA 12	-118	-1	2131	1.01	-4.68	0
15	SLE RA 13	-121	-1	2133	0.66	-4.8	0
15	SLE RA 14	-114	-1	2127	1.53	-4.5	0
15	SLE RA 15	-118	-1	2131	1.01	-4.68	0
15	SLE RA 16	-114	-1	2127	1.53	-4.5	0
15	SLE RA 17	-118	-1	2131	1.01	-4.68	0
15	SLE RA 18	-125	-1	2191	1.82	-4.91	0
15	SLE RA 19	-129	-1	2195	1.29	-5.09	0
15	SLE RA 20	-125	-1	2191	1.82	-4.91	0
15	SLE RA 21	-129	-1	2195	1.29	-5.09	0
15	SLE FR 1	-89	0	1977	0.87	-3.54	0
15	SLE FR 2	-90	0	1978	0.7	-3.6	0
15	SLE FR 3	-89	0	1977	0.87	-3.54	0
15	SLE FR 4	-101	0	2042	0.98	-4.01	0
15	SLE FR 5	-99	0	2041	1.15	-3.95	0
15	SLE FR 6	-107	-1	2084	1.34	-4.23	0
15	SLE QP 1	-89	0	1977	0.87	-3.54	0
15	SLE QP 2	-99	0	2041	1.15	-3.95	0
15	SLD 1	159	19	1956	-22.27	6.81	0.02
15	SLD 2	159	19	1956	-22.27	6.81	0.02
15	SLD 3	109	1	1835	4.13	4.68	0
15	SLD 4	109	1	1835	4.13	4.68	0
15	SLD 5	54	32	2199	-45.91	2.51	0.03
15	SLD 6	54	32	2199	-45.91	2.51	0.03
15	SLD 7	-113	-27	1796	42.09	-4.59	-0.02
15	SLD 8	-113	-27	1796	42.09	-4.59	-0.02
15	SLD 9	-86	26	2286	-39.78	-3.31	0.02
15	SLD 10	-86	26	2286	-39.78	-3.31	0.02
15	SLD 11	-253	-33	1883	48.22	-10.41	-0.03
15	SLD 12	-253	-33	1883	48.22	-10.41	-0.03
15	SLD 13	-308	-2	2247	-1.82	-12.59	0
15	SLD 14	-308	-2	2247	-1.82	-12.59	0
15	SLD 15	-358	-20	2126	24.58	-14.72	-0.02
15	SLD 16	-358	-20	2126	24.58	-14.72	-0.02
15	SLV 1	518	48	1839	-58.74	21.75	0.04
15	SLV 2	518	48	1839	-58.74	21.75	0.04
15	SLV 3	392	4	1559	9.72	16.39	0.01
15	SLV 4	392	4	1559	9.72	16.39	0.01
15	SLV 5	276	82	2405	-120.64	11.88	0.06
15	SLV 6	276	82	2405	-120.64	11.88	0.06
15	SLV 7	-143	-67	1472	107.55	-5.97	-0.05
15	SLV 8	-143	-67	1472	107.55	-5.97	-0.05
15	SLV 9	-56	66	2610	-105.24	-1.94	0.05
15	SLV 10	-56	66	2610	-105.24	-1.94	0.05
15	SLV 11	-475	-83	1678	122.95	-19.78	-0.07
15	SLV 12	-475	-83	1678	122.95	-19.78	-0.07
15	SLV 13	-591	-5	2523	-7.41	-24.3	-0.01
15	SLV 14	-591	-5	2523	-7.41	-24.3	-0.01
15	SLV 15	-717	-49	2244	61.05	-29.65	-0.04
15	SLV 16	-717	-49	2244	61.05	-29.65	-0.04
16	SLU 1	-107	0	1916	0.64	-4.33	0
16	SLU 2	-118	-1	1928	-0.2	-4.77	0
16	SLU 3	-107	0	1916	0.64	-4.33	0
16	SLU 4	-114	0	1924	0.13	-4.59	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
16	SLU 5	-118	-1	1928	-0.2	-4.77	0
16	SLU 6	-107	0	1916	0.64	-4.33	0
16	SLU 7	-114	0	1924	0.13	-4.59	0
16	SLU 8	-107	0	1916	0.64	-4.33	0
16	SLU 9	-114	0	1924	0.13	-4.59	0
16	SLU 10	-160	-1	2125	0.59	-6.41	0
16	SLU 11	-150	-1	2114	1.43	-5.97	0
16	SLU 12	-156	-1	2121	0.92	-6.24	0
16	SLU 13	-160	-1	2125	0.59	-6.41	0
16	SLU 14	-150	-1	2114	1.43	-5.97	0
16	SLU 15	-156	-1	2121	0.92	-6.24	0
16	SLU 16	-150	-1	2114	1.43	-5.97	0
16	SLU 17	-156	-1	2121	0.92	-6.24	0
16	SLU 18	-168	-1	2198	1.77	-6.68	0
16	SLU 19	-174	-1	2205	1.26	-6.94	0
16	SLU 20	-168	-1	2198	1.77	-6.68	0
16	SLU 21	-174	-1	2205	1.26	-6.94	0
16	SLU 22	-127	0	2026	0.96	-5.08	0
16	SLU 23	-137	-1	2037	0.12	-5.53	0
16	SLU 24	-127	0	2026	0.96	-5.08	0
16	SLU 25	-133	-1	2033	0.46	-5.35	0
16	SLU 26	-137	-1	2037	0.12	-5.53	0
16	SLU 27	-127	0	2026	0.96	-5.08	0
16	SLU 28	-133	-1	2033	0.46	-5.35	0
16	SLU 29	-127	0	2026	0.96	-5.08	0
16	SLU 30	-133	-1	2033	0.46	-5.35	0
16	SLU 31	-180	-1	2235	0.91	-7.17	0
16	SLU 32	-169	-1	2223	1.75	-6.73	0
16	SLU 33	-175	-1	2230	1.24	-6.99	0
16	SLU 34	-180	-1	2235	0.91	-7.17	0
16	SLU 35	-169	-1	2223	1.75	-6.73	0
16	SLU 36	-175	-1	2230	1.24	-6.99	0
16	SLU 37	-169	-1	2223	1.75	-6.73	0
16	SLU 38	-175	-1	2230	1.24	-6.99	0
16	SLU 39	-187	-1	2307	2.09	-7.43	0
16	SLU 40	-193	-1	2315	1.58	-7.7	0
16	SLU 41	-187	-1	2307	2.09	-7.43	0
16	SLU 42	-193	-1	2315	1.58	-7.7	0
16	SLU 43	-133	0	2454	0.72	-5.36	0
16	SLU 44	-143	-1	2466	-0.12	-5.81	0
16	SLU 45	-133	0	2454	0.72	-5.36	0
16	SLU 46	-139	-1	2461	0.21	-5.63	0
16	SLU 47	-143	-1	2466	-0.12	-5.81	0
16	SLU 48	-133	0	2454	0.72	-5.36	0
16	SLU 49	-139	-1	2461	0.21	-5.63	0
16	SLU 50	-133	0	2454	0.72	-5.36	0
16	SLU 51	-139	-1	2461	0.21	-5.63	0
16	SLU 52	-186	-1	2663	0.67	-7.45	0
16	SLU 53	-175	-1	2651	1.51	-7.01	0
16	SLU 54	-181	-1	2658	1	-7.28	0
16	SLU 55	-186	-1	2663	0.67	-7.45	0
16	SLU 56	-175	-1	2651	1.51	-7.01	0
16	SLU 57	-181	-1	2658	1	-7.28	0
16	SLU 58	-175	-1	2651	1.51	-7.01	0
16	SLU 59	-181	-1	2658	1	-7.28	0
16	SLU 60	-193	-1	2736	1.85	-7.71	0
16	SLU 61	-200	-1	2743	1.34	-7.98	0
16	SLU 62	-193	-1	2736	1.85	-7.71	0
16	SLU 63	-200	-1	2743	1.34	-7.98	0
16	SLU 64	-152	0	2563	1.04	-6.12	0
16	SLU 65	-163	-1	2575	0.2	-6.56	0
16	SLU 66	-152	0	2563	1.04	-6.12	0
16	SLU 67	-158	-1	2570	0.54	-6.39	0
16	SLU 68	-163	-1	2575	0.2	-6.56	0
16	SLU 69	-152	0	2563	1.04	-6.12	0
16	SLU 70	-158	-1	2570	0.54	-6.39	0
16	SLU 71	-152	0	2563	1.04	-6.12	0
16	SLU 72	-158	-1	2570	0.54	-6.39	0
16	SLU 73	-205	-1	2772	0.99	-8.21	0
16	SLU 74	-195	-1	2760	1.83	-7.76	0
16	SLU 75	-201	-1	2767	1.33	-8.03	0
16	SLU 76	-205	-1	2772	0.99	-8.21	0
16	SLU 77	-195	-1	2760	1.83	-7.76	0
16	SLU 78	-201	-1	2767	1.33	-8.03	0
16	SLU 79	-195	-1	2760	1.83	-7.76	0
16	SLU 80	-201	-1	2767	1.33	-8.03	0
16	SLU 81	-213	-1	2845	2.17	-8.47	0
16	SLU 82	-219	-1	2852	1.66	-8.74	0
16	SLU 83	-213	-1	2845	2.17	-8.47	0
16	SLU 84	-219	-1	2852	1.66	-8.74	0
16	SLE RA 1	-113	0	1948	0.73	-4.54	0
16	SLE RA 2	-120	-1	1956	0.17	-4.84	0
16	SLE RA 3	-113	0	1948	0.73	-4.54	0
16	SLE RA 4	-117	0	1952	0.39	-4.72	0
16	SLE RA 5	-120	-1	1956	0.17	-4.84	0
16	SLE RA 6	-113	0	1948	0.73	-4.54	0
16	SLE RA 7	-117	0	1952	0.39	-4.72	0
16	SLE RA 8	-113	0	1948	0.73	-4.54	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
16	SLE RA 9	-117	0	1952	0.39	-4.72	0
16	SLE RA 10	-148	-1	2087	0.7	-5.93	0
16	SLE RA 11	-141	0	2079	1.26	-5.64	0
16	SLE RA 12	-145	-1	2084	0.92	-5.82	0
16	SLE RA 13	-148	-1	2087	0.7	-5.93	0
16	SLE RA 14	-141	0	2079	1.26	-5.64	0
16	SLE RA 15	-145	-1	2084	0.92	-5.82	0
16	SLE RA 16	-141	0	2079	1.26	-5.64	0
16	SLE RA 17	-145	-1	2084	0.92	-5.82	0
16	SLE RA 18	-153	-1	2136	1.48	-6.11	0
16	SLE RA 19	-157	-1	2140	1.15	-6.29	0
16	SLE RA 20	-153	-1	2136	1.48	-6.11	0
16	SLE RA 21	-157	-1	2140	1.15	-6.29	0
16	SLE FR 1	-113	0	1948	0.73	-4.54	0
16	SLE FR 2	-114	0	1949	0.62	-4.6	0
16	SLE FR 3	-113	0	1948	0.73	-4.54	0
16	SLE FR 4	-126	0	2006	0.84	-5.07	0
16	SLE FR 5	-125	0	2004	0.96	-5.01	0
16	SLE FR 6	-133	0	2042	1.11	-5.32	0
16	SLE QP 1	-113	0	1948	0.73	-4.54	0
16	SLE QP 2	-125	0	2004	0.96	-5.01	0
16	SLD 1	134	15	1892	-17.92	5.79	0.01
16	SLD 2	134	15	1892	-17.92	5.79	0.01
16	SLD 3	85	4	1734	1.8	3.75	0.01
16	SLD 4	85	4	1734	1.8	3.75	0.01
16	SLD 5	27	22	2211	-34.6	1.34	-0.01
16	SLD 6	27	22	2211	-34.6	1.34	-0.01
16	SLD 7	-136	-17	1683	31.1	-5.49	0.01
16	SLD 8	-136	-17	1683	31.1	-5.49	0.01
16	SLD 9	-114	16	2325	-29.19	-4.53	-0.01
16	SLD 10	-114	16	2325	-29.19	-4.53	-0.01
16	SLD 11	-276	-23	1797	36.51	-11.36	0.01
16	SLD 12	-276	-23	1797	36.51	-11.36	0.01
16	SLD 13	-335	-5	2275	0.12	-13.77	-0.01
16	SLD 14	-335	-5	2275	0.12	-13.77	-0.01
16	SLD 15	-384	-16	2116	19.83	-15.82	-0.01
16	SLD 16	-384	-16	2116	19.83	-15.82	-0.01
16	SLV 1	492	39	1737	-47.1	20.79	0.01
16	SLV 2	492	39	1737	-47.1	20.79	0.01
16	SLV 3	371	10	1369	3.85	15.68	0.03
16	SLV 4	371	10	1369	3.85	15.68	0.03
16	SLV 5	244	56	2482	-90.73	10.49	-0.02
16	SLV 6	244	56	2482	-90.73	10.49	-0.02
16	SLV 7	-160	-41	1256	79.09	-6.57	0.03
16	SLV 8	-160	-41	1256	79.09	-6.57	0.03
16	SLV 9	-89	41	2752	-77.18	-3.46	-0.03
16	SLV 10	-89	41	2752	-77.18	-3.46	-0.03
16	SLV 11	-494	-56	1526	92.64	-20.51	0.02
16	SLV 12	-494	-56	1526	92.64	-20.51	0.02
16	SLV 13	-621	-11	2639	-1.94	-25.7	-0.03
16	SLV 14	-621	-11	2639	-1.94	-25.7	-0.03
16	SLV 15	-742	-40	2271	49.01	-30.82	-0.01
16	SLV 16	-742	-40	2271	49.01	-30.82	-0.01
17	SLU 1	-131	0	1891	0.49	-5.3	0
17	SLU 2	-142	-1	1904	0.04	-5.73	0
17	SLU 3	-131	0	1891	0.49	-5.3	0
17	SLU 4	-137	-1	1899	0.22	-5.56	0
17	SLU 5	-142	-1	1904	0.04	-5.73	0
17	SLU 6	-131	0	1891	0.49	-5.3	0
17	SLU 7	-137	-1	1899	0.22	-5.56	0
17	SLU 8	-131	0	1891	0.49	-5.3	0
17	SLU 9	-137	-1	1899	0.22	-5.56	0
17	SLU 10	-185	-1	2076	0.58	-7.38	0
17	SLU 11	-175	0	2062	1.03	-6.95	0
17	SLU 12	-181	-1	2070	0.76	-7.2	0
17	SLU 13	-185	-1	2076	0.58	-7.38	0
17	SLU 14	-175	0	2062	1.03	-6.95	0
17	SLU 15	-181	-1	2070	0.76	-7.2	0
17	SLU 16	-175	0	2062	1.03	-6.95	0
17	SLU 17	-181	-1	2070	0.76	-7.2	0
17	SLU 18	-194	0	2136	1.27	-7.65	0
17	SLU 19	-200	-1	2144	1	-7.91	0
17	SLU 20	-194	0	2136	1.27	-7.65	0
17	SLU 21	-200	-1	2144	1	-7.91	0
17	SLU 22	-151	0	1989	0.71	-6.06	0
17	SLU 23	-161	-1	2003	0.26	-6.49	0
17	SLU 24	-151	0	1989	0.71	-6.06	0
17	SLU 25	-157	-1	1998	0.44	-6.32	0
17	SLU 26	-161	-1	2003	0.26	-6.49	0
17	SLU 27	-151	0	1989	0.71	-6.06	0
17	SLU 28	-157	-1	1998	0.44	-6.32	0
17	SLU 29	-151	0	1989	0.71	-6.06	0
17	SLU 30	-157	-1	1998	0.44	-6.32	0
17	SLU 31	-205	-1	2174	0.81	-8.13	0
17	SLU 32	-195	0	2161	1.26	-7.7	0
17	SLU 33	-201	-1	2169	0.99	-7.96	0
17	SLU 34	-205	-1	2174	0.81	-8.13	0
17	SLU 35	-195	0	2161	1.26	-7.7	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
17	SLU 36	-201	-1	2169	0.99	-7.96	0
17	SLU 37	-195	0	2161	1.26	-7.7	0
17	SLU 38	-201	-1	2169	0.99	-7.96	0
17	SLU 39	-213	0	2234	1.49	-8.41	0
17	SLU 40	-219	-1	2242	1.22	-8.67	0
17	SLU 41	-213	0	2234	1.49	-8.41	0
17	SLU 42	-219	-1	2242	1.22	-8.67	0
17	SLU 43	-164	0	2424	0.56	-6.63	0
17	SLU 44	-174	-1	2438	0.11	-7.06	0
17	SLU 45	-164	0	2424	0.56	-6.63	0
17	SLU 46	-170	-1	2432	0.29	-6.89	0
17	SLU 47	-174	-1	2438	0.11	-7.06	0
17	SLU 48	-164	0	2424	0.56	-6.63	0
17	SLU 49	-170	-1	2432	0.29	-6.89	0
17	SLU 50	-164	0	2424	0.56	-6.63	0
17	SLU 51	-170	-1	2432	0.29	-6.89	0
17	SLU 52	-218	-1	2609	0.65	-8.71	0
17	SLU 53	-207	0	2596	1.1	-8.28	0
17	SLU 54	-214	-1	2604	0.83	-8.54	0
17	SLU 55	-218	-1	2609	0.65	-8.71	0
17	SLU 56	-207	0	2596	1.1	-8.28	0
17	SLU 57	-214	-1	2604	0.83	-8.54	0
17	SLU 58	-207	0	2596	1.1	-8.28	0
17	SLU 59	-214	-1	2604	0.83	-8.54	0
17	SLU 60	-226	0	2669	1.34	-8.98	0
17	SLU 61	-232	-1	2677	1.07	-9.24	0
17	SLU 62	-226	0	2669	1.34	-8.98	0
17	SLU 63	-232	-1	2677	1.07	-9.24	0
17	SLU 64	-184	0	2523	0.78	-7.39	0
17	SLU 65	-194	-1	2536	0.33	-7.82	0
17	SLU 66	-184	0	2523	0.78	-7.39	0
17	SLU 67	-190	-1	2531	0.51	-7.65	0
17	SLU 68	-194	-1	2536	0.33	-7.82	0
17	SLU 69	-184	0	2523	0.78	-7.39	0
17	SLU 70	-190	-1	2531	0.51	-7.65	0
17	SLU 71	-184	0	2523	0.78	-7.39	0
17	SLU 72	-190	-1	2531	0.51	-7.65	0
17	SLU 73	-237	-1	2708	0.88	-9.46	0
17	SLU 74	-227	0	2694	1.33	-9.03	0
17	SLU 75	-233	-1	2702	1.06	-9.29	0
17	SLU 76	-237	-1	2708	0.88	-9.46	0
17	SLU 77	-227	0	2694	1.33	-9.03	0
17	SLU 78	-233	-1	2702	1.06	-9.29	0
17	SLU 79	-227	0	2694	1.33	-9.03	0
17	SLU 80	-233	-1	2702	1.06	-9.29	0
17	SLU 81	-246	0	2768	1.56	-9.74	0
17	SLU 82	-252	-1	2776	1.29	-10	0
17	SLU 83	-246	0	2768	1.56	-9.74	0
17	SLU 84	-252	-1	2776	1.29	-10	0
17	SLE RA 1	-137	0	1919	0.55	-5.52	0
17	SLE RA 2	-144	-1	1928	0.25	-5.8	0
17	SLE RA 3	-137	0	1919	0.55	-5.52	0
17	SLE RA 4	-141	-1	1924	0.37	-5.69	0
17	SLE RA 5	-144	-1	1928	0.25	-5.8	0
17	SLE RA 6	-137	0	1919	0.55	-5.52	0
17	SLE RA 7	-141	-1	1924	0.37	-5.69	0
17	SLE RA 8	-137	0	1919	0.55	-5.52	0
17	SLE RA 9	-141	-1	1924	0.37	-5.69	0
17	SLE RA 10	-173	-1	2042	0.62	-6.9	0
17	SLE RA 11	-166	0	2033	0.92	-6.61	0
17	SLE RA 12	-170	-1	2039	0.74	-6.79	0
17	SLE RA 13	-173	-1	2042	0.62	-6.9	0
17	SLE RA 14	-166	0	2033	0.92	-6.61	0
17	SLE RA 15	-170	-1	2039	0.74	-6.79	0
17	SLE RA 16	-166	0	2033	0.92	-6.61	0
17	SLE RA 17	-170	-1	2039	0.74	-6.79	0
17	SLE RA 18	-178	0	2082	1.07	-7.08	0
17	SLE RA 19	-183	-1	2088	0.89	-7.26	0
17	SLE RA 20	-178	0	2082	1.07	-7.08	0
17	SLE RA 21	-183	-1	2088	0.89	-7.26	0
17	SLE FR 1	-137	0	1919	0.55	-5.52	0
17	SLE FR 2	-138	0	1921	0.49	-5.57	0
17	SLE FR 3	-137	0	1919	0.55	-5.52	0
17	SLE FR 4	-151	0	1970	0.65	-6.04	0
17	SLE FR 5	-149	0	1968	0.71	-5.99	0
17	SLE FR 6	-158	0	2001	0.81	-6.3	0
17	SLE QP 1	-137	0	1919	0.55	-5.52	0
17	SLE QP 2	-149	0	1968	0.71	-5.99	0
17	SLD 1	108	6	1824	-13.32	4.7	0.01
17	SLD 2	108	6	1824	-13.32	4.7	0.01
17	SLD 3	59	13	1617	-0.39	2.7	0.01
17	SLD 4	59	13	1617	-0.39	2.7	0.01
17	SLD 5	1	-8	2239	-23.1	0.26	-0.01
17	SLD 6	1	-8	2239	-23.1	0.26	-0.01
17	SLD 7	-160	13	1548	19.98	-6.42	0.02
17	SLD 8	-160	13	1548	19.98	-6.42	0.02
17	SLD 9	-138	-14	2388	-18.57	-5.55	-0.02
17	SLD 10	-138	-14	2388	-18.57	-5.55	-0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
17	SLD 11	-300	7	1697	24.52	-12.24	0.01
17	SLD 12	-300	7	1697	24.52	-12.24	0.01
17	SLD 13	-358	-13	2319	1.81	-14.67	-0.02
17	SLD 14	-358	-13	2319	1.81	-14.67	-0.02
17	SLD 15	-407	-7	2112	14.73	-16.68	-0.01
17	SLD 16	-407	-7	2112	14.73	-16.68	-0.01
17	SLV 1	464	17	1625	-34.91	19.5	0.02
17	SLV 2	464	17	1625	-34.91	19.5	0.02
17	SLV 3	344	32	1143	-1.67	14.51	0.04
17	SLV 4	344	32	1143	-1.67	14.51	0.04
17	SLV 5	216	-18	2596	-60.39	9.23	-0.03
17	SLV 6	216	-18	2596	-60.39	9.23	-0.03
17	SLV 7	-183	32	990	50.41	-7.41	0.04
17	SLV 8	-183	32	990	50.41	-7.41	0.04
17	SLV 9	-116	-33	2946	-49	-4.57	-0.04
17	SLV 10	-116	-33	2946	-49	-4.57	-0.04
17	SLV 11	-515	17	1340	61.81	-21.2	0.03
17	SLV 12	-515	17	1340	61.81	-21.2	0.03
17	SLV 13	-643	-33	2793	3.08	-26.48	-0.04
17	SLV 14	-643	-33	2793	3.08	-26.48	-0.04
17	SLV 15	-762	-18	2311	36.32	-31.47	-0.02
17	SLV 16	-762	-18	2311	36.32	-31.47	-0.02
18	SLU 1	-156	0	1867	0.23	-6.44	-0.01
18	SLU 2	-166	-1	1882	0.07	-6.87	-0.01
18	SLU 3	-156	0	1867	0.23	-6.44	-0.01
18	SLU 4	-162	-1	1876	0.13	-6.7	-0.01
18	SLU 5	-166	-1	1882	0.07	-6.87	-0.01
18	SLU 6	-156	0	1867	0.23	-6.44	-0.01
18	SLU 7	-162	-1	1876	0.13	-6.7	-0.01
18	SLU 8	-156	0	1867	0.23	-6.44	-0.01
18	SLU 9	-162	-1	1876	0.13	-6.7	-0.01
18	SLU 10	-208	-1	2031	0.32	-8.62	-0.01
18	SLU 11	-198	0	2016	0.48	-8.19	-0.01
18	SLU 12	-204	0	2025	0.39	-8.45	-0.01
18	SLU 13	-208	-1	2031	0.32	-8.62	-0.01
18	SLU 14	-198	0	2016	0.48	-8.19	-0.01
18	SLU 15	-204	0	2025	0.39	-8.45	-0.01
18	SLU 16	-198	0	2016	0.48	-8.19	-0.01
18	SLU 17	-204	0	2025	0.39	-8.45	-0.01
18	SLU 18	-217	0	2080	0.59	-8.94	-0.01
18	SLU 19	-223	0	2089	0.49	-9.2	-0.01
18	SLU 20	-217	0	2080	0.59	-8.94	-0.01
18	SLU 21	-223	0	2089	0.49	-9.2	-0.01
18	SLU 22	-175	0	1957	0.34	-7.24	-0.01
18	SLU 23	-185	-1	1972	0.17	-7.67	-0.01
18	SLU 24	-175	0	1957	0.34	-7.24	-0.01
18	SLU 25	-181	-1	1966	0.24	-7.5	-0.01
18	SLU 26	-185	-1	1972	0.17	-7.67	-0.01
18	SLU 27	-175	0	1957	0.34	-7.24	-0.01
18	SLU 28	-181	-1	1966	0.24	-7.5	-0.01
18	SLU 29	-175	0	1957	0.34	-7.24	-0.01
18	SLU 30	-181	-1	1966	0.24	-7.5	-0.01
18	SLU 31	-228	-1	2121	0.43	-9.42	-0.01
18	SLU 32	-218	0	2106	0.59	-8.99	-0.01
18	SLU 33	-224	0	2115	0.49	-9.25	-0.01
18	SLU 34	-228	-1	2121	0.43	-9.42	-0.01
18	SLU 35	-218	0	2106	0.59	-8.99	-0.01
18	SLU 36	-224	0	2115	0.49	-9.25	-0.01
18	SLU 37	-218	0	2106	0.59	-8.99	-0.01
18	SLU 38	-224	0	2115	0.49	-9.25	-0.01
18	SLU 39	-236	0	2169	0.7	-9.74	-0.01
18	SLU 40	-242	0	2178	0.6	-10	-0.01
18	SLU 41	-236	0	2169	0.7	-9.74	-0.01
18	SLU 42	-242	0	2178	0.6	-10	-0.01
18	SLU 43	-196	0	2397	0.26	-8.1	-0.01
18	SLU 44	-206	-1	2412	0.1	-8.52	-0.01
18	SLU 45	-196	0	2397	0.26	-8.1	-0.01
18	SLU 46	-202	-1	2406	0.17	-8.35	-0.01
18	SLU 47	-206	-1	2412	0.1	-8.52	-0.01
18	SLU 48	-196	0	2397	0.26	-8.1	-0.01
18	SLU 49	-202	-1	2406	0.17	-8.35	-0.01
18	SLU 50	-196	0	2397	0.26	-8.1	-0.01
18	SLU 51	-202	-1	2406	0.17	-8.35	-0.01
18	SLU 52	-249	-1	2560	0.35	-10.27	-0.01
18	SLU 53	-239	0	2545	0.52	-9.85	-0.01
18	SLU 54	-245	-1	2554	0.42	-10.1	-0.01
18	SLU 55	-249	-1	2560	0.35	-10.27	-0.01
18	SLU 56	-239	0	2545	0.52	-9.85	-0.01
18	SLU 57	-245	-1	2554	0.42	-10.1	-0.01
18	SLU 58	-239	0	2545	0.52	-9.85	-0.01
18	SLU 59	-245	-1	2554	0.42	-10.1	-0.01
18	SLU 60	-257	0	2609	0.62	-10.6	-0.01
18	SLU 61	-263	-1	2618	0.53	-10.85	-0.01
18	SLU 62	-257	0	2609	0.62	-10.6	-0.01
18	SLU 63	-263	-1	2618	0.53	-10.85	-0.01
18	SLU 64	-216	0	2486	0.37	-8.9	-0.01
18	SLU 65	-226	-1	2501	0.21	-9.32	-0.01
18	SLU 66	-216	0	2486	0.37	-8.9	-0.01





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
18	SLU 67	-222	-1	2495	0.27	-9.15	-0.01
18	SLU 68	-226	-1	2501	0.21	-9.32	-0.01
18	SLU 69	-216	0	2486	0.37	-8.9	-0.01
18	SLU 70	-222	-1	2495	0.27	-9.15	-0.01
18	SLU 71	-216	0	2486	0.37	-8.9	-0.01
18	SLU 72	-222	-1	2495	0.27	-9.15	-0.01
18	SLU 73	-268	-1	2650	0.46	-11.07	-0.01
18	SLU 74	-258	0	2635	0.62	-10.65	-0.01
18	SLU 75	-264	-1	2644	0.52	-10.91	-0.01
18	SLU 76	-268	-1	2650	0.46	-11.07	-0.01
18	SLU 77	-258	0	2635	0.62	-10.65	-0.01
18	SLU 78	-264	-1	2644	0.52	-10.91	-0.01
18	SLU 79	-258	0	2635	0.62	-10.65	-0.01
18	SLU 80	-264	-1	2644	0.52	-10.91	-0.01
18	SLU 81	-276	0	2699	0.73	-11.4	-0.01
18	SLU 82	-282	0	2708	0.63	-11.66	-0.01
18	SLU 83	-276	0	2699	0.73	-11.4	-0.01
18	SLU 84	-282	0	2708	0.63	-11.66	-0.01
18	SLE RA 1	-162	0	1893	0.26	-6.67	-0.01
18	SLE RA 2	-168	-1	1903	0.15	-6.95	-0.01
18	SLE RA 3	-162	0	1893	0.26	-6.67	-0.01
18	SLE RA 4	-166	-1	1899	0.2	-6.84	-0.01
18	SLE RA 5	-168	-1	1903	0.15	-6.95	-0.01
18	SLE RA 6	-162	0	1893	0.26	-6.67	-0.01
18	SLE RA 7	-166	-1	1899	0.2	-6.84	-0.01
18	SLE RA 8	-162	0	1893	0.26	-6.67	-0.01
18	SLE RA 9	-166	-1	1899	0.2	-6.84	-0.01
18	SLE RA 10	-197	-1	2002	0.32	-8.12	-0.01
18	SLE RA 11	-190	0	1992	0.43	-7.84	-0.01
18	SLE RA 12	-194	0	1998	0.36	-8.01	-0.01
18	SLE RA 13	-197	-1	2002	0.32	-8.12	-0.01
18	SLE RA 14	-190	0	1992	0.43	-7.84	-0.01
18	SLE RA 15	-194	0	1998	0.36	-8.01	-0.01
18	SLE RA 16	-190	0	1992	0.43	-7.84	-0.01
18	SLE RA 17	-194	0	1998	0.36	-8.01	-0.01
18	SLE RA 18	-202	0	2034	0.5	-8.34	-0.01
18	SLE RA 19	-206	0	2040	0.44	-8.51	-0.01
18	SLE RA 20	-202	0	2034	0.5	-8.34	-0.01
18	SLE RA 21	-206	0	2040	0.44	-8.51	-0.01
18	SLE FR 1	-162	0	1893	0.26	-6.67	-0.01
18	SLE FR 2	-163	0	1895	0.24	-6.73	-0.01
18	SLE FR 3	-162	0	1893	0.26	-6.67	-0.01
18	SLE FR 4	-175	0	1937	0.31	-7.23	-0.01
18	SLE FR 5	-174	0	1935	0.33	-7.17	-0.01
18	SLE FR 6	-182	0	1964	0.38	-7.5	-0.01
18	SLE QP 1	-162	0	1893	0.26	-6.67	-0.01
18	SLE QP 2	-174	0	1935	0.33	-7.17	-0.01
18	SLD 1	85	7	1754	-8.97	3.5	0
18	SLD 2	85	7	1754	-8.97	3.5	0
18	SLD 3	35	13	1481	-2.07	1.56	0.01
18	SLD 4	35	13	1481	-2.07	1.56	0.01
18	SLD 5	-20	-6	2295	-12.92	-1.04	-0.02
18	SLD 6	-20	-6	2295	-12.92	-1.04	-0.02
18	SLD 7	-187	12	1385	10.08	-7.48	0.02
18	SLD 8	-187	12	1385	10.08	-7.48	0.02
18	SLD 9	-160	-12	2486	-9.41	-6.86	-0.03
18	SLD 10	-160	-12	2486	-9.41	-6.86	-0.03
18	SLD 11	-327	6	1576	13.59	-13.3	0.01
18	SLD 12	-327	6	1576	13.59	-13.3	0.01
18	SLD 13	-382	-13	2390	2.73	-15.9	-0.02
18	SLD 14	-382	-13	2390	2.73	-15.9	-0.02
18	SLD 15	-432	-8	2117	9.63	-17.84	-0.01
18	SLD 16	-432	-8	2117	9.63	-17.84	-0.01
18	SLV 1	441	18	1502	-23.28	18.24	0
18	SLV 2	441	18	1502	-23.28	18.24	0
18	SLV 3	319	32	867	-5.65	13.5	0.04
18	SLV 4	319	32	867	-5.65	13.5	0.04
18	SLV 5	196	-16	2768	-33.49	7.64	-0.05
18	SLV 6	196	-16	2768	-33.49	7.64	-0.05
18	SLV 7	-211	31	652	25.28	-8.16	0.05
18	SLV 8	-211	31	652	25.28	-8.16	0.05
18	SLV 9	-137	-31	3219	-24.61	-6.18	-0.06
18	SLV 10	-137	-31	3219	-24.61	-6.18	-0.06
18	SLV 11	-543	16	1103	34.16	-21.98	0.04
18	SLV 12	-543	16	1103	34.16	-21.98	0.04
18	SLV 13	-667	-33	3004	6.31	-27.84	-0.05
18	SLV 14	-667	-33	3004	6.31	-27.84	-0.05
18	SLV 15	-789	-19	2369	23.95	-32.58	-0.02
18	SLV 16	-789	-19	2369	23.95	-32.58	-0.02
19	SLU 1	-170	2	1879	-0.43	-7.28	0.01
19	SLU 2	-181	1	1895	-0.45	-7.71	0.01
19	SLU 3	-170	2	1879	-0.43	-7.28	0.01
19	SLU 4	-176	2	1889	-0.44	-7.54	0.01
19	SLU 5	-181	1	1895	-0.45	-7.71	0.01
19	SLU 6	-170	2	1879	-0.43	-7.28	0.01
19	SLU 7	-176	2	1889	-0.44	-7.54	0.01
19	SLU 8	-170	2	1879	-0.43	-7.28	0.01
19	SLU 9	-176	2	1889	-0.44	-7.54	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione		
		x	y	z		x	y	z
19	SLU 10	-208	3	2050		-0.66	-8.95	0.02
19	SLU 11	-198	4	2034		-0.65	-8.53	0.02
19	SLU 12	-204	3	2043		-0.66	-8.78	0.02
19	SLU 13	-208	3	2050		-0.66	-8.95	0.02
19	SLU 14	-198	4	2034		-0.65	-8.53	0.02
19	SLU 15	-204	3	2043		-0.66	-8.78	0.02
19	SLU 16	-198	4	2034		-0.65	-8.53	0.02
19	SLU 17	-204	3	2043		-0.66	-8.78	0.02
19	SLU 18	-210	4	2100		-0.74	-9.06	0.02
19	SLU 19	-216	4	2110		-0.75	-9.32	0.02
19	SLU 20	-210	4	2100		-0.74	-9.06	0.02
19	SLU 21	-216	4	2110		-0.75	-9.32	0.02
19	SLU 22	-184	3	1971		-0.52	-7.89	0.01
19	SLU 23	-194	2	1988		-0.53	-8.32	0.01
19	SLU 24	-184	3	1971		-0.52	-7.89	0.01
19	SLU 25	-190	2	1981		-0.53	-8.15	0.01
19	SLU 26	-194	2	1988		-0.53	-8.32	0.01
19	SLU 27	-184	3	1971		-0.52	-7.89	0.01
19	SLU 28	-190	2	1981		-0.53	-8.15	0.01
19	SLU 29	-184	3	1971		-0.52	-7.89	0.01
19	SLU 30	-190	2	1981		-0.53	-8.15	0.01
19	SLU 31	-222	4	2142		-0.75	-9.56	0.02
19	SLU 32	-212	4	2126		-0.73	-9.14	0.02
19	SLU 33	-218	4	2136		-0.74	-9.39	0.02
19	SLU 34	-222	4	2142		-0.75	-9.56	0.02
19	SLU 35	-212	4	2126		-0.73	-9.14	0.02
19	SLU 36	-218	4	2136		-0.74	-9.39	0.02
19	SLU 37	-212	4	2126		-0.73	-9.14	0.02
19	SLU 38	-218	4	2136		-0.74	-9.39	0.02
19	SLU 39	-223	5	2193		-0.83	-9.67	0.02
19	SLU 40	-230	5	2202		-0.84	-9.93	0.02
19	SLU 41	-223	5	2193		-0.83	-9.67	0.02
19	SLU 42	-230	5	2202		-0.84	-9.93	0.02
19	SLU 43	-217	2	2411		-0.53	-9.26	0.01
19	SLU 44	-227	2	2427		-0.55	-9.68	0.01
19	SLU 45	-217	2	2411		-0.53	-9.26	0.01
19	SLU 46	-223	2	2420		-0.54	-9.51	0.01
19	SLU 47	-227	2	2427		-0.55	-9.68	0.01
19	SLU 48	-217	2	2411		-0.53	-9.26	0.01
19	SLU 49	-223	2	2420		-0.54	-9.51	0.01
19	SLU 50	-217	2	2411		-0.53	-9.26	0.01
19	SLU 51	-223	2	2420		-0.54	-9.51	0.01
19	SLU 52	-255	3	2582		-0.76	-10.93	0.02
19	SLU 53	-244	4	2566		-0.75	-10.5	0.02
19	SLU 54	-250	4	2575		-0.76	-10.76	0.02
19	SLU 55	-255	3	2582		-0.76	-10.93	0.02
19	SLU 56	-244	4	2566		-0.75	-10.5	0.02
19	SLU 57	-250	4	2575		-0.76	-10.76	0.02
19	SLU 58	-244	4	2566		-0.75	-10.5	0.02
19	SLU 59	-250	4	2575		-0.76	-10.76	0.02
19	SLU 60	-256	5	2632		-0.84	-11.03	0.02
19	SLU 61	-262	4	2642		-0.85	-11.29	0.02
19	SLU 62	-256	5	2632		-0.84	-11.03	0.02
19	SLU 63	-262	4	2642		-0.85	-11.29	0.02
19	SLU 64	-230	3	2503		-0.62	-9.87	0.02
19	SLU 65	-241	2	2519		-0.64	-10.29	0.02
19	SLU 66	-230	3	2503		-0.62	-9.87	0.02
19	SLU 67	-237	3	2513		-0.63	-10.12	0.02
19	SLU 68	-241	2	2519		-0.64	-10.29	0.02
19	SLU 69	-230	3	2503		-0.62	-9.87	0.02
19	SLU 70	-237	3	2513		-0.63	-10.12	0.02
19	SLU 71	-230	3	2503		-0.62	-9.87	0.02
19	SLU 72	-237	3	2513		-0.63	-10.12	0.02
19	SLU 73	-268	4	2674		-0.85	-11.54	0.02
19	SLU 74	-258	5	2658		-0.84	-11.11	0.02
19	SLU 75	-264	4	2668		-0.84	-11.37	0.02
19	SLU 76	-268	4	2674		-0.85	-11.54	0.02
19	SLU 77	-258	5	2658		-0.84	-11.11	0.02
19	SLU 78	-264	4	2668		-0.84	-11.37	0.02
19	SLU 79	-258	5	2658		-0.84	-11.11	0.02
19	SLU 80	-264	4	2668		-0.84	-11.37	0.02
19	SLU 81	-270	5	2724		-0.93	-11.64	0.02
19	SLU 82	-276	5	2734		-0.94	-11.9	0.02
19	SLU 83	-270	5	2724		-0.93	-11.64	0.02
19	SLU 84	-276	5	2734		-0.94	-11.9	0.02
19	SLE RA 1	-174	2	1905		-0.46	-7.45	0.01
19	SLE RA 2	-181	2	1916		-0.47	-7.74	0.01
19	SLE RA 3	-174	2	1905		-0.46	-7.45	0.01
19	SLE RA 4	-178	2	1912		-0.46	-7.63	0.01
19	SLE RA 5	-181	2	1916		-0.47	-7.74	0.01
19	SLE RA 6	-174	2	1905		-0.46	-7.45	0.01
19	SLE RA 7	-178	2	1912		-0.46	-7.63	0.01
19	SLE RA 8	-174	2	1905		-0.46	-7.45	0.01
19	SLE RA 9	-178	2	1912		-0.46	-7.63	0.01
19	SLE RA 10	-199	3	2019		-0.61	-8.57	0.02
19	SLE RA 11	-193	3	2008		-0.6	-8.28	0.02
19	SLE RA 12	-197	3	2015		-0.61	-8.46	0.02
19	SLE RA 13	-199	3	2019		-0.61	-8.57	0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione		
		x	y	z		x	y	z
19	SLE RA 14	-193	3	2008		-0.6	-8.28	0.02
19	SLE RA 15	-197	3	2015		-0.61	-8.46	0.02
19	SLE RA 16	-193	3	2008		-0.6	-8.28	0.02
19	SLE RA 17	-197	3	2015		-0.61	-8.46	0.02
19	SLE RA 18	-200	4	2053		-0.66	-8.64	0.02
19	SLE RA 19	-205	4	2059		-0.67	-8.81	0.02
19	SLE RA 20	-200	4	2053		-0.66	-8.64	0.02
19	SLE RA 21	-205	4	2059		-0.67	-8.81	0.02
19	SLE FR 1	-174	2	1905		-0.46	-7.45	0.01
19	SLE FR 2	-176	2	1907		-0.46	-7.51	0.01
19	SLE FR 3	-174	2	1905		-0.46	-7.45	0.01
19	SLE FR 4	-183	3	1952		-0.52	-7.87	0.01
19	SLE FR 5	-182	3	1949		-0.52	-7.81	0.01
19	SLE FR 6	-187	3	1979		-0.56	-8.05	0.01
19	SLE QP 1	-174	2	1905		-0.46	-7.45	0.01
19	SLE QP 2	-182	3	1949		-0.52	-7.81	0.01
19	SLD 1	78	7	1726		-5.41	2.71	0.01
19	SLD 2	78	7	1726		-5.41	2.71	0.01
19	SLD 3	21	13	1342		-2.59	0.76	0
19	SLD 4	21	13	1342		-2.59	0.76	0
19	SLD 5	-18	-5	2465		-6.26	-1.71	0.03
19	SLD 6	-18	-5	2465		-6.26	-1.71	0.03
19	SLD 7	-207	15	1185		3.13	-8.18	-0.01
19	SLD 8	-207	15	1185		3.13	-8.18	-0.01
19	SLD 9	-157	-9	2714		-4.17	-7.44	0.04
19	SLD 10	-157	-9	2714		-4.17	-7.44	0.04
19	SLD 11	-346	10	1434		5.22	-13.91	0
19	SLD 12	-346	10	1434		5.22	-13.91	0
19	SLD 13	-385	-8	2557		1.55	-16.39	0.03
19	SLD 14	-385	-8	2557		1.55	-16.39	0.03
19	SLD 15	-442	-2	2173		4.37	-18.33	0.02
19	SLD 16	-442	-2	2173		4.37	-18.33	0.02
19	SLV 1	433	15	1413		-12.91	17.14	0
19	SLV 2	433	15	1413		-12.91	17.14	0
19	SLV 3	299	29	525		-5.82	12.45	-0.03
19	SLV 4	299	29	525		-5.82	12.45	-0.03
19	SLV 5	206	-16	3136		-14.99	6.79	0.06
19	SLV 6	206	-16	3136		-14.99	6.79	0.06
19	SLV 7	-241	33	175		8.64	-8.85	-0.05
19	SLV 8	-241	33	175		8.64	-8.85	-0.05
19	SLV 9	-123	-28	3724		-9.68	-6.77	0.07
19	SLV 10	-123	-28	3724		-9.68	-6.77	0.07
19	SLV 11	-570	22	763		13.95	-22.41	-0.03
19	SLV 12	-570	22	763		13.95	-22.41	-0.03
19	SLV 13	-663	-24	3374		4.78	-28.07	0.06
19	SLV 14	-663	-24	3374		4.78	-28.07	0.06
19	SLV 15	-797	-9	2486		11.87	-32.77	0.03
19	SLV 16	-797	-9	2486		11.87	-32.77	0.03
20	SLU 1	-252	228	2646		-8.06	-9.98	0
20	SLU 2	-262	225	2666		-7.93	-10.41	0
20	SLU 3	-252	228	2646		-8.06	-9.98	0
20	SLU 4	-258	226	2658		-7.98	-10.24	0
20	SLU 5	-262	225	2666		-7.93	-10.41	0
20	SLU 6	-252	228	2646		-8.06	-9.98	0
20	SLU 7	-258	226	2658		-7.98	-10.24	0
20	SLU 8	-252	228	2646		-8.06	-9.98	0
20	SLU 9	-258	226	2658		-7.98	-10.24	0
20	SLU 10	-310	340	2991		-13.51	-12.23	0
20	SLU 11	-300	343	2971		-13.65	-11.8	0
20	SLU 12	-306	341	2983		-13.56	-12.06	0
20	SLU 13	-310	340	2991		-13.51	-12.23	0
20	SLU 14	-300	343	2971		-13.65	-11.8	0
20	SLU 15	-306	341	2983		-13.56	-12.06	0
20	SLU 16	-300	343	2971		-13.65	-11.8	0
20	SLU 17	-306	341	2983		-13.56	-12.06	0
20	SLU 18	-320	392	3110		-16.04	-12.58	0
20	SLU 19	-326	391	3123		-15.95	-12.83	0
20	SLU 20	-320	392	3110		-16.04	-12.58	0
20	SLU 21	-326	391	3123		-15.95	-12.83	0
20	SLU 22	-274	276	2818		-10.33	-10.85	0
20	SLU 23	-284	273	2838		-10.2	-11.27	0
20	SLU 24	-274	276	2818		-10.33	-10.85	0
20	SLU 25	-280	274	2830		-10.25	-11.1	0
20	SLU 26	-284	273	2838		-10.2	-11.27	0
20	SLU 27	-274	276	2818		-10.33	-10.85	0
20	SLU 28	-280	274	2830		-10.25	-11.1	0
20	SLU 29	-274	276	2818		-10.33	-10.85	0
20	SLU 30	-280	274	2830		-10.25	-11.1	0
20	SLU 31	-332	388	3163		-15.78	-13.09	0
20	SLU 32	-322	391	3143		-15.91	-12.67	0
20	SLU 33	-328	389	3155		-15.83	-12.92	0
20	SLU 34	-332	388	3163		-15.78	-13.09	0
20	SLU 35	-322	391	3143		-15.91	-12.67	0
20	SLU 36	-328	389	3155		-15.83	-12.92	0
20	SLU 37	-322	391	3143		-15.91	-12.67	0
20	SLU 38	-328	389	3155		-15.83	-12.92	0
20	SLU 39	-343	440	3282		-18.31	-13.45	0.01
20	SLU 40	-348	438	3294		-18.22	-13.7	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
20	SLU 41	-343	440	3282	-18.31	-13.45	0.01
20	SLU 42	-348	438	3294	-18.22	-13.7	0.01
20	SLU 43	-320	280	3381	-9.71	-12.68	0
20	SLU 44	-330	277	3401	-9.57	-13.1	0
20	SLU 45	-320	280	3381	-9.71	-12.68	0
20	SLU 46	-326	278	3393	-9.62	-12.93	0
20	SLU 47	-330	277	3401	-9.57	-13.1	0
20	SLU 48	-320	280	3381	-9.71	-12.68	0
20	SLU 49	-326	278	3393	-9.62	-12.93	0
20	SLU 50	-320	280	3381	-9.71	-12.68	0
20	SLU 51	-326	278	3393	-9.62	-12.93	0
20	SLU 52	-378	392	3726	-15.15	-14.92	0
20	SLU 53	-368	395	3706	-15.29	-14.5	0
20	SLU 54	-374	393	3718	-15.2	-14.75	0
20	SLU 55	-378	392	3726	-15.15	-14.92	0
20	SLU 56	-368	395	3706	-15.29	-14.5	0
20	SLU 57	-374	393	3718	-15.2	-14.75	0
20	SLU 58	-368	395	3706	-15.29	-14.5	0
20	SLU 59	-374	393	3718	-15.2	-14.75	0
20	SLU 60	-388	444	3845	-17.68	-15.28	0
20	SLU 61	-394	442	3857	-17.6	-15.53	0
20	SLU 62	-388	444	3845	-17.68	-15.28	0
20	SLU 63	-394	442	3857	-17.6	-15.53	0
20	SLU 64	-342	327	3553	-11.98	-13.55	0
20	SLU 65	-352	325	3573	-11.84	-13.97	0
20	SLU 66	-342	327	3553	-11.98	-13.55	0
20	SLU 67	-348	326	3565	-11.89	-13.8	0
20	SLU 68	-352	325	3573	-11.84	-13.97	0
20	SLU 69	-342	327	3553	-11.98	-13.55	0
20	SLU 70	-348	326	3565	-11.89	-13.8	0
20	SLU 71	-342	327	3553	-11.98	-13.55	0
20	SLU 72	-348	326	3565	-11.89	-13.8	0
20	SLU 73	-400	440	3898	-17.42	-15.79	0
20	SLU 74	-390	443	3878	-17.56	-15.36	0
20	SLU 75	-396	441	3890	-17.47	-15.62	0
20	SLU 76	-400	440	3898	-17.42	-15.79	0
20	SLU 77	-390	443	3878	-17.56	-15.36	0
20	SLU 78	-396	441	3890	-17.47	-15.62	0
20	SLU 79	-390	443	3878	-17.56	-15.36	0
20	SLU 80	-396	441	3890	-17.47	-15.62	0
20	SLU 81	-410	492	4017	-19.95	-16.14	0
20	SLU 82	-416	490	4029	-19.86	-16.4	0
20	SLU 83	-410	492	4017	-19.95	-16.14	0
20	SLU 84	-416	490	4029	-19.86	-16.4	0
20	SLE RA 1	-258	241	2695	-8.71	-10.23	0
20	SLE RA 2	-265	239	2708	-8.62	-10.51	0
20	SLE RA 3	-258	241	2695	-8.71	-10.23	0
20	SLE RA 4	-262	240	2703	-8.66	-10.4	0
20	SLE RA 5	-265	239	2708	-8.62	-10.51	0
20	SLE RA 6	-258	241	2695	-8.71	-10.23	0
20	SLE RA 7	-262	240	2703	-8.66	-10.4	0
20	SLE RA 8	-258	241	2695	-8.71	-10.23	0
20	SLE RA 9	-262	240	2703	-8.66	-10.4	0
20	SLE RA 10	-297	316	2925	-12.34	-11.73	0
20	SLE RA 11	-290	318	2912	-12.43	-11.44	0
20	SLE RA 12	-294	317	2920	-12.38	-11.61	0
20	SLE RA 13	-297	316	2925	-12.34	-11.73	0
20	SLE RA 14	-290	318	2912	-12.43	-11.44	0
20	SLE RA 15	-294	317	2920	-12.38	-11.61	0
20	SLE RA 16	-290	318	2912	-12.43	-11.44	0
20	SLE RA 17	-294	317	2920	-12.38	-11.61	0
20	SLE RA 18	-304	351	3005	-14.03	-11.96	0
20	SLE RA 19	-308	350	3013	-13.97	-12.13	0
20	SLE RA 20	-304	351	3005	-14.03	-11.96	0
20	SLE RA 21	-308	350	3013	-13.97	-12.13	0
20	SLE FR 1	-258	241	2695	-8.71	-10.23	0
20	SLE FR 2	-260	241	2698	-8.69	-10.29	0
20	SLE FR 3	-258	241	2695	-8.71	-10.23	0
20	SLE FR 4	-273	274	2791	-10.29	-10.81	0
20	SLE FR 5	-272	274	2788	-10.31	-10.75	0
20	SLE FR 6	-281	296	2850	-11.37	-11.09	0
20	SLE QP 1	-258	241	2695	-8.71	-10.23	0
20	SLE QP 2	-272	274	2788	-10.31	-10.75	0
20	SLD 1	-48	413	2427	-16.82	-1.47	-0.02
20	SLD 2	-48	413	2427	-16.82	-1.47	-0.02
20	SLD 3	-8	284	1696	-10.66	0.05	-0.02
20	SLD 4	-8	284	1696	-10.66	0.05	-0.02
20	SLD 5	-265	512	3788	-21.6	-10.27	0.01
20	SLD 6	-265	512	3788	-21.6	-10.27	0.01
20	SLD 7	-133	81	1353	-1.08	-5.2	-0.02
20	SLD 8	-133	81	1353	-1.08	-5.2	-0.02
20	SLD 9	-411	468	4223	-19.54	-16.29	0.02
20	SLD 10	-411	468	4223	-19.54	-16.29	0.02
20	SLD 11	-279	36	1788	0.98	-11.23	-0.01
20	SLD 12	-279	36	1788	0.98	-11.23	-0.01
20	SLD 13	-536	265	3880	-9.95	-21.55	0.03
20	SLD 14	-536	265	3880	-9.95	-21.55	0.03
20	SLD 15	-496	135	3149	-3.8	-20.03	0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
20	SLD 16	-496	135	3149	-3.8	-20.03	0.02
20	SLV 1	257	597	1917	-25.51	11.21	-0.04
20	SLV 2	257	597	1917	-25.51	11.21	-0.04
20	SLV 3	353	296	232	-11.14	14.85	-0.06
20	SLV 4	353	296	232	-11.14	14.85	-0.06
20	SLV 5	-260	827	5082	-36.67	-9.68	0.02
20	SLV 6	-260	827	5082	-36.67	-9.68	0.02
20	SLV 7	62	-175	-534	11.25	2.45	-0.05
20	SLV 8	62	-175	-534	11.25	2.45	-0.05
20	SLV 9	-606	724	6110	-31.86	-23.95	0.05
20	SLV 10	-606	724	6110	-31.86	-23.95	0.05
20	SLV 11	-284	-279	494	16.06	-11.82	-0.02
20	SLV 12	-284	-279	494	16.06	-11.82	-0.02
20	SLV 13	-897	252	5344	-9.48	-36.35	0.06
20	SLV 14	-897	252	5344	-9.48	-36.35	0.06
20	SLV 15	-801	-48	3659	4.9	-32.71	0.04
20	SLV 16	-801	-48	3659	4.9	-32.71	0.04
21	SLU 1	-354	9	2201	-2.66	-14.94	0.03
21	SLU 2	-363	9	2232	-2.67	-15.39	0.03
21	SLU 3	-354	9	2201	-2.66	-14.94	0.03
21	SLU 4	-359	9	2220	-2.67	-15.21	0.03
21	SLU 5	-363	9	2232	-2.67	-15.39	0.03
21	SLU 6	-354	9	2201	-2.66	-14.94	0.03
21	SLU 7	-359	9	2220	-2.67	-15.21	0.03
21	SLU 8	-354	9	2201	-2.66	-14.94	0.03
21	SLU 9	-359	9	2220	-2.67	-15.21	0.03
21	SLU 10	-428	11	2364	-3.16	-17.56	0.03
21	SLU 11	-418	11	2333	-3.15	-17.11	0.02
21	SLU 12	-424	11	2352	-3.16	-17.38	0.03
21	SLU 13	-428	11	2364	-3.16	-17.56	0.03
21	SLU 14	-418	11	2333	-3.15	-17.11	0.02
21	SLU 15	-424	11	2352	-3.16	-17.38	0.03
21	SLU 16	-418	11	2333	-3.15	-17.11	0.02
21	SLU 17	-424	11	2352	-3.16	-17.38	0.03
21	SLU 18	-446	11	2389	-3.36	-18.04	0.02
21	SLU 19	-452	11	2408	-3.37	-18.31	0.02
21	SLU 20	-446	11	2389	-3.36	-18.04	0.02
21	SLU 21	-452	11	2408	-3.37	-18.31	0.02
21	SLU 22	-384	10	2293	-2.9	-16.03	0.03
21	SLU 23	-394	10	2325	-2.91	-16.48	0.03
21	SLU 24	-384	10	2293	-2.9	-16.03	0.03
21	SLU 25	-390	10	2312	-2.91	-16.3	0.03
21	SLU 26	-394	10	2325	-2.91	-16.48	0.03
21	SLU 27	-384	10	2293	-2.9	-16.03	0.03
21	SLU 28	-390	10	2312	-2.91	-16.3	0.03
21	SLU 29	-384	10	2293	-2.9	-16.03	0.03
21	SLU 30	-390	10	2312	-2.91	-16.3	0.03
21	SLU 31	-458	11	2456	-3.4	-18.65	0.02
21	SLU 32	-449	11	2425	-3.39	-18.21	0.02
21	SLU 33	-455	11	2444	-3.39	-18.47	0.02
21	SLU 34	-458	11	2456	-3.4	-18.65	0.02
21	SLU 35	-449	11	2425	-3.39	-18.21	0.02
21	SLU 36	-455	11	2444	-3.39	-18.47	0.02
21	SLU 37	-449	11	2425	-3.39	-18.21	0.02
21	SLU 38	-455	11	2444	-3.39	-18.47	0.02
21	SLU 39	-477	12	2481	-3.6	-19.14	0.02
21	SLU 40	-482	12	2500	-3.6	-19.4	0.02
21	SLU 41	-477	12	2481	-3.6	-19.14	0.02
21	SLU 42	-482	12	2500	-3.6	-19.4	0.02
21	SLU 43	-449	11	2829	-3.38	-19.05	0.04
21	SLU 44	-459	11	2861	-3.39	-19.49	0.04
21	SLU 45	-449	11	2829	-3.38	-19.05	0.04
21	SLU 46	-455	11	2848	-3.39	-19.32	0.04
21	SLU 47	-459	11	2861	-3.39	-19.49	0.04
21	SLU 48	-449	11	2829	-3.38	-19.05	0.04
21	SLU 49	-455	11	2848	-3.39	-19.32	0.04
21	SLU 50	-449	11	2829	-3.38	-19.05	0.04
21	SLU 51	-455	11	2848	-3.39	-19.32	0.04
21	SLU 52	-523	13	2993	-3.88	-21.67	0.04
21	SLU 53	-514	13	2961	-3.87	-21.22	0.03
21	SLU 54	-519	13	2980	-3.88	-21.49	0.03
21	SLU 55	-523	13	2993	-3.88	-21.67	0.04
21	SLU 56	-514	13	2961	-3.87	-21.22	0.03
21	SLU 57	-519	13	2980	-3.88	-21.49	0.03
21	SLU 58	-514	13	2961	-3.87	-21.22	0.03
21	SLU 59	-519	13	2980	-3.88	-21.49	0.03
21	SLU 60	-542	14	3018	-4.08	-22.15	0.03
21	SLU 61	-547	14	3037	-4.08	-22.42	0.03
21	SLU 62	-542	14	3018	-4.08	-22.15	0.03
21	SLU 63	-547	14	3037	-4.08	-22.42	0.03
21	SLU 64	-480	12	2922	-3.62	-20.14	0.04
21	SLU 65	-489	12	2953	-3.63	-20.59	0.04
21	SLU 66	-480	12	2922	-3.62	-20.14	0.04
21	SLU 67	-486	12	2941	-3.62	-20.41	0.04
21	SLU 68	-489	12	2953	-3.63	-20.59	0.04
21	SLU 69	-480	12	2922	-3.62	-20.14	0.04
21	SLU 70	-486	12	2941	-3.62	-20.41	0.04
21	SLU 71	-480	12	2922	-3.62	-20.14	0.04



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
21	SLU 72	-486	12	2941	-3.62	-20.41	0.04
21	SLU 73	-554	14	3085	-4.12	-22.76	0.03
21	SLU 74	-545	14	3054	-4.11	-22.31	0.03
21	SLU 75	-550	14	3072	-4.11	-22.58	0.03
21	SLU 76	-554	14	3085	-4.12	-22.76	0.03
21	SLU 77	-545	14	3054	-4.11	-22.31	0.03
21	SLU 78	-550	14	3072	-4.11	-22.58	0.03
21	SLU 79	-545	14	3054	-4.11	-22.31	0.03
21	SLU 80	-550	14	3072	-4.11	-22.58	0.03
21	SLU 81	-572	15	3110	-4.32	-23.24	0.03
21	SLU 82	-578	15	3129	-4.32	-23.51	0.03
21	SLU 83	-572	15	3110	-4.32	-23.24	0.03
21	SLU 84	-578	15	3129	-4.32	-23.51	0.03
21	SLE RA 1	-363	9	2227	-2.73	-15.25	0.03
21	SLE RA 2	-369	9	2248	-2.74	-15.55	0.03
21	SLE RA 3	-363	9	2227	-2.73	-15.25	0.03
21	SLE RA 4	-366	9	2240	-2.73	-15.43	0.03
21	SLE RA 5	-369	9	2248	-2.74	-15.55	0.03
21	SLE RA 6	-363	9	2227	-2.73	-15.25	0.03
21	SLE RA 7	-366	9	2240	-2.73	-15.43	0.03
21	SLE RA 8	-363	9	2227	-2.73	-15.25	0.03
21	SLE RA 9	-366	9	2240	-2.73	-15.43	0.03
21	SLE RA 10	-412	10	2336	-3.06	-17	0.03
21	SLE RA 11	-406	10	2315	-3.06	-16.7	0.03
21	SLE RA 12	-409	10	2328	-3.06	-16.88	0.03
21	SLE RA 13	-412	10	2336	-3.06	-17	0.03
21	SLE RA 14	-406	10	2315	-3.06	-16.7	0.03
21	SLE RA 15	-409	10	2328	-3.06	-16.88	0.03
21	SLE RA 16	-406	10	2315	-3.06	-16.7	0.03
21	SLE RA 17	-409	10	2328	-3.06	-16.88	0.03
21	SLE RA 18	-424	11	2353	-3.2	-17.32	0.02
21	SLE RA 19	-428	11	2365	-3.2	-17.5	0.03
21	SLE RA 20	-424	11	2353	-3.2	-17.32	0.02
21	SLE RA 21	-428	11	2365	-3.2	-17.5	0.03
21	SLE FR 1	-363	9	2227	-2.73	-15.25	0.03
21	SLE FR 2	-364	9	2231	-2.73	-15.31	0.03
21	SLE FR 3	-363	9	2227	-2.73	-15.25	0.03
21	SLE FR 4	-382	10	2269	-2.87	-15.93	0.03
21	SLE FR 5	-381	10	2265	-2.87	-15.87	0.03
21	SLE FR 6	-393	10	2290	-2.96	-16.29	0.03
21	SLE QP 1	-363	9	2227	-2.73	-15.25	0.03
21	SLE QP 2	-381	10	2265	-2.87	-15.87	0.03
21	SLD 1	-160	-3	1042	0.8	-6.85	0
21	SLD 2	-160	-3	1042	0.8	-6.85	0
21	SLD 3	-77	3	1745	-1.06	-3.98	0.02
21	SLD 4	-77	3	1745	-1.06	-3.98	0.02
21	SLD 5	-440	-3	832	1.05	-17.52	0
21	SLD 6	-440	-3	832	1.05	-17.52	0
21	SLD 7	-165	17	3175	-5.14	-7.95	0.05
21	SLD 8	-165	17	3175	-5.14	-7.95	0.05
21	SLD 9	-597	3	1355	-0.6	-23.8	0.01
21	SLD 10	-597	3	1355	-0.6	-23.8	0.01
21	SLD 11	-322	23	3698	-6.79	-14.23	0.06
21	SLD 12	-322	23	3698	-6.79	-14.23	0.06
21	SLD 13	-685	17	2785	-4.69	-27.77	0.04
21	SLD 14	-685	17	2785	-4.69	-27.77	0.04
21	SLD 15	-602	23	3488	-6.54	-24.9	0.06
21	SLD 16	-602	23	3488	-6.54	-24.9	0.06
21	SLV 1	139	-23	-668	6.31	5.5	-0.04
21	SLV 2	139	-23	-668	6.31	5.5	-0.04
21	SLV 3	341	-8	1007	1.72	12.19	0
21	SLV 4	341	-8	1007	1.72	12.19	0
21	SLV 5	-532	-23	-1156	6.86	-19.6	-0.06
21	SLV 6	-532	-23	-1156	6.86	-19.6	-0.06
21	SLV 7	143	27	4429	-8.47	2.69	0.08
21	SLV 8	143	27	4429	-8.47	2.69	0.08
21	SLV 9	-905	-8	101	2.73	-34.44	-0.03
21	SLV 10	-905	-8	101	2.73	-34.44	-0.03
21	SLV 11	-230	43	5686	-12.6	-12.14	0.11
21	SLV 12	-230	43	5686	-12.6	-12.14	0.11
21	SLV 13	-1103	27	3522	-7.46	-43.94	0.06
21	SLV 14	-1103	27	3522	-7.46	-43.94	0.06
21	SLV 15	-901	42	5198	-12.05	-37.25	0.1
21	SLV 16	-901	42	5198	-12.05	-37.25	0.1
22	SLU 1	-191	107	2078	-4.48	-8.31	-0.01
22	SLU 2	-196	109	2118	-4.59	-8.55	-0.01
22	SLU 3	-191	107	2078	-4.48	-8.31	-0.01
22	SLU 4	-194	109	2102	-4.55	-8.46	-0.01
22	SLU 5	-196	109	2118	-4.59	-8.55	-0.01
22	SLU 6	-191	107	2078	-4.48	-8.31	-0.01
22	SLU 7	-194	109	2102	-4.55	-8.46	-0.01
22	SLU 8	-191	107	2078	-4.48	-8.31	-0.01
22	SLU 9	-194	109	2102	-4.55	-8.46	-0.01
22	SLU 10	-231	110	2204	-4.68	-10	-0.01
22	SLU 11	-226	108	2164	-4.58	-9.76	-0.01
22	SLU 12	-229	109	2188	-4.64	-9.9	-0.01
22	SLU 13	-231	110	2204	-4.68	-10	-0.01
22	SLU 14	-226	108	2164	-4.58	-9.76	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
22	SLU 15	-229	109	2188	-4.64	-9.9	-0.01
22	SLU 16	-226	108	2164	-4.58	-9.76	-0.01
22	SLU 17	-229	109	2188	-4.64	-9.9	-0.01
22	SLU 18	-241	108	2200	-4.62	-10.38	0
22	SLU 19	-244	109	2224	-4.68	-10.52	0
22	SLU 20	-241	108	2200	-4.62	-10.38	0
22	SLU 21	-244	109	2224	-4.68	-10.52	0
22	SLU 22	-208	109	2150	-4.6	-9.03	-0.01
22	SLU 23	-213	111	2191	-4.71	-9.27	-0.01
22	SLU 24	-208	109	2150	-4.6	-9.03	-0.01
22	SLU 25	-211	111	2174	-4.66	-9.17	-0.01
22	SLU 26	-213	111	2191	-4.71	-9.27	-0.01
22	SLU 27	-208	109	2150	-4.6	-9.03	-0.01
22	SLU 28	-211	111	2174	-4.66	-9.17	-0.01
22	SLU 29	-208	109	2150	-4.6	-9.03	-0.01
22	SLU 30	-211	111	2174	-4.66	-9.17	-0.01
22	SLU 31	-248	112	2276	-4.8	-10.72	0
22	SLU 32	-243	110	2236	-4.7	-10.48	0
22	SLU 33	-246	111	2260	-4.76	-10.62	0
22	SLU 34	-248	112	2276	-4.8	-10.72	0
22	SLU 35	-243	110	2236	-4.7	-10.48	0
22	SLU 36	-246	111	2260	-4.76	-10.62	0
22	SLU 37	-243	110	2236	-4.7	-10.48	0
22	SLU 38	-246	111	2260	-4.76	-10.62	0
22	SLU 39	-258	110	2273	-4.74	-11.1	0
22	SLU 40	-261	111	2297	-4.8	-11.24	0
22	SLU 41	-258	110	2273	-4.74	-11.1	0
22	SLU 42	-261	111	2297	-4.8	-11.24	0
22	SLU 43	-242	139	2676	-5.79	-10.56	-0.01
22	SLU 44	-247	141	2716	-5.89	-10.8	-0.01
22	SLU 45	-242	139	2676	-5.79	-10.56	-0.01
22	SLU 46	-245	140	2700	-5.85	-10.71	-0.01
22	SLU 47	-247	141	2716	-5.89	-10.8	-0.01
22	SLU 48	-242	139	2676	-5.79	-10.56	-0.01
22	SLU 49	-245	140	2700	-5.85	-10.71	-0.01
22	SLU 50	-242	139	2676	-5.79	-10.56	-0.01
22	SLU 51	-245	140	2700	-5.85	-10.71	-0.01
22	SLU 52	-282	141	2802	-5.99	-12.25	-0.01
22	SLU 53	-278	139	2762	-5.88	-12.01	-0.01
22	SLU 54	-281	140	2786	-5.95	-12.15	-0.01
22	SLU 55	-282	141	2802	-5.99	-12.25	-0.01
22	SLU 56	-278	139	2762	-5.88	-12.01	-0.01
22	SLU 57	-281	140	2786	-5.95	-12.15	-0.01
22	SLU 58	-278	139	2762	-5.88	-12.01	-0.01
22	SLU 59	-281	140	2786	-5.95	-12.15	-0.01
22	SLU 60	-293	139	2799	-5.92	-12.63	-0.01
22	SLU 61	-296	140	2823	-5.99	-12.77	-0.01
22	SLU 62	-293	139	2799	-5.92	-12.63	-0.01
22	SLU 63	-296	140	2823	-5.99	-12.77	-0.01
22	SLU 64	-260	141	2749	-5.91	-11.28	-0.01
22	SLU 65	-265	143	2789	-6.01	-11.52	-0.01
22	SLU 66	-260	141	2749	-5.91	-11.28	-0.01
22	SLU 67	-263	142	2773	-5.97	-11.42	-0.01
22	SLU 68	-265	143	2789	-6.01	-11.52	-0.01
22	SLU 69	-260	141	2749	-5.91	-11.28	-0.01
22	SLU 70	-263	142	2773	-5.97	-11.42	-0.01
22	SLU 71	-260	141	2749	-5.91	-11.28	-0.01
22	SLU 72	-263	142	2773	-5.97	-11.42	-0.01
22	SLU 73	-300	143	2875	-6.1	-12.96	-0.01
22	SLU 74	-295	141	2835	-6	-12.73	-0.01
22	SLU 75	-298	142	2859	-6.06	-12.87	-0.01
22	SLU 76	-300	143	2875	-6.1	-12.96	-0.01
22	SLU 77	-295	141	2835	-6	-12.73	-0.01
22	SLU 78	-298	142	2859	-6.06	-12.87	-0.01
22	SLU 79	-295	141	2835	-6	-12.73	-0.01
22	SLU 80	-298	142	2859	-6.06	-12.87	-0.01
22	SLU 81	-310	141	2871	-6.04	-13.35	-0.01
22	SLU 82	-313	142	2896	-6.1	-13.49	-0.01
22	SLU 83	-310	141	2871	-6.04	-13.35	-0.01
22	SLU 84	-313	142	2896	-6.1	-13.49	-0.01
22	SLE RA 1	-196	108	2098	-4.52	-8.52	-0.01
22	SLE RA 2	-199	109	2125	-4.59	-8.68	-0.01
22	SLE RA 3	-196	108	2098	-4.52	-8.52	-0.01
22	SLE RA 4	-198	109	2114	-4.56	-8.61	-0.01
22	SLE RA 5	-199	109	2125	-4.59	-8.68	-0.01
22	SLE RA 6	-196	108	2098	-4.52	-8.52	-0.01
22	SLE RA 7	-198	109	2114	-4.56	-8.61	-0.01
22	SLE RA 8	-196	108	2098	-4.52	-8.52	-0.01
22	SLE RA 9	-198	109	2114	-4.56	-8.61	-0.01
22	SLE RA 10	-223	109	2182	-4.65	-9.64	-0.01
22	SLE RA 11	-219	108	2156	-4.58	-9.48	-0.01
22	SLE RA 12	-221	109	2172	-4.62	-9.58	-0.01
22	SLE RA 13	-223	109	2182	-4.65	-9.64	-0.01
22	SLE RA 14	-219	108	2156	-4.58	-9.48	-0.01
22	SLE RA 15	-221	109	2172	-4.62	-9.58	-0.01
22	SLE RA 16	-219	108	2156	-4.58	-9.48	-0.01
22	SLE RA 17	-221	109	2172	-4.62	-9.58	-0.01
22	SLE RA 18	-229	108	2180	-4.61	-9.9	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
22	SLE RA 19	-231	109	2196	-4.65	-9.99	-0.01
22	SLE RA 20	-229	108	2180	-4.61	-9.9	-0.01
22	SLE RA 21	-231	109	2196	-4.65	-9.99	-0.01
22	SLE FR 1	-196	108	2098	-4.52	-8.52	-0.01
22	SLE FR 2	-197	108	2104	-4.53	-8.55	-0.01
22	SLE FR 3	-196	108	2098	-4.52	-8.52	-0.01
22	SLE FR 4	-207	108	2128	-4.56	-8.96	-0.01
22	SLE FR 5	-206	108	2123	-4.54	-8.93	-0.01
22	SLE FR 6	-213	108	2139	-4.56	-9.21	-0.01
22	SLE QP 1	-196	108	2098	-4.52	-8.52	-0.01
22	SLE QP 2	-206	108	2123	-4.54	-8.93	-0.01
22	SLD 1	-36	-21	668	2.51	-1.8	0.05
22	SLD 2	-36	-21	668	2.51	-1.8	0.05
22	SLD 3	37	46	1461	-1.13	0.92	0.02
22	SLD 4	37	46	1461	-1.13	0.92	0.02
22	SLD 5	-266	-33	483	3.11	-10.91	0.05
22	SLD 6	-266	-33	483	3.11	-10.91	0.05
22	SLD 7	-22	191	3127	-9.06	-1.86	-0.04
22	SLD 8	-22	191	3127	-9.06	-1.86	-0.04
22	SLD 9	-390	25	1119	-0.03	-16.01	0.02
22	SLD 10	-390	25	1119	-0.03	-16.01	0.02
22	SLD 11	-146	248	3762	-12.2	-6.95	-0.07
22	SLD 12	-146	248	3762	-12.2	-6.95	-0.07
22	SLD 13	-449	170	2785	-7.95	-18.78	-0.04
22	SLD 14	-449	170	2785	-7.95	-18.78	-0.04
22	SLD 15	-376	237	3578	-11.6	-16.06	-0.06
22	SLD 16	-376	237	3578	-11.6	-16.06	-0.06
22	SLV 1	193	-211	-1423	12.96	7.76	0.13
22	SLV 2	193	-211	-1423	12.96	7.76	0.13
22	SLV 3	382	-43	513	3.83	14.77	0.06
22	SLV 4	382	-43	513	3.83	14.77	0.06
22	SLV 5	-374	-242	-1878	14.56	-14.54	0.14
22	SLV 6	-374	-242	-1878	14.56	-14.54	0.14
22	SLV 7	258	317	4577	-15.88	8.8	-0.1
22	SLV 8	258	317	4577	-15.88	8.8	-0.1
22	SLV 9	-670	-101	-331	6.79	-26.66	0.08
22	SLV 10	-670	-101	-331	6.79	-26.66	0.08
22	SLV 11	-38	458	6124	-23.64	-3.32	-0.16
22	SLV 12	-38	458	6124	-23.64	-3.32	-0.16
22	SLV 13	-794	259	3733	-12.91	-32.63	-0.08
22	SLV 14	-794	259	3733	-12.91	-32.63	-0.08
22	SLV 15	-605	427	5669	-22.04	-25.63	-0.15
22	SLV 16	-605	427	5669	-22.04	-25.63	-0.15
23	SLU 1	36	28	1367	-3.28	1.69	-0.02
23	SLU 2	36	28	1392	-3.4	1.72	-0.02
23	SLU 3	36	28	1367	-3.28	1.69	-0.02
23	SLU 4	36	28	1382	-3.35	1.71	-0.02
23	SLU 5	36	28	1392	-3.4	1.72	-0.02
23	SLU 6	36	28	1367	-3.28	1.69	-0.02
23	SLU 7	36	28	1382	-3.35	1.71	-0.02
23	SLU 8	36	28	1367	-3.28	1.69	-0.02
23	SLU 9	36	28	1382	-3.35	1.71	-0.02
23	SLU 10	24	22	1430	-3.3	1.34	-0.02
23	SLU 11	23	21	1405	-3.18	1.3	-0.02
23	SLU 12	23	22	1420	-3.25	1.32	-0.02
23	SLU 13	24	22	1430	-3.3	1.34	-0.02
23	SLU 14	23	21	1405	-3.18	1.3	-0.02
23	SLU 15	23	22	1420	-3.25	1.32	-0.02
23	SLU 16	23	21	1405	-3.18	1.3	-0.02
23	SLU 17	23	22	1420	-3.25	1.32	-0.02
23	SLU 18	17	19	1421	-3.14	1.14	-0.02
23	SLU 19	18	19	1436	-3.21	1.16	-0.02
23	SLU 20	17	19	1421	-3.14	1.14	-0.02
23	SLU 21	18	19	1436	-3.21	1.16	-0.02
23	SLU 22	31	25	1407	-3.29	1.56	-0.02
23	SLU 23	31	26	1431	-3.42	1.59	-0.02
23	SLU 24	31	25	1407	-3.29	1.56	-0.02
23	SLU 25	31	26	1422	-3.37	1.57	-0.02
23	SLU 26	31	26	1431	-3.42	1.59	-0.02
23	SLU 27	31	25	1407	-3.29	1.56	-0.02
23	SLU 28	31	26	1422	-3.37	1.57	-0.02
23	SLU 29	31	25	1407	-3.29	1.56	-0.02
23	SLU 30	31	26	1422	-3.37	1.57	-0.02
23	SLU 31	19	20	1469	-3.32	1.2	-0.02
23	SLU 32	18	19	1444	-3.19	1.17	-0.02
23	SLU 33	18	19	1459	-3.27	1.19	-0.02
23	SLU 34	19	20	1469	-3.32	1.2	-0.02
23	SLU 35	18	19	1444	-3.19	1.17	-0.02
23	SLU 36	18	19	1459	-3.27	1.19	-0.02
23	SLU 37	18	19	1444	-3.19	1.17	-0.02
23	SLU 38	18	19	1459	-3.27	1.19	-0.02
23	SLU 39	13	16	1461	-3.15	1	-0.02
23	SLU 40	13	17	1475	-3.23	1.02	-0.02
23	SLU 41	13	16	1461	-3.15	1	-0.02
23	SLU 42	13	17	1475	-3.23	1.02	-0.02
23	SLU 43	48	37	1764	-4.26	2.25	-0.03
23	SLU 44	49	37	1789	-4.38	2.28	-0.03
23	SLU 45	48	37	1764	-4.26	2.25	-0.03





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
23	SLU 46	48	37	1779	-4.33	2.27	-0.03
23	SLU 47	49	37	1789	-4.38	2.28	-0.03
23	SLU 48	48	37	1764	-4.26	2.25	-0.03
23	SLU 49	48	37	1779	-4.33	2.27	-0.03
23	SLU 50	48	37	1764	-4.26	2.25	-0.03
23	SLU 51	48	37	1779	-4.33	2.27	-0.03
23	SLU 52	36	31	1826	-4.28	1.89	-0.03
23	SLU 53	35	30	1802	-4.16	1.86	-0.03
23	SLU 54	36	31	1816	-4.23	1.88	-0.03
23	SLU 55	36	31	1826	-4.28	1.89	-0.03
23	SLU 56	35	30	1802	-4.16	1.86	-0.03
23	SLU 57	36	31	1816	-4.23	1.88	-0.03
23	SLU 58	35	30	1802	-4.16	1.86	-0.03
23	SLU 59	36	31	1816	-4.23	1.88	-0.03
23	SLU 60	30	28	1818	-4.12	1.69	-0.03
23	SLU 61	30	28	1833	-4.19	1.71	-0.03
23	SLU 62	30	28	1818	-4.12	1.69	-0.03
23	SLU 63	30	28	1833	-4.19	1.71	-0.03
23	SLU 64	43	34	1804	-4.27	2.11	-0.03
23	SLU 65	44	35	1828	-4.4	2.14	-0.03
23	SLU 66	43	34	1804	-4.27	2.11	-0.03
23	SLU 67	43	35	1818	-4.35	2.13	-0.03
23	SLU 68	44	35	1828	-4.4	2.14	-0.03
23	SLU 69	43	34	1804	-4.27	2.11	-0.03
23	SLU 70	43	35	1818	-4.35	2.13	-0.03
23	SLU 71	43	34	1804	-4.27	2.11	-0.03
23	SLU 72	43	35	1818	-4.35	2.13	-0.03
23	SLU 73	31	29	1866	-4.3	1.75	-0.03
23	SLU 74	30	28	1841	-4.17	1.72	-0.03
23	SLU 75	31	28	1856	-4.25	1.74	-0.03
23	SLU 76	31	29	1866	-4.3	1.75	-0.03
23	SLU 77	30	28	1841	-4.17	1.72	-0.03
23	SLU 78	31	28	1856	-4.25	1.74	-0.03
23	SLU 79	30	28	1841	-4.17	1.72	-0.03
23	SLU 80	31	28	1856	-4.25	1.74	-0.03
23	SLU 81	25	25	1857	-4.13	1.56	-0.03
23	SLU 82	25	26	1872	-4.2	1.58	-0.03
23	SLU 83	25	25	1857	-4.13	1.56	-0.03
23	SLU 84	25	26	1872	-4.2	1.58	-0.03
23	SLE RA 1	34	27	1379	-3.28	1.65	-0.02
23	SLE RA 2	35	27	1395	-3.37	1.68	-0.02
23	SLE RA 3	34	27	1379	-3.28	1.65	-0.02
23	SLE RA 4	34	27	1388	-3.33	1.67	-0.02
23	SLE RA 5	35	27	1395	-3.37	1.68	-0.02
23	SLE RA 6	34	27	1379	-3.28	1.65	-0.02
23	SLE RA 7	34	27	1388	-3.33	1.67	-0.02
23	SLE RA 8	34	27	1379	-3.28	1.65	-0.02
23	SLE RA 9	34	27	1388	-3.33	1.67	-0.02
23	SLE RA 10	26	23	1420	-3.3	1.42	-0.02
23	SLE RA 11	26	23	1404	-3.22	1.4	-0.02
23	SLE RA 12	26	23	1414	-3.27	1.41	-0.02
23	SLE RA 13	26	23	1420	-3.3	1.42	-0.02
23	SLE RA 14	26	23	1404	-3.22	1.4	-0.02
23	SLE RA 15	26	23	1414	-3.27	1.41	-0.02
23	SLE RA 16	26	23	1404	-3.22	1.4	-0.02
23	SLE RA 17	26	23	1414	-3.27	1.41	-0.02
23	SLE RA 18	22	21	1414	-3.19	1.28	-0.02
23	SLE RA 19	22	21	1424	-3.24	1.3	-0.02
23	SLE RA 20	22	21	1414	-3.19	1.28	-0.02
23	SLE RA 21	22	21	1424	-3.24	1.3	-0.02
23	SLE FR 1	34	27	1379	-3.28	1.65	-0.02
23	SLE FR 2	34	27	1382	-3.3	1.66	-0.02
23	SLE FR 3	34	27	1379	-3.28	1.65	-0.02
23	SLE FR 4	31	25	1393	-3.27	1.55	-0.02
23	SLE FR 5	31	25	1389	-3.26	1.54	-0.02
23	SLE FR 6	28	24	1397	-3.24	1.47	-0.02
23	SLE QP 1	34	27	1379	-3.28	1.65	-0.02
23	SLE QP 2	31	25	1389	-3.26	1.54	-0.02
23	SLD 1	-217	-110	710	5.61	-11.36	-0.01
23	SLD 2	-217	-110	710	5.61	-11.36	-0.01
23	SLD 3	-107	-48	1081	1.25	-5.44	-0.02
23	SLD 4	-107	-48	1081	1.25	-5.44	-0.02
23	SLD 5	-211	-108	623	6.01	-11.3	0
23	SLD 6	-211	-108	623	6.01	-11.3	0
23	SLD 7	156	96	1860	-8.51	8.42	-0.03
23	SLD 8	156	96	1860	-8.51	8.42	-0.03
23	SLD 9	-95	-46	919	2	-5.33	-0.01
23	SLD 10	-95	-46	919	2	-5.33	-0.01
23	SLD 11	272	158	2156	-12.52	14.38	-0.04
23	SLD 12	272	158	2156	-12.52	14.38	-0.04
23	SLD 13	168	99	1698	-7.76	8.53	-0.02
23	SLD 14	168	99	1698	-7.76	8.53	-0.02
23	SLD 15	278	160	2069	-12.12	14.44	-0.03
23	SLD 16	278	160	2069	-12.12	14.44	-0.03
23	SLV 1	-581	-308	-260	18.68	-30.39	0.01
23	SLV 2	-581	-308	-260	18.68	-30.39	0.01
23	SLV 3	-301	-153	640	7.77	-15.35	-0.01
23	SLV 4	-301	-153	640	7.77	-15.35	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
23	SLV 5	-577	-310	-472	19.88	-30.85	0.02
23	SLV 6	-577	-310	-472	19.88	-30.85	0.02
23	SLV 7	356	207	2531	-16.5	19.29	-0.05
23	SLV 8	356	207	2531	-16.5	19.29	-0.05
23	SLV 9	-295	-157	248	9.99	-16.2	0.01
23	SLV 10	-295	-157	248	9.99	-16.2	0.01
23	SLV 11	639	360	3250	-26.39	33.94	-0.06
23	SLV 12	639	360	3250	-26.39	33.94	-0.06
23	SLV 13	362	203	2139	-14.28	18.43	-0.03
23	SLV 14	362	203	2139	-14.28	18.43	-0.03
23	SLV 15	642	358	3039	-25.19	33.47	-0.05
23	SLV 16	642	358	3039	-25.19	33.47	-0.05
24	SLU 1	2	3	1297	-1.17	-0.34	0
24	SLU 2	3	4	1318	-1.29	-0.34	0
24	SLU 3	2	3	1297	-1.17	-0.34	0
24	SLU 4	3	3	1310	-1.24	-0.34	0
24	SLU 5	3	4	1318	-1.29	-0.34	0
24	SLU 6	2	3	1297	-1.17	-0.34	0
24	SLU 7	3	3	1310	-1.24	-0.34	0
24	SLU 8	2	3	1297	-1.17	-0.34	0
24	SLU 9	3	3	1310	-1.24	-0.34	0
24	SLU 10	-11	-4	1337	-0.95	-1.02	0
24	SLU 11	-12	-4	1316	-0.84	-1.03	0
24	SLU 12	-11	-4	1329	-0.91	-1.02	0
24	SLU 13	-11	-4	1337	-0.95	-1.02	0
24	SLU 14	-12	-4	1316	-0.84	-1.03	0
24	SLU 15	-11	-4	1329	-0.91	-1.02	0
24	SLU 16	-12	-4	1316	-0.84	-1.03	0
24	SLU 17	-11	-4	1329	-0.91	-1.02	0
24	SLU 18	-18	-8	1324	-0.69	-1.32	0
24	SLU 19	-17	-7	1337	-0.76	-1.32	0
24	SLU 20	-18	-8	1324	-0.69	-1.32	0
24	SLU 21	-17	-7	1337	-0.76	-1.32	0
24	SLU 22	-4	0	1326	-1.06	-0.64	0
24	SLU 23	-3	1	1347	-1.17	-0.63	0
24	SLU 24	-4	0	1326	-1.06	-0.64	0
24	SLU 25	-3	0	1339	-1.12	-0.63	0
24	SLU 26	-3	1	1347	-1.17	-0.63	0
24	SLU 27	-4	0	1326	-1.06	-0.64	0
24	SLU 28	-3	0	1339	-1.12	-0.63	0
24	SLU 29	-4	0	1326	-1.06	-0.64	0
24	SLU 30	-3	0	1339	-1.12	-0.63	0
24	SLU 31	-17	-7	1366	-0.83	-1.32	0
24	SLU 32	-18	-8	1345	-0.72	-1.32	0
24	SLU 33	-18	-7	1358	-0.79	-1.32	0
24	SLU 34	-17	-7	1366	-0.83	-1.32	0
24	SLU 35	-18	-8	1345	-0.72	-1.32	0
24	SLU 36	-18	-7	1358	-0.79	-1.32	0
24	SLU 37	-18	-8	1345	-0.72	-1.32	0
24	SLU 38	-18	-7	1358	-0.79	-1.32	0
24	SLU 39	-24	-11	1353	-0.57	-1.62	0
24	SLU 40	-24	-10	1366	-0.64	-1.61	0
24	SLU 41	-24	-11	1353	-0.57	-1.62	0
24	SLU 42	-24	-10	1366	-0.64	-1.61	0
24	SLU 43	5	5	1677	-1.57	-0.34	0
24	SLU 44	6	6	1698	-1.68	-0.34	0
24	SLU 45	5	5	1677	-1.57	-0.34	0
24	SLU 46	6	6	1689	-1.64	-0.34	0
24	SLU 47	6	6	1698	-1.68	-0.34	0
24	SLU 48	5	5	1677	-1.57	-0.34	0
24	SLU 49	6	6	1689	-1.64	-0.34	0
24	SLU 50	5	5	1677	-1.57	-0.34	0
24	SLU 51	6	6	1689	-1.64	-0.34	0
24	SLU 52	-8	-2	1716	-1.35	-1.02	0
24	SLU 53	-9	-2	1695	-1.23	-1.03	0
24	SLU 54	-9	-2	1708	-1.3	-1.02	0
24	SLU 55	-8	-2	1716	-1.35	-1.02	0
24	SLU 56	-9	-2	1695	-1.23	-1.03	0
24	SLU 57	-9	-2	1708	-1.3	-1.02	0
24	SLU 58	-9	-2	1695	-1.23	-1.03	0
24	SLU 59	-9	-2	1708	-1.3	-1.02	0
24	SLU 60	-15	-6	1703	-1.09	-1.32	0
24	SLU 61	-15	-5	1716	-1.16	-1.32	0
24	SLU 62	-15	-6	1703	-1.09	-1.32	0
24	SLU 63	-15	-5	1716	-1.16	-1.32	0
24	SLU 64	-1	2	1705	-1.45	-0.64	0
24	SLU 65	0	3	1727	-1.56	-0.63	0
24	SLU 66	-1	2	1705	-1.45	-0.64	0
24	SLU 67	-1	2	1718	-1.52	-0.63	0
24	SLU 68	0	3	1727	-1.56	-0.63	0
24	SLU 69	-1	2	1705	-1.45	-0.64	0
24	SLU 70	-1	2	1718	-1.52	-0.63	0
24	SLU 71	-1	2	1705	-1.45	-0.64	0
24	SLU 72	-1	2	1718	-1.52	-0.63	0
24	SLU 73	-14	-5	1745	-1.23	-1.32	0
24	SLU 74	-15	-6	1724	-1.11	-1.32	0
24	SLU 75	-15	-5	1737	-1.18	-1.32	0
24	SLU 76	-14	-5	1745	-1.23	-1.32	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
24	SLU 77	-15	-6	1724	-1.11	-1.32	0
24	SLU 78	-15	-5	1737	-1.18	-1.32	0
24	SLU 79	-15	-6	1724	-1.11	-1.32	0
24	SLU 80	-15	-5	1737	-1.18	-1.32	0
24	SLU 81	-21	-9	1732	-0.97	-1.62	0
24	SLU 82	-21	-8	1745	-1.04	-1.61	0
24	SLU 83	-21	-9	1732	-0.97	-1.62	0
24	SLU 84	-21	-8	1745	-1.04	-1.61	0
24	SLE RA 1	0	2	1306	-1.14	-0.42	0
24	SLE RA 2	1	3	1320	-1.22	-0.42	0
24	SLE RA 3	0	2	1306	-1.14	-0.42	0
24	SLE RA 4	1	2	1314	-1.19	-0.42	0
24	SLE RA 5	1	3	1320	-1.22	-0.42	0
24	SLE RA 6	0	2	1306	-1.14	-0.42	0
24	SLE RA 7	1	2	1314	-1.19	-0.42	0
24	SLE RA 8	0	2	1306	-1.14	-0.42	0
24	SLE RA 9	1	2	1314	-1.19	-0.42	0
24	SLE RA 10	-8	-2	1332	-0.99	-0.88	0
24	SLE RA 11	-9	-3	1318	-0.92	-0.88	0
24	SLE RA 12	-9	-3	1326	-0.96	-0.88	0
24	SLE RA 13	-8	-2	1332	-0.99	-0.88	0
24	SLE RA 14	-9	-3	1318	-0.92	-0.88	0
24	SLE RA 15	-9	-3	1326	-0.96	-0.88	0
24	SLE RA 16	-9	-3	1318	-0.92	-0.88	0
24	SLE RA 17	-9	-3	1326	-0.96	-0.88	0
24	SLE RA 18	-13	-5	1323	-0.82	-1.08	0
24	SLE RA 19	-13	-5	1332	-0.87	-1.08	0
24	SLE RA 20	-13	-5	1323	-0.82	-1.08	0
24	SLE RA 21	-13	-5	1332	-0.87	-1.08	0
24	SLE FR 1	0	2	1306	-1.14	-0.42	0
24	SLE FR 2	1	2	1308	-1.16	-0.42	0
24	SLE FR 3	0	2	1306	-1.14	-0.42	0
24	SLE FR 4	-3	0	1314	-1.06	-0.62	0
24	SLE FR 5	-4	0	1311	-1.04	-0.62	0
24	SLE FR 6	-6	-1	1314	-0.98	-0.75	0
24	SLE QP 1	0	2	1306	-1.14	-0.42	0
24	SLE QP 2	-4	0	1311	-1.04	-0.62	0
24	SLD 1	-258	-136	1160	6.93	-13.28	0
24	SLD 2	-258	-136	1160	6.93	-13.28	0
24	SLD 3	-143	-74	991	3.12	-7.39	0
24	SLD 4	-143	-74	991	3.12	-7.39	0
24	SLD 5	-255	-134	1523	7.13	-13.35	0
24	SLD 6	-255	-134	1523	7.13	-13.35	0
24	SLD 7	129	71	958	-5.58	6.28	0.01
24	SLD 8	129	71	958	-5.58	6.28	0.01
24	SLD 9	-136	-71	1664	3.49	-7.53	0
24	SLD 10	-136	-71	1664	3.49	-7.53	0
24	SLD 11	248	134	1099	-9.22	12.11	0.01
24	SLD 12	248	134	1099	-9.22	12.11	0.01
24	SLD 13	136	74	1631	-5.21	6.15	0.01
24	SLD 14	136	74	1631	-5.21	6.15	0.01
24	SLD 15	251	136	1461	-9.02	12.04	0.01
24	SLD 16	251	136	1461	-9.02	12.04	0.01
24	SLV 1	-635	-336	949	18.73	-31.98	-0.01
24	SLV 2	-635	-336	949	18.73	-31.98	-0.01
24	SLV 3	-342	-180	550	9.19	-16.96	-0.01
24	SLV 4	-342	-180	550	9.19	-16.96	-0.01
24	SLV 5	-637	-337	1807	19.36	-32.81	-0.01
24	SLV 6	-637	-337	1807	19.36	-32.81	-0.01
24	SLV 7	339	182	478	-12.45	17.26	0.01
24	SLV 8	339	182	478	-12.45	17.26	0.01
24	SLV 9	-346	-182	2144	10.36	-18.5	0
24	SLV 10	-346	-182	2144	10.36	-18.5	0
24	SLV 11	630	337	814	-21.45	31.57	0.02
24	SLV 12	630	337	814	-21.45	31.57	0.02
24	SLV 13	335	180	2072	-11.28	15.72	0.01
24	SLV 14	335	180	2072	-11.28	15.72	0.01
24	SLV 15	628	336	1673	-20.82	30.74	0.02
24	SLV 16	628	336	1673	-20.82	30.74	0.02
25	SLU 1	0	203	1085	-6.33	-0.16	0
25	SLU 2	0	196	1084	-6.07	-0.16	0
25	SLU 3	0	203	1085	-6.33	-0.16	0
25	SLU 4	0	199	1084	-6.17	-0.16	0
25	SLU 5	0	196	1084	-6.07	-0.16	0
25	SLU 6	0	203	1085	-6.33	-0.16	0
25	SLU 7	0	199	1084	-6.17	-0.16	0
25	SLU 8	0	203	1085	-6.33	-0.16	0
25	SLU 9	0	199	1084	-6.17	-0.16	0
25	SLU 10	-1	352	1387	-8.53	-0.21	0
25	SLU 11	-1	359	1389	-8.78	-0.21	0
25	SLU 12	-1	355	1388	-8.63	-0.21	0
25	SLU 13	-1	352	1387	-8.53	-0.21	0
25	SLU 14	-1	359	1389	-8.78	-0.21	0
25	SLU 15	-1	355	1388	-8.63	-0.21	0
25	SLU 16	-1	359	1389	-8.78	-0.21	0
25	SLU 17	-1	355	1388	-8.63	-0.21	0
25	SLU 18	-1	426	1519	-9.84	-0.23	0
25	SLU 19	-1	422	1518	-9.68	-0.23	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
25	SLU 20	-1	426	1519	-9.84	-0.23	0
25	SLU 21	-1	422	1518	-9.68	-0.23	0
25	SLU 22	-1	266	1220	-7.35	-0.18	0
25	SLU 23	-1	259	1219	-7.09	-0.18	0
25	SLU 24	-1	266	1220	-7.35	-0.18	0
25	SLU 25	-1	261	1219	-7.19	-0.18	0
25	SLU 26	-1	259	1219	-7.09	-0.18	0
25	SLU 27	-1	266	1220	-7.35	-0.18	0
25	SLU 28	-1	261	1219	-7.19	-0.18	0
25	SLU 29	-1	266	1220	-7.35	-0.18	0
25	SLU 30	-1	261	1219	-7.19	-0.18	0
25	SLU 31	-1	415	1522	-9.55	-0.23	0
25	SLU 32	-1	422	1524	-9.8	-0.23	0
25	SLU 33	-1	418	1523	-9.65	-0.23	0
25	SLU 34	-1	415	1522	-9.55	-0.23	0
25	SLU 35	-1	422	1524	-9.8	-0.23	0
25	SLU 36	-1	418	1523	-9.65	-0.23	0
25	SLU 37	-1	422	1524	-9.8	-0.23	0
25	SLU 38	-1	418	1523	-9.65	-0.23	0
25	SLU 39	-1	489	1654	-10.86	-0.25	0
25	SLU 40	-1	484	1653	-10.7	-0.25	0
25	SLU 41	-1	489	1654	-10.86	-0.25	0
25	SLU 42	-1	484	1653	-10.7	-0.25	0
25	SLU 43	-1	242	1365	-7.88	-0.21	0
25	SLU 44	-1	235	1363	-7.62	-0.21	0
25	SLU 45	-1	242	1365	-7.88	-0.21	0
25	SLU 46	-1	238	1364	-7.72	-0.21	0
25	SLU 47	-1	235	1363	-7.62	-0.21	0
25	SLU 48	-1	242	1365	-7.88	-0.21	0
25	SLU 49	-1	238	1364	-7.72	-0.21	0
25	SLU 50	-1	242	1365	-7.88	-0.21	0
25	SLU 51	-1	238	1364	-7.72	-0.21	0
25	SLU 52	-1	391	1667	-10.08	-0.25	0
25	SLU 53	-1	398	1668	-10.33	-0.25	0
25	SLU 54	-1	394	1667	-10.18	-0.25	0
25	SLU 55	-1	391	1667	-10.08	-0.25	0
25	SLU 56	-1	398	1668	-10.33	-0.25	0
25	SLU 57	-1	394	1667	-10.18	-0.25	0
25	SLU 58	-1	398	1668	-10.33	-0.25	0
25	SLU 59	-1	394	1667	-10.18	-0.25	0
25	SLU 60	-1	465	1799	-11.38	-0.27	0
25	SLU 61	-1	461	1798	-11.23	-0.27	0
25	SLU 62	-1	465	1799	-11.38	-0.27	0
25	SLU 63	-1	461	1798	-11.23	-0.27	0
25	SLU 64	-1	305	1500	-8.9	-0.23	0
25	SLU 65	-1	298	1498	-8.64	-0.23	0
25	SLU 66	-1	305	1500	-8.9	-0.23	0
25	SLU 67	-1	301	1499	-8.74	-0.23	0
25	SLU 68	-1	298	1498	-8.64	-0.23	0
25	SLU 69	-1	305	1500	-8.9	-0.23	0
25	SLU 70	-1	301	1499	-8.74	-0.23	0
25	SLU 71	-1	305	1500	-8.9	-0.23	0
25	SLU 72	-1	301	1499	-8.74	-0.23	0
25	SLU 73	-1	454	1802	-11.1	-0.27	0
25	SLU 74	-1	461	1804	-11.35	-0.27	0
25	SLU 75	-1	457	1803	-11.2	-0.27	0
25	SLU 76	-1	454	1802	-11.1	-0.27	0
25	SLU 77	-1	461	1804	-11.35	-0.27	0
25	SLU 78	-1	457	1803	-11.2	-0.27	0
25	SLU 79	-1	461	1804	-11.35	-0.27	0
25	SLU 80	-1	457	1803	-11.2	-0.27	0
25	SLU 81	-1	528	1934	-12.4	-0.29	0
25	SLU 82	-1	524	1933	-12.25	-0.29	0
25	SLU 83	-1	528	1934	-12.4	-0.29	0
25	SLU 84	-1	524	1933	-12.25	-0.29	0
25	SLE RA 1	-1	221	1124	-6.62	-0.17	0
25	SLE RA 2	0	216	1123	-6.45	-0.17	0
25	SLE RA 3	-1	221	1124	-6.62	-0.17	0
25	SLE RA 4	0	218	1123	-6.52	-0.17	0
25	SLE RA 5	0	216	1123	-6.45	-0.17	0
25	SLE RA 6	-1	221	1124	-6.62	-0.17	0
25	SLE RA 7	0	218	1123	-6.52	-0.17	0
25	SLE RA 8	-1	221	1124	-6.62	-0.17	0
25	SLE RA 9	0	218	1123	-6.52	-0.17	0
25	SLE RA 10	-1	320	1325	-8.09	-0.2	0
25	SLE RA 11	-1	325	1326	-8.26	-0.2	0
25	SLE RA 12	-1	322	1326	-8.15	-0.2	0
25	SLE RA 13	-1	320	1325	-8.09	-0.2	0
25	SLE RA 14	-1	325	1326	-8.26	-0.2	0
25	SLE RA 15	-1	322	1326	-8.15	-0.2	0
25	SLE RA 16	-1	325	1326	-8.26	-0.2	0
25	SLE RA 17	-1	322	1326	-8.15	-0.2	0
25	SLE RA 18	-1	370	1413	-8.96	-0.21	0
25	SLE RA 19	-1	367	1413	-8.86	-0.21	0
25	SLE RA 20	-1	370	1413	-8.96	-0.21	0
25	SLE RA 21	-1	367	1413	-8.86	-0.21	0
25	SLE FR 1	-1	221	1124	-6.62	-0.17	0
25	SLE FR 2	-1	220	1124	-6.58	-0.17	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
25	SLE FR 3	-1	221	1124	-6.62	-0.17	0
25	SLE FR 4	-1	264	1211	-7.29	-0.18	0
25	SLE FR 5	-1	265	1211	-7.32	-0.18	0
25	SLE FR 6	-1	295	1269	-7.79	-0.19	0
25	SLE QP 1	-1	221	1124	-6.62	-0.17	0
25	SLE QP 2	-1	265	1211	-7.32	-0.18	0
25	SLD 1	-9	475	946	-17.44	1.48	0
25	SLD 2	-9	475	946	-17.44	1.48	0
25	SLD 3	-7	274	1110	-7.75	1.03	0
25	SLD 4	-7	274	1110	-7.75	1.03	0
25	SLD 5	-5	632	882	-25.07	1	0
25	SLD 6	-5	632	882	-25.07	1	0
25	SLD 7	-1	-36	1430	7.26	-0.5	0
25	SLD 8	-1	-36	1430	7.26	-0.5	0
25	SLD 9	0	567	992	-21.9	0.14	0
25	SLD 10	0	567	992	-21.9	0.14	0
25	SLD 11	4	-101	1539	10.42	-1.37	-0.01
25	SLD 12	4	-101	1539	10.42	-1.37	-0.01
25	SLD 13	6	257	1311	-6.9	-1.4	-0.01
25	SLD 14	6	257	1311	-6.9	-1.4	-0.01
25	SLD 15	8	56	1476	2.8	-1.85	-0.01
25	SLD 16	8	56	1476	2.8	-1.85	-0.01
25	SLV 1	-21	757	586	-31.03	4.03	0.01
25	SLV 2	-21	757	586	-31.03	4.03	0.01
25	SLV 3	-18	286	970	-8.29	2.87	0.01
25	SLV 4	-18	286	970	-8.29	2.87	0.01
25	SLV 5	-12	1128	440	-48.92	2.84	0.01
25	SLV 6	-12	1128	440	-48.92	2.84	0.01
25	SLV 7	-1	-443	1722	26.88	-1.03	0
25	SLV 8	-1	-443	1722	26.88	-1.03	0
25	SLV 9	0	974	700	-41.52	0.66	0
25	SLV 10	0	974	700	-41.52	0.66	0
25	SLV 11	11	-597	1981	34.28	-3.21	-0.01
25	SLV 12	11	-597	1981	34.28	-3.21	-0.01
25	SLV 13	17	245	1452	-6.35	-3.23	-0.01
25	SLV 14	17	245	1452	-6.35	-3.23	-0.01
25	SLV 15	20	-226	1836	16.39	-4.39	-0.02
25	SLV 16	20	-226	1836	16.39	-4.39	-0.02
26	SLU 1	3	244	1929	-12.92	1.06	0.01
26	SLU 2	2	240	1903	-12.71	-0.08	0.01
26	SLU 3	3	244	1929	-12.92	1.06	0.01
26	SLU 4	3	241	1913	-12.79	0.37	0.01
26	SLU 5	2	240	1903	-12.71	-0.08	0.01
26	SLU 6	3	244	1929	-12.92	1.06	0.01
26	SLU 7	3	241	1913	-12.79	0.37	0.01
26	SLU 8	3	244	1929	-12.92	1.06	0.01
26	SLU 9	3	241	1913	-12.79	0.37	0.01
26	SLU 10	3	289	2288	-15.56	0.3	0.01
26	SLU 11	4	294	2314	-15.77	1.44	0.01
26	SLU 12	4	291	2298	-15.64	0.76	0.01
26	SLU 13	3	289	2288	-15.56	0.3	0.01
26	SLU 14	4	294	2314	-15.77	1.44	0.01
26	SLU 15	4	291	2298	-15.64	0.76	0.01
26	SLU 16	4	294	2314	-15.77	1.44	0.01
26	SLU 17	4	291	2298	-15.64	0.76	0.01
26	SLU 18	5	315	2479	-17	1.61	0.01
26	SLU 19	4	313	2463	-16.87	0.92	0.01
26	SLU 20	5	315	2479	-17	1.61	0.01
26	SLU 21	4	313	2463	-16.87	0.92	0.01
26	SLU 22	4	266	2107	-14.2	1.23	0.01
26	SLU 23	3	262	2081	-13.99	0.09	0.01
26	SLU 24	4	266	2107	-14.2	1.23	0.01
26	SLU 25	3	263	2092	-14.07	0.55	0.01
26	SLU 26	3	262	2081	-13.99	0.09	0.01
26	SLU 27	4	266	2107	-14.2	1.23	0.01
26	SLU 28	3	263	2092	-14.07	0.55	0.01
26	SLU 29	4	266	2107	-14.2	1.23	0.01
26	SLU 30	3	263	2092	-14.07	0.55	0.01
26	SLU 31	4	312	2466	-16.84	0.48	0.01
26	SLU 32	5	316	2492	-17.05	1.61	0.01
26	SLU 33	4	313	2476	-16.92	0.93	0.01
26	SLU 34	4	312	2466	-16.84	0.48	0.01
26	SLU 35	5	316	2492	-17.05	1.61	0.01
26	SLU 36	4	313	2476	-16.92	0.93	0.01
26	SLU 37	5	316	2492	-17.05	1.61	0.01
26	SLU 38	4	313	2476	-16.92	0.93	0.01
26	SLU 39	5	337	2657	-18.28	1.78	0.01
26	SLU 40	5	335	2641	-18.15	1.1	0.01
26	SLU 41	5	337	2657	-18.28	1.78	0.01
26	SLU 42	5	335	2641	-18.15	1.1	0.01
26	SLU 43	4	309	2447	-16.36	1.31	0.01
26	SLU 44	3	305	2421	-16.14	0.18	0.01
26	SLU 45	4	309	2447	-16.36	1.31	0.01
26	SLU 46	3	307	2431	-16.23	0.63	0.01
26	SLU 47	3	305	2421	-16.14	0.18	0.01
26	SLU 48	4	309	2447	-16.36	1.31	0.01
26	SLU 49	3	307	2431	-16.23	0.63	0.01
26	SLU 50	4	309	2447	-16.36	1.31	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
26	SLU 51	3	307	2431	-16.23	0.63	0.01
26	SLU 52	4	355	2805	-18.99	0.56	0.01
26	SLU 53	5	359	2831	-19.21	1.7	0.01
26	SLU 54	4	357	2816	-19.08	1.02	0.01
26	SLU 55	4	355	2805	-18.99	0.56	0.01
26	SLU 56	5	359	2831	-19.21	1.7	0.01
26	SLU 57	4	357	2816	-19.08	1.02	0.01
26	SLU 58	5	359	2831	-19.21	1.7	0.01
26	SLU 59	4	357	2816	-19.08	1.02	0.01
26	SLU 60	6	381	2996	-20.43	1.86	0.01
26	SLU 61	5	378	2981	-20.3	1.18	0.01
26	SLU 62	6	381	2996	-20.43	1.86	0.01
26	SLU 63	5	378	2981	-20.3	1.18	0.01
26	SLU 64	5	332	2625	-17.64	1.49	0.01
26	SLU 65	3	327	2599	-17.42	0.35	0.01
26	SLU 66	5	332	2625	-17.64	1.49	0.01
26	SLU 67	4	329	2609	-17.51	0.8	0.01
26	SLU 68	3	327	2599	-17.42	0.35	0.01
26	SLU 69	5	332	2625	-17.64	1.49	0.01
26	SLU 70	4	329	2609	-17.51	0.8	0.01
26	SLU 71	5	332	2625	-17.64	1.49	0.01
26	SLU 72	4	329	2609	-17.51	0.8	0.01
26	SLU 73	4	377	2984	-20.28	0.73	0.01
26	SLU 74	6	381	3010	-20.49	1.87	0.01
26	SLU 75	5	379	2994	-20.36	1.19	0.01
26	SLU 76	4	377	2984	-20.28	0.73	0.01
26	SLU 77	6	381	3010	-20.49	1.87	0.01
26	SLU 78	5	379	2994	-20.36	1.19	0.01
26	SLU 79	6	381	3010	-20.49	1.87	0.01
26	SLU 80	5	379	2994	-20.36	1.19	0.01
26	SLU 81	6	403	3174	-21.71	2.04	0.01
26	SLU 82	5	400	3159	-21.58	1.35	0.01
26	SLU 83	6	403	3174	-21.71	2.04	0.01
26	SLU 84	5	400	3159	-21.58	1.35	0.01
26	SLE RA 1	3	250	1980	-13.29	1.1	0.01
26	SLE RA 2	3	247	1963	-13.14	0.35	0.01
26	SLE RA 3	3	250	1980	-13.29	1.1	0.01
26	SLE RA 4	3	248	1970	-13.2	0.65	0.01
26	SLE RA 5	3	247	1963	-13.14	0.35	0.01
26	SLE RA 6	3	250	1980	-13.29	1.1	0.01
26	SLE RA 7	3	248	1970	-13.2	0.65	0.01
26	SLE RA 8	3	250	1980	-13.29	1.1	0.01
26	SLE RA 9	3	248	1970	-13.2	0.65	0.01
26	SLE RA 10	3	281	2219	-15.04	0.6	0.01
26	SLE RA 11	4	283	2236	-15.19	1.36	0.01
26	SLE RA 12	4	282	2226	-15.1	0.91	0.01
26	SLE RA 13	3	281	2219	-15.04	0.6	0.01
26	SLE RA 14	4	283	2236	-15.19	1.36	0.01
26	SLE RA 15	4	282	2226	-15.1	0.91	0.01
26	SLE RA 16	4	283	2236	-15.19	1.36	0.01
26	SLE RA 17	4	282	2226	-15.1	0.91	0.01
26	SLE RA 18	4	298	2346	-16	1.47	0.01
26	SLE RA 19	4	296	2336	-15.92	1.02	0.01
26	SLE RA 20	4	298	2346	-16	1.47	0.01
26	SLE RA 21	4	296	2336	-15.92	1.02	0.01
26	SLE FR 1	3	250	1980	-13.29	1.1	0.01
26	SLE FR 2	3	250	1976	-13.26	0.95	0.01
26	SLE FR 3	3	250	1980	-13.29	1.1	0.01
26	SLE FR 4	4	264	2086	-14.07	1.06	0.01
26	SLE FR 5	4	264	2090	-14.1	1.21	0.01
26	SLE FR 6	4	274	2163	-14.65	1.29	0.01
26	SLE QP 1	3	250	1980	-13.29	1.1	0.01
26	SLE QP 2	4	264	2090	-14.1	1.21	0.01
26	SLD 1	4	264	2463	-14.62	2.28	0.01
26	SLD 2	4	264	2463	-14.62	2.28	0.01
26	SLD 3	11	177	2303	-10.48	5.42	-0.02
26	SLD 4	11	177	2303	-10.48	5.42	-0.02
26	SLD 5	-7	397	2444	-20.54	-3.23	0.04
26	SLD 6	-7	397	2444	-20.54	-3.23	0.04
26	SLD 7	17	105	1911	-6.73	7.24	-0.03
26	SLD 8	17	105	1911	-6.73	7.24	-0.03
26	SLD 9	-9	423	2268	-21.48	-4.81	0.05
26	SLD 10	-9	423	2268	-21.48	-4.81	0.05
26	SLD 11	14	132	1736	-7.66	5.66	-0.03
26	SLD 12	14	132	1736	-7.66	5.66	-0.03
26	SLD 13	-4	352	1877	-17.73	-2.99	0.03
26	SLD 14	-4	352	1877	-17.73	-2.99	0.03
26	SLD 15	3	265	1717	-13.59	0.15	0.01
26	SLD 16	3	265	1717	-13.59	0.15	0.01
26	SLV 1	5	264	2978	-15.34	3.55	0.01
26	SLV 2	5	264	2978	-15.34	3.55	0.01
26	SLV 3	23	57	2587	-5.56	11.7	-0.05
26	SLV 4	23	57	2587	-5.56	11.7	-0.05
26	SLV 5	-23	578	2949	-29.31	-10.45	0.09
26	SLV 6	-23	578	2949	-29.31	-10.45	0.09
26	SLV 7	37	-111	1647	3.3	16.72	-0.1
26	SLV 8	37	-111	1647	3.3	16.72	-0.1
26	SLV 9	-29	640	2533	-31.5	-14.29	0.11



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
26	SLV 10	-29	640	2533	-31.5	-14.29	0.11
26	SLV 11	31	-49	1231	1.11	12.88	-0.08
26	SLV 12	31	-49	1231	1.11	12.88	-0.08
26	SLV 13	-15	472	1592	-22.65	-9.27	0.06
26	SLV 14	-15	472	1592	-22.65	-9.27	0.06
26	SLV 15	3	265	1202	-12.87	-1.12	0
26	SLV 16	3	265	1202	-12.87	-1.12	0
27	SLU 1	-47	-23	1293	0.3	-2.51	0
27	SLU 2	-46	-23	1313	0.19	-2.53	0
27	SLU 3	-47	-23	1293	0.3	-2.51	0
27	SLU 4	-46	-23	1305	0.23	-2.52	0
27	SLU 5	-46	-23	1313	0.19	-2.53	0
27	SLU 6	-47	-23	1293	0.3	-2.51	0
27	SLU 7	-46	-23	1305	0.23	-2.52	0
27	SLU 8	-47	-23	1293	0.3	-2.51	0
27	SLU 9	-46	-23	1305	0.23	-2.52	0
27	SLU 10	-58	-30	1317	0.38	-2.84	0
27	SLU 11	-59	-30	1297	0.48	-2.82	0
27	SLU 12	-59	-30	1309	0.42	-2.84	0
27	SLU 13	-58	-30	1317	0.38	-2.84	0
27	SLU 14	-59	-30	1297	0.48	-2.82	0
27	SLU 15	-59	-30	1309	0.42	-2.84	0
27	SLU 16	-59	-30	1297	0.48	-2.82	0
27	SLU 17	-59	-30	1309	0.42	-2.84	0
27	SLU 18	-64	-33	1299	0.56	-2.96	0
27	SLU 19	-64	-33	1311	0.5	-2.97	0
27	SLU 20	-64	-33	1299	0.56	-2.96	0
27	SLU 21	-64	-33	1311	0.5	-2.97	0
27	SLU 22	-53	-27	1314	0.38	-2.7	0
27	SLU 23	-52	-26	1334	0.28	-2.72	0
27	SLU 24	-53	-27	1314	0.38	-2.7	0
27	SLU 25	-53	-26	1326	0.32	-2.71	0
27	SLU 26	-52	-26	1334	0.28	-2.72	0
27	SLU 27	-53	-27	1314	0.38	-2.7	0
27	SLU 28	-53	-26	1326	0.32	-2.71	0
27	SLU 29	-53	-27	1314	0.38	-2.7	0
27	SLU 30	-53	-26	1326	0.32	-2.71	0
27	SLU 31	-65	-33	1338	0.46	-3.03	0
27	SLU 32	-65	-33	1318	0.57	-3.01	0
27	SLU 33	-65	-33	1330	0.51	-3.02	0
27	SLU 34	-65	-33	1338	0.46	-3.03	0
27	SLU 35	-65	-33	1318	0.57	-3.01	0
27	SLU 36	-65	-33	1330	0.51	-3.02	0
27	SLU 37	-65	-33	1318	0.57	-3.01	0
27	SLU 38	-65	-33	1330	0.51	-3.02	0
27	SLU 39	-71	-36	1320	0.65	-3.15	0
27	SLU 40	-70	-36	1332	0.59	-3.16	0
27	SLU 41	-71	-36	1320	0.65	-3.15	0
27	SLU 42	-70	-36	1332	0.59	-3.16	0
27	SLU 43	-58	-29	1674	0.35	-3.2	0
27	SLU 44	-58	-29	1694	0.25	-3.22	0
27	SLU 45	-58	-29	1674	0.35	-3.2	0
27	SLU 46	-58	-29	1686	0.29	-3.21	0
27	SLU 47	-58	-29	1694	0.25	-3.22	0
27	SLU 48	-58	-29	1674	0.35	-3.2	0
27	SLU 49	-58	-29	1686	0.29	-3.21	0
27	SLU 50	-58	-29	1674	0.35	-3.2	0
27	SLU 51	-58	-29	1686	0.29	-3.21	0
27	SLU 52	-70	-35	1698	0.44	-3.53	0
27	SLU 53	-71	-36	1678	0.54	-3.51	0
27	SLU 54	-70	-36	1690	0.48	-3.52	0
27	SLU 55	-70	-35	1698	0.44	-3.53	0
27	SLU 56	-71	-36	1678	0.54	-3.51	0
27	SLU 57	-70	-36	1690	0.48	-3.52	0
27	SLU 58	-71	-36	1678	0.54	-3.51	0
27	SLU 59	-70	-36	1690	0.48	-3.52	0
27	SLU 60	-76	-39	1680	0.62	-3.65	0
27	SLU 61	-76	-38	1692	0.56	-3.66	0
27	SLU 62	-76	-39	1680	0.62	-3.65	0
27	SLU 63	-76	-38	1692	0.56	-3.66	0
27	SLU 64	-65	-33	1695	0.44	-3.39	0
27	SLU 65	-64	-32	1715	0.34	-3.41	0
27	SLU 66	-65	-33	1695	0.44	-3.39	0
27	SLU 67	-64	-32	1707	0.38	-3.4	0
27	SLU 68	-64	-32	1715	0.34	-3.41	0
27	SLU 69	-65	-33	1695	0.44	-3.39	0
27	SLU 70	-64	-32	1707	0.38	-3.4	0
27	SLU 71	-65	-33	1695	0.44	-3.39	0
27	SLU 72	-64	-32	1707	0.38	-3.4	0
27	SLU 73	-77	-39	1719	0.52	-3.72	0
27	SLU 74	-77	-39	1699	0.63	-3.7	0
27	SLU 75	-77	-39	1711	0.57	-3.71	0
27	SLU 76	-77	-39	1719	0.52	-3.72	0
27	SLU 77	-77	-39	1699	0.63	-3.7	0
27	SLU 78	-77	-39	1711	0.57	-3.71	0
27	SLU 79	-77	-39	1699	0.63	-3.7	0
27	SLU 80	-77	-39	1711	0.57	-3.71	0
27	SLU 81	-82	-42	1701	0.71	-3.84	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
27	SLU 82	-82	-42	1713	0.64	-3.85	0
27	SLU 83	-82	-42	1701	0.71	-3.84	0
27	SLU 84	-82	-42	1713	0.64	-3.85	0
27	SLE RA 1	-48	-24	1299	0.32	-2.57	0
27	SLE RA 2	-48	-24	1312	0.25	-2.58	0
27	SLE RA 3	-48	-24	1299	0.32	-2.57	0
27	SLE RA 4	-48	-24	1307	0.28	-2.57	0
27	SLE RA 5	-48	-24	1312	0.25	-2.58	0
27	SLE RA 6	-48	-24	1299	0.32	-2.57	0
27	SLE RA 7	-48	-24	1307	0.28	-2.57	0
27	SLE RA 8	-48	-24	1299	0.32	-2.57	0
27	SLE RA 9	-48	-24	1307	0.28	-2.57	0
27	SLE RA 10	-56	-28	1315	0.38	-2.79	0
27	SLE RA 11	-57	-29	1302	0.44	-2.77	0
27	SLE RA 12	-56	-29	1310	0.4	-2.78	0
27	SLE RA 13	-56	-28	1315	0.38	-2.79	0
27	SLE RA 14	-57	-29	1302	0.44	-2.77	0
27	SLE RA 15	-56	-29	1310	0.4	-2.78	0
27	SLE RA 16	-57	-29	1302	0.44	-2.77	0
27	SLE RA 17	-56	-29	1310	0.4	-2.78	0
27	SLE RA 18	-60	-31	1303	0.5	-2.86	0
27	SLE RA 19	-60	-30	1311	0.46	-2.87	0
27	SLE RA 20	-60	-31	1303	0.5	-2.86	0
27	SLE RA 21	-60	-30	1311	0.46	-2.87	0
27	SLE FR 1	-48	-24	1299	0.32	-2.57	0
27	SLE FR 2	-48	-24	1302	0.31	-2.57	0
27	SLE FR 3	-48	-24	1299	0.32	-2.57	0
27	SLE FR 4	-52	-26	1303	0.36	-2.66	0
27	SLE FR 5	-52	-26	1300	0.37	-2.66	0
27	SLE FR 6	-54	-28	1301	0.41	-2.72	0
27	SLE QP 1	-48	-24	1299	0.32	-2.57	0
27	SLE QP 2	-52	-26	1300	0.37	-2.66	0
27	SLD 1	-308	-162	1138	8.02	-15.72	-0.01
27	SLD 2	-308	-162	1138	8.02	-15.72	-0.01
27	SLD 3	-191	-101	1014	4.51	-9.67	0
27	SLD 4	-191	-101	1014	4.51	-9.67	0
27	SLD 5	-306	-161	1439	7.99	-15.76	-0.01
27	SLD 6	-306	-161	1439	7.99	-15.76	-0.01
27	SLD 7	84	45	1027	-3.71	4.42	0
27	SLD 8	84	45	1027	-3.71	4.42	0
27	SLD 9	-188	-97	1574	4.45	-9.73	0
27	SLD 10	-188	-97	1574	4.45	-9.73	0
27	SLD 11	203	108	1162	-7.24	10.45	0
27	SLD 12	203	108	1162	-7.24	10.45	0
27	SLD 13	88	48	1586	-3.76	4.35	0
27	SLD 14	88	48	1586	-3.76	4.35	0
27	SLD 15	205	110	1463	-7.27	10.41	0.01
27	SLD 16	205	110	1463	-7.27	10.41	0.01
27	SLV 1	-688	-364	923	19.38	-35.04	-0.02
27	SLV 2	-688	-364	923	19.38	-35.04	-0.02
27	SLV 3	-390	-208	616	10.59	-19.58	-0.01
27	SLV 4	-390	-208	616	10.59	-19.58	-0.01
27	SLV 5	-695	-365	1652	19.42	-35.83	-0.01
27	SLV 6	-695	-365	1652	19.42	-35.83	-0.01
27	SLV 7	298	157	630	-9.9	15.72	0
27	SLV 8	298	157	630	-9.9	15.72	0
27	SLV 9	-402	-209	1971	10.65	-21.03	0
27	SLV 10	-402	-209	1971	10.65	-21.03	0
27	SLV 11	591	313	948	-18.67	30.52	0.01
27	SLV 12	591	313	948	-18.67	30.52	0.01
27	SLV 13	287	155	1984	-9.84	14.27	0.01
27	SLV 14	287	155	1984	-9.84	14.27	0.01
27	SLV 15	585	312	1678	-18.64	29.73	0.01
27	SLV 16	585	312	1678	-18.64	29.73	0.01
28	SLU 1	-86	-41	1362	1.51	-5.4	0.01
28	SLU 2	-86	-41	1384	1.44	-5.43	0.01
28	SLU 3	-86	-41	1362	1.51	-5.4	0.01
28	SLU 4	-86	-41	1375	1.46	-5.42	0.01
28	SLU 5	-86	-41	1384	1.44	-5.43	0.01
28	SLU 6	-86	-41	1362	1.51	-5.4	0.01
28	SLU 7	-86	-41	1375	1.46	-5.42	0.01
28	SLU 8	-86	-41	1362	1.51	-5.4	0.01
28	SLU 9	-86	-41	1375	1.46	-5.42	0.01
28	SLU 10	-100	-48	1374	1.86	-6.18	0.01
28	SLU 11	-100	-49	1353	1.93	-6.14	0.01
28	SLU 12	-100	-48	1365	1.88	-6.16	0.01
28	SLU 13	-100	-48	1374	1.86	-6.18	0.01
28	SLU 14	-100	-49	1353	1.93	-6.14	0.01
28	SLU 15	-100	-48	1365	1.88	-6.16	0.01
28	SLU 16	-100	-49	1353	1.93	-6.14	0.01
28	SLU 17	-100	-48	1365	1.88	-6.16	0.01
28	SLU 18	-106	-52	1349	2.11	-6.46	0.01
28	SLU 19	-106	-51	1361	2.06	-6.48	0.01
28	SLU 20	-106	-52	1349	2.11	-6.46	0.01
28	SLU 21	-106	-51	1361	2.06	-6.48	0.01
28	SLU 22	-94	-45	1378	1.7	-5.79	0.01
28	SLU 23	-93	-44	1399	1.63	-5.82	0.01
28	SLU 24	-94	-45	1378	1.7	-5.79	0.01





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
28	SLU 25	-93	-45	1391	1.66	-5.81	0.01
28	SLU 26	-93	-44	1399	1.63	-5.82	0.01
28	SLU 27	-94	-45	1378	1.7	-5.79	0.01
28	SLU 28	-93	-45	1391	1.66	-5.81	0.01
28	SLU 29	-94	-45	1378	1.7	-5.79	0.01
28	SLU 30	-93	-45	1391	1.66	-5.81	0.01
28	SLU 31	-107	-52	1390	2.05	-6.57	0.01
28	SLU 32	-108	-52	1368	2.12	-6.53	0.01
28	SLU 33	-107	-52	1381	2.08	-6.55	0.01
28	SLU 34	-107	-52	1390	2.05	-6.57	0.01
28	SLU 35	-108	-52	1368	2.12	-6.53	0.01
28	SLU 36	-107	-52	1381	2.08	-6.55	0.01
28	SLU 37	-108	-52	1368	2.12	-6.53	0.01
28	SLU 38	-107	-52	1381	2.08	-6.55	0.01
28	SLU 39	-114	-56	1364	2.3	-6.85	0.01
28	SLU 40	-113	-55	1377	2.26	-6.87	0.01
28	SLU 41	-114	-56	1364	2.3	-6.85	0.01
28	SLU 42	-113	-55	1377	2.26	-6.87	0.01
28	SLU 43	-110	-52	1766	1.89	-6.88	0.01
28	SLU 44	-109	-52	1787	1.82	-6.92	0.01
28	SLU 45	-110	-52	1766	1.89	-6.88	0.01
28	SLU 46	-109	-52	1779	1.85	-6.9	0.01
28	SLU 47	-109	-52	1787	1.82	-6.92	0.01
28	SLU 48	-110	-52	1766	1.89	-6.88	0.01
28	SLU 49	-109	-52	1779	1.85	-6.9	0.01
28	SLU 50	-110	-52	1766	1.89	-6.88	0.01
28	SLU 51	-109	-52	1779	1.85	-6.9	0.01
28	SLU 52	-123	-59	1777	2.24	-7.66	0.01
28	SLU 53	-124	-60	1756	2.31	-7.62	0.01
28	SLU 54	-123	-59	1769	2.27	-7.65	0.01
28	SLU 55	-123	-59	1777	2.24	-7.66	0.01
28	SLU 56	-124	-60	1756	2.31	-7.62	0.01
28	SLU 57	-123	-59	1769	2.27	-7.65	0.01
28	SLU 58	-124	-60	1756	2.31	-7.62	0.01
28	SLU 59	-123	-59	1769	2.27	-7.65	0.01
28	SLU 60	-130	-63	1752	2.49	-7.94	0.01
28	SLU 61	-129	-62	1765	2.45	-7.96	0.01
28	SLU 62	-130	-63	1752	2.49	-7.94	0.01
28	SLU 63	-129	-62	1765	2.45	-7.96	0.01
28	SLU 64	-117	-56	1781	2.09	-7.27	0.01
28	SLU 65	-117	-55	1803	2.01	-7.31	0.01
28	SLU 66	-117	-56	1781	2.09	-7.27	0.01
28	SLU 67	-117	-56	1794	2.04	-7.3	0.01
28	SLU 68	-117	-55	1803	2.01	-7.31	0.01
28	SLU 69	-117	-56	1781	2.09	-7.27	0.01
28	SLU 70	-117	-56	1794	2.04	-7.3	0.01
28	SLU 71	-117	-56	1781	2.09	-7.27	0.01
28	SLU 72	-117	-56	1794	2.04	-7.3	0.01
28	SLU 73	-131	-63	1793	2.43	-8.05	0.01
28	SLU 74	-131	-63	1772	2.51	-8.01	0.01
28	SLU 75	-131	-63	1784	2.46	-8.04	0.01
28	SLU 76	-131	-63	1793	2.43	-8.05	0.01
28	SLU 77	-131	-63	1772	2.51	-8.01	0.01
28	SLU 78	-131	-63	1784	2.46	-8.04	0.01
28	SLU 79	-131	-63	1772	2.51	-8.01	0.01
28	SLU 80	-131	-63	1784	2.46	-8.04	0.01
28	SLU 81	-137	-67	1767	2.69	-8.33	0.01
28	SLU 82	-137	-66	1780	2.64	-8.35	0.01
28	SLU 83	-137	-67	1767	2.69	-8.33	0.01
28	SLU 84	-137	-66	1780	2.64	-8.35	0.01
28	SLE RA 1	-88	-42	1367	1.56	-5.51	0.01
28	SLE RA 2	-88	-42	1381	1.51	-5.53	0.01
28	SLE RA 3	-88	-42	1367	1.56	-5.51	0.01
28	SLE RA 4	-88	-42	1375	1.53	-5.52	0.01
28	SLE RA 5	-88	-42	1381	1.51	-5.53	0.01
28	SLE RA 6	-88	-42	1367	1.56	-5.51	0.01
28	SLE RA 7	-88	-42	1375	1.53	-5.52	0.01
28	SLE RA 8	-88	-42	1367	1.56	-5.51	0.01
28	SLE RA 9	-88	-42	1375	1.53	-5.52	0.01
28	SLE RA 10	-97	-47	1375	1.79	-6.03	0.01
28	SLE RA 11	-98	-47	1360	1.84	-6	0.01
28	SLE RA 12	-98	-47	1369	1.81	-6.02	0.01
28	SLE RA 13	-97	-47	1375	1.79	-6.03	0.01
28	SLE RA 14	-98	-47	1360	1.84	-6	0.01
28	SLE RA 15	-98	-47	1369	1.81	-6.02	0.01
28	SLE RA 16	-98	-47	1360	1.84	-6	0.01
28	SLE RA 17	-98	-47	1369	1.81	-6.02	0.01
28	SLE RA 18	-102	-49	1358	1.96	-6.21	0.01
28	SLE RA 19	-102	-49	1366	1.93	-6.23	0.01
28	SLE RA 20	-102	-49	1358	1.96	-6.21	0.01
28	SLE RA 21	-102	-49	1366	1.93	-6.23	0.01
28	SLE FR 1	-88	-42	1367	1.56	-5.51	0.01
28	SLE FR 2	-88	-42	1370	1.55	-5.51	0.01
28	SLE FR 3	-88	-42	1367	1.56	-5.51	0.01
28	SLE FR 4	-92	-44	1367	1.67	-5.73	0.01
28	SLE FR 5	-92	-44	1364	1.68	-5.72	0.01
28	SLE FR 6	-95	-46	1362	1.76	-5.86	0.01
28	SLE QP 1	-88	-42	1367	1.56	-5.51	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
28	SLE QP 2	-92	-44	1364	1.68	-5.72	0.01
28	SLD 1	-346	-177	1037	8.97	-19.61	0.02
28	SLD 2	-346	-177	1037	8.97	-19.61	0.02
28	SLD 3	-228	-115	738	5.57	-13.07	0.02
28	SLD 4	-228	-115	738	5.57	-13.07	0.02
28	SLD 5	-348	-177	1719	9.02	-19.81	0.02
28	SLD 6	-348	-177	1719	9.02	-19.81	0.02
28	SLD 7	46	28	724	-2.3	1.99	0.01
28	SLD 8	46	28	724	-2.3	1.99	0.01
28	SLD 9	-231	-116	2005	5.67	-13.43	0.01
28	SLD 10	-231	-116	2005	5.67	-13.43	0.01
28	SLD 11	163	89	1010	-5.65	8.37	0
28	SLD 12	163	89	1010	-5.65	8.37	0
28	SLD 13	43	27	1990	-2.21	1.63	0.01
28	SLD 14	43	27	1990	-2.21	1.63	0.01
28	SLD 15	161	88	1691	-5.6	8.17	0
28	SLD 16	161	88	1691	-5.6	8.17	0
28	SLV 1	-721	-373	594	19.79	-40.11	0.03
28	SLV 2	-721	-373	594	19.79	-40.11	0.03
28	SLV 3	-420	-217	-162	11.23	-23.4	0.02
28	SLV 4	-420	-217	-162	11.23	-23.4	0.02
28	SLV 5	-738	-380	2281	20.09	-41.38	0.03
28	SLV 6	-738	-380	2281	20.09	-41.38	0.03
28	SLV 7	266	141	-242	-8.44	14.32	0
28	SLV 8	266	141	-242	-8.44	14.32	0
28	SLV 9	-451	-229	2970	11.8	-25.76	0.02
28	SLV 10	-451	-229	2970	11.8	-25.76	0.02
28	SLV 11	553	291	447	-16.73	29.94	-0.01
28	SLV 12	553	291	447	-16.73	29.94	-0.01
28	SLV 13	235	129	2891	-7.86	11.96	0
28	SLV 14	235	129	2891	-7.86	11.96	0
28	SLV 15	536	285	2134	-16.42	28.67	-0.01
28	SLV 16	536	285	2134	-16.42	28.67	-0.01
29	SLU 1	0	177	1228	-10.14	-0.15	0
29	SLU 2	0	170	1216	-9.88	-0.15	0
29	SLU 3	0	177	1228	-10.14	-0.15	0
29	SLU 4	0	172	1221	-9.98	-0.15	0
29	SLU 5	0	170	1216	-9.88	-0.15	0
29	SLU 6	0	177	1228	-10.14	-0.15	0
29	SLU 7	0	172	1221	-9.98	-0.15	0
29	SLU 8	0	177	1228	-10.14	-0.15	0
29	SLU 9	0	172	1221	-9.98	-0.15	0
29	SLU 10	0	369	1754	-22.04	-0.22	0
29	SLU 11	0	376	1766	-22.3	-0.22	0
29	SLU 12	0	371	1759	-22.15	-0.22	0
29	SLU 13	0	369	1754	-22.04	-0.22	0
29	SLU 14	0	376	1766	-22.3	-0.22	0
29	SLU 15	0	371	1759	-22.15	-0.22	0
29	SLU 16	0	376	1766	-22.3	-0.22	0
29	SLU 17	0	371	1759	-22.15	-0.22	0
29	SLU 18	0	461	1996	-27.52	-0.25	0
29	SLU 19	0	457	1989	-27.36	-0.25	0
29	SLU 20	0	461	1996	-27.52	-0.25	0
29	SLU 21	0	457	1989	-27.36	-0.25	0
29	SLU 22	0	255	1455	-14.96	-0.18	0
29	SLU 23	0	248	1443	-14.7	-0.18	0
29	SLU 24	0	255	1455	-14.96	-0.18	0
29	SLU 25	0	251	1448	-14.8	-0.18	0
29	SLU 26	0	248	1443	-14.7	-0.18	0
29	SLU 27	0	255	1455	-14.96	-0.18	0
29	SLU 28	0	251	1448	-14.8	-0.18	0
29	SLU 29	0	255	1455	-14.96	-0.18	0
29	SLU 30	0	251	1448	-14.8	-0.18	0
29	SLU 31	0	447	1981	-26.86	-0.25	0
29	SLU 32	0	454	1992	-27.13	-0.25	0
29	SLU 33	0	450	1985	-26.97	-0.25	0
29	SLU 34	0	447	1981	-26.86	-0.25	0
29	SLU 35	0	454	1992	-27.13	-0.25	0
29	SLU 36	0	450	1985	-26.97	-0.25	0
29	SLU 37	0	454	1992	-27.13	-0.25	0
29	SLU 38	0	450	1985	-26.97	-0.25	0
29	SLU 39	0	540	2223	-32.34	-0.28	0
29	SLU 40	0	536	2216	-32.18	-0.28	0
29	SLU 41	0	540	2223	-32.34	-0.28	0
29	SLU 42	0	536	2216	-32.18	-0.28	0
29	SLU 43	0	203	1519	-11.53	-0.19	0
29	SLU 44	0	196	1507	-11.26	-0.19	0
29	SLU 45	0	203	1519	-11.53	-0.19	0
29	SLU 46	0	198	1512	-11.37	-0.19	0
29	SLU 47	0	196	1507	-11.26	-0.19	0
29	SLU 48	0	203	1519	-11.53	-0.19	0
29	SLU 49	0	198	1512	-11.37	-0.19	0
29	SLU 50	0	203	1519	-11.53	-0.19	0
29	SLU 51	0	198	1512	-11.37	-0.19	0
29	SLU 52	0	395	2045	-23.43	-0.25	0
29	SLU 53	0	402	2056	-23.69	-0.26	0
29	SLU 54	0	397	2049	-23.53	-0.25	0
29	SLU 55	0	395	2045	-23.43	-0.25	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
29	SLU 56	0	402	2056	-23.69	-0.26	0
29	SLU 57	0	397	2049	-23.53	-0.25	0
29	SLU 58	0	402	2056	-23.69	-0.26	0
29	SLU 59	0	397	2049	-23.53	-0.25	0
29	SLU 60	0	487	2287	-28.9	-0.28	0
29	SLU 61	0	483	2280	-28.75	-0.28	0
29	SLU 62	0	487	2287	-28.9	-0.28	0
29	SLU 63	0	483	2280	-28.75	-0.28	0
29	SLU 64	0	281	1745	-16.35	-0.22	0
29	SLU 65	0	274	1734	-16.09	-0.22	0
29	SLU 66	0	281	1745	-16.35	-0.22	0
29	SLU 67	0	277	1738	-16.19	-0.22	0
29	SLU 68	0	274	1734	-16.09	-0.22	0
29	SLU 69	0	281	1745	-16.35	-0.22	0
29	SLU 70	0	277	1738	-16.19	-0.22	0
29	SLU 71	0	281	1745	-16.35	-0.22	0
29	SLU 72	0	277	1738	-16.19	-0.22	0
29	SLU 73	0	473	2271	-28.25	-0.28	0
29	SLU 74	0	480	2283	-28.52	-0.29	0
29	SLU 75	0	476	2276	-28.36	-0.28	0
29	SLU 76	0	473	2271	-28.25	-0.28	0
29	SLU 77	0	480	2283	-28.52	-0.29	0
29	SLU 78	0	476	2276	-28.36	-0.28	0
29	SLU 79	0	480	2283	-28.52	-0.29	0
29	SLU 80	0	476	2276	-28.36	-0.28	0
29	SLU 81	0	566	2513	-33.73	-0.31	0
29	SLU 82	0	561	2506	-33.57	-0.31	0
29	SLU 83	0	566	2513	-33.73	-0.31	0
29	SLU 84	0	561	2506	-33.57	-0.31	0
29	SLE RA 1	0	199	1293	-11.52	-0.16	0
29	SLE RA 2	0	194	1285	-11.34	-0.16	0
29	SLE RA 3	0	199	1293	-11.52	-0.16	0
29	SLE RA 4	0	196	1288	-11.41	-0.16	0
29	SLE RA 5	0	194	1285	-11.34	-0.16	0
29	SLE RA 6	0	199	1293	-11.52	-0.16	0
29	SLE RA 7	0	196	1288	-11.41	-0.16	0
29	SLE RA 8	0	199	1293	-11.52	-0.16	0
29	SLE RA 9	0	196	1288	-11.41	-0.16	0
29	SLE RA 10	0	327	1643	-19.45	-0.2	0
29	SLE RA 11	0	332	1651	-19.63	-0.21	0
29	SLE RA 12	0	329	1647	-19.52	-0.21	0
29	SLE RA 13	0	327	1643	-19.45	-0.2	0
29	SLE RA 14	0	332	1651	-19.63	-0.21	0
29	SLE RA 15	0	329	1647	-19.52	-0.21	0
29	SLE RA 16	0	332	1651	-19.63	-0.21	0
29	SLE RA 17	0	329	1647	-19.52	-0.21	0
29	SLE RA 18	0	389	1805	-23.1	-0.23	0
29	SLE RA 19	0	386	1800	-23	-0.22	0
29	SLE RA 20	0	389	1805	-23.1	-0.23	0
29	SLE RA 21	0	386	1800	-23	-0.22	0
29	SLE FR 1	0	199	1293	-11.52	-0.16	0
29	SLE FR 2	0	198	1291	-11.48	-0.16	0
29	SLE FR 3	0	199	1293	-11.52	-0.16	0
29	SLE FR 4	0	255	1445	-14.96	-0.18	0
29	SLE FR 5	0	256	1446	-14.99	-0.18	0
29	SLE FR 6	0	294	1549	-17.31	-0.19	0
29	SLE QP 1	0	199	1293	-11.52	-0.16	0
29	SLE QP 2	0	256	1446	-14.99	-0.18	0
29	SLD 1	-5	464	1547	-25.24	5.38	-0.01
29	SLD 2	-5	464	1547	-25.24	5.38	-0.01
29	SLD 3	-4	265	1642	-15.48	4.27	-0.01
29	SLD 4	-4	265	1642	-15.48	4.27	-0.01
29	SLD 5	-4	620	1332	-32.87	3.16	0
29	SLD 6	-4	620	1332	-32.87	3.16	0
29	SLD 7	1	-43	1649	-0.34	-0.52	-0.01
29	SLD 8	1	-43	1649	-0.34	-0.52	-0.01
29	SLD 9	-1	555	1244	-29.65	0.16	0.01
29	SLD 10	-1	555	1244	-29.65	0.16	0.01
29	SLD 11	3	-108	1561	2.88	-3.53	0
29	SLD 12	3	-108	1561	2.88	-3.53	0
29	SLD 13	3	247	1251	-14.51	-4.63	0.01
29	SLD 14	3	247	1251	-14.51	-4.63	0.01
29	SLD 15	5	48	1346	-4.75	-5.74	0.01
29	SLD 16	5	48	1346	-4.75	-5.74	0.01
29	SLV 1	-13	747	1677	-39.18	13.9	-0.03
29	SLV 2	-13	747	1677	-39.18	13.9	-0.03
29	SLV 3	-10	277	1922	-16.12	11.06	-0.04
29	SLV 4	-10	277	1922	-16.12	11.06	-0.04
29	SLV 5	-9	1116	1145	-57.22	8.35	0
29	SLV 6	-9	1116	1145	-57.22	8.35	0
29	SLV 7	2	-450	1960	19.64	-1.12	-0.02
29	SLV 8	2	-450	1960	19.64	-1.12	-0.02
29	SLV 9	-3	962	933	-49.62	0.76	0.02
29	SLV 10	-3	962	933	-49.62	0.76	0.02
29	SLV 11	9	-604	1748	27.23	-8.71	0
29	SLV 12	9	-604	1748	27.23	-8.71	0
29	SLV 13	9	235	971	-13.86	-11.42	0.03
29	SLV 14	9	235	971	-13.86	-11.42	0.03



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
29	SLV 15	13	-235	1215	9.19	-14.26	0.03
29	SLV 16	13	-235	1215	9.19	-14.26	0.03
30	SLU 1	-194	257	1991	-9.22	-4.31	-0.02
30	SLU 2	-196	264	2024	-9.53	-4.32	-0.02
30	SLU 3	-194	257	1991	-9.22	-4.31	-0.02
30	SLU 4	-196	261	2010	-9.41	-4.31	-0.02
30	SLU 5	-196	264	2024	-9.53	-4.32	-0.02
30	SLU 6	-194	257	1991	-9.22	-4.31	-0.02
30	SLU 7	-196	261	2010	-9.41	-4.31	-0.02
30	SLU 8	-194	257	1991	-9.22	-4.31	-0.02
30	SLU 9	-196	261	2010	-9.41	-4.31	-0.02
30	SLU 10	-199	263	2005	-9.92	-4.41	-0.01
30	SLU 11	-197	255	1972	-9.62	-4.4	-0.01
30	SLU 12	-198	260	1991	-9.8	-4.4	-0.01
30	SLU 13	-199	263	2005	-9.92	-4.41	-0.01
30	SLU 14	-197	255	1972	-9.62	-4.4	-0.01
30	SLU 15	-198	260	1991	-9.8	-4.4	-0.01
30	SLU 16	-197	255	1972	-9.62	-4.4	-0.01
30	SLU 17	-198	260	1991	-9.8	-4.4	-0.01
30	SLU 18	-198	255	1963	-9.79	-4.43	-0.01
30	SLU 19	-200	259	1983	-9.97	-4.44	-0.01
30	SLU 20	-198	255	1963	-9.79	-4.43	-0.01
30	SLU 21	-200	259	1983	-9.97	-4.44	-0.01
30	SLU 22	-198	261	2011	-9.57	-4.42	-0.02
30	SLU 23	-201	269	2044	-9.88	-4.43	-0.02
30	SLU 24	-198	261	2011	-9.57	-4.42	-0.02
30	SLU 25	-200	266	2031	-9.75	-4.42	-0.02
30	SLU 26	-201	269	2044	-9.88	-4.43	-0.02
30	SLU 27	-198	261	2011	-9.57	-4.42	-0.02
30	SLU 28	-200	266	2031	-9.75	-4.42	-0.02
30	SLU 29	-198	261	2011	-9.57	-4.42	-0.02
30	SLU 30	-200	266	2031	-9.75	-4.42	-0.02
30	SLU 31	-204	268	2025	-10.27	-4.52	-0.01
30	SLU 32	-201	260	1992	-9.97	-4.5	-0.01
30	SLU 33	-203	264	2012	-10.15	-4.51	-0.01
30	SLU 34	-204	268	2025	-10.27	-4.52	-0.01
30	SLU 35	-201	260	1992	-9.97	-4.5	-0.01
30	SLU 36	-203	264	2012	-10.15	-4.51	-0.01
30	SLU 37	-201	260	1992	-9.97	-4.5	-0.01
30	SLU 38	-203	264	2012	-10.15	-4.51	-0.01
30	SLU 39	-203	259	1984	-10.13	-4.54	-0.01
30	SLU 40	-204	264	2004	-10.32	-4.55	-0.01
30	SLU 41	-203	259	1984	-10.13	-4.54	-0.01
30	SLU 42	-204	264	2004	-10.32	-4.55	-0.01
30	SLU 43	-251	332	2581	-11.87	-5.56	-0.02
30	SLU 44	-253	340	2614	-12.18	-5.57	-0.02
30	SLU 45	-251	332	2581	-11.87	-5.56	-0.02
30	SLU 46	-252	337	2600	-12.06	-5.57	-0.02
30	SLU 47	-253	340	2614	-12.18	-5.57	-0.02
30	SLU 48	-251	332	2581	-11.87	-5.56	-0.02
30	SLU 49	-252	337	2600	-12.06	-5.57	-0.02
30	SLU 50	-251	332	2581	-11.87	-5.56	-0.02
30	SLU 51	-252	337	2600	-12.06	-5.57	-0.02
30	SLU 52	-256	338	2595	-12.57	-5.66	-0.02
30	SLU 53	-254	331	2562	-12.27	-5.65	-0.02
30	SLU 54	-255	335	2581	-12.45	-5.66	-0.02
30	SLU 55	-256	338	2595	-12.57	-5.66	-0.02
30	SLU 56	-254	331	2562	-12.27	-5.65	-0.02
30	SLU 57	-255	335	2581	-12.45	-5.66	-0.02
30	SLU 58	-254	331	2562	-12.27	-5.65	-0.02
30	SLU 59	-255	335	2581	-12.45	-5.66	-0.02
30	SLU 60	-255	330	2553	-12.44	-5.69	-0.02
30	SLU 61	-257	335	2573	-12.62	-5.7	-0.02
30	SLU 62	-255	330	2553	-12.44	-5.69	-0.02
30	SLU 63	-257	335	2573	-12.62	-5.7	-0.02
30	SLU 64	-255	336	2602	-12.22	-5.67	-0.02
30	SLU 65	-257	344	2634	-12.53	-5.68	-0.02
30	SLU 66	-255	336	2602	-12.22	-5.67	-0.02
30	SLU 67	-256	341	2621	-12.4	-5.68	-0.02
30	SLU 68	-257	344	2634	-12.53	-5.68	-0.02
30	SLU 69	-255	336	2602	-12.22	-5.67	-0.02
30	SLU 70	-256	341	2621	-12.4	-5.68	-0.02
30	SLU 71	-255	336	2602	-12.22	-5.67	-0.02
30	SLU 72	-256	341	2621	-12.4	-5.68	-0.02
30	SLU 73	-260	343	2615	-12.92	-5.77	-0.02
30	SLU 74	-258	335	2582	-12.61	-5.76	-0.02
30	SLU 75	-259	340	2602	-12.8	-5.77	-0.02
30	SLU 76	-260	343	2615	-12.92	-5.77	-0.02
30	SLU 77	-258	335	2582	-12.61	-5.76	-0.02
30	SLU 78	-259	340	2602	-12.8	-5.77	-0.02
30	SLU 79	-258	335	2582	-12.61	-5.76	-0.02
30	SLU 80	-259	340	2602	-12.8	-5.77	-0.02
30	SLU 81	-259	335	2574	-12.78	-5.8	-0.02
30	SLU 82	-261	339	2594	-12.97	-5.8	-0.02
30	SLU 83	-259	335	2574	-12.78	-5.8	-0.02
30	SLU 84	-261	339	2594	-12.97	-5.8	-0.02
30	SLE RA 1	-195	258	1997	-9.32	-4.34	-0.02
30	SLE RA 2	-197	263	2019	-9.53	-4.35	-0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
30	SLE RA 3	-195	258	1997	-9.32	-4.34	-0.02
30	SLE RA 4	-196	261	2010	-9.45	-4.34	-0.02
30	SLE RA 5	-197	263	2019	-9.53	-4.35	-0.02
30	SLE RA 6	-195	258	1997	-9.32	-4.34	-0.02
30	SLE RA 7	-196	261	2010	-9.45	-4.34	-0.02
30	SLE RA 8	-195	258	1997	-9.32	-4.34	-0.02
30	SLE RA 9	-196	261	2010	-9.45	-4.34	-0.02
30	SLE RA 10	-199	262	2006	-9.79	-4.41	-0.01
30	SLE RA 11	-197	257	1984	-9.59	-4.4	-0.01
30	SLE RA 12	-198	260	1997	-9.71	-4.4	-0.01
30	SLE RA 13	-199	262	2006	-9.79	-4.41	-0.01
30	SLE RA 14	-197	257	1984	-9.59	-4.4	-0.01
30	SLE RA 15	-198	260	1997	-9.71	-4.4	-0.01
30	SLE RA 16	-197	257	1984	-9.59	-4.4	-0.01
30	SLE RA 17	-198	260	1997	-9.71	-4.4	-0.01
30	SLE RA 18	-198	257	1978	-9.7	-4.42	-0.01
30	SLE RA 19	-199	260	1992	-9.82	-4.43	-0.01
30	SLE RA 20	-198	257	1978	-9.7	-4.42	-0.01
30	SLE RA 21	-199	260	1992	-9.82	-4.43	-0.01
30	SLE FR 1	-195	258	1997	-9.32	-4.34	-0.02
30	SLE FR 2	-196	259	2001	-9.36	-4.34	-0.02
30	SLE FR 3	-195	258	1997	-9.32	-4.34	-0.02
30	SLE FR 4	-196	258	1996	-9.48	-4.37	-0.01
30	SLE FR 5	-196	257	1991	-9.44	-4.36	-0.01
30	SLE FR 6	-197	257	1988	-9.51	-4.38	-0.01
30	SLE QP 1	-195	258	1997	-9.32	-4.34	-0.02
30	SLE QP 2	-196	257	1991	-9.44	-4.36	-0.01
30	SLD 1	-422	227	1324	-7.91	-13.05	0.06
30	SLD 2	-422	227	1324	-7.91	-13.05	0.06
30	SLD 3	-317	132	680	-3.85	-9.05	0.02
30	SLD 4	-317	132	680	-3.85	-9.05	0.02
30	SLD 5	-423	391	2768	-15.14	-13.04	0.07
30	SLD 6	-423	391	2768	-15.14	-13.04	0.07
30	SLD 7	-73	77	621	-1.6	0.3	-0.07
30	SLD 8	-73	77	621	-1.6	0.3	-0.07
30	SLD 9	-319	438	3361	-17.27	-9.03	0.04
30	SLD 10	-319	438	3361	-17.27	-9.03	0.04
30	SLD 11	31	124	1214	-3.74	4.31	-0.1
30	SLD 12	31	124	1214	-3.74	4.31	-0.1
30	SLD 13	-76	383	3302	-15.03	0.32	-0.05
30	SLD 14	-76	383	3302	-15.03	0.32	-0.05
30	SLD 15	29	288	2658	-10.97	4.32	-0.09
30	SLD 16	29	288	2658	-10.97	4.32	-0.09
30	SLV 1	-753	181	414	-5.59	-25.91	0.17
30	SLV 2	-753	181	414	-5.59	-25.91	0.17
30	SLV 3	-484	-43	-1213	4.1	-15.72	0.07
30	SLV 4	-484	-43	-1213	4.1	-15.72	0.07
30	SLV 5	-770	574	3985	-22.97	-26.29	0.2
30	SLV 6	-770	574	3985	-22.97	-26.29	0.2
30	SLV 7	125	-172	-1437	9.31	7.69	-0.15
30	SLV 8	125	-172	-1437	9.31	7.69	-0.15
30	SLV 9	-517	687	5420	-28.19	-16.42	0.12
30	SLV 10	-517	687	5420	-28.19	-16.42	0.12
30	SLV 11	378	-59	-3	4.1	17.56	-0.23
30	SLV 12	378	-59	-3	4.1	17.56	-0.23
30	SLV 13	92	558	5195	-22.97	6.99	-0.1
30	SLV 14	92	558	5195	-22.97	6.99	-0.1
30	SLV 15	360	334	3568	-13.28	17.18	-0.2
30	SLV 16	360	334	3568	-13.28	17.18	-0.2
31	SLU 1	1	194	1726	-9.04	0.57	-0.01
31	SLU 2	-1	190	1705	-8.84	-1.49	0
31	SLU 3	1	194	1726	-9.04	0.57	-0.01
31	SLU 4	-1	191	1713	-8.92	-0.67	0
31	SLU 5	-1	190	1705	-8.84	-1.49	0
31	SLU 6	1	194	1726	-9.04	0.57	-0.01
31	SLU 7	-1	191	1713	-8.92	-0.67	0
31	SLU 8	1	194	1726	-9.04	0.57	-0.01
31	SLU 9	-1	191	1713	-8.92	-0.67	0
31	SLU 10	-1	234	2023	-10.98	-1.17	0
31	SLU 11	1	238	2044	-11.18	0.89	-0.01
31	SLU 12	0	236	2032	-11.06	-0.35	0
31	SLU 13	-1	234	2023	-10.98	-1.17	0
31	SLU 14	1	238	2044	-11.18	0.89	-0.01
31	SLU 15	0	236	2032	-11.06	-0.35	0
31	SLU 16	1	238	2044	-11.18	0.89	-0.01
31	SLU 17	0	236	2032	-11.06	-0.35	0
31	SLU 18	1	257	2181	-12.1	1.03	-0.01
31	SLU 19	0	255	2168	-11.98	-0.21	0
31	SLU 20	1	257	2181	-12.1	1.03	-0.01
31	SLU 21	0	255	2168	-11.98	-0.21	0
31	SLU 22	1	214	1873	-10.02	0.71	-0.01
31	SLU 23	-1	210	1852	-9.82	-1.36	0
31	SLU 24	1	214	1873	-10.02	0.71	-0.01
31	SLU 25	-1	212	1861	-9.9	-0.53	0
31	SLU 26	-1	210	1852	-9.82	-1.36	0
31	SLU 27	1	214	1873	-10.02	0.71	-0.01
31	SLU 28	-1	212	1861	-9.9	-0.53	0
31	SLU 29	1	214	1873	-10.02	0.71	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
31	SLU 30	-1	212	1861	-9.9	-0.53	0
31	SLU 31	-1	254	2170	-11.96	-1.04	0
31	SLU 32	1	258	2191	-12.16	1.03	-0.01
31	SLU 33	0	256	2179	-12.04	-0.21	0
31	SLU 34	-1	254	2170	-11.96	-1.04	0
31	SLU 35	1	258	2191	-12.16	1.03	-0.01
31	SLU 36	0	256	2179	-12.04	-0.21	0
31	SLU 37	1	258	2191	-12.16	1.03	-0.01
31	SLU 38	0	256	2179	-12.04	-0.21	0
31	SLU 39	1	277	2328	-13.08	1.16	-0.01
31	SLU 40	0	275	2315	-12.96	-0.08	0
31	SLU 41	1	277	2328	-13.08	1.16	-0.01
31	SLU 42	0	275	2315	-12.96	-0.08	0
31	SLU 43	1	245	2194	-11.42	0.7	-0.01
31	SLU 44	-1	241	2172	-11.21	-1.37	0
31	SLU 45	1	245	2194	-11.42	0.7	-0.01
31	SLU 46	-1	242	2181	-11.29	-0.54	0
31	SLU 47	-1	241	2172	-11.21	-1.37	0
31	SLU 48	1	245	2194	-11.42	0.7	-0.01
31	SLU 49	-1	242	2181	-11.29	-0.54	0
31	SLU 50	1	245	2194	-11.42	0.7	-0.01
31	SLU 51	-1	242	2181	-11.29	-0.54	0
31	SLU 52	-1	285	2491	-13.36	-1.05	0
31	SLU 53	1	289	2512	-13.56	1.02	-0.01
31	SLU 54	0	287	2499	-13.44	-0.22	0
31	SLU 55	-1	285	2491	-13.36	-1.05	0
31	SLU 56	1	289	2512	-13.56	1.02	-0.01
31	SLU 57	0	287	2499	-13.44	-0.22	0
31	SLU 58	1	289	2512	-13.56	1.02	-0.01
31	SLU 59	0	287	2499	-13.44	-0.22	0
31	SLU 60	1	308	2648	-14.48	1.15	-0.01
31	SLU 61	0	306	2635	-14.35	-0.09	-0.01
31	SLU 62	1	308	2648	-14.48	1.15	-0.01
31	SLU 63	0	306	2635	-14.35	-0.09	-0.01
31	SLU 64	1	265	2341	-12.4	0.83	-0.01
31	SLU 65	-1	261	2320	-12.19	-1.23	0
31	SLU 66	1	265	2341	-12.4	0.83	-0.01
31	SLU 67	0	263	2328	-12.28	-0.41	0
31	SLU 68	-1	261	2320	-12.19	-1.23	0
31	SLU 69	1	265	2341	-12.4	0.83	-0.01
31	SLU 70	0	263	2328	-12.28	-0.41	0
31	SLU 71	1	265	2341	-12.4	0.83	-0.01
31	SLU 72	0	263	2328	-12.28	-0.41	0
31	SLU 73	-1	305	2638	-14.34	-0.91	0
31	SLU 74	1	309	2659	-14.54	1.15	-0.01
31	SLU 75	0	307	2646	-14.42	-0.09	-0.01
31	SLU 76	-1	305	2638	-14.34	-0.91	0
31	SLU 77	1	309	2659	-14.54	1.15	-0.01
31	SLU 78	0	307	2646	-14.42	-0.09	-0.01
31	SLU 79	1	309	2659	-14.54	1.15	-0.01
31	SLU 80	0	307	2646	-14.42	-0.09	-0.01
31	SLU 81	1	328	2795	-15.46	1.29	-0.01
31	SLU 82	0	326	2783	-15.34	0.05	-0.01
31	SLU 83	1	328	2795	-15.46	1.29	-0.01
31	SLU 84	0	326	2783	-15.34	0.05	-0.01
31	SLE RA 1	1	199	1768	-9.32	0.61	-0.01
31	SLE RA 2	-1	197	1754	-9.19	-0.76	0
31	SLE RA 3	1	199	1768	-9.32	0.61	-0.01
31	SLE RA 4	0	198	1760	-9.24	-0.21	0
31	SLE RA 5	-1	197	1754	-9.19	-0.76	0
31	SLE RA 6	1	199	1768	-9.32	0.61	-0.01
31	SLE RA 7	0	198	1760	-9.24	-0.21	0
31	SLE RA 8	1	199	1768	-9.32	0.61	-0.01
31	SLE RA 9	0	198	1760	-9.24	-0.21	0
31	SLE RA 10	-1	226	1966	-10.61	-0.55	0
31	SLE RA 11	1	229	1980	-10.75	0.82	-0.01
31	SLE RA 12	0	227	1972	-10.67	0	0
31	SLE RA 13	-1	226	1966	-10.61	-0.55	0
31	SLE RA 14	1	229	1980	-10.75	0.82	-0.01
31	SLE RA 15	0	227	1972	-10.67	0	0
31	SLE RA 16	1	229	1980	-10.75	0.82	-0.01
31	SLE RA 17	0	227	1972	-10.67	0	0
31	SLE RA 18	1	242	2071	-11.36	0.91	-0.01
31	SLE RA 19	0	240	2063	-11.28	0.09	0
31	SLE RA 20	1	242	2071	-11.36	0.91	-0.01
31	SLE RA 21	0	240	2063	-11.28	0.09	0
31	SLE FR 1	1	199	1768	-9.32	0.61	-0.01
31	SLE FR 2	0	199	1765	-9.29	0.34	-0.01
31	SLE FR 3	1	199	1768	-9.32	0.61	-0.01
31	SLE FR 4	0	212	1856	-9.91	0.43	-0.01
31	SLE FR 5	1	212	1859	-9.93	0.7	-0.01
31	SLE FR 6	1	220	1920	-10.34	0.76	-0.01
31	SLE QP 1	1	199	1768	-9.32	0.61	-0.01
31	SLE QP 2	1	212	1859	-9.93	0.7	-0.01
31	SLD 1	3	222	2115	-10.55	3.05	-0.02
31	SLD 2	3	222	2115	-10.55	3.05	-0.02
31	SLD 3	13	130	2008	-6.35	8.22	-0.05
31	SLD 4	13	130	2008	-6.35	8.22	-0.05



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
31	SLD 5	-14	355	2098	-16.48	-6.43	0.03
31	SLD 6	-14	355	2098	-16.48	-6.43	0.03
31	SLD 7	20	48	1742	-2.49	10.8	-0.07
31	SLD 8	20	48	1742	-2.49	10.8	-0.07
31	SLD 9	-18	377	1976	-17.37	-9.39	0.05
31	SLD 10	-18	377	1976	-17.37	-9.39	0.05
31	SLD 11	15	69	1621	-3.38	7.84	-0.05
31	SLD 12	15	69	1621	-3.38	7.84	-0.05
31	SLD 13	-11	294	1710	-13.52	-6.82	0.04
31	SLD 14	-11	294	1710	-13.52	-6.82	0.04
31	SLD 15	-1	202	1604	-9.32	-1.65	0.01
31	SLD 16	-1	202	1604	-9.32	-1.65	0.01
31	SLV 1	4	236	2467	-11.39	5.88	-0.04
31	SLV 2	4	236	2467	-11.39	5.88	-0.04
31	SLV 3	31	18	2206	-1.48	19.34	-0.11
31	SLV 4	31	18	2206	-1.48	19.34	-0.11
31	SLV 5	-38	549	2437	-25.39	-18.15	0.1
31	SLV 6	-38	549	2437	-25.39	-18.15	0.1
31	SLV 7	49	-176	1568	7.63	26.7	-0.16
31	SLV 8	49	-176	1568	7.63	26.7	-0.16
31	SLV 9	-48	600	2151	-27.49	-25.3	0.14
31	SLV 10	-48	600	2151	-27.49	-25.3	0.14
31	SLV 11	39	-125	1281	5.53	19.56	-0.12
31	SLV 12	39	-125	1281	5.53	19.56	-0.12
31	SLV 13	-29	406	1512	-18.38	-17.94	0.1
31	SLV 14	-29	406	1512	-18.38	-17.94	0.1
31	SLV 15	-3	188	1251	-8.48	-4.48	0.02
31	SLV 16	-3	188	1251	-8.48	-4.48	0.02
32	SLU 1	0	57	1365	2.16	-0.16	0
32	SLU 2	0	51	1343	2.34	-0.17	0
32	SLU 3	0	57	1365	2.16	-0.16	0
32	SLU 4	0	54	1352	2.27	-0.16	0
32	SLU 5	0	51	1343	2.34	-0.17	0
32	SLU 6	0	57	1365	2.16	-0.16	0
32	SLU 7	0	54	1352	2.27	-0.16	0
32	SLU 8	0	57	1365	2.16	-0.16	0
32	SLU 9	0	54	1352	2.27	-0.16	0
32	SLU 10	0	139	2098	5.58	-0.27	0
32	SLU 11	0	144	2119	5.39	-0.26	0
32	SLU 12	0	141	2106	5.5	-0.26	0
32	SLU 13	0	139	2098	5.58	-0.27	0
32	SLU 14	0	144	2119	5.39	-0.26	0
32	SLU 15	0	141	2106	5.5	-0.26	0
32	SLU 16	0	144	2119	5.39	-0.26	0
32	SLU 17	0	141	2106	5.5	-0.26	0
32	SLU 18	0	182	2443	6.78	-0.3	0
32	SLU 19	0	178	2430	6.89	-0.3	0
32	SLU 20	0	182	2443	6.78	-0.3	0
32	SLU 21	0	178	2430	6.89	-0.3	0
32	SLU 22	0	91	1677	3.47	-0.2	0
32	SLU 23	0	85	1655	3.66	-0.21	0
32	SLU 24	0	91	1677	3.47	-0.2	0
32	SLU 25	0	88	1664	3.58	-0.21	0
32	SLU 26	0	85	1655	3.66	-0.21	0
32	SLU 27	0	91	1677	3.47	-0.2	0
32	SLU 28	0	88	1664	3.58	-0.21	0
32	SLU 29	0	91	1677	3.47	-0.2	0
32	SLU 30	0	88	1664	3.58	-0.21	0
32	SLU 31	0	173	2410	6.89	-0.31	0
32	SLU 32	0	178	2431	6.71	-0.3	0
32	SLU 33	0	175	2418	6.82	-0.31	0
32	SLU 34	0	173	2410	6.89	-0.31	0
32	SLU 35	0	178	2431	6.71	-0.3	0
32	SLU 36	0	175	2418	6.82	-0.31	0
32	SLU 37	0	178	2431	6.71	-0.3	0
32	SLU 38	0	175	2418	6.82	-0.31	0
32	SLU 39	0	216	2755	8.1	-0.34	0
32	SLU 40	0	212	2742	8.21	-0.35	0
32	SLU 41	0	216	2755	8.1	-0.34	0
32	SLU 42	0	212	2742	8.21	-0.35	0
32	SLU 43	0	62	1667	2.35	-0.19	0
32	SLU 44	0	57	1646	2.54	-0.2	0
32	SLU 45	0	62	1667	2.35	-0.19	0
32	SLU 46	0	59	1654	2.46	-0.19	0
32	SLU 47	0	57	1646	2.54	-0.2	0
32	SLU 48	0	62	1667	2.35	-0.19	0
32	SLU 49	0	59	1654	2.46	-0.19	0
32	SLU 50	0	62	1667	2.35	-0.19	0
32	SLU 51	0	59	1654	2.46	-0.19	0
32	SLU 52	0	144	2400	5.77	-0.3	0
32	SLU 53	0	150	2422	5.59	-0.29	0
32	SLU 54	0	146	2409	5.7	-0.29	0
32	SLU 55	0	144	2400	5.77	-0.3	0
32	SLU 56	0	150	2422	5.59	-0.29	0
32	SLU 57	0	146	2409	5.7	-0.29	0
32	SLU 58	0	150	2422	5.59	-0.29	0
32	SLU 59	0	146	2409	5.7	-0.29	0
32	SLU 60	0	187	2745	6.98	-0.33	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
32	SLU 61	0	184	2732	7.09	-0.34	0
32	SLU 62	0	187	2745	6.98	-0.33	0
32	SLU 63	0	184	2732	7.09	-0.34	0
32	SLU 64	0	96	1979	3.67	-0.23	0
32	SLU 65	0	91	1958	3.85	-0.24	0
32	SLU 66	0	96	1979	3.67	-0.23	0
32	SLU 67	0	93	1966	3.78	-0.24	0
32	SLU 68	0	91	1958	3.85	-0.24	0
32	SLU 69	0	96	1979	3.67	-0.23	0
32	SLU 70	0	93	1966	3.78	-0.24	0
32	SLU 71	0	96	1979	3.67	-0.23	0
32	SLU 72	0	93	1966	3.78	-0.24	0
32	SLU 73	0	178	2712	7.09	-0.34	0
32	SLU 74	0	184	2734	6.9	-0.33	0
32	SLU 75	0	180	2721	7.02	-0.34	0
32	SLU 76	0	178	2712	7.09	-0.34	0
32	SLU 77	0	184	2734	6.9	-0.33	0
32	SLU 78	0	180	2721	7.02	-0.34	0
32	SLU 79	0	184	2734	6.9	-0.33	0
32	SLU 80	0	180	2721	7.02	-0.34	0
32	SLU 81	0	221	3057	8.29	-0.37	0
32	SLU 82	0	218	3044	8.4	-0.38	0
32	SLU 83	0	221	3057	8.29	-0.37	0
32	SLU 84	0	218	3044	8.4	-0.38	0
32	SLE RA 1	0	67	1454	2.53	-0.17	0
32	SLE RA 2	0	63	1440	2.65	-0.18	0
32	SLE RA 3	0	67	1454	2.53	-0.17	0
32	SLE RA 4	0	64	1445	2.61	-0.17	0
32	SLE RA 5	0	63	1440	2.65	-0.18	0
32	SLE RA 6	0	67	1454	2.53	-0.17	0
32	SLE RA 7	0	64	1445	2.61	-0.17	0
32	SLE RA 8	0	67	1454	2.53	-0.17	0
32	SLE RA 9	0	64	1445	2.61	-0.17	0
32	SLE RA 10	0	121	1943	4.81	-0.24	0
32	SLE RA 11	0	125	1957	4.69	-0.23	0
32	SLE RA 12	0	123	1948	4.76	-0.24	0
32	SLE RA 13	0	121	1943	4.81	-0.24	0
32	SLE RA 14	0	125	1957	4.69	-0.23	0
32	SLE RA 15	0	123	1948	4.76	-0.24	0
32	SLE RA 16	0	125	1957	4.69	-0.23	0
32	SLE RA 17	0	123	1948	4.76	-0.24	0
32	SLE RA 18	0	150	2173	5.62	-0.26	0
32	SLE RA 19	0	148	2164	5.69	-0.27	0
32	SLE RA 20	0	150	2173	5.62	-0.26	0
32	SLE RA 21	0	148	2164	5.69	-0.27	0
32	SLE FR 1	0	67	1454	2.53	-0.17	0
32	SLE FR 2	0	66	1451	2.56	-0.17	0
32	SLE FR 3	0	67	1454	2.53	-0.17	0
32	SLE FR 4	0	91	1667	3.48	-0.2	0
32	SLE FR 5	0	92	1669	3.46	-0.2	0
32	SLE FR 6	0	108	1813	4.07	-0.22	0
32	SLE QP 1	0	67	1454	2.53	-0.17	0
32	SLE QP 2	0	92	1669	3.46	-0.2	0
32	SLD 1	9	283	1789	-6.12	11.3	0
32	SLD 2	9	283	1789	-6.12	11.3	0
32	SLD 3	7	100	1925	3.03	9.29	-0.01
32	SLD 4	7	100	1925	3.03	9.29	-0.01
32	SLD 5	6	426	1499	-13.3	6.3	0
32	SLD 6	6	426	1499	-13.3	6.3	0
32	SLD 7	-1	-183	1953	17.21	-0.4	-0.01
32	SLD 8	-1	-183	1953	17.21	-0.4	-0.01
32	SLD 9	1	366	1386	-10.3	0	0.01
32	SLD 10	1	366	1386	-10.3	0	0.01
32	SLD 11	-6	-243	1840	20.21	-6.69	0
32	SLD 12	-6	-243	1840	20.21	-6.69	0
32	SLD 13	-8	83	1414	3.88	-9.68	0.01
32	SLD 14	-8	83	1414	3.88	-9.68	0.01
32	SLD 15	-10	-100	1550	13.04	-11.69	0
32	SLD 16	-10	-100	1550	13.04	-11.69	0
32	SLV 1	23	545	1943	-19.15	28.97	-0.01
32	SLV 2	23	545	1943	-19.15	28.97	-0.01
32	SLV 3	18	112	2291	2.47	23.81	-0.02
32	SLV 4	18	112	2291	2.47	23.81	-0.02
32	SLV 5	15	884	1224	-36.12	16.39	0.01
32	SLV 6	15	884	1224	-36.12	16.39	0.01
32	SLV 7	-3	-558	2383	35.96	-0.83	-0.02
32	SLV 8	-3	-558	2383	35.96	-0.83	-0.02
32	SLV 9	3	741	956	-29.05	0.44	0.02
32	SLV 10	3	741	956	-29.05	0.44	0.02
32	SLV 11	-16	-701	2115	43.04	-16.78	-0.01
32	SLV 12	-16	-701	2115	43.04	-16.78	-0.01
32	SLV 13	-18	71	1048	4.44	-24.2	0.02
32	SLV 14	-18	71	1048	4.44	-24.2	0.02
32	SLV 15	-24	-362	1396	26.07	-29.36	0.01
32	SLV 16	-24	-362	1396	26.07	-29.36	0.01
33	SLU 1	0	144	1643	-6.81	0.35	0
33	SLU 2	-2	141	1624	-6.68	-2.37	0.01
33	SLU 3	0	144	1643	-6.81	0.35	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
33	SLU 4	-1	142	1631	-6.73	-1.28	0.01
33	SLU 5	-2	141	1624	-6.68	-2.37	0.01
33	SLU 6	0	144	1643	-6.81	0.35	0
33	SLU 7	-1	142	1631	-6.73	-1.28	0.01
33	SLU 8	0	144	1643	-6.81	0.35	0
33	SLU 9	-1	142	1631	-6.73	-1.28	0.01
33	SLU 10	-3	182	1910	-8.64	-2.12	0.01
33	SLU 11	0	185	1929	-8.76	0.59	0
33	SLU 12	-2	183	1918	-8.69	-1.04	0.01
33	SLU 13	-3	182	1910	-8.64	-2.12	0.01
33	SLU 14	0	185	1929	-8.76	0.59	0
33	SLU 15	-2	183	1918	-8.69	-1.04	0.01
33	SLU 16	0	185	1929	-8.76	0.59	0
33	SLU 17	-2	183	1918	-8.69	-1.04	0.01
33	SLU 18	0	202	2052	-9.6	0.7	0
33	SLU 19	-2	200	2040	-9.52	-0.93	0.01
33	SLU 20	0	202	2052	-9.6	0.7	0
33	SLU 21	-2	200	2040	-9.52	-0.93	0.01
33	SLU 22	0	164	1776	-7.73	0.45	0
33	SLU 23	-3	160	1757	-7.6	-2.26	0.01
33	SLU 24	0	164	1776	-7.73	0.45	0
33	SLU 25	-1	162	1765	-7.65	-1.18	0.01
33	SLU 26	-3	160	1757	-7.6	-2.26	0.01
33	SLU 27	0	164	1776	-7.73	0.45	0
33	SLU 28	-1	162	1765	-7.65	-1.18	0.01
33	SLU 29	0	164	1776	-7.73	0.45	0
33	SLU 30	-1	162	1765	-7.65	-1.18	0.01
33	SLU 31	-3	201	2043	-9.55	-2.02	0.01
33	SLU 32	0	204	2062	-9.68	0.69	0
33	SLU 33	-2	202	2051	-9.61	-0.93	0.01
33	SLU 34	-3	201	2043	-9.55	-2.02	0.01
33	SLU 35	0	204	2062	-9.68	0.69	0
33	SLU 36	-2	202	2051	-9.61	-0.93	0.01
33	SLU 37	0	204	2062	-9.68	0.69	0
33	SLU 38	-2	202	2051	-9.61	-0.93	0.01
33	SLU 39	0	222	2185	-10.52	0.8	0
33	SLU 40	-2	220	2174	-10.44	-0.83	0.01
33	SLU 41	0	222	2185	-10.52	0.8	0
33	SLU 42	-2	220	2174	-10.44	-0.83	0.01
33	SLU 43	0	181	2090	-8.54	0.42	0
33	SLU 44	-2	178	2071	-8.41	-2.3	0.01
33	SLU 45	0	181	2090	-8.54	0.42	0
33	SLU 46	-1	179	2079	-8.46	-1.21	0.01
33	SLU 47	-2	178	2071	-8.41	-2.3	0.01
33	SLU 48	0	181	2090	-8.54	0.42	0
33	SLU 49	-1	179	2079	-8.46	-1.21	0.01
33	SLU 50	0	181	2090	-8.54	0.42	0
33	SLU 51	-1	179	2079	-8.46	-1.21	0.01
33	SLU 52	-3	218	2357	-10.36	-2.05	0.01
33	SLU 53	0	222	2377	-10.49	0.66	0
33	SLU 54	-1	220	2365	-10.41	-0.97	0.01
33	SLU 55	-3	218	2357	-10.36	-2.05	0.01
33	SLU 56	0	222	2377	-10.49	0.66	0
33	SLU 57	-1	220	2365	-10.41	-0.97	0.01
33	SLU 58	0	222	2377	-10.49	0.66	0
33	SLU 59	-1	220	2365	-10.41	-0.97	0.01
33	SLU 60	0	239	2499	-11.33	0.77	0
33	SLU 61	-1	237	2488	-11.25	-0.86	0.01
33	SLU 62	0	239	2499	-11.33	0.77	0
33	SLU 63	-1	237	2488	-11.25	-0.86	0.01
33	SLU 64	0	200	2223	-9.46	0.52	0
33	SLU 65	-2	197	2204	-9.33	-2.2	0.01
33	SLU 66	0	200	2223	-9.46	0.52	0
33	SLU 67	-1	198	2212	-9.38	-1.11	0.01
33	SLU 68	-2	197	2204	-9.33	-2.2	0.01
33	SLU 69	0	200	2223	-9.46	0.52	0
33	SLU 70	-1	198	2212	-9.38	-1.11	0.01
33	SLU 71	0	200	2223	-9.46	0.52	0
33	SLU 72	-1	198	2212	-9.38	-1.11	0.01
33	SLU 73	-3	238	2490	-11.28	-1.95	0.01
33	SLU 74	0	241	2510	-11.41	0.76	0
33	SLU 75	-1	239	2498	-11.33	-0.86	0.01
33	SLU 76	-3	238	2490	-11.28	-1.95	0.01
33	SLU 77	0	241	2510	-11.41	0.76	0
33	SLU 78	-1	239	2498	-11.33	-0.86	0.01
33	SLU 79	0	241	2510	-11.41	0.76	0
33	SLU 80	-1	239	2498	-11.33	-0.86	0.01
33	SLU 81	0	258	2632	-12.25	0.87	0
33	SLU 82	-2	256	2621	-12.17	-0.76	0.01
33	SLU 83	0	258	2632	-12.25	0.87	0
33	SLU 84	-2	256	2621	-12.17	-0.76	0.01
33	SLE RA 1	0	150	1681	-7.07	0.38	0
33	SLE RA 2	-2	148	1668	-6.99	-1.43	0.01
33	SLE RA 3	0	150	1681	-7.07	0.38	0
33	SLE RA 4	-1	149	1673	-7.02	-0.71	0
33	SLE RA 5	-2	148	1668	-6.99	-1.43	0.01
33	SLE RA 6	0	150	1681	-7.07	0.38	0
33	SLE RA 7	-1	149	1673	-7.02	-0.71	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
33	SLE RA 8	0	150	1681	-7.07	0.38	0
33	SLE RA 9	-1	149	1673	-7.02	-0.71	0
33	SLE RA 10	-2	175	1859	-8.29	-1.27	0.01
33	SLE RA 11	0	177	1872	-8.37	0.54	0
33	SLE RA 12	-1	176	1864	-8.32	-0.55	0
33	SLE RA 13	-2	175	1859	-8.29	-1.27	0.01
33	SLE RA 14	0	177	1872	-8.37	0.54	0
33	SLE RA 15	-1	176	1864	-8.32	-0.55	0
33	SLE RA 16	0	177	1872	-8.37	0.54	0
33	SLE RA 17	-1	176	1864	-8.32	-0.55	0
33	SLE RA 18	0	188	1954	-8.93	0.61	0
33	SLE RA 19	-1	187	1946	-8.88	-0.48	0
33	SLE RA 20	0	188	1954	-8.93	0.61	0
33	SLE RA 21	-1	187	1946	-8.88	-0.48	0
33	SLE FR 1	0	150	1681	-7.07	0.38	0
33	SLE FR 2	0	149	1679	-7.06	0.01	0
33	SLE FR 3	0	150	1681	-7.07	0.38	0
33	SLE FR 4	0	161	1760	-7.61	0.08	0
33	SLE FR 5	0	161	1763	-7.63	0.45	0
33	SLE FR 6	0	169	1817	-8	0.49	0
33	SLE QP 1	0	150	1681	-7.07	0.38	0
33	SLE QP 2	0	161	1763	-7.63	0.45	0
33	SLD 1	5	177	1957	-8.44	4.24	-0.03
33	SLD 2	5	177	1957	-8.44	4.24	-0.03
33	SLD 3	14	80	1880	-4.06	10.03	-0.07
33	SLD 4	14	80	1880	-4.06	10.03	-0.07
33	SLD 5	-13	314	1937	-14.51	-7.2	0.05
33	SLD 6	-13	314	1937	-14.51	-7.2	0.05
33	SLD 7	19	-10	1682	0.08	12.11	-0.09
33	SLD 8	19	-10	1682	0.08	12.11	-0.09
33	SLD 9	-19	333	1844	-15.34	-11.22	0.08
33	SLD 10	-19	333	1844	-15.34	-11.22	0.08
33	SLD 11	13	9	1588	-0.75	8.1	-0.06
33	SLD 12	13	9	1588	-0.75	8.1	-0.06
33	SLD 13	-14	243	1646	-11.2	-9.14	0.07
33	SLD 14	-14	243	1646	-11.2	-9.14	0.07
33	SLD 15	-5	145	1569	-6.82	-3.35	0.03
33	SLD 16	-5	145	1569	-6.82	-3.35	0.03
33	SLV 1	11	199	2224	-9.54	8.95	-0.06
33	SLV 2	11	199	2224	-9.54	8.95	-0.06
33	SLV 3	35	-30	2037	0.79	24.04	-0.17
33	SLV 4	35	-30	2037	0.79	24.04	-0.17
33	SLV 5	-34	520	2185	-23.87	-19.89	0.15
33	SLV 6	-34	520	2185	-23.87	-19.89	0.15
33	SLV 7	48	-244	1561	10.56	30.41	-0.22
33	SLV 8	48	-244	1561	10.56	30.41	-0.22
33	SLV 9	-48	566	1965	-25.82	-29.52	0.22
33	SLV 10	-48	566	1965	-25.82	-29.52	0.22
33	SLV 11	34	-197	1341	8.61	20.78	-0.15
33	SLV 12	34	-197	1341	8.61	20.78	-0.15
33	SLV 13	-35	353	1489	-16.05	-23.15	0.17
33	SLV 14	-35	353	1489	-16.05	-23.15	0.17
33	SLV 15	-11	124	1301	-5.72	-8.06	0.06
33	SLV 16	-11	124	1301	-5.72	-8.06	0.06
34	SLU 1	-3	336	1949	-14.86	-1.06	-0.02
34	SLU 2	-3	348	1980	-15.38	-0.91	-0.02
34	SLU 3	-3	336	1949	-14.86	-1.06	-0.02
34	SLU 4	-3	343	1967	-15.17	-0.97	-0.02
34	SLU 5	-3	348	1980	-15.38	-0.91	-0.02
34	SLU 6	-3	336	1949	-14.86	-1.06	-0.02
34	SLU 7	-3	343	1967	-15.17	-0.97	-0.02
34	SLU 8	-3	336	1949	-14.86	-1.06	-0.02
34	SLU 9	-3	343	1967	-15.17	-0.97	-0.02
34	SLU 10	-3	339	1968	-14	-1.04	-0.02
34	SLU 11	-3	327	1936	-13.48	-1.18	-0.02
34	SLU 12	-3	334	1955	-13.79	-1.09	-0.02
34	SLU 13	-3	339	1968	-14	-1.04	-0.02
34	SLU 14	-3	327	1936	-13.48	-1.18	-0.02
34	SLU 15	-3	334	1955	-13.79	-1.09	-0.02
34	SLU 16	-3	327	1936	-13.48	-1.18	-0.02
34	SLU 17	-3	334	1955	-13.79	-1.09	-0.02
34	SLU 18	-3	324	1931	-12.88	-1.23	-0.02
34	SLU 19	-3	331	1950	-13.2	-1.15	-0.02
34	SLU 20	-3	324	1931	-12.88	-1.23	-0.02
34	SLU 21	-3	331	1950	-13.2	-1.15	-0.02
34	SLU 22	-3	341	1969	-14.69	-1.13	-0.02
34	SLU 23	-3	353	2001	-15.21	-0.98	-0.02
34	SLU 24	-3	341	1969	-14.69	-1.13	-0.02
34	SLU 25	-3	348	1988	-15.01	-1.04	-0.02
34	SLU 26	-3	353	2001	-15.21	-0.98	-0.02
34	SLU 27	-3	341	1969	-14.69	-1.13	-0.02
34	SLU 28	-3	348	1988	-15.01	-1.04	-0.02
34	SLU 29	-3	341	1969	-14.69	-1.13	-0.02
34	SLU 30	-3	348	1988	-15.01	-1.04	-0.02
34	SLU 31	-3	344	1988	-13.83	-1.1	-0.02
34	SLU 32	-3	332	1957	-13.31	-1.25	-0.02
34	SLU 33	-3	340	1976	-13.62	-1.16	-0.02
34	SLU 34	-3	344	1988	-13.83	-1.1	-0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
34	SLU 35	-3	332	1957	-13.31	-1.25	-0.02
34	SLU 36	-3	340	1976	-13.62	-1.16	-0.02
34	SLU 37	-3	332	1957	-13.31	-1.25	-0.02
34	SLU 38	-3	340	1976	-13.62	-1.16	-0.02
34	SLU 39	-3	329	1952	-12.72	-1.3	-0.02
34	SLU 40	-3	336	1971	-13.03	-1.21	-0.02
34	SLU 41	-3	329	1952	-12.72	-1.3	-0.02
34	SLU 42	-3	336	1971	-13.03	-1.21	-0.02
34	SLU 43	-4	435	2526	-19.38	-1.35	-0.03
34	SLU 44	-4	447	2557	-19.9	-1.21	-0.03
34	SLU 45	-4	435	2526	-19.38	-1.35	-0.03
34	SLU 46	-4	442	2545	-19.69	-1.27	-0.03
34	SLU 47	-4	447	2557	-19.9	-1.21	-0.03
34	SLU 48	-4	435	2526	-19.38	-1.35	-0.03
34	SLU 49	-4	442	2545	-19.69	-1.27	-0.03
34	SLU 50	-4	435	2526	-19.38	-1.35	-0.03
34	SLU 51	-4	442	2545	-19.69	-1.27	-0.03
34	SLU 52	-4	438	2545	-18.51	-1.33	-0.03
34	SLU 53	-4	426	2514	-17.99	-1.48	-0.03
34	SLU 54	-4	433	2533	-18.3	-1.39	-0.03
34	SLU 55	-4	438	2545	-18.51	-1.33	-0.03
34	SLU 56	-4	426	2514	-17.99	-1.48	-0.03
34	SLU 57	-4	433	2533	-18.3	-1.39	-0.03
34	SLU 58	-4	426	2514	-17.99	-1.48	-0.03
34	SLU 59	-4	433	2533	-18.3	-1.39	-0.03
34	SLU 60	-4	423	2509	-17.4	-1.53	-0.03
34	SLU 61	-4	430	2527	-17.71	-1.44	-0.03
34	SLU 62	-4	423	2509	-17.4	-1.53	-0.03
34	SLU 63	-4	430	2527	-17.71	-1.44	-0.03
34	SLU 64	-4	440	2547	-19.21	-1.42	-0.03
34	SLU 65	-4	452	2578	-19.73	-1.28	-0.03
34	SLU 66	-4	440	2547	-19.21	-1.42	-0.03
34	SLU 67	-4	447	2566	-19.52	-1.33	-0.03
34	SLU 68	-4	452	2578	-19.73	-1.28	-0.03
34	SLU 69	-4	440	2547	-19.21	-1.42	-0.03
34	SLU 70	-4	447	2566	-19.52	-1.33	-0.03
34	SLU 71	-4	440	2547	-19.21	-1.42	-0.03
34	SLU 72	-4	447	2566	-19.52	-1.33	-0.03
34	SLU 73	-4	443	2566	-18.34	-1.4	-0.03
34	SLU 74	-4	432	2535	-17.83	-1.54	-0.03
34	SLU 75	-4	439	2553	-18.14	-1.46	-0.03
34	SLU 76	-4	443	2566	-18.34	-1.4	-0.03
34	SLU 77	-4	432	2535	-17.83	-1.54	-0.03
34	SLU 78	-4	439	2553	-18.14	-1.46	-0.03
34	SLU 79	-4	432	2535	-17.83	-1.54	-0.03
34	SLU 80	-4	439	2553	-18.14	-1.46	-0.03
34	SLU 81	-4	428	2529	-17.23	-1.6	-0.03
34	SLU 82	-4	435	2548	-17.54	-1.51	-0.03
34	SLU 83	-4	428	2529	-17.23	-1.6	-0.03
34	SLU 84	-4	435	2548	-17.54	-1.51	-0.03
34	SLE RA 1	-3	337	1955	-14.81	-1.08	-0.02
34	SLE RA 2	-3	345	1975	-15.16	-0.98	-0.02
34	SLE RA 3	-3	337	1955	-14.81	-1.08	-0.02
34	SLE RA 4	-3	342	1967	-15.02	-1.02	-0.02
34	SLE RA 5	-3	345	1975	-15.16	-0.98	-0.02
34	SLE RA 6	-3	337	1955	-14.81	-1.08	-0.02
34	SLE RA 7	-3	342	1967	-15.02	-1.02	-0.02
34	SLE RA 8	-3	337	1955	-14.81	-1.08	-0.02
34	SLE RA 9	-3	342	1967	-15.02	-1.02	-0.02
34	SLE RA 10	-3	340	1967	-14.24	-1.06	-0.02
34	SLE RA 11	-3	332	1946	-13.89	-1.16	-0.02
34	SLE RA 12	-3	336	1959	-14.1	-1.1	-0.02
34	SLE RA 13	-3	340	1967	-14.24	-1.06	-0.02
34	SLE RA 14	-3	332	1946	-13.89	-1.16	-0.02
34	SLE RA 15	-3	336	1959	-14.1	-1.1	-0.02
34	SLE RA 16	-3	332	1946	-13.89	-1.16	-0.02
34	SLE RA 17	-3	336	1959	-14.1	-1.1	-0.02
34	SLE RA 18	-3	329	1943	-13.5	-1.19	-0.02
34	SLE RA 19	-3	334	1955	-13.7	-1.14	-0.02
34	SLE RA 20	-3	329	1943	-13.5	-1.19	-0.02
34	SLE RA 21	-3	334	1955	-13.7	-1.14	-0.02
34	SLE FR 1	-3	337	1955	-14.81	-1.08	-0.02
34	SLE FR 2	-3	339	1959	-14.88	-1.06	-0.02
34	SLE FR 3	-3	337	1955	-14.81	-1.08	-0.02
34	SLE FR 4	-3	337	1955	-14.49	-1.09	-0.02
34	SLE FR 5	-3	335	1951	-14.42	-1.11	-0.02
34	SLE FR 6	-3	333	1949	-14.15	-1.14	-0.02
34	SLE QP 1	-3	337	1955	-14.81	-1.08	-0.02
34	SLE QP 2	-3	335	1951	-14.42	-1.11	-0.02
34	SLD 1	-8	287	1414	-13.1	-5.65	-0.01
34	SLD 2	-8	287	1414	-13.1	-5.65	-0.01
34	SLD 3	-5	138	889	-6.73	-4.26	-0.01
34	SLD 4	-5	138	889	-6.73	-4.26	-0.01
34	SLD 5	-8	547	2586	-23.67	-4.58	-0.03
34	SLD 6	-8	547	2586	-23.67	-4.58	-0.03
34	SLD 7	0	49	837	-2.46	0.04	0
34	SLD 8	0	49	837	-2.46	0.04	0
34	SLD 9	-6	621	3065	-26.37	-2.27	-0.04



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
34	SLD 10	-6	621	3065	-26.37	-2.27	-0.04
34	SLD 11	2	123	1317	-5.17	2.35	-0.01
34	SLD 12	2	123	1317	-5.17	2.35	-0.01
34	SLD 13	0	532	3013	-22.1	2.04	-0.04
34	SLD 14	0	532	3013	-22.1	2.04	-0.04
34	SLD 15	2	383	2488	-15.74	3.42	-0.03
34	SLD 16	2	383	2488	-15.74	3.42	-0.03
34	SLV 1	-15	217	691	-11.28	-12.44	0
34	SLV 2	-15	217	691	-11.28	-12.44	0
34	SLV 3	-9	-139	-633	3.75	-9.11	0.02
34	SLV 4	-9	-139	-633	3.75	-9.11	0.02
34	SLV 5	-16	838	3581	-36.27	-9.56	-0.04
34	SLV 6	-16	838	3581	-36.27	-9.56	-0.04
34	SLV 7	4	-346	-832	13.83	1.54	0.02
34	SLV 8	4	-346	-832	13.83	1.54	0.02
34	SLV 9	-10	1016	4734	-42.67	-3.76	-0.06
34	SLV 10	-10	1016	4734	-42.67	-3.76	-0.06
34	SLV 11	10	-168	321	7.44	7.33	0
34	SLV 12	10	-168	321	7.44	7.33	0
34	SLV 13	3	809	4535	-32.59	6.88	-0.06
34	SLV 14	3	809	4535	-32.59	6.88	-0.06
34	SLV 15	9	453	3211	-17.56	10.21	-0.04
34	SLV 16	9	453	3211	-17.56	10.21	-0.04
35	SLU 1	0	0	280	0	0	0
35	SLU 2	0	0	280	0	0	0
35	SLU 3	0	0	280	0	0	0
35	SLU 4	0	0	280	0	0	0
35	SLU 5	0	0	280	0	0	0
35	SLU 6	0	0	280	0	0	0
35	SLU 7	0	0	280	0	0	0
35	SLU 8	0	0	280	0	0	0
35	SLU 9	0	0	280	0	0	0
35	SLU 10	0	0	349	0.01	0	0
35	SLU 11	0	0	350	0.01	0	0
35	SLU 12	0	0	350	0.01	0	0
35	SLU 13	0	0	349	0.01	0	0
35	SLU 14	0	0	350	0.01	0	0
35	SLU 15	0	0	350	0.01	0	0
35	SLU 16	0	0	350	0.01	0	0
35	SLU 17	0	0	350	0.01	0	0
35	SLU 18	0	0	379	0.01	0	0
35	SLU 19	0	0	379	0.01	0	0
35	SLU 20	0	0	379	0.01	0	0
35	SLU 21	0	0	379	0.01	0	0
35	SLU 22	0	0	331	0	0	0
35	SLU 23	0	0	331	0.01	0	0
35	SLU 24	0	0	331	0	0	0
35	SLU 25	0	0	331	0.01	0	0
35	SLU 26	0	0	331	0.01	0	0
35	SLU 27	0	0	331	0	0	0
35	SLU 28	0	0	331	0.01	0	0
35	SLU 29	0	0	331	0	0	0
35	SLU 30	0	0	331	0.01	0	0
35	SLU 31	0	0	401	0.01	0	0
35	SLU 32	0	0	401	0.01	0	0
35	SLU 33	0	0	401	0.01	0	0
35	SLU 34	0	0	401	0.01	0	0
35	SLU 35	0	0	401	0.01	0	0
35	SLU 36	0	0	401	0.01	0	0
35	SLU 37	0	0	401	0.01	0	0
35	SLU 38	0	0	401	0.01	0	0
35	SLU 39	0	0	430	0.01	0	0
35	SLU 40	0	0	430	0.01	0	0
35	SLU 41	0	0	430	0.01	0	0
35	SLU 42	0	0	430	0.01	0	0
35	SLU 43	0	0	347	0	0	0
35	SLU 44	0	0	347	0	0	0
35	SLU 45	0	0	347	0	0	0
35	SLU 46	0	0	347	0	0	0
35	SLU 47	0	0	347	0	0	0
35	SLU 48	0	0	347	0	0	0
35	SLU 49	0	0	347	0	0	0
35	SLU 50	0	0	347	0	0	0
35	SLU 51	0	0	347	0	0	0
35	SLU 52	0	0	416	0.01	0	0
35	SLU 53	0	0	416	0.01	0	0
35	SLU 54	0	0	416	0.01	0	0
35	SLU 55	0	0	416	0.01	0	0
35	SLU 56	0	0	416	0.01	0	0
35	SLU 57	0	0	416	0.01	0	0
35	SLU 58	0	0	416	0.01	0	0
35	SLU 59	0	0	416	0.01	0	0
35	SLU 60	0	0	446	0.01	0	0
35	SLU 61	0	0	446	0.01	0	0
35	SLU 62	0	0	446	0.01	0	0
35	SLU 63	0	0	446	0.01	0	0
35	SLU 64	0	0	398	0	0	0
35	SLU 65	0	0	398	0.01	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
35	SLU 66	0	0	398	0	0	0
35	SLU 67	0	0	398	0.01	0	0
35	SLU 68	0	0	398	0.01	0	0
35	SLU 69	0	0	398	0	0	0
35	SLU 70	0	0	398	0.01	0	0
35	SLU 71	0	0	398	0	0	0
35	SLU 72	0	0	398	0.01	0	0
35	SLU 73	0	0	467	0.01	0	0
35	SLU 74	0	0	467	0.01	0	0
35	SLU 75	0	0	467	0.01	0	0
35	SLU 76	0	0	467	0.01	0	0
35	SLU 77	0	0	467	0.01	0	0
35	SLU 78	0	0	467	0.01	0	0
35	SLU 79	0	0	467	0.01	0	0
35	SLU 80	0	0	467	0.01	0	0
35	SLU 81	0	0	497	0.01	0	0
35	SLU 82	0	0	497	0.01	0	0
35	SLU 83	0	0	497	0.01	0	0
35	SLU 84	0	0	497	0.01	0	0
35	SLE RA 1	0	0	295	0	0	0
35	SLE RA 2	0	0	295	0	0	0
35	SLE RA 3	0	0	295	0	0	0
35	SLE RA 4	0	0	295	0	0	0
35	SLE RA 5	0	0	295	0	0	0
35	SLE RA 6	0	0	295	0	0	0
35	SLE RA 7	0	0	295	0	0	0
35	SLE RA 8	0	0	295	0	0	0
35	SLE RA 9	0	0	295	0	0	0
35	SLE RA 10	0	0	341	0.01	0	0
35	SLE RA 11	0	0	341	0.01	0	0
35	SLE RA 12	0	0	341	0.01	0	0
35	SLE RA 13	0	0	341	0.01	0	0
35	SLE RA 14	0	0	341	0.01	0	0
35	SLE RA 15	0	0	341	0.01	0	0
35	SLE RA 16	0	0	341	0.01	0	0
35	SLE RA 17	0	0	341	0.01	0	0
35	SLE RA 18	0	0	361	0.01	0	0
35	SLE RA 19	0	0	361	0.01	0	0
35	SLE RA 20	0	0	361	0.01	0	0
35	SLE RA 21	0	0	361	0.01	0	0
35	SLE FR 1	0	0	295	0	0	0
35	SLE FR 2	0	0	295	0	0	0
35	SLE FR 3	0	0	295	0	0	0
35	SLE FR 4	0	0	314	0	0	0
35	SLE FR 5	0	0	314	0	0	0
35	SLE FR 6	0	0	328	0	0	0
35	SLE QP 1	0	0	295	0	0	0
35	SLE QP 2	0	0	314	0	0	0
35	SLD 1	11	1	339	-2.98	0.02	0
35	SLD 2	11	1	339	-2.98	0.02	0
35	SLD 3	9	-1	335	2.65	0.02	0
35	SLD 4	9	-1	335	2.65	0.02	0
35	SLD 5	6	4	327	-9.44	0.01	0
35	SLD 6	6	4	327	-9.44	0.01	0
35	SLD 7	0	-4	315	9.34	0	0
35	SLD 8	0	-4	315	9.34	0	0
35	SLD 9	0	4	314	-9.33	0	0
35	SLD 10	0	4	314	-9.33	0	0
35	SLD 11	-7	-4	302	9.44	-0.01	0
35	SLD 12	-7	-4	302	9.44	-0.01	0
35	SLD 13	-10	1	294	-2.64	-0.02	0
35	SLD 14	-10	1	294	-2.64	-0.02	0
35	SLD 15	-12	-1	290	2.99	-0.03	0
35	SLD 16	-12	-1	290	2.99	-0.03	0
35	SLV 1	29	4	376	-7.42	0.06	0
35	SLV 2	29	4	376	-7.42	0.06	0
35	SLV 3	24	-2	367	6.59	0.05	0
35	SLV 4	24	-2	367	6.59	0.05	0
35	SLV 5	16	10	347	-23.47	0.04	-0.01
35	SLV 6	16	10	347	-23.47	0.04	-0.01
35	SLV 7	-1	-10	316	23.22	0	0.01
35	SLV 8	-1	-10	316	23.22	0	0.01
35	SLV 9	0	10	313	-23.21	0	-0.01
35	SLV 10	0	10	313	-23.21	0	-0.01
35	SLV 11	-16	-10	282	23.48	-0.04	0.01
35	SLV 12	-16	-10	282	23.48	-0.04	0.01
35	SLV 13	-24	2	262	-6.58	-0.05	0
35	SLV 14	-24	2	262	-6.58	-0.05	0
35	SLV 15	-29	-4	253	7.43	-0.06	0
35	SLV 16	-29	-4	253	7.43	-0.06	0
36	SLU 1	0	0	561	0.01	0	0
36	SLU 2	0	0	561	0.01	0	0
36	SLU 3	0	0	561	0.01	0	0
36	SLU 4	0	0	561	0.01	0	0
36	SLU 5	0	0	561	0.01	0	0
36	SLU 6	0	0	561	0.01	0	0
36	SLU 7	0	0	561	0.01	0	0
36	SLU 8	0	0	561	0.01	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
36	SLU 9	0	0	561	0.01	0	0
36	SLU 10	0	0	700	0.02	0	0
36	SLU 11	0	0	700	0.02	0	0
36	SLU 12	0	0	700	0.02	0	0
36	SLU 13	0	0	700	0.02	0	0
36	SLU 14	0	0	700	0.02	0	0
36	SLU 15	0	0	700	0.02	0	0
36	SLU 16	0	0	700	0.02	0	0
36	SLU 17	0	0	700	0.02	0	0
36	SLU 18	0	0	760	0.02	0	0
36	SLU 19	0	0	760	0.02	0	0
36	SLU 20	0	0	760	0.02	0	0
36	SLU 21	0	0	760	0.02	0	0
36	SLU 22	0	0	663	0.01	0	0
36	SLU 23	0	0	663	0.01	0	0
36	SLU 24	0	0	663	0.01	0	0
36	SLU 25	0	0	663	0.01	0	0
36	SLU 26	0	0	663	0.01	0	0
36	SLU 27	0	0	663	0.01	0	0
36	SLU 28	0	0	663	0.01	0	0
36	SLU 29	0	0	663	0.01	0	0
36	SLU 30	0	0	663	0.01	0	0
36	SLU 31	0	0	803	0.02	0	0
36	SLU 32	0	0	803	0.02	0	0
36	SLU 33	0	0	803	0.02	0	0
36	SLU 34	0	0	803	0.02	0	0
36	SLU 35	0	0	803	0.02	0	0
36	SLU 36	0	0	803	0.02	0	0
36	SLU 37	0	0	803	0.02	0	0
36	SLU 38	0	0	803	0.02	0	0
36	SLU 39	0	0	862	0.02	0	0
36	SLU 40	0	0	862	0.02	0	0
36	SLU 41	0	0	862	0.02	0	0
36	SLU 42	0	0	862	0.02	0	0
36	SLU 43	0	0	694	0.01	0	0
36	SLU 44	0	0	694	0.01	0	0
36	SLU 45	0	0	694	0.01	0	0
36	SLU 46	0	0	694	0.01	0	0
36	SLU 47	0	0	694	0.01	0	0
36	SLU 48	0	0	694	0.01	0	0
36	SLU 49	0	0	694	0.01	0	0
36	SLU 50	0	0	694	0.01	0	0
36	SLU 51	0	0	694	0.01	0	0
36	SLU 52	0	0	833	0.02	0	0
36	SLU 53	0	0	833	0.02	0	0
36	SLU 54	0	0	833	0.02	0	0
36	SLU 55	0	0	833	0.02	0	0
36	SLU 56	0	0	833	0.02	0	0
36	SLU 57	0	0	833	0.02	0	0
36	SLU 58	0	0	833	0.02	0	0
36	SLU 59	0	0	833	0.02	0	0
36	SLU 60	0	0	893	0.02	0	0
36	SLU 61	0	0	893	0.02	0	0
36	SLU 62	0	0	893	0.02	0	0
36	SLU 63	0	0	893	0.02	0	0
36	SLU 64	0	0	796	0.01	0	0
36	SLU 65	0	0	796	0.01	0	0
36	SLU 66	0	0	796	0.01	0	0
36	SLU 67	0	0	796	0.01	0	0
36	SLU 68	0	0	796	0.01	0	0
36	SLU 69	0	0	796	0.01	0	0
36	SLU 70	0	0	796	0.01	0	0
36	SLU 71	0	0	796	0.01	0	0
36	SLU 72	0	0	796	0.01	0	0
36	SLU 73	0	0	936	0.02	0	0
36	SLU 74	0	0	936	0.02	0	0
36	SLU 75	0	0	936	0.02	0	0
36	SLU 76	0	0	936	0.02	0	0
36	SLU 77	0	0	936	0.02	0	0
36	SLU 78	0	0	936	0.02	0	0
36	SLU 79	0	0	936	0.02	0	0
36	SLU 80	0	0	936	0.02	0	0
36	SLU 81	0	0	996	0.02	0	0
36	SLU 82	0	0	996	0.03	0	0
36	SLU 83	0	0	996	0.02	0	0
36	SLU 84	0	0	996	0.03	0	0
36	SLE RA 1	0	0	590	0.01	0	0
36	SLE RA 2	0	0	590	0.01	0	0
36	SLE RA 3	0	0	590	0.01	0	0
36	SLE RA 4	0	0	590	0.01	0	0
36	SLE RA 5	0	0	590	0.01	0	0
36	SLE RA 6	0	0	590	0.01	0	0
36	SLE RA 7	0	0	590	0.01	0	0
36	SLE RA 8	0	0	590	0.01	0	0
36	SLE RA 9	0	0	590	0.01	0	0
36	SLE RA 10	0	0	683	0.02	0	0
36	SLE RA 11	0	0	683	0.01	0	0
36	SLE RA 12	0	0	683	0.01	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione		
		x	y	z		x	y	z
36	SLE RA 13	0	0	683	0.02	0	0	0
36	SLE RA 14	0	0	683	0.01	0	0	0
36	SLE RA 15	0	0	683	0.01	0	0	0
36	SLE RA 16	0	0	683	0.01	0	0	0
36	SLE RA 17	0	0	683	0.01	0	0	0
36	SLE RA 18	0	0	723	0.02	0	0	0
36	SLE RA 19	0	0	723	0.02	0	0	0
36	SLE RA 20	0	0	723	0.02	0	0	0
36	SLE RA 21	0	0	723	0.02	0	0	0
36	SLE FR 1	0	0	590	0.01	0	0	0
36	SLE FR 2	0	0	590	0.01	0	0	0
36	SLE FR 3	0	0	590	0.01	0	0	0
36	SLE FR 4	0	0	630	0.01	0	0	0
36	SLE FR 5	0	0	630	0.01	0	0	0
36	SLE FR 6	0	0	656	0.01	0	0	0
36	SLE QP 1	0	0	590	0.01	0	0	0
36	SLE QP 2	0	0	630	0.01	0	0	0
36	SLD 1	2	2	630	-5.27	0.05	0	0
36	SLD 2	2	2	630	-5.27	0.05	0	0
36	SLD 3	1	-2	630	4.79	0.04	0	0
36	SLD 4	1	-2	630	4.79	0.04	0	0
36	SLD 5	1	7	630	-16.82	0.03	0	0
36	SLD 6	1	7	630	-16.82	0.03	0	0
36	SLD 7	0	-7	630	16.69	0	0	0
36	SLD 8	0	-7	630	16.69	0	0	0
36	SLD 9	0	7	630	-16.67	0	0	0
36	SLD 10	0	7	630	-16.67	0	0	0
36	SLD 11	-1	-7	630	16.84	-0.03	0	0
36	SLD 12	-1	-7	630	16.84	-0.03	0	0
36	SLD 13	-2	2	630	-4.77	-0.04	0	0
36	SLD 14	-2	2	630	-4.77	-0.04	0	0
36	SLD 15	-2	-2	630	5.29	-0.05	0	0
36	SLD 16	-2	-2	630	5.29	-0.05	0	0
36	SLV 1	5	6	630	-13.09	0.14	-0.01	0
36	SLV 2	5	6	630	-13.09	0.14	-0.01	0
36	SLV 3	4	-5	630	11.91	0.11	0	0
36	SLV 4	4	-5	630	11.91	0.11	0	0
36	SLV 5	2	18	630	-41.83	0.07	-0.01	0
36	SLV 6	2	18	630	-41.83	0.07	-0.01	0
36	SLV 7	0	-17	630	41.49	0	0.01	0
36	SLV 8	0	-17	630	41.49	0	0.01	0
36	SLV 9	0	17	630	-41.47	0	-0.01	0
36	SLV 10	0	17	630	-41.47	0	-0.01	0
36	SLV 11	-2	-18	630	41.85	-0.08	0.01	0
36	SLV 12	-2	-18	630	41.85	-0.08	0.01	0
36	SLV 13	-4	5	630	-11.88	-0.11	0	0
36	SLV 14	-4	5	630	-11.88	-0.11	0	0
36	SLV 15	-5	-6	630	13.11	-0.14	0.01	0
36	SLV 16	-5	-6	630	13.11	-0.14	0.01	0
37	SLU 1	0	0	561	0.01	0	0	0
37	SLU 2	0	0	561	0.01	0	0	0
37	SLU 3	0	0	561	0.01	0	0	0
37	SLU 4	0	0	561	0.01	0	0	0
37	SLU 5	0	0	561	0.01	0	0	0
37	SLU 6	0	0	561	0.01	0	0	0
37	SLU 7	0	0	561	0.01	0	0	0
37	SLU 8	0	0	561	0.01	0	0	0
37	SLU 9	0	0	561	0.01	0	0	0
37	SLU 10	0	0	700	0.02	0	0	0
37	SLU 11	0	0	700	0.02	0	0	0
37	SLU 12	0	0	700	0.02	0	0	0
37	SLU 13	0	0	700	0.02	0	0	0
37	SLU 14	0	0	700	0.02	0	0	0
37	SLU 15	0	0	700	0.02	0	0	0
37	SLU 16	0	0	700	0.02	0	0	0
37	SLU 17	0	0	700	0.02	0	0	0
37	SLU 18	0	0	760	0.02	0	0	0
37	SLU 19	0	0	760	0.03	0	0	0
37	SLU 20	0	0	760	0.02	0	0	0
37	SLU 21	0	0	760	0.03	0	0	0
37	SLU 22	0	0	663	0.01	0	0	0
37	SLU 23	0	0	663	0.02	0	0	0
37	SLU 24	0	0	663	0.01	0	0	0
37	SLU 25	0	0	663	0.01	0	0	0
37	SLU 26	0	0	663	0.02	0	0	0
37	SLU 27	0	0	663	0.01	0	0	0
37	SLU 28	0	0	663	0.01	0	0	0
37	SLU 29	0	0	663	0.01	0	0	0
37	SLU 30	0	0	663	0.01	0	0	0
37	SLU 31	0	0	803	0.03	0	0	0
37	SLU 32	0	0	803	0.02	0	0	0
37	SLU 33	0	0	803	0.03	0	0	0
37	SLU 34	0	0	803	0.03	0	0	0
37	SLU 35	0	0	803	0.02	0	0	0
37	SLU 36	0	0	803	0.03	0	0	0
37	SLU 37	0	0	803	0.02	0	0	0
37	SLU 38	0	0	803	0.03	0	0	0
37	SLU 39	0	0	863	0.03	0	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
37	SLU 40	0	0	863	0.03	0	0
37	SLU 41	0	0	863	0.03	0	0
37	SLU 42	0	0	863	0.03	0	0
37	SLU 43	0	0	694	0.01	0	0
37	SLU 44	0	0	694	0.01	0	0
37	SLU 45	0	0	694	0.01	0	0
37	SLU 46	0	0	694	0.01	0	0
37	SLU 47	0	0	694	0.01	0	0
37	SLU 48	0	0	694	0.01	0	0
37	SLU 49	0	0	694	0.01	0	0
37	SLU 50	0	0	694	0.01	0	0
37	SLU 51	0	0	694	0.01	0	0
37	SLU 52	0	0	833	0.02	0	0
37	SLU 53	0	0	833	0.02	0	0
37	SLU 54	0	0	833	0.02	0	0
37	SLU 55	0	0	833	0.02	0	0
37	SLU 56	0	0	833	0.02	0	0
37	SLU 57	0	0	833	0.02	0	0
37	SLU 58	0	0	833	0.02	0	0
37	SLU 59	0	0	833	0.02	0	0
37	SLU 60	0	0	893	0.02	0	0
37	SLU 61	0	0	893	0.03	0	0
37	SLU 62	0	0	893	0.02	0	0
37	SLU 63	0	0	893	0.03	0	0
37	SLU 64	0	0	796	0.01	0	0
37	SLU 65	0	0	796	0.02	0	0
37	SLU 66	0	0	796	0.01	0	0
37	SLU 67	0	0	796	0.02	0	0
37	SLU 68	0	0	796	0.02	0	0
37	SLU 69	0	0	796	0.01	0	0
37	SLU 70	0	0	796	0.02	0	0
37	SLU 71	0	0	796	0.01	0	0
37	SLU 72	0	0	796	0.02	0	0
37	SLU 73	0	0	936	0.03	0	0
37	SLU 74	0	0	936	0.02	0	0
37	SLU 75	0	0	936	0.03	0	0
37	SLU 76	0	0	936	0.03	0	0
37	SLU 77	0	0	936	0.02	0	0
37	SLU 78	0	0	936	0.03	0	0
37	SLU 79	0	0	936	0.02	0	0
37	SLU 80	0	0	936	0.03	0	0
37	SLU 81	0	0	996	0.03	0	0
37	SLU 82	0	0	996	0.03	0	0
37	SLU 83	0	0	996	0.03	0	0
37	SLU 84	0	0	996	0.03	0	0
37	SLE RA 1	0	0	590	0.01	0	0
37	SLE RA 2	0	0	590	0.01	0	0
37	SLE RA 3	0	0	590	0.01	0	0
37	SLE RA 4	0	0	590	0.01	0	0
37	SLE RA 5	0	0	590	0.01	0	0
37	SLE RA 6	0	0	590	0.01	0	0
37	SLE RA 7	0	0	590	0.01	0	0
37	SLE RA 8	0	0	590	0.01	0	0
37	SLE RA 9	0	0	590	0.01	0	0
37	SLE RA 10	0	0	683	0.02	0	0
37	SLE RA 11	0	0	683	0.02	0	0
37	SLE RA 12	0	0	683	0.02	0	0
37	SLE RA 13	0	0	683	0.02	0	0
37	SLE RA 14	0	0	683	0.02	0	0
37	SLE RA 15	0	0	683	0.02	0	0
37	SLE RA 16	0	0	683	0.02	0	0
37	SLE RA 17	0	0	683	0.02	0	0
37	SLE RA 18	0	0	723	0.02	0	0
37	SLE RA 19	0	0	723	0.02	0	0
37	SLE RA 20	0	0	723	0.02	0	0
37	SLE RA 21	0	0	723	0.02	0	0
37	SLE FR 1	0	0	590	0.01	0	0
37	SLE FR 2	0	0	590	0.01	0	0
37	SLE FR 3	0	0	590	0.01	0	0
37	SLE FR 4	0	0	630	0.01	0	0
37	SLE FR 5	0	0	630	0.01	0	0
37	SLE FR 6	0	0	656	0.01	0	0
37	SLE QP 1	0	0	590	0.01	0	0
37	SLE QP 2	0	0	630	0.01	0	0
37	SLD 1	2	2	630	-4.34	0.05	0
37	SLD 2	2	2	630	-4.34	0.05	0
37	SLD 3	1	-1	630	3.94	0.04	0
37	SLD 4	1	-1	630	3.94	0.04	0
37	SLD 5	2	6	630	-13.84	0.03	0
37	SLD 6	2	6	630	-13.84	0.03	0
37	SLD 7	-1	-6	630	13.74	0	0
37	SLD 8	-1	-6	630	13.74	0	0
37	SLD 9	1	6	630	-13.72	0	0
37	SLD 10	1	6	630	-13.72	0	0
37	SLD 11	-2	-6	630	13.87	-0.03	0
37	SLD 12	-2	-6	630	13.87	-0.03	0
37	SLD 13	-1	1	630	-3.91	-0.04	0
37	SLD 14	-1	1	630	-3.91	-0.04	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
37	SLD 15	-2	-2	630	4.37	-0.05	0
37	SLD 16	-2	-2	630	4.37	-0.05	0
37	SLV 1	5	5	630	-10.8	0.13	0
37	SLV 2	5	5	630	-10.8	0.13	0
37	SLV 3	3	-4	630	9.78	0.11	0
37	SLV 4	3	-4	630	9.78	0.11	0
37	SLV 5	4	15	630	-34.44	0.07	-0.01
37	SLV 6	4	15	630	-34.44	0.07	-0.01
37	SLV 7	-1	-14	630	34.15	0	0.01
37	SLV 8	-1	-14	630	34.15	0	0.01
37	SLV 9	1	14	630	-34.13	0	-0.01
37	SLV 10	1	14	630	-34.13	0	-0.01
37	SLV 11	-4	-15	630	34.46	-0.08	0.01
37	SLV 12	-4	-15	630	34.46	-0.08	0.01
37	SLV 13	-3	4	630	-9.76	-0.11	0
37	SLV 14	-3	4	630	-9.76	-0.11	0
37	SLV 15	-5	-5	630	10.82	-0.13	0
37	SLV 16	-5	-5	630	10.82	-0.13	0
38	SLU 1	0	0	561	0.01	0	0
38	SLU 2	0	0	561	0.01	0	0
38	SLU 3	0	0	561	0.01	0	0
38	SLU 4	0	0	561	0.01	0	0
38	SLU 5	0	0	561	0.01	0	0
38	SLU 6	0	0	561	0.01	0	0
38	SLU 7	0	0	561	0.01	0	0
38	SLU 8	0	0	561	0.01	0	0
38	SLU 9	0	0	561	0.01	0	0
38	SLU 10	0	0	700	0.03	0	0
38	SLU 11	0	0	700	0.02	0	0
38	SLU 12	0	0	700	0.02	0	0
38	SLU 13	0	0	700	0.03	0	0
38	SLU 14	0	0	700	0.02	0	0
38	SLU 15	0	0	700	0.02	0	0
38	SLU 16	0	0	700	0.02	0	0
38	SLU 17	0	0	700	0.02	0	0
38	SLU 18	0	0	760	0.03	0	0
38	SLU 19	0	0	760	0.03	0	0
38	SLU 20	0	0	760	0.03	0	0
38	SLU 21	0	0	760	0.03	0	0
38	SLU 22	0	0	663	0.01	0	0
38	SLU 23	0	0	663	0.02	0	0
38	SLU 24	0	0	663	0.01	0	0
38	SLU 25	0	0	663	0.02	0	0
38	SLU 26	0	0	663	0.02	0	0
38	SLU 27	0	0	663	0.01	0	0
38	SLU 28	0	0	663	0.02	0	0
38	SLU 29	0	0	663	0.01	0	0
38	SLU 30	0	0	663	0.02	0	0
38	SLU 31	0	0	803	0.03	0	0
38	SLU 32	0	0	803	0.03	0	0
38	SLU 33	0	0	803	0.03	0	0
38	SLU 34	0	0	803	0.03	0	0
38	SLU 35	0	0	803	0.03	0	0
38	SLU 36	0	0	803	0.03	0	0
38	SLU 37	0	0	803	0.03	0	0
38	SLU 38	0	0	803	0.03	0	0
38	SLU 39	0	0	862	0.03	0	0
38	SLU 40	0	0	862	0.03	0	0
38	SLU 41	0	0	862	0.03	0	0
38	SLU 42	0	0	862	0.03	0	0
38	SLU 43	0	0	694	0.01	0	0
38	SLU 44	0	0	694	0.01	0	0
38	SLU 45	0	0	694	0.01	0	0
38	SLU 46	0	0	694	0.01	0	0
38	SLU 47	0	0	694	0.01	0	0
38	SLU 48	0	0	694	0.01	0	0
38	SLU 49	0	0	694	0.01	0	0
38	SLU 50	0	0	694	0.01	0	0
38	SLU 51	0	0	694	0.01	0	0
38	SLU 52	0	0	833	0.03	0	0
38	SLU 53	0	0	833	0.02	0	0
38	SLU 54	0	0	833	0.03	0	0
38	SLU 55	0	0	833	0.03	0	0
38	SLU 56	0	0	833	0.02	0	0
38	SLU 57	0	0	833	0.03	0	0
38	SLU 58	0	0	833	0.02	0	0
38	SLU 59	0	0	833	0.03	0	0
38	SLU 60	0	0	893	0.03	0	0
38	SLU 61	0	0	893	0.03	0	0
38	SLU 62	0	0	893	0.03	0	0
38	SLU 63	0	0	893	0.03	0	0
38	SLU 64	0	0	796	0.02	0	0
38	SLU 65	0	0	796	0.02	0	0
38	SLU 66	0	0	796	0.02	0	0
38	SLU 67	0	0	796	0.02	0	0
38	SLU 68	0	0	796	0.02	0	0
38	SLU 69	0	0	796	0.02	0	0
38	SLU 70	0	0	796	0.02	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
38	SLU 71	0	0	796	0.02	0	0
38	SLU 72	0	0	796	0.02	0	0
38	SLU 73	0	0	936	0.03	0	0
38	SLU 74	0	0	936	0.03	0	0
38	SLU 75	0	0	936	0.03	0	0
38	SLU 76	0	0	936	0.03	0	0
38	SLU 77	0	0	936	0.03	0	0
38	SLU 78	0	0	936	0.03	0	0
38	SLU 79	0	0	936	0.03	0	0
38	SLU 80	0	0	936	0.03	0	0
38	SLU 81	0	0	996	0.03	0	0
38	SLU 82	0	0	996	0.04	0	0
38	SLU 83	0	0	996	0.03	0	0
38	SLU 84	0	0	996	0.04	0	0
38	SLE RA 1	0	0	590	0.01	0	0
38	SLE RA 2	0	0	590	0.01	0	0
38	SLE RA 3	0	0	590	0.01	0	0
38	SLE RA 4	0	0	590	0.01	0	0
38	SLE RA 5	0	0	590	0.01	0	0
38	SLE RA 6	0	0	590	0.01	0	0
38	SLE RA 7	0	0	590	0.01	0	0
38	SLE RA 8	0	0	590	0.01	0	0
38	SLE RA 9	0	0	590	0.01	0	0
38	SLE RA 10	0	0	683	0.02	0	0
38	SLE RA 11	0	0	683	0.02	0	0
38	SLE RA 12	0	0	683	0.02	0	0
38	SLE RA 13	0	0	683	0.02	0	0
38	SLE RA 14	0	0	683	0.02	0	0
38	SLE RA 15	0	0	683	0.02	0	0
38	SLE RA 16	0	0	683	0.02	0	0
38	SLE RA 17	0	0	683	0.02	0	0
38	SLE RA 18	0	0	723	0.02	0	0
38	SLE RA 19	0	0	723	0.02	0	0
38	SLE RA 20	0	0	723	0.02	0	0
38	SLE RA 21	0	0	723	0.02	0	0
38	SLE FR 1	0	0	590	0.01	0	0
38	SLE FR 2	0	0	590	0.01	0	0
38	SLE FR 3	0	0	590	0.01	0	0
38	SLE FR 4	0	0	630	0.01	0	0
38	SLE FR 5	0	0	630	0.01	0	0
38	SLE FR 6	0	0	656	0.02	0	0
38	SLE QP 1	0	0	590	0.01	0	0
38	SLE QP 2	0	0	630	0.01	0	0
38	SLD 1	3	2	630	-3.54	0.05	0
38	SLD 2	3	2	630	-3.54	0.05	0
38	SLD 3	1	-1	630	3.03	0.04	0
38	SLD 4	1	-1	630	3.03	0.04	0
38	SLD 5	3	5	630	-11.02	0.03	0
38	SLD 6	3	5	630	-11.02	0.03	0
38	SLD 7	-2	-5	630	10.89	0	0
38	SLD 8	-2	-5	630	10.89	0	0
38	SLD 9	2	5	630	-10.86	0	0
38	SLD 10	2	5	630	-10.86	0	0
38	SLD 11	-3	-5	630	11.05	-0.03	0
38	SLD 12	-3	-5	630	11.05	-0.03	0
38	SLD 13	-1	1	630	-3	-0.04	0
38	SLD 14	-1	1	630	-3	-0.04	0
38	SLD 15	-3	-2	630	3.57	-0.05	0
38	SLD 16	-3	-2	630	3.57	-0.05	0
38	SLV 1	7	5	630	-8.82	0.13	0
38	SLV 2	7	5	630	-8.82	0.13	0
38	SLV 3	3	-3	630	7.51	0.11	0
38	SLV 4	3	-3	630	7.51	0.11	0
38	SLV 5	7	12	630	-27.41	0.07	-0.01
38	SLV 6	7	12	630	-27.41	0.07	-0.01
38	SLV 7	-4	-12	630	27.03	0	0.01
38	SLV 8	-4	-12	630	27.03	0	0.01
38	SLV 9	4	12	630	-27	0	-0.01
38	SLV 10	4	12	630	-27	0	-0.01
38	SLV 11	-7	-12	630	27.43	-0.07	0.01
38	SLV 12	-7	-12	630	27.43	-0.07	0.01
38	SLV 13	-3	3	630	-7.48	-0.11	0
38	SLV 14	-3	3	630	-7.48	-0.11	0
38	SLV 15	-7	-5	630	8.85	-0.13	0
38	SLV 16	-7	-5	630	8.85	-0.13	0
39	SLU 1	0	0	561	0.01	0	0
39	SLU 2	0	0	561	0.01	0	0
39	SLU 3	0	0	561	0.01	0	0
39	SLU 4	0	0	561	0.01	0	0
39	SLU 5	0	0	561	0.01	0	0
39	SLU 6	0	0	561	0.01	0	0
39	SLU 7	0	0	561	0.01	0	0
39	SLU 8	0	0	561	0.01	0	0
39	SLU 9	0	0	561	0.01	0	0
39	SLU 10	0	0	700	0.03	0	0
39	SLU 11	0	0	700	0.02	0	0
39	SLU 12	0	0	700	0.02	0	0
39	SLU 13	0	0	700	0.03	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
39	SLU 14	0	0	700	0.02	0	0
39	SLU 15	0	0	700	0.02	0	0
39	SLU 16	0	0	700	0.02	0	0
39	SLU 17	0	0	700	0.02	0	0
39	SLU 18	0	0	760	0.03	0	0
39	SLU 19	0	0	760	0.03	0	0
39	SLU 20	0	0	760	0.03	0	0
39	SLU 21	0	0	760	0.03	0	0
39	SLU 22	0	0	663	0.01	0	0
39	SLU 23	0	0	663	0.02	0	0
39	SLU 24	0	0	663	0.01	0	0
39	SLU 25	0	0	663	0.02	0	0
39	SLU 26	0	0	663	0.02	0	0
39	SLU 27	0	0	663	0.01	0	0
39	SLU 28	0	0	663	0.02	0	0
39	SLU 29	0	0	663	0.01	0	0
39	SLU 30	0	0	663	0.02	0	0
39	SLU 31	0	0	803	0.03	0	0
39	SLU 32	0	0	803	0.03	0	0
39	SLU 33	0	0	803	0.03	0	0
39	SLU 34	0	0	803	0.03	0	0
39	SLU 35	0	0	803	0.03	0	0
39	SLU 36	0	0	803	0.03	0	0
39	SLU 37	0	0	803	0.03	0	0
39	SLU 38	0	0	803	0.03	0	0
39	SLU 39	0	0	863	0.03	0	0
39	SLU 40	0	0	863	0.03	0	0
39	SLU 41	0	0	863	0.03	0	0
39	SLU 42	0	0	863	0.03	0	0
39	SLU 43	0	0	694	0.01	0	0
39	SLU 44	0	0	694	0.01	0	0
39	SLU 45	0	0	694	0.01	0	0
39	SLU 46	0	0	694	0.01	0	0
39	SLU 47	0	0	694	0.01	0	0
39	SLU 48	0	0	694	0.01	0	0
39	SLU 49	0	0	694	0.01	0	0
39	SLU 50	0	0	694	0.01	0	0
39	SLU 51	0	0	694	0.01	0	0
39	SLU 52	0	0	833	0.03	0	0
39	SLU 53	0	0	833	0.02	0	0
39	SLU 54	0	0	833	0.03	0	0
39	SLU 55	0	0	833	0.03	0	0
39	SLU 56	0	0	833	0.02	0	0
39	SLU 57	0	0	833	0.03	0	0
39	SLU 58	0	0	833	0.02	0	0
39	SLU 59	0	0	833	0.03	0	0
39	SLU 60	0	0	893	0.03	0	0
39	SLU 61	0	0	893	0.03	0	0
39	SLU 62	0	0	893	0.03	0	0
39	SLU 63	0	0	893	0.03	0	0
39	SLU 64	0	0	796	0.01	0	0
39	SLU 65	0	0	796	0.02	0	0
39	SLU 66	0	0	796	0.01	0	0
39	SLU 67	0	0	796	0.02	0	0
39	SLU 68	0	0	796	0.02	0	0
39	SLU 69	0	0	796	0.01	0	0
39	SLU 70	0	0	796	0.02	0	0
39	SLU 71	0	0	796	0.01	0	0
39	SLU 72	0	0	796	0.02	0	0
39	SLU 73	0	0	936	0.03	0	0
39	SLU 74	0	0	936	0.03	0	0
39	SLU 75	0	0	936	0.03	0	0
39	SLU 76	0	0	936	0.03	0	0
39	SLU 77	0	0	936	0.03	0	0
39	SLU 78	0	0	936	0.03	0	0
39	SLU 79	0	0	936	0.03	0	0
39	SLU 80	0	0	936	0.03	0	0
39	SLU 81	0	0	996	0.03	0	0
39	SLU 82	0	0	996	0.04	0	0
39	SLU 83	0	0	996	0.03	0	0
39	SLU 84	0	0	996	0.04	0	0
39	SLE RA 1	0	0	590	0.01	0	0
39	SLE RA 2	0	0	590	0.01	0	0
39	SLE RA 3	0	0	590	0.01	0	0
39	SLE RA 4	0	0	590	0.01	0	0
39	SLE RA 5	0	0	590	0.01	0	0
39	SLE RA 6	0	0	590	0.01	0	0
39	SLE RA 7	0	0	590	0.01	0	0
39	SLE RA 8	0	0	590	0.01	0	0
39	SLE RA 9	0	0	590	0.01	0	0
39	SLE RA 10	0	0	683	0.02	0	0
39	SLE RA 11	0	0	683	0.02	0	0
39	SLE RA 12	0	0	683	0.02	0	0
39	SLE RA 13	0	0	683	0.02	0	0
39	SLE RA 14	0	0	683	0.02	0	0
39	SLE RA 15	0	0	683	0.02	0	0
39	SLE RA 16	0	0	683	0.02	0	0
39	SLE RA 17	0	0	683	0.02	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
39	SLE RA 18	0	0	723	0.02	0	0
39	SLE RA 19	0	0	723	0.02	0	0
39	SLE RA 20	0	0	723	0.02	0	0
39	SLE RA 21	0	0	723	0.02	0	0
39	SLE FR 1	0	0	590	0.01	0	0
39	SLE FR 2	0	0	590	0.01	0	0
39	SLE FR 3	0	0	590	0.01	0	0
39	SLE FR 4	0	0	630	0.01	0	0
39	SLE FR 5	0	0	630	0.01	0	0
39	SLE FR 6	0	0	656	0.02	0	0
39	SLE QP 1	0	0	590	0.01	0	0
39	SLE QP 2	0	0	630	0.01	0	0
39	SLD 1	2	2	630	-2.9	0.05	0
39	SLD 2	2	2	630	-2.9	0.05	0
39	SLD 3	1	-1	630	2.07	0.04	0
39	SLD 4	1	-1	630	2.07	0.04	0
39	SLD 5	3	4	630	-8.39	0.03	0
39	SLD 6	3	4	630	-8.39	0.03	0
39	SLD 7	-1	-4	630	8.16	0	0
39	SLD 8	-1	-4	630	8.16	0	0
39	SLD 9	1	4	630	-8.14	0	0
39	SLD 10	1	4	630	-8.14	0	0
39	SLD 11	-3	-4	630	8.42	-0.03	0
39	SLD 12	-3	-4	630	8.42	-0.03	0
39	SLD 13	-1	1	630	-2.04	-0.04	0
39	SLD 14	-1	1	630	-2.04	-0.04	0
39	SLD 15	-2	-2	630	2.92	-0.05	0
39	SLD 16	-2	-2	630	2.92	-0.05	0
39	SLV 1	6	5	630	-7.23	0.13	0
39	SLV 2	6	5	630	-7.23	0.13	0
39	SLV 3	3	-2	630	5.1	0.11	0
39	SLV 4	3	-2	630	5.1	0.11	0
39	SLV 5	6	11	630	-20.86	0.07	-0.01
39	SLV 6	6	11	630	-20.86	0.07	-0.01
39	SLV 7	-3	-10	630	20.24	0	0
39	SLV 8	-3	-10	630	20.24	0	0
39	SLV 9	3	10	630	-20.21	0	0
39	SLV 10	3	10	630	-20.21	0	0
39	SLV 11	-6	-11	630	20.88	-0.07	0.01
39	SLV 12	-6	-11	630	20.88	-0.07	0.01
39	SLV 13	-3	2	630	-5.07	-0.11	0
39	SLV 14	-3	2	630	-5.07	-0.11	0
39	SLV 15	-6	-5	630	7.26	-0.13	0
39	SLV 16	-6	-5	630	7.26	-0.13	0
40	SLU 1	0	0	561	0.01	0	0
40	SLU 2	0	0	561	0.01	0	0
40	SLU 3	0	0	561	0.01	0	0
40	SLU 4	0	0	561	0.01	0	0
40	SLU 5	0	0	561	0.01	0	0
40	SLU 6	0	0	561	0.01	0	0
40	SLU 7	0	0	561	0.01	0	0
40	SLU 8	0	0	561	0.01	0	0
40	SLU 9	0	0	561	0.01	0	0
40	SLU 10	0	0	700	0.02	0	0
40	SLU 11	0	0	700	0.02	0	0
40	SLU 12	0	0	700	0.02	0	0
40	SLU 13	0	0	700	0.02	0	0
40	SLU 14	0	0	700	0.02	0	0
40	SLU 15	0	0	700	0.02	0	0
40	SLU 16	0	0	700	0.02	0	0
40	SLU 17	0	0	700	0.02	0	0
40	SLU 18	0	0	760	0.02	0	0
40	SLU 19	0	0	760	0.03	0	0
40	SLU 20	0	0	760	0.02	0	0
40	SLU 21	0	0	760	0.03	0	0
40	SLU 22	0	0	663	0.01	0	0
40	SLU 23	0	0	663	0.02	0	0
40	SLU 24	0	0	663	0.01	0	0
40	SLU 25	0	0	663	0.01	0	0
40	SLU 26	0	0	663	0.02	0	0
40	SLU 27	0	0	663	0.01	0	0
40	SLU 28	0	0	663	0.01	0	0
40	SLU 29	0	0	663	0.01	0	0
40	SLU 30	0	0	663	0.01	0	0
40	SLU 31	0	0	803	0.03	0	0
40	SLU 32	0	0	803	0.02	0	0
40	SLU 33	0	0	803	0.03	0	0
40	SLU 34	0	0	803	0.03	0	0
40	SLU 35	0	0	803	0.02	0	0
40	SLU 36	0	0	803	0.03	0	0
40	SLU 37	0	0	803	0.02	0	0
40	SLU 38	0	0	803	0.03	0	0
40	SLU 39	0	0	862	0.03	0	0
40	SLU 40	0	0	862	0.03	0	0
40	SLU 41	0	0	862	0.03	0	0
40	SLU 42	0	0	862	0.03	0	0
40	SLU 43	0	0	694	0.01	0	0
40	SLU 44	0	0	694	0.01	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
40	SLU 45	0	0	694	0.01	0	0
40	SLU 46	0	0	694	0.01	0	0
40	SLU 47	0	0	694	0.01	0	0
40	SLU 48	0	0	694	0.01	0	0
40	SLU 49	0	0	694	0.01	0	0
40	SLU 50	0	0	694	0.01	0	0
40	SLU 51	0	0	694	0.01	0	0
40	SLU 52	0	0	833	0.02	0	0
40	SLU 53	0	0	833	0.02	0	0
40	SLU 54	0	0	833	0.02	0	0
40	SLU 55	0	0	833	0.02	0	0
40	SLU 56	0	0	833	0.02	0	0
40	SLU 57	0	0	833	0.02	0	0
40	SLU 58	0	0	833	0.02	0	0
40	SLU 59	0	0	833	0.02	0	0
40	SLU 60	0	0	893	0.02	0	0
40	SLU 61	0	0	893	0.03	0	0
40	SLU 62	0	0	893	0.02	0	0
40	SLU 63	0	0	893	0.03	0	0
40	SLU 64	0	0	796	0.01	0	0
40	SLU 65	0	0	796	0.02	0	0
40	SLU 66	0	0	796	0.01	0	0
40	SLU 67	0	0	796	0.02	0	0
40	SLU 68	0	0	796	0.02	0	0
40	SLU 69	0	0	796	0.01	0	0
40	SLU 70	0	0	796	0.02	0	0
40	SLU 71	0	0	796	0.01	0	0
40	SLU 72	0	0	796	0.02	0	0
40	SLU 73	0	0	936	0.03	0	0
40	SLU 74	0	0	936	0.02	0	0
40	SLU 75	0	0	936	0.03	0	0
40	SLU 76	0	0	936	0.03	0	0
40	SLU 77	0	0	936	0.02	0	0
40	SLU 78	0	0	936	0.03	0	0
40	SLU 79	0	0	936	0.02	0	0
40	SLU 80	0	0	936	0.03	0	0
40	SLU 81	0	0	996	0.03	0	0
40	SLU 82	0	0	996	0.03	0	0
40	SLU 83	0	0	996	0.03	0	0
40	SLU 84	0	0	996	0.03	0	0
40	SLE RA 1	0	0	590	0.01	0	0
40	SLE RA 2	0	0	590	0.01	0	0
40	SLE RA 3	0	0	590	0.01	0	0
40	SLE RA 4	0	0	590	0.01	0	0
40	SLE RA 5	0	0	590	0.01	0	0
40	SLE RA 6	0	0	590	0.01	0	0
40	SLE RA 7	0	0	590	0.01	0	0
40	SLE RA 8	0	0	590	0.01	0	0
40	SLE RA 9	0	0	590	0.01	0	0
40	SLE RA 10	0	0	683	0.02	0	0
40	SLE RA 11	0	0	683	0.02	0	0
40	SLE RA 12	0	0	683	0.02	0	0
40	SLE RA 13	0	0	683	0.02	0	0
40	SLE RA 14	0	0	683	0.02	0	0
40	SLE RA 15	0	0	683	0.02	0	0
40	SLE RA 16	0	0	683	0.02	0	0
40	SLE RA 17	0	0	683	0.02	0	0
40	SLE RA 18	0	0	723	0.02	0	0
40	SLE RA 19	0	0	723	0.02	0	0
40	SLE RA 20	0	0	723	0.02	0	0
40	SLE RA 21	0	0	723	0.02	0	0
40	SLE FR 1	0	0	590	0.01	0	0
40	SLE FR 2	0	0	590	0.01	0	0
40	SLE FR 3	0	0	590	0.01	0	0
40	SLE FR 4	0	0	630	0.01	0	0
40	SLE FR 5	0	0	630	0.01	0	0
40	SLE FR 6	0	0	656	0.01	0	0
40	SLE QP 1	0	0	590	0.01	0	0
40	SLE QP 2	0	0	630	0.01	0	0
40	SLD 1	2	2	630	-2.39	0.05	0
40	SLD 2	2	2	630	-2.39	0.05	0
40	SLD 3	2	0	630	1.11	0.04	0
40	SLD 4	2	0	630	1.11	0.04	0
40	SLD 5	1	4	630	-6.01	0.03	0
40	SLD 6	1	4	630	-6.01	0.03	0
40	SLD 7	0	-3	630	5.65	0	0
40	SLD 8	0	-3	630	5.65	0	0
40	SLD 9	0	3	630	-5.62	0	0
40	SLD 10	0	3	630	-5.62	0	0
40	SLD 11	-1	-4	630	6.04	-0.03	0
40	SLD 12	-1	-4	630	6.04	-0.03	0
40	SLD 13	-2	0	630	-1.08	-0.04	0
40	SLD 14	-2	0	630	-1.08	-0.04	0
40	SLD 15	-2	-2	630	2.41	-0.05	0
40	SLD 16	-2	-2	630	2.41	-0.05	0
40	SLV 1	5	5	630	-5.99	0.13	0
40	SLV 2	5	5	630	-5.99	0.13	0
40	SLV 3	4	0	630	2.68	0.11	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
40	SLV 4	4	0	630	2.68	0.11	0
40	SLV 5	3	10	630	-14.93	0.07	0
40	SLV 6	3	10	630	-14.93	0.07	0
40	SLV 7	0	-8	630	13.95	0	0
40	SLV 8	0	-8	630	13.95	0	0
40	SLV 9	0	8	630	-13.93	0	0
40	SLV 10	0	8	630	-13.93	0	0
40	SLV 11	-3	-10	630	14.95	-0.07	0
40	SLV 12	-3	-10	630	14.95	-0.07	0
40	SLV 13	-4	0	630	-2.65	-0.11	0
40	SLV 14	-4	0	630	-2.65	-0.11	0
40	SLV 15	-5	-5	630	6.01	-0.13	0
40	SLV 16	-5	-5	630	6.01	-0.13	0
41	SLU 1	0	0	561	0.01	0	0
41	SLU 2	0	0	561	0.01	0	0
41	SLU 3	0	0	561	0.01	0	0
41	SLU 4	0	0	561	0.01	0	0
41	SLU 5	0	0	561	0.01	0	0
41	SLU 6	0	0	561	0.01	0	0
41	SLU 7	0	0	561	0.01	0	0
41	SLU 8	0	0	561	0.01	0	0
41	SLU 9	0	0	561	0.01	0	0
41	SLU 10	0	0	700	0.02	0	0
41	SLU 11	0	0	700	0.01	0	0
41	SLU 12	0	0	700	0.02	0	0
41	SLU 13	0	0	700	0.02	0	0
41	SLU 14	0	0	700	0.01	0	0
41	SLU 15	0	0	700	0.02	0	0
41	SLU 16	0	0	700	0.01	0	0
41	SLU 17	0	0	700	0.02	0	0
41	SLU 18	0	0	760	0.02	0	0
41	SLU 19	0	0	760	0.02	0	0
41	SLU 20	0	0	760	0.02	0	0
41	SLU 21	0	0	760	0.02	0	0
41	SLU 22	0	0	663	0.01	0	0
41	SLU 23	0	0	663	0.01	0	0
41	SLU 24	0	0	663	0.01	0	0
41	SLU 25	0	0	663	0.01	0	0
41	SLU 26	0	0	663	0.01	0	0
41	SLU 27	0	0	663	0.01	0	0
41	SLU 28	0	0	663	0.01	0	0
41	SLU 29	0	0	663	0.01	0	0
41	SLU 30	0	0	663	0.01	0	0
41	SLU 31	0	0	803	0.02	0	0
41	SLU 32	0	0	803	0.02	0	0
41	SLU 33	0	0	803	0.02	0	0
41	SLU 34	0	0	803	0.02	0	0
41	SLU 35	0	0	803	0.02	0	0
41	SLU 36	0	0	803	0.02	0	0
41	SLU 37	0	0	803	0.02	0	0
41	SLU 38	0	0	803	0.02	0	0
41	SLU 39	0	0	863	0.02	0	0
41	SLU 40	0	0	863	0.02	0	0
41	SLU 41	0	0	863	0.02	0	0
41	SLU 42	0	0	863	0.02	0	0
41	SLU 43	0	0	694	0.01	0	0
41	SLU 44	0	0	694	0.01	0	0
41	SLU 45	0	0	694	0.01	0	0
41	SLU 46	0	0	694	0.01	0	0
41	SLU 47	0	0	694	0.01	0	0
41	SLU 48	0	0	694	0.01	0	0
41	SLU 49	0	0	694	0.01	0	0
41	SLU 50	0	0	694	0.01	0	0
41	SLU 51	0	0	694	0.01	0	0
41	SLU 52	0	0	833	0.02	0	0
41	SLU 53	0	0	833	0.01	0	0
41	SLU 54	0	0	833	0.02	0	0
41	SLU 55	0	0	833	0.02	0	0
41	SLU 56	0	0	833	0.01	0	0
41	SLU 57	0	0	833	0.02	0	0
41	SLU 58	0	0	833	0.01	0	0
41	SLU 59	0	0	833	0.02	0	0
41	SLU 60	0	0	893	0.02	0	0
41	SLU 61	0	0	893	0.02	0	0
41	SLU 62	0	0	893	0.02	0	0
41	SLU 63	0	0	893	0.02	0	0
41	SLU 64	0	0	796	0.01	0	0
41	SLU 65	0	0	796	0.01	0	0
41	SLU 66	0	0	796	0.01	0	0
41	SLU 67	0	0	796	0.01	0	0
41	SLU 68	0	0	796	0.01	0	0
41	SLU 69	0	0	796	0.01	0	0
41	SLU 70	0	0	796	0.01	0	0
41	SLU 71	0	0	796	0.01	0	0
41	SLU 72	0	0	796	0.01	0	0
41	SLU 73	0	0	936	0.02	0	0
41	SLU 74	0	0	936	0.02	0	0
41	SLU 75	0	0	936	0.02	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
41	SLU 76	0	0	936	0.02	0	0
41	SLU 77	0	0	936	0.02	0	0
41	SLU 78	0	0	936	0.02	0	0
41	SLU 79	0	0	936	0.02	0	0
41	SLU 80	0	0	936	0.02	0	0
41	SLU 81	0	0	996	0.02	0	0
41	SLU 82	0	0	996	0.02	0	0
41	SLU 83	0	0	996	0.02	0	0
41	SLU 84	0	0	996	0.02	0	0
41	SLE RA 1	0	0	590	0.01	0	0
41	SLE RA 2	0	0	590	0.01	0	0
41	SLE RA 3	0	0	590	0.01	0	0
41	SLE RA 4	0	0	590	0.01	0	0
41	SLE RA 5	0	0	590	0.01	0	0
41	SLE RA 6	0	0	590	0.01	0	0
41	SLE RA 7	0	0	590	0.01	0	0
41	SLE RA 8	0	0	590	0.01	0	0
41	SLE RA 9	0	0	590	0.01	0	0
41	SLE RA 10	0	0	683	0.02	0	0
41	SLE RA 11	0	0	683	0.01	0	0
41	SLE RA 12	0	0	683	0.01	0	0
41	SLE RA 13	0	0	683	0.02	0	0
41	SLE RA 14	0	0	683	0.01	0	0
41	SLE RA 15	0	0	683	0.01	0	0
41	SLE RA 16	0	0	683	0.01	0	0
41	SLE RA 17	0	0	683	0.01	0	0
41	SLE RA 18	0	0	723	0.01	0	0
41	SLE RA 19	0	0	723	0.02	0	0
41	SLE RA 20	0	0	723	0.01	0	0
41	SLE RA 21	0	0	723	0.02	0	0
41	SLE FR 1	0	0	590	0.01	0	0
41	SLE FR 2	0	0	590	0.01	0	0
41	SLE FR 3	0	0	590	0.01	0	0
41	SLE FR 4	0	0	630	0.01	0	0
41	SLE FR 5	0	0	630	0.01	0	0
41	SLE FR 6	0	0	656	0.01	0	0
41	SLE QP 1	0	0	590	0.01	0	0
41	SLE QP 2	0	0	630	0.01	0	0
41	SLD 1	2	2	630	-1.91	0.05	0
41	SLD 2	2	2	630	-1.91	0.05	0
41	SLD 3	2	0	630	0.3	0.05	0
41	SLD 4	2	0	630	0.3	0.05	0
41	SLD 5	1	3	630	-3.92	0.03	0
41	SLD 6	1	3	630	-3.92	0.03	0
41	SLD 7	0	-2	630	3.45	0	0
41	SLD 8	0	-2	630	3.45	0	0
41	SLD 9	0	2	630	-3.43	0	0
41	SLD 10	0	2	630	-3.43	0	0
41	SLD 11	-1	-3	630	3.94	-0.03	0
41	SLD 12	-1	-3	630	3.94	-0.03	0
41	SLD 13	-2	0	630	-0.28	-0.05	0
41	SLD 14	-2	0	630	-0.28	-0.05	0
41	SLD 15	-2	-2	630	1.93	-0.05	0
41	SLD 16	-2	-2	630	1.93	-0.05	0
41	SLV 1	6	5	630	-4.81	0.14	0
41	SLV 2	6	5	630	-4.81	0.14	0
41	SLV 3	5	1	630	0.65	0.12	0
41	SLV 4	5	1	630	0.65	0.12	0
41	SLV 5	3	7	630	-9.73	0.08	-0.01
41	SLV 6	3	7	630	-9.73	0.08	-0.01
41	SLV 7	0	-6	630	8.49	0	0
41	SLV 8	0	-6	630	8.49	0	0
41	SLV 9	0	6	630	-8.47	0	0
41	SLV 10	0	6	630	-8.47	0	0
41	SLV 11	-3	-7	630	9.74	-0.08	0.01
41	SLV 12	-3	-7	630	9.74	-0.08	0.01
41	SLV 13	-5	-1	630	-0.63	-0.12	0
41	SLV 14	-5	-1	630	-0.63	-0.12	0
41	SLV 15	-6	-5	630	4.83	-0.14	0
41	SLV 16	-6	-5	630	4.83	-0.14	0
42	SLU 1	0	0	561	0	0	0
42	SLU 2	0	0	561	0.01	0	0
42	SLU 3	0	0	561	0	0	0
42	SLU 4	0	0	561	0.01	0	0
42	SLU 5	0	0	561	0.01	0	0
42	SLU 6	0	0	561	0	0	0
42	SLU 7	0	0	561	0.01	0	0
42	SLU 8	0	0	561	0	0	0
42	SLU 9	0	0	561	0.01	0	0
42	SLU 10	0	0	700	0.01	-0.01	0
42	SLU 11	0	0	700	0.01	-0.01	0
42	SLU 12	0	0	700	0.01	-0.01	0
42	SLU 13	0	0	700	0.01	-0.01	0
42	SLU 14	0	0	700	0.01	-0.01	0
42	SLU 15	0	0	700	0.01	-0.01	0
42	SLU 16	0	0	700	0.01	-0.01	0
42	SLU 17	0	0	700	0.01	-0.01	0
42	SLU 18	0	0	760	0.01	-0.01	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
42	SLU 19	0	0	760	0.02	-0.01	0
42	SLU 20	0	0	760	0.01	-0.01	0
42	SLU 21	0	0	760	0.02	-0.01	0
42	SLU 22	0	0	663	0.01	-0.01	0
42	SLU 23	0	0	663	0.01	-0.01	0
42	SLU 24	0	0	663	0.01	-0.01	0
42	SLU 25	0	0	663	0.01	-0.01	0
42	SLU 26	0	0	663	0.01	-0.01	0
42	SLU 27	0	0	663	0.01	-0.01	0
42	SLU 28	0	0	663	0.01	-0.01	0
42	SLU 29	0	0	663	0.01	-0.01	0
42	SLU 30	0	0	663	0.01	-0.01	0
42	SLU 31	0	0	802	0.02	-0.01	0
42	SLU 32	0	0	802	0.01	-0.01	0
42	SLU 33	0	0	802	0.02	-0.01	0
42	SLU 34	0	0	802	0.02	-0.01	0
42	SLU 35	0	0	802	0.01	-0.01	0
42	SLU 36	0	0	802	0.02	-0.01	0
42	SLU 37	0	0	802	0.01	-0.01	0
42	SLU 38	0	0	802	0.02	-0.01	0
42	SLU 39	0	0	862	0.02	-0.01	0
42	SLU 40	0	0	862	0.02	-0.01	0
42	SLU 41	0	0	862	0.02	-0.01	0
42	SLU 42	0	0	862	0.02	-0.01	0
42	SLU 43	0	0	694	0	0	0
42	SLU 44	0	0	694	0.01	0	0
42	SLU 45	0	0	694	0	0	0
42	SLU 46	0	0	694	0.01	0	0
42	SLU 47	0	0	694	0.01	0	0
42	SLU 48	0	0	694	0	0	0
42	SLU 49	0	0	694	0.01	0	0
42	SLU 50	0	0	694	0	0	0
42	SLU 51	0	0	694	0.01	0	0
42	SLU 52	0	0	833	0.01	-0.01	0
42	SLU 53	0	0	833	0.01	-0.01	0
42	SLU 54	0	0	833	0.01	-0.01	0
42	SLU 55	0	0	833	0.01	-0.01	0
42	SLU 56	0	0	833	0.01	-0.01	0
42	SLU 57	0	0	833	0.01	-0.01	0
42	SLU 58	0	0	833	0.01	-0.01	0
42	SLU 59	0	0	833	0.01	-0.01	0
42	SLU 60	0	0	893	0.01	-0.01	0
42	SLU 61	0	0	893	0.02	-0.01	0
42	SLU 62	0	0	893	0.01	-0.01	0
42	SLU 63	0	0	893	0.02	-0.01	0
42	SLU 64	0	0	796	0.01	-0.01	0
42	SLU 65	0	0	796	0.01	-0.01	0
42	SLU 66	0	0	796	0.01	-0.01	0
42	SLU 67	0	0	796	0.01	-0.01	0
42	SLU 68	0	0	796	0.01	-0.01	0
42	SLU 69	0	0	796	0.01	-0.01	0
42	SLU 70	0	0	796	0.01	-0.01	0
42	SLU 71	0	0	796	0.01	-0.01	0
42	SLU 72	0	0	796	0.01	-0.01	0
42	SLU 73	0	0	935	0.02	-0.01	0
42	SLU 74	0	0	935	0.01	-0.01	0
42	SLU 75	0	0	935	0.02	-0.01	0
42	SLU 76	0	0	935	0.02	-0.01	0
42	SLU 77	0	0	935	0.01	-0.01	0
42	SLU 78	0	0	935	0.02	-0.01	0
42	SLU 79	0	0	935	0.01	-0.01	0
42	SLU 80	0	0	935	0.02	-0.01	0
42	SLU 81	0	0	995	0.02	-0.01	0
42	SLU 82	0	0	995	0.02	-0.01	0
42	SLU 83	0	0	995	0.02	-0.01	0
42	SLU 84	0	0	995	0.02	-0.01	0
42	SLE RA 1	0	0	590	0	0	0
42	SLE RA 2	0	0	590	0.01	0	0
42	SLE RA 3	0	0	590	0	0	0
42	SLE RA 4	0	0	590	0.01	0	0
42	SLE RA 5	0	0	590	0.01	0	0
42	SLE RA 6	0	0	590	0	0	0
42	SLE RA 7	0	0	590	0.01	0	0
42	SLE RA 8	0	0	590	0	0	0
42	SLE RA 9	0	0	590	0.01	0	0
42	SLE RA 10	0	0	683	0.01	-0.01	0
42	SLE RA 11	0	0	683	0.01	-0.01	0
42	SLE RA 12	0	0	683	0.01	-0.01	0
42	SLE RA 13	0	0	683	0.01	-0.01	0
42	SLE RA 14	0	0	683	0.01	-0.01	0
42	SLE RA 15	0	0	683	0.01	-0.01	0
42	SLE RA 16	0	0	683	0.01	-0.01	0
42	SLE RA 17	0	0	683	0.01	-0.01	0
42	SLE RA 18	0	0	723	0.01	-0.01	0
42	SLE RA 19	0	0	723	0.01	-0.01	0
42	SLE RA 20	0	0	723	0.01	-0.01	0
42	SLE RA 21	0	0	723	0.01	-0.01	0
42	SLE FR 1	0	0	590	0	0	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione		
		x	y	z		x	y	z
42	SLE FR 2	0	0	590	0.01	0	0	0
42	SLE FR 3	0	0	590	0	0	0	0
42	SLE FR 4	0	0	630	0.01	-0.01	0	0
42	SLE FR 5	0	0	630	0.01	-0.01	0	0
42	SLE FR 6	0	0	656	0.01	-0.01	0	0
42	SLE QP 1	0	0	590	0	0	0	0
42	SLE QP 2	0	0	630	0.01	-0.01	0	0
42	SLD 1	4	2	630	-1.37	0.02	0	0
42	SLD 2	4	2	630	-1.37	0.02	0	0
42	SLD 3	3	1	630	-0.21	0.01	0	0
42	SLD 4	3	1	630	-0.21	0.01	0	0
42	SLD 5	2	2	630	-2.17	0.01	0	0
42	SLD 6	2	2	630	-2.17	0.01	0	0
42	SLD 7	0	-1	630	1.71	-0.01	0	0
42	SLD 8	0	-1	630	1.71	-0.01	0	0
42	SLD 9	0	1	630	-1.69	-0.01	0	0
42	SLD 10	0	1	630	-1.69	-0.01	0	0
42	SLD 11	-2	-2	629	2.19	-0.02	0	0
42	SLD 12	-2	-2	629	2.19	-0.02	0	0
42	SLD 13	-3	-1	629	0.22	-0.02	0	0
42	SLD 14	-3	-1	629	0.22	-0.02	0	0
42	SLD 15	-4	-1	629	1.39	-0.03	0	0
42	SLD 16	-4	-1	629	1.39	-0.03	0	0
42	SLV 1	10	4	632	-3.47	0.05	0	0
42	SLV 2	10	4	632	-3.47	0.05	0	0
42	SLV 3	8	1	631	-0.6	0.04	0	0
42	SLV 4	8	1	631	-0.6	0.04	0	0
42	SLV 5	5	5	631	-5.39	0.03	0	0
42	SLV 6	5	5	631	-5.39	0.03	0	0
42	SLV 7	0	-3	630	4.18	-0.01	0	0
42	SLV 8	0	-3	630	4.18	-0.01	0	0
42	SLV 9	0	3	630	-4.16	0	0	0
42	SLV 10	0	3	630	-4.16	0	0	0
42	SLV 11	-5	-5	628	5.4	-0.04	0	0
42	SLV 12	-5	-5	628	5.4	-0.04	0	0
42	SLV 13	-8	-1	628	0.62	-0.05	0	0
42	SLV 14	-8	-1	628	0.62	-0.05	0	0
42	SLV 15	-10	-4	628	3.49	-0.06	0	0
42	SLV 16	-10	-4	628	3.49	-0.06	0	0
43	SLU 1	0	0	561	0	0.02	0	0
43	SLU 2	0	0	561	0.01	0.01	0	0
43	SLU 3	0	0	561	0	0.02	0	0
43	SLU 4	0	0	561	0.01	0.01	0	0
43	SLU 5	0	0	561	0.01	0.01	0	0
43	SLU 6	0	0	561	0	0.02	0	0
43	SLU 7	0	0	561	0.01	0.01	0	0
43	SLU 8	0	0	561	0	0.02	0	0
43	SLU 9	0	0	561	0.01	0.01	0	0
43	SLU 10	0	0	701	0.01	0.03	0	0
43	SLU 11	0	0	701	0.01	0.03	0	0
43	SLU 12	0	0	701	0.01	0.03	0	0
43	SLU 13	0	0	701	0.01	0.03	0	0
43	SLU 14	0	0	701	0.01	0.03	0	0
43	SLU 15	0	0	701	0.01	0.03	0	0
43	SLU 16	0	0	701	0.01	0.03	0	0
43	SLU 17	0	0	701	0.01	0.03	0	0
43	SLU 18	0	0	761	0.01	0.04	0	0
43	SLU 19	0	0	761	0.01	0.04	0	0
43	SLU 20	0	0	761	0.01	0.04	0	0
43	SLU 21	0	0	761	0.01	0.04	0	0
43	SLU 22	0	0	664	0.01	0.02	0	0
43	SLU 23	0	0	664	0.01	0.02	0	0
43	SLU 24	0	0	664	0.01	0.02	0	0
43	SLU 25	0	0	664	0.01	0.02	0	0
43	SLU 26	0	0	664	0.01	0.02	0	0
43	SLU 27	0	0	664	0.01	0.02	0	0
43	SLU 28	0	0	664	0.01	0.02	0	0
43	SLU 29	0	0	664	0.01	0.02	0	0
43	SLU 30	0	0	664	0.01	0.02	0	0
43	SLU 31	0	0	804	0.01	0.04	0	0
43	SLU 32	0	0	804	0.01	0.04	0	0
43	SLU 33	0	0	804	0.01	0.04	0	0
43	SLU 34	0	0	804	0.01	0.04	0	0
43	SLU 35	0	0	804	0.01	0.04	0	0
43	SLU 36	0	0	804	0.01	0.04	0	0
43	SLU 37	0	0	804	0.01	0.04	0	0
43	SLU 38	0	0	804	0.01	0.04	0	0
43	SLU 39	0	0	864	0.01	0.05	0	0
43	SLU 40	0	0	864	0.01	0.05	0	0
43	SLU 41	0	0	864	0.01	0.05	0	0
43	SLU 42	0	0	864	0.01	0.05	0	0
43	SLU 43	0	0	694	0.01	0.02	0	0
43	SLU 44	0	0	694	0.01	0.02	0	0
43	SLU 45	0	0	694	0.01	0.02	0	0
43	SLU 46	0	0	694	0.01	0.02	0	0
43	SLU 47	0	0	694	0.01	0.02	0	0
43	SLU 48	0	0	694	0.01	0.02	0	0
43	SLU 49	0	0	694	0.01	0.02	0	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione		
		x	y	z		x	y	z
43	SLU 50	0	0	694		0.01	0.02	0
43	SLU 51	0	0	694		0.01	0.02	0
43	SLU 52	0	0	834		0.01	0.04	0
43	SLU 53	0	0	834		0.01	0.04	0
43	SLU 54	0	0	834		0.01	0.04	0
43	SLU 55	0	0	834		0.01	0.04	0
43	SLU 56	0	0	834		0.01	0.04	0
43	SLU 57	0	0	834		0.01	0.04	0
43	SLU 58	0	0	834		0.01	0.04	0
43	SLU 59	0	0	834		0.01	0.04	0
43	SLU 60	0	0	894		0.01	0.04	0
43	SLU 61	0	0	894		0.01	0.04	0
43	SLU 62	0	0	894		0.01	0.04	0
43	SLU 63	0	0	894		0.01	0.04	0
43	SLU 64	0	0	797		0.01	0.02	0
43	SLU 65	0	0	797		0.01	0.02	0
43	SLU 66	0	0	797		0.01	0.02	0
43	SLU 67	0	0	797		0.01	0.02	0
43	SLU 68	0	0	797		0.01	0.02	0
43	SLU 69	0	0	797		0.01	0.02	0
43	SLU 70	0	0	797		0.01	0.02	0
43	SLU 71	0	0	797		0.01	0.02	0
43	SLU 72	0	0	797		0.01	0.02	0
43	SLU 73	0	0	937		0.01	0.04	0
43	SLU 74	0	0	937		0.01	0.04	0
43	SLU 75	0	0	937		0.01	0.04	0
43	SLU 76	0	0	937		0.01	0.04	0
43	SLU 77	0	0	937		0.01	0.04	0
43	SLU 78	0	0	937		0.01	0.04	0
43	SLU 79	0	0	937		0.01	0.04	0
43	SLU 80	0	0	937		0.01	0.04	0
43	SLU 81	0	0	997		0.01	0.05	0
43	SLU 82	0	0	997		0.01	0.05	0
43	SLU 83	0	0	997		0.01	0.05	0
43	SLU 84	0	0	997		0.01	0.05	0
43	SLE RA 1	0	0	590		0	0.02	0
43	SLE RA 2	0	0	590		0.01	0.02	0
43	SLE RA 3	0	0	590		0	0.02	0
43	SLE RA 4	0	0	590		0.01	0.02	0
43	SLE RA 5	0	0	590		0.01	0.02	0
43	SLE RA 6	0	0	590		0	0.02	0
43	SLE RA 7	0	0	590		0.01	0.02	0
43	SLE RA 8	0	0	590		0	0.02	0
43	SLE RA 9	0	0	590		0.01	0.02	0
43	SLE RA 10	0	0	684		0.01	0.03	0
43	SLE RA 11	0	0	684		0.01	0.03	0
43	SLE RA 12	0	0	684		0.01	0.03	0
43	SLE RA 13	0	0	684		0.01	0.03	0
43	SLE RA 14	0	0	684		0.01	0.03	0
43	SLE RA 15	0	0	684		0.01	0.03	0
43	SLE RA 16	0	0	684		0.01	0.03	0
43	SLE RA 17	0	0	684		0.01	0.03	0
43	SLE RA 18	0	0	724		0.01	0.04	0
43	SLE RA 19	0	0	724		0.01	0.04	0
43	SLE RA 20	0	0	724		0.01	0.04	0
43	SLE RA 21	0	0	724		0.01	0.04	0
43	SLE FR 1	0	0	590		0	0.02	0
43	SLE FR 2	0	0	590		0.01	0.02	0
43	SLE FR 3	0	0	590		0	0.02	0
43	SLE FR 4	0	0	630		0.01	0.02	0
43	SLE FR 5	0	0	630		0.01	0.02	0
43	SLE FR 6	0	0	657		0.01	0.03	0
43	SLE QP 1	0	0	590		0	0.02	0
43	SLE QP 2	0	0	630		0.01	0.02	0
43	SLD 1	8	1	633		-0.74	-0.12	0
43	SLD 2	8	1	633		-0.74	-0.12	0
43	SLD 3	6	1	633		-0.31	-0.1	0
43	SLD 4	6	1	633		-0.31	-0.1	0
43	SLD 5	5	1	632		-0.86	-0.06	0
43	SLD 6	5	1	632		-0.86	-0.06	0
43	SLD 7	-1	0	630		0.55	0.02	0
43	SLD 8	-1	0	630		0.55	0.02	0
43	SLD 9	0	0	630		-0.54	0.02	0
43	SLD 10	0	0	630		-0.54	0.02	0
43	SLD 11	-5	-1	629		0.87	0.1	0
43	SLD 12	-5	-1	629		0.87	0.1	0
43	SLD 13	-6	-1	628		0.33	0.14	0
43	SLD 14	-6	-1	628		0.33	0.14	0
43	SLD 15	-8	-1	627		0.75	0.17	0
43	SLD 16	-8	-1	627		0.75	0.17	0
43	SLV 1	20	2	638		-1.88	-0.35	0
43	SLV 2	20	2	638		-1.88	-0.35	0
43	SLV 3	16	1	637		-0.83	-0.28	0
43	SLV 4	16	1	637		-0.83	-0.28	0
43	SLV 5	12	2	634		-2.15	-0.18	0
43	SLV 6	12	2	634		-2.15	-0.18	0
43	SLV 7	-1	-1	631		1.34	0.03	0
43	SLV 8	-1	-1	631		1.34	0.03	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
43	SLV 9	1	1	630	-1.33	0.02	0
43	SLV 10	1	1	630	-1.33	0.02	0
43	SLV 11	-12	-2	626	2.16	0.23	0
43	SLV 12	-12	-2	626	2.16	0.23	0
43	SLV 13	-16	-1	624	0.84	0.33	0
43	SLV 14	-16	-1	624	0.84	0.33	0
43	SLV 15	-20	-2	623	1.89	0.39	0
43	SLV 16	-20	-2	623	1.89	0.39	0
44	SLU 1	0	19	1622	-4.49	-0.15	0
44	SLU 2	0	16	1591	-4.38	-0.18	0
44	SLU 3	0	19	1622	-4.49	-0.15	0
44	SLU 4	0	18	1603	-4.42	-0.17	0
44	SLU 5	0	16	1591	-4.38	-0.18	0
44	SLU 6	0	19	1622	-4.49	-0.15	0
44	SLU 7	0	18	1603	-4.42	-0.17	0
44	SLU 8	0	19	1622	-4.49	-0.15	0
44	SLU 9	0	18	1603	-4.42	-0.17	0
44	SLU 10	0	102	2587	-13.85	-0.31	0
44	SLU 11	0	105	2617	-13.96	-0.28	0
44	SLU 12	0	103	2599	-13.89	-0.29	0
44	SLU 13	0	102	2587	-13.85	-0.31	0
44	SLU 14	0	105	2617	-13.96	-0.28	0
44	SLU 15	0	103	2599	-13.89	-0.29	0
44	SLU 16	0	105	2617	-13.96	-0.28	0
44	SLU 17	0	103	2599	-13.89	-0.29	0
44	SLU 18	0	141	3044	-18.01	-0.33	0
44	SLU 19	0	139	3026	-17.95	-0.35	0
44	SLU 20	0	141	3044	-18.01	-0.33	0
44	SLU 21	0	139	3026	-17.95	-0.35	0
44	SLU 22	0	52	2038	-8.19	-0.2	0
44	SLU 23	0	49	2008	-8.08	-0.23	0
44	SLU 24	0	52	2038	-8.19	-0.2	0
44	SLU 25	0	50	2020	-8.13	-0.22	0
44	SLU 26	0	49	2008	-8.08	-0.23	0
44	SLU 27	0	52	2038	-8.19	-0.2	0
44	SLU 28	0	50	2020	-8.13	-0.22	0
44	SLU 29	0	52	2038	-8.19	-0.2	0
44	SLU 30	0	50	2020	-8.13	-0.22	0
44	SLU 31	0	134	3004	-17.55	-0.36	0
44	SLU 32	0	137	3034	-17.66	-0.33	0
44	SLU 33	0	135	3016	-17.59	-0.35	0
44	SLU 34	0	134	3004	-17.55	-0.36	0
44	SLU 35	0	137	3034	-17.66	-0.33	0
44	SLU 36	0	135	3016	-17.59	-0.35	0
44	SLU 37	0	137	3034	-17.66	-0.33	0
44	SLU 38	0	135	3016	-17.59	-0.35	0
44	SLU 39	0	174	3461	-21.71	-0.38	0
44	SLU 40	0	172	3442	-21.65	-0.4	0
44	SLU 41	0	174	3461	-21.71	-0.38	0
44	SLU 42	0	172	3442	-21.65	-0.4	0
44	SLU 43	0	14	1965	-4.57	-0.18	0
44	SLU 44	0	11	1935	-4.46	-0.21	0
44	SLU 45	0	14	1965	-4.57	-0.18	0
44	SLU 46	0	12	1947	-4.5	-0.19	0
44	SLU 47	0	11	1935	-4.46	-0.21	0
44	SLU 48	0	14	1965	-4.57	-0.18	0
44	SLU 49	0	12	1947	-4.5	-0.19	0
44	SLU 50	0	14	1965	-4.57	-0.18	0
44	SLU 51	0	12	1947	-4.5	-0.19	0
44	SLU 52	0	96	2930	-13.92	-0.33	0
44	SLU 53	0	99	2961	-14.03	-0.3	0
44	SLU 54	0	97	2942	-13.97	-0.32	0
44	SLU 55	0	96	2930	-13.92	-0.33	0
44	SLU 56	0	99	2961	-14.03	-0.3	0
44	SLU 57	0	97	2942	-13.97	-0.32	0
44	SLU 58	0	99	2961	-14.03	-0.3	0
44	SLU 59	0	97	2942	-13.97	-0.32	0
44	SLU 60	0	136	3387	-18.09	-0.36	0
44	SLU 61	0	134	3369	-18.02	-0.37	0
44	SLU 62	0	136	3387	-18.09	-0.36	0
44	SLU 63	0	134	3369	-18.02	-0.37	0
44	SLU 64	0	47	2382	-8.27	-0.23	0
44	SLU 65	0	44	2352	-8.16	-0.26	0
44	SLU 66	0	47	2382	-8.27	-0.23	0
44	SLU 67	0	45	2364	-8.2	-0.25	0
44	SLU 68	0	44	2352	-8.16	-0.26	0
44	SLU 69	0	47	2382	-8.27	-0.23	0
44	SLU 70	0	45	2364	-8.2	-0.25	0
44	SLU 71	0	47	2382	-8.27	-0.23	0
44	SLU 72	0	45	2364	-8.2	-0.25	0
44	SLU 73	0	129	3347	-17.63	-0.38	0
44	SLU 74	0	132	3377	-17.74	-0.35	0
44	SLU 75	0	130	3359	-17.67	-0.37	0
44	SLU 76	0	129	3347	-17.63	-0.38	0
44	SLU 77	0	132	3377	-17.74	-0.35	0
44	SLU 78	0	130	3359	-17.67	-0.37	0
44	SLU 79	0	132	3377	-17.74	-0.35	0
44	SLU 80	0	130	3359	-17.67	-0.37	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
44	SLU 81	0	168	3804	-21.79	-0.41	0
44	SLU 82	0	167	3786	-21.73	-0.43	0
44	SLU 83	0	168	3804	-21.79	-0.41	0
44	SLU 84	0	167	3786	-21.73	-0.43	0
44	SLE RA 1	0	29	1741	-5.55	-0.16	0
44	SLE RA 2	0	27	1720	-5.48	-0.18	0
44	SLE RA 3	0	29	1741	-5.55	-0.16	0
44	SLE RA 4	0	27	1729	-5.5	-0.18	0
44	SLE RA 5	0	27	1720	-5.48	-0.18	0
44	SLE RA 6	0	29	1741	-5.55	-0.16	0
44	SLE RA 7	0	27	1729	-5.5	-0.18	0
44	SLE RA 8	0	29	1741	-5.55	-0.16	0
44	SLE RA 9	0	27	1729	-5.5	-0.18	0
44	SLE RA 10	0	84	2384	-11.78	-0.27	0
44	SLE RA 11	0	85	2404	-11.86	-0.25	0
44	SLE RA 12	0	84	2392	-11.81	-0.26	0
44	SLE RA 13	0	84	2384	-11.78	-0.27	0
44	SLE RA 14	0	85	2404	-11.86	-0.25	0
44	SLE RA 15	0	84	2392	-11.81	-0.26	0
44	SLE RA 16	0	85	2404	-11.86	-0.25	0
44	SLE RA 17	0	84	2392	-11.81	-0.26	0
44	SLE RA 18	0	110	2689	-14.56	-0.28	0
44	SLE RA 19	0	109	2677	-14.52	-0.3	0
44	SLE RA 20	0	110	2689	-14.56	-0.28	0
44	SLE RA 21	0	109	2677	-14.52	-0.3	0
44	SLE FR 1	0	29	1741	-5.55	-0.16	0
44	SLE FR 2	0	28	1737	-5.53	-0.17	0
44	SLE FR 3	0	29	1741	-5.55	-0.16	0
44	SLE FR 4	0	53	2021	-8.24	-0.2	0
44	SLE FR 5	0	53	2025	-8.25	-0.2	0
44	SLE FR 6	0	69	2215	-10.06	-0.22	0
44	SLE QP 1	0	29	1741	-5.55	-0.16	0
44	SLE QP 2	0	53	2025	-8.25	-0.2	0
44	SLD 1	-7	198	2169	-16.66	14.74	0.01
44	SLD 2	-7	198	2169	-16.66	14.74	0.01
44	SLD 3	-6	61	2432	-8.79	12.21	0.02
44	SLD 4	-6	61	2432	-8.79	12.21	0.02
44	SLD 5	-4	305	1669	-22.7	8.11	-0.01
44	SLD 6	-4	305	1669	-22.7	8.11	-0.01
44	SLD 7	1	-153	2546	3.51	-0.31	0.02
44	SLD 8	1	-153	2546	3.51	-0.31	0.02
44	SLD 9	0	259	1504	-20.02	-0.09	-0.02
44	SLD 10	0	259	1504	-20.02	-0.09	-0.02
44	SLD 11	5	-199	2381	6.2	-8.51	0.01
44	SLD 12	5	-199	2381	6.2	-8.51	0.01
44	SLD 13	6	45	1618	-7.71	-12.61	-0.02
44	SLD 14	6	45	1618	-7.71	-12.61	-0.02
44	SLD 15	8	-92	1881	0.15	-15.14	-0.01
44	SLD 16	8	-92	1881	0.15	-15.14	-0.01
44	SLV 1	-19	398	2358	-28.2	37.75	0.04
44	SLV 2	-19	398	2358	-28.2	37.75	0.04
44	SLV 3	-15	71	2999	-9.52	31.24	0.05
44	SLV 4	-15	71	2999	-9.52	31.24	0.05
44	SLV 5	-11	653	1154	-42.56	21.05	-0.01
44	SLV 6	-11	653	1154	-42.56	21.05	-0.01
44	SLV 7	1	-438	3288	19.69	-0.64	0.04
44	SLV 8	1	-438	3288	19.69	-0.64	0.04
44	SLV 9	-1	544	762	-36.2	0.23	-0.04
44	SLV 10	-1	544	762	-36.2	0.23	-0.04
44	SLV 11	11	-547	2896	26.06	-21.45	0.01
44	SLV 12	11	-547	2896	26.06	-21.45	0.01
44	SLV 13	15	35	1052	-6.98	-31.65	-0.05
44	SLV 14	15	35	1052	-6.98	-31.65	-0.05
44	SLV 15	19	-292	1692	11.7	-38.15	-0.04
44	SLV 16	19	-292	1692	11.7	-38.15	-0.04
45	SLU 1	0	116	1574	-5.58	0.22	0
45	SLU 2	-3	112	1555	-5.37	-2.8	0.02
45	SLU 3	0	116	1574	-5.58	0.22	0
45	SLU 4	-2	114	1562	-5.45	-1.59	0.01
45	SLU 5	-3	112	1555	-5.37	-2.8	0.02
45	SLU 6	0	116	1574	-5.58	0.22	0
45	SLU 7	-2	114	1562	-5.45	-1.59	0.01
45	SLU 8	0	116	1574	-5.58	0.22	0
45	SLU 9	-2	114	1562	-5.45	-1.59	0.01
45	SLU 10	-3	154	1819	-7.33	-2.63	0.02
45	SLU 11	0	158	1838	-7.54	0.39	0
45	SLU 12	-2	155	1827	-7.42	-1.42	0.01
45	SLU 13	-3	154	1819	-7.33	-2.63	0.02
45	SLU 14	0	158	1838	-7.54	0.39	0
45	SLU 15	-2	155	1827	-7.42	-1.42	0.01
45	SLU 16	0	158	1838	-7.54	0.39	0
45	SLU 17	-2	155	1827	-7.42	-1.42	0.01
45	SLU 18	-1	176	1951	-8.38	0.46	0
45	SLU 19	-2	173	1940	-8.26	-1.35	0.01
45	SLU 20	-1	176	1951	-8.38	0.46	0
45	SLU 21	-2	173	1940	-8.26	-1.35	0.01
45	SLU 22	0	137	1698	-6.55	0.29	0
45	SLU 23	-3	133	1679	-6.34	-2.73	0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
45	SLU 24	0	137	1698	-6.55	0.29	0
45	SLU 25	-2	134	1686	-6.42	-1.52	0.01
45	SLU 26	-3	133	1679	-6.34	-2.73	0.02
45	SLU 27	0	137	1698	-6.55	0.29	0
45	SLU 28	-2	134	1686	-6.42	-1.52	0.01
45	SLU 29	0	137	1698	-6.55	0.29	0
45	SLU 30	-2	134	1686	-6.42	-1.52	0.01
45	SLU 31	-3	175	1943	-8.3	-2.56	0.02
45	SLU 32	-1	179	1962	-8.51	0.46	0
45	SLU 33	-2	176	1951	-8.38	-1.35	0.01
45	SLU 34	-3	175	1943	-8.3	-2.56	0.02
45	SLU 35	-1	179	1962	-8.51	0.46	0
45	SLU 36	-2	176	1951	-8.38	-1.35	0.01
45	SLU 37	-1	179	1962	-8.51	0.46	0
45	SLU 38	-2	176	1951	-8.38	-1.35	0.01
45	SLU 39	-1	197	2076	-9.35	0.53	0
45	SLU 40	-2	194	2064	-9.23	-1.28	0.01
45	SLU 41	-1	197	2076	-9.35	0.53	0
45	SLU 42	-2	194	2064	-9.23	-1.28	0.01
45	SLU 43	0	144	2003	-6.92	0.27	0
45	SLU 44	-3	140	1984	-6.71	-2.76	0.02
45	SLU 45	0	144	2003	-6.92	0.27	0
45	SLU 46	-2	141	1992	-6.79	-1.55	0.01
45	SLU 47	-3	140	1984	-6.71	-2.76	0.02
45	SLU 48	0	144	2003	-6.92	0.27	0
45	SLU 49	-2	141	1992	-6.79	-1.55	0.01
45	SLU 50	0	144	2003	-6.92	0.27	0
45	SLU 51	-2	141	1992	-6.79	-1.55	0.01
45	SLU 52	-3	181	2249	-8.67	-2.59	0.02
45	SLU 53	0	186	2268	-8.88	0.43	0
45	SLU 54	-2	183	2256	-8.76	-1.38	0.01
45	SLU 55	-3	181	2249	-8.67	-2.59	0.02
45	SLU 56	0	186	2268	-8.88	0.43	0
45	SLU 57	-2	183	2256	-8.76	-1.38	0.01
45	SLU 58	0	186	2268	-8.88	0.43	0
45	SLU 59	-2	183	2256	-8.76	-1.38	0.01
45	SLU 60	-1	204	2381	-9.73	0.51	0
45	SLU 61	-2	201	2370	-9.6	-1.31	0.01
45	SLU 62	-1	204	2381	-9.73	0.51	0
45	SLU 63	-2	201	2370	-9.6	-1.31	0.01
45	SLU 64	0	165	2127	-7.89	0.34	0
45	SLU 65	-3	160	2108	-7.68	-2.69	0.02
45	SLU 66	0	165	2127	-7.89	0.34	0
45	SLU 67	-2	162	2116	-7.76	-1.48	0.01
45	SLU 68	-3	160	2108	-7.68	-2.69	0.02
45	SLU 69	0	165	2127	-7.89	0.34	0
45	SLU 70	-2	162	2116	-7.76	-1.48	0.01
45	SLU 71	0	165	2127	-7.89	0.34	0
45	SLU 72	-2	162	2116	-7.76	-1.48	0.01
45	SLU 73	-3	202	2373	-9.64	-2.52	0.02
45	SLU 74	-1	206	2392	-9.85	0.5	0
45	SLU 75	-2	204	2380	-9.73	-1.31	0.01
45	SLU 76	-3	202	2373	-9.64	-2.52	0.02
45	SLU 77	-1	206	2392	-9.85	0.5	0
45	SLU 78	-2	204	2380	-9.73	-1.31	0.01
45	SLU 79	-1	206	2392	-9.85	0.5	0
45	SLU 80	-2	204	2380	-9.73	-1.31	0.01
45	SLU 81	-1	224	2505	-10.69	0.58	0
45	SLU 82	-2	222	2494	-10.57	-1.24	0.01
45	SLU 83	-1	224	2505	-10.69	0.58	0
45	SLU 84	-2	222	2494	-10.57	-1.24	0.01
45	SLE RA 1	0	122	1609	-5.85	0.24	0
45	SLE RA 2	-2	119	1596	-5.71	-1.77	0.01
45	SLE RA 3	0	122	1609	-5.85	0.24	0
45	SLE RA 4	-1	120	1601	-5.77	-0.97	0.01
45	SLE RA 5	-2	119	1596	-5.71	-1.77	0.01
45	SLE RA 6	0	122	1609	-5.85	0.24	0
45	SLE RA 7	-1	120	1601	-5.77	-0.97	0.01
45	SLE RA 8	0	122	1609	-5.85	0.24	0
45	SLE RA 9	-1	120	1601	-5.77	-0.97	0.01
45	SLE RA 10	-2	147	1773	-7.02	-1.66	0.01
45	SLE RA 11	0	150	1785	-7.16	0.36	0
45	SLE RA 12	-1	148	1778	-7.08	-0.85	0.01
45	SLE RA 13	-2	147	1773	-7.02	-1.66	0.01
45	SLE RA 14	0	150	1785	-7.16	0.36	0
45	SLE RA 15	-1	148	1778	-7.08	-0.85	0.01
45	SLE RA 16	0	150	1785	-7.16	0.36	0
45	SLE RA 17	-1	148	1778	-7.08	-0.85	0.01
45	SLE RA 18	0	162	1861	-7.73	0.4	0
45	SLE RA 19	-2	160	1853	-7.64	-0.81	0.01
45	SLE RA 20	0	162	1861	-7.73	0.4	0
45	SLE RA 21	-2	160	1853	-7.64	-0.81	0.01
45	SLE FR 1	0	122	1609	-5.85	0.24	0
45	SLE FR 2	-1	121	1607	-5.83	-0.16	0
45	SLE FR 3	0	122	1609	-5.85	0.24	0
45	SLE FR 4	-1	133	1682	-6.39	-0.11	0
45	SLE FR 5	0	134	1685	-6.42	0.29	0
45	SLE FR 6	0	142	1735	-6.79	0.32	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
45	SLE QP 1	0	122	1609	-5.85	0.24	0
45	SLE QP 2	0	134	1685	-6.42	0.29	0
45	SLD 1	7	154	1836	-7.37	5.04	-0.04
45	SLD 2	7	154	1836	-7.37	5.04	-0.04
45	SLD 3	14	51	1780	-2.69	10.48	-0.08
45	SLD 4	14	51	1780	-2.69	10.48	-0.08
45	SLD 5	-9	297	1815	-13.8	-6.53	0.05
45	SLD 6	-9	297	1815	-13.8	-6.53	0.05
45	SLD 7	15	-47	1629	1.8	11.6	-0.09
45	SLD 8	15	-47	1629	1.8	11.6	-0.09
45	SLD 9	-16	315	1740	-14.63	-11.02	0.09
45	SLD 10	-16	315	1740	-14.63	-11.02	0.09
45	SLD 11	9	-29	1555	0.97	7.12	-0.05
45	SLD 12	9	-29	1555	0.97	7.12	-0.05
45	SLD 13	-15	217	1589	-10.14	-9.9	0.09
45	SLD 14	-15	217	1589	-10.14	-9.9	0.09
45	SLD 15	-7	114	1533	-5.46	-4.46	0.04
45	SLD 16	-7	114	1533	-5.46	-4.46	0.04
45	SLV 1	16	182	2045	-8.67	11.11	-0.09
45	SLV 2	16	182	2045	-8.67	11.11	-0.09
45	SLV 3	35	-61	1910	2.37	25.24	-0.21
45	SLV 4	35	-61	1910	2.37	25.24	-0.21
45	SLV 5	-25	518	1998	-23.84	-17.89	0.14
45	SLV 6	-25	518	1998	-23.84	-17.89	0.14
45	SLV 7	39	-294	1546	12.96	29.21	-0.23
45	SLV 8	39	-294	1546	12.96	29.21	-0.23
45	SLV 9	-40	562	1823	-25.8	-28.62	0.23
45	SLV 10	-40	562	1823	-25.8	-28.62	0.23
45	SLV 11	24	-250	1371	11.01	18.48	-0.14
45	SLV 12	24	-250	1371	11.01	18.48	-0.14
45	SLV 13	-35	329	1460	-15.2	-24.65	0.21
45	SLV 14	-35	329	1460	-15.2	-24.65	0.21
45	SLV 15	-16	86	1324	-4.16	-10.52	0.1
45	SLV 16	-16	86	1324	-4.16	-10.52	0.1
46	SLU 1	0	292	1892	-12.69	-0.65	0.01
46	SLU 2	0	303	1923	-13.13	-0.3	0.01
46	SLU 3	0	292	1892	-12.69	-0.65	0.01
46	SLU 4	0	298	1911	-12.95	-0.44	0.01
46	SLU 5	0	303	1923	-13.13	-0.3	0.01
46	SLU 6	0	292	1892	-12.69	-0.65	0.01
46	SLU 7	0	298	1911	-12.95	-0.44	0.01
46	SLU 8	0	292	1892	-12.69	-0.65	0.01
46	SLU 9	0	298	1911	-12.95	-0.44	0.01
46	SLU 10	0	327	1941	-14.95	-0.67	0.01
46	SLU 11	0	317	1909	-14.5	-1.02	0.01
46	SLU 12	0	323	1928	-14.77	-0.81	0.01
46	SLU 13	0	327	1941	-14.95	-0.67	0.01
46	SLU 14	0	317	1909	-14.5	-1.02	0.01
46	SLU 15	0	323	1928	-14.77	-0.81	0.01
46	SLU 16	0	317	1909	-14.5	-1.02	0.01
46	SLU 17	0	323	1928	-14.77	-0.81	0.01
46	SLU 18	0	327	1917	-15.28	-1.18	0.01
46	SLU 19	0	334	1936	-15.55	-0.97	0.01
46	SLU 20	0	327	1917	-15.28	-1.18	0.01
46	SLU 21	0	334	1936	-15.55	-0.97	0.01
46	SLU 22	0	311	1925	-13.79	-0.81	0.01
46	SLU 23	0	322	1956	-14.23	-0.46	0.01
46	SLU 24	0	311	1925	-13.79	-0.81	0.01
46	SLU 25	0	318	1943	-14.06	-0.6	0.01
46	SLU 26	0	322	1956	-14.23	-0.46	0.01
46	SLU 27	0	311	1925	-13.79	-0.81	0.01
46	SLU 28	0	318	1943	-14.06	-0.6	0.01
46	SLU 29	0	311	1925	-13.79	-0.81	0.01
46	SLU 30	0	318	1943	-14.06	-0.6	0.01
46	SLU 31	0	346	1973	-16.05	-0.83	0.01
46	SLU 32	0	336	1942	-15.6	-1.18	0.01
46	SLU 33	0	342	1961	-15.87	-0.97	0.01
46	SLU 34	0	346	1973	-16.05	-0.83	0.01
46	SLU 35	0	336	1942	-15.6	-1.18	0.01
46	SLU 36	0	342	1961	-15.87	-0.97	0.01
46	SLU 37	0	336	1942	-15.6	-1.18	0.01
46	SLU 38	0	342	1961	-15.87	-0.97	0.01
46	SLU 39	0	346	1949	-16.38	-1.34	0.01
46	SLU 40	0	353	1968	-16.65	-1.13	0.01
46	SLU 41	0	346	1949	-16.38	-1.34	0.01
46	SLU 42	0	353	1968	-16.65	-1.13	0.01
46	SLU 43	0	373	2448	-16.11	-0.79	0.01
46	SLU 44	0	384	2480	-16.56	-0.44	0.01
46	SLU 45	0	373	2448	-16.11	-0.79	0.01
46	SLU 46	0	379	2467	-16.38	-0.58	0.01
46	SLU 47	0	384	2480	-16.56	-0.44	0.01
46	SLU 48	0	373	2448	-16.11	-0.79	0.01
46	SLU 49	0	379	2467	-16.38	-0.58	0.01
46	SLU 50	0	373	2448	-16.11	-0.79	0.01
46	SLU 51	0	379	2467	-16.38	-0.58	0.01
46	SLU 52	0	408	2497	-18.37	-0.81	0.01
46	SLU 53	0	398	2466	-17.93	-1.16	0.01
46	SLU 54	0	404	2485	-18.2	-0.95	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
46	SLU 55	0	408	2497	-18.37	-0.81	0.01
46	SLU 56	0	398	2466	-17.93	-1.16	0.01
46	SLU 57	0	404	2485	-18.2	-0.95	0.01
46	SLU 58	0	398	2466	-17.93	-1.16	0.01
46	SLU 59	0	404	2485	-18.2	-0.95	0.01
46	SLU 60	0	408	2473	-18.71	-1.32	0.01
46	SLU 61	0	415	2492	-18.97	-1.11	0.01
46	SLU 62	0	408	2473	-18.71	-1.32	0.01
46	SLU 63	0	415	2492	-18.97	-1.11	0.01
46	SLU 64	0	392	2481	-17.22	-0.95	0.01
46	SLU 65	0	403	2512	-17.66	-0.6	0.01
46	SLU 66	0	392	2481	-17.22	-0.95	0.01
46	SLU 67	0	399	2500	-17.48	-0.74	0.01
46	SLU 68	0	403	2512	-17.66	-0.6	0.01
46	SLU 69	0	392	2481	-17.22	-0.95	0.01
46	SLU 70	0	399	2500	-17.48	-0.74	0.01
46	SLU 71	0	392	2481	-17.22	-0.95	0.01
46	SLU 72	0	399	2500	-17.48	-0.74	0.01
46	SLU 73	0	427	2530	-19.48	-0.97	0.01
46	SLU 74	0	417	2498	-19.03	-1.32	0.01
46	SLU 75	0	423	2517	-19.3	-1.11	0.01
46	SLU 76	0	427	2530	-19.48	-0.97	0.01
46	SLU 77	0	417	2498	-19.03	-1.32	0.01
46	SLU 78	0	423	2517	-19.3	-1.11	0.01
46	SLU 79	0	417	2498	-19.03	-1.32	0.01
46	SLU 80	0	423	2517	-19.3	-1.11	0.01
46	SLU 81	0	427	2506	-19.81	-1.48	0.01
46	SLU 82	0	434	2525	-20.08	-1.27	0.01
46	SLU 83	0	427	2506	-19.81	-1.48	0.01
46	SLU 84	0	434	2525	-20.08	-1.27	0.01
46	SLE RA 1	0	297	1901	-13	-0.69	0.01
46	SLE RA 2	0	305	1922	-13.3	-0.46	0.01
46	SLE RA 3	0	297	1901	-13	-0.69	0.01
46	SLE RA 4	0	302	1914	-13.18	-0.55	0.01
46	SLE RA 5	0	305	1922	-13.3	-0.46	0.01
46	SLE RA 6	0	297	1901	-13	-0.69	0.01
46	SLE RA 7	0	302	1914	-13.18	-0.55	0.01
46	SLE RA 8	0	297	1901	-13	-0.69	0.01
46	SLE RA 9	0	302	1914	-13.18	-0.55	0.01
46	SLE RA 10	0	321	1934	-14.51	-0.71	0.01
46	SLE RA 11	0	314	1913	-14.21	-0.94	0.01
46	SLE RA 12	0	318	1925	-14.39	-0.8	0.01
46	SLE RA 13	0	321	1934	-14.51	-0.71	0.01
46	SLE RA 14	0	314	1913	-14.21	-0.94	0.01
46	SLE RA 15	0	318	1925	-14.39	-0.8	0.01
46	SLE RA 16	0	314	1913	-14.21	-0.94	0.01
46	SLE RA 17	0	318	1925	-14.39	-0.8	0.01
46	SLE RA 18	0	321	1918	-14.73	-1.05	0.01
46	SLE RA 19	0	325	1930	-14.91	-0.91	0.01
46	SLE RA 20	0	321	1918	-14.73	-1.05	0.01
46	SLE RA 21	0	325	1930	-14.91	-0.91	0.01
46	SLE FR 1	0	297	1901	-13	-0.69	0.01
46	SLE FR 2	0	299	1905	-13.06	-0.65	0.01
46	SLE FR 3	0	297	1901	-13	-0.69	0.01
46	SLE FR 4	0	306	1910	-13.58	-0.75	0.01
46	SLE FR 5	0	304	1906	-13.52	-0.8	0.01
46	SLE FR 6	0	309	1910	-13.86	-0.87	0.01
46	SLE QP 1	0	297	1901	-13	-0.69	0.01
46	SLE QP 2	0	304	1906	-13.52	-0.8	0.01
46	SLD 1	-11	263	1518	-12.13	-9.02	0.02
46	SLD 2	-11	263	1518	-12.13	-9.02	0.02
46	SLD 3	-8	110	1147	-5.64	-7.14	0.02
46	SLD 4	-8	110	1147	-5.64	-7.14	0.02
46	SLD 5	-7	524	2354	-22.94	-6.12	0.01
46	SLD 6	-7	524	2354	-22.94	-6.12	0.01
46	SLD 7	2	14	1114	-1.32	0.16	0.01
46	SLD 8	2	14	1114	-1.32	0.16	0.01
46	SLD 9	-2	595	2698	-25.72	-1.76	0.01
46	SLD 10	-2	595	2698	-25.72	-1.76	0.01
46	SLD 11	7	85	1459	-4.1	4.52	0
46	SLD 12	7	85	1459	-4.1	4.52	0
46	SLD 13	8	499	2666	-21.39	5.53	-0.01
46	SLD 14	8	499	2666	-21.39	5.53	-0.01
46	SLD 15	10	346	2294	-14.91	7.42	-0.01
46	SLD 16	10	346	2294	-14.91	7.42	-0.01
46	SLV 1	-26	204	1006	-10.18	-21.42	0.04
46	SLV 2	-26	204	1006	-10.18	-21.42	0.04
46	SLV 3	-20	-160	69	5.19	-16.94	0.03
46	SLV 4	-20	-160	69	5.19	-16.94	0.03
46	SLV 5	-18	826	3057	-35.84	-13.78	0.03
46	SLV 6	-18	826	3057	-35.84	-13.78	0.03
46	SLV 7	4	-386	-66	15.41	1.15	0
46	SLV 8	4	-386	-66	15.41	1.15	0
46	SLV 9	-4	995	3878	-42.45	-2.75	0.01
46	SLV 10	-4	995	3878	-42.45	-2.75	0.01
46	SLV 11	18	-217	755	8.8	12.18	-0.02
46	SLV 12	18	-217	755	8.8	12.18	-0.02
46	SLV 13	20	768	3743	-32.23	15.34	-0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
46	SLV 14	20	768	3743	-32.23	15.34	-0.02
46	SLV 15	26	405	2806	-16.86	19.82	-0.03
46	SLV 16	26	405	2806	-16.86	19.82	-0.03
47	SLU 1	0	-76	1111	8.85	-0.11	0
47	SLU 2	0	-76	1086	8.8	-0.15	0
47	SLU 3	0	-76	1111	8.85	-0.11	0
47	SLU 4	0	-76	1096	8.82	-0.14	0
47	SLU 5	0	-76	1086	8.8	-0.15	0
47	SLU 6	0	-76	1111	8.85	-0.11	0
47	SLU 7	0	-76	1096	8.82	-0.14	0
47	SLU 8	0	-76	1111	8.85	-0.11	0
47	SLU 9	0	-76	1096	8.82	-0.14	0
47	SLU 10	0	-109	1856	17.33	-0.25	0
47	SLU 11	0	-108	1881	17.38	-0.21	0
47	SLU 12	0	-109	1866	17.35	-0.24	0
47	SLU 13	0	-109	1856	17.33	-0.25	0
47	SLU 14	0	-108	1881	17.38	-0.21	0
47	SLU 15	0	-109	1866	17.35	-0.24	0
47	SLU 16	0	-108	1881	17.38	-0.21	0
47	SLU 17	0	-109	1866	17.35	-0.24	0
47	SLU 18	0	-122	2211	21.04	-0.25	0
47	SLU 19	0	-122	2196	21.01	-0.28	0
47	SLU 20	0	-122	2211	21.04	-0.25	0
47	SLU 21	0	-122	2196	21.01	-0.28	0
47	SLU 22	0	-90	1425	12.3	-0.15	0
47	SLU 23	0	-90	1400	12.25	-0.2	0
47	SLU 24	0	-90	1425	12.3	-0.15	0
47	SLU 25	0	-90	1410	12.27	-0.18	0
47	SLU 26	0	-90	1400	12.25	-0.2	0
47	SLU 27	0	-90	1425	12.3	-0.15	0
47	SLU 28	0	-90	1410	12.27	-0.18	0
47	SLU 29	0	-90	1425	12.3	-0.15	0
47	SLU 30	0	-90	1410	12.27	-0.18	0
47	SLU 31	0	-123	2170	20.78	-0.3	0
47	SLU 32	0	-122	2195	20.83	-0.25	0
47	SLU 33	0	-123	2180	20.8	-0.28	0
47	SLU 34	0	-123	2170	20.78	-0.3	0
47	SLU 35	0	-122	2195	20.83	-0.25	0
47	SLU 36	0	-123	2180	20.8	-0.28	0
47	SLU 37	0	-122	2195	20.83	-0.25	0
47	SLU 38	0	-123	2180	20.8	-0.28	0
47	SLU 39	0	-136	2525	24.49	-0.3	0
47	SLU 40	0	-136	2510	24.46	-0.32	0
47	SLU 41	0	-136	2525	24.49	-0.3	0
47	SLU 42	0	-136	2510	24.46	-0.32	0
47	SLU 43	0	-94	1336	10.32	-0.13	0
47	SLU 44	0	-94	1311	10.27	-0.17	0
47	SLU 45	0	-94	1336	10.32	-0.13	0
47	SLU 46	0	-94	1321	10.29	-0.15	0
47	SLU 47	0	-94	1311	10.27	-0.17	0
47	SLU 48	0	-94	1336	10.32	-0.13	0
47	SLU 49	0	-94	1321	10.29	-0.15	0
47	SLU 50	0	-94	1336	10.32	-0.13	0
47	SLU 51	0	-94	1321	10.29	-0.15	0
47	SLU 52	0	-127	2081	18.8	-0.27	0
47	SLU 53	0	-126	2107	18.85	-0.23	0
47	SLU 54	0	-127	2091	18.82	-0.26	0
47	SLU 55	0	-127	2081	18.8	-0.27	0
47	SLU 56	0	-126	2107	18.85	-0.23	0
47	SLU 57	0	-127	2091	18.82	-0.26	0
47	SLU 58	0	-126	2107	18.85	-0.23	0
47	SLU 59	0	-127	2091	18.82	-0.26	0
47	SLU 60	0	-140	2437	22.51	-0.27	0
47	SLU 61	0	-140	2422	22.48	-0.3	0
47	SLU 62	0	-140	2437	22.51	-0.27	0
47	SLU 63	0	-140	2422	22.48	-0.3	0
47	SLU 64	0	-108	1650	13.77	-0.17	0
47	SLU 65	0	-108	1625	13.72	-0.21	0
47	SLU 66	0	-108	1650	13.77	-0.17	0
47	SLU 67	0	-108	1635	13.74	-0.2	0
47	SLU 68	0	-108	1625	13.72	-0.21	0
47	SLU 69	0	-108	1650	13.77	-0.17	0
47	SLU 70	0	-108	1635	13.74	-0.2	0
47	SLU 71	0	-108	1650	13.77	-0.17	0
47	SLU 72	0	-108	1635	13.74	-0.2	0
47	SLU 73	0	-141	2395	22.25	-0.32	0
47	SLU 74	0	-140	2420	22.3	-0.27	0
47	SLU 75	0	-141	2405	22.27	-0.3	0
47	SLU 76	0	-141	2395	22.25	-0.32	0
47	SLU 77	0	-140	2420	22.3	-0.27	0
47	SLU 78	0	-141	2405	22.27	-0.3	0
47	SLU 79	0	-140	2420	22.3	-0.27	0
47	SLU 80	0	-141	2405	22.27	-0.3	0
47	SLU 81	0	-154	2750	25.96	-0.32	0
47	SLU 82	-1	-154	2735	25.93	-0.34	0
47	SLU 83	0	-154	2750	25.96	-0.32	0
47	SLU 84	-1	-154	2735	25.93	-0.34	0
47	SLE RA 1	0	-80	1200	9.83	-0.12	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
47	SLE RA 2	0	-80	1184	9.8	-0.15	0
47	SLE RA 3	0	-80	1200	9.83	-0.12	0
47	SLE RA 4	0	-80	1190	9.81	-0.14	0
47	SLE RA 5	0	-80	1184	9.8	-0.15	0
47	SLE RA 6	0	-80	1200	9.83	-0.12	0
47	SLE RA 7	0	-80	1190	9.81	-0.14	0
47	SLE RA 8	0	-80	1200	9.83	-0.12	0
47	SLE RA 9	0	-80	1190	9.81	-0.14	0
47	SLE RA 10	0	-102	1697	15.49	-0.22	0
47	SLE RA 11	0	-102	1714	15.52	-0.19	0
47	SLE RA 12	0	-102	1704	15.5	-0.21	0
47	SLE RA 13	0	-102	1697	15.49	-0.22	0
47	SLE RA 14	0	-102	1714	15.52	-0.19	0
47	SLE RA 15	0	-102	1704	15.5	-0.21	0
47	SLE RA 16	0	-102	1714	15.52	-0.19	0
47	SLE RA 17	0	-102	1704	15.5	-0.21	0
47	SLE RA 18	0	-111	1934	17.96	-0.22	0
47	SLE RA 19	0	-111	1924	17.94	-0.24	0
47	SLE RA 20	0	-111	1934	17.96	-0.22	0
47	SLE RA 21	0	-111	1924	17.94	-0.24	0
47	SLE FR 1	0	-80	1200	9.83	-0.12	0
47	SLE FR 2	0	-80	1197	9.83	-0.13	0
47	SLE FR 3	0	-80	1200	9.83	-0.12	0
47	SLE FR 4	0	-89	1417	12.27	-0.16	0
47	SLE FR 5	0	-89	1420	12.27	-0.15	0
47	SLE FR 6	0	-95	1567	13.9	-0.17	0
47	SLE QP 1	0	-80	1200	9.83	-0.12	0
47	SLE QP 2	0	-89	1420	12.27	-0.15	0
47	SLD 1	26	0	1534	6.14	14.9	-0.04
47	SLD 2	26	0	1534	6.14	14.9	-0.04
47	SLD 3	22	-82	1870	11.76	12.34	-0.03
47	SLD 4	22	-82	1870	11.76	12.34	-0.03
47	SLD 5	15	62	946	1.91	8.24	-0.02
47	SLD 6	15	62	946	1.91	8.24	-0.02
47	SLD 7	-1	-211	2064	20.64	-0.29	0
47	SLD 8	-1	-211	2064	20.64	-0.29	0
47	SLD 9	0	33	777	3.91	-0.02	0
47	SLD 10	0	33	777	3.91	-0.02	0
47	SLD 11	-15	-240	1895	22.63	-8.55	0.02
47	SLD 12	-15	-240	1895	22.63	-8.55	0.02
47	SLD 13	-22	-97	971	12.79	-12.64	0.03
47	SLD 14	-22	-97	971	12.79	-12.64	0.03
47	SLD 15	-27	-179	1307	18.4	-15.2	0.04
47	SLD 16	-27	-179	1307	18.4	-15.2	0.04
47	SLV 1	67	123	1685	-2.25	38.09	-0.09
47	SLV 2	67	123	1685	-2.25	38.09	-0.09
47	SLV 3	56	-72	2486	11.08	31.49	-0.08
47	SLV 4	56	-72	2486	11.08	31.49	-0.08
47	SLV 5	38	271	284	-12.31	21.32	-0.05
47	SLV 6	38	271	284	-12.31	21.32	-0.05
47	SLV 7	-1	-380	2956	32.15	-0.66	0
47	SLV 8	-1	-380	2956	32.15	-0.66	0
47	SLV 9	1	202	-115	-7.6	0.36	0
47	SLV 10	1	202	-115	-7.6	0.36	0
47	SLV 11	-38	-449	2557	36.86	-21.63	0.05
47	SLV 12	-38	-449	2557	36.86	-21.63	0.05
47	SLV 13	-56	-106	355	13.46	-31.79	0.08
47	SLV 14	-56	-106	355	13.46	-31.79	0.08
47	SLV 15	-68	-302	1156	26.8	-38.39	0.09
47	SLV 16	-68	-302	1156	26.8	-38.39	0.09
48	SLU 1	0	-195	643	-0.17	-0.05	-0.01
48	SLU 2	0	-191	629	-0.18	-0.08	-0.02
48	SLU 3	0	-195	643	-0.17	-0.05	-0.01
48	SLU 4	0	-193	634	-0.17	-0.07	-0.02
48	SLU 5	0	-191	629	-0.18	-0.08	-0.02
48	SLU 6	0	-195	643	-0.17	-0.05	-0.01
48	SLU 7	0	-193	634	-0.17	-0.07	-0.02
48	SLU 8	0	-195	643	-0.17	-0.05	-0.01
48	SLU 9	0	-193	634	-0.17	-0.07	-0.02
48	SLU 10	0	-312	1078	-2.82	-0.13	-0.03
48	SLU 11	0	-317	1092	-2.81	-0.1	-0.03
48	SLU 12	0	-314	1083	-2.82	-0.12	-0.03
48	SLU 13	0	-312	1078	-2.82	-0.13	-0.03
48	SLU 14	0	-317	1092	-2.81	-0.1	-0.03
48	SLU 15	0	-314	1083	-2.82	-0.12	-0.03
48	SLU 16	0	-317	1092	-2.81	-0.1	-0.03
48	SLU 17	0	-314	1083	-2.82	-0.12	-0.03
48	SLU 18	0	-369	1285	-3.94	-0.12	-0.03
48	SLU 19	0	-366	1276	-3.95	-0.14	-0.04
48	SLU 20	0	-369	1285	-3.94	-0.12	-0.03
48	SLU 21	0	-366	1276	-3.95	-0.14	-0.04
48	SLU 22	0	-245	826	-1.19	-0.07	-0.02
48	SLU 23	0	-241	812	-1.2	-0.1	-0.03
48	SLU 24	0	-245	826	-1.19	-0.07	-0.02
48	SLU 25	0	-243	817	-1.19	-0.09	-0.02
48	SLU 26	0	-241	812	-1.2	-0.1	-0.03
48	SLU 27	0	-245	826	-1.19	-0.07	-0.02
48	SLU 28	0	-243	817	-1.19	-0.09	-0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
48	SLU 29	0	-245	826	-1.19	-0.07	-0.02
48	SLU 30	0	-243	817	-1.19	-0.09	-0.02
48	SLU 31	0	-362	1261	-3.84	-0.15	-0.04
48	SLU 32	0	-366	1275	-3.83	-0.12	-0.03
48	SLU 33	0	-364	1266	-3.84	-0.14	-0.04
48	SLU 34	0	-362	1261	-3.84	-0.15	-0.04
48	SLU 35	0	-366	1275	-3.83	-0.12	-0.03
48	SLU 36	0	-364	1266	-3.84	-0.14	-0.04
48	SLU 37	0	-366	1275	-3.83	-0.12	-0.03
48	SLU 38	0	-364	1266	-3.84	-0.14	-0.04
48	SLU 39	0	-418	1468	-4.96	-0.14	-0.04
48	SLU 40	0	-416	1459	-4.97	-0.16	-0.04
48	SLU 41	0	-418	1468	-4.96	-0.14	-0.04
48	SLU 42	0	-416	1459	-4.97	-0.16	-0.04
48	SLU 43	0	-237	773	0.13	-0.06	-0.01
48	SLU 44	0	-233	759	0.12	-0.09	-0.02
48	SLU 45	0	-237	773	0.13	-0.06	-0.01
48	SLU 46	0	-234	765	0.13	-0.08	-0.02
48	SLU 47	0	-233	759	0.12	-0.09	-0.02
48	SLU 48	0	-237	773	0.13	-0.06	-0.01
48	SLU 49	0	-234	765	0.13	-0.08	-0.02
48	SLU 50	0	-237	773	0.13	-0.06	-0.01
48	SLU 51	0	-234	765	0.13	-0.08	-0.02
48	SLU 52	0	-354	1208	-2.52	-0.14	-0.04
48	SLU 53	0	-358	1222	-2.51	-0.11	-0.03
48	SLU 54	0	-356	1214	-2.52	-0.13	-0.03
48	SLU 55	0	-354	1208	-2.52	-0.14	-0.04
48	SLU 56	0	-358	1222	-2.51	-0.11	-0.03
48	SLU 57	0	-356	1214	-2.52	-0.13	-0.03
48	SLU 58	0	-358	1222	-2.51	-0.11	-0.03
48	SLU 59	0	-356	1214	-2.52	-0.13	-0.03
48	SLU 60	0	-410	1415	-3.64	-0.13	-0.03
48	SLU 61	0	-408	1406	-3.65	-0.15	-0.04
48	SLU 62	0	-410	1415	-3.64	-0.13	-0.03
48	SLU 63	0	-408	1406	-3.65	-0.15	-0.04
48	SLU 64	0	-287	956	-0.89	-0.08	-0.02
48	SLU 65	0	-282	942	-0.9	-0.11	-0.03
48	SLU 66	0	-287	956	-0.89	-0.08	-0.02
48	SLU 67	0	-284	948	-0.89	-0.1	-0.03
48	SLU 68	0	-282	942	-0.9	-0.11	-0.03
48	SLU 69	0	-287	956	-0.89	-0.08	-0.02
48	SLU 70	0	-284	948	-0.89	-0.1	-0.03
48	SLU 71	0	-287	956	-0.89	-0.08	-0.02
48	SLU 72	0	-284	948	-0.89	-0.1	-0.03
48	SLU 73	0	-404	1391	-3.54	-0.16	-0.04
48	SLU 74	0	-408	1405	-3.53	-0.13	-0.03
48	SLU 75	0	-405	1397	-3.54	-0.15	-0.04
48	SLU 76	0	-404	1391	-3.54	-0.16	-0.04
48	SLU 77	0	-408	1405	-3.53	-0.13	-0.03
48	SLU 78	0	-405	1397	-3.54	-0.15	-0.04
48	SLU 79	0	-408	1405	-3.53	-0.13	-0.03
48	SLU 80	0	-405	1397	-3.54	-0.15	-0.04
48	SLU 81	0	-460	1598	-4.66	-0.15	-0.04
48	SLU 82	0	-457	1589	-4.67	-0.17	-0.04
48	SLU 83	0	-460	1598	-4.66	-0.15	-0.04
48	SLU 84	0	-457	1589	-4.67	-0.17	-0.04
48	SLE RA 1	0	-209	696	-0.46	-0.06	-0.01
48	SLE RA 2	0	-207	686	-0.47	-0.08	-0.02
48	SLE RA 3	0	-209	696	-0.46	-0.06	-0.01
48	SLE RA 4	0	-208	690	-0.46	-0.07	-0.02
48	SLE RA 5	0	-207	686	-0.47	-0.08	-0.02
48	SLE RA 6	0	-209	696	-0.46	-0.06	-0.01
48	SLE RA 7	0	-208	690	-0.46	-0.07	-0.02
48	SLE RA 8	0	-209	696	-0.46	-0.06	-0.01
48	SLE RA 9	0	-208	690	-0.46	-0.07	-0.02
48	SLE RA 10	0	-288	985	-2.23	-0.11	-0.03
48	SLE RA 11	0	-290	995	-2.22	-0.09	-0.02
48	SLE RA 12	0	-289	989	-2.22	-0.1	-0.03
48	SLE RA 13	0	-288	985	-2.23	-0.11	-0.03
48	SLE RA 14	0	-290	995	-2.22	-0.09	-0.02
48	SLE RA 15	0	-289	989	-2.22	-0.1	-0.03
48	SLE RA 16	0	-290	995	-2.22	-0.09	-0.02
48	SLE RA 17	0	-289	989	-2.22	-0.1	-0.03
48	SLE RA 18	0	-325	1123	-2.98	-0.1	-0.03
48	SLE RA 19	0	-323	1117	-2.98	-0.12	-0.03
48	SLE RA 20	0	-325	1123	-2.98	-0.1	-0.03
48	SLE RA 21	0	-323	1117	-2.98	-0.12	-0.03
48	SLE FR 1	0	-209	696	-0.46	-0.06	-0.01
48	SLE FR 2	0	-209	694	-0.46	-0.06	-0.02
48	SLE FR 3	0	-209	696	-0.46	-0.06	-0.01
48	SLE FR 4	0	-244	822	-1.22	-0.07	-0.02
48	SLE FR 5	0	-244	824	-1.21	-0.07	-0.02
48	SLE FR 6	0	-267	909	-1.72	-0.08	-0.02
48	SLE QP 1	0	-209	696	-0.46	-0.06	-0.01
48	SLE QP 2	0	-244	824	-1.21	-0.07	-0.02
48	SLD 1	16	-265	892	-4.19	8.14	2.17
48	SLD 2	16	-265	892	-4.19	8.14	2.17
48	SLD 3	13	-373	1169	-1.48	6.72	1.79



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
48	SLD 4	13	-373	1169	-1.48	6.72	1.79
48	SLD 5	10	-86	424	-6.22	4.54	1.21
48	SLD 6	10	-86	424	-6.22	4.54	1.21
48	SLD 7	-1	-447	1347	2.82	-0.18	-0.05
48	SLD 8	-1	-447	1347	2.82	-0.18	-0.05
48	SLD 9	2	-41	300	-5.25	0.04	0.02
48	SLD 10	2	-41	300	-5.25	0.04	0.02
48	SLD 11	-10	-402	1223	3.79	-4.68	-1.25
48	SLD 12	-10	-402	1223	3.79	-4.68	-1.25
48	SLD 13	-13	-115	479	-0.94	-6.86	-1.82
48	SLD 14	-13	-115	479	-0.94	-6.86	-1.82
48	SLD 15	-16	-224	756	1.77	-8.28	-2.2
48	SLD 16	-16	-224	756	1.77	-8.28	-2.2
48	SLV 1	41	-292	982	-8.28	20.79	5.53
48	SLV 2	41	-292	982	-8.28	20.79	5.53
48	SLV 3	32	-549	1641	-1.83	17.13	4.56
48	SLV 4	32	-549	1641	-1.83	17.13	4.56
48	SLV 5	26	-133	-128	-13.11	11.73	3.13
48	SLV 6	26	133	-128	-13.11	11.73	3.13
48	SLV 7	-4	-727	2069	8.38	-0.46	-0.13
48	SLV 8	-4	-727	2069	8.38	-0.46	-0.13
48	SLV 9	4	238	-421	-10.81	0.31	0.09
48	SLV 10	4	238	-421	-10.81	0.31	0.09
48	SLV 11	-26	-621	1776	10.69	-11.87	-3.17
48	SLV 12	-26	-621	1776	10.69	-11.87	-3.17
48	SLV 13	-32	61	7	-0.59	-17.27	-4.59
48	SLV 14	-32	61	7	-0.59	-17.27	-4.59
48	SLV 15	-41	-197	666	5.85	-20.93	-5.57
48	SLV 16	-41	-197	666	5.85	-20.93	-5.57
49	SLU 1	0	106	1518	-5	0.15	0
49	SLU 2	-3	101	1498	-4.83	-2.82	0.02
49	SLU 3	0	106	1518	-5	0.15	0
49	SLU 4	-2	103	1506	-4.9	-1.63	0.01
49	SLU 5	-3	101	1498	-4.83	-2.82	0.02
49	SLU 6	0	106	1518	-5	0.15	0
49	SLU 7	-2	103	1506	-4.9	-1.63	0.01
49	SLU 8	0	106	1518	-5	0.15	0
49	SLU 9	-2	103	1506	-4.9	-1.63	0.01
49	SLU 10	-3	149	1751	-7	-2.72	0.02
49	SLU 11	-1	154	1770	-7.18	0.25	0
49	SLU 12	-2	151	1759	-7.07	-1.53	0.01
49	SLU 13	-3	149	1751	-7	-2.72	0.02
49	SLU 14	-1	154	1770	-7.18	0.25	0
49	SLU 15	-2	151	1759	-7.07	-1.53	0.01
49	SLU 16	-1	154	1770	-7.18	0.25	0
49	SLU 17	-2	151	1759	-7.07	-1.53	0.01
49	SLU 18	-1	174	1879	-8.11	0.29	0.01
49	SLU 19	-2	171	1867	-8	-1.49	0.01
49	SLU 20	-1	174	1879	-8.11	0.29	0.01
49	SLU 21	-2	171	1867	-8	-1.49	0.01
49	SLU 22	0	130	1638	-6.11	0.2	0
49	SLU 23	-3	126	1619	-5.93	-2.78	0.02
49	SLU 24	0	130	1638	-6.11	0.2	0
49	SLU 25	-2	127	1627	-6	-1.59	0.01
49	SLU 26	-3	126	1619	-5.93	-2.78	0.02
49	SLU 27	0	130	1638	-6.11	0.2	0
49	SLU 28	-2	127	1627	-6	-1.59	0.01
49	SLU 29	0	130	1638	-6.11	0.2	0
49	SLU 30	-2	127	1627	-6	-1.59	0.01
49	SLU 31	-3	173	1871	-8.1	-2.68	0.02
49	SLU 32	-1	178	1891	-8.28	0.3	0.01
49	SLU 33	-2	175	1879	-8.17	-1.49	0.01
49	SLU 34	-3	173	1871	-8.1	-2.68	0.02
49	SLU 35	-1	178	1891	-8.28	0.3	0.01
49	SLU 36	-2	175	1879	-8.17	-1.49	0.01
49	SLU 37	-1	178	1891	-8.28	0.3	0.01
49	SLU 38	-2	175	1879	-8.17	-1.49	0.01
49	SLU 39	-1	199	1999	-9.21	0.34	0.01
49	SLU 40	-3	196	1988	-9.11	-1.44	0.02
49	SLU 41	-1	199	1999	-9.21	0.34	0.01
49	SLU 42	-3	196	1988	-9.11	-1.44	0.02
49	SLU 43	0	129	1932	-6.13	0.18	0
49	SLU 44	-3	124	1912	-5.95	-2.79	0.02
49	SLU 45	0	129	1932	-6.13	0.18	0
49	SLU 46	-2	126	1920	-6.02	-1.6	0.01
49	SLU 47	-3	124	1912	-5.95	-2.79	0.02
49	SLU 48	0	129	1932	-6.13	0.18	0
49	SLU 49	-2	126	1920	-6.02	-1.6	0.01
49	SLU 50	0	129	1932	-6.13	0.18	0
49	SLU 51	-2	126	1920	-6.02	-1.6	0.01
49	SLU 52	-3	172	2165	-8.12	-2.69	0.02
49	SLU 53	-1	177	2184	-8.3	0.28	0
49	SLU 54	-2	174	2173	-8.2	-1.5	0.01
49	SLU 55	-3	172	2165	-8.12	-2.69	0.02
49	SLU 56	-1	177	2184	-8.3	0.28	0
49	SLU 57	-2	174	2173	-8.2	-1.5	0.01
49	SLU 58	-1	177	2184	-8.3	0.28	0
49	SLU 59	-2	174	2173	-8.2	-1.5	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
49	SLU 60	-1	197	2293	-9.23	0.33	0.01
49	SLU 61	-2	194	2281	-9.13	-1.46	0.01
49	SLU 62	-1	197	2293	-9.23	0.33	0.01
49	SLU 63	-2	194	2281	-9.13	-1.46	0.01
49	SLU 64	0	154	2052	-7.23	0.23	0
49	SLU 65	-3	149	2033	-7.05	-2.74	0.02
49	SLU 66	0	154	2052	-7.23	0.23	0
49	SLU 67	-2	151	2040	-7.12	-1.56	0.01
49	SLU 68	-3	149	2033	-7.05	-2.74	0.02
49	SLU 69	0	154	2052	-7.23	0.23	0
49	SLU 70	-2	151	2040	-7.12	-1.56	0.01
49	SLU 71	0	154	2052	-7.23	0.23	0
49	SLU 72	-2	151	2040	-7.12	-1.56	0.01
49	SLU 73	-3	197	2285	-9.23	-2.65	0.02
49	SLU 74	-1	201	2305	-9.41	0.33	0.01
49	SLU 75	-2	199	2293	-9.3	-1.46	0.01
49	SLU 76	-3	197	2285	-9.23	-2.65	0.02
49	SLU 77	-1	201	2305	-9.41	0.33	0.01
49	SLU 78	-2	199	2293	-9.3	-1.46	0.01
49	SLU 79	-1	201	2305	-9.41	0.33	0.01
49	SLU 80	-2	199	2293	-9.3	-1.46	0.01
49	SLU 81	-1	222	2413	-10.34	0.37	0.01
49	SLU 82	-3	219	2402	-10.23	-1.41	0.02
49	SLU 83	-1	222	2413	-10.34	0.37	0.01
49	SLU 84	-3	219	2402	-10.23	-1.41	0.02
49	SLE RA 1	0	113	1552	-5.32	0.16	0
49	SLE RA 2	-2	110	1539	-5.2	-1.82	0.01
49	SLE RA 3	0	113	1552	-5.32	0.16	0
49	SLE RA 4	-1	111	1544	-5.25	-1.02	0.01
49	SLE RA 5	-2	110	1539	-5.2	-1.82	0.01
49	SLE RA 6	0	113	1552	-5.32	0.16	0
49	SLE RA 7	-1	111	1544	-5.25	-1.02	0.01
49	SLE RA 8	0	113	1552	-5.32	0.16	0
49	SLE RA 9	-1	111	1544	-5.25	-1.02	0.01
49	SLE RA 10	-2	141	1708	-6.65	-1.75	0.01
49	SLE RA 11	-1	145	1721	-6.77	0.23	0
49	SLE RA 12	-2	143	1713	-6.7	-0.96	0.01
49	SLE RA 13	-2	141	1708	-6.65	-1.75	0.01
49	SLE RA 14	-1	145	1721	-6.77	0.23	0
49	SLE RA 15	-2	143	1713	-6.7	-0.96	0.01
49	SLE RA 16	-1	145	1721	-6.77	0.23	0
49	SLE RA 17	-2	143	1713	-6.7	-0.96	0.01
49	SLE RA 18	-1	158	1793	-7.39	0.26	0
49	SLE RA 19	-2	156	1785	-7.32	-0.93	0.01
49	SLE RA 20	-1	158	1793	-7.39	0.26	0
49	SLE RA 21	-2	156	1785	-7.32	-0.93	0.01
49	SLE FR 1	0	113	1552	-5.32	0.16	0
49	SLE FR 2	-1	112	1549	-5.3	-0.23	0
49	SLE FR 3	0	113	1552	-5.32	0.16	0
49	SLE FR 4	-1	126	1622	-5.92	-0.2	0
49	SLE FR 5	0	126	1624	-5.94	0.19	0
49	SLE FR 6	-1	136	1672	-6.35	0.21	0
49	SLE QP 1	0	113	1552	-5.32	0.16	0
49	SLE QP 2	0	126	1624	-5.94	0.19	0
49	SLD 1	7	149	1749	-6.96	5.02	-0.04
49	SLD 2	7	149	1749	-6.96	5.02	-0.04
49	SLD 3	12	40	1708	-2.08	9.59	-0.07
49	SLD 4	12	40	1708	-2.08	9.59	-0.07
49	SLD 5	-6	298	1725	-13.66	-5.28	0.04
49	SLD 6	-6	298	1725	-13.66	-5.28	0.04
49	SLD 7	11	-65	1586	2.63	9.94	-0.07
49	SLD 8	11	-65	1586	2.63	9.94	-0.07
49	SLD 9	-12	318	1663	-14.51	-9.55	0.08
49	SLD 10	-12	318	1663	-14.51	-9.55	0.08
49	SLD 11	6	-46	1523	1.77	5.67	-0.04
49	SLD 12	6	-46	1523	1.77	5.67	-0.04
49	SLD 13	-13	213	1541	-9.81	-9.2	0.08
49	SLD 14	-13	213	1541	-9.81	-9.2	0.08
49	SLD 15	-8	104	1499	-4.92	-4.64	0.05
49	SLD 16	-8	104	1499	-4.92	-4.64	0.05
49	SLV 1	16	180	1922	-8.35	11.36	-0.1
49	SLV 2	16	180	1922	-8.35	11.36	-0.1
49	SLV 3	30	-77	1821	3.18	23.14	-0.18
49	SLV 4	30	-77	1821	3.18	23.14	-0.18
49	SLV 5	-16	533	1867	-24.15	-14.33	0.1
49	SLV 6	-16	533	1867	-24.15	-14.33	0.1
49	SLV 7	29	-325	1530	14.28	24.95	-0.18
49	SLV 8	29	-325	1530	14.28	24.95	-0.18
49	SLV 9	-30	578	1719	-26.16	-24.56	0.19
49	SLV 10	-30	578	1719	-26.16	-24.56	0.19
49	SLV 11	15	-280	1382	12.27	14.71	-0.1
49	SLV 12	15	-280	1382	12.27	14.71	-0.1
49	SLV 13	-31	330	1428	-15.06	-22.76	0.19
49	SLV 14	-31	330	1428	-15.06	-22.76	0.19
49	SLV 15	-17	73	1327	-3.53	-10.97	0.1
49	SLV 16	-17	73	1327	-3.53	-10.97	0.1
50	SLU 1	-1	244	1942	-9.64	-0.89	0
50	SLU 2	0	253	1975	-10.03	-0.37	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
50	SLU 3	-1	244	1942	-9.64	-0.89	0
50	SLU 4	0	249	1962	-9.87	-0.58	0
50	SLU 5	0	253	1975	-10.03	-0.37	0
50	SLU 6	-1	244	1942	-9.64	-0.89	0
50	SLU 7	0	249	1962	-9.87	-0.58	0
50	SLU 8	-1	244	1942	-9.64	-0.89	0
50	SLU 9	0	249	1962	-9.87	-0.58	0
50	SLU 10	0	275	2038	-9.76	-1.16	0
50	SLU 11	-1	266	2005	-9.38	-1.68	0
50	SLU 12	-1	272	2025	-9.61	-1.37	0
50	SLU 13	0	275	2038	-9.76	-1.16	0
50	SLU 14	-1	266	2005	-9.38	-1.68	0
50	SLU 15	-1	272	2025	-9.61	-1.37	0
50	SLU 16	-1	266	2005	-9.38	-1.68	0
50	SLU 17	-1	272	2025	-9.61	-1.37	0
50	SLU 18	-2	276	2032	-9.27	-2.02	0
50	SLU 19	-1	282	2052	-9.5	-1.71	0
50	SLU 20	-2	276	2032	-9.27	-2.02	0
50	SLU 21	-1	282	2052	-9.5	-1.71	0
50	SLU 22	-1	263	1996	-9.96	-1.22	0
50	SLU 23	0	272	2030	-10.34	-0.7	0
50	SLU 24	-1	263	1996	-9.96	-1.22	0
50	SLU 25	0	268	2016	-10.19	-0.91	0
50	SLU 26	0	272	2030	-10.34	-0.7	0
50	SLU 27	-1	263	1996	-9.96	-1.22	0
50	SLU 28	0	268	2016	-10.19	-0.91	0
50	SLU 29	-1	263	1996	-9.96	-1.22	0
50	SLU 30	0	268	2016	-10.19	-0.91	0
50	SLU 31	-1	295	2092	-10.08	-1.5	0
50	SLU 32	-2	286	2059	-9.7	-2.02	0
50	SLU 33	-1	291	2079	-9.93	-1.71	0
50	SLU 34	-1	295	2092	-10.08	-1.5	0
50	SLU 35	-2	286	2059	-9.7	-2.02	0
50	SLU 36	-1	291	2079	-9.93	-1.71	0
50	SLU 37	-2	286	2059	-9.7	-2.02	0
50	SLU 38	-1	291	2079	-9.93	-1.71	0
50	SLU 39	-2	295	2086	-9.58	-2.36	0
50	SLU 40	-1	301	2106	-9.81	-2.05	0
50	SLU 41	-2	295	2086	-9.58	-2.36	0
50	SLU 42	-1	301	2106	-9.81	-2.05	0
50	SLU 43	-1	310	2506	-12.43	-1.04	0
50	SLU 44	0	319	2539	-12.81	-0.52	0
50	SLU 45	-1	310	2506	-12.43	-1.04	0
50	SLU 46	0	316	2526	-12.66	-0.73	0
50	SLU 47	0	319	2539	-12.81	-0.52	0
50	SLU 48	-1	310	2506	-12.43	-1.04	0
50	SLU 49	0	316	2526	-12.66	-0.73	0
50	SLU 50	-1	310	2506	-12.43	-1.04	0
50	SLU 51	0	316	2526	-12.66	-0.73	0
50	SLU 52	-1	342	2602	-12.55	-1.31	0
50	SLU 53	-1	333	2568	-12.17	-1.83	0
50	SLU 54	-1	338	2589	-12.4	-1.52	0
50	SLU 55	-1	342	2602	-12.55	-1.31	0
50	SLU 56	-1	333	2568	-12.17	-1.83	0
50	SLU 57	-1	338	2589	-12.4	-1.52	0
50	SLU 58	-1	333	2568	-12.17	-1.83	0
50	SLU 59	-1	338	2589	-12.4	-1.52	0
50	SLU 60	-2	342	2595	-12.05	-2.17	0
50	SLU 61	-1	348	2615	-12.28	-1.86	0
50	SLU 62	-2	342	2595	-12.05	-2.17	0
50	SLU 63	-1	348	2615	-12.28	-1.86	0
50	SLU 64	-1	329	2560	-12.74	-1.38	0
50	SLU 65	0	339	2593	-13.13	-0.86	0
50	SLU 66	-1	329	2560	-12.74	-1.38	0
50	SLU 67	0	335	2580	-12.97	-1.06	0
50	SLU 68	0	339	2593	-13.13	-0.86	0
50	SLU 69	-1	329	2560	-12.74	-1.38	0
50	SLU 70	0	335	2580	-12.97	-1.06	0
50	SLU 71	-1	329	2560	-12.74	-1.38	0
50	SLU 72	0	335	2580	-12.97	-1.06	0
50	SLU 73	-1	361	2656	-12.86	-1.65	0
50	SLU 74	-2	352	2623	-12.48	-2.17	0
50	SLU 75	-1	358	2643	-12.71	-1.86	0
50	SLU 76	-1	361	2656	-12.86	-1.65	0
50	SLU 77	-2	352	2623	-12.48	-2.17	0
50	SLU 78	-1	358	2643	-12.71	-1.86	0
50	SLU 79	-2	352	2623	-12.48	-2.17	0
50	SLU 80	-1	358	2643	-12.71	-1.86	0
50	SLU 81	-2	362	2650	-12.37	-2.51	0
50	SLU 82	-1	367	2670	-12.6	-2.2	0
50	SLU 83	-2	362	2650	-12.37	-2.51	0
50	SLU 84	-1	367	2670	-12.6	-2.2	0
50	SLE RA 1	-1	249	1957	-9.73	-0.98	0
50	SLE RA 2	0	255	1980	-9.99	-0.64	0
50	SLE RA 3	-1	249	1957	-9.73	-0.98	0
50	SLE RA 4	0	253	1971	-9.89	-0.78	0
50	SLE RA 5	0	255	1980	-9.99	-0.64	0
50	SLE RA 6	-1	249	1957	-9.73	-0.98	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
50	SLE RA 7	0	253	1971	-9.89	-0.78	0
50	SLE RA 8	-1	249	1957	-9.73	-0.98	0
50	SLE RA 9	0	253	1971	-9.89	-0.78	0
50	SLE RA 10	-1	270	2021	-9.81	-1.17	0
50	SLE RA 11	-1	264	1999	-9.56	-1.51	0
50	SLE RA 12	-1	268	2013	-9.71	-1.31	0
50	SLE RA 13	-1	270	2021	-9.81	-1.17	0
50	SLE RA 14	-1	264	1999	-9.56	-1.51	0
50	SLE RA 15	-1	268	2013	-9.71	-1.31	0
50	SLE RA 16	-1	264	1999	-9.56	-1.51	0
50	SLE RA 17	-1	268	2013	-9.71	-1.31	0
50	SLE RA 18	-1	271	2017	-9.48	-1.74	0
50	SLE RA 19	-1	274	2031	-9.64	-1.53	0
50	SLE RA 20	-1	271	2017	-9.48	-1.74	0
50	SLE RA 21	-1	274	2031	-9.64	-1.53	0
50	SLE FR 1	-1	249	1957	-9.73	-0.98	0
50	SLE FR 2	-1	250	1962	-9.79	-0.91	0
50	SLE FR 3	-1	249	1957	-9.73	-0.98	0
50	SLE FR 4	-1	257	1980	-9.71	-1.14	0
50	SLE FR 5	-1	256	1975	-9.66	-1.21	0
50	SLE FR 6	-1	260	1987	-9.61	-1.36	0
50	SLE QP 1	-1	249	1957	-9.73	-0.98	0
50	SLE QP 2	-1	256	1975	-9.66	-1.21	0
50	SLD 1	-20	224	1661	-8.62	-12.55	0.01
50	SLD 2	-20	224	1661	-8.62	-12.55	0.01
50	SLD 3	-16	69	1375	-1.97	-10.35	0.01
50	SLD 4	-16	69	1375	-1.97	-10.35	0.01
50	SLD 5	-12	481	2316	-19.43	-7.95	-0.01
50	SLD 6	-12	481	2316	-19.43	-7.95	-0.01
50	SLD 7	0	-35	1360	2.73	-0.61	0.01
50	SLD 8	0	-35	1360	2.73	-0.61	0.01
50	SLD 9	-2	546	2590	-22.04	-1.81	-0.01
50	SLD 10	-2	546	2590	-22.04	-1.81	-0.01
50	SLD 11	10	30	1634	0.11	5.53	0.01
50	SLD 12	10	30	1634	0.11	5.53	0.01
50	SLD 13	14	442	2576	-17.34	7.93	-0.01
50	SLD 14	14	442	2576	-17.34	7.93	-0.01
50	SLD 15	18	287	2289	-10.7	10.13	-0.01
50	SLD 16	18	287	2289	-10.7	10.13	-0.01
50	SLV 1	-48	181	1252	-7.22	-29.9	0.01
50	SLV 2	-48	181	1252	-7.22	-29.9	0.01
50	SLV 3	-40	-187	531	8.51	-24.62	0.03
50	SLV 4	-40	-187	531	8.51	-24.62	0.03
50	SLV 5	-28	790	2851	-32.8	-17.82	-0.01
50	SLV 6	-28	790	2851	-32.8	-17.82	-0.01
50	SLV 7	0	-434	449	19.66	-0.23	0.03
50	SLV 8	0	-434	449	19.66	-0.23	0.03
50	SLV 9	-2	945	3501	-38.98	-2.19	-0.03
50	SLV 10	-2	945	3501	-38.98	-2.19	-0.03
50	SLV 11	26	-279	1100	13.48	15.4	0.01
50	SLV 12	26	-279	1100	13.48	15.4	0.01
50	SLV 13	38	698	3419	-27.83	22.2	-0.03
50	SLV 14	38	698	3419	-27.83	22.2	-0.03
50	SLV 15	46	331	2699	-12.09	27.48	-0.01
50	SLV 16	46	331	2699	-12.09	27.48	-0.01
51	SLU 1	0	116	1484	-5.44	0.14	0
51	SLU 2	-3	109	1463	-5.13	-2.46	0.01
51	SLU 3	0	116	1484	-5.44	0.14	0
51	SLU 4	-2	112	1471	-5.26	-1.42	0.01
51	SLU 5	-3	109	1463	-5.13	-2.46	0.01
51	SLU 6	0	116	1484	-5.44	0.14	0
51	SLU 7	-2	112	1471	-5.26	-1.42	0.01
51	SLU 8	0	116	1484	-5.44	0.14	0
51	SLU 9	-2	112	1471	-5.26	-1.42	0.01
51	SLU 10	-3	167	1716	-7.74	-2.4	0.02
51	SLU 11	-1	174	1738	-8.05	0.2	0
51	SLU 12	-2	170	1725	-7.86	-1.36	0.01
51	SLU 13	-3	167	1716	-7.74	-2.4	0.02
51	SLU 14	-1	174	1738	-8.05	0.2	0
51	SLU 15	-2	170	1725	-7.86	-1.36	0.01
51	SLU 16	-1	174	1738	-8.05	0.2	0
51	SLU 17	-2	170	1725	-7.86	-1.36	0.01
51	SLU 18	-1	198	1846	-9.17	0.22	0
51	SLU 19	-2	194	1833	-8.98	-1.33	0.01
51	SLU 20	-1	198	1846	-9.17	0.22	0
51	SLU 21	-2	194	1833	-8.98	-1.33	0.01
51	SLU 22	0	146	1608	-6.79	0.17	0
51	SLU 23	-3	139	1586	-6.49	-2.43	0.02
51	SLU 24	0	146	1608	-6.79	0.17	0
51	SLU 25	-2	142	1595	-6.61	-1.39	0.01
51	SLU 26	-3	139	1586	-6.49	-2.43	0.02
51	SLU 27	0	146	1608	-6.79	0.17	0
51	SLU 28	-2	142	1595	-6.61	-1.39	0.01
51	SLU 29	0	146	1608	-6.79	0.17	0
51	SLU 30	-2	142	1595	-6.61	-1.39	0.01
51	SLU 31	-3	197	1840	-9.1	-2.36	0.02
51	SLU 32	-1	204	1861	-9.4	0.23	0
51	SLU 33	-2	200	1848	-9.22	-1.33	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
51	SLU 34	-3	197	1840	-9.1	-2.36	0.02
51	SLU 35	-1	204	1861	-9.4	0.23	0
51	SLU 36	-2	200	1848	-9.22	-1.33	0.01
51	SLU 37	-1	204	1861	-9.4	0.23	0
51	SLU 38	-2	200	1848	-9.22	-1.33	0.01
51	SLU 39	-1	229	1970	-10.52	0.26	0.01
51	SLU 40	-2	225	1957	-10.34	-1.3	0.01
51	SLU 41	-1	229	1970	-10.52	0.26	0.01
51	SLU 42	-2	225	1957	-10.34	-1.3	0.01
51	SLU 43	0	140	1887	-6.61	0.16	0
51	SLU 44	-3	133	1865	-6.3	-2.43	0.02
51	SLU 45	0	140	1887	-6.61	0.16	0
51	SLU 46	-2	136	1874	-6.42	-1.39	0.01
51	SLU 47	-3	133	1865	-6.3	-2.43	0.02
51	SLU 48	0	140	1887	-6.61	0.16	0
51	SLU 49	-2	136	1874	-6.42	-1.39	0.01
51	SLU 50	0	140	1887	-6.61	0.16	0
51	SLU 51	-2	136	1874	-6.42	-1.39	0.01
51	SLU 52	-3	191	2119	-8.91	-2.37	0.02
51	SLU 53	-1	198	2141	-9.22	0.23	0
51	SLU 54	-2	194	2128	-9.03	-1.33	0.01
51	SLU 55	-3	191	2119	-8.91	-2.37	0.02
51	SLU 56	-1	198	2141	-9.22	0.23	0
51	SLU 57	-2	194	2128	-9.03	-1.33	0.01
51	SLU 58	-1	198	2141	-9.22	0.23	0
51	SLU 59	-2	194	2128	-9.03	-1.33	0.01
51	SLU 60	-1	223	2249	-10.33	0.25	0
51	SLU 61	-2	219	2236	-10.15	-1.3	0.01
51	SLU 62	-1	223	2249	-10.33	0.25	0
51	SLU 63	-2	219	2236	-10.15	-1.3	0.01
51	SLU 64	0	170	2011	-7.96	0.2	0
51	SLU 65	-3	164	1989	-7.66	-2.4	0.02
51	SLU 66	0	170	2011	-7.96	0.2	0
51	SLU 67	-2	166	1998	-7.78	-1.36	0.01
51	SLU 68	-3	164	1989	-7.66	-2.4	0.02
51	SLU 69	0	170	2011	-7.96	0.2	0
51	SLU 70	-2	166	1998	-7.78	-1.36	0.01
51	SLU 71	0	170	2011	-7.96	0.2	0
51	SLU 72	-2	166	1998	-7.78	-1.36	0.01
51	SLU 73	-3	222	2242	-10.26	-2.33	0.02
51	SLU 74	-1	228	2264	-10.57	0.26	0
51	SLU 75	-2	224	2251	-10.39	-1.3	0.01
51	SLU 76	-3	222	2242	-10.26	-2.33	0.02
51	SLU 77	-1	228	2264	-10.57	0.26	0
51	SLU 78	-2	224	2251	-10.39	-1.3	0.01
51	SLU 79	-1	228	2264	-10.57	0.26	0
51	SLU 80	-2	224	2251	-10.39	-1.3	0.01
51	SLU 81	-1	253	2373	-11.69	0.28	0.01
51	SLU 82	-2	249	2360	-11.5	-1.27	0.01
51	SLU 83	-1	253	2373	-11.69	0.28	0.01
51	SLU 84	-2	249	2360	-11.5	-1.27	0.01
51	SLE RA 1	0	124	1520	-5.83	0.14	0
51	SLE RA 2	-2	120	1505	-5.62	-1.58	0.01
51	SLE RA 3	0	124	1520	-5.83	0.14	0
51	SLE RA 4	-1	122	1511	-5.7	-0.89	0.01
51	SLE RA 5	-2	120	1505	-5.62	-1.58	0.01
51	SLE RA 6	0	124	1520	-5.83	0.14	0
51	SLE RA 7	-1	122	1511	-5.7	-0.89	0.01
51	SLE RA 8	0	124	1520	-5.83	0.14	0
51	SLE RA 9	-1	122	1511	-5.7	-0.89	0.01
51	SLE RA 10	-2	159	1674	-7.36	-1.54	0.01
51	SLE RA 11	-1	163	1689	-7.57	0.19	0
51	SLE RA 12	-1	160	1680	-7.44	-0.85	0.01
51	SLE RA 13	-2	159	1674	-7.36	-1.54	0.01
51	SLE RA 14	-1	163	1689	-7.57	0.19	0
51	SLE RA 15	-1	160	1680	-7.44	-0.85	0.01
51	SLE RA 16	-1	163	1689	-7.57	0.19	0
51	SLE RA 17	-1	160	1680	-7.44	-0.85	0.01
51	SLE RA 18	-1	179	1761	-8.31	0.2	0
51	SLE RA 19	-2	177	1752	-8.19	-0.83	0.01
51	SLE RA 20	-1	179	1761	-8.31	0.2	0
51	SLE RA 21	-2	177	1752	-8.19	-0.83	0.01
51	SLE FR 1	0	124	1520	-5.83	0.14	0
51	SLE FR 2	-1	123	1517	-5.79	-0.2	0
51	SLE FR 3	0	124	1520	-5.83	0.14	0
51	SLE FR 4	-1	140	1589	-6.53	-0.18	0
51	SLE FR 5	0	141	1592	-6.57	0.16	0
51	SLE FR 6	0	152	1640	-7.07	0.17	0
51	SLE QP 1	0	124	1520	-5.83	0.14	0
51	SLE QP 2	0	141	1592	-6.57	0.16	0
51	SLD 1	5	163	1707	-7.57	4.22	-0.03
51	SLD 2	5	163	1707	-7.57	4.22	-0.03
51	SLD 3	9	48	1673	-2.36	7.75	-0.06
51	SLD 4	9	48	1673	-2.36	7.75	-0.06
51	SLD 5	-5	322	1679	-14.77	-3.97	0.04
51	SLD 6	-5	322	1679	-14.77	-3.97	0.04
51	SLD 7	9	-61	1564	2.59	7.79	-0.06
51	SLD 8	9	-61	1564	2.59	7.79	-0.06



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
51	SLD 9	-10	343	1620	-15.73	-7.46	0.06
51	SLD 10	-10	343	1620	-15.73	-7.46	0.06
51	SLD 11	5	-40	1505	1.62	4.29	-0.03
51	SLD 12	5	-40	1505	1.62	4.29	-0.03
51	SLD 13	-10	233	1512	-10.79	-7.42	0.06
51	SLD 14	-10	233	1512	-10.79	-7.42	0.06
51	SLD 15	-6	119	1477	-5.58	-3.9	0.03
51	SLD 16	-6	119	1477	-5.58	-3.9	0.03
51	SLV 1	12	194	1865	-8.93	9.74	-0.07
51	SLV 2	12	194	1865	-8.93	9.74	-0.07
51	SLV 3	23	-78	1783	3.36	18.75	-0.14
51	SLV 4	23	-78	1783	3.36	18.75	-0.14
51	SLV 5	-13	568	1799	-25.92	-10.63	0.09
51	SLV 6	-13	568	1799	-25.92	-10.63	0.09
51	SLV 7	23	-336	1524	15.05	19.41	-0.15
51	SLV 8	23	-336	1524	15.05	19.41	-0.15
51	SLV 9	-24	618	1660	-28.2	-19.08	0.15
51	SLV 10	-24	618	1660	-28.2	-19.08	0.15
51	SLV 11	12	-286	1385	12.78	10.96	-0.08
51	SLV 12	12	-286	1385	12.78	10.96	-0.08
51	SLV 13	-24	359	1401	-16.51	-18.43	0.15
51	SLV 14	-24	359	1401	-16.51	-18.43	0.15
51	SLV 15	-13	88	1319	-4.22	-9.42	0.08
51	SLV 16	-13	88	1319	-4.22	-9.42	0.08
52	SLU 1	-2	244	2031	-10.48	-1.44	0
52	SLU 2	-1	251	2066	-10.78	-0.89	0
52	SLU 3	-2	244	2031	-10.48	-1.44	0
52	SLU 4	-1	248	2052	-10.66	-1.11	0
52	SLU 5	-1	251	2066	-10.78	-0.89	0
52	SLU 6	-2	244	2031	-10.48	-1.44	0
52	SLU 7	-1	248	2052	-10.66	-1.11	0
52	SLU 8	-2	244	2031	-10.48	-1.44	0
52	SLU 9	-1	248	2052	-10.66	-1.11	0
52	SLU 10	-2	321	2206	-14.18	-2.26	0
52	SLU 11	-3	314	2170	-13.88	-2.81	0
52	SLU 12	-3	318	2191	-14.06	-2.48	0
52	SLU 13	-2	321	2206	-14.18	-2.26	0
52	SLU 14	-3	314	2170	-13.88	-2.81	0
52	SLU 15	-3	318	2191	-14.06	-2.48	0
52	SLU 16	-3	314	2170	-13.88	-2.81	0
52	SLU 17	-3	318	2191	-14.06	-2.48	0
52	SLU 18	-4	344	2230	-15.33	-3.39	0
52	SLU 19	-3	348	2251	-15.52	-3.06	0
52	SLU 20	-4	344	2230	-15.33	-3.39	0
52	SLU 21	-3	348	2251	-15.52	-3.06	0
52	SLU 22	-2	283	2121	-12.28	-2.02	0
52	SLU 23	-1	290	2157	-12.59	-1.47	0
52	SLU 24	-2	283	2121	-12.28	-2.02	0
52	SLU 25	-2	288	2143	-12.46	-1.69	0
52	SLU 26	-1	290	2157	-12.59	-1.47	0
52	SLU 27	-2	283	2121	-12.28	-2.02	0
52	SLU 28	-2	288	2143	-12.46	-1.69	0
52	SLU 29	-2	283	2121	-12.28	-2.02	0
52	SLU 30	-2	288	2143	-12.46	-1.69	0
52	SLU 31	-3	360	2296	-15.99	-2.83	0
52	SLU 32	-4	353	2261	-15.68	-3.38	0
52	SLU 33	-3	357	2282	-15.87	-3.05	0
52	SLU 34	-3	360	2296	-15.99	-2.83	0
52	SLU 35	-4	353	2261	-15.68	-3.38	0
52	SLU 36	-3	357	2282	-15.87	-3.05	0
52	SLU 37	-4	353	2261	-15.68	-3.38	0
52	SLU 38	-3	357	2282	-15.87	-3.05	0
52	SLU 39	-5	383	2320	-17.14	-3.97	0
52	SLU 40	-4	387	2342	-17.32	-3.64	0
52	SLU 41	-5	383	2320	-17.14	-3.97	0
52	SLU 42	-4	387	2342	-17.32	-3.64	0
52	SLU 43	-2	304	2609	-13	-1.68	0
52	SLU 44	-1	311	2644	-13.3	-1.13	0
52	SLU 45	-2	304	2609	-13	-1.68	0
52	SLU 46	-1	308	2630	-13.18	-1.35	0
52	SLU 47	-1	311	2644	-13.3	-1.13	0
52	SLU 48	-2	304	2609	-13	-1.68	0
52	SLU 49	-1	308	2630	-13.18	-1.35	0
52	SLU 50	-2	304	2609	-13	-1.68	0
52	SLU 51	-1	308	2630	-13.18	-1.35	0
52	SLU 52	-3	381	2784	-16.7	-2.49	0
52	SLU 53	-4	374	2748	-16.4	-3.04	0
52	SLU 54	-3	378	2769	-16.58	-2.71	0
52	SLU 55	-3	381	2784	-16.7	-2.49	0
52	SLU 56	-4	374	2748	-16.4	-3.04	0
52	SLU 57	-3	378	2769	-16.58	-2.71	0
52	SLU 58	-4	374	2748	-16.4	-3.04	0
52	SLU 59	-3	378	2769	-16.58	-2.71	0
52	SLU 60	-4	404	2808	-17.86	-3.62	0
52	SLU 61	-4	408	2829	-18.04	-3.29	0
52	SLU 62	-4	404	2808	-17.86	-3.62	0
52	SLU 63	-4	408	2829	-18.04	-3.29	0
52	SLU 64	-3	343	2699	-14.81	-2.26	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
52	SLU 65	-2	350	2735	-15.11	-1.71	0
52	SLU 66	-3	343	2699	-14.81	-2.26	0
52	SLU 67	-2	347	2721	-14.99	-1.93	0
52	SLU 68	-2	350	2735	-15.11	-1.71	0
52	SLU 69	-3	343	2699	-14.81	-2.26	0
52	SLU 70	-2	347	2721	-14.99	-1.93	0
52	SLU 71	-3	343	2699	-14.81	-2.26	0
52	SLU 72	-2	347	2721	-14.99	-1.93	0
52	SLU 73	-3	420	2874	-18.51	-3.07	0
52	SLU 74	-4	413	2839	-18.21	-3.62	0
52	SLU 75	-4	417	2860	-18.39	-3.29	0
52	SLU 76	-3	420	2874	-18.51	-3.07	0
52	SLU 77	-4	413	2839	-18.21	-3.62	0
52	SLU 78	-4	417	2860	-18.39	-3.29	0
52	SLU 79	-4	413	2839	-18.21	-3.62	0
52	SLU 80	-4	417	2860	-18.39	-3.29	0
52	SLU 81	-5	443	2899	-19.66	-4.2	0
52	SLU 82	-4	447	2920	-19.85	-3.87	0
52	SLU 83	-5	443	2899	-19.66	-4.2	0
52	SLU 84	-4	447	2920	-19.85	-3.87	0
52	SLE RA 1	-2	255	2057	-10.99	-1.61	0
52	SLE RA 2	-1	260	2080	-11.19	-1.24	0
52	SLE RA 3	-2	255	2057	-10.99	-1.61	0
52	SLE RA 4	-1	258	2071	-11.11	-1.39	0
52	SLE RA 5	-1	260	2080	-11.19	-1.24	0
52	SLE RA 6	-2	255	2057	-10.99	-1.61	0
52	SLE RA 7	-1	258	2071	-11.11	-1.39	0
52	SLE RA 8	-2	255	2057	-10.99	-1.61	0
52	SLE RA 9	-1	258	2071	-11.11	-1.39	0
52	SLE RA 10	-2	307	2173	-13.46	-2.15	0
52	SLE RA 11	-3	302	2149	-13.26	-2.52	0
52	SLE RA 12	-3	305	2164	-13.38	-2.3	0
52	SLE RA 13	-2	307	2173	-13.46	-2.15	0
52	SLE RA 14	-3	302	2149	-13.26	-2.52	0
52	SLE RA 15	-3	305	2164	-13.38	-2.3	0
52	SLE RA 16	-3	302	2149	-13.26	-2.52	0
52	SLE RA 17	-3	305	2164	-13.38	-2.3	0
52	SLE RA 18	-4	322	2189	-14.23	-2.91	0
52	SLE RA 19	-3	325	2203	-14.35	-2.69	0
52	SLE RA 20	-4	322	2189	-14.23	-2.91	0
52	SLE RA 21	-3	325	2203	-14.35	-2.69	0
52	SLE FR 1	-2	255	2057	-10.99	-1.61	0
52	SLE FR 2	-2	256	2061	-11.03	-1.54	0
52	SLE FR 3	-2	255	2057	-10.99	-1.61	0
52	SLE FR 4	-2	276	2101	-12	-1.93	0
52	SLE FR 5	-2	275	2096	-11.96	-2	0
52	SLE FR 6	-3	289	2123	-12.61	-2.26	0
52	SLE QP 1	-2	255	2057	-10.99	-1.61	0
52	SLE QP 2	-2	275	2096	-11.96	-2	0
52	SLD 1	-22	257	1829	-11.42	-11.78	0.01
52	SLD 2	-22	257	1829	-11.42	-11.78	0.01
52	SLD 3	-26	101	1603	-4.56	-13.8	0.01
52	SLD 4	-26	101	1603	-4.56	-13.8	0.01
52	SLD 5	-3	506	2359	-22.2	-1.87	0
52	SLD 6	-3	506	2359	-22.2	-1.87	0
52	SLD 7	-15	-14	1606	0.66	-8.61	0.01
52	SLD 8	-15	-14	1606	0.66	-8.61	0.01
52	SLD 9	10	564	2587	-24.58	4.61	-0.01
52	SLD 10	10	564	2587	-24.58	4.61	-0.01
52	SLD 11	-2	44	1834	-1.73	-2.13	0
52	SLD 12	-2	44	1834	-1.73	-2.13	0
52	SLD 13	21	450	2590	-19.37	9.8	-0.02
52	SLD 14	21	450	2590	-19.37	9.8	-0.02
52	SLD 15	17	294	2364	-12.51	7.78	-0.01
52	SLD 16	17	294	2364	-12.51	7.78	-0.01
52	SLV 1	-53	232	1481	-10.68	-27.21	0.03
52	SLV 2	-53	232	1481	-10.68	-27.21	0.03
52	SLV 3	-62	-138	917	5.54	-32.11	0.03
52	SLV 4	-62	-138	917	5.54	-32.11	0.03
52	SLV 5	-4	823	2767	-36.18	-2.12	-0.01
52	SLV 6	-4	823	2767	-36.18	-2.12	-0.01
52	SLV 7	-34	-409	887	17.89	-18.47	0.02
52	SLV 8	-34	-409	887	17.89	-18.47	0.02
52	SLV 9	29	959	3305	-41.82	14.47	-0.03
52	SLV 10	29	959	3305	-41.82	14.47	-0.03
52	SLV 11	-1	-272	1426	12.25	-1.88	0
52	SLV 12	-1	-272	1426	12.25	-1.88	0
52	SLV 13	58	688	3275	-29.47	28.11	-0.04
52	SLV 14	58	688	3275	-29.47	28.11	-0.04
52	SLV 15	49	319	2712	-13.25	23.21	-0.03
52	SLV 16	49	319	2712	-13.25	23.21	-0.03
53	SLU 1	0	136	1485	-5.97	0.21	0
53	SLU 2	-2	129	1459	-5.69	-1.75	0.01
53	SLU 3	0	136	1485	-5.97	0.21	0
53	SLU 4	-1	132	1470	-5.8	-0.97	0.01
53	SLU 5	-2	129	1459	-5.69	-1.75	0.01
53	SLU 6	0	136	1485	-5.97	0.21	0
53	SLU 7	-1	132	1470	-5.8	-0.97	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
53	SLU 8	0	136	1485	-5.97	0.21	0
53	SLU 9	-1	132	1470	-5.8	-0.97	0.01
53	SLU 10	-2	196	1726	-8.57	-1.7	0.01
53	SLU 11	0	203	1753	-8.85	0.27	0
53	SLU 12	-1	199	1737	-8.68	-0.91	0.01
53	SLU 13	-2	196	1726	-8.57	-1.7	0.01
53	SLU 14	0	203	1753	-8.85	0.27	0
53	SLU 15	-1	199	1737	-8.68	-0.91	0.01
53	SLU 16	0	203	1753	-8.85	0.27	0
53	SLU 17	-1	199	1737	-8.68	-0.91	0.01
53	SLU 18	0	232	1867	-10.08	0.29	0
53	SLU 19	-1	228	1851	-9.92	-0.89	0.01
53	SLU 20	0	232	1867	-10.08	0.29	0
53	SLU 21	-1	228	1851	-9.92	-0.89	0.01
53	SLU 22	0	172	1619	-7.48	0.25	0
53	SLU 23	-2	164	1593	-7.2	-1.72	0.01
53	SLU 24	0	172	1619	-7.48	0.25	0
53	SLU 25	-1	167	1603	-7.31	-0.93	0.01
53	SLU 26	-2	164	1593	-7.2	-1.72	0.01
53	SLU 27	0	172	1619	-7.48	0.25	0
53	SLU 28	-1	167	1603	-7.31	-0.93	0.01
53	SLU 29	0	172	1619	-7.48	0.25	0
53	SLU 30	-1	167	1603	-7.31	-0.93	0.01
53	SLU 31	-2	231	1860	-10.08	-1.66	0.01
53	SLU 32	0	239	1886	-10.36	0.3	0
53	SLU 33	-1	234	1871	-10.19	-0.88	0.01
53	SLU 34	-2	231	1860	-10.08	-1.66	0.01
53	SLU 35	0	239	1886	-10.36	0.3	0
53	SLU 36	-1	234	1871	-10.19	-0.88	0.01
53	SLU 37	0	239	1886	-10.36	0.3	0
53	SLU 38	-1	234	1871	-10.19	-0.88	0.01
53	SLU 39	0	268	2001	-11.59	0.33	0
53	SLU 40	-1	263	1985	-11.43	-0.85	0.01
53	SLU 41	0	268	2001	-11.59	0.33	0
53	SLU 42	-1	263	1985	-11.43	-0.85	0.01
53	SLU 43	0	165	1885	-7.24	0.26	0
53	SLU 44	-2	157	1859	-6.96	-1.7	0.01
53	SLU 45	0	165	1885	-7.24	0.26	0
53	SLU 46	-1	160	1870	-7.07	-0.92	0.01
53	SLU 47	-2	157	1859	-6.96	-1.7	0.01
53	SLU 48	0	165	1885	-7.24	0.26	0
53	SLU 49	-1	160	1870	-7.07	-0.92	0.01
53	SLU 50	0	165	1885	-7.24	0.26	0
53	SLU 51	-1	160	1870	-7.07	-0.92	0.01
53	SLU 52	-2	224	2126	-9.84	-1.65	0.01
53	SLU 53	0	232	2152	-10.12	0.32	0
53	SLU 54	-1	227	2137	-9.95	-0.86	0.01
53	SLU 55	-2	224	2126	-9.84	-1.65	0.01
53	SLU 56	0	232	2152	-10.12	0.32	0
53	SLU 57	-1	227	2137	-9.95	-0.86	0.01
53	SLU 58	0	232	2152	-10.12	0.32	0
53	SLU 59	-1	227	2137	-9.95	-0.86	0.01
53	SLU 60	0	261	2267	-11.35	0.34	0
53	SLU 61	-1	256	2251	-11.19	-0.84	0.01
53	SLU 62	0	261	2267	-11.35	0.34	0
53	SLU 63	-1	256	2251	-11.19	-0.84	0.01
53	SLU 64	0	200	2019	-8.75	0.3	0
53	SLU 65	-2	193	1993	-8.47	-1.67	0.01
53	SLU 66	0	200	2019	-8.75	0.3	0
53	SLU 67	-1	196	2003	-8.58	-0.88	0.01
53	SLU 68	-2	193	1993	-8.47	-1.67	0.01
53	SLU 69	0	200	2019	-8.75	0.3	0
53	SLU 70	-1	196	2003	-8.58	-0.88	0.01
53	SLU 71	0	200	2019	-8.75	0.3	0
53	SLU 72	-1	196	2003	-8.58	-0.88	0.01
53	SLU 73	-2	260	2260	-11.35	-1.61	0.01
53	SLU 74	0	268	2286	-11.63	0.35	0
53	SLU 75	-1	263	2270	-11.46	-0.82	0.01
53	SLU 76	-2	260	2260	-11.35	-1.61	0.01
53	SLU 77	0	268	2286	-11.63	0.35	0
53	SLU 78	-1	263	2270	-11.46	-0.82	0.01
53	SLU 79	0	268	2286	-11.63	0.35	0
53	SLU 80	-1	263	2270	-11.46	-0.82	0.01
53	SLU 81	0	296	2401	-12.86	0.38	0
53	SLU 82	-1	292	2385	-12.7	-0.8	0.01
53	SLU 83	0	296	2401	-12.86	0.38	0
53	SLU 84	-1	292	2385	-12.7	-0.8	0.01
53	SLE RA 1	0	146	1524	-6.4	0.22	0
53	SLE RA 2	-1	141	1506	-6.21	-1.09	0.01
53	SLE RA 3	0	146	1524	-6.4	0.22	0
53	SLE RA 4	-1	143	1513	-6.29	-0.56	0
53	SLE RA 5	-1	141	1506	-6.21	-1.09	0.01
53	SLE RA 6	0	146	1524	-6.4	0.22	0
53	SLE RA 7	-1	143	1513	-6.29	-0.56	0
53	SLE RA 8	0	146	1524	-6.4	0.22	0
53	SLE RA 9	-1	143	1513	-6.29	-0.56	0
53	SLE RA 10	-1	186	1684	-8.13	-1.05	0.01
53	SLE RA 11	0	191	1702	-8.32	0.26	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
53	SLE RA 12	-1	188	1691	-8.21	-0.53	0
53	SLE RA 13	-1	186	1684	-8.13	-1.05	0.01
53	SLE RA 14	0	191	1702	-8.32	0.26	0
53	SLE RA 15	-1	188	1691	-8.21	-0.53	0
53	SLE RA 16	0	191	1702	-8.32	0.26	0
53	SLE RA 17	-1	188	1691	-8.21	-0.53	0
53	SLE RA 18	0	210	1778	-9.14	0.27	0
53	SLE RA 19	-1	207	1768	-9.03	-0.51	0.01
53	SLE RA 20	0	210	1778	-9.14	0.27	0
53	SLE RA 21	-1	207	1768	-9.03	-0.51	0.01
53	SLE FR 1	0	146	1524	-6.4	0.22	0
53	SLE FR 2	0	145	1520	-6.36	-0.04	0
53	SLE FR 3	0	146	1524	-6.4	0.22	0
53	SLE FR 4	0	165	1596	-7.18	-0.03	0
53	SLE FR 5	0	166	1600	-7.22	0.24	0
53	SLE FR 6	0	178	1651	-7.77	0.25	0
53	SLE QP 1	0	146	1524	-6.4	0.22	0
53	SLE QP 2	0	166	1600	-7.22	0.24	0
53	SLD 1	8	263	1724	-11.49	3.07	-0.04
53	SLD 2	8	263	1724	-11.49	3.07	-0.04
53	SLD 3	3	146	1691	-6.28	5.58	-0.02
53	SLD 4	3	146	1691	-6.28	5.58	-0.02
53	SLD 5	9	373	1688	-16.41	-2.72	-0.05
53	SLD 6	9	373	1688	-16.41	-2.72	-0.05
53	SLD 7	-6	-18	1577	0.97	5.64	0.03
53	SLD 8	-6	-18	1577	0.97	5.64	0.03
53	SLD 9	6	349	1623	-15.41	-5.17	-0.03
53	SLD 10	6	349	1623	-15.41	-5.17	-0.03
53	SLD 11	-9	-42	1512	1.96	3.19	0.05
53	SLD 12	-9	-42	1512	1.96	3.19	0.05
53	SLD 13	-4	185	1509	-8.16	-5.1	0.02
53	SLD 14	-4	185	1509	-8.16	-5.1	0.02
53	SLD 15	-8	68	1476	-2.95	-2.6	0.04
53	SLD 16	-8	68	1476	-2.95	-2.6	0.04
53	SLV 1	20	396	1895	-17.29	7.12	-0.11
53	SLV 2	20	396	1895	-17.29	7.12	-0.11
53	SLV 3	9	119	1816	-4.99	13.47	-0.05
53	SLV 4	9	119	1816	-4.99	13.47	-0.05
53	SLV 5	23	655	1808	-28.91	-7.33	-0.12
53	SLV 6	23	655	1808	-28.91	-7.33	-0.12
53	SLV 7	-14	-269	1545	12.11	13.84	0.08
53	SLV 8	-14	-269	1545	12.11	13.84	0.08
53	SLV 9	14	600	1655	-26.56	-13.36	-0.07
53	SLV 10	14	600	1655	-26.56	-13.36	-0.07
53	SLV 11	-23	-324	1392	14.47	7.8	0.13
53	SLV 12	-23	-324	1392	14.47	7.8	0.13
53	SLV 13	-9	212	1384	-9.46	-13	0.05
53	SLV 14	-9	212	1384	-9.46	-13	0.05
53	SLV 15	-20	-65	1305	2.85	-6.65	0.11
53	SLV 16	-20	-65	1305	2.85	-6.65	0.11
54	SLU 1	0	125	1036	2.5	-0.02	0
54	SLU 2	-1	131	1034	1.93	-0.17	0.04
54	SLU 3	0	125	1036	2.5	-0.02	0
54	SLU 4	0	128	1035	2.16	-0.11	0.02
54	SLU 5	-1	131	1034	1.93	-0.17	0.04
54	SLU 6	0	125	1036	2.5	-0.02	0
54	SLU 7	0	128	1035	2.16	-0.11	0.02
54	SLU 8	0	125	1036	2.5	-0.02	0
54	SLU 9	0	128	1035	2.16	-0.11	0.02
54	SLU 10	-1	224	1705	-0.46	-0.16	0.03
54	SLU 11	0	218	1707	0.1	0	0
54	SLU 12	0	221	1706	-0.24	-0.09	0.02
54	SLU 13	-1	224	1705	-0.46	-0.16	0.03
54	SLU 14	0	218	1707	0.1	0	0
54	SLU 15	0	221	1706	-0.24	-0.09	0.02
54	SLU 16	0	218	1707	0.1	0	0
54	SLU 17	0	221	1706	-0.24	-0.09	0.02
54	SLU 18	0	258	1995	-0.92	0	-0.01
54	SLU 19	0	261	1994	-1.26	-0.09	0.02
54	SLU 20	0	258	1995	-0.92	0	-0.01
54	SLU 21	0	261	1994	-1.26	-0.09	0.02
54	SLU 22	0	167	1331	1.57	-0.02	0
54	SLU 23	-1	172	1329	1.01	-0.17	0.04
54	SLU 24	0	167	1331	1.57	-0.02	0
54	SLU 25	0	170	1329	1.23	-0.11	0.02
54	SLU 26	-1	172	1329	1.01	-0.17	0.04
54	SLU 27	0	167	1331	1.57	-0.02	0
54	SLU 28	0	170	1329	1.23	-0.11	0.02
54	SLU 29	0	167	1331	1.57	-0.02	0
54	SLU 30	0	170	1329	1.23	-0.11	0.02
54	SLU 31	0	265	1999	-1.38	-0.15	0.03
54	SLU 32	0	259	2002	-0.82	0	-0.01
54	SLU 33	0	263	2000	-1.16	-0.09	0.02
54	SLU 34	0	265	1999	-1.38	-0.15	0.03
54	SLU 35	0	259	2002	-0.82	0	-0.01
54	SLU 36	0	263	2000	-1.16	-0.09	0.02
54	SLU 37	0	259	2002	-0.82	0	-0.01
54	SLU 38	0	263	2000	-1.16	-0.09	0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
54	SLU 39	0	299	2289	-1.84	0.01	-0.01
54	SLU 40	0	303	2288	-2.18	-0.08	0.01
54	SLU 41	0	299	2289	-1.84	0.01	-0.01
54	SLU 42	0	303	2288	-2.18	-0.08	0.01
54	SLU 43	0	148	1247	3.56	-0.03	0
54	SLU 44	-1	154	1245	2.99	-0.18	0.04
54	SLU 45	0	148	1247	3.56	-0.03	0
54	SLU 46	0	152	1245	3.22	-0.12	0.02
54	SLU 47	-1	154	1245	2.99	-0.18	0.04
54	SLU 48	0	148	1247	3.56	-0.03	0
54	SLU 49	0	152	1245	3.22	-0.12	0.02
54	SLU 50	0	148	1247	3.56	-0.03	0
54	SLU 51	0	152	1245	3.22	-0.12	0.02
54	SLU 52	-1	247	1915	0.6	-0.16	0.03
54	SLU 53	0	241	1918	1.17	-0.01	0
54	SLU 54	0	245	1916	0.83	-0.1	0.02
54	SLU 55	-1	247	1915	0.6	-0.16	0.03
54	SLU 56	0	241	1918	1.17	-0.01	0
54	SLU 57	0	245	1916	0.83	-0.1	0.02
54	SLU 58	0	241	1918	1.17	-0.01	0
54	SLU 59	0	245	1916	0.83	-0.1	0.02
54	SLU 60	0	281	2205	0.14	0	-0.01
54	SLU 61	0	284	2204	-0.2	-0.09	0.02
54	SLU 62	0	281	2205	0.14	0	-0.01
54	SLU 63	0	284	2204	-0.2	-0.09	0.02
54	SLU 64	0	190	1541	2.64	-0.02	0
54	SLU 65	-1	196	1539	2.07	-0.18	0.04
54	SLU 66	0	190	1541	2.64	-0.02	0
54	SLU 67	0	193	1539	2.3	-0.12	0.02
54	SLU 68	-1	196	1539	2.07	-0.18	0.04
54	SLU 69	0	190	1541	2.64	-0.02	0
54	SLU 70	0	193	1539	2.3	-0.12	0.02
54	SLU 71	0	190	1541	2.64	-0.02	0
54	SLU 72	0	193	1539	2.3	-0.12	0.02
54	SLU 73	0	288	2210	-0.32	-0.16	0.03
54	SLU 74	0	283	2212	0.25	-0.01	0
54	SLU 75	0	286	2210	-0.09	-0.1	0.02
54	SLU 76	0	288	2210	-0.32	-0.16	0.03
54	SLU 77	0	283	2212	0.25	-0.01	0
54	SLU 78	0	286	2210	-0.09	-0.1	0.02
54	SLU 79	0	283	2212	0.25	-0.01	0
54	SLU 80	0	286	2210	-0.09	-0.1	0.02
54	SLU 81	0	322	2499	-0.78	0	-0.01
54	SLU 82	0	326	2498	-1.12	-0.09	0.01
54	SLU 83	0	322	2499	-0.78	0	-0.01
54	SLU 84	0	326	2498	-1.12	-0.09	0.01
54	SLE RA 1	0	137	1121	2.23	-0.02	0
54	SLE RA 2	0	141	1119	1.85	-0.12	0.03
54	SLE RA 3	0	137	1121	2.23	-0.02	0
54	SLE RA 4	0	139	1120	2.01	-0.08	0.02
54	SLE RA 5	0	141	1119	1.85	-0.12	0.03
54	SLE RA 6	0	137	1121	2.23	-0.02	0
54	SLE RA 7	0	139	1120	2.01	-0.08	0.02
54	SLE RA 8	0	137	1121	2.23	-0.02	0
54	SLE RA 9	0	139	1120	2.01	-0.08	0.02
54	SLE RA 10	0	203	1566	0.26	-0.11	0.02
54	SLE RA 11	0	199	1568	0.64	-0.01	0
54	SLE RA 12	0	201	1567	0.41	-0.07	0.01
54	SLE RA 13	0	203	1566	0.26	-0.11	0.02
54	SLE RA 14	0	199	1568	0.64	-0.01	0
54	SLE RA 15	0	201	1567	0.41	-0.07	0.01
54	SLE RA 16	0	199	1568	0.64	-0.01	0
54	SLE RA 17	0	201	1567	0.41	-0.07	0.01
54	SLE RA 18	0	225	1760	-0.05	0	0
54	SLE RA 19	0	228	1759	-0.27	-0.06	0.01
54	SLE RA 20	0	225	1760	-0.05	0	0
54	SLE RA 21	0	228	1759	-0.27	-0.06	0.01
54	SLE FR 1	0	137	1121	2.23	-0.02	0
54	SLE FR 2	0	138	1120	2.16	-0.04	0.01
54	SLE FR 3	0	137	1121	2.23	-0.02	0
54	SLE FR 4	0	164	1312	1.47	-0.03	0
54	SLE FR 5	0	163	1312	1.55	-0.01	0
54	SLE FR 6	0	181	1440	1.09	-0.01	0
54	SLE QP 1	0	137	1121	2.23	-0.02	0
54	SLE QP 2	0	163	1312	1.55	-0.01	0
54	SLD 1	19	136	1495	4.9	3.42	-0.86
54	SLD 2	19	136	1495	4.9	3.42	-0.86
54	SLD 3	14	96	1334	7.65	2.61	-0.66
54	SLD 4	14	96	1334	7.65	2.61	-0.66
54	SLD 5	12	215	1612	-1.6	2.24	-0.57
54	SLD 6	12	215	1612	-1.6	2.24	-0.57
54	SLD 7	-2	83	1074	7.54	-0.45	0.11
54	SLD 8	-2	83	1074	7.54	-0.45	0.11
54	SLD 9	3	244	1551	-4.44	0.42	-0.11
54	SLD 10	3	244	1551	-4.44	0.42	-0.11
54	SLD 11	-12	111	1012	4.7	-2.27	0.56
54	SLD 12	-12	111	1012	4.7	-2.27	0.56
54	SLD 13	-14	231	1291	-4.55	-2.64	0.66



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
54	SLD 14	-14	231	1291	-4.55	-2.64	0.66
54	SLD 15	-18	191	1129	-1.8	-3.45	0.86
54	SLD 16	-18	191	1129	-1.8	-3.45	0.86
54	SLV 1	48	98	1745	9.42	8.9	-2.23
54	SLV 2	48	98	1745	9.42	8.9	-2.23
54	SLV 3	37	4	1364	15.93	6.9	-1.73
54	SLV 4	37	4	1364	15.93	6.9	-1.73
54	SLV 5	31	287	2020	-5.95	5.71	-1.43
54	SLV 6	31	287	2020	-5.95	5.71	-1.43
54	SLV 7	-5	-27	750	15.72	-0.99	0.24
54	SLV 8	-5	-27	750	15.72	-0.99	0.24
54	SLV 9	6	354	1875	-12.62	0.96	-0.24
54	SLV 10	6	354	1875	-12.62	0.96	-0.24
54	SLV 11	-31	40	604	9.05	-5.74	1.43
54	SLV 12	-31	40	604	9.05	-5.74	1.43
54	SLV 13	-37	323	1260	-12.83	-6.92	1.73
54	SLV 14	-37	323	1260	-12.83	-6.92	1.73
54	SLV 15	-48	229	879	-6.33	-8.93	2.23
54	SLV 16	-48	229	879	-6.33	-8.93	2.23
55	SLU 1	-4	242	2228	-8.83	-2.2	0.01
55	SLU 2	-3	246	2264	-9.04	-1.84	0.01
55	SLU 3	-4	242	2228	-8.83	-2.2	0.01
55	SLU 4	-4	244	2250	-8.96	-1.98	0.01
55	SLU 5	-3	246	2264	-9.04	-1.84	0.01
55	SLU 6	-4	242	2228	-8.83	-2.2	0.01
55	SLU 7	-4	244	2250	-8.96	-1.98	0.01
55	SLU 8	-4	242	2228	-8.83	-2.2	0.01
55	SLU 9	-4	244	2250	-8.96	-1.98	0.01
55	SLU 10	-7	337	2580	-10.85	-3.84	0.01
55	SLU 11	-8	332	2543	-10.65	-4.2	0.01
55	SLU 12	-7	335	2565	-10.77	-3.98	0.01
55	SLU 13	-7	337	2580	-10.85	-3.84	0.01
55	SLU 14	-8	332	2543	-10.65	-4.2	0.01
55	SLU 15	-7	335	2565	-10.77	-3.98	0.01
55	SLU 16	-8	332	2543	-10.65	-4.2	0.01
55	SLU 17	-7	335	2565	-10.77	-3.98	0.01
55	SLU 18	-9	371	2678	-11.42	-5.06	0.01
55	SLU 19	-8	374	2700	-11.55	-4.84	0.01
55	SLU 20	-9	371	2678	-11.42	-5.06	0.01
55	SLU 21	-8	374	2700	-11.55	-4.84	0.01
55	SLU 22	-6	290	2399	-10.06	-3.06	0.01
55	SLU 23	-5	295	2435	-10.27	-2.69	0.01
55	SLU 24	-6	290	2399	-10.06	-3.06	0.01
55	SLU 25	-5	293	2420	-10.18	-2.84	0.01
55	SLU 26	-5	295	2435	-10.27	-2.69	0.01
55	SLU 27	-6	290	2399	-10.06	-3.06	0.01
55	SLU 28	-5	293	2420	-10.18	-2.84	0.01
55	SLU 29	-6	290	2399	-10.06	-3.06	0.01
55	SLU 30	-5	293	2420	-10.18	-2.84	0.01
55	SLU 31	-8	386	2750	-12.08	-4.69	0.01
55	SLU 32	-9	381	2714	-11.87	-5.06	0.01
55	SLU 33	-8	384	2736	-12	-4.84	0.01
55	SLU 34	-8	386	2750	-12.08	-4.69	0.01
55	SLU 35	-9	381	2714	-11.87	-5.06	0.01
55	SLU 36	-8	384	2736	-12	-4.84	0.01
55	SLU 37	-9	381	2714	-11.87	-5.06	0.01
55	SLU 38	-8	384	2736	-12	-4.84	0.01
55	SLU 39	-10	420	2849	-12.65	-5.92	0.01
55	SLU 40	-10	423	2871	-12.77	-5.7	0.01
55	SLU 41	-10	420	2849	-12.65	-5.92	0.01
55	SLU 42	-10	423	2871	-12.77	-5.7	0.01
55	SLU 43	-5	297	2838	-11.07	-2.57	0.01
55	SLU 44	-4	302	2874	-11.27	-2.2	0.01
55	SLU 45	-5	297	2838	-11.07	-2.57	0.01
55	SLU 46	-4	300	2860	-11.19	-2.35	0.01
55	SLU 47	-4	302	2874	-11.27	-2.2	0.01
55	SLU 48	-5	297	2838	-11.07	-2.57	0.01
55	SLU 49	-4	300	2860	-11.19	-2.35	0.01
55	SLU 50	-5	297	2838	-11.07	-2.57	0.01
55	SLU 51	-4	300	2860	-11.19	-2.35	0.01
55	SLU 52	-7	393	3190	-13.09	-4.2	0.01
55	SLU 53	-8	388	3153	-12.88	-4.57	0.01
55	SLU 54	-8	391	3175	-13	-4.35	0.01
55	SLU 55	-7	393	3190	-13.09	-4.2	0.01
55	SLU 56	-8	388	3153	-12.88	-4.57	0.01
55	SLU 57	-8	391	3175	-13	-4.35	0.01
55	SLU 58	-8	388	3153	-12.88	-4.57	0.01
55	SLU 59	-8	391	3175	-13	-4.35	0.01
55	SLU 60	-10	427	3288	-13.66	-5.43	0.01
55	SLU 61	-9	430	3310	-13.78	-5.21	0.01
55	SLU 62	-10	427	3288	-13.66	-5.43	0.01
55	SLU 63	-9	430	3310	-13.78	-5.21	0.01
55	SLU 64	-6	346	3008	-12.29	-3.43	0.01
55	SLU 65	-5	351	3045	-12.5	-3.06	0.01
55	SLU 66	-6	346	3008	-12.29	-3.43	0.01
55	SLU 67	-6	349	3030	-12.41	-3.21	0.01
55	SLU 68	-5	351	3045	-12.5	-3.06	0.01
55	SLU 69	-6	346	3008	-12.29	-3.43	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
55	SLU 70	-6	349	3030	-12.41	-3.21	0.01
55	SLU 71	-6	346	3008	-12.29	-3.43	0.01
55	SLU 72	-6	349	3030	-12.41	-3.21	0.01
55	SLU 73	-9	441	3360	-14.31	-5.06	0.01
55	SLU 74	-10	437	3324	-14.1	-5.43	0.01
55	SLU 75	-9	440	3346	-14.23	-5.21	0.01
55	SLU 76	-9	441	3360	-14.31	-5.06	0.01
55	SLU 77	-10	437	3324	-14.1	-5.43	0.01
55	SLU 78	-9	440	3346	-14.23	-5.21	0.01
55	SLU 79	-10	437	3324	-14.1	-5.43	0.01
55	SLU 80	-9	440	3346	-14.23	-5.21	0.01
55	SLU 81	-11	476	3459	-14.88	-6.28	0.01
55	SLU 82	-11	478	3481	-15	-6.06	0.01
55	SLU 83	-11	476	3459	-14.88	-6.28	0.01
55	SLU 84	-11	478	3481	-15	-6.06	0.01
55	SLE RA 1	-5	256	2277	-9.18	-2.45	0.01
55	SLE RA 2	-4	259	2301	-9.32	-2.2	0.01
55	SLE RA 3	-5	256	2277	-9.18	-2.45	0.01
55	SLE RA 4	-4	257	2291	-9.27	-2.3	0.01
55	SLE RA 5	-4	259	2301	-9.32	-2.2	0.01
55	SLE RA 6	-5	256	2277	-9.18	-2.45	0.01
55	SLE RA 7	-4	257	2291	-9.27	-2.3	0.01
55	SLE RA 8	-5	256	2277	-9.18	-2.45	0.01
55	SLE RA 9	-4	257	2291	-9.27	-2.3	0.01
55	SLE RA 10	-6	319	2511	-10.53	-3.54	0.01
55	SLE RA 11	-7	316	2487	-10.39	-3.78	0.01
55	SLE RA 12	-6	318	2501	-10.48	-3.63	0.01
55	SLE RA 13	-6	319	2511	-10.53	-3.54	0.01
55	SLE RA 14	-7	316	2487	-10.39	-3.78	0.01
55	SLE RA 15	-6	318	2501	-10.48	-3.63	0.01
55	SLE RA 16	-7	316	2487	-10.39	-3.78	0.01
55	SLE RA 17	-6	318	2501	-10.48	-3.63	0.01
55	SLE RA 18	-8	342	2577	-10.91	-4.35	0.01
55	SLE RA 19	-7	344	2592	-10.99	-4.21	0.01
55	SLE RA 20	-8	342	2577	-10.91	-4.35	0.01
55	SLE RA 21	-7	344	2592	-10.99	-4.21	0.01
55	SLE FR 1	-5	256	2277	-9.18	-2.45	0.01
55	SLE FR 2	-4	256	2282	-9.21	-2.4	0.01
55	SLE FR 3	-5	256	2277	-9.18	-2.45	0.01
55	SLE FR 4	-5	282	2372	-9.73	-2.97	0.01
55	SLE FR 5	-6	281	2367	-9.7	-3.02	0.01
55	SLE FR 6	-6	299	2427	-10.05	-3.4	0.01
55	SLE QP 1	-5	256	2277	-9.18	-2.45	0.01
55	SLE QP 2	-6	281	2367	-9.7	-3.02	0.01
55	SLD 1	-23	277	2123	-9.71	-9.79	-0.01
55	SLD 2	-23	277	2123	-9.71	-9.79	-0.01
55	SLD 3	-25	120	1938	-2.72	-11.06	-0.02
55	SLD 4	-25	120	1938	-2.72	-11.06	-0.02
55	SLD 5	-6	518	2574	-20.31	-3.14	0.01
55	SLD 6	-6	518	2574	-20.31	-3.14	0.01
55	SLD 7	-16	-5	1958	3	-7.34	-0.01
55	SLD 8	-16	-5	1958	3	-7.34	-0.01
55	SLD 9	5	568	2776	-22.41	1.31	0.02
55	SLD 10	5	568	2776	-22.41	1.31	0.02
55	SLD 11	-5	45	2159	0.91	-2.9	0.01
55	SLD 12	-5	45	2159	0.91	-2.9	0.01
55	SLD 13	14	443	2795	-16.69	5.02	0.03
55	SLD 14	14	443	2795	-16.69	5.02	0.03
55	SLD 15	12	286	2610	-9.69	3.76	0.03
55	SLD 16	12	286	2610	-9.69	3.76	0.03
55	SLV 1	-50	273	1804	-9.78	-20.52	-0.04
55	SLV 2	-50	273	1804	-9.78	-20.52	-0.04
55	SLV 3	-57	-98	1351	6.75	-23.61	-0.05
55	SLV 4	-57	-98	1351	6.75	-23.61	-0.05
55	SLV 5	-8	842	2886	-34.79	-3.58	0.01
55	SLV 6	-8	842	2886	-34.79	-3.58	0.01
55	SLV 7	-32	-395	1374	20.3	-13.89	-0.03
55	SLV 8	-32	-395	1374	20.3	-13.89	-0.03
55	SLV 9	21	958	3360	-39.7	7.85	0.04
55	SLV 10	21	958	3360	-39.7	7.85	0.04
55	SLV 11	-3	-279	1847	15.39	-2.46	0.01
55	SLV 12	-3	-279	1847	15.39	-2.46	0.01
55	SLV 13	46	661	3383	-26.15	17.58	0.07
55	SLV 14	46	661	3383	-26.15	17.58	0.07
55	SLV 15	39	290	2929	-9.63	14.48	0.06
55	SLV 16	39	290	2929	-9.63	14.48	0.06
56	SLU 1	2	161	1531	-6.84	0.45	-0.01
56	SLU 2	0	151	1497	-6.44	-0.68	-0.01
56	SLU 3	2	161	1531	-6.84	0.45	-0.01
56	SLU 4	1	155	1511	-6.6	-0.23	-0.01
56	SLU 5	0	151	1497	-6.44	-0.68	-0.01
56	SLU 6	2	161	1531	-6.84	0.45	-0.01
56	SLU 7	1	155	1511	-6.6	-0.23	-0.01
56	SLU 8	2	161	1531	-6.84	0.45	-0.01
56	SLU 9	1	155	1511	-6.6	-0.23	-0.01
56	SLU 10	0	224	1787	-9.6	-0.63	-0.01
56	SLU 11	2	234	1821	-10.01	0.5	-0.01
56	SLU 12	1	228	1801	-9.76	-0.18	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
56	SLU 13	0	224	1787	-9.6	-0.63	-0.01
56	SLU 14	2	234	1821	-10.01	0.5	-0.01
56	SLU 15	1	228	1801	-9.76	-0.18	-0.01
56	SLU 16	2	234	1821	-10.01	0.5	-0.01
56	SLU 17	1	228	1801	-9.76	-0.18	-0.01
56	SLU 18	2	265	1945	-11.36	0.52	-0.01
56	SLU 19	1	259	1925	-11.12	-0.16	-0.01
56	SLU 20	2	265	1945	-11.36	0.52	-0.01
56	SLU 21	1	259	1925	-11.12	-0.16	-0.01
56	SLU 22	2	200	1681	-8.53	0.5	-0.01
56	SLU 23	0	191	1647	-8.12	-0.63	-0.01
56	SLU 24	2	200	1681	-8.53	0.5	-0.01
56	SLU 25	1	195	1661	-8.28	-0.18	-0.01
56	SLU 26	0	191	1647	-8.12	-0.63	-0.01
56	SLU 27	2	200	1681	-8.53	0.5	-0.01
56	SLU 28	1	195	1661	-8.28	-0.18	-0.01
56	SLU 29	2	200	1681	-8.53	0.5	-0.01
56	SLU 30	1	195	1661	-8.28	-0.18	-0.01
56	SLU 31	0	264	1937	-11.29	-0.58	-0.01
56	SLU 32	2	273	1971	-11.69	0.55	-0.01
56	SLU 33	1	268	1951	-11.45	-0.13	-0.01
56	SLU 34	0	264	1937	-11.29	-0.58	-0.01
56	SLU 35	2	273	1971	-11.69	0.55	-0.01
56	SLU 36	1	268	1951	-11.45	-0.13	-0.01
56	SLU 37	2	273	1971	-11.69	0.55	-0.01
56	SLU 38	1	268	1951	-11.45	-0.13	-0.01
56	SLU 39	2	305	2095	-13.05	0.57	-0.01
56	SLU 40	1	299	2075	-12.8	-0.11	-0.01
56	SLU 41	2	305	2095	-13.05	0.57	-0.01
56	SLU 42	1	299	2075	-12.8	-0.11	-0.01
56	SLU 43	2	195	1939	-8.32	0.56	-0.01
56	SLU 44	0	186	1905	-7.91	-0.56	-0.01
56	SLU 45	2	195	1939	-8.32	0.56	-0.01
56	SLU 46	1	190	1918	-8.07	-0.11	-0.01
56	SLU 47	0	186	1905	-7.91	-0.56	-0.01
56	SLU 48	2	195	1939	-8.32	0.56	-0.01
56	SLU 49	1	190	1918	-8.07	-0.11	-0.01
56	SLU 50	2	195	1939	-8.32	0.56	-0.01
56	SLU 51	1	190	1918	-8.07	-0.11	-0.01
56	SLU 52	1	259	2195	-11.08	-0.51	-0.01
56	SLU 53	2	269	2229	-11.48	0.61	-0.01
56	SLU 54	1	263	2208	-11.24	-0.06	-0.01
56	SLU 55	1	259	2195	-11.08	-0.51	-0.01
56	SLU 56	2	269	2229	-11.48	0.61	-0.01
56	SLU 57	1	263	2208	-11.24	-0.06	-0.01
56	SLU 58	2	269	2229	-11.48	0.61	-0.01
56	SLU 59	1	263	2208	-11.24	-0.06	-0.01
56	SLU 60	2	300	2353	-12.84	0.63	-0.01
56	SLU 61	1	294	2333	-12.59	-0.04	-0.01
56	SLU 62	2	300	2353	-12.84	0.63	-0.01
56	SLU 63	1	294	2333	-12.59	-0.04	-0.01
56	SLU 64	2	235	2089	-10	0.62	-0.01
56	SLU 65	1	225	2055	-9.6	-0.51	-0.01
56	SLU 66	2	235	2089	-10	0.62	-0.01
56	SLU 67	1	229	2068	-9.76	-0.06	-0.01
56	SLU 68	1	225	2055	-9.6	-0.51	-0.01
56	SLU 69	2	235	2089	-10	0.62	-0.01
56	SLU 70	1	229	2068	-9.76	-0.06	-0.01
56	SLU 71	2	235	2089	-10	0.62	-0.01
56	SLU 72	1	229	2068	-9.76	-0.06	-0.01
56	SLU 73	1	299	2345	-12.76	-0.46	-0.01
56	SLU 74	2	308	2379	-13.17	0.66	-0.01
56	SLU 75	1	302	2358	-12.92	-0.01	-0.01
56	SLU 76	1	299	2345	-12.76	-0.46	-0.01
56	SLU 77	2	308	2379	-13.17	0.66	-0.01
56	SLU 78	1	302	2358	-12.92	-0.01	-0.01
56	SLU 79	2	308	2379	-13.17	0.66	-0.01
56	SLU 80	1	302	2358	-12.92	-0.01	-0.01
56	SLU 81	2	339	2503	-14.52	0.69	-0.01
56	SLU 82	1	334	2483	-14.28	0.01	-0.01
56	SLU 83	2	339	2503	-14.52	0.69	-0.01
56	SLU 84	1	334	2483	-14.28	0.01	-0.01
56	SLE RA 1	2	172	1574	-7.32	0.46	-0.01
56	SLE RA 2	1	166	1551	-7.05	-0.29	-0.01
56	SLE RA 3	2	172	1574	-7.32	0.46	-0.01
56	SLE RA 4	1	168	1560	-7.16	0.01	-0.01
56	SLE RA 5	1	166	1551	-7.05	-0.29	-0.01
56	SLE RA 6	2	172	1574	-7.32	0.46	-0.01
56	SLE RA 7	1	168	1560	-7.16	0.01	-0.01
56	SLE RA 8	2	172	1574	-7.32	0.46	-0.01
56	SLE RA 9	1	168	1560	-7.16	0.01	-0.01
56	SLE RA 10	1	214	1744	-9.16	-0.26	-0.01
56	SLE RA 11	2	221	1767	-9.43	0.49	-0.01
56	SLE RA 12	1	217	1754	-9.27	0.04	-0.01
56	SLE RA 13	1	214	1744	-9.16	-0.26	-0.01
56	SLE RA 14	2	221	1767	-9.43	0.49	-0.01
56	SLE RA 15	1	217	1754	-9.27	0.04	-0.01
56	SLE RA 16	2	221	1767	-9.43	0.49	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
56	SLE RA 17	1	217	1754	-9.27	0.04	-0.01
56	SLE RA 18	2	242	1850	-10.34	0.51	-0.01
56	SLE RA 19	1	238	1836	-10.17	0.06	-0.01
56	SLE RA 20	2	242	1850	-10.34	0.51	-0.01
56	SLE RA 21	1	238	1836	-10.17	0.06	-0.01
56	SLE FR 1	2	172	1574	-7.32	0.46	-0.01
56	SLE FR 2	1	171	1569	-7.27	0.31	-0.01
56	SLE FR 3	2	172	1574	-7.32	0.46	-0.01
56	SLE FR 4	1	192	1652	-8.17	0.33	-0.01
56	SLE FR 5	2	193	1657	-8.23	0.48	-0.01
56	SLE FR 6	2	207	1712	-8.83	0.49	-0.01
56	SLE QP 1	2	172	1574	-7.32	0.46	-0.01
56	SLE QP 2	2	193	1657	-8.23	0.48	-0.01
56	SLD 1	8	298	1823	-12.85	2.05	-0.03
56	SLD 2	8	298	1823	-12.85	2.05	-0.03
56	SLD 3	5	179	1785	-7.46	3.45	-0.02
56	SLD 4	5	179	1785	-7.46	3.45	-0.02
56	SLD 5	9	405	1764	-17.79	-1.17	-0.03
56	SLD 6	9	405	1764	-17.79	-1.17	-0.03
56	SLD 7	-3	8	1638	0.18	3.49	0
56	SLD 8	-3	8	1638	0.18	3.49	0
56	SLD 9	6	377	1675	-16.64	-2.54	-0.02
56	SLD 10	6	377	1675	-16.64	-2.54	-0.02
56	SLD 11	-6	-19	1549	1.34	2.12	0.01
56	SLD 12	-6	-19	1549	1.34	2.12	0.01
56	SLD 13	-1	207	1528	-8.99	-2.5	0
56	SLD 14	-1	207	1528	-8.99	-2.5	0
56	SLD 15	-5	88	1490	-3.6	-1.1	0.01
56	SLD 16	-5	88	1490	-3.6	-1.1	0.01
56	SLV 1	19	440	2051	-19.15	4.4	-0.07
56	SLV 2	19	440	2051	-19.15	4.4	-0.07
56	SLV 3	10	159	1962	-6.41	7.93	-0.04
56	SLV 4	10	159	1962	-6.41	7.93	-0.04
56	SLV 5	20	693	1910	-30.81	-3.69	-0.07
56	SLV 6	20	693	1910	-30.81	-3.69	-0.07
56	SLV 7	-9	-243	1613	11.63	8.06	0.02
56	SLV 8	-9	-243	1613	11.63	8.06	0.02
56	SLV 9	12	629	1701	-28.08	-7.1	-0.04
56	SLV 10	12	629	1701	-28.08	-7.1	-0.04
56	SLV 11	-17	-307	1403	14.36	4.64	0.05
56	SLV 12	-17	-307	1403	14.36	4.64	0.05
56	SLV 13	-7	227	1352	-10.04	-6.98	0.02
56	SLV 14	-7	227	1352	-10.04	-6.98	0.02
56	SLV 15	-15	-54	1262	2.69	-3.45	0.05
56	SLV 16	-15	-54	1262	2.69	-3.45	0.05
57	SLU 1	145	171	2220	-7.26	3.58	0.01
57	SLU 2	138	164	2161	-6.95	3.58	0.01
57	SLU 3	145	171	2220	-7.26	3.58	0.01
57	SLU 4	141	167	2184	-7.07	3.58	0.01
57	SLU 5	138	164	2161	-6.95	3.58	0.01
57	SLU 6	145	171	2220	-7.26	3.58	0.01
57	SLU 7	141	167	2184	-7.07	3.58	0.01
57	SLU 8	145	171	2220	-7.26	3.58	0.01
57	SLU 9	141	167	2184	-7.07	3.58	0.01
57	SLU 10	147	244	2594	-10.26	3.15	0.01
57	SLU 11	155	251	2653	-10.56	3.16	0.01
57	SLU 12	150	247	2618	-10.38	3.16	0.01
57	SLU 13	147	244	2594	-10.26	3.15	0.01
57	SLU 14	155	251	2653	-10.56	3.16	0.01
57	SLU 15	150	247	2618	-10.38	3.16	0.01
57	SLU 16	155	251	2653	-10.56	3.16	0.01
57	SLU 17	150	247	2618	-10.38	3.16	0.01
57	SLU 18	159	285	2839	-11.98	2.98	0.02
57	SLU 19	154	281	2803	-11.8	2.97	0.01
57	SLU 20	159	285	2839	-11.98	2.98	0.02
57	SLU 21	154	281	2803	-11.8	2.97	0.01
57	SLU 22	158	212	2455	-8.95	3.75	0.01
57	SLU 23	151	205	2396	-8.65	3.74	0.01
57	SLU 24	158	212	2455	-8.95	3.75	0.01
57	SLU 25	154	208	2419	-8.77	3.75	0.01
57	SLU 26	151	205	2396	-8.65	3.74	0.01
57	SLU 27	158	212	2455	-8.95	3.75	0.01
57	SLU 28	154	208	2419	-8.77	3.75	0.01
57	SLU 29	158	212	2455	-8.95	3.75	0.01
57	SLU 30	154	208	2419	-8.77	3.75	0.01
57	SLU 31	160	285	2829	-11.96	3.32	0.01
57	SLU 32	168	292	2888	-12.26	3.33	0.02
57	SLU 33	163	288	2852	-12.08	3.32	0.01
57	SLU 34	160	285	2829	-11.96	3.32	0.01
57	SLU 35	168	292	2888	-12.26	3.33	0.02
57	SLU 36	163	288	2852	-12.08	3.32	0.01
57	SLU 37	168	292	2888	-12.26	3.33	0.02
57	SLU 38	163	288	2852	-12.08	3.32	0.01
57	SLU 39	172	326	3074	-13.68	3.15	0.02
57	SLU 40	167	322	3038	-13.5	3.14	0.02
57	SLU 41	172	326	3074	-13.68	3.15	0.02
57	SLU 42	167	322	3038	-13.5	3.14	0.02
57	SLU 43	184	208	2806	-8.85	4.6	0.01





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
57	SLU 44	177	202	2746	-8.55	4.59	0.01
57	SLU 45	184	208	2806	-8.85	4.6	0.01
57	SLU 46	180	204	2770	-8.67	4.6	0.01
57	SLU 47	177	202	2746	-8.55	4.59	0.01
57	SLU 48	184	208	2806	-8.85	4.6	0.01
57	SLU 49	180	204	2770	-8.67	4.6	0.01
57	SLU 50	184	208	2806	-8.85	4.6	0.01
57	SLU 51	180	204	2770	-8.67	4.6	0.01
57	SLU 52	187	281	3179	-11.86	4.17	0.01
57	SLU 53	194	288	3239	-12.16	4.18	0.02
57	SLU 54	190	284	3203	-11.98	4.17	0.01
57	SLU 55	187	281	3179	-11.86	4.17	0.01
57	SLU 56	194	288	3239	-12.16	4.18	0.02
57	SLU 57	190	284	3203	-11.98	4.17	0.01
57	SLU 58	194	288	3239	-12.16	4.18	0.02
57	SLU 59	190	284	3203	-11.98	4.17	0.01
57	SLU 60	198	322	3424	-13.58	4	0.02
57	SLU 61	194	318	3389	-13.4	3.99	0.02
57	SLU 62	198	322	3424	-13.58	4	0.02
57	SLU 63	194	318	3389	-13.4	3.99	0.02
57	SLU 64	197	249	3041	-10.55	4.77	0.01
57	SLU 65	190	243	2981	-10.25	4.76	0.01
57	SLU 66	197	249	3041	-10.55	4.77	0.01
57	SLU 67	193	245	3005	-10.37	4.76	0.01
57	SLU 68	190	243	2981	-10.25	4.76	0.01
57	SLU 69	197	249	3041	-10.55	4.77	0.01
57	SLU 70	193	245	3005	-10.37	4.76	0.01
57	SLU 71	197	249	3041	-10.55	4.77	0.01
57	SLU 72	193	245	3005	-10.37	4.76	0.01
57	SLU 73	199	322	3414	-13.56	4.34	0.02
57	SLU 74	207	329	3474	-13.86	4.35	0.02
57	SLU 75	202	325	3438	-13.68	4.34	0.02
57	SLU 76	199	322	3414	-13.56	4.34	0.02
57	SLU 77	207	329	3474	-13.86	4.35	0.02
57	SLU 78	202	325	3438	-13.68	4.34	0.02
57	SLU 79	207	329	3474	-13.86	4.35	0.02
57	SLU 80	202	325	3438	-13.68	4.34	0.02
57	SLU 81	211	363	3659	-15.28	4.16	0.02
57	SLU 82	206	359	3624	-15.1	4.16	0.02
57	SLU 83	211	363	3659	-15.28	4.16	0.02
57	SLU 84	206	359	3624	-15.1	4.16	0.02
57	SLE RA 1	149	183	2287	-7.74	3.63	0.01
57	SLE RA 2	144	178	2248	-7.54	3.63	0.01
57	SLE RA 3	149	183	2287	-7.74	3.63	0.01
57	SLE RA 4	146	180	2263	-7.62	3.63	0.01
57	SLE RA 5	144	178	2248	-7.54	3.63	0.01
57	SLE RA 6	149	183	2287	-7.74	3.63	0.01
57	SLE RA 7	146	180	2263	-7.62	3.63	0.01
57	SLE RA 8	149	183	2287	-7.74	3.63	0.01
57	SLE RA 9	146	180	2263	-7.62	3.63	0.01
57	SLE RA 10	150	231	2536	-9.75	3.34	0.01
57	SLE RA 11	155	236	2576	-9.95	3.35	0.01
57	SLE RA 12	152	233	2552	-9.83	3.35	0.01
57	SLE RA 13	150	231	2536	-9.75	3.34	0.01
57	SLE RA 14	155	236	2576	-9.95	3.35	0.01
57	SLE RA 15	152	233	2552	-9.83	3.35	0.01
57	SLE RA 16	155	236	2576	-9.95	3.35	0.01
57	SLE RA 17	152	233	2552	-9.83	3.35	0.01
57	SLE RA 18	158	259	2700	-10.89	3.23	0.01
57	SLE RA 19	155	256	2676	-10.77	3.23	0.01
57	SLE RA 20	158	259	2700	-10.89	3.23	0.01
57	SLE RA 21	155	256	2676	-10.77	3.23	0.01
57	SLE FR 1	149	183	2287	-7.74	3.63	0.01
57	SLE FR 2	148	182	2279	-7.7	3.63	0.01
57	SLE FR 3	149	183	2287	-7.74	3.63	0.01
57	SLE FR 4	151	205	2403	-8.65	3.51	0.01
57	SLE FR 5	152	205	2411	-8.69	3.51	0.01
57	SLE FR 6	153	221	2494	-9.32	3.43	0.01
57	SLE QP 1	149	183	2287	-7.74	3.63	0.01
57	SLE QP 2	152	205	2411	-8.69	3.51	0.01
57	SLD 1	242	305	2739	-13.11	7.79	0.02
57	SLD 2	242	305	2739	-13.11	7.79	0.02
57	SLD 3	229	183	2675	-7.69	7.14	0.01
57	SLD 4	229	183	2675	-7.69	7.14	0.01
57	SLD 5	199	420	2607	-18.24	5.79	0.03
57	SLD 6	199	420	2607	-18.24	5.79	0.03
57	SLD 7	154	15	2393	-0.16	3.6	0
57	SLD 8	154	15	2393	-0.16	3.6	0
57	SLD 9	149	396	2429	-17.21	3.42	0.02
57	SLD 10	149	396	2429	-17.21	3.42	0.02
57	SLD 11	104	-9	2215	0.87	1.23	0
57	SLD 12	104	-9	2215	0.87	1.23	0
57	SLD 13	75	228	2147	-9.69	-0.12	0.01
57	SLD 14	75	228	2147	-9.69	-0.12	0.01
57	SLD 15	61	106	2083	-4.26	-0.77	0
57	SLD 16	61	106	2083	-4.26	-0.77	0
57	SLV 1	364	440	3185	-19.15	13.58	0.03
57	SLV 2	364	440	3185	-19.15	13.58	0.03



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
57	SLV 3	333	153	3034	-6.34	12.05	0.01
57	SLV 4	333	153	3034	-6.34	12.05	0.01
57	SLV 5	264	711	2872	-31.26	8.86	0.05
57	SLV 6	264	711	2872	-31.26	8.86	0.05
57	SLV 7	158	-245	2369	11.46	3.74	-0.02
57	SLV 8	158	-245	2369	11.46	3.74	-0.02
57	SLV 9	146	656	2453	-28.83	3.28	0.04
57	SLV 10	146	656	2453	-28.83	3.28	0.04
57	SLV 11	40	-300	1950	13.89	-1.84	-0.02
57	SLV 12	40	-300	1950	13.89	-1.84	-0.02
57	SLV 13	-29	258	1788	-11.04	-5.03	0.01
57	SLV 14	-29	258	1788	-11.04	-5.03	0.01
57	SLV 15	-61	-29	1637	1.78	-6.56	-0.01
57	SLV 16	-61	-29	1637	1.78	-6.56	-0.01
58	SLU 1	83	0	958	-0.1	4.44	0
58	SLU 2	63	0	948	0.23	2.75	0
58	SLU 3	83	0	958	-0.1	4.44	0
58	SLU 4	71	0	952	0.1	3.43	0
58	SLU 5	63	0	948	0.23	2.75	0
58	SLU 6	83	0	958	-0.1	4.44	0
58	SLU 7	71	0	952	0.1	3.43	0
58	SLU 8	83	0	958	-0.1	4.44	0
58	SLU 9	71	0	952	0.1	3.43	0
58	SLU 10	47	0	1136	0.16	2.55	0
58	SLU 11	68	0	1146	-0.17	4.24	0
58	SLU 12	55	0	1140	0.03	3.22	0
58	SLU 13	47	0	1136	0.16	2.55	0
58	SLU 14	68	0	1146	-0.17	4.24	0
58	SLU 15	55	0	1140	0.03	3.22	0
58	SLU 16	68	0	1146	-0.17	4.24	0
58	SLU 17	55	0	1140	0.03	3.22	0
58	SLU 18	61	1	1227	-0.2	4.16	0
58	SLU 19	49	0	1221	0	3.14	0
58	SLU 20	61	1	1227	-0.2	4.16	0
58	SLU 21	49	0	1221	0	3.14	0
58	SLU 22	89	0	1063	-0.13	4.88	0
58	SLU 23	68	0	1053	0.2	3.18	0
58	SLU 24	89	0	1063	-0.13	4.88	0
58	SLU 25	76	0	1057	0.07	3.86	0
58	SLU 26	68	0	1053	0.2	3.18	0
58	SLU 27	89	0	1063	-0.13	4.88	0
58	SLU 28	76	0	1057	0.07	3.86	0
58	SLU 29	89	0	1063	-0.13	4.88	0
58	SLU 30	76	0	1057	0.07	3.86	0
58	SLU 31	52	0	1242	0.13	2.98	0
58	SLU 32	73	1	1252	-0.2	4.68	0
58	SLU 33	61	0	1246	0	3.66	0
58	SLU 34	52	0	1242	0.13	2.98	0
58	SLU 35	73	1	1252	-0.2	4.68	0
58	SLU 36	61	0	1246	0	3.66	0
58	SLU 37	73	1	1252	-0.2	4.68	0
58	SLU 38	61	0	1246	0	3.66	0
58	SLU 39	66	1	1332	-0.23	4.59	0
58	SLU 40	54	0	1326	-0.03	3.58	0
58	SLU 41	66	1	1332	-0.23	4.59	0
58	SLU 42	54	0	1326	-0.03	3.58	0
58	SLU 43	106	0	1209	-0.12	5.63	0
58	SLU 44	86	0	1199	0.21	3.93	0
58	SLU 45	106	0	1209	-0.12	5.63	0
58	SLU 46	94	0	1203	0.08	4.61	0
58	SLU 47	86	0	1199	0.21	3.93	0
58	SLU 48	106	0	1209	-0.12	5.63	0
58	SLU 49	94	0	1203	0.08	4.61	0
58	SLU 50	106	0	1209	-0.12	5.63	0
58	SLU 51	94	0	1203	0.08	4.61	0
58	SLU 52	70	0	1387	0.14	3.73	0
58	SLU 53	91	0	1397	-0.19	5.43	0
58	SLU 54	78	0	1391	0.01	4.41	0
58	SLU 55	70	0	1387	0.14	3.73	0
58	SLU 56	91	0	1397	-0.19	5.43	0
58	SLU 57	78	0	1391	0.01	4.41	0
58	SLU 58	91	0	1397	-0.19	5.43	0
58	SLU 59	78	0	1391	0.01	4.41	0
58	SLU 60	84	1	1478	-0.22	5.34	0
58	SLU 61	72	0	1472	-0.02	4.32	0
58	SLU 62	84	1	1478	-0.22	5.34	0
58	SLU 63	72	0	1472	-0.02	4.32	0
58	SLU 64	112	0	1314	-0.15	6.06	0
58	SLU 65	91	0	1304	0.18	4.37	0
58	SLU 66	112	0	1314	-0.15	6.06	0
58	SLU 67	99	0	1308	0.05	5.05	0
58	SLU 68	91	0	1304	0.18	4.37	0
58	SLU 69	112	0	1314	-0.15	6.06	0
58	SLU 70	99	0	1308	0.05	5.05	0
58	SLU 71	112	0	1314	-0.15	6.06	0
58	SLU 72	99	0	1308	0.05	5.05	0
58	SLU 73	76	0	1493	0.11	4.17	0
58	SLU 74	96	1	1503	-0.22	5.86	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
58	SLU 75	84	0	1497	-0.02	4.85	0
58	SLU 76	76	0	1493	0.11	4.17	0
58	SLU 77	96	1	1503	-0.22	5.86	0
58	SLU 78	84	0	1497	-0.02	4.85	0
58	SLU 79	96	1	1503	-0.22	5.86	0
58	SLU 80	84	0	1497	-0.02	4.85	0
58	SLU 81	89	1	1583	-0.25	5.78	0
58	SLU 82	77	0	1577	-0.05	4.76	0
58	SLU 83	89	1	1583	-0.25	5.78	0
58	SLU 84	77	0	1577	-0.05	4.76	0
58	SLE RA 1	85	0	988	-0.11	4.57	0
58	SLE RA 2	71	0	981	0.11	3.44	0
58	SLE RA 3	85	0	988	-0.11	4.57	0
58	SLE RA 4	77	0	984	0.02	3.89	0
58	SLE RA 5	71	0	981	0.11	3.44	0
58	SLE RA 6	85	0	988	-0.11	4.57	0
58	SLE RA 7	77	0	984	0.02	3.89	0
58	SLE RA 8	85	0	988	-0.11	4.57	0
58	SLE RA 9	77	0	984	0.02	3.89	0
58	SLE RA 10	61	0	1107	0.07	3.3	0
58	SLE RA 11	74	0	1113	-0.15	4.43	0
58	SLE RA 12	66	0	1109	-0.02	3.76	0
58	SLE RA 13	61	0	1107	0.07	3.3	0
58	SLE RA 14	74	0	1113	-0.15	4.43	0
58	SLE RA 15	66	0	1109	-0.02	3.76	0
58	SLE RA 16	74	0	1113	-0.15	4.43	0
58	SLE RA 17	66	0	1109	-0.02	3.76	0
58	SLE RA 18	70	0	1167	-0.17	4.38	0
58	SLE RA 19	62	0	1163	-0.04	3.7	0
58	SLE RA 20	70	0	1167	-0.17	4.38	0
58	SLE RA 21	62	0	1163	-0.04	3.7	0
58	SLE FR 1	85	0	988	-0.11	4.57	0
58	SLE FR 2	82	0	986	-0.06	4.34	0
58	SLE FR 3	85	0	988	-0.11	4.57	0
58	SLE FR 4	78	0	1040	-0.08	4.28	0
58	SLE FR 5	80	0	1042	-0.13	4.51	0
58	SLE FR 6	77	0	1078	-0.14	4.47	0
58	SLE QP 1	85	0	988	-0.11	4.57	0
58	SLE QP 2	80	0	1042	-0.13	4.51	0
58	SLD 1	233	-4	1120	-1.02	10.93	-0.01
58	SLD 2	233	-4	1120	-1.02	10.93	-0.01
58	SLD 3	209	0	1097	-0.45	12.16	0
58	SLD 4	209	0	1097	-0.45	12.16	0
58	SLD 5	163	-7	1099	-1.25	4.56	-0.01
58	SLD 6	163	-7	1099	-1.25	4.56	-0.01
58	SLD 7	83	6	1024	0.63	8.68	0.01
58	SLD 8	83	6	1024	0.63	8.68	0.01
58	SLD 9	78	-6	1059	-0.88	0.34	-0.01
58	SLD 10	78	-6	1059	-0.88	0.34	-0.01
58	SLD 11	-2	8	984	1	4.46	0.01
58	SLD 12	-2	8	984	1	4.46	0.01
58	SLD 13	-49	1	986	0.2	-3.14	0
58	SLD 14	-49	1	986	0.2	-3.14	0
58	SLD 15	-73	5	963	0.76	-1.91	0
58	SLD 16	-73	5	963	0.76	-1.91	0
58	SLV 1	441	-11	1227	-2.39	19.68	-0.01
58	SLV 2	441	-11	1227	-2.39	19.68	-0.01
58	SLV 3	384	-1	1174	-0.96	22.59	0
58	SLV 4	384	-1	1174	-0.96	22.59	0
58	SLV 5	274	-19	1178	-2.96	4.63	-0.03
58	SLV 6	274	-19	1178	-2.96	4.63	-0.03
58	SLV 7	86	15	1000	1.78	14.36	0.02
58	SLV 8	86	15	1000	1.78	14.36	0.02
58	SLV 9	75	-15	1083	-2.03	-5.34	-0.02
58	SLV 10	75	-15	1083	-2.03	-5.34	-0.02
58	SLV 11	-113	19	905	2.71	4.39	0.02
58	SLV 12	-113	19	905	2.71	4.39	0.02
58	SLV 13	-223	1	910	0.71	-13.57	0
58	SLV 14	-223	1	910	0.71	-13.57	0
58	SLV 15	-280	12	856	2.13	-10.65	0.01
58	SLV 16	-280	12	856	2.13	-10.65	0.01
59	SLU 1	23	0	928	-0.07	0.85	0
59	SLU 2	13	-1	935	0.48	0.95	0
59	SLU 3	23	0	928	-0.07	0.85	0
59	SLU 4	17	0	932	0.26	0.91	0
59	SLU 5	13	-1	935	0.48	0.95	0
59	SLU 6	23	0	928	-0.07	0.85	0
59	SLU 7	17	0	932	0.26	0.91	0
59	SLU 8	23	0	928	-0.07	0.85	0
59	SLU 9	17	0	932	0.26	0.91	0
59	SLU 10	-23	-1	1115	0.4	-1.1	0
59	SLU 11	-13	0	1108	-0.15	-1.2	0
59	SLU 12	-19	0	1112	0.18	-1.14	0
59	SLU 13	-23	-1	1115	0.4	-1.1	0
59	SLU 14	-13	0	1108	-0.15	-1.2	0
59	SLU 15	-19	0	1112	0.18	-1.14	0
59	SLU 16	-13	0	1108	-0.15	-1.2	0
59	SLU 17	-19	0	1112	0.18	-1.14	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
59	SLU 18	-28	0	1185	-0.18	-2.08	0
59	SLU 19	-34	0	1189	0.15	-2.02	0
59	SLU 20	-28	0	1185	-0.18	-2.08	0
59	SLU 21	-34	0	1189	0.15	-2.02	0
59	SLU 22	19	0	1035	-0.11	0.47	0
59	SLU 23	9	-1	1042	0.44	0.58	0
59	SLU 24	19	0	1035	-0.11	0.47	0
59	SLU 25	13	0	1039	0.22	0.53	0
59	SLU 26	9	-1	1042	0.44	0.58	0
59	SLU 27	19	0	1035	-0.11	0.47	0
59	SLU 28	13	0	1039	0.22	0.53	0
59	SLU 29	19	0	1035	-0.11	0.47	0
59	SLU 30	13	0	1039	0.22	0.53	0
59	SLU 31	-27	-1	1221	0.37	-1.48	0
59	SLU 32	-17	0	1214	-0.18	-1.58	0
59	SLU 33	-23	0	1219	0.15	-1.52	0
59	SLU 34	-27	-1	1221	0.37	-1.48	0
59	SLU 35	-17	0	1214	-0.18	-1.58	0
59	SLU 36	-23	0	1219	0.15	-1.52	0
59	SLU 37	-17	0	1214	-0.18	-1.58	0
59	SLU 38	-23	0	1219	0.15	-1.52	0
59	SLU 39	-32	0	1291	-0.21	-2.46	0
59	SLU 40	-39	0	1296	0.12	-2.4	0
59	SLU 41	-32	0	1291	-0.21	-2.46	0
59	SLU 42	-39	0	1296	0.12	-2.4	0
59	SLU 43	32	0	1170	-0.09	1.24	0
59	SLU 44	21	-1	1177	0.46	1.34	0
59	SLU 45	32	0	1170	-0.09	1.24	0
59	SLU 46	25	0	1174	0.24	1.3	0
59	SLU 47	21	-1	1177	0.46	1.34	0
59	SLU 48	32	0	1170	-0.09	1.24	0
59	SLU 49	25	0	1174	0.24	1.3	0
59	SLU 50	32	0	1170	-0.09	1.24	0
59	SLU 51	25	0	1174	0.24	1.3	0
59	SLU 52	-15	-1	1357	0.39	-0.71	0
59	SLU 53	-4	0	1350	-0.16	-0.82	0
59	SLU 54	-11	0	1354	0.17	-0.75	0
59	SLU 55	-15	-1	1357	0.39	-0.71	0
59	SLU 56	-4	0	1350	-0.16	-0.82	0
59	SLU 57	-11	0	1354	0.17	-0.75	0
59	SLU 58	-4	0	1350	-0.16	-0.82	0
59	SLU 59	-11	0	1354	0.17	-0.75	0
59	SLU 60	-20	0	1427	-0.19	-1.69	0
59	SLU 61	-26	0	1431	0.14	-1.63	0
59	SLU 62	-20	0	1427	-0.19	-1.69	0
59	SLU 63	-26	0	1431	0.14	-1.63	0
59	SLU 64	27	0	1277	-0.12	0.86	0
59	SLU 65	17	-1	1284	0.43	0.96	0
59	SLU 66	27	0	1277	-0.12	0.86	0
59	SLU 67	21	0	1281	0.21	0.92	0
59	SLU 68	17	-1	1284	0.43	0.96	0
59	SLU 69	27	0	1277	-0.12	0.86	0
59	SLU 70	21	0	1281	0.21	0.92	0
59	SLU 71	27	0	1277	-0.12	0.86	0
59	SLU 72	21	0	1281	0.21	0.92	0
59	SLU 73	-19	-1	1463	0.36	-1.09	0
59	SLU 74	-8	0	1456	-0.19	-1.19	0
59	SLU 75	-15	0	1461	0.14	-1.13	0
59	SLU 76	-19	-1	1463	0.36	-1.09	0
59	SLU 77	-8	0	1456	-0.19	-1.19	0
59	SLU 78	-15	0	1461	0.14	-1.13	0
59	SLU 79	-8	0	1456	-0.19	-1.19	0
59	SLU 80	-15	0	1461	0.14	-1.13	0
59	SLU 81	-24	0	1533	-0.23	-2.07	0
59	SLU 82	-30	0	1538	0.1	-2.01	0
59	SLU 83	-24	0	1533	-0.23	-2.07	0
59	SLU 84	-30	0	1538	0.1	-2.01	0
59	SLE RA 1	22	0	959	-0.08	0.74	0
59	SLE RA 2	15	0	963	0.28	0.81	0
59	SLE RA 3	22	0	959	-0.08	0.74	0
59	SLE RA 4	18	0	961	0.14	0.78	0
59	SLE RA 5	15	0	963	0.28	0.81	0
59	SLE RA 6	22	0	959	-0.08	0.74	0
59	SLE RA 7	18	0	961	0.14	0.78	0
59	SLE RA 8	22	0	959	-0.08	0.74	0
59	SLE RA 9	18	0	961	0.14	0.78	0
59	SLE RA 10	-9	0	1083	0.23	-0.56	0
59	SLE RA 11	-2	0	1078	-0.13	-0.63	0
59	SLE RA 12	-6	0	1081	0.09	-0.58	0
59	SLE RA 13	-9	0	1083	0.23	-0.56	0
59	SLE RA 14	-2	0	1078	-0.13	-0.63	0
59	SLE RA 15	-6	0	1081	0.09	-0.58	0
59	SLE RA 16	-2	0	1078	-0.13	-0.63	0
59	SLE RA 17	-6	0	1081	0.09	-0.58	0
59	SLE RA 18	-12	0	1130	-0.16	-1.21	0
59	SLE RA 19	-16	0	1133	0.06	-1.17	0
59	SLE RA 20	-12	0	1130	-0.16	-1.21	0
59	SLE RA 21	-16	0	1133	0.06	-1.17	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
59	SLE FR 1	22	0	959	-0.08	0.74	0
59	SLE FR 2	21	0	959	-0.01	0.76	0
59	SLE FR 3	22	0	959	-0.08	0.74	0
59	SLE FR 4	10	0	1011	-0.03	0.17	0
59	SLE FR 5	12	0	1010	-0.11	0.16	0
59	SLE FR 6	5	0	1044	-0.12	-0.23	0
59	SLE QP 1	22	0	959	-0.08	0.74	0
59	SLE QP 2	12	0	1010	-0.11	0.16	0
59	SLD 1	142	-4	1041	-2.33	7.46	0.02
59	SLD 2	142	-4	1041	-2.33	7.46	0.02
59	SLD 3	167	0	1023	-0.25	6.34	0
59	SLD 4	167	0	1023	-0.25	6.34	0
59	SLD 5	14	-7	1046	-3.93	4.05	0.03
59	SLD 6	14	-7	1046	-3.93	4.05	0.03
59	SLD 7	95	6	987	3.01	0.31	-0.03
59	SLD 8	95	6	987	3.01	0.31	-0.03
59	SLD 9	-71	-6	1033	-3.22	0	0.03
59	SLD 10	-71	-6	1033	-3.22	0	0.03
59	SLD 11	9	8	973	3.72	-3.74	-0.03
59	SLD 12	9	8	973	3.72	-3.74	-0.03
59	SLD 13	-143	1	997	0.04	-6.03	0
59	SLD 14	-143	1	997	0.04	-6.03	0
59	SLD 15	-119	5	979	2.12	-7.15	-0.02
59	SLD 16	-119	5	979	2.12	-7.15	-0.02
59	SLV 1	319	-12	1087	-5.83	17.33	0.05
59	SLV 2	319	-12	1087	-5.83	17.33	0.05
59	SLV 3	376	-2	1044	-0.53	14.7	0
59	SLV 4	376	-2	1044	-0.53	14.7	0
59	SLV 5	18	-19	1098	-9.85	9.3	0.09
59	SLV 6	18	-19	1098	-9.85	9.3	0.09
59	SLV 7	207	15	955	7.8	0.53	-0.07
59	SLV 8	207	15	955	7.8	0.53	-0.07
59	SLV 9	-184	-15	1064	-8.01	-0.22	0.07
59	SLV 10	-184	-15	1064	-8.01	-0.22	0.07
59	SLV 11	6	19	922	9.64	-8.99	-0.09
59	SLV 12	6	19	922	9.64	-8.99	-0.09
59	SLV 13	-352	2	976	0.32	-14.39	0
59	SLV 14	-352	2	976	0.32	-14.39	0
59	SLV 15	-295	12	933	5.62	-17.02	-0.05
59	SLV 16	-295	12	933	5.62	-17.02	-0.05
60	SLU 1	-4	0	905	-0.06	0.27	0
60	SLU 2	-29	-1	926	0.61	-1.64	0
60	SLU 3	-4	0	905	-0.06	0.27	0
60	SLU 4	-19	0	918	0.34	-0.88	0
60	SLU 5	-29	-1	926	0.61	-1.64	0
60	SLU 6	-4	0	905	-0.06	0.27	0
60	SLU 7	-19	0	918	0.34	-0.88	0
60	SLU 8	-4	0	905	-0.06	0.27	0
60	SLU 9	-19	0	918	0.34	-0.88	0
60	SLU 10	-60	-1	1099	0.53	-2.56	0
60	SLU 11	-35	0	1078	-0.14	-0.66	0
60	SLU 12	-50	0	1091	0.26	-1.8	0
60	SLU 13	-60	-1	1099	0.53	-2.56	0
60	SLU 14	-35	0	1078	-0.14	-0.66	0
60	SLU 15	-50	0	1091	0.26	-1.8	0
60	SLU 16	-35	0	1078	-0.14	-0.66	0
60	SLU 17	-50	0	1091	0.26	-1.8	0
60	SLU 18	-48	0	1152	-0.18	-1.05	0
60	SLU 19	-64	0	1165	0.23	-2.2	0
60	SLU 20	-48	0	1152	-0.18	-1.05	0
60	SLU 21	-64	0	1165	0.23	-2.2	0
60	SLU 22	-8	0	1014	-0.1	0.25	0
60	SLU 23	-33	-1	1034	0.58	-1.66	0
60	SLU 24	-8	0	1014	-0.1	0.25	0
60	SLU 25	-23	0	1026	0.31	-0.89	0
60	SLU 26	-33	-1	1034	0.58	-1.66	0
60	SLU 27	-8	0	1014	-0.1	0.25	0
60	SLU 28	-23	0	1026	0.31	-0.89	0
60	SLU 29	-8	0	1014	-0.1	0.25	0
60	SLU 30	-23	0	1026	0.31	-0.89	0
60	SLU 31	-64	-1	1207	0.5	-2.58	0
60	SLU 32	-39	0	1187	-0.18	-0.67	0
60	SLU 33	-54	0	1199	0.23	-1.82	0
60	SLU 34	-64	-1	1207	0.5	-2.58	0
60	SLU 35	-39	0	1187	-0.18	-0.67	0
60	SLU 36	-54	0	1199	0.23	-1.82	0
60	SLU 37	-39	0	1187	-0.18	-0.67	0
60	SLU 38	-54	0	1199	0.23	-1.82	0
60	SLU 39	-52	0	1261	-0.21	-1.07	0
60	SLU 40	-68	0	1273	0.2	-2.21	0
60	SLU 41	-52	0	1261	-0.21	-1.07	0
60	SLU 42	-68	0	1273	0.2	-2.21	0
60	SLU 43	-4	0	1140	-0.07	0.36	0
60	SLU 44	-29	-1	1161	0.61	-1.55	0
60	SLU 45	-4	0	1140	-0.07	0.36	0
60	SLU 46	-19	0	1152	0.33	-0.79	0
60	SLU 47	-29	-1	1161	0.61	-1.55	0
60	SLU 48	-4	0	1140	-0.07	0.36	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
60	SLU 49	-19	0	1152	0.33	-0.79	0
60	SLU 50	-4	0	1140	-0.07	0.36	0
60	SLU 51	-19	0	1152	0.33	-0.79	0
60	SLU 52	-60	-1	1333	0.53	-2.48	0
60	SLU 53	-35	0	1313	-0.15	-0.57	0
60	SLU 54	-50	0	1325	0.26	-1.71	0
60	SLU 55	-60	-1	1333	0.53	-2.48	0
60	SLU 56	-35	0	1313	-0.15	-0.57	0
60	SLU 57	-50	0	1325	0.26	-1.71	0
60	SLU 58	-35	0	1313	-0.15	-0.57	0
60	SLU 59	-50	0	1325	0.26	-1.71	0
60	SLU 60	-48	0	1387	-0.19	-0.96	0
60	SLU 61	-63	0	1399	0.22	-2.11	0
60	SLU 62	-48	0	1387	-0.19	-0.96	0
60	SLU 63	-63	0	1399	0.22	-2.11	0
60	SLU 64	-8	0	1248	-0.1	0.34	0
60	SLU 65	-33	-1	1269	0.57	-1.57	0
60	SLU 66	-8	0	1248	-0.1	0.34	0
60	SLU 67	-23	0	1261	0.3	-0.81	0
60	SLU 68	-33	-1	1269	0.57	-1.57	0
60	SLU 69	-8	0	1248	-0.1	0.34	0
60	SLU 70	-23	0	1261	0.3	-0.81	0
60	SLU 71	-8	0	1248	-0.1	0.34	0
60	SLU 72	-23	0	1261	0.3	-0.81	0
60	SLU 73	-64	-1	1442	0.49	-2.5	0
60	SLU 74	-39	0	1421	-0.18	-0.59	0
60	SLU 75	-54	0	1433	0.22	-1.73	0
60	SLU 76	-64	-1	1442	0.49	-2.5	0
60	SLU 77	-39	0	1421	-0.18	-0.59	0
60	SLU 78	-54	0	1433	0.22	-1.73	0
60	SLU 79	-39	0	1421	-0.18	-0.59	0
60	SLU 80	-54	0	1433	0.22	-1.73	0
60	SLU 81	-52	0	1495	-0.22	-0.98	0
60	SLU 82	-67	0	1507	0.19	-2.13	0
60	SLU 83	-52	0	1495	-0.22	-0.98	0
60	SLU 84	-67	0	1507	0.19	-2.13	0
60	SLE RA 1	-5	0	936	-0.07	0.26	0
60	SLE RA 2	-22	0	950	0.38	-1.01	0
60	SLE RA 3	-5	0	936	-0.07	0.26	0
60	SLE RA 4	-15	0	945	0.2	-0.5	0
60	SLE RA 5	-22	0	950	0.38	-1.01	0
60	SLE RA 6	-5	0	936	-0.07	0.26	0
60	SLE RA 7	-15	0	945	0.2	-0.5	0
60	SLE RA 8	-5	0	936	-0.07	0.26	0
60	SLE RA 9	-15	0	945	0.2	-0.5	0
60	SLE RA 10	-43	0	1065	0.33	-1.62	0
60	SLE RA 11	-26	0	1052	-0.13	-0.35	0
60	SLE RA 12	-36	0	1060	0.14	-1.12	0
60	SLE RA 13	-43	0	1065	0.33	-1.62	0
60	SLE RA 14	-26	0	1052	-0.13	-0.35	0
60	SLE RA 15	-36	0	1060	0.14	-1.12	0
60	SLE RA 16	-26	0	1052	-0.13	-0.35	0
60	SLE RA 17	-36	0	1060	0.14	-1.12	0
60	SLE RA 18	-35	0	1101	-0.15	-0.62	0
60	SLE RA 19	-45	0	1109	0.12	-1.38	0
60	SLE RA 20	-35	0	1101	-0.15	-0.62	0
60	SLE RA 21	-45	0	1109	0.12	-1.38	0
60	SLE FR 1	-5	0	936	-0.07	0.26	0
60	SLE FR 2	-9	0	939	0.02	0.01	0
60	SLE FR 3	-5	0	936	-0.07	0.26	0
60	SLE FR 4	-17	0	989	-0.01	-0.25	0
60	SLE FR 5	-14	0	986	-0.1	0	0
60	SLE FR 6	-20	0	1019	-0.11	-0.18	0
60	SLE QP 1	-5	0	936	-0.07	0.26	0
60	SLE QP 2	-14	0	986	-0.1	0	0
60	SLD 1	116	-3	946	-4.48	6.39	0
60	SLD 2	116	-3	946	-4.48	6.39	0
60	SLD 3	141	-1	929	0.15	7.67	-0.01
60	SLD 4	141	-1	929	0.15	7.67	-0.01
60	SLD 5	-13	-3	1000	-8.42	-0.03	0.01
60	SLD 6	-13	-3	1000	-8.42	-0.03	0.01
60	SLD 7	71	2	943	6.99	4.25	-0.01
60	SLD 8	71	2	943	6.99	4.25	-0.01
60	SLD 9	-99	-2	1028	-7.18	-4.25	0.01
60	SLD 10	-99	-2	1028	-7.18	-4.25	0.01
60	SLD 11	-15	3	972	8.23	0.03	-0.01
60	SLD 12	-15	3	972	8.23	0.03	-0.01
60	SLD 13	-169	1	1042	-0.34	-7.67	0.01
60	SLD 14	-169	1	1042	-0.34	-7.67	0.01
60	SLD 15	-144	3	1025	4.28	-6.39	0
60	SLD 16	-144	3	1025	4.28	-6.39	0
60	SLV 1	293	-7	890	-11.45	15.12	-0.01
60	SLV 2	293	-7	890	-11.45	15.12	-0.01
60	SLV 3	352	-3	849	0.35	18.18	-0.01
60	SLV 4	352	-3	849	0.35	18.18	-0.01
60	SLV 5	-12	-8	1019	-21.39	-0.1	0.01
60	SLV 6	-12	-8	1019	-21.39	-0.1	0.01
60	SLV 7	186	5	883	17.93	10.09	-0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
60	SLV 8	186	5	883	17.93	10.09	-0.02
60	SLV 9	-214	-5	1089	-18.12	-10.09	0.02
60	SLV 10	-214	-5	1089	-18.12	-10.09	0.02
60	SLV 11	-16	8	953	21.2	0.1	-0.01
60	SLV 12	-16	8	953	21.2	0.1	-0.01
60	SLV 13	-380	3	1122	-0.54	-18.18	0.01
60	SLV 14	-380	3	1122	-0.54	-18.18	0.01
60	SLV 15	-321	7	1081	11.26	-15.12	0
60	SLV 16	-321	7	1081	11.26	-15.12	0
61	SLU 1	-34	0	885	-0.06	-1.75	0
61	SLU 2	-50	-1	918	0.71	-1.94	0
61	SLU 3	-34	0	885	-0.06	-1.75	0
61	SLU 4	-44	0	905	0.4	-1.86	0
61	SLU 5	-50	-1	918	0.71	-1.94	0
61	SLU 6	-34	0	885	-0.06	-1.75	0
61	SLU 7	-44	0	905	0.4	-1.86	0
61	SLU 8	-34	0	885	-0.06	-1.75	0
61	SLU 9	-44	0	905	0.4	-1.86	0
61	SLU 10	-89	-1	1089	0.63	-4.17	0
61	SLU 11	-72	0	1057	-0.14	-3.98	0
61	SLU 12	-82	0	1076	0.32	-4.09	0
61	SLU 13	-89	-1	1089	0.63	-4.17	0
61	SLU 14	-72	0	1057	-0.14	-3.98	0
61	SLU 15	-82	0	1076	0.32	-4.09	0
61	SLU 16	-72	0	1057	-0.14	-3.98	0
61	SLU 17	-82	0	1076	0.32	-4.09	0
61	SLU 18	-89	0	1130	-0.17	-4.94	0
61	SLU 19	-99	0	1150	0.28	-5.05	0
61	SLU 20	-89	0	1130	-0.17	-4.94	0
61	SLU 21	-99	0	1150	0.28	-5.05	0
61	SLU 22	-43	0	997	-0.09	-2.38	0
61	SLU 23	-59	-1	1030	0.67	-2.56	0
61	SLU 24	-43	0	997	-0.09	-2.38	0
61	SLU 25	-53	0	1017	0.37	-2.49	0
61	SLU 26	-59	-1	1030	0.67	-2.56	0
61	SLU 27	-43	0	997	-0.09	-2.38	0
61	SLU 28	-53	0	1017	0.37	-2.49	0
61	SLU 29	-43	0	997	-0.09	-2.38	0
61	SLU 30	-53	0	1017	0.37	-2.49	0
61	SLU 31	-98	-1	1202	0.59	-4.79	0
61	SLU 32	-81	0	1169	-0.17	-4.61	0
61	SLU 33	-91	0	1189	0.29	-4.72	0
61	SLU 34	-98	-1	1202	0.59	-4.79	0
61	SLU 35	-81	0	1169	-0.17	-4.61	0
61	SLU 36	-91	0	1189	0.29	-4.72	0
61	SLU 37	-81	0	1169	-0.17	-4.61	0
61	SLU 38	-91	0	1189	0.29	-4.72	0
61	SLU 39	-98	0	1243	-0.21	-5.56	0
61	SLU 40	-108	0	1262	0.25	-5.68	0
61	SLU 41	-98	0	1243	-0.21	-5.56	0
61	SLU 42	-108	0	1262	0.25	-5.68	0
61	SLU 43	-41	0	1112	-0.07	-2.06	0
61	SLU 44	-57	-1	1145	0.7	-2.25	0
61	SLU 45	-41	0	1112	-0.07	-2.06	0
61	SLU 46	-50	0	1132	0.39	-2.17	0
61	SLU 47	-57	-1	1145	0.7	-2.25	0
61	SLU 48	-41	0	1112	-0.07	-2.06	0
61	SLU 49	-50	0	1132	0.39	-2.17	0
61	SLU 50	-41	0	1112	-0.07	-2.06	0
61	SLU 51	-50	0	1132	0.39	-2.17	0
61	SLU 52	-96	-1	1317	0.62	-4.48	0
61	SLU 53	-79	0	1284	-0.15	-4.29	0
61	SLU 54	-89	0	1303	0.31	-4.4	0
61	SLU 55	-96	-1	1317	0.62	-4.48	0
61	SLU 56	-79	0	1284	-0.15	-4.29	0
61	SLU 57	-89	0	1303	0.31	-4.4	0
61	SLU 58	-79	0	1284	-0.15	-4.29	0
61	SLU 59	-89	0	1303	0.31	-4.4	0
61	SLU 60	-96	0	1357	-0.18	-5.25	0
61	SLU 61	-105	0	1377	0.28	-5.36	0
61	SLU 62	-96	0	1357	-0.18	-5.25	0
61	SLU 63	-105	0	1377	0.28	-5.36	0
61	SLU 64	-50	0	1225	-0.1	-2.69	0
61	SLU 65	-66	-1	1257	0.67	-2.87	0
61	SLU 66	-50	0	1225	-0.1	-2.69	0
61	SLU 67	-60	0	1244	0.36	-2.8	0
61	SLU 68	-66	-1	1257	0.67	-2.87	0
61	SLU 69	-50	0	1225	-0.1	-2.69	0
61	SLU 70	-60	0	1244	0.36	-2.8	0
61	SLU 71	-50	0	1225	-0.1	-2.69	0
61	SLU 72	-60	0	1244	0.36	-2.8	0
61	SLU 73	-105	-1	1429	0.59	-5.1	0
61	SLU 74	-88	0	1396	-0.18	-4.92	0
61	SLU 75	-98	0	1416	0.28	-5.03	0
61	SLU 76	-105	-1	1429	0.59	-5.1	0
61	SLU 77	-88	0	1396	-0.18	-4.92	0
61	SLU 78	-98	0	1416	0.28	-5.03	0
61	SLU 79	-88	0	1396	-0.18	-4.92	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione			
		x	y	z		x	y	z	
61	SLU 80	-98	0	1416		0.28	-5.03	0	0
61	SLU 81	-105	0	1470		-0.21	-5.87	0	0
61	SLU 82	-115	0	1489		0.25	-5.98	0	0
61	SLU 83	-105	0	1470		-0.21	-5.87	0	0
61	SLU 84	-115	0	1489		0.25	-5.98	0	0
61	SLE RA 1	-36	0	917		-0.07	-1.93	0	0
61	SLE RA 2	-47	0	939		0.44	-2.05	0	0
61	SLE RA 3	-36	0	917		-0.07	-1.93	0	0
61	SLE RA 4	-43	0	930		0.24	-2	0	0
61	SLE RA 5	-47	0	939		0.44	-2.05	0	0
61	SLE RA 6	-36	0	917		-0.07	-1.93	0	0
61	SLE RA 7	-43	0	930		0.24	-2	0	0
61	SLE RA 8	-36	0	917		-0.07	-1.93	0	0
61	SLE RA 9	-43	0	930		0.24	-2	0	0
61	SLE RA 10	-73	0	1053		0.39	-3.54	0	0
61	SLE RA 11	-62	0	1032		-0.12	-3.42	0	0
61	SLE RA 12	-69	0	1045		0.18	-3.49	0	0
61	SLE RA 13	-73	0	1053		0.39	-3.54	0	0
61	SLE RA 14	-62	0	1032		-0.12	-3.42	0	0
61	SLE RA 15	-69	0	1045		0.18	-3.49	0	0
61	SLE RA 16	-62	0	1032		-0.12	-3.42	0	0
61	SLE RA 17	-69	0	1045		0.18	-3.49	0	0
61	SLE RA 18	-73	0	1081		-0.15	-4.05	0	0
61	SLE RA 19	-80	0	1094		0.16	-4.13	0	0
61	SLE RA 20	-73	0	1081		-0.15	-4.05	0	0
61	SLE RA 21	-80	0	1094		0.16	-4.13	0	0
61	SLE FR 1	-36	0	917		-0.07	-1.93	0	0
61	SLE FR 2	-38	0	922		0.03	-1.95	0	0
61	SLE FR 3	-36	0	917		-0.07	-1.93	0	0
61	SLE FR 4	-49	0	971		0.01	-2.59	0	0
61	SLE FR 5	-47	0	966		-0.09	-2.57	0	0
61	SLE FR 6	-55	0	999		-0.11	-2.99	0	0
61	SLE QP 1	-36	0	917		-0.07	-1.93	0	0
61	SLE QP 2	-47	0	966		-0.09	-2.57	0	0
61	SLD 1	76	4	880		-7.19	4.44	0.01	0
61	SLD 2	76	4	880		-7.19	4.44	0.01	0
61	SLD 3	99	0	859		0.51	3.38	0	0
61	SLD 4	99	0	859		0.51	3.38	0	0
61	SLD 5	-45	7	972		-13.91	1.16	0.01	0
61	SLD 6	-45	7	972		-13.91	1.16	0.01	0
61	SLD 7	32	-6	903		11.78	-2.4	-0.01	0
61	SLD 8	32	-6	903		11.78	-2.4	-0.01	0
61	SLD 9	-126	6	1030		-11.96	-2.73	0.01	0
61	SLD 10	-126	6	1030		-11.96	-2.73	0.01	0
61	SLD 11	-49	-7	961		13.73	-6.29	-0.01	0
61	SLD 12	-49	-7	961		13.73	-6.29	-0.01	0
61	SLD 13	-194	0	1074		-0.69	-8.51	0	0
61	SLD 14	-194	0	1074		-0.69	-8.51	0	0
61	SLD 15	-171	-4	1053		7.01	-9.57	-0.01	0
61	SLD 16	-171	-4	1053		7.01	-9.57	-0.01	0
61	SLV 1	243	11	760		-18.63	13.91	0.02	0
61	SLV 2	243	11	760		-18.63	13.91	0.02	0
61	SLV 3	298	1	710		1.05	11.4	0	0
61	SLV 4	298	1	710		1.05	11.4	0	0
61	SLV 5	-43	19	980		-35.5	6.18	0.03	0
61	SLV 6	-43	19	980		-35.5	6.18	0.03	0
61	SLV 7	139	-15	814		30.1	-2.18	-0.02	0
61	SLV 8	139	-15	814		30.1	-2.18	-0.02	0
61	SLV 9	-234	15	1119		-30.28	-2.96	0.02	0
61	SLV 10	-234	15	1119		-30.28	-2.96	0.02	0
61	SLV 11	-52	-18	952		35.31	-11.31	-0.03	0
61	SLV 12	-52	-18	952		35.31	-11.31	-0.03	0
61	SLV 13	-393	-1	1222		-1.23	-16.54	0	0
61	SLV 14	-393	-1	1222		-1.23	-16.54	0	0
61	SLV 15	-338	-11	1172		18.45	-19.04	-0.02	0
61	SLV 16	-338	-11	1172		18.45	-19.04	-0.02	0
62	SLU 1	-58	0	868		-0.06	-2.25	0	0
62	SLU 2	-86	-1	915		0.79	-4.25	0	0
62	SLU 3	-58	0	868		-0.06	-2.25	0	0
62	SLU 4	-75	0	896		0.45	-3.45	0	0
62	SLU 5	-86	-1	915		0.79	-4.25	0	0
62	SLU 6	-58	0	868		-0.06	-2.25	0	0
62	SLU 7	-75	0	896		0.45	-3.45	0	0
62	SLU 8	-58	0	868		-0.06	-2.25	0	0
62	SLU 9	-75	0	896		0.45	-3.45	0	0
62	SLU 10	-117	-1	1093		0.7	-5.33	0	0
62	SLU 11	-89	0	1046		-0.14	-3.33	0	0
62	SLU 12	-106	0	1074		0.37	-4.53	0	0
62	SLU 13	-117	-1	1093		0.7	-5.33	0	0
62	SLU 14	-89	0	1046		-0.14	-3.33	0	0
62	SLU 15	-106	0	1074		0.37	-4.53	0	0
62	SLU 16	-89	0	1046		-0.14	-3.33	0	0
62	SLU 17	-106	0	1074		0.37	-4.53	0	0
62	SLU 18	-103	0	1122		-0.18	-3.79	0	0
62	SLU 19	-119	0	1150		0.33	-4.99	0	0
62	SLU 20	-103	0	1122		-0.18	-3.79	0	0
62	SLU 21	-119	0	1150		0.33	-4.99	0	0
62	SLU 22	-67	0	986		-0.09	-2.56	0	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
62	SLU 23	-95	-1	1033	0.76	-4.56	0
62	SLU 24	-67	0	986	-0.09	-2.56	0
62	SLU 25	-84	0	1014	0.42	-3.76	0
62	SLU 26	-95	-1	1033	0.76	-4.56	0
62	SLU 27	-67	0	986	-0.09	-2.56	0
62	SLU 28	-84	0	1014	0.42	-3.76	0
62	SLU 29	-67	0	986	-0.09	-2.56	0
62	SLU 30	-84	0	1014	0.42	-3.76	0
62	SLU 31	-126	-1	1211	0.67	-5.63	0
62	SLU 32	-99	0	1164	-0.18	-3.63	0
62	SLU 33	-115	0	1192	0.33	-4.83	0
62	SLU 34	-126	-1	1211	0.67	-5.63	0
62	SLU 35	-99	0	1164	-0.18	-3.63	0
62	SLU 36	-115	0	1192	0.33	-4.83	0
62	SLU 37	-99	0	1164	-0.18	-3.63	0
62	SLU 38	-115	0	1192	0.33	-4.83	0
62	SLU 39	-112	0	1240	-0.21	-4.09	0
62	SLU 40	-129	0	1268	0.3	-5.29	0
62	SLU 41	-112	0	1240	-0.21	-4.09	0
62	SLU 42	-129	0	1268	0.3	-5.29	0
62	SLU 43	-72	0	1087	-0.06	-2.82	0
62	SLU 44	-100	-1	1135	0.78	-4.82	0
62	SLU 45	-72	0	1087	-0.06	-2.82	0
62	SLU 46	-89	0	1116	0.45	-4.02	0
62	SLU 47	-100	-1	1135	0.78	-4.82	0
62	SLU 48	-72	0	1087	-0.06	-2.82	0
62	SLU 49	-89	0	1116	0.45	-4.02	0
62	SLU 50	-72	0	1087	-0.06	-2.82	0
62	SLU 51	-89	0	1116	0.45	-4.02	0
62	SLU 52	-131	-1	1313	0.7	-5.9	0
62	SLU 53	-103	0	1265	-0.15	-3.9	0
62	SLU 54	-120	0	1294	0.36	-5.1	0
62	SLU 55	-131	-1	1313	0.7	-5.9	0
62	SLU 56	-103	0	1265	-0.15	-3.9	0
62	SLU 57	-120	0	1294	0.36	-5.1	0
62	SLU 58	-103	0	1265	-0.15	-3.9	0
62	SLU 59	-120	0	1294	0.36	-5.1	0
62	SLU 60	-117	0	1342	-0.18	-4.36	0
62	SLU 61	-133	0	1370	0.32	-5.56	0
62	SLU 62	-117	0	1342	-0.18	-4.36	0
62	SLU 63	-133	0	1370	0.32	-5.56	0
62	SLU 64	-82	0	1206	-0.1	-3.13	0
62	SLU 65	-109	-1	1253	0.75	-5.13	0
62	SLU 66	-82	0	1206	-0.1	-3.13	0
62	SLU 67	-98	0	1234	0.41	-4.33	0
62	SLU 68	-109	-1	1253	0.75	-5.13	0
62	SLU 69	-82	0	1206	-0.1	-3.13	0
62	SLU 70	-98	0	1234	0.41	-4.33	0
62	SLU 71	-82	0	1206	-0.1	-3.13	0
62	SLU 72	-98	0	1234	0.41	-4.33	0
62	SLU 73	-141	-1	1431	0.67	-6.2	0
62	SLU 74	-113	0	1384	-0.18	-4.2	0
62	SLU 75	-129	0	1412	0.33	-5.4	0
62	SLU 76	-141	-1	1431	0.67	-6.2	0
62	SLU 77	-113	0	1384	-0.18	-4.2	0
62	SLU 78	-129	0	1412	0.33	-5.4	0
62	SLU 79	-113	0	1384	-0.18	-4.2	0
62	SLU 80	-129	0	1412	0.33	-5.4	0
62	SLU 81	-126	0	1460	-0.22	-4.66	0
62	SLU 82	-143	0	1488	0.29	-5.86	0
62	SLU 83	-126	0	1460	-0.22	-4.66	0
62	SLU 84	-143	0	1488	0.29	-5.86	0
62	SLE RA 1	-61	0	901	-0.07	-2.34	0
62	SLE RA 2	-79	0	933	0.5	-3.67	0
62	SLE RA 3	-61	0	901	-0.07	-2.34	0
62	SLE RA 4	-72	0	920	0.27	-3.14	0
62	SLE RA 5	-79	0	933	0.5	-3.67	0
62	SLE RA 6	-61	0	901	-0.07	-2.34	0
62	SLE RA 7	-72	0	920	0.27	-3.14	0
62	SLE RA 8	-61	0	901	-0.07	-2.34	0
62	SLE RA 9	-72	0	920	0.27	-3.14	0
62	SLE RA 10	-100	0	1052	0.44	-4.39	0
62	SLE RA 11	-81	0	1020	-0.12	-3.06	0
62	SLE RA 12	-93	0	1039	0.21	-3.86	0
62	SLE RA 13	-100	0	1052	0.44	-4.39	0
62	SLE RA 14	-81	0	1020	-0.12	-3.06	0
62	SLE RA 15	-93	0	1039	0.21	-3.86	0
62	SLE RA 16	-81	0	1020	-0.12	-3.06	0
62	SLE RA 17	-93	0	1039	0.21	-3.86	0
62	SLE RA 18	-90	0	1071	-0.15	-3.36	0
62	SLE RA 19	-102	0	1090	0.19	-4.16	0
62	SLE RA 20	-90	0	1071	-0.15	-3.36	0
62	SLE RA 21	-102	0	1090	0.19	-4.16	0
62	SLE FR 1	-61	0	901	-0.07	-2.34	0
62	SLE FR 2	-64	0	908	0.05	-2.6	0
62	SLE FR 3	-61	0	901	-0.07	-2.34	0
62	SLE FR 4	-73	0	959	0.02	-2.91	0
62	SLE FR 5	-70	0	952	-0.09	-2.65	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
62	SLE FR 6	-76	0	986	-0.11	-2.85	0
62	SLE QP 1	-61	0	901	-0.07	-2.34	0
62	SLE QP 2	-70	0	952	-0.09	-2.65	0
62	SLD 1	45	8	800	-10.15	3.34	0.02
62	SLD 2	45	8	800	-10.15	3.34	0.02
62	SLD 3	68	0	769	0.78	4.57	0
62	SLD 4	68	0	769	0.78	4.57	0
62	SLD 5	-69	15	953	-19.68	-2.7	0.03
62	SLD 6	-69	15	953	-19.68	-2.7	0.03
62	SLD 7	6	-13	851	16.74	1.37	-0.03
62	SLD 8	6	-13	851	16.74	1.37	-0.03
62	SLD 9	-145	13	1054	-16.93	-6.66	0.03
62	SLD 10	-145	13	1054	-16.93	-6.66	0.03
62	SLD 11	-70	-15	951	19.5	-2.59	-0.03
62	SLD 12	-70	-15	951	19.5	-2.59	-0.03
62	SLD 13	-207	1	1135	-0.96	-9.86	0
62	SLD 14	-207	1	1135	-0.96	-9.86	0
62	SLD 15	-184	-8	1104	9.97	-8.63	-0.02
62	SLD 16	-184	-8	1104	9.97	-8.63	-0.02
62	SLV 1	202	21	593	-26.51	11.54	0.04
62	SLV 2	202	21	593	-26.51	11.54	0.04
62	SLV 3	255	-1	519	1.4	14.47	0
62	SLV 4	255	-1	519	1.4	14.47	0
62	SLV 5	-69	39	956	-50.36	-2.82	0.08
62	SLV 6	-69	39	956	-50.36	-2.82	0.08
62	SLV 7	109	-33	711	42.7	6.92	-0.07
62	SLV 8	109	-33	711	42.7	6.92	-0.07
62	SLV 9	-248	33	1193	-42.88	-12.21	0.07
62	SLV 10	-248	33	1193	-42.88	-12.21	0.07
62	SLV 11	-70	-39	949	50.18	-2.47	-0.08
62	SLV 12	-70	-39	949	50.18	-2.47	-0.08
62	SLV 13	-394	1	1385	-1.59	-19.76	0
62	SLV 14	-394	1	1385	-1.59	-19.76	0
62	SLV 15	-341	-20	1312	26.33	-16.83	-0.04
62	SLV 16	-341	-20	1312	26.33	-16.83	-0.04
63	SLU 1	-95	0	879	-0.06	-5.02	0
63	SLU 2	-112	-1	953	0.86	-5.53	0
63	SLU 3	-95	0	879	-0.06	-5.02	0
63	SLU 4	-105	-1	923	0.49	-5.32	0
63	SLU 5	-112	-1	953	0.86	-5.53	0
63	SLU 6	-95	0	879	-0.06	-5.02	0
63	SLU 7	-105	-1	923	0.49	-5.32	0
63	SLU 8	-95	0	879	-0.06	-5.02	0
63	SLU 9	-105	-1	923	0.49	-5.32	0
63	SLU 10	-150	-1	1158	0.77	-7.92	0
63	SLU 11	-133	0	1085	-0.15	-7.41	0
63	SLU 12	-143	0	1129	0.4	-7.71	0
63	SLU 13	-150	-1	1158	0.77	-7.92	0
63	SLU 14	-133	0	1085	-0.15	-7.41	0
63	SLU 15	-143	0	1129	0.4	-7.71	0
63	SLU 16	-133	0	1085	-0.15	-7.41	0
63	SLU 17	-143	0	1129	0.4	-7.71	0
63	SLU 18	-150	0	1173	-0.19	-8.43	0
63	SLU 19	-160	0	1217	0.36	-8.74	0
63	SLU 20	-150	0	1173	-0.19	-8.43	0
63	SLU 21	-160	0	1217	0.36	-8.74	0
63	SLU 22	-111	0	1011	-0.09	-6.04	0
63	SLU 23	-128	-1	1084	0.82	-6.54	0
63	SLU 24	-111	0	1011	-0.09	-6.04	0
63	SLU 25	-121	-1	1055	0.45	-6.34	0
63	SLU 26	-128	-1	1084	0.82	-6.54	0
63	SLU 27	-111	0	1011	-0.09	-6.04	0
63	SLU 28	-121	-1	1055	0.45	-6.34	0
63	SLU 29	-111	0	1011	-0.09	-6.04	0
63	SLU 30	-121	-1	1055	0.45	-6.34	0
63	SLU 31	-166	-1	1290	0.73	-8.93	0
63	SLU 32	-150	0	1217	-0.18	-8.43	0
63	SLU 33	-160	0	1261	0.37	-8.73	0
63	SLU 34	-166	-1	1290	0.73	-8.93	0
63	SLU 35	-150	0	1217	-0.18	-8.43	0
63	SLU 36	-160	0	1261	0.37	-8.73	0
63	SLU 37	-150	0	1217	-0.18	-8.43	0
63	SLU 38	-160	0	1261	0.37	-8.73	0
63	SLU 39	-166	0	1305	-0.22	-9.45	0
63	SLU 40	-176	0	1349	0.33	-9.76	0
63	SLU 41	-166	0	1305	-0.22	-9.45	0
63	SLU 42	-176	0	1349	0.33	-9.76	0
63	SLU 43	-118	0	1098	-0.06	-6.18	0
63	SLU 44	-135	-1	1171	0.85	-6.68	0
63	SLU 45	-118	0	1098	-0.06	-6.18	0
63	SLU 46	-128	-1	1142	0.49	-6.48	0
63	SLU 47	-135	-1	1171	0.85	-6.68	0
63	SLU 48	-118	0	1098	-0.06	-6.18	0
63	SLU 49	-128	-1	1142	0.49	-6.48	0
63	SLU 50	-118	0	1098	-0.06	-6.18	0
63	SLU 51	-128	-1	1142	0.49	-6.48	0
63	SLU 52	-173	-1	1377	0.76	-9.07	0
63	SLU 53	-156	0	1304	-0.15	-8.57	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
63	SLU 54	-166	0	1348	0.4	-8.87	0
63	SLU 55	-173	-1	1377	0.76	-9.07	0
63	SLU 56	-156	0	1304	-0.15	-8.57	0
63	SLU 57	-166	0	1348	0.4	-8.87	0
63	SLU 58	-156	0	1304	-0.15	-8.57	0
63	SLU 59	-166	0	1348	0.4	-8.87	0
63	SLU 60	-173	0	1392	-0.19	-9.59	0
63	SLU 61	-183	0	1436	0.36	-9.89	0
63	SLU 62	-173	0	1392	-0.19	-9.59	0
63	SLU 63	-183	0	1436	0.36	-9.89	0
63	SLU 64	-134	0	1230	-0.1	-7.2	0
63	SLU 65	-151	-1	1303	0.82	-7.7	0
63	SLU 66	-134	0	1230	-0.1	-7.2	0
63	SLU 67	-144	-1	1274	0.45	-7.5	0
63	SLU 68	-151	-1	1303	0.82	-7.7	0
63	SLU 69	-134	0	1230	-0.1	-7.2	0
63	SLU 70	-144	-1	1274	0.45	-7.5	0
63	SLU 71	-134	0	1230	-0.1	-7.2	0
63	SLU 72	-144	-1	1274	0.45	-7.5	0
63	SLU 73	-189	-1	1509	0.73	-10.09	0
63	SLU 74	-172	0	1435	-0.19	-9.59	0
63	SLU 75	-183	0	1479	0.36	-9.89	0
63	SLU 76	-189	-1	1509	0.73	-10.09	0
63	SLU 77	-172	0	1435	-0.19	-9.59	0
63	SLU 78	-183	0	1479	0.36	-9.89	0
63	SLU 79	-172	0	1435	-0.19	-9.59	0
63	SLU 80	-183	0	1479	0.36	-9.89	0
63	SLU 81	-189	0	1523	-0.23	-10.61	0
63	SLU 82	-199	0	1567	0.32	-10.91	0
63	SLU 83	-189	0	1523	-0.23	-10.61	0
63	SLU 84	-199	0	1567	0.32	-10.91	0
63	SLE RA 1	-100	0	917	-0.07	-5.31	0
63	SLE RA 2	-111	-1	966	0.54	-5.65	0
63	SLE RA 3	-100	0	917	-0.07	-5.31	0
63	SLE RA 4	-106	0	946	0.3	-5.51	0
63	SLE RA 5	-111	-1	966	0.54	-5.65	0
63	SLE RA 6	-100	0	917	-0.07	-5.31	0
63	SLE RA 7	-106	0	946	0.3	-5.51	0
63	SLE RA 8	-100	0	917	-0.07	-5.31	0
63	SLE RA 9	-106	0	946	0.3	-5.51	0
63	SLE RA 10	-136	-1	1103	0.48	-7.24	0
63	SLE RA 11	-125	0	1054	-0.13	-6.91	0
63	SLE RA 12	-132	0	1083	0.24	-7.11	0
63	SLE RA 13	-136	-1	1103	0.48	-7.24	0
63	SLE RA 14	-125	0	1054	-0.13	-6.91	0
63	SLE RA 15	-132	0	1083	0.24	-7.11	0
63	SLE RA 16	-125	0	1054	-0.13	-6.91	0
63	SLE RA 17	-132	0	1083	0.24	-7.11	0
63	SLE RA 18	-136	0	1113	-0.15	-7.59	0
63	SLE RA 19	-143	0	1142	0.21	-7.79	0
63	SLE RA 20	-136	0	1113	-0.15	-7.59	0
63	SLE RA 21	-143	0	1142	0.21	-7.79	0
63	SLE FR 1	-100	0	917	-0.07	-5.31	0
63	SLE FR 2	-102	0	927	0.05	-5.38	0
63	SLE FR 3	-100	0	917	-0.07	-5.31	0
63	SLE FR 4	-113	0	985	0.03	-6.06	0
63	SLE FR 5	-111	0	976	-0.09	-5.99	0
63	SLE FR 6	-118	0	1015	-0.11	-6.45	0
63	SLE QP 1	-100	0	917	-0.07	-5.31	0
63	SLE QP 2	-111	0	976	-0.09	-5.99	0
63	SLD 1	-15	16	696	-12.97	-0.62	0.08
63	SLD 2	-15	16	696	-12.97	-0.62	0.08
63	SLD 3	3	-1	642	0.88	0.35	-0.01
63	SLD 4	3	-1	642	0.88	0.35	-0.01
63	SLD 5	-109	31	973	-24.96	-5.85	0.15
63	SLD 6	-109	31	973	-24.96	-5.85	0.15
63	SLD 7	-49	-26	794	21.2	-2.62	-0.13
63	SLD 8	-49	-26	794	21.2	-2.62	-0.13
63	SLD 9	-172	26	1157	-21.39	-9.37	0.13
63	SLD 10	-172	26	1157	-21.39	-9.37	0.13
63	SLD 11	-112	-30	978	24.77	-6.14	-0.15
63	SLD 12	-112	-30	978	24.77	-6.14	-0.15
63	SLD 13	-224	1	1309	-1.07	-12.34	0.01
63	SLD 14	-224	1	1309	-1.07	-12.34	0.01
63	SLD 15	-206	-16	1256	12.78	-11.37	-0.08
63	SLD 16	-206	-16	1256	12.78	-11.37	-0.08
63	SLV 1	114	42	315	-34.13	6.64	0.2
63	SLV 2	114	42	315	-34.13	6.64	0.2
63	SLV 3	156	-1	188	1.24	8.92	-0.01
63	SLV 4	156	-1	188	1.24	8.92	-0.01
63	SLV 5	-108	78	970	-63.97	-5.66	0.38
63	SLV 6	-108	78	970	-63.97	-5.66	0.38
63	SLV 7	34	-66	547	53.97	1.94	-0.32
63	SLV 8	34	-66	547	53.97	1.94	-0.32
63	SLV 9	-255	66	1405	-54.16	-13.93	0.32
63	SLV 10	-255	66	1405	-54.16	-13.93	0.32
63	SLV 11	-113	-78	981	63.78	-6.33	-0.38
63	SLV 12	-113	-78	981	63.78	-6.33	-0.38



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
63	SLV 13	-378	1	1764	-1.43	-20.91	0.01
63	SLV 14	-378	1	1764	-1.43	-20.91	0.01
63	SLV 15	-335	-42	1637	33.94	-18.63	-0.2
63	SLV 16	-335	-42	1637	33.94	-18.63	-0.2
64	SLU 1	-139	0	511	-0.03	-2.94	-0.01
64	SLU 2	-162	0	571	0.42	-4	0.08
64	SLU 3	-139	0	511	-0.03	-2.94	-0.01
64	SLU 4	-153	0	547	0.24	-3.58	0.04
64	SLU 5	-162	0	571	0.42	-4	0.08
64	SLU 6	-139	0	511	-0.03	-2.94	-0.01
64	SLU 7	-153	0	547	0.24	-3.58	0.04
64	SLU 8	-139	0	511	-0.03	-2.94	-0.01
64	SLU 9	-153	0	547	0.24	-3.58	0.04
64	SLU 10	-202	0	708	0.38	-4.83	0.07
64	SLU 11	-179	0	647	-0.07	-3.77	-0.01
64	SLU 12	-193	0	684	0.2	-4.41	0.04
64	SLU 13	-202	0	708	0.38	-4.83	0.07
64	SLU 14	-179	0	647	-0.07	-3.77	-0.01
64	SLU 15	-193	0	684	0.2	-4.41	0.04
64	SLU 16	-179	0	647	-0.07	-3.77	-0.01
64	SLU 17	-193	0	684	0.2	-4.41	0.04
64	SLU 18	-197	0	706	-0.09	-4.13	-0.02
64	SLU 19	-210	0	742	0.18	-4.76	0.03
64	SLU 20	-197	0	706	-0.09	-4.13	-0.02
64	SLU 21	-210	0	742	0.18	-4.76	0.03
64	SLU 22	-162	0	593	-0.05	-3.37	-0.01
64	SLU 23	-184	0	654	0.4	-4.43	0.07
64	SLU 24	-162	0	593	-0.05	-3.37	-0.01
64	SLU 25	-175	0	629	0.22	-4.01	0.04
64	SLU 26	-184	0	654	0.4	-4.43	0.07
64	SLU 27	-162	0	593	-0.05	-3.37	-0.01
64	SLU 28	-175	0	629	0.22	-4.01	0.04
64	SLU 29	-162	0	593	-0.05	-3.37	-0.01
64	SLU 30	-175	0	629	0.22	-4.01	0.04
64	SLU 31	-224	0	790	0.36	-5.26	0.07
64	SLU 32	-202	0	730	-0.09	-4.2	-0.02
64	SLU 33	-215	0	766	0.18	-4.84	0.03
64	SLU 34	-224	0	790	0.36	-5.26	0.07
64	SLU 35	-202	0	730	-0.09	-4.2	-0.02
64	SLU 36	-215	0	766	0.18	-4.84	0.03
64	SLU 37	-202	0	730	-0.09	-4.2	-0.02
64	SLU 38	-215	0	766	0.18	-4.84	0.03
64	SLU 39	-219	0	788	-0.11	-4.56	-0.02
64	SLU 40	-232	0	825	0.16	-5.19	0.03
64	SLU 41	-219	0	788	-0.11	-4.56	-0.02
64	SLU 42	-232	0	825	0.16	-5.19	0.03
64	SLU 43	-174	0	636	-0.03	-3.68	-0.01
64	SLU 44	-196	0	696	0.42	-4.73	0.08
64	SLU 45	-174	0	636	-0.03	-3.68	-0.01
64	SLU 46	-187	0	672	0.24	-4.31	0.04
64	SLU 47	-196	0	696	0.42	-4.73	0.08
64	SLU 48	-174	0	636	-0.03	-3.68	-0.01
64	SLU 49	-187	0	672	0.24	-4.31	0.04
64	SLU 50	-174	0	636	-0.03	-3.68	-0.01
64	SLU 51	-187	0	672	0.24	-4.31	0.04
64	SLU 52	-236	0	833	0.38	-5.56	0.07
64	SLU 53	-214	0	773	-0.07	-4.51	-0.01
64	SLU 54	-227	0	809	0.2	-5.14	0.04
64	SLU 55	-236	0	833	0.38	-5.56	0.07
64	SLU 56	-214	0	773	-0.07	-4.51	-0.01
64	SLU 57	-227	0	809	0.2	-5.14	0.04
64	SLU 58	-214	0	773	-0.07	-4.51	-0.01
64	SLU 59	-227	0	809	0.2	-5.14	0.04
64	SLU 60	-231	0	831	-0.09	-4.86	-0.02
64	SLU 61	-244	0	867	0.18	-5.5	0.03
64	SLU 62	-231	0	831	-0.09	-4.86	-0.02
64	SLU 63	-244	0	867	0.18	-5.5	0.03
64	SLU 64	-196	0	718	-0.05	-4.11	-0.01
64	SLU 65	-218	0	779	0.4	-5.17	0.07
64	SLU 66	-196	0	718	-0.05	-4.11	-0.01
64	SLU 67	-209	0	755	0.22	-4.74	0.04
64	SLU 68	-218	0	779	0.4	-5.17	0.07
64	SLU 69	-196	0	718	-0.05	-4.11	-0.01
64	SLU 70	-209	0	755	0.22	-4.74	0.04
64	SLU 71	-196	0	718	-0.05	-4.11	-0.01
64	SLU 72	-209	0	755	0.22	-4.74	0.04
64	SLU 73	-258	0	915	0.36	-6	0.07
64	SLU 74	-236	0	855	-0.09	-4.94	-0.02
64	SLU 75	-249	0	891	0.18	-5.57	0.03
64	SLU 76	-258	0	915	0.36	-6	0.07
64	SLU 77	-236	0	855	-0.09	-4.94	-0.02
64	SLU 78	-249	0	891	0.18	-5.57	0.03
64	SLU 79	-236	0	855	-0.09	-4.94	-0.02
64	SLU 80	-249	0	891	0.18	-5.57	0.03
64	SLU 81	-253	0	913	-0.11	-5.29	-0.02
64	SLU 82	-267	0	950	0.16	-5.93	0.03
64	SLU 83	-253	0	913	-0.11	-5.29	-0.02
64	SLU 84	-267	0	950	0.16	-5.93	0.03



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione		
		x	y	z		x	y	z
64	SLE RA 1	-146	0	534		-0.03	-3.07	-0.01
64	SLE RA 2	-161	0	575		0.27	-3.77	0.05
64	SLE RA 3	-146	0	534		-0.03	-3.07	-0.01
64	SLE RA 4	-155	0	559		0.15	-3.49	0.03
64	SLE RA 5	-161	0	575		0.27	-3.77	0.05
64	SLE RA 6	-146	0	534		-0.03	-3.07	-0.01
64	SLE RA 7	-155	0	559		0.15	-3.49	0.03
64	SLE RA 8	-146	0	534		-0.03	-3.07	-0.01
64	SLE RA 9	-155	0	559		0.15	-3.49	0.03
64	SLE RA 10	-187	0	666		0.24	-4.32	0.04
64	SLE RA 11	-173	0	625		-0.06	-3.62	-0.01
64	SLE RA 12	-181	0	650		0.12	-4.04	0.02
64	SLE RA 13	-187	0	666		0.24	-4.32	0.04
64	SLE RA 14	-173	0	625		-0.06	-3.62	-0.01
64	SLE RA 15	-181	0	650		0.12	-4.04	0.02
64	SLE RA 16	-173	0	625		-0.06	-3.62	-0.01
64	SLE RA 17	-181	0	650		0.12	-4.04	0.02
64	SLE RA 18	-184	0	664		-0.07	-3.86	-0.01
64	SLE RA 19	-193	0	689		0.11	-4.28	0.02
64	SLE RA 20	-184	0	664		-0.07	-3.86	-0.01
64	SLE RA 21	-193	0	689		0.11	-4.28	0.02
64	SLE FR 1	-146	0	534		-0.03	-3.07	-0.01
64	SLE FR 2	-149	0	542		0.03	-3.21	0
64	SLE FR 3	-146	0	534		-0.03	-3.07	-0.01
64	SLE FR 4	-160	0	582		0.01	-3.44	0
64	SLE FR 5	-157	0	573		-0.05	-3.3	-0.01
64	SLE FR 6	-165	0	599		-0.05	-3.46	-0.01
64	SLE QP 1	-146	0	534		-0.03	-3.07	-0.01
64	SLE QP 2	-157	0	573		-0.05	-3.3	-0.01
64	SLD 1	-71	9	326		-7.08	-0.35	-1.35
64	SLD 2	-71	9	326		-7.08	-0.35	-1.35
64	SLD 3	-55	1	279		0.39	0.25	0.07
64	SLD 4	-55	1	279		0.39	0.25	0.07
64	SLD 5	-157	16	570		-13.49	-3.33	-2.56
64	SLD 6	-157	16	570		-13.49	-3.33	-2.56
64	SLD 7	-101	-13	414		11.42	-1.32	2.16
64	SLD 8	-101	-13	414		11.42	-1.32	2.16
64	SLD 9	-213	13	733		-11.51	-5.28	-2.18
64	SLD 10	-213	13	733		-11.51	-5.28	-2.18
64	SLD 11	-158	-16	577		13.4	-3.27	2.54
64	SLD 12	-158	-16	577		13.4	-3.27	2.54
64	SLD 13	-260	-1	868		-0.48	-6.85	-0.09
64	SLD 14	-260	-1	868		-0.48	-6.85	-0.09
64	SLD 15	-243	-9	821		6.99	-6.25	1.33
64	SLD 16	-243	-9	821		6.99	-6.25	1.33
64	SLV 1	45	25	-11		-18.74	3.69	-3.57
64	SLV 2	45	25	-11		-18.74	3.69	-3.57
64	SLV 3	84	3	-122		0.34	5.13	0.04
64	SLV 4	84	3	-122		0.34	5.13	0.04
64	SLV 5	-156	40	567		-34.59	-3.39	-6.56
64	SLV 6	-156	40	567		-34.59	-3.39	-6.56
64	SLV 7	-25	-32	196		29.01	1.42	5.49
64	SLV 8	-25	-32	196		29.01	1.42	5.49
64	SLV 9	-289	32	951		-29.1	-8.02	-5.51
64	SLV 10	-289	32	951		-29.1	-8.02	-5.51
64	SLV 11	-158	-40	580		34.5	-3.21	6.54
64	SLV 12	-158	-40	580		34.5	-3.21	6.54
64	SLV 13	-399	-3	1269		-0.43	-11.74	-0.06
64	SLV 14	-399	-3	1269		-0.43	-11.74	-0.06
64	SLV 15	-360	-25	1158		18.65	-10.3	3.55
64	SLV 16	-360	-25	1158		18.65	-10.3	3.55
65	SLU 1	95	0	330		-0.07	1.9	0.01
65	SLU 2	80	-2	292		0.61	1.38	-0.13
65	SLU 3	95	0	330		-0.07	1.9	0.01
65	SLU 4	86	-1	307		0.34	1.59	-0.07
65	SLU 5	80	-2	292		0.61	1.38	-0.13
65	SLU 6	95	0	330		-0.07	1.9	0.01
65	SLU 7	86	-1	307		0.34	1.59	-0.07
65	SLU 8	95	0	330		-0.07	1.9	0.01
65	SLU 9	86	-1	307		0.34	1.59	-0.07
65	SLU 10	56	-1	209		0.52	0.73	-0.11
65	SLU 11	71	0	247		-0.15	1.25	0.03
65	SLU 12	62	-1	224		0.25	0.94	-0.06
65	SLU 13	56	-1	209		0.52	0.73	-0.11
65	SLU 14	71	0	247		-0.15	1.25	0.03
65	SLU 15	62	-1	224		0.25	0.94	-0.06
65	SLU 16	71	0	247		-0.15	1.25	0.03
65	SLU 17	62	-1	224		0.25	0.94	-0.06
65	SLU 18	61	0	211		-0.19	0.97	0.04
65	SLU 19	52	-1	188		0.22	0.66	-0.05
65	SLU 20	61	0	211		-0.19	0.97	0.04
65	SLU 21	52	-1	188		0.22	0.66	-0.05
65	SLU 22	95	0	329		-0.1	1.85	0.02
65	SLU 23	80	-1	291		0.57	1.33	-0.12
65	SLU 24	95	0	329		-0.1	1.85	0.02
65	SLU 25	86	-1	306		0.3	1.54	-0.07
65	SLU 26	80	-1	291		0.57	1.33	-0.12
65	SLU 27	95	0	329		-0.1	1.85	0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
65	SLU 28	86	-1	306	0.3	1.54	-0.07
65	SLU 29	95	0	329	-0.1	1.85	0.02
65	SLU 30	86	-1	306	0.3	1.54	-0.07
65	SLU 31	56	-1	207	0.49	0.68	-0.11
65	SLU 32	71	0	245	-0.19	1.2	0.04
65	SLU 33	62	-1	222	0.22	0.89	-0.05
65	SLU 34	56	-1	207	0.49	0.68	-0.11
65	SLU 35	71	0	245	-0.19	1.2	0.04
65	SLU 36	62	-1	222	0.22	0.89	-0.05
65	SLU 37	71	0	245	-0.19	1.2	0.04
65	SLU 38	62	-1	222	0.22	0.89	-0.05
65	SLU 39	61	0	210	-0.22	0.92	0.04
65	SLU 40	52	-1	187	0.18	0.61	-0.04
65	SLU 41	61	0	210	-0.22	0.92	0.04
65	SLU 42	52	-1	187	0.18	0.61	-0.04
65	SLU 43	124	0	429	-0.08	2.49	0.01
65	SLU 44	109	-2	391	0.6	1.97	-0.13
65	SLU 45	124	0	429	-0.08	2.49	0.01
65	SLU 46	115	-1	407	0.33	2.18	-0.07
65	SLU 47	109	-2	391	0.6	1.97	-0.13
65	SLU 48	124	0	429	-0.08	2.49	0.01
65	SLU 49	115	-1	407	0.33	2.18	-0.07
65	SLU 50	124	0	429	-0.08	2.49	0.01
65	SLU 51	115	-1	407	0.33	2.18	-0.07
65	SLU 52	85	-1	308	0.51	1.32	-0.11
65	SLU 53	99	0	346	-0.16	1.84	0.03
65	SLU 54	91	-1	323	0.24	1.53	-0.05
65	SLU 55	85	-1	308	0.51	1.32	-0.11
65	SLU 56	99	0	346	-0.16	1.84	0.03
65	SLU 57	91	-1	323	0.24	1.53	-0.05
65	SLU 58	99	0	346	-0.16	1.84	0.03
65	SLU 59	91	-1	323	0.24	1.53	-0.05
65	SLU 60	89	0	311	-0.2	1.56	0.04
65	SLU 61	80	-1	288	0.21	1.25	-0.05
65	SLU 62	89	0	311	-0.2	1.56	0.04
65	SLU 63	80	-1	288	0.21	1.25	-0.05
65	SLU 64	124	0	428	-0.11	2.44	0.02
65	SLU 65	109	-1	390	0.56	1.92	-0.12
65	SLU 66	124	0	428	-0.11	2.44	0.02
65	SLU 67	115	-1	405	0.29	2.13	-0.06
65	SLU 68	109	-1	390	0.56	1.92	-0.12
65	SLU 69	124	0	428	-0.11	2.44	0.02
65	SLU 70	115	-1	405	0.29	2.13	-0.06
65	SLU 71	124	0	428	-0.11	2.44	0.02
65	SLU 72	115	-1	405	0.29	2.13	-0.06
65	SLU 73	85	-1	307	0.48	1.27	-0.1
65	SLU 74	99	0	345	-0.2	1.79	0.04
65	SLU 75	91	-1	322	0.21	1.47	-0.05
65	SLU 76	85	-1	307	0.48	1.27	-0.1
65	SLU 77	99	0	345	-0.2	1.79	0.04
65	SLU 78	91	-1	322	0.21	1.47	-0.05
65	SLU 79	99	0	345	-0.2	1.79	0.04
65	SLU 80	91	-1	322	0.21	1.47	-0.05
65	SLU 81	89	0	309	-0.23	1.51	0.05
65	SLU 82	80	-1	286	0.17	1.2	-0.04
65	SLU 83	89	0	309	-0.23	1.51	0.05
65	SLU 84	80	-1	286	0.17	1.2	-0.04
65	SLE RA 1	95	0	330	-0.08	1.89	0.02
65	SLE RA 2	85	-1	304	0.37	1.54	-0.08
65	SLE RA 3	95	0	330	-0.08	1.89	0.02
65	SLE RA 4	89	-1	314	0.19	1.68	-0.04
65	SLE RA 5	85	-1	304	0.37	1.54	-0.08
65	SLE RA 6	95	0	330	-0.08	1.89	0.02
65	SLE RA 7	89	-1	314	0.19	1.68	-0.04
65	SLE RA 8	95	0	330	-0.08	1.89	0.02
65	SLE RA 9	89	-1	314	0.19	1.68	-0.04
65	SLE RA 10	69	-1	249	0.32	1.11	-0.07
65	SLE RA 11	79	0	274	-0.13	1.45	0.03
65	SLE RA 12	73	-1	259	0.14	1.24	-0.03
65	SLE RA 13	69	-1	249	0.32	1.11	-0.07
65	SLE RA 14	79	0	274	-0.13	1.45	0.03
65	SLE RA 15	73	-1	259	0.14	1.24	-0.03
65	SLE RA 16	79	0	274	-0.13	1.45	0.03
65	SLE RA 17	73	-1	259	0.14	1.24	-0.03
65	SLE RA 18	72	0	250	-0.16	1.27	0.03
65	SLE RA 19	66	-1	235	0.11	1.06	-0.03
65	SLE RA 20	72	0	250	-0.16	1.27	0.03
65	SLE RA 21	66	-1	235	0.11	1.06	-0.03
65	SLE FR 1	95	0	330	-0.08	1.89	0.02
65	SLE FR 2	93	0	325	0.01	1.82	0
65	SLE FR 3	95	0	330	-0.08	1.89	0.02
65	SLE FR 4	86	0	301	-0.01	1.63	0
65	SLE FR 5	88	0	306	-0.1	1.7	0.02
65	SLE FR 6	84	0	290	-0.12	1.58	0.02
65	SLE QP 1	95	0	330	-0.08	1.89	0.02
65	SLE QP 2	88	0	306	-0.1	1.7	0.02
65	SLD 1	219	16	649	-6.19	6.07	1.33
65	SLD 2	219	16	649	-6.19	6.07	1.33



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
65	SLD 3	196	2	586	-1.76	5.34	0.35
65	SLD 4	196	2	586	-1.76	5.34	0.35
65	SLD 5	163	25	505	-8.64	4.13	1.89
65	SLD 6	163	25	505	-8.64	4.13	1.89
65	SLD 7	85	-20	294	6.11	1.67	-1.36
65	SLD 8	85	-20	294	6.11	1.67	-1.36
65	SLD 9	91	20	318	-6.31	1.73	1.39
65	SLD 10	91	20	318	-6.31	1.73	1.39
65	SLD 11	13	-25	107	8.43	-0.73	-1.85
65	SLD 12	13	-25	107	8.43	-0.73	-1.85
65	SLD 13	-19	-2	26	1.56	-1.93	-0.31
65	SLD 14	-19	-2	26	1.56	-1.93	-0.31
65	SLD 15	-43	-15	-37	5.98	-2.67	-1.29
65	SLD 16	-43	-15	-37	5.98	-2.67	-1.29
65	SLV 1	398	44	1118	-17.55	12.07	3.76
65	SLV 2	398	44	1118	-17.55	12.07	3.76
65	SLV 3	344	10	971	-6.25	10.36	1.27
65	SLV 4	344	10	971	-6.25	10.36	1.27
65	SLV 5	263	65	771	-22.48	7.41	4.91
65	SLV 6	263	65	771	-22.48	7.41	4.91
65	SLV 7	83	-49	283	15.2	1.7	-3.37
65	SLV 8	83	-49	283	15.2	1.7	-3.37
65	SLV 9	94	49	328	-15.4	1.7	3.41
65	SLV 10	94	49	328	-15.4	1.7	3.41
65	SLV 11	-87	-65	-160	22.27	-4.01	-4.87
65	SLV 12	-87	-65	-160	22.27	-4.01	-4.87
65	SLV 13	-167	-10	-360	6.04	-6.96	-1.23
65	SLV 14	-167	-10	-360	6.04	-6.96	-1.23
65	SLV 15	-222	-44	-506	17.34	-8.67	-3.72
65	SLV 16	-222	-44	-506	17.34	-8.67	-3.72
66	SLU 1	58	0	630	-0.17	2.35	0
66	SLU 2	41	-2	587	0.98	1.38	0
66	SLU 3	58	0	630	-0.17	2.35	0
66	SLU 4	48	-1	604	0.52	1.77	0
66	SLU 5	41	-2	587	0.98	1.38	0
66	SLU 6	58	0	630	-0.17	2.35	0
66	SLU 7	48	-1	604	0.52	1.77	0
66	SLU 8	58	0	630	-0.17	2.35	0
66	SLU 9	48	-1	604	0.52	1.77	0
66	SLU 10	23	-1	526	0.81	-0.42	0
66	SLU 11	41	1	569	-0.34	0.55	0
66	SLU 12	30	-1	543	0.35	-0.03	0
66	SLU 13	23	-1	526	0.81	-0.42	0
66	SLU 14	41	1	569	-0.34	0.55	0
66	SLU 15	30	-1	543	0.35	-0.03	0
66	SLU 16	41	1	569	-0.34	0.55	0
66	SLU 17	30	-1	543	0.35	-0.03	0
66	SLU 18	33	1	542	-0.41	-0.22	0
66	SLU 19	22	-1	517	0.27	-0.8	0
66	SLU 20	33	1	542	-0.41	-0.22	0
66	SLU 21	22	-1	517	0.27	-0.8	0
66	SLU 22	58	0	660	-0.25	1.95	0
66	SLU 23	40	-2	617	0.9	0.99	0
66	SLU 24	58	0	660	-0.25	1.95	0
66	SLU 25	47	-1	634	0.44	1.38	0
66	SLU 26	40	-2	617	0.9	0.99	0
66	SLU 27	58	0	660	-0.25	1.95	0
66	SLU 28	47	-1	634	0.44	1.38	0
66	SLU 29	58	0	660	-0.25	1.95	0
66	SLU 30	47	-1	634	0.44	1.38	0
66	SLU 31	22	-1	555	0.73	-0.81	0
66	SLU 32	40	1	598	-0.42	0.16	0
66	SLU 33	29	-1	573	0.27	-0.42	0
66	SLU 34	22	-1	555	0.73	-0.81	0
66	SLU 35	40	1	598	-0.42	0.16	0
66	SLU 36	29	-1	573	0.27	-0.42	0
66	SLU 37	40	1	598	-0.42	0.16	0
66	SLU 38	29	-1	573	0.27	-0.42	0
66	SLU 39	32	1	572	-0.49	-0.62	0
66	SLU 40	21	0	546	0.2	-1.2	0
66	SLU 41	32	1	572	-0.49	-0.62	0
66	SLU 42	21	0	546	0.2	-1.2	0
66	SLU 43	76	0	809	-0.19	3.19	0
66	SLU 44	59	-2	766	0.96	2.22	0
66	SLU 45	76	0	809	-0.19	3.19	0
66	SLU 46	66	-1	783	0.5	2.61	0
66	SLU 47	59	-2	766	0.96	2.22	0
66	SLU 48	76	0	809	-0.19	3.19	0
66	SLU 49	66	-1	783	0.5	2.61	0
66	SLU 50	76	0	809	-0.19	3.19	0
66	SLU 51	66	-1	783	0.5	2.61	0
66	SLU 52	41	-1	705	0.78	0.42	0
66	SLU 53	58	1	747	-0.36	1.39	0
66	SLU 54	48	-1	722	0.32	0.81	0
66	SLU 55	41	-1	705	0.78	0.42	0
66	SLU 56	58	1	747	-0.36	1.39	0
66	SLU 57	48	-1	722	0.32	0.81	0
66	SLU 58	58	1	747	-0.36	1.39	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
66	SLU 59	48	-1	722	0.32	0.81	0
66	SLU 60	51	1	721	-0.44	0.62	0
66	SLU 61	40	0	696	0.25	0.04	0
66	SLU 62	51	1	721	-0.44	0.62	0
66	SLU 63	40	0	696	0.25	0.04	0
66	SLU 64	75	0	838	-0.27	2.79	0
66	SLU 65	58	-1	796	0.88	1.83	0
66	SLU 66	75	0	838	-0.27	2.79	0
66	SLU 67	65	-1	813	0.42	2.21	0
66	SLU 68	58	-1	796	0.88	1.83	0
66	SLU 69	75	0	838	-0.27	2.79	0
66	SLU 70	65	-1	813	0.42	2.21	0
66	SLU 71	75	0	838	-0.27	2.79	0
66	SLU 72	65	-1	813	0.42	2.21	0
66	SLU 73	40	-1	734	0.71	0.03	0
66	SLU 74	57	1	777	-0.44	1	0
66	SLU 75	47	0	751	0.25	0.42	0
66	SLU 76	40	-1	734	0.71	0.03	0
66	SLU 77	57	1	777	-0.44	1	0
66	SLU 78	47	0	751	0.25	0.42	0
66	SLU 79	57	1	777	-0.44	1	0
66	SLU 80	47	0	751	0.25	0.42	0
66	SLU 81	50	1	751	-0.52	0.22	0
66	SLU 82	39	0	725	0.17	-0.36	0
66	SLU 83	50	1	751	-0.52	0.22	0
66	SLU 84	39	0	725	0.17	-0.36	0
66	SLE RA 1	58	0	638	-0.19	2.24	0
66	SLE RA 2	46	-1	610	0.57	1.59	0
66	SLE RA 3	58	0	638	-0.19	2.24	0
66	SLE RA 4	51	0	621	0.27	1.85	0
66	SLE RA 5	46	-1	610	0.57	1.59	0
66	SLE RA 6	58	0	638	-0.19	2.24	0
66	SLE RA 7	51	0	621	0.27	1.85	0
66	SLE RA 8	58	0	638	-0.19	2.24	0
66	SLE RA 9	51	0	621	0.27	1.85	0
66	SLE RA 10	35	-1	569	0.46	0.39	0
66	SLE RA 11	46	0	598	-0.3	1.04	0
66	SLE RA 12	39	0	580	0.15	0.65	0
66	SLE RA 13	35	-1	569	0.46	0.39	0
66	SLE RA 14	46	0	598	-0.3	1.04	0
66	SLE RA 15	39	0	580	0.15	0.65	0
66	SLE RA 16	46	0	598	-0.3	1.04	0
66	SLE RA 17	39	0	580	0.15	0.65	0
66	SLE RA 18	41	1	580	-0.35	0.52	0
66	SLE RA 19	34	0	563	0.1	0.14	0
66	SLE RA 20	41	1	580	-0.35	0.52	0
66	SLE RA 21	34	0	563	0.1	0.14	0
66	SLE FR 1	58	0	638	-0.19	2.24	0
66	SLE FR 2	56	0	633	-0.04	2.11	0
66	SLE FR 3	58	0	638	-0.19	2.24	0
66	SLE FR 4	51	0	615	-0.09	1.59	0
66	SLE FR 5	53	0	621	-0.24	1.72	0
66	SLE FR 6	50	0	609	-0.27	1.38	0
66	SLE QP 1	58	0	638	-0.19	2.24	0
66	SLE QP 2	53	0	621	-0.24	1.72	0
66	SLD 1	210	15	1010	-9.97	10.63	-0.03
66	SLD 2	210	15	1010	-9.97	10.63	-0.03
66	SLD 3	183	7	932	-3.59	9.1	-0.01
66	SLD 4	183	7	932	-3.59	9.1	-0.01
66	SLD 5	141	17	856	-12.85	6.72	-0.05
66	SLD 6	141	17	856	-12.85	6.72	-0.05
66	SLD 7	52	-9	596	8.44	1.61	0.04
66	SLD 8	52	-9	596	8.44	1.61	0.04
66	SLD 9	55	10	646	-8.92	1.83	-0.04
66	SLD 10	55	10	646	-8.92	1.83	-0.04
66	SLD 11	-34	-16	386	12.37	-3.27	0.05
66	SLD 12	-34	-16	386	12.37	-3.27	0.05
66	SLD 13	-77	-6	310	3.11	-5.66	0.01
66	SLD 14	-77	-6	310	3.11	-5.66	0.01
66	SLD 15	-104	-14	232	9.5	-7.19	0.03
66	SLD 16	-104	-14	232	9.5	-7.19	0.03
66	SLV 1	423	43	1542	-28.37	22.75	-0.09
66	SLV 2	423	43	1542	-28.37	22.75	-0.09
66	SLV 3	361	23	1360	-12.07	19.2	-0.03
66	SLV 4	361	23	1360	-12.07	19.2	-0.03
66	SLV 5	258	43	1172	-33.4	13.42	-0.13
66	SLV 6	258	43	1172	-33.4	13.42	-0.13
66	SLV 7	51	-23	568	20.94	1.58	0.09
66	SLV 8	51	-23	568	20.94	1.58	0.09
66	SLV 9	55	23	674	-21.42	1.87	-0.09
66	SLV 10	55	23	674	-21.42	1.87	-0.09
66	SLV 11	-152	-42	70	32.92	-9.97	0.13
66	SLV 12	-152	-42	70	32.92	-9.97	0.13
66	SLV 13	-255	-23	-119	11.59	-15.75	0.03
66	SLV 14	-255	-23	-119	11.59	-15.75	0.03
66	SLV 15	-317	-42	-300	27.89	-19.31	0.09
66	SLV 16	-317	-42	-300	27.89	-19.31	0.09
67	SLU 1	41	0	699	-0.23	1.44	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
67	SLU 2	18	-1	673	0.57	0.27	0
67	SLU 3	41	0	699	-0.23	1.44	0
67	SLU 4	27	0	683	0.25	0.74	0
67	SLU 5	18	-1	673	0.57	0.27	0
67	SLU 6	41	0	699	-0.23	1.44	0
67	SLU 7	27	0	683	0.25	0.74	0
67	SLU 8	41	0	699	-0.23	1.44	0
67	SLU 9	27	0	683	0.25	0.74	0
67	SLU 10	2	0	713	0.39	-0.84	0
67	SLU 11	25	1	739	-0.42	0.33	0
67	SLU 12	11	0	723	0.07	-0.37	0
67	SLU 13	2	0	713	0.39	-0.84	0
67	SLU 14	25	1	739	-0.42	0.33	0
67	SLU 15	11	0	723	0.07	-0.37	0
67	SLU 16	25	1	739	-0.42	0.33	0
67	SLU 17	11	0	723	0.07	-0.37	0
67	SLU 18	18	1	756	-0.5	-0.15	0
67	SLU 19	5	0	741	-0.01	-0.85	0
67	SLU 20	18	1	756	-0.5	-0.15	0
67	SLU 21	5	0	741	-0.01	-0.85	0
67	SLU 22	39	0	768	-0.32	1.19	0
67	SLU 23	16	-1	743	0.48	0.02	0
67	SLU 24	39	0	768	-0.32	1.19	0
67	SLU 25	25	0	753	0.16	0.49	0
67	SLU 26	16	-1	743	0.48	0.02	0
67	SLU 27	39	0	768	-0.32	1.19	0
67	SLU 28	25	0	753	0.16	0.49	0
67	SLU 29	39	0	768	-0.32	1.19	0
67	SLU 30	25	0	753	0.16	0.49	0
67	SLU 31	1	0	783	0.3	-1.09	0
67	SLU 32	23	1	809	-0.51	0.08	0
67	SLU 33	10	0	793	-0.03	-0.62	0
67	SLU 34	1	0	783	0.3	-1.09	0
67	SLU 35	23	1	809	-0.51	0.08	0
67	SLU 36	10	0	793	-0.03	-0.62	0
67	SLU 37	23	1	809	-0.51	0.08	0
67	SLU 38	10	0	793	-0.03	-0.62	0
67	SLU 39	17	1	826	-0.59	-0.39	0
67	SLU 40	3	0	810	-0.1	-1.09	0
67	SLU 41	17	1	826	-0.59	-0.39	0
67	SLU 42	3	0	810	-0.1	-1.09	0
67	SLU 43	53	0	884	-0.27	1.95	0
67	SLU 44	30	-1	858	0.53	0.78	0
67	SLU 45	53	0	884	-0.27	1.95	0
67	SLU 46	40	0	869	0.21	1.25	0
67	SLU 47	30	-1	858	0.53	0.78	0
67	SLU 48	53	0	884	-0.27	1.95	0
67	SLU 49	40	0	869	0.21	1.25	0
67	SLU 50	53	0	884	-0.27	1.95	0
67	SLU 51	40	0	869	0.21	1.25	0
67	SLU 52	15	0	899	0.35	-0.32	0
67	SLU 53	38	1	924	-0.45	0.85	0
67	SLU 54	24	0	909	0.03	0.14	0
67	SLU 55	15	0	899	0.35	-0.32	0
67	SLU 56	38	1	924	-0.45	0.85	0
67	SLU 57	24	0	909	0.03	0.14	0
67	SLU 58	38	1	924	-0.45	0.85	0
67	SLU 59	24	0	909	0.03	0.14	0
67	SLU 60	31	1	942	-0.53	0.37	0
67	SLU 61	17	0	926	-0.05	-0.33	0
67	SLU 62	31	1	942	-0.53	0.37	0
67	SLU 63	17	0	926	-0.05	-0.33	0
67	SLU 64	52	1	954	-0.36	1.7	0
67	SLU 65	29	-1	928	0.44	0.54	0
67	SLU 66	52	1	954	-0.36	1.7	0
67	SLU 67	38	0	939	0.12	1	0
67	SLU 68	29	-1	928	0.44	0.54	0
67	SLU 69	52	1	954	-0.36	1.7	0
67	SLU 70	38	0	939	0.12	1	0
67	SLU 71	52	1	954	-0.36	1.7	0
67	SLU 72	38	0	939	0.12	1	0
67	SLU 73	13	0	969	0.26	-0.57	0
67	SLU 74	36	1	994	-0.55	0.6	0
67	SLU 75	22	0	979	-0.06	-0.1	0
67	SLU 76	13	0	969	0.26	-0.57	0
67	SLU 77	36	1	994	-0.55	0.6	0
67	SLU 78	22	0	979	-0.06	-0.1	0
67	SLU 79	36	1	994	-0.55	0.6	0
67	SLU 80	22	0	979	-0.06	-0.1	0
67	SLU 81	29	1	1011	-0.62	0.12	0
67	SLU 82	16	0	996	-0.14	-0.58	0
67	SLU 83	29	1	1011	-0.62	0.12	0
67	SLU 84	16	0	996	-0.14	-0.58	0
67	SLE RA 1	40	0	719	-0.26	1.37	0
67	SLE RA 2	25	0	701	0.28	0.59	0
67	SLE RA 3	40	0	719	-0.26	1.37	0
67	SLE RA 4	31	0	708	0.06	0.9	0
67	SLE RA 5	25	0	701	0.28	0.59	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
67	SLE RA 6	40	0	719	-0.26	1.37	0
67	SLE RA 7	31	0	708	0.06	0.9	0
67	SLE RA 8	40	0	719	-0.26	1.37	0
67	SLE RA 9	31	0	708	0.06	0.9	0
67	SLE RA 10	14	0	728	0.15	-0.15	0
67	SLE RA 11	30	1	745	-0.38	0.63	0
67	SLE RA 12	21	0	735	-0.06	0.16	0
67	SLE RA 13	14	0	728	0.15	-0.15	0
67	SLE RA 14	30	1	745	-0.38	0.63	0
67	SLE RA 15	21	0	735	-0.06	0.16	0
67	SLE RA 16	30	1	745	-0.38	0.63	0
67	SLE RA 17	21	0	735	-0.06	0.16	0
67	SLE RA 18	25	1	757	-0.43	0.31	0
67	SLE RA 19	16	0	747	-0.11	-0.16	0
67	SLE RA 20	25	1	757	-0.43	0.31	0
67	SLE RA 21	16	0	747	-0.11	-0.16	0
67	SLE FR 1	40	0	719	-0.26	1.37	0
67	SLE FR 2	37	0	715	-0.15	1.21	0
67	SLE FR 3	40	0	719	-0.26	1.37	0
67	SLE FR 4	33	0	727	-0.2	0.89	0
67	SLE FR 5	36	0	730	-0.31	1.05	0
67	SLE FR 6	33	1	738	-0.35	0.84	0
67	SLE QP 1	40	0	719	-0.26	1.37	0
67	SLE QP 2	36	0	730	-0.31	1.05	0
67	SLD 1	235	6	968	-6.56	10.91	0.01
67	SLD 2	235	6	968	-6.56	10.91	0.01
67	SLD 3	202	8	906	-3.21	9.31	0.01
67	SLD 4	202	8	906	-3.21	9.31	0.01
67	SLD 5	146	-1	895	-7.27	6.43	0.01
67	SLD 6	146	-1	895	-7.27	6.43	0.01
67	SLD 7	36	6	689	3.91	1.1	-0.01
67	SLD 8	36	6	689	3.91	1.1	-0.01
67	SLD 9	36	-5	771	-4.53	0.99	0.01
67	SLD 10	36	-5	771	-4.53	0.99	0.01
67	SLD 11	-74	2	565	6.65	-4.33	-0.01
67	SLD 12	-74	2	565	6.65	-4.33	-0.01
67	SLD 13	-131	-7	554	2.59	-7.21	-0.01
67	SLD 14	-131	-7	554	2.59	-7.21	-0.01
67	SLD 15	-164	-5	492	5.94	-8.81	-0.01
67	SLD 16	-164	-5	492	5.94	-8.81	-0.01
67	SLV 1	507	18	1294	-18.56	24.42	0.04
67	SLV 2	507	18	1294	-18.56	24.42	0.04
67	SLV 3	431	23	1149	-10.02	20.7	0.02
67	SLV 4	431	23	1149	-10.02	20.7	0.02
67	SLV 5	293	-1	1119	-18.74	13.69	0.03
67	SLV 6	293	-1	1119	-18.74	13.69	0.03
67	SLV 7	38	14	636	9.73	1.31	-0.01
67	SLV 8	38	14	636	9.73	1.31	-0.01
67	SLV 9	34	-13	824	-10.35	0.79	0.01
67	SLV 10	34	-13	824	-10.35	0.79	0.01
67	SLV 11	-222	2	341	18.12	-11.6	-0.03
67	SLV 12	-222	2	341	18.12	-11.6	-0.03
67	SLV 13	-359	-22	311	9.4	-18.6	-0.02
67	SLV 14	-359	-22	311	9.4	-18.6	-0.02
67	SLV 15	-436	-17	166	17.94	-22.32	-0.04
67	SLV 16	-436	-17	166	17.94	-22.32	-0.04
68	SLU 1	34	1	808	-0.38	0.58	0
68	SLU 2	8	1	788	0.03	-0.53	0
68	SLU 3	34	1	808	-0.38	0.58	0
68	SLU 4	19	1	796	-0.13	-0.08	0
68	SLU 5	8	1	788	0.03	-0.53	0
68	SLU 6	34	1	808	-0.38	0.58	0
68	SLU 7	19	1	796	-0.13	-0.08	0
68	SLU 8	34	1	808	-0.38	0.58	0
68	SLU 9	19	1	796	-0.13	-0.08	0
68	SLU 10	3	2	930	-0.2	-1.61	0.01
68	SLU 11	28	2	949	-0.62	-0.51	0
68	SLU 12	13	2	938	-0.37	-1.17	0.01
68	SLU 13	3	2	930	-0.2	-1.61	0.01
68	SLU 14	28	2	949	-0.62	-0.51	0
68	SLU 15	13	2	938	-0.37	-1.17	0.01
68	SLU 16	28	2	949	-0.62	-0.51	0
68	SLU 17	13	2	938	-0.37	-1.17	0.01
68	SLU 18	26	2	1010	-0.72	-0.97	0.01
68	SLU 19	11	2	998	-0.47	-1.63	0.01
68	SLU 20	26	2	1010	-0.72	-0.97	0.01
68	SLU 21	11	2	998	-0.47	-1.63	0.01
68	SLU 22	35	2	924	-0.51	0.26	0
68	SLU 23	10	1	904	-0.09	-0.85	0.01
68	SLU 24	35	2	924	-0.51	0.26	0
68	SLU 25	20	1	912	-0.26	-0.41	0.01
68	SLU 26	10	1	904	-0.09	-0.85	0.01
68	SLU 27	35	2	924	-0.51	0.26	0
68	SLU 28	20	1	912	-0.26	-0.41	0.01
68	SLU 29	35	2	924	-0.51	0.26	0
68	SLU 30	20	1	912	-0.26	-0.41	0.01
68	SLU 31	4	2	1045	-0.33	-1.93	0.01
68	SLU 32	30	2	1065	-0.75	-0.83	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
68	SLU 33	15	2	1053	-0.5	-1.49	0.01
68	SLU 34	4	2	1045	-0.33	-1.93	0.01
68	SLU 35	30	2	1065	-0.75	-0.83	0.01
68	SLU 36	15	2	1053	-0.5	-1.49	0.01
68	SLU 37	30	2	1065	-0.75	-0.83	0.01
68	SLU 38	15	2	1053	-0.5	-1.49	0.01
68	SLU 39	27	3	1126	-0.85	-1.29	0.01
68	SLU 40	12	2	1114	-0.6	-1.96	0.01
68	SLU 41	27	3	1126	-0.85	-1.29	0.01
68	SLU 42	12	2	1114	-0.6	-1.96	0.01
68	SLU 43	43	2	1011	-0.45	0.86	0
68	SLU 44	18	1	991	-0.04	-0.24	0.01
68	SLU 45	43	2	1011	-0.45	0.86	0
68	SLU 46	28	1	999	-0.21	0.2	0
68	SLU 47	18	1	991	-0.04	-0.24	0.01
68	SLU 48	43	2	1011	-0.45	0.86	0
68	SLU 49	28	1	999	-0.21	0.2	0
68	SLU 50	43	2	1011	-0.45	0.86	0
68	SLU 51	28	1	999	-0.21	0.2	0
68	SLU 52	13	2	1132	-0.28	-1.33	0.01
68	SLU 53	38	2	1152	-0.69	-0.22	0.01
68	SLU 54	23	2	1140	-0.44	-0.89	0.01
68	SLU 55	13	2	1132	-0.28	-1.33	0.01
68	SLU 56	38	2	1152	-0.69	-0.22	0.01
68	SLU 57	23	2	1140	-0.44	-0.89	0.01
68	SLU 58	38	2	1152	-0.69	-0.22	0.01
68	SLU 59	23	2	1140	-0.44	-0.89	0.01
68	SLU 60	36	3	1213	-0.79	-0.69	0.01
68	SLU 61	21	2	1201	-0.54	-1.35	0.01
68	SLU 62	36	3	1213	-0.79	-0.69	0.01
68	SLU 63	21	2	1201	-0.54	-1.35	0.01
68	SLU 64	45	2	1127	-0.58	0.54	0
68	SLU 65	19	1	1107	-0.17	-0.56	0.01
68	SLU 66	45	2	1127	-0.58	0.54	0
68	SLU 67	30	2	1115	-0.33	-0.12	0.01
68	SLU 68	19	1	1107	-0.17	-0.56	0.01
68	SLU 69	45	2	1127	-0.58	0.54	0
68	SLU 70	30	2	1115	-0.33	-0.12	0.01
68	SLU 71	45	2	1127	-0.58	0.54	0
68	SLU 72	30	2	1115	-0.33	-0.12	0.01
68	SLU 73	14	2	1248	-0.4	-1.65	0.01
68	SLU 74	39	3	1268	-0.82	-0.54	0.01
68	SLU 75	24	2	1256	-0.57	-1.21	0.01
68	SLU 76	14	2	1248	-0.4	-1.65	0.01
68	SLU 77	39	3	1268	-0.82	-0.54	0.01
68	SLU 78	24	2	1256	-0.57	-1.21	0.01
68	SLU 79	39	3	1268	-0.82	-0.54	0.01
68	SLU 80	24	2	1256	-0.57	-1.21	0.01
68	SLU 81	37	3	1328	-0.92	-1.01	0.01
68	SLU 82	22	3	1317	-0.67	-1.67	0.01
68	SLU 83	37	3	1328	-0.92	-1.01	0.01
68	SLU 84	22	3	1317	-0.67	-1.67	0.01
68	SLE RA 1	34	1	841	-0.42	0.49	0
68	SLE RA 2	17	1	828	-0.14	-0.25	0
68	SLE RA 3	34	1	841	-0.42	0.49	0
68	SLE RA 4	24	1	833	-0.25	0.05	0
68	SLE RA 5	17	1	828	-0.14	-0.25	0
68	SLE RA 6	34	1	841	-0.42	0.49	0
68	SLE RA 7	24	1	833	-0.25	0.05	0
68	SLE RA 8	34	1	841	-0.42	0.49	0
68	SLE RA 9	24	1	833	-0.25	0.05	0
68	SLE RA 10	14	2	922	-0.3	-0.97	0.01
68	SLE RA 11	31	2	935	-0.58	-0.24	0
68	SLE RA 12	20	2	927	-0.41	-0.68	0.01
68	SLE RA 13	14	2	922	-0.3	-0.97	0.01
68	SLE RA 14	31	2	935	-0.58	-0.24	0
68	SLE RA 15	20	2	927	-0.41	-0.68	0.01
68	SLE RA 16	31	2	935	-0.58	-0.24	0
68	SLE RA 17	20	2	927	-0.41	-0.68	0.01
68	SLE RA 18	29	2	976	-0.64	-0.55	0
68	SLE RA 19	19	2	968	-0.48	-0.99	0.01
68	SLE RA 20	29	2	976	-0.64	-0.55	0
68	SLE RA 21	19	2	968	-0.48	-0.99	0.01
68	SLE FR 1	34	1	841	-0.42	0.49	0
68	SLE FR 2	31	1	839	-0.36	0.34	0
68	SLE FR 3	34	1	841	-0.42	0.49	0
68	SLE FR 4	29	2	879	-0.43	0.03	0
68	SLE FR 5	33	2	882	-0.49	0.18	0
68	SLE FR 6	32	2	909	-0.53	-0.03	0
68	SLE QP 1	34	1	841	-0.42	0.49	0
68	SLE QP 2	33	2	882	-0.49	0.18	0
68	SLD 1	255	4	1075	-3.52	10.15	0
68	SLD 2	255	4	1075	-3.52	10.15	0
68	SLD 3	219	7	997	-2.23	8.53	-0.01
68	SLD 4	219	7	997	-2.23	8.53	-0.01
68	SLD 5	155	-1	1057	-3.35	5.63	0.01
68	SLD 6	155	-1	1057	-3.35	5.63	0.01
68	SLD 7	33	7	799	0.94	0.22	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
68	SLD 8	33	7	799	0.94	0.22	-0.01
68	SLD 9	32	-4	964	-1.92	0.13	0.02
68	SLD 10	32	-4	964	-1.92	0.13	0.02
68	SLD 11	-90	5	706	2.37	-5.28	0
68	SLD 12	-90	5	706	2.37	-5.28	0
68	SLD 13	-154	-3	766	1.26	-8.18	0.02
68	SLD 14	-154	-3	766	1.26	-8.18	0.02
68	SLD 15	-190	-1	688	2.54	-9.8	0.01
68	SLD 16	-190	-1	688	2.54	-9.8	0.01
68	SLV 1	558	10	1340	-9.4	23.71	-0.02
68	SLV 2	558	10	1340	-9.4	23.71	-0.02
68	SLV 3	473	16	1157	-6.14	19.93	-0.04
68	SLV 4	473	16	1157	-6.14	19.93	-0.04
68	SLV 5	319	-6	1295	-8.11	12.96	0.02
68	SLV 6	319	-6	1295	-8.11	12.96	0.02
68	SLV 7	36	16	688	2.76	0.38	-0.03
68	SLV 8	36	16	688	2.76	0.38	-0.03
68	SLV 9	29	-13	1075	-3.74	-0.03	0.04
68	SLV 10	29	-13	1075	-3.74	-0.03	0.04
68	SLV 11	-254	9	468	7.13	-12.6	-0.01
68	SLV 12	-254	9	468	7.13	-12.6	-0.01
68	SLV 13	-408	-13	606	5.16	-19.58	0.04
68	SLV 14	-408	-13	606	5.16	-19.58	0.04
68	SLV 15	-493	-6	424	8.42	-23.35	0.03
68	SLV 16	-493	-6	424	8.42	-23.35	0.03
69	SLU 1	2	281	1577	-9.29	0.14	0
69	SLU 2	-29	280	1550	-9.27	-1.31	0
69	SLU 3	2	281	1577	-9.29	0.14	0
69	SLU 4	-16	281	1561	-9.27	-0.73	0
69	SLU 5	-29	280	1550	-9.27	-1.31	0
69	SLU 6	2	281	1577	-9.29	0.14	0
69	SLU 7	-16	281	1561	-9.27	-0.73	0
69	SLU 8	2	281	1577	-9.29	0.14	0
69	SLU 9	-16	281	1561	-9.27	-0.73	0
69	SLU 10	-31	419	2009	-14.2	-1.53	0.01
69	SLU 11	0	420	2036	-14.22	-0.08	0
69	SLU 12	-18	419	2020	-14.21	-0.95	0.01
69	SLU 13	-31	419	2009	-14.2	-1.53	0.01
69	SLU 14	0	420	2036	-14.22	-0.08	0
69	SLU 15	-18	419	2020	-14.21	-0.95	0.01
69	SLU 16	0	420	2036	-14.22	-0.08	0
69	SLU 17	-18	419	2020	-14.21	-0.95	0.01
69	SLU 18	-1	479	2233	-16.33	-0.17	0.01
69	SLU 19	-19	479	2217	-16.32	-1.04	0.01
69	SLU 20	-1	479	2233	-16.33	-0.17	0.01
69	SLU 21	-19	479	2217	-16.32	-1.04	0.01
69	SLU 22	-2	361	1875	-12.13	-0.05	0
69	SLU 23	-32	360	1848	-12.11	-1.5	0
69	SLU 24	-2	361	1875	-12.13	-0.05	0
69	SLU 25	-20	361	1859	-12.12	-0.92	0
69	SLU 26	-32	360	1848	-12.11	-1.5	0
69	SLU 27	-2	361	1875	-12.13	-0.05	0
69	SLU 28	-20	361	1859	-12.12	-0.92	0
69	SLU 29	-2	361	1875	-12.13	-0.05	0
69	SLU 30	-20	361	1859	-12.12	-0.92	0
69	SLU 31	-35	499	2307	-17.04	-1.72	0.01
69	SLU 32	-4	500	2334	-17.06	-0.26	0.01
69	SLU 33	-22	500	2318	-17.05	-1.14	0.01
69	SLU 34	-35	499	2307	-17.04	-1.72	0.01
69	SLU 35	-4	500	2334	-17.06	-0.26	0.01
69	SLU 36	-22	500	2318	-17.05	-1.14	0.01
69	SLU 37	-4	500	2334	-17.06	-0.26	0.01
69	SLU 38	-22	500	2318	-17.05	-1.14	0.01
69	SLU 39	-5	560	2530	-19.17	-0.36	0.01
69	SLU 40	-23	559	2514	-19.16	-1.23	0.01
69	SLU 41	-5	560	2530	-19.17	-0.36	0.01
69	SLU 42	-23	559	2514	-19.16	-1.23	0.01
69	SLU 43	4	338	1949	-11.1	0.25	0
69	SLU 44	-26	337	1922	-11.08	-1.21	0
69	SLU 45	4	338	1949	-11.1	0.25	0
69	SLU 46	-14	337	1933	-11.09	-0.63	0
69	SLU 47	-26	337	1922	-11.08	-1.21	0
69	SLU 48	4	338	1949	-11.1	0.25	0
69	SLU 49	-14	337	1933	-11.09	-0.63	0
69	SLU 50	4	338	1949	-11.1	0.25	0
69	SLU 51	-14	337	1933	-11.09	-0.63	0
69	SLU 52	-29	476	2381	-16.01	-1.42	0.01
69	SLU 53	2	477	2407	-16.03	0.03	0
69	SLU 54	-16	476	2391	-16.02	-0.84	0.01
69	SLU 55	-29	476	2381	-16.01	-1.42	0.01
69	SLU 56	2	477	2407	-16.03	0.03	0
69	SLU 57	-16	476	2391	-16.02	-0.84	0.01
69	SLU 58	2	477	2407	-16.03	0.03	0
69	SLU 59	-16	476	2391	-16.02	-0.84	0.01
69	SLU 60	1	536	2604	-18.15	-0.06	0.01
69	SLU 61	-17	536	2588	-18.13	-0.93	0.01
69	SLU 62	1	536	2604	-18.15	-0.06	0.01
69	SLU 63	-17	536	2588	-18.13	-0.93	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
69	SLU 64	0	418	2246	-13.94	0.06	0
69	SLU 65	-30	417	2219	-13.92	-1.4	0.01
69	SLU 66	0	418	2246	-13.94	0.06	0
69	SLU 67	-18	418	2230	-13.93	-0.81	0
69	SLU 68	-30	417	2219	-13.92	-1.4	0.01
69	SLU 69	0	418	2246	-13.94	0.06	0
69	SLU 70	-18	418	2230	-13.93	-0.81	0
69	SLU 71	0	418	2246	-13.94	0.06	0
69	SLU 72	-18	418	2230	-13.93	-0.81	0
69	SLU 73	-33	556	2678	-18.85	-1.61	0.01
69	SLU 74	-2	557	2705	-18.87	-0.16	0.01
69	SLU 75	-20	556	2689	-18.86	-1.03	0.01
69	SLU 76	-33	556	2678	-18.85	-1.61	0.01
69	SLU 77	-2	557	2705	-18.87	-0.16	0.01
69	SLU 78	-20	556	2689	-18.86	-1.03	0.01
69	SLU 79	-2	557	2705	-18.87	-0.16	0.01
69	SLU 80	-20	556	2689	-18.86	-1.03	0.01
69	SLU 81	-3	617	2902	-20.99	-0.25	0.01
69	SLU 82	-21	616	2885	-20.97	-1.12	0.01
69	SLU 83	-3	617	2902	-20.99	-0.25	0.01
69	SLU 84	-21	616	2885	-20.97	-1.12	0.01
69	SLE RA 1	1	304	1662	-10.1	0.09	0
69	SLE RA 2	-19	303	1644	-10.08	-0.88	0
69	SLE RA 3	1	304	1662	-10.1	0.09	0
69	SLE RA 4	-11	304	1652	-10.09	-0.5	0
69	SLE RA 5	-19	303	1644	-10.08	-0.88	0
69	SLE RA 6	1	304	1662	-10.1	0.09	0
69	SLE RA 7	-11	304	1652	-10.09	-0.5	0
69	SLE RA 8	1	304	1662	-10.1	0.09	0
69	SLE RA 9	-11	304	1652	-10.09	-0.5	0
69	SLE RA 10	-21	396	1950	-13.37	-1.03	0.01
69	SLE RA 11	0	397	1968	-13.39	-0.06	0
69	SLE RA 12	-13	396	1958	-13.38	-0.64	0
69	SLE RA 13	-21	396	1950	-13.37	-1.03	0.01
69	SLE RA 14	0	397	1968	-13.39	-0.06	0
69	SLE RA 15	-13	396	1958	-13.38	-0.64	0
69	SLE RA 16	0	397	1968	-13.39	-0.06	0
69	SLE RA 17	-13	396	1958	-13.38	-0.64	0
69	SLE RA 18	-1	436	2099	-14.8	-0.12	0
69	SLE RA 19	-13	436	2089	-14.79	-0.7	0.01
69	SLE RA 20	-1	436	2099	-14.8	-0.12	0
69	SLE RA 21	-13	436	2089	-14.79	-0.7	0.01
69	SLE FR 1	1	304	1662	-10.1	0.09	0
69	SLE FR 2	-3	304	1659	-10.1	-0.11	0
69	SLE FR 3	1	304	1662	-10.1	0.09	0
69	SLE FR 4	-4	344	1790	-11.51	-0.17	0
69	SLE FR 5	0	344	1794	-11.51	0.03	0
69	SLE FR 6	0	370	1881	-12.45	-0.02	0
69	SLE QP 1	1	304	1662	-10.1	0.09	0
69	SLE QP 2	0	344	1794	-11.51	0.03	0
69	SLD 1	226	398	2089	-8.11	10.13	-0.01
69	SLD 2	226	398	2089	-8.11	10.13	-0.01
69	SLD 3	266	330	1909	-13.18	11.92	-0.01
69	SLD 4	266	330	1909	-13.18	11.92	-0.01
69	SLD 5	6	464	2155	-2.8	0.34	0
69	SLD 6	6	464	2155	-2.8	0.34	0
69	SLD 7	142	236	1556	-19.7	6.31	-0.01
69	SLD 8	142	236	1556	-19.7	6.31	-0.01
69	SLD 9	-141	451	2032	-3.31	-6.26	0.01
69	SLD 10	-141	451	2032	-3.31	-6.26	0.01
69	SLD 11	-5	224	1432	-20.22	-0.29	0
69	SLD 12	-5	224	1432	-20.22	-0.29	0
69	SLD 13	-265	358	1678	-9.83	-11.87	0.02
69	SLD 14	-265	358	1678	-9.83	-11.87	0.02
69	SLD 15	-225	289	1498	-14.9	-10.08	0.02
69	SLD 16	-225	289	1498	-14.9	-10.08	0.02
69	SLV 1	533	473	2494	-3.1	24.07	-0.03
69	SLV 2	533	473	2494	-3.1	24.07	-0.03
69	SLV 3	629	310	2070	-15.84	28.25	-0.04
69	SLV 4	629	310	2070	-15.84	28.25	-0.04
69	SLV 5	15	629	2646	10.34	0.9	0.01
69	SLV 6	15	629	2646	10.34	0.9	0.01
69	SLV 7	334	87	1234	-32.13	14.83	-0.02
69	SLV 8	334	87	1234	-32.13	14.83	-0.02
69	SLV 9	-333	601	2353	9.12	-14.78	0.03
69	SLV 10	-333	601	2353	9.12	-14.78	0.03
69	SLV 11	-14	58	941	-33.36	-0.85	0
69	SLV 12	-14	58	941	-33.36	-0.85	0
69	SLV 13	-628	377	1517	-7.18	-28.2	0.05
69	SLV 14	-628	377	1517	-7.18	-28.2	0.05
69	SLV 15	-532	215	1093	-19.92	-24.02	0.04
69	SLV 16	-532	215	1093	-19.92	-24.02	0.04
70	SLU 1	-18	1	1033	-0.32	-1.14	-0.01
70	SLU 2	-54	2	1009	-0.79	-2.63	0
70	SLU 3	-18	1	1033	-0.32	-1.14	-0.01
70	SLU 4	-40	2	1018	-0.6	-2.03	0
70	SLU 5	-54	2	1009	-0.79	-2.63	0
70	SLU 6	-18	1	1033	-0.32	-1.14	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
70	SLU 7	-40	2	1018	-0.6	-2.03	0
70	SLU 8	-18	1	1033	-0.32	-1.14	-0.01
70	SLU 9	-40	2	1018	-0.6	-2.03	0
70	SLU 10	-46	3	1347	-0.92	-3.09	-0.01
70	SLU 11	-11	2	1371	-0.46	-1.61	-0.01
70	SLU 12	-32	3	1356	-0.74	-2.5	-0.01
70	SLU 13	-46	3	1347	-0.92	-3.09	-0.01
70	SLU 14	-11	2	1371	-0.46	-1.61	-0.01
70	SLU 15	-32	3	1356	-0.74	-2.5	-0.01
70	SLU 16	-11	2	1371	-0.46	-1.61	-0.01
70	SLU 17	-32	3	1356	-0.74	-2.5	-0.01
70	SLU 18	-7	2	1516	-0.51	-1.81	-0.01
70	SLU 19	-29	3	1501	-0.79	-2.7	-0.01
70	SLU 20	-7	2	1516	-0.51	-1.81	-0.01
70	SLU 21	-29	3	1501	-0.79	-2.7	-0.01
70	SLU 22	-24	2	1227	-0.41	-1.65	-0.01
70	SLU 23	-60	3	1203	-0.88	-3.13	-0.01
70	SLU 24	-24	2	1227	-0.41	-1.65	-0.01
70	SLU 25	-46	2	1213	-0.69	-2.54	-0.01
70	SLU 26	-60	3	1203	-0.88	-3.13	-0.01
70	SLU 27	-24	2	1227	-0.41	-1.65	-0.01
70	SLU 28	-46	2	1213	-0.69	-2.54	-0.01
70	SLU 29	-24	2	1227	-0.41	-1.65	-0.01
70	SLU 30	-46	2	1213	-0.69	-2.54	-0.01
70	SLU 31	-52	3	1541	-1.01	-3.6	-0.01
70	SLU 32	-17	2	1565	-0.55	-2.11	-0.01
70	SLU 33	-38	3	1551	-0.82	-3	-0.01
70	SLU 34	-52	3	1541	-1.01	-3.6	-0.01
70	SLU 35	-17	2	1565	-0.55	-2.11	-0.01
70	SLU 36	-38	3	1551	-0.82	-3	-0.01
70	SLU 37	-17	2	1565	-0.55	-2.11	-0.01
70	SLU 38	-38	3	1551	-0.82	-3	-0.01
70	SLU 39	-13	3	1710	-0.6	-2.31	-0.01
70	SLU 40	-35	3	1696	-0.88	-3.2	-0.01
70	SLU 41	-13	3	1710	-0.6	-2.31	-0.01
70	SLU 42	-35	3	1696	-0.88	-3.2	-0.01
70	SLU 43	-22	2	1276	-0.39	-1.31	-0.01
70	SLU 44	-58	3	1252	-0.86	-2.79	0
70	SLU 45	-22	2	1276	-0.39	-1.31	-0.01
70	SLU 46	-43	2	1261	-0.67	-2.2	-0.01
70	SLU 47	-58	3	1252	-0.86	-2.79	0
70	SLU 48	-22	2	1276	-0.39	-1.31	-0.01
70	SLU 49	-43	2	1261	-0.67	-2.2	-0.01
70	SLU 50	-22	2	1276	-0.39	-1.31	-0.01
70	SLU 51	-43	2	1261	-0.67	-2.2	-0.01
70	SLU 52	-50	3	1590	-0.99	-3.26	-0.01
70	SLU 53	-14	2	1614	-0.52	-1.77	-0.01
70	SLU 54	-35	3	1599	-0.8	-2.67	-0.01
70	SLU 55	-50	3	1590	-0.99	-3.26	-0.01
70	SLU 56	-14	2	1614	-0.52	-1.77	-0.01
70	SLU 57	-35	3	1599	-0.8	-2.67	-0.01
70	SLU 58	-14	2	1614	-0.52	-1.77	-0.01
70	SLU 59	-35	3	1599	-0.8	-2.67	-0.01
70	SLU 60	-11	2	1759	-0.58	-1.97	-0.01
70	SLU 61	-32	3	1744	-0.86	-2.87	-0.01
70	SLU 62	-11	2	1759	-0.58	-1.97	-0.01
70	SLU 63	-32	3	1744	-0.86	-2.87	-0.01
70	SLU 64	-28	2	1471	-0.48	-1.82	-0.01
70	SLU 65	-64	3	1446	-0.94	-3.3	-0.01
70	SLU 66	-28	2	1471	-0.48	-1.82	-0.01
70	SLU 67	-49	3	1456	-0.76	-2.71	-0.01
70	SLU 68	-64	3	1446	-0.94	-3.3	-0.01
70	SLU 69	-28	2	1471	-0.48	-1.82	-0.01
70	SLU 70	-49	3	1456	-0.76	-2.71	-0.01
70	SLU 71	-28	2	1471	-0.48	-1.82	-0.01
70	SLU 72	-49	3	1456	-0.76	-2.71	-0.01
70	SLU 73	-56	4	1784	-1.08	-3.77	-0.01
70	SLU 74	-20	3	1808	-0.61	-2.28	-0.01
70	SLU 75	-41	3	1794	-0.89	-3.17	-0.01
70	SLU 76	-56	4	1784	-1.08	-3.77	-0.01
70	SLU 77	-20	3	1808	-0.61	-2.28	-0.01
70	SLU 78	-41	3	1794	-0.89	-3.17	-0.01
70	SLU 79	-20	3	1808	-0.61	-2.28	-0.01
70	SLU 80	-41	3	1794	-0.89	-3.17	-0.01
70	SLU 81	-17	3	1953	-0.67	-2.48	-0.01
70	SLU 82	-38	3	1939	-0.95	-3.37	-0.01
70	SLU 83	-17	3	1953	-0.67	-2.48	-0.01
70	SLU 84	-38	3	1939	-0.95	-3.37	-0.01
70	SLE RA 1	-20	1	1088	-0.35	-1.29	-0.01
70	SLE RA 2	-44	2	1072	-0.66	-2.28	0
70	SLE RA 3	-20	1	1088	-0.35	-1.29	-0.01
70	SLE RA 4	-34	2	1079	-0.53	-1.88	-0.01
70	SLE RA 5	-44	2	1072	-0.66	-2.28	0
70	SLE RA 6	-20	1	1088	-0.35	-1.29	-0.01
70	SLE RA 7	-34	2	1079	-0.53	-1.88	-0.01
70	SLE RA 8	-20	1	1088	-0.35	-1.29	-0.01
70	SLE RA 9	-34	2	1079	-0.53	-1.88	-0.01
70	SLE RA 10	-39	3	1298	-0.75	-2.59	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
70	SLE RA 11	-15	2	1314	-0.44	-1.6	-0.01
70	SLE RA 12	-29	2	1304	-0.62	-2.19	-0.01
70	SLE RA 13	-39	3	1298	-0.75	-2.59	-0.01
70	SLE RA 14	-15	2	1314	-0.44	-1.6	-0.01
70	SLE RA 15	-29	2	1304	-0.62	-2.19	-0.01
70	SLE RA 16	-15	2	1314	-0.44	-1.6	-0.01
70	SLE RA 17	-29	2	1304	-0.62	-2.19	-0.01
70	SLE RA 18	-13	2	1410	-0.48	-1.73	-0.01
70	SLE RA 19	-27	2	1401	-0.66	-2.32	-0.01
70	SLE RA 20	-13	2	1410	-0.48	-1.73	-0.01
70	SLE RA 21	-27	2	1401	-0.66	-2.32	-0.01
70	SLE FR 1	-20	1	1088	-0.35	-1.29	-0.01
70	SLE FR 2	-25	2	1085	-0.41	-1.48	-0.01
70	SLE FR 3	-20	1	1088	-0.35	-1.29	-0.01
70	SLE FR 4	-23	2	1182	-0.45	-1.62	-0.01
70	SLE FR 5	-18	2	1185	-0.39	-1.42	-0.01
70	SLE FR 6	-16	2	1249	-0.41	-1.51	-0.01
70	SLE QP 1	-20	1	1088	-0.35	-1.29	-0.01
70	SLE QP 2	-18	2	1185	-0.39	-1.42	-0.01
70	SLD 1	239	-6	1331	3.09	9.52	-0.01
70	SLD 2	239	-6	1331	3.09	9.52	-0.01
70	SLD 3	291	-3	1412	1.74	11.66	-0.01
70	SLD 4	291	-3	1412	1.74	11.66	-0.01
70	SLD 5	-20	-5	1106	2.69	-1.37	-0.01
70	SLD 6	-20	-5	1106	2.69	-1.37	-0.01
70	SLD 7	154	5	1376	-1.79	5.74	0
70	SLD 8	154	5	1376	-1.79	5.74	0
70	SLD 9	-190	-1	994	1.01	-8.58	-0.01
70	SLD 10	-190	-1	994	1.01	-8.58	-0.01
70	SLD 11	-16	8	1264	-3.47	-1.47	0
70	SLD 12	-16	8	1264	-3.47	-1.47	0
70	SLD 13	-327	6	958	-2.52	-14.49	0
70	SLD 14	-327	6	958	-2.52	-14.49	0
70	SLD 15	-275	9	1039	-3.86	-12.36	0
70	SLD 16	-275	9	1039	-3.86	-12.36	0
70	SLV 1	590	-22	1531	9.76	24.45	-0.03
70	SLV 2	590	-22	1531	9.76	24.45	-0.03
70	SLV 3	713	-14	1723	6.38	29.44	-0.02
70	SLV 4	713	-14	1723	6.38	29.44	-0.02
70	SLV 5	-21	-17	998	7.77	-1.24	-0.02
70	SLV 6	-21	-17	998	7.77	-1.24	-0.02
70	SLV 7	387	8	1637	-3.47	15.42	0
70	SLV 8	387	8	1637	-3.47	15.42	0
70	SLV 9	-423	-5	733	2.7	-18.26	-0.01
70	SLV 10	-423	-5	733	2.7	-18.26	-0.01
70	SLV 11	-14	20	1372	-8.55	-1.6	0.01
70	SLV 12	-14	20	1372	-8.55	-1.6	0.01
70	SLV 13	-748	17	647	-7.16	-32.28	0.01
70	SLV 14	-748	17	647	-7.16	-32.28	0.01
70	SLV 15	-626	25	839	-10.53	-27.28	0.02
70	SLV 16	-626	25	839	-10.53	-27.28	0.02
71	SLU 1	48	0	1084	-0.06	2.07	0
71	SLU 2	9	2	1054	-0.78	0.3	0
71	SLU 3	48	0	1084	-0.06	2.07	0
71	SLU 4	25	1	1066	-0.49	1.01	0
71	SLU 5	9	2	1054	-0.78	0.3	0
71	SLU 6	48	0	1084	-0.06	2.07	0
71	SLU 7	25	1	1066	-0.49	1.01	0
71	SLU 8	48	0	1084	-0.06	2.07	0
71	SLU 9	25	1	1066	-0.49	1.01	0
71	SLU 10	89	2	1505	-0.73	3.53	0
71	SLU 11	128	0	1535	-0.01	5.3	0
71	SLU 12	105	1	1517	-0.44	4.24	0
71	SLU 13	89	2	1505	-0.73	3.53	0
71	SLU 14	128	0	1535	-0.01	5.3	0
71	SLU 15	105	1	1517	-0.44	4.24	0
71	SLU 16	128	0	1535	-0.01	5.3	0
71	SLU 17	105	1	1517	-0.44	4.24	0
71	SLU 18	163	0	1728	0.01	6.69	0
71	SLU 19	139	1	1710	-0.42	5.63	0
71	SLU 20	163	0	1728	0.01	6.69	0
71	SLU 21	139	1	1710	-0.42	5.63	0
71	SLU 22	72	0	1312	-0.06	3.07	0
71	SLU 23	33	2	1282	-0.78	1.3	0
71	SLU 24	72	0	1312	-0.06	3.07	0
71	SLU 25	49	1	1294	-0.49	2.01	0
71	SLU 26	33	2	1282	-0.78	1.3	0
71	SLU 27	72	0	1312	-0.06	3.07	0
71	SLU 28	49	1	1294	-0.49	2.01	0
71	SLU 29	72	0	1312	-0.06	3.07	0
71	SLU 30	49	1	1294	-0.49	2.01	0
71	SLU 31	113	2	1733	-0.73	4.53	0
71	SLU 32	153	0	1763	-0.01	6.3	0
71	SLU 33	129	1	1745	-0.44	5.24	0
71	SLU 34	113	2	1733	-0.73	4.53	0
71	SLU 35	153	0	1763	-0.01	6.3	0
71	SLU 36	129	1	1745	-0.44	5.24	0
71	SLU 37	153	0	1763	-0.01	6.3	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
71	SLU 38	129	1	1745	-0.44	5.24	0
71	SLU 39	187	0	1956	0.01	7.68	0
71	SLU 40	163	1	1938	-0.42	6.62	0
71	SLU 41	187	0	1956	0.01	7.68	0
71	SLU 42	163	1	1938	-0.42	6.62	0
71	SLU 43	55	0	1331	-0.08	2.35	0
71	SLU 44	15	2	1302	-0.8	0.58	0
71	SLU 45	55	0	1331	-0.08	2.35	0
71	SLU 46	31	1	1313	-0.51	1.29	0
71	SLU 47	15	2	1302	-0.8	0.58	0
71	SLU 48	55	0	1331	-0.08	2.35	0
71	SLU 49	31	1	1313	-0.51	1.29	0
71	SLU 50	55	0	1331	-0.08	2.35	0
71	SLU 51	31	1	1313	-0.51	1.29	0
71	SLU 52	95	2	1752	-0.75	3.81	0
71	SLU 53	135	0	1782	-0.03	5.58	0
71	SLU 54	111	1	1764	-0.46	4.52	0
71	SLU 55	95	2	1752	-0.75	3.81	0
71	SLU 56	135	0	1782	-0.03	5.58	0
71	SLU 57	111	1	1764	-0.46	4.52	0
71	SLU 58	135	0	1782	-0.03	5.58	0
71	SLU 59	111	1	1764	-0.46	4.52	0
71	SLU 60	169	0	1975	-0.01	6.96	0
71	SLU 61	145	1	1957	-0.44	5.9	0
71	SLU 62	169	0	1975	-0.01	6.96	0
71	SLU 63	145	1	1957	-0.44	5.9	0
71	SLU 64	79	0	1559	-0.08	3.34	0
71	SLU 65	39	2	1530	-0.8	1.58	0
71	SLU 66	79	0	1559	-0.08	3.34	0
71	SLU 67	55	1	1541	-0.51	2.28	0
71	SLU 68	39	2	1530	-0.8	1.58	0
71	SLU 69	79	0	1559	-0.08	3.34	0
71	SLU 70	55	1	1541	-0.51	2.28	0
71	SLU 71	79	0	1559	-0.08	3.34	0
71	SLU 72	55	1	1541	-0.51	2.28	0
71	SLU 73	119	2	1980	-0.75	4.81	0
71	SLU 74	159	0	2010	-0.03	6.58	0
71	SLU 75	135	1	1992	-0.46	5.52	0
71	SLU 76	119	2	1980	-0.75	4.81	0
71	SLU 77	159	0	2010	-0.03	6.58	0
71	SLU 78	135	1	1992	-0.46	5.52	0
71	SLU 79	159	0	2010	-0.03	6.58	0
71	SLU 80	135	1	1992	-0.46	5.52	0
71	SLU 81	193	0	2203	-0.01	7.96	0
71	SLU 82	169	1	2185	-0.44	6.9	0
71	SLU 83	193	0	2203	-0.01	7.96	0
71	SLU 84	169	1	2185	-0.44	6.9	0
71	SLE RA 1	55	0	1149	-0.06	2.35	0
71	SLE RA 2	29	1	1129	-0.54	1.18	0
71	SLE RA 3	55	0	1149	-0.06	2.35	0
71	SLE RA 4	39	1	1137	-0.35	1.65	0
71	SLE RA 5	29	1	1129	-0.54	1.18	0
71	SLE RA 6	55	0	1149	-0.06	2.35	0
71	SLE RA 7	39	1	1137	-0.35	1.65	0
71	SLE RA 8	55	0	1149	-0.06	2.35	0
71	SLE RA 9	39	1	1137	-0.35	1.65	0
71	SLE RA 10	82	1	1430	-0.51	3.33	0
71	SLE RA 11	109	0	1450	-0.03	4.51	0
71	SLE RA 12	93	1	1438	-0.32	3.8	0
71	SLE RA 13	82	1	1430	-0.51	3.33	0
71	SLE RA 14	109	0	1450	-0.03	4.51	0
71	SLE RA 15	93	1	1438	-0.32	3.8	0
71	SLE RA 16	109	0	1450	-0.03	4.51	0
71	SLE RA 17	93	1	1438	-0.32	3.8	0
71	SLE RA 18	132	0	1578	-0.01	5.43	0
71	SLE RA 19	116	1	1566	-0.3	4.73	0
71	SLE RA 20	132	0	1578	-0.01	5.43	0
71	SLE RA 21	116	1	1566	-0.3	4.73	0
71	SLE FR 1	55	0	1149	-0.06	2.35	0
71	SLE FR 2	50	0	1145	-0.16	2.12	0
71	SLE FR 3	55	0	1149	-0.06	2.35	0
71	SLE FR 4	73	0	1274	-0.14	3.04	0
71	SLE FR 5	78	0	1278	-0.05	3.28	0
71	SLE FR 6	93	0	1364	-0.04	3.89	0
71	SLE QP 1	55	0	1149	-0.06	2.35	0
71	SLE QP 2	78	0	1278	-0.05	3.28	0
71	SLD 1	353	-11	1479	5.69	15.39	0.01
71	SLD 2	353	-11	1479	5.69	15.39	0.01
71	SLD 3	406	-7	1544	3.46	17.66	0.01
71	SLD 4	406	-7	1544	3.46	17.66	0.01
71	SLD 5	80	-10	1239	5.06	3.47	0.01
71	SLD 6	80	-10	1239	5.06	3.47	0.01
71	SLD 7	257	4	1457	-2.38	11.03	-0.01
71	SLD 8	257	4	1457	-2.38	11.03	-0.01
71	SLD 9	-100	-4	1099	2.28	-4.48	0.01
71	SLD 10	-100	-4	1099	2.28	-4.48	0.01
71	SLD 11	76	10	1317	-5.15	3.08	-0.01
71	SLD 12	76	10	1317	-5.15	3.08	-0.01





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
71	SLD 13	-249	7	1012	-3.56	-11.11	0
71	SLD 14	-249	7	1012	-3.56	-11.11	0
71	SLD 15	-197	11	1077	-5.79	-8.84	-0.01
71	SLD 16	-197	11	1077	-5.79	-8.84	-0.01
71	SLV 1	729	-33	1752	16.45	32.03	0.03
71	SLV 2	729	-33	1752	16.45	32.03	0.03
71	SLV 3	854	-22	1907	10.89	37.37	0.02
71	SLV 4	854	-22	1907	10.89	37.37	0.02
71	SLV 5	85	-26	1185	13.33	3.81	0.03
71	SLV 6	85	-26	1185	13.33	3.81	0.03
71	SLV 7	500	9	1702	-5.2	21.6	-0.01
71	SLV 8	500	9	1702	-5.2	21.6	-0.01
71	SLV 9	-343	-9	854	5.1	-15.05	0.02
71	SLV 10	-343	-9	854	5.1	-15.05	0.02
71	SLV 11	72	26	1371	-13.43	2.75	-0.03
71	SLV 12	72	26	1371	-13.43	2.75	-0.03
71	SLV 13	-697	22	649	-10.99	-30.82	-0.02
71	SLV 14	-697	22	649	-10.99	-30.82	-0.02
71	SLV 15	-573	33	803	-16.55	-25.48	-0.03
71	SLV 16	-573	33	803	-16.55	-25.48	-0.03
72	SLU 1	97	0	1235	0.1	2.69	0
72	SLU 2	57	1	1199	-0.63	1	0
72	SLU 3	97	0	1235	0.1	2.69	0
72	SLU 4	73	1	1214	-0.34	1.68	0
72	SLU 5	57	1	1199	-0.63	1	0
72	SLU 6	97	0	1235	0.1	2.69	0
72	SLU 7	73	1	1214	-0.34	1.68	0
72	SLU 8	97	0	1235	0.1	2.69	0
72	SLU 9	73	1	1214	-0.34	1.68	0
72	SLU 10	191	1	1845	-0.45	5.03	0
72	SLU 11	231	0	1881	0.28	6.72	0
72	SLU 12	207	0	1860	-0.16	5.71	0
72	SLU 13	191	1	1845	-0.45	5.03	0
72	SLU 14	231	0	1881	0.28	6.72	0
72	SLU 15	207	0	1860	-0.16	5.71	0
72	SLU 16	231	0	1881	0.28	6.72	0
72	SLU 17	207	0	1860	-0.16	5.71	0
72	SLU 18	289	0	2158	0.36	8.45	0
72	SLU 19	265	0	2137	-0.08	7.43	0
72	SLU 20	289	0	2158	0.36	8.45	0
72	SLU 21	265	0	2137	-0.08	7.43	0
72	SLU 22	144	0	1535	0.16	4.01	0
72	SLU 23	104	1	1499	-0.57	2.33	0
72	SLU 24	144	0	1535	0.16	4.01	0
72	SLU 25	120	1	1513	-0.28	3	0
72	SLU 26	104	1	1499	-0.57	2.33	0
72	SLU 27	144	0	1535	0.16	4.01	0
72	SLU 28	120	1	1513	-0.28	3	0
72	SLU 29	144	0	1535	0.16	4.01	0
72	SLU 30	120	1	1513	-0.28	3	0
72	SLU 31	238	1	2145	-0.39	6.35	0
72	SLU 32	278	0	2181	0.34	8.04	0
72	SLU 33	254	0	2160	-0.09	7.03	0
72	SLU 34	238	1	2145	-0.39	6.35	0
72	SLU 35	278	0	2181	0.34	8.04	0
72	SLU 36	254	0	2160	-0.09	7.03	0
72	SLU 37	278	0	2181	0.34	8.04	0
72	SLU 38	254	0	2160	-0.09	7.03	0
72	SLU 39	336	0	2458	0.42	9.77	0
72	SLU 40	312	0	2436	-0.01	8.76	0
72	SLU 41	336	0	2458	0.42	9.77	0
72	SLU 42	312	0	2436	-0.01	8.76	0
72	SLU 43	110	0	1503	0.1	3.05	0
72	SLU 44	70	1	1467	-0.63	1.36	0
72	SLU 45	110	0	1503	0.1	3.05	0
72	SLU 46	86	1	1482	-0.33	2.03	0
72	SLU 47	70	1	1467	-0.63	1.36	0
72	SLU 48	110	0	1503	0.1	3.05	0
72	SLU 49	86	1	1482	-0.33	2.03	0
72	SLU 50	110	0	1503	0.1	3.05	0
72	SLU 51	86	1	1482	-0.33	2.03	0
72	SLU 52	205	1	2113	-0.44	5.39	0
72	SLU 53	244	0	2149	0.29	7.07	0
72	SLU 54	221	0	2128	-0.15	6.06	0
72	SLU 55	205	1	2113	-0.44	5.39	0
72	SLU 56	244	0	2149	0.29	7.07	0
72	SLU 57	221	0	2128	-0.15	6.06	0
72	SLU 58	244	0	2149	0.29	7.07	0
72	SLU 59	221	0	2128	-0.15	6.06	0
72	SLU 60	302	0	2426	0.37	8.8	0
72	SLU 61	278	0	2404	-0.07	7.79	0
72	SLU 62	302	0	2426	0.37	8.8	0
72	SLU 63	278	0	2404	-0.07	7.79	0
72	SLU 64	157	0	1803	0.17	4.37	0
72	SLU 65	117	1	1767	-0.56	2.68	0
72	SLU 66	157	0	1803	0.17	4.37	0
72	SLU 67	133	1	1781	-0.27	3.36	0
72	SLU 68	117	1	1767	-0.56	2.68	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
72	SLU 69	157	0	1803	0.17	4.37	0
72	SLU 70	133	1	1781	-0.27	3.36	0
72	SLU 71	157	0	1803	0.17	4.37	0
72	SLU 72	133	1	1781	-0.27	3.36	0
72	SLU 73	251	1	2413	-0.38	6.71	0
72	SLU 74	291	0	2449	0.35	8.4	0
72	SLU 75	267	0	2427	-0.09	7.38	0
72	SLU 76	251	1	2413	-0.38	6.71	0
72	SLU 77	291	0	2449	0.35	8.4	0
72	SLU 78	267	0	2427	-0.09	7.38	0
72	SLU 79	291	0	2449	0.35	8.4	0
72	SLU 80	267	0	2427	-0.09	7.38	0
72	SLU 81	349	0	2726	0.43	10.12	0
72	SLU 82	325	0	2704	-0.01	9.11	0
72	SLU 83	349	0	2726	0.43	10.12	0
72	SLU 84	325	0	2704	-0.01	9.11	0
72	SLE RA 1	110	0	1321	0.11	3.07	0
72	SLE RA 2	84	1	1297	-0.37	1.95	0
72	SLE RA 3	110	0	1321	0.11	3.07	0
72	SLE RA 4	94	0	1307	-0.18	2.4	0
72	SLE RA 5	84	1	1297	-0.37	1.95	0
72	SLE RA 6	110	0	1321	0.11	3.07	0
72	SLE RA 7	94	0	1307	-0.18	2.4	0
72	SLE RA 8	110	0	1321	0.11	3.07	0
72	SLE RA 9	94	0	1307	-0.18	2.4	0
72	SLE RA 10	173	1	1728	-0.25	4.63	0
72	SLE RA 11	200	0	1752	0.24	5.76	0
72	SLE RA 12	184	0	1737	-0.05	5.08	0
72	SLE RA 13	173	1	1728	-0.25	4.63	0
72	SLE RA 14	200	0	1752	0.24	5.76	0
72	SLE RA 15	184	0	1737	-0.05	5.08	0
72	SLE RA 16	200	0	1752	0.24	5.76	0
72	SLE RA 17	184	0	1737	-0.05	5.08	0
72	SLE RA 18	238	0	1936	0.29	6.91	0
72	SLE RA 19	222	0	1922	0	6.23	0
72	SLE RA 20	238	0	1936	0.29	6.91	0
72	SLE RA 21	222	0	1922	0	6.23	0
72	SLE FR 1	110	0	1321	0.11	3.07	0
72	SLE FR 2	105	0	1316	0.02	2.85	0
72	SLE FR 3	110	0	1321	0.11	3.07	0
72	SLE FR 4	143	0	1501	0.07	4	0
72	SLE FR 5	149	0	1506	0.17	4.22	0
72	SLE FR 6	174	0	1629	0.2	4.99	0
72	SLE QP 1	110	0	1321	0.11	3.07	0
72	SLE QP 2	149	0	1506	0.17	4.22	0
72	SLD 1	426	-11	1753	6.86	16.25	0.01
72	SLD 2	426	-11	1753	6.86	16.25	0.01
72	SLD 3	479	-7	1832	4.3	18.49	0.01
72	SLD 4	479	-7	1832	4.3	18.49	0.01
72	SLD 5	152	-10	1460	6.06	4.44	0.01
72	SLD 6	152	-10	1460	6.06	4.44	0.01
72	SLD 7	328	4	1723	-2.48	11.89	0
72	SLD 8	328	4	1723	-2.48	11.89	0
72	SLD 9	-30	-5	1288	2.82	-3.45	0
72	SLD 10	-30	-5	1288	2.82	-3.45	0
72	SLD 11	145	10	1551	-5.73	4	-0.01
72	SLD 12	145	10	1551	-5.73	4	-0.01
72	SLD 13	-181	7	1180	-3.97	-10.04	-0.01
72	SLD 14	-181	7	1180	-3.97	-10.04	-0.01
72	SLD 15	-129	11	1259	-6.53	-7.81	-0.01
72	SLD 16	-129	11	1259	-6.53	-7.81	-0.01
72	SLV 1	806	-32	2087	18.92	32.67	0.03
72	SLV 2	806	-32	2087	18.92	32.67	0.03
72	SLV 3	930	-21	2275	12.59	37.94	0.02
72	SLV 4	930	-21	2275	12.59	37.94	0.02
72	SLV 5	157	-26	1395	15.41	4.76	0.02
72	SLV 6	157	-26	1395	15.41	4.76	0.02
72	SLV 7	572	10	2022	-5.72	22.33	-0.01
72	SLV 8	572	10	2022	-5.72	22.33	-0.01
72	SLV 9	-274	-10	990	6.05	-13.89	0.01
72	SLV 10	-274	-10	990	6.05	-13.89	0.01
72	SLV 11	141	25	1616	-15.07	3.68	-0.02
72	SLV 12	141	25	1616	-15.07	3.68	-0.02
72	SLV 13	-632	21	736	-12.25	-29.5	-0.02
72	SLV 14	-632	21	736	-12.25	-29.5	-0.02
72	SLV 15	-508	32	924	-18.59	-24.23	-0.03
72	SLV 16	-508	32	924	-18.59	-24.23	-0.03
73	SLU 1	159	0	1469	0.23	6.31	0
73	SLU 2	118	1	1426	-0.37	4.46	0
73	SLU 3	159	0	1469	0.23	6.31	0
73	SLU 4	134	0	1443	-0.13	5.2	0
73	SLU 5	118	1	1426	-0.37	4.46	0
73	SLU 6	159	0	1469	0.23	6.31	0
73	SLU 7	134	0	1443	-0.13	5.2	0
73	SLU 8	159	0	1469	0.23	6.31	0
73	SLU 9	134	0	1443	-0.13	5.2	0
73	SLU 10	323	0	2349	-0.06	12.68	0
73	SLU 11	363	-1	2391	0.54	14.52	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
73	SLU 12	339	0	2366	0.18	13.41	0
73	SLU 13	323	0	2349	-0.06	12.68	0
73	SLU 14	363	-1	2391	0.54	14.52	0
73	SLU 15	339	0	2366	0.18	13.41	0
73	SLU 16	363	-1	2391	0.54	14.52	0
73	SLU 17	339	0	2366	0.18	13.41	0
73	SLU 18	451	-1	2787	0.67	18.04	0
73	SLU 19	427	0	2761	0.31	16.93	0
73	SLU 20	451	-1	2787	0.67	18.04	0
73	SLU 21	427	0	2761	0.31	16.93	0
73	SLU 22	235	0	1875	0.34	9.36	0
73	SLU 23	194	0	1832	-0.26	7.51	0
73	SLU 24	235	0	1875	0.34	9.36	0
73	SLU 25	210	0	1849	-0.02	8.25	0
73	SLU 26	194	0	1832	-0.26	7.51	0
73	SLU 27	235	0	1875	0.34	9.36	0
73	SLU 28	210	0	1849	-0.02	8.25	0
73	SLU 29	235	0	1875	0.34	9.36	0
73	SLU 30	210	0	1849	-0.02	8.25	0
73	SLU 31	399	0	2755	0.05	15.72	0
73	SLU 32	439	-1	2798	0.65	17.57	0
73	SLU 33	415	0	2772	0.29	16.46	0
73	SLU 34	399	0	2755	0.05	15.72	0
73	SLU 35	439	-1	2798	0.65	17.57	0
73	SLU 36	415	0	2772	0.29	16.46	0
73	SLU 37	439	-1	2798	0.65	17.57	0
73	SLU 38	415	0	2772	0.29	16.46	0
73	SLU 39	527	-1	3193	0.78	21.09	0
73	SLU 40	503	0	3167	0.42	19.98	0
73	SLU 41	527	-1	3193	0.78	21.09	0
73	SLU 42	503	0	3167	0.42	19.98	0
73	SLU 43	180	0	1770	0.25	7.16	0
73	SLU 44	140	1	1727	-0.34	5.31	0
73	SLU 45	180	0	1770	0.25	7.16	0
73	SLU 46	156	0	1744	-0.1	6.05	0
73	SLU 47	140	1	1727	-0.34	5.31	0
73	SLU 48	180	0	1770	0.25	7.16	0
73	SLU 49	156	0	1744	-0.1	6.05	0
73	SLU 50	180	0	1770	0.25	7.16	0
73	SLU 51	156	0	1744	-0.1	6.05	0
73	SLU 52	344	0	2650	-0.03	13.52	0
73	SLU 53	385	-1	2693	0.56	15.37	0
73	SLU 54	361	0	2667	0.21	14.26	0
73	SLU 55	344	0	2650	-0.03	13.52	0
73	SLU 56	385	-1	2693	0.56	15.37	0
73	SLU 57	361	0	2667	0.21	14.26	0
73	SLU 58	385	-1	2693	0.56	15.37	0
73	SLU 59	361	0	2667	0.21	14.26	0
73	SLU 60	472	-1	3088	0.7	18.89	0
73	SLU 61	448	0	3063	0.34	17.78	0
73	SLU 62	472	-1	3088	0.7	18.89	0
73	SLU 63	448	0	3063	0.34	17.78	0
73	SLU 64	256	0	2176	0.37	10.21	0
73	SLU 65	216	0	2134	-0.23	8.36	0
73	SLU 66	256	0	2176	0.37	10.21	0
73	SLU 67	232	0	2151	0.01	9.1	0
73	SLU 68	216	0	2134	-0.23	8.36	0
73	SLU 69	256	0	2176	0.37	10.21	0
73	SLU 70	232	0	2151	0.01	9.1	0
73	SLU 71	256	0	2176	0.37	10.21	0
73	SLU 72	232	0	2151	0.01	9.1	0
73	SLU 73	420	0	3056	0.08	16.57	0
73	SLU 74	461	-1	3099	0.68	18.42	0
73	SLU 75	437	0	3073	0.32	17.31	0
73	SLU 76	420	0	3056	0.08	16.57	0
73	SLU 77	461	-1	3099	0.68	18.42	0
73	SLU 78	437	0	3073	0.32	17.31	0
73	SLU 79	461	-1	3099	0.68	18.42	0
73	SLU 80	437	0	3073	0.32	17.31	0
73	SLU 81	549	-1	3494	0.81	21.94	0
73	SLU 82	524	-1	3469	0.45	20.83	0
73	SLU 83	549	-1	3494	0.81	21.94	0
73	SLU 84	524	-1	3469	0.45	20.83	0
73	SLE RA 1	180	0	1585	0.26	7.18	0
73	SLE RA 2	153	0	1556	-0.14	5.95	0
73	SLE RA 3	180	0	1585	0.26	7.18	0
73	SLE RA 4	164	0	1568	0.02	6.44	0
73	SLE RA 5	153	0	1556	-0.14	5.95	0
73	SLE RA 6	180	0	1585	0.26	7.18	0
73	SLE RA 7	164	0	1568	0.02	6.44	0
73	SLE RA 8	180	0	1585	0.26	7.18	0
73	SLE RA 9	164	0	1568	0.02	6.44	0
73	SLE RA 10	290	0	2171	0.07	11.42	0
73	SLE RA 11	317	-1	2200	0.46	12.66	0
73	SLE RA 12	301	0	2183	0.23	11.92	0
73	SLE RA 13	290	0	2171	0.07	11.42	0
73	SLE RA 14	317	-1	2200	0.46	12.66	0
73	SLE RA 15	301	0	2183	0.23	11.92	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
73	SLE RA 16	317	-1	2200	0.46	12.66	0
73	SLE RA 17	301	0	2183	0.23	11.92	0
73	SLE RA 18	375	-1	2464	0.55	15	0
73	SLE RA 19	359	0	2446	0.31	14.26	0
73	SLE RA 20	375	-1	2464	0.55	15	0
73	SLE RA 21	359	0	2446	0.31	14.26	0
73	SLE FR 1	180	0	1585	0.26	7.18	0
73	SLE FR 2	175	0	1579	0.18	6.93	0
73	SLE FR 3	180	0	1585	0.26	7.18	0
73	SLE FR 4	233	0	1843	0.27	9.28	0
73	SLE FR 5	239	0	1848	0.35	9.53	0
73	SLE FR 6	278	-1	2024	0.41	11.09	0
73	SLE QP 1	180	0	1585	0.26	7.18	0
73	SLE QP 2	239	0	1848	0.35	9.53	0
73	SLD 1	513	-11	2133	7	22.01	0.01
73	SLD 2	513	-11	2133	7	22.01	0.01
73	SLD 3	567	-8	2245	4.62	24.4	0
73	SLD 4	567	-8	2245	4.62	24.4	0
73	SLD 5	239	-9	1764	5.95	9.66	0.01
73	SLD 6	239	-9	1764	5.95	9.66	0.01
73	SLD 7	419	3	2138	-1.98	17.6	0
73	SLD 8	419	3	2138	-1.98	17.6	0
73	SLD 9	58	-4	1559	2.67	1.45	0.01
73	SLD 10	58	-4	1559	2.67	1.45	0.01
73	SLD 11	239	8	1933	-5.26	9.4	-0.01
73	SLD 12	239	8	1933	-5.26	9.4	-0.01
73	SLD 13	-89	7	1452	-3.93	-5.34	0
73	SLD 14	-89	7	1452	-3.93	-5.34	0
73	SLD 15	-35	10	1564	-6.31	-2.96	-0.01
73	SLD 16	-35	10	1564	-6.31	-2.96	-0.01
73	SLV 1	888	-30	2517	18.45	39.13	0.03
73	SLV 2	888	-30	2517	18.45	39.13	0.03
73	SLV 3	1016	-21	2783	12.6	44.78	0.02
73	SLV 4	1016	-21	2783	12.6	44.78	0.02
73	SLV 5	238	-23	1646	14.64	9.84	0.02
73	SLV 6	238	-23	1646	14.64	9.84	0.02
73	SLV 7	667	7	2532	-4.84	28.68	-0.01
73	SLV 8	667	7	2532	-4.84	28.68	-0.01
73	SLV 9	-190	-8	1164	5.53	-9.62	0.01
73	SLV 10	-190	-8	1164	5.53	-9.62	0.01
73	SLV 11	239	22	2051	-13.95	9.22	-0.02
73	SLV 12	239	22	2051	-13.95	9.22	-0.02
73	SLV 13	-539	20	913	-11.91	-25.73	-0.01
73	SLV 14	-539	20	913	-11.91	-25.73	-0.01
73	SLV 15	-410	29	1179	-17.75	-20.08	-0.03
73	SLV 16	-410	29	1179	-17.75	-20.08	-0.03
74	SLU 1	171	0	1780	0.35	4.94	0
74	SLU 2	134	0	1732	-0.06	3.34	0
74	SLU 3	171	0	1780	0.35	4.94	0
74	SLU 4	149	0	1751	0.11	3.98	0
74	SLU 5	134	0	1732	-0.06	3.34	0
74	SLU 6	171	0	1780	0.35	4.94	0
74	SLU 7	149	0	1751	0.11	3.98	0
74	SLU 8	171	0	1780	0.35	4.94	0
74	SLU 9	149	0	1751	0.11	3.98	0
74	SLU 10	358	-1	3010	0.37	10.31	0
74	SLU 11	395	-1	3058	0.78	11.9	0
74	SLU 12	372	-1	3029	0.54	10.95	0
74	SLU 13	358	-1	3010	0.37	10.31	0
74	SLU 14	395	-1	3058	0.78	11.9	0
74	SLU 15	372	-1	3029	0.54	10.95	0
74	SLU 16	395	-1	3058	0.78	11.9	0
74	SLU 17	372	-1	3029	0.54	10.95	0
74	SLU 18	490	-1	3606	0.97	14.89	0
74	SLU 19	468	-1	3577	0.72	13.93	0
74	SLU 20	490	-1	3606	0.97	14.89	0
74	SLU 21	468	-1	3577	0.72	13.93	0
74	SLU 22	255	-1	2325	0.52	7.49	0
74	SLU 23	218	0	2277	0.11	5.9	0
74	SLU 24	255	-1	2325	0.52	7.49	0
74	SLU 25	233	0	2296	0.27	6.54	0
74	SLU 26	218	0	2277	0.11	5.9	0
74	SLU 27	255	-1	2325	0.52	7.49	0
74	SLU 28	233	0	2296	0.27	6.54	0
74	SLU 29	255	-1	2325	0.52	7.49	0
74	SLU 30	233	0	2296	0.27	6.54	0
74	SLU 31	442	-1	3555	0.54	12.87	0
74	SLU 32	479	-1	3604	0.95	14.46	0
74	SLU 33	457	-1	3575	0.7	13.5	0
74	SLU 34	442	-1	3555	0.54	12.87	0
74	SLU 35	479	-1	3604	0.95	14.46	0
74	SLU 36	457	-1	3575	0.7	13.5	0
74	SLU 37	479	-1	3604	0.95	14.46	0
74	SLU 38	457	-1	3575	0.7	13.5	0
74	SLU 39	574	-2	4151	1.13	17.45	0
74	SLU 40	552	-1	4123	0.89	16.49	0
74	SLU 41	574	-2	4151	1.13	17.45	0
74	SLU 42	552	-1	4123	0.89	16.49	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
74	SLU 43	194	-1	2127	0.4	5.54	0
74	SLU 44	157	0	2078	-0.01	3.95	0
74	SLU 45	194	-1	2127	0.4	5.54	0
74	SLU 46	172	0	2098	0.16	4.59	0
74	SLU 47	157	0	2078	-0.01	3.95	0
74	SLU 48	194	-1	2127	0.4	5.54	0
74	SLU 49	172	0	2098	0.16	4.59	0
74	SLU 50	194	-1	2127	0.4	5.54	0
74	SLU 51	172	0	2098	0.16	4.59	0
74	SLU 52	380	-1	3357	0.42	10.91	0
74	SLU 53	417	-1	3405	0.83	12.51	0
74	SLU 54	395	-1	3376	0.59	11.55	0
74	SLU 55	380	-1	3357	0.42	10.91	0
74	SLU 56	417	-1	3405	0.83	12.51	0
74	SLU 57	395	-1	3376	0.59	11.55	0
74	SLU 58	417	-1	3405	0.83	12.51	0
74	SLU 59	395	-1	3376	0.59	11.55	0
74	SLU 60	513	-1	3953	1.02	15.49	0
74	SLU 61	491	-1	3924	0.77	14.54	0
74	SLU 62	513	-1	3953	1.02	15.49	0
74	SLU 63	491	-1	3924	0.77	14.54	0
74	SLU 64	278	-1	2672	0.56	8.1	0
74	SLU 65	241	0	2624	0.16	6.51	0
74	SLU 66	278	-1	2672	0.56	8.1	0
74	SLU 67	256	0	2643	0.32	7.14	0
74	SLU 68	241	0	2624	0.16	6.51	0
74	SLU 69	278	-1	2672	0.56	8.1	0
74	SLU 70	256	0	2643	0.32	7.14	0
74	SLU 71	278	-1	2672	0.56	8.1	0
74	SLU 72	256	0	2643	0.32	7.14	0
74	SLU 73	464	-1	3902	0.59	13.47	0
74	SLU 74	501	-1	3950	1	15.07	0
74	SLU 75	479	-1	3922	0.75	14.11	0
74	SLU 76	464	-1	3902	0.59	13.47	0
74	SLU 77	501	-1	3950	1	15.07	0
74	SLU 78	479	-1	3922	0.75	14.11	0
74	SLU 79	501	-1	3950	1	15.07	0
74	SLU 80	479	-1	3922	0.75	14.11	0
74	SLU 81	597	-2	4498	1.18	18.05	0
74	SLU 82	575	-1	4469	0.94	17.09	0
74	SLU 83	597	-2	4498	1.18	18.05	0
74	SLU 84	575	-1	4469	0.94	17.09	0
74	SLE RA 1	195	-1	1936	0.4	5.67	0
74	SLE RA 2	171	0	1904	0.13	4.61	0
74	SLE RA 3	195	-1	1936	0.4	5.67	0
74	SLE RA 4	181	0	1916	0.24	5.03	0
74	SLE RA 5	171	0	1904	0.13	4.61	0
74	SLE RA 6	195	-1	1936	0.4	5.67	0
74	SLE RA 7	181	0	1916	0.24	5.03	0
74	SLE RA 8	195	-1	1936	0.4	5.67	0
74	SLE RA 9	181	0	1916	0.24	5.03	0
74	SLE RA 10	320	-1	2756	0.41	9.25	0
74	SLE RA 11	344	-1	2788	0.69	10.31	0
74	SLE RA 12	329	-1	2769	0.52	9.67	0
74	SLE RA 13	320	-1	2756	0.41	9.25	0
74	SLE RA 14	344	-1	2788	0.69	10.31	0
74	SLE RA 15	329	-1	2769	0.52	9.67	0
74	SLE RA 16	344	-1	2788	0.69	10.31	0
74	SLE RA 17	329	-1	2769	0.52	9.67	0
74	SLE RA 18	408	-1	3153	0.81	12.3	0
74	SLE RA 19	393	-1	3134	0.65	11.66	0
74	SLE RA 20	408	-1	3153	0.81	12.3	0
74	SLE RA 21	393	-1	3134	0.65	11.66	0
74	SLE FR 1	195	-1	1936	0.4	5.67	0
74	SLE FR 2	190	0	1929	0.34	5.46	0
74	SLE FR 3	195	-1	1936	0.4	5.67	0
74	SLE FR 4	254	-1	2294	0.47	7.45	0
74	SLE FR 5	259	-1	2301	0.52	7.66	0
74	SLE FR 6	302	-1	2544	0.6	8.99	0
74	SLE QP 1	195	-1	1936	0.4	5.67	0
74	SLE QP 2	259	-1	2301	0.52	7.66	0
74	SLD 1	510	-12	2610	6.27	18.89	0.01
74	SLD 2	510	-12	2610	6.27	18.89	0.01
74	SLD 3	563	-9	2773	4.45	21.03	0
74	SLD 4	563	-9	2773	4.45	21.03	0
74	SLD 5	254	-8	2147	5	7.79	0.01
74	SLD 6	254	-8	2147	5	7.79	0.01
74	SLD 7	430	1	2689	-1.05	14.91	0
74	SLD 8	430	1	2689	-1.05	14.91	0
74	SLD 9	88	-2	1913	2.09	0.41	0.01
74	SLD 10	88	-2	1913	2.09	0.41	0.01
74	SLD 11	264	7	2455	-3.95	7.53	-0.01
74	SLD 12	264	7	2455	-3.95	7.53	-0.01
74	SLD 13	-44	8	1829	-3.41	-5.71	0
74	SLD 14	-44	8	1829	-3.41	-5.71	0
74	SLD 15	8	10	1991	-5.22	-3.57	0
74	SLD 16	8	10	1991	-5.22	-3.57	0
74	SLV 1	852	-29	3028	15.76	34.21	0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
74	SLV 2	852	-29	3028	15.76	34.21	0.02
74	SLV 3	978	-22	3412	11.32	39.28	0.01
74	SLV 4	978	-22	3412	11.32	39.28	0.01
74	SLV 5	246	-19	1937	11.84	7.93	0.02
74	SLV 6	246	-19	1937	11.84	7.93	0.02
74	SLV 7	665	3	3217	-2.98	24.84	-0.01
74	SLV 8	665	3	3217	-2.98	24.84	-0.01
74	SLV 9	-147	-4	1385	4.02	-9.52	0.01
74	SLV 10	-147	-4	1385	4.02	-9.52	0.01
74	SLV 11	272	18	2665	-10.79	7.39	-0.02
74	SLV 12	272	18	2665	-10.79	7.39	-0.02
74	SLV 13	-459	21	1190	-10.28	-23.96	-0.01
74	SLV 14	-459	21	1190	-10.28	-23.96	-0.01
74	SLV 15	-334	28	1574	-14.72	-18.89	-0.02
74	SLV 16	-334	28	1574	-14.72	-18.89	-0.02
75	SLU 1	168	-1	2197	0.55	5.92	0
75	SLU 2	134	-1	2144	0.33	4.32	0
75	SLU 3	168	-1	2197	0.55	5.92	0
75	SLU 4	147	-1	2165	0.42	4.96	0
75	SLU 5	134	-1	2144	0.33	4.32	0
75	SLU 6	168	-1	2197	0.55	5.92	0
75	SLU 7	147	-1	2165	0.42	4.96	0
75	SLU 8	168	-1	2197	0.55	5.92	0
75	SLU 9	147	-1	2165	0.42	4.96	0
75	SLU 10	370	-2	3897	0.95	12.98	0
75	SLU 11	404	-3	3951	1.17	14.57	0
75	SLU 12	383	-3	3919	1.04	13.62	0
75	SLU 13	370	-2	3897	0.95	12.98	0
75	SLU 14	404	-3	3951	1.17	14.57	0
75	SLU 15	383	-3	3919	1.04	13.62	0
75	SLU 16	404	-3	3951	1.17	14.57	0
75	SLU 17	383	-3	3919	1.04	13.62	0
75	SLU 18	505	-3	4702	1.43	18.28	-0.01
75	SLU 19	484	-3	4670	1.3	17.33	-0.01
75	SLU 20	505	-3	4702	1.43	18.28	-0.01
75	SLU 21	484	-3	4670	1.3	17.33	-0.01
75	SLU 22	257	-2	2931	0.79	9.17	0
75	SLU 23	223	-2	2877	0.57	7.57	0
75	SLU 24	257	-2	2931	0.79	9.17	0
75	SLU 25	237	-2	2899	0.66	8.21	0
75	SLU 26	223	-2	2877	0.57	7.57	0
75	SLU 27	257	-2	2931	0.79	9.17	0
75	SLU 28	237	-2	2899	0.66	8.21	0
75	SLU 29	257	-2	2931	0.79	9.17	0
75	SLU 30	237	-2	2899	0.66	8.21	0
75	SLU 31	459	-3	4631	1.19	16.23	-0.01
75	SLU 32	493	-3	4684	1.41	17.82	-0.01
75	SLU 33	473	-3	4652	1.28	16.87	-0.01
75	SLU 34	459	-3	4631	1.19	16.23	-0.01
75	SLU 35	493	-3	4684	1.41	17.82	-0.01
75	SLU 36	473	-3	4652	1.28	16.87	-0.01
75	SLU 37	493	-3	4684	1.41	17.82	-0.01
75	SLU 38	473	-3	4652	1.28	16.87	-0.01
75	SLU 39	594	-4	5436	1.68	21.54	-0.01
75	SLU 40	574	-4	5404	1.54	20.58	-0.01
75	SLU 41	594	-4	5436	1.68	21.54	-0.01
75	SLU 42	574	-4	5404	1.54	20.58	-0.01
75	SLU 43	187	-2	2605	0.63	6.58	0
75	SLU 44	154	-1	2552	0.41	4.98	0
75	SLU 45	187	-2	2605	0.63	6.58	0
75	SLU 46	167	-1	2573	0.5	5.62	0
75	SLU 47	154	-1	2552	0.41	4.98	0
75	SLU 48	187	-2	2605	0.63	6.58	0
75	SLU 49	167	-1	2573	0.5	5.62	0
75	SLU 50	187	-2	2605	0.63	6.58	0
75	SLU 51	167	-1	2573	0.5	5.62	0
75	SLU 52	390	-3	4305	1.03	13.64	0
75	SLU 53	423	-3	4359	1.25	15.24	-0.01
75	SLU 54	403	-3	4327	1.12	14.28	0
75	SLU 55	390	-3	4305	1.03	13.64	0
75	SLU 56	423	-3	4359	1.25	15.24	-0.01
75	SLU 57	403	-3	4327	1.12	14.28	0
75	SLU 58	423	-3	4359	1.25	15.24	-0.01
75	SLU 59	403	-3	4327	1.12	14.28	0
75	SLU 60	524	-4	5110	1.52	18.95	-0.01
75	SLU 61	504	-3	5078	1.38	17.99	-0.01
75	SLU 62	524	-4	5110	1.52	18.95	-0.01
75	SLU 63	504	-3	5078	1.38	17.99	-0.01
75	SLU 64	276	-2	3339	0.87	9.83	0
75	SLU 65	243	-2	3285	0.65	8.23	0
75	SLU 66	276	-2	3339	0.87	9.83	0
75	SLU 67	256	-2	3307	0.74	8.87	0
75	SLU 68	243	-2	3285	0.65	8.23	0
75	SLU 69	276	-2	3339	0.87	9.83	0
75	SLU 70	256	-2	3307	0.74	8.87	0
75	SLU 71	276	-2	3339	0.87	9.83	0
75	SLU 72	256	-2	3307	0.74	8.87	0
75	SLU 73	479	-3	5039	1.27	16.89	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
75	SLU 74	512	-4	5092	1.49	18.49	-0.01
75	SLU 75	492	-3	5060	1.36	17.53	-0.01
75	SLU 76	479	-3	5039	1.27	16.89	-0.01
75	SLU 77	512	-4	5092	1.49	18.49	-0.01
75	SLU 78	492	-3	5060	1.36	17.53	-0.01
75	SLU 79	512	-4	5092	1.49	18.49	-0.01
75	SLU 80	492	-3	5060	1.36	17.53	-0.01
75	SLU 81	614	-4	5843	1.76	22.2	-0.01
75	SLU 82	593	-4	5811	1.63	21.24	-0.01
75	SLU 83	614	-4	5843	1.76	22.2	-0.01
75	SLU 84	593	-4	5811	1.63	21.24	-0.01
75	SLE RA 1	193	-1	2407	0.62	6.85	0
75	SLE RA 2	171	-1	2371	0.47	5.78	0
75	SLE RA 3	193	-1	2407	0.62	6.85	0
75	SLE RA 4	180	-1	2386	0.53	6.21	0
75	SLE RA 5	171	-1	2371	0.47	5.78	0
75	SLE RA 6	193	-1	2407	0.62	6.85	0
75	SLE RA 7	180	-1	2386	0.53	6.21	0
75	SLE RA 8	193	-1	2407	0.62	6.85	0
75	SLE RA 9	180	-1	2386	0.53	6.21	0
75	SLE RA 10	328	-2	3540	0.88	11.55	0
75	SLE RA 11	350	-2	3576	1.03	12.62	0
75	SLE RA 12	337	-2	3554	0.94	11.98	0
75	SLE RA 13	328	-2	3540	0.88	11.55	0
75	SLE RA 14	350	-2	3576	1.03	12.62	0
75	SLE RA 15	337	-2	3554	0.94	11.98	0
75	SLE RA 16	350	-2	3576	1.03	12.62	0
75	SLE RA 17	337	-2	3554	0.94	11.98	0
75	SLE RA 18	418	-3	4077	1.21	15.09	-0.01
75	SLE RA 19	404	-3	4055	1.12	14.45	0
75	SLE RA 20	418	-3	4077	1.21	15.09	-0.01
75	SLE RA 21	404	-3	4055	1.12	14.45	0
75	SLE FR 1	193	-1	2407	0.62	6.85	0
75	SLE FR 2	189	-1	2400	0.59	6.63	0
75	SLE FR 3	193	-1	2407	0.62	6.85	0
75	SLE FR 4	256	-2	2901	0.77	9.11	0
75	SLE FR 5	260	-2	2908	0.79	9.32	0
75	SLE FR 6	305	-2	3242	0.91	10.97	0
75	SLE QP 1	193	-1	2407	0.62	6.85	0
75	SLE QP 2	260	-2	2908	0.79	9.32	0
75	SLD 1	482	-12	3241	4.49	20.03	-0.01
75	SLD 2	482	-12	3241	4.49	20.03	-0.01
75	SLD 3	535	-10	3481	3.44	22.3	-0.01
75	SLD 4	535	-10	3481	3.44	22.3	-0.01
75	SLD 5	247	-8	2643	3.49	9.1	-0.01
75	SLD 6	247	-8	2643	3.49	9.1	-0.01
75	SLD 7	422	-1	3445	0	16.64	0
75	SLD 8	422	-1	3445	0	16.64	0
75	SLD 9	99	-3	2371	1.59	1.99	-0.01
75	SLD 10	99	-3	2371	1.59	1.99	-0.01
75	SLD 11	274	4	3173	-1.9	9.54	0.01
75	SLD 12	274	4	3173	-1.9	9.54	0.01
75	SLD 13	-14	7	2335	-1.85	-3.66	0
75	SLD 14	-14	7	2335	-1.85	-3.66	0
75	SLD 15	39	9	2575	-2.9	-1.4	0.01
75	SLD 16	39	9	2575	-2.9	-1.4	0.01
75	SLV 1	785	-29	3690	10.44	34.71	-0.03
75	SLV 2	785	-29	3690	10.44	34.71	-0.03
75	SLV 3	910	-24	4256	7.88	40.09	-0.02
75	SLV 4	910	-24	4256	7.88	40.09	-0.02
75	SLV 5	228	-18	2284	7.57	8.78	-0.03
75	SLV 6	228	-18	2284	7.57	8.78	-0.03
75	SLV 7	645	-1	4171	-0.96	26.7	0.01
75	SLV 8	645	-1	4171	-0.96	26.7	0.01
75	SLV 9	-124	-3	1645	2.55	-8.07	-0.02
75	SLV 10	-124	-3	1645	2.55	-8.07	-0.02
75	SLV 11	293	14	3532	-5.98	9.85	0.02
75	SLV 12	293	14	3532	-5.98	9.85	0.02
75	SLV 13	-389	20	1560	-6.29	-21.45	0.02
75	SLV 14	-389	20	1560	-6.29	-21.45	0.02
75	SLV 15	-264	25	2126	-8.85	-16.08	0.03
75	SLV 16	-264	25	2126	-8.85	-16.08	0.03
76	SLU 1	-80	-450	4505	4.34	-6.6	-0.03
76	SLU 2	-98	-433	4424	4.03	-7.67	-0.03
76	SLU 3	-80	-450	4505	4.34	-6.6	-0.03
76	SLU 4	-91	-440	4457	4.15	-7.24	-0.03
76	SLU 5	-98	-433	4424	4.03	-7.67	-0.03
76	SLU 6	-80	-450	4505	4.34	-6.6	-0.03
76	SLU 7	-91	-440	4457	4.15	-7.24	-0.03
76	SLU 8	-80	-450	4505	4.34	-6.6	-0.03
76	SLU 9	-91	-440	4457	4.15	-7.24	-0.03
76	SLU 10	-101	-897	8220	7.37	-10.48	-0.05
76	SLU 11	-82	-914	8301	7.69	-9.41	-0.04
76	SLU 12	-93	-904	8253	7.5	-10.05	-0.05
76	SLU 13	-101	-897	8220	7.37	-10.48	-0.05
76	SLU 14	-82	-914	8301	7.69	-9.41	-0.04
76	SLU 15	-93	-904	8253	7.5	-10.05	-0.05
76	SLU 16	-82	-914	8301	7.69	-9.41	-0.04



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
76	SLU 17	-93	-904	8253	7.5	-10.05	-0.05
76	SLU 18	-83	-1113	9928	9.12	-10.61	-0.05
76	SLU 19	-94	-1103	9879	8.93	-11.25	-0.05
76	SLU 20	-83	-1113	9928	9.12	-10.61	-0.05
76	SLU 21	-94	-1103	9879	8.93	-11.25	-0.05
76	SLU 22	-87	-636	6078	5.67	-8.05	-0.03
76	SLU 23	-105	-619	5998	5.36	-9.13	-0.04
76	SLU 24	-87	-636	6078	5.67	-8.05	-0.03
76	SLU 25	-98	-626	6030	5.48	-8.7	-0.04
76	SLU 26	-105	-619	5998	5.36	-9.13	-0.04
76	SLU 27	-87	-636	6078	5.67	-8.05	-0.03
76	SLU 28	-98	-626	6030	5.48	-8.7	-0.04
76	SLU 29	-87	-636	6078	5.67	-8.05	-0.03
76	SLU 30	-98	-626	6030	5.48	-8.7	-0.04
76	SLU 31	-108	-1083	9793	8.71	-11.93	-0.06
76	SLU 32	-89	-1100	9874	9.02	-10.86	-0.05
76	SLU 33	-100	-1090	9826	8.83	-11.51	-0.05
76	SLU 34	-108	-1083	9793	8.71	-11.93	-0.06
76	SLU 35	-89	-1100	9874	9.02	-10.86	-0.05
76	SLU 36	-100	-1090	9826	8.83	-11.51	-0.05
76	SLU 37	-89	-1100	9874	9.02	-10.86	-0.05
76	SLU 38	-100	-1090	9826	8.83	-11.51	-0.05
76	SLU 39	-90	-1299	11501	10.45	-12.07	-0.06
76	SLU 40	-101	-1289	11452	10.26	-12.71	-0.06
76	SLU 41	-90	-1299	11501	10.45	-12.07	-0.06
76	SLU 42	-101	-1289	11452	10.26	-12.71	-0.06
76	SLU 43	-101	-521	5317	5.18	-8.08	-0.03
76	SLU 44	-120	-504	5237	4.87	-9.15	-0.04
76	SLU 45	-101	-521	5317	5.18	-8.08	-0.03
76	SLU 46	-113	-511	5269	4.99	-8.72	-0.03
76	SLU 47	-120	-504	5237	4.87	-9.15	-0.04
76	SLU 48	-101	-521	5317	5.18	-8.08	-0.03
76	SLU 49	-113	-511	5269	4.99	-8.72	-0.03
76	SLU 50	-101	-521	5317	5.18	-8.08	-0.03
76	SLU 51	-113	-511	5269	4.99	-8.72	-0.03
76	SLU 52	-122	-968	9032	8.22	-11.96	-0.05
76	SLU 53	-104	-985	9113	8.53	-10.89	-0.05
76	SLU 54	-115	-975	9065	8.34	-11.53	-0.05
76	SLU 55	-122	-968	9032	8.22	-11.96	-0.05
76	SLU 56	-104	-985	9113	8.53	-10.89	-0.05
76	SLU 57	-115	-975	9065	8.34	-11.53	-0.05
76	SLU 58	-104	-985	9113	8.53	-10.89	-0.05
76	SLU 59	-115	-975	9065	8.34	-11.53	-0.05
76	SLU 60	-105	-1184	10740	9.96	-12.09	-0.06
76	SLU 61	-116	-1174	10691	9.78	-12.73	-0.06
76	SLU 62	-105	-1184	10740	9.96	-12.09	-0.06
76	SLU 63	-116	-1174	10691	9.78	-12.73	-0.06
76	SLU 64	-108	-708	6890	6.51	-9.53	-0.04
76	SLU 65	-127	-690	6810	6.2	-10.61	-0.04
76	SLU 66	-108	-708	6890	6.51	-9.53	-0.04
76	SLU 67	-120	-697	6842	6.33	-10.18	-0.04
76	SLU 68	-127	-690	6810	6.2	-10.61	-0.04
76	SLU 69	-108	-708	6890	6.51	-9.53	-0.04
76	SLU 70	-120	-697	6842	6.33	-10.18	-0.04
76	SLU 71	-108	-708	6890	6.51	-9.53	-0.04
76	SLU 72	-120	-697	6842	6.33	-10.18	-0.04
76	SLU 73	-129	-1154	10606	9.55	-13.41	-0.06
76	SLU 74	-111	-1172	10686	9.86	-12.34	-0.06
76	SLU 75	-122	-1161	10638	9.67	-12.99	-0.06
76	SLU 76	-129	-1154	10606	9.55	-13.41	-0.06
76	SLU 77	-111	-1172	10686	9.86	-12.34	-0.06
76	SLU 78	-122	-1161	10638	9.67	-12.99	-0.06
76	SLU 79	-111	-1172	10686	9.86	-12.34	-0.06
76	SLU 80	-122	-1161	10638	9.67	-12.99	-0.06
76	SLU 81	-112	-1370	12313	11.3	-13.55	-0.06
76	SLU 82	-123	-1360	12265	11.11	-14.19	-0.07
76	SLU 83	-112	-1370	12313	11.3	-13.55	-0.06
76	SLU 84	-123	-1360	12265	11.11	-14.19	-0.07
76	SLE RA 1	-82	-503	4955	4.72	-7.01	-0.03
76	SLE RA 2	-94	-492	4901	4.51	-7.73	-0.03
76	SLE RA 3	-82	-503	4955	4.72	-7.01	-0.03
76	SLE RA 4	-89	-496	4922	4.59	-7.44	-0.03
76	SLE RA 5	-94	-492	4901	4.51	-7.73	-0.03
76	SLE RA 6	-82	-503	4955	4.72	-7.01	-0.03
76	SLE RA 7	-89	-496	4922	4.59	-7.44	-0.03
76	SLE RA 8	-82	-503	4955	4.72	-7.01	-0.03
76	SLE RA 9	-89	-496	4922	4.59	-7.44	-0.03
76	SLE RA 10	-96	-801	7431	6.74	-9.6	-0.04
76	SLE RA 11	-83	-813	7485	6.95	-8.89	-0.04
76	SLE RA 12	-91	-806	7453	6.83	-9.32	-0.04
76	SLE RA 13	-96	-801	7431	6.74	-9.6	-0.04
76	SLE RA 14	-83	-813	7485	6.95	-8.89	-0.04
76	SLE RA 15	-91	-806	7453	6.83	-9.32	-0.04
76	SLE RA 16	-83	-813	7485	6.95	-8.89	-0.04
76	SLE RA 17	-91	-806	7453	6.83	-9.32	-0.04
76	SLE RA 18	-84	-945	8570	7.91	-9.69	-0.04
76	SLE RA 19	-91	-938	8537	7.78	-10.12	-0.05
76	SLE RA 20	-84	-945	8570	7.91	-9.69	-0.04





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
76	SLE RA 21	-91	-938	8537	7.78	-10.12	-0.05
76	SLE FR 1	-82	-503	4955	4.72	-7.01	-0.03
76	SLE FR 2	-84	-501	4944	4.68	-7.16	-0.03
76	SLE FR 3	-82	-503	4955	4.72	-7.01	-0.03
76	SLE FR 4	-85	-634	6028	5.63	-7.96	-0.03
76	SLE FR 5	-83	-636	6039	5.67	-7.82	-0.03
76	SLE FR 6	-83	-724	6762	6.31	-8.35	-0.04
76	SLE QP 1	-82	-503	4955	4.72	-7.01	-0.03
76	SLE QP 2	-83	-636	6039	5.67	-7.82	-0.03
76	SLD 1	61	-730	6595	7.81	2.25	0.01
76	SLD 2	61	-730	6595	7.81	2.25	0.01
76	SLD 3	90	-802	7075	9.02	0.6	-0.01
76	SLD 4	90	-802	7075	9.02	0.6	-0.01
76	SLD 5	-83	-554	5477	4.49	-2.3	0
76	SLD 6	-83	-554	5477	4.49	-2.3	0
76	SLD 7	13	-796	7079	8.51	-7.78	-0.05
76	SLD 8	13	-796	7079	8.51	-7.78	-0.05
76	SLD 9	-178	-476	4999	2.84	-7.85	-0.02
76	SLD 10	-178	-476	4999	2.84	-7.85	-0.02
76	SLD 11	-82	-718	6601	6.86	-13.33	-0.07
76	SLD 12	-82	-718	6601	6.86	-13.33	-0.07
76	SLD 13	-255	-470	5003	2.33	-16.24	-0.06
76	SLD 14	-255	-470	5003	2.33	-16.24	-0.06
76	SLD 15	-226	-542	5483	3.53	-17.88	-0.07
76	SLD 16	-226	-542	5483	3.53	-17.88	-0.07
76	SLV 1	257	-857	7346	10.74	16.03	0.08
76	SLV 2	257	-857	7346	10.74	16.03	0.08
76	SLV 3	324	-1028	8474	13.63	12.19	0.04
76	SLV 4	324	-1028	8474	13.63	12.19	0.04
76	SLV 5	-82	-443	4720	2.81	5.15	0.06
76	SLV 6	-82	-443	4720	2.81	5.15	0.06
76	SLV 7	141	-1013	8481	12.45	-7.63	-0.07
76	SLV 8	141	-1013	8481	12.45	-7.63	-0.07
76	SLV 9	-306	-259	3597	-1.1	-8.01	0
76	SLV 10	-306	-259	3597	-1.1	-8.01	0
76	SLV 11	-83	-829	7359	8.54	-20.78	-0.12
76	SLV 12	-83	-829	7359	8.54	-20.78	-0.12
76	SLV 13	-489	-244	3604	-2.29	-27.83	-0.1
76	SLV 14	-489	-244	3604	-2.29	-27.83	-0.1
76	SLV 15	-422	-415	4732	0.6	-31.66	-0.14
76	SLV 16	-422	-415	4732	0.6	-31.66	-0.14
77	SLU 1	-405	0	1915	0.33	-8.87	0.04
77	SLU 2	-410	-1	1907	0.45	-9.32	0.06
77	SLU 3	-405	0	1915	0.33	-8.87	0.04
77	SLU 4	-408	-1	1910	0.4	-9.14	0.05
77	SLU 5	-410	-1	1907	0.45	-9.32	0.06
77	SLU 6	-405	0	1915	0.33	-8.87	0.04
77	SLU 7	-408	-1	1910	0.4	-9.14	0.05
77	SLU 8	-405	0	1915	0.33	-8.87	0.04
77	SLU 9	-408	-1	1910	0.4	-9.14	0.05
77	SLU 10	-742	-2	3541	0.8	-16.19	0.1
77	SLU 11	-737	-1	3549	0.68	-15.74	0.08
77	SLU 12	-740	-1	3544	0.75	-16.01	0.09
77	SLU 13	-742	-2	3541	0.8	-16.19	0.1
77	SLU 14	-737	-1	3549	0.68	-15.74	0.08
77	SLU 15	-740	-1	3544	0.75	-16.01	0.09
77	SLU 16	-737	-1	3549	0.68	-15.74	0.08
77	SLU 17	-740	-1	3544	0.75	-16.01	0.09
77	SLU 18	-879	-1	4249	0.83	-18.69	0.09
77	SLU 19	-882	-1	4244	0.9	-18.96	0.11
77	SLU 20	-879	-1	4249	0.83	-18.69	0.09
77	SLU 21	-882	-1	4244	0.9	-18.96	0.11
77	SLU 22	-544	-1	2592	0.47	-11.78	0.05
77	SLU 23	-549	-1	2584	0.59	-12.23	0.08
77	SLU 24	-544	-1	2592	0.47	-11.78	0.05
77	SLU 25	-547	-1	2587	0.54	-12.05	0.07
77	SLU 26	-549	-1	2584	0.59	-12.23	0.08
77	SLU 27	-544	-1	2592	0.47	-11.78	0.05
77	SLU 28	-547	-1	2587	0.54	-12.05	0.07
77	SLU 29	-544	-1	2592	0.47	-11.78	0.05
77	SLU 30	-547	-1	2587	0.54	-12.05	0.07
77	SLU 31	-881	-2	4219	0.94	-19.11	0.12
77	SLU 32	-876	-1	4226	0.82	-18.66	0.09
77	SLU 33	-879	-1	4222	0.89	-18.93	0.11
77	SLU 34	-881	-2	4219	0.94	-19.11	0.12
77	SLU 35	-876	-1	4226	0.82	-18.66	0.09
77	SLU 36	-879	-1	4222	0.89	-18.93	0.11
77	SLU 37	-876	-1	4226	0.82	-18.66	0.09
77	SLU 38	-879	-1	4222	0.89	-18.93	0.11
77	SLU 39	-1019	-1	4927	0.96	-21.61	0.13
77	SLU 40	-1022	-2	4922	1.04	-21.88	0.13
77	SLU 41	-1019	-1	4927	0.96	-21.61	0.13
77	SLU 42	-1022	-2	4922	1.04	-21.88	0.13
77	SLU 43	-479	-1	2257	0.38	-10.53	0.04
77	SLU 44	-484	-1	2249	0.5	-10.98	0.07
77	SLU 45	-479	-1	2257	0.38	-10.53	0.04
77	SLU 46	-482	-1	2252	0.45	-10.8	0.06
77	SLU 47	-484	-1	2249	0.5	-10.98	0.07



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
77	SLU 48	-479	-1	2257	0.38	-10.53	0.04
77	SLU 49	-482	-1	2252	0.45	-10.8	0.06
77	SLU 50	-479	-1	2257	0.38	-10.53	0.04
77	SLU 51	-482	-1	2252	0.45	-10.8	0.06
77	SLU 52	-816	-2	3883	0.85	-17.85	0.11
77	SLU 53	-811	-1	3891	0.73	-17.4	0.08
77	SLU 54	-814	-1	3886	0.8	-17.67	0.1
77	SLU 55	-816	-2	3883	0.85	-17.85	0.11
77	SLU 56	-811	-1	3891	0.73	-17.4	0.08
77	SLU 57	-814	-1	3886	0.8	-17.67	0.1
77	SLU 58	-811	-1	3891	0.73	-17.4	0.08
77	SLU 59	-814	-1	3886	0.8	-17.67	0.1
77	SLU 60	-953	-1	4591	0.88	-20.35	0.1
77	SLU 61	-956	-1	4586	0.95	-20.62	0.12
77	SLU 62	-953	-1	4591	0.88	-20.35	0.1
77	SLU 63	-956	-1	4586	0.95	-20.62	0.12
77	SLU 64	-618	-1	2934	0.52	-13.44	0.06
77	SLU 65	-623	-1	2926	0.64	-13.89	0.08
77	SLU 66	-618	-1	2934	0.52	-13.44	0.06
77	SLU 67	-621	-1	2930	0.59	-13.71	0.08
77	SLU 68	-623	-1	2926	0.64	-13.89	0.08
77	SLU 69	-618	-1	2934	0.52	-13.44	0.06
77	SLU 70	-621	-1	2930	0.59	-13.71	0.08
77	SLU 71	-618	-1	2934	0.52	-13.44	0.06
77	SLU 72	-621	-1	2930	0.59	-13.71	0.08
77	SLU 73	-955	-2	4561	0.99	-20.77	0.12
77	SLU 74	-950	-1	4568	0.87	-20.32	0.1
77	SLU 75	-953	-1	4564	0.94	-20.59	0.11
77	SLU 76	-955	-2	4561	0.99	-20.77	0.12
77	SLU 77	-950	-1	4568	0.87	-20.32	0.1
77	SLU 78	-953	-1	4564	0.94	-20.59	0.11
77	SLU 79	-950	-1	4568	0.87	-20.32	0.1
77	SLU 80	-953	-1	4564	0.94	-20.59	0.11
77	SLU 81	-1092	-1	5269	1.02	-23.27	0.12
77	SLU 82	-1095	-2	5264	1.09	-23.54	0.13
77	SLU 83	-1092	-1	5269	1.02	-23.27	0.12
77	SLU 84	-1095	-2	5264	1.09	-23.54	0.13
77	SLE RA 1	-445	0	2108	0.37	-9.7	0.04
77	SLE RA 2	-448	-1	2103	0.45	-10	0.06
77	SLE RA 3	-445	0	2108	0.37	-9.7	0.04
77	SLE RA 4	-447	-1	2105	0.42	-9.88	0.05
77	SLE RA 5	-448	-1	2103	0.45	-10	0.06
77	SLE RA 6	-445	0	2108	0.37	-9.7	0.04
77	SLE RA 7	-447	-1	2105	0.42	-9.88	0.05
77	SLE RA 8	-445	0	2108	0.37	-9.7	0.04
77	SLE RA 9	-447	-1	2105	0.42	-9.88	0.05
77	SLE RA 10	-670	-1	3192	0.68	-14.58	0.09
77	SLE RA 11	-666	-1	3197	0.6	-14.28	0.07
77	SLE RA 12	-668	-1	3194	0.65	-14.46	0.08
77	SLE RA 13	-670	-1	3192	0.68	-14.58	0.09
77	SLE RA 14	-666	-1	3197	0.6	-14.28	0.07
77	SLE RA 15	-668	-1	3194	0.65	-14.46	0.08
77	SLE RA 16	-666	-1	3197	0.6	-14.28	0.07
77	SLE RA 17	-668	-1	3194	0.65	-14.46	0.08
77	SLE RA 18	-761	-1	3664	0.7	-16.25	0.08
77	SLE RA 19	-763	-1	3661	0.75	-16.43	0.09
77	SLE RA 20	-761	-1	3664	0.7	-16.25	0.08
77	SLE RA 21	-763	-1	3661	0.75	-16.43	0.09
77	SLE FR 1	-445	0	2108	0.37	-9.7	0.04
77	SLE FR 2	-446	-1	2107	0.38	-9.76	0.05
77	SLE FR 3	-445	0	2108	0.37	-9.7	0.04
77	SLE FR 4	-540	-1	2574	0.48	-11.72	0.06
77	SLE FR 5	-540	-1	2575	0.47	-11.66	0.05
77	SLE FR 6	-603	-1	2886	0.53	-12.97	0.06
77	SLE QP 1	-445	0	2108	0.37	-9.7	0.04
77	SLE QP 2	-540	-1	2575	0.47	-11.66	0.05
77	SLD 1	-402	18	2108	-2.87	-6.26	-0.58
77	SLD 2	-402	18	2108	-2.87	-6.26	-0.58
77	SLD 3	-458	13	2349	-2.1	-7.73	-0.44
77	SLD 4	-458	13	2349	-2.1	-7.73	-0.44
77	SLD 5	-414	12	2068	-1.71	-7.82	-0.36
77	SLD 6	-414	12	2068	-1.71	-7.82	-0.36
77	SLD 7	-600	-3	2874	0.87	-12.71	0.13
77	SLD 8	-600	-3	2874	0.87	-12.71	0.13
77	SLD 9	-480	2	2276	0.06	-10.62	-0.02
77	SLD 10	-480	2	2276	0.06	-10.62	-0.02
77	SLD 11	-666	-13	3082	2.64	-15.51	0.47
77	SLD 12	-666	-13	3082	2.64	-15.51	0.47
77	SLD 13	-621	-14	2801	3.04	-15.6	0.54
77	SLD 14	-621	-14	2801	3.04	-15.6	0.54
77	SLD 15	-677	-19	3042	3.81	-17.07	0.69
77	SLD 16	-677	-19	3042	3.81	-17.07	0.69
77	SLV 1	-216	47	1475	-8.2	1.13	-1.6
77	SLV 2	-216	47	1475	-8.2	1.13	-1.6
77	SLV 3	-346	36	2041	-6.27	-2.27	-1.23
77	SLV 4	-346	36	2041	-6.27	-2.27	-1.23
77	SLV 5	-245	30	1388	-5.07	-2.67	-1
77	SLV 6	-245	30	1388	-5.07	-2.67	-1



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
77	SLV 7	-679	-6	3272	1.38	-14	0.23
77	SLV 8	-679	-6	3272	1.38	-14	0.23
77	SLV 9	-401	5	1878	-0.45	-9.33	-0.12
77	SLV 10	-401	5	1878	-0.45	-9.33	-0.12
77	SLV 11	-834	-31	3762	6.01	-20.66	1.11
77	SLV 12	-834	-31	3762	6.01	-20.66	1.11
77	SLV 13	-734	-37	3109	7.2	-21.06	1.34
77	SLV 14	-734	-37	3109	7.2	-21.06	1.34
77	SLV 15	-864	-48	3675	9.14	-24.46	1.71
77	SLV 16	-864	-48	3675	9.14	-24.46	1.71
78	SLU 1	-125	0	-22	-0.02	-10.39	0
78	SLU 2	-124	0	-27	0.03	-10.41	-0.01
78	SLU 3	-125	0	-22	-0.02	-10.39	0
78	SLU 4	-124	0	-25	0.01	-10.41	0
78	SLU 5	-124	0	-27	0.03	-10.41	-0.01
78	SLU 6	-125	0	-22	-0.02	-10.39	0
78	SLU 7	-124	0	-25	0.01	-10.41	0
78	SLU 8	-125	0	-22	-0.02	-10.39	0
78	SLU 9	-124	0	-25	0.01	-10.41	0
78	SLU 10	-333	0	-601	0.04	-20.93	-0.01
78	SLU 11	-334	0	-596	-0.01	-20.91	0
78	SLU 12	-333	0	-599	0.02	-20.92	-0.01
78	SLU 13	-333	0	-601	0.04	-20.93	-0.01
78	SLU 14	-334	0	-596	-0.01	-20.91	0
78	SLU 15	-333	0	-599	0.02	-20.92	-0.01
78	SLU 16	-334	0	-596	-0.01	-20.91	0
78	SLU 17	-333	0	-599	0.02	-20.92	-0.01
78	SLU 18	-423	0	-842	-0.01	-25.41	0
78	SLU 19	-423	0	-845	0.03	-25.43	-0.01
78	SLU 20	-423	0	-842	-0.01	-25.41	0
78	SLU 21	-423	0	-845	0.03	-25.43	-0.01
78	SLU 22	-212	0	-255	-0.02	-14.89	0
78	SLU 23	-211	0	-259	0.04	-14.91	-0.01
78	SLU 24	-212	0	-255	-0.02	-14.89	0
78	SLU 25	-212	0	-257	0.01	-14.9	-0.01
78	SLU 26	-211	0	-259	0.04	-14.91	-0.01
78	SLU 27	-212	0	-255	-0.02	-14.89	0
78	SLU 28	-212	0	-257	0.01	-14.9	-0.01
78	SLU 29	-212	0	-255	-0.02	-14.89	0
78	SLU 30	-212	0	-257	0.01	-14.9	-0.01
78	SLU 31	-420	0	-833	0.05	-25.42	-0.01
78	SLU 32	-421	0	-828	-0.01	-25.4	0
78	SLU 33	-421	0	-831	0.02	-25.41	-0.01
78	SLU 34	-420	0	-833	0.05	-25.42	-0.01
78	SLU 35	-421	0	-828	-0.01	-25.4	0
78	SLU 36	-421	0	-831	0.02	-25.41	-0.01
78	SLU 37	-421	0	-828	-0.01	-25.4	0
78	SLU 38	-421	0	-831	0.02	-25.41	-0.01
78	SLU 39	-511	0	-1074	-0.01	-29.91	0
78	SLU 40	-510	0	-1077	0.03	-29.92	-0.01
78	SLU 41	-511	0	-1074	-0.01	-29.91	0
78	SLU 42	-510	0	-1077	0.03	-29.92	-0.01
78	SLU 43	-132	0	50	-0.03	-11.97	0
78	SLU 44	-131	0	46	0.03	-11.99	-0.01
78	SLU 45	-132	0	50	-0.03	-11.97	0
78	SLU 46	-132	0	48	0	-11.98	0
78	SLU 47	-131	0	46	0.03	-11.99	-0.01
78	SLU 48	-132	0	50	-0.03	-11.97	0
78	SLU 49	-132	0	48	0	-11.98	0
78	SLU 50	-132	0	50	-0.03	-11.97	0
78	SLU 51	-132	0	48	0	-11.98	0
78	SLU 52	-340	0	-528	0.04	-22.5	-0.01
78	SLU 53	-341	0	-523	-0.02	-22.48	0
78	SLU 54	-341	0	-526	0.01	-22.5	-0.01
78	SLU 55	-340	0	-528	0.04	-22.5	-0.01
78	SLU 56	-341	0	-523	-0.02	-22.48	0
78	SLU 57	-341	0	-526	0.01	-22.5	-0.01
78	SLU 58	-341	0	-523	-0.02	-22.48	0
78	SLU 59	-341	0	-526	0.01	-22.5	-0.01
78	SLU 60	-431	0	-769	-0.02	-26.99	0
78	SLU 61	-430	0	-772	0.02	-27	-0.01
78	SLU 62	-431	0	-769	-0.02	-26.99	0
78	SLU 63	-430	0	-772	0.02	-27	-0.01
78	SLU 64	-220	0	-182	-0.03	-16.46	0
78	SLU 65	-219	0	-186	0.03	-16.49	-0.01
78	SLU 66	-220	0	-182	-0.03	-16.46	0
78	SLU 67	-219	0	-184	0.01	-16.48	0
78	SLU 68	-219	0	-186	0.03	-16.49	-0.01
78	SLU 69	-220	0	-182	-0.03	-16.46	0
78	SLU 70	-219	0	-184	0.01	-16.48	0
78	SLU 71	-220	0	-182	-0.03	-16.46	0
78	SLU 72	-219	0	-184	0.01	-16.48	0
78	SLU 73	-428	0	-760	0.04	-27	-0.01
78	SLU 74	-429	0	-756	-0.02	-26.98	0
78	SLU 75	-428	0	-758	0.02	-26.99	-0.01
78	SLU 76	-428	0	-760	0.04	-27	-0.01
78	SLU 77	-429	0	-756	-0.02	-26.98	0
78	SLU 78	-428	0	-758	0.02	-26.99	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
78	SLU 79	-429	0	-756	-0.02	-26.98	0
78	SLU 80	-428	0	-758	0.02	-26.99	-0.01
78	SLU 81	-518	0	-1002	-0.01	-31.49	0
78	SLU 82	-518	0	-1004	0.02	-31.5	-0.01
78	SLU 83	-518	0	-1002	-0.01	-31.49	0
78	SLU 84	-518	0	-1004	0.02	-31.5	-0.01
78	SLE RA 1	-150	0	-89	-0.02	-11.68	0
78	SLE RA 2	-149	0	-92	0.02	-11.69	-0.01
78	SLE RA 3	-150	0	-89	-0.02	-11.68	0
78	SLE RA 4	-150	0	-91	0	-11.69	0
78	SLE RA 5	-149	0	-92	0.02	-11.69	-0.01
78	SLE RA 6	-150	0	-89	-0.02	-11.68	0
78	SLE RA 7	-150	0	-91	0	-11.69	0
78	SLE RA 8	-150	0	-89	-0.02	-11.68	0
78	SLE RA 9	-150	0	-91	0	-11.69	0
78	SLE RA 10	-288	0	-474	0.02	-18.7	-0.01
78	SLE RA 11	-289	0	-471	-0.02	-18.69	0
78	SLE RA 12	-289	0	-473	0.01	-18.7	0
78	SLE RA 13	-288	0	-474	0.02	-18.7	-0.01
78	SLE RA 14	-289	0	-471	-0.02	-18.69	0
78	SLE RA 15	-289	0	-473	0.01	-18.7	0
78	SLE RA 16	-289	0	-471	-0.02	-18.69	0
78	SLE RA 17	-289	0	-473	0.01	-18.7	0
78	SLE RA 18	-349	0	-635	-0.01	-21.69	0
78	SLE RA 19	-348	0	-637	0.01	-21.7	-0.01
78	SLE RA 20	-349	0	-635	-0.01	-21.69	0
78	SLE RA 21	-348	0	-637	0.01	-21.7	-0.01
78	SLE FR 1	-150	0	-89	-0.02	-11.68	0
78	SLE FR 2	-150	0	-89	-0.01	-11.68	0
78	SLE FR 3	-150	0	-89	-0.02	-11.68	0
78	SLE FR 4	-209	0	-253	-0.01	-14.68	0
78	SLE FR 5	-210	0	-253	-0.02	-14.68	0
78	SLE FR 6	-249	0	-362	-0.02	-16.68	0
78	SLE QP 1	-150	0	-89	-0.02	-11.68	0
78	SLE QP 2	-210	0	-253	-0.02	-14.68	0
78	SLD 1	-247	8	-19	-1.26	-11.45	0.27
78	SLD 2	-247	8	-19	-1.26	-11.45	0.27
78	SLD 3	-275	7	-101	-1.07	-12.85	0.23
78	SLD 4	-275	7	-101	-1.07	-12.85	0.23
78	SLD 5	-179	4	-58	-0.69	-11.58	0.14
78	SLD 6	-179	4	-58	-0.69	-11.58	0.14
78	SLD 7	-271	0	-332	-0.04	-16.27	0.01
78	SLD 8	-271	0	-332	-0.04	-16.27	0.01
78	SLD 9	-148	0	-174	0	-13.09	0
78	SLD 10	-148	0	-174	0	-13.09	0
78	SLD 11	-241	-4	-448	0.65	-17.79	-0.14
78	SLD 12	-241	-4	-448	0.65	-17.79	-0.14
78	SLD 13	-144	-7	-404	1.03	-16.51	-0.22
78	SLD 14	-144	-7	-404	1.03	-16.51	-0.22
78	SLD 15	-172	-8	-487	1.22	-17.92	-0.26
78	SLD 16	-172	-8	-487	1.22	-17.92	-0.26
78	SLV 1	-296	20	302	-3.22	-7.14	0.68
78	SLV 2	-296	20	302	-3.22	-7.14	0.68
78	SLV 3	-363	17	103	-2.74	-10.43	0.58
78	SLV 4	-363	17	103	-2.74	-10.43	0.58
78	SLV 5	-135	11	217	-1.71	-7.44	0.36
78	SLV 6	-135	11	217	-1.71	-7.44	0.36
78	SLV 7	-356	1	-449	-0.11	-18.38	0.02
78	SLV 8	-356	1	-449	-0.11	-18.38	0.02
78	SLV 9	-63	-1	-56	0.07	-10.98	-0.02
78	SLV 10	-63	-1	-56	0.07	-10.98	-0.02
78	SLV 11	-284	-11	-722	1.67	-21.92	-0.36
78	SLV 12	-284	-11	-722	1.67	-21.92	-0.36
78	SLV 13	-57	-17	-608	2.7	-18.94	-0.58
78	SLV 14	-57	-17	-608	2.7	-18.94	-0.58
78	SLV 15	-123	-21	-808	3.18	-22.22	-0.68
78	SLV 16	-123	-21	-808	3.18	-22.22	-0.68
79	SLU 1	-186	140	2820	-6.54	-11.55	-0.01
79	SLU 2	-184	143	2856	-6.64	-11.5	-0.01
79	SLU 3	-186	140	2820	-6.54	-11.55	-0.01
79	SLU 4	-185	142	2842	-6.6	-11.52	-0.01
79	SLU 5	-184	143	2856	-6.64	-11.5	-0.01
79	SLU 6	-186	140	2820	-6.54	-11.55	-0.01
79	SLU 7	-185	142	2842	-6.6	-11.52	-0.01
79	SLU 8	-186	140	2820	-6.54	-11.55	-0.01
79	SLU 9	-185	142	2842	-6.6	-11.52	-0.01
79	SLU 10	-276	177	3249	-8.86	-22.18	-0.01
79	SLU 11	-278	174	3213	-8.76	-22.24	-0.01
79	SLU 12	-277	176	3235	-8.82	-22.2	-0.01
79	SLU 13	-276	177	3249	-8.86	-22.18	-0.01
79	SLU 14	-278	174	3213	-8.76	-22.24	-0.01
79	SLU 15	-277	176	3235	-8.82	-22.2	-0.01
79	SLU 16	-278	174	3213	-8.76	-22.24	-0.01
79	SLU 17	-277	176	3235	-8.82	-22.2	-0.01
79	SLU 18	-318	189	3382	-9.72	-26.82	-0.01
79	SLU 19	-316	190	3403	-9.77	-26.78	-0.01
79	SLU 20	-318	189	3382	-9.72	-26.82	-0.01
79	SLU 21	-316	190	3403	-9.77	-26.78	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
79	SLU 22	-228	163	3041	-7.81	-16.15	-0.01
79	SLU 23	-226	166	3077	-7.91	-16.09	-0.01
79	SLU 24	-228	163	3041	-7.81	-16.15	-0.01
79	SLU 25	-227	165	3062	-7.87	-16.12	-0.01
79	SLU 26	-226	166	3077	-7.91	-16.09	-0.01
79	SLU 27	-228	163	3041	-7.81	-16.15	-0.01
79	SLU 28	-227	165	3062	-7.87	-16.12	-0.01
79	SLU 29	-228	163	3041	-7.81	-16.15	-0.01
79	SLU 30	-227	165	3062	-7.87	-16.12	-0.01
79	SLU 31	-318	200	3470	-10.13	-26.78	-0.01
79	SLU 32	-320	197	3434	-10.04	-26.84	-0.01
79	SLU 33	-319	199	3455	-10.09	-26.8	-0.01
79	SLU 34	-318	200	3470	-10.13	-26.78	-0.01
79	SLU 35	-320	197	3434	-10.04	-26.84	-0.01
79	SLU 36	-319	199	3455	-10.09	-26.8	-0.01
79	SLU 37	-320	197	3434	-10.04	-26.84	-0.01
79	SLU 38	-319	199	3455	-10.09	-26.8	-0.01
79	SLU 39	-360	211	3602	-10.99	-31.42	-0.01
79	SLU 40	-358	213	3624	-11.04	-31.38	-0.01
79	SLU 41	-360	211	3602	-10.99	-31.42	-0.01
79	SLU 42	-358	213	3624	-11.04	-31.38	-0.01
79	SLU 43	-228	175	3591	-8.07	-13.44	-0.01
79	SLU 44	-226	178	3627	-8.16	-13.39	-0.01
79	SLU 45	-228	175	3591	-8.07	-13.44	-0.01
79	SLU 46	-226	176	3613	-8.12	-13.41	-0.01
79	SLU 47	-226	178	3627	-8.16	-13.39	-0.01
79	SLU 48	-228	175	3591	-8.07	-13.44	-0.01
79	SLU 49	-226	176	3613	-8.12	-13.41	-0.01
79	SLU 50	-228	175	3591	-8.07	-13.44	-0.01
79	SLU 51	-226	176	3613	-8.12	-13.41	-0.01
79	SLU 52	-318	211	4020	-10.38	-24.07	-0.01
79	SLU 53	-320	208	3984	-10.29	-24.13	-0.01
79	SLU 54	-318	210	4006	-10.35	-24.09	-0.01
79	SLU 55	-318	211	4020	-10.38	-24.07	-0.01
79	SLU 56	-320	208	3984	-10.29	-24.13	-0.01
79	SLU 57	-318	210	4006	-10.35	-24.09	-0.01
79	SLU 58	-320	208	3984	-10.29	-24.13	-0.01
79	SLU 59	-318	210	4006	-10.35	-24.09	-0.01
79	SLU 60	-359	223	4152	-11.24	-28.71	-0.02
79	SLU 61	-358	225	4174	-11.3	-28.67	-0.01
79	SLU 62	-359	223	4152	-11.24	-28.71	-0.02
79	SLU 63	-358	225	4174	-11.3	-28.67	-0.01
79	SLU 64	-270	198	3811	-9.34	-18.04	-0.01
79	SLU 65	-267	200	3847	-9.43	-17.98	-0.01
79	SLU 66	-270	198	3811	-9.34	-18.04	-0.01
79	SLU 67	-268	199	3833	-9.4	-18.01	-0.01
79	SLU 68	-267	200	3847	-9.43	-17.98	-0.01
79	SLU 69	-270	198	3811	-9.34	-18.04	-0.01
79	SLU 70	-268	199	3833	-9.4	-18.01	-0.01
79	SLU 71	-270	198	3811	-9.34	-18.04	-0.01
79	SLU 72	-268	199	3833	-9.4	-18.01	-0.01
79	SLU 73	-359	234	4240	-11.66	-28.67	-0.02
79	SLU 74	-362	231	4204	-11.56	-28.73	-0.02
79	SLU 75	-360	233	4226	-11.62	-28.69	-0.02
79	SLU 76	-359	234	4240	-11.66	-28.67	-0.02
79	SLU 77	-362	231	4204	-11.56	-28.73	-0.02
79	SLU 78	-360	233	4226	-11.62	-28.69	-0.02
79	SLU 79	-362	231	4204	-11.56	-28.73	-0.02
79	SLU 80	-360	233	4226	-11.62	-28.69	-0.02
79	SLU 81	-401	246	4373	-12.51	-33.31	-0.02
79	SLU 82	-400	247	4394	-12.57	-33.27	-0.02
79	SLU 83	-401	246	4373	-12.51	-33.31	-0.02
79	SLU 84	-400	247	4394	-12.57	-33.27	-0.02
79	SLE RA 1	-198	147	2883	-6.91	-12.87	-0.01
79	SLE RA 2	-197	149	2907	-6.97	-12.83	-0.01
79	SLE RA 3	-198	147	2883	-6.91	-12.87	-0.01
79	SLE RA 4	-197	148	2898	-6.94	-12.84	-0.01
79	SLE RA 5	-197	149	2907	-6.97	-12.83	-0.01
79	SLE RA 6	-198	147	2883	-6.91	-12.87	-0.01
79	SLE RA 7	-197	148	2898	-6.94	-12.84	-0.01
79	SLE RA 8	-198	147	2883	-6.91	-12.87	-0.01
79	SLE RA 9	-197	148	2898	-6.94	-12.84	-0.01
79	SLE RA 10	-258	171	3169	-8.45	-19.95	-0.01
79	SLE RA 11	-260	169	3145	-8.39	-19.99	-0.01
79	SLE RA 12	-259	171	3160	-8.42	-19.97	-0.01
79	SLE RA 13	-258	171	3169	-8.45	-19.95	-0.01
79	SLE RA 14	-260	169	3145	-8.39	-19.99	-0.01
79	SLE RA 15	-259	171	3160	-8.42	-19.97	-0.01
79	SLE RA 16	-260	169	3145	-8.39	-19.99	-0.01
79	SLE RA 17	-259	171	3160	-8.42	-19.97	-0.01
79	SLE RA 18	-286	179	3258	-9.02	-23.04	-0.01
79	SLE RA 19	-285	180	3272	-9.06	-23.02	-0.01
79	SLE RA 20	-286	179	3258	-9.02	-23.04	-0.01
79	SLE RA 21	-285	180	3272	-9.06	-23.02	-0.01
79	SLE FR 1	-198	147	2883	-6.91	-12.87	-0.01
79	SLE FR 2	-198	147	2888	-6.92	-12.86	-0.01
79	SLE FR 3	-198	147	2883	-6.91	-12.87	-0.01
79	SLE FR 4	-224	157	3000	-7.55	-15.91	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
79	SLE FR 5	-224	157	2996	-7.54	-15.92	-0.01
79	SLE FR 6	-242	163	3070	-7.96	-17.96	-0.01
79	SLE QP 1	-198	147	2883	-6.91	-12.87	-0.01
79	SLE QP 2	-224	157	2996	-7.54	-15.92	-0.01
79	SLD 1	-243	169	2767	-8.08	-18	-0.03
79	SLD 2	-243	169	2767	-8.08	-18	-0.03
79	SLD 3	-256	15	2590	-1.08	-19.43	-0.02
79	SLD 4	-256	15	2590	-1.08	-19.43	-0.02
79	SLD 5	-210	394	3195	-18.31	-14.37	-0.03
79	SLD 6	-210	394	3195	-18.31	-14.37	-0.03
79	SLD 7	-254	-119	2605	5.01	-19.15	0
79	SLD 8	-254	-119	2605	5.01	-19.15	0
79	SLD 9	-195	432	3386	-20.09	-12.7	-0.02
79	SLD 10	-195	432	3386	-20.09	-12.7	-0.02
79	SLD 11	-238	-80	2796	3.24	-17.47	0.01
79	SLD 12	-238	-80	2796	3.24	-17.47	0.01
79	SLD 13	-193	298	3401	-14	-12.41	0
79	SLD 14	-193	298	3401	-14	-12.41	0
79	SLD 15	-206	144	3224	-7	-13.84	0.01
79	SLD 16	-206	144	3224	-7	-13.84	0.01
79	SLV 1	-272	186	2465	-8.79	-20.78	-0.06
79	SLV 2	-272	186	2465	-8.79	-20.78	-0.06
79	SLV 3	-301	-177	2033	7.72	-24.12	-0.04
79	SLV 4	-301	-177	2033	7.72	-24.12	-0.04
79	SLV 5	-194	716	3491	-32.96	-12.31	-0.06
79	SLV 6	-194	716	3491	-32.96	-12.31	-0.06
79	SLV 7	-293	-494	2052	22.08	-23.44	0.02
79	SLV 8	-293	-494	2052	22.08	-23.44	0.02
79	SLV 9	-156	807	3939	-37.16	-8.4	-0.04
79	SLV 10	-156	807	3939	-37.16	-8.4	-0.04
79	SLV 11	-255	-403	2500	17.88	-19.53	0.04
79	SLV 12	-255	-403	2500	17.88	-19.53	0.04
79	SLV 13	-147	490	3958	-22.8	-7.73	0.02
79	SLV 14	-147	490	3958	-22.8	-7.73	0.02
79	SLV 15	-177	127	3526	-6.29	-11.06	0.04
79	SLV 16	-177	127	3526	-6.29	-11.06	0.04
80	SLU 1	1	155	1822	-6.37	0.33	0.01
80	SLU 2	4	150	1774	-6.09	1.81	0
80	SLU 3	1	155	1822	-6.37	0.33	0.01
80	SLU 4	3	152	1793	-6.2	1.22	0
80	SLU 5	4	150	1774	-6.09	1.81	0
80	SLU 6	1	155	1822	-6.37	0.33	0.01
80	SLU 7	3	152	1793	-6.2	1.22	0
80	SLU 8	1	155	1822	-6.37	0.33	0.01
80	SLU 9	3	152	1793	-6.2	1.22	0
80	SLU 10	4	226	2177	-9.2	1.63	0
80	SLU 11	1	231	2224	-9.47	0.15	0.01
80	SLU 12	3	228	2196	-9.31	1.04	0
80	SLU 13	4	226	2177	-9.2	1.63	0
80	SLU 14	1	231	2224	-9.47	0.15	0.01
80	SLU 15	3	228	2196	-9.31	1.04	0
80	SLU 16	1	231	2224	-9.47	0.15	0.01
80	SLU 17	3	228	2196	-9.31	1.04	0
80	SLU 18	1	264	2397	-10.8	0.07	0.01
80	SLU 19	3	261	2368	-10.64	0.96	0.01
80	SLU 20	1	264	2397	-10.8	0.07	0.01
80	SLU 21	3	261	2368	-10.64	0.96	0.01
80	SLU 22	1	192	2030	-7.91	0.29	0.01
80	SLU 23	4	187	1983	-7.63	1.78	0
80	SLU 24	1	192	2030	-7.91	0.29	0.01
80	SLU 25	3	189	2002	-7.74	1.18	0
80	SLU 26	4	187	1983	-7.63	1.78	0
80	SLU 27	1	192	2030	-7.91	0.29	0.01
80	SLU 28	3	189	2002	-7.74	1.18	0
80	SLU 29	1	192	2030	-7.91	0.29	0.01
80	SLU 30	3	189	2002	-7.74	1.18	0
80	SLU 31	4	263	2385	-10.74	1.6	0
80	SLU 32	1	269	2433	-11.01	0.12	0.01
80	SLU 33	3	265	2404	-10.85	1	0.01
80	SLU 34	4	263	2385	-10.74	1.6	0
80	SLU 35	1	269	2433	-11.01	0.12	0.01
80	SLU 36	3	265	2404	-10.85	1	0.01
80	SLU 37	1	269	2433	-11.01	0.12	0.01
80	SLU 38	3	265	2404	-10.85	1	0.01
80	SLU 39	1	301	2605	-12.34	0.04	0.01
80	SLU 40	3	298	2577	-12.18	0.93	0.01
80	SLU 41	1	301	2605	-12.34	0.04	0.01
80	SLU 42	3	298	2577	-12.18	0.93	0.01
80	SLU 43	2	189	2297	-7.75	0.44	0.01
80	SLU 44	4	183	2249	-7.47	1.92	0
80	SLU 45	2	189	2297	-7.75	0.44	0.01
80	SLU 46	3	185	2268	-7.58	1.33	0
80	SLU 47	4	183	2249	-7.47	1.92	0
80	SLU 48	2	189	2297	-7.75	0.44	0.01
80	SLU 49	3	185	2268	-7.58	1.33	0
80	SLU 50	2	189	2297	-7.75	0.44	0.01
80	SLU 51	3	185	2268	-7.58	1.33	0
80	SLU 52	4	260	2652	-10.58	1.74	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
80	SLU 53	2	265	2700	-10.85	0.26	0.01
80	SLU 54	3	262	2671	-10.69	1.15	0.01
80	SLU 55	4	260	2652	-10.58	1.74	0
80	SLU 56	2	265	2700	-10.85	0.26	0.01
80	SLU 57	3	262	2671	-10.69	1.15	0.01
80	SLU 58	2	265	2700	-10.85	0.26	0.01
80	SLU 59	3	262	2671	-10.69	1.15	0.01
80	SLU 60	1	298	2872	-12.18	0.18	0.01
80	SLU 61	3	294	2843	-12.02	1.07	0.01
80	SLU 62	1	298	2872	-12.18	0.18	0.01
80	SLU 63	3	294	2843	-12.02	1.07	0.01
80	SLU 64	2	226	2506	-9.29	0.4	0.01
80	SLU 65	4	221	2458	-9.01	1.89	0
80	SLU 66	2	226	2506	-9.29	0.4	0.01
80	SLU 67	3	223	2477	-9.12	1.29	0.01
80	SLU 68	4	221	2458	-9.01	1.89	0
80	SLU 69	2	226	2506	-9.29	0.4	0.01
80	SLU 70	3	223	2477	-9.12	1.29	0.01
80	SLU 71	2	226	2506	-9.29	0.4	0.01
80	SLU 72	3	223	2477	-9.12	1.29	0.01
80	SLU 73	4	297	2860	-12.12	1.71	0
80	SLU 74	2	302	2908	-12.39	0.23	0.01
80	SLU 75	3	299	2879	-12.23	1.12	0.01
80	SLU 76	4	297	2860	-12.12	1.71	0
80	SLU 77	2	302	2908	-12.39	0.23	0.01
80	SLU 78	3	299	2879	-12.23	1.12	0.01
80	SLU 79	2	302	2908	-12.39	0.23	0.01
80	SLU 80	3	299	2879	-12.23	1.12	0.01
80	SLU 81	2	335	3080	-13.72	0.15	0.01
80	SLU 82	3	332	3052	-13.56	1.04	0.01
80	SLU 83	2	335	3080	-13.72	0.15	0.01
80	SLU 84	3	332	3052	-13.56	1.04	0.01
80	SLE RA 1	1	166	1882	-6.81	0.32	0.01
80	SLE RA 2	3	162	1850	-6.62	1.31	0
80	SLE RA 3	1	166	1882	-6.81	0.32	0.01
80	SLE RA 4	2	163	1862	-6.7	0.91	0
80	SLE RA 5	3	162	1850	-6.62	1.31	0
80	SLE RA 6	1	166	1882	-6.81	0.32	0.01
80	SLE RA 7	2	163	1862	-6.7	0.91	0
80	SLE RA 8	1	166	1882	-6.81	0.32	0.01
80	SLE RA 9	2	163	1862	-6.7	0.91	0
80	SLE RA 10	3	213	2118	-8.69	1.19	0
80	SLE RA 11	1	217	2150	-8.87	0.2	0.01
80	SLE RA 12	2	214	2131	-8.77	0.79	0.01
80	SLE RA 13	3	213	2118	-8.69	1.19	0
80	SLE RA 14	1	217	2150	-8.87	0.2	0.01
80	SLE RA 15	2	214	2131	-8.77	0.79	0.01
80	SLE RA 16	1	217	2150	-8.87	0.2	0.01
80	SLE RA 17	2	214	2131	-8.77	0.79	0.01
80	SLE RA 18	1	238	2265	-9.76	0.15	0.01
80	SLE RA 19	2	236	2246	-9.65	0.74	0.01
80	SLE RA 20	1	238	2265	-9.76	0.15	0.01
80	SLE RA 21	2	236	2246	-9.65	0.74	0.01
80	SLE FR 1	1	166	1882	-6.81	0.32	0.01
80	SLE FR 2	2	165	1875	-6.77	0.52	0.01
80	SLE FR 3	1	166	1882	-6.81	0.32	0.01
80	SLE FR 4	2	187	1990	-7.66	0.47	0.01
80	SLE FR 5	1	187	1997	-7.69	0.27	0.01
80	SLE FR 6	1	202	2073	-8.28	0.23	0.01
80	SLE QP 1	1	166	1882	-6.81	0.32	0.01
80	SLE QP 2	1	187	1997	-7.69	0.27	0.01
80	SLD 1	-1	298	2183	-12.48	-2.03	0.02
80	SLD 2	-1	298	2183	-12.48	-2.03	0.02
80	SLD 3	-5	172	2141	-6.92	-3.65	0.03
80	SLD 4	-5	172	2141	-6.92	-3.65	0.03
80	SLD 5	6	411	2117	-17.57	2.04	0
80	SLD 6	6	411	2117	-17.57	2.04	0
80	SLD 7	-7	-8	1976	0.98	-3.37	0.02
80	SLD 8	-7	-8	1976	0.98	-3.37	0.02
80	SLD 9	9	383	2017	-16.37	3.9	-0.01
80	SLD 10	9	383	2017	-16.37	3.9	-0.01
80	SLD 11	-4	-36	1877	2.18	-1.5	0.02
80	SLD 12	-4	-36	1877	2.18	-1.5	0.02
80	SLD 13	8	203	1852	-8.47	4.19	-0.01
80	SLD 14	8	203	1852	-8.47	4.19	-0.01
80	SLD 15	4	77	1810	-2.9	2.56	0
80	SLD 16	4	77	1810	-2.9	2.56	0
80	SLV 1	-5	448	2438	-19.02	-5.72	0.03
80	SLV 2	-5	448	2438	-19.02	-5.72	0.03
80	SLV 3	-15	152	2338	-5.88	-9.76	0.05
80	SLV 4	-15	152	2338	-5.88	-9.76	0.05
80	SLV 5	14	716	2280	-31.03	4.6	-0.01
80	SLV 6	14	716	2280	-31.03	4.6	-0.01
80	SLV 7	-19	-273	1948	12.79	-8.86	0.05
80	SLV 8	-19	-273	1948	12.79	-8.86	0.05
80	SLV 9	21	648	2045	-28.18	9.4	-0.03
80	SLV 10	21	648	2045	-28.18	9.4	-0.03
80	SLV 11	-12	-341	1713	15.65	-4.06	0.03



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
80	SLV 12	-12	-341	1713	15.65	-4.06	0.03
80	SLV 13	18	223	1655	-9.51	10.29	-0.03
80	SLV 14	18	223	1655	-9.51	10.29	-0.03
80	SLV 15	8	-73	1555	3.64	6.26	-0.02
80	SLV 16	8	-73	1555	3.64	6.26	-0.02
81	SLU 1	0	406	1016	-17.28	0.01	0
81	SLU 2	1	406	1006	-17.29	-0.45	0
81	SLU 3	0	406	1016	-17.28	0.01	0
81	SLU 4	1	406	1010	-17.29	-0.27	0
81	SLU 5	1	406	1006	-17.29	-0.45	0
81	SLU 6	0	406	1016	-17.28	0.01	0
81	SLU 7	1	406	1010	-17.29	-0.27	0
81	SLU 8	0	406	1016	-17.28	0.01	0
81	SLU 9	1	406	1010	-17.29	-0.27	0
81	SLU 10	1	661	1314	-28.31	-0.43	0
81	SLU 11	0	661	1324	-28.3	0.02	0
81	SLU 12	1	661	1318	-28.31	-0.25	0
81	SLU 13	1	661	1314	-28.31	-0.43	0
81	SLU 14	0	661	1324	-28.3	0.02	0
81	SLU 15	1	661	1318	-28.31	-0.25	0
81	SLU 16	0	661	1324	-28.3	0.02	0
81	SLU 17	1	661	1318	-28.31	-0.25	0
81	SLU 18	0	770	1456	-33.02	0.03	0
81	SLU 19	1	770	1450	-33.03	-0.24	0
81	SLU 20	0	770	1456	-33.02	0.03	0
81	SLU 21	1	770	1450	-33.03	-0.24	0
81	SLU 22	0	543	1216	-23.16	0.01	0
81	SLU 23	1	544	1206	-23.17	-0.44	0
81	SLU 24	0	543	1216	-23.16	0.01	0
81	SLU 25	1	544	1210	-23.17	-0.26	0
81	SLU 26	1	544	1206	-23.17	-0.44	0
81	SLU 27	0	543	1216	-23.16	0.01	0
81	SLU 28	1	544	1210	-23.17	-0.26	0
81	SLU 29	0	543	1216	-23.16	0.01	0
81	SLU 30	1	544	1210	-23.17	-0.26	0
81	SLU 31	1	799	1514	-34.19	-0.43	0
81	SLU 32	0	799	1524	-34.18	0.03	0
81	SLU 33	1	799	1518	-34.19	-0.25	0
81	SLU 34	1	799	1514	-34.19	-0.43	0
81	SLU 35	0	799	1524	-34.18	0.03	0
81	SLU 36	1	799	1518	-34.19	-0.25	0
81	SLU 37	0	799	1524	-34.18	0.03	0
81	SLU 38	1	799	1518	-34.19	-0.25	0
81	SLU 39	0	908	1656	-38.9	0.03	0
81	SLU 40	1	908	1650	-38.91	-0.24	0
81	SLU 41	0	908	1656	-38.9	0.03	0
81	SLU 42	1	908	1650	-38.91	-0.24	0
81	SLU 43	0	480	1252	-20.45	0.01	0
81	SLU 44	1	480	1242	-20.46	-0.45	0
81	SLU 45	0	480	1252	-20.45	0.01	0
81	SLU 46	1	480	1246	-20.45	-0.27	0
81	SLU 47	1	480	1242	-20.46	-0.45	0
81	SLU 48	0	480	1252	-20.45	0.01	0
81	SLU 49	1	480	1246	-20.45	-0.27	0
81	SLU 50	0	480	1252	-20.45	0.01	0
81	SLU 51	1	480	1246	-20.45	-0.27	0
81	SLU 52	1	736	1550	-31.48	-0.43	0
81	SLU 53	0	735	1560	-31.47	0.02	0
81	SLU 54	1	735	1554	-31.48	-0.25	0
81	SLU 55	1	736	1550	-31.48	-0.43	0
81	SLU 56	0	735	1560	-31.47	0.02	0
81	SLU 57	1	735	1554	-31.48	-0.25	0
81	SLU 58	0	735	1560	-31.47	0.02	0
81	SLU 59	1	735	1554	-31.48	-0.25	0
81	SLU 60	0	845	1692	-36.19	0.03	0
81	SLU 61	1	845	1686	-36.2	-0.24	0
81	SLU 62	0	845	1692	-36.19	0.03	0
81	SLU 63	1	845	1686	-36.2	-0.24	0
81	SLU 64	0	618	1452	-26.33	0.01	0
81	SLU 65	1	618	1442	-26.34	-0.44	0
81	SLU 66	0	618	1452	-26.33	0.01	0
81	SLU 67	1	618	1446	-26.33	-0.26	0
81	SLU 68	1	618	1442	-26.34	-0.44	0
81	SLU 69	0	618	1452	-26.33	0.01	0
81	SLU 70	1	618	1446	-26.33	-0.26	0
81	SLU 71	0	618	1452	-26.33	0.01	0
81	SLU 72	1	618	1446	-26.33	-0.26	0
81	SLU 73	1	873	1750	-37.36	-0.43	0
81	SLU 74	0	873	1760	-37.35	0.03	0
81	SLU 75	1	873	1754	-37.36	-0.25	0
81	SLU 76	1	873	1750	-37.36	-0.43	0
81	SLU 77	0	873	1760	-37.35	0.03	0
81	SLU 78	1	873	1754	-37.36	-0.25	0
81	SLU 79	0	873	1760	-37.35	0.03	0
81	SLU 80	1	873	1754	-37.36	-0.25	0
81	SLU 81	0	982	1892	-42.07	0.03	0
81	SLU 82	1	983	1886	-42.08	-0.24	0
81	SLU 83	0	982	1892	-42.07	0.03	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
81	SLU 84	1	983	1886	-42.08	-0.24	0
81	SLE RA 1	0	445	1073	-18.96	0.01	0
81	SLE RA 2	1	445	1067	-18.97	-0.3	0
81	SLE RA 3	0	445	1073	-18.96	0.01	0
81	SLE RA 4	1	445	1069	-18.96	-0.17	0
81	SLE RA 5	1	445	1067	-18.97	-0.3	0
81	SLE RA 6	0	445	1073	-18.96	0.01	0
81	SLE RA 7	1	445	1069	-18.96	-0.17	0
81	SLE RA 8	0	445	1073	-18.96	0.01	0
81	SLE RA 9	1	445	1069	-18.96	-0.17	0
81	SLE RA 10	1	615	1272	-26.32	-0.28	0
81	SLE RA 11	0	615	1279	-26.31	0.02	0
81	SLE RA 12	0	615	1275	-26.31	-0.16	0
81	SLE RA 13	1	615	1272	-26.32	-0.28	0
81	SLE RA 14	0	615	1279	-26.31	0.02	0
81	SLE RA 15	0	615	1275	-26.31	-0.16	0
81	SLE RA 16	0	615	1279	-26.31	0.02	0
81	SLE RA 17	0	615	1275	-26.31	-0.16	0
81	SLE RA 18	0	688	1367	-29.46	0.02	0
81	SLE RA 19	0	688	1363	-29.46	-0.16	0
81	SLE RA 20	0	688	1367	-29.46	0.02	0
81	SLE RA 21	0	688	1363	-29.46	-0.16	0
81	SLE FR 1	0	445	1073	-18.96	0.01	0
81	SLE FR 2	0	445	1072	-18.96	-0.05	0
81	SLE FR 3	0	445	1073	-18.96	0.01	0
81	SLE FR 4	0	518	1160	-22.11	-0.05	0
81	SLE FR 5	0	518	1161	-22.11	0.01	0
81	SLE FR 6	0	567	1220	-24.21	0.02	0
81	SLE QP 1	0	445	1073	-18.96	0.01	0
81	SLE QP 2	0	518	1161	-22.11	0.01	0
81	SLD 1	-4	550	1272	-26.47	3.08	0.01
81	SLD 2	-4	550	1272	-26.47	3.08	0.01
81	SLD 3	-7	410	1202	-14.4	2.13	0.02
81	SLD 4	-7	410	1202	-14.4	2.13	0.02
81	SLD 5	3	740	1301	-41.72	2.38	0
81	SLD 6	3	740	1301	-41.72	2.38	0
81	SLD 7	-7	273	1067	-1.49	-0.8	0.01
81	SLD 8	-7	273	1067	-1.49	-0.8	0.01
81	SLD 9	7	762	1255	-42.72	0.82	-0.01
81	SLD 10	7	762	1255	-42.72	0.82	-0.01
81	SLD 11	-3	296	1021	-2.5	-2.35	0
81	SLD 12	-3	296	1021	-2.5	-2.35	0
81	SLD 13	7	626	1120	-29.81	-2.11	-0.02
81	SLD 14	7	626	1120	-29.81	-2.11	-0.02
81	SLD 15	4	486	1050	-17.75	-3.06	-0.01
81	SLD 16	4	486	1050	-17.75	-3.06	-0.01
81	SLV 1	-14	600	1425	-33.43	9.08	0.04
81	SLV 2	-14	600	1425	-33.43	9.08	0.04
81	SLV 3	-21	258	1259	-2.84	6.68	0.06
81	SLV 4	-21	258	1259	-2.84	6.68	0.06
81	SLV 5	7	1061	1493	-71.89	6.37	0
81	SLV 6	7	1061	1493	-71.89	6.37	0
81	SLV 7	-18	-79	938	30.06	-1.63	0.03
81	SLV 8	-18	-79	938	30.06	-1.63	0.03
81	SLV 9	18	1115	1384	-74.27	1.65	-0.03
81	SLV 10	18	1115	1384	-74.27	1.65	-0.03
81	SLV 11	-7	-25	829	27.67	-6.35	0
81	SLV 12	-7	-25	829	27.67	-6.35	0
81	SLV 13	21	778	1064	-41.37	-6.65	-0.06
81	SLV 14	21	778	1064	-41.37	-6.65	-0.06
81	SLV 15	14	436	897	-10.79	-9.05	-0.04
81	SLV 16	14	436	897	-10.79	-9.05	-0.04
82	SLU 1	-4	18	2173	-1.15	-2.26	-0.01
82	SLU 2	-4	19	2207	-1.19	-2.61	-0.01
82	SLU 3	-4	18	2173	-1.15	-2.26	-0.01
82	SLU 4	-4	18	2194	-1.17	-2.47	-0.01
82	SLU 5	-4	19	2207	-1.19	-2.61	-0.01
82	SLU 6	-4	18	2173	-1.15	-2.26	-0.01
82	SLU 7	-4	18	2194	-1.17	-2.47	-0.01
82	SLU 8	-4	18	2173	-1.15	-2.26	-0.01
82	SLU 9	-4	18	2194	-1.17	-2.47	-0.01
82	SLU 10	-7	-45	2566	1.77	-4.69	-0.01
82	SLU 11	-8	-46	2531	1.81	-4.35	-0.01
82	SLU 12	-7	-46	2552	1.79	-4.56	-0.01
82	SLU 13	-7	-45	2566	1.77	-4.69	-0.01
82	SLU 14	-8	-46	2531	1.81	-4.35	-0.01
82	SLU 15	-7	-46	2552	1.79	-4.56	-0.01
82	SLU 16	-8	-46	2531	1.81	-4.35	-0.01
82	SLU 17	-7	-46	2552	1.79	-4.56	-0.01
82	SLU 18	-9	-74	2685	3.08	-5.24	-0.01
82	SLU 19	-9	-73	2705	3.06	-5.45	-0.01
82	SLU 20	-9	-74	2685	3.08	-5.24	-0.01
82	SLU 21	-9	-73	2705	3.06	-5.45	-0.01
82	SLU 22	-6	-2	2368	-0.23	-3.16	-0.01
82	SLU 23	-5	-1	2402	-0.27	-3.5	-0.01
82	SLU 24	-6	-2	2368	-0.23	-3.16	-0.01
82	SLU 25	-6	-2	2388	-0.26	-3.36	-0.01
82	SLU 26	-5	-1	2402	-0.27	-3.5	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
82	SLU 27	-6	-2	2368	-0.23	-3.16	-0.01
82	SLU 28	-6	-2	2388	-0.26	-3.36	-0.01
82	SLU 29	-6	-2	2368	-0.23	-3.16	-0.01
82	SLU 30	-6	-2	2388	-0.26	-3.36	-0.01
82	SLU 31	-9	-65	2760	2.69	-5.59	-0.01
82	SLU 32	-9	-66	2726	2.73	-5.25	-0.01
82	SLU 33	-9	-66	2747	2.7	-5.45	-0.01
82	SLU 34	-9	-65	2760	2.69	-5.59	-0.01
82	SLU 35	-9	-66	2726	2.73	-5.25	-0.01
82	SLU 36	-9	-66	2747	2.7	-5.45	-0.01
82	SLU 37	-9	-66	2726	2.73	-5.25	-0.01
82	SLU 38	-9	-66	2747	2.7	-5.45	-0.01
82	SLU 39	-11	-94	2880	3.99	-6.14	-0.01
82	SLU 40	-10	-93	2900	3.97	-6.35	-0.01
82	SLU 41	-11	-94	2880	3.99	-6.14	-0.01
82	SLU 42	-10	-93	2900	3.97	-6.35	-0.01
82	SLU 43	-5	30	2758	-1.81	-2.63	-0.01
82	SLU 44	-5	31	2792	-1.84	-2.98	-0.01
82	SLU 45	-5	30	2758	-1.81	-2.63	-0.01
82	SLU 46	-5	31	2779	-1.83	-2.84	-0.01
82	SLU 47	-5	31	2792	-1.84	-2.98	-0.01
82	SLU 48	-5	30	2758	-1.81	-2.63	-0.01
82	SLU 49	-5	31	2779	-1.83	-2.84	-0.01
82	SLU 50	-5	30	2758	-1.81	-2.63	-0.01
82	SLU 51	-5	31	2779	-1.83	-2.84	-0.01
82	SLU 52	-8	-33	3151	1.11	-5.06	-0.01
82	SLU 53	-8	-34	3116	1.15	-4.72	-0.01
82	SLU 54	-8	-34	3137	1.13	-4.93	-0.01
82	SLU 55	-8	-33	3151	1.11	-5.06	-0.01
82	SLU 56	-8	-34	3116	1.15	-4.72	-0.01
82	SLU 57	-8	-34	3137	1.13	-4.93	-0.01
82	SLU 58	-8	-34	3116	1.15	-4.72	-0.01
82	SLU 59	-8	-34	3137	1.13	-4.93	-0.01
82	SLU 60	-10	-62	3270	2.42	-5.62	-0.01
82	SLU 61	-10	-61	3291	2.4	-5.82	-0.01
82	SLU 62	-10	-62	3270	2.42	-5.62	-0.01
82	SLU 63	-10	-61	3291	2.4	-5.82	-0.01
82	SLU 64	-6	10	2953	-0.89	-3.53	-0.01
82	SLU 65	-6	11	2987	-0.93	-3.87	-0.01
82	SLU 66	-6	10	2953	-0.89	-3.53	-0.01
82	SLU 67	-6	11	2973	-0.91	-3.73	-0.01
82	SLU 68	-6	11	2987	-0.93	-3.87	-0.01
82	SLU 69	-6	10	2953	-0.89	-3.53	-0.01
82	SLU 70	-6	11	2973	-0.91	-3.73	-0.01
82	SLU 71	-6	10	2953	-0.89	-3.53	-0.01
82	SLU 72	-6	11	2973	-0.91	-3.73	-0.01
82	SLU 73	-10	-53	3346	2.03	-5.96	-0.01
82	SLU 74	-10	-54	3311	2.07	-5.62	-0.01
82	SLU 75	-10	-54	3332	2.04	-5.82	-0.01
82	SLU 76	-10	-53	3346	2.03	-5.96	-0.01
82	SLU 77	-10	-54	3311	2.07	-5.62	-0.01
82	SLU 78	-10	-54	3332	2.04	-5.82	-0.01
82	SLU 79	-10	-54	3311	2.07	-5.62	-0.01
82	SLU 80	-10	-54	3332	2.04	-5.82	-0.01
82	SLU 81	-11	-82	3465	3.33	-6.51	-0.01
82	SLU 82	-11	-81	3485	3.31	-6.72	-0.02
82	SLU 83	-11	-82	3465	3.33	-6.51	-0.01
82	SLU 84	-11	-81	3485	3.31	-6.72	-0.02
82	SLE RA 1	-5	12	2229	-0.89	-2.52	-0.01
82	SLE RA 2	-4	13	2251	-0.91	-2.75	-0.01
82	SLE RA 3	-5	12	2229	-0.89	-2.52	-0.01
82	SLE RA 4	-5	13	2242	-0.9	-2.65	-0.01
82	SLE RA 5	-4	13	2251	-0.91	-2.75	-0.01
82	SLE RA 6	-5	12	2229	-0.89	-2.52	-0.01
82	SLE RA 7	-5	13	2242	-0.9	-2.65	-0.01
82	SLE RA 8	-5	12	2229	-0.89	-2.52	-0.01
82	SLE RA 9	-5	13	2242	-0.9	-2.65	-0.01
82	SLE RA 10	-7	-30	2490	1.06	-4.14	-0.01
82	SLE RA 11	-7	-31	2468	1.09	-3.91	-0.01
82	SLE RA 12	-7	-30	2481	1.07	-4.05	-0.01
82	SLE RA 13	-7	-30	2490	1.06	-4.14	-0.01
82	SLE RA 14	-7	-31	2468	1.09	-3.91	-0.01
82	SLE RA 15	-7	-30	2481	1.07	-4.05	-0.01
82	SLE RA 16	-7	-31	2468	1.09	-3.91	-0.01
82	SLE RA 17	-7	-30	2481	1.07	-4.05	-0.01
82	SLE RA 18	-8	-49	2570	1.93	-4.51	-0.01
82	SLE RA 19	-8	-49	2584	1.92	-4.64	-0.01
82	SLE RA 20	-8	-49	2570	1.93	-4.51	-0.01
82	SLE RA 21	-8	-49	2584	1.92	-4.64	-0.01
82	SLE FR 1	-5	12	2229	-0.89	-2.52	-0.01
82	SLE FR 2	-5	12	2233	-0.89	-2.56	-0.01
82	SLE FR 3	-5	12	2229	-0.89	-2.52	-0.01
82	SLE FR 4	-6	-6	2336	-0.05	-3.16	-0.01
82	SLE FR 5	-6	-6	2331	-0.04	-3.11	-0.01
82	SLE FR 6	-6	-18	2399	0.52	-3.51	-0.01
82	SLE QP 1	-5	12	2229	-0.89	-2.52	-0.01
82	SLE QP 2	-6	-6	2331	-0.04	-3.11	-0.01
82	SLD 1	-9	128	2133	-6.08	5.45	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
82	SLD 2	-9	128	2133	-6.08	5.45	0.01
82	SLD 3	-11	-22	2015	0.79	4.06	0.02
82	SLD 4	-11	-22	2015		4.06	0.02
82	SLD 5	-4	261	2451	-12.27	1.56	-0.01
82	SLD 6	-4	261	2451	-12.27	1.56	-0.01
82	SLD 7	-10	-238	2057	10.62	-3.07	0
82	SLD 8	-10	-238	2057	10.62	-3.07	0
82	SLD 9	-1	226	2605	-10.7	-3.15	-0.02
82	SLD 10	-1	226	2605	-10.7	-3.15	-0.02
82	SLD 11	-7	-274	2211	12.18	-7.79	-0.01
82	SLD 12	-7	-274	2211	12.18	-7.79	-0.01
82	SLD 13	0	10	2647	-0.87	-10.28	-0.03
82	SLD 14	0	10	2647	-0.87	-10.28	-0.03
82	SLD 15	-2	-140	2529	6	-11.67	-0.03
82	SLD 16	-2	-140	2529	6	-11.67	-0.03
82	SLV 1	-15	310	1870	-14.32	18.85	0.05
82	SLV 2	-15	310	1870	-14.32	18.85	0.05
82	SLV 3	-20	-44	1586	1.86	15.41	0.06
82	SLV 4	-20	-44	1586	1.86	15.41	0.06
82	SLV 5	-2	625	2623	-28.86	8.69	0
82	SLV 6	-2	625	2623	-28.86	8.69	0
82	SLV 7	-16	-553	1678	25.07	-2.77	0.02
82	SLV 8	-16	-553	1678	25.07	-2.77	0.02
82	SLV 9	5	541	2984	-25.15	-3.46	-0.04
82	SLV 10	5	541	2984	-25.15	-3.46	-0.04
82	SLV 11	-9	-637	2039	28.78	-14.91	-0.01
82	SLV 12	-9	-637	2039	28.78	-14.91	-0.01
82	SLV 13	8	32	3076	-1.95	-21.64	-0.07
82	SLV 14	8	32	3076	-1.95	-21.64	-0.07
82	SLV 15	4	-322	2792	14.23	-25.07	-0.06
82	SLV 16	4	-322	2792	14.23	-25.07	-0.06
83	SLU 1	0	122	1895	-5.02	0.01	0
83	SLU 2	5	117	1845	-4.86	2.66	-0.01
83	SLU 3	0	122	1895	-5.02	0.01	0
83	SLU 4	3	119	1865	-4.93	1.6	-0.01
83	SLU 5	5	117	1845	-4.86	2.66	-0.01
83	SLU 6	0	122	1895	-5.02	0.01	0
83	SLU 7	3	119	1865	-4.93	1.6	-0.01
83	SLU 8	0	122	1895	-5.02	0.01	0
83	SLU 9	3	119	1865	-4.93	1.6	-0.01
83	SLU 10	5	172	2293	-7.03	2.36	-0.01
83	SLU 11	-1	177	2342	-7.18	-0.28	0
83	SLU 12	2	174	2313	-7.09	1.3	0
83	SLU 13	5	172	2293	-7.03	2.36	-0.01
83	SLU 14	-1	177	2342	-7.18	-0.28	0
83	SLU 15	2	174	2313	-7.09	1.3	0
83	SLU 16	-1	177	2342	-7.18	-0.28	0
83	SLU 17	2	174	2313	-7.09	1.3	0
83	SLU 18	-1	200	2534	-8.11	-0.41	0
83	SLU 19	2	197	2504	-8.02	1.18	0
83	SLU 20	-1	200	2534	-8.11	-0.41	0
83	SLU 21	2	197	2504	-8.02	1.18	0
83	SLU 22	-1	150	2123	-6.14	-0.09	0
83	SLU 23	5	145	2073	-5.98	2.55	-0.01
83	SLU 24	-1	150	2123	-6.14	-0.09	0
83	SLU 25	3	147	2093	-6.04	1.5	-0.01
83	SLU 26	5	145	2073	-5.98	2.55	-0.01
83	SLU 27	-1	150	2123	-6.14	-0.09	0
83	SLU 28	3	147	2093	-6.04	1.5	-0.01
83	SLU 29	-1	150	2123	-6.14	-0.09	0
83	SLU 30	3	147	2093	-6.04	1.5	-0.01
83	SLU 31	4	199	2521	-8.14	2.26	-0.01
83	SLU 32	-1	204	2571	-8.3	-0.38	0
83	SLU 33	2	201	2541	-8.21	1.2	0
83	SLU 34	4	199	2521	-8.14	2.26	-0.01
83	SLU 35	-1	204	2571	-8.3	-0.38	0
83	SLU 36	2	201	2541	-8.21	1.2	0
83	SLU 37	-1	204	2571	-8.3	-0.38	0
83	SLU 38	2	201	2541	-8.21	1.2	0
83	SLU 39	-2	228	2762	-9.23	-0.51	0
83	SLU 40	2	225	2733	-9.13	1.08	0
83	SLU 41	-2	228	2762	-9.23	-0.51	0
83	SLU 42	2	225	2733	-9.13	1.08	0
83	SLU 43	0	149	2385	-6.15	0.05	0
83	SLU 44	5	144	2335	-5.99	2.69	-0.01
83	SLU 45	0	149	2385	-6.15	0.05	0
83	SLU 46	3	146	2355	-6.05	1.64	-0.01
83	SLU 47	5	144	2335	-5.99	2.69	-0.01
83	SLU 48	0	149	2385	-6.15	0.05	0
83	SLU 49	3	146	2355	-6.05	1.64	-0.01
83	SLU 50	0	149	2385	-6.15	0.05	0
83	SLU 51	3	146	2355	-6.05	1.64	-0.01
83	SLU 52	5	199	2783	-8.15	2.4	-0.01
83	SLU 53	-1	204	2833	-8.31	-0.25	0
83	SLU 54	2	201	2803	-8.21	1.34	-0.01
83	SLU 55	5	199	2783	-8.15	2.4	-0.01
83	SLU 56	-1	204	2833	-8.31	-0.25	0
83	SLU 57	2	201	2803	-8.21	1.34	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
83	SLU 58	-1	204	2833	-8.31	-0.25	0
83	SLU 59	2	201	2803	-8.21	1.34	-0.01
83	SLU 60	-1	227	3024	-9.23	-0.37	0
83	SLU 61	2	224	2995	-9.14	1.21	-0.01
83	SLU 62	-1	227	3024	-9.23	-0.37	0
83	SLU 63	2	224	2995	-9.14	1.21	-0.01
83	SLU 64	-1	177	2613	-7.26	-0.05	0
83	SLU 65	5	172	2563	-7.1	2.59	-0.01
83	SLU 66	-1	177	2613	-7.26	-0.05	0
83	SLU 67	3	174	2583	-7.17	1.54	-0.01
83	SLU 68	5	172	2563	-7.1	2.59	-0.01
83	SLU 69	-1	177	2613	-7.26	-0.05	0
83	SLU 70	3	174	2583	-7.17	1.54	-0.01
83	SLU 71	-1	177	2613	-7.26	-0.05	0
83	SLU 72	3	174	2583	-7.17	1.54	-0.01
83	SLU 73	4	227	3011	-9.27	2.3	-0.01
83	SLU 74	-1	231	3061	-9.42	-0.35	0
83	SLU 75	2	229	3031	-9.33	1.24	-0.01
83	SLU 76	4	227	3011	-9.27	2.3	-0.01
83	SLU 77	-1	231	3061	-9.42	-0.35	0
83	SLU 78	2	229	3031	-9.33	1.24	-0.01
83	SLU 79	-1	231	3061	-9.42	-0.35	0
83	SLU 80	2	229	3031	-9.33	1.24	-0.01
83	SLU 81	-2	255	3253	-10.35	-0.47	0
83	SLU 82	2	252	3223	-10.26	1.11	-0.01
83	SLU 83	-2	255	3253	-10.35	-0.47	0
83	SLU 84	2	252	3223	-10.26	1.11	-0.01
83	SLE RA 1	0	130	1960	-5.34	-0.02	0
83	SLE RA 2	3	127	1927	-5.24	1.75	-0.01
83	SLE RA 3	0	130	1960	-5.34	-0.02	0
83	SLE RA 4	2	128	1940	-5.28	1.04	0
83	SLE RA 5	3	127	1927	-5.24	1.75	-0.01
83	SLE RA 6	0	130	1960	-5.34	-0.02	0
83	SLE RA 7	2	128	1940	-5.28	1.04	0
83	SLE RA 8	0	130	1960	-5.34	-0.02	0
83	SLE RA 9	2	128	1940	-5.28	1.04	0
83	SLE RA 10	3	163	2225	-6.68	1.55	-0.01
83	SLE RA 11	-1	166	2258	-6.78	-0.21	0
83	SLE RA 12	1	164	2238	-6.72	0.84	0
83	SLE RA 13	3	163	2225	-6.68	1.55	-0.01
83	SLE RA 14	-1	166	2258	-6.78	-0.21	0
83	SLE RA 15	1	164	2238	-6.72	0.84	0
83	SLE RA 16	-1	166	2258	-6.78	-0.21	0
83	SLE RA 17	1	164	2238	-6.72	0.84	0
83	SLE RA 18	-1	182	2386	-7.4	-0.3	0
83	SLE RA 19	1	180	2366	-7.34	0.76	0
83	SLE RA 20	-1	182	2386	-7.4	-0.3	0
83	SLE RA 21	1	180	2366	-7.34	0.76	0
83	SLE FR 1	0	130	1960	-5.34	-0.02	0
83	SLE FR 2	0	129	1953	-5.32	0.34	0
83	SLE FR 3	0	130	1960	-5.34	-0.02	0
83	SLE FR 4	0	145	2081	-5.94	0.25	0
83	SLE FR 5	-1	146	2088	-5.96	-0.1	0
83	SLE FR 6	-1	156	2173	-6.37	-0.16	0
83	SLE QP 1	0	130	1960	-5.34	-0.02	0
83	SLE QP 2	-1	146	2088	-5.96	-0.1	0
83	SLD 1	-10	249	2235	-10.39	-4.79	0.02
83	SLD 2	-10	249	2235	-10.39	-4.79	0.02
83	SLD 3	-15	128	2202	-5.1	-7.46	0.02
83	SLD 4	-15	128	2202	-5.1	-7.46	0.02
83	SLD 5	5	361	2182	-15.3	2.54	0.02
83	SLD 6	5	361	2182	-15.3	2.54	0.02
83	SLD 7	-14	-44	2072	2.32	-6.35	-0.01
83	SLD 8	-14	-44	2072	2.32	-6.35	-0.01
83	SLD 9	13	335	2103	-14.23	6.15	0.01
83	SLD 10	13	335	2103	-14.23	6.15	0.01
83	SLD 11	-7	-70	1994	3.39	-2.74	-0.02
83	SLD 12	-7	-70	1994	3.39	-2.74	-0.02
83	SLD 13	14	164	1973	-6.81	7.26	-0.02
83	SLD 14	14	164	1973	-6.81	7.26	-0.02
83	SLD 15	8	42	1941	-1.53	4.59	-0.03
83	SLD 16	8	42	1941	-1.53	4.59	-0.03
83	SLV 1	-24	392	2440	-16.46	-12.38	0.06
83	SLV 2	-24	392	2440	-16.46	-12.38	0.06
83	SLV 3	-38	104	2362	-3.97	-18.92	0.04
83	SLV 4	-38	104	2362	-3.97	-18.92	0.04
83	SLV 5	14	655	2311	-28.05	6.14	0.05
83	SLV 6	14	655	2311	-28.05	6.14	0.05
83	SLV 7	-34	-302	2052	13.58	-15.67	-0.02
83	SLV 8	-34	-302	2052	13.58	-15.67	-0.02
83	SLV 9	32	594	2123	-25.5	15.47	0.02
83	SLV 10	32	594	2123	-25.5	15.47	0.02
83	SLV 11	-15	-364	1865	16.13	-6.34	-0.05
83	SLV 12	-15	-364	1865	16.13	-6.34	-0.05
83	SLV 13	37	187	1814	-7.95	18.72	-0.05
83	SLV 14	37	187	1814	-7.95	18.72	-0.05
83	SLV 15	23	-100	1736	4.54	12.18	-0.07
83	SLV 16	23	-100	1736	4.54	12.18	-0.07



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
84	SLU 1	0	367	1154	-13.93	0.03	0
84	SLU 2	1	366	1148	-13.87	-1.31	0
84	SLU 3	0	367	1154	-13.93	0.03	0
84	SLU 4	1	366	1150	-13.89	-0.77	0
84	SLU 5	1	366	1148	-13.87	-1.31	0
84	SLU 6	0	367	1154	-13.93	0.03	0
84	SLU 7	1	366	1150	-13.89	-0.77	0
84	SLU 8	0	367	1154	-13.93	0.03	0
84	SLU 9	1	366	1150	-13.89	-0.77	0
84	SLU 10	1	625	1568	-23.37	-1.23	0
84	SLU 11	0	626	1574	-23.44	0.11	0
84	SLU 12	1	625	1571	-23.4	-0.7	0
84	SLU 13	1	625	1568	-23.37	-1.23	0
84	SLU 14	0	626	1574	-23.44	0.11	0
84	SLU 15	1	625	1571	-23.4	-0.7	0
84	SLU 16	0	626	1574	-23.44	0.11	0
84	SLU 17	1	625	1571	-23.4	-0.7	0
84	SLU 18	0	737	1754	-27.51	0.14	0
84	SLU 19	1	736	1751	-27.47	-0.66	0
84	SLU 20	0	737	1754	-27.51	0.14	0
84	SLU 21	1	736	1751	-27.47	-0.66	0
84	SLU 22	0	502	1411	-18.98	0.06	0
84	SLU 23	1	501	1404	-18.91	-1.28	0
84	SLU 24	0	502	1411	-18.98	0.06	0
84	SLU 25	1	501	1407	-18.94	-0.74	0
84	SLU 26	1	501	1404	-18.91	-1.28	0
84	SLU 27	0	502	1411	-18.98	0.06	0
84	SLU 28	1	501	1407	-18.94	-0.74	0
84	SLU 29	0	502	1411	-18.98	0.06	0
84	SLU 30	1	501	1407	-18.94	-0.74	0
84	SLU 31	1	760	1824	-28.41	-1.2	0
84	SLU 32	0	760	1831	-28.48	0.14	0
84	SLU 33	1	760	1827	-28.44	-0.67	0
84	SLU 34	1	760	1824	-28.41	-1.2	0
84	SLU 35	0	760	1831	-28.48	0.14	0
84	SLU 36	1	760	1827	-28.44	-0.67	0
84	SLU 37	0	760	1831	-28.48	0.14	0
84	SLU 38	1	760	1827	-28.44	-0.67	0
84	SLU 39	0	871	2011	-32.55	0.17	0
84	SLU 40	1	871	2007	-32.51	-0.63	0
84	SLU 41	0	871	2011	-32.55	0.17	0
84	SLU 42	1	871	2007	-32.51	-0.63	0
84	SLU 43	0	431	1413	-16.38	0.03	0
84	SLU 44	1	430	1406	-16.32	-1.31	0
84	SLU 45	0	431	1413	-16.38	0.03	0
84	SLU 46	1	430	1409	-16.35	-0.77	0
84	SLU 47	1	430	1406	-16.32	-1.31	0
84	SLU 48	0	431	1413	-16.38	0.03	0
84	SLU 49	1	430	1409	-16.35	-0.77	0
84	SLU 50	0	431	1413	-16.38	0.03	0
84	SLU 51	1	430	1409	-16.35	-0.77	0
84	SLU 52	1	689	1826	-25.82	-1.23	0
84	SLU 53	0	690	1833	-25.89	0.11	0
84	SLU 54	1	689	1829	-25.85	-0.7	0
84	SLU 55	1	689	1826	-25.82	-1.23	0
84	SLU 56	0	690	1833	-25.89	0.11	0
84	SLU 57	1	689	1829	-25.85	-0.7	0
84	SLU 58	0	690	1833	-25.89	0.11	0
84	SLU 59	1	689	1829	-25.85	-0.7	0
84	SLU 60	0	801	2013	-29.96	0.14	0
84	SLU 61	1	800	2009	-29.92	-0.66	0
84	SLU 62	0	801	2013	-29.96	0.14	0
84	SLU 63	1	800	2009	-29.92	-0.66	0
84	SLU 64	0	565	1669	-21.43	0.06	0
84	SLU 65	1	565	1663	-21.36	-1.28	0
84	SLU 66	0	565	1669	-21.43	0.06	0
84	SLU 67	1	565	1665	-21.39	-0.74	0
84	SLU 68	1	565	1663	-21.36	-1.28	0
84	SLU 69	0	565	1669	-21.43	0.06	0
84	SLU 70	1	565	1665	-21.39	-0.74	0
84	SLU 71	0	565	1669	-21.43	0.06	0
84	SLU 72	1	565	1665	-21.39	-0.74	0
84	SLU 73	1	824	2083	-30.87	-1.2	0
84	SLU 74	0	824	2089	-30.93	0.14	0
84	SLU 75	1	824	2085	-30.89	-0.67	0
84	SLU 76	1	824	2083	-30.87	-1.2	0
84	SLU 77	0	824	2089	-30.93	0.14	0
84	SLU 78	1	824	2085	-30.89	-0.67	0
84	SLU 79	0	824	2089	-30.93	0.14	0
84	SLU 80	1	824	2085	-30.89	-0.67	0
84	SLU 81	0	935	2269	-35	0.17	0
84	SLU 82	1	935	2265	-34.96	-0.63	0
84	SLU 83	0	935	2269	-35	0.17	0
84	SLU 84	1	935	2265	-34.96	-0.63	0
84	SLE RA 1	0	405	1228	-15.37	0.04	0
84	SLE RA 2	1	405	1223	-15.33	-0.85	0
84	SLE RA 3	0	405	1228	-15.37	0.04	0
84	SLE RA 4	1	405	1225	-15.35	-0.49	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione		
		x	y	z		x	y	z
84	SLE RA 5	1	405	1223		-15.33	-0.85	0
84	SLE RA 6	0	405	1228		-15.37	0.04	0
84	SLE RA 7	1	405	1225		-15.35	-0.49	0
84	SLE RA 8	0	405	1228		-15.37	0.04	0
84	SLE RA 9	1	405	1225		-15.35	-0.49	0
84	SLE RA 10	1	577	1503		-21.67	-0.8	0
84	SLE RA 11	0	578	1508		-21.71	0.09	0
84	SLE RA 12	0	578	1505		-21.68	-0.44	0
84	SLE RA 13	1	577	1503		-21.67	-0.8	0
84	SLE RA 14	0	578	1508		-21.71	0.09	0
84	SLE RA 15	0	578	1505		-21.68	-0.44	0
84	SLE RA 16	0	578	1508		-21.71	0.09	0
84	SLE RA 17	0	578	1505		-21.68	-0.44	0
84	SLE RA 18	0	652	1628		-24.43	0.11	0
84	SLE RA 19	0	652	1625		-24.4	-0.42	0
84	SLE RA 20	0	652	1628		-24.43	0.11	0
84	SLE RA 21	0	652	1625		-24.4	-0.42	0
84	SLE FR 1	0	405	1228		-15.37	0.04	0
84	SLE FR 2	0	405	1227		-15.37	-0.14	0
84	SLE FR 3	0	405	1228		-15.37	0.04	0
84	SLE FR 4	0	479	1347		-18.08	-0.12	0
84	SLE FR 5	0	479	1348		-18.09	0.06	0
84	SLE FR 6	0	529	1428		-19.9	0.08	0
84	SLE QP 1	0	405	1228		-15.37	0.04	0
84	SLE QP 2	0	479	1348		-18.09	0.06	0
84	SLD 1	-3	376	1415		-10.41	7.81	-0.01
84	SLD 2	-3	376	1415		-10.41	7.81	-0.01
84	SLD 3	-7	506	1375		-22.43	6.37	-0.01
84	SLD 4	-7	506	1375		-22.43	6.37	-0.01
84	SLD 5	4	250	1428		2.44	4.58	-0.01
84	SLD 6	4	250	1428		2.44	4.58	-0.01
84	SLD 7	-7	685	1295		-37.62	-0.24	0
84	SLD 8	-7	685	1295		-37.62	-0.24	0
84	SLD 9	7	273	1400		1.44	0.36	0
84	SLD 10	7	273	1400		1.44	0.36	0
84	SLD 11	-4	708	1267		-38.62	-4.45	0.01
84	SLD 12	-4	708	1267		-38.62	-4.45	0.01
84	SLD 13	6	452	1321		-13.75	-6.24	0.01
84	SLD 14	6	452	1321		-13.75	-6.24	0.01
84	SLD 15	3	583	1281		-25.77	-7.69	0.01
84	SLD 16	3	583	1281		-25.77	-7.69	0.01
84	SLV 1	-10	231	1507		1.1	23.45	-0.03
84	SLV 2	-10	231	1507		1.1	23.45	-0.03
84	SLV 3	-19	546	1412		-29.34	19.8	-0.02
84	SLV 4	-19	546	1412		-29.34	19.8	-0.02
84	SLV 5	9	-72	1538		33.82	12.61	-0.02
84	SLV 6	9	-72	1538		33.82	12.61	-0.02
84	SLV 7	-18	977	1224		-67.62	0.45	0
84	SLV 8	-18	977	1224		-67.62	0.45	0
84	SLV 9	18	-18	1471		31.44	-0.33	0
84	SLV 10	18	-18	1471		31.44	-0.33	0
84	SLV 11	-10	1031	1157		-70	-12.48	0.02
84	SLV 12	-10	1031	1157		-70	-12.48	0.02
84	SLV 13	19	412	1283		-6.84	-19.68	0.02
84	SLV 14	19	412	1283		-6.84	-19.68	0.02
84	SLV 15	10	727	1189		-37.27	-23.32	0.03
84	SLV 16	10	727	1189		-37.27	-23.32	0.03
85	SLU 1	-2	37	2060		-2.56	-1.72	0
85	SLU 2	-2	36	2094		-2.5	-2.5	0
85	SLU 3	-2	37	2060		-2.56	-1.72	0
85	SLU 4	-2	36	2080		-2.52	-2.19	0
85	SLU 5	-2	36	2094		-2.5	-2.5	0
85	SLU 6	-2	37	2060		-2.56	-1.72	0
85	SLU 7	-2	36	2080		-2.52	-2.19	0
85	SLU 8	-2	37	2060		-2.56	-1.72	0
85	SLU 9	-2	36	2080		-2.52	-2.19	0
85	SLU 10	-4	21	2337		-3.12	-4.2	0
85	SLU 11	-4	23	2303		-3.18	-3.42	0
85	SLU 12	-4	22	2323		-3.14	-3.89	0
85	SLU 13	-4	21	2337		-3.12	-4.2	0
85	SLU 14	-4	23	2303		-3.18	-3.42	0
85	SLU 15	-4	22	2323		-3.14	-3.89	0
85	SLU 16	-4	23	2303		-3.18	-3.42	0
85	SLU 17	-4	22	2323		-3.14	-3.89	0
85	SLU 18	-5	17	2407		-3.44	-4.15	0
85	SLU 19	-5	16	2427		-3.41	-4.62	0
85	SLU 20	-5	17	2407		-3.44	-4.15	0
85	SLU 21	-5	16	2427		-3.41	-4.62	0
85	SLU 22	-3	37	2209		-3.04	-2.45	0
85	SLU 23	-2	35	2242		-2.98	-3.22	0
85	SLU 24	-3	37	2209		-3.04	-2.45	0
85	SLU 25	-3	36	2229		-3	-2.91	0
85	SLU 26	-2	35	2242		-2.98	-3.22	0
85	SLU 27	-3	37	2209		-3.04	-2.45	0
85	SLU 28	-3	36	2229		-3	-2.91	0
85	SLU 29	-3	37	2209		-3.04	-2.45	0
85	SLU 30	-3	36	2229		-3	-2.91	0
85	SLU 31	-4	21	2485		-3.6	-4.93	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione		
		x	y	z		x	y	z
85	SLU 32	-5	22	2451		-3.66	-4.15	0
85	SLU 33	-5	22	2472		-3.62	-4.62	0
85	SLU 34	-4	21	2485		-3.6	-4.93	0
85	SLU 35	-5	22	2451		-3.66	-4.15	0
85	SLU 36	-5	22	2472		-3.62	-4.62	0
85	SLU 37	-5	22	2451		-3.66	-4.15	0
85	SLU 38	-5	22	2472		-3.62	-4.62	0
85	SLU 39	-6	16	2556		-3.92	-4.88	0
85	SLU 40	-5	15	2576		-3.89	-5.35	0
85	SLU 41	-6	16	2556		-3.92	-4.88	0
85	SLU 42	-5	15	2576		-3.89	-5.35	0
85	SLU 43	-2	49	2627		-3.17	-1.98	0
85	SLU 44	-2	47	2661		-3.1	-2.76	0
85	SLU 45	-2	49	2627		-3.17	-1.98	0
85	SLU 46	-2	48	2647		-3.13	-2.45	0
85	SLU 47	-2	47	2661		-3.1	-2.76	0
85	SLU 48	-2	49	2627		-3.17	-1.98	0
85	SLU 49	-2	48	2647		-3.13	-2.45	0
85	SLU 50	-2	49	2627		-3.17	-1.98	0
85	SLU 51	-2	48	2647		-3.13	-2.45	0
85	SLU 52	-4	33	2904		-3.72	-4.47	0
85	SLU 53	-4	34	2870		-3.78	-3.69	0
85	SLU 54	-4	33	2890		-3.75	-4.16	0
85	SLU 55	-4	33	2904		-3.72	-4.47	0
85	SLU 56	-4	34	2870		-3.78	-3.69	0
85	SLU 57	-4	33	2890		-3.75	-4.16	0
85	SLU 58	-4	34	2870		-3.78	-3.69	0
85	SLU 59	-4	33	2890		-3.75	-4.16	0
85	SLU 60	-5	28	2974		-4.05	-4.42	0
85	SLU 61	-5	27	2995		-4.01	-4.89	0
85	SLU 62	-5	28	2974		-4.05	-4.42	0
85	SLU 63	-5	27	2995		-4.01	-4.89	0
85	SLU 64	-3	48	2776		-3.64	-2.71	0
85	SLU 65	-3	47	2810		-3.58	-3.49	0
85	SLU 66	-3	48	2776		-3.64	-2.71	0
85	SLU 67	-3	47	2796		-3.61	-3.18	0
85	SLU 68	-3	47	2810		-3.58	-3.49	0
85	SLU 69	-3	48	2776		-3.64	-2.71	0
85	SLU 70	-3	47	2796		-3.61	-3.18	0
85	SLU 71	-3	48	2776		-3.64	-2.71	0
85	SLU 72	-3	47	2796		-3.61	-3.18	0
85	SLU 73	-5	32	3053		-4.2	-5.19	0
85	SLU 74	-5	34	3019		-4.26	-4.42	0
85	SLU 75	-5	33	3039		-4.22	-4.88	0
85	SLU 76	-5	32	3053		-4.2	-5.19	0
85	SLU 77	-5	34	3019		-4.26	-4.42	0
85	SLU 78	-5	33	3039		-4.22	-4.88	0
85	SLU 79	-5	34	3019		-4.26	-4.42	0
85	SLU 80	-5	33	3039		-4.22	-4.88	0
85	SLU 81	-6	28	3123		-4.53	-5.15	0
85	SLU 82	-6	27	3143		-4.49	-5.61	0
85	SLU 83	-6	28	3123		-4.53	-5.15	0
85	SLU 84	-6	27	3143		-4.49	-5.61	0
85	SLE RA 1	-2	37	2102		-2.7	-1.93	0
85	SLE RA 2	-2	36	2125		-2.66	-2.45	0
85	SLE RA 3	-2	37	2102		-2.7	-1.93	0
85	SLE RA 4	-2	36	2116		-2.67	-2.24	0
85	SLE RA 5	-2	36	2125		-2.66	-2.45	0
85	SLE RA 6	-2	37	2102		-2.7	-1.93	0
85	SLE RA 7	-2	36	2116		-2.67	-2.24	0
85	SLE RA 8	-2	37	2102		-2.7	-1.93	0
85	SLE RA 9	-2	36	2116		-2.67	-2.24	0
85	SLE RA 10	-3	27	2287		-3.07	-3.58	0
85	SLE RA 11	-4	28	2264		-3.11	-3.06	0
85	SLE RA 12	-3	27	2278		-3.09	-3.37	0
85	SLE RA 13	-3	27	2287		-3.07	-3.58	0
85	SLE RA 14	-4	28	2264		-3.11	-3.06	0
85	SLE RA 15	-3	27	2278		-3.09	-3.37	0
85	SLE RA 16	-4	28	2264		-3.11	-3.06	0
85	SLE RA 17	-3	27	2278		-3.09	-3.37	0
85	SLE RA 18	-4	23	2334		-3.29	-3.55	0
85	SLE RA 19	-4	23	2347		-3.26	-3.86	0
85	SLE RA 20	-4	23	2334		-3.29	-3.55	0
85	SLE RA 21	-4	23	2347		-3.26	-3.86	0
85	SLE FR 1	-2	37	2102		-2.7	-1.93	0
85	SLE FR 2	-2	37	2107		-2.69	-2.03	0
85	SLE FR 3	-2	37	2102		-2.7	-1.93	0
85	SLE FR 4	-3	33	2176		-2.87	-2.52	0
85	SLE FR 5	-3	33	2172		-2.87	-2.41	0
85	SLE FR 6	-3	30	2218		-2.99	-2.74	0
85	SLE QP 1	-2	37	2102		-2.7	-1.93	0
85	SLE QP 2	-3	33	2172		-2.87	-2.41	0
85	SLD 1	-8	160	1991		-8.59	16.71	-0.02
85	SLD 2	-8	160	1991		-8.59	16.71	-0.02
85	SLD 3	-11	9	1900		-1.75	13.93	-0.01
85	SLD 4	-11	9	1900		-1.75	13.93	-0.01
85	SLD 5	0	300	2256		-14.95	7.55	-0.01
85	SLD 6	0	300	2256		-14.95	7.55	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
85	SLD 7	-9	-203	1952	7.83	-1.74	0
85	SLD 8	-9	-203	1952	7.83	-1.74	0
85	SLD 9	4	269	2391	-13.57	-3.09	0
85	SLD 10	4	269	2391	-13.57	-3.09	0
85	SLD 11	-5	-234	2088	9.2	-12.37	0.01
85	SLD 12	-5	-234	2088	9.2	-12.37	0.01
85	SLD 13	5	57	2443	-3.99	-18.75	0.02
85	SLD 14	5	57	2443	-3.99	-18.75	0.02
85	SLD 15	3	-94	2352	2.84	-21.54	0.02
85	SLD 16	3	-94	2352	2.84	-21.54	0.02
85	SLV 1	-16	335	1751	-16.41	46.81	-0.05
85	SLV 2	-16	335	1751	-16.41	46.81	-0.05
85	SLV 3	-23	-21	1530	-0.31	39.84	-0.04
85	SLV 4	-23	-21	1530	-0.31	39.84	-0.04
85	SLV 5	3	663	2381	-31.36	22.92	-0.03
85	SLV 6	3	663	2381	-31.36	22.92	-0.03
85	SLV 7	-19	-523	1644	22.32	-0.3	0
85	SLV 8	-19	-523	1644	22.32	-0.3	0
85	SLV 9	13	589	2699	-28.07	-4.52	0
85	SLV 10	13	589	2699	-28.07	-4.52	0
85	SLV 11	-8	-597	1963	25.61	-27.75	0.03
85	SLV 12	-8	-597	1963	25.61	-27.75	0.03
85	SLV 13	17	87	2813	-5.44	-44.67	0.04
85	SLV 14	17	87	2813	-5.44	-44.67	0.04
85	SLV 15	11	-269	2593	10.66	-51.64	0.05
85	SLV 16	11	-269	2593	10.66	-51.64	0.05
86	SLU 1	0	74	1946	-2.95	0.05	0
86	SLU 2	6	69	1891	-2.72	2.81	0
86	SLU 3	0	74	1946	-2.95	0.05	0
86	SLU 4	3	71	1913	-2.81	1.71	0
86	SLU 5	6	69	1891	-2.72	2.81	0
86	SLU 6	0	74	1946	-2.95	0.05	0
86	SLU 7	3	71	1913	-2.81	1.71	0
86	SLU 8	0	74	1946	-2.95	0.05	0
86	SLU 9	3	71	1913	-2.81	1.71	0
86	SLU 10	5	99	2364	-3.97	2.58	0
86	SLU 11	-1	105	2419	-4.2	-0.18	0
86	SLU 12	3	101	2386	-4.06	1.48	0
86	SLU 13	5	99	2364	-3.97	2.58	0
86	SLU 14	-1	105	2419	-4.2	-0.18	0
86	SLU 15	3	101	2386	-4.06	1.48	0
86	SLU 16	-1	105	2419	-4.2	-0.18	0
86	SLU 17	3	101	2386	-4.06	1.48	0
86	SLU 18	-1	118	2622	-4.73	-0.28	0
86	SLU 19	3	114	2589	-4.6	1.38	0
86	SLU 20	-1	118	2622	-4.73	-0.28	0
86	SLU 21	3	114	2589	-4.6	1.38	0
86	SLU 22	0	91	2187	-3.64	-0.03	0
86	SLU 23	6	85	2132	-3.41	2.73	0
86	SLU 24	0	91	2187	-3.64	-0.03	0
86	SLU 25	3	88	2154	-3.51	1.63	0
86	SLU 26	6	85	2132	-3.41	2.73	0
86	SLU 27	0	91	2187	-3.64	-0.03	0
86	SLU 28	3	88	2154	-3.51	1.63	0
86	SLU 29	0	91	2187	-3.64	-0.03	0
86	SLU 30	3	88	2154	-3.51	1.63	0
86	SLU 31	5	116	2604	-4.66	2.5	0
86	SLU 32	-1	121	2659	-4.89	-0.26	0
86	SLU 33	3	118	2626	-4.75	1.39	0
86	SLU 34	5	116	2604	-4.66	2.5	0
86	SLU 35	-1	121	2659	-4.89	-0.26	0
86	SLU 36	3	118	2626	-4.75	1.39	0
86	SLU 37	-1	121	2659	-4.89	-0.26	0
86	SLU 38	3	118	2626	-4.75	1.39	0
86	SLU 39	-1	134	2862	-5.43	-0.36	0
86	SLU 40	3	131	2829	-5.29	1.3	0
86	SLU 41	-1	134	2862	-5.43	-0.36	0
86	SLU 42	3	131	2829	-5.29	1.3	0
86	SLU 43	0	91	2448	-3.6	0.09	0
86	SLU 44	6	85	2393	-3.37	2.86	0
86	SLU 45	0	91	2448	-3.6	0.09	0
86	SLU 46	3	87	2415	-3.46	1.75	0
86	SLU 47	6	85	2393	-3.37	2.86	0
86	SLU 48	0	91	2448	-3.6	0.09	0
86	SLU 49	3	87	2415	-3.46	1.75	0
86	SLU 50	0	91	2448	-3.6	0.09	0
86	SLU 51	3	87	2415	-3.46	1.75	0
86	SLU 52	5	116	2865	-4.62	2.62	0
86	SLU 53	-1	121	2921	-4.85	-0.14	0
86	SLU 54	3	118	2888	-4.71	1.52	0
86	SLU 55	5	116	2865	-4.62	2.62	0
86	SLU 56	-1	121	2921	-4.85	-0.14	0
86	SLU 57	3	118	2888	-4.71	1.52	0
86	SLU 58	-1	121	2921	-4.85	-0.14	0
86	SLU 59	3	118	2888	-4.71	1.52	0
86	SLU 60	-1	134	3123	-5.38	-0.24	0
86	SLU 61	3	131	3090	-5.24	1.42	0
86	SLU 62	-1	134	3123	-5.38	-0.24	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
86	SLU 63	3	131	3090	-5.24	1.42	0
86	SLU 64	0	107	2688	-4.29	0.01	0
86	SLU 65	6	102	2633	-4.06	2.77	0
86	SLU 66	0	107	2688	-4.29	0.01	0
86	SLU 67	3	104	2655	-4.15	1.67	0
86	SLU 68	6	102	2633	-4.06	2.77	0
86	SLU 69	0	107	2688	-4.29	0.01	0
86	SLU 70	3	104	2655	-4.15	1.67	0
86	SLU 71	0	107	2688	-4.29	0.01	0
86	SLU 72	3	104	2655	-4.15	1.67	0
86	SLU 73	5	132	3106	-5.31	2.54	0
86	SLU 74	-1	138	3161	-5.54	-0.22	0
86	SLU 75	3	135	3128	-5.4	1.44	0
86	SLU 76	5	132	3106	-5.31	2.54	0
86	SLU 77	-1	138	3161	-5.54	-0.22	0
86	SLU 78	3	135	3128	-5.4	1.44	0
86	SLU 79	-1	138	3161	-5.54	-0.22	0
86	SLU 80	3	135	3128	-5.4	1.44	0
86	SLU 81	-1	151	3364	-6.08	-0.32	0
86	SLU 82	3	148	3330	-5.94	1.34	0
86	SLU 83	-1	151	3364	-6.08	-0.32	0
86	SLU 84	3	148	3330	-5.94	1.34	0
86	SLE RA 1	0	79	2015	-3.15	0.02	0
86	SLE RA 2	4	75	1978	-3	1.87	0
86	SLE RA 3	0	79	2015	-3.15	0.02	0
86	SLE RA 4	2	77	1993	-3.06	1.13	0
86	SLE RA 5	4	75	1978	-3	1.87	0
86	SLE RA 6	0	79	2015	-3.15	0.02	0
86	SLE RA 7	2	77	1993	-3.06	1.13	0
86	SLE RA 8	0	79	2015	-3.15	0.02	0
86	SLE RA 9	2	77	1993	-3.06	1.13	0
86	SLE RA 10	3	96	2293	-3.83	1.71	0
86	SLE RA 11	-1	99	2330	-3.98	-0.13	0
86	SLE RA 12	2	97	2308	-3.89	0.98	0
86	SLE RA 13	3	96	2293	-3.83	1.71	0
86	SLE RA 14	-1	99	2330	-3.98	-0.13	0
86	SLE RA 15	2	97	2308	-3.89	0.98	0
86	SLE RA 16	-1	99	2330	-3.98	-0.13	0
86	SLE RA 17	2	97	2308	-3.89	0.98	0
86	SLE RA 18	-1	108	2465	-4.34	-0.2	0
86	SLE RA 19	2	106	2443	-4.25	0.91	0
86	SLE RA 20	-1	108	2465	-4.34	-0.2	0
86	SLE RA 21	2	106	2443	-4.25	0.91	0
86	SLE FR 1	0	79	2015	-3.15	0.02	0
86	SLE FR 2	0	78	2008	-3.12	0.39	0
86	SLE FR 3	0	79	2015	-3.15	0.02	0
86	SLE FR 4	0	87	2143	-3.48	0.33	0
86	SLE FR 5	0	88	2150	-3.51	-0.04	0
86	SLE FR 6	-1	93	2240	-3.74	-0.09	0
86	SLE QP 1	0	79	2015	-3.15	0.02	0
86	SLE QP 2	0	88	2150	-3.51	-0.04	0
86	SLD 1	-21	190	2292	-7.97	-5.84	0.03
86	SLD 2	-21	190	2292	-7.97	-5.84	0.03
86	SLD 3	-15	69	2270	-2.69	-8.75	0.02
86	SLD 4	-15	69	2270	-2.69	-8.75	0.02
86	SLD 5	-17	302	2226	-12.85	2.63	0.02
86	SLD 6	-17	302	2226	-12.85	2.63	0.02
86	SLD 7	6	-102	2153	4.74	-7.07	-0.01
86	SLD 8	6	-102	2153	4.74	-7.07	-0.01
86	SLD 9	-7	277	2147	-11.76	6.98	0.01
86	SLD 10	-7	277	2147	-11.76	6.98	0.01
86	SLD 11	16	-127	2074	5.84	-2.71	-0.02
86	SLD 12	16	-127	2074	5.84	-2.71	-0.02
86	SLD 13	14	107	2030	-4.32	8.67	-0.01
86	SLD 14	14	107	2030	-4.32	8.67	-0.01
86	SLD 15	21	-14	2008	0.96	5.76	-0.02
86	SLD 16	21	-14	2008	0.96	5.76	-0.02
86	SLV 1	-54	331	2494	-14.11	-15.25	0.06
86	SLV 2	-54	331	2494	-14.11	-15.25	0.06
86	SLV 3	-37	45	2441	-1.65	-22.27	0.04
86	SLV 4	-37	45	2441	-1.65	-22.27	0.04
86	SLV 5	-41	594	2333	-25.6	6.03	0.06
86	SLV 6	-41	594	2333	-25.6	6.03	0.06
86	SLV 7	13	-359	2158	15.96	-17.34	-0.02
86	SLV 8	13	-359	2158	15.96	-17.34	-0.02
86	SLV 9	-14	534	2142	-22.97	17.26	0.02
86	SLV 10	-14	534	2142	-22.97	17.26	0.02
86	SLV 11	41	-419	1967	18.59	-6.11	-0.05
86	SLV 12	41	-419	1967	18.59	-6.11	-0.05
86	SLV 13	37	131	1859	-5.37	22.18	-0.04
86	SLV 14	37	131	1859	-5.37	22.18	-0.04
86	SLV 15	53	-155	1806	7.1	15.17	-0.06
86	SLV 16	53	-155	1806	7.1	15.17	-0.06
87	SLU 1	0	353	1337	-14.47	0.07	0
87	SLU 2	0	353	1332	-14.46	-2.69	0
87	SLU 3	0	353	1337	-14.47	0.07	0
87	SLU 4	0	353	1334	-14.46	-1.59	0
87	SLU 5	0	353	1332	-14.46	-2.69	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
87	SLU 6	0	353	1337	-14.47	0.07	0
87	SLU 7	0	353	1334	-14.46	-1.59	0
87	SLU 8	0	353	1337	-14.47	0.07	0
87	SLU 9	0	353	1334	-14.46	-1.59	0
87	SLU 10	0	635	1910	-26.13	-2.53	0
87	SLU 11	0	636	1915	-26.14	0.23	0
87	SLU 12	0	636	1912	-26.13	-1.43	0
87	SLU 13	0	635	1910	-26.13	-2.53	0
87	SLU 14	0	636	1915	-26.14	0.23	0
87	SLU 15	0	636	1912	-26.13	-1.43	0
87	SLU 16	0	636	1915	-26.14	0.23	0
87	SLU 17	0	636	1912	-26.13	-1.43	0
87	SLU 18	0	757	2163	-31.14	0.29	0
87	SLU 19	0	757	2160	-31.14	-1.36	0
87	SLU 20	0	757	2163	-31.14	0.29	0
87	SLU 21	0	757	2160	-31.14	-1.36	0
87	SLU 22	0	492	1669	-20.15	0.13	0
87	SLU 23	0	491	1664	-20.14	-2.63	0
87	SLU 24	0	492	1669	-20.15	0.13	0
87	SLU 25	0	491	1666	-20.14	-1.52	0
87	SLU 26	0	491	1664	-20.14	-2.63	0
87	SLU 27	0	492	1669	-20.15	0.13	0
87	SLU 28	0	491	1666	-20.14	-1.52	0
87	SLU 29	0	492	1669	-20.15	0.13	0
87	SLU 30	0	491	1666	-20.14	-1.52	0
87	SLU 31	0	774	2242	-31.81	-2.47	0
87	SLU 32	0	774	2247	-31.82	0.29	0
87	SLU 33	0	774	2244	-31.81	-1.37	0
87	SLU 34	0	774	2242	-31.81	-2.47	0
87	SLU 35	0	774	2247	-31.82	0.29	0
87	SLU 36	0	774	2244	-31.81	-1.37	0
87	SLU 37	0	774	2247	-31.82	0.29	0
87	SLU 38	0	774	2244	-31.81	-1.37	0
87	SLU 39	0	896	2495	-36.82	0.36	0
87	SLU 40	0	895	2492	-36.82	-1.3	0
87	SLU 41	0	896	2495	-36.82	0.36	0
87	SLU 42	0	895	2492	-36.82	-1.3	0
87	SLU 43	0	412	1624	-16.86	0.07	0
87	SLU 44	0	411	1620	-16.85	-2.69	0
87	SLU 45	0	412	1624	-16.86	0.07	0
87	SLU 46	0	411	1622	-16.86	-1.59	0
87	SLU 47	0	411	1620	-16.85	-2.69	0
87	SLU 48	0	412	1624	-16.86	0.07	0
87	SLU 49	0	411	1622	-16.86	-1.59	0
87	SLU 50	0	412	1624	-16.86	0.07	0
87	SLU 51	0	411	1622	-16.86	-1.59	0
87	SLU 52	0	694	2198	-28.52	-2.53	0
87	SLU 53	0	694	2202	-28.53	0.23	0
87	SLU 54	0	694	2200	-28.53	-1.43	0
87	SLU 55	0	694	2198	-28.52	-2.53	0
87	SLU 56	0	694	2202	-28.53	0.23	0
87	SLU 57	0	694	2200	-28.53	-1.43	0
87	SLU 58	0	694	2202	-28.53	0.23	0
87	SLU 59	0	694	2200	-28.53	-1.43	0
87	SLU 60	0	816	2450	-33.53	0.29	0
87	SLU 61	0	815	2447	-33.53	-1.36	0
87	SLU 62	0	816	2450	-33.53	0.29	0
87	SLU 63	0	815	2447	-33.53	-1.36	0
87	SLU 64	0	550	1956	-22.54	0.13	0
87	SLU 65	0	550	1952	-22.53	-2.63	0
87	SLU 66	0	550	1956	-22.54	0.13	0
87	SLU 67	0	550	1953	-22.54	-1.53	0
87	SLU 68	0	550	1952	-22.53	-2.63	0
87	SLU 69	0	550	1956	-22.54	0.13	0
87	SLU 70	0	550	1953	-22.54	-1.53	0
87	SLU 71	0	550	1956	-22.54	0.13	0
87	SLU 72	0	550	1953	-22.54	-1.53	0
87	SLU 73	0	832	2530	-34.2	-2.47	0
87	SLU 74	0	833	2534	-34.21	0.29	0
87	SLU 75	0	833	2531	-34.21	-1.37	0
87	SLU 76	0	832	2530	-34.2	-2.47	0
87	SLU 77	0	833	2534	-34.21	0.29	0
87	SLU 78	0	833	2531	-34.21	-1.37	0
87	SLU 79	0	833	2534	-34.21	0.29	0
87	SLU 80	0	833	2531	-34.21	-1.37	0
87	SLU 81	0	954	2782	-39.21	0.36	0
87	SLU 82	0	954	2779	-39.21	-1.3	0
87	SLU 83	0	954	2782	-39.21	0.36	0
87	SLU 84	0	954	2779	-39.21	-1.3	0
87	SLE RA 1	0	393	1432	-16.09	0.09	0
87	SLE RA 2	0	392	1429	-16.09	-1.75	0
87	SLE RA 3	0	393	1432	-16.09	0.09	0
87	SLE RA 4	0	393	1430	-16.09	-1.02	0
87	SLE RA 5	0	392	1429	-16.09	-1.75	0
87	SLE RA 6	0	393	1432	-16.09	0.09	0
87	SLE RA 7	0	393	1430	-16.09	-1.02	0
87	SLE RA 8	0	393	1432	-16.09	0.09	0
87	SLE RA 9	0	393	1430	-16.09	-1.02	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
87	SLE RA 10	0	581	1814	-23.87	-1.65	0
87	SLE RA 11	0	581	1817	-23.87	0.19	0
87	SLE RA 12	0	581	1815	-23.87	-0.91	0
87	SLE RA 13	0	581	1814	-23.87	-1.65	0
87	SLE RA 14	0	581	1817	-23.87	0.19	0
87	SLE RA 15	0	581	1815	-23.87	-0.91	0
87	SLE RA 16	0	581	1817	-23.87	0.19	0
87	SLE RA 17	0	581	1815	-23.87	-0.91	0
87	SLE RA 18	0	662	1982	-27.2	0.24	0
87	SLE RA 19	0	662	1980	-27.2	-0.87	0
87	SLE RA 20	0	662	1982	-27.2	0.24	0
87	SLE RA 21	0	662	1980	-27.2	-0.87	0
87	SLE FR 1	0	393	1432	-16.09	0.09	0
87	SLE FR 2	0	393	1431	-16.09	-0.28	0
87	SLE FR 3	0	393	1432	-16.09	0.09	0
87	SLE FR 4	0	474	1596	-19.42	-0.24	0
87	SLE FR 5	0	474	1597	-19.42	0.13	0
87	SLE FR 6	0	527	1707	-21.65	0.16	0
87	SLE QP 1	0	393	1432	-16.09	0.09	0
87	SLE QP 2	0	474	1597	-19.42	0.13	0
87	SLD 1	6	515	1645	-25.13	14.43	-0.02
87	SLD 2	6	515	1645	-25.13	14.43	-0.02
87	SLD 3	4	355	1607	-10.22	12.69	-0.01
87	SLD 4	4	355	1607	-10.22	12.69	-0.01
87	SLD 5	6	729	1668	-43.75	7.06	-0.01
87	SLD 6	6	729	1668	-43.75	7.06	-0.01
87	SLD 7	-3	195	1543	5.95	1.26	0
87	SLD 8	-3	195	1543	5.95	1.26	0
87	SLD 9	3	753	1651	-44.8	-1	0
87	SLD 10	3	753	1651	-44.8	-1	0
87	SLD 11	-6	218	1525	4.9	-6.8	0.01
87	SLD 12	-6	218	1525	4.9	-6.8	0.01
87	SLD 13	-4	593	1586	-28.63	-12.43	0.01
87	SLD 14	-4	593	1586	-28.63	-12.43	0.01
87	SLD 15	-6	432	1549	-13.71	-14.16	0.02
87	SLD 16	-6	432	1549	-13.71	-14.16	0.02
87	SLV 1	17	579	1713	-34.22	43.78	-0.05
87	SLV 2	17	579	1713	-34.22	43.78	-0.05
87	SLV 3	10	185	1620	3.72	39.35	-0.04
87	SLV 4	10	185	1620	3.72	39.35	-0.04
87	SLV 5	14	1104	1773	-81.41	19.93	-0.03
87	SLV 6	14	1104	1773	-81.41	19.93	-0.03
87	SLV 7	-6	-212	1462	45.06	5.19	0
87	SLV 8	-6	-212	1462	45.06	5.19	0
87	SLV 9	6	1159	1731	-83.91	-4.93	0
87	SLV 10	6	1159	1731	-83.91	-4.93	0
87	SLV 11	-14	-157	1421	42.56	-19.67	0.03
87	SLV 12	-14	-157	1421	42.56	-19.67	0.03
87	SLV 13	-10	763	1574	-42.57	-39.09	0.04
87	SLV 14	-10	763	1574	-42.57	-39.09	0.04
87	SLV 15	-17	368	1481	-4.63	-43.51	0.05
87	SLV 16	-17	368	1481	-4.63	-43.51	0.05
88	SLU 1	-1	26	2036	-0.71	-1.31	0
88	SLU 2	-1	23	2068	-0.59	-2.67	0
88	SLU 3	-1	26	2036	-0.71	-1.31	0
88	SLU 4	-1	24	2055	-0.64	-2.12	0
88	SLU 5	-1	23	2068	-0.59	-2.67	0
88	SLU 6	-1	26	2036	-0.71	-1.31	0
88	SLU 7	-1	24	2055	-0.64	-2.12	0
88	SLU 8	-1	26	2036	-0.71	-1.31	0
88	SLU 9	-1	24	2055	-0.64	-2.12	0
88	SLU 10	-2	12	2285	0.68	-4.03	0
88	SLU 11	-2	15	2253	0.56	-2.68	0
88	SLU 12	-2	13	2272	0.63	-3.49	0
88	SLU 13	-2	12	2285	0.68	-4.03	0
88	SLU 14	-2	15	2253	0.56	-2.68	0
88	SLU 15	-2	13	2272	0.63	-3.49	0
88	SLU 16	-2	15	2253	0.56	-2.68	0
88	SLU 17	-2	13	2272	0.63	-3.49	0
88	SLU 18	-3	10	2346	1.1	-3.26	0
88	SLU 19	-3	9	2365	1.18	-4.07	0
88	SLU 20	-3	10	2346	1.1	-3.26	0
88	SLU 21	-3	9	2365	1.18	-4.07	0
88	SLU 22	-2	26	2175	-0.39	-1.89	0
88	SLU 23	-2	23	2208	-0.27	-3.24	0
88	SLU 24	-2	26	2175	-0.39	-1.89	0
88	SLU 25	-2	24	2195	-0.32	-2.7	0
88	SLU 26	-2	23	2208	-0.27	-3.24	0
88	SLU 27	-2	26	2175	-0.39	-1.89	0
88	SLU 28	-2	24	2195	-0.32	-2.7	0
88	SLU 29	-2	26	2175	-0.39	-1.89	0
88	SLU 30	-2	24	2195	-0.32	-2.7	0
88	SLU 31	-3	12	2425	1	-4.61	0
88	SLU 32	-3	15	2392	0.88	-3.25	0
88	SLU 33	-3	13	2412	0.95	-4.07	0
88	SLU 34	-3	12	2425	1	-4.61	0
88	SLU 35	-3	15	2392	0.88	-3.25	0
88	SLU 36	-3	13	2412	0.95	-4.07	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
88	SLU 37	-3	15	2392	0.88	-3.25	0
88	SLU 38	-3	13	2412	0.95	-4.07	0
88	SLU 39	-3	11	2485	1.42	-3.84	0
88	SLU 40	-3	9	2505	1.49	-4.65	0
88	SLU 41	-3	11	2485	1.42	-3.84	0
88	SLU 42	-3	9	2505	1.49	-4.65	0
88	SLU 43	-1	33	2598	-1.03	-1.51	0
88	SLU 44	-1	30	2631	-0.91	-2.86	0
88	SLU 45	-1	33	2598	-1.03	-1.51	0
88	SLU 46	-1	31	2618	-0.96	-2.32	0
88	SLU 47	-1	30	2631	-0.91	-2.86	0
88	SLU 48	-1	33	2598	-1.03	-1.51	0
88	SLU 49	-1	31	2618	-0.96	-2.32	0
88	SLU 50	-1	33	2598	-1.03	-1.51	0
88	SLU 51	-1	31	2618	-0.96	-2.32	0
88	SLU 52	-2	20	2848	0.36	-4.23	0
88	SLU 53	-3	23	2815	0.24	-2.87	0
88	SLU 54	-2	21	2835	0.31	-3.68	0
88	SLU 55	-2	20	2848	0.36	-4.23	0
88	SLU 56	-3	23	2815	0.24	-2.87	0
88	SLU 57	-2	21	2835	0.31	-3.68	0
88	SLU 58	-3	23	2815	0.24	-2.87	0
88	SLU 59	-2	21	2835	0.31	-3.68	0
88	SLU 60	-3	18	2908	0.78	-3.46	0
88	SLU 61	-3	16	2928	0.85	-4.27	0
88	SLU 62	-3	18	2908	0.78	-3.46	0
88	SLU 63	-3	16	2928	0.85	-4.27	0
88	SLU 64	-2	33	2738	-0.71	-2.08	0
88	SLU 65	-2	30	2771	-0.59	-3.44	0
88	SLU 66	-2	33	2738	-0.71	-2.08	0
88	SLU 67	-2	32	2758	-0.64	-2.9	0
88	SLU 68	-2	30	2771	-0.59	-3.44	0
88	SLU 69	-2	33	2738	-0.71	-2.08	0
88	SLU 70	-2	32	2758	-0.64	-2.9	0
88	SLU 71	-2	33	2738	-0.71	-2.08	0
88	SLU 72	-2	32	2758	-0.64	-2.9	0
88	SLU 73	-3	20	2988	0.68	-4.8	0
88	SLU 74	-3	23	2955	0.56	-3.45	0
88	SLU 75	-3	21	2975	0.63	-4.26	0
88	SLU 76	-3	20	2988	0.68	-4.8	0
88	SLU 77	-3	23	2955	0.56	-3.45	0
88	SLU 78	-3	21	2975	0.63	-4.26	0
88	SLU 79	-3	23	2955	0.56	-3.45	0
88	SLU 80	-3	21	2975	0.63	-4.26	0
88	SLU 81	-4	18	3048	1.1	-4.03	0
88	SLU 82	-4	16	3068	1.17	-4.85	0
88	SLU 83	-4	18	3048	1.1	-4.03	0
88	SLU 84	-4	16	3068	1.17	-4.85	0
88	SLE RA 1	-1	26	2076	-0.62	-1.48	0
88	SLE RA 2	-1	24	2097	-0.54	-2.38	0
88	SLE RA 3	-1	26	2076	-0.62	-1.48	0
88	SLE RA 4	-1	24	2089	-0.57	-2.02	0
88	SLE RA 5	-1	24	2097	-0.54	-2.38	0
88	SLE RA 6	-1	26	2076	-0.62	-1.48	0
88	SLE RA 7	-1	24	2089	-0.57	-2.02	0
88	SLE RA 8	-1	26	2076	-0.62	-1.48	0
88	SLE RA 9	-1	24	2089	-0.57	-2.02	0
88	SLE RA 10	-2	17	2242	0.31	-3.29	0
88	SLE RA 11	-2	19	2220	0.23	-2.39	0
88	SLE RA 12	-2	17	2233	0.28	-2.93	0
88	SLE RA 13	-2	17	2242	0.31	-3.29	0
88	SLE RA 14	-2	19	2220	0.23	-2.39	0
88	SLE RA 15	-2	17	2233	0.28	-2.93	0
88	SLE RA 16	-2	19	2220	0.23	-2.39	0
88	SLE RA 17	-2	17	2233	0.28	-2.93	0
88	SLE RA 18	-3	16	2282	0.59	-2.78	0
88	SLE RA 19	-2	14	2295	0.64	-3.32	0
88	SLE RA 20	-3	16	2282	0.59	-2.78	0
88	SLE RA 21	-2	14	2295	0.64	-3.32	0
88	SLE FR 1	-1	26	2076	-0.62	-1.48	0
88	SLE FR 2	-1	25	2080	-0.6	-1.66	0
88	SLE FR 3	-1	26	2076	-0.62	-1.48	0
88	SLE FR 4	-2	22	2142	-0.24	-2.05	0
88	SLE FR 5	-2	23	2138	-0.25	-1.87	0
88	SLE FR 6	-2	21	2179	-0.01	-2.13	0
88	SLE QP 1	-1	26	2076	-0.62	-1.48	0
88	SLE QP 2	-2	23	2138	-0.25	-1.87	0
88	SLD 1	17	150	1972	-5.97	25.53	-0.02
88	SLD 2	17	150	1972	-5.97	25.53	-0.02
88	SLD 3	13	-2	1899	0.85	29.81	-0.02
88	SLD 4	13	-2	1899	0.85	29.81	-0.02
88	SLD 5	10	292	2199	-12.31	-0.14	0
88	SLD 6	10	292	2199	-12.31	-0.14	0
88	SLD 7	-3	-216	1956	10.42	14.13	-0.01
88	SLD 8	-3	-216	1956	10.42	14.13	-0.01
88	SLD 9	0	261	2320	-10.93	-17.86	0.01
88	SLD 10	0	261	2320	-10.93	-17.86	0.01
88	SLD 11	-14	-247	2077	11.8	-3.59	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
88	SLD 12	-14	-247	2077	11.8	-3.59	0
88	SLD 13	-17	47	2376	-1.36	-33.54	0.02
88	SLD 14	-17	47	2376	-1.36	-33.54	0.02
88	SLD 15	-21	-105	2303	5.46	-29.26	0.02
88	SLD 16	-21	-105	2303	5.46	-29.26	0.02
88	SLV 1	46	327	1751	-13.87	69.13	-0.04
88	SLV 2	46	327	1751	-13.87	69.13	-0.04
88	SLV 3	36	-32	1575	2.2	79.92	-0.05
88	SLV 4	36	-32	1575	2.2	79.92	-0.05
88	SLV 5	28	658	2290	-28.72	3.07	0.01
88	SLV 6	28	658	2290	-28.72	3.07	0.01
88	SLV 7	-6	-538	1700	24.86	39.03	-0.03
88	SLV 8	-6	-538	1700	24.86	39.03	-0.03
88	SLV 9	2	583	2575	-25.37	-42.76	0.04
88	SLV 10	2	583	2575	-25.37	-42.76	0.04
88	SLV 11	-31	-613	1985	28.21	-6.81	0
88	SLV 12	-31	-613	1985	28.21	-6.81	0
88	SLV 13	-39	78	2701	-2.71	-83.65	0.06
88	SLV 14	-39	78	2701	-2.71	-83.65	0.06
88	SLV 15	-50	-281	2524	13.36	-72.87	0.04
88	SLV 16	-50	-281	2524	13.36	-72.87	0.04
89	SLU 1	2	36	1978	-1.35	0.42	-0.01
89	SLU 2	5	30	1911	-1.23	2.09	0
89	SLU 3	2	36	1978	-1.35	0.42	-0.01
89	SLU 4	4	32	1938	-1.28	1.42	0
89	SLU 5	5	30	1911	-1.23	2.09	0
89	SLU 6	2	36	1978	-1.35	0.42	-0.01
89	SLU 7	4	32	1938	-1.28	1.42	0
89	SLU 8	2	36	1978	-1.35	0.42	-0.01
89	SLU 9	4	32	1938	-1.28	1.42	0
89	SLU 10	5	39	2395	-1.57	2.08	0
89	SLU 11	2	45	2462	-1.69	0.41	-0.01
89	SLU 12	4	42	2422	-1.62	1.41	-0.01
89	SLU 13	5	39	2395	-1.57	2.08	0
89	SLU 14	2	45	2462	-1.69	0.41	-0.01
89	SLU 15	4	42	2422	-1.62	1.41	-0.01
89	SLU 16	2	45	2462	-1.69	0.41	-0.01
89	SLU 17	4	42	2422	-1.62	1.41	-0.01
89	SLU 18	2	49	2669	-1.84	0.41	-0.01
89	SLU 19	4	46	2629	-1.77	1.41	-0.01
89	SLU 20	2	49	2669	-1.84	0.41	-0.01
89	SLU 21	4	46	2629	-1.77	1.41	-0.01
89	SLU 22	2	43	2224	-1.62	0.43	-0.01
89	SLU 23	5	37	2157	-1.5	2.1	0
89	SLU 24	2	43	2224	-1.62	0.43	-0.01
89	SLU 25	4	39	2184	-1.55	1.43	0
89	SLU 26	5	37	2157	-1.5	2.1	0
89	SLU 27	2	43	2224	-1.62	0.43	-0.01
89	SLU 28	4	39	2184	-1.55	1.43	0
89	SLU 29	2	43	2224	-1.62	0.43	-0.01
89	SLU 30	4	39	2184	-1.55	1.43	0
89	SLU 31	5	47	2641	-1.84	2.09	0
89	SLU 32	2	52	2708	-1.96	0.42	-0.01
89	SLU 33	4	49	2668	-1.89	1.42	-0.01
89	SLU 34	5	47	2641	-1.84	2.09	0
89	SLU 35	2	52	2708	-1.96	0.42	-0.01
89	SLU 36	4	49	2668	-1.89	1.42	-0.01
89	SLU 37	2	52	2708	-1.96	0.42	-0.01
89	SLU 38	4	49	2668	-1.89	1.42	-0.01
89	SLU 39	2	56	2915	-2.11	0.41	-0.01
89	SLU 40	4	53	2875	-2.04	1.41	-0.01
89	SLU 41	2	56	2915	-2.11	0.41	-0.01
89	SLU 42	4	53	2875	-2.04	1.41	-0.01
89	SLU 43	2	44	2487	-1.66	0.54	-0.01
89	SLU 44	5	38	2420	-1.54	2.21	0
89	SLU 45	2	44	2487	-1.66	0.54	-0.01
89	SLU 46	4	41	2447	-1.59	1.54	-0.01
89	SLU 47	5	38	2420	-1.54	2.21	0
89	SLU 48	2	44	2487	-1.66	0.54	-0.01
89	SLU 49	4	41	2447	-1.59	1.54	-0.01
89	SLU 50	2	44	2487	-1.66	0.54	-0.01
89	SLU 51	4	41	2447	-1.59	1.54	-0.01
89	SLU 52	6	48	2904	-1.89	2.2	0
89	SLU 53	2	53	2971	-2	0.53	-0.01
89	SLU 54	4	50	2931	-1.93	1.53	-0.01
89	SLU 55	6	48	2904	-1.89	2.2	0
89	SLU 56	2	53	2971	-2	0.53	-0.01
89	SLU 57	4	50	2931	-1.93	1.53	-0.01
89	SLU 58	2	53	2971	-2	0.53	-0.01
89	SLU 59	4	50	2931	-1.93	1.53	-0.01
89	SLU 60	2	57	3178	-2.15	0.53	-0.01
89	SLU 61	5	54	3138	-2.08	1.53	-0.01
89	SLU 62	2	57	3178	-2.15	0.53	-0.01
89	SLU 63	5	54	3138	-2.08	1.53	-0.01
89	SLU 64	2	51	2733	-1.93	0.55	-0.01
89	SLU 65	6	45	2667	-1.81	2.22	0
89	SLU 66	2	51	2733	-1.93	0.55	-0.01
89	SLU 67	4	48	2693	-1.86	1.55	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
89	SLU 68	6	45	2667	-1.81	2.22	0
89	SLU 69	2	51	2733	-1.93	0.55	-0.01
89	SLU 70	4	48	2693	-1.86	1.55	-0.01
89	SLU 71	2	51	2733	-1.93	0.55	-0.01
89	SLU 72	4	48	2693	-1.86	1.55	-0.01
89	SLU 73	6	55	3150	-2.16	2.21	-0.01
89	SLU 74	2	60	3217	-2.27	0.54	-0.01
89	SLU 75	5	57	3177	-2.2	1.54	-0.01
89	SLU 76	6	55	3150	-2.16	2.21	-0.01
89	SLU 77	2	60	3217	-2.27	0.54	-0.01
89	SLU 78	5	57	3177	-2.2	1.54	-0.01
89	SLU 79	2	60	3217	-2.27	0.54	-0.01
89	SLU 80	5	57	3177	-2.2	1.54	-0.01
89	SLU 81	3	64	3424	-2.42	0.54	-0.02
89	SLU 82	5	61	3384	-2.35	1.54	-0.01
89	SLU 83	3	64	3424	-2.42	0.54	-0.02
89	SLU 84	5	61	3384	-2.35	1.54	-0.01
89	SLE RA 1	2	38	2048	-1.42	0.42	-0.01
89	SLE RA 2	4	34	2004	-1.35	1.53	0
89	SLE RA 3	2	38	2048	-1.42	0.42	-0.01
89	SLE RA 4	3	35	2022	-1.38	1.09	-0.01
89	SLE RA 5	4	34	2004	-1.35	1.53	0
89	SLE RA 6	2	38	2048	-1.42	0.42	-0.01
89	SLE RA 7	3	35	2022	-1.38	1.09	-0.01
89	SLE RA 8	2	38	2048	-1.42	0.42	-0.01
89	SLE RA 9	3	35	2022	-1.38	1.09	-0.01
89	SLE RA 10	4	40	2326	-1.58	1.53	0
89	SLE RA 11	2	44	2371	-1.65	0.42	-0.01
89	SLE RA 12	3	42	2344	-1.61	1.08	-0.01
89	SLE RA 13	4	40	2326	-1.58	1.53	0
89	SLE RA 14	2	44	2371	-1.65	0.42	-0.01
89	SLE RA 15	3	42	2344	-1.61	1.08	-0.01
89	SLE RA 16	2	44	2371	-1.65	0.42	-0.01
89	SLE RA 17	3	42	2344	-1.61	1.08	-0.01
89	SLE RA 18	2	47	2509	-1.75	0.41	-0.01
89	SLE RA 19	3	44	2482	-1.7	1.08	-0.01
89	SLE RA 20	2	47	2509	-1.75	0.41	-0.01
89	SLE RA 21	3	44	2482	-1.7	1.08	-0.01
89	SLE FR 1	2	38	2048	-1.42	0.42	-0.01
89	SLE FR 2	2	37	2039	-1.41	0.65	-0.01
89	SLE FR 3	2	38	2048	-1.42	0.42	-0.01
89	SLE FR 4	2	40	2178	-1.51	0.64	-0.01
89	SLE FR 5	2	40	2187	-1.52	0.42	-0.01
89	SLE FR 6	2	42	2279	-1.59	0.42	-0.01
89	SLE QP 1	2	38	2048	-1.42	0.42	-0.01
89	SLE QP 2	2	40	2187	-1.52	0.42	-0.01
89	SLD 1	-16	142	2362	-5.83	-5.75	-0.03
89	SLD 2	-16	142	2362	-5.83	-5.75	-0.03
89	SLD 3	-10	23	2344	-0.67	-3.72	-0.02
89	SLD 4	-10	23	2344	-0.67	-3.72	-0.02
89	SLD 5	-12	251	2267	-10.63	-4.5	-0.02
89	SLD 6	-12	251	2267	-10.63	-4.5	-0.02
89	SLD 7	7	-146	2206	6.56	2.25	-0.01
89	SLD 8	7	-146	2206	6.56	2.25	-0.01
89	SLD 9	-4	226	2168	-9.6	-1.41	-0.01
89	SLD 10	-4	226	2168	-9.6	-1.41	-0.01
89	SLD 11	16	-171	2106	7.59	5.34	0
89	SLD 12	16	-171	2106	7.59	5.34	0
89	SLD 13	13	58	2030	-2.37	4.56	0
89	SLD 14	13	58	2030	-2.37	4.56	0
89	SLD 15	19	-61	2011	2.78	6.59	0.01
89	SLD 16	19	-61	2011	2.78	6.59	0.01
89	SLV 1	-42	283	2612	-11.74	-15.27	-0.06
89	SLV 2	-42	283	2612	-11.74	-15.27	-0.06
89	SLV 3	-29	2	2568	0.44	-10.44	-0.05
89	SLV 4	-29	2	2568	0.44	-10.44	-0.05
89	SLV 5	-32	540	2382	-23.06	-11.61	-0.05
89	SLV 6	-32	540	2382	-23.06	-11.61	-0.05
89	SLV 7	13	-398	2234	17.54	4.49	0
89	SLV 8	13	-398	2234	17.54	4.49	0
89	SLV 9	-10	479	2140	-20.58	-3.65	-0.02
89	SLV 10	-10	479	2140	-20.58	-3.65	-0.02
89	SLV 11	36	-459	1991	20.02	12.46	0.03
89	SLV 12	36	-459	1991	20.02	12.46	0.03
89	SLV 13	32	79	1805	-3.48	11.28	0.03
89	SLV 14	32	79	1805	-3.48	11.28	0.03
89	SLV 15	46	-202	1761	8.7	16.11	0.04
89	SLV 16	46	-202	1761	8.7	16.11	0.04
90	SLU 1	0	313	1526	-11.63	0.11	0
90	SLU 2	-2	312	1523	-11.52	-4.4	0.01
90	SLU 3	0	313	1526	-11.63	0.11	0
90	SLU 4	-1	312	1524	-11.56	-2.6	0
90	SLU 5	-2	312	1523	-11.52	-4.4	0.01
90	SLU 6	0	313	1526	-11.63	0.11	0
90	SLU 7	-1	312	1524	-11.56	-2.6	0
90	SLU 8	0	313	1526	-11.63	0.11	0
90	SLU 9	-1	312	1524	-11.56	-2.6	0
90	SLU 10	-2	582	2279	-21.27	-4.14	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
90	SLU 11	0	583	2282	-21.38	0.37	0
90	SLU 12	-1	582	2280	-21.32	-2.34	0
90	SLU 13	-2	582	2279	-21.27	-4.14	0
90	SLU 14	0	583	2282	-21.38	0.37	0
90	SLU 15	-1	582	2280	-21.32	-2.34	0
90	SLU 16	0	583	2282	-21.38	0.37	0
90	SLU 17	-1	582	2280	-21.32	-2.34	0
90	SLU 18	0	699	2606	-25.56	0.48	0
90	SLU 19	-1	698	2604	-25.5	-2.23	0
90	SLU 20	0	699	2606	-25.56	0.48	0
90	SLU 21	-1	698	2604	-25.5	-2.23	0
90	SLU 22	0	441	1939	-16.33	0.21	0
90	SLU 23	-2	439	1935	-16.21	-4.3	0.01
90	SLU 24	0	441	1939	-16.33	0.21	0
90	SLU 25	-1	440	1937	-16.26	-2.49	0
90	SLU 26	-2	439	1935	-16.21	-4.3	0.01
90	SLU 27	0	441	1939	-16.33	0.21	0
90	SLU 28	-1	440	1937	-16.26	-2.49	0
90	SLU 29	0	441	1939	-16.33	0.21	0
90	SLU 30	-1	440	1937	-16.26	-2.49	0
90	SLU 31	-2	709	2691	-25.97	-4.04	0
90	SLU 32	0	711	2695	-26.08	0.47	0
90	SLU 33	-1	710	2693	-26.01	-2.24	0
90	SLU 34	-2	709	2691	-25.97	-4.04	0
90	SLU 35	0	711	2695	-26.08	0.47	0
90	SLU 36	-1	710	2693	-26.01	-2.24	0
90	SLU 37	0	711	2695	-26.08	0.47	0
90	SLU 38	-1	710	2693	-26.01	-2.24	0
90	SLU 39	0	827	3019	-30.26	0.58	0
90	SLU 40	-1	826	3017	-30.19	-2.13	0
90	SLU 41	0	827	3019	-30.26	0.58	0
90	SLU 42	-1	826	3017	-30.19	-2.13	0
90	SLU 43	0	364	1843	-13.51	0.11	0
90	SLU 44	-2	362	1839	-13.4	-4.4	0.01
90	SLU 45	0	364	1843	-13.51	0.11	0
90	SLU 46	-1	362	1841	-13.44	-2.6	0
90	SLU 47	-2	362	1839	-13.4	-4.4	0.01
90	SLU 48	0	364	1843	-13.51	0.11	0
90	SLU 49	-1	362	1841	-13.44	-2.6	0
90	SLU 50	0	364	1843	-13.51	0.11	0
90	SLU 51	-1	362	1841	-13.44	-2.6	0
90	SLU 52	-2	632	2595	-23.15	-4.14	0
90	SLU 53	0	634	2599	-23.26	0.36	0
90	SLU 54	-1	632	2596	-23.2	-2.34	0
90	SLU 55	-2	632	2595	-23.15	-4.14	0
90	SLU 56	0	634	2599	-23.26	0.36	0
90	SLU 57	-1	632	2596	-23.2	-2.34	0
90	SLU 58	0	634	2599	-23.26	0.36	0
90	SLU 59	-1	632	2596	-23.2	-2.34	0
90	SLU 60	0	749	2922	-27.44	0.47	0
90	SLU 61	-1	748	2920	-27.38	-2.23	0
90	SLU 62	0	749	2922	-27.44	0.47	0
90	SLU 63	-1	748	2920	-27.38	-2.23	0
90	SLU 64	0	491	2255	-18.21	0.21	0
90	SLU 65	-2	490	2252	-18.09	-4.3	0.01
90	SLU 66	0	491	2255	-18.21	0.21	0
90	SLU 67	-1	490	2253	-18.14	-2.5	0
90	SLU 68	-2	490	2252	-18.09	-4.3	0.01
90	SLU 69	0	491	2255	-18.21	0.21	0
90	SLU 70	-1	490	2253	-18.14	-2.5	0
90	SLU 71	0	491	2255	-18.21	0.21	0
90	SLU 72	-1	490	2253	-18.14	-2.5	0
90	SLU 73	-2	760	3008	-27.85	-4.04	0
90	SLU 74	0	761	3011	-27.96	0.47	0
90	SLU 75	-1	760	3009	-27.89	-2.24	0
90	SLU 76	-2	760	3008	-27.85	-4.04	0
90	SLU 77	0	761	3011	-27.96	0.47	0
90	SLU 78	-1	760	3009	-27.89	-2.24	0
90	SLU 79	0	761	3011	-27.96	0.47	0
90	SLU 80	-1	760	3009	-27.89	-2.24	0
90	SLU 81	0	877	3335	-32.14	0.58	0
90	SLU 82	-1	876	3333	-32.07	-2.13	0
90	SLU 83	0	877	3335	-32.14	0.58	0
90	SLU 84	-1	876	3333	-32.07	-2.13	0
90	SLE RA 1	0	350	1644	-12.97	0.14	0
90	SLE RA 2	-1	349	1642	-12.9	-2.87	0
90	SLE RA 3	0	350	1644	-12.97	0.14	0
90	SLE RA 4	-1	349	1643	-12.93	-1.67	0
90	SLE RA 5	-1	349	1642	-12.9	-2.87	0
90	SLE RA 6	0	350	1644	-12.97	0.14	0
90	SLE RA 7	-1	349	1643	-12.93	-1.67	0
90	SLE RA 8	0	350	1644	-12.97	0.14	0
90	SLE RA 9	-1	349	1643	-12.93	-1.67	0
90	SLE RA 10	-1	529	2146	-19.4	-2.7	0
90	SLE RA 11	0	530	2148	-19.47	0.31	0
90	SLE RA 12	-1	529	2147	-19.43	-1.49	0
90	SLE RA 13	-1	529	2146	-19.4	-2.7	0
90	SLE RA 14	0	530	2148	-19.47	0.31	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
90	SLE RA 15	-1	529	2147	-19.43	-1.49	0
90	SLE RA 16	0	530	2148	-19.47	0.31	0
90	SLE RA 17	-1	529	2147	-19.43	-1.49	0
90	SLE RA 18	0	607	2364	-22.26	0.38	0
90	SLE RA 19	-1	606	2363	-22.22	-1.42	0
90	SLE RA 20	0	607	2364	-22.26	0.38	0
90	SLE RA 21	-1	606	2363	-22.22	-1.42	0
90	SLE FR 1	0	350	1644	-12.97	0.14	0
90	SLE FR 2	0	350	1644	-12.96	-0.46	0
90	SLE FR 3	0	350	1644	-12.97	0.14	0
90	SLE FR 4	0	427	1860	-15.74	-0.39	0
90	SLE FR 5	0	427	1860	-15.76	0.21	0
90	SLE FR 6	0	478	2004	-17.62	0.26	0
90	SLE QP 1	0	350	1644	-12.97	0.14	0
90	SLE QP 2	0	427	1860	-15.76	0.21	0
90	SLD 1	14	311	1890	-9.56	21.89	-0.03
90	SLD 2	14	311	1890	-9.56	21.89	-0.03
90	SLD 3	12	466	1867	-25.48	19.84	-0.02
90	SLD 4	12	466	1867	-25.48	19.84	-0.02
90	SLD 5	8	157	1903	10.26	9.83	-0.01
90	SLD 6	8	157	1903	10.26	9.83	-0.01
90	SLD 7	0	673	1828	-42.83	2.99	0
90	SLD 8	0	673	1828	-42.83	2.99	0
90	SLD 9	0	181	1892	11.31	-2.57	0
90	SLD 10	0	181	1892	11.31	-2.57	0
90	SLD 11	-8	697	1817	-41.77	-9.4	0.01
90	SLD 12	-8	697	1817	-41.77	-9.4	0.01
90	SLD 13	-12	388	1853	-6.04	-19.41	0.02
90	SLD 14	-12	388	1853	-6.04	-19.41	0.02
90	SLD 15	-14	543	1831	-21.96	-21.47	0.03
90	SLD 16	-14	543	1831	-21.96	-21.47	0.03
90	SLV 1	42	146	1931	0.3	66.75	-0.08
90	SLV 2	42	146	1931	0.3	66.75	-0.08
90	SLV 3	36	525	1876	-40.23	61.49	-0.07
90	SLV 4	36	525	1876	-40.23	61.49	-0.07
90	SLV 5	22	-231	1965	50.53	28.15	-0.04
90	SLV 6	22	-231	1965	50.53	28.15	-0.04
90	SLV 7	2	1030	1781	-84.57	10.62	-0.01
90	SLV 8	2	1030	1781	-84.57	10.62	-0.01
90	SLV 9	-2	-176	1940	53.05	-10.19	0.01
90	SLV 10	-2	-176	1940	53.05	-10.19	0.01
90	SLV 11	-22	1085	1755	-82.05	-27.73	0.04
90	SLV 12	-22	1085	1755	-82.05	-27.73	0.04
90	SLV 13	-36	329	1845	8.71	-61.07	0.07
90	SLV 14	-36	329	1845	8.71	-61.07	0.07
90	SLV 15	-42	708	1789	-31.82	-66.33	0.08
90	SLV 16	-42	708	1789	-31.82	-66.33	0.08
91	SLU 1	-1	24	2034	-1.45	-1.03	0
91	SLU 2	-1	19	2065	-1.28	-3.04	0
91	SLU 3	-1	24	2034	-1.45	-1.03	0
91	SLU 4	-1	21	2052	-1.35	-2.24	0
91	SLU 5	-1	19	2065	-1.28	-3.04	0
91	SLU 6	-1	24	2034	-1.45	-1.03	0
91	SLU 7	-1	21	2052	-1.35	-2.24	0
91	SLU 8	-1	24	2034	-1.45	-1.03	0
91	SLU 9	-1	21	2052	-1.35	-2.24	0
91	SLU 10	-2	35	2281	-2.69	-4.15	0
91	SLU 11	-2	39	2250	-2.86	-2.14	0
91	SLU 12	-2	36	2269	-2.76	-3.35	0
91	SLU 13	-2	35	2281	-2.69	-4.15	0
91	SLU 14	-2	39	2250	-2.86	-2.14	0
91	SLU 15	-2	36	2269	-2.76	-3.35	0
91	SLU 16	-2	39	2250	-2.86	-2.14	0
91	SLU 17	-2	36	2269	-2.76	-3.35	0
91	SLU 18	-2	45	2343	-3.46	-2.62	0
91	SLU 19	-2	43	2361	-3.36	-3.82	0
91	SLU 20	-2	45	2343	-3.46	-2.62	0
91	SLU 21	-2	43	2361	-3.36	-3.82	0
91	SLU 22	-1	33	2176	-2.14	-1.49	0
91	SLU 23	-1	28	2206	-1.96	-3.51	0
91	SLU 24	-1	33	2176	-2.14	-1.49	0
91	SLU 25	-1	30	2194	-2.03	-2.7	0
91	SLU 26	-1	28	2206	-1.96	-3.51	0
91	SLU 27	-1	33	2176	-2.14	-1.49	0
91	SLU 28	-1	30	2194	-2.03	-2.7	0
91	SLU 29	-1	33	2176	-2.14	-1.49	0
91	SLU 30	-1	30	2194	-2.03	-2.7	0
91	SLU 31	-2	44	2422	-3.37	-4.62	0
91	SLU 32	-2	48	2392	-3.55	-2.6	0
91	SLU 33	-2	45	2410	-3.44	-3.81	0
91	SLU 34	-2	44	2422	-3.37	-4.62	0
91	SLU 35	-2	48	2392	-3.55	-2.6	0
91	SLU 36	-2	45	2410	-3.44	-3.81	0
91	SLU 37	-2	48	2392	-3.55	-2.6	0
91	SLU 38	-2	45	2410	-3.44	-3.81	0
91	SLU 39	-2	55	2484	-4.15	-3.08	0
91	SLU 40	-2	52	2502	-4.05	-4.29	0
91	SLU 41	-2	55	2484	-4.15	-3.08	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
91	SLU 42	-2	52	2502	-4.05	-4.29	0
91	SLU 43	-1	27	2596	-1.65	-1.18	0
91	SLU 44	-1	23	2626	-1.48	-3.19	0
91	SLU 45	-1	27	2596	-1.65	-1.18	0
91	SLU 46	-1	25	2614	-1.55	-2.38	0
91	SLU 47	-1	23	2626	-1.48	-3.19	0
91	SLU 48	-1	27	2596	-1.65	-1.18	0
91	SLU 49	-1	25	2614	-1.55	-2.38	0
91	SLU 50	-1	27	2596	-1.65	-1.18	0
91	SLU 51	-1	25	2614	-1.55	-2.38	0
91	SLU 52	-2	39	2842	-2.88	-4.3	0
91	SLU 53	-2	43	2812	-3.06	-2.29	0
91	SLU 54	-2	40	2830	-2.96	-3.5	0
91	SLU 55	-2	39	2842	-2.88	-4.3	0
91	SLU 56	-2	43	2812	-3.06	-2.29	0
91	SLU 57	-2	40	2830	-2.96	-3.5	0
91	SLU 58	-2	43	2812	-3.06	-2.29	0
91	SLU 59	-2	40	2830	-2.96	-3.5	0
91	SLU 60	-2	49	2905	-3.66	-2.76	0
91	SLU 61	-2	47	2923	-3.56	-3.97	0
91	SLU 62	-2	49	2905	-3.66	-2.76	0
91	SLU 63	-2	47	2923	-3.56	-3.97	0
91	SLU 64	-1	37	2738	-2.34	-1.64	0
91	SLU 65	-2	32	2768	-2.16	-3.66	0
91	SLU 66	-1	37	2738	-2.34	-1.64	0
91	SLU 67	-1	34	2756	-2.23	-2.85	0
91	SLU 68	-2	32	2768	-2.16	-3.66	0
91	SLU 69	-1	37	2738	-2.34	-1.64	0
91	SLU 70	-1	34	2756	-2.23	-2.85	0
91	SLU 71	-1	37	2738	-2.34	-1.64	0
91	SLU 72	-1	34	2756	-2.23	-2.85	0
91	SLU 73	-2	48	2984	-3.57	-4.77	0
91	SLU 74	-2	52	2954	-3.75	-2.75	0
91	SLU 75	-2	49	2972	-3.64	-3.96	0
91	SLU 76	-2	48	2984	-3.57	-4.77	0
91	SLU 77	-2	52	2954	-3.75	-2.75	0
91	SLU 78	-2	49	2972	-3.64	-3.96	0
91	SLU 79	-2	52	2954	-3.75	-2.75	0
91	SLU 80	-2	49	2972	-3.64	-3.96	0
91	SLU 81	-2	58	3046	-4.35	-3.23	0
91	SLU 82	-3	56	3064	-4.25	-4.44	0
91	SLU 83	-2	58	3046	-4.35	-3.23	0
91	SLU 84	-3	56	3064	-4.25	-4.44	0
91	SLE RA 1	-1	26	2075	-1.65	-1.16	0
91	SLE RA 2	-1	23	2095	-1.53	-2.5	0
91	SLE RA 3	-1	26	2075	-1.65	-1.16	0
91	SLE RA 4	-1	24	2087	-1.58	-1.97	0
91	SLE RA 5	-1	23	2095	-1.53	-2.5	0
91	SLE RA 6	-1	26	2075	-1.65	-1.16	0
91	SLE RA 7	-1	24	2087	-1.58	-1.97	0
91	SLE RA 8	-1	26	2075	-1.65	-1.16	0
91	SLE RA 9	-1	24	2087	-1.58	-1.97	0
91	SLE RA 10	-2	34	2239	-2.47	-3.24	0
91	SLE RA 11	-1	36	2219	-2.59	-1.9	0
91	SLE RA 12	-2	35	2231	-2.52	-2.71	0
91	SLE RA 13	-2	34	2239	-2.47	-3.24	0
91	SLE RA 14	-1	36	2219	-2.59	-1.9	0
91	SLE RA 15	-2	35	2231	-2.52	-2.71	0
91	SLE RA 16	-1	36	2219	-2.59	-1.9	0
91	SLE RA 17	-2	35	2231	-2.52	-2.71	0
91	SLE RA 18	-2	41	2280	-2.99	-2.22	0
91	SLE RA 19	-2	39	2293	-2.92	-3.02	0
91	SLE RA 20	-2	41	2280	-2.99	-2.22	0
91	SLE RA 21	-2	39	2293	-2.92	-3.02	0
91	SLE FR 1	-1	26	2075	-1.65	-1.16	0
91	SLE FR 2	-1	26	2079	-1.62	-1.43	0
91	SLE FR 3	-1	26	2075	-1.65	-1.16	0
91	SLE FR 4	-1	30	2140	-2.03	-1.75	0
91	SLE FR 5	-1	31	2136	-2.05	-1.48	0
91	SLE FR 6	-1	33	2178	-2.32	-1.69	0
91	SLE QP 1	-1	26	2075	-1.65	-1.16	0
91	SLE QP 2	-1	31	2136	-2.05	-1.48	0
91	SLD 1	31	160	1987	-7.88	37.39	-0.02
91	SLD 2	31	160	1987	-7.88	37.39	-0.02
91	SLD 3	26	8	1929	-0.99	43.02	-0.02
91	SLD 4	26	8	1929	-0.99	43.02	-0.02
91	SLD 5	17	301	2180	-14.26	1.65	0
91	SLD 6	17	301	2180	-14.26	1.65	0
91	SLD 7	-1	-208	1986	8.72	20.4	-0.01
91	SLD 8	-1	-208	1986	8.72	20.4	-0.01
91	SLD 9	-1	269	2287	-12.83	-23.36	0.01
91	SLD 10	-1	269	2287	-12.83	-23.36	0.01
91	SLD 11	-19	-240	2093	10.16	-4.61	0
91	SLD 12	-19	-240	2093	10.16	-4.61	0
91	SLD 13	-28	53	2344	-3.11	-45.97	0.02
91	SLD 14	-28	53	2344	-3.11	-45.97	0.02
91	SLD 15	-33	-99	2286	3.78	-40.35	0.02
91	SLD 16	-33	-99	2286	3.78	-40.35	0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
91	SLV 1	81	339	1786	-15.91	99.45	-0.04
91	SLV 2	81	339	1786	-15.91	99.45	-0.04
91	SLV 3	67	-21	1646	0.34	113.7	-0.05
91	SLV 4	67	-21	1646	0.34	113.7	-0.05
91	SLV 5	45	669	2245	-30.85	7.2	0
91	SLV 6	45	669	2245	-30.85	7.2	0
91	SLV 7	-2	-531	1776	23.31	54.68	-0.03
91	SLV 8	-2	-531	1776	23.31	54.68	-0.03
91	SLV 9	0	592	2497	-27.41	-57.64	0.03
91	SLV 10	0	592	2497	-27.41	-57.64	0.03
91	SLV 11	-47	-608	2028	26.75	-10.15	0
91	SLV 12	-47	-608	2028	26.75	-10.15	0
91	SLV 13	-69	82	2627	-4.44	-116.66	0.05
91	SLV 14	-69	82	2627	-4.44	-116.66	0.05
91	SLV 15	-83	-278	2486	11.81	-102.41	0.04
91	SLV 16	-83	-278	2486	11.81	-102.41	0.04
92	SLU 1	231	-8	3081	0.33	5.97	0
92	SLU 2	213	-8	2958	0.01	6.1	0
92	SLU 3	231	-8	3081	0.33	5.97	0
92	SLU 4	220	-8	3007	0.14	6.05	0
92	SLU 5	213	-8	2958	0.01	6.1	0
92	SLU 6	231	-8	3081	0.33	5.97	0
92	SLU 7	220	-8	3007	0.14	6.05	0
92	SLU 8	231	-8	3081	0.33	5.97	0
92	SLU 9	220	-8	3007	0.14	6.05	0
92	SLU 10	257	-16	3694	0.37	6.99	0
92	SLU 11	275	-17	3816	0.68	6.86	-0.01
92	SLU 12	265	-16	3743	0.49	6.94	0
92	SLU 13	257	-16	3694	0.37	6.99	0
92	SLU 14	275	-17	3816	0.68	6.86	-0.01
92	SLU 15	265	-16	3743	0.49	6.94	0
92	SLU 16	275	-17	3816	0.68	6.86	-0.01
92	SLU 17	265	-16	3743	0.49	6.94	0
92	SLU 18	294	-20	4132	0.83	7.24	-0.01
92	SLU 19	284	-20	4058	0.64	7.32	0
92	SLU 20	294	-20	4132	0.83	7.24	-0.01
92	SLU 21	284	-20	4058	0.64	7.32	0
92	SLU 22	253	-9	3456	0.37	6.45	0
92	SLU 23	235	-9	3333	0.06	6.58	0
92	SLU 24	253	-9	3456	0.37	6.45	0
92	SLU 25	243	-9	3382	0.18	6.53	0
92	SLU 26	235	-9	3333	0.06	6.58	0
92	SLU 27	253	-9	3456	0.37	6.45	0
92	SLU 28	243	-9	3382	0.18	6.53	0
92	SLU 29	253	-9	3456	0.37	6.45	0
92	SLU 30	243	-9	3382	0.18	6.53	0
92	SLU 31	280	-18	4069	0.41	7.47	0
92	SLU 32	298	-18	4192	0.73	7.34	-0.01
92	SLU 33	287	-18	4118	0.54	7.42	0
92	SLU 34	280	-18	4069	0.41	7.47	0
92	SLU 35	298	-18	4192	0.73	7.34	-0.01
92	SLU 36	287	-18	4118	0.54	7.42	0
92	SLU 37	298	-18	4192	0.73	7.34	-0.01
92	SLU 38	287	-18	4118	0.54	7.42	0
92	SLU 39	317	-22	4507	0.88	7.72	-0.01
92	SLU 40	306	-21	4433	0.69	7.8	0
92	SLU 41	317	-22	4507	0.88	7.72	-0.01
92	SLU 42	306	-21	4433	0.69	7.8	0
92	SLU 43	292	-10	3876	0.41	7.59	0
92	SLU 44	274	-10	3753	0.09	7.73	0
92	SLU 45	292	-10	3876	0.41	7.59	0
92	SLU 46	281	-10	3802	0.22	7.67	0
92	SLU 47	274	-10	3753	0.09	7.73	0
92	SLU 48	292	-10	3876	0.41	7.59	0
92	SLU 49	281	-10	3802	0.22	7.67	0
92	SLU 50	292	-10	3876	0.41	7.59	0
92	SLU 51	281	-10	3802	0.22	7.67	0
92	SLU 52	319	-18	4489	0.45	8.62	0
92	SLU 53	337	-19	4612	0.76	8.48	-0.01
92	SLU 54	326	-18	4538	0.57	8.56	0
92	SLU 55	319	-18	4489	0.45	8.62	0
92	SLU 56	337	-19	4612	0.76	8.48	-0.01
92	SLU 57	326	-18	4538	0.57	8.56	0
92	SLU 58	337	-19	4612	0.76	8.48	-0.01
92	SLU 59	326	-18	4538	0.57	8.56	0
92	SLU 60	356	-22	4927	0.92	8.86	-0.01
92	SLU 61	345	-22	4853	0.73	8.94	0
92	SLU 62	356	-22	4927	0.92	8.86	-0.01
92	SLU 63	345	-22	4853	0.73	8.94	0
92	SLU 64	315	-11	4251	0.45	8.07	0
92	SLU 65	297	-11	4129	0.14	8.21	0
92	SLU 66	315	-11	4251	0.45	8.07	0
92	SLU 67	304	-11	4178	0.26	8.15	0
92	SLU 68	297	-11	4129	0.14	8.21	0
92	SLU 69	315	-11	4251	0.45	8.07	0
92	SLU 70	304	-11	4178	0.26	8.15	0
92	SLU 71	315	-11	4251	0.45	8.07	0
92	SLU 72	304	-11	4178	0.26	8.15	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
92	SLU 73	341	-19	4864	0.49	9.1	0
92	SLU 74	359	-20	4987	0.81	8.96	-0.01
92	SLU 75	349	-20	4913	0.62	9.04	0
92	SLU 76	341	-19	4864	0.49	9.1	0
92	SLU 77	359	-20	4987	0.81	8.96	-0.01
92	SLU 78	349	-20	4913	0.62	9.04	0
92	SLU 79	359	-20	4987	0.81	8.96	-0.01
92	SLU 80	349	-20	4913	0.62	9.04	0
92	SLU 81	378	-24	5302	0.96	9.34	-0.01
92	SLU 82	368	-23	5229	0.77	9.42	-0.01
92	SLU 83	378	-24	5302	0.96	9.34	-0.01
92	SLU 84	368	-23	5229	0.77	9.42	-0.01
92	SLE RA 1	237	-8	3188	0.34	6.11	0
92	SLE RA 2	225	-8	3106	0.13	6.2	0
92	SLE RA 3	237	-8	3188	0.34	6.11	0
92	SLE RA 4	230	-8	3139	0.21	6.16	0
92	SLE RA 5	225	-8	3106	0.13	6.2	0
92	SLE RA 6	237	-8	3188	0.34	6.11	0
92	SLE RA 7	230	-8	3139	0.21	6.16	0
92	SLE RA 8	237	-8	3188	0.34	6.11	0
92	SLE RA 9	230	-8	3139	0.21	6.16	0
92	SLE RA 10	255	-14	3596	0.37	6.79	0
92	SLE RA 11	267	-14	3678	0.58	6.7	0
92	SLE RA 12	260	-14	3629	0.45	6.75	0
92	SLE RA 13	255	-14	3596	0.37	6.79	0
92	SLE RA 14	267	-14	3678	0.58	6.7	0
92	SLE RA 15	260	-14	3629	0.45	6.75	0
92	SLE RA 16	267	-14	3678	0.58	6.7	0
92	SLE RA 17	260	-14	3629	0.45	6.75	0
92	SLE RA 18	280	-17	3889	0.68	6.95	-0.01
92	SLE RA 19	272	-16	3839	0.55	7	0
92	SLE RA 20	280	-17	3889	0.68	6.95	-0.01
92	SLE RA 21	272	-16	3839	0.55	7	0
92	SLE FR 1	237	-8	3188	0.34	6.11	0
92	SLE FR 2	235	-8	3171	0.3	6.12	0
92	SLE FR 3	237	-8	3188	0.34	6.11	0
92	SLE FR 4	247	-11	3382	0.4	6.38	0
92	SLE FR 5	250	-11	3398	0.44	6.36	0
92	SLE FR 6	258	-12	3538	0.51	6.53	0
92	SLE QP 1	237	-8	3188	0.34	6.11	0
92	SLE QP 2	250	-11	3398	0.44	6.36	0
92	SLD 1	356	97	3725	-0.24	2.54	0
92	SLD 2	356	97	3725	-0.24	2.54	0
92	SLD 3	343	-27	3771	5.19	1.95	-0.03
92	SLD 4	343	-27	3771	5.19	1.95	-0.03
92	SLD 5	302	210	3426	-8	6.1	0.04
92	SLD 6	302	210	3426	-8	6.1	0.04
92	SLD 7	257	-204	3580	10.1	4.15	-0.05
92	SLD 8	257	-204	3580	10.1	4.15	-0.05
92	SLD 9	242	182	3216	-9.22	8.57	0.05
92	SLD 10	242	182	3216	-9.22	8.57	0.05
92	SLD 11	197	-231	3370	8.88	6.61	-0.05
92	SLD 12	197	-231	3370	8.88	6.61	-0.05
92	SLD 13	157	6	3025	-4.31	10.76	0.02
92	SLD 14	157	6	3025	-4.31	10.76	0.02
92	SLD 15	143	-119	3071	1.12	10.18	0
92	SLD 16	143	-119	3071	1.12	10.18	0
92	SLV 1	503	244	4192	-1.14	-2.69	0
92	SLV 2	503	244	4192	-1.14	-2.69	0
92	SLV 3	471	-49	4301	11.68	-4.08	-0.07
92	SLV 4	471	-49	4301	11.68	-4.08	-0.07
92	SLV 5	374	510	3470	-19.47	5.75	0.1
92	SLV 6	374	510	3470	-19.47	5.75	0.1
92	SLV 7	267	-467	3835	23.25	1.12	-0.12
92	SLV 8	267	-467	3835	23.25	1.12	-0.12
92	SLV 9	232	445	2961	-22.37	11.6	0.12
92	SLV 10	232	445	2961	-22.37	11.6	0.12
92	SLV 11	125	-532	3326	20.35	6.96	-0.1
92	SLV 12	125	-532	3326	20.35	6.96	-0.1
92	SLV 13	29	27	2495	-10.8	16.8	0.06
92	SLV 14	29	27	2495	-10.8	16.8	0.06
92	SLV 15	-3	-266	2604	2.02	15.4	0
92	SLV 16	-3	-266	2604	2.02	15.4	0
93	SLU 1	96	0	1705	0.07	6.07	0
93	SLU 2	28	3	1675	-1.88	0.96	0
93	SLU 3	96	0	1705	0.07	6.07	0
93	SLU 4	55	2	1687	-1.1	3	0
93	SLU 5	28	3	1675	-1.88	0.96	0
93	SLU 6	96	0	1705	0.07	6.07	0
93	SLU 7	55	2	1687	-1.1	3	0
93	SLU 8	96	0	1705	0.07	6.07	0
93	SLU 9	55	2	1687	-1.1	3	0
93	SLU 10	38	3	2029	-1.79	2.67	0
93	SLU 11	106	0	2059	0.16	7.79	0
93	SLU 12	65	1	2041	-1.01	4.72	0
93	SLU 13	38	3	2029	-1.79	2.67	0
93	SLU 14	106	0	2059	0.16	7.79	0
93	SLU 15	65	1	2041	-1.01	4.72	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
93	SLU 16	106	0	2059	0.16	7.79	0
93	SLU 17	65	1	2041	-1.01	4.72	0
93	SLU 18	110	0	2211	0.2	8.52	0
93	SLU 19	70	1	2192	-0.97	5.45	0
93	SLU 20	110	0	2211	0.2	8.52	0
93	SLU 21	70	1	2192	-0.97	5.45	0
93	SLU 22	99	0	1886	0.11	6.82	0
93	SLU 23	32	3	1855	-1.85	1.71	0
93	SLU 24	99	0	1886	0.11	6.82	0
93	SLU 25	59	2	1868	-1.07	3.75	0
93	SLU 26	32	3	1855	-1.85	1.71	0
93	SLU 27	99	0	1886	0.11	6.82	0
93	SLU 28	59	2	1868	-1.07	3.75	0
93	SLU 29	99	0	1886	0.11	6.82	0
93	SLU 30	59	2	1868	-1.07	3.75	0
93	SLU 31	42	3	2209	-1.76	3.42	0
93	SLU 32	110	0	2239	0.2	8.54	0
93	SLU 33	69	1	2221	-0.98	5.47	0
93	SLU 34	42	3	2209	-1.76	3.42	0
93	SLU 35	110	0	2239	0.2	8.54	0
93	SLU 36	69	1	2221	-0.98	5.47	0
93	SLU 37	110	0	2239	0.2	8.54	0
93	SLU 38	69	1	2221	-0.98	5.47	0
93	SLU 39	114	-1	2391	0.23	9.27	0
93	SLU 40	74	1	2373	-0.94	6.21	0
93	SLU 41	114	-1	2391	0.23	9.27	0
93	SLU 42	74	1	2373	-0.94	6.21	0
93	SLU 43	123	0	2155	0.08	7.63	0
93	SLU 44	56	3	2125	-1.87	2.52	0
93	SLU 45	123	0	2155	0.08	7.63	0
93	SLU 46	83	2	2137	-1.09	4.57	0
93	SLU 47	56	3	2125	-1.87	2.52	0
93	SLU 48	123	0	2155	0.08	7.63	0
93	SLU 49	83	2	2137	-1.09	4.57	0
93	SLU 50	123	0	2155	0.08	7.63	0
93	SLU 51	83	2	2137	-1.09	4.57	0
93	SLU 52	66	3	2479	-1.78	4.24	0
93	SLU 53	133	0	2509	0.17	9.35	0
93	SLU 54	93	1	2491	-1	6.28	0
93	SLU 55	66	3	2479	-1.78	4.24	0
93	SLU 56	133	0	2509	0.17	9.35	0
93	SLU 57	93	1	2491	-1	6.28	0
93	SLU 58	133	0	2509	0.17	9.35	0
93	SLU 59	93	1	2491	-1	6.28	0
93	SLU 60	138	-1	2660	0.21	10.09	0
93	SLU 61	97	1	2642	-0.96	7.02	0
93	SLU 62	138	-1	2660	0.21	10.09	0
93	SLU 63	97	1	2642	-0.96	7.02	0
93	SLU 64	127	0	2336	0.12	8.39	0
93	SLU 65	59	3	2305	-1.84	3.27	0
93	SLU 66	127	0	2336	0.12	8.39	0
93	SLU 67	86	2	2317	-1.06	5.32	0
93	SLU 68	59	3	2305	-1.84	3.27	0
93	SLU 69	127	0	2336	0.12	8.39	0
93	SLU 70	86	2	2317	-1.06	5.32	0
93	SLU 71	127	0	2336	0.12	8.39	0
93	SLU 72	86	2	2317	-1.06	5.32	0
93	SLU 73	70	2	2659	-1.75	4.99	0
93	SLU 74	137	-1	2689	0.21	10.1	0
93	SLU 75	97	1	2671	-0.97	7.03	0
93	SLU 76	70	2	2659	-1.75	4.99	0
93	SLU 77	137	-1	2689	0.21	10.1	0
93	SLU 78	97	1	2671	-0.97	7.03	0
93	SLU 79	137	-1	2689	0.21	10.1	0
93	SLU 80	97	1	2671	-0.97	7.03	0
93	SLU 81	141	-1	2841	0.25	10.84	0
93	SLU 82	101	1	2823	-0.93	7.77	0
93	SLU 83	141	-1	2841	0.25	10.84	0
93	SLU 84	101	1	2823	-0.93	7.77	0
93	SLE RA 1	97	0	1757	0.08	6.29	0
93	SLE RA 2	52	2	1737	-1.22	2.88	0
93	SLE RA 3	97	0	1757	0.08	6.29	0
93	SLE RA 4	70	1	1745	-0.7	4.24	0
93	SLE RA 5	52	2	1737	-1.22	2.88	0
93	SLE RA 6	97	0	1757	0.08	6.29	0
93	SLE RA 7	70	1	1745	-0.7	4.24	0
93	SLE RA 8	97	0	1757	0.08	6.29	0
93	SLE RA 9	70	1	1745	-0.7	4.24	0
93	SLE RA 10	59	2	1973	-1.16	4.02	0
93	SLE RA 11	104	0	1993	0.14	7.43	0
93	SLE RA 12	77	1	1981	-0.64	5.38	0
93	SLE RA 13	59	2	1973	-1.16	4.02	0
93	SLE RA 14	104	0	1993	0.14	7.43	0
93	SLE RA 15	77	1	1981	-0.64	5.38	0
93	SLE RA 16	104	0	1993	0.14	7.43	0
93	SLE RA 17	77	1	1981	-0.64	5.38	0
93	SLE RA 18	106	0	2094	0.17	7.92	0
93	SLE RA 19	80	1	2082	-0.61	5.87	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
93	SLE RA 20	106	0	2094	0.17	7.92	0
93	SLE RA 21	80	1	2082	-0.61	5.87	0
93	SLE FR 1	97	0	1757	0.08	6.29	0
93	SLE FR 2	88	0	1753	-0.18	5.6	0
93	SLE FR 3	97	0	1757	0.08	6.29	0
93	SLE FR 4	91	0	1854	-0.15	6.09	0
93	SLE FR 5	100	0	1858	0.11	6.78	0
93	SLE FR 6	102	0	1925	0.13	7.1	0
93	SLE QP 1	97	0	1757	0.08	6.29	0
93	SLE QP 2	100	0	1858	0.11	6.78	0
93	SLD 1	296	-14	1945	5.32	17.07	-0.02
93	SLD 2	296	-14	1945	5.32	17.07	-0.02
93	SLD 3	272	-7	1959	8.72	15.86	0
93	SLD 4	272	-7	1959	8.72	15.86	0
93	SLD 5	195	-14	1862	-3.49	11.69	-0.03
93	SLD 6	195	-14	1862	-3.49	11.69	-0.03
93	SLD 7	115	7	1910	7.85	7.68	0.02
93	SLD 8	115	7	1910	7.85	7.68	0.02
93	SLD 9	85	-8	1806	-7.63	5.88	-0.02
93	SLD 10	85	-8	1806	-7.63	5.88	-0.02
93	SLD 11	4	14	1854	3.71	1.86	0.03
93	SLD 12	4	14	1854	3.71	1.86	0.03
93	SLD 13	-72	7	1757	-8.5	-2.31	0
93	SLD 14	-72	7	1757	-8.5	-2.31	0
93	SLD 15	-97	13	1771	-5.1	-3.51	0.02
93	SLD 16	-97	13	1771	-5.1	-3.51	0.02
93	SLV 1	577	-34	2067	13.89	32.47	-0.04
93	SLV 2	577	-34	2067	13.89	32.47	-0.04
93	SLV 3	519	-18	2101	21.9	29.59	-0.01
93	SLV 4	519	-18	2101	21.9	29.59	-0.01
93	SLV 5	330	-33	1868	-7.91	18.85	-0.06
93	SLV 6	330	-33	1868	-7.91	18.85	-0.06
93	SLV 7	138	17	1983	18.79	9.25	0.05
93	SLV 8	138	17	1983	18.79	9.25	0.05
93	SLV 9	61	-18	1733	-18.58	4.3	-0.05
93	SLV 10	61	-18	1733	-18.58	4.3	-0.05
93	SLV 11	-131	33	1848	8.12	-5.3	0.06
93	SLV 12	-131	33	1848	8.12	-5.3	0.06
93	SLV 13	-320	18	1615	-21.68	-16.04	0.01
93	SLV 14	-320	18	1615	-21.68	-16.04	0.01
93	SLV 15	-377	33	1649	-13.67	-18.92	0.04
93	SLV 16	-377	33	1649	-13.67	-18.92	0.04
94	SLU 1	-13	0	1414	0.1	0.28	0
94	SLU 2	-40	4	1435	-3.25	1.03	0
94	SLU 3	-13	0	1414	0.1	0.28	0
94	SLU 4	-29	2	1426	-1.91	0.73	0
94	SLU 5	-40	4	1435	-3.25	1.03	0
94	SLU 6	-13	0	1414	0.1	0.28	0
94	SLU 7	-29	2	1426	-1.91	0.73	0
94	SLU 8	-13	0	1414	0.1	0.28	0
94	SLU 9	-29	2	1426	-1.91	0.73	0
94	SLU 10	-62	4	1656	-3.14	0.09	0
94	SLU 11	-36	0	1635	0.21	-0.66	0
94	SLU 12	-52	2	1648	-1.8	-0.21	0
94	SLU 13	-62	4	1656	-3.14	0.09	0
94	SLU 14	-36	0	1635	0.21	-0.66	0
94	SLU 15	-52	2	1648	-1.8	-0.21	0
94	SLU 16	-36	0	1635	0.21	-0.66	0
94	SLU 17	-52	2	1648	-1.8	-0.21	0
94	SLU 18	-45	0	1730	0.26	-1.06	0
94	SLU 19	-61	2	1743	-1.75	-0.61	0
94	SLU 20	-45	0	1730	0.26	-1.06	0
94	SLU 21	-61	2	1743	-1.75	-0.61	0
94	SLU 22	-25	0	1527	0.14	-0.13	0
94	SLU 23	-51	4	1548	-3.21	0.62	0
94	SLU 24	-25	0	1527	0.14	-0.13	0
94	SLU 25	-41	2	1540	-1.87	0.32	0
94	SLU 26	-51	4	1548	-3.21	0.62	0
94	SLU 27	-25	0	1527	0.14	-0.13	0
94	SLU 28	-41	2	1540	-1.87	0.32	0
94	SLU 29	-25	0	1527	0.14	-0.13	0
94	SLU 30	-41	2	1540	-1.87	0.32	0
94	SLU 31	-74	4	1770	-3.09	-0.32	0
94	SLU 32	-47	0	1749	0.25	-1.07	0
94	SLU 33	-63	2	1761	-1.76	-0.62	0
94	SLU 34	-74	4	1770	-3.09	-0.32	0
94	SLU 35	-47	0	1749	0.25	-1.07	0
94	SLU 36	-63	2	1761	-1.76	-0.62	0
94	SLU 37	-47	0	1749	0.25	-1.07	0
94	SLU 38	-63	2	1761	-1.76	-0.62	0
94	SLU 39	-57	-1	1844	0.3	-1.47	0
94	SLU 40	-73	2	1856	-1.71	-1.02	0
94	SLU 41	-57	-1	1844	0.3	-1.47	0
94	SLU 42	-73	2	1856	-1.71	-1.02	0
94	SLU 43	-13	0	1799	0.11	0.5	0
94	SLU 44	-40	4	1820	-3.24	1.25	0
94	SLU 45	-13	0	1799	0.11	0.5	0
94	SLU 46	-29	2	1811	-1.9	0.95	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione			
		x	y	z		x	y	z	
94	SLU 47	-40	4	1820		-3.24	1.25	0	
94	SLU 48	-13	0	1799		0.11	0.5	0	
94	SLU 49	-29	2	1811		-1.9	0.95	0	
94	SLU 50	-13	0	1799		0.11	0.5	0	
94	SLU 51	-29	2	1811		-1.9	0.95	0	
94	SLU 52	-63	4	2041		-3.13	0.31	0	
94	SLU 53	-36	0	2021		0.22	-0.44	0	
94	SLU 54	-52	2	2033		-1.79	0.01	0	
94	SLU 55	-63	4	2041		-3.13	0.31	0	
94	SLU 56	-36	0	2021		0.22	-0.44	0	
94	SLU 57	-52	2	2033		-1.79	0.01	0	
94	SLU 58	-36	0	2021		0.22	-0.44	0	
94	SLU 59	-52	2	2033		-1.79	0.01	0	
94	SLU 60	-46	-1	2116		0.27	-0.84	0	
94	SLU 61	-62	2	2128		-1.74	-0.39	0	
94	SLU 62	-46	-1	2116		0.27	-0.84	0	
94	SLU 63	-62	2	2128		-1.74	-0.39	0	
94	SLU 64	-25	0	1912		0.15	0.09	0	
94	SLU 65	-51	4	1933		-3.2	0.84	0	
94	SLU 66	-25	0	1912		0.15	0.09	0	
94	SLU 67	-41	2	1925		-1.86	0.54	0	
94	SLU 68	-51	4	1933		-3.2	0.84	0	
94	SLU 69	-25	0	1912		0.15	0.09	0	
94	SLU 70	-41	2	1925		-1.86	0.54	0	
94	SLU 71	-25	0	1912		0.15	0.09	0	
94	SLU 72	-41	2	1925		-1.86	0.54	0	
94	SLU 73	-74	4	2155		-3.08	-0.09	0	
94	SLU 74	-47	-1	2134		0.27	-0.84	0	
94	SLU 75	-63	2	2147		-1.74	-0.39	0	
94	SLU 76	-74	4	2155		-3.08	-0.09	0	
94	SLU 77	-47	-1	2134		0.27	-0.84	0	
94	SLU 78	-63	2	2147		-1.74	-0.39	0	
94	SLU 79	-47	-1	2134		0.27	-0.84	0	
94	SLU 80	-63	2	2147		-1.74	-0.39	0	
94	SLU 81	-57	-1	2229		0.32	-1.25	0	
94	SLU 82	-73	2	2242		-1.69	-0.8	0	
94	SLU 83	-57	-1	2229		0.32	-1.25	0	
94	SLU 84	-73	2	2242		-1.69	-0.8	0	
94	SLE RA 1	-16	0	1446		0.11	0.16	0	
94	SLE RA 2	-34	3	1460		-2.12	0.66	0	
94	SLE RA 3	-16	0	1446		0.11	0.16	0	
94	SLE RA 4	-27	2	1454		-1.23	0.46	0	
94	SLE RA 5	-34	3	1460		-2.12	0.66	0	
94	SLE RA 6	-16	0	1446		0.11	0.16	0	
94	SLE RA 7	-27	2	1454		-1.23	0.46	0	
94	SLE RA 8	-16	0	1446		0.11	0.16	0	
94	SLE RA 9	-27	2	1454		-1.23	0.46	0	
94	SLE RA 10	-49	3	1608		-2.05	0.04	0	
94	SLE RA 11	-32	0	1594		0.18	-0.46	0	
94	SLE RA 12	-42	1	1602		-1.15	-0.16	0	
94	SLE RA 13	-49	3	1608		-2.05	0.04	0	
94	SLE RA 14	-32	0	1594		0.18	-0.46	0	
94	SLE RA 15	-42	1	1602		-1.15	-0.16	0	
94	SLE RA 16	-32	0	1594		0.18	-0.46	0	
94	SLE RA 17	-42	1	1602		-1.15	-0.16	0	
94	SLE RA 18	-38	0	1657		0.22	-0.73	0	
94	SLE RA 19	-49	1	1666		-1.12	-0.43	0	
94	SLE RA 20	-38	0	1657		0.22	-0.73	0	
94	SLE RA 21	-49	1	1666		-1.12	-0.43	0	
94	SLE FR 1	-16	0	1446		0.11	0.16	0	
94	SLE FR 2	-20	0	1449		-0.34	0.26	0	
94	SLE FR 3	-16	0	1446		0.11	0.16	0	
94	SLE FR 4	-26	0	1512		-0.3	-0.01	0	
94	SLE FR 5	-23	0	1509		0.14	-0.11	0	
94	SLE FR 6	-27	0	1552		0.16	-0.28	0	
94	SLE QP 1	-16	0	1446		0.11	0.16	0	
94	SLE QP 2	-23	0	1509		0.14	-0.11	0	
94	SLD 1	160	-17	1468		8.18	-6.68	0.02	
94	SLD 2	160	-17	1468		8.18	-6.68	0.02	
94	SLD 3	136	-12	1476		17.43	-7.67	0	
94	SLD 4	136	-12	1476		17.43	-7.67	0	
94	SLD 5	68	-12	1485		-11.49	-0.57	0.02	
94	SLD 6	68	-12	1485		-11.49	-0.57	0.02	
94	SLD 7	-11	3	1512		19.37	-3.88	-0.02	
94	SLD 8	-11	3	1512		19.37	-3.88	-0.02	
94	SLD 9	-35	-4	1507		-19.08	3.67	0.02	
94	SLD 10	-35	-4	1507		-19.08	3.67	0.02	
94	SLD 11	-113	12	1534		11.77	0.36	-0.02	
94	SLD 12	-113	12	1534		11.77	0.36	-0.02	
94	SLD 13	-182	11	1543		-17.15	7.46	0	
94	SLD 14	-182	11	1543		-17.15	7.46	0	
94	SLD 15	-206	16	1551		-7.89	6.47	-0.02	
94	SLD 16	-206	16	1551		-7.89	6.47	-0.02	
94	SLV 1	413	-42	1403		21.79	-15.72	0.04	
94	SLV 2	413	-42	1403		21.79	-15.72	0.04	
94	SLV 3	357	-31	1423		43.52	-18.08	0.01	
94	SLV 4	357	-31	1423		43.52	-18.08	0.01	
94	SLV 5	192	-29	1448		-26.31	-1.22	0.06	



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
94	SLV 6	192	-29	1448	-26.31	-1.22	0.06
94	SLV 7	7	7	1513	46.1	-9.07	-0.04
94	SLV 8	7	7	1513	46.1	-9.07	-0.04
94	SLV 9	-52	-8	1506	-45.82	8.86	0.04
94	SLV 10	-52	-8	1506	-45.82	8.86	0.04
94	SLV 11	-238	29	1571	26.59	1.01	-0.06
94	SLV 12	-238	29	1571	26.59	1.01	-0.06
94	SLV 13	-403	30	1596	-43.23	17.87	-0.01
94	SLV 14	-403	30	1596	-43.23	17.87	-0.01
94	SLV 15	-459	41	1616	-21.51	15.51	-0.04
94	SLV 16	-459	41	1616	-21.51	15.51	-0.04
95	SLU 1	-46	0	1145	0.1	-0.23	0
95	SLU 2	-121	4	1210	-4.01	-5.57	0
95	SLU 3	-46	0	1145	0.1	-0.23	0
95	SLU 4	-91	3	1184	-2.37	-3.43	0
95	SLU 5	-121	4	1210	-4.01	-5.57	0
95	SLU 6	-46	0	1145	0.1	-0.23	0
95	SLU 7	-91	3	1184	-2.37	-3.43	0
95	SLU 8	-46	0	1145	0.1	-0.23	0
95	SLU 9	-91	3	1184	-2.37	-3.43	0
95	SLU 10	-132	4	1310	-3.91	-4.86	0
95	SLU 11	-56	0	1245	0.2	0.48	0
95	SLU 12	-101	2	1284	-2.26	-2.72	0
95	SLU 13	-132	4	1310	-3.91	-4.86	0
95	SLU 14	-56	0	1245	0.2	0.48	0
95	SLU 15	-101	2	1284	-2.26	-2.72	0
95	SLU 16	-56	0	1245	0.2	0.48	0
95	SLU 17	-101	2	1284	-2.26	-2.72	0
95	SLU 18	-60	0	1288	0.25	0.78	0
95	SLU 19	-106	2	1327	-2.22	-2.42	0
95	SLU 20	-60	0	1288	0.25	0.78	0
95	SLU 21	-106	2	1327	-2.22	-2.42	0
95	SLU 22	-52	0	1197	0.14	0.01	0
95	SLU 23	-128	4	1262	-3.97	-5.32	0
95	SLU 24	-52	0	1197	0.14	0.01	0
95	SLU 25	-98	2	1236	-2.33	-3.19	0
95	SLU 26	-128	4	1262	-3.97	-5.32	0
95	SLU 27	-52	0	1197	0.14	0.01	0
95	SLU 28	-98	2	1236	-2.33	-3.19	0
95	SLU 29	-52	0	1197	0.14	0.01	0
95	SLU 30	-98	2	1236	-2.33	-3.19	0
95	SLU 31	-138	4	1362	-3.86	-4.62	0
95	SLU 32	-63	0	1297	0.25	0.72	0
95	SLU 33	-108	2	1336	-2.22	-2.48	0
95	SLU 34	-138	4	1362	-3.86	-4.62	0
95	SLU 35	-63	0	1297	0.25	0.72	0
95	SLU 36	-108	2	1336	-2.22	-2.48	0
95	SLU 37	-63	0	1297	0.25	0.72	0
95	SLU 38	-108	2	1336	-2.22	-2.48	0
95	SLU 39	-67	0	1340	0.29	1.02	0
95	SLU 40	-112	2	1379	-2.17	-2.18	0
95	SLU 41	-67	0	1340	0.29	1.02	0
95	SLU 42	-112	2	1379	-2.17	-2.18	0
95	SLU 43	-57	0	1471	0.11	-0.38	0
95	SLU 44	-133	4	1536	-4	-5.72	0
95	SLU 45	-57	0	1471	0.11	-0.38	0
95	SLU 46	-103	2	1510	-2.35	-3.58	0
95	SLU 47	-133	4	1536	-4	-5.72	0
95	SLU 48	-57	0	1471	0.11	-0.38	0
95	SLU 49	-103	2	1510	-2.35	-3.58	0
95	SLU 50	-57	0	1471	0.11	-0.38	0
95	SLU 51	-103	2	1510	-2.35	-3.58	0
95	SLU 52	-143	4	1636	-3.89	-5.01	0
95	SLU 53	-67	0	1571	0.22	0.33	0
95	SLU 54	-113	2	1610	-2.25	-2.87	0
95	SLU 55	-143	4	1636	-3.89	-5.01	0
95	SLU 56	-67	0	1571	0.22	0.33	0
95	SLU 57	-113	2	1610	-2.25	-2.87	0
95	SLU 58	-67	0	1571	0.22	0.33	0
95	SLU 59	-113	2	1610	-2.25	-2.87	0
95	SLU 60	-72	0	1613	0.26	0.63	0
95	SLU 61	-117	2	1653	-2.2	-2.57	0
95	SLU 62	-72	0	1613	0.26	0.63	0
95	SLU 63	-117	2	1653	-2.2	-2.57	0
95	SLU 64	-64	0	1523	0.15	-0.14	0
95	SLU 65	-139	4	1588	-3.96	-5.48	0
95	SLU 66	-64	0	1523	0.15	-0.14	0
95	SLU 67	-109	2	1562	-2.31	-3.34	0
95	SLU 68	-139	4	1588	-3.96	-5.48	0
95	SLU 69	-64	0	1523	0.15	-0.14	0
95	SLU 70	-109	2	1562	-2.31	-3.34	0
95	SLU 71	-64	0	1523	0.15	-0.14	0
95	SLU 72	-109	2	1562	-2.31	-3.34	0
95	SLU 73	-150	4	1688	-3.85	-4.77	0
95	SLU 74	-74	0	1623	0.26	0.57	0
95	SLU 75	-119	2	1662	-2.21	-2.63	0
95	SLU 76	-150	4	1688	-3.85	-4.77	0
95	SLU 77	-74	0	1623	0.26	0.57	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
95	SLU 78	-119	2	1662	-2.21	-2.63	0
95	SLU 79	-74	0	1623	0.26	0.57	0
95	SLU 80	-119	2	1662	-2.21	-2.63	0
95	SLU 81	-78	0	1665	0.3	0.87	0
95	SLU 82	-124	2	1705	-2.16	-2.33	0
95	SLU 83	-78	0	1665	0.3	0.87	0
95	SLU 84	-124	2	1705	-2.16	-2.33	0
95	SLE RA 1	-48	0	1160	0.11	-0.16	0
95	SLE RA 2	-98	3	1203	-2.63	-3.72	0
95	SLE RA 3	-48	0	1160	0.11	-0.16	0
95	SLE RA 4	-78	2	1186	-1.53	-2.29	0
95	SLE RA 5	-98	3	1203	-2.63	-3.72	0
95	SLE RA 6	-48	0	1160	0.11	-0.16	0
95	SLE RA 7	-78	2	1186	-1.53	-2.29	0
95	SLE RA 8	-48	0	1160	0.11	-0.16	0
95	SLE RA 9	-78	2	1186	-1.53	-2.29	0
95	SLE RA 10	-105	3	1270	-2.56	-3.25	0
95	SLE RA 11	-54	0	1226	0.18	0.31	0
95	SLE RA 12	-85	2	1253	-1.46	-1.82	0
95	SLE RA 13	-105	3	1270	-2.56	-3.25	0
95	SLE RA 14	-54	0	1226	0.18	0.31	0
95	SLE RA 15	-85	2	1253	-1.46	-1.82	0
95	SLE RA 16	-54	0	1226	0.18	0.31	0
95	SLE RA 17	-85	2	1253	-1.46	-1.82	0
95	SLE RA 18	-57	0	1255	0.21	0.51	0
95	SLE RA 19	-88	1	1281	-1.43	-1.62	0
95	SLE RA 20	-57	0	1255	0.21	0.51	0
95	SLE RA 21	-88	1	1281	-1.43	-1.62	0
95	SLE FR 1	-48	0	1160	0.11	-0.16	0
95	SLE FR 2	-58	0	1169	-0.44	-0.87	0
95	SLE FR 3	-48	0	1160	0.11	-0.16	0
95	SLE FR 4	-61	0	1197	-0.41	-0.67	0
95	SLE FR 5	-50	0	1188	0.14	0.04	0
95	SLE FR 6	-52	0	1207	0.16	0.18	0
95	SLE QP 1	-48	0	1160	0.11	-0.16	0
95	SLE QP 2	-50	0	1188	0.14	0.04	0
95	SLD 1	155	-19	1046	8.93	10.48	0.01
95	SLD 2	155	-19	1046	8.93	10.48	0.01
95	SLD 3	130	-12	1063	26.61	9.28	0.01
95	SLD 4	130	-12	1063	26.61	9.28	0.01
95	SLD 5	49	-17	1120	-24.04	5	0.01
95	SLD 6	49	-17	1120	-24.04	5	0.01
95	SLD 7	-34	8	1176	34.9	0.99	0
95	SLD 8	-34	8	1176	34.9	0.99	0
95	SLD 9	-67	-8	1201	-34.62	-0.91	0
95	SLD 10	-67	-8	1201	-34.62	-0.91	0
95	SLD 11	-150	17	1257	24.32	-4.91	-0.01
95	SLD 12	-150	17	1257	24.32	-4.91	-0.01
95	SLD 13	-231	11	1314	-26.34	-9.2	-0.01
95	SLD 14	-231	11	1314	-26.34	-9.2	-0.01
95	SLD 15	-256	18	1331	-8.65	-10.4	-0.01
95	SLD 16	-256	18	1331	-8.65	-10.4	-0.01
95	SLV 1	453	-47	832	24.35	26.26	0.02
95	SLV 2	453	-47	832	24.35	26.26	0.02
95	SLV 3	394	-30	872	65.8	23.38	0.02
95	SLV 4	394	-30	872	65.8	23.38	0.02
95	SLV 5	190	-40	1020	-55.47	12.28	0.02
95	SLV 6	190	-40	1020	-55.47	12.28	0.02
95	SLV 7	-7	17	1155	82.71	2.67	0
95	SLV 8	-7	17	1155	82.71	2.67	0
95	SLV 9	-94	-17	1222	-82.43	-2.59	0
95	SLV 10	-94	-17	1222	-82.43	-2.59	0
95	SLV 11	-291	40	1357	55.75	-12.19	-0.02
95	SLV 12	-291	40	1357	55.75	-12.19	-0.02
95	SLV 13	-495	30	1505	-65.52	-23.3	-0.02
95	SLV 14	-495	30	1505	-65.52	-23.3	-0.02
95	SLV 15	-554	47	1545	-24.07	-26.18	-0.02
95	SLV 16	-554	47	1545	-24.07	-26.18	-0.02
96	SLU 1	-77	0	886	0.09	-2.27	0
96	SLU 2	-112	4	997	-4.39	-2.05	0
96	SLU 3	-77	0	886	0.09	-2.27	0
96	SLU 4	-98	2	953	-2.6	-2.14	0
96	SLU 5	-112	4	997	-4.39	-2.05	0
96	SLU 6	-77	0	886	0.09	-2.27	0
96	SLU 7	-98	2	953	-2.6	-2.14	0
96	SLU 8	-77	0	886	0.09	-2.27	0
96	SLU 9	-98	2	953	-2.6	-2.14	0
96	SLU 10	-127	4	983	-4.31	-2.69	0
96	SLU 11	-92	0	873	0.18	-2.91	0
96	SLU 12	-113	2	939	-2.51	-2.77	0
96	SLU 13	-127	4	983	-4.31	-2.69	0
96	SLU 14	-92	0	873	0.18	-2.91	0
96	SLU 15	-113	2	939	-2.51	-2.77	0
96	SLU 16	-92	0	873	0.18	-2.91	0
96	SLU 17	-113	2	939	-2.51	-2.77	0
96	SLU 18	-98	0	867	0.21	-3.18	0
96	SLU 19	-120	2	933	-2.48	-3.05	0
96	SLU 20	-98	0	867	0.21	-3.18	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
96	SLU 21	-120	2	933	-2.48	-3.05	0
96	SLU 22	-84	0	881	0.12	-2.53	0
96	SLU 23	-120	4	992	-4.36	-2.32	0
96	SLU 24	-84	0	881	0.12	-2.53	0
96	SLU 25	-106	2	947	-2.57	-2.4	0
96	SLU 26	-120	4	992	-4.36	-2.32	0
96	SLU 27	-84	0	881	0.12	-2.53	0
96	SLU 28	-106	2	947	-2.57	-2.4	0
96	SLU 29	-84	0	881	0.12	-2.53	0
96	SLU 30	-106	2	947	-2.57	-2.4	0
96	SLU 31	-135	4	978	-4.27	-2.95	0
96	SLU 32	-100	0	867	0.21	-3.17	0
96	SLU 33	-121	2	934	-2.48	-3.04	0
96	SLU 34	-135	4	978	-4.27	-2.95	0
96	SLU 35	-100	0	867	0.21	-3.17	0
96	SLU 36	-121	2	934	-2.48	-3.04	0
96	SLU 37	-100	0	867	0.21	-3.17	0
96	SLU 38	-121	2	934	-2.48	-3.04	0
96	SLU 39	-106	0	861	0.25	-3.44	0
96	SLU 40	-127	2	928	-2.44	-3.31	0
96	SLU 41	-106	0	861	0.25	-3.44	0
96	SLU 42	-127	2	928	-2.44	-3.31	0
96	SLU 43	-97	0	1154	0.1	-2.86	0
96	SLU 44	-132	4	1265	-4.38	-2.64	0
96	SLU 45	-97	0	1154	0.1	-2.86	0
96	SLU 46	-118	2	1220	-2.59	-2.73	0
96	SLU 47	-132	4	1265	-4.38	-2.64	0
96	SLU 48	-97	0	1154	0.1	-2.86	0
96	SLU 49	-118	2	1220	-2.59	-2.73	0
96	SLU 50	-97	0	1154	0.1	-2.86	0
96	SLU 51	-118	2	1220	-2.59	-2.73	0
96	SLU 52	-148	4	1251	-4.29	-3.28	0
96	SLU 53	-112	0	1140	0.19	-3.49	0
96	SLU 54	-133	2	1207	-2.5	-3.36	0
96	SLU 55	-148	4	1251	-4.29	-3.28	0
96	SLU 56	-112	0	1140	0.19	-3.49	0
96	SLU 57	-133	2	1207	-2.5	-3.36	0
96	SLU 58	-112	0	1140	0.19	-3.49	0
96	SLU 59	-133	2	1207	-2.5	-3.36	0
96	SLU 60	-119	0	1134	0.23	-3.77	0
96	SLU 61	-140	2	1201	-2.46	-3.64	0
96	SLU 62	-119	0	1134	0.23	-3.77	0
96	SLU 63	-140	2	1201	-2.46	-3.64	0
96	SLU 64	-105	0	1149	0.14	-3.12	0
96	SLU 65	-140	4	1259	-4.34	-2.91	0
96	SLU 66	-105	0	1149	0.14	-3.12	0
96	SLU 67	-126	2	1215	-2.55	-2.99	0
96	SLU 68	-140	4	1259	-4.34	-2.91	0
96	SLU 69	-105	0	1149	0.14	-3.12	0
96	SLU 70	-126	2	1215	-2.55	-2.99	0
96	SLU 71	-105	0	1149	0.14	-3.12	0
96	SLU 72	-126	2	1215	-2.55	-2.99	0
96	SLU 73	-155	4	1246	-4.26	-3.54	0
96	SLU 74	-120	0	1135	0.23	-3.76	0
96	SLU 75	-141	2	1201	-2.46	-3.63	0
96	SLU 76	-155	4	1246	-4.26	-3.54	0
96	SLU 77	-120	0	1135	0.23	-3.76	0
96	SLU 78	-141	2	1201	-2.46	-3.63	0
96	SLU 79	-120	0	1135	0.23	-3.76	0
96	SLU 80	-141	2	1201	-2.46	-3.63	0
96	SLU 81	-126	0	1129	0.26	-4.03	0
96	SLU 82	-148	2	1195	-2.43	-3.9	0
96	SLU 83	-126	0	1129	0.26	-4.03	0
96	SLU 84	-148	2	1195	-2.43	-3.9	0
96	SLE RA 1	-79	0	885	0.1	-2.35	0
96	SLE RA 2	-103	3	959	-2.89	-2.2	0
96	SLE RA 3	-79	0	885	0.1	-2.35	0
96	SLE RA 4	-93	2	929	-1.7	-2.26	0
96	SLE RA 5	-103	3	959	-2.89	-2.2	0
96	SLE RA 6	-79	0	885	0.1	-2.35	0
96	SLE RA 7	-93	2	929	-1.7	-2.26	0
96	SLE RA 8	-79	0	885	0.1	-2.35	0
96	SLE RA 9	-93	2	929	-1.7	-2.26	0
96	SLE RA 10	-113	3	949	-2.83	-2.62	0
96	SLE RA 11	-89	0	876	0.16	-2.77	0
96	SLE RA 12	-103	2	920	-1.64	-2.68	0
96	SLE RA 13	-113	3	949	-2.83	-2.62	0
96	SLE RA 14	-89	0	876	0.16	-2.77	0
96	SLE RA 15	-103	2	920	-1.64	-2.68	0
96	SLE RA 16	-89	0	876	0.16	-2.77	0
96	SLE RA 17	-103	2	920	-1.64	-2.68	0
96	SLE RA 18	-93	0	872	0.18	-2.95	0
96	SLE RA 19	-107	1	916	-1.61	-2.86	0
96	SLE RA 20	-93	0	872	0.18	-2.95	0
96	SLE RA 21	-107	1	916	-1.61	-2.86	0
96	SLE FR 1	-79	0	885	0.1	-2.35	0
96	SLE FR 2	-84	0	900	-0.5	-2.32	0
96	SLE FR 3	-79	0	885	0.1	-2.35	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
96	SLE FR 4	-88	0	896	-0.47	-2.5	0
96	SLE FR 5	-83	0	881	0.12	-2.53	0
96	SLE FR 6	-86	0	878	0.14	-2.65	0
96	SLE QP 1	-79	0	885	0.1	-2.35	0
96	SLE QP 2	-83	0	881	0.12	-2.53	0
96	SLD 1	91	-9	619	8.88	-8.82	0
96	SLD 2	91	-9	619	8.88	-8.82	0
96	SLD 3	69	-28	649	37.03	-9.75	0.02
96	SLD 4	69	-28	649	37.03	-9.75	0.02
96	SLD 5	2	26	756	-39.94	-2.99	-0.02
96	SLD 6	2	26	756	-39.94	-2.99	-0.02
96	SLD 7	-71	-37	857	53.89	-6.12	0.03
96	SLD 8	-71	-37	857	53.89	-6.12	0.03
96	SLD 9	-96	37	905	-53.64	1.06	-0.03
96	SLD 10	-96	37	905	-53.64	1.06	-0.03
96	SLD 11	-168	-26	1005	40.19	-2.06	0.02
96	SLD 12	-168	-26	1005	40.19	-2.06	0.02
96	SLD 13	-235	28	1113	-36.78	4.7	-0.02
96	SLD 14	-235	28	1113	-36.78	4.7	-0.02
96	SLD 15	-257	9	1143	-8.63	3.76	0
96	SLD 16	-257	9	1143	-8.63	3.76	0
96	SLV 1	334	-25	232	24.72	-17.47	0.01
96	SLV 2	334	-25	232	24.72	-17.47	0.01
96	SLV 3	282	-69	304	90.67	-19.7	0.04
96	SLV 4	282	-69	304	90.67	-19.7	0.04
96	SLV 5	120	59	577	-92.52	-3.64	-0.05
96	SLV 6	120	59	577	-92.52	-3.64	-0.05
96	SLV 7	-52	-88	817	127.31	-11.05	0.06
96	SLV 8	-52	-88	817	127.31	-11.05	0.06
96	SLV 9	-114	87	944	-127.07	6	-0.06
96	SLV 10	-114	87	944	-127.07	6	-0.06
96	SLV 11	-287	-60	1185	92.77	-1.42	0.05
96	SLV 12	-287	-60	1185	92.77	-1.42	0.05
96	SLV 13	-448	68	1458	-90.42	14.64	-0.04
96	SLV 14	-448	68	1458	-90.42	14.64	-0.04
96	SLV 15	-500	24	1530	-24.47	12.42	-0.01
96	SLV 16	-500	24	1530	-24.47	12.42	-0.01
97	SLU 1	-89	0	639	0.08	-2.32	0
97	SLU 2	-162	5	829	-4.46	-7.79	0.02
97	SLU 3	-89	0	639	0.08	-2.32	0
97	SLU 4	-133	3	753	-2.64	-5.6	0.01
97	SLU 5	-162	5	829	-4.46	-7.79	0.02
97	SLU 6	-89	0	639	0.08	-2.32	0
97	SLU 7	-133	3	753	-2.64	-5.6	0.01
97	SLU 8	-89	0	639	0.08	-2.32	0
97	SLU 9	-133	3	753	-2.64	-5.6	0.01
97	SLU 10	-155	5	695	-4.39	-6.32	0.02
97	SLU 11	-82	0	506	0.15	-0.84	0
97	SLU 12	-126	3	619	-2.57	-4.13	0.01
97	SLU 13	-155	5	695	-4.39	-6.32	0.02
97	SLU 14	-82	0	506	0.15	-0.84	0
97	SLU 15	-126	3	619	-2.57	-4.13	0.01
97	SLU 16	-82	0	506	0.15	-0.84	0
97	SLU 17	-126	3	619	-2.57	-4.13	0.01
97	SLU 18	-79	0	448	0.18	-0.21	0
97	SLU 19	-123	3	562	-2.54	-3.49	0.01
97	SLU 20	-79	0	448	0.18	-0.21	0
97	SLU 21	-123	3	562	-2.54	-3.49	0.01
97	SLU 22	-87	0	574	0.11	-1.69	0
97	SLU 23	-160	5	764	-4.43	-7.16	0.02
97	SLU 24	-87	0	574	0.11	-1.69	0
97	SLU 25	-130	3	688	-2.61	-4.97	0.01
97	SLU 26	-160	5	764	-4.43	-7.16	0.02
97	SLU 27	-87	0	574	0.11	-1.69	0
97	SLU 28	-130	3	688	-2.61	-4.97	0.01
97	SLU 29	-87	0	574	0.11	-1.69	0
97	SLU 30	-130	3	688	-2.61	-4.97	0.01
97	SLU 31	-152	5	630	-4.36	-5.69	0.02
97	SLU 32	-80	0	441	0.18	-0.21	0
97	SLU 33	-123	3	554	-2.54	-3.5	0.01
97	SLU 34	-152	5	630	-4.36	-5.69	0.02
97	SLU 35	-80	0	441	0.18	-0.21	0
97	SLU 36	-123	3	554	-2.54	-3.5	0.01
97	SLU 37	-80	0	441	0.18	-0.21	0
97	SLU 38	-123	3	554	-2.54	-3.5	0.01
97	SLU 39	-76	0	384	0.21	0.42	0
97	SLU 40	-120	3	497	-2.51	-2.86	0.01
97	SLU 41	-76	0	384	0.21	0.42	0
97	SLU 42	-120	3	497	-2.51	-2.86	0.01
97	SLU 43	-117	0	853	0.09	-3.23	0
97	SLU 44	-190	5	1042	-4.44	-8.71	0.02
97	SLU 45	-117	0	853	0.09	-3.23	0
97	SLU 46	-160	3	967	-2.63	-6.51	0.01
97	SLU 47	-190	5	1042	-4.44	-8.71	0.02
97	SLU 48	-117	0	853	0.09	-3.23	0
97	SLU 49	-160	3	967	-2.63	-6.51	0.01
97	SLU 50	-117	0	853	0.09	-3.23	0
97	SLU 51	-160	3	967	-2.63	-6.51	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
97	SLU 52	-182	5	909	-4.37	-7.23	0.02
97	SLU 53	-110	0	719	0.16	-1.75	0
97	SLU 54	-153	3	833	-2.56	-5.04	0.01
97	SLU 55	-182	5	909	-4.37	-7.23	0.02
97	SLU 56	-110	0	719	0.16	-1.75	0
97	SLU 57	-153	3	833	-2.56	-5.04	0.01
97	SLU 58	-110	0	719	0.16	-1.75	0
97	SLU 59	-153	3	833	-2.56	-5.04	0.01
97	SLU 60	-106	0	662	0.19	-1.12	0
97	SLU 61	-150	3	776	-2.53	-4.41	0.01
97	SLU 62	-106	0	662	0.19	-1.12	0
97	SLU 63	-150	3	776	-2.53	-4.41	0.01
97	SLU 64	-114	0	788	0.12	-2.6	0
97	SLU 65	-187	5	978	-4.41	-8.07	0.02
97	SLU 66	-114	0	788	0.12	-2.6	0
97	SLU 67	-158	3	902	-2.6	-5.88	0.01
97	SLU 68	-187	5	978	-4.41	-8.07	0.02
97	SLU 69	-114	0	788	0.12	-2.6	0
97	SLU 70	-158	3	902	-2.6	-5.88	0.01
97	SLU 71	-114	0	788	0.12	-2.6	0
97	SLU 72	-158	3	902	-2.6	-5.88	0.01
97	SLU 73	-180	5	844	-4.34	-6.6	0.02
97	SLU 74	-107	0	655	0.19	-1.12	0
97	SLU 75	-151	3	768	-2.53	-4.41	0.01
97	SLU 76	-180	5	844	-4.34	-6.6	0.02
97	SLU 77	-107	0	655	0.19	-1.12	0
97	SLU 78	-151	3	768	-2.53	-4.41	0.01
97	SLU 79	-107	0	655	0.19	-1.12	0
97	SLU 80	-151	3	768	-2.53	-4.41	0.01
97	SLU 81	-104	0	597	0.22	-0.49	0
97	SLU 82	-148	3	711	-2.5	-3.77	0.01
97	SLU 83	-104	0	597	0.22	-0.49	0
97	SLU 84	-148	3	711	-2.5	-3.77	0.01
97	SLE RA 1	-88	0	620	0.08	-2.14	0
97	SLE RA 2	-137	3	747	-2.94	-5.79	0.01
97	SLE RA 3	-88	0	620	0.08	-2.14	0
97	SLE RA 4	-118	2	696	-1.73	-4.33	0.01
97	SLE RA 5	-137	3	747	-2.94	-5.79	0.01
97	SLE RA 6	-88	0	620	0.08	-2.14	0
97	SLE RA 7	-118	2	696	-1.73	-4.33	0.01
97	SLE RA 8	-88	0	620	0.08	-2.14	0
97	SLE RA 9	-118	2	696	-1.73	-4.33	0.01
97	SLE RA 10	-132	3	658	-2.89	-4.8	0.01
97	SLE RA 11	-84	0	531	0.13	-1.15	0
97	SLE RA 12	-113	2	607	-1.68	-3.34	0.01
97	SLE RA 13	-132	3	658	-2.89	-4.8	0.01
97	SLE RA 14	-84	0	531	0.13	-1.15	0
97	SLE RA 15	-113	2	607	-1.68	-3.34	0.01
97	SLE RA 16	-84	0	531	0.13	-1.15	0
97	SLE RA 17	-113	2	607	-1.68	-3.34	0.01
97	SLE RA 18	-82	0	493	0.15	-0.73	0
97	SLE RA 19	-111	2	569	-1.66	-2.92	0.01
97	SLE RA 20	-82	0	493	0.15	-0.73	0
97	SLE RA 21	-111	2	569	-1.66	-2.92	0.01
97	SLE FR 1	-88	0	620	0.08	-2.14	0
97	SLE FR 2	-98	1	646	-0.52	-2.87	0
97	SLE FR 3	-88	0	620	0.08	-2.14	0
97	SLE FR 4	-96	1	607	-0.5	-2.45	0
97	SLE FR 5	-86	0	582	0.1	-1.71	0
97	SLE FR 6	-85	0	557	0.12	-1.43	0
97	SLE QP 1	-88	0	620	0.08	-2.14	0
97	SLE QP 2	-86	0	582	0.1	-1.71	0
97	SLD 1	89	-9	98	8.47	8.68	-0.04
97	SLD 2	89	-9	98	8.47	8.68	-0.04
97	SLD 3	68	-57	154	48.31	7.5	-0.25
97	SLD 4	68	-57	154	48.31	7.5	-0.25
97	SLD 5	-3	70	351	-57.82	3.18	0.3
97	SLD 6	-3	70	351	-57.82	3.18	0.3
97	SLD 7	-71	-90	539	75	-0.73	-0.39
97	SLD 8	-71	-90	539	75	-0.73	-0.39
97	SLD 9	-102	90	625	-74.79	-2.7	0.39
97	SLD 10	-102	90	625	-74.79	-2.7	0.39
97	SLD 11	-170	-70	813	58.03	-6.61	-0.31
97	SLD 12	-170	-70	813	58.03	-6.61	-0.31
97	SLD 13	-241	57	1010	-48.11	-10.93	0.25
97	SLD 14	-241	57	1010	-48.11	-10.93	0.25
97	SLD 15	-262	9	1066	-8.26	-12.11	0.04
97	SLD 16	-262	9	1066	-8.26	-12.11	0.04
97	SLV 1	346	-27	-608	23.98	24.47	-0.11
97	SLV 2	346	-27	-608	23.98	24.47	-0.11
97	SLV 3	297	-139	-474	117.31	21.65	-0.6
97	SLV 4	297	-139	-474	117.31	21.65	-0.6
97	SLV 5	118	162	21	-134.29	10.42	0.71
97	SLV 6	118	162	21	-134.29	10.42	0.71
97	SLV 7	-46	-212	469	176.83	1.02	-0.92
97	SLV 8	-46	-212	469	176.83	1.02	-0.92
97	SLV 9	-127	211	695	-176.62	-4.45	0.92
97	SLV 10	-127	211	695	-176.62	-4.45	0.92



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
97	SLV 11	-291	-162	1143	134.5	-13.85	-0.71
97	SLV 12	-291	-162	1143	134.5	-13.85	-0.71
97	SLV 13	-470	139	1638	-117.1	-25.08	0.6
97	SLV 14	-470	139	1638	-117.1	-25.08	0.6
97	SLV 15	-519	27	1772	-23.77	-27.9	0.11
97	SLV 16	-519	27	1772	-23.77	-27.9	0.11
98	SLU 1	-80	0	274	0.03	-2.05	0
98	SLU 2	-120	0	431	-2	-2.33	-0.28
98	SLU 3	-80	0	274	0.03	-2.05	0
98	SLU 4	-104	0	368	-1.19	-2.22	-0.16
98	SLU 5	-120	0	431	-2	-2.33	-0.28
98	SLU 6	-80	0	274	0.03	-2.05	0
98	SLU 7	-104	0	368	-1.19	-2.22	-0.16
98	SLU 8	-80	0	274	0.03	-2.05	0
98	SLU 9	-104	0	368	-1.19	-2.22	-0.16
98	SLU 10	-99	0	310	-1.97	-2.01	-0.27
98	SLU 11	-59	0	154	0.06	-1.72	0.01
98	SLU 12	-83	0	248	-1.16	-1.9	-0.16
98	SLU 13	-99	0	310	-1.97	-2.01	-0.27
98	SLU 14	-59	0	154	0.06	-1.72	0.01
98	SLU 15	-83	0	248	-1.16	-1.9	-0.16
98	SLU 16	-59	0	154	0.06	-1.72	0.01
98	SLU 17	-83	0	248	-1.16	-1.9	-0.16
98	SLU 18	-50	0	102	0.07	-1.59	0.01
98	SLU 19	-74	0	196	-1.15	-1.76	-0.16
98	SLU 20	-50	0	102	0.07	-1.59	0.01
98	SLU 21	-74	0	196	-1.15	-1.76	-0.16
98	SLU 22	-70	0	215	0.04	-1.86	0.01
98	SLU 23	-109	0	372	-1.99	-2.15	-0.27
98	SLU 24	-70	0	215	0.04	-1.86	0.01
98	SLU 25	-94	0	309	-1.18	-2.03	-0.16
98	SLU 26	-109	0	372	-1.99	-2.15	-0.27
98	SLU 27	-70	0	215	0.04	-1.86	0.01
98	SLU 28	-94	0	309	-1.18	-2.03	-0.16
98	SLU 29	-70	0	215	0.04	-1.86	0.01
98	SLU 30	-94	0	309	-1.18	-2.03	-0.16
98	SLU 31	-88	0	251	-1.96	-1.83	-0.27
98	SLU 32	-49	0	95	0.07	-1.54	0.01
98	SLU 33	-72	0	189	-1.15	-1.71	-0.16
98	SLU 34	-88	0	251	-1.96	-1.83	-0.27
98	SLU 35	-49	0	95	0.07	-1.54	0.01
98	SLU 36	-72	0	189	-1.15	-1.71	-0.16
98	SLU 37	-49	0	95	0.07	-1.54	0.01
98	SLU 38	-72	0	189	-1.15	-1.71	-0.16
98	SLU 39	-39	0	43	0.08	-1.4	0.01
98	SLU 40	-63	0	137	-1.14	-1.57	-0.16
98	SLU 41	-39	0	43	0.08	-1.4	0.01
98	SLU 42	-63	0	137	-1.14	-1.57	-0.16
98	SLU 43	-108	0	376	0.04	-2.72	0
98	SLU 44	-148	0	533	-1.99	-3.01	-0.28
98	SLU 45	-108	0	376	0.04	-2.72	0
98	SLU 46	-132	0	470	-1.18	-2.89	-0.16
98	SLU 47	-148	0	533	-1.99	-3.01	-0.28
98	SLU 48	-108	0	376	0.04	-2.72	0
98	SLU 49	-132	0	470	-1.18	-2.89	-0.16
98	SLU 50	-108	0	376	0.04	-2.72	0
98	SLU 51	-132	0	470	-1.18	-2.89	-0.16
98	SLU 52	-126	0	413	-1.97	-2.69	-0.27
98	SLU 53	-87	0	256	0.06	-2.4	0.01
98	SLU 54	-111	0	350	-1.15	-2.57	-0.16
98	SLU 55	-126	0	413	-1.97	-2.69	-0.27
98	SLU 56	-87	0	256	0.06	-2.4	0.01
98	SLU 57	-111	0	350	-1.15	-2.57	-0.16
98	SLU 58	-87	0	256	0.06	-2.4	0.01
98	SLU 59	-111	0	350	-1.15	-2.57	-0.16
98	SLU 60	-78	0	204	0.07	-2.26	0.01
98	SLU 61	-101	0	298	-1.14	-2.44	-0.16
98	SLU 62	-78	0	204	0.07	-2.26	0.01
98	SLU 63	-101	0	298	-1.14	-2.44	-0.16
98	SLU 64	-98	0	317	0.05	-2.54	0.01
98	SLU 65	-137	0	474	-1.98	-2.82	-0.27
98	SLU 66	-98	0	317	0.05	-2.54	0.01
98	SLU 67	-121	0	411	-1.17	-2.71	-0.16
98	SLU 68	-137	0	474	-1.98	-2.82	-0.27
98	SLU 69	-98	0	317	0.05	-2.54	0.01
98	SLU 70	-121	0	411	-1.17	-2.71	-0.16
98	SLU 71	-98	0	317	0.05	-2.54	0.01
98	SLU 72	-121	0	411	-1.17	-2.71	-0.16
98	SLU 73	-116	0	354	-1.95	-2.5	-0.27
98	SLU 74	-76	0	197	0.07	-2.22	0.01
98	SLU 75	-100	0	291	-1.14	-2.39	-0.16
98	SLU 76	-116	0	354	-1.95	-2.5	-0.27
98	SLU 77	-76	0	197	0.07	-2.22	0.01
98	SLU 78	-100	0	291	-1.14	-2.39	-0.16
98	SLU 79	-76	0	197	0.07	-2.22	0.01
98	SLU 80	-100	0	291	-1.14	-2.39	-0.16
98	SLU 81	-67	0	145	0.08	-2.08	0.01
98	SLU 82	-91	0	239	-1.13	-2.25	-0.16



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
98	SLU 83	-67	0	145	0.08	-2.08	0.01
98	SLU 84	-91	0	239	-1.13	-2.25	-0.16
98	SLE RA 1	-77	0	257	0.03	-1.99	0
98	SLE RA 2	-104	0	362	-1.32	-2.18	-0.18
98	SLE RA 3	-77	0	257	0.03	-1.99	0
98	SLE RA 4	-93	0	320	-0.78	-2.11	-0.11
98	SLE RA 5	-104	0	362	-1.32	-2.18	-0.18
98	SLE RA 6	-77	0	257	0.03	-1.99	0
98	SLE RA 7	-93	0	320	-0.78	-2.11	-0.11
98	SLE RA 8	-77	0	257	0.03	-1.99	0
98	SLE RA 9	-93	0	320	-0.78	-2.11	-0.11
98	SLE RA 10	-90	0	281	-1.3	-1.97	-0.18
98	SLE RA 11	-63	0	177	0.05	-1.78	0.01
98	SLE RA 12	-79	0	239	-0.76	-1.89	-0.11
98	SLE RA 13	-90	0	281	-1.3	-1.97	-0.18
98	SLE RA 14	-63	0	177	0.05	-1.78	0.01
98	SLE RA 15	-79	0	239	-0.76	-1.89	-0.11
98	SLE RA 16	-63	0	177	0.05	-1.78	0.01
98	SLE RA 17	-79	0	239	-0.76	-1.89	-0.11
98	SLE RA 18	-57	0	142	0.06	-1.69	0.01
98	SLE RA 19	-73	0	205	-0.75	-1.8	-0.1
98	SLE RA 20	-57	0	142	0.06	-1.69	0.01
98	SLE RA 21	-73	0	205	-0.75	-1.8	-0.1
98	SLE FR 1	-77	0	257	0.03	-1.99	0
98	SLE FR 2	-83	0	278	-0.24	-2.03	-0.03
98	SLE FR 3	-77	0	257	0.03	-1.99	0
98	SLE FR 4	-77	0	244	-0.23	-1.94	-0.03
98	SLE FR 5	-71	0	223	0.04	-1.9	0.01
98	SLE FR 6	-67	0	200	0.05	-1.84	0.01
98	SLE QP 1	-77	0	257	0.03	-1.99	0
98	SLE QP 2	-71	0	223	0.04	-1.9	0.01
98	SLD 1	62	34	-202	3.72	2.16	0.51
98	SLD 2	62	34	-202	3.72	2.16	0.51
98	SLD 3	46	1	-152	26.74	1.65	3.97
98	SLD 4	46	1	-152	26.74	1.65	3.97
98	SLD 5	-7	60	19	-33.76	0.09	-5.08
98	SLD 6	-7	60	19	-33.76	0.09	-5.08
98	SLD 7	-60	-49	186	42.96	-1.61	6.43
98	SLD 8	-60	-49	186	42.96	-1.61	6.43
98	SLD 9	-82	49	259	-42.87	-2.19	-6.42
98	SLD 10	-82	49	259	-42.87	-2.19	-6.42
98	SLD 11	-136	-60	426	33.84	-3.89	5.09
98	SLD 12	-136	-60	426	33.84	-3.89	5.09
98	SLD 13	-189	-1	597	-26.66	-5.45	-3.96
98	SLD 14	-189	-1	597	-26.66	-5.45	-3.96
98	SLD 15	-205	-34	647	-3.64	-5.96	-0.5
98	SLD 16	-205	-34	647	-3.64	-5.96	-0.5
98	SLV 1	253	81	-817	10.66	7.77	1.47
98	SLV 2	253	81	-817	10.66	7.77	1.47
98	SLV 3	215	4	-698	64.56	6.56	9.56
98	SLV 4	215	4	-698	64.56	6.56	9.56
98	SLV 5	84	141	-270	-78.52	2.83	-11.82
98	SLV 6	84	141	-270	-78.52	2.83	-11.82
98	SLV 7	-44	-115	127	101.14	-1.2	15.14
98	SLV 8	-44	-115	127	101.14	-1.2	15.14
98	SLV 9	-99	115	318	-101.06	-2.61	-15.13
98	SLV 10	-99	115	318	-101.06	-2.61	-15.13
98	SLV 11	-227	-141	715	78.6	-6.64	11.83
98	SLV 12	-227	-141	715	78.6	-6.64	11.83
98	SLV 13	-357	-4	1143	-64.48	-10.36	-9.55
98	SLV 14	-357	-4	1143	-64.48	-10.36	-9.55
98	SLV 15	-396	-81	1262	-10.58	-11.57	-1.46
98	SLV 16	-396	-81	1262	-10.58	-11.57	-1.46
99	SLU 1	0	284	1713	-11.53	0.15	0
99	SLU 2	-4	282	1709	-11.5	-6.18	0.01
99	SLU 3	0	284	1713	-11.53	0.15	0
99	SLU 4	-3	283	1711	-11.51	-3.65	0.01
99	SLU 5	-4	282	1709	-11.5	-6.18	0.01
99	SLU 6	0	284	1713	-11.53	0.15	0
99	SLU 7	-3	283	1711	-11.51	-3.65	0.01
99	SLU 8	0	284	1713	-11.53	0.15	0
99	SLU 9	-3	283	1711	-11.51	-3.65	0.01
99	SLU 10	-4	548	2651	-22.32	-5.83	0.01
99	SLU 11	0	549	2655	-22.36	0.51	0
99	SLU 12	-2	548	2653	-22.34	-3.29	0.01
99	SLU 13	-4	548	2651	-22.32	-5.83	0.01
99	SLU 14	0	549	2655	-22.36	0.51	0
99	SLU 15	-2	548	2653	-22.34	-3.29	0.01
99	SLU 16	0	549	2655	-22.36	0.51	0
99	SLU 17	-2	548	2653	-22.34	-3.29	0.01
99	SLU 18	0	663	3058	-26.99	0.66	0
99	SLU 19	-2	662	3056	-26.97	-3.14	0.01
99	SLU 20	0	663	3058	-26.99	0.66	0
99	SLU 21	-2	662	3056	-26.97	-3.14	0.01
99	SLU 22	0	405	2207	-16.44	0.29	0
99	SLU 23	-4	403	2204	-16.4	-6.04	0.01
99	SLU 24	0	405	2207	-16.44	0.29	0
99	SLU 25	-3	404	2205	-16.41	-3.51	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
99	SLU 26	-4	403	2204	-16.4	-6.04	0.01
99	SLU 27	0	405	2207	-16.44	0.29	0
99	SLU 28	-3	404	2205	-16.41	-3.51	0.01
99	SLU 29	0	405	2207	-16.44	0.29	0
99	SLU 30	-3	404	2205	-16.41	-3.51	0.01
99	SLU 31	-4	668	3146	-27.22	-5.68	0.01
99	SLU 32	0	670	3149	-27.26	0.65	0
99	SLU 33	-2	669	3147	-27.24	-3.15	0.01
99	SLU 34	-4	668	3146	-27.22	-5.68	0.01
99	SLU 35	0	670	3149	-27.26	0.65	0
99	SLU 36	-2	669	3147	-27.24	-3.15	0.01
99	SLU 37	0	670	3149	-27.26	0.65	0
99	SLU 38	-2	669	3147	-27.24	-3.15	0.01
99	SLU 39	1	784	3553	-31.89	0.8	0
99	SLU 40	-2	783	3551	-31.87	-3	0
99	SLU 41	1	784	3553	-31.89	0.8	0
99	SLU 42	-2	783	3551	-31.87	-3	0
99	SLU 43	0	328	2057	-13.32	0.15	0
99	SLU 44	-4	326	2054	-13.28	-6.19	0.01
99	SLU 45	0	328	2057	-13.32	0.15	0
99	SLU 46	-3	327	2055	-13.29	-3.65	0.01
99	SLU 47	-4	326	2054	-13.28	-6.19	0.01
99	SLU 48	0	328	2057	-13.32	0.15	0
99	SLU 49	-3	327	2055	-13.29	-3.65	0.01
99	SLU 50	0	328	2057	-13.32	0.15	0
99	SLU 51	-3	327	2055	-13.29	-3.65	0.01
99	SLU 52	-4	592	2996	-24.1	-5.83	0.01
99	SLU 53	0	593	2999	-24.14	0.5	0
99	SLU 54	-2	592	2997	-24.12	-3.3	0.01
99	SLU 55	-4	592	2996	-24.1	-5.83	0.01
99	SLU 56	0	593	2999	-24.14	0.5	0
99	SLU 57	-2	592	2997	-24.12	-3.3	0.01
99	SLU 58	0	593	2999	-24.14	0.5	0
99	SLU 59	-2	592	2997	-24.12	-3.3	0.01
99	SLU 60	0	707	3403	-28.77	0.66	0
99	SLU 61	-2	706	3401	-28.75	-3.14	0.01
99	SLU 62	0	707	3403	-28.77	0.66	0
99	SLU 63	-2	706	3401	-28.75	-3.14	0.01
99	SLU 64	0	448	2551	-18.22	0.29	0
99	SLU 65	-4	447	2548	-18.18	-6.05	0.01
99	SLU 66	0	448	2551	-18.22	0.29	0
99	SLU 67	-3	447	2549	-18.2	-3.51	0.01
99	SLU 68	-4	447	2548	-18.18	-6.05	0.01
99	SLU 69	0	448	2551	-18.22	0.29	0
99	SLU 70	-3	447	2549	-18.2	-3.51	0.01
99	SLU 71	0	448	2551	-18.22	0.29	0
99	SLU 72	-3	447	2549	-18.2	-3.51	0.01
99	SLU 73	-4	712	3490	-29	-5.69	0.01
99	SLU 74	0	714	3493	-29.04	0.65	0
99	SLU 75	-2	713	3491	-29.02	-3.15	0.01
99	SLU 76	-4	712	3490	-29	-5.69	0.01
99	SLU 77	0	714	3493	-29.04	0.65	0
99	SLU 78	-2	713	3491	-29.02	-3.15	0.01
99	SLU 79	0	714	3493	-29.04	0.65	0
99	SLU 80	-2	713	3491	-29.02	-3.15	0.01
99	SLU 81	1	828	3897	-33.67	0.8	0
99	SLU 82	-2	827	3895	-33.65	-3	0
99	SLU 83	1	828	3897	-33.67	0.8	0
99	SLU 84	-2	827	3895	-33.65	-3	0
99	SLE RA 1	0	318	1854	-12.93	0.19	0
99	SLE RA 2	-3	317	1852	-12.91	-4.03	0.01
99	SLE RA 3	0	318	1854	-12.93	0.19	0
99	SLE RA 4	-2	318	1853	-12.92	-2.34	0
99	SLE RA 5	-3	317	1852	-12.91	-4.03	0.01
99	SLE RA 6	0	318	1854	-12.93	0.19	0
99	SLE RA 7	-2	318	1853	-12.92	-2.34	0
99	SLE RA 8	0	318	1854	-12.93	0.19	0
99	SLE RA 9	-2	318	1853	-12.92	-2.34	0
99	SLE RA 10	-3	494	2480	-20.13	-3.79	0.01
99	SLE RA 11	0	495	2482	-20.15	0.43	0
99	SLE RA 12	-2	495	2481	-20.14	-2.1	0
99	SLE RA 13	-3	494	2480	-20.13	-3.79	0.01
99	SLE RA 14	0	495	2482	-20.15	0.43	0
99	SLE RA 15	-2	495	2481	-20.14	-2.1	0
99	SLE RA 16	0	495	2482	-20.15	0.43	0
99	SLE RA 17	-2	495	2481	-20.14	-2.1	0
99	SLE RA 18	0	571	2751	-23.24	0.53	0
99	SLE RA 19	-1	571	2750	-23.23	-2	0
99	SLE RA 20	0	571	2751	-23.24	0.53	0
99	SLE RA 21	-1	571	2750	-23.23	-2	0
99	SLE FR 1	0	318	1854	-12.93	0.19	0
99	SLE FR 2	0	318	1853	-12.93	-0.65	0
99	SLE FR 3	0	318	1854	-12.93	0.19	0
99	SLE FR 4	0	394	2123	-16.02	-0.55	0
99	SLE FR 5	0	394	2123	-16.03	0.29	0
99	SLE FR 6	0	445	2302	-18.09	0.36	0
99	SLE QP 1	0	318	1854	-12.93	0.19	0
99	SLE QP 2	0	394	2123	-16.03	0.29	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
99	SLD 1	23	448	2153	-23.81	28.96	-0.05
99	SLD 2	23	448	2153	-23.81	28.96	-0.05
99	SLD 3	20	262	2116	-4.55	26.75	-0.04
99	SLD 4	20	262	2116	-4.55	26.75	-0.04
99	SLD 5	11	692	2189	-47.57	12.25	-0.02
99	SLD 6	11	692	2189	-47.57	12.25	-0.02
99	SLD 7	2	73	2064	16.62	4.87	-0.01
99	SLD 8	2	73	2064	16.62	4.87	-0.01
99	SLD 9	-2	716	2182	-48.68	-4.28	0.01
99	SLD 10	-2	716	2182	-48.68	-4.28	0.01
99	SLD 11	-11	96	2058	15.52	-11.67	0.02
99	SLD 12	-11	96	2058	15.52	-11.67	0.02
99	SLD 13	-20	526	2130	-27.5	-26.16	0.04
99	SLD 14	-20	526	2130	-27.5	-26.16	0.04
99	SLD 15	-22	340	2093	-8.24	-28.37	0.04
99	SLD 16	-22	340	2093	-8.24	-28.37	0.04
99	SLV 1	69	532	2198	-36.15	88.56	-0.14
99	SLV 2	69	532	2198	-36.15	88.56	-0.14
99	SLV 3	62	71	2103	13	82.83	-0.13
99	SLV 4	62	71	2103	13	82.83	-0.13
99	SLV 5	31	1136	2290	-96.61	35.45	-0.06
99	SLV 6	31	1136	2290	-96.61	35.45	-0.06
99	SLV 7	9	-403	1973	67.23	16.38	-0.02
99	SLV 8	9	-403	1973	67.23	16.38	-0.02
99	SLV 9	-8	1192	2273	-99.28	-15.79	0.02
99	SLV 10	-8	1192	2273	-99.28	-15.79	0.02
99	SLV 11	-30	-348	1956	64.55	-34.87	0.06
99	SLV 12	-30	-348	1956	64.55	-34.87	0.06
99	SLV 13	-62	718	2143	-45.06	-82.25	0.13
99	SLV 14	-62	718	2143	-45.06	-82.25	0.13
99	SLV 15	-68	256	2048	4.1	-87.97	0.14
99	SLV 16	-68	256	2048	4.1	-87.97	0.14
100	SLU 1	0	0	2043	0.44	-0.84	0
100	SLU 2	-1	-4	2071	0.64	-3.5	0
100	SLU 3	0	0	2043	0.44	-0.84	0
100	SLU 4	-1	-3	2060	0.56	-2.44	0
100	SLU 5	-1	-4	2071	0.64	-3.5	0
100	SLU 6	0	0	2043	0.44	-0.84	0
100	SLU 7	-1	-3	2060	0.56	-2.44	0
100	SLU 8	0	0	2043	0.44	-0.84	0
100	SLU 9	-1	-3	2060	0.56	-2.44	0
100	SLU 10	-2	2	2300	1.12	-4.44	0
100	SLU 11	-1	7	2272	0.92	-1.78	0
100	SLU 12	-2	4	2289	1.04	-3.38	0
100	SLU 13	-2	2	2300	1.12	-4.44	0
100	SLU 14	-1	7	2272	0.92	-1.78	0
100	SLU 15	-2	4	2289	1.04	-3.38	0
100	SLU 16	-1	7	2272	0.92	-1.78	0
100	SLU 17	-2	4	2289	1.04	-3.38	0
100	SLU 18	-1	10	2370	1.12	-2.18	0
100	SLU 19	-2	7	2387	1.24	-3.78	0
100	SLU 20	-1	10	2370	1.12	-2.18	0
100	SLU 21	-2	7	2387	1.24	-3.78	0
100	SLU 22	-1	5	2191	0.56	-1.23	0
100	SLU 23	-2	0	2219	0.76	-3.89	0
100	SLU 24	-1	5	2191	0.56	-1.23	0
100	SLU 25	-1	2	2208	0.68	-2.83	0
100	SLU 26	-2	0	2219	0.76	-3.89	0
100	SLU 27	-1	5	2191	0.56	-1.23	0
100	SLU 28	-1	2	2208	0.68	-2.83	0
100	SLU 29	-1	5	2191	0.56	-1.23	0
100	SLU 30	-1	2	2208	0.68	-2.83	0
100	SLU 31	-2	7	2448	1.24	-4.83	0
100	SLU 32	-1	12	2420	1.04	-2.17	0
100	SLU 33	-2	9	2436	1.16	-3.77	0
100	SLU 34	-2	7	2448	1.24	-4.83	0
100	SLU 35	-1	12	2420	1.04	-2.17	0
100	SLU 36	-2	9	2436	1.16	-3.77	0
100	SLU 37	-1	12	2420	1.04	-2.17	0
100	SLU 38	-2	9	2436	1.16	-3.77	0
100	SLU 39	-2	15	2518	1.24	-2.58	0
100	SLU 40	-2	12	2534	1.36	-4.17	0
100	SLU 41	-2	15	2518	1.24	-2.58	0
100	SLU 42	-2	12	2534	1.36	-4.17	0
100	SLU 43	-1	-1	2605	0.53	-0.96	0
100	SLU 44	-2	-6	2633	0.73	-3.62	0
100	SLU 45	-1	-1	2605	0.53	-0.96	0
100	SLU 46	-1	-4	2622	0.65	-2.55	0
100	SLU 47	-2	-6	2633	0.73	-3.62	0
100	SLU 48	-1	-1	2605	0.53	-0.96	0
100	SLU 49	-1	-4	2622	0.65	-2.55	0
100	SLU 50	-1	-1	2605	0.53	-0.96	0
100	SLU 51	-1	-4	2622	0.65	-2.55	0
100	SLU 52	-2	1	2862	1.21	-4.56	0
100	SLU 53	-1	6	2834	1.01	-1.9	0
100	SLU 54	-2	3	2851	1.13	-3.5	0
100	SLU 55	-2	1	2862	1.21	-4.56	0
100	SLU 56	-1	6	2834	1.01	-1.9	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
100	SLU 57	-2	3	2851	1.13	-3.5	0
100	SLU 58	-1	6	2834	1.01	-1.9	0
100	SLU 59	-2	3	2851	1.13	-3.5	0
100	SLU 60	-1	9	2932	1.21	-2.3	0
100	SLU 61	-2	6	2949	1.33	-3.9	0
100	SLU 62	-1	9	2932	1.21	-2.3	0
100	SLU 63	-2	6	2949	1.33	-3.9	0
100	SLU 64	-1	3	2753	0.65	-1.35	0
100	SLU 65	-2	-1	2781	0.85	-4.01	0
100	SLU 66	-1	3	2753	0.65	-1.35	0
100	SLU 67	-1	0	2770	0.77	-2.94	0
100	SLU 68	-2	-1	2781	0.85	-4.01	0
100	SLU 69	-1	3	2753	0.65	-1.35	0
100	SLU 70	-1	0	2770	0.77	-2.94	0
100	SLU 71	-1	3	2753	0.65	-1.35	0
100	SLU 72	-1	0	2770	0.77	-2.94	0
100	SLU 73	-2	5	3010	1.33	-4.95	0
100	SLU 74	-1	10	2982	1.13	-2.29	0
100	SLU 75	-2	7	2999	1.25	-3.89	0
100	SLU 76	-2	5	3010	1.33	-4.95	0
100	SLU 77	-1	10	2982	1.13	-2.29	0
100	SLU 78	-2	7	2999	1.25	-3.89	0
100	SLU 79	-1	10	2982	1.13	-2.29	0
100	SLU 80	-2	7	2999	1.25	-3.89	0
100	SLU 81	-2	13	3080	1.33	-2.69	0
100	SLU 82	-2	10	3097	1.45	-4.29	0
100	SLU 83	-2	13	3080	1.33	-2.69	0
100	SLU 84	-2	10	3097	1.45	-4.29	0
100	SLE RA 1	-1	2	2085	0.47	-0.95	0
100	SLE RA 2	-1	-2	2104	0.61	-2.72	0
100	SLE RA 3	-1	2	2085	0.47	-0.95	0
100	SLE RA 4	-1	0	2097	0.55	-2.01	0
100	SLE RA 5	-1	-2	2104	0.61	-2.72	0
100	SLE RA 6	-1	2	2085	0.47	-0.95	0
100	SLE RA 7	-1	0	2097	0.55	-2.01	0
100	SLE RA 8	-1	2	2085	0.47	-0.95	0
100	SLE RA 9	-1	0	2097	0.55	-2.01	0
100	SLE RA 10	-2	3	2256	0.93	-3.35	0
100	SLE RA 11	-1	6	2238	0.79	-1.58	0
100	SLE RA 12	-1	4	2249	0.87	-2.64	0
100	SLE RA 13	-2	3	2256	0.93	-3.35	0
100	SLE RA 14	-1	6	2238	0.79	-1.58	0
100	SLE RA 15	-1	4	2249	0.87	-2.64	0
100	SLE RA 16	-1	6	2238	0.79	-1.58	0
100	SLE RA 17	-1	4	2249	0.87	-2.64	0
100	SLE RA 18	-1	8	2303	0.93	-1.85	0
100	SLE RA 19	-1	6	2314	1.01	-2.91	0
100	SLE RA 20	-1	8	2303	0.93	-1.85	0
100	SLE RA 21	-1	6	2314	1.01	-2.91	0
100	SLE FR 1	-1	2	2085	0.47	-0.95	0
100	SLE FR 2	-1	1	2089	0.5	-1.31	0
100	SLE FR 3	-1	2	2085	0.47	-0.95	0
100	SLE FR 4	-1	3	2154	0.64	-1.57	0
100	SLE FR 5	-1	4	2151	0.61	-1.22	0
100	SLE FR 6	-1	5	2194	0.7	-1.4	0
100	SLE QP 1	-1	2	2085	0.47	-0.95	0
100	SLE QP 2	-1	4	2151	0.61	-1.22	0
100	SLD 1	37	138	2018	-5.36	48.16	-0.01
100	SLD 2	37	138	2018	-5.36	48.16	-0.01
100	SLD 3	43	-16	1972	1.52	54.77	-0.02
100	SLD 4	43	-16	1972	1.52	54.77	-0.02
100	SLD 5	1	279	2181	-11.61	3.58	0.01
100	SLD 6	1	279	2181	-11.61	3.58	0.01
100	SLD 7	22	-237	2027	11.31	25.59	-0.02
100	SLD 8	22	-237	2027	11.31	25.59	-0.02
100	SLD 9	-24	244	2274	-10.09	-28.03	0.02
100	SLD 10	-24	244	2274	-10.09	-28.03	0.02
100	SLD 11	-2	-272	2121	12.83	-6.02	-0.01
100	SLD 12	-2	-272	2121	12.83	-6.02	-0.01
100	SLD 13	-45	23	2330	-0.3	-57.21	0.02
100	SLD 14	-45	23	2330	-0.3	-57.21	0.02
100	SLD 15	-38	-131	2284	6.58	-50.6	0.01
100	SLD 16	-38	-131	2284	6.58	-50.6	0.01
100	SLV 1	96	325	1838	-13.63	127.2	-0.04
100	SLV 2	96	325	1838	-13.63	127.2	-0.04
100	SLV 3	112	-40	1728	2.58	144.01	-0.06
100	SLV 4	112	-40	1728	2.58	144.01	-0.06
100	SLV 5	3	653	2224	-28.26	11.81	0.02
100	SLV 6	3	653	2224	-28.26	11.81	0.02
100	SLV 7	58	-562	1856	25.8	67.84	-0.05
100	SLV 8	58	-562	1856	25.8	67.84	-0.05
100	SLV 9	-60	570	2445	-24.58	-70.28	0.05
100	SLV 10	-60	570	2445	-24.58	-70.28	0.05
100	SLV 11	-4	-646	2077	29.48	-14.25	-0.02
100	SLV 12	-4	-646	2077	29.48	-14.25	-0.02
100	SLV 13	-114	47	2574	-1.36	-146.45	0.06
100	SLV 14	-114	47	2574	-1.36	-146.45	0.06
100	SLV 15	-97	-318	2463	14.85	-129.64	0.04





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
100	SLV 16	-97	-318	2463	14.85	-129.64	0.04
101	SLU 1	2	-56	2060	2.26	0.52	0.01
101	SLU 2	3	-43	1997	1.79	-1.32	0
101	SLU 3	2	-56	2060	2.26	0.52	0.01
101	SLU 4	3	-48	2022	1.98	-0.58	0
101	SLU 5	3	-43	1997	1.79	-1.32	0
101	SLU 6	2	-56	2060	2.26	0.52	0.01
101	SLU 7	3	-48	2022	1.98	-0.58	0
101	SLU 8	2	-56	2060	2.26	0.52	0.01
101	SLU 9	3	-48	2022	1.98	-0.58	0
101	SLU 10	4	-71	2498	2.96	-1.2	0
101	SLU 11	2	-84	2561	3.43	0.64	0.01
101	SLU 12	3	-76	2523	3.14	-0.46	0.01
101	SLU 13	4	-71	2498	2.96	-1.2	0
101	SLU 14	2	-84	2561	3.43	0.64	0.01
101	SLU 15	3	-76	2523	3.14	-0.46	0.01
101	SLU 16	2	-84	2561	3.43	0.64	0.01
101	SLU 17	3	-76	2523	3.14	-0.46	0.01
101	SLU 18	2	-95	2775	3.92	0.7	0.01
101	SLU 19	3	-88	2737	3.64	-0.41	0.01
101	SLU 20	2	-95	2775	3.92	0.7	0.01
101	SLU 21	3	-88	2737	3.64	-0.41	0.01
101	SLU 22	2	-66	2317	2.71	0.59	0.01
101	SLU 23	3	-54	2254	2.24	-1.25	0
101	SLU 24	2	-66	2317	2.71	0.59	0.01
101	SLU 25	3	-59	2279	2.43	-0.52	0
101	SLU 26	3	-54	2254	2.24	-1.25	0
101	SLU 27	2	-66	2317	2.71	0.59	0.01
101	SLU 28	3	-59	2279	2.43	-0.52	0
101	SLU 29	2	-66	2317	2.71	0.59	0.01
101	SLU 30	3	-59	2279	2.43	-0.52	0
101	SLU 31	4	-82	2755	3.4	-1.13	0
101	SLU 32	2	-94	2818	3.87	0.71	0.01
101	SLU 33	3	-87	2780	3.59	-0.4	0.01
101	SLU 34	4	-82	2755	3.4	-1.13	0
101	SLU 35	2	-94	2818	3.87	0.71	0.01
101	SLU 36	3	-87	2780	3.59	-0.4	0.01
101	SLU 37	2	-94	2818	3.87	0.71	0.01
101	SLU 38	3	-87	2780	3.59	-0.4	0.01
101	SLU 39	3	-106	3032	4.37	0.76	0.01
101	SLU 40	4	-99	2995	4.09	-0.35	0.01
101	SLU 41	3	-106	3032	4.37	0.76	0.01
101	SLU 42	4	-99	2995	4.09	-0.35	0.01
101	SLU 43	2	-69	2590	2.79	0.66	0.01
101	SLU 44	4	-56	2527	2.32	-1.18	0
101	SLU 45	2	-69	2590	2.79	0.66	0.01
101	SLU 46	3	-61	2552	2.51	-0.44	0.01
101	SLU 47	4	-56	2527	2.32	-1.18	0
101	SLU 48	2	-69	2590	2.79	0.66	0.01
101	SLU 49	3	-61	2552	2.51	-0.44	0.01
101	SLU 50	2	-69	2590	2.79	0.66	0.01
101	SLU 51	3	-61	2552	2.51	-0.44	0.01
101	SLU 52	4	-84	3027	3.48	-1.06	0
101	SLU 53	3	-97	3090	3.95	0.78	0.01
101	SLU 54	3	-89	3053	3.67	-0.32	0.01
101	SLU 55	4	-84	3027	3.48	-1.06	0
101	SLU 56	3	-97	3090	3.95	0.78	0.01
101	SLU 57	3	-89	3053	3.67	-0.32	0.01
101	SLU 58	3	-97	3090	3.95	0.78	0.01
101	SLU 59	3	-89	3053	3.67	-0.32	0.01
101	SLU 60	3	-109	3305	4.45	0.83	0.01
101	SLU 61	4	-101	3267	4.17	-0.27	0.01
101	SLU 62	3	-109	3305	4.45	0.83	0.01
101	SLU 63	4	-101	3267	4.17	-0.27	0.01
101	SLU 64	2	-79	2847	3.24	0.72	0.01
101	SLU 65	4	-67	2784	2.77	-1.12	0
101	SLU 66	2	-79	2847	3.24	0.72	0.01
101	SLU 67	3	-72	2809	2.96	-0.38	0.01
101	SLU 68	4	-67	2784	2.77	-1.12	0
101	SLU 69	2	-79	2847	3.24	0.72	0.01
101	SLU 70	3	-72	2809	2.96	-0.38	0.01
101	SLU 71	2	-79	2847	3.24	0.72	0.01
101	SLU 72	3	-72	2809	2.96	-0.38	0.01
101	SLU 73	4	-95	3285	3.93	-1	0.01
101	SLU 74	3	-107	3348	4.4	0.84	0.01
101	SLU 75	4	-100	3310	4.12	-0.26	0.01
101	SLU 76	4	-95	3285	3.93	-1	0.01
101	SLU 77	3	-107	3348	4.4	0.84	0.01
101	SLU 78	4	-100	3310	4.12	-0.26	0.01
101	SLU 79	3	-107	3348	4.4	0.84	0.01
101	SLU 80	4	-100	3310	4.12	-0.26	0.01
101	SLU 81	3	-119	3562	4.9	0.89	0.02
101	SLU 82	4	-112	3524	4.61	-0.21	0.01
101	SLU 83	3	-119	3562	4.9	0.89	0.02
101	SLU 84	4	-112	3524	4.61	-0.21	0.01
101	SLE RA 1	2	-59	2134	2.39	0.54	0.01
101	SLE RA 2	3	-50	2091	2.08	-0.69	0
101	SLE RA 3	2	-59	2134	2.39	0.54	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
101	SLE RA 4	2	-54	2108	2.2	-0.19	0.01
101	SLE RA 5	3	-50	2091	2.08	-0.69	0
101	SLE RA 6	2	-59	2134	2.39	0.54	0.01
101	SLE RA 7	2	-54	2108	2.2	-0.19	0.01
101	SLE RA 8	2	-59	2134	2.39	0.54	0.01
101	SLE RA 9	2	-54	2108	2.2	-0.19	0.01
101	SLE RA 10	3	-69	2425	2.85	-0.6	0
101	SLE RA 11	2	-77	2467	3.17	0.62	0.01
101	SLE RA 12	3	-72	2442	2.98	-0.11	0.01
101	SLE RA 13	3	-69	2425	2.85	-0.6	0
101	SLE RA 14	2	-77	2467	3.17	0.62	0.01
101	SLE RA 15	3	-72	2442	2.98	-0.11	0.01
101	SLE RA 16	2	-77	2467	3.17	0.62	0.01
101	SLE RA 17	3	-72	2442	2.98	-0.11	0.01
101	SLE RA 18	2	-85	2610	3.5	0.66	0.01
101	SLE RA 19	3	-80	2585	3.31	-0.08	0.01
101	SLE RA 20	2	-85	2610	3.5	0.66	0.01
101	SLE RA 21	3	-80	2585	3.31	-0.08	0.01
101	SLE FR 1	2	-59	2134	2.39	0.54	0.01
101	SLE FR 2	2	-57	2125	2.33	0.3	0.01
101	SLE FR 3	2	-59	2134	2.39	0.54	0.01
101	SLE FR 4	2	-65	2268	2.66	0.33	0.01
101	SLE FR 5	2	-67	2277	2.72	0.58	0.01
101	SLE FR 6	2	-72	2372	2.95	0.6	0.01
101	SLE QP 1	2	-59	2134	2.39	0.54	0.01
101	SLE QP 2	2	-67	2277	2.72	0.58	0.01
101	SLD 1	-7	-66	2414	2.43	9.58	0.03
101	SLD 2	-7	-66	2414	2.43	9.58	0.03
101	SLD 3	-2	-193	2448	7.82	7.2	0.02
101	SLD 4	-2	-193	2448	7.82	7.2	0.02
101	SLD 5	-9	126	2267	-5.54	6.88	0.02
101	SLD 6	-9	126	2267	-5.54	6.88	0.02
101	SLD 7	9	-297	2379	12.43	-1.04	0.01
101	SLD 8	9	-297	2379	12.43	-1.04	0.01
101	SLD 9	-5	164	2174	-6.99	2.19	0.01
101	SLD 10	-5	164	2174	-6.99	2.19	0.01
101	SLD 11	13	-260	2286	10.99	-5.73	0
101	SLD 12	13	-260	2286	10.99	-5.73	0
101	SLD 13	5	60	2105	-2.37	-6.05	0
101	SLD 14	5	60	2105	-2.37	-6.05	0
101	SLD 15	11	-67	2139	3.02	-8.43	-0.01
101	SLD 16	11	-67	2139	3.02	-8.43	-0.01
101	SLV 1	-20	-65	2614	2.02	23.45	0.06
101	SLV 2	-20	-65	2614	2.02	23.45	0.06
101	SLV 3	-8	-365	2693	14.76	17.81	0.05
101	SLV 4	-8	-365	2693	14.76	17.81	0.05
101	SLV 5	-23	389	2257	-16.81	16	0.04
101	SLV 6	-23	389	2257	-16.81	16	0.04
101	SLV 7	18	-612	2522	25.65	-2.82	0
101	SLV 8	18	-612	2522	25.65	-2.82	0
101	SLV 9	-14	478	2031	-20.2	3.97	0.02
101	SLV 10	-14	478	2031	-20.2	3.97	0.02
101	SLV 11	27	-523	2296	22.26	-14.85	-0.02
101	SLV 12	27	-523	2296	22.26	-14.85	-0.02
101	SLV 13	11	232	1860	-9.31	-16.65	-0.03
101	SLV 14	11	232	1860	-9.31	-16.65	-0.03
101	SLV 15	24	-68	1939	3.43	-22.3	-0.04
101	SLV 16	24	-68	1939	3.43	-22.3	-0.04
102	SLU 1	0	209	1882	-7.61	0.18	0
102	SLU 2	-7	206	1879	-7.46	-7.78	0.02
102	SLU 3	0	209	1882	-7.61	0.18	0
102	SLU 4	-4	208	1880	-7.52	-4.59	0.01
102	SLU 5	-7	206	1879	-7.46	-7.78	0.02
102	SLU 6	0	209	1882	-7.61	0.18	0
102	SLU 7	-4	208	1880	-7.52	-4.59	0.01
102	SLU 8	0	209	1882	-7.61	0.18	0
102	SLU 9	-4	208	1880	-7.52	-4.59	0.01
102	SLU 10	-6	410	2997	-14.74	-7.33	0.01
102	SLU 11	0	413	3001	-14.89	0.63	0
102	SLU 12	-4	411	2999	-14.8	-4.15	0.01
102	SLU 13	-6	410	2997	-14.74	-7.33	0.01
102	SLU 14	0	413	3001	-14.89	0.63	0
102	SLU 15	-4	411	2999	-14.8	-4.15	0.01
102	SLU 16	0	413	3001	-14.89	0.63	0
102	SLU 17	-4	411	2999	-14.8	-4.15	0.01
102	SLU 18	1	500	3480	-18	0.82	0
102	SLU 19	-3	499	3478	-17.91	-3.95	0.01
102	SLU 20	1	500	3480	-18	0.82	0
102	SLU 21	-3	499	3478	-17.91	-3.95	0.01
102	SLU 22	0	300	2451	-10.91	0.36	0
102	SLU 23	-6	298	2448	-10.76	-7.6	0.01
102	SLU 24	0	300	2451	-10.91	0.36	0
102	SLU 25	-4	299	2449	-10.82	-4.42	0.01
102	SLU 26	-6	298	2448	-10.76	-7.6	0.01
102	SLU 27	0	300	2451	-10.91	0.36	0
102	SLU 28	-4	299	2449	-10.82	-4.42	0.01
102	SLU 29	0	300	2451	-10.91	0.36	0
102	SLU 30	-4	299	2449	-10.82	-4.42	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
102	SLU 31	-6	501	3567	-18.03	-7.15	0.01
102	SLU 32	1	504	3570	-18.18	0.81	0
102	SLU 33	-3	503	3568	-18.09	-3.97	0.01
102	SLU 34	-6	501	3567	-18.03	-7.15	0.01
102	SLU 35	1	504	3570	-18.18	0.81	0
102	SLU 36	-3	503	3568	-18.09	-3.97	0.01
102	SLU 37	1	504	3570	-18.18	0.81	0
102	SLU 38	-3	503	3568	-18.09	-3.97	0.01
102	SLU 39	1	592	4049	-21.3	1	0
102	SLU 40	-3	590	4047	-21.21	-3.78	0.01
102	SLU 41	1	592	4049	-21.3	1	0
102	SLU 42	-3	590	4047	-21.21	-3.78	0.01
102	SLU 43	0	241	2252	-8.77	0.18	0
102	SLU 44	-7	238	2248	-8.62	-7.78	0.02
102	SLU 45	0	241	2252	-8.77	0.18	0
102	SLU 46	-4	239	2250	-8.68	-4.6	0.01
102	SLU 47	-7	238	2248	-8.62	-7.78	0.02
102	SLU 48	0	241	2252	-8.77	0.18	0
102	SLU 49	-4	239	2250	-8.68	-4.6	0.01
102	SLU 50	0	241	2252	-8.77	0.18	0
102	SLU 51	-4	239	2250	-8.68	-4.6	0.01
102	SLU 52	-6	442	3367	-15.89	-7.34	0.01
102	SLU 53	0	445	3370	-16.04	0.63	0
102	SLU 54	-4	443	3368	-15.95	-4.15	0.01
102	SLU 55	-6	442	3367	-15.89	-7.34	0.01
102	SLU 56	0	445	3370	-16.04	0.63	0
102	SLU 57	-4	443	3368	-15.95	-4.15	0.01
102	SLU 58	0	445	3370	-16.04	0.63	0
102	SLU 59	-4	443	3368	-15.95	-4.15	0.01
102	SLU 60	1	532	3850	-19.16	0.82	0
102	SLU 61	-3	530	3848	-19.07	-3.96	0.01
102	SLU 62	1	532	3850	-19.16	0.82	0
102	SLU 63	-3	530	3848	-19.07	-3.96	0.01
102	SLU 64	0	332	2821	-12.06	0.36	0
102	SLU 65	-6	329	2817	-11.91	-7.6	0.01
102	SLU 66	0	332	2821	-12.06	0.36	0
102	SLU 67	-4	330	2819	-11.97	-4.42	0.01
102	SLU 68	-6	329	2817	-11.91	-7.6	0.01
102	SLU 69	0	332	2821	-12.06	0.36	0
102	SLU 70	-4	330	2819	-11.97	-4.42	0.01
102	SLU 71	0	332	2821	-12.06	0.36	0
102	SLU 72	-4	330	2819	-11.97	-4.42	0.01
102	SLU 73	-6	533	3936	-19.19	-7.16	0.01
102	SLU 74	1	536	3939	-19.33	0.8	0
102	SLU 75	-3	534	3937	-19.25	-3.97	0.01
102	SLU 76	-6	533	3936	-19.19	-7.16	0.01
102	SLU 77	1	536	3939	-19.33	0.8	0
102	SLU 78	-3	534	3937	-19.25	-3.97	0.01
102	SLU 79	1	536	3939	-19.33	0.8	0
102	SLU 80	-3	534	3937	-19.25	-3.97	0.01
102	SLU 81	1	623	4419	-22.45	0.99	0
102	SLU 82	-3	621	4417	-22.36	-3.78	0.01
102	SLU 83	1	623	4419	-22.45	0.99	0
102	SLU 84	-3	621	4417	-22.36	-3.78	0.01
102	SLE RA 1	0	235	2045	-8.55	0.23	0
102	SLE RA 2	-4	233	2042	-8.46	-5.07	0.01
102	SLE RA 3	0	235	2045	-8.55	0.23	0
102	SLE RA 4	-3	234	2043	-8.49	-2.95	0.01
102	SLE RA 5	-4	233	2042	-8.46	-5.07	0.01
102	SLE RA 6	0	235	2045	-8.55	0.23	0
102	SLE RA 7	-3	234	2043	-8.49	-2.95	0.01
102	SLE RA 8	0	235	2045	-8.55	0.23	0
102	SLE RA 9	-3	234	2043	-8.49	-2.95	0.01
102	SLE RA 10	-4	369	2788	-13.3	-4.77	0.01
102	SLE RA 11	0	371	2791	-13.4	0.53	0
102	SLE RA 12	-2	370	2789	-13.34	-2.65	0.01
102	SLE RA 13	-4	369	2788	-13.3	-4.77	0.01
102	SLE RA 14	0	371	2791	-13.4	0.53	0
102	SLE RA 15	-2	370	2789	-13.34	-2.65	0.01
102	SLE RA 16	0	371	2791	-13.4	0.53	0
102	SLE RA 17	-2	370	2789	-13.34	-2.65	0.01
102	SLE RA 18	1	429	3110	-15.48	0.66	0
102	SLE RA 19	-2	428	3109	-15.42	-2.52	0.01
102	SLE RA 20	1	429	3110	-15.48	0.66	0
102	SLE RA 21	-2	428	3109	-15.42	-2.52	0.01
102	SLE FR 1	0	235	2045	-8.55	0.23	0
102	SLE FR 2	-1	235	2044	-8.53	-0.83	0
102	SLE FR 3	0	235	2045	-8.55	0.23	0
102	SLE FR 4	-1	293	2364	-10.61	-0.7	0
102	SLE FR 5	0	293	2364	-10.63	0.36	0
102	SLE FR 6	0	332	2577	-12.02	0.45	0
102	SLE QP 1	0	235	2045	-8.55	0.23	0
102	SLE QP 2	0	293	2364	-10.63	0.36	0
102	SLD 1	30	237	2382	-1.96	34.64	-0.06
102	SLD 2	30	237	2382	-1.96	34.64	-0.06
102	SLD 3	27	428	2364	-23.08	32.54	-0.06
102	SLD 4	27	428	2364	-23.08	32.54	-0.06
102	SLD 5	13	-14	2398	24.01	13.84	-0.03



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
102	SLD 6	13	-14	2398	24.01	13.84	-0.03
102	SLD 7	5	624	2336	-46.41	6.83	-0.01
102	SLD 8	5	624	2336	-46.41	6.83	-0.01
102	SLD 9	-4	-37	2393	25.15	-6.1	0.01
102	SLD 10	-4	-37	2393	25.15	-6.1	0.01
102	SLD 11	-12	600	2331	-45.28	-13.11	0.02
102	SLD 12	-12	600	2331	-45.28	-13.11	0.02
102	SLD 13	-27	159	2365	1.82	-31.81	0.06
102	SLD 14	-27	159	2365	1.82	-31.81	0.06
102	SLD 15	-29	350	2346	-19.31	-33.92	0.06
102	SLD 16	-29	350	2346	-19.31	-33.92	0.06
102	SLV 1	91	149	2410	11.79	106.11	-0.19
102	SLV 2	91	149	2410	11.79	106.11	-0.19
102	SLV 3	84	624	2362	-42.15	100.63	-0.18
102	SLV 4	84	624	2362	-42.15	100.63	-0.18
102	SLV 5	37	-470	2450	77.9	40.39	-0.07
102	SLV 6	37	-470	2450	77.9	40.39	-0.07
102	SLV 7	16	1113	2291	-101.9	22.14	-0.04
102	SLV 8	16	1113	2291	-101.9	22.14	-0.04
102	SLV 9	-15	-526	2437	80.63	-21.41	0.04
102	SLV 10	-15	-526	2437	80.63	-21.41	0.04
102	SLV 11	-36	1057	2278	-99.17	-39.67	0.07
102	SLV 12	-36	1057	2278	-99.17	-39.67	0.07
102	SLV 13	-84	-37	2366	20.89	-99.91	0.18
102	SLV 14	-84	-37	2366	20.89	-99.91	0.18
102	SLV 15	-90	438	2319	-33.05	-105.38	0.19
102	SLV 16	-90	438	2319	-33.05	-105.38	0.19
103	SLU 1	0	-12	2054	0.22	-0.72	0
103	SLU 2	-2	-17	2080	0.44	-3.93	0
103	SLU 3	0	-12	2054	0.22	-0.72	0
103	SLU 4	-1	-15	2069	0.35	-2.65	0
103	SLU 5	-2	-17	2080	0.44	-3.93	0
103	SLU 6	0	-12	2054	0.22	-0.72	0
103	SLU 7	-1	-15	2069	0.35	-2.65	0
103	SLU 8	0	-12	2054	0.22	-0.72	0
103	SLU 9	-1	-15	2069	0.35	-2.65	0
103	SLU 10	-2	4	2325	-1.02	-4.77	0
103	SLU 11	-1	9	2299	-1.23	-1.55	0
103	SLU 12	-2	6	2315	-1.1	-3.48	0
103	SLU 13	-2	4	2325	-1.02	-4.77	0
103	SLU 14	-1	9	2299	-1.23	-1.55	0
103	SLU 15	-2	6	2315	-1.1	-3.48	0
103	SLU 16	-1	9	2299	-1.23	-1.55	0
103	SLU 17	-2	6	2315	-1.1	-3.48	0
103	SLU 18	-1	18	2404	-1.85	-1.91	0
103	SLU 19	-2	14	2420	-1.73	-3.84	0
103	SLU 20	-1	18	2404	-1.85	-1.91	0
103	SLU 21	-2	14	2420	-1.73	-3.84	0
103	SLU 22	-1	-3	2209	-0.36	-1.06	0
103	SLU 23	-2	-9	2235	-0.14	-4.28	0
103	SLU 24	-1	-3	2209	-0.36	-1.06	0
103	SLU 25	-1	-7	2225	-0.23	-2.99	0
103	SLU 26	-2	-9	2235	-0.14	-4.28	0
103	SLU 27	-1	-3	2209	-0.36	-1.06	0
103	SLU 28	-1	-7	2225	-0.23	-2.99	0
103	SLU 29	-1	-3	2209	-0.36	-1.06	0
103	SLU 30	-1	-7	2225	-0.23	-2.99	0
103	SLU 31	-3	12	2480	-1.6	-5.11	0
103	SLU 32	-1	17	2455	-1.81	-1.89	0
103	SLU 33	-2	14	2470	-1.68	-3.82	0
103	SLU 34	-3	12	2480	-1.6	-5.11	0
103	SLU 35	-1	17	2455	-1.81	-1.89	0
103	SLU 36	-2	14	2470	-1.68	-3.82	0
103	SLU 37	-1	17	2455	-1.81	-1.89	0
103	SLU 38	-2	14	2470	-1.68	-3.82	0
103	SLU 39	-1	26	2560	-2.43	-2.25	0
103	SLU 40	-2	23	2575	-2.3	-4.18	0
103	SLU 41	-1	26	2560	-2.43	-2.25	0
103	SLU 42	-2	23	2575	-2.3	-4.18	0
103	SLU 43	0	-18	2617	0.49	-0.82	0
103	SLU 44	-2	-23	2643	0.7	-4.03	0
103	SLU 45	0	-18	2617	0.49	-0.82	0
103	SLU 46	-1	-21	2632	0.62	-2.75	0
103	SLU 47	-2	-23	2643	0.7	-4.03	0
103	SLU 48	0	-18	2617	0.49	-0.82	0
103	SLU 49	-1	-21	2632	0.62	-2.75	0
103	SLU 50	0	-18	2617	0.49	-0.82	0
103	SLU 51	-1	-21	2632	0.62	-2.75	0
103	SLU 52	-2	-3	2888	-0.75	-4.86	0
103	SLU 53	-1	2	2862	-0.97	-1.65	0
103	SLU 54	-2	-1	2878	-0.84	-3.58	0
103	SLU 55	-2	-3	2888	-0.75	-4.86	0
103	SLU 56	-1	2	2862	-0.97	-1.65	0
103	SLU 57	-2	-1	2878	-0.84	-3.58	0
103	SLU 58	-1	2	2862	-0.97	-1.65	0
103	SLU 59	-2	-1	2878	-0.84	-3.58	0
103	SLU 60	-1	11	2967	-1.59	-2.01	0
103	SLU 61	-2	8	2983	-1.46	-3.93	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
103	SLU 62	-1	11	2967	-1.59	-2.01	0
103	SLU 63	-2	8	2983	-1.46	-3.93	0
103	SLU 64	-1	-10	2772	-0.09	-1.16	0
103	SLU 65	-2	-15	2798	0.12	-4.37	0
103	SLU 66	-1	-10	2772	-0.09	-1.16	0
103	SLU 67	-1	-13	2788	0.04	-3.09	0
103	SLU 68	-2	-15	2798	0.12	-4.37	0
103	SLU 69	-1	-10	2772	-0.09	-1.16	0
103	SLU 70	-1	-13	2788	0.04	-3.09	0
103	SLU 71	-1	-10	2772	-0.09	-1.16	0
103	SLU 72	-1	-13	2788	0.04	-3.09	0
103	SLU 73	-3	6	3043	-1.33	-5.21	0
103	SLU 74	-1	11	3018	-1.55	-1.99	0
103	SLU 75	-2	8	3033	-1.42	-3.92	0
103	SLU 76	-3	6	3043	-1.33	-5.21	0
103	SLU 77	-1	11	3018	-1.55	-1.99	0
103	SLU 78	-2	8	3033	-1.42	-3.92	0
103	SLU 79	-1	11	3018	-1.55	-1.99	0
103	SLU 80	-2	8	3033	-1.42	-3.92	0
103	SLU 81	-1	19	3123	-2.17	-2.35	0
103	SLU 82	-2	16	3138	-2.04	-4.28	0
103	SLU 83	-1	19	3123	-2.17	-2.35	0
103	SLU 84	-2	16	3138	-2.04	-4.28	0
103	SLE RA 1	0	-9	2098	0.06	-0.82	0
103	SLE RA 2	-1	-13	2115	0.2	-2.96	0
103	SLE RA 3	0	-9	2098	0.06	-0.82	0
103	SLE RA 4	-1	-11	2109	0.14	-2.1	0
103	SLE RA 5	-1	-13	2115	0.2	-2.96	0
103	SLE RA 6	0	-9	2098	0.06	-0.82	0
103	SLE RA 7	-1	-11	2109	0.14	-2.1	0
103	SLE RA 8	0	-9	2098	0.06	-0.82	0
103	SLE RA 9	-1	-11	2109	0.14	-2.1	0
103	SLE RA 10	-2	1	2279	-0.77	-3.51	0
103	SLE RA 11	-1	4	2262	-0.91	-1.37	0
103	SLE RA 12	-1	2	2272	-0.83	-2.66	0
103	SLE RA 13	-2	1	2279	-0.77	-3.51	0
103	SLE RA 14	-1	4	2262	-0.91	-1.37	0
103	SLE RA 15	-1	2	2272	-0.83	-2.66	0
103	SLE RA 16	-1	4	2262	-0.91	-1.37	0
103	SLE RA 17	-1	2	2272	-0.83	-2.66	0
103	SLE RA 18	-1	10	2332	-1.33	-1.61	0
103	SLE RA 19	-1	8	2342	-1.24	-2.89	0
103	SLE RA 20	-1	10	2332	-1.33	-1.61	0
103	SLE RA 21	-1	8	2342	-1.24	-2.89	0
103	SLE FR 1	0	-9	2098	0.06	-0.82	0
103	SLE FR 2	-1	-10	2102	0.09	-1.25	0
103	SLE FR 3	0	-9	2098	0.06	-0.82	0
103	SLE FR 4	-1	-4	2172	-0.33	-1.48	0
103	SLE FR 5	-1	-4	2168	-0.36	-1.05	0
103	SLE FR 6	-1	0	2215	-0.64	-1.21	0
103	SLE QP 1	0	-9	2098	0.06	-0.82	0
103	SLE QP 2	-1	-4	2168	-0.36	-1.05	0
103	SLD 1	46	135	2052	-6.46	56.86	-0.01
103	SLD 2	46	135	2052	-6.46	56.86	-0.01
103	SLD 3	53	-20	2015	0.44	64.03	-0.02
103	SLD 4	53	-20	2015	0.44	64.03	-0.02
103	SLD 5	3	273	2189	-12.66	5.46	0
103	SLD 6	3	273	2189	-12.66	5.46	0
103	SLD 7	26	-244	2067	10.35	29.33	-0.01
103	SLD 8	26	-244	2067	10.35	29.33	-0.01
103	SLD 9	-27	237	2270	-11.07	-31.44	0.01
103	SLD 10	-27	237	2270	-11.07	-31.44	0.01
103	SLD 11	-4	-280	2148	11.94	-7.57	0
103	SLD 12	-4	-280	2148	11.94	-7.57	0
103	SLD 13	-54	13	2322	-1.16	-66.13	0.02
103	SLD 14	-54	13	2322	-1.16	-66.13	0.02
103	SLD 15	-47	-142	2285	5.75	-58.97	0.02
103	SLD 16	-47	-142	2285	5.75	-58.97	0.02
103	SLV 1	119	326	1892	-14.86	149.7	-0.04
103	SLV 2	119	326	1892	-14.86	149.7	-0.04
103	SLV 3	136	-40	1805	1.41	168	-0.05
103	SLV 4	136	-40	1805	1.41	168	-0.05
103	SLV 5	9	650	2218	-29.39	16.41	0.01
103	SLV 6	9	650	2218	-29.39	16.41	0.01
103	SLV 7	67	-569	1927	24.85	77.42	-0.03
103	SLV 8	67	-569	1927	24.85	77.42	-0.03
103	SLV 9	-68	562	2410	-25.56	-79.53	0.03
103	SLV 10	-68	562	2410	-25.56	-79.53	0.03
103	SLV 11	-10	-657	2119	28.67	-18.52	-0.01
103	SLV 12	-10	-657	2119	28.67	-18.52	-0.01
103	SLV 13	-137	33	2532	-2.12	-170.11	0.05
103	SLV 14	-137	33	2532	-2.12	-170.11	0.05
103	SLV 15	-120	-333	2445	14.15	-151.81	0.04
103	SLV 16	-120	-333	2445	14.15	-151.81	0.04
104	SLU 1	0	-96	2030	3.74	0.18	0
104	SLU 2	1	-85	1983	3.39	-4.03	0
104	SLU 3	0	-96	2030	3.74	0.18	0
104	SLU 4	1	-89	2001	3.53	-2.34	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
104	SLU 5	1	-85	1983	3.39	-4.03	0
104	SLU 6	0	-96	2030	3.74	0.18	0
104	SLU 7	1	-89	2001	3.53	-2.34	0
104	SLU 8	0	-96	2030	3.74	0.18	0
104	SLU 9	1	-89	2001	3.53	-2.34	0
104	SLU 10	1	-131	2471	5.21	-4.05	0
104	SLU 11	0	-142	2518	5.56	0.16	0
104	SLU 12	1	-135	2489	5.35	-2.37	0
104	SLU 13	1	-131	2471	5.21	-4.05	0
104	SLU 14	0	-142	2518	5.56	0.16	0
104	SLU 15	1	-135	2489	5.35	-2.37	0
104	SLU 16	0	-142	2518	5.56	0.16	0
104	SLU 17	1	-135	2489	5.35	-2.37	0
104	SLU 18	0	-161	2727	6.34	0.14	0
104	SLU 19	0	-155	2698	6.13	-2.38	0
104	SLU 20	0	-161	2727	6.34	0.14	0
104	SLU 21	0	-155	2698	6.13	-2.38	0
104	SLU 22	0	-115	2282	4.52	0.18	0
104	SLU 23	1	-104	2235	4.16	-4.03	0
104	SLU 24	0	-115	2282	4.52	0.18	0
104	SLU 25	1	-109	2254	4.31	-2.34	0
104	SLU 26	1	-104	2235	4.16	-4.03	0
104	SLU 27	0	-115	2282	4.52	0.18	0
104	SLU 28	1	-109	2254	4.31	-2.34	0
104	SLU 29	0	-115	2282	4.52	0.18	0
104	SLU 30	1	-109	2254	4.31	-2.34	0
104	SLU 31	1	-150	2723	5.98	-4.06	0
104	SLU 32	0	-161	2770	6.34	0.15	0
104	SLU 33	0	-155	2742	6.12	-2.37	0
104	SLU 34	1	-150	2723	5.98	-4.06	0
104	SLU 35	0	-161	2770	6.34	0.15	0
104	SLU 36	0	-155	2742	6.12	-2.37	0
104	SLU 37	0	-161	2770	6.34	0.15	0
104	SLU 38	0	-155	2742	6.12	-2.37	0
104	SLU 39	0	-181	2979	7.12	0.14	0
104	SLU 40	0	-174	2951	6.9	-2.39	0
104	SLU 41	0	-181	2979	7.12	0.14	0
104	SLU 42	0	-174	2951	6.9	-2.39	0
104	SLU 43	0	-117	2552	4.6	0.24	0
104	SLU 44	1	-106	2505	4.25	-3.97	0
104	SLU 45	0	-117	2552	4.6	0.24	0
104	SLU 46	1	-111	2524	4.39	-2.29	0
104	SLU 47	1	-106	2505	4.25	-3.97	0
104	SLU 48	0	-117	2552	4.6	0.24	0
104	SLU 49	1	-111	2524	4.39	-2.29	0
104	SLU 50	0	-117	2552	4.6	0.24	0
104	SLU 51	1	-111	2524	4.39	-2.29	0
104	SLU 52	1	-152	2993	6.06	-4	0
104	SLU 53	0	-163	3040	6.42	0.21	0
104	SLU 54	1	-157	3012	6.21	-2.31	0
104	SLU 55	1	-152	2993	6.06	-4	0
104	SLU 56	0	-163	3040	6.42	0.21	0
104	SLU 57	1	-157	3012	6.21	-2.31	0
104	SLU 58	0	-163	3040	6.42	0.21	0
104	SLU 59	1	-157	3012	6.21	-2.31	0
104	SLU 60	0	-183	3249	7.2	0.2	0
104	SLU 61	0	-177	3221	6.99	-2.33	0
104	SLU 62	0	-183	3249	7.2	0.2	0
104	SLU 63	0	-177	3221	6.99	-2.33	0
104	SLU 64	0	-137	2804	5.38	0.24	0
104	SLU 65	1	-126	2757	5.02	-3.97	0
104	SLU 66	0	-137	2804	5.38	0.24	0
104	SLU 67	1	-131	2776	5.16	-2.29	0
104	SLU 68	1	-126	2757	5.02	-3.97	0
104	SLU 69	0	-137	2804	5.38	0.24	0
104	SLU 70	1	-131	2776	5.16	-2.29	0
104	SLU 71	0	-137	2804	5.38	0.24	0
104	SLU 72	1	-131	2776	5.16	-2.29	0
104	SLU 73	1	-172	3245	6.84	-4	0
104	SLU 74	0	-183	3292	7.19	0.21	0
104	SLU 75	0	-177	3264	6.98	-2.32	0
104	SLU 76	1	-172	3245	6.84	-4	0
104	SLU 77	0	-183	3292	7.19	0.21	0
104	SLU 78	0	-177	3264	6.98	-2.32	0
104	SLU 79	0	-183	3292	7.19	0.21	0
104	SLU 80	0	-177	3264	6.98	-2.32	0
104	SLU 81	0	-203	3501	7.97	0.2	0
104	SLU 82	0	-196	3473	7.76	-2.33	0
104	SLU 83	0	-203	3501	7.97	0.2	0
104	SLU 84	0	-196	3473	7.76	-2.33	0
104	SLE RA 1	0	-101	2102	3.97	0.18	0
104	SLE RA 2	1	-94	2070	3.73	-2.62	0
104	SLE RA 3	0	-101	2102	3.97	0.18	0
104	SLE RA 4	0	-97	2083	3.82	-1.5	0
104	SLE RA 5	1	-94	2070	3.73	-2.62	0
104	SLE RA 6	0	-101	2102	3.97	0.18	0
104	SLE RA 7	0	-97	2083	3.82	-1.5	0
104	SLE RA 8	0	-101	2102	3.97	0.18	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
104	SLE RA 9	0	-97	2083	3.82	-1.5	0
104	SLE RA 10	1	-125	2396	4.94	-2.64	0
104	SLE RA 11	0	-132	2427	5.18	0.16	0
104	SLE RA 12	0	-127	2408	5.04	-1.52	0
104	SLE RA 13	1	-125	2396	4.94	-2.64	0
104	SLE RA 14	0	-132	2427	5.18	0.16	0
104	SLE RA 15	0	-127	2408	5.04	-1.52	0
104	SLE RA 16	0	-132	2427	5.18	0.16	0
104	SLE RA 17	0	-127	2408	5.04	-1.52	0
104	SLE RA 18	0	-145	2566	5.7	0.16	0
104	SLE RA 19	0	-141	2548	5.55	-1.53	0
104	SLE RA 20	0	-145	2566	5.7	0.16	0
104	SLE RA 21	0	-141	2548	5.55	-1.53	0
104	SLE FR 1	0	-101	2102	3.97	0.18	0
104	SLE FR 2	0	-100	2095	3.92	-0.38	0
104	SLE FR 3	0	-101	2102	3.97	0.18	0
104	SLE FR 4	0	-113	2235	4.44	-0.39	0
104	SLE FR 5	0	-114	2241	4.49	0.18	0
104	SLE FR 6	0	-123	2334	4.83	0.17	0
104	SLE QP 1	0	-101	2102	3.97	0.18	0
104	SLE QP 2	0	-114	2241	4.49	0.18	0
104	SLD 1	-10	-108	2322	4.09	20.74	-0.03
104	SLD 2	-10	-108	2322	4.09	20.74	-0.03
104	SLD 3	-3	-239	2365	9.68	16.89	-0.02
104	SLD 4	-3	-239	2365	9.68	16.89	-0.02
104	SLD 5	-14	86	2201	-4.12	12.18	-0.02
104	SLD 6	-14	86	2201	-4.12	12.18	-0.02
104	SLD 7	10	-351	2343	14.53	-0.64	0.01
104	SLD 8	10	-351	2343	14.53	-0.64	0.01
104	SLD 9	-10	122	2139	-5.56	0.99	-0.01
104	SLD 10	-10	122	2139	-5.56	0.99	-0.01
104	SLD 11	13	-315	2282	13.09	-11.83	0.02
104	SLD 12	13	-315	2282	13.09	-11.83	0.02
104	SLD 13	2	10	2117	-0.71	-16.54	0.02
104	SLD 14	2	10	2117	-0.71	-16.54	0.02
104	SLD 15	9	-121	2160	4.88	-20.39	0.02
104	SLD 16	9	-121	2160	4.88	-20.39	0.02
104	SLV 1	-24	-99	2443	3.52	52.63	-0.07
104	SLV 2	-24	-99	2443	3.52	52.63	-0.07
104	SLV 3	-7	-408	2544	16.74	43.4	-0.05
104	SLV 4	-7	-408	2544	16.74	43.4	-0.05
104	SLV 5	-32	360	2149	-15.84	29.91	-0.05
104	SLV 6	-32	360	2149	-15.84	29.91	-0.05
104	SLV 7	23	-672	2485	28.2	-0.85	0.02
104	SLV 8	23	-672	2485	28.2	-0.85	0.02
104	SLV 9	-23	443	1997	-19.23	1.2	-0.02
104	SLV 10	-23	443	1997	-19.23	1.2	-0.02
104	SLV 11	32	-588	2333	24.81	-29.56	0.05
104	SLV 12	32	-588	2333	24.81	-29.56	0.05
104	SLV 13	7	180	1938	-7.77	-43.05	0.04
104	SLV 14	7	180	1938	-7.77	-43.05	0.04
104	SLV 15	24	-130	2039	5.45	-52.28	0.07
104	SLV 16	24	-130	2039	5.45	-52.28	0.07
105	SLU 1	0	125	2004	-5.04	0.21	0
105	SLU 2	-8	123	2000	-5	-8.9	0.02
105	SLU 3	0	125	2004	-5.04	0.21	0
105	SLU 4	-5	124	2002	-5.02	-5.26	0.01
105	SLU 5	-8	123	2000	-5	-8.9	0.02
105	SLU 6	0	125	2004	-5.04	0.21	0
105	SLU 7	-5	124	2002	-5.02	-5.26	0.01
105	SLU 8	0	125	2004	-5.04	0.21	0
105	SLU 9	-5	124	2002	-5.02	-5.26	0.01
105	SLU 10	-8	252	3249	-10.22	-8.39	0.02
105	SLU 11	1	254	3253	-10.27	0.72	0
105	SLU 12	-4	252	3250	-10.24	-4.75	0.01
105	SLU 13	-8	252	3249	-10.22	-8.39	0.02
105	SLU 14	1	254	3253	-10.27	0.72	0
105	SLU 15	-4	252	3250	-10.24	-4.75	0.01
105	SLU 16	1	254	3253	-10.27	0.72	0
105	SLU 17	-4	252	3250	-10.24	-4.75	0.01
105	SLU 18	1	309	3788	-12.51	0.93	0
105	SLU 19	-4	308	3786	-12.48	-4.53	0.01
105	SLU 20	1	309	3788	-12.51	0.93	0
105	SLU 21	-4	308	3786	-12.48	-4.53	0.01
105	SLU 22	0	181	2627	-7.34	0.41	0
105	SLU 23	-8	179	2623	-7.29	-8.7	0.02
105	SLU 24	0	181	2627	-7.34	0.41	0
105	SLU 25	-5	180	2625	-7.31	-5.05	0.01
105	SLU 26	-8	179	2623	-7.29	-8.7	0.02
105	SLU 27	0	181	2627	-7.34	0.41	0
105	SLU 28	-5	180	2625	-7.31	-5.05	0.01
105	SLU 29	0	181	2627	-7.34	0.41	0
105	SLU 30	-5	180	2625	-7.31	-5.05	0.01
105	SLU 31	-8	308	3872	-12.52	-8.19	0.02
105	SLU 32	1	310	3876	-12.56	0.92	0
105	SLU 33	-4	309	3874	-12.54	-4.55	0.01
105	SLU 34	-8	308	3872	-12.52	-8.19	0.02
105	SLU 35	1	310	3876	-12.56	0.92	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
105	SLU 36	-4	309	3874	-12.54	-4.55	0.01
105	SLU 37	1	310	3876	-12.56	0.92	0
105	SLU 38	-4	309	3874	-12.54	-4.55	0.01
105	SLU 39	1	365	4411	-14.8	1.13	0
105	SLU 40	-4	364	4409	-14.78	-4.33	0.01
105	SLU 41	1	365	4411	-14.8	1.13	0
105	SLU 42	-4	364	4409	-14.78	-4.33	0.01
105	SLU 43	0	143	2391	-5.77	0.2	0
105	SLU 44	-8	141	2388	-5.73	-8.9	0.02
105	SLU 45	0	143	2391	-5.77	0.2	0
105	SLU 46	-5	142	2389	-5.74	-5.26	0.01
105	SLU 47	-8	141	2388	-5.73	-8.9	0.02
105	SLU 48	0	143	2391	-5.77	0.2	0
105	SLU 49	-5	142	2389	-5.74	-5.26	0.01
105	SLU 50	0	143	2391	-5.77	0.2	0
105	SLU 51	-5	142	2389	-5.74	-5.26	0.01
105	SLU 52	-8	270	3636	-10.95	-8.4	0.02
105	SLU 53	1	272	3640	-11	0.71	0
105	SLU 54	-4	270	3638	-10.97	-4.75	0.01
105	SLU 55	-8	270	3636	-10.95	-8.4	0.02
105	SLU 56	1	272	3640	-11	0.71	0
105	SLU 57	-4	270	3638	-10.97	-4.75	0.01
105	SLU 58	1	272	3640	-11	0.71	0
105	SLU 59	-4	270	3638	-10.97	-4.75	0.01
105	SLU 60	1	327	4175	-13.23	0.93	0
105	SLU 61	-4	326	4173	-13.21	-4.54	0.01
105	SLU 62	1	327	4175	-13.23	0.93	0
105	SLU 63	-4	326	4173	-13.21	-4.54	0.01
105	SLU 64	0	200	3015	-8.06	0.4	0
105	SLU 65	-8	198	3011	-8.02	-8.7	0.02
105	SLU 66	0	200	3015	-8.06	0.4	0
105	SLU 67	-5	198	3012	-8.04	-5.06	0.01
105	SLU 68	-8	198	3011	-8.02	-8.7	0.02
105	SLU 69	0	200	3015	-8.06	0.4	0
105	SLU 70	-5	198	3012	-8.04	-5.06	0.01
105	SLU 71	0	200	3015	-8.06	0.4	0
105	SLU 72	-5	198	3012	-8.04	-5.06	0.01
105	SLU 73	-8	326	4260	-13.24	-8.2	0.02
105	SLU 74	1	328	4263	-13.29	0.91	0
105	SLU 75	-4	327	4261	-13.26	-4.55	0.01
105	SLU 76	-8	326	4260	-13.24	-8.2	0.02
105	SLU 77	1	328	4263	-13.29	0.91	0
105	SLU 78	-4	327	4261	-13.26	-4.55	0.01
105	SLU 79	1	328	4263	-13.29	0.91	0
105	SLU 80	-4	327	4261	-13.26	-4.55	0.01
105	SLU 81	1	383	4798	-15.53	1.13	0
105	SLU 82	-4	382	4796	-15.5	-4.34	0.01
105	SLU 83	1	383	4798	-15.53	1.13	0
105	SLU 84	-4	382	4796	-15.5	-4.34	0.01
105	SLE RA 1	0	141	2182	-5.7	0.26	0
105	SLE RA 2	-5	140	2180	-5.67	-5.81	0.01
105	SLE RA 3	0	141	2182	-5.7	0.26	0
105	SLE RA 4	-3	140	2180	-5.68	-3.38	0.01
105	SLE RA 5	-5	140	2180	-5.67	-5.81	0.01
105	SLE RA 6	0	141	2182	-5.7	0.26	0
105	SLE RA 7	-3	140	2180	-5.68	-3.38	0.01
105	SLE RA 8	0	141	2182	-5.7	0.26	0
105	SLE RA 9	-3	140	2180	-5.68	-3.38	0.01
105	SLE RA 10	-5	226	3012	-9.15	-5.47	0.01
105	SLE RA 11	0	227	3014	-9.18	0.6	0
105	SLE RA 12	-3	226	3013	-9.16	-3.04	0.01
105	SLE RA 13	-5	226	3012	-9.15	-5.47	0.01
105	SLE RA 14	0	227	3014	-9.18	0.6	0
105	SLE RA 15	-3	226	3013	-9.16	-3.04	0.01
105	SLE RA 16	0	227	3014	-9.18	0.6	0
105	SLE RA 17	-3	226	3013	-9.16	-3.04	0.01
105	SLE RA 18	1	264	3371	-10.68	0.75	0
105	SLE RA 19	-3	263	3370	-10.66	-2.89	0.01
105	SLE RA 20	1	264	3371	-10.68	0.75	0
105	SLE RA 21	-3	263	3370	-10.66	-2.89	0.01
105	SLE FR 1	0	141	2182	-5.7	0.26	0
105	SLE FR 2	-1	141	2181	-5.69	-0.95	0
105	SLE FR 3	0	141	2182	-5.7	0.26	0
105	SLE FR 4	-1	178	2538	-7.19	-0.8	0
105	SLE FR 5	0	178	2539	-7.19	0.41	0
105	SLE FR 6	0	202	2777	-8.19	0.51	0
105	SLE QP 1	0	141	2182	-5.7	0.26	0
105	SLE QP 2	0	178	2539	-7.19	0.41	0
105	SLD 1	34	323	2541	-20.94	38.19	-0.08
105	SLD 2	34	323	2541	-20.94	38.19	-0.08
105	SLD 3	33	113	2518	2.61	36.41	-0.07
105	SLD 4	33	113	2518	2.61	36.41	-0.07
105	SLD 5	14	540	2575	-47.04	14.45	-0.03
105	SLD 6	14	540	2575	-47.04	14.45	-0.03
105	SLD 7	7	-160	2497	31.47	8.5	-0.02
105	SLD 8	7	-160	2497	31.47	8.5	-0.02
105	SLD 9	-6	516	2580	-45.86	-7.68	0.02
105	SLD 10	-6	516	2580	-45.86	-7.68	0.02





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
105	SLD 11	-13	-184	2503	32.66	-13.63	0.03
105	SLD 12	-13	-184	2503	32.66	-13.63	0.03
105	SLD 13	-32	243	2560	-17	-35.59	0.07
105	SLD 14	-32	243	2560	-17	-35.59	0.07
105	SLD 15	-34	33	2537	6.56	-37.37	0.08
105	SLD 16	-34	33	2537	6.56	-37.37	0.08
105	SLV 1	105	535	2545	-42.12	117.14	-0.23
105	SLV 2	105	535	2545	-42.12	117.14	-0.23
105	SLV 3	100	10	2485	18.1	112.43	-0.23
105	SLV 4	100	10	2485	18.1	112.43	-0.23
105	SLV 5	39	1080	2632	-109	42.57	-0.09
105	SLV 6	39	1080	2632	-109	42.57	-0.09
105	SLV 7	22	-668	2431	91.73	26.88	-0.05
105	SLV 8	22	-668	2431	91.73	26.88	-0.05
105	SLV 9	-22	1023	2646	-106.11	-26.06	0.05
105	SLV 10	-22	1023	2646	-106.11	-26.06	0.05
105	SLV 11	-39	-725	2446	94.62	-41.75	0.08
105	SLV 12	-39	-725	2446	94.62	-41.75	0.08
105	SLV 13	-99	345	2593	-32.48	-111.61	0.22
105	SLV 14	-99	345	2593	-32.48	-111.61	0.22
105	SLV 15	-104	-179	2533	27.74	-116.32	0.23
105	SLV 16	-104	-179	2533	27.74	-116.32	0.23
106	SLU 1	0	-40	2065	2.18	-0.64	0
106	SLU 2	-2	-45	2089	2.39	-4.26	0
106	SLU 3	0	-40	2065	2.18	-0.64	0
106	SLU 4	-1	-43	2079	2.3	-2.81	0
106	SLU 5	-2	-45	2089	2.39	-4.26	0
106	SLU 6	0	-40	2065	2.18	-0.64	0
106	SLU 7	-1	-43	2079	2.3	-2.81	0
106	SLU 8	0	-40	2065	2.18	-0.64	0
106	SLU 9	-1	-43	2079	2.3	-2.81	0
106	SLU 10	-3	-39	2354	2.79	-5.01	0
106	SLU 11	-1	-34	2330	2.58	-1.39	0
106	SLU 12	-2	-37	2344	2.71	-3.56	0
106	SLU 13	-3	-39	2354	2.79	-5.01	0
106	SLU 14	-1	-34	2330	2.58	-1.39	0
106	SLU 15	-2	-37	2344	2.71	-3.56	0
106	SLU 16	-1	-34	2330	2.58	-1.39	0
106	SLU 17	-2	-37	2344	2.71	-3.56	0
106	SLU 18	-1	-31	2444	2.75	-1.72	0
106	SLU 19	-2	-34	2458	2.88	-3.89	0
106	SLU 20	-1	-31	2444	2.75	-1.72	0
106	SLU 21	-2	-34	2458	2.88	-3.89	0
106	SLU 22	0	-39	2229	2.4	-0.95	0
106	SLU 23	-2	-44	2252	2.61	-4.56	0
106	SLU 24	0	-39	2229	2.4	-0.95	0
106	SLU 25	-2	-42	2243	2.52	-3.12	0
106	SLU 26	-2	-44	2252	2.61	-4.56	0
106	SLU 27	0	-39	2229	2.4	-0.95	0
106	SLU 28	-2	-42	2243	2.52	-3.12	0
106	SLU 29	0	-39	2229	2.4	-0.95	0
106	SLU 30	-2	-42	2243	2.52	-3.12	0
106	SLU 31	-3	-38	2517	3.01	-5.32	0
106	SLU 32	-1	-33	2494	2.8	-1.7	0
106	SLU 33	-2	-36	2508	2.93	-3.87	0
106	SLU 34	-3	-38	2517	3.01	-5.32	0
106	SLU 35	-1	-33	2494	2.8	-1.7	0
106	SLU 36	-2	-36	2508	2.93	-3.87	0
106	SLU 37	-1	-33	2494	2.8	-1.7	0
106	SLU 38	-2	-36	2508	2.93	-3.87	0
106	SLU 39	-1	-30	2607	2.98	-2.02	0
106	SLU 40	-2	-33	2621	3.1	-4.19	0
106	SLU 41	-1	-30	2607	2.98	-2.02	0
106	SLU 42	-2	-33	2621	3.1	-4.19	0
106	SLU 43	0	-53	2628	2.75	-0.73	0
106	SLU 44	-2	-58	2652	2.97	-4.34	0
106	SLU 45	0	-53	2628	2.75	-0.73	0
106	SLU 46	-1	-56	2643	2.88	-2.9	0
106	SLU 47	-2	-58	2652	2.97	-4.34	0
106	SLU 48	0	-53	2628	2.75	-0.73	0
106	SLU 49	-1	-56	2643	2.88	-2.9	0
106	SLU 50	0	-53	2628	2.75	-0.73	0
106	SLU 51	-1	-56	2643	2.88	-2.9	0
106	SLU 52	-3	-52	2917	3.37	-5.1	0
106	SLU 53	-1	-46	2893	3.16	-1.48	0
106	SLU 54	-2	-49	2908	3.29	-3.65	0
106	SLU 55	-3	-52	2917	3.37	-5.1	0
106	SLU 56	-1	-46	2893	3.16	-1.48	0
106	SLU 57	-2	-49	2908	3.29	-3.65	0
106	SLU 58	-1	-46	2893	3.16	-1.48	0
106	SLU 59	-2	-49	2908	3.29	-3.65	0
106	SLU 60	-1	-44	3007	3.33	-1.8	0
106	SLU 61	-2	-47	3021	3.46	-3.97	0
106	SLU 62	-1	-44	3007	3.33	-1.8	0
106	SLU 63	-2	-47	3021	3.46	-3.97	0
106	SLU 64	-1	-52	2792	2.97	-1.03	0
106	SLU 65	-2	-57	2816	3.19	-4.65	0
106	SLU 66	-1	-52	2792	2.97	-1.03	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
106	SLU 67	-2	-55	2806	3.1	-3.2	0
106	SLU 68	-2	-57	2816	3.19	-4.65	0
106	SLU 69	-1	-52	2792	2.97	-1.03	0
106	SLU 70	-2	-55	2806	3.1	-3.2	0
106	SLU 71	-1	-52	2792	2.97	-1.03	0
106	SLU 72	-2	-55	2806	3.1	-3.2	0
106	SLU 73	-3	-50	3081	3.59	-5.41	0
106	SLU 74	-1	-45	3057	3.38	-1.79	0
106	SLU 75	-2	-48	3071	3.51	-3.96	0
106	SLU 76	-3	-50	3081	3.59	-5.41	0
106	SLU 77	-1	-45	3057	3.38	-1.79	0
106	SLU 78	-2	-48	3071	3.51	-3.96	0
106	SLU 79	-1	-45	3057	3.38	-1.79	0
106	SLU 80	-2	-48	3071	3.51	-3.96	0
106	SLU 81	-1	-42	3171	3.55	-2.11	0
106	SLU 82	-2	-45	3185	3.68	-4.28	0
106	SLU 83	-1	-42	3171	3.55	-2.11	0
106	SLU 84	-2	-45	3185	3.68	-4.28	0
106	SLE RA 1	0	-40	2112	2.24	-0.73	0
106	SLE RA 2	-2	-43	2127	2.38	-3.14	0
106	SLE RA 3	0	-40	2112	2.24	-0.73	0
106	SLE RA 4	-1	-42	2121	2.32	-2.17	0
106	SLE RA 5	-2	-43	2127	2.38	-3.14	0
106	SLE RA 6	0	-40	2112	2.24	-0.73	0
106	SLE RA 7	-1	-42	2121	2.32	-2.17	0
106	SLE RA 8	0	-40	2112	2.24	-0.73	0
106	SLE RA 9	-1	-42	2121	2.32	-2.17	0
106	SLE RA 10	-2	-39	2304	2.65	-3.64	0
106	SLE RA 11	-1	-36	2289	2.51	-1.23	0
106	SLE RA 12	-1	-38	2298	2.59	-2.68	0
106	SLE RA 13	-2	-39	2304	2.65	-3.64	0
106	SLE RA 14	-1	-36	2289	2.51	-1.23	0
106	SLE RA 15	-1	-38	2298	2.59	-2.68	0
106	SLE RA 16	-1	-36	2289	2.51	-1.23	0
106	SLE RA 17	-1	-38	2298	2.59	-2.68	0
106	SLE RA 18	-1	-34	2364	2.62	-1.44	0
106	SLE RA 19	-2	-36	2374	2.71	-2.89	0
106	SLE RA 20	-1	-34	2364	2.62	-1.44	0
106	SLE RA 21	-2	-36	2374	2.71	-2.89	0
106	SLE FR 1	0	-40	2112	2.24	-0.73	0
106	SLE FR 2	-1	-41	2115	2.27	-1.21	0
106	SLE FR 3	0	-40	2112	2.24	-0.73	0
106	SLE FR 4	-1	-39	2191	2.38	-1.42	0
106	SLE FR 5	0	-38	2188	2.35	-0.94	0
106	SLE FR 6	-1	-37	2238	2.43	-1.09	0
106	SLE QP 1	0	-40	2112	2.24	-0.73	0
106	SLE QP 2	0	-38	2188	2.35	-0.94	0
106	SLD 1	52	103	2085	-3.86	62.76	-0.02
106	SLD 2	52	103	2085	-3.86	62.76	-0.02
106	SLD 3	59	-52	2055	3.02	70.12	-0.02
106	SLD 4	59	-52	2055	3.02	70.12	-0.02
106	SLD 5	5	240	2202	-9.93	7.02	0
106	SLD 6	5	240	2202	-9.93	7.02	0
106	SLD 7	28	-279	2102	12.98	31.53	-0.01
106	SLD 8	28	-279	2102	12.98	31.53	-0.01
106	SLD 9	-29	202	2273	-8.27	-33.41	0.01
106	SLD 10	-29	202	2273	-8.27	-33.41	0.01
106	SLD 11	-6	-317	2173	14.64	-8.9	0
106	SLD 12	-6	-317	2173	14.64	-8.9	0
106	SLD 13	-60	-24	2320	1.69	-72	0.02
106	SLD 14	-60	-24	2320	1.69	-72	0.02
106	SLD 15	-53	-180	2290	8.56	-64.65	0.02
106	SLD 16	-53	-180	2290	8.56	-64.65	0.02
106	SLV 1	135	299	1943	-12.44	164.96	-0.04
106	SLV 2	135	299	1943	-12.44	164.96	-0.04
106	SLV 3	152	-68	1873	3.77	183.82	-0.05
106	SLV 4	152	-68	1873	3.77	183.82	-0.05
106	SLV 5	14	620	2221	-26.66	20.22	0
106	SLV 6	14	620	2221	-26.66	20.22	0
106	SLV 7	71	-604	1986	27.36	83.09	-0.02
106	SLV 8	71	-604	1986	27.36	83.09	-0.02
106	SLV 9	-72	528	2389	-22.65	-84.97	0.03
106	SLV 10	-72	528	2389	-22.65	-84.97	0.03
106	SLV 11	-15	-696	2154	31.37	-22.11	0
106	SLV 12	-15	-696	2154	31.37	-22.11	0
106	SLV 13	-153	-8	2502	0.94	-185.7	0.05
106	SLV 14	-153	-8	2502	0.94	-185.7	0.05
106	SLV 15	-136	-375	2432	17.15	-166.84	0.04
106	SLV 16	-136	-375	2432	17.15	-166.84	0.04
107	SLU 1	0	-139	1979	5.82	0.06	0
107	SLU 2	-3	-128	1941	5.32	-7.32	0
107	SLU 3	0	-139	1979	5.82	0.06	0
107	SLU 4	-2	-132	1957	5.52	-4.36	0
107	SLU 5	-3	-128	1941	5.32	-7.32	0
107	SLU 6	0	-139	1979	5.82	0.06	0
107	SLU 7	-2	-132	1957	5.52	-4.36	0
107	SLU 8	0	-139	1979	5.82	0.06	0
107	SLU 9	-2	-132	1957	5.52	-4.36	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
107	SLU 10	-3	-192	2405	7.99	-7.44	0
107	SLU 11	-1	-204	2443	8.49	-0.06	0
107	SLU 12	-2	-197	2420	8.19	-4.48	0
107	SLU 13	-3	-192	2405	7.99	-7.44	0
107	SLU 14	-1	-204	2443	8.49	-0.06	0
107	SLU 15	-2	-197	2420	8.19	-4.48	0
107	SLU 16	-1	-204	2443	8.49	-0.06	0
107	SLU 17	-2	-197	2420	8.19	-4.48	0
107	SLU 18	-1	-231	2641	9.64	-0.11	0
107	SLU 19	-2	-225	2619	9.34	-4.54	0
107	SLU 20	-1	-231	2641	9.64	-0.11	0
107	SLU 21	-2	-225	2619	9.34	-4.54	0
107	SLU 22	-1	-169	2220	7.05	0.02	0
107	SLU 23	-3	-157	2183	6.55	-7.36	0
107	SLU 24	-1	-169	2220	7.05	0.02	0
107	SLU 25	-2	-162	2198	6.75	-4.41	0
107	SLU 26	-3	-157	2183	6.55	-7.36	0
107	SLU 27	-1	-169	2220	7.05	0.02	0
107	SLU 28	-2	-162	2198	6.75	-4.41	0
107	SLU 29	-1	-169	2220	7.05	0.02	0
107	SLU 30	-2	-162	2198	6.75	-4.41	0
107	SLU 31	-3	-222	2646	9.23	-7.48	0
107	SLU 32	-1	-233	2684	9.73	-0.1	0
107	SLU 33	-2	-226	2661	9.43	-4.53	0
107	SLU 34	-3	-222	2646	9.23	-7.48	0
107	SLU 35	-1	-233	2684	9.73	-0.1	0
107	SLU 36	-2	-226	2661	9.43	-4.53	0
107	SLU 37	-1	-233	2684	9.73	-0.1	0
107	SLU 38	-2	-226	2661	9.43	-4.53	0
107	SLU 39	-1	-261	2883	10.87	-0.15	0
107	SLU 40	-3	-254	2860	10.57	-4.58	0
107	SLU 41	-1	-261	2883	10.87	-0.15	0
107	SLU 42	-3	-254	2860	10.57	-4.58	0
107	SLU 43	0	-171	2490	7.14	0.09	0
107	SLU 44	-3	-159	2453	6.64	-7.28	0
107	SLU 45	0	-171	2490	7.14	0.09	0
107	SLU 46	-2	-164	2468	6.84	-4.33	0
107	SLU 47	-3	-159	2453	6.64	-7.28	0
107	SLU 48	0	-171	2490	7.14	0.09	0
107	SLU 49	-2	-164	2468	6.84	-4.33	0
107	SLU 50	0	-171	2490	7.14	0.09	0
107	SLU 51	-2	-164	2468	6.84	-4.33	0
107	SLU 52	-3	-224	2916	9.32	-7.4	0
107	SLU 53	-1	-235	2954	9.82	-0.03	0
107	SLU 54	-2	-228	2931	9.52	-4.45	0
107	SLU 55	-3	-224	2916	9.32	-7.4	0
107	SLU 56	-1	-235	2954	9.82	-0.03	0
107	SLU 57	-2	-228	2931	9.52	-4.45	0
107	SLU 58	-1	-235	2954	9.82	-0.03	0
107	SLU 59	-2	-228	2931	9.52	-4.45	0
107	SLU 60	-1	-263	3153	10.96	-0.08	0
107	SLU 61	-2	-256	3130	10.66	-4.5	0
107	SLU 62	-1	-263	3153	10.96	-0.08	0
107	SLU 63	-2	-256	3130	10.66	-4.5	0
107	SLU 64	-1	-200	2732	8.37	0.05	0
107	SLU 65	-3	-189	2694	7.87	-7.32	0
107	SLU 66	-1	-200	2732	8.37	0.05	0
107	SLU 67	-2	-194	2709	8.07	-4.37	0
107	SLU 68	-3	-189	2694	7.87	-7.32	0
107	SLU 69	-1	-200	2732	8.37	0.05	0
107	SLU 70	-2	-194	2709	8.07	-4.37	0
107	SLU 71	-1	-200	2732	8.37	0.05	0
107	SLU 72	-2	-194	2709	8.07	-4.37	0
107	SLU 73	-3	-253	3157	10.55	-7.44	0
107	SLU 74	-1	-265	3195	11.05	-0.07	0
107	SLU 75	-2	-258	3172	10.75	-4.49	0
107	SLU 76	-3	-253	3157	10.55	-7.44	0
107	SLU 77	-1	-265	3195	11.05	-0.07	0
107	SLU 78	-2	-258	3172	10.75	-4.49	0
107	SLU 79	-1	-265	3195	11.05	-0.07	0
107	SLU 80	-2	-258	3172	10.75	-4.49	0
107	SLU 81	-1	-293	3394	12.2	-0.12	0
107	SLU 82	-3	-286	3371	11.9	-4.54	0
107	SLU 83	-1	-293	3394	12.2	-0.12	0
107	SLU 84	-3	-286	3371	11.9	-4.54	0
107	SLE RA 1	0	-148	2048	6.17	0.05	0
107	SLE RA 2	-2	-140	2023	5.84	-4.87	0
107	SLE RA 3	0	-148	2048	6.17	0.05	0
107	SLE RA 4	-1	-143	2033	5.97	-2.9	0
107	SLE RA 5	-2	-140	2023	5.84	-4.87	0
107	SLE RA 6	0	-148	2048	6.17	0.05	0
107	SLE RA 7	-1	-143	2033	5.97	-2.9	0
107	SLE RA 8	0	-148	2048	6.17	0.05	0
107	SLE RA 9	-1	-143	2033	5.97	-2.9	0
107	SLE RA 10	-2	-183	2332	7.62	-4.95	0
107	SLE RA 11	-1	-191	2357	7.95	-0.03	0
107	SLE RA 12	-2	-186	2342	7.75	-2.98	0
107	SLE RA 13	-2	-183	2332	7.62	-4.95	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
107	SLE RA 14	-1	-191	2357	7.95	-0.03	0
107	SLE RA 15	-2	-186	2342	7.75	-2.98	0
107	SLE RA 16	-1	-191	2357	7.95	-0.03	0
107	SLE RA 17	-2	-186	2342	7.75	-2.98	0
107	SLE RA 18	-1	-209	2490	8.72	-0.06	0
107	SLE RA 19	-2	-205	2475	8.52	-3.01	0
107	SLE RA 20	-1	-209	2490	8.72	-0.06	0
107	SLE RA 21	-2	-205	2475	8.52	-3.01	0
107	SLE FR 1	0	-148	2048	6.17	0.05	0
107	SLE FR 2	-1	-146	2043	6.1	-0.93	0
107	SLE FR 3	0	-148	2048	6.17	0.05	0
107	SLE FR 4	-1	-165	2176	6.87	-0.97	0
107	SLE FR 5	-1	-166	2181	6.94	0.02	0
107	SLE FR 6	-1	-178	2269	7.45	-0.01	0
107	SLE QP 1	0	-148	2048	6.17	0.05	0
107	SLE QP 2	-1	-166	2181	6.94	0.02	0
107	SLD 1	19	-159	2236	6.55	33.72	-0.02
107	SLD 2	19	-159	2236	6.55	33.72	-0.02
107	SLD 3	26	-294	2285	12.33	29.27	-0.01
107	SLD 4	26	-294	2285	12.33	29.27	-0.01
107	SLD 5	-5	41	2123	-1.95	16.88	-0.03
107	SLD 6	-5	41	2123	-1.95	16.88	-0.03
107	SLD 7	17	-409	2286	17.32	2.04	0.01
107	SLD 8	17	-409	2286	17.32	2.04	0.01
107	SLD 9	-18	77	2075	-3.45	-2.01	-0.02
107	SLD 10	-18	77	2075	-3.45	-2.01	-0.02
107	SLD 11	3	-373	2239	15.82	-16.85	0.02
107	SLD 12	3	-373	2239	15.82	-16.85	0.02
107	SLD 13	-27	-38	2077	1.54	-29.24	0.01
107	SLD 14	-27	-38	2077	1.54	-29.24	0.01
107	SLD 15	-21	-174	2126	7.32	-33.69	0.02
107	SLD 16	-21	-174	2126	7.32	-33.69	0.02
107	SLV 1	51	-148	2319	6.03	86.32	-0.06
107	SLV 2	51	-148	2319	6.03	86.32	-0.06
107	SLV 3	67	-467	2435	19.68	75.45	-0.03
107	SLV 4	67	-467	2435	19.68	75.45	-0.03
107	SLV 5	-9	323	2047	-14.05	42.4	-0.06
107	SLV 6	-9	323	2047	-14.05	42.4	-0.06
107	SLV 7	43	-741	2432	31.47	6.15	0.03
107	SLV 8	43	-741	2432	31.47	6.15	0.03
107	SLV 9	-44	408	1929	-17.6	-6.12	-0.04
107	SLV 10	-44	408	1929	-17.6	-6.12	-0.04
107	SLV 11	8	-656	2314	27.92	-42.37	0.06
107	SLV 12	8	-656	2314	27.92	-42.37	0.06
107	SLV 13	-68	135	1927	-5.81	-75.41	0.03
107	SLV 14	-68	135	1927	-5.81	-75.41	0.03
107	SLV 15	-52	-184	2042	7.84	-86.29	0.05
107	SLV 16	-52	-184	2042	7.84	-86.29	0.05
108	SLU 1	0	9	2062	-0.17	0.22	0
108	SLU 2	-9	7	2058	-0.02	-9.32	0.02
108	SLU 3	0	9	2062	-0.17	0.22	0
108	SLU 4	-5	8	2060	-0.08	-5.5	0.01
108	SLU 5	-9	7	2058	-0.02	-9.32	0.02
108	SLU 6	0	9	2062	-0.17	0.22	0
108	SLU 7	-5	8	2060	-0.08	-5.5	0.01
108	SLU 8	0	9	2062	-0.17	0.22	0
108	SLU 9	-5	8	2060	-0.08	-5.5	0.01
108	SLU 10	-8	20	3369	-0.33	-8.79	0.02
108	SLU 11	1	23	3373	-0.48	0.74	0
108	SLU 12	-5	22	3370	-0.39	-4.97	0.01
108	SLU 13	-8	20	3369	-0.33	-8.79	0.02
108	SLU 14	1	23	3373	-0.48	0.74	0
108	SLU 15	-5	22	3370	-0.39	-4.97	0.01
108	SLU 16	1	23	3373	-0.48	0.74	0
108	SLU 17	-5	22	3370	-0.39	-4.97	0.01
108	SLU 18	1	29	3935	-0.62	0.97	0
108	SLU 19	-5	27	3932	-0.53	-4.75	0.01
108	SLU 20	1	29	3935	-0.62	0.97	0
108	SLU 21	-5	27	3932	-0.53	-4.75	0.01
108	SLU 22	0	16	2710	-0.34	0.43	0
108	SLU 23	-9	13	2706	-0.19	-9.11	0.02
108	SLU 24	0	16	2710	-0.34	0.43	0
108	SLU 25	-5	14	2708	-0.25	-5.29	0.01
108	SLU 26	-9	13	2706	-0.19	-9.11	0.02
108	SLU 27	0	16	2710	-0.34	0.43	0
108	SLU 28	-5	14	2708	-0.25	-5.29	0.01
108	SLU 29	0	16	2710	-0.34	0.43	0
108	SLU 30	-5	14	2708	-0.25	-5.29	0.01
108	SLU 31	-8	27	4017	-0.51	-8.58	0.02
108	SLU 32	1	30	4021	-0.66	0.95	0
108	SLU 33	-5	28	4019	-0.57	-4.76	0.01
108	SLU 34	-8	27	4017	-0.51	-8.58	0.02
108	SLU 35	1	30	4021	-0.66	0.95	0
108	SLU 36	-5	28	4019	-0.57	-4.76	0.01
108	SLU 37	1	30	4021	-0.66	0.95	0
108	SLU 38	-5	28	4019	-0.57	-4.76	0.01
108	SLU 39	1	36	4583	-0.79	1.18	0
108	SLU 40	-4	34	4581	-0.7	-4.54	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
108	SLU 41	1	36	4583	-0.79	1.18	0
108	SLU 42	-4	34	4581	-0.7	-4.54	0.01
108	SLU 43	0	10	2458	-0.15	0.21	0
108	SLU 44	-9	7	2454	-0.01	-9.32	0.02
108	SLU 45	0	10	2458	-0.15	0.21	0
108	SLU 46	-5	8	2456	-0.07	-5.51	0.01
108	SLU 47	-9	7	2454	-0.01	-9.32	0.02
108	SLU 48	0	10	2458	-0.15	0.21	0
108	SLU 49	-5	8	2456	-0.07	-5.51	0.01
108	SLU 50	0	10	2458	-0.15	0.21	0
108	SLU 51	-5	8	2456	-0.07	-5.51	0.01
108	SLU 52	-8	21	3765	-0.32	-8.79	0.02
108	SLU 53	1	24	3769	-0.47	0.74	0
108	SLU 54	-5	22	3767	-0.38	-4.98	0.01
108	SLU 55	-8	21	3765	-0.32	-8.79	0.02
108	SLU 56	1	24	3769	-0.47	0.74	0
108	SLU 57	-5	22	3767	-0.38	-4.98	0.01
108	SLU 58	1	24	3769	-0.47	0.74	0
108	SLU 59	-5	22	3767	-0.38	-4.98	0.01
108	SLU 60	1	30	4331	-0.61	0.96	0
108	SLU 61	-5	28	4328	-0.52	-4.75	0.01
108	SLU 62	1	30	4331	-0.61	0.96	0
108	SLU 63	-5	28	4328	-0.52	-4.75	0.01
108	SLU 64	0	16	3107	-0.33	0.42	0
108	SLU 65	-9	14	3103	-0.18	-9.11	0.02
108	SLU 66	0	16	3107	-0.33	0.42	0
108	SLU 67	-5	15	3104	-0.24	-5.3	0.01
108	SLU 68	-9	14	3103	-0.18	-9.11	0.02
108	SLU 69	0	16	3107	-0.33	0.42	0
108	SLU 70	-5	15	3104	-0.24	-5.3	0.01
108	SLU 71	0	16	3107	-0.33	0.42	0
108	SLU 72	-5	15	3104	-0.24	-5.3	0.01
108	SLU 73	-8	28	4414	-0.5	-8.58	0.02
108	SLU 74	1	30	4417	-0.65	0.95	0
108	SLU 75	-5	29	4415	-0.56	-4.77	0.01
108	SLU 76	-8	28	4414	-0.5	-8.58	0.02
108	SLU 77	1	30	4417	-0.65	0.95	0
108	SLU 78	-5	29	4415	-0.56	-4.77	0.01
108	SLU 79	1	30	4417	-0.65	0.95	0
108	SLU 80	-5	29	4415	-0.56	-4.77	0.01
108	SLU 81	1	36	4979	-0.78	1.17	0
108	SLU 82	-4	35	4977	-0.69	-4.54	0.01
108	SLU 83	1	36	4979	-0.78	1.17	0
108	SLU 84	-4	35	4977	-0.69	-4.54	0.01
108	SLE RA 1	0	11	2247	-0.22	0.28	0
108	SLE RA 2	-6	9	2245	-0.12	-6.08	0.01
108	SLE RA 3	0	11	2247	-0.22	0.28	0
108	SLE RA 4	-3	10	2246	-0.16	-3.54	0.01
108	SLE RA 5	-6	9	2245	-0.12	-6.08	0.01
108	SLE RA 6	0	11	2247	-0.22	0.28	0
108	SLE RA 7	-3	10	2246	-0.16	-3.54	0.01
108	SLE RA 8	0	11	2247	-0.22	0.28	0
108	SLE RA 9	-3	10	2246	-0.16	-3.54	0.01
108	SLE RA 10	-6	19	3118	-0.33	-5.73	0.01
108	SLE RA 11	1	20	3121	-0.43	0.63	0
108	SLE RA 12	-3	19	3119	-0.37	-3.18	0.01
108	SLE RA 13	-6	19	3118	-0.33	-5.73	0.01
108	SLE RA 14	1	20	3121	-0.43	0.63	0
108	SLE RA 15	-3	19	3119	-0.37	-3.18	0.01
108	SLE RA 16	1	20	3121	-0.43	0.63	0
108	SLE RA 17	-3	19	3119	-0.37	-3.18	0.01
108	SLE RA 18	1	24	3496	-0.52	0.78	0
108	SLE RA 19	-3	23	3494	-0.46	-3.03	0.01
108	SLE RA 20	1	24	3496	-0.52	0.78	0
108	SLE RA 21	-3	23	3494	-0.46	-3.03	0.01
108	SLE FR 1	0	11	2247	-0.22	0.28	0
108	SLE FR 2	-1	11	2247	-0.2	-1	0
108	SLE FR 3	0	11	2247	-0.22	0.28	0
108	SLE FR 4	-1	15	2621	-0.29	-0.84	0
108	SLE FR 5	0	15	2622	-0.31	0.43	0
108	SLE FR 6	0	18	2871	-0.37	0.53	0
108	SLE QP 1	0	11	2247	-0.22	0.28	0
108	SLE QP 2	0	15	2622	-0.31	0.43	0
108	SLD 1	36	-53	2619	10.07	39.15	-0.08
108	SLD 2	36	-53	2619	10.07	39.15	-0.08
108	SLD 3	34	163	2602	-14.66	37.69	-0.08
108	SLD 4	34	163	2602	-14.66	37.69	-0.08
108	SLD 5	14	-334	2646	40.32	14.26	-0.03
108	SLD 6	14	-334	2646	40.32	14.26	-0.03
108	SLD 7	8	388	2591	-42.13	9.39	-0.02
108	SLD 8	8	388	2591	-42.13	9.39	-0.02
108	SLD 9	-7	-358	2653	41.52	-8.54	0.02
108	SLD 10	-7	-358	2653	41.52	-8.54	0.02
108	SLD 11	-13	364	2597	-40.93	-13.41	0.03
108	SLD 12	-13	364	2597	-40.93	-13.41	0.03
108	SLD 13	-34	-133	2641	14.05	-36.84	0.07
108	SLD 14	-34	-133	2641	14.05	-36.84	0.07
108	SLD 15	-35	84	2624	-10.68	-38.3	0.08



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
108	SLD 16	-35	84	2624	-10.68	-38.3	0.08
108	SLV 1	110	-161	2615	26.49	120.2	-0.24
108	SLV 2	110	-161	2615	26.49	120.2	-0.24
108	SLV 3	105	380	2572	-36.74	116.28	-0.23
108	SLV 4	105	380	2572	-36.74	116.28	-0.23
108	SLV 5	40	-859	2686	103.62	42.31	-0.09
108	SLV 6	40	-859	2686	103.62	42.31	-0.09
108	SLV 7	25	946	2541	-107.13	29.23	-0.06
108	SLV 8	25	946	2541	-107.13	29.23	-0.06
108	SLV 9	-25	-916	2702	106.52	-28.38	0.05
108	SLV 10	-25	-916	2702	106.52	-28.38	0.05
108	SLV 11	-39	889	2558	-104.24	-41.46	0.09
108	SLV 12	-39	889	2558	-104.24	-41.46	0.09
108	SLV 13	-105	-350	2671	36.13	-115.42	0.23
108	SLV 14	-105	-350	2671	36.13	-115.42	0.23
108	SLV 15	-109	192	2628	-27.1	-119.35	0.24
108	SLV 16	-109	192	2628	-27.1	-119.35	0.24
109	SLU 1	0	-58	2074	2.29	-0.58	0
109	SLU 2	-2	-63	2096	2.49	-4.41	0
109	SLU 3	0	-58	2074	2.29	-0.58	0
109	SLU 4	-2	-61	2087	2.41	-2.88	0
109	SLU 5	-2	-63	2096	2.49	-4.41	0
109	SLU 6	0	-58	2074	2.29	-0.58	0
109	SLU 7	-2	-61	2087	2.41	-2.88	0
109	SLU 8	0	-58	2074	2.29	-0.58	0
109	SLU 9	-2	-61	2087	2.41	-2.88	0
109	SLU 10	-3	-50	2380	1.48	-5.1	0
109	SLU 11	-1	-45	2358	1.28	-1.27	0
109	SLU 12	-2	-48	2371	1.4	-3.57	0
109	SLU 13	-3	-50	2380	1.48	-5.1	0
109	SLU 14	-1	-45	2358	1.28	-1.27	0
109	SLU 15	-2	-48	2371	1.4	-3.57	0
109	SLU 16	-1	-45	2358	1.28	-1.27	0
109	SLU 17	-2	-48	2371	1.4	-3.57	0
109	SLU 18	-1	-39	2480	0.84	-1.56	0
109	SLU 19	-2	-42	2493	0.96	-3.86	0
109	SLU 20	-1	-39	2480	0.84	-1.56	0
109	SLU 21	-2	-42	2493	0.96	-3.86	0
109	SLU 22	0	-56	2245	2.02	-0.86	0
109	SLU 23	-3	-61	2267	2.22	-4.69	0
109	SLU 24	0	-56	2245	2.02	-0.86	0
109	SLU 25	-2	-59	2258	2.14	-3.16	0
109	SLU 26	-3	-61	2267	2.22	-4.69	0
109	SLU 27	0	-56	2245	2.02	-0.86	0
109	SLU 28	-2	-59	2258	2.14	-3.16	0
109	SLU 29	0	-56	2245	2.02	-0.86	0
109	SLU 30	-2	-59	2258	2.14	-3.16	0
109	SLU 31	-3	-47	2551	1.2	-5.38	0
109	SLU 32	-1	-43	2529	1	-1.55	0
109	SLU 33	-2	-45	2542	1.12	-3.84	0
109	SLU 34	-3	-47	2551	1.2	-5.38	0
109	SLU 35	-1	-43	2529	1	-1.55	0
109	SLU 36	-2	-45	2542	1.12	-3.84	0
109	SLU 37	-1	-43	2529	1	-1.55	0
109	SLU 38	-2	-45	2542	1.12	-3.84	0
109	SLU 39	-1	-37	2651	0.56	-1.84	0
109	SLU 40	-2	-40	2664	0.68	-4.14	0
109	SLU 41	-1	-37	2651	0.56	-1.84	0
109	SLU 42	-2	-40	2664	0.68	-4.14	0
109	SLU 43	0	-77	2638	3.08	-0.66	0
109	SLU 44	-2	-81	2659	3.28	-4.49	0
109	SLU 45	0	-77	2638	3.08	-0.66	0
109	SLU 46	-2	-79	2651	3.2	-2.95	0
109	SLU 47	-2	-81	2659	3.28	-4.49	0
109	SLU 48	0	-77	2638	3.08	-0.66	0
109	SLU 49	-2	-79	2651	3.2	-2.95	0
109	SLU 50	0	-77	2638	3.08	-0.66	0
109	SLU 51	-2	-79	2651	3.2	-2.95	0
109	SLU 52	-3	-68	2943	2.26	-5.17	0
109	SLU 53	-1	-63	2922	2.06	-1.35	0
109	SLU 54	-2	-66	2935	2.18	-3.64	0
109	SLU 55	-3	-68	2943	2.26	-5.17	0
109	SLU 56	-1	-63	2922	2.06	-1.35	0
109	SLU 57	-2	-66	2935	2.18	-3.64	0
109	SLU 58	-1	-63	2922	2.06	-1.35	0
109	SLU 59	-2	-66	2935	2.18	-3.64	0
109	SLU 60	-1	-58	3044	1.62	-1.64	0
109	SLU 61	-2	-60	3057	1.74	-3.94	0
109	SLU 62	-1	-58	3044	1.62	-1.64	0
109	SLU 63	-2	-60	3057	1.74	-3.94	0
109	SLU 64	0	-74	2809	2.8	-0.94	0
109	SLU 65	-3	-79	2831	3	-4.76	0
109	SLU 66	0	-74	2809	2.8	-0.94	0
109	SLU 67	-2	-77	2822	2.92	-3.23	0
109	SLU 68	-3	-79	2831	3	-4.76	0
109	SLU 69	0	-74	2809	2.8	-0.94	0
109	SLU 70	-2	-77	2822	2.92	-3.23	0
109	SLU 71	0	-74	2809	2.8	-0.94	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
109	SLU 72	-2	-77	2822	2.92	-3.23	0
109	SLU 73	-3	-66	3115	1.98	-5.45	0
109	SLU 74	-1	-61	3093	1.78	-1.63	0
109	SLU 75	-2	-64	3106	1.9	-3.92	0
109	SLU 76	-3	-66	3115	1.98	-5.45	0
109	SLU 77	-1	-61	3093	1.78	-1.63	0
109	SLU 78	-2	-64	3106	1.9	-3.92	0
109	SLU 79	-1	-61	3093	1.78	-1.63	0
109	SLU 80	-2	-64	3106	1.9	-3.92	0
109	SLU 81	-1	-55	3215	1.34	-1.92	0
109	SLU 82	-2	-58	3228	1.46	-4.22	0
109	SLU 83	-1	-55	3215	1.34	-1.92	0
109	SLU 84	-2	-58	3228	1.46	-4.22	0
109	SLE RA 1	0	-58	2123	2.21	-0.66	0
109	SLE RA 2	-2	-61	2138	2.35	-3.21	0
109	SLE RA 3	0	-58	2123	2.21	-0.66	0
109	SLE RA 4	-1	-60	2132	2.29	-2.19	0
109	SLE RA 5	-2	-61	2138	2.35	-3.21	0
109	SLE RA 6	0	-58	2123	2.21	-0.66	0
109	SLE RA 7	-1	-60	2132	2.29	-2.19	0
109	SLE RA 8	0	-58	2123	2.21	-0.66	0
109	SLE RA 9	-1	-60	2132	2.29	-2.19	0
109	SLE RA 10	-2	-52	2327	1.67	-3.67	0
109	SLE RA 11	-1	-49	2312	1.54	-1.12	0
109	SLE RA 12	-1	-51	2321	1.62	-2.65	0
109	SLE RA 13	-2	-52	2327	1.67	-3.67	0
109	SLE RA 14	-1	-49	2312	1.54	-1.12	0
109	SLE RA 15	-1	-51	2321	1.62	-2.65	0
109	SLE RA 16	-1	-49	2312	1.54	-1.12	0
109	SLE RA 17	-1	-51	2321	1.62	-2.65	0
109	SLE RA 18	-1	-45	2394	1.24	-1.32	0
109	SLE RA 19	-2	-47	2402	1.32	-2.85	0
109	SLE RA 20	-1	-45	2394	1.24	-1.32	0
109	SLE RA 21	-2	-47	2402	1.32	-2.85	0
109	SLE FR 1	0	-58	2123	2.21	-0.66	0
109	SLE FR 2	-1	-58	2126	2.24	-1.17	0
109	SLE FR 3	0	-58	2123	2.21	-0.66	0
109	SLE FR 4	-1	-54	2207	1.95	-1.37	0
109	SLE FR 5	0	-54	2204	1.92	-0.86	0
109	SLE FR 6	-1	-51	2258	1.73	-0.99	0
109	SLE QP 1	0	-58	2123	2.21	-0.66	0
109	SLE QP 2	0	-54	2204	1.92	-0.86	0
109	SLD 1	55	91	2085	-4.36	65.33	-0.01
109	SLD 2	55	91	2085	-4.36	65.33	-0.01
109	SLD 3	61	-66	2113	2.5	72.63	-0.02
109	SLD 4	61	-66	2113	2.5	72.63	-0.02
109	SLD 5	6	226	2127	-10.38	7.93	0
109	SLD 6	6	226	2127	-10.38	7.93	0
109	SLD 7	28	-294	2219	12.51	32.27	-0.01
109	SLD 8	28	-294	2219	12.51	32.27	-0.01
109	SLD 9	-29	187	2190	-8.66	-33.98	0.01
109	SLD 10	-29	187	2190	-8.66	-33.98	0.01
109	SLD 11	-7	-334	2282	14.22	-9.64	0
109	SLD 12	-7	-334	2282	14.22	-9.64	0
109	SLD 13	-62	-42	2296	1.34	-74.35	0.02
109	SLD 14	-62	-42	2296	1.34	-74.35	0.02
109	SLD 15	-56	-198	2323	8.21	-67.04	0.01
109	SLD 16	-56	-198	2323	8.21	-67.04	0.01
109	SLV 1	142	289	1921	-13	171.56	-0.03
109	SLV 2	142	289	1921	-13	171.56	-0.03
109	SLV 3	158	-79	1986	3.19	190.32	-0.04
109	SLV 4	158	-79	1986	3.19	190.32	-0.04
109	SLV 5	17	608	2022	-27.1	22.42	0.01
109	SLV 6	17	608	2022	-27.1	22.42	0.01
109	SLV 7	72	-620	2236	26.85	84.95	-0.03
109	SLV 8	72	-620	2236	26.85	84.95	-0.03
109	SLV 9	-73	512	2172	-23.01	-86.66	0.03
109	SLV 10	-73	512	2172	-23.01	-86.66	0.03
109	SLV 11	-18	-715	2387	30.95	-24.13	-0.01
109	SLV 12	-18	-715	2387	30.95	-24.13	-0.01
109	SLV 13	-159	-28	2423	0.66	-192.03	0.04
109	SLV 14	-159	-28	2423	0.66	-192.03	0.04
109	SLV 15	-143	-397	2487	16.85	-173.28	0.03
109	SLV 16	-143	-397	2487	16.85	-173.28	0.03
110	SLU 1	0	-153	1920	6.09	0.06	0
110	SLU 2	-7	-144	1889	5.78	-10.53	-0.01
110	SLU 3	0	-153	1920	6.09	0.06	0
110	SLU 4	-5	-147	1901	5.9	-6.3	-0.01
110	SLU 5	-7	-144	1889	5.78	-10.53	-0.01
110	SLU 6	0	-153	1920	6.09	0.06	0
110	SLU 7	-5	-147	1901	5.9	-6.3	-0.01
110	SLU 8	0	-153	1920	6.09	0.06	0
110	SLU 9	-5	-147	1901	5.9	-6.3	-0.01
110	SLU 10	-8	-215	2321	8.63	-10.65	-0.01
110	SLU 11	-1	-225	2352	8.94	-0.05	0
110	SLU 12	-5	-219	2333	8.76	-6.41	-0.01
110	SLU 13	-8	-215	2321	8.63	-10.65	-0.01
110	SLU 14	-1	-225	2352	8.94	-0.05	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
110	SLU 15	-5	-219	2333	8.76	-6.41	-0.01
110	SLU 16	-1	-225	2352	8.94	-0.05	0
110	SLU 17	-5	-219	2333	8.76	-6.41	-0.01
110	SLU 18	-1	-255	2537	10.17	-0.1	0
110	SLU 19	-5	-250	2519	9.98	-6.46	-0.01
110	SLU 20	-1	-255	2537	10.17	-0.1	0
110	SLU 21	-5	-250	2519	9.98	-6.46	-0.01
110	SLU 22	-1	-186	2146	7.42	0.02	0
110	SLU 23	-8	-177	2115	7.11	-10.57	-0.01
110	SLU 24	-1	-186	2146	7.42	0.02	0
110	SLU 25	-5	-181	2128	7.23	-6.33	-0.01
110	SLU 26	-8	-177	2115	7.11	-10.57	-0.01
110	SLU 27	-1	-186	2146	7.42	0.02	0
110	SLU 28	-5	-181	2128	7.23	-6.33	-0.01
110	SLU 29	-1	-186	2146	7.42	0.02	0
110	SLU 30	-5	-181	2128	7.23	-6.33	-0.01
110	SLU 31	-8	-249	2547	9.96	-10.69	-0.02
110	SLU 32	-1	-258	2578	10.27	-0.09	0
110	SLU 33	-5	-253	2560	10.09	-6.45	-0.01
110	SLU 34	-8	-249	2547	9.96	-10.69	-0.02
110	SLU 35	-1	-258	2578	10.27	-0.09	0
110	SLU 36	-5	-253	2560	10.09	-6.45	-0.01
110	SLU 37	-1	-258	2578	10.27	-0.09	0
110	SLU 38	-5	-253	2560	10.09	-6.45	-0.01
110	SLU 39	-1	-289	2764	11.5	-0.14	0
110	SLU 40	-6	-284	2745	11.31	-6.5	-0.01
110	SLU 41	-1	-289	2764	11.5	-0.14	0
110	SLU 42	-6	-284	2745	11.31	-6.5	-0.01
110	SLU 43	0	-187	2418	7.46	0.09	0
110	SLU 44	-7	-178	2387	7.15	-10.5	-0.01
110	SLU 45	0	-187	2418	7.46	0.09	0
110	SLU 46	-5	-182	2400	7.27	-6.27	-0.01
110	SLU 47	-7	-178	2387	7.15	-10.5	-0.01
110	SLU 48	0	-187	2418	7.46	0.09	0
110	SLU 49	-5	-182	2400	7.27	-6.27	-0.01
110	SLU 50	0	-187	2418	7.46	0.09	0
110	SLU 51	-5	-182	2400	7.27	-6.27	-0.01
110	SLU 52	-8	-250	2819	10	-10.62	-0.01
110	SLU 53	-1	-259	2850	10.31	-0.02	0
110	SLU 54	-5	-253	2832	10.13	-6.38	-0.01
110	SLU 55	-8	-250	2819	10	-10.62	-0.01
110	SLU 56	-1	-259	2850	10.31	-0.02	0
110	SLU 57	-5	-253	2832	10.13	-6.38	-0.01
110	SLU 58	-1	-259	2850	10.31	-0.02	0
110	SLU 59	-5	-253	2832	10.13	-6.38	-0.01
110	SLU 60	-1	-290	3036	11.54	-0.07	0
110	SLU 61	-5	-284	3017	11.35	-6.43	-0.01
110	SLU 62	-1	-290	3036	11.54	-0.07	0
110	SLU 63	-5	-284	3017	11.35	-6.43	-0.01
110	SLU 64	-1	-221	2645	8.79	0.05	0
110	SLU 65	-8	-212	2614	8.48	-10.54	-0.01
110	SLU 66	-1	-221	2645	8.79	0.05	0
110	SLU 67	-5	-215	2626	8.6	-6.3	-0.01
110	SLU 68	-8	-212	2614	8.48	-10.54	-0.01
110	SLU 69	-1	-221	2645	8.79	0.05	0
110	SLU 70	-5	-215	2626	8.6	-6.3	-0.01
110	SLU 71	-1	-221	2645	8.79	0.05	0
110	SLU 72	-5	-215	2626	8.6	-6.3	-0.01
110	SLU 73	-8	-283	3046	11.33	-10.65	-0.02
110	SLU 74	-1	-292	3077	11.64	-0.06	0
110	SLU 75	-5	-287	3058	11.46	-6.42	-0.01
110	SLU 76	-8	-283	3046	11.33	-10.65	-0.02
110	SLU 77	-1	-292	3077	11.64	-0.06	0
110	SLU 78	-5	-287	3058	11.46	-6.42	-0.01
110	SLU 79	-1	-292	3077	11.64	-0.06	0
110	SLU 80	-5	-287	3058	11.46	-6.42	-0.01
110	SLU 81	-1	-323	3262	12.87	-0.11	0
110	SLU 82	-6	-318	3243	12.68	-6.47	-0.01
110	SLU 83	-1	-323	3262	12.87	-0.11	0
110	SLU 84	-6	-318	3243	12.68	-6.47	-0.01
110	SLE RA 1	0	-162	1985	6.47	0.05	0
110	SLE RA 2	-5	-156	1964	6.26	-7.01	-0.01
110	SLE RA 3	0	-162	1985	6.47	0.05	0
110	SLE RA 4	-3	-159	1972	6.34	-4.19	-0.01
110	SLE RA 5	-5	-156	1964	6.26	-7.01	-0.01
110	SLE RA 6	0	-162	1985	6.47	0.05	0
110	SLE RA 7	-3	-159	1972	6.34	-4.19	-0.01
110	SLE RA 8	0	-162	1985	6.47	0.05	0
110	SLE RA 9	-3	-159	1972	6.34	-4.19	-0.01
110	SLE RA 10	-5	-204	2252	8.16	-7.09	-0.01
110	SLE RA 11	-1	-210	2273	8.37	-0.03	0
110	SLE RA 12	-4	-207	2260	8.25	-4.26	-0.01
110	SLE RA 13	-5	-204	2252	8.16	-7.09	-0.01
110	SLE RA 14	-1	-210	2273	8.37	-0.03	0
110	SLE RA 15	-4	-207	2260	8.25	-4.26	-0.01
110	SLE RA 16	-1	-210	2273	8.37	-0.03	0
110	SLE RA 17	-4	-207	2260	8.25	-4.26	-0.01
110	SLE RA 18	-1	-231	2396	9.19	-0.06	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
110	SLE RA 19	-4	-227	2384	9.06	-4.3	-0.01
110	SLE RA 20	-1	-231	2396	9.19	-0.06	0
110	SLE RA 21	-4	-227	2384	9.06	-4.3	-0.01
110	SLE FR 1	0	-162	1985	6.47	0.05	0
110	SLE FR 2	-1	-161	1980	6.43	-1.36	0
110	SLE FR 3	0	-162	1985	6.47	0.05	0
110	SLE FR 4	-1	-182	2104	7.24	-1.4	0
110	SLE FR 5	-1	-183	2108	7.28	0.02	0
110	SLE FR 6	-1	-196	2190	7.83	-0.01	0
110	SLE QP 1	0	-162	1985	6.47	0.05	0
110	SLE QP 2	-1	-183	2108	7.28	0.02	0
110	SLD 1	43	-174	2150	6.79	45.32	0.09
110	SLD 2	43	-174	2150	6.79	45.32	0.09
110	SLD 3	37	-314	2199	12.78	40.7	0.08
110	SLD 4	37	-314	2199	12.78	40.7	0.08
110	SLD 5	21	31	2047	-1.94	20.61	0.05
110	SLD 6	21	31	2047	-1.94	20.61	0.05
110	SLD 7	2	-433	2209	18.01	5.21	0
110	SLD 8	2	-433	2209	18.01	5.21	0
110	SLD 9	-3	68	2007	-3.44	-5.18	0
110	SLD 10	-3	68	2007	-3.44	-5.18	0
110	SLD 11	-22	-397	2169	16.51	-20.58	-0.05
110	SLD 12	-22	-397	2169	16.51	-20.58	-0.05
110	SLD 13	-38	-52	2017	1.79	-40.67	-0.08
110	SLD 14	-38	-52	2017	1.79	-40.67	-0.08
110	SLD 15	-44	-191	2066	7.77	-45.29	-0.09
110	SLD 16	-44	-191	2066	7.77	-45.29	-0.09
110	SLV 1	110	-162	2215	6.1	116.3	0.23
110	SLV 2	110	-162	2215	6.1	116.3	0.23
110	SLV 3	96	-491	2329	20.24	104.77	0.2
110	SLV 4	96	-491	2329	20.24	104.77	0.2
110	SLV 5	53	322	1967	-14.51	52.39	0.12
110	SLV 6	53	322	1967	-14.51	52.39	0.12
110	SLV 7	7	-774	2347	32.61	13.96	0
110	SLV 8	7	-774	2347	32.61	13.96	0
110	SLV 9	-9	409	1869	-18.04	-13.92	-0.01
110	SLV 10	-9	409	1869	-18.04	-13.92	-0.01
110	SLV 11	-55	-688	2249	29.07	-52.35	-0.13
110	SLV 12	-55	-688	2249	29.07	-52.35	-0.13
110	SLV 13	-97	126	1887	-5.67	-104.74	-0.2
110	SLV 14	-97	126	1887	-5.67	-104.74	-0.2
110	SLV 15	-111	-203	2001	8.46	-116.27	-0.24
110	SLV 16	-111	-203	2001	8.46	-116.27	-0.24
111	SLU 1	0	-104	2035	4.06	0.21	0
111	SLU 2	-8	-106	2031	4.11	-8.92	0.02
111	SLU 3	0	-104	2035	4.06	0.21	0
111	SLU 4	-5	-105	2033	4.09	-5.27	0.01
111	SLU 5	-8	-106	2031	4.11	-8.92	0.02
111	SLU 6	0	-104	2035	4.06	0.21	0
111	SLU 7	-5	-105	2033	4.09	-5.27	0.01
111	SLU 8	0	-104	2035	4.06	0.21	0
111	SLU 9	-5	-105	2033	4.09	-5.27	0.01
111	SLU 10	-8	-204	3311	7.87	-8.41	0.02
111	SLU 11	1	-202	3316	7.82	0.71	0
111	SLU 12	-5	-203	3313	7.85	-4.76	0.01
111	SLU 13	-8	-204	3311	7.87	-8.41	0.02
111	SLU 14	1	-202	3316	7.82	0.71	0
111	SLU 15	-5	-203	3313	7.85	-4.76	0.01
111	SLU 16	1	-202	3316	7.82	0.71	0
111	SLU 17	-5	-203	3313	7.85	-4.76	0.01
111	SLU 18	1	-244	3864	9.43	0.93	0
111	SLU 19	-4	-245	3862	9.46	-4.54	0.01
111	SLU 20	1	-244	3864	9.43	0.93	0
111	SLU 21	-4	-245	3862	9.46	-4.54	0.01
111	SLU 22	0	-147	2670	5.7	0.41	0
111	SLU 23	-8	-148	2666	5.75	-8.72	0.02
111	SLU 24	0	-147	2670	5.7	0.41	0
111	SLU 25	-5	-148	2668	5.73	-5.07	0.01
111	SLU 26	-8	-148	2666	5.75	-8.72	0.02
111	SLU 27	0	-147	2670	5.7	0.41	0
111	SLU 28	-5	-148	2668	5.73	-5.07	0.01
111	SLU 29	0	-147	2670	5.7	0.41	0
111	SLU 30	-5	-148	2668	5.73	-5.07	0.01
111	SLU 31	-8	-247	3946	9.51	-8.21	0.02
111	SLU 32	1	-245	3950	9.46	0.91	0
111	SLU 33	-4	-246	3948	9.49	-4.56	0.01
111	SLU 34	-8	-247	3946	9.51	-8.21	0.02
111	SLU 35	1	-245	3950	9.46	0.91	0
111	SLU 36	-4	-246	3948	9.49	-4.56	0.01
111	SLU 37	1	-245	3950	9.46	0.91	0
111	SLU 38	-4	-246	3948	9.49	-4.56	0.01
111	SLU 39	1	-287	4499	11.07	1.13	0
111	SLU 40	-4	-288	4496	11.1	-4.34	0.01
111	SLU 41	1	-287	4499	11.07	1.13	0
111	SLU 42	-4	-288	4496	11.1	-4.34	0.01
111	SLU 43	0	-121	2429	4.72	0.2	0
111	SLU 44	-8	-122	2424	4.77	-8.92	0.02
111	SLU 45	0	-121	2429	4.72	0.2	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
111	SLU 46	-5	-122	2426	4.75	-5.28	0.01
111	SLU 47	-8	-122	2424	4.77	-8.92	0.02
111	SLU 48	0	-121	2429	4.72	0.2	0
111	SLU 49	-5	-122	2426	4.75	-5.28	0.01
111	SLU 50	0	-121	2429	4.72	0.2	0
111	SLU 51	-5	-122	2426	4.75	-5.28	0.01
111	SLU 52	-8	-221	3704	8.53	-8.42	0.02
111	SLU 53	1	-219	3709	8.48	0.71	0
111	SLU 54	-5	-220	3706	8.51	-4.77	0.01
111	SLU 55	-8	-221	3704	8.53	-8.42	0.02
111	SLU 56	1	-219	3709	8.48	0.71	0
111	SLU 57	-5	-220	3706	8.51	-4.77	0.01
111	SLU 58	1	-219	3709	8.48	0.71	0
111	SLU 59	-5	-220	3706	8.51	-4.77	0.01
111	SLU 60	1	-261	4257	10.09	0.92	0
111	SLU 61	-4	-262	4255	10.12	-4.55	0.01
111	SLU 62	1	-261	4257	10.09	0.92	0
111	SLU 63	-4	-262	4255	10.12	-4.55	0.01
111	SLU 64	0	-163	3063	6.36	0.4	0
111	SLU 65	-8	-165	3059	6.41	-8.72	0.02
111	SLU 66	0	-163	3063	6.36	0.4	0
111	SLU 67	-5	-164	3061	6.39	-5.07	0.01
111	SLU 68	-8	-165	3059	6.41	-8.72	0.02
111	SLU 69	0	-163	3063	6.36	0.4	0
111	SLU 70	-5	-164	3061	6.39	-5.07	0.01
111	SLU 71	0	-163	3063	6.36	0.4	0
111	SLU 72	-5	-164	3061	6.39	-5.07	0.01
111	SLU 73	-8	-263	4339	10.17	-8.22	0.02
111	SLU 74	1	-261	4343	10.12	0.91	0
111	SLU 75	-4	-262	4341	10.15	-4.57	0.01
111	SLU 76	-8	-263	4339	10.17	-8.22	0.02
111	SLU 77	1	-261	4343	10.12	0.91	0
111	SLU 78	-4	-262	4341	10.15	-4.57	0.01
111	SLU 79	1	-261	4343	10.12	0.91	0
111	SLU 80	-4	-262	4341	10.15	-4.57	0.01
111	SLU 81	1	-303	4892	11.73	1.12	0
111	SLU 82	-4	-305	4889	11.76	-4.35	0.01
111	SLU 83	1	-303	4892	11.73	1.12	0
111	SLU 84	-4	-305	4889	11.76	-4.35	0.01
111	SLE RA 1	0	-116	2217	4.53	0.26	0
111	SLE RA 2	-5	-117	2214	4.56	-5.82	0.01
111	SLE RA 3	0	-116	2217	4.53	0.26	0
111	SLE RA 4	-3	-117	2215	4.55	-3.39	0.01
111	SLE RA 5	-5	-117	2214	4.56	-5.82	0.01
111	SLE RA 6	0	-116	2217	4.53	0.26	0
111	SLE RA 7	-3	-117	2215	4.55	-3.39	0.01
111	SLE RA 8	0	-116	2217	4.53	0.26	0
111	SLE RA 9	-3	-117	2215	4.55	-3.39	0.01
111	SLE RA 10	-5	-183	3067	7.07	-5.48	0.01
111	SLE RA 11	0	-182	3070	7.04	0.6	0
111	SLE RA 12	-3	-182	3069	7.06	-3.05	0.01
111	SLE RA 13	-5	-183	3067	7.07	-5.48	0.01
111	SLE RA 14	0	-182	3070	7.04	0.6	0
111	SLE RA 15	-3	-182	3069	7.06	-3.05	0.01
111	SLE RA 16	0	-182	3070	7.04	0.6	0
111	SLE RA 17	-3	-182	3069	7.06	-3.05	0.01
111	SLE RA 18	1	-210	3436	8.11	0.75	0
111	SLE RA 19	-3	-210	3434	8.13	-2.9	0.01
111	SLE RA 20	1	-210	3436	8.11	0.75	0
111	SLE RA 21	-3	-210	3434	8.13	-2.9	0.01
111	SLE FR 1	0	-116	2217	4.53	0.26	0
111	SLE FR 2	-1	-116	2216	4.54	-0.95	0
111	SLE FR 3	0	-116	2217	4.53	0.26	0
111	SLE FR 4	-1	-144	2582	5.61	-0.81	0
111	SLE FR 5	0	-144	2583	5.61	0.41	0
111	SLE FR 6	0	-163	2826	6.32	0.5	0
111	SLE QP 1	0	-116	2217	4.53	0.26	0
111	SLE QP 2	0	-144	2583	5.61	0.41	0
111	SLD 1	34	3	2580	-8.58	37.38	-0.07
111	SLD 2	34	3	2580	-8.58	37.38	-0.07
111	SLD 3	32	-211	2559	15.71	36.07	-0.07
111	SLD 4	32	-211	2559	15.71	36.07	-0.07
111	SLD 5	13	224	2615	-35.49	13.5	-0.03
111	SLD 6	13	224	2615	-35.49	13.5	-0.03
111	SLD 7	7	-489	2543	45.48	9.11	-0.01
111	SLD 8	7	-489	2543	45.48	9.11	-0.01
111	SLD 9	-7	200	2622	-34.26	-8.29	0.01
111	SLD 10	-7	200	2622	-34.26	-8.29	0.01
111	SLD 11	-12	-513	2551	46.7	-12.68	0.03
111	SLD 12	-12	-513	2551	46.7	-12.68	0.03
111	SLD 13	-32	-77	2606	-4.5	-35.25	0.07
111	SLD 14	-32	-77	2606	-4.5	-35.25	0.07
111	SLD 15	-33	-291	2585	19.79	-36.57	0.07
111	SLD 16	-33	-291	2585	19.79	-36.57	0.07
111	SLV 1	103	219	2578	-30.45	114.81	-0.22
111	SLV 2	103	219	2578	-30.45	114.81	-0.22
111	SLV 3	99	-316	2521	31.66	111.25	-0.21
111	SLV 4	99	-316	2521	31.66	111.25	-0.21



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
111	SLV 5	38	776	2667	-99.41	40.13	-0.08
111	SLV 6	38	776	2667	-99.41	40.13	-0.08
111	SLV 7	23	-1007	2478	107.62	28.26	-0.05
111	SLV 8	23	-1007	2478	107.62	28.26	-0.05
111	SLV 9	-23	718	2687	-96.41	-27.44	0.04
111	SLV 10	-23	718	2687	-96.41	-27.44	0.04
111	SLV 11	-37	-1064	2498	110.62	-39.31	0.08
111	SLV 12	-37	-1064	2498	110.62	-39.31	0.08
111	SLV 13	-98	27	2644	-20.45	-110.43	0.2
111	SLV 14	-98	27	2644	-20.45	-110.43	0.2
111	SLV 15	-103	-507	2588	41.66	-113.99	0.21
111	SLV 16	-103	-507	2588	41.66	-113.99	0.21
112	SLU 1	0	-91	2082	4.27	-0.53	0
112	SLU 2	-2	-95	2102	4.46	-4.35	0
112	SLU 3	0	-91	2082	4.27	-0.53	0
112	SLU 4	-2	-93	2094	4.39	-2.82	0
112	SLU 5	-2	-95	2102	4.46	-4.35	0
112	SLU 6	0	-91	2082	4.27	-0.53	0
112	SLU 7	-2	-93	2094	4.39	-2.82	0
112	SLU 8	0	-91	2082	4.27	-0.53	0
112	SLU 9	-2	-93	2094	4.39	-2.82	0
112	SLU 10	-3	-97	2407	5.15	-4.97	0
112	SLU 11	-1	-93	2386	4.96	-1.15	0
112	SLU 12	-2	-96	2399	5.07	-3.44	0
112	SLU 13	-3	-97	2407	5.15	-4.97	0
112	SLU 14	-1	-93	2386	4.96	-1.15	0
112	SLU 15	-2	-96	2399	5.07	-3.44	0
112	SLU 16	-1	-93	2386	4.96	-1.15	0
112	SLU 17	-2	-96	2399	5.07	-3.44	0
112	SLU 18	-1	-94	2517	5.26	-1.42	0
112	SLU 19	-2	-97	2529	5.37	-3.71	0
112	SLU 20	-1	-94	2517	5.26	-1.42	0
112	SLU 21	-2	-97	2529	5.37	-3.71	0
112	SLU 22	0	-96	2261	4.74	-0.78	0
112	SLU 23	-2	-101	2281	4.93	-4.6	0
112	SLU 24	0	-96	2261	4.74	-0.78	0
112	SLU 25	-2	-99	2273	4.85	-3.07	0
112	SLU 26	-2	-101	2281	4.93	-4.6	0
112	SLU 27	0	-96	2261	4.74	-0.78	0
112	SLU 28	-2	-99	2273	4.85	-3.07	0
112	SLU 29	0	-96	2261	4.74	-0.78	0
112	SLU 30	-2	-99	2273	4.85	-3.07	0
112	SLU 31	-3	-103	2585	5.61	-5.23	0
112	SLU 32	-1	-98	2565	5.43	-1.4	0
112	SLU 33	-2	-101	2577	5.54	-3.7	0
112	SLU 34	-3	-103	2585	5.61	-5.23	0
112	SLU 35	-1	-98	2565	5.43	-1.4	0
112	SLU 36	-2	-101	2577	5.54	-3.7	0
112	SLU 37	-1	-98	2565	5.43	-1.4	0
112	SLU 38	-2	-101	2577	5.54	-3.7	0
112	SLU 39	-1	-99	2695	5.72	-1.67	0
112	SLU 40	-2	-102	2708	5.83	-3.96	0
112	SLU 41	-1	-99	2695	5.72	-1.67	0
112	SLU 42	-2	-102	2708	5.83	-3.96	0
112	SLU 43	0	-116	2646	5.4	-0.6	0
112	SLU 44	-2	-120	2666	5.58	-4.42	0
112	SLU 45	0	-116	2646	5.4	-0.6	0
112	SLU 46	-2	-119	2658	5.51	-2.89	0
112	SLU 47	-2	-120	2666	5.58	-4.42	0
112	SLU 48	0	-116	2646	5.4	-0.6	0
112	SLU 49	-2	-119	2658	5.51	-2.89	0
112	SLU 50	0	-116	2646	5.4	-0.6	0
112	SLU 51	-2	-119	2658	5.51	-2.89	0
112	SLU 52	-3	-123	2970	6.27	-5.05	0
112	SLU 53	-1	-118	2950	6.08	-1.22	0
112	SLU 54	-2	-121	2962	6.2	-3.52	0
112	SLU 55	-3	-123	2970	6.27	-5.05	0
112	SLU 56	-1	-118	2950	6.08	-1.22	0
112	SLU 57	-2	-121	2962	6.2	-3.52	0
112	SLU 58	-1	-118	2950	6.08	-1.22	0
112	SLU 59	-2	-121	2962	6.2	-3.52	0
112	SLU 60	-1	-119	3080	6.38	-1.49	0
112	SLU 61	-2	-122	3092	6.49	-3.78	0
112	SLU 62	-1	-119	3080	6.38	-1.49	0
112	SLU 63	-2	-122	3092	6.49	-3.78	0
112	SLU 64	0	-121	2824	5.86	-0.85	0
112	SLU 65	-3	-126	2845	6.05	-4.68	0
112	SLU 66	0	-121	2824	5.86	-0.85	0
112	SLU 67	-2	-124	2836	5.97	-3.15	0
112	SLU 68	-3	-126	2845	6.05	-4.68	0
112	SLU 69	0	-121	2824	5.86	-0.85	0
112	SLU 70	-2	-124	2836	5.97	-3.15	0
112	SLU 71	0	-121	2824	5.86	-0.85	0
112	SLU 72	-2	-124	2836	5.97	-3.15	0
112	SLU 73	-3	-128	3149	6.74	-5.3	0
112	SLU 74	-1	-124	3128	6.55	-1.47	0
112	SLU 75	-2	-126	3141	6.66	-3.77	0
112	SLU 76	-3	-128	3149	6.74	-5.3	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
112	SLU 77	-1	-124	3128	6.55	-1.47	0
112	SLU 78	-2	-126	3141	6.66	-3.77	0
112	SLU 79	-1	-124	3128	6.55	-1.47	0
112	SLU 80	-2	-126	3141	6.66	-3.77	0
112	SLU 81	-1	-125	3259	6.84	-1.74	0
112	SLU 82	-2	-127	3271	6.96	-4.04	0
112	SLU 83	-1	-125	3259	6.84	-1.74	0
112	SLU 84	-2	-127	3271	6.96	-4.04	0
112	SLE RA 1	0	-92	2133	4.41	-0.6	0
112	SLE RA 2	-2	-95	2147	4.53	-3.15	0
112	SLE RA 3	0	-92	2133	4.41	-0.6	0
112	SLE RA 4	-1	-94	2141	4.48	-2.13	0
112	SLE RA 5	-2	-95	2147	4.53	-3.15	0
112	SLE RA 6	0	-92	2133	4.41	-0.6	0
112	SLE RA 7	-1	-94	2141	4.48	-2.13	0
112	SLE RA 8	0	-92	2133	4.41	-0.6	0
112	SLE RA 9	-1	-94	2141	4.48	-2.13	0
112	SLE RA 10	-2	-97	2350	4.99	-3.56	0
112	SLE RA 11	-1	-94	2336	4.86	-1.01	0
112	SLE RA 12	-1	-96	2344	4.94	-2.54	0
112	SLE RA 13	-2	-97	2350	4.99	-3.56	0
112	SLE RA 14	-1	-94	2336	4.86	-1.01	0
112	SLE RA 15	-1	-96	2344	4.94	-2.54	0
112	SLE RA 16	-1	-94	2336	4.86	-1.01	0
112	SLE RA 17	-1	-96	2344	4.94	-2.54	0
112	SLE RA 18	-1	-94	2423	5.06	-1.19	0
112	SLE RA 19	-1	-96	2431	5.14	-2.72	0
112	SLE RA 20	-1	-94	2423	5.06	-1.19	0
112	SLE RA 21	-1	-96	2431	5.14	-2.72	0
112	SLE FR 1	0	-92	2133	4.41	-0.6	0
112	SLE FR 2	-1	-93	2136	4.43	-1.11	0
112	SLE FR 3	0	-92	2133	4.41	-0.6	0
112	SLE FR 4	-1	-93	2223	4.63	-1.29	0
112	SLE FR 5	0	-93	2220	4.6	-0.78	0
112	SLE FR 6	0	-93	2278	4.73	-0.9	0
112	SLE QP 1	0	-92	2133	4.41	-0.6	0
112	SLE QP 2	0	-93	2220	4.6	-0.78	0
112	SLD 1	54	52	2106	-1.73	64.31	-0.01
112	SLD 2	54	52	2106	-1.73	64.31	-0.01
112	SLD 3	60	-103	2136	5.1	71.41	-0.02
112	SLD 4	60	-103	2136	5.1	71.41	-0.02
112	SLD 5	6	187	2140	-7.65	7.98	0
112	SLD 6	6	187	2140	-7.65	7.98	0
112	SLD 7	27	-332	2240	15.11	31.65	-0.01
112	SLD 8	27	-332	2240	15.11	31.65	-0.01
112	SLD 9	-28	146	2200	-5.9	-33.2	0.01
112	SLD 10	-28	146	2200	-5.9	-33.2	0.01
112	SLD 11	-7	-372	2300	16.86	-9.54	0
112	SLD 12	-7	-372	2300	16.86	-9.54	0
112	SLD 13	-61	-83	2305	4.11	-72.97	0.02
112	SLD 14	-61	-83	2305	4.11	-72.97	0.02
112	SLD 15	-55	-238	2335	10.93	-65.87	0.01
112	SLD 16	-55	-238	2335	10.93	-65.87	0.01
112	SLV 1	139	252	1947	-10.45	168.84	-0.03
112	SLV 2	139	252	1947	-10.45	168.84	-0.03
112	SLV 3	155	-115	2017	5.65	187.08	-0.04
112	SLV 4	155	-115	2017	5.65	187.08	-0.04
112	SLV 5	17	567	2032	-24.32	22.45	0
112	SLV 6	17	567	2032	-24.32	22.45	0
112	SLV 7	71	-656	2266	29.33	83.24	-0.02
112	SLV 8	71	-656	2266	29.33	83.24	-0.02
112	SLV 9	-71	470	2175	-20.12	-84.79	0.02
112	SLV 10	-71	470	2175	-20.12	-84.79	0.02
112	SLV 11	-18	-753	2408	33.53	-24	0
112	SLV 12	-18	-753	2408	33.53	-24	0
112	SLV 13	-156	-71	2423	3.56	-188.63	0.04
112	SLV 14	-156	-71	2423	3.56	-188.63	0.04
112	SLV 15	-140	-438	2493	19.65	-170.39	0.03
112	SLV 16	-140	-438	2493	19.65	-170.39	0.03
113	SLU 1	0	-152	1882	6.63	0.11	0
113	SLU 2	-11	-144	1856	6.26	-12.77	-0.03
113	SLU 3	0	-152	1882	6.63	0.11	0
113	SLU 4	-7	-148	1866	6.41	-7.62	-0.02
113	SLU 5	-11	-144	1856	6.26	-12.77	-0.03
113	SLU 6	0	-152	1882	6.63	0.11	0
113	SLU 7	-7	-148	1866	6.41	-7.62	-0.02
113	SLU 8	0	-152	1882	6.63	0.11	0
113	SLU 9	-7	-148	1866	6.41	-7.62	-0.02
113	SLU 10	-11	-217	2261	9.32	-12.81	-0.03
113	SLU 11	-1	-225	2287	9.69	0.07	0
113	SLU 12	-7	-220	2271	9.47	-7.66	-0.02
113	SLU 13	-11	-217	2261	9.32	-12.81	-0.03
113	SLU 14	-1	-225	2287	9.69	0.07	0
113	SLU 15	-7	-220	2271	9.47	-7.66	-0.02
113	SLU 16	-1	-225	2287	9.69	0.07	0
113	SLU 17	-7	-220	2271	9.47	-7.66	-0.02
113	SLU 18	-1	-256	2461	11	0.05	0
113	SLU 19	-7	-251	2445	10.78	-7.68	-0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
113	SLU 20	-1	-256	2461	11	0.05	0
113	SLU 21	-7	-251	2445	10.78	-7.68	-0.02
113	SLU 22	0	-187	2096	8.11	0.1	0
113	SLU 23	-11	-179	2069	7.74	-12.78	-0.03
113	SLU 24	0	-187	2096	8.11	0.1	0
113	SLU 25	-7	-182	2080	7.89	-7.63	-0.02
113	SLU 26	-11	-179	2069	7.74	-12.78	-0.03
113	SLU 27	0	-187	2096	8.11	0.1	0
113	SLU 28	-7	-182	2080	7.89	-7.63	-0.02
113	SLU 29	0	-187	2096	8.11	0.1	0
113	SLU 30	-7	-182	2080	7.89	-7.63	-0.02
113	SLU 31	-11	-251	2474	10.8	-12.82	-0.03
113	SLU 32	-1	-259	2501	11.17	0.06	0
113	SLU 33	-7	-255	2485	10.95	-7.67	-0.02
113	SLU 34	-11	-251	2474	10.8	-12.82	-0.03
113	SLU 35	-1	-259	2501	11.17	0.06	0
113	SLU 36	-7	-255	2485	10.95	-7.67	-0.02
113	SLU 37	-1	-259	2501	11.17	0.06	0
113	SLU 38	-7	-255	2485	10.95	-7.67	-0.02
113	SLU 39	-1	-290	2674	12.48	0.04	0
113	SLU 40	-7	-286	2658	12.26	-7.69	-0.02
113	SLU 41	-1	-290	2674	12.48	0.04	0
113	SLU 42	-7	-286	2658	12.26	-7.69	-0.02
113	SLU 43	0	-186	2374	8.12	0.15	0
113	SLU 44	-11	-178	2347	7.74	-12.73	-0.03
113	SLU 45	0	-186	2374	8.12	0.15	0
113	SLU 46	-7	-181	2358	7.89	-7.58	-0.02
113	SLU 47	-11	-178	2347	7.74	-12.73	-0.03
113	SLU 48	0	-186	2374	8.12	0.15	0
113	SLU 49	-7	-181	2358	7.89	-7.58	-0.02
113	SLU 50	0	-186	2374	8.12	0.15	0
113	SLU 51	-7	-181	2358	7.89	-7.58	-0.02
113	SLU 52	-11	-250	2752	10.8	-12.78	-0.03
113	SLU 53	-1	-258	2779	11.18	0.11	0
113	SLU 54	-7	-254	2763	10.95	-7.62	-0.02
113	SLU 55	-11	-250	2752	10.8	-12.78	-0.03
113	SLU 56	-1	-258	2779	11.18	0.11	0
113	SLU 57	-7	-254	2763	10.95	-7.62	-0.02
113	SLU 58	-1	-258	2779	11.18	0.11	0
113	SLU 59	-7	-254	2763	10.95	-7.62	-0.02
113	SLU 60	-1	-289	2952	12.49	0.09	0
113	SLU 61	-7	-285	2936	12.27	-7.64	-0.02
113	SLU 62	-1	-289	2952	12.49	0.09	0
113	SLU 63	-7	-285	2936	12.27	-7.64	-0.02
113	SLU 64	0	-221	2587	9.59	0.14	0
113	SLU 65	-11	-213	2561	9.22	-12.74	-0.03
113	SLU 66	0	-221	2587	9.59	0.14	0
113	SLU 67	-7	-216	2571	9.37	-7.59	-0.02
113	SLU 68	-11	-213	2561	9.22	-12.74	-0.03
113	SLU 69	0	-221	2587	9.59	0.14	0
113	SLU 70	-7	-216	2571	9.37	-7.59	-0.02
113	SLU 71	0	-221	2587	9.59	0.14	0
113	SLU 72	-7	-216	2571	9.37	-7.59	-0.02
113	SLU 73	-11	-285	2965	12.28	-12.79	-0.03
113	SLU 74	-1	-293	2992	12.65	0.1	0
113	SLU 75	-7	-288	2976	12.43	-7.63	-0.02
113	SLU 76	-11	-285	2965	12.28	-12.79	-0.03
113	SLU 77	-1	-293	2992	12.65	0.1	0
113	SLU 78	-7	-288	2976	12.43	-7.63	-0.02
113	SLU 79	-1	-293	2992	12.65	0.1	0
113	SLU 80	-7	-288	2976	12.43	-7.63	-0.02
113	SLU 81	-1	-324	3166	13.96	0.08	0
113	SLU 82	-7	-319	3150	13.74	-7.65	-0.02
113	SLU 83	-1	-324	3166	13.96	0.08	0
113	SLU 84	-7	-319	3150	13.74	-7.65	-0.02
113	SLE RA 1	0	-162	1943	7.05	0.11	0
113	SLE RA 2	-7	-157	1926	6.81	-8.48	-0.02
113	SLE RA 3	0	-162	1943	7.05	0.11	0
113	SLE RA 4	-5	-159	1933	6.91	-5.04	-0.01
113	SLE RA 5	-7	-157	1926	6.81	-8.48	-0.02
113	SLE RA 6	0	-162	1943	7.05	0.11	0
113	SLE RA 7	-5	-159	1933	6.91	-5.04	-0.01
113	SLE RA 8	0	-162	1943	7.05	0.11	0
113	SLE RA 9	-5	-159	1933	6.91	-5.04	-0.01
113	SLE RA 10	-8	-205	2195	8.85	-8.51	-0.02
113	SLE RA 11	0	-210	2213	9.09	0.08	0
113	SLE RA 12	-5	-207	2203	8.95	-5.07	-0.01
113	SLE RA 13	-8	-205	2195	8.85	-8.51	-0.02
113	SLE RA 14	0	-210	2213	9.09	0.08	0
113	SLE RA 15	-5	-207	2203	8.95	-5.07	-0.01
113	SLE RA 16	0	-210	2213	9.09	0.08	0
113	SLE RA 17	-5	-207	2203	8.95	-5.07	-0.01
113	SLE RA 18	-1	-231	2329	9.97	0.07	0
113	SLE RA 19	-5	-228	2318	9.82	-5.08	-0.01
113	SLE RA 20	-1	-231	2329	9.97	0.07	0
113	SLE RA 21	-5	-228	2318	9.82	-5.08	-0.01
113	SLE FR 1	0	-162	1943	7.05	0.11	0
113	SLE FR 2	-2	-161	1940	7	-1.61	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
113	SLE FR 3	0	-162	1943	7.05	0.11	0
113	SLE FR 4	-2	-182	2055	7.88	-1.62	-0.01
113	SLE FR 5	0	-183	2059	7.93	0.1	0
113	SLE FR 6	0	-197	2136	8.51	0.09	0
113	SLE QP 1	0	-162	1943	7.05	0.11	0
113	SLE QP 2	0	-183	2059	7.93	0.1	0
113	SLD 1	54	-174	2102	7.52	52.78	0.16
113	SLD 2	54	-174	2102	7.52	52.78	0.16
113	SLD 3	49	-314	2148	13.51	48.07	0.14
113	SLD 4	49	-314	2148	13.51	48.07	0.14
113	SLD 5	24	32	2002	-1.28	23.04	0.07
113	SLD 6	24	32	2002	-1.28	23.04	0.07
113	SLD 7	7	-434	2156	18.69	7.35	0.02
113	SLD 8	7	-434	2156	18.69	7.35	0.02
113	SLD 9	-7	69	1962	-2.83	-7.15	-0.02
113	SLD 10	-7	69	1962	-2.83	-7.15	-0.02
113	SLD 11	-24	-398	2116	17.14	-22.85	-0.07
113	SLD 12	-24	-398	2116	17.14	-22.85	-0.07
113	SLD 13	-49	-52	1970	2.35	-47.88	-0.15
113	SLD 14	-49	-52	1970	2.35	-47.88	-0.15
113	SLD 15	-54	-192	2016	8.34	-52.58	-0.16
113	SLD 16	-54	-192	2016	8.34	-52.58	-0.16
113	SLV 1	138	-161	2165	6.95	135.5	0.41
113	SLV 2	138	-161	2165	6.95	135.5	0.41
113	SLV 3	125	-491	2273	21.1	123.6	0.37
113	SLV 4	125	-491	2273	21.1	123.6	0.37
113	SLV 5	61	325	1927	-13.83	58.76	0.18
113	SLV 6	61	325	1927	-13.83	58.76	0.18
113	SLV 7	18	-777	2287	33.34	19.1	0.05
113	SLV 8	18	-777	2287	33.34	19.1	0.05
113	SLV 9	-18	411	1831	-17.48	-18.91	-0.05
113	SLV 10	-18	411	1831	-17.48	-18.91	-0.05
113	SLV 11	-61	-691	2191	29.69	-58.57	-0.19
113	SLV 12	-61	-691	2191	29.69	-58.57	-0.19
113	SLV 13	-126	126	1845	-5.24	-123.4	-0.37
113	SLV 14	-126	126	1845	-5.24	-123.4	-0.37
113	SLV 15	-139	-205	1953	8.91	-135.3	-0.41
113	SLV 16	-139	-205	1953	8.91	-135.3	-0.41
114	SLU 1	0	-198	1941	7.47	0.18	0
114	SLU 2	-7	-200	1937	7.57	-7.76	0.01
114	SLU 3	0	-198	1941	7.47	0.18	0
114	SLU 4	-4	-200	1939	7.53	-4.58	0.01
114	SLU 5	-7	-200	1937	7.57	-7.76	0.01
114	SLU 6	0	-198	1941	7.47	0.18	0
114	SLU 7	-4	-200	1939	7.53	-4.58	0.01
114	SLU 8	0	-198	1941	7.47	0.18	0
114	SLU 9	-4	-200	1939	7.53	-4.58	0.01
114	SLU 10	-6	-390	3112	14.58	-7.31	0.01
114	SLU 11	0	-388	3116	14.48	0.62	0
114	SLU 12	-4	-389	3114	14.54	-4.14	0.01
114	SLU 13	-6	-390	3112	14.58	-7.31	0.01
114	SLU 14	0	-388	3116	14.48	0.62	0
114	SLU 15	-4	-389	3114	14.54	-4.14	0.01
114	SLU 16	0	-388	3116	14.48	0.62	0
114	SLU 17	-4	-389	3114	14.54	-4.14	0.01
114	SLU 18	1	-469	3620	17.48	0.81	0
114	SLU 19	-4	-470	3617	17.54	-3.95	0.01
114	SLU 20	1	-469	3620	17.48	0.81	0
114	SLU 21	-4	-470	3617	17.54	-3.95	0.01
114	SLU 22	0	-282	2530	10.59	0.36	0
114	SLU 23	-7	-284	2526	10.69	-7.58	0.01
114	SLU 24	0	-282	2530	10.59	0.36	0
114	SLU 25	-4	-283	2528	10.65	-4.41	0.01
114	SLU 26	-7	-284	2526	10.69	-7.58	0.01
114	SLU 27	0	-282	2530	10.59	0.36	0
114	SLU 28	-4	-283	2528	10.65	-4.41	0.01
114	SLU 29	0	-282	2530	10.59	0.36	0
114	SLU 30	-4	-283	2528	10.65	-4.41	0.01
114	SLU 31	-6	-473	3701	17.7	-7.14	0.01
114	SLU 32	1	-471	3705	17.6	0.8	0
114	SLU 33	-4	-473	3703	17.66	-3.96	0.01
114	SLU 34	-6	-473	3701	17.7	-7.14	0.01
114	SLU 35	1	-471	3705	17.6	0.8	0
114	SLU 36	-4	-473	3703	17.66	-3.96	0.01
114	SLU 37	1	-471	3705	17.6	0.8	0
114	SLU 38	-4	-473	3703	17.66	-3.96	0.01
114	SLU 39	1	-553	4209	20.6	0.99	0
114	SLU 40	-3	-554	4207	20.66	-3.77	0.01
114	SLU 41	1	-553	4209	20.6	0.99	0
114	SLU 42	-3	-554	4207	20.66	-3.77	0.01
114	SLU 43	0	-229	2322	8.64	0.17	0
114	SLU 44	-7	-231	2318	8.74	-7.76	0.01
114	SLU 45	0	-229	2322	8.64	0.17	0
114	SLU 46	-4	-230	2319	8.7	-4.59	0.01
114	SLU 47	-7	-231	2318	8.74	-7.76	0.01
114	SLU 48	0	-229	2322	8.64	0.17	0
114	SLU 49	-4	-230	2319	8.7	-4.59	0.01
114	SLU 50	0	-229	2322	8.64	0.17	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
114	SLU 51	-4	-230	2319	8.7	-4.59	0.01
114	SLU 52	-6	-420	3493	15.75	-7.32	0.01
114	SLU 53	0	-418	3497	15.65	0.62	0
114	SLU 54	-4	-419	3494	15.71	-4.15	0.01
114	SLU 55	-6	-420	3493	15.75	-7.32	0.01
114	SLU 56	0	-418	3497	15.65	0.62	0
114	SLU 57	-4	-419	3494	15.71	-4.15	0.01
114	SLU 58	0	-418	3497	15.65	0.62	0
114	SLU 59	-4	-419	3494	15.71	-4.15	0.01
114	SLU 60	1	-499	4000	18.65	0.81	0
114	SLU 61	-4	-501	3998	18.71	-3.96	0.01
114	SLU 62	1	-499	4000	18.65	0.81	0
114	SLU 63	-4	-501	3998	18.71	-3.96	0.01
114	SLU 64	0	-313	2911	11.76	0.35	0
114	SLU 65	-7	-315	2907	11.86	-7.59	0.01
114	SLU 66	0	-313	2911	11.76	0.35	0
114	SLU 67	-4	-314	2908	11.82	-4.41	0.01
114	SLU 68	-7	-315	2907	11.86	-7.59	0.01
114	SLU 69	0	-313	2911	11.76	0.35	0
114	SLU 70	-4	-314	2908	11.82	-4.41	0.01
114	SLU 71	0	-313	2911	11.76	0.35	0
114	SLU 72	-4	-314	2908	11.82	-4.41	0.01
114	SLU 73	-6	-504	4082	18.87	-7.15	0.01
114	SLU 74	1	-502	4086	18.77	0.79	0
114	SLU 75	-4	-503	4083	18.83	-3.97	0.01
114	SLU 76	-6	-504	4082	18.87	-7.15	0.01
114	SLU 77	1	-502	4086	18.77	0.79	0
114	SLU 78	-4	-503	4083	18.83	-3.97	0.01
114	SLU 79	1	-502	4086	18.77	0.79	0
114	SLU 80	-4	-503	4083	18.83	-3.97	0.01
114	SLU 81	1	-583	4589	21.77	0.98	0
114	SLU 82	-3	-584	4587	21.83	-3.78	0.01
114	SLU 83	1	-583	4589	21.77	0.98	0
114	SLU 84	-3	-584	4587	21.83	-3.78	0.01
114	SLE RA 1	0	-222	2110	8.36	0.23	0
114	SLE RA 2	-4	-224	2107	8.43	-5.06	0.01
114	SLE RA 3	0	-222	2110	8.36	0.23	0
114	SLE RA 4	-3	-223	2108	8.4	-2.95	0
114	SLE RA 5	-4	-224	2107	8.43	-5.06	0.01
114	SLE RA 6	0	-222	2110	8.36	0.23	0
114	SLE RA 7	-3	-223	2108	8.4	-2.95	0
114	SLE RA 8	0	-222	2110	8.36	0.23	0
114	SLE RA 9	-3	-223	2108	8.4	-2.95	0
114	SLE RA 10	-4	-350	2890	13.1	-4.77	0.01
114	SLE RA 11	0	-348	2893	13.03	0.53	0
114	SLE RA 12	-2	-349	2891	13.07	-2.65	0
114	SLE RA 13	-4	-350	2890	13.1	-4.77	0.01
114	SLE RA 14	0	-348	2893	13.03	0.53	0
114	SLE RA 15	-2	-349	2891	13.07	-2.65	0
114	SLE RA 16	0	-348	2893	13.03	0.53	0
114	SLE RA 17	-2	-349	2891	13.07	-2.65	0
114	SLE RA 18	0	-402	3229	15.04	0.65	0
114	SLE RA 19	-2	-403	3227	15.08	-2.52	0
114	SLE RA 20	0	-402	3229	15.04	0.65	0
114	SLE RA 21	-2	-403	3227	15.08	-2.52	0
114	SLE FR 1	0	-222	2110	8.36	0.23	0
114	SLE FR 2	-1	-223	2109	8.37	-0.83	0
114	SLE FR 3	0	-222	2110	8.36	0.23	0
114	SLE FR 4	-1	-277	2445	10.38	-0.7	0
114	SLE FR 5	0	-276	2445	10.36	0.36	0
114	SLE FR 6	0	-312	2669	11.7	0.44	0
114	SLE QP 1	0	-222	2110	8.36	0.23	0
114	SLE QP 2	0	-276	2445	10.36	0.36	0
114	SLD 1	27	-336	2441	19.52	33.07	-0.05
114	SLD 2	27	-336	2441	19.52	33.07	-0.05
114	SLD 3	28	-138	2421	-2.66	31.74	-0.05
114	SLD 4	28	-138	2421	-2.66	31.74	-0.05
114	SLD 5	5	-594	2474	46.75	12.19	-0.01
114	SLD 6	5	-594	2474	46.75	12.19	-0.01
114	SLD 7	11	65	2408	-27.18	7.75	-0.02
114	SLD 8	11	65	2408	-27.18	7.75	-0.02
114	SLD 9	-11	-617	2482	47.91	-7.04	0.02
114	SLD 10	-11	-617	2482	47.91	-7.04	0.02
114	SLD 11	-5	41	2417	-26.02	-11.47	0.01
114	SLD 12	-5	41	2417	-26.02	-11.47	0.01
114	SLD 13	-28	-415	2470	23.39	-31.02	0.05
114	SLD 14	-28	-415	2470	23.39	-31.02	0.05
114	SLD 15	-26	-217	2450	1.21	-32.35	0.05
114	SLD 16	-26	-217	2450	1.21	-32.35	0.05
114	SLV 1	82	-428	2435	34.03	101.51	-0.15
114	SLV 2	82	-428	2435	34.03	101.51	-0.15
114	SLV 3	87	63	2383	-22.62	97.95	-0.15
114	SLV 4	87	63	2383	-22.62	97.95	-0.15
114	SLV 5	18	-1066	2521	103.38	36.1	-0.03
114	SLV 6	18	-1066	2521	103.38	36.1	-0.03
114	SLV 7	33	570	2348	-85.45	24.24	-0.06
114	SLV 8	33	570	2348	-85.45	24.24	-0.06
114	SLV 9	-33	-1122	2543	106.18	-23.53	0.06



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
114	SLV 10	-33	-1122	2543	106.18	-23.53	0.06
114	SLV 11	-17	514	2369	-82.66	-35.38	0.03
114	SLV 12	-17	514	2369	-82.66	-35.38	0.03
114	SLV 13	-86	-615	2508	43.35	-97.24	0.15
114	SLV 14	-86	-615	2508	43.35	-97.24	0.15
114	SLV 15	-81	-124	2456	-13.3	-100.79	0.14
114	SLV 16	-81	-124	2456	-13.3	-100.79	0.14
115	SLU 1	0	-115	2088	4.75	-0.48	0
115	SLU 2	-2	-119	2107	4.91	-4.09	0
115	SLU 3	0	-115	2088	4.75	-0.48	0
115	SLU 4	-1	-117	2100	4.85	-2.64	0
115	SLU 5	-2	-119	2107	4.91	-4.09	0
115	SLU 6	0	-115	2088	4.75	-0.48	0
115	SLU 7	-1	-117	2100	4.85	-2.64	0
115	SLU 8	0	-115	2088	4.75	-0.48	0
115	SLU 9	-1	-117	2100	4.85	-2.64	0
115	SLU 10	-2	-119	2430	4.58	-4.63	0
115	SLU 11	-1	-115	2411	4.41	-1.03	0
115	SLU 12	-2	-117	2423	4.51	-3.19	0
115	SLU 13	-2	-119	2430	4.58	-4.63	0
115	SLU 14	-1	-115	2411	4.41	-1.03	0
115	SLU 15	-2	-117	2423	4.51	-3.19	0
115	SLU 16	-1	-115	2411	4.41	-1.03	0
115	SLU 17	-2	-117	2423	4.51	-3.19	0
115	SLU 18	-1	-115	2549	4.27	-1.26	0
115	SLU 19	-2	-117	2561	4.37	-3.43	0
115	SLU 20	-1	-115	2549	4.27	-1.26	0
115	SLU 21	-2	-117	2561	4.37	-3.43	0
115	SLU 22	0	-121	2273	4.88	-0.7	0
115	SLU 23	-2	-125	2292	5.04	-4.31	0
115	SLU 24	0	-121	2273	4.88	-0.7	0
115	SLU 25	-2	-123	2284	4.98	-2.86	0
115	SLU 26	-2	-125	2292	5.04	-4.31	0
115	SLU 27	0	-121	2273	4.88	-0.7	0
115	SLU 28	-2	-123	2284	4.98	-2.86	0
115	SLU 29	0	-121	2273	4.88	-0.7	0
115	SLU 30	-2	-123	2284	4.98	-2.86	0
115	SLU 31	-3	-125	2615	4.71	-4.86	0
115	SLU 32	-1	-121	2596	4.55	-1.25	0
115	SLU 33	-2	-124	2607	4.65	-3.41	0
115	SLU 34	-3	-125	2615	4.71	-4.86	0
115	SLU 35	-1	-121	2596	4.55	-1.25	0
115	SLU 36	-2	-124	2607	4.65	-3.41	0
115	SLU 37	-1	-121	2596	4.55	-1.25	0
115	SLU 38	-2	-124	2607	4.65	-3.41	0
115	SLU 39	-1	-121	2734	4.4	-1.48	0
115	SLU 40	-2	-124	2746	4.5	-3.65	0
115	SLU 41	-1	-121	2734	4.4	-1.48	0
115	SLU 42	-2	-124	2746	4.5	-3.65	0
115	SLU 43	0	-147	2651	6.12	-0.54	0
115	SLU 44	-2	-151	2670	6.29	-4.15	0
115	SLU 45	0	-147	2651	6.12	-0.54	0
115	SLU 46	-1	-149	2663	6.22	-2.71	0
115	SLU 47	-2	-151	2670	6.29	-4.15	0
115	SLU 48	0	-147	2651	6.12	-0.54	0
115	SLU 49	-1	-149	2663	6.22	-2.71	0
115	SLU 50	0	-147	2651	6.12	-0.54	0
115	SLU 51	-1	-149	2663	6.22	-2.71	0
115	SLU 52	-2	-151	2993	5.96	-4.7	0
115	SLU 53	-1	-147	2974	5.79	-1.09	0
115	SLU 54	-2	-150	2986	5.89	-3.26	0
115	SLU 55	-2	-151	2993	5.96	-4.7	0
115	SLU 56	-1	-147	2974	5.79	-1.09	0
115	SLU 57	-2	-150	2986	5.89	-3.26	0
115	SLU 58	-1	-147	2974	5.79	-1.09	0
115	SLU 59	-2	-150	2986	5.89	-3.26	0
115	SLU 60	-1	-147	3112	5.65	-1.33	0
115	SLU 61	-2	-150	3124	5.75	-3.49	0
115	SLU 62	-1	-147	3112	5.65	-1.33	0
115	SLU 63	-2	-150	3124	5.75	-3.49	0
115	SLU 64	0	-153	2836	6.26	-0.77	0
115	SLU 65	-2	-157	2855	6.42	-4.38	0
115	SLU 66	0	-153	2836	6.26	-0.77	0
115	SLU 67	-2	-156	2848	6.36	-2.93	0
115	SLU 68	-2	-157	2855	6.42	-4.38	0
115	SLU 69	0	-153	2836	6.26	-0.77	0
115	SLU 70	-2	-156	2848	6.36	-2.93	0
115	SLU 71	0	-153	2836	6.26	-0.77	0
115	SLU 72	-2	-156	2848	6.36	-2.93	0
115	SLU 73	-3	-157	3178	6.09	-4.92	0
115	SLU 74	-1	-153	3159	5.92	-1.31	0
115	SLU 75	-2	-156	3170	6.02	-3.48	0
115	SLU 76	-3	-157	3178	6.09	-4.92	0
115	SLU 77	-1	-153	3159	5.92	-1.31	0
115	SLU 78	-2	-156	3170	6.02	-3.48	0
115	SLU 79	-1	-153	3159	5.92	-1.31	0
115	SLU 80	-2	-156	3170	6.02	-3.48	0
115	SLU 81	-1	-154	3297	5.78	-1.55	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
115	SLU 82	-2	-156	3309	5.88	-3.71	0
115	SLU 83	-1	-154	3297	5.78	-1.55	0
115	SLU 84	-2	-156	3309	5.88	-3.71	0
115	SLE RA 1	0	-117	2141	4.78	-0.54	0
115	SLE RA 2	-2	-119	2154	4.89	-2.95	0
115	SLE RA 3	0	-117	2141	4.78	-0.54	0
115	SLE RA 4	-1	-118	2149	4.85	-1.98	0
115	SLE RA 5	-2	-119	2154	4.89	-2.95	0
115	SLE RA 6	0	-117	2141	4.78	-0.54	0
115	SLE RA 7	-1	-118	2149	4.85	-1.98	0
115	SLE RA 8	0	-117	2141	4.78	-0.54	0
115	SLE RA 9	-1	-118	2149	4.85	-1.98	0
115	SLE RA 10	-2	-119	2369	4.67	-3.31	0
115	SLE RA 11	0	-117	2356	4.56	-0.91	0
115	SLE RA 12	-1	-118	2364	4.63	-2.35	0
115	SLE RA 13	-2	-119	2369	4.67	-3.31	0
115	SLE RA 14	0	-117	2356	4.56	-0.91	0
115	SLE RA 15	-1	-118	2364	4.63	-2.35	0
115	SLE RA 16	0	-117	2356	4.56	-0.91	0
115	SLE RA 17	-1	-118	2364	4.63	-2.35	0
115	SLE RA 18	-1	-117	2448	4.47	-1.06	0
115	SLE RA 19	-1	-118	2456	4.53	-2.51	0
115	SLE RA 20	-1	-117	2448	4.47	-1.06	0
115	SLE RA 21	-1	-118	2456	4.53	-2.51	0
115	SLE FR 1	0	-117	2141	4.78	-0.54	0
115	SLE FR 2	-1	-117	2143	4.81	-1.02	0
115	SLE FR 3	0	-117	2141	4.78	-0.54	0
115	SLE FR 4	-1	-117	2236	4.71	-1.18	0
115	SLE FR 5	0	-117	2233	4.69	-0.7	0
115	SLE FR 6	0	-117	2295	4.63	-0.8	0
115	SLE QP 1	0	-117	2141	4.78	-0.54	0
115	SLE QP 2	0	-117	2233	4.69	-0.7	0
115	SLD 1	49	29	2113	-1.61	59.79	-0.01
115	SLD 2	49	29	2113	-1.61	59.79	-0.01
115	SLD 3	55	-125	2150	5.15	66.56	-0.01
115	SLD 4	55	-125	2150	5.15	66.56	-0.01
115	SLD 5	5	162	2141	-7.44	7.17	0
115	SLD 6	5	162	2141	-7.44	7.17	0
115	SLD 7	26	-354	2265	15.07	29.76	-0.01
115	SLD 8	26	-354	2265	15.07	29.76	-0.01
115	SLD 9	-26	121	2201	-5.69	-31.15	0.01
115	SLD 10	-26	121	2201	-5.69	-31.15	0.01
115	SLD 11	-6	-395	2326	16.82	-8.56	0
115	SLD 12	-6	-395	2326	16.82	-8.56	0
115	SLD 13	-56	-108	2316	4.23	-67.96	0.01
115	SLD 14	-56	-108	2316	4.23	-67.96	0.01
115	SLD 15	-50	-262	2353	10.99	-61.18	0.01
115	SLD 16	-50	-262	2353	10.99	-61.18	0.01
115	SLV 1	127	229	1946	-10.24	156.96	-0.03
115	SLV 2	127	229	1946	-10.24	156.96	-0.03
115	SLV 3	143	-136	2034	5.68	174.35	-0.03
115	SLV 4	143	-136	2034	5.68	174.35	-0.03
115	SLV 5	14	540	2014	-23.94	20.22	0.01
115	SLV 6	14	540	2014	-23.94	20.22	0.01
115	SLV 7	66	-675	2307	29.14	78.19	-0.02
115	SLV 8	66	-675	2307	29.14	78.19	-0.02
115	SLV 9	-67	442	2159	-19.76	-79.59	0.03
115	SLV 10	-67	442	2159	-19.76	-79.59	0.03
115	SLV 11	-15	-774	2452	33.32	-21.62	-0.01
115	SLV 12	-15	-774	2452	33.32	-21.62	-0.01
115	SLV 13	-144	-98	2432	3.7	-175.74	0.03
115	SLV 14	-144	-98	2432	3.7	-175.74	0.03
115	SLV 15	-128	-462	2520	19.62	-158.35	0.03
115	SLV 16	-128	-462	2520	19.62	-158.35	0.03
116	SLU 1	0	-138	1890	6.07	0.18	0
116	SLU 2	-12	-133	1865	5.9	-13.4	-0.04
116	SLU 3	0	-138	1890	6.07	0.18	0
116	SLU 4	-7	-135	1875	5.97	-7.97	-0.03
116	SLU 5	-12	-133	1865	5.9	-13.4	-0.04
116	SLU 6	0	-138	1890	6.07	0.18	0
116	SLU 7	-7	-135	1875	5.97	-7.97	-0.03
116	SLU 8	0	-138	1890	6.07	0.18	0
116	SLU 9	-7	-135	1875	5.97	-7.97	-0.03
116	SLU 10	-12	-198	2256	8.65	-13.36	-0.04
116	SLU 11	0	-203	2281	8.82	0.22	0
116	SLU 12	-7	-200	2266	8.72	-7.93	-0.03
116	SLU 13	-12	-198	2256	8.65	-13.36	-0.04
116	SLU 14	0	-203	2281	8.82	0.22	0
116	SLU 15	-7	-200	2266	8.72	-7.93	-0.03
116	SLU 16	0	-203	2281	8.82	0.22	0
116	SLU 17	-7	-200	2266	8.72	-7.93	-0.03
116	SLU 18	0	-231	2449	10	0.24	0
116	SLU 19	-8	-228	2434	9.9	-7.91	-0.03
116	SLU 20	0	-231	2449	10	0.24	0
116	SLU 21	-8	-228	2434	9.9	-7.91	-0.03
116	SLU 22	0	-170	2097	7.42	0.2	0
116	SLU 23	-12	-165	2072	7.25	-13.38	-0.04
116	SLU 24	0	-170	2097	7.42	0.2	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
116	SLU 25	-7	-167	2082	7.32	-7.95	-0.03
116	SLU 26	-12	-165	2072	7.25	-13.38	-0.04
116	SLU 27	0	-170	2097	7.42	0.2	0
116	SLU 28	-7	-167	2082	7.32	-7.95	-0.03
116	SLU 29	0	-170	2097	7.42	0.2	0
116	SLU 30	-7	-167	2082	7.32	-7.95	-0.03
116	SLU 31	-12	-230	2463	10.01	-13.34	-0.04
116	SLU 32	0	-235	2488	10.18	0.25	0
116	SLU 33	-8	-232	2473	10.07	-7.9	-0.03
116	SLU 34	-12	-230	2463	10.01	-13.34	-0.04
116	SLU 35	0	-235	2488	10.18	0.25	0
116	SLU 36	-8	-232	2473	10.07	-7.9	-0.03
116	SLU 37	0	-235	2488	10.18	0.25	0
116	SLU 38	-8	-232	2473	10.07	-7.9	-0.03
116	SLU 39	0	-263	2656	11.36	0.26	0
116	SLU 40	-8	-260	2641	11.25	-7.89	-0.03
116	SLU 41	0	-263	2656	11.36	0.26	0
116	SLU 42	-8	-260	2641	11.25	-7.89	-0.03
116	SLU 43	0	-168	2386	7.42	0.23	0
116	SLU 44	-12	-164	2361	7.25	-13.36	-0.04
116	SLU 45	0	-168	2386	7.42	0.23	0
116	SLU 46	-7	-165	2371	7.32	-7.92	-0.03
116	SLU 47	-12	-164	2361	7.25	-13.36	-0.04
116	SLU 48	0	-168	2386	7.42	0.23	0
116	SLU 49	-7	-165	2371	7.32	-7.92	-0.03
116	SLU 50	0	-168	2386	7.42	0.23	0
116	SLU 51	-7	-165	2371	7.32	-7.92	-0.03
116	SLU 52	-12	-228	2752	10.01	-13.32	-0.04
116	SLU 53	0	-233	2777	10.18	0.27	0
116	SLU 54	-7	-230	2762	10.08	-7.88	-0.03
116	SLU 55	-12	-228	2752	10.01	-13.32	-0.04
116	SLU 56	0	-233	2777	10.18	0.27	0
116	SLU 57	-7	-230	2762	10.08	-7.88	-0.03
116	SLU 58	0	-233	2777	10.18	0.27	0
116	SLU 59	-7	-230	2762	10.08	-7.88	-0.03
116	SLU 60	0	-261	2945	11.36	0.29	0
116	SLU 61	-8	-258	2930	11.26	-7.86	-0.03
116	SLU 62	0	-261	2945	11.36	0.29	0
116	SLU 63	-8	-258	2930	11.26	-7.86	-0.03
116	SLU 64	0	-200	2593	8.78	0.25	0
116	SLU 65	-12	-196	2568	8.61	-13.33	-0.04
116	SLU 66	0	-200	2593	8.78	0.25	0
116	SLU 67	-7	-197	2578	8.68	-7.9	-0.03
116	SLU 68	-12	-196	2568	8.61	-13.33	-0.04
116	SLU 69	0	-200	2593	8.78	0.25	0
116	SLU 70	-7	-197	2578	8.68	-7.9	-0.03
116	SLU 71	0	-200	2593	8.78	0.25	0
116	SLU 72	-7	-197	2578	8.68	-7.9	-0.03
116	SLU 73	-12	-260	2959	11.36	-13.29	-0.04
116	SLU 74	0	-265	2984	11.53	0.29	0
116	SLU 75	-8	-262	2969	11.43	-7.86	-0.03
116	SLU 76	-12	-260	2959	11.36	-13.29	-0.04
116	SLU 77	0	-265	2984	11.53	0.29	0
116	SLU 78	-8	-262	2969	11.43	-7.86	-0.03
116	SLU 79	0	-265	2984	11.53	0.29	0
116	SLU 80	-8	-262	2969	11.43	-7.86	-0.03
116	SLU 81	0	-293	3152	12.71	0.31	0
116	SLU 82	-8	-290	3137	12.61	-7.84	-0.03
116	SLU 83	0	-293	3152	12.71	0.31	0
116	SLU 84	-8	-290	3137	12.61	-7.84	-0.03
116	SLE RA 1	0	-147	1949	6.45	0.19	0
116	SLE RA 2	-8	-144	1932	6.34	-8.87	-0.03
116	SLE RA 3	0	-147	1949	6.45	0.19	0
116	SLE RA 4	-5	-145	1939	6.39	-5.25	-0.02
116	SLE RA 5	-8	-144	1932	6.34	-8.87	-0.03
116	SLE RA 6	0	-147	1949	6.45	0.19	0
116	SLE RA 7	-5	-145	1939	6.39	-5.25	-0.02
116	SLE RA 8	0	-147	1949	6.45	0.19	0
116	SLE RA 9	-5	-145	1939	6.39	-5.25	-0.02
116	SLE RA 10	-8	-187	2193	8.18	-8.84	-0.03
116	SLE RA 11	0	-190	2210	8.29	0.21	0
116	SLE RA 12	-5	-188	2200	8.22	-5.22	-0.02
116	SLE RA 13	-8	-187	2193	8.18	-8.84	-0.03
116	SLE RA 14	0	-190	2210	8.29	0.21	0
116	SLE RA 15	-5	-188	2200	8.22	-5.22	-0.02
116	SLE RA 16	0	-190	2210	8.29	0.21	0
116	SLE RA 17	-5	-188	2200	8.22	-5.22	-0.02
116	SLE RA 18	0	-209	2322	9.08	0.23	0
116	SLE RA 19	-5	-207	2312	9.01	-5.21	-0.02
116	SLE RA 20	0	-209	2322	9.08	0.23	0
116	SLE RA 21	-5	-207	2312	9.01	-5.21	-0.02
116	SLE FR 1	0	-147	1949	6.45	0.19	0
116	SLE FR 2	-2	-146	1946	6.43	-1.62	-0.01
116	SLE FR 3	0	-147	1949	6.45	0.19	0
116	SLE FR 4	-2	-165	2058	7.22	-1.61	-0.01
116	SLE FR 5	0	-166	2061	7.24	0.2	0
116	SLE FR 6	0	-178	2135	7.77	0.21	0
116	SLE QP 1	0	-147	1949	6.45	0.19	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
116	SLE QP 2	0	-166	2061	7.24	0.2	0
116	SLD 1	57	-38	2113	1.83	54.5	0.21
116	SLD 2	57	-38	2113	1.83	54.5	0.21
116	SLD 3	51	-174	2160	7.73	49.62	0.19
116	SLD 4	51	-174	2160	7.73	49.62	0.19
116	SLD 5	25	79	2006	-3.34	23.89	0.09
116	SLD 6	25	79	2006	-3.34	23.89	0.09
116	SLD 7	7	-375	2162	16.35	7.63	0.03
116	SLD 8	7	-375	2162	16.35	7.63	0.03
116	SLD 9	-7	43	1960	-1.87	-7.23	-0.03
116	SLD 10	-7	43	1960	-1.87	-7.23	-0.03
116	SLD 11	-25	-410	2116	17.82	-23.49	-0.09
116	SLD 12	-25	-410	2116	17.82	-23.49	-0.09
116	SLD 13	-51	-157	1962	6.75	-49.23	-0.19
116	SLD 14	-51	-157	1962	6.75	-49.23	-0.19
116	SLD 15	-57	-293	2009	12.65	-54.11	-0.21
116	SLD 16	-57	-293	2009	12.65	-54.11	-0.21
116	SLV 1	145	135	2187	-5.5	139.78	0.53
116	SLV 2	145	135	2187	-5.5	139.78	0.53
116	SLV 3	132	-187	2297	8.44	127.51	0.48
116	SLV 4	132	-187	2297	8.44	127.51	0.48
116	SLV 5	64	412	1933	-17.73	60.69	0.23
116	SLV 6	64	412	1933	-17.73	60.69	0.23
116	SLV 7	19	-659	2298	28.75	19.78	0.07
116	SLV 8	19	-659	2298	28.75	19.78	0.07
116	SLV 9	-19	328	1824	-14.27	-19.38	-0.07
116	SLV 10	-19	328	1824	-14.27	-19.38	-0.07
116	SLV 11	-64	-743	2189	32.22	-60.29	-0.24
116	SLV 12	-64	-743	2189	32.22	-60.29	-0.24
116	SLV 13	-132	-145	1825	6.04	-127.11	-0.49
116	SLV 14	-132	-145	1825	6.04	-127.11	-0.49
116	SLV 15	-146	-466	1935	19.99	-139.38	-0.54
116	SLV 16	-146	-466	1935	19.99	-139.38	-0.54
117	SLU 1	0	-276	1793	11.15	0.14	0
117	SLU 2	-4	-277	1789	11.21	-6.05	0.01
117	SLU 3	0	-276	1793	11.15	0.14	0
117	SLU 4	-3	-277	1791	11.19	-3.57	0
117	SLU 5	-4	-277	1789	11.21	-6.05	0.01
117	SLU 6	0	-276	1793	11.15	0.14	0
117	SLU 7	-3	-277	1791	11.19	-3.57	0
117	SLU 8	0	-276	1793	11.15	0.14	0
117	SLU 9	-3	-277	1791	11.19	-3.57	0
117	SLU 10	-4	-535	2801	21.57	-5.7	0
117	SLU 11	0	-533	2805	21.5	0.49	0
117	SLU 12	-2	-534	2802	21.54	-3.22	0
117	SLU 13	-4	-535	2801	21.57	-5.7	0
117	SLU 14	0	-533	2805	21.5	0.49	0
117	SLU 15	-2	-534	2802	21.54	-3.22	0
117	SLU 16	0	-533	2805	21.5	0.49	0
117	SLU 17	-2	-534	2802	21.54	-3.22	0
117	SLU 18	0	-644	3238	25.94	0.64	0
117	SLU 19	-2	-645	3236	25.98	-3.07	0
117	SLU 20	0	-644	3238	25.94	0.64	0
117	SLU 21	-2	-645	3236	25.98	-3.07	0
117	SLU 22	0	-393	2310	15.84	0.28	0
117	SLU 23	-4	-394	2306	15.91	-5.91	0.01
117	SLU 24	0	-393	2310	15.84	0.28	0
117	SLU 25	-3	-394	2308	15.88	-3.43	0
117	SLU 26	-4	-394	2306	15.91	-5.91	0.01
117	SLU 27	0	-393	2310	15.84	0.28	0
117	SLU 28	-3	-394	2308	15.88	-3.43	0
117	SLU 29	0	-393	2310	15.84	0.28	0
117	SLU 30	-3	-394	2308	15.88	-3.43	0
117	SLU 31	-4	-652	3318	26.26	-5.56	0
117	SLU 32	0	-650	3322	26.2	0.63	0
117	SLU 33	-2	-651	3320	26.24	-3.09	0
117	SLU 34	-4	-652	3318	26.26	-5.56	0
117	SLU 35	0	-650	3322	26.2	0.63	0
117	SLU 36	-2	-651	3320	26.24	-3.09	0
117	SLU 37	0	-650	3322	26.2	0.63	0
117	SLU 38	-2	-651	3320	26.24	-3.09	0
117	SLU 39	0	-761	3756	30.63	0.78	0
117	SLU 40	-2	-762	3753	30.67	-2.94	0
117	SLU 41	0	-761	3756	30.63	0.78	0
117	SLU 42	-2	-762	3753	30.67	-2.94	0
117	SLU 43	0	-318	2153	12.89	0.13	0
117	SLU 44	-4	-320	2150	12.95	-6.05	0.01
117	SLU 45	0	-318	2153	12.89	0.13	0
117	SLU 46	-3	-319	2151	12.93	-3.58	0
117	SLU 47	-4	-320	2150	12.95	-6.05	0.01
117	SLU 48	0	-318	2153	12.89	0.13	0
117	SLU 49	-3	-319	2151	12.93	-3.58	0
117	SLU 50	0	-318	2153	12.89	0.13	0
117	SLU 51	-3	-319	2151	12.93	-3.58	0
117	SLU 52	-4	-577	3161	23.31	-5.7	0
117	SLU 53	0	-576	3165	23.24	0.48	0
117	SLU 54	-2	-577	3163	23.28	-3.23	0
117	SLU 55	-4	-577	3161	23.31	-5.7	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
117	SLU 56	0	-576	3165	23.24	0.48	0
117	SLU 57	-2	-577	3163	23.28	-3.23	0
117	SLU 58	0	-576	3165	23.24	0.48	0
117	SLU 59	-2	-577	3163	23.28	-3.23	0
117	SLU 60	0	-686	3599	27.68	0.63	0
117	SLU 61	-2	-687	3597	27.72	-3.08	0
117	SLU 62	0	-686	3599	27.68	0.63	0
117	SLU 63	-2	-687	3597	27.72	-3.08	0
117	SLU 64	0	-435	2671	17.58	0.27	0
117	SLU 65	-4	-437	2667	17.64	-5.92	0.01
117	SLU 66	0	-435	2671	17.58	0.27	0
117	SLU 67	-3	-436	2669	17.62	-3.44	0
117	SLU 68	-4	-437	2667	17.64	-5.92	0.01
117	SLU 69	0	-435	2671	17.58	0.27	0
117	SLU 70	-3	-436	2669	17.62	-3.44	0
117	SLU 71	0	-435	2671	17.58	0.27	0
117	SLU 72	-3	-436	2669	17.62	-3.44	0
117	SLU 73	-4	-694	3679	28	-5.57	0
117	SLU 74	0	-693	3682	27.93	0.62	0
117	SLU 75	-2	-694	3680	27.97	-3.09	0
117	SLU 76	-4	-694	3679	28	-5.57	0
117	SLU 77	0	-693	3682	27.93	0.62	0
117	SLU 78	-2	-694	3680	27.97	-3.09	0
117	SLU 79	0	-693	3682	27.93	0.62	0
117	SLU 80	-2	-694	3680	27.97	-3.09	0
117	SLU 81	0	-803	4116	32.37	0.77	0
117	SLU 82	-2	-804	4114	32.41	-2.94	0
117	SLU 83	0	-803	4116	32.37	0.77	0
117	SLU 84	-2	-804	4114	32.41	-2.94	0
117	SLE RA 1	0	-309	1941	12.49	0.18	0
117	SLE RA 2	-3	-310	1938	12.53	-3.95	0
117	SLE RA 3	0	-309	1941	12.49	0.18	0
117	SLE RA 4	-2	-310	1939	12.52	-2.3	0
117	SLE RA 5	-3	-310	1938	12.53	-3.95	0
117	SLE RA 6	0	-309	1941	12.49	0.18	0
117	SLE RA 7	-2	-310	1939	12.52	-2.3	0
117	SLE RA 8	0	-309	1941	12.49	0.18	0
117	SLE RA 9	-2	-310	1939	12.52	-2.3	0
117	SLE RA 10	-3	-482	2613	19.44	-3.71	0
117	SLE RA 11	0	-481	2615	19.39	0.41	0
117	SLE RA 12	-2	-481	2614	19.42	-2.06	0
117	SLE RA 13	-3	-482	2613	19.44	-3.71	0
117	SLE RA 14	0	-481	2615	19.39	0.41	0
117	SLE RA 15	-2	-481	2614	19.42	-2.06	0
117	SLE RA 16	0	-481	2615	19.39	0.41	0
117	SLE RA 17	-2	-481	2614	19.42	-2.06	0
117	SLE RA 18	0	-554	2904	22.35	0.51	0
117	SLE RA 19	-1	-555	2903	22.38	-1.96	0
117	SLE RA 20	0	-554	2904	22.35	0.51	0
117	SLE RA 21	-1	-555	2903	22.38	-1.96	0
117	SLE FR 1	0	-309	1941	12.49	0.18	0
117	SLE FR 2	0	-309	1940	12.5	-0.65	0
117	SLE FR 3	0	-309	1941	12.49	0.18	0
117	SLE FR 4	0	-383	2229	15.46	-0.55	0
117	SLE FR 5	0	-383	2230	15.45	0.28	0
117	SLE FR 6	0	-432	2423	17.42	0.35	0
117	SLE QP 1	0	-309	1941	12.49	0.18	0
117	SLE QP 2	0	-383	2230	15.45	0.28	0
117	SLD 1	19	-246	2233	3.31	25.37	-0.03
117	SLD 2	19	-246	2233	3.31	25.37	-0.03
117	SLD 3	20	-439	2195	23.62	26.69	-0.03
117	SLD 4	20	-439	2195	23.62	26.69	-0.03
117	SLD 5	3	-49	2289	-19.01	5.8	0
117	SLD 6	3	-49	2289	-19.01	5.8	0
117	SLD 7	9	-693	2161	48.72	10.21	-0.01
117	SLD 8	9	-693	2161	48.72	10.21	-0.01
117	SLD 9	-9	-73	2299	-17.82	-9.65	0.01
117	SLD 10	-9	-73	2299	-17.82	-9.65	0.01
117	SLD 11	-3	-716	2170	49.91	-5.24	0
117	SLD 12	-3	-716	2170	49.91	-5.24	0
117	SLD 13	-20	-326	2265	7.28	-26.13	0.03
117	SLD 14	-20	-326	2265	7.28	-26.13	0.03
117	SLD 15	-18	-519	2226	27.59	-24.81	0.02
117	SLD 16	-18	-519	2226	27.59	-24.81	0.02
117	SLV 1	57	-48	2240	-15.34	78.33	-0.08
117	SLV 2	57	-48	2240	-15.34	78.33	-0.08
117	SLV 3	62	-528	2140	36.54	81.81	-0.08
117	SLV 4	62	-528	2140	36.54	81.81	-0.08
117	SLV 5	11	446	2385	-72.48	18.41	-0.01
117	SLV 6	11	446	2385	-72.48	18.41	-0.01
117	SLV 7	25	-1154	2051	100.47	30.02	-0.04
117	SLV 8	25	-1154	2051	100.47	30.02	-0.04
117	SLV 9	-25	389	2409	-69.57	-29.46	0.04
117	SLV 10	-25	389	2409	-69.57	-29.46	0.04
117	SLV 11	-10	-1211	2075	103.38	-17.85	0.01
117	SLV 12	-10	-1211	2075	103.38	-17.85	0.01
117	SLV 13	-61	-237	2320	-5.65	-81.25	0.08
117	SLV 14	-61	-237	2320	-5.65	-81.25	0.08



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
117	SLV 15	-57	-718	2220	46.24	-77.77	0.08
117	SLV 16	-57	-718	2220	46.24	-77.77	0.08
118	SLU 1	0	-153	2093	6.87	-0.43	0
118	SLU 2	-2	-157	2113	7.03	-3.63	0
118	SLU 3	0	-153	2093	6.87	-0.43	0
118	SLU 4	-1	-155	2105	6.96	-2.35	0
118	SLU 5	-2	-157	2113	7.03	-3.63	0
118	SLU 6	0	-153	2093	6.87	-0.43	0
118	SLU 7	-1	-155	2105	6.96	-2.35	0
118	SLU 8	0	-153	2093	6.87	-0.43	0
118	SLU 9	-1	-155	2105	6.96	-2.35	0
118	SLU 10	-2	-173	2455	8.22	-4.09	0
118	SLU 11	0	-169	2436	8.06	-0.89	0
118	SLU 12	-1	-172	2447	8.16	-2.81	0
118	SLU 13	-2	-173	2455	8.22	-4.09	0
118	SLU 14	0	-169	2436	8.06	-0.89	0
118	SLU 15	-1	-172	2447	8.16	-2.81	0
118	SLU 16	0	-169	2436	8.06	-0.89	0
118	SLU 17	-1	-172	2447	8.16	-2.81	0
118	SLU 18	-1	-176	2583	8.57	-1.09	0
118	SLU 19	-2	-179	2594	8.67	-3.01	0
118	SLU 20	-1	-176	2583	8.57	-1.09	0
118	SLU 21	-2	-179	2594	8.67	-3.01	0
118	SLU 22	0	-168	2284	7.68	-0.62	0
118	SLU 23	-2	-171	2303	7.84	-3.82	0
118	SLU 24	0	-168	2284	7.68	-0.62	0
118	SLU 25	-1	-170	2296	7.78	-2.54	0
118	SLU 26	-2	-171	2303	7.84	-3.82	0
118	SLU 27	0	-168	2284	7.68	-0.62	0
118	SLU 28	-1	-170	2296	7.78	-2.54	0
118	SLU 29	0	-168	2284	7.68	-0.62	0
118	SLU 30	-1	-170	2296	7.78	-2.54	0
118	SLU 31	-2	-188	2646	9.03	-4.28	0
118	SLU 32	-1	-184	2627	8.87	-1.08	0
118	SLU 33	-2	-186	2638	8.97	-3	0
118	SLU 34	-2	-188	2646	9.03	-4.28	0
118	SLU 35	-1	-184	2627	8.87	-1.08	0
118	SLU 36	-2	-186	2638	8.97	-3	0
118	SLU 37	-1	-184	2627	8.87	-1.08	0
118	SLU 38	-2	-186	2638	8.97	-3	0
118	SLU 39	-1	-191	2774	9.39	-1.28	0
118	SLU 40	-2	-193	2785	9.48	-3.2	0
118	SLU 41	-1	-191	2774	9.39	-1.28	0
118	SLU 42	-2	-193	2785	9.48	-3.2	0
118	SLU 43	0	-194	2656	8.65	-0.49	0
118	SLU 44	-2	-198	2675	8.81	-3.69	0
118	SLU 45	0	-194	2656	8.65	-0.49	0
118	SLU 46	-1	-196	2668	8.75	-2.41	0
118	SLU 47	-2	-198	2675	8.81	-3.69	0
118	SLU 48	0	-194	2656	8.65	-0.49	0
118	SLU 49	-1	-196	2668	8.75	-2.41	0
118	SLU 50	0	-194	2656	8.65	-0.49	0
118	SLU 51	-1	-196	2668	8.75	-2.41	0
118	SLU 52	-2	-214	3018	10	-4.16	0
118	SLU 53	0	-210	2999	9.84	-0.96	0
118	SLU 54	-1	-212	3010	9.94	-2.88	0
118	SLU 55	-2	-214	3018	10	-4.16	0
118	SLU 56	0	-210	2999	9.84	-0.96	0
118	SLU 57	-1	-212	3010	9.94	-2.88	0
118	SLU 58	0	-210	2999	9.84	-0.96	0
118	SLU 59	-1	-212	3010	9.94	-2.88	0
118	SLU 60	-1	-217	3145	10.36	-1.15	0
118	SLU 61	-2	-219	3157	10.45	-3.08	0
118	SLU 62	-1	-217	3145	10.36	-1.15	0
118	SLU 63	-2	-219	3157	10.45	-3.08	0
118	SLU 64	0	-209	2847	9.46	-0.68	0
118	SLU 65	-2	-212	2866	9.62	-3.88	0
118	SLU 66	0	-209	2847	9.46	-0.68	0
118	SLU 67	-1	-211	2858	9.56	-2.6	0
118	SLU 68	-2	-212	2866	9.62	-3.88	0
118	SLU 69	0	-209	2847	9.46	-0.68	0
118	SLU 70	-1	-211	2858	9.56	-2.6	0
118	SLU 71	0	-209	2847	9.46	-0.68	0
118	SLU 72	-1	-211	2858	9.56	-2.6	0
118	SLU 73	-2	-229	3208	10.82	-4.35	0
118	SLU 74	-1	-225	3189	10.66	-1.14	0
118	SLU 75	-2	-227	3201	10.75	-3.07	0
118	SLU 76	-2	-229	3208	10.82	-4.35	0
118	SLU 77	-1	-225	3189	10.66	-1.14	0
118	SLU 78	-2	-227	3201	10.75	-3.07	0
118	SLU 79	-1	-225	3189	10.66	-1.14	0
118	SLU 80	-2	-227	3201	10.75	-3.07	0
118	SLU 81	-1	-232	3336	11.17	-1.34	0
118	SLU 82	-2	-234	3348	11.26	-3.26	0
118	SLU 83	-1	-232	3336	11.17	-1.34	0
118	SLU 84	-2	-234	3348	11.26	-3.26	0
118	SLE RA 1	0	-157	2148	7.1	-0.48	0
118	SLE RA 2	-1	-160	2161	7.21	-2.62	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
118	SLE RA 3	0	-157	2148	7.1	-0.48	0
118	SLE RA 4	-1	-159	2156	7.16	-1.76	0
118	SLE RA 5	-1	-160	2161	7.21	-2.62	0
118	SLE RA 6	0	-157	2148	7.1	-0.48	0
118	SLE RA 7	-1	-159	2156	7.16	-1.76	0
118	SLE RA 8	0	-157	2148	7.1	-0.48	0
118	SLE RA 9	-1	-159	2156	7.16	-1.76	0
118	SLE RA 10	-1	-171	2389	8	-2.93	0
118	SLE RA 11	0	-168	2376	7.9	-0.79	0
118	SLE RA 12	-1	-170	2384	7.96	-2.07	0
118	SLE RA 13	-1	-171	2389	8	-2.93	0
118	SLE RA 14	0	-168	2376	7.9	-0.79	0
118	SLE RA 15	-1	-170	2384	7.96	-2.07	0
118	SLE RA 16	0	-168	2376	7.9	-0.79	0
118	SLE RA 17	-1	-170	2384	7.96	-2.07	0
118	SLE RA 18	0	-173	2474	8.24	-0.92	0
118	SLE RA 19	-1	-174	2482	8.3	-2.2	0
118	SLE RA 20	0	-173	2474	8.24	-0.92	0
118	SLE RA 21	-1	-174	2482	8.3	-2.2	0
118	SLE FR 1	0	-157	2148	7.1	-0.48	0
118	SLE FR 2	0	-158	2151	7.12	-0.91	0
118	SLE FR 3	0	-157	2148	7.1	-0.48	0
118	SLE FR 4	-1	-162	2248	7.46	-1.04	0
118	SLE FR 5	0	-162	2246	7.44	-0.61	0
118	SLE FR 6	0	-165	2311	7.67	-0.7	0
118	SLE QP 1	0	-157	2148	7.1	-0.48	0
118	SLE QP 2	0	-162	2246	7.44	-0.61	0
118	SLD 1	41	-17	2110	1.24	52.13	-0.01
118	SLD 2	41	-17	2110	1.24	52.13	-0.01
118	SLD 3	47	-170	2159	7.87	58.46	-0.01
118	SLD 4	47	-170	2159	7.87	58.46	-0.01
118	SLD 5	3	113	2131	-4.48	5.61	0
118	SLD 6	3	113	2131	-4.48	5.61	0
118	SLD 7	23	-396	2294	17.63	26.71	-0.01
118	SLD 8	23	-396	2294	17.63	26.71	-0.01
118	SLD 9	-24	72	2198	-2.75	-27.94	0.01
118	SLD 10	-24	72	2198	-2.75	-27.94	0.01
118	SLD 11	-4	-437	2360	19.37	-6.84	0
118	SLD 12	-4	-437	2360	19.37	-6.84	0
118	SLD 13	-48	-154	2333	7.01	-59.69	0.01
118	SLD 14	-48	-154	2333	7.01	-59.69	0.01
118	SLD 15	-42	-306	2381	13.65	-53.36	0.01
118	SLD 16	-42	-306	2381	13.65	-53.36	0.01
118	SLV 1	107	181	1923	-7.29	136.88	-0.02
118	SLV 2	107	181	1923	-7.29	136.88	-0.02
118	SLV 3	122	-180	2038	8.36	153.09	-0.03
118	SLV 4	122	-180	2038	8.36	153.09	-0.03
118	SLV 5	9	488	1974	-20.71	16.05	0.01
118	SLV 6	9	488	1974	-20.71	16.05	0.01
118	SLV 7	60	-714	2359	31.45	70.08	-0.02
118	SLV 8	60	-714	2359	31.45	70.08	-0.02
118	SLV 9	-60	390	2133	-16.57	-71.31	0.02
118	SLV 10	-60	390	2133	-16.57	-71.31	0.02
118	SLV 11	-9	-812	2518	35.6	-17.28	-0.01
118	SLV 12	-9	-812	2518	35.6	-17.28	-0.01
118	SLV 13	-123	-144	2454	6.53	-154.32	0.03
118	SLV 14	-123	-144	2454	6.53	-154.32	0.03
118	SLV 15	-107	-505	2569	22.18	-138.11	0.02
118	SLV 16	-107	-505	2569	22.18	-138.11	0.02
119	SLU 1	0	-148	1943	6.89	0.24	0
119	SLU 2	-11	-144	1917	6.67	-12.3	-0.04
119	SLU 3	0	-148	1943	6.89	0.24	0
119	SLU 4	-6	-146	1927	6.76	-7.28	-0.03
119	SLU 5	-11	-144	1917	6.67	-12.3	-0.04
119	SLU 6	0	-148	1943	6.89	0.24	0
119	SLU 7	-6	-146	1927	6.76	-7.28	-0.03
119	SLU 8	0	-148	1943	6.89	0.24	0
119	SLU 9	-6	-146	1927	6.76	-7.28	-0.03
119	SLU 10	-11	-206	2311	9.44	-12.19	-0.04
119	SLU 11	0	-210	2337	9.66	0.34	0
119	SLU 12	-6	-208	2322	9.53	-7.18	-0.03
119	SLU 13	-11	-206	2311	9.44	-12.19	-0.04
119	SLU 14	0	-210	2337	9.66	0.34	0
119	SLU 15	-6	-208	2322	9.53	-7.18	-0.03
119	SLU 16	0	-210	2337	9.66	0.34	0
119	SLU 17	-6	-208	2322	9.53	-7.18	-0.03
119	SLU 18	0	-237	2506	10.85	0.39	0
119	SLU 19	-6	-235	2491	10.72	-7.13	-0.03
119	SLU 20	0	-237	2506	10.85	0.39	0
119	SLU 21	-6	-235	2491	10.72	-7.13	-0.03
119	SLU 22	0	-181	2151	8.33	0.28	0
119	SLU 23	-11	-177	2125	8.11	-12.25	-0.04
119	SLU 24	0	-181	2151	8.33	0.28	0
119	SLU 25	-6	-178	2136	8.2	-7.23	-0.03
119	SLU 26	-11	-177	2125	8.11	-12.25	-0.04
119	SLU 27	0	-181	2151	8.33	0.28	0
119	SLU 28	-6	-178	2136	8.2	-7.23	-0.03
119	SLU 29	0	-181	2151	8.33	0.28	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
119	SLU 30	-6	-178	2136	8.2	-7.23	-0.03
119	SLU 31	-11	-239	2520	10.89	-12.14	-0.04
119	SLU 32	0	-243	2545	11.11	0.39	0
119	SLU 33	-6	-240	2530	10.97	-7.13	-0.03
119	SLU 34	-11	-239	2520	10.89	-12.14	-0.04
119	SLU 35	0	-243	2545	11.11	0.39	0
119	SLU 36	-6	-240	2530	10.97	-7.13	-0.03
119	SLU 37	0	-243	2545	11.11	0.39	0
119	SLU 38	-6	-240	2530	10.97	-7.13	-0.03
119	SLU 39	0	-269	2714	12.29	0.43	0
119	SLU 40	-6	-267	2699	12.16	-7.08	-0.03
119	SLU 41	0	-269	2714	12.29	0.43	0
119	SLU 42	-6	-267	2699	12.16	-7.08	-0.03
119	SLU 43	0	-182	2454	8.46	0.29	0
119	SLU 44	-11	-178	2429	8.24	-12.24	-0.04
119	SLU 45	0	-182	2454	8.46	0.29	0
119	SLU 46	-6	-179	2439	8.33	-7.23	-0.02
119	SLU 47	-11	-178	2429	8.24	-12.24	-0.04
119	SLU 48	0	-182	2454	8.46	0.29	0
119	SLU 49	-6	-179	2439	8.33	-7.23	-0.02
119	SLU 50	0	-182	2454	8.46	0.29	0
119	SLU 51	-6	-179	2439	8.33	-7.23	-0.02
119	SLU 52	-11	-240	2823	11.02	-12.14	-0.04
119	SLU 53	0	-244	2849	11.24	0.4	0
119	SLU 54	-6	-241	2833	11.1	-7.12	-0.03
119	SLU 55	-11	-240	2823	11.02	-12.14	-0.04
119	SLU 56	0	-244	2849	11.24	0.4	0
119	SLU 57	-6	-241	2833	11.1	-7.12	-0.03
119	SLU 58	0	-244	2849	11.24	0.4	0
119	SLU 59	-6	-241	2833	11.1	-7.12	-0.03
119	SLU 60	0	-270	3018	12.42	0.44	0
119	SLU 61	-6	-268	3002	12.29	-7.08	-0.03
119	SLU 62	0	-270	3018	12.42	0.44	0
119	SLU 63	-6	-268	3002	12.29	-7.08	-0.03
119	SLU 64	0	-214	2662	9.9	0.34	0
119	SLU 65	-11	-210	2637	9.68	-12.19	-0.04
119	SLU 66	0	-214	2662	9.9	0.34	0
119	SLU 67	-6	-212	2647	9.77	-7.18	-0.03
119	SLU 68	-11	-210	2637	9.68	-12.19	-0.04
119	SLU 69	0	-214	2662	9.9	0.34	0
119	SLU 70	-6	-212	2647	9.77	-7.18	-0.03
119	SLU 71	0	-214	2662	9.9	0.34	0
119	SLU 72	-6	-212	2647	9.77	-7.18	-0.03
119	SLU 73	-11	-272	3031	12.46	-12.09	-0.04
119	SLU 74	0	-276	3057	12.68	0.44	0
119	SLU 75	-6	-274	3041	12.55	-7.08	-0.03
119	SLU 76	-11	-272	3031	12.46	-12.09	-0.04
119	SLU 77	0	-276	3057	12.68	0.44	0
119	SLU 78	-6	-274	3041	12.55	-7.08	-0.03
119	SLU 79	0	-276	3057	12.68	0.44	0
119	SLU 80	-6	-274	3041	12.55	-7.08	-0.03
119	SLU 81	0	-303	3226	13.87	0.49	0
119	SLU 82	-6	-300	3210	13.73	-7.03	-0.03
119	SLU 83	0	-303	3226	13.87	0.49	0
119	SLU 84	-6	-300	3210	13.73	-7.03	-0.03
119	SLE RA 1	0	-158	2002	7.3	0.25	0
119	SLE RA 2	-7	-155	1985	7.16	-8.1	-0.03
119	SLE RA 3	0	-158	2002	7.3	0.25	0
119	SLE RA 4	-4	-156	1992	7.21	-4.76	-0.02
119	SLE RA 5	-7	-155	1985	7.16	-8.1	-0.03
119	SLE RA 6	0	-158	2002	7.3	0.25	0
119	SLE RA 7	-4	-156	1992	7.21	-4.76	-0.02
119	SLE RA 8	0	-158	2002	7.3	0.25	0
119	SLE RA 9	-4	-156	1992	7.21	-4.76	-0.02
119	SLE RA 10	-7	-196	2248	9	-8.03	-0.03
119	SLE RA 11	0	-199	2265	9.15	0.32	0
119	SLE RA 12	-4	-197	2255	9.06	-4.69	-0.02
119	SLE RA 13	-7	-196	2248	9	-8.03	-0.03
119	SLE RA 14	0	-199	2265	9.15	0.32	0
119	SLE RA 15	-4	-197	2255	9.06	-4.69	-0.02
119	SLE RA 16	0	-199	2265	9.15	0.32	0
119	SLE RA 17	-4	-197	2255	9.06	-4.69	-0.02
119	SLE RA 18	0	-217	2378	9.94	0.35	0
119	SLE RA 19	-4	-215	2368	9.86	-4.66	-0.02
119	SLE RA 20	0	-217	2378	9.94	0.35	0
119	SLE RA 21	-4	-215	2368	9.86	-4.66	-0.02
119	SLE FR 1	0	-158	2002	7.3	0.25	0
119	SLE FR 2	-1	-157	1999	7.27	-1.42	-0.01
119	SLE FR 3	0	-158	2002	7.3	0.25	0
119	SLE FR 4	-1	-175	2112	8.06	-1.39	-0.01
119	SLE FR 5	0	-175	2115	8.09	0.28	0
119	SLE FR 6	0	-187	2190	8.62	0.3	0
119	SLE QP 1	0	-158	2002	7.3	0.25	0
119	SLE QP 2	0	-175	2115	8.09	0.28	0
119	SLD 1	51	-58	2180	3.03	50.18	0.2
119	SLD 2	51	-58	2180	3.03	50.18	0.2
119	SLD 3	45	-186	2235	8.59	45.1	0.18
119	SLD 4	45	-186	2235	8.59	45.1	0.18



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
119	SLD 5	25	54	2051	-1.85	22.96	0.1
119	SLD 6	25	54	2051	-1.85	22.96	0.1
119	SLD 7	4	-372	2234	16.67	6.01	0.02
119	SLD 8	4	-372	2234	16.67	6.01	0.02
119	SLD 9	-4	22	1996	-0.48	-5.45	-0.02
119	SLD 10	-4	22	1996	-0.48	-5.45	-0.02
119	SLD 11	-25	-404	2179	18.04	-22.4	-0.1
119	SLD 12	-25	-404	2179	18.04	-22.4	-0.1
119	SLD 13	-45	-165	1995	7.6	-44.54	-0.18
119	SLD 14	-45	-165	1995	7.6	-44.54	-0.18
119	SLD 15	-51	-293	2050	13.16	-49.62	-0.2
119	SLD 16	-51	-293	2050	13.16	-49.62	-0.2
119	SLV 1	131	101	2270	-3.84	128.43	0.52
119	SLV 2	131	101	2270	-3.84	128.43	0.52
119	SLV 3	115	-200	2398	9.27	115.87	0.46
119	SLV 4	115	-200	2398	9.27	115.87	0.46
119	SLV 5	63	365	1967	-15.38	57.78	0.24
119	SLV 6	63	365	1967	-15.38	57.78	0.24
119	SLV 7	11	-641	2394	28.34	15.9	0.05
119	SLV 8	11	-641	2394	28.34	15.9	0.05
119	SLV 9	-11	290	1836	-12.15	-15.34	-0.05
119	SLV 10	-11	290	1836	-12.15	-15.34	-0.05
119	SLV 11	-63	-716	2263	31.57	-57.22	-0.24
119	SLV 12	-63	-716	2263	31.57	-57.22	-0.24
119	SLV 13	-115	-150	1832	6.91	-115.31	-0.46
119	SLV 14	-115	-150	1832	6.91	-115.31	-0.46
119	SLV 15	-131	-452	1960	20.03	-127.87	-0.52
119	SLV 16	-131	-452	1960	20.03	-127.87	-0.52
120	SLU 1	0	-309	1626	11.62	0.09	0
120	SLU 2	-2	-310	1623	11.65	-4.09	0
120	SLU 3	0	-309	1626	11.62	0.09	0
120	SLU 4	-1	-310	1624	11.64	-2.42	0
120	SLU 5	-2	-310	1623	11.65	-4.09	0
120	SLU 6	0	-309	1626	11.62	0.09	0
120	SLU 7	-1	-310	1624	11.64	-2.42	0
120	SLU 8	0	-309	1626	11.62	0.09	0
120	SLU 9	-1	-310	1624	11.64	-2.42	0
120	SLU 10	-2	-583	2455	21.66	-3.85	0
120	SLU 11	0	-582	2458	21.63	0.33	0
120	SLU 12	-1	-583	2456	21.65	-2.18	0
120	SLU 13	-2	-583	2455	21.66	-3.85	0
120	SLU 14	0	-582	2458	21.63	0.33	0
120	SLU 15	-1	-583	2456	21.65	-2.18	0
120	SLU 16	0	-582	2458	21.63	0.33	0
120	SLU 17	-1	-583	2456	21.65	-2.18	0
120	SLU 18	0	-699	2814	25.92	0.44	0
120	SLU 19	-1	-699	2813	25.94	-2.07	0
120	SLU 20	0	-699	2814	25.92	0.44	0
120	SLU 21	-1	-699	2813	25.94	-2.07	0
120	SLU 22	0	-439	2061	16.42	0.19	0
120	SLU 23	-2	-440	2058	16.44	-3.99	0
120	SLU 24	0	-439	2061	16.42	0.19	0
120	SLU 25	-1	-439	2059	16.44	-2.32	0
120	SLU 26	-2	-440	2058	16.44	-3.99	0
120	SLU 27	0	-439	2061	16.42	0.19	0
120	SLU 28	-1	-439	2059	16.44	-2.32	0
120	SLU 29	0	-439	2061	16.42	0.19	0
120	SLU 30	-1	-439	2059	16.44	-2.32	0
120	SLU 31	-2	-712	2890	26.45	-3.76	0
120	SLU 32	0	-712	2893	26.43	0.43	0
120	SLU 33	-1	-712	2891	26.45	-2.08	0
120	SLU 34	-2	-712	2890	26.45	-3.76	0
120	SLU 35	0	-712	2893	26.43	0.43	0
120	SLU 36	-1	-712	2891	26.45	-2.08	0
120	SLU 37	0	-712	2893	26.43	0.43	0
120	SLU 38	-1	-712	2891	26.45	-2.08	0
120	SLU 39	0	-829	3250	30.72	0.53	0
120	SLU 40	-1	-829	3248	30.74	-1.98	0
120	SLU 41	0	-829	3250	30.72	0.53	0
120	SLU 42	-1	-829	3248	30.74	-1.98	0
120	SLU 43	0	-357	1964	13.47	0.09	0
120	SLU 44	-2	-358	1962	13.49	-4.09	0
120	SLU 45	0	-357	1964	13.47	0.09	0
120	SLU 46	-1	-358	1963	13.48	-2.42	0
120	SLU 47	-2	-358	1962	13.49	-4.09	0
120	SLU 48	0	-357	1964	13.47	0.09	0
120	SLU 49	-1	-358	1963	13.48	-2.42	0
120	SLU 50	0	-357	1964	13.47	0.09	0
120	SLU 51	-1	-358	1963	13.48	-2.42	0
120	SLU 52	-2	-631	2793	23.5	-3.85	0
120	SLU 53	0	-630	2796	23.48	0.33	0
120	SLU 54	-1	-631	2795	23.49	-2.18	0
120	SLU 55	-2	-631	2793	23.5	-3.85	0
120	SLU 56	0	-630	2796	23.48	0.33	0
120	SLU 57	-1	-631	2795	23.49	-2.18	0
120	SLU 58	0	-630	2796	23.48	0.33	0
120	SLU 59	-1	-631	2795	23.49	-2.18	0
120	SLU 60	0	-747	3153	27.77	0.43	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
120	SLU 61	-1	-748	3151	27.78	-2.08	0
120	SLU 62	0	-747	3153	27.77	0.43	0
120	SLU 63	-1	-748	3151	27.78	-2.08	0
120	SLU 64	0	-487	2400	18.26	0.18	0
120	SLU 65	-2	-488	2397	18.29	-4	0
120	SLU 66	0	-487	2400	18.26	0.18	0
120	SLU 67	-1	-488	2398	18.28	-2.33	0
120	SLU 68	-2	-488	2397	18.29	-4	0
120	SLU 69	0	-487	2400	18.26	0.18	0
120	SLU 70	-1	-488	2398	18.28	-2.33	0
120	SLU 71	0	-487	2400	18.26	0.18	0
120	SLU 72	-1	-488	2398	18.28	-2.33	0
120	SLU 73	-2	-761	3229	28.3	-3.76	0
120	SLU 74	0	-760	3232	28.27	0.42	0
120	SLU 75	-1	-760	3230	28.29	-2.09	0
120	SLU 76	-2	-761	3229	28.3	-3.76	0
120	SLU 77	0	-760	3232	28.27	0.42	0
120	SLU 78	-1	-760	3230	28.29	-2.09	0
120	SLU 79	0	-760	3232	28.27	0.42	0
120	SLU 80	-1	-760	3230	28.29	-2.09	0
120	SLU 81	0	-877	3588	32.56	0.53	0
120	SLU 82	-1	-877	3586	32.58	-1.98	0
120	SLU 83	0	-877	3588	32.56	0.53	0
120	SLU 84	-1	-877	3586	32.58	-1.98	0
120	SLE RA 1	0	-346	1750	12.99	0.12	0
120	SLE RA 2	-1	-347	1748	13.01	-2.67	0
120	SLE RA 3	0	-346	1750	12.99	0.12	0
120	SLE RA 4	-1	-347	1749	13	-1.55	0
120	SLE RA 5	-1	-347	1748	13.01	-2.67	0
120	SLE RA 6	0	-346	1750	12.99	0.12	0
120	SLE RA 7	-1	-347	1749	13	-1.55	0
120	SLE RA 8	0	-346	1750	12.99	0.12	0
120	SLE RA 9	-1	-347	1749	13	-1.55	0
120	SLE RA 10	-1	-529	2303	19.68	-2.51	0
120	SLE RA 11	0	-528	2305	19.67	0.28	0
120	SLE RA 12	-1	-528	2304	19.68	-1.39	0
120	SLE RA 13	-1	-529	2303	19.68	-2.51	0
120	SLE RA 14	0	-528	2305	19.67	0.28	0
120	SLE RA 15	-1	-528	2304	19.68	-1.39	0
120	SLE RA 16	0	-528	2305	19.67	0.28	0
120	SLE RA 17	-1	-528	2304	19.68	-1.39	0
120	SLE RA 18	0	-606	2542	22.53	0.35	0
120	SLE RA 19	-1	-606	2541	22.54	-1.32	0
120	SLE RA 20	0	-606	2542	22.53	0.35	0
120	SLE RA 21	-1	-606	2541	22.54	-1.32	0
120	SLE FR 1	0	-346	1750	12.99	0.12	0
120	SLE FR 2	0	-346	1750	13	-0.44	0
120	SLE FR 3	0	-346	1750	12.99	0.12	0
120	SLE FR 4	0	-424	1988	15.86	-0.37	0
120	SLE FR 5	0	-424	1988	15.85	0.19	0
120	SLE FR 6	0	-476	2146	17.76	0.23	0
120	SLE QP 1	0	-346	1750	12.99	0.12	0
120	SLE QP 2	0	-424	1988	15.85	0.19	0
120	SLD 1	9	-465	1984	22.32	17.88	0
120	SLD 2	9	-465	1984	22.32	17.88	0
120	SLD 3	11	-306	1960	5.76	19.05	-0.01
120	SLD 4	11	-306	1960	5.76	19.05	-0.01
120	SLD 5	1	-678	2023	42.9	3.72	0.01
120	SLD 6	1	-678	2023	42.9	3.72	0.01
120	SLD 7	5	-148	1944	-12.28	7.63	-0.01
120	SLD 8	5	-148	1944	-12.28	7.63	-0.01
120	SLD 9	-5	-701	2032	43.99	-7.25	0.01
120	SLD 10	-5	-701	2032	43.99	-7.25	0.01
120	SLD 11	-1	-171	1953	-11.2	-3.34	-0.01
120	SLD 12	-1	-171	1953	-11.2	-3.34	-0.01
120	SLD 13	-11	-542	2016	25.94	-18.67	0.01
120	SLD 14	-11	-542	2016	25.94	-18.67	0.01
120	SLD 15	-9	-383	1992	9.39	-17.5	0
120	SLD 16	-9	-383	1992	9.39	-17.5	0
120	SLV 1	28	-528	1979	32.6	55.17	-0.01
120	SLV 2	28	-528	1979	32.6	55.17	-0.01
120	SLV 3	32	-140	1918	-9.55	58.22	-0.02
120	SLV 4	32	-140	1918	-9.55	58.22	-0.02
120	SLV 5	3	-1045	2078	84.8	12.05	0.01
120	SLV 6	3	-1045	2078	84.8	12.05	0.01
120	SLV 7	15	251	1874	-55.69	22.24	-0.02
120	SLV 8	15	251	1874	-55.69	22.24	-0.02
120	SLV 9	-15	-1099	2102	87.4	-21.86	0.02
120	SLV 10	-15	-1099	2102	87.4	-21.86	0.02
120	SLV 11	-3	197	1898	-53.1	-11.67	-0.01
120	SLV 12	-3	197	1898	-53.1	-11.67	-0.01
120	SLV 13	-32	-709	2058	41.26	-57.85	0.02
120	SLV 14	-32	-709	2058	41.26	-57.85	0.02
120	SLV 15	-28	-320	1997	-0.89	-54.79	0.01
120	SLV 16	-28	-320	1997	-0.89	-54.79	0.01
121	SLU 1	0	-188	2099	7.87	-0.39	0
121	SLU 2	-1	-191	2118	8.01	-3.03	0
121	SLU 3	0	-188	2099	7.87	-0.39	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
121	SLU 4	-1	-190	2110	7.95	-1.97	0
121	SLU 5	-1	-191	2118	8.01	-3.03	0
121	SLU 6	0	-188	2099	7.87	-0.39	0
121	SLU 7	-1	-190	2110	7.95	-1.97	0
121	SLU 8	0	-188	2099	7.87	-0.39	0
121	SLU 9	-1	-190	2110	7.95	-1.97	0
121	SLU 10	-2	-209	2479	8.53	-3.4	0
121	SLU 11	0	-206	2460	8.39	-0.76	0
121	SLU 12	-1	-208	2472	8.48	-2.35	0
121	SLU 13	-2	-209	2479	8.53	-3.4	0
121	SLU 14	0	-206	2460	8.39	-0.76	0
121	SLU 15	-1	-208	2472	8.48	-2.35	0
121	SLU 16	0	-206	2460	8.39	-0.76	0
121	SLU 17	-1	-208	2472	8.48	-2.35	0
121	SLU 18	0	-214	2615	8.61	-0.92	0
121	SLU 19	-1	-216	2627	8.7	-2.51	0
121	SLU 20	0	-214	2615	8.61	-0.92	0
121	SLU 21	-1	-216	2627	8.7	-2.51	0
121	SLU 22	0	-205	2295	8.49	-0.54	0
121	SLU 23	-1	-208	2314	8.64	-3.18	0
121	SLU 24	0	-205	2295	8.49	-0.54	0
121	SLU 25	-1	-207	2306	8.58	-2.13	0
121	SLU 26	-1	-208	2314	8.64	-3.18	0
121	SLU 27	0	-205	2295	8.49	-0.54	0
121	SLU 28	-1	-207	2306	8.58	-2.13	0
121	SLU 29	0	-205	2295	8.49	-0.54	0
121	SLU 30	-1	-207	2306	8.58	-2.13	0
121	SLU 31	-2	-226	2675	9.16	-3.56	0
121	SLU 32	0	-223	2656	9.01	-0.91	0
121	SLU 33	-1	-225	2668	9.1	-2.5	0
121	SLU 34	-2	-226	2675	9.16	-3.56	0
121	SLU 35	0	-223	2656	9.01	-0.91	0
121	SLU 36	-1	-225	2668	9.1	-2.5	0
121	SLU 37	0	-223	2656	9.01	-0.91	0
121	SLU 38	-1	-225	2668	9.1	-2.5	0
121	SLU 39	0	-231	2811	9.24	-1.07	0
121	SLU 40	-1	-233	2823	9.32	-2.66	0
121	SLU 41	0	-231	2811	9.24	-1.07	0
121	SLU 42	-1	-233	2823	9.32	-2.66	0
121	SLU 43	0	-238	2661	10.01	-0.45	0
121	SLU 44	-1	-242	2681	10.16	-3.09	0
121	SLU 45	0	-238	2661	10.01	-0.45	0
121	SLU 46	-1	-240	2673	10.1	-2.04	0
121	SLU 47	-1	-242	2681	10.16	-3.09	0
121	SLU 48	0	-238	2661	10.01	-0.45	0
121	SLU 49	-1	-240	2673	10.1	-2.04	0
121	SLU 50	0	-238	2661	10.01	-0.45	0
121	SLU 51	-1	-240	2673	10.1	-2.04	0
121	SLU 52	-2	-260	3042	10.68	-3.47	0
121	SLU 53	0	-256	3023	10.53	-0.82	0
121	SLU 54	-1	-258	3034	10.62	-2.41	0
121	SLU 55	-2	-260	3042	10.68	-3.47	0
121	SLU 56	0	-256	3023	10.53	-0.82	0
121	SLU 57	-1	-258	3034	10.62	-2.41	0
121	SLU 58	0	-256	3023	10.53	-0.82	0
121	SLU 59	-1	-258	3034	10.62	-2.41	0
121	SLU 60	0	-264	3178	10.76	-0.98	0
121	SLU 61	-1	-266	3189	10.84	-2.57	0
121	SLU 62	0	-264	3178	10.76	-0.98	0
121	SLU 63	-1	-266	3189	10.84	-2.57	0
121	SLU 64	0	-255	2857	10.64	-0.6	0
121	SLU 65	-1	-259	2877	10.78	-3.25	0
121	SLU 66	0	-255	2857	10.64	-0.6	0
121	SLU 67	-1	-257	2869	10.72	-2.19	0
121	SLU 68	-1	-259	2877	10.78	-3.25	0
121	SLU 69	0	-255	2857	10.64	-0.6	0
121	SLU 70	-1	-257	2869	10.72	-2.19	0
121	SLU 71	0	-255	2857	10.64	-0.6	0
121	SLU 72	-1	-257	2869	10.72	-2.19	0
121	SLU 73	-2	-277	3238	11.3	-3.62	0
121	SLU 74	0	-273	3219	11.16	-0.98	0
121	SLU 75	-1	-275	3230	11.25	-2.56	0
121	SLU 76	-2	-277	3238	11.3	-3.62	0
121	SLU 77	0	-273	3219	11.16	-0.98	0
121	SLU 78	-1	-275	3230	11.25	-2.56	0
121	SLU 79	0	-273	3219	11.16	-0.98	0
121	SLU 80	-1	-275	3230	11.25	-2.56	0
121	SLU 81	0	-281	3374	11.38	-1.14	0
121	SLU 82	-1	-283	3385	11.47	-2.72	0
121	SLU 83	0	-281	3374	11.38	-1.14	0
121	SLU 84	-1	-283	3385	11.47	-2.72	0
121	SLE RA 1	0	-193	2155	8.04	-0.43	0
121	SLE RA 2	-1	-195	2168	8.14	-2.19	0
121	SLE RA 3	0	-193	2155	8.04	-0.43	0
121	SLE RA 4	-1	-194	2163	8.1	-1.49	0
121	SLE RA 5	-1	-195	2168	8.14	-2.19	0
121	SLE RA 6	0	-193	2155	8.04	-0.43	0
121	SLE RA 7	-1	-194	2163	8.1	-1.49	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
121	SLE RA 8	0	-193	2155	8.04	-0.43	0
121	SLE RA 9	-1	-194	2163	8.1	-1.49	0
121	SLE RA 10	-1	-207	2409	8.49	-2.44	0
121	SLE RA 11	0	-205	2396	8.39	-0.68	0
121	SLE RA 12	-1	-206	2404	8.45	-1.74	0
121	SLE RA 13	-1	-207	2409	8.49	-2.44	0
121	SLE RA 14	0	-205	2396	8.39	-0.68	0
121	SLE RA 15	-1	-206	2404	8.45	-1.74	0
121	SLE RA 16	0	-205	2396	8.39	-0.68	0
121	SLE RA 17	-1	-206	2404	8.45	-1.74	0
121	SLE RA 18	0	-210	2499	8.54	-0.79	0
121	SLE RA 19	-1	-211	2507	8.6	-1.84	0
121	SLE RA 20	0	-210	2499	8.54	-0.79	0
121	SLE RA 21	-1	-211	2507	8.6	-1.84	0
121	SLE FR 1	0	-193	2155	8.04	-0.43	0
121	SLE FR 2	0	-193	2158	8.06	-0.78	0
121	SLE FR 3	0	-193	2155	8.04	-0.43	0
121	SLE FR 4	0	-198	2261	8.21	-0.89	0
121	SLE FR 5	0	-198	2258	8.19	-0.54	0
121	SLE FR 6	0	-201	2327	8.29	-0.61	0
121	SLE QP 1	0	-193	2155	8.04	-0.43	0
121	SLE QP 2	0	-198	2258	8.19	-0.54	0
121	SLD 1	31	-56	2099	2.12	41.95	0.01
121	SLD 2	31	-56	2099	2.12	41.95	0.01
121	SLD 3	37	-206	2164	8.62	47.72	0
121	SLD 4	37	-206	2164	8.62	47.72	0
121	SLD 5	0	72	2113	-3.5	3.45	0.01
121	SLD 6	0	72	2113	-3.5	3.45	0.01
121	SLD 7	20	-428	2327	18.19	22.7	-0.01
121	SLD 8	20	-428	2327	18.19	22.7	-0.01
121	SLD 9	-21	32	2189	-1.8	-23.77	0
121	SLD 10	-21	32	2189	-1.8	-23.77	0
121	SLD 11	0	-468	2403	19.89	-4.53	-0.01
121	SLD 12	0	-468	2403	19.89	-4.53	-0.01
121	SLD 13	-37	-189	2353	7.77	-48.8	0
121	SLD 14	-37	-189	2353	7.77	-48.8	0
121	SLD 15	-31	-340	2417	14.27	-43.03	-0.01
121	SLD 16	-31	-340	2417	14.27	-43.03	-0.01
121	SLV 1	79	138	1879	-6.23	110.24	0.02
121	SLV 2	79	138	1879	-6.23	110.24	0.02
121	SLV 3	95	-216	2032	9.12	124.95	0.01
121	SLV 4	95	-216	2032	9.12	124.95	0.01
121	SLV 5	0	440	1912	-19.41	10.39	0.02
121	SLV 6	0	440	1912	-19.41	10.39	0.02
121	SLV 7	52	-740	2422	31.75	59.41	-0.01
121	SLV 8	52	-740	2422	31.75	59.41	-0.01
121	SLV 9	-52	345	2094	-15.36	-60.49	0.01
121	SLV 10	-52	345	2094	-15.36	-60.49	0.01
121	SLV 11	-1	-836	2604	35.8	-11.47	-0.02
121	SLV 12	-1	-836	2604	35.8	-11.47	-0.02
121	SLV 13	-95	-180	2484	7.27	-126.02	-0.01
121	SLV 14	-95	-180	2484	7.27	-126.02	-0.01
121	SLV 15	-80	-534	2637	22.62	-111.32	-0.02
121	SLV 16	-80	-534	2637	22.62	-111.32	-0.02
122	SLU 1	0	-186	2021	8.31	0.29	0
122	SLU 2	-7	-183	1992	8.22	-9.77	-0.03
122	SLU 3	0	-186	2021	8.31	0.29	0
122	SLU 4	-4	-184	2004	8.25	-5.75	-0.02
122	SLU 5	-7	-183	1992	8.22	-9.77	-0.03
122	SLU 6	0	-186	2021	8.31	0.29	0
122	SLU 7	-4	-184	2004	8.25	-5.75	-0.02
122	SLU 8	0	-186	2021	8.31	0.29	0
122	SLU 9	-4	-184	2004	8.25	-5.75	-0.02
122	SLU 10	-7	-249	2402	11.09	-9.63	-0.03
122	SLU 11	0	-251	2430	11.18	0.43	0
122	SLU 12	-4	-250	2413	11.13	-5.61	-0.02
122	SLU 13	-7	-249	2402	11.09	-9.63	-0.03
122	SLU 14	0	-251	2430	11.18	0.43	0
122	SLU 15	-4	-250	2413	11.13	-5.61	-0.02
122	SLU 16	0	-251	2430	11.18	0.43	0
122	SLU 17	-4	-250	2413	11.13	-5.61	-0.02
122	SLU 18	0	-279	2605	12.41	0.49	0
122	SLU 19	-4	-278	2588	12.36	-5.55	-0.02
122	SLU 20	0	-279	2605	12.41	0.49	0
122	SLU 21	-4	-278	2588	12.36	-5.55	-0.02
122	SLU 22	0	-221	2235	9.86	0.35	0
122	SLU 23	-7	-219	2206	9.77	-9.71	-0.03
122	SLU 24	0	-221	2235	9.86	0.35	0
122	SLU 25	-4	-220	2218	9.8	-5.68	-0.02
122	SLU 26	-7	-219	2206	9.77	-9.71	-0.03
122	SLU 27	0	-221	2235	9.86	0.35	0
122	SLU 28	-4	-220	2218	9.8	-5.68	-0.02
122	SLU 29	0	-221	2235	9.86	0.35	0
122	SLU 30	-4	-220	2218	9.8	-5.68	-0.02
122	SLU 31	-7	-284	2616	12.64	-9.57	-0.03
122	SLU 32	0	-287	2644	12.73	0.49	0
122	SLU 33	-4	-285	2627	12.68	-5.55	-0.02
122	SLU 34	-7	-284	2616	12.64	-9.57	-0.03



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
122	SLU 35	0	-287	2644	12.73	0.49	0
122	SLU 36	-4	-285	2627	12.68	-5.55	-0.02
122	SLU 37	0	-287	2644	12.73	0.49	0
122	SLU 38	-4	-285	2627	12.68	-5.55	-0.02
122	SLU 39	0	-315	2820	13.96	0.55	0
122	SLU 40	-4	-313	2803	13.91	-5.49	-0.02
122	SLU 41	0	-315	2820	13.96	0.55	0
122	SLU 42	-4	-313	2803	13.91	-5.49	-0.02
122	SLU 43	0	-229	2554	10.27	0.36	0
122	SLU 44	-7	-226	2525	10.18	-9.7	-0.03
122	SLU 45	0	-229	2554	10.27	0.36	0
122	SLU 46	-4	-227	2536	10.21	-5.68	-0.02
122	SLU 47	-7	-226	2525	10.18	-9.7	-0.03
122	SLU 48	0	-229	2554	10.27	0.36	0
122	SLU 49	-4	-227	2536	10.21	-5.68	-0.02
122	SLU 50	0	-229	2554	10.27	0.36	0
122	SLU 51	-4	-227	2536	10.21	-5.68	-0.02
122	SLU 52	-7	-292	2934	13.05	-9.57	-0.03
122	SLU 53	0	-295	2963	13.14	0.5	0
122	SLU 54	-4	-293	2946	13.09	-5.54	-0.02
122	SLU 55	-7	-292	2934	13.05	-9.57	-0.03
122	SLU 56	0	-295	2963	13.14	0.5	0
122	SLU 57	-4	-293	2946	13.09	-5.54	-0.02
122	SLU 58	0	-295	2963	13.14	0.5	0
122	SLU 59	-4	-293	2946	13.09	-5.54	-0.02
122	SLU 60	0	-323	3138	14.38	0.56	0
122	SLU 61	-4	-321	3121	14.32	-5.48	-0.02
122	SLU 62	0	-323	3138	14.38	0.56	0
122	SLU 63	-4	-321	3121	14.32	-5.48	-0.02
122	SLU 64	0	-265	2768	11.82	0.42	0
122	SLU 65	-7	-262	2739	11.73	-9.64	-0.03
122	SLU 66	0	-265	2768	11.82	0.42	0
122	SLU 67	-4	-263	2751	11.76	-5.62	-0.02
122	SLU 68	-7	-262	2739	11.73	-9.64	-0.03
122	SLU 69	0	-265	2768	11.82	0.42	0
122	SLU 70	-4	-263	2751	11.76	-5.62	-0.02
122	SLU 71	0	-265	2768	11.82	0.42	0
122	SLU 72	-4	-263	2751	11.76	-5.62	-0.02
122	SLU 73	-7	-328	3149	14.6	-9.5	-0.03
122	SLU 74	0	-330	3177	14.69	0.56	0
122	SLU 75	-4	-329	3160	14.64	-5.48	-0.02
122	SLU 76	-7	-328	3149	14.6	-9.5	-0.03
122	SLU 77	0	-330	3177	14.69	0.56	0
122	SLU 78	-4	-329	3160	14.64	-5.48	-0.02
122	SLU 79	0	-330	3177	14.69	0.56	0
122	SLU 80	-4	-329	3160	14.64	-5.48	-0.02
122	SLU 81	0	-358	3352	15.92	0.62	0
122	SLU 82	-4	-357	3335	15.87	-5.42	-0.02
122	SLU 83	0	-358	3352	15.92	0.62	0
122	SLU 84	-4	-357	3335	15.87	-5.42	-0.02
122	SLE RA 1	0	-196	2082	8.75	0.31	0
122	SLE RA 2	-5	-194	2063	8.69	-6.4	-0.02
122	SLE RA 3	0	-196	2082	8.75	0.31	0
122	SLE RA 4	-3	-195	2071	8.71	-3.72	-0.01
122	SLE RA 5	-5	-194	2063	8.69	-6.4	-0.02
122	SLE RA 6	0	-196	2082	8.75	0.31	0
122	SLE RA 7	-3	-195	2071	8.71	-3.72	-0.01
122	SLE RA 8	0	-196	2082	8.75	0.31	0
122	SLE RA 9	-3	-195	2071	8.71	-3.72	-0.01
122	SLE RA 10	-5	-238	2336	10.61	-6.31	-0.02
122	SLE RA 11	0	-239	2355	10.67	0.4	0
122	SLE RA 12	-3	-238	2343	10.63	-3.62	-0.01
122	SLE RA 13	-5	-238	2336	10.61	-6.31	-0.02
122	SLE RA 14	0	-239	2355	10.67	0.4	0
122	SLE RA 15	-3	-238	2343	10.63	-3.62	-0.01
122	SLE RA 16	0	-239	2355	10.67	0.4	0
122	SLE RA 17	-3	-238	2343	10.63	-3.62	-0.01
122	SLE RA 18	0	-258	2472	11.49	0.44	0
122	SLE RA 19	-3	-257	2460	11.45	-3.58	-0.01
122	SLE RA 20	0	-258	2472	11.49	0.44	0
122	SLE RA 21	-3	-257	2460	11.45	-3.58	-0.01
122	SLE FR 1	0	-196	2082	8.75	0.31	0
122	SLE FR 2	-1	-195	2078	8.74	-1.03	0
122	SLE FR 3	0	-196	2082	8.75	0.31	0
122	SLE FR 4	-1	-214	2195	9.56	-0.99	0
122	SLE FR 5	0	-215	2199	9.57	0.35	0
122	SLE FR 6	0	-227	2277	10.12	0.38	0
122	SLE QP 1	0	-196	2082	8.75	0.31	0
122	SLE QP 2	0	-215	2199	9.57	0.35	0
122	SLD 1	39	-109	2274	4.95	40.72	0.16
122	SLD 2	39	-109	2274	4.95	40.72	0.16
122	SLD 3	31	-227	2348	10.19	35.64	0.13
122	SLD 4	31	-227	2348	10.19	35.64	0.13
122	SLD 5	23	-3	2109	0.25	20.17	0.09
122	SLD 6	23	-3	2109	0.25	20.17	0.09
122	SLD 7	-2	-398	2356	17.7	3.23	0
122	SLD 8	-2	-398	2356	17.7	3.23	0
122	SLD 9	2	-31	2041	1.44	-2.53	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
122	SLD 10	2	-31	2041	1.44	-2.53	0
122	SLD 11	-23	-426	2289	18.9	-19.47	-0.08
122	SLD 12	-23	-426	2289		-19.47	-0.08
122	SLD 13	-31	-202	2050	8.95	-34.94	-0.13
122	SLD 14	-31	-202	2050	8.95	-34.94	-0.13
122	SLD 15	-39	-321	2124	14.19	-40.02	-0.16
122	SLD 16	-39	-321	2124	14.19	-40.02	-0.16
122	SLV 1	99	35	2378	-1.3	103.88	0.4
122	SLV 2	99	35	2378	-1.3	103.88	0.4
122	SLV 3	81	-244	2552	11.06	91.56	0.34
122	SLV 4	81	-244	2552	11.06	91.56	0.34
122	SLV 5	58	285	1988	-12.44	50.09	0.21
122	SLV 6	58	285	1988	-12.44	50.09	0.21
122	SLV 7	-3	-648	2569	28.76	9.03	0.01
122	SLV 8	-3	-648	2569	28.76	9.03	0.01
122	SLV 9	3	219	1829	-9.62	-8.33	-0.01
122	SLV 10	3	219	1829	-9.62	-8.33	-0.01
122	SLV 11	-57	-714	2409	31.58	-49.39	-0.21
122	SLV 12	-57	-714	2409	31.58	-49.39	-0.21
122	SLV 13	-81	-185	1846	8.09	-90.86	-0.34
122	SLV 14	-81	-185	1846	8.09	-90.86	-0.34
122	SLV 15	-99	-464	2020	20.45	-103.18	-0.4
122	SLV 16	-99	-464	2020	20.45	-103.18	-0.4
123	SLU 1	0	-348	1457	14.32	0.05	0
123	SLU 2	1	-349	1455	14.39	-2.22	0
123	SLU 3	0	-348	1457	14.32	0.05	0
123	SLU 4	0	-349	1456	14.36	-1.31	0
123	SLU 5	1	-349	1455	14.39	-2.22	0
123	SLU 6	0	-348	1457	14.32	0.05	0
123	SLU 7	0	-349	1456	14.36	-1.31	0
123	SLU 8	0	-348	1457	14.32	0.05	0
123	SLU 9	0	-349	1456	14.36	-1.31	0
123	SLU 10	1	-637	2112	26.21	-2.09	0
123	SLU 11	0	-637	2114	26.13	0.18	0
123	SLU 12	0	-637	2113	26.18	-1.18	0
123	SLU 13	1	-637	2112	26.21	-2.09	0
123	SLU 14	0	-637	2114	26.13	0.18	0
123	SLU 15	0	-637	2113	26.18	-1.18	0
123	SLU 16	0	-637	2114	26.13	0.18	0
123	SLU 17	0	-637	2113	26.18	-1.18	0
123	SLU 18	0	-760	2395	31.2	0.24	0
123	SLU 19	0	-761	2394	31.24	-1.12	0
123	SLU 20	0	-760	2395	31.2	0.24	0
123	SLU 21	0	-761	2394	31.24	-1.12	0
123	SLU 22	0	-491	1808	20.11	0.1	0
123	SLU 23	1	-492	1806	20.18	-2.16	0
123	SLU 24	0	-491	1808	20.11	0.1	0
123	SLU 25	0	-491	1807	20.15	-1.26	0
123	SLU 26	1	-492	1806	20.18	-2.16	0
123	SLU 27	0	-491	1808	20.11	0.1	0
123	SLU 28	0	-491	1807	20.15	-1.26	0
123	SLU 29	0	-491	1808	20.11	0.1	0
123	SLU 30	0	-491	1807	20.15	-1.26	0
123	SLU 31	1	-780	2463	32	-2.03	0
123	SLU 32	0	-779	2465	31.92	0.23	0
123	SLU 33	0	-780	2464	31.97	-1.13	0
123	SLU 34	1	-780	2463	32	-2.03	0
123	SLU 35	0	-779	2465	31.92	0.23	0
123	SLU 36	0	-780	2464	31.97	-1.13	0
123	SLU 37	0	-779	2465	31.92	0.23	0
123	SLU 38	0	-780	2464	31.97	-1.13	0
123	SLU 39	0	-902	2746	36.98	0.29	0
123	SLU 40	0	-903	2745	37.03	-1.07	0
123	SLU 41	0	-902	2746	36.98	0.29	0
123	SLU 42	0	-903	2745	37.03	-1.07	0
123	SLU 43	0	-404	1774	16.63	0.05	0
123	SLU 44	1	-405	1772	16.7	-2.22	0
123	SLU 45	0	-404	1774	16.63	0.05	0
123	SLU 46	0	-405	1773	16.67	-1.31	0
123	SLU 47	1	-405	1772	16.7	-2.22	0
123	SLU 48	0	-404	1774	16.63	0.05	0
123	SLU 49	0	-405	1773	16.67	-1.31	0
123	SLU 50	0	-404	1774	16.63	0.05	0
123	SLU 51	0	-405	1773	16.67	-1.31	0
123	SLU 52	1	-693	2429	28.52	-2.09	0
123	SLU 53	0	-692	2431	28.44	0.18	0
123	SLU 54	0	-693	2430	28.49	-1.18	0
123	SLU 55	1	-693	2429	28.52	-2.09	0
123	SLU 56	0	-692	2431	28.44	0.18	0
123	SLU 57	0	-693	2430	28.49	-1.18	0
123	SLU 58	0	-692	2431	28.44	0.18	0
123	SLU 59	0	-693	2430	28.49	-1.18	0
123	SLU 60	0	-816	2712	33.51	0.23	0
123	SLU 61	0	-816	2711	33.55	-1.13	0
123	SLU 62	0	-816	2712	33.51	0.23	0
123	SLU 63	0	-816	2711	33.55	-1.13	0
123	SLU 64	0	-547	2125	22.42	0.1	0
123	SLU 65	1	-548	2123	22.49	-2.17	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
123	SLU 66	0	-547	2125	22.42	0.1	0
123	SLU 67	0	-547	2124	22.46	-1.26	0
123	SLU 68	1	-548	2123	22.49	-2.17	0
123	SLU 69	0	-547	2125	22.42	0.1	0
123	SLU 70	0	-547	2124	22.46	-1.26	0
123	SLU 71	0	-547	2125	22.42	0.1	0
123	SLU 72	0	-547	2124	22.46	-1.26	0
123	SLU 73	1	-836	2780	34.31	-2.04	0
123	SLU 74	0	-835	2782	34.23	0.23	0
123	SLU 75	0	-835	2780	34.28	-1.13	0
123	SLU 76	1	-836	2780	34.31	-2.04	0
123	SLU 77	0	-835	2782	34.23	0.23	0
123	SLU 78	0	-835	2780	34.28	-1.13	0
123	SLU 79	0	-835	2782	34.23	0.23	0
123	SLU 80	0	-835	2780	34.28	-1.13	0
123	SLU 81	0	-958	3063	39.29	0.29	0
123	SLU 82	0	-959	3062	39.34	-1.07	0
123	SLU 83	0	-958	3063	39.29	0.29	0
123	SLU 84	0	-959	3062	39.34	-1.07	0
123	SLE RA 1	0	-389	1557	15.97	0.06	0
123	SLE RA 2	0	-390	1556	16.02	-1.45	0
123	SLE RA 3	0	-389	1557	15.97	0.06	0
123	SLE RA 4	0	-390	1557	16	-0.84	0
123	SLE RA 5	0	-390	1556	16.02	-1.45	0
123	SLE RA 6	0	-389	1557	15.97	0.06	0
123	SLE RA 7	0	-390	1557	16	-0.84	0
123	SLE RA 8	0	-389	1557	15.97	0.06	0
123	SLE RA 9	0	-390	1557	16	-0.84	0
123	SLE RA 10	0	-582	1994	23.9	-1.36	0
123	SLE RA 11	0	-581	1995	23.85	0.15	0
123	SLE RA 12	0	-582	1994	23.88	-0.75	0
123	SLE RA 13	0	-582	1994	23.9	-1.36	0
123	SLE RA 14	0	-581	1995	23.85	0.15	0
123	SLE RA 15	0	-582	1994	23.88	-0.75	0
123	SLE RA 16	0	-581	1995	23.85	0.15	0
123	SLE RA 17	0	-582	1994	23.88	-0.75	0
123	SLE RA 18	0	-664	2183	27.22	0.19	0
123	SLE RA 19	0	-664	2182	27.25	-0.72	0
123	SLE RA 20	0	-664	2183	27.22	0.19	0
123	SLE RA 21	0	-664	2182	27.25	-0.72	0
123	SLE FR 1	0	-389	1557	15.97	0.06	0
123	SLE FR 2	0	-389	1557	15.98	-0.24	0
123	SLE FR 3	0	-389	1557	15.97	0.06	0
123	SLE FR 4	0	-472	1745	19.36	-0.2	0
123	SLE FR 5	0	-471	1745	19.35	0.1	0
123	SLE FR 6	0	-526	1870	21.6	0.13	0
123	SLE QP 1	0	-389	1557	15.97	0.06	0
123	SLE QP 2	0	-471	1745	19.35	0.1	0
123	SLD 1	-4	-351	1747	13.64	10.37	0.01
123	SLD 2	-4	-351	1747	13.64	10.37	0.01
123	SLD 3	-3	-516	1711	28.77	11.25	0.01
123	SLD 4	-3	-516	1711	28.77	11.25	0.01
123	SLD 5	-3	-186	1801	-5.31	1.85	0.01
123	SLD 6	-3	-186	1801	-5.31	1.85	0.01
123	SLD 7	0	-734	1680	45.12	4.78	0
123	SLD 8	0	-734	1680	45.12	4.78	0
123	SLD 9	-1	-209	1810	-6.43	-4.57	0
123	SLD 10	-1	-209	1810	-6.43	-4.57	0
123	SLD 11	2	-757	1689	44.01	-1.65	-0.01
123	SLD 12	2	-757	1689	44.01	-1.65	-0.01
123	SLD 13	3	-427	1779	9.92	-11.05	-0.01
123	SLD 14	3	-427	1779	9.92	-11.05	-0.01
123	SLD 15	4	-592	1743	25.05	-10.17	-0.01
123	SLD 16	4	-592	1743	25.05	-10.17	-0.01
123	SLV 1	-10	-179	1752	4.6	31.93	0.04
123	SLV 2	-10	-179	1752	4.6	31.93	0.04
123	SLV 3	-7	-583	1660	43.11	34.19	0.03
123	SLV 4	-7	-583	1660	43.11	34.19	0.03
123	SLV 5	-6	228	1888	-43.48	6.22	0.02
123	SLV 6	-6	228	1888	-43.48	6.22	0.02
123	SLV 7	1	-1117	1579	84.88	13.75	0
123	SLV 8	1	-1117	1579	84.88	13.75	0
123	SLV 9	-1	174	1911	-46.18	-13.55	0
123	SLV 10	-1	174	1911	-46.18	-13.55	0
123	SLV 11	6	-1171	1602	82.17	-6.02	-0.02
123	SLV 12	6	-1171	1602	82.17	-6.02	-0.02
123	SLV 13	7	-360	1830	-4.42	-33.99	-0.03
123	SLV 14	7	-360	1830	-4.42	-33.99	-0.03
123	SLV 15	9	-764	1738	34.09	-31.73	-0.04
123	SLV 16	9	-764	1738	34.09	-31.73	-0.04
124	SLU 1	0	-240	2110	10.51	-0.38	0
124	SLU 2	-1	-243	2130	10.66	-2.36	0
124	SLU 3	0	-240	2110	10.51	-0.38	0
124	SLU 4	-1	-242	2122	10.6	-1.57	0
124	SLU 5	-1	-243	2130	10.66	-2.36	0
124	SLU 6	0	-240	2110	10.51	-0.38	0
124	SLU 7	-1	-242	2122	10.6	-1.57	0
124	SLU 8	0	-240	2110	10.51	-0.38	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
124	SLU 9	-1	-242	2122	10.6	-1.57	0
124	SLU 10	-1	-279	2512	12.63	-2.65	0
124	SLU 11	0	-275	2493	12.47	-0.66	0
124	SLU 12	-1	-278	2505	12.57	-1.85	0
124	SLU 13	-1	-279	2512	12.63	-2.65	0
124	SLU 14	0	-275	2493	12.47	-0.66	0
124	SLU 15	-1	-278	2505	12.57	-1.85	0
124	SLU 16	0	-275	2493	12.47	-0.66	0
124	SLU 17	-1	-278	2505	12.57	-1.85	0
124	SLU 18	0	-291	2657	13.31	-0.78	0
124	SLU 19	-1	-293	2669	13.41	-1.98	0
124	SLU 20	0	-291	2657	13.31	-0.78	0
124	SLU 21	-1	-293	2669	13.41	-1.98	0
124	SLU 22	0	-266	2312	11.79	-0.49	0
124	SLU 23	-1	-269	2331	11.94	-2.48	0
124	SLU 24	0	-266	2312	11.79	-0.49	0
124	SLU 25	-1	-268	2323	11.88	-1.69	0
124	SLU 26	-1	-269	2331	11.94	-2.48	0
124	SLU 27	0	-266	2312	11.79	-0.49	0
124	SLU 28	-1	-268	2323	11.88	-1.69	0
124	SLU 29	0	-266	2312	11.79	-0.49	0
124	SLU 30	-1	-268	2323	11.88	-1.69	0
124	SLU 31	-1	-305	2714	13.91	-2.77	0
124	SLU 32	0	-302	2694	13.75	-0.78	0
124	SLU 33	-1	-304	2706	13.85	-1.97	0
124	SLU 34	-1	-305	2714	13.91	-2.77	0
124	SLU 35	0	-302	2694	13.75	-0.78	0
124	SLU 36	-1	-304	2706	13.85	-1.97	0
124	SLU 37	0	-302	2694	13.75	-0.78	0
124	SLU 38	-1	-304	2706	13.85	-1.97	0
124	SLU 39	0	-317	2859	14.59	-0.9	0
124	SLU 40	-1	-319	2870	14.69	-2.09	0
124	SLU 41	0	-317	2859	14.59	-0.9	0
124	SLU 42	-1	-319	2870	14.69	-2.09	0
124	SLU 43	0	-302	2674	13.22	-0.45	0
124	SLU 44	-1	-306	2693	13.38	-2.43	0
124	SLU 45	0	-302	2674	13.22	-0.45	0
124	SLU 46	-1	-305	2686	13.31	-1.64	0
124	SLU 47	-1	-306	2693	13.38	-2.43	0
124	SLU 48	0	-302	2674	13.22	-0.45	0
124	SLU 49	-1	-305	2686	13.31	-1.64	0
124	SLU 50	0	-302	2674	13.22	-0.45	0
124	SLU 51	-1	-305	2686	13.31	-1.64	0
124	SLU 52	-1	-342	3076	15.34	-2.72	0
124	SLU 53	0	-338	3057	15.19	-0.73	0
124	SLU 54	-1	-340	3069	15.28	-1.93	0
124	SLU 55	-1	-342	3076	15.34	-2.72	0
124	SLU 56	0	-338	3057	15.19	-0.73	0
124	SLU 57	-1	-340	3069	15.28	-1.93	0
124	SLU 58	0	-338	3057	15.19	-0.73	0
124	SLU 59	-1	-340	3069	15.28	-1.93	0
124	SLU 60	0	-354	3221	16.03	-0.86	0
124	SLU 61	-1	-356	3233	16.12	-2.05	0
124	SLU 62	0	-354	3221	16.03	-0.86	0
124	SLU 63	-1	-356	3233	16.12	-2.05	0
124	SLU 64	0	-329	2875	14.5	-0.57	0
124	SLU 65	-1	-332	2895	14.66	-2.55	0
124	SLU 66	0	-329	2875	14.5	-0.57	0
124	SLU 67	-1	-331	2887	14.59	-1.76	0
124	SLU 68	-1	-332	2895	14.66	-2.55	0
124	SLU 69	0	-329	2875	14.5	-0.57	0
124	SLU 70	-1	-331	2887	14.59	-1.76	0
124	SLU 71	0	-329	2875	14.5	-0.57	0
124	SLU 72	-1	-331	2887	14.59	-1.76	0
124	SLU 73	-1	-368	3278	16.62	-2.84	0
124	SLU 74	0	-365	3258	16.47	-0.85	0
124	SLU 75	-1	-367	3270	16.56	-2.04	0
124	SLU 76	-1	-368	3278	16.62	-2.84	0
124	SLU 77	0	-365	3258	16.47	-0.85	0
124	SLU 78	-1	-367	3270	16.56	-2.04	0
124	SLU 79	0	-365	3258	16.47	-0.85	0
124	SLU 80	-1	-367	3270	16.56	-2.04	0
124	SLU 81	0	-380	3422	17.31	-0.97	0
124	SLU 82	-1	-382	3434	17.4	-2.17	0
124	SLU 83	0	-380	3422	17.31	-0.97	0
124	SLU 84	-1	-382	3434	17.4	-2.17	0
124	SLE RA 1	0	-247	2168	10.87	-0.41	0
124	SLE RA 2	-1	-249	2181	10.98	-1.73	0
124	SLE RA 3	0	-247	2168	10.87	-0.41	0
124	SLE RA 4	0	-249	2175	10.94	-1.2	0
124	SLE RA 5	-1	-249	2181	10.98	-1.73	0
124	SLE RA 6	0	-247	2168	10.87	-0.41	0
124	SLE RA 7	0	-249	2175	10.94	-1.2	0
124	SLE RA 8	0	-247	2168	10.87	-0.41	0
124	SLE RA 9	0	-249	2175	10.94	-1.2	0
124	SLE RA 10	-1	-273	2436	12.29	-1.92	0
124	SLE RA 11	0	-271	2423	12.18	-0.6	0
124	SLE RA 12	0	-272	2431	12.25	-1.39	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
124	SLE RA 13	-1	-273	2436	12.29	-1.92	0
124	SLE RA 14	0	-271	2423	12.18	-0.6	0
124	SLE RA 15	0	-272	2431	12.25	-1.39	0
124	SLE RA 16	0	-271	2423	12.18	-0.6	0
124	SLE RA 17	0	-272	2431	12.25	-1.39	0
124	SLE RA 18	0	-281	2532	12.74	-0.68	0
124	SLE RA 19	-1	-283	2540	12.81	-1.48	0
124	SLE RA 20	0	-281	2532	12.74	-0.68	0
124	SLE RA 21	-1	-283	2540	12.81	-1.48	0
124	SLE FR 1	0	-247	2168	10.87	-0.41	0
124	SLE FR 2	0	-248	2170	10.89	-0.67	0
124	SLE FR 3	0	-247	2168	10.87	-0.41	0
124	SLE FR 4	0	-258	2280	11.46	-0.76	0
124	SLE FR 5	0	-257	2277	11.44	-0.49	0
124	SLE FR 6	0	-264	2350	11.81	-0.55	0
124	SLE QP 1	0	-247	2168	10.87	-0.41	0
124	SLE QP 2	0	-257	2277	11.44	-0.49	0
124	SLD 1	18	-121	2087	5.55	30.15	0.01
124	SLD 2	18	-121	2087	5.55	30.15	0.01
124	SLD 3	25	-267	2173	11.9	35.26	0
124	SLD 4	25	-267	2173	11.9	35.26	0
124	SLD 5	-5	4	2089	0.03	0.96	0.01
124	SLD 6	-5	4	2089	0.03	0.96	0.01
124	SLD 7	17	-481	2377	21.21	17.98	-0.01
124	SLD 8	17	-481	2377	21.21	17.98	-0.01
124	SLD 9	-18	-34	2177	1.66	-18.96	0.01
124	SLD 10	-18	-34	2177	1.66	-18.96	0.01
124	SLD 11	5	-519	2465	22.84	-1.94	-0.01
124	SLD 12	5	-519	2465	22.84	-1.94	-0.01
124	SLD 13	-25	-248	2381	10.97	-36.24	-0.01
124	SLD 14	-25	-248	2381	10.97	-36.24	-0.01
124	SLD 15	-18	-393	2467	17.32	-31.13	-0.01
124	SLD 16	-18	-393	2467	17.32	-31.13	-0.01
124	SLV 1	46	66	1823	-2.56	79.47	0.03
124	SLV 2	46	66	1823	-2.56	79.47	0.03
124	SLV 3	63	-278	2029	12.42	92.34	0.01
124	SLV 4	63	-278	2029	12.42	92.34	0.01
124	SLV 5	-11	360	1829	-15.49	3.99	0.03
124	SLV 6	-11	360	1829	-15.49	3.99	0.03
124	SLV 7	44	-784	2514	34.46	46.87	-0.02
124	SLV 8	44	-784	2514	34.46	46.87	-0.02
124	SLV 9	-44	269	2040	-11.59	-47.85	0.02
124	SLV 10	-44	269	2040	-11.59	-47.85	0.02
124	SLV 11	11	-875	2725	38.36	-4.97	-0.03
124	SLV 12	11	-875	2725	38.36	-4.97	-0.03
124	SLV 13	-63	-237	2525	10.45	-93.32	-0.01
124	SLV 14	-63	-237	2525	10.45	-93.32	-0.01
124	SLV 15	-47	-580	2731	25.43	-80.46	-0.03
124	SLV 16	-47	-580	2731	25.43	-80.46	-0.03
125	SLU 1	0	-267	2101	11.75	0.42	0
125	SLU 2	-4	-263	2068	11.52	-6.37	-0.01
125	SLU 3	0	-267	2101	11.75	0.42	0
125	SLU 4	-2	-264	2081	11.61	-3.65	0
125	SLU 5	-4	-263	2068	11.52	-6.37	-0.01
125	SLU 6	0	-267	2101	11.75	0.42	0
125	SLU 7	-2	-264	2081	11.61	-3.65	0
125	SLU 8	0	-267	2101	11.75	0.42	0
125	SLU 9	-2	-264	2081	11.61	-3.65	0
125	SLU 10	-4	-343	2498	15.08	-6.21	-0.01
125	SLU 11	0	-348	2530	15.32	0.59	0.01
125	SLU 12	-2	-345	2511	15.18	-3.49	0
125	SLU 13	-4	-343	2498	15.08	-6.21	-0.01
125	SLU 14	0	-348	2530	15.32	0.59	0.01
125	SLU 15	-2	-345	2511	15.18	-3.49	0
125	SLU 16	0	-348	2530	15.32	0.59	0.01
125	SLU 17	-2	-345	2511	15.18	-3.49	0
125	SLU 18	0	-382	2714	16.85	0.66	0.01
125	SLU 19	-2	-380	2695	16.7	-3.42	0
125	SLU 20	0	-382	2714	16.85	0.66	0.01
125	SLU 21	-2	-380	2695	16.7	-3.42	0
125	SLU 22	0	-312	2322	13.72	0.5	0.01
125	SLU 23	-4	-308	2290	13.49	-6.3	-0.01
125	SLU 24	0	-312	2322	13.72	0.5	0.01
125	SLU 25	-2	-309	2303	13.58	-3.58	0
125	SLU 26	-4	-308	2290	13.49	-6.3	-0.01
125	SLU 27	0	-312	2322	13.72	0.5	0.01
125	SLU 28	-2	-309	2303	13.58	-3.58	0
125	SLU 29	0	-312	2322	13.72	0.5	0.01
125	SLU 30	-2	-309	2303	13.58	-3.58	0
125	SLU 31	-4	-389	2719	17.05	-6.13	-0.01
125	SLU 32	0	-393	2752	17.29	0.66	0.01
125	SLU 33	-2	-390	2732	17.15	-3.42	0
125	SLU 34	-4	-389	2719	17.05	-6.13	-0.01
125	SLU 35	0	-393	2752	17.29	0.66	0.01
125	SLU 36	-2	-390	2732	17.15	-3.42	0
125	SLU 37	0	-393	2752	17.29	0.66	0.01
125	SLU 38	-2	-390	2732	17.15	-3.42	0
125	SLU 39	0	-427	2936	18.82	0.73	0.01





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
125	SLU 40	-2	-425	2916	18.67	-3.35	0
125	SLU 41	0	-427	2936	18.82	0.73	0.01
125	SLU 42	-2	-425	2916	18.67	-3.35	0
125	SLU 43	0	-331	2655	14.6	0.52	0.01
125	SLU 44	-4	-327	2623	14.37	-6.27	-0.01
125	SLU 45	0	-331	2655	14.6	0.52	0.01
125	SLU 46	-2	-329	2636	14.46	-3.55	0
125	SLU 47	-4	-327	2623	14.37	-6.27	-0.01
125	SLU 48	0	-331	2655	14.6	0.52	0.01
125	SLU 49	-2	-329	2636	14.46	-3.55	0
125	SLU 50	0	-331	2655	14.6	0.52	0.01
125	SLU 51	-2	-329	2636	14.46	-3.55	0
125	SLU 52	-3	-408	3052	17.93	-6.11	-0.01
125	SLU 53	0	-412	3085	18.17	0.69	0.01
125	SLU 54	-2	-410	3065	18.03	-3.39	0
125	SLU 55	-3	-408	3052	17.93	-6.11	-0.01
125	SLU 56	0	-412	3085	18.17	0.69	0.01
125	SLU 57	-2	-410	3065	18.03	-3.39	0
125	SLU 58	0	-412	3085	18.17	0.69	0.01
125	SLU 59	-2	-410	3065	18.03	-3.39	0
125	SLU 60	0	-447	3269	19.7	0.76	0.01
125	SLU 61	-2	-444	3249	19.55	-3.32	0
125	SLU 62	0	-447	3269	19.7	0.76	0.01
125	SLU 63	-2	-444	3249	19.55	-3.32	0
125	SLU 64	0	-377	2877	16.57	0.6	0.01
125	SLU 65	-4	-372	2844	16.34	-6.2	-0.01
125	SLU 66	0	-377	2877	16.57	0.6	0.01
125	SLU 67	-2	-374	2857	16.43	-3.48	0
125	SLU 68	-4	-372	2844	16.34	-6.2	-0.01
125	SLU 69	0	-377	2877	16.57	0.6	0.01
125	SLU 70	-2	-374	2857	16.43	-3.48	0
125	SLU 71	0	-377	2877	16.57	0.6	0.01
125	SLU 72	-2	-374	2857	16.43	-3.48	0
125	SLU 73	-3	-453	3273	19.9	-6.03	-0.01
125	SLU 74	0	-457	3306	20.14	0.76	0.01
125	SLU 75	-2	-455	3286	20	-3.31	0
125	SLU 76	-3	-453	3273	19.9	-6.03	-0.01
125	SLU 77	0	-457	3306	20.14	0.76	0.01
125	SLU 78	-2	-455	3286	20	-3.31	0
125	SLU 79	0	-457	3306	20.14	0.76	0.01
125	SLU 80	-2	-455	3286	20	-3.31	0
125	SLU 81	0	-492	3490	21.67	0.83	0.01
125	SLU 82	-2	-489	3470	21.52	-3.24	0
125	SLU 83	0	-492	3490	21.67	0.83	0.01
125	SLU 84	-2	-489	3470	21.52	-3.24	0
125	SLE RA 1	0	-280	2164	12.32	0.44	0.01
125	SLE RA 2	-2	-277	2142	12.16	-4.09	-0.01
125	SLE RA 3	0	-280	2164	12.32	0.44	0.01
125	SLE RA 4	-1	-278	2151	12.22	-2.27	0
125	SLE RA 5	-2	-277	2142	12.16	-4.09	-0.01
125	SLE RA 6	0	-280	2164	12.32	0.44	0.01
125	SLE RA 7	-1	-278	2151	12.22	-2.27	0
125	SLE RA 8	0	-280	2164	12.32	0.44	0.01
125	SLE RA 9	-1	-278	2151	12.22	-2.27	0
125	SLE RA 10	-2	-331	2429	14.53	-3.98	0
125	SLE RA 11	0	-334	2450	14.69	0.55	0.01
125	SLE RA 12	-1	-332	2437	14.6	-2.16	0
125	SLE RA 13	-2	-331	2429	14.53	-3.98	0
125	SLE RA 14	0	-334	2450	14.69	0.55	0.01
125	SLE RA 15	-1	-332	2437	14.6	-2.16	0
125	SLE RA 16	0	-334	2450	14.69	0.55	0.01
125	SLE RA 17	-1	-332	2437	14.6	-2.16	0
125	SLE RA 18	0	-357	2573	15.71	0.6	0.01
125	SLE RA 19	-1	-355	2560	15.62	-2.12	0
125	SLE RA 20	0	-357	2573	15.71	0.6	0.01
125	SLE RA 21	-1	-355	2560	15.62	-2.12	0
125	SLE FR 1	0	-280	2164	12.32	0.44	0.01
125	SLE FR 2	0	-279	2160	12.29	-0.46	0
125	SLE FR 3	0	-280	2164	12.32	0.44	0.01
125	SLE FR 4	0	-302	2282	13.3	-0.42	0
125	SLE FR 5	0	-303	2287	13.34	0.49	0.01
125	SLE FR 6	0	-318	2369	14.01	0.52	0.01
125	SLE QP 1	0	-280	2164	12.32	0.44	0.01
125	SLE QP 2	0	-303	2287	13.34	0.49	0.01
125	SLD 1	24	-208	2368	12.65	28.02	0.09
125	SLD 2	24	-208	2368	12.65	28.02	0.09
125	SLD 3	15	-318	2475	17.53	23.54	0.07
125	SLD 4	15	-318	2475	17.53	23.54	0.07
125	SLD 5	20	-108	2148	5.73	15.55	0.06
125	SLD 6	20	-108	2148	5.73	15.55	0.06
125	SLD 7	-8	-474	2507	22	0.6	0
125	SLD 8	-8	-474	2507	22	0.6	0
125	SLD 9	9	-132	2067	4.68	0.38	0.01
125	SLD 10	9	-132	2067	4.68	0.38	0.01
125	SLD 11	-19	-498	2426	20.94	-14.57	-0.05
125	SLD 12	-19	-498	2426	20.94	-14.57	-0.05
125	SLD 13	-15	-288	2098	9.14	-22.55	-0.06
125	SLD 14	-15	-288	2098	9.14	-22.55	-0.06



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
125	SLD 15	-23	-398	2206	14.02	-27.04	-0.08
125	SLD 16	-23	-398	2206	14.02	-27.04	-0.08
125	SLV 1	59	-78	2479	11.73	70.95	0.22
125	SLV 2	59	-78	2479	11.73	70.95	0.22
125	SLV 3	39	-337	2732	23.26	60.23	0.18
125	SLV 4	39	-337	2732	23.26	60.23	0.18
125	SLV 5	48	157	1961	-4.62	37.89	0.14
125	SLV 6	48	157	1961	-4.62	37.89	0.14
125	SLV 7	-18	-706	2804	33.78	2.15	-0.01
125	SLV 8	-18	-706	2804	33.78	2.15	-0.01
125	SLV 9	19	100	1769	-7.11	-1.17	0.02
125	SLV 10	19	100	1769	-7.11	-1.17	0.02
125	SLV 11	-47	-763	2613	31.29	-36.91	-0.13
125	SLV 12	-47	-763	2613	31.29	-36.91	-0.13
125	SLV 13	-39	-268	1841	3.42	-59.25	-0.17
125	SLV 14	-39	-268	1841	3.42	-59.25	-0.17
125	SLV 15	-59	-527	2094	14.94	-69.97	-0.21
125	SLV 16	-59	-527	2094	14.94	-69.97	-0.21
126	SLU 1	0	-367	1296	14.08	0.01	0
126	SLU 2	2	-367	1296	14.02	-0.78	0
126	SLU 3	0	-367	1296	14.08	0.01	0
126	SLU 4	1	-367	1296	14.05	-0.46	0
126	SLU 5	2	-367	1296	14.02	-0.78	0
126	SLU 6	0	-367	1296	14.08	0.01	0
126	SLU 7	1	-367	1296	14.05	-0.46	0
126	SLU 8	0	-367	1296	14.08	0.01	0
126	SLU 9	1	-367	1296	14.05	-0.46	0
126	SLU 10	2	-637	1795	24.07	-0.73	0
126	SLU 11	0	-637	1795	24.12	0.06	0
126	SLU 12	1	-637	1795	24.09	-0.41	0
126	SLU 13	2	-637	1795	24.07	-0.73	0
126	SLU 14	0	-637	1795	24.12	0.06	0
126	SLU 15	1	-637	1795	24.09	-0.41	0
126	SLU 16	0	-637	1795	24.12	0.06	0
126	SLU 17	1	-637	1795	24.09	-0.41	0
126	SLU 18	0	-753	2009	28.43	0.08	0
126	SLU 19	1	-753	2009	28.4	-0.39	0
126	SLU 20	0	-753	2009	28.43	0.08	0
126	SLU 21	1	-753	2009	28.4	-0.39	0
126	SLU 22	0	-509	1565	19.38	0.03	0
126	SLU 23	2	-508	1565	19.33	-0.76	0
126	SLU 24	0	-509	1565	19.38	0.03	0
126	SLU 25	1	-508	1565	19.35	-0.44	0
126	SLU 26	2	-508	1565	19.33	-0.76	0
126	SLU 27	0	-509	1565	19.38	0.03	0
126	SLU 28	1	-508	1565	19.35	-0.44	0
126	SLU 29	0	-509	1565	19.38	0.03	0
126	SLU 30	1	-508	1565	19.35	-0.44	0
126	SLU 31	2	-778	2065	29.38	-0.71	0
126	SLU 32	0	-779	2065	29.43	0.08	0
126	SLU 33	1	-778	2065	29.4	-0.4	0
126	SLU 34	2	-778	2065	29.38	-0.71	0
126	SLU 35	0	-779	2065	29.43	0.08	0
126	SLU 36	1	-778	2065	29.4	-0.4	0
126	SLU 37	0	-779	2065	29.43	0.08	0
126	SLU 38	1	-778	2065	29.4	-0.4	0
126	SLU 39	0	-894	2279	33.73	0.1	0
126	SLU 40	1	-894	2279	33.7	-0.38	0
126	SLU 41	0	-894	2279	33.73	0.1	0
126	SLU 42	1	-894	2279	33.7	-0.38	0
126	SLU 43	0	-429	1592	16.48	0.01	0
126	SLU 44	2	-429	1592	16.43	-0.78	0
126	SLU 45	0	-429	1592	16.48	0.01	0
126	SLU 46	1	-429	1592	16.45	-0.46	0
126	SLU 47	2	-429	1592	16.43	-0.78	0
126	SLU 48	0	-429	1592	16.48	0.01	0
126	SLU 49	1	-429	1592	16.45	-0.46	0
126	SLU 50	0	-429	1592	16.48	0.01	0
126	SLU 51	1	-429	1592	16.45	-0.46	0
126	SLU 52	2	-699	2091	26.47	-0.73	0
126	SLU 53	0	-699	2092	26.53	0.06	0
126	SLU 54	1	-699	2091	26.5	-0.42	0
126	SLU 55	2	-699	2091	26.47	-0.73	0
126	SLU 56	0	-699	2092	26.53	0.06	0
126	SLU 57	1	-699	2091	26.5	-0.42	0
126	SLU 58	0	-699	2092	26.53	0.06	0
126	SLU 59	1	-699	2091	26.5	-0.42	0
126	SLU 60	0	-815	2306	30.83	0.08	0
126	SLU 61	1	-815	2306	30.8	-0.4	0
126	SLU 62	0	-815	2306	30.83	0.08	0
126	SLU 63	1	-815	2306	30.8	-0.4	0
126	SLU 64	0	-570	1862	21.79	0.03	0
126	SLU 65	2	-570	1861	21.73	-0.76	0
126	SLU 66	0	-570	1862	21.79	0.03	0
126	SLU 67	1	-570	1861	21.76	-0.45	0
126	SLU 68	2	-570	1861	21.73	-0.76	0
126	SLU 69	0	-570	1862	21.79	0.03	0
126	SLU 70	1	-570	1861	21.76	-0.45	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
126	SLU 71	0	-570	1862	21.79	0.03	0
126	SLU 72	1	-570	1861	21.76	-0.45	0
126	SLU 73	2	-840	2361	31.78	-0.72	0
126	SLU 74	0	-840	2361	31.83	0.08	0
126	SLU 75	1	-840	2361	31.8	-0.4	0
126	SLU 76	2	-840	2361	31.78	-0.72	0
126	SLU 77	0	-840	2361	31.83	0.08	0
126	SLU 78	1	-840	2361	31.8	-0.4	0
126	SLU 79	0	-840	2361	31.83	0.08	0
126	SLU 80	1	-840	2361	31.8	-0.4	0
126	SLU 81	0	-956	2575	36.14	0.1	0
126	SLU 82	1	-956	2575	36.11	-0.38	0
126	SLU 83	0	-956	2575	36.14	0.1	0
126	SLU 84	1	-956	2575	36.11	-0.38	0
126	SLE RA 1	0	-408	1373	15.59	0.02	0
126	SLE RA 2	2	-407	1373	15.56	-0.51	0
126	SLE RA 3	0	-408	1373	15.59	0.02	0
126	SLE RA 4	1	-407	1373	15.57	-0.3	0
126	SLE RA 5	2	-407	1373	15.56	-0.51	0
126	SLE RA 6	0	-408	1373	15.59	0.02	0
126	SLE RA 7	1	-407	1373	15.57	-0.3	0
126	SLE RA 8	0	-408	1373	15.59	0.02	0
126	SLE RA 9	1	-407	1373	15.57	-0.3	0
126	SLE RA 10	1	-587	1706	22.26	-0.48	0
126	SLE RA 11	0	-588	1706	22.29	0.05	0
126	SLE RA 12	1	-588	1706	22.27	-0.27	0
126	SLE RA 13	1	-587	1706	22.26	-0.48	0
126	SLE RA 14	0	-588	1706	22.29	0.05	0
126	SLE RA 15	1	-588	1706	22.27	-0.27	0
126	SLE RA 16	0	-588	1706	22.29	0.05	0
126	SLE RA 17	1	-588	1706	22.27	-0.27	0
126	SLE RA 18	0	-665	1848	25.16	0.06	0
126	SLE RA 19	1	-665	1848	25.14	-0.25	0
126	SLE RA 20	0	-665	1848	25.16	0.06	0
126	SLE RA 21	1	-665	1848	25.14	-0.25	0
126	SLE FR 1	0	-408	1373	15.59	0.02	0
126	SLE FR 2	0	-408	1373	15.59	-0.09	0
126	SLE FR 3	0	-408	1373	15.59	0.02	0
126	SLE FR 4	0	-485	1515	18.46	-0.07	0
126	SLE FR 5	0	-485	1515	18.46	0.03	0
126	SLE FR 6	0	-536	1611	20.38	0.04	0
126	SLE QP 1	0	-408	1373	15.59	0.02	0
126	SLE QP 2	0	-485	1515	18.46	0.03	0
126	SLD 1	-10	-514	1513	22.53	4.23	0.02
126	SLD 2	-10	-514	1513	22.53	4.23	0.02
126	SLD 3	-9	-382	1485	11	4.76	0.02
126	SLD 4	-9	-382	1485	11	4.76	0.02
126	SLD 5	-4	-694	1557	37.17	0.49	0
126	SLD 6	-4	-694	1557	37.17	0.49	0
126	SLD 7	-2	-254	1463	-1.26	2.25	0.01
126	SLD 8	-2	-254	1463	-1.26	2.25	0.01
126	SLD 9	1	-716	1567	38.19	-2.19	-0.01
126	SLD 10	1	-716	1567	38.19	-2.19	-0.01
126	SLD 11	4	-276	1473	-0.24	-0.42	0
126	SLD 12	4	-276	1473	-0.24	-0.42	0
126	SLD 13	9	-587	1546	25.92	-4.69	-0.02
126	SLD 14	9	-587	1546	25.92	-4.69	-0.02
126	SLD 15	9	-455	1518	14.39	-4.16	-0.02
126	SLD 16	9	-455	1518	14.39	-4.16	-0.02
126	SLV 1	-29	-557	1510	29.01	12.93	0.05
126	SLV 2	-29	-557	1510	29.01	12.93	0.05
126	SLV 3	-27	-241	1442	-0.16	14.27	0.05
126	SLV 4	-27	-241	1442	-0.16	14.27	0.05
126	SLV 5	-11	-987	1616	65.86	1.87	0.01
126	SLV 6	-11	-987	1616	65.86	1.87	0.01
126	SLV 7	-6	69	1391	-31.36	6.34	0.02
126	SLV 8	-6	69	1391	-31.36	6.34	0.02
126	SLV 9	5	-1039	1640	68.29	-6.27	-0.02
126	SLV 10	5	-1039	1640	68.29	-6.27	-0.02
126	SLV 11	11	17	1414	-28.94	-1.8	-0.01
126	SLV 12	11	17	1414	-28.94	-1.8	-0.01
126	SLV 13	27	-729	1588	37.08	-14.2	-0.05
126	SLV 14	27	-729	1588	37.08	-14.2	-0.05
126	SLV 15	29	-412	1521	7.91	-12.86	-0.05
126	SLV 16	29	-412	1521	7.91	-12.86	-0.05
127	SLU 1	0	-302	2130	12.74	-0.47	0
127	SLU 2	-1	-306	2151	12.91	-1.77	0
127	SLU 3	0	-302	2130	12.74	-0.47	0
127	SLU 4	0	-305	2142	12.84	-1.25	0
127	SLU 5	-1	-306	2151	12.91	-1.77	0
127	SLU 6	0	-302	2130	12.74	-0.47	0
127	SLU 7	0	-305	2142	12.84	-1.25	0
127	SLU 8	0	-302	2130	12.74	-0.47	0
127	SLU 9	0	-305	2142	12.84	-1.25	0
127	SLU 10	-1	-351	2557	14.65	-2	0
127	SLU 11	0	-347	2536	14.48	-0.69	0
127	SLU 12	-1	-350	2549	14.58	-1.48	0
127	SLU 13	-1	-351	2557	14.65	-2	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
127	SLU 14	0	-347	2536	14.48	-0.69	0
127	SLU 15	-1	-350	2549	14.58	-1.48	0
127	SLU 16	0	-347	2536	14.48	-0.69	0
127	SLU 17	-1	-350	2549	14.58	-1.48	0
127	SLU 18	0	-367	2711	15.23	-0.79	0
127	SLU 19	-1	-369	2723	15.33	-1.57	0
127	SLU 20	0	-367	2711	15.23	-0.79	0
127	SLU 21	-1	-369	2723	15.33	-1.57	0
127	SLU 22	0	-334	2338	14.02	-0.57	0
127	SLU 23	-1	-338	2358	14.18	-1.87	0
127	SLU 24	0	-334	2338	14.02	-0.57	0
127	SLU 25	0	-337	2350	14.12	-1.35	0
127	SLU 26	-1	-338	2358	14.18	-1.87	0
127	SLU 27	0	-334	2338	14.02	-0.57	0
127	SLU 28	0	-337	2350	14.12	-1.35	0
127	SLU 29	0	-334	2338	14.02	-0.57	0
127	SLU 30	0	-337	2350	14.12	-1.35	0
127	SLU 31	-1	-383	2765	15.93	-2.09	-0.01
127	SLU 32	0	-379	2744	15.76	-0.79	0
127	SLU 33	-1	-382	2756	15.86	-1.57	0
127	SLU 34	-1	-383	2765	15.93	-2.09	-0.01
127	SLU 35	0	-379	2744	15.76	-0.79	0
127	SLU 36	-1	-382	2756	15.86	-1.57	0
127	SLU 37	0	-379	2744	15.76	-0.79	0
127	SLU 38	-1	-382	2756	15.86	-1.57	0
127	SLU 39	0	-399	2918	16.5	-0.89	-0.01
127	SLU 40	-1	-401	2931	16.61	-1.67	-0.01
127	SLU 41	0	-399	2918	16.5	-0.89	-0.01
127	SLU 42	-1	-401	2931	16.61	-1.67	-0.01
127	SLU 43	0	-382	2698	16.12	-0.58	0
127	SLU 44	-1	-386	2718	16.29	-1.88	0
127	SLU 45	0	-382	2698	16.12	-0.58	0
127	SLU 46	-1	-384	2710	16.23	-1.36	0
127	SLU 47	-1	-386	2718	16.29	-1.88	0
127	SLU 48	0	-382	2698	16.12	-0.58	0
127	SLU 49	-1	-384	2710	16.23	-1.36	0
127	SLU 50	0	-382	2698	16.12	-0.58	0
127	SLU 51	-1	-384	2710	16.23	-1.36	0
127	SLU 52	-1	-431	3125	18.03	-2.11	-0.01
127	SLU 53	0	-427	3104	17.87	-0.8	-0.01
127	SLU 54	-1	-429	3117	17.97	-1.58	-0.01
127	SLU 55	-1	-431	3125	18.03	-2.11	-0.01
127	SLU 56	0	-427	3104	17.87	-0.8	-0.01
127	SLU 57	-1	-429	3117	17.97	-1.58	-0.01
127	SLU 58	0	-427	3104	17.87	-0.8	-0.01
127	SLU 59	-1	-429	3117	17.97	-1.58	-0.01
127	SLU 60	0	-446	3278	18.61	-0.9	-0.01
127	SLU 61	-1	-449	3291	18.71	-1.68	-0.01
127	SLU 62	0	-446	3278	18.61	-0.9	-0.01
127	SLU 63	-1	-449	3291	18.71	-1.68	-0.01
127	SLU 64	0	-414	2906	17.4	-0.67	0
127	SLU 65	-1	-418	2926	17.57	-1.98	-0.01
127	SLU 66	0	-414	2906	17.4	-0.67	0
127	SLU 67	-1	-416	2918	17.5	-1.46	-0.01
127	SLU 68	-1	-418	2926	17.57	-1.98	-0.01
127	SLU 69	0	-414	2906	17.4	-0.67	0
127	SLU 70	-1	-416	2918	17.5	-1.46	-0.01
127	SLU 71	0	-414	2906	17.4	-0.67	0
127	SLU 72	-1	-416	2918	17.5	-1.46	-0.01
127	SLU 73	-1	-463	3332	19.31	-2.2	-0.01
127	SLU 74	0	-459	3312	19.14	-0.9	-0.01
127	SLU 75	-1	-461	3324	19.24	-1.68	-0.01
127	SLU 76	-1	-463	3332	19.31	-2.2	-0.01
127	SLU 77	0	-459	3312	19.14	-0.9	-0.01
127	SLU 78	-1	-461	3324	19.24	-1.68	-0.01
127	SLU 79	0	-459	3312	19.14	-0.9	-0.01
127	SLU 80	-1	-461	3324	19.24	-1.68	-0.01
127	SLU 81	0	-478	3486	19.89	-1	-0.01
127	SLU 82	-1	-481	3498	19.99	-1.78	-0.01
127	SLU 83	0	-478	3486	19.89	-1	-0.01
127	SLU 84	-1	-481	3498	19.99	-1.78	-0.01
127	SLE RA 1	0	-311	2189	13.1	-0.5	0
127	SLE RA 2	0	-314	2203	13.22	-1.37	0
127	SLE RA 3	0	-311	2189	13.1	-0.5	0
127	SLE RA 4	0	-313	2198	13.17	-1.02	0
127	SLE RA 5	0	-314	2203	13.22	-1.37	0
127	SLE RA 6	0	-311	2189	13.1	-0.5	0
127	SLE RA 7	0	-313	2198	13.17	-1.02	0
127	SLE RA 8	0	-311	2189	13.1	-0.5	0
127	SLE RA 9	0	-313	2198	13.17	-1.02	0
127	SLE RA 10	-1	-344	2474	14.38	-1.52	0
127	SLE RA 11	0	-341	2460	14.27	-0.65	0
127	SLE RA 12	0	-343	2469	14.33	-1.17	0
127	SLE RA 13	-1	-344	2474	14.38	-1.52	0
127	SLE RA 14	0	-341	2460	14.27	-0.65	0
127	SLE RA 15	0	-343	2469	14.33	-1.17	0
127	SLE RA 16	0	-341	2460	14.27	-0.65	0
127	SLE RA 17	0	-343	2469	14.33	-1.17	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
127	SLE RA 18	0	-354	2576	14.76	-0.71	0
127	SLE RA 19	0	-356	2585	14.83	-1.23	0
127	SLE RA 20	0	-354	2576	14.76	-0.71	0
127	SLE RA 21	0	-356	2585	14.83	-1.23	0
127	SLE FR 1	0	-311	2189	13.1	-0.5	0
127	SLE FR 2	0	-312	2192	13.13	-0.67	0
127	SLE FR 3	0	-311	2189	13.1	-0.5	0
127	SLE FR 4	0	-325	2308	13.62	-0.73	0
127	SLE FR 5	0	-324	2306	13.6	-0.56	0
127	SLE FR 6	0	-333	2383	13.93	-0.6	0
127	SLE QP 1	0	-311	2189	13.1	-0.5	0
127	SLE QP 2	0	-324	2306	13.6	-0.56	0
127	SLD 1	5	-194	2074	7.92	18.05	0.01
127	SLD 2	5	-194	2074	7.92	18.05	0.01
127	SLD 3	12	-335	2193	14.1	22.22	0.01
127	SLD 4	12	-335	2193	14.1	22.22	0.01
127	SLD 5	-10	-71	2056	2.53	-1.31	0.01
127	SLD 6	-10	-71	2056	2.53	-1.31	0.01
127	SLD 7	15	-541	2452	23.12	12.6	-0.01
127	SLD 8	15	-541	2452	23.12	12.6	-0.01
127	SLD 9	-15	-107	2159	4.08	-13.73	0
127	SLD 10	-15	-107	2159	4.08	-13.73	0
127	SLD 11	9	-577	2555	24.67	0.18	-0.02
127	SLD 12	9	-577	2555	24.67	0.18	-0.02
127	SLD 13	-13	-314	2418	13.1	-23.35	-0.01
127	SLD 14	-13	-314	2418	13.1	-23.35	-0.01
127	SLD 15	-6	-455	2537	19.28	-19.17	-0.02
127	SLD 16	-6	-455	2537	19.28	-19.17	-0.02
127	SLV 1	13	-13	1754	0.07	48.16	0.04
127	SLV 2	13	-13	1754	0.07	48.16	0.04
127	SLV 3	31	-346	2037	14.64	58.5	0.02
127	SLV 4	31	-346	2037	14.64	58.5	0.02
127	SLV 5	-23	273	1711	-12.56	-1.63	0.03
127	SLV 6	-23	273	1711	-12.56	-1.63	0.03
127	SLV 7	36	-835	2654	36.02	32.84	-0.02
127	SLV 8	36	-835	2654	36.02	32.84	-0.02
127	SLV 9	-37	186	1957	-8.81	-33.96	0.01
127	SLV 10	-37	186	1957	-8.81	-33.96	0.01
127	SLV 11	23	-922	2900	39.77	0.5	-0.04
127	SLV 12	23	-922	2900	39.77	0.5	-0.04
127	SLV 13	-32	-303	2574	12.56	-59.62	-0.03
127	SLV 14	-32	-303	2574	12.56	-59.62	-0.03
127	SLV 15	-14	-635	2857	27.14	-49.28	-0.04
127	SLV 16	-14	-635	2857	27.14	-49.28	-0.04
128	SLU 1	3	-367	2265	17.35	0.8	-0.01
128	SLU 2	1	-359	2226	17.03	-2.56	-0.01
128	SLU 3	3	-367	2265	17.35	0.8	-0.01
128	SLU 4	2	-362	2242	17.16	-1.21	-0.01
128	SLU 5	1	-359	2226	17.03	-2.56	-0.01
128	SLU 6	3	-367	2265	17.35	0.8	-0.01
128	SLU 7	2	-362	2242	17.16	-1.21	-0.01
128	SLU 8	3	-367	2265	17.35	0.8	-0.01
128	SLU 9	2	-362	2242	17.16	-1.21	-0.01
128	SLU 10	2	-460	2699	21.71	-2.34	-0.01
128	SLU 11	3	-467	2738	22.04	1.01	-0.01
128	SLU 12	2	-463	2715	21.84	-1	-0.01
128	SLU 13	2	-460	2699	21.71	-2.34	-0.01
128	SLU 14	3	-467	2738	22.04	1.01	-0.01
128	SLU 15	2	-463	2715	21.84	-1	-0.01
128	SLU 16	3	-467	2738	22.04	1.01	-0.01
128	SLU 17	2	-463	2715	21.84	-1	-0.01
128	SLU 18	3	-510	2941	24.05	1.1	-0.01
128	SLU 19	3	-506	2917	23.85	-0.91	-0.01
128	SLU 20	3	-510	2941	24.05	1.1	-0.01
128	SLU 21	3	-506	2917	23.85	-0.91	-0.01
128	SLU 22	3	-422	2505	19.91	0.89	-0.01
128	SLU 23	1	-415	2466	19.58	-2.46	-0.01
128	SLU 24	3	-422	2505	19.91	0.89	-0.01
128	SLU 25	2	-418	2481	19.71	-1.12	-0.01
128	SLU 26	1	-415	2466	19.58	-2.46	-0.01
128	SLU 27	3	-422	2505	19.91	0.89	-0.01
128	SLU 28	2	-418	2481	19.71	-1.12	-0.01
128	SLU 29	3	-422	2505	19.91	0.89	-0.01
128	SLU 30	2	-418	2481	19.71	-1.12	-0.01
128	SLU 31	2	-515	2939	24.27	-2.25	-0.01
128	SLU 32	3	-523	2978	24.59	1.11	-0.01
128	SLU 33	3	-518	2954	24.4	-0.9	-0.01
128	SLU 34	2	-515	2939	24.27	-2.25	-0.01
128	SLU 35	3	-523	2978	24.59	1.11	-0.01
128	SLU 36	3	-518	2954	24.4	-0.9	-0.01
128	SLU 37	3	-523	2978	24.59	1.11	-0.01
128	SLU 38	3	-518	2954	24.4	-0.9	-0.01
128	SLU 39	4	-566	3180	26.6	1.2	-0.01
128	SLU 40	3	-561	3157	26.41	-0.81	-0.01
128	SLU 41	4	-566	3180	26.6	1.2	-0.01
128	SLU 42	3	-561	3157	26.41	-0.81	-0.01
128	SLU 43	3	-457	2863	21.68	1.01	-0.01
128	SLU 44	2	-450	2824	21.36	-2.35	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
128	SLU 45	3	-457	2863	21.68	1.01	-0.01
128	SLU 46	2	-453	2839	21.49	-1.01	-0.01
128	SLU 47	2	-450	2824	21.36	-2.35	-0.01
128	SLU 48	3	-457	2863	21.68	1.01	-0.01
128	SLU 49	2	-453	2839	21.49	-1.01	-0.01
128	SLU 50	3	-457	2863	21.68	1.01	-0.01
128	SLU 51	2	-453	2839	21.49	-1.01	-0.01
128	SLU 52	2	-551	3297	26.04	-2.14	-0.01
128	SLU 53	4	-558	3336	26.37	1.22	-0.01
128	SLU 54	3	-553	3312	26.17	-0.79	-0.01
128	SLU 55	2	-551	3297	26.04	-2.14	-0.01
128	SLU 56	4	-558	3336	26.37	1.22	-0.01
128	SLU 57	3	-553	3312	26.17	-0.79	-0.01
128	SLU 58	4	-558	3336	26.37	1.22	-0.01
128	SLU 59	3	-553	3312	26.17	-0.79	-0.01
128	SLU 60	4	-601	3538	28.38	1.31	-0.01
128	SLU 61	3	-596	3515	28.18	-0.7	-0.01
128	SLU 62	4	-601	3538	28.38	1.31	-0.01
128	SLU 63	3	-596	3515	28.18	-0.7	-0.01
128	SLU 64	3	-513	3102	24.24	1.1	-0.01
128	SLU 65	2	-506	3063	23.91	-2.25	-0.01
128	SLU 66	3	-513	3102	24.24	1.1	-0.01
128	SLU 67	3	-509	3079	24.04	-0.91	-0.01
128	SLU 68	2	-506	3063	23.91	-2.25	-0.01
128	SLU 69	3	-513	3102	24.24	1.1	-0.01
128	SLU 70	3	-509	3079	24.04	-0.91	-0.01
128	SLU 71	3	-513	3102	24.24	1.1	-0.01
128	SLU 72	3	-509	3079	24.04	-0.91	-0.01
128	SLU 73	3	-606	3536	28.6	-2.04	-0.02
128	SLU 74	4	-613	3575	28.92	1.31	-0.01
128	SLU 75	3	-609	3552	28.73	-0.7	-0.01
128	SLU 76	3	-606	3536	28.6	-2.04	-0.02
128	SLU 77	4	-613	3575	28.92	1.31	-0.01
128	SLU 78	3	-609	3552	28.73	-0.7	-0.01
128	SLU 79	4	-613	3575	28.92	1.31	-0.01
128	SLU 80	3	-609	3552	28.73	-0.7	-0.01
128	SLU 81	4	-656	3778	30.93	1.41	-0.02
128	SLU 82	3	-652	3754	30.74	-0.61	-0.02
128	SLU 83	4	-656	3778	30.93	1.41	-0.02
128	SLU 84	3	-652	3754	30.74	-0.61	-0.02
128	SLE RA 1	3	-382	2334	18.08	0.83	-0.01
128	SLE RA 2	2	-378	2308	17.87	-1.41	-0.01
128	SLE RA 3	3	-382	2334	18.08	0.83	-0.01
128	SLE RA 4	2	-380	2318	17.95	-0.52	-0.01
128	SLE RA 5	2	-378	2308	17.87	-1.41	-0.01
128	SLE RA 6	3	-382	2334	18.08	0.83	-0.01
128	SLE RA 7	2	-380	2318	17.95	-0.52	-0.01
128	SLE RA 8	3	-382	2334	18.08	0.83	-0.01
128	SLE RA 9	2	-380	2318	17.95	-0.52	-0.01
128	SLE RA 10	2	-445	2623	20.99	-1.27	-0.01
128	SLE RA 11	3	-449	2649	21.21	0.97	-0.01
128	SLE RA 12	2	-446	2633	21.08	-0.37	-0.01
128	SLE RA 13	2	-445	2623	20.99	-1.27	-0.01
128	SLE RA 14	3	-449	2649	21.21	0.97	-0.01
128	SLE RA 15	2	-446	2633	21.08	-0.37	-0.01
128	SLE RA 16	3	-449	2649	21.21	0.97	-0.01
128	SLE RA 17	2	-446	2633	21.08	-0.37	-0.01
128	SLE RA 18	3	-478	2784	22.55	1.03	-0.01
128	SLE RA 19	3	-475	2769	22.42	-0.31	-0.01
128	SLE RA 20	3	-478	2784	22.55	1.03	-0.01
128	SLE RA 21	3	-475	2769	22.42	-0.31	-0.01
128	SLE FR 1	3	-382	2334	18.08	0.83	-0.01
128	SLE FR 2	2	-382	2329	18.04	0.38	-0.01
128	SLE FR 3	3	-382	2334	18.08	0.83	-0.01
128	SLE FR 4	3	-410	2464	19.38	0.44	-0.01
128	SLE FR 5	3	-411	2469	19.42	0.89	-0.01
128	SLE FR 6	3	-430	2559	20.31	0.93	-0.01
128	SLE QP 1	3	-382	2334	18.08	0.83	-0.01
128	SLE QP 2	3	-411	2469	19.42	0.89	-0.01
128	SLD 1	12	-400	2562	18.68	14.48	0.01
128	SLD 2	12	-400	2562	18.68	14.48	0.01
128	SLD 3	6	-502	2734	23.52	11.67	-0.01
128	SLD 4	6	-502	2734	23.52	11.67	-0.01
128	SLD 5	16	-253	2236	11.87	9.22	0.02
128	SLD 6	16	-253	2236	11.87	9.22	0.02
128	SLD 7	-6	-593	2809	27.98	-0.14	-0.03
128	SLD 8	-6	-593	2809	27.98	-0.14	-0.03
128	SLD 9	12	-229	2129	10.86	1.91	0.01
128	SLD 10	12	-229	2129	10.86	1.91	0.01
128	SLD 11	-10	-569	2701	26.98	-7.45	-0.04
128	SLD 12	-10	-569	2701	26.98	-7.45	-0.04
128	SLD 13	0	-320	2204	15.33	-9.9	-0.01
128	SLD 14	0	-320	2204	15.33	-9.9	-0.01
128	SLD 15	-7	-422	2376	20.16	-12.71	-0.03
128	SLD 16	-7	-422	2376	20.16	-12.71	-0.03
128	SLV 1	26	-386	2690	17.73	35.62	0.03
128	SLV 2	26	-386	2690	17.73	35.62	0.03
128	SLV 3	11	-628	3095	29.15	28.96	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
128	SLV 4	11	-628	3095	29.15	28.96	0
128	SLV 5	33	-38	1921	1.6	21.41	0.06
128	SLV 6	33	-38	1921	1.6	21.41	0.06
128	SLV 7	-18	-842	3270	39.65	-0.8	-0.06
128	SLV 8	-18	-842	3270	39.65	-0.8	-0.06
128	SLV 9	24	20	1667	-0.81	2.57	0.04
128	SLV 10	24	20	1667	-0.81	2.57	0.04
128	SLV 11	-28	-784	3016	37.24	-19.64	-0.08
128	SLV 12	-28	-784	3016	37.24	-19.64	-0.08
128	SLV 13	-5	-195	1843	9.7	-27.19	-0.02
128	SLV 14	-5	-195	1843	9.7	-27.19	-0.02
128	SLV 15	-21	-436	2248	21.11	-33.85	-0.05
128	SLV 16	-21	-436	2248	21.11	-33.85	-0.05
129	SLU 1	0	-422	1160	17.83	-0.01	0
129	SLU 2	2	-422	1162	17.9	-0.07	0
129	SLU 3	0	-422	1160	17.83	-0.01	0
129	SLU 4	1	-422	1162	17.87	-0.05	0
129	SLU 5	2	-422	1162	17.9	-0.07	0
129	SLU 6	0	-422	1160	17.83	-0.01	0
129	SLU 7	1	-422	1162	17.87	-0.05	0
129	SLU 8	0	-422	1160	17.83	-0.01	0
129	SLU 9	1	-422	1162	17.87	-0.05	0
129	SLU 10	2	-698	1538	29.51	-0.07	0
129	SLU 11	0	-697	1536	29.44	0	0
129	SLU 12	1	-697	1537	29.48	-0.04	0
129	SLU 13	2	-698	1538	29.51	-0.07	0
129	SLU 14	0	-697	1536	29.44	0	0
129	SLU 15	1	-697	1537	29.48	-0.04	0
129	SLU 16	0	-697	1536	29.44	0	0
129	SLU 17	1	-697	1537	29.48	-0.04	0
129	SLU 18	0	-815	1697	34.42	0	0
129	SLU 19	1	-815	1698	34.46	-0.04	0
129	SLU 20	0	-815	1697	34.42	0	0
129	SLU 21	1	-815	1698	34.46	-0.04	0
129	SLU 22	0	-570	1360	23.96	0	0
129	SLU 23	2	-570	1362	24.03	-0.07	0
129	SLU 24	0	-570	1360	23.96	0	0
129	SLU 25	1	-570	1362	24	-0.04	0
129	SLU 26	2	-570	1362	24.03	-0.07	0
129	SLU 27	0	-570	1360	23.96	0	0
129	SLU 28	1	-570	1362	24	-0.04	0
129	SLU 29	0	-570	1360	23.96	0	0
129	SLU 30	1	-570	1362	24	-0.04	0
129	SLU 31	2	-845	1738	35.64	-0.07	0
129	SLU 32	0	-845	1736	35.58	0	0
129	SLU 33	1	-845	1737	35.61	-0.04	0
129	SLU 34	2	-845	1738	35.64	-0.07	0
129	SLU 35	0	-845	1736	35.58	0	0
129	SLU 36	1	-845	1737	35.61	-0.04	0
129	SLU 37	0	-845	1736	35.58	0	0
129	SLU 38	1	-845	1737	35.61	-0.04	0
129	SLU 39	0	-963	1897	40.55	0	0
129	SLU 40	1	-963	1898	40.59	-0.04	0
129	SLU 41	0	-963	1897	40.55	0	0
129	SLU 42	1	-963	1898	40.59	-0.04	0
129	SLU 43	0	-498	1440	21.08	-0.01	0
129	SLU 44	2	-499	1442	21.14	-0.08	0
129	SLU 45	0	-498	1440	21.08	-0.01	0
129	SLU 46	1	-499	1441	21.12	-0.05	0
129	SLU 47	2	-499	1442	21.14	-0.08	0
129	SLU 48	0	-498	1440	21.08	-0.01	0
129	SLU 49	1	-499	1441	21.12	-0.05	0
129	SLU 50	0	-498	1440	21.08	-0.01	0
129	SLU 51	1	-499	1441	21.12	-0.05	0
129	SLU 52	2	-774	1817	32.76	-0.07	0
129	SLU 53	0	-774	1815	32.69	0	0
129	SLU 54	1	-774	1816	32.73	-0.05	0
129	SLU 55	2	-774	1817	32.76	-0.07	0
129	SLU 56	0	-774	1815	32.69	0	0
129	SLU 57	1	-774	1816	32.73	-0.05	0
129	SLU 58	0	-774	1815	32.69	0	0
129	SLU 59	1	-774	1816	32.73	-0.05	0
129	SLU 60	0	-891	1976	37.67	0	0
129	SLU 61	1	-892	1977	37.71	-0.04	0
129	SLU 62	0	-891	1976	37.67	0	0
129	SLU 63	1	-892	1977	37.71	-0.04	0
129	SLU 64	0	-646	1640	27.21	-0.01	0
129	SLU 65	2	-646	1642	27.28	-0.07	0
129	SLU 66	0	-646	1640	27.21	-0.01	0
129	SLU 67	1	-646	1641	27.25	-0.05	0
129	SLU 68	2	-646	1642	27.28	-0.07	0
129	SLU 69	0	-646	1640	27.21	-0.01	0
129	SLU 70	1	-646	1641	27.25	-0.05	0
129	SLU 71	0	-646	1640	27.21	-0.01	0
129	SLU 72	1	-646	1641	27.25	-0.05	0
129	SLU 73	2	-921	2017	38.89	-0.07	0
129	SLU 74	0	-921	2015	38.82	0	0
129	SLU 75	1	-921	2016	38.86	-0.04	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
129	SLU 76	2	-921	2017	38.89	-0.07	0
129	SLU 77	0	-921	2015	38.82	0	0
129	SLU 78	1	-921	2016	38.86	-0.04	0
129	SLU 79	0	-921	2015	38.82	0	0
129	SLU 80	1	-921	2016	38.86	-0.04	0
129	SLU 81	0	-1039	2176	43.8	0	0
129	SLU 82	1	-1039	2177	43.84	-0.04	0
129	SLU 83	0	-1039	2176	43.8	0	0
129	SLU 84	1	-1039	2177	43.84	-0.04	0
129	SLE RA 1	0	-464	1218	19.58	-0.01	0
129	SLE RA 2	1	-464	1219	19.63	-0.05	0
129	SLE RA 3	0	-464	1218	19.58	-0.01	0
129	SLE RA 4	1	-464	1218	19.61	-0.03	0
129	SLE RA 5	1	-464	1219	19.63	-0.05	0
129	SLE RA 6	0	-464	1218	19.58	-0.01	0
129	SLE RA 7	1	-464	1218	19.61	-0.03	0
129	SLE RA 8	0	-464	1218	19.58	-0.01	0
129	SLE RA 9	1	-464	1218	19.61	-0.03	0
129	SLE RA 10	1	-648	1469	27.37	-0.05	0
129	SLE RA 11	0	-648	1468	27.33	0	0
129	SLE RA 12	1	-648	1468	27.35	-0.03	0
129	SLE RA 13	1	-648	1469	27.37	-0.05	0
129	SLE RA 14	0	-648	1468	27.33	0	0
129	SLE RA 15	1	-648	1468	27.35	-0.03	0
129	SLE RA 16	0	-648	1468	27.33	0	0
129	SLE RA 17	1	-648	1468	27.35	-0.03	0
129	SLE RA 18	0	-726	1575	30.64	0	0
129	SLE RA 19	1	-726	1576	30.67	-0.03	0
129	SLE RA 20	0	-726	1575	30.64	0	0
129	SLE RA 21	1	-726	1576	30.67	-0.03	0
129	SLE FR 1	0	-464	1218	19.58	-0.01	0
129	SLE FR 2	0	-464	1218	19.59	-0.01	0
129	SLE FR 3	0	-464	1218	19.58	-0.01	0
129	SLE FR 4	0	-543	1325	22.91	-0.01	0
129	SLE FR 5	0	-543	1325	22.9	0	0
129	SLE FR 6	0	-595	1396	25.11	0	0
129	SLE QP 1	0	-464	1218	19.58	-0.01	0
129	SLE QP 2	0	-543	1325	22.9	0	0
129	SLD 1	-10	-439	1278	15.72	0.87	-0.02
129	SLD 2	-10	-439	1278	15.72	0.87	-0.02
129	SLD 3	-9	-576	1329	26.67	1.11	-0.02
129	SLD 4	-9	-576	1329	26.67	1.11	-0.02
129	SLD 5	-4	-304	1234	4.14	-0.12	-0.01
129	SLD 6	-4	-304	1234	4.14	-0.12	-0.01
129	SLD 7	-2	-761	1403	40.64	0.71	0
129	SLD 8	-2	-761	1403	40.64	0.71	0
129	SLD 9	1	-325	1247	5.17	-0.71	0
129	SLD 10	1	-325	1247	5.17	-0.71	0
129	SLD 11	4	-782	1416	41.66	0.11	0.01
129	SLD 12	4	-782	1416	41.66	0.11	0.01
129	SLD 13	9	-510	1321	19.13	-1.12	0.02
129	SLD 14	9	-510	1321	19.13	-1.12	0.02
129	SLD 15	9	-647	1372	30.08	-0.88	0.02
129	SLD 16	9	-647	1372	30.08	-0.88	0.02
129	SLV 1	-29	-293	1214	4.96	2.52	-0.05
129	SLV 2	-29	-293	1214	4.96	2.52	-0.05
129	SLV 3	-28	-626	1335	32.65	3.14	-0.05
129	SLV 4	-28	-626	1335	32.65	3.14	-0.05
129	SLV 5	-12	37	1107	-24.46	-0.17	-0.02
129	SLV 6	-12	37	1107	-24.46	-0.17	-0.02
129	SLV 7	-6	-1073	1512	67.81	1.86	-0.01
129	SLV 8	-6	-1073	1512	67.81	1.86	-0.01
129	SLV 9	5	-13	1137	-22	-1.87	0.01
129	SLV 10	5	-13	1137	-22	-1.87	0.01
129	SLV 11	11	-1123	1542	70.27	0.16	0.02
129	SLV 12	11	-1123	1542	70.27	0.16	0.02
129	SLV 13	27	-460	1314	13.16	-3.14	0.05
129	SLV 14	27	-460	1314	13.16	-3.14	0.05
129	SLV 15	29	-793	1436	40.84	-2.53	0.05
129	SLV 16	29	-793	1436	40.84	-2.53	0.05
130	SLU 1	-3	-384	2264	18.26	-0.85	0.01
130	SLU 2	-3	-389	2287	18.5	-1.5	0.01
130	SLU 3	-3	-384	2264	18.26	-0.85	0.01
130	SLU 4	-3	-387	2278	18.4	-1.24	0.01
130	SLU 5	-3	-389	2287	18.5	-1.5	0.01
130	SLU 6	-3	-384	2264	18.26	-0.85	0.01
130	SLU 7	-3	-387	2278	18.4	-1.24	0.01
130	SLU 8	-3	-384	2264	18.26	-0.85	0.01
130	SLU 9	-3	-387	2278	18.4	-1.24	0.01
130	SLU 10	-3	-458	2741	22.19	-1.74	0.02
130	SLU 11	-3	-453	2718	21.95	-1.09	0.02
130	SLU 12	-3	-456	2732	22.1	-1.48	0.02
130	SLU 13	-3	-458	2741	22.19	-1.74	0.02
130	SLU 14	-3	-453	2718	21.95	-1.09	0.02
130	SLU 15	-3	-456	2732	22.1	-1.48	0.02
130	SLU 16	-3	-453	2718	21.95	-1.09	0.02
130	SLU 17	-3	-456	2732	22.1	-1.48	0.02
130	SLU 18	-3	-483	2912	23.53	-1.19	0.02





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
130	SLU 19	-3	-486	2926	23.68	-1.58	0.02
130	SLU 20	-3	-483	2912	23.53	-1.19	0.02
130	SLU 21	-3	-486	2926	23.68	-1.58	0.02
130	SLU 22	-3	-427	2490	20.42	-0.96	0.01
130	SLU 23	-3	-432	2513	20.66	-1.6	0.02
130	SLU 24	-3	-427	2490	20.42	-0.96	0.01
130	SLU 25	-3	-430	2504	20.56	-1.34	0.02
130	SLU 26	-3	-432	2513	20.66	-1.6	0.02
130	SLU 27	-3	-427	2490	20.42	-0.96	0.01
130	SLU 28	-3	-430	2504	20.56	-1.34	0.02
130	SLU 29	-3	-427	2490	20.42	-0.96	0.01
130	SLU 30	-3	-430	2504	20.56	-1.34	0.02
130	SLU 31	-4	-502	2967	24.35	-1.84	0.02
130	SLU 32	-3	-497	2943	24.11	-1.19	0.02
130	SLU 33	-3	-500	2957	24.25	-1.58	0.02
130	SLU 34	-4	-502	2967	24.35	-1.84	0.02
130	SLU 35	-3	-497	2943	24.11	-1.19	0.02
130	SLU 36	-3	-500	2957	24.25	-1.58	0.02
130	SLU 37	-3	-497	2943	24.11	-1.19	0.02
130	SLU 38	-3	-500	2957	24.25	-1.58	0.02
130	SLU 39	-4	-527	3138	25.69	-1.3	0.02
130	SLU 40	-4	-530	3152	25.84	-1.68	0.02
130	SLU 41	-4	-527	3138	25.69	-1.3	0.02
130	SLU 42	-4	-530	3152	25.84	-1.68	0.02
130	SLU 43	-3	-484	2866	23	-1.07	0.02
130	SLU 44	-4	-489	2889	23.24	-1.72	0.02
130	SLU 45	-3	-484	2866	23	-1.07	0.02
130	SLU 46	-3	-487	2880	23.14	-1.46	0.02
130	SLU 47	-4	-489	2889	23.24	-1.72	0.02
130	SLU 48	-3	-484	2866	23	-1.07	0.02
130	SLU 49	-3	-487	2880	23.14	-1.46	0.02
130	SLU 50	-3	-484	2866	23	-1.07	0.02
130	SLU 51	-3	-487	2880	23.14	-1.46	0.02
130	SLU 52	-4	-558	3343	26.93	-1.96	0.02
130	SLU 53	-4	-554	3319	26.69	-1.31	0.02
130	SLU 54	-4	-556	3333	26.83	-1.7	0.02
130	SLU 55	-4	-558	3343	26.93	-1.96	0.02
130	SLU 56	-4	-554	3319	26.69	-1.31	0.02
130	SLU 57	-4	-556	3333	26.83	-1.7	0.02
130	SLU 58	-4	-554	3319	26.69	-1.31	0.02
130	SLU 59	-4	-556	3333	26.83	-1.7	0.02
130	SLU 60	-4	-583	3514	28.27	-1.41	0.02
130	SLU 61	-4	-586	3528	28.41	-1.8	0.02
130	SLU 62	-4	-583	3514	28.27	-1.41	0.02
130	SLU 63	-4	-586	3528	28.41	-1.8	0.02
130	SLU 64	-4	-527	3091	25.16	-1.17	0.02
130	SLU 65	-4	-532	3115	25.4	-1.82	0.02
130	SLU 66	-4	-527	3091	25.16	-1.17	0.02
130	SLU 67	-4	-530	3105	25.3	-1.56	0.02
130	SLU 68	-4	-532	3115	25.4	-1.82	0.02
130	SLU 69	-4	-527	3091	25.16	-1.17	0.02
130	SLU 70	-4	-530	3105	25.3	-1.56	0.02
130	SLU 71	-4	-527	3091	25.16	-1.17	0.02
130	SLU 72	-4	-530	3105	25.3	-1.56	0.02
130	SLU 73	-4	-602	3568	29.09	-2.06	0.02
130	SLU 74	-4	-597	3545	28.85	-1.41	0.02
130	SLU 75	-4	-600	3559	28.99	-1.8	0.02
130	SLU 76	-4	-602	3568	29.09	-2.06	0.02
130	SLU 77	-4	-597	3545	28.85	-1.41	0.02
130	SLU 78	-4	-600	3559	28.99	-1.8	0.02
130	SLU 79	-4	-597	3545	28.85	-1.41	0.02
130	SLU 80	-4	-600	3559	28.99	-1.8	0.02
130	SLU 81	-4	-627	3739	30.43	-1.51	0.02
130	SLU 82	-4	-630	3753	30.57	-1.9	0.02
130	SLU 83	-4	-627	3739	30.43	-1.51	0.02
130	SLU 84	-4	-630	3753	30.57	-1.9	0.02
130	SLE RA 1	-3	-396	2328	18.88	-0.88	0.01
130	SLE RA 2	-3	-399	2344	19.04	-1.31	0.01
130	SLE RA 3	-3	-396	2328	18.88	-0.88	0.01
130	SLE RA 4	-3	-398	2338	18.97	-1.14	0.01
130	SLE RA 5	-3	-399	2344	19.04	-1.31	0.01
130	SLE RA 6	-3	-396	2328	18.88	-0.88	0.01
130	SLE RA 7	-3	-398	2338	18.97	-1.14	0.01
130	SLE RA 8	-3	-396	2328	18.88	-0.88	0.01
130	SLE RA 9	-3	-398	2338	18.97	-1.14	0.01
130	SLE RA 10	-3	-446	2646	21.5	-1.47	0.02
130	SLE RA 11	-3	-443	2631	21.34	-1.04	0.02
130	SLE RA 12	-3	-445	2640	21.43	-1.3	0.02
130	SLE RA 13	-3	-446	2646	21.5	-1.47	0.02
130	SLE RA 14	-3	-443	2631	21.34	-1.04	0.02
130	SLE RA 15	-3	-445	2640	21.43	-1.3	0.02
130	SLE RA 16	-3	-443	2631	21.34	-1.04	0.02
130	SLE RA 17	-3	-445	2640	21.43	-1.3	0.02
130	SLE RA 18	-3	-463	2760	22.39	-1.11	0.02
130	SLE RA 19	-3	-464	2770	22.49	-1.37	0.02
130	SLE RA 20	-3	-463	2760	22.39	-1.11	0.02
130	SLE RA 21	-3	-464	2770	22.49	-1.37	0.02
130	SLE FR 1	-3	-396	2328	18.88	-0.88	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
130	SLE FR 2	-3	-397	2331	18.91	-0.97	0.01
130	SLE FR 3	-3	-396	2328	18.88	-0.88	0.01
130	SLE FR 4	-3	-417	2461	19.96	-1.04	0.01
130	SLE FR 5	-3	-416	2458	19.93	-0.95	0.01
130	SLE FR 6	-3	-429	2544	20.63	-0.99	0.01
130	SLE QP 1	-3	-396	2328	18.88	-0.88	0.01
130	SLE QP 2	-3	-416	2458	19.93	-0.95	0.01
130	SLD 1	-3	-290	2150	14.22	7.26	0
130	SLD 2	-3	-290	2150	14.22	7.26	0
130	SLD 3	3	-423	2334	20.39	9.79	0
130	SLD 4	3	-423	2334	20.39	9.79	0
130	SLD 5	-12	-177	2086	8.87	-2.32	0
130	SLD 6	-12	-177	2086	8.87	-2.32	0
130	SLD 7	8	-620	2700	29.42	6.11	0.02
130	SLD 8	8	-620	2700	29.42	6.11	0.02
130	SLD 9	-14	-212	2216	10.44	-8.01	0.01
130	SLD 10	-14	-212	2216	10.44	-8.01	0.01
130	SLD 11	6	-655	2830	30.99	0.43	0.03
130	SLD 12	6	-655	2830	30.99	0.43	0.03
130	SLD 13	-9	-409	2582	19.48	-11.69	0.03
130	SLD 14	-9	-409	2582	19.48	-11.69	0.03
130	SLD 15	-3	-542	2766	25.64	-9.16	0.03
130	SLD 16	-3	-542	2766	25.64	-9.16	0.03
130	SLV 1	-3	-114	1723	6.18	20.67	-0.03
130	SLV 2	-3	-114	1723	6.18	20.67	-0.03
130	SLV 3	11	-427	2160	20.74	26.85	-0.01
130	SLV 4	11	-427	2160	20.74	26.85	-0.01
130	SLV 5	-24	151	1575	-6.27	-3.84	-0.02
130	SLV 6	-24	151	1575	-6.27	-3.84	-0.02
130	SLV 7	22	-895	3032	42.25	16.76	0.03
130	SLV 8	22	-895	3032	42.25	16.76	0.03
130	SLV 9	-28	63	1884	-2.39	-18.66	0
130	SLV 10	-28	63	1884	-2.39	-18.66	0
130	SLV 11	18	-983	3341	46.13	1.94	0.05
130	SLV 12	18	-983	3341	46.13	1.94	0.05
130	SLV 13	-17	-405	2756	19.12	-28.75	0.04
130	SLV 14	-17	-405	2756	19.12	-28.75	0.04
130	SLV 15	-3	-718	3193	33.68	-22.56	0.06
130	SLV 16	-3	-718	3193	33.68	-22.56	0.06
131	SLU 1	283	-416	2630	12.26	6.71	-0.04
131	SLU 2	282	-403	2580	12.32	6.16	-0.04
131	SLU 3	283	-416	2630	12.26	6.71	-0.04
131	SLU 4	282	-408	2600	12.3	6.38	-0.04
131	SLU 5	282	-403	2580	12.32	6.16	-0.04
131	SLU 6	283	-416	2630	12.26	6.71	-0.04
131	SLU 7	282	-408	2600	12.3	6.38	-0.04
131	SLU 8	283	-416	2630	12.26	6.71	-0.04
131	SLU 9	282	-408	2600	12.3	6.38	-0.04
131	SLU 10	334	-504	3138	15.47	7.33	-0.06
131	SLU 11	335	-517	3188	15.41	7.88	-0.06
131	SLU 12	334	-509	3158	15.45	7.55	-0.06
131	SLU 13	334	-504	3138	15.47	7.33	-0.06
131	SLU 14	335	-517	3188	15.41	7.88	-0.06
131	SLU 15	334	-509	3158	15.45	7.55	-0.06
131	SLU 16	335	-517	3188	15.41	7.88	-0.06
131	SLU 17	334	-509	3158	15.45	7.55	-0.06
131	SLU 18	357	-561	3426	16.76	8.38	-0.06
131	SLU 19	357	-553	3397	16.8	8.05	-0.06
131	SLU 20	357	-561	3426	16.76	8.38	-0.06
131	SLU 21	357	-553	3397	16.8	8.05	-0.06
131	SLU 22	306	-470	2909	13.96	7.19	-0.05
131	SLU 23	306	-457	2859	14.01	6.64	-0.05
131	SLU 24	306	-470	2909	13.96	7.19	-0.05
131	SLU 25	306	-462	2879	13.99	6.86	-0.05
131	SLU 26	306	-457	2859	14.01	6.64	-0.05
131	SLU 27	306	-470	2909	13.96	7.19	-0.05
131	SLU 28	306	-462	2879	13.99	6.86	-0.05
131	SLU 29	306	-470	2909	13.96	7.19	-0.05
131	SLU 30	306	-462	2879	13.99	6.86	-0.05
131	SLU 31	358	-557	3416	17.16	7.81	-0.07
131	SLU 32	358	-571	3466	17.11	8.36	-0.07
131	SLU 33	358	-563	3436	17.14	8.03	-0.07
131	SLU 34	358	-557	3416	17.16	7.81	-0.07
131	SLU 35	358	-571	3466	17.11	8.36	-0.07
131	SLU 36	358	-563	3436	17.14	8.03	-0.07
131	SLU 37	358	-571	3466	17.11	8.36	-0.07
131	SLU 38	358	-563	3436	17.14	8.03	-0.07
131	SLU 39	380	-614	3705	18.46	8.86	-0.07
131	SLU 40	380	-606	3675	18.49	8.53	-0.07
131	SLU 41	380	-614	3705	18.46	8.86	-0.07
131	SLU 42	380	-606	3675	18.49	8.53	-0.07
131	SLU 43	359	-523	3324	15.36	8.56	-0.05
131	SLU 44	359	-510	3274	15.42	8.01	-0.05
131	SLU 45	359	-523	3324	15.36	8.56	-0.05
131	SLU 46	359	-515	3294	15.4	8.23	-0.05
131	SLU 47	359	-510	3274	15.42	8.01	-0.05
131	SLU 48	359	-523	3324	15.36	8.56	-0.05
131	SLU 49	359	-515	3294	15.4	8.23	-0.05



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
131	SLU 50	359	-523	3324	15.36	8.56	-0.05
131	SLU 51	359	-515	3294	15.4	8.23	-0.05
131	SLU 52	411	-611	3831	18.57	9.18	-0.07
131	SLU 53	411	-624	3881	18.51	9.73	-0.07
131	SLU 54	411	-616	3851	18.55	9.4	-0.07
131	SLU 55	411	-611	3831	18.57	9.18	-0.07
131	SLU 56	411	-624	3881	18.51	9.73	-0.07
131	SLU 57	411	-616	3851	18.55	9.4	-0.07
131	SLU 58	411	-624	3881	18.51	9.73	-0.07
131	SLU 59	411	-616	3851	18.55	9.4	-0.07
131	SLU 60	434	-667	4120	19.86	10.23	-0.07
131	SLU 61	433	-659	4090	19.9	9.9	-0.07
131	SLU 62	434	-667	4120	19.86	10.23	-0.07
131	SLU 63	433	-659	4090	19.9	9.9	-0.07
131	SLU 64	383	-576	3602	17.06	9.04	-0.06
131	SLU 65	382	-563	3552	17.11	8.49	-0.06
131	SLU 66	383	-576	3602	17.06	9.04	-0.06
131	SLU 67	383	-568	3572	17.09	8.71	-0.06
131	SLU 68	382	-563	3552	17.11	8.49	-0.06
131	SLU 69	383	-576	3602	17.06	9.04	-0.06
131	SLU 70	383	-568	3572	17.09	8.71	-0.06
131	SLU 71	383	-576	3602	17.06	9.04	-0.06
131	SLU 72	383	-568	3572	17.09	8.71	-0.06
131	SLU 73	434	-664	4110	20.26	9.66	-0.08
131	SLU 74	435	-677	4160	20.21	10.21	-0.08
131	SLU 75	435	-669	4130	20.24	9.88	-0.08
131	SLU 76	434	-664	4110	20.26	9.66	-0.08
131	SLU 77	435	-677	4160	20.21	10.21	-0.08
131	SLU 78	435	-669	4130	20.24	9.88	-0.08
131	SLU 79	435	-677	4160	20.21	10.21	-0.08
131	SLU 80	435	-669	4130	20.24	9.88	-0.08
131	SLU 81	457	-720	4399	21.56	10.71	-0.08
131	SLU 82	457	-713	4369	21.59	10.38	-0.08
131	SLU 83	457	-720	4399	21.56	10.71	-0.08
131	SLU 84	457	-713	4369	21.59	10.38	-0.08
131	SLE RA 1	289	-432	2710	12.75	6.85	-0.04
131	SLE RA 2	289	-423	2677	12.79	6.48	-0.04
131	SLE RA 3	289	-432	2710	12.75	6.85	-0.04
131	SLE RA 4	289	-426	2690	12.77	6.63	-0.04
131	SLE RA 5	289	-423	2677	12.79	6.48	-0.04
131	SLE RA 6	289	-432	2710	12.75	6.85	-0.04
131	SLE RA 7	289	-426	2690	12.77	6.63	-0.04
131	SLE RA 8	289	-432	2710	12.75	6.85	-0.04
131	SLE RA 9	289	-426	2690	12.77	6.63	-0.04
131	SLE RA 10	324	-490	3048	14.89	7.26	-0.06
131	SLE RA 11	324	-499	3081	14.85	7.63	-0.05
131	SLE RA 12	324	-494	3061	14.87	7.41	-0.06
131	SLE RA 13	324	-490	3048	14.89	7.26	-0.06
131	SLE RA 14	324	-499	3081	14.85	7.63	-0.05
131	SLE RA 15	324	-494	3061	14.87	7.41	-0.06
131	SLE RA 16	324	-499	3081	14.85	7.63	-0.05
131	SLE RA 17	324	-494	3061	14.87	7.41	-0.06
131	SLE RA 18	339	-528	3241	15.75	7.96	-0.06
131	SLE RA 19	339	-522	3221	15.77	7.74	-0.06
131	SLE RA 20	339	-528	3241	15.75	7.96	-0.06
131	SLE RA 21	339	-522	3221	15.77	7.74	-0.06
131	SLE FR 1	289	-432	2710	12.75	6.85	-0.04
131	SLE FR 2	289	-430	2703	12.76	6.77	-0.04
131	SLE FR 3	289	-432	2710	12.75	6.85	-0.04
131	SLE FR 4	304	-459	2862	13.66	7.11	-0.05
131	SLE FR 5	304	-460	2869	13.65	7.18	-0.05
131	SLE FR 6	314	-480	2975	14.25	7.4	-0.05
131	SLE QP 1	289	-432	2710	12.75	6.85	-0.04
131	SLE QP 2	304	-460	2869	13.65	7.18	-0.05
131	SLD 1	363	-464	2997	13.38	10.57	-0.01
131	SLD 2	363	-464	2997	13.38	10.57	-0.01
131	SLD 3	381	-535	3262	16.11	9.98	-0.04
131	SLD 4	381	-535	3262	16.11	9.98	-0.04
131	SLD 5	294	-354	2505	9.43	9.1	0
131	SLD 6	294	-354	2505	9.43	9.1	0
131	SLD 7	355	-590	3389	18.53	7.12	-0.08
131	SLD 8	355	-590	3389	18.53	7.12	-0.08
131	SLD 9	253	-330	2349	8.77	7.24	-0.01
131	SLD 10	253	-330	2349	8.77	7.24	-0.01
131	SLD 11	314	-567	3233	17.87	5.26	-0.1
131	SLD 12	314	-567	3233	17.87	5.26	-0.1
131	SLD 13	227	-386	2476	11.19	4.38	-0.06
131	SLD 14	227	-386	2476	11.19	4.38	-0.06
131	SLD 15	245	-457	2741	13.92	3.79	-0.09
131	SLD 16	245	-457	2741	13.92	3.79	-0.09
131	SLV 1	442	-473	3173	13.08	15.35	0.04
131	SLV 2	442	-473	3173	13.08	15.35	0.04
131	SLV 3	485	-641	3798	19.53	13.96	-0.02
131	SLV 4	485	-641	3798	19.53	13.96	-0.02
131	SLV 5	281	-210	2011	3.7	11.73	0.07
131	SLV 6	281	-210	2011	3.7	11.73	0.07
131	SLV 7	423	-769	4096	25.19	7.12	-0.13
131	SLV 8	423	-769	4096	25.19	7.12	-0.13



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
131	SLV 9	185	-152	1642	2.1	7.25	0.03
131	SLV 10	185	-152	1642	2.1	7.25	0.03
131	SLV 11	327	-711	3727	23.6	2.63	-0.17
131	SLV 12	327	-711	3727	23.6	2.63	-0.17
131	SLV 13	123	-280	1940	7.77	0.4	-0.08
131	SLV 14	123	-280	1940	7.77	0.4	-0.08
131	SLV 15	166	-448	2565	14.22	-0.99	-0.14
131	SLV 16	166	-448	2565	14.22	-0.99	-0.14
132	SLU 1	127	-3	1955	0.92	7.88	0.01
132	SLU 2	126	-7	1924	3.72	7.75	0
132	SLU 3	127	-3	1955	0.92	7.88	0.01
132	SLU 4	127	-5	1936	2.6	7.8	0.01
132	SLU 5	126	-7	1924	3.72	7.75	0
132	SLU 6	127	-3	1955	0.92	7.88	0.01
132	SLU 7	127	-5	1936	2.6	7.8	0.01
132	SLU 8	127	-3	1955	0.92	7.88	0.01
132	SLU 9	127	-5	1936	2.6	7.8	0.01
132	SLU 10	137	-8	2303	3.9	8.94	0.01
132	SLU 11	139	-4	2333	1.1	9.07	0.01
132	SLU 12	138	-6	2315	2.78	8.99	0.01
132	SLU 13	137	-8	2303	3.9	8.94	0.01
132	SLU 14	139	-4	2333	1.1	9.07	0.01
132	SLU 15	138	-6	2315	2.78	8.99	0.01
132	SLU 16	139	-4	2333	1.1	9.07	0.01
132	SLU 17	138	-6	2315	2.78	8.99	0.01
132	SLU 18	143	-4	2496	1.18	9.58	0.01
132	SLU 19	143	-6	2477	2.86	9.5	0.01
132	SLU 20	143	-4	2496	1.18	9.58	0.01
132	SLU 21	143	-6	2477	2.86	9.5	0.01
132	SLU 22	128	-3	2142	1.02	8.28	0.01
132	SLU 23	127	-7	2112	3.82	8.15	0
132	SLU 24	128	-3	2142	1.02	8.28	0.01
132	SLU 25	128	-6	2124	2.7	8.2	0.01
132	SLU 26	127	-7	2112	3.82	8.15	0
132	SLU 27	128	-3	2142	1.02	8.28	0.01
132	SLU 28	128	-6	2124	2.7	8.2	0.01
132	SLU 29	128	-3	2142	1.02	8.28	0.01
132	SLU 30	128	-6	2124	2.7	8.2	0.01
132	SLU 31	138	-8	2490	4	9.34	0.01
132	SLU 32	140	-4	2521	1.2	9.47	0.01
132	SLU 33	139	-6	2503	2.88	9.39	0.01
132	SLU 34	138	-8	2490	4	9.34	0.01
132	SLU 35	140	-4	2521	1.2	9.47	0.01
132	SLU 36	139	-6	2503	2.88	9.39	0.01
132	SLU 37	140	-4	2521	1.2	9.47	0.01
132	SLU 38	139	-6	2503	2.88	9.39	0.01
132	SLU 39	144	-4	2683	1.28	9.98	0.01
132	SLU 40	144	-7	2665	2.96	9.91	0.01
132	SLU 41	144	-4	2683	1.28	9.98	0.01
132	SLU 42	144	-7	2665	2.96	9.91	0.01
132	SLU 43	165	-4	2477	1.16	10.1	0.01
132	SLU 44	164	-8	2446	3.96	9.97	0.01
132	SLU 45	165	-4	2477	1.16	10.1	0.01
132	SLU 46	165	-6	2458	2.84	10.02	0.01
132	SLU 47	164	-8	2446	3.96	9.97	0.01
132	SLU 48	165	-4	2477	1.16	10.1	0.01
132	SLU 49	165	-6	2458	2.84	10.02	0.01
132	SLU 50	165	-4	2477	1.16	10.1	0.01
132	SLU 51	165	-6	2458	2.84	10.02	0.01
132	SLU 52	175	-8	2825	4.14	11.17	0.01
132	SLU 53	177	-4	2855	1.34	11.3	0.01
132	SLU 54	176	-7	2837	3.02	11.22	0.01
132	SLU 55	175	-8	2825	4.14	11.17	0.01
132	SLU 56	177	-4	2855	1.34	11.3	0.01
132	SLU 57	176	-7	2837	3.02	11.22	0.01
132	SLU 58	177	-4	2855	1.34	11.3	0.01
132	SLU 59	176	-7	2837	3.02	11.22	0.01
132	SLU 60	181	-5	3018	1.42	11.81	0.02
132	SLU 61	181	-7	2999	3.1	11.73	0.01
132	SLU 62	181	-5	3018	1.42	11.81	0.02
132	SLU 63	181	-7	2999	3.1	11.73	0.01
132	SLU 64	166	-4	2664	1.26	10.5	0.01
132	SLU 65	165	-8	2634	4.07	10.37	0.01
132	SLU 66	166	-4	2664	1.26	10.5	0.01
132	SLU 67	166	-7	2646	2.94	10.42	0.01
132	SLU 68	165	-8	2634	4.07	10.37	0.01
132	SLU 69	166	-4	2664	1.26	10.5	0.01
132	SLU 70	166	-7	2646	2.94	10.42	0.01
132	SLU 71	166	-4	2664	1.26	10.5	0.01
132	SLU 72	166	-7	2646	2.94	10.42	0.01
132	SLU 73	176	-9	3012	4.24	11.57	0.01
132	SLU 74	178	-5	3043	1.44	11.7	0.02
132	SLU 75	177	-7	3025	3.12	11.62	0.01
132	SLU 76	176	-9	3012	4.24	11.57	0.01
132	SLU 77	178	-5	3043	1.44	11.7	0.02
132	SLU 78	177	-7	3025	3.12	11.62	0.01
132	SLU 79	178	-5	3043	1.44	11.7	0.02
132	SLU 80	177	-7	3025	3.12	11.62	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
132	SLU 81	182	-5	3205	1.52	12.21	0.02
132	SLU 82	182	-8	3187	3.2	12.13	0.01
132	SLU 83	182	-5	3205	1.52	12.21	0.02
132	SLU 84	182	-8	3187	3.2	12.13	0.01
132	SLE RA 1	128	-3	2008	0.95	7.99	0.01
132	SLE RA 2	127	-6	1988	2.82	7.9	0.01
132	SLE RA 3	128	-3	2008	0.95	7.99	0.01
132	SLE RA 4	127	-5	1996	2.07	7.94	0.01
132	SLE RA 5	127	-6	1988	2.82	7.9	0.01
132	SLE RA 6	128	-3	2008	0.95	7.99	0.01
132	SLE RA 7	127	-5	1996	2.07	7.94	0.01
132	SLE RA 8	128	-3	2008	0.95	7.99	0.01
132	SLE RA 9	127	-5	1996	2.07	7.94	0.01
132	SLE RA 10	134	-6	2240	2.94	8.7	0.01
132	SLE RA 11	135	-4	2261	1.07	8.79	0.01
132	SLE RA 12	135	-5	2248	2.19	8.74	0.01
132	SLE RA 13	134	-6	2240	2.94	8.7	0.01
132	SLE RA 14	135	-4	2261	1.07	8.79	0.01
132	SLE RA 15	135	-5	2248	2.19	8.74	0.01
132	SLE RA 16	135	-4	2261	1.07	8.79	0.01
132	SLE RA 17	135	-5	2248	2.19	8.74	0.01
132	SLE RA 18	138	-4	2369	1.12	9.13	0.01
132	SLE RA 19	138	-5	2357	2.24	9.08	0.01
132	SLE RA 20	138	-4	2369	1.12	9.13	0.01
132	SLE RA 21	138	-5	2357	2.24	9.08	0.01
132	SLE FR 1	128	-3	2008	0.95	7.99	0.01
132	SLE FR 2	128	-4	2004	1.32	7.97	0.01
132	SLE FR 3	128	-3	2008	0.95	7.99	0.01
132	SLE FR 4	131	-4	2112	1.37	8.31	0.01
132	SLE FR 5	131	-3	2116	1	8.33	0.01
132	SLE FR 6	133	-3	2189	1.03	8.56	0.01
132	SLE QP 1	128	-3	2008	0.95	7.99	0.01
132	SLE QP 2	131	-3	2116	1	8.33	0.01
132	SLD 1	246	14	2184	-9.81	13.58	0.04
132	SLD 2	246	14	2184	-9.81	13.58	0.04
132	SLD 3	220	12	2352	-6.91	12.7	0.03
132	SLD 4	220	12	2352	-6.91	12.7	0.03
132	SLD 5	204	5	1882	-6.63	11.25	0.03
132	SLD 6	204	5	1882	-6.63	11.25	0.03
132	SLD 7	119	-2	2442	3.02	8.3	0.01
132	SLD 8	119	-2	2442	3.02	8.3	0.01
132	SLD 9	143	-5	1791	-1.02	8.36	0.01
132	SLD 10	143	-5	1791	-1.02	8.36	0.01
132	SLD 11	58	-12	2351	8.63	5.42	0
132	SLD 12	58	-12	2351	8.63	5.42	0
132	SLD 13	42	-19	1881	8.91	3.96	-0.01
132	SLD 14	42	-19	1881	8.91	3.96	-0.01
132	SLD 15	16	-21	2049	11.81	3.08	-0.02
132	SLD 16	16	-21	2049	11.81	3.08	-0.02
132	SLV 1	400	41	2277	-26.61	20.66	0.08
132	SLV 2	400	41	2277	-26.61	20.66	0.08
132	SLV 3	340	36	2673	-19.77	18.6	0.06
132	SLV 4	340	36	2673	-19.77	18.6	0.06
132	SLV 5	303	18	1564	-17.65	15.15	0.05
132	SLV 6	303	18	1564	-17.65	15.15	0.05
132	SLV 7	103	1	2884	5.14	8.29	0.01
132	SLV 8	103	1	2884	5.14	8.29	0.01
132	SLV 9	159	-8	1349	-3.14	8.37	0.01
132	SLV 10	159	-8	1349	-3.14	8.37	0.01
132	SLV 11	-41	-24	2669	19.65	1.51	-0.03
132	SLV 12	-41	-24	2669	19.65	1.51	-0.03
132	SLV 13	-78	-43	1560	21.77	-1.94	-0.04
132	SLV 14	-78	-43	1560	21.77	-1.94	-0.04
132	SLV 15	-138	-48	1956	28.61	-4	-0.05
132	SLV 16	-138	-48	1956	28.61	-4	-0.05
133	SLU 1	74	0	1679	0.31	4.18	0
133	SLU 2	68	-7	1665	5.36	3.83	-0.01
133	SLU 3	74	0	1679	0.31	4.18	0
133	SLU 4	71	-4	1671	3.34	3.97	-0.01
133	SLU 5	68	-7	1665	5.36	3.83	-0.01
133	SLU 6	74	0	1679	0.31	4.18	0
133	SLU 7	71	-4	1671	3.34	3.97	-0.01
133	SLU 8	74	0	1679	0.31	4.18	0
133	SLU 9	71	-4	1671	3.34	3.97	-0.01
133	SLU 10	75	-7	1951	5.33	4.49	-0.01
133	SLU 11	81	0	1965	0.29	4.85	-0.01
133	SLU 12	77	-4	1957	3.31	4.63	-0.01
133	SLU 13	75	-7	1951	5.33	4.49	-0.01
133	SLU 14	81	0	1965	0.29	4.85	-0.01
133	SLU 15	77	-4	1957	3.31	4.63	-0.01
133	SLU 16	81	0	1965	0.29	4.85	-0.01
133	SLU 17	77	-4	1957	3.31	4.63	-0.01
133	SLU 18	84	0	2088	0.27	5.13	-0.01
133	SLU 19	80	-4	2079	3.3	4.91	-0.01
133	SLU 20	84	0	2088	0.27	5.13	-0.01
133	SLU 21	80	-4	2079	3.3	4.91	-0.01
133	SLU 22	73	0	1820	0.31	4.32	0
133	SLU 23	67	-7	1806	5.36	3.96	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
133	SLU 24	73	0	1820	0.31	4.32	0
133	SLU 25	70	-4	1812	3.34	4.11	-0.01
133	SLU 26	67	-7	1806	5.36	3.96	-0.01
133	SLU 27	73	0	1820	0.31	4.32	0
133	SLU 28	70	-4	1812	3.34	4.11	-0.01
133	SLU 29	73	0	1820	0.31	4.32	0
133	SLU 30	70	-4	1812	3.34	4.11	-0.01
133	SLU 31	74	-7	2092	5.33	4.62	-0.01
133	SLU 32	80	0	2106	0.29	4.98	-0.01
133	SLU 33	76	-4	2098	3.31	4.77	-0.01
133	SLU 34	74	-7	2092	5.33	4.62	-0.01
133	SLU 35	80	0	2106	0.29	4.98	-0.01
133	SLU 36	76	-4	2098	3.31	4.77	-0.01
133	SLU 37	80	0	2106	0.29	4.98	-0.01
133	SLU 38	76	-4	2098	3.31	4.77	-0.01
133	SLU 39	83	0	2228	0.28	5.27	-0.01
133	SLU 40	79	-4	2220	3.3	5.05	-0.01
133	SLU 41	83	0	2228	0.28	5.27	-0.01
133	SLU 42	79	-4	2220	3.3	5.05	-0.01
133	SLU 43	97	0	2135	0.41	5.39	-0.01
133	SLU 44	91	-7	2121	5.45	5.03	-0.01
133	SLU 45	97	0	2135	0.41	5.39	-0.01
133	SLU 46	94	-4	2126	3.43	5.18	-0.01
133	SLU 47	91	-7	2121	5.45	5.03	-0.01
133	SLU 48	97	0	2135	0.41	5.39	-0.01
133	SLU 49	94	-4	2126	3.43	5.18	-0.01
133	SLU 50	97	0	2135	0.41	5.39	-0.01
133	SLU 51	94	-4	2126	3.43	5.18	-0.01
133	SLU 52	98	-7	2407	5.42	5.69	-0.01
133	SLU 53	104	0	2421	0.38	6.05	-0.01
133	SLU 54	100	-4	2412	3.41	5.84	-0.01
133	SLU 55	98	-7	2407	5.42	5.69	-0.01
133	SLU 56	104	0	2421	0.38	6.05	-0.01
133	SLU 57	100	-4	2412	3.41	5.84	-0.01
133	SLU 58	104	0	2421	0.38	6.05	-0.01
133	SLU 59	100	-4	2412	3.41	5.84	-0.01
133	SLU 60	107	0	2543	0.37	6.34	-0.01
133	SLU 61	103	-4	2535	3.39	6.12	-0.01
133	SLU 62	107	0	2543	0.37	6.34	-0.01
133	SLU 63	103	-4	2535	3.39	6.12	-0.01
133	SLU 64	96	0	2276	0.41	5.53	-0.01
133	SLU 65	90	-7	2262	5.45	5.17	-0.01
133	SLU 66	96	0	2276	0.41	5.53	-0.01
133	SLU 67	92	-4	2267	3.44	5.32	-0.01
133	SLU 68	90	-7	2262	5.45	5.17	-0.01
133	SLU 69	96	0	2276	0.41	5.53	-0.01
133	SLU 70	92	-4	2267	3.44	5.32	-0.01
133	SLU 71	96	0	2276	0.41	5.53	-0.01
133	SLU 72	92	-4	2267	3.44	5.32	-0.01
133	SLU 73	97	-7	2547	5.43	5.83	-0.01
133	SLU 74	103	0	2561	0.38	6.19	-0.01
133	SLU 75	99	-4	2553	3.41	5.98	-0.01
133	SLU 76	97	-7	2547	5.43	5.83	-0.01
133	SLU 77	103	0	2561	0.38	6.19	-0.01
133	SLU 78	99	-4	2553	3.41	5.98	-0.01
133	SLU 79	103	0	2561	0.38	6.19	-0.01
133	SLU 80	99	-4	2553	3.41	5.98	-0.01
133	SLU 81	105	0	2684	0.37	6.47	-0.01
133	SLU 82	102	-4	2676	3.4	6.26	-0.01
133	SLU 83	105	0	2684	0.37	6.47	-0.01
133	SLU 84	102	-4	2676	3.4	6.26	-0.01
133	SLE RA 1	74	0	1720	0.31	4.22	0
133	SLE RA 2	70	-5	1710	3.68	3.98	-0.01
133	SLE RA 3	74	0	1720	0.31	4.22	0
133	SLE RA 4	72	-3	1714	2.33	4.08	-0.01
133	SLE RA 5	70	-5	1710	3.68	3.98	-0.01
133	SLE RA 6	74	0	1720	0.31	4.22	0
133	SLE RA 7	72	-3	1714	2.33	4.08	-0.01
133	SLE RA 8	74	0	1720	0.31	4.22	0
133	SLE RA 9	72	-3	1714	2.33	4.08	-0.01
133	SLE RA 10	75	-5	1901	3.66	4.43	-0.01
133	SLE RA 11	79	0	1910	0.29	4.66	-0.01
133	SLE RA 12	76	-3	1904	2.31	4.52	-0.01
133	SLE RA 13	75	-5	1901	3.66	4.43	-0.01
133	SLE RA 14	79	0	1910	0.29	4.66	-0.01
133	SLE RA 15	76	-3	1904	2.31	4.52	-0.01
133	SLE RA 16	79	0	1910	0.29	4.66	-0.01
133	SLE RA 17	76	-3	1904	2.31	4.52	-0.01
133	SLE RA 18	80	0	1992	0.29	4.85	-0.01
133	SLE RA 19	78	-3	1986	2.31	4.71	-0.01
133	SLE RA 20	80	0	1992	0.29	4.85	-0.01
133	SLE RA 21	78	-3	1986	2.31	4.71	-0.01
133	SLE FR 1	74	0	1720	0.31	4.22	0
133	SLE FR 2	73	-1	1718	0.99	4.18	-0.01
133	SLE FR 3	74	0	1720	0.31	4.22	0
133	SLE FR 4	75	-1	1799	0.98	4.37	-0.01
133	SLE FR 5	76	0	1801	0.31	4.41	0
133	SLE FR 6	77	0	1856	0.3	4.54	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
133	SLE QP 1	74	0	1720	0.31	4.22	0
133	SLE QP 2	76	0	1801	0.31	4.41	0
133	SLD 1	201	27	1832	-19.13	9.91	0.01
133	SLD 2	201	27	1832	-19.13	9.91	0.01
133	SLD 3	177	22	1945	-12.91	8.99	0
133	SLD 4	177	22	1945	-12.91	8.99	0
133	SLD 5	149	15	1638	-14.97	7.46	0.02
133	SLD 6	149	15	1638	-14.97	7.46	0.02
133	SLD 7	71	-1	2016	5.78	4.39	-0.02
133	SLD 8	71	-1	2016	5.78	4.39	-0.02
133	SLD 9	81	0	1586	-5.17	4.44	0.01
133	SLD 10	81	0	1586	-5.17	4.44	0.01
133	SLD 11	3	-15	1964	15.58	1.36	-0.02
133	SLD 12	3	-15	1964	15.58	1.36	-0.02
133	SLD 13	-25	-22	1657	13.52	-0.17	-0.01
133	SLD 14	-25	-22	1657	13.52	-0.17	-0.01
133	SLD 15	-49	-27	1771	19.74	-1.09	-0.02
133	SLD 16	-49	-27	1771	19.74	-1.09	-0.02
133	SLV 1	369	68	1874	-49.27	17.35	0.04
133	SLV 2	369	68	1874	-49.27	17.35	0.04
133	SLV 3	314	57	2141	-34.6	15.19	0.02
133	SLV 4	314	57	2141	-34.6	15.19	0.02
133	SLV 5	248	37	1418	-36.82	11.57	0.04
133	SLV 6	248	37	1418	-36.82	11.57	0.04
133	SLV 7	64	0	2308	12.08	4.37	-0.03
133	SLV 8	64	0	2308	12.08	4.37	-0.03
133	SLV 9	88	0	1294	-11.47	4.45	0.02
133	SLV 10	88	0	1294	-11.47	4.45	0.02
133	SLV 11	-96	-38	2184	37.43	-2.74	-0.05
133	SLV 12	-96	-38	2184	37.43	-2.74	-0.05
133	SLV 13	-162	-58	1462	35.21	-6.37	-0.03
133	SLV 14	-162	-58	1462	35.21	-6.37	-0.03
133	SLV 15	-217	-69	1729	49.88	-8.52	-0.05
133	SLV 16	-217	-69	1729	49.88	-8.52	-0.05
134	SLU 1	45	0	1519	0.06	2.63	0
134	SLU 2	36	-8	1516	6.46	2.2	-0.01
134	SLU 3	45	0	1519	0.06	2.63	0
134	SLU 4	39	-5	1517	3.9	2.37	0
134	SLU 5	36	-8	1516	6.46	2.2	-0.01
134	SLU 6	45	0	1519	0.06	2.63	0
134	SLU 7	39	-5	1517	3.9	2.37	0
134	SLU 8	45	0	1519	0.06	2.63	0
134	SLU 9	39	-5	1517	3.9	2.37	0
134	SLU 10	44	-7	1744	6.33	2.81	-0.01
134	SLU 11	54	0	1746	-0.07	3.24	0
134	SLU 12	48	-4	1745	3.77	2.98	0
134	SLU 13	44	-7	1744	6.33	2.81	-0.01
134	SLU 14	54	0	1746	-0.07	3.24	0
134	SLU 15	48	-4	1745	3.77	2.98	0
134	SLU 16	54	0	1746	-0.07	3.24	0
134	SLU 17	48	-4	1745	3.77	2.98	0
134	SLU 18	58	0	1844	-0.13	3.51	0
134	SLU 19	52	-4	1842	3.71	3.25	0
134	SLU 20	58	0	1844	-0.13	3.51	0
134	SLU 21	52	-4	1842	3.71	3.25	0
134	SLU 22	45	0	1630	0.02	2.75	0
134	SLU 23	35	-8	1627	6.42	2.31	-0.01
134	SLU 24	45	0	1630	0.02	2.75	0
134	SLU 25	39	-4	1629	3.86	2.49	0
134	SLU 26	35	-8	1627	6.42	2.31	-0.01
134	SLU 27	45	0	1630	0.02	2.75	0
134	SLU 28	39	-4	1629	3.86	2.49	0
134	SLU 29	45	0	1630	0.02	2.75	0
134	SLU 30	39	-4	1629	3.86	2.49	0
134	SLU 31	44	-7	1855	6.28	2.92	-0.01
134	SLU 32	54	0	1858	-0.12	3.36	0
134	SLU 33	48	-4	1856	3.72	3.1	0
134	SLU 34	44	-7	1855	6.28	2.92	-0.01
134	SLU 35	54	0	1858	-0.12	3.36	0
134	SLU 36	48	-4	1856	3.72	3.1	0
134	SLU 37	54	0	1858	-0.12	3.36	0
134	SLU 38	48	-4	1856	3.72	3.1	0
134	SLU 39	58	0	1955	-0.18	3.62	0
134	SLU 40	52	-4	1953	3.66	3.36	0
134	SLU 41	58	0	1955	-0.18	3.62	0
134	SLU 42	52	-4	1953	3.66	3.36	0
134	SLU 43	59	0	1937	0.1	3.38	0
134	SLU 44	49	-8	1934	6.5	2.95	-0.01
134	SLU 45	59	0	1937	0.1	3.38	0
134	SLU 46	53	-5	1935	3.94	3.12	0
134	SLU 47	49	-8	1934	6.5	2.95	-0.01
134	SLU 48	59	0	1937	0.1	3.38	0
134	SLU 49	53	-5	1935	3.94	3.12	0
134	SLU 50	59	0	1937	0.1	3.38	0
134	SLU 51	53	-5	1935	3.94	3.12	0
134	SLU 52	58	-7	2161	6.36	3.56	-0.01
134	SLU 53	68	0	2164	-0.03	3.99	0
134	SLU 54	62	-4	2162	3.8	3.73	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
134	SLU 55	58	-7	2161	6.36	3.56	-0.01
134	SLU 56	68	0	2164	-0.03	3.99	0
134	SLU 57	62	-4	2162	3.8	3.73	0
134	SLU 58	68	0	2164	-0.03	3.99	0
134	SLU 59	62	-4	2162	3.8	3.73	0
134	SLU 60	72	0	2261	-0.09	4.26	0
134	SLU 61	66	-4	2260	3.75	4	0
134	SLU 62	72	0	2261	-0.09	4.26	0
134	SLU 63	66	-4	2260	3.75	4	0
134	SLU 64	59	0	2048	0.05	3.49	0
134	SLU 65	49	-8	2045	6.45	3.06	-0.01
134	SLU 66	59	0	2048	0.05	3.49	0
134	SLU 67	53	-4	2046	3.89	3.23	0
134	SLU 68	49	-8	2045	6.45	3.06	-0.01
134	SLU 69	59	0	2048	0.05	3.49	0
134	SLU 70	53	-4	2046	3.89	3.23	0
134	SLU 71	59	0	2048	0.05	3.49	0
134	SLU 72	53	-4	2046	3.89	3.23	0
134	SLU 73	58	-7	2272	6.32	3.67	-0.01
134	SLU 74	68	0	2275	-0.08	4.11	0
134	SLU 75	62	-4	2273	3.76	3.85	0
134	SLU 76	58	-7	2272	6.32	3.67	-0.01
134	SLU 77	68	0	2275	-0.08	4.11	0
134	SLU 78	62	-4	2273	3.76	3.85	0
134	SLU 79	68	0	2275	-0.08	4.11	0
134	SLU 80	62	-4	2273	3.76	3.85	0
134	SLU 81	71	0	2373	-0.14	4.37	0
134	SLU 82	66	-4	2371	3.7	4.11	0
134	SLU 83	71	0	2373	-0.14	4.37	0
134	SLU 84	66	-4	2371	3.7	4.11	0
134	SLE RA 1	45	0	1551	0.05	2.66	0
134	SLE RA 2	39	-5	1549	4.32	2.37	0
134	SLE RA 3	45	0	1551	0.05	2.66	0
134	SLE RA 4	41	-3	1550	2.61	2.49	0
134	SLE RA 5	39	-5	1549	4.32	2.37	0
134	SLE RA 6	45	0	1551	0.05	2.66	0
134	SLE RA 7	41	-3	1550	2.61	2.49	0
134	SLE RA 8	45	0	1551	0.05	2.66	0
134	SLE RA 9	41	-3	1550	2.61	2.49	0
134	SLE RA 10	45	-5	1700	4.23	2.78	0
134	SLE RA 11	51	0	1702	-0.04	3.07	0
134	SLE RA 12	47	-3	1701	2.52	2.9	0
134	SLE RA 13	45	-5	1700	4.23	2.78	0
134	SLE RA 14	51	0	1702	-0.04	3.07	0
134	SLE RA 15	47	-3	1701	2.52	2.9	0
134	SLE RA 16	51	0	1702	-0.04	3.07	0
134	SLE RA 17	47	-3	1701	2.52	2.9	0
134	SLE RA 18	54	0	1767	-0.08	3.25	0
134	SLE RA 19	50	-3	1766	2.48	3.07	0
134	SLE RA 20	54	0	1767	-0.08	3.25	0
134	SLE RA 21	50	-3	1766	2.48	3.07	0
134	SLE FR 1	45	0	1551	0.05	2.66	0
134	SLE FR 2	44	-1	1550	0.9	2.61	0
134	SLE FR 3	45	0	1551	0.05	2.66	0
134	SLE FR 4	46	-1	1615	0.87	2.78	0
134	SLE FR 5	48	0	1616	0.01	2.84	0
134	SLE FR 6	49	0	1659	-0.01	2.95	0
134	SLE QP 1	45	0	1551	0.05	2.66	0
134	SLE QP 2	48	0	1616	0.01	2.84	0
134	SLD 1	182	31	1630	-25.2	8.63	0.03
134	SLD 2	182	31	1630	-25.2	8.63	0.03
134	SLD 3	158	21	1712	-15.46	7.68	0.01
134	SLD 4	158	21	1712	-15.46	7.68	0.01
134	SLD 5	123	24	1496	-22.32	6.01	0.03
134	SLD 6	123	24	1496	-22.32	6.01	0.03
134	SLD 7	46	-8	1769	10.14	2.86	-0.02
134	SLD 8	46	-8	1769	10.14	2.86	-0.02
134	SLD 9	50	8	1462	-10.11	2.82	0.02
134	SLD 10	50	8	1462	-10.11	2.82	0.02
134	SLD 11	-28	-23	1736	22.34	-0.33	-0.03
134	SLD 12	-28	-23	1736	22.34	-0.33	-0.03
134	SLD 13	-63	-21	1519	15.49	-2	-0.02
134	SLD 14	-63	-21	1519	15.49	-2	-0.02
134	SLD 15	-86	-31	1601	25.22	-2.95	-0.03
134	SLD 16	-86	-31	1601	25.22	-2.95	-0.03
134	SLV 1	363	78	1650	-64.12	16.46	0.07
134	SLV 2	363	78	1650	-64.12	16.46	0.07
134	SLV 3	308	56	1843	-41.2	14.25	0.04
134	SLV 4	308	56	1843	-41.2	14.25	0.04
134	SLV 5	225	57	1333	-54	10.28	0.07
134	SLV 6	225	57	1333	-54	10.28	0.07
134	SLV 7	43	-16	1977	22.42	2.91	-0.04
134	SLV 8	43	-16	1977	22.42	2.91	-0.04
134	SLV 9	52	17	1254	-22.39	2.77	0.04
134	SLV 10	52	17	1254	-22.39	2.77	0.04
134	SLV 11	-130	-57	1899	54.02	-4.61	-0.07
134	SLV 12	-130	-57	1899	54.02	-4.61	-0.07
134	SLV 13	-213	-56	1388	41.22	-8.57	-0.04





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
134	SLV 14	-213	-56	1388	41.22	-8.57	-0.04
134	SLV 15	-268	-78	1582	64.14	-10.79	-0.07
134	SLV 16	-268	-78	1582	64.14	-10.79	-0.07
135	SLU 1	51	0	1395	-0.04	2.79	0
135	SLU 2	37	-7	1399	6.87	2.12	-0.01
135	SLU 3	51	0	1395	-0.04	2.79	0
135	SLU 4	42	-4	1398	4.11	2.39	0
135	SLU 5	37	-7	1399	6.87	2.12	-0.01
135	SLU 6	51	0	1395	-0.04	2.79	0
135	SLU 7	42	-4	1398	4.11	2.39	0
135	SLU 8	51	0	1395	-0.04	2.79	0
135	SLU 9	42	-4	1398	4.11	2.39	0
135	SLU 10	57	-7	1585	6.68	3.21	-0.01
135	SLU 11	72	0	1581	-0.23	3.89	0
135	SLU 12	63	-4	1584	3.92	3.48	0
135	SLU 13	57	-7	1585	6.68	3.21	-0.01
135	SLU 14	72	0	1581	-0.23	3.89	0
135	SLU 15	63	-4	1584	3.92	3.48	0
135	SLU 16	72	0	1581	-0.23	3.89	0
135	SLU 17	63	-4	1584	3.92	3.48	0
135	SLU 18	81	0	1661	-0.31	4.36	0
135	SLU 19	72	-4	1663	3.84	3.95	0
135	SLU 20	81	0	1661	-0.31	4.36	0
135	SLU 21	72	-4	1663	3.84	3.95	0
135	SLU 22	57	0	1485	-0.11	3.14	0
135	SLU 23	42	-7	1489	6.8	2.46	-0.01
135	SLU 24	57	0	1485	-0.11	3.14	0
135	SLU 25	48	-4	1488	4.03	2.73	0
135	SLU 26	42	-7	1489	6.8	2.46	-0.01
135	SLU 27	57	0	1485	-0.11	3.14	0
135	SLU 28	48	-4	1488	4.03	2.73	0
135	SLU 29	57	0	1485	-0.11	3.14	0
135	SLU 30	48	-4	1488	4.03	2.73	0
135	SLU 31	63	-7	1675	6.61	3.55	-0.01
135	SLU 32	78	0	1671	-0.3	4.23	0
135	SLU 33	69	-4	1673	3.85	3.83	0
135	SLU 34	63	-7	1675	6.61	3.55	-0.01
135	SLU 35	78	0	1671	-0.3	4.23	0
135	SLU 36	69	-4	1673	3.85	3.83	0
135	SLU 37	78	0	1671	-0.3	4.23	0
135	SLU 38	69	-4	1673	3.85	3.83	0
135	SLU 39	87	1	1751	-0.38	4.7	0
135	SLU 40	78	-4	1753	3.77	4.3	0
135	SLU 41	87	1	1751	-0.38	4.7	0
135	SLU 42	78	-4	1753	3.77	4.3	0
135	SLU 43	65	0	1783	-0.03	3.51	0
135	SLU 44	50	-7	1787	6.88	2.84	-0.01
135	SLU 45	65	0	1783	-0.03	3.51	0
135	SLU 46	56	-4	1785	4.12	3.11	0
135	SLU 47	50	-7	1787	6.88	2.84	-0.01
135	SLU 48	65	0	1783	-0.03	3.51	0
135	SLU 49	56	-4	1785	4.12	3.11	0
135	SLU 50	65	0	1783	-0.03	3.51	0
135	SLU 51	56	-4	1785	4.12	3.11	0
135	SLU 52	71	-7	1973	6.7	3.93	-0.01
135	SLU 53	86	0	1969	-0.22	4.61	0
135	SLU 54	77	-4	1971	3.93	4.2	0
135	SLU 55	71	-7	1973	6.7	3.93	-0.01
135	SLU 56	86	0	1969	-0.22	4.61	0
135	SLU 57	77	-4	1971	3.93	4.2	0
135	SLU 58	86	0	1969	-0.22	4.61	0
135	SLU 59	77	-4	1971	3.93	4.2	0
135	SLU 60	95	0	2048	-0.3	5.08	0
135	SLU 61	86	-4	2051	3.85	4.67	0
135	SLU 62	95	0	2048	-0.3	5.08	0
135	SLU 63	86	-4	2051	3.85	4.67	0
135	SLU 64	70	0	1873	-0.1	3.86	0
135	SLU 65	56	-7	1877	6.81	3.18	-0.01
135	SLU 66	70	0	1873	-0.1	3.86	0
135	SLU 67	61	-4	1875	4.05	3.45	0
135	SLU 68	56	-7	1877	6.81	3.18	-0.01
135	SLU 69	70	0	1873	-0.1	3.86	0
135	SLU 70	61	-4	1875	4.05	3.45	0
135	SLU 71	70	0	1873	-0.1	3.86	0
135	SLU 72	61	-4	1875	4.05	3.45	0
135	SLU 73	76	-7	2063	6.62	4.27	-0.01
135	SLU 74	91	0	2059	-0.29	4.95	0
135	SLU 75	82	-4	2061	3.86	4.55	0
135	SLU 76	76	-7	2063	6.62	4.27	-0.01
135	SLU 77	91	0	2059	-0.29	4.95	0
135	SLU 78	82	-4	2061	3.86	4.55	0
135	SLU 79	91	0	2059	-0.29	4.95	0
135	SLU 80	82	-4	2061	3.86	4.55	0
135	SLU 81	100	1	2138	-0.37	5.42	0
135	SLU 82	91	-4	2141	3.78	5.02	0
135	SLU 83	100	1	2138	-0.37	5.42	0
135	SLU 84	91	-4	2141	3.78	5.02	0
135	SLE RA 1	53	0	1421	-0.06	2.89	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
135	SLE RA 2	43	-5	1424	4.55	2.44	0
135	SLE RA 3	53	0	1421	-0.06	2.89	0
135	SLE RA 4	47	-3	1423	2.7	2.62	0
135	SLE RA 5	43	-5	1424	4.55	2.44	0
135	SLE RA 6	53	0	1421	-0.06	2.89	0
135	SLE RA 7	47	-3	1423	2.7	2.62	0
135	SLE RA 8	53	0	1421	-0.06	2.89	0
135	SLE RA 9	47	-3	1423	2.7	2.62	0
135	SLE RA 10	57	-5	1548	4.42	3.17	0
135	SLE RA 11	67	0	1545	-0.19	3.62	0
135	SLE RA 12	61	-3	1546	2.58	3.35	0
135	SLE RA 13	57	-5	1548	4.42	3.17	0
135	SLE RA 14	67	0	1545	-0.19	3.62	0
135	SLE RA 15	61	-3	1546	2.58	3.35	0
135	SLE RA 16	67	0	1545	-0.19	3.62	0
135	SLE RA 17	61	-3	1546	2.58	3.35	0
135	SLE RA 18	73	0	1598	-0.24	3.93	0
135	SLE RA 19	67	-3	1600	2.52	3.66	0
135	SLE RA 20	73	0	1598	-0.24	3.93	0
135	SLE RA 21	67	-3	1600	2.52	3.66	0
135	SLE FR 1	53	0	1421	-0.06	2.89	0
135	SLE FR 2	51	-1	1421	0.86	2.8	0
135	SLE FR 3	53	0	1421	-0.06	2.89	0
135	SLE FR 4	57	-1	1475	0.81	3.11	0
135	SLE FR 5	59	0	1474	-0.11	3.2	0
135	SLE FR 6	63	0	1509	-0.15	3.41	0
135	SLE QP 1	53	0	1421	-0.06	2.89	0
135	SLE QP 2	59	0	1474	-0.11	3.2	0
135	SLD 1	204	32	1484	-28.48	9.48	0.03
135	SLD 2	204	32	1484	-28.48	9.48	0.03
135	SLD 3	180	18	1543	-15.68	8.47	0.01
135	SLD 4	180	18	1543	-15.68	8.47	0.01
135	SLD 5	139	30	1387	-28.03	6.61	0.04
135	SLD 6	139	30	1387	-28.03	6.61	0.04
135	SLD 7	59	-15	1584	14.63	3.26	-0.03
135	SLD 8	59	-15	1584	14.63	3.26	-0.03
135	SLD 9	59	16	1363	-14.86	3.15	0.03
135	SLD 10	59	16	1363	-14.86	3.15	0.03
135	SLD 11	-21	-30	1561	27.8	-0.2	-0.04
135	SLD 12	-21	-30	1561	27.8	-0.2	-0.04
135	SLD 13	-63	-18	1404	15.45	-2.07	-0.01
135	SLD 14	-63	-18	1404	15.45	-2.07	-0.01
135	SLD 15	-87	-31	1464	28.25	-3.07	-0.03
135	SLD 16	-87	-31	1464	28.25	-3.07	-0.03
135	SLV 1	401	80	1499	-72.01	18	0.08
135	SLV 2	401	80	1499	-72.01	18	0.08
135	SLV 3	345	48	1638	-41.89	15.65	0.03
135	SLV 4	345	48	1638	-41.89	15.65	0.03
135	SLV 5	247	73	1270	-67.37	11.21	0.09
135	SLV 6	247	73	1270	-67.37	11.21	0.09
135	SLV 7	60	-34	1735	33.03	3.37	-0.06
135	SLV 8	60	-34	1735	33.03	3.37	-0.06
135	SLV 9	58	34	1213	-33.26	3.04	0.06
135	SLV 10	58	34	1213	-33.26	3.04	0.06
135	SLV 11	-129	-72	1678	67.14	-4.8	-0.09
135	SLV 12	-129	-72	1678	67.14	-4.8	-0.09
135	SLV 13	-228	-48	1310	41.67	-9.24	-0.03
135	SLV 14	-228	-48	1310	41.67	-9.24	-0.03
135	SLV 15	-284	-80	1449	71.79	-11.59	-0.08
135	SLV 16	-284	-80	1449	71.79	-11.59	-0.08
136	SLU 1	73	0	1314	-0.08	3.39	0
136	SLU 2	55	-6	1321	6.66	2.63	-0.01
136	SLU 3	73	0	1314	-0.08	3.39	0
136	SLU 4	62	-4	1318	3.96	2.93	0
136	SLU 5	55	-6	1321	6.66	2.63	-0.01
136	SLU 6	73	0	1314	-0.08	3.39	0
136	SLU 7	62	-4	1318	3.96	2.93	0
136	SLU 8	73	0	1314	-0.08	3.39	0
136	SLU 9	62	-4	1318	3.96	2.93	0
136	SLU 10	91	-6	1485	6.45	4.21	-0.01
136	SLU 11	109	0	1478	-0.28	4.96	0
136	SLU 12	98	-3	1482	3.76	4.51	0
136	SLU 13	91	-6	1485	6.45	4.21	-0.01
136	SLU 14	109	0	1478	-0.28	4.96	0
136	SLU 15	98	-3	1482	3.76	4.51	0
136	SLU 16	109	0	1478	-0.28	4.96	0
136	SLU 17	98	-3	1482	3.76	4.51	0
136	SLU 18	124	0	1548	-0.37	5.63	0
136	SLU 19	114	-3	1552	3.67	5.18	0
136	SLU 20	124	0	1548	-0.37	5.63	0
136	SLU 21	114	-3	1552	3.67	5.18	0
136	SLU 22	86	0	1392	-0.16	3.96	0
136	SLU 23	68	-6	1399	6.58	3.21	-0.01
136	SLU 24	86	0	1392	-0.16	3.96	0
136	SLU 25	75	-4	1396	3.88	3.51	0
136	SLU 26	68	-6	1399	6.58	3.21	-0.01
136	SLU 27	86	0	1392	-0.16	3.96	0
136	SLU 28	75	-4	1396	3.88	3.51	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
136	SLU 29	86	0	1392	-0.16	3.96	0
136	SLU 30	75	-4	1396	3.88	3.51	0
136	SLU 31	104	-6	1562	6.38	4.78	-0.01
136	SLU 32	122	0	1555	-0.36	5.53	0
136	SLU 33	111	-3	1559	3.68	5.08	0
136	SLU 34	104	-6	1562	6.38	4.78	-0.01
136	SLU 35	122	0	1555	-0.36	5.53	0
136	SLU 36	111	-3	1559	3.68	5.08	0
136	SLU 37	122	0	1555	-0.36	5.53	0
136	SLU 38	111	-3	1559	3.68	5.08	0
136	SLU 39	137	1	1625	-0.45	6.21	0
136	SLU 40	126	-3	1629	3.59	5.76	0
136	SLU 41	137	1	1625	-0.45	6.21	0
136	SLU 42	126	-3	1629	3.59	5.76	0
136	SLU 43	91	0	1682	-0.08	4.2	0
136	SLU 44	73	-6	1689	6.66	3.45	-0.01
136	SLU 45	91	0	1682	-0.08	4.2	0
136	SLU 46	80	-4	1686	3.96	3.75	0
136	SLU 47	73	-6	1689	6.66	3.45	-0.01
136	SLU 48	91	0	1682	-0.08	4.2	0
136	SLU 49	80	-4	1686	3.96	3.75	0
136	SLU 50	91	0	1682	-0.08	4.2	0
136	SLU 51	80	-4	1686	3.96	3.75	0
136	SLU 52	109	-6	1852	6.46	5.02	-0.01
136	SLU 53	126	0	1845	-0.28	5.78	0
136	SLU 54	116	-3	1849	3.76	5.32	0
136	SLU 55	109	-6	1852	6.46	5.02	-0.01
136	SLU 56	126	0	1845	-0.28	5.78	0
136	SLU 57	116	-3	1849	3.76	5.32	0
136	SLU 58	126	0	1845	-0.28	5.78	0
136	SLU 59	116	-3	1849	3.76	5.32	0
136	SLU 60	142	0	1915	-0.37	6.45	0
136	SLU 61	131	-3	1919	3.67	6	0
136	SLU 62	142	0	1915	-0.37	6.45	0
136	SLU 63	131	-3	1919	3.67	6	0
136	SLU 64	103	0	1759	-0.16	4.78	0
136	SLU 65	85	-6	1766	6.58	4.03	-0.01
136	SLU 66	103	0	1759	-0.16	4.78	0
136	SLU 67	93	-4	1764	3.88	4.33	0
136	SLU 68	85	-6	1766	6.58	4.03	-0.01
136	SLU 69	103	0	1759	-0.16	4.78	0
136	SLU 70	93	-4	1764	3.88	4.33	0
136	SLU 71	103	0	1759	-0.16	4.78	0
136	SLU 72	93	-4	1764	3.88	4.33	0
136	SLU 73	121	-6	1930	6.38	5.6	-0.01
136	SLU 74	139	0	1923	-0.36	6.35	0
136	SLU 75	129	-3	1927	3.68	5.9	0
136	SLU 76	121	-6	1930	6.38	5.6	-0.01
136	SLU 77	139	0	1923	-0.36	6.35	0
136	SLU 78	129	-3	1927	3.68	5.9	0
136	SLU 79	139	0	1923	-0.36	6.35	0
136	SLU 80	129	-3	1927	3.68	5.9	0
136	SLU 81	155	1	1993	-0.45	7.02	0
136	SLU 82	144	-3	1997	3.6	6.57	0
136	SLU 83	155	1	1993	-0.45	7.02	0
136	SLU 84	144	-3	1997	3.6	6.57	0
136	SLE RA 1	77	0	1336	-0.11	3.55	0
136	SLE RA 2	65	-4	1341	4.39	3.05	0
136	SLE RA 3	77	0	1336	-0.11	3.55	0
136	SLE RA 4	70	-2	1339	2.59	3.25	0
136	SLE RA 5	65	-4	1341	4.39	3.05	0
136	SLE RA 6	77	0	1336	-0.11	3.55	0
136	SLE RA 7	70	-2	1339	2.59	3.25	0
136	SLE RA 8	77	0	1336	-0.11	3.55	0
136	SLE RA 9	70	-2	1339	2.59	3.25	0
136	SLE RA 10	89	-4	1450	4.25	4.1	0
136	SLE RA 11	101	0	1445	-0.24	4.6	0
136	SLE RA 12	93	-2	1448	2.46	4.3	0
136	SLE RA 13	89	-4	1450	4.25	4.1	0
136	SLE RA 14	101	0	1445	-0.24	4.6	0
136	SLE RA 15	93	-2	1448	2.46	4.3	0
136	SLE RA 16	101	0	1445	-0.24	4.6	0
136	SLE RA 17	93	-2	1448	2.46	4.3	0
136	SLE RA 18	111	0	1492	-0.3	5.05	0
136	SLE RA 19	104	-2	1495	2.4	4.75	0
136	SLE RA 20	111	0	1492	-0.3	5.05	0
136	SLE RA 21	104	-2	1495	2.4	4.75	0
136	SLE FR 1	77	0	1336	-0.11	3.55	0
136	SLE FR 2	74	-1	1337	0.79	3.45	0
136	SLE FR 3	77	0	1336	-0.11	3.55	0
136	SLE FR 4	85	-1	1384	0.74	3.9	0
136	SLE FR 5	87	0	1383	-0.16	4	0
136	SLE FR 6	94	0	1414	-0.2	4.3	0
136	SLE QP 1	77	0	1336	-0.11	3.55	0
136	SLE QP 2	87	0	1383	-0.16	4	0
136	SLD 1	241	31	1399	-29.4	10.54	0.04
136	SLD 2	241	31	1399	-29.4	10.54	0.04
136	SLD 3	216	14	1442	-14.51	9.49	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
136	SLD 4	216	14	1442	-14.51	9.49	0.01
136	SLD 5	171	34	1322	-31.52	7.55	0.06
136	SLD 6	171	34	1322	-31.52	7.55	0.06
136	SLD 7	88	-21	1466	18.12	4.06	-0.05
136	SLD 8	88	-21	1466	18.12	4.06	-0.05
136	SLD 9	86	21	1300	-18.45	3.94	0.05
136	SLD 10	86	21	1300	-18.45	3.94	0.05
136	SLD 11	3	-34	1444	31.2	0.45	-0.06
136	SLD 12	3	-34	1444	31.2	0.45	-0.06
136	SLD 13	-42	-14	1324	14.18	-1.49	-0.01
136	SLD 14	-42	-14	1324	14.18	-1.49	-0.01
136	SLD 15	-67	-30	1367	29.07	-2.54	-0.04
136	SLD 16	-67	-30	1367	29.07	-2.54	-0.04
136	SLV 1	451	77	1422	-73.96	19.43	0.1
136	SLV 2	451	77	1422	-73.96	19.43	0.1
136	SLV 3	392	38	1524	-38.91	16.98	0.02
136	SLV 4	392	38	1524	-38.91	16.98	0.02
136	SLV 5	285	82	1240	-75.46	12.35	0.14
136	SLV 6	285	82	1240	-75.46	12.35	0.14
136	SLV 7	90	-47	1580	41.37	4.18	-0.11
136	SLV 8	90	-47	1580	41.37	4.18	-0.11
136	SLV 9	84	48	1186	-41.7	3.82	0.11
136	SLV 10	84	48	1186	-41.7	3.82	0.11
136	SLV 11	-111	-82	1526	75.13	-4.35	-0.14
136	SLV 12	-111	-82	1526	75.13	-4.35	-0.14
136	SLV 13	-218	-38	1242	38.58	-8.99	-0.02
136	SLV 14	-218	-38	1242	38.58	-8.99	-0.02
136	SLV 15	-277	-77	1344	73.63	-11.44	-0.1
136	SLV 16	-277	-77	1344	73.63	-11.44	-0.1
137	SLU 1	105	0	1277	-0.09	4.61	0
137	SLU 2	85	-5	1284	5.98	3.72	0
137	SLU 3	105	0	1277	-0.09	4.61	0
137	SLU 4	93	-3	1281	3.55	4.07	0
137	SLU 5	85	-5	1284	5.98	3.72	0
137	SLU 6	105	0	1277	-0.09	4.61	0
137	SLU 7	93	-3	1281	3.55	4.07	0
137	SLU 8	105	0	1277	-0.09	4.61	0
137	SLU 9	93	-3	1281	3.55	4.07	0
137	SLU 10	137	-5	1444	5.79	5.97	0
137	SLU 11	158	0	1437	-0.27	6.87	0
137	SLU 12	146	-3	1441	3.37	6.33	0
137	SLU 13	137	-5	1444	5.79	5.97	0
137	SLU 14	158	0	1437	-0.27	6.87	0
137	SLU 15	146	-3	1441	3.37	6.33	0
137	SLU 16	158	0	1437	-0.27	6.87	0
137	SLU 17	146	-3	1441	3.37	6.33	0
137	SLU 18	181	0	1506	-0.35	7.83	0
137	SLU 19	168	-3	1510	3.29	7.29	0
137	SLU 20	181	0	1506	-0.35	7.83	0
137	SLU 21	168	-3	1510	3.29	7.29	0
137	SLU 22	126	0	1352	-0.16	5.52	0
137	SLU 23	106	-5	1359	5.9	4.63	0
137	SLU 24	126	0	1352	-0.16	5.52	0
137	SLU 25	114	-3	1356	3.48	4.98	0
137	SLU 26	106	-5	1359	5.9	4.63	0
137	SLU 27	126	0	1352	-0.16	5.52	0
137	SLU 28	114	-3	1356	3.48	4.98	0
137	SLU 29	126	0	1352	-0.16	5.52	0
137	SLU 30	114	-3	1356	3.48	4.98	0
137	SLU 31	158	-5	1518	5.72	6.88	0
137	SLU 32	179	0	1512	-0.34	7.78	0
137	SLU 33	167	-3	1516	3.29	7.24	0
137	SLU 34	158	-5	1518	5.72	6.88	0
137	SLU 35	179	0	1512	-0.34	7.78	0
137	SLU 36	167	-3	1516	3.29	7.24	0
137	SLU 37	179	0	1512	-0.34	7.78	0
137	SLU 38	167	-3	1516	3.29	7.24	0
137	SLU 39	202	0	1580	-0.42	8.74	0
137	SLU 40	189	-3	1584	3.22	8.2	0
137	SLU 41	202	0	1580	-0.42	8.74	0
137	SLU 42	189	-3	1584	3.22	8.2	0
137	SLU 43	130	0	1635	-0.09	5.68	0
137	SLU 44	109	-5	1642	5.97	4.79	0
137	SLU 45	130	0	1635	-0.09	5.68	0
137	SLU 46	117	-3	1639	3.55	5.15	0
137	SLU 47	109	-5	1642	5.97	4.79	0
137	SLU 48	130	0	1635	-0.09	5.68	0
137	SLU 49	117	-3	1639	3.55	5.15	0
137	SLU 50	130	0	1635	-0.09	5.68	0
137	SLU 51	117	-3	1639	3.55	5.15	0
137	SLU 52	162	-5	1802	5.79	7.04	0
137	SLU 53	182	0	1795	-0.27	7.94	0
137	SLU 54	170	-3	1799	3.37	7.4	0
137	SLU 55	162	-5	1802	5.79	7.04	0
137	SLU 56	182	0	1795	-0.27	7.94	0
137	SLU 57	170	-3	1799	3.37	7.4	0
137	SLU 58	182	0	1795	-0.27	7.94	0
137	SLU 59	170	-3	1799	3.37	7.4	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
137	SLU 60	205	0	1864	-0.35	8.9	0
137	SLU 61	193	-3	1868	3.29	8.37	0
137	SLU 62	205	0	1864	-0.35	8.9	0
137	SLU 63	193	-3	1868	3.29	8.37	0
137	SLU 64	151	0	1710	-0.16	6.59	0
137	SLU 65	130	-5	1716	5.9	5.7	0
137	SLU 66	151	0	1710	-0.16	6.59	0
137	SLU 67	138	-3	1714	3.48	6.06	0
137	SLU 68	130	-5	1716	5.9	5.7	0
137	SLU 69	151	0	1710	-0.16	6.59	0
137	SLU 70	138	-3	1714	3.48	6.06	0
137	SLU 71	151	0	1710	-0.16	6.59	0
137	SLU 72	138	-3	1714	3.48	6.06	0
137	SLU 73	183	-5	1876	5.72	7.95	0
137	SLU 74	203	0	1869	-0.34	8.85	0
137	SLU 75	191	-3	1873	3.29	8.31	0
137	SLU 76	183	-5	1876	5.72	7.95	0
137	SLU 77	203	0	1869	-0.34	8.85	0
137	SLU 78	191	-3	1873	3.29	8.31	0
137	SLU 79	203	0	1869	-0.34	8.85	0
137	SLU 80	191	-3	1873	3.29	8.31	0
137	SLU 81	226	0	1938	-0.42	9.81	0
137	SLU 82	214	-3	1942	3.21	9.28	0
137	SLU 83	226	0	1938	-0.42	9.81	0
137	SLU 84	214	-3	1942	3.21	9.28	0
137	SLE RA 1	111	0	1299	-0.11	4.87	0
137	SLE RA 2	98	-3	1303	3.93	4.27	0
137	SLE RA 3	111	0	1299	-0.11	4.87	0
137	SLE RA 4	103	-2	1301	2.32	4.51	0
137	SLE RA 5	98	-3	1303	3.93	4.27	0
137	SLE RA 6	111	0	1299	-0.11	4.87	0
137	SLE RA 7	103	-2	1301	2.32	4.51	0
137	SLE RA 8	111	0	1299	-0.11	4.87	0
137	SLE RA 9	103	-2	1301	2.32	4.51	0
137	SLE RA 10	133	-3	1410	3.81	5.78	0
137	SLE RA 11	146	0	1405	-0.23	6.38	0
137	SLE RA 12	138	-2	1408	2.2	6.02	0
137	SLE RA 13	133	-3	1410	3.81	5.78	0
137	SLE RA 14	146	0	1405	-0.23	6.38	0
137	SLE RA 15	138	-2	1408	2.2	6.02	0
137	SLE RA 16	146	0	1405	-0.23	6.38	0
137	SLE RA 17	138	-2	1408	2.2	6.02	0
137	SLE RA 18	162	0	1451	-0.28	7.02	0
137	SLE RA 19	153	-2	1454	2.14	6.66	0
137	SLE RA 20	162	0	1451	-0.28	7.02	0
137	SLE RA 21	153	-2	1454	2.14	6.66	0
137	SLE FR 1	111	0	1299	-0.11	4.87	0
137	SLE FR 2	109	-1	1300	0.7	4.75	0
137	SLE FR 3	111	0	1299	-0.11	4.87	0
137	SLE FR 4	124	0	1345	0.65	5.4	0
137	SLE FR 5	126	0	1344	-0.16	5.52	0
137	SLE FR 6	136	0	1375	-0.19	5.95	0
137	SLE QP 1	111	0	1299	-0.11	4.87	0
137	SLE QP 2	126	0	1344	-0.16	5.52	0
137	SLD 1	288	28	1377	-28.31	12.41	0.03
137	SLD 2	288	28	1377	-28.31	12.41	0.03
137	SLD 3	261	10	1410	-12.6	11.27	0.01
137	SLD 4	261	10	1410	-12.6	11.27	0.01
137	SLD 5	216	35	1303	-32.43	9.32	0.04
137	SLD 6	216	35	1303	-32.43	9.32	0.04
137	SLD 7	126	-23	1415	19.94	5.51	-0.02
137	SLD 8	126	-23	1415	19.94	5.51	-0.02
137	SLD 9	127	24	1274	-20.25	5.52	0.02
137	SLD 10	127	24	1274	-20.25	5.52	0.02
137	SLD 11	37	-35	1385	32.11	1.72	-0.04
137	SLD 12	37	-35	1385	32.11	1.72	-0.04
137	SLD 13	-8	-10	1278	12.28	-0.24	-0.01
137	SLD 14	-8	-10	1278	12.28	-0.24	-0.01
137	SLD 15	-35	-28	1312	27.99	-1.38	-0.03
137	SLD 16	-35	-28	1312	27.99	-1.38	-0.03
137	SLV 1	508	70	1422	-70.83	21.79	0.08
137	SLV 2	508	70	1422	-70.83	21.79	0.08
137	SLV 3	445	28	1502	-33.86	19.12	0.03
137	SLV 4	445	28	1502	-33.86	19.12	0.03
137	SLV 5	336	84	1247	-77.44	14.45	0.09
137	SLV 6	336	84	1247	-77.44	14.45	0.09
137	SLV 7	127	-54	1512	45.81	5.55	-0.06
137	SLV 8	127	-54	1512	45.81	5.55	-0.06
137	SLV 9	126	55	1177	-46.13	5.49	0.06
137	SLV 10	126	55	1177	-46.13	5.49	0.06
137	SLV 11	-83	-83	1442	77.12	-3.42	-0.09
137	SLV 12	-83	-83	1442	77.12	-3.42	-0.09
137	SLV 13	-192	-28	1187	33.54	-8.08	-0.03
137	SLV 14	-192	-28	1187	33.54	-8.08	-0.03
137	SLV 15	-255	-69	1266	70.51	-10.76	-0.08
137	SLV 16	-255	-69	1266	70.51	-10.76	-0.08
138	SLU 1	134	0	1284	-0.06	5.59	0
138	SLU 2	113	-3	1289	4.99	4.71	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
138	SLU 3	134	0	1284	-0.06	5.59	0
138	SLU 4	121	-2	1287	2.97	5.06	0
138	SLU 5	113	-3	1289	4.99	4.71	0
138	SLU 6	134	0	1284	-0.06	5.59	0
138	SLU 7	121	-2	1287	2.97	5.06	0
138	SLU 8	134	0	1284	-0.06	5.59	0
138	SLU 9	121	-2	1287	2.97	5.06	0
138	SLU 10	178	-3	1463	4.85	7.37	0
138	SLU 11	199	0	1458	-0.2	8.25	0
138	SLU 12	187	-2	1461	2.83	7.72	0
138	SLU 13	178	-3	1463	4.85	7.37	0
138	SLU 14	199	0	1458	-0.2	8.25	0
138	SLU 15	187	-2	1461	2.83	7.72	0
138	SLU 16	199	0	1458	-0.2	8.25	0
138	SLU 17	187	-2	1461	2.83	7.72	0
138	SLU 18	227	0	1532	-0.26	9.39	0
138	SLU 19	215	-2	1535	2.77	8.86	0
138	SLU 20	227	0	1532	-0.26	9.39	0
138	SLU 21	215	-2	1535	2.77	8.86	0
138	SLU 22	162	0	1364	-0.11	6.72	0
138	SLU 23	141	-3	1368	4.93	5.83	0
138	SLU 24	162	0	1364	-0.11	6.72	0
138	SLU 25	149	-2	1367	2.92	6.19	0
138	SLU 26	141	-3	1368	4.93	5.83	0
138	SLU 27	162	0	1364	-0.11	6.72	0
138	SLU 28	149	-2	1367	2.92	6.19	0
138	SLU 29	162	0	1364	-0.11	6.72	0
138	SLU 30	149	-2	1367	2.92	6.19	0
138	SLU 31	206	-3	1542	4.79	8.49	0
138	SLU 32	227	0	1537	-0.25	9.37	0
138	SLU 33	214	-2	1540	2.77	8.85	0
138	SLU 34	206	-3	1542	4.79	8.49	0
138	SLU 35	227	0	1537	-0.25	9.37	0
138	SLU 36	214	-2	1540	2.77	8.85	0
138	SLU 37	227	0	1537	-0.25	9.37	0
138	SLU 38	214	-2	1540	2.77	8.85	0
138	SLU 39	255	0	1612	-0.31	10.51	0
138	SLU 40	242	-2	1615	2.71	9.98	0
138	SLU 41	255	0	1612	-0.31	10.51	0
138	SLU 42	242	-2	1615	2.71	9.98	0
138	SLU 43	165	0	1642	-0.06	6.88	0
138	SLU 44	144	-3	1647	4.99	6	0
138	SLU 45	165	0	1642	-0.06	6.88	0
138	SLU 46	152	-2	1645	2.97	6.35	0
138	SLU 47	144	-3	1647	4.99	6	0
138	SLU 48	165	0	1642	-0.06	6.88	0
138	SLU 49	152	-2	1645	2.97	6.35	0
138	SLU 50	165	0	1642	-0.06	6.88	0
138	SLU 51	152	-2	1645	2.97	6.35	0
138	SLU 52	209	-3	1821	4.85	8.66	0
138	SLU 53	230	0	1816	-0.2	9.54	0
138	SLU 54	217	-2	1819	2.83	9.01	0
138	SLU 55	209	-3	1821	4.85	8.66	0
138	SLU 56	230	0	1816	-0.2	9.54	0
138	SLU 57	217	-2	1819	2.83	9.01	0
138	SLU 58	230	0	1816	-0.2	9.54	0
138	SLU 59	217	-2	1819	2.83	9.01	0
138	SLU 60	258	0	1890	-0.26	10.68	0
138	SLU 61	245	-2	1893	2.77	10.15	0
138	SLU 62	258	0	1890	-0.26	10.68	0
138	SLU 63	245	-2	1893	2.77	10.15	0
138	SLU 64	193	0	1722	-0.11	8.01	0
138	SLU 65	171	-3	1726	4.93	7.13	0
138	SLU 66	193	0	1722	-0.11	8.01	0
138	SLU 67	180	-2	1725	2.92	7.48	0
138	SLU 68	171	-3	1726	4.93	7.13	0
138	SLU 69	193	0	1722	-0.11	8.01	0
138	SLU 70	180	-2	1725	2.92	7.48	0
138	SLU 71	193	0	1722	-0.11	8.01	0
138	SLU 72	180	-2	1725	2.92	7.48	0
138	SLU 73	237	-3	1900	4.79	9.78	0
138	SLU 74	258	0	1895	-0.25	10.67	0
138	SLU 75	245	-2	1898	2.78	10.14	0
138	SLU 76	237	-3	1900	4.79	9.78	0
138	SLU 77	258	0	1895	-0.25	10.67	0
138	SLU 78	245	-2	1898	2.78	10.14	0
138	SLU 79	258	0	1895	-0.25	10.67	0
138	SLU 80	245	-2	1898	2.78	10.14	0
138	SLU 81	286	0	1970	-0.31	11.8	0
138	SLU 82	273	-2	1973	2.71	11.28	0
138	SLU 83	286	0	1970	-0.31	11.8	0
138	SLU 84	273	-2	1973	2.71	11.28	0
138	SLE RA 1	142	0	1307	-0.07	5.91	0
138	SLE RA 2	128	-2	1310	3.29	5.32	0
138	SLE RA 3	142	0	1307	-0.07	5.91	0
138	SLE RA 4	134	-1	1309	1.94	5.56	0
138	SLE RA 5	128	-2	1310	3.29	5.32	0
138	SLE RA 6	142	0	1307	-0.07	5.91	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
138	SLE RA 7	134	-1	1309	1.94	5.56	0
138	SLE RA 8	142	0	1307	-0.07	5.91	0
138	SLE RA 9	134	-1	1309	1.94	5.56	0
138	SLE RA 10	171	-2	1426	3.2	7.1	0
138	SLE RA 11	186	0	1423	-0.17	7.68	0
138	SLE RA 12	177	-1	1425	1.85	7.33	0
138	SLE RA 13	171	-2	1426	3.2	7.1	0
138	SLE RA 14	186	0	1423	-0.17	7.68	0
138	SLE RA 15	177	-1	1425	1.85	7.33	0
138	SLE RA 16	186	0	1423	-0.17	7.68	0
138	SLE RA 17	177	-1	1425	1.85	7.33	0
138	SLE RA 18	204	0	1472	-0.21	8.44	0
138	SLE RA 19	196	-1	1474	1.81	8.09	0
138	SLE RA 20	204	0	1472	-0.21	8.44	0
138	SLE RA 21	196	-1	1474	1.81	8.09	0
138	SLE FR 1	142	0	1307	-0.07	5.91	0
138	SLE FR 2	139	0	1308	0.6	5.79	0
138	SLE FR 3	142	0	1307	-0.07	5.91	0
138	SLE FR 4	158	0	1357	0.56	6.55	0
138	SLE FR 5	161	0	1357	-0.11	6.67	0
138	SLE FR 6	173	0	1390	-0.14	7.18	0
138	SLE QP 1	142	0	1307	-0.07	5.91	0
138	SLE QP 2	161	0	1357	-0.11	6.67	0
138	SLD 1	322	24	1409	-25.53	12.35	0.01
138	SLD 2	322	24	1409	-25.53	12.35	0.01
138	SLD 3	295	7	1440	-10.41	13.49	0.03
138	SLD 4	295	7	1440	-10.41	13.49	0.03
138	SLD 5	251	33	1326	-30.66	6.65	-0.04
138	SLD 6	251	33	1326	-30.66	6.65	-0.04
138	SLD 7	160	-23	1428	19.72	10.44	0.05
138	SLD 8	160	-23	1428	19.72	10.44	0.05
138	SLD 9	162	23	1285	-19.95	2.9	-0.05
138	SLD 10	162	23	1285	-19.95	2.9	-0.05
138	SLD 11	71	-32	1387	30.44	6.69	0.04
138	SLD 12	71	-32	1387	30.44	6.69	0.04
138	SLD 13	26	-7	1273	10.19	-0.14	-0.03
138	SLD 14	26	-7	1273	10.19	-0.14	-0.03
138	SLD 15	-1	-24	1304	25.3	0.99	-0.01
138	SLD 16	-1	-24	1304	25.3	0.99	-0.01
138	SLV 1	543	59	1481	-63.52	20.13	0.02
138	SLV 2	543	59	1481	-63.52	20.13	0.02
138	SLV 3	479	20	1554	-27.94	22.79	0.08
138	SLV 4	479	20	1554	-27.94	22.79	0.08
138	SLV 5	372	77	1283	-73.1	6.68	-0.09
138	SLV 6	372	77	1283	-73.1	6.68	-0.09
138	SLV 7	160	-53	1526	45.5	15.54	0.12
138	SLV 8	160	-53	1526	45.5	15.54	0.12
138	SLV 9	162	54	1187	-45.73	-2.19	-0.12
138	SLV 10	162	54	1187	-45.73	-2.19	-0.12
138	SLV 11	-51	-77	1430	72.87	6.66	0.09
138	SLV 12	-51	-77	1430	72.87	6.66	0.09
138	SLV 13	-158	-20	1159	27.71	-9.45	-0.08
138	SLV 14	-158	-20	1159	27.71	-9.45	-0.08
138	SLV 15	-221	-59	1232	63.29	-6.79	-0.02
138	SLV 16	-221	-59	1232	63.29	-6.79	-0.02
139	SLU 1	152	0	1326	0	6.22	0
139	SLU 2	132	-2	1328	3.84	5.35	0
139	SLU 3	152	0	1326	0	6.22	0
139	SLU 4	140	-1	1327	2.3	5.7	0
139	SLU 5	132	-2	1328	3.84	5.35	0
139	SLU 6	152	0	1326	0	6.22	0
139	SLU 7	140	-1	1327	2.3	5.7	0
139	SLU 8	152	0	1326	0	6.22	0
139	SLU 9	140	-1	1327	2.3	5.7	0
139	SLU 10	204	-2	1528	3.76	8.29	0
139	SLU 11	225	0	1526	-0.08	9.16	0
139	SLU 12	212	-1	1528	2.23	8.64	0
139	SLU 13	204	-2	1528	3.76	8.29	0
139	SLU 14	225	0	1526	-0.08	9.16	0
139	SLU 15	212	-1	1528	2.23	8.64	0
139	SLU 16	225	0	1526	-0.08	9.16	0
139	SLU 17	212	-1	1528	2.23	8.64	0
139	SLU 18	256	0	1612	-0.11	10.42	0
139	SLU 19	243	-1	1613	2.2	9.9	0
139	SLU 20	256	0	1612	-0.11	10.42	0
139	SLU 21	243	-1	1613	2.2	9.9	0
139	SLU 22	184	0	1417	-0.02	7.52	0
139	SLU 23	164	-2	1419	3.82	6.65	0
139	SLU 24	184	0	1417	-0.02	7.52	0
139	SLU 25	172	-1	1418	2.28	7	0
139	SLU 26	164	-2	1419	3.82	6.65	0
139	SLU 27	184	0	1417	-0.02	7.52	0
139	SLU 28	172	-1	1418	2.28	7	0
139	SLU 29	184	0	1417	-0.02	7.52	0
139	SLU 30	172	-1	1418	2.28	7	0
139	SLU 31	236	-2	1620	3.74	9.6	0
139	SLU 32	257	0	1617	-0.1	10.47	0
139	SLU 33	245	-1	1619	2.2	9.94	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
139	SLU 34	236	-2	1620	3.74	9.6	0
139	SLU 35	257	0	1617	-0.1	10.47	0
139	SLU 36	245	-1	1619	2.2	9.94	0
139	SLU 37	257	0	1617	-0.1	10.47	0
139	SLU 38	245	-1	1619	2.2	9.94	0
139	SLU 39	288	0	1703	-0.13	11.73	0
139	SLU 40	276	-1	1705	2.17	11.21	0
139	SLU 41	288	0	1703	-0.13	11.73	0
139	SLU 42	276	-1	1705	2.17	11.21	0
139	SLU 43	187	0	1692	0.01	7.63	0
139	SLU 44	166	-2	1695	3.85	6.77	0
139	SLU 45	187	0	1692	0.01	7.63	0
139	SLU 46	175	-1	1694	2.31	7.11	0
139	SLU 47	166	-2	1695	3.85	6.77	0
139	SLU 48	187	0	1692	0.01	7.63	0
139	SLU 49	175	-1	1694	2.31	7.11	0
139	SLU 50	187	0	1692	0.01	7.63	0
139	SLU 51	175	-1	1694	2.31	7.11	0
139	SLU 52	239	-2	1895	3.77	9.71	0
139	SLU 53	259	0	1893	-0.07	10.58	0
139	SLU 54	247	-1	1894	2.24	10.06	0
139	SLU 55	239	-2	1895	3.77	9.71	0
139	SLU 56	259	0	1893	-0.07	10.58	0
139	SLU 57	247	-1	1894	2.24	10.06	0
139	SLU 58	259	0	1893	-0.07	10.58	0
139	SLU 59	247	-1	1894	2.24	10.06	0
139	SLU 60	290	0	1979	-0.1	11.84	0
139	SLU 61	278	-1	1980	2.2	11.32	0
139	SLU 62	290	0	1979	-0.1	11.84	0
139	SLU 63	278	-1	1980	2.2	11.32	0
139	SLU 64	219	0	1784	-0.02	8.94	0
139	SLU 65	199	-2	1786	3.82	8.07	0
139	SLU 66	219	0	1784	-0.02	8.94	0
139	SLU 67	207	-1	1785	2.29	8.42	0
139	SLU 68	199	-2	1786	3.82	8.07	0
139	SLU 69	219	0	1784	-0.02	8.94	0
139	SLU 70	207	-1	1785	2.29	8.42	0
139	SLU 71	219	0	1784	-0.02	8.94	0
139	SLU 72	207	-1	1785	2.29	8.42	0
139	SLU 73	271	-2	1986	3.75	11.01	0
139	SLU 74	292	0	1984	-0.09	11.88	0
139	SLU 75	279	-1	1985	2.21	11.36	0
139	SLU 76	271	-2	1986	3.75	11.01	0
139	SLU 77	292	0	1984	-0.09	11.88	0
139	SLU 78	279	-1	1985	2.21	11.36	0
139	SLU 79	292	0	1984	-0.09	11.88	0
139	SLU 80	279	-1	1985	2.21	11.36	0
139	SLU 81	323	0	2070	-0.12	13.14	0
139	SLU 82	310	-1	2071	2.18	12.62	0
139	SLU 83	323	0	2070	-0.12	13.14	0
139	SLU 84	310	-1	2071	2.18	12.62	0
139	SLE RA 1	161	0	1352	-0.01	6.59	0
139	SLE RA 2	148	-1	1353	2.55	6.01	0
139	SLE RA 3	161	0	1352	-0.01	6.59	0
139	SLE RA 4	153	-1	1353	1.53	6.24	0
139	SLE RA 5	148	-1	1353	2.55	6.01	0
139	SLE RA 6	161	0	1352	-0.01	6.59	0
139	SLE RA 7	153	-1	1353	1.53	6.24	0
139	SLE RA 8	161	0	1352	-0.01	6.59	0
139	SLE RA 9	153	-1	1353	1.53	6.24	0
139	SLE RA 10	196	-1	1487	2.5	7.97	0
139	SLE RA 11	210	0	1486	-0.06	8.55	0
139	SLE RA 12	202	-1	1486	1.48	8.2	0
139	SLE RA 13	196	-1	1487	2.5	7.97	0
139	SLE RA 14	210	0	1486	-0.06	8.55	0
139	SLE RA 15	202	-1	1486	1.48	8.2	0
139	SLE RA 16	210	0	1486	-0.06	8.55	0
139	SLE RA 17	202	-1	1486	1.48	8.2	0
139	SLE RA 18	230	0	1543	-0.08	9.39	0
139	SLE RA 19	222	-1	1544	1.46	9.05	0
139	SLE RA 20	230	0	1543	-0.08	9.39	0
139	SLE RA 21	222	-1	1544	1.46	9.05	0
139	SLE FR 1	161	0	1352	-0.01	6.59	0
139	SLE FR 2	159	0	1352	0.5	6.47	0
139	SLE FR 3	161	0	1352	-0.01	6.59	0
139	SLE FR 4	179	0	1409	0.48	7.31	0
139	SLE FR 5	182	0	1409	-0.03	7.43	0
139	SLE FR 6	196	0	1447	-0.04	7.99	0
139	SLE QP 1	161	0	1352	-0.01	6.59	0
139	SLE QP 2	182	0	1409	-0.03	7.43	0
139	SLD 1	313	-19	1476	-21.45	13.02	-0.02
139	SLD 2	313	-19	1476	-21.45	13.02	-0.02
139	SLD 3	341	-5	1509	-8.25	14.19	-0.01
139	SLD 4	341	-5	1509	-8.25	14.19	-0.01
139	SLD 5	180	-27	1380	-26.48	7.33	-0.02
139	SLD 6	180	-27	1380	-26.48	7.33	-0.02
139	SLD 7	271	19	1489	17.52	11.23	0.02
139	SLD 8	271	19	1489	17.52	11.23	0.02





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
139	SLD 9	93	-19	1330	-17.58	3.63	-0.02
139	SLD 10	93	-19	1330	-17.58	3.63	-0.02
139	SLD 11	185	27	1439	26.42	7.53	0.02
139	SLD 12	185	27	1439	26.42	7.53	0.02
139	SLD 13	24	5	1309	8.2	0.67	0.01
139	SLD 14	24	5	1309	8.2	0.67	0.01
139	SLD 15	51	19	1342	21.4	1.84	0.02
139	SLD 16	51	19	1342	21.4	1.84	0.02
139	SLV 1	492	-47	1567	-53.1	20.63	-0.05
139	SLV 2	492	-47	1567	-53.1	20.63	-0.05
139	SLV 3	556	-14	1645	-22.02	23.37	-0.02
139	SLV 4	556	-14	1645	-22.02	23.37	-0.02
139	SLV 5	177	-63	1339	-63.1	7.24	-0.06
139	SLV 6	177	-63	1339	-63.1	7.24	-0.06
139	SLV 7	392	45	1598	40.52	16.37	0.04
139	SLV 8	392	45	1598	40.52	16.37	0.04
139	SLV 9	-28	-45	1221	-40.58	-1.51	-0.04
139	SLV 10	-28	-45	1221	-40.58	-1.51	-0.04
139	SLV 11	187	64	1479	63.04	7.63	0.06
139	SLV 12	187	64	1479	63.04	7.63	0.06
139	SLV 13	-192	14	1173	21.96	-8.51	0.02
139	SLV 14	-192	14	1173	21.96	-8.51	0.02
139	SLV 15	-128	47	1251	53.05	-5.77	0.05
139	SLV 16	-128	47	1251	53.05	-5.77	0.05
140	SLU 1	154	0	1391	0.09	6.23	0
140	SLU 2	136	0	1391	2.68	5.44	0
140	SLU 3	154	0	1391	0.09	6.23	0
140	SLU 4	143	0	1391	1.65	5.75	0
140	SLU 5	136	0	1391	2.68	5.44	0
140	SLU 6	154	0	1391	0.09	6.23	0
140	SLU 7	143	0	1391	1.65	5.75	0
140	SLU 8	154	0	1391	0.09	6.23	0
140	SLU 9	143	0	1391	1.65	5.75	0
140	SLU 10	207	-1	1626	2.7	8.3	0
140	SLU 11	226	0	1626	0.11	9.09	0
140	SLU 12	215	0	1626	1.66	8.62	0
140	SLU 13	207	-1	1626	2.7	8.3	0
140	SLU 14	226	0	1626	0.11	9.09	0
140	SLU 15	215	0	1626	1.66	8.62	0
140	SLU 16	226	0	1626	0.11	9.09	0
140	SLU 17	215	0	1626	1.66	8.62	0
140	SLU 18	256	0	1727	0.11	10.32	0
140	SLU 19	245	0	1727	1.67	9.84	0
140	SLU 20	256	0	1727	0.11	10.32	0
140	SLU 21	245	0	1727	1.67	9.84	0
140	SLU 22	187	0	1498	0.11	7.54	0
140	SLU 23	169	-1	1499	2.7	6.75	0
140	SLU 24	187	0	1498	0.11	7.54	0
140	SLU 25	176	0	1499	1.67	7.07	0
140	SLU 26	169	-1	1499	2.7	6.75	0
140	SLU 27	187	0	1498	0.11	7.54	0
140	SLU 28	176	0	1499	1.67	7.07	0
140	SLU 29	187	0	1498	0.11	7.54	0
140	SLU 30	176	0	1499	1.67	7.07	0
140	SLU 31	240	-1	1734	2.71	9.62	0
140	SLU 32	259	0	1734	0.12	10.41	0
140	SLU 33	248	0	1734	1.68	9.93	0
140	SLU 34	240	-1	1734	2.71	9.62	0
140	SLU 35	259	0	1734	0.12	10.41	0
140	SLU 36	248	0	1734	1.68	9.93	0
140	SLU 37	259	0	1734	0.12	10.41	0
140	SLU 38	248	0	1734	1.68	9.93	0
140	SLU 39	290	0	1834	0.13	11.63	0
140	SLU 40	279	0	1835	1.68	11.16	0
140	SLU 41	290	0	1834	0.13	11.63	0
140	SLU 42	279	0	1835	1.68	11.16	0
140	SLU 43	189	0	1771	0.11	7.64	0
140	SLU 44	170	0	1772	2.7	6.85	0
140	SLU 45	189	0	1771	0.11	7.64	0
140	SLU 46	178	0	1772	1.67	7.17	0
140	SLU 47	170	0	1772	2.7	6.85	0
140	SLU 48	189	0	1771	0.11	7.64	0
140	SLU 49	178	0	1772	1.67	7.17	0
140	SLU 50	189	0	1771	0.11	7.64	0
140	SLU 51	178	0	1772	1.67	7.17	0
140	SLU 52	242	-1	2007	2.72	9.72	0
140	SLU 53	261	0	2006	0.13	10.51	0
140	SLU 54	249	0	2007	1.68	10.03	0
140	SLU 55	242	-1	2007	2.72	9.72	0
140	SLU 56	261	0	2006	0.13	10.51	0
140	SLU 57	249	0	2007	1.68	10.03	0
140	SLU 58	261	0	2006	0.13	10.51	0
140	SLU 59	249	0	2007	1.68	10.03	0
140	SLU 60	291	0	2107	0.13	11.73	0
140	SLU 61	280	0	2107	1.69	11.26	0
140	SLU 62	291	0	2107	0.13	11.73	0
140	SLU 63	280	0	2107	1.69	11.26	0
140	SLU 64	222	0	1879	0.13	8.96	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
140	SLU 65	204	-1	1879	2.72	8.17	0
140	SLU 66	222	0	1879	0.13	8.96	0
140	SLU 67	211	0	1879	1.69	8.49	0
140	SLU 68	204	-1	1879	2.72	8.17	0
140	SLU 69	222	0	1879	0.13	8.96	0
140	SLU 70	211	0	1879	1.69	8.49	0
140	SLU 71	222	0	1879	0.13	8.96	0
140	SLU 72	211	0	1879	1.69	8.49	0
140	SLU 73	275	-1	2114	2.74	11.03	0
140	SLU 74	294	0	2114	0.15	11.82	0
140	SLU 75	283	0	2114	1.7	11.35	0
140	SLU 76	275	-1	2114	2.74	11.03	0
140	SLU 77	294	0	2114	0.15	11.82	0
140	SLU 78	283	0	2114	1.7	11.35	0
140	SLU 79	294	0	2114	0.15	11.82	0
140	SLU 80	283	0	2114	1.7	11.35	0
140	SLU 81	324	0	2215	0.15	13.05	0
140	SLU 82	313	0	2215	1.71	12.58	0
140	SLU 83	324	0	2215	0.15	13.05	0
140	SLU 84	313	0	2215	1.71	12.58	0
140	SLE RA 1	164	0	1422	0.1	6.6	0
140	SLE RA 2	151	0	1422	1.82	6.08	0
140	SLE RA 3	164	0	1422	0.1	6.6	0
140	SLE RA 4	156	0	1422	1.13	6.29	0
140	SLE RA 5	151	0	1422	1.82	6.08	0
140	SLE RA 6	164	0	1422	0.1	6.6	0
140	SLE RA 7	156	0	1422	1.13	6.29	0
140	SLE RA 8	164	0	1422	0.1	6.6	0
140	SLE RA 9	156	0	1422	1.13	6.29	0
140	SLE RA 10	199	0	1579	1.83	7.98	0
140	SLE RA 11	211	0	1578	0.11	8.51	0
140	SLE RA 12	204	0	1579	1.14	8.2	0
140	SLE RA 13	199	0	1579	1.83	7.98	0
140	SLE RA 14	211	0	1578	0.11	8.51	0
140	SLE RA 15	204	0	1579	1.14	8.2	0
140	SLE RA 16	211	0	1578	0.11	8.51	0
140	SLE RA 17	204	0	1579	1.14	8.2	0
140	SLE RA 18	232	0	1646	0.11	9.33	0
140	SLE RA 19	224	0	1646	1.15	9.01	0
140	SLE RA 20	232	0	1646	0.11	9.33	0
140	SLE RA 21	224	0	1646	1.15	9.01	0
140	SLE FR 1	164	0	1422	0.1	6.6	0
140	SLE FR 2	161	0	1422	0.44	6.5	0
140	SLE FR 3	164	0	1422	0.1	6.6	0
140	SLE FR 4	182	0	1489	0.45	7.32	0
140	SLE FR 5	184	0	1489	0.1	7.42	0
140	SLE FR 6	198	0	1534	0.1	7.97	0
140	SLE QP 1	164	0	1422	0.1	6.6	0
140	SLE QP 2	184	0	1489	0.1	7.42	0
140	SLD 1	309	-14	1559	-16.57	12.79	-0.02
140	SLD 2	309	-14	1559	-16.57	12.79	-0.02
140	SLD 3	337	-5	1597	-6.31	13.93	0
140	SLD 4	337	-5	1597	-6.31	13.93	0
140	SLD 5	180	-19	1454	-20.47	7.31	-0.03
140	SLD 6	180	-19	1454	-20.47	7.31	-0.03
140	SLD 7	271	13	1577	13.74	11.09	0.02
140	SLD 8	271	13	1577	13.74	11.09	0.02
140	SLD 9	97	-13	1400	-13.54	3.75	-0.02
140	SLD 10	97	-13	1400	-13.54	3.75	-0.02
140	SLD 11	188	19	1524	20.67	7.53	0.03
140	SLD 12	188	19	1524	20.67	7.53	0.03
140	SLD 13	32	5	1381	6.51	0.91	0
140	SLD 14	32	5	1381	6.51	0.91	0
140	SLD 15	59	14	1418	16.77	2.05	0.02
140	SLD 16	59	14	1418	16.77	2.05	0.02
140	SLV 1	481	-35	1655	-40.96	20.16	-0.04
140	SLV 2	481	-35	1655	-40.96	20.16	-0.04
140	SLV 3	544	-13	1743	-16.76	22.82	-0.01
140	SLV 4	544	-13	1743	-16.76	22.82	-0.01
140	SLV 5	176	-45	1405	-48.91	7.21	-0.06
140	SLV 6	176	-45	1405	-48.91	7.21	-0.06
140	SLV 7	389	30	1699	31.74	16.08	0.05
140	SLV 8	389	30	1699	31.74	16.08	0.05
140	SLV 9	-21	-30	1279	-31.53	-1.23	-0.05
140	SLV 10	-21	-30	1279	-31.53	-1.23	-0.05
140	SLV 11	192	45	1573	49.11	7.64	0.06
140	SLV 12	192	45	1573	49.11	7.64	0.06
140	SLV 13	-176	13	1235	16.97	-7.98	0.01
140	SLV 14	-176	13	1235	16.97	-7.98	0.01
140	SLV 15	-113	35	1323	41.16	-5.32	0.04
140	SLV 16	-113	35	1323	41.16	-5.32	0.04
141	SLU 1	137	0	1465	0.25	5.45	0
141	SLU 2	121	1	1465	1.7	4.78	0
141	SLU 3	137	0	1465	0.25	5.45	0
141	SLU 4	127	0	1465	1.12	5.05	0
141	SLU 5	121	1	1465	1.7	4.78	0
141	SLU 6	137	0	1465	0.25	5.45	0
141	SLU 7	127	0	1465	1.12	5.05	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
141	SLU 8	137	0	1465	0.25	5.45	0
141	SLU 9	127	0	1465	1.12	5.05	0
141	SLU 10	185	1	1738	1.83	7.32	0
141	SLU 11	201	0	1738	0.38	7.99	0
141	SLU 12	191	0	1738	1.25	7.59	0
141	SLU 13	185	1	1738	1.83	7.32	0
141	SLU 14	201	0	1738	0.38	7.99	0
141	SLU 15	191	0	1738	1.25	7.59	0
141	SLU 16	201	0	1738	0.38	7.99	0
141	SLU 17	191	0	1738	1.25	7.59	0
141	SLU 18	228	0	1855	0.44	9.08	0
141	SLU 19	219	0	1855	1.31	8.68	0
141	SLU 20	228	0	1855	0.44	9.08	0
141	SLU 21	219	0	1855	1.31	8.68	0
141	SLU 22	168	0	1592	0.33	6.68	0
141	SLU 23	152	1	1592	1.78	6.02	0
141	SLU 24	168	0	1592	0.33	6.68	0
141	SLU 25	159	0	1592	1.2	6.29	0
141	SLU 26	152	1	1592	1.78	6.02	0
141	SLU 27	168	0	1592	0.33	6.68	0
141	SLU 28	159	0	1592	1.2	6.29	0
141	SLU 29	168	0	1592	0.33	6.68	0
141	SLU 30	159	0	1592	1.2	6.29	0
141	SLU 31	216	0	1865	1.91	8.56	0
141	SLU 32	232	0	1865	0.46	9.23	0
141	SLU 33	222	0	1865	1.33	8.83	0
141	SLU 34	216	0	1865	1.91	8.56	0
141	SLU 35	232	0	1865	0.46	9.23	0
141	SLU 36	222	0	1865	1.33	8.83	0
141	SLU 37	232	0	1865	0.46	9.23	0
141	SLU 38	222	0	1865	1.33	8.83	0
141	SLU 39	259	-1	1981	0.52	10.32	0
141	SLU 40	250	0	1981	1.39	9.92	0
141	SLU 41	259	-1	1981	0.52	10.32	0
141	SLU 42	250	0	1981	1.39	9.92	0
141	SLU 43	167	0	1862	0.3	6.65	0
141	SLU 44	151	1	1862	1.74	5.99	0
141	SLU 45	167	0	1862	0.3	6.65	0
141	SLU 46	158	0	1862	1.17	6.25	0
141	SLU 47	151	1	1862	1.74	5.99	0
141	SLU 48	167	0	1862	0.3	6.65	0
141	SLU 49	158	0	1862	1.17	6.25	0
141	SLU 50	167	0	1862	0.3	6.65	0
141	SLU 51	158	0	1862	1.17	6.25	0
141	SLU 52	215	0	2134	1.88	8.53	0
141	SLU 53	231	0	2134	0.43	9.2	0
141	SLU 54	222	0	2134	1.3	8.8	0
141	SLU 55	215	0	2134	1.88	8.53	0
141	SLU 56	231	0	2134	0.43	9.2	0
141	SLU 57	222	0	2134	1.3	8.8	0
141	SLU 58	231	0	2134	0.43	9.2	0
141	SLU 59	222	0	2134	1.3	8.8	0
141	SLU 60	258	-1	2251	0.49	10.29	0
141	SLU 61	249	0	2251	1.36	9.89	0
141	SLU 62	258	-1	2251	0.49	10.29	0
141	SLU 63	249	0	2251	1.36	9.89	0
141	SLU 64	198	0	1988	0.38	7.89	0
141	SLU 65	183	1	1988	1.82	7.23	0
141	SLU 66	198	0	1988	0.38	7.89	0
141	SLU 67	189	0	1988	1.24	7.49	0
141	SLU 68	183	1	1988	1.82	7.23	0
141	SLU 69	198	0	1988	0.38	7.89	0
141	SLU 70	189	0	1988	1.24	7.49	0
141	SLU 71	198	0	1988	0.38	7.89	0
141	SLU 72	189	0	1988	1.24	7.49	0
141	SLU 73	246	0	2261	1.96	9.77	0
141	SLU 74	262	-1	2261	0.51	10.44	0
141	SLU 75	253	0	2261	1.38	10.04	0
141	SLU 76	246	0	2261	1.96	9.77	0
141	SLU 77	262	-1	2261	0.51	10.44	0
141	SLU 78	253	0	2261	1.38	10.04	0
141	SLU 79	262	-1	2261	0.51	10.44	0
141	SLU 80	253	0	2261	1.38	10.04	0
141	SLU 81	290	-1	2378	0.57	11.53	0
141	SLU 82	280	0	2378	1.44	11.13	0
141	SLU 83	290	-1	2378	0.57	11.53	0
141	SLU 84	280	0	2378	1.44	11.13	0
141	SLE RA 1	146	0	1501	0.27	5.8	0
141	SLE RA 2	135	0	1502	1.24	5.36	0
141	SLE RA 3	146	0	1501	0.27	5.8	0
141	SLE RA 4	139	0	1502	0.85	5.53	0
141	SLE RA 5	135	0	1502	1.24	5.36	0
141	SLE RA 6	146	0	1501	0.27	5.8	0
141	SLE RA 7	139	0	1502	0.85	5.53	0
141	SLE RA 8	146	0	1501	0.27	5.8	0
141	SLE RA 9	139	0	1502	0.85	5.53	0
141	SLE RA 10	178	0	1683	1.33	7.05	0
141	SLE RA 11	188	0	1683	0.36	7.5	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
141	SLE RA 12	182	0	1683	0.94	7.23	0
141	SLE RA 13	178	0	1683	1.33	7.05	0
141	SLE RA 14	188	0	1683	0.36	7.5	0
141	SLE RA 15	182	0	1683	0.94	7.23	0
141	SLE RA 16	188	0	1683	0.36	7.5	0
141	SLE RA 17	182	0	1683	0.94	7.23	0
141	SLE RA 18	207	0	1761	0.4	8.22	0
141	SLE RA 19	200	0	1761	0.98	7.96	0
141	SLE RA 20	207	0	1761	0.4	8.22	0
141	SLE RA 21	200	0	1761	0.98	7.96	0
141	SLE FR 1	146	0	1501	0.27	5.8	0
141	SLE FR 2	144	0	1502	0.46	5.71	0
141	SLE FR 3	146	0	1501	0.27	5.8	0
141	SLE FR 4	162	0	1579	0.5	6.44	0
141	SLE FR 5	164	0	1579	0.31	6.53	0
141	SLE FR 6	176	0	1631	0.34	7.01	0
141	SLE QP 1	146	0	1501	0.27	5.8	0
141	SLE QP 2	164	0	1579	0.31	6.53	0
141	SLD 1	284	-11	1638	12.07	11.64	-0.01
141	SLD 2	284	-11	1638	12.07	11.64	-0.01
141	SLD 3	311	-6	1681	5.26	12.79	0
141	SLD 4	311	-6	1681	5.26	12.79	0
141	SLD 5	158	-11	1531	14.16	6.32	-0.02
141	SLD 6	158	-11	1531	14.16	6.32	-0.02
141	SLD 7	250	5	1676	-8.53	10.15	0.01
141	SLD 8	250	5	1676	-8.53	10.15	0.01
141	SLD 9	78	-6	1483	9.15	2.9	-0.01
141	SLD 10	78	-6	1483	9.15	2.9	-0.01
141	SLD 11	170	10	1628	-13.54	6.73	0.02
141	SLD 12	170	10	1628	-13.54	6.73	0.02
141	SLD 13	17	6	1478	-4.64	0.26	0.01
141	SLD 14	17	6	1478	-4.64	0.26	0.01
141	SLD 15	44	11	1521	-11.45	1.41	0.01
141	SLD 16	44	11	1521	-11.45	1.41	0.01
141	SLV 1	446	-29	1716	29.33	18.59	-0.04
141	SLV 2	446	-29	1716	29.33	18.59	-0.04
141	SLV 3	511	-17	1820	13.24	21.29	-0.02
141	SLV 4	511	-17	1820	13.24	21.29	-0.02
141	SLV 5	151	-26	1463	33.42	6.05	-0.04
141	SLV 6	151	-26	1463	33.42	6.05	-0.04
141	SLV 7	366	12	1809	-20.21	15.05	0.03
141	SLV 8	366	12	1809	-20.21	15.05	0.03
141	SLV 9	-38	-13	1350	20.83	-1.99	-0.03
141	SLV 10	-38	-13	1350	20.83	-1.99	-0.03
141	SLV 11	177	26	1696	-32.8	7	0.04
141	SLV 12	177	26	1696	-32.8	7	0.04
141	SLV 13	-183	17	1339	-12.62	-8.23	0.02
141	SLV 14	-183	17	1339	-12.62	-8.23	0.02
141	SLV 15	-118	28	1443	-28.71	-5.54	0.04
141	SLV 16	-118	28	1443	-28.71	-5.54	0.04
142	SLU 1	107	-1	1541	0.57	4.16	0
142	SLU 2	94	1	1542	1.15	3.55	0.01
142	SLU 3	107	-1	1541	0.57	4.16	0
142	SLU 4	99	0	1542	0.92	3.79	0.01
142	SLU 5	94	1	1542	1.15	3.55	0.01
142	SLU 6	107	-1	1541	0.57	4.16	0
142	SLU 7	99	0	1542	0.92	3.79	0.01
142	SLU 8	107	-1	1541	0.57	4.16	0
142	SLU 9	99	0	1542	0.92	3.79	0.01
142	SLU 10	146	1	1853	1.49	5.5	0.01
142	SLU 11	159	-1	1852	0.91	6.11	0.01
142	SLU 12	151	0	1853	1.26	5.74	0.01
142	SLU 13	146	1	1853	1.49	5.5	0.01
142	SLU 14	159	-1	1852	0.91	6.11	0.01
142	SLU 15	151	0	1853	1.26	5.74	0.01
142	SLU 16	159	-1	1852	0.91	6.11	0.01
142	SLU 17	151	0	1853	1.26	5.74	0.01
142	SLU 18	181	-1	1986	1.05	6.95	0.01
142	SLU 19	173	0	1986	1.4	6.58	0.01
142	SLU 20	181	-1	1986	1.05	6.95	0.01
142	SLU 21	173	0	1986	1.4	6.58	0.01
142	SLU 22	135	-1	1689	0.75	5.16	0.01
142	SLU 23	121	1	1690	1.33	4.56	0.01
142	SLU 24	135	-1	1689	0.75	5.16	0.01
142	SLU 25	126	0	1690	1.1	4.8	0.01
142	SLU 26	121	1	1690	1.33	4.56	0.01
142	SLU 27	135	-1	1689	0.75	5.16	0.01
142	SLU 28	126	0	1690	1.1	4.8	0.01
142	SLU 29	135	-1	1689	0.75	5.16	0.01
142	SLU 30	126	0	1690	1.1	4.8	0.01
142	SLU 31	173	0	2002	1.67	6.51	0.01
142	SLU 32	186	-1	2000	1.09	7.12	0.01
142	SLU 33	178	0	2001	1.44	6.75	0.01
142	SLU 34	173	0	2002	1.67	6.51	0.01
142	SLU 35	186	-1	2000	1.09	7.12	0.01
142	SLU 36	178	0	2001	1.44	6.75	0.01
142	SLU 37	186	-1	2000	1.09	7.12	0.01
142	SLU 38	178	0	2001	1.44	6.75	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
142	SLU 39	208	-2	2134	1.24	7.95	0.01
142	SLU 40	200	-1	2134	1.58	7.59	0.01
142	SLU 41	208	-2	2134	1.24	7.95	0.01
142	SLU 42	200	-1	2134	1.58	7.59	0.01
142	SLU 43	130	-1	1952	0.68	5.06	0.01
142	SLU 44	117	1	1954	1.26	4.45	0.01
142	SLU 45	130	-1	1952	0.68	5.06	0.01
142	SLU 46	122	0	1953	1.03	4.69	0.01
142	SLU 47	117	1	1954	1.26	4.45	0.01
142	SLU 48	130	-1	1952	0.68	5.06	0.01
142	SLU 49	122	0	1953	1.03	4.69	0.01
142	SLU 50	130	-1	1952	0.68	5.06	0.01
142	SLU 51	122	0	1953	1.03	4.69	0.01
142	SLU 52	169	0	2265	1.6	6.4	0.01
142	SLU 53	182	-1	2264	1.02	7.01	0.01
142	SLU 54	174	0	2264	1.36	6.65	0.01
142	SLU 55	169	0	2265	1.6	6.4	0.01
142	SLU 56	182	-1	2264	1.02	7.01	0.01
142	SLU 57	174	0	2264	1.36	6.65	0.01
142	SLU 58	182	-1	2264	1.02	7.01	0.01
142	SLU 59	174	0	2264	1.36	6.65	0.01
142	SLU 60	204	-2	2397	1.16	7.85	0.01
142	SLU 61	196	-1	2398	1.51	7.48	0.01
142	SLU 62	204	-2	2397	1.16	7.85	0.01
142	SLU 63	196	-1	2398	1.51	7.48	0.01
142	SLU 64	158	-1	2100	0.86	6.07	0.01
142	SLU 65	144	1	2102	1.44	5.46	0.01
142	SLU 66	158	-1	2100	0.86	6.07	0.01
142	SLU 67	149	0	2101	1.21	5.7	0.01
142	SLU 68	144	1	2102	1.44	5.46	0.01
142	SLU 69	158	-1	2100	0.86	6.07	0.01
142	SLU 70	149	0	2101	1.21	5.7	0.01
142	SLU 71	158	-1	2100	0.86	6.07	0.01
142	SLU 72	149	0	2101	1.21	5.7	0.01
142	SLU 73	196	0	2413	1.78	7.41	0.01
142	SLU 74	209	-2	2412	1.2	8.02	0.01
142	SLU 75	201	-1	2412	1.55	7.65	0.01
142	SLU 76	196	0	2413	1.78	7.41	0.01
142	SLU 77	209	-2	2412	1.2	8.02	0.01
142	SLU 78	201	-1	2412	1.55	7.65	0.01
142	SLU 79	209	-2	2412	1.2	8.02	0.01
142	SLU 80	201	-1	2412	1.55	7.65	0.01
142	SLU 81	231	-2	2545	1.34	8.86	0.01
142	SLU 82	223	-1	2546	1.69	8.49	0.01
142	SLU 83	231	-2	2545	1.34	8.86	0.01
142	SLU 84	223	-1	2546	1.69	8.49	0.01
142	SLE RA 1	115	-1	1583	0.62	4.44	0
142	SLE RA 2	106	0	1584	1.01	4.04	0.01
142	SLE RA 3	115	-1	1583	0.62	4.44	0
142	SLE RA 4	110	0	1584	0.85	4.2	0.01
142	SLE RA 5	106	0	1584	1.01	4.04	0.01
142	SLE RA 6	115	-1	1583	0.62	4.44	0
142	SLE RA 7	110	0	1584	0.85	4.2	0.01
142	SLE RA 8	115	-1	1583	0.62	4.44	0
142	SLE RA 9	110	0	1584	0.85	4.2	0.01
142	SLE RA 10	141	0	1792	1.23	5.34	0.01
142	SLE RA 11	150	-1	1791	0.85	5.75	0.01
142	SLE RA 12	144	0	1791	1.08	5.5	0.01
142	SLE RA 13	141	0	1792	1.23	5.34	0.01
142	SLE RA 14	150	-1	1791	0.85	5.75	0.01
142	SLE RA 15	144	0	1791	1.08	5.5	0.01
142	SLE RA 16	150	-1	1791	0.85	5.75	0.01
142	SLE RA 17	144	0	1791	1.08	5.5	0.01
142	SLE RA 18	164	-1	1880	0.94	6.3	0.01
142	SLE RA 19	159	-1	1880	1.18	6.06	0.01
142	SLE RA 20	164	-1	1880	0.94	6.3	0.01
142	SLE RA 21	159	-1	1880	1.18	6.06	0.01
142	SLE FR 1	115	-1	1583	0.62	4.44	0
142	SLE FR 2	113	-1	1583	0.7	4.36	0
142	SLE FR 3	115	-1	1583	0.62	4.44	0
142	SLE FR 4	128	-1	1672	0.8	4.92	0.01
142	SLE FR 5	130	-1	1672	0.72	5	0.01
142	SLE FR 6	140	-1	1731	0.78	5.37	0.01
142	SLE QP 1	115	-1	1583	0.62	4.44	0
142	SLE QP 2	130	-1	1672	0.72	5	0.01
142	SLD 1	247	-11	1702	8.02	10.09	0
142	SLD 2	247	-11	1702	8.02	10.09	0
142	SLD 3	276	-8	1758	4.46	11.24	-0.01
142	SLD 4	276	-8	1758	4.46	11.24	-0.01
142	SLD 5	121	-10	1597	8.32	4.78	0.02
142	SLD 6	121	-10	1597	8.32	4.78	0.02
142	SLD 7	218	3	1782	-3.57	8.62	-0.01
142	SLD 8	218	3	1782	-3.57	8.62	-0.01
142	SLD 9	42	-5	1562	5.01	1.39	0.03
142	SLD 10	42	-5	1562	5.01	1.39	0.03
142	SLD 11	139	8	1747	-6.88	5.22	-0.01
142	SLD 12	139	8	1747	-6.88	5.22	-0.01
142	SLD 13	-16	6	1586	-3.02	-1.23	0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione			
		x	y	z		x	y	z	
142	SLD 14	-16	6	1586		-3.02	-1.23	0.02	
142	SLD 15	13	9	1642		-6.59	-0.08	0.01	
142	SLD 16	13	9	1642		-6.59	-0.08	0.01	
142	SLV 1	406	-30	1743		19.13	17.04	-0.01	
142	SLV 2	406	-30	1743		19.13	17.04	-0.01	
142	SLV 3	474	-21	1875		10.63	19.74	-0.03	
142	SLV 4	474	-21	1875		10.63	19.74	-0.03	
142	SLV 5	110	-23	1492		19.13	4.51	0.04	
142	SLV 6	110	-23	1492		19.13	4.51	0.04	
142	SLV 7	336	7	1934		-9.19	13.53	-0.04	
142	SLV 8	336	7	1934		-9.19	13.53	-0.04	
142	SLV 9	-76	-9	1410		10.63	-3.52	0.05	
142	SLV 10	-76	-9	1410		10.63	-3.52	0.05	
142	SLV 11	150	22	1852		-17.69	5.5	-0.03	
142	SLV 12	150	22	1852		-17.69	5.5	-0.03	
142	SLV 13	-214	19	1469		-9.19	-9.74	0.04	
142	SLV 14	-214	19	1469		-9.19	-9.74	0.04	
142	SLV 15	-146	28	1602		-17.69	-7.03	0.02	
142	SLV 16	-146	28	1602		-17.69	-7.03	0.02	
143	SLU 1	78	-4	1649		1.32	2.59	-0.02	
143	SLU 2	67	-3	1653		1.44	2.13	-0.02	
143	SLU 3	78	-4	1649		1.32	2.59	-0.02	
143	SLU 4	72	-4	1652		1.39	2.31	-0.02	
143	SLU 5	67	-3	1653		1.44	2.13	-0.02	
143	SLU 6	78	-4	1649		1.32	2.59	-0.02	
143	SLU 7	72	-4	1652		1.39	2.31	-0.02	
143	SLU 8	78	-4	1649		1.32	2.59	-0.02	
143	SLU 9	72	-4	1652		1.39	2.31	-0.02	
143	SLU 10	111	-6	2028		2.18	3.55	-0.03	
143	SLU 11	122	-7	2024		2.06	4.02	-0.03	
143	SLU 12	115	-6	2026		2.13	3.74	-0.03	
143	SLU 13	111	-6	2028		2.18	3.55	-0.03	
143	SLU 14	122	-7	2024		2.06	4.02	-0.03	
143	SLU 15	115	-6	2026		2.13	3.74	-0.03	
143	SLU 16	122	-7	2024		2.06	4.02	-0.03	
143	SLU 17	115	-6	2026		2.13	3.74	-0.03	
143	SLU 18	140	-8	2184		2.38	4.63	-0.03	
143	SLU 19	134	-7	2187		2.45	4.35	-0.03	
143	SLU 20	140	-8	2184		2.38	4.63	-0.03	
143	SLU 21	134	-7	2187		2.45	4.35	-0.03	
143	SLU 22	103	-6	1834		1.72	3.41	-0.02	
143	SLU 23	92	-4	1838		1.84	2.94	-0.02	
143	SLU 24	103	-6	1834		1.72	3.41	-0.02	
143	SLU 25	96	-5	1836		1.79	3.13	-0.02	
143	SLU 26	92	-4	1838		1.84	2.94	-0.02	
143	SLU 27	103	-6	1834		1.72	3.41	-0.02	
143	SLU 28	96	-5	1836		1.79	3.13	-0.02	
143	SLU 29	103	-6	1834		1.72	3.41	-0.02	
143	SLU 30	96	-5	1836		1.79	3.13	-0.02	
143	SLU 31	135	-7	2212		2.58	4.37	-0.03	
143	SLU 32	146	-8	2208		2.46	4.83	-0.03	
143	SLU 33	140	-7	2211		2.53	4.55	-0.03	
143	SLU 34	135	-7	2212		2.58	4.37	-0.03	
143	SLU 35	146	-8	2208		2.46	4.83	-0.03	
143	SLU 36	140	-7	2211		2.53	4.55	-0.03	
143	SLU 37	146	-8	2208		2.46	4.83	-0.03	
143	SLU 38	140	-7	2211		2.53	4.55	-0.03	
143	SLU 39	165	-9	2369		2.78	5.44	-0.03	
143	SLU 40	158	-9	2371		2.85	5.16	-0.04	
143	SLU 41	165	-9	2369		2.78	5.44	-0.03	
143	SLU 42	158	-9	2371		2.85	5.16	-0.04	
143	SLU 43	93	-5	2081		1.57	3.09	-0.02	
143	SLU 44	82	-4	2085		1.7	2.63	-0.02	
143	SLU 45	93	-5	2081		1.57	3.09	-0.02	
143	SLU 46	87	-5	2083		1.65	2.81	-0.02	
143	SLU 47	82	-4	2085		1.7	2.63	-0.02	
143	SLU 48	93	-5	2081		1.57	3.09	-0.02	
143	SLU 49	87	-5	2083		1.65	2.81	-0.02	
143	SLU 50	93	-5	2081		1.57	3.09	-0.02	
143	SLU 51	87	-5	2083		1.65	2.81	-0.02	
143	SLU 52	126	-6	2459		2.44	4.05	-0.03	
143	SLU 53	137	-8	2455		2.32	4.52	-0.03	
143	SLU 54	130	-7	2458		2.39	4.24	-0.03	
143	SLU 55	126	-6	2459		2.44	4.05	-0.03	
143	SLU 56	137	-8	2455		2.32	4.52	-0.03	
143	SLU 57	130	-7	2458		2.39	4.24	-0.03	
143	SLU 58	137	-8	2455		2.32	4.52	-0.03	
143	SLU 59	130	-7	2458		2.39	4.24	-0.03	
143	SLU 60	155	-9	2616		2.63	5.13	-0.03	
143	SLU 61	149	-8	2618		2.71	4.85	-0.03	
143	SLU 62	155	-9	2616		2.63	5.13	-0.03	
143	SLU 63	149	-8	2618		2.71	4.85	-0.03	
143	SLU 64	118	-7	2266		1.97	3.91	-0.03	
143	SLU 65	107	-5	2270		2.1	3.44	-0.03	
143	SLU 66	118	-7	2266		1.97	3.91	-0.03	
143	SLU 67	111	-6	2268		2.05	3.63	-0.03	
143	SLU 68	107	-5	2270		2.1	3.44	-0.03	
143	SLU 69	118	-7	2266		1.97	3.91	-0.03	



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
143	SLU 70	111	-6	2268	2.05	3.63	-0.03
143	SLU 71	118	-7	2266	1.97	3.91	-0.03
143	SLU 72	111	-6	2268	2.05	3.63	-0.03
143	SLU 73	150	-8	2644	2.84	4.86	-0.04
143	SLU 74	161	-9	2640	2.72	5.33	-0.03
143	SLU 75	155	-8	2642	2.79	5.05	-0.04
143	SLU 76	150	-8	2644	2.84	4.86	-0.04
143	SLU 77	161	-9	2640	2.72	5.33	-0.03
143	SLU 78	155	-8	2642	2.79	5.05	-0.04
143	SLU 79	161	-9	2640	2.72	5.33	-0.03
143	SLU 80	155	-8	2642	2.79	5.05	-0.04
143	SLU 81	180	-10	2800	3.03	5.94	-0.04
143	SLU 82	173	-9	2803	3.11	5.66	-0.04
143	SLU 83	180	-10	2800	3.03	5.94	-0.04
143	SLU 84	173	-9	2803	3.11	5.66	-0.04
143	SLE RA 1	85	-5	1702	1.43	2.83	-0.02
143	SLE RA 2	78	-4	1705	1.51	2.51	-0.02
143	SLE RA 3	85	-5	1702	1.43	2.83	-0.02
143	SLE RA 4	81	-4	1704	1.48	2.64	-0.02
143	SLE RA 5	78	-4	1705	1.51	2.51	-0.02
143	SLE RA 6	85	-5	1702	1.43	2.83	-0.02
143	SLE RA 7	81	-4	1704	1.48	2.64	-0.02
143	SLE RA 8	85	-5	1702	1.43	2.83	-0.02
143	SLE RA 9	81	-4	1704	1.48	2.64	-0.02
143	SLE RA 10	107	-6	1954	2.01	3.46	-0.03
143	SLE RA 11	114	-7	1952	1.92	3.78	-0.02
143	SLE RA 12	110	-6	1953	1.97	3.59	-0.03
143	SLE RA 13	107	-6	1954	2.01	3.46	-0.03
143	SLE RA 14	114	-7	1952	1.92	3.78	-0.02
143	SLE RA 15	110	-6	1953	1.97	3.59	-0.03
143	SLE RA 16	114	-7	1952	1.92	3.78	-0.02
143	SLE RA 17	110	-6	1953	1.97	3.59	-0.03
143	SLE RA 18	127	-7	2059	2.14	4.18	-0.03
143	SLE RA 19	122	-7	2060	2.19	4	-0.03
143	SLE RA 20	127	-7	2059	2.14	4.18	-0.03
143	SLE RA 21	122	-7	2060	2.19	4	-0.03
143	SLE FR 1	85	-5	1702	1.43	2.83	-0.02
143	SLE FR 2	84	-5	1703	1.45	2.76	-0.02
143	SLE FR 3	85	-5	1702	1.43	2.83	-0.02
143	SLE FR 4	96	-5	1810	1.66	3.17	-0.02
143	SLE FR 5	98	-6	1809	1.64	3.23	-0.02
143	SLE FR 6	106	-6	1880	1.78	3.5	-0.02
143	SLE QP 1	85	-5	1702	1.43	2.83	-0.02
143	SLE QP 2	98	-6	1809	1.64	3.23	-0.02
143	SLD 1	211	-14	1801	5.2	8.1	-0.01
143	SLD 2	211	-14	1801	5.2	8.1	-0.01
143	SLD 3	243	-10	1887	3.82	9.31	-0.02
143	SLD 4	243	-10	1887	3.82	9.31	-0.02
143	SLD 5	84	-15	1676	4.8	2.87	0
143	SLD 6	84	-15	1676	4.8	2.87	0
143	SLD 7	189	0	1964	0.2	6.88	-0.03
143	SLD 8	189	0	1964	0.2	6.88	-0.03
143	SLD 9	6	-12	1655	3.08	-0.42	-0.01
143	SLD 10	6	-12	1655	3.08	-0.42	-0.01
143	SLD 11	112	4	1943	-1.52	3.6	-0.04
143	SLD 12	112	4	1943	-1.52	3.6	-0.04
143	SLD 13	-47	-2	1731	-0.53	-2.84	-0.03
143	SLD 14	-47	-2	1731	-0.53	-2.84	-0.03
143	SLD 15	-15	3	1817	-1.91	-1.64	-0.04
143	SLD 16	-15	3	1817	-1.91	-1.64	-0.04
143	SLV 1	364	-29	1791	10.9	14.68	0.02
143	SLV 2	364	-29	1791	10.9	14.68	0.02
143	SLV 3	438	-18	1996	7.57	17.51	0
143	SLV 4	438	-18	1996	7.57	17.51	0
143	SLV 5	64	-30	1493	9.47	2.38	0.03
143	SLV 6	64	-30	1493	9.47	2.38	0.03
143	SLV 7	313	8	2176	-1.63	11.81	-0.05
143	SLV 8	313	8	2176	-1.63	11.81	-0.05
143	SLV 9	-118	-19	1442	4.91	-5.34	0.01
143	SLV 10	-118	-19	1442	4.91	-5.34	0.01
143	SLV 11	131	19	2125	-6.18	4.09	-0.07
143	SLV 12	131	19	2125	-6.18	4.09	-0.07
143	SLV 13	-243	7	1623	-4.29	-11.05	-0.04
143	SLV 14	-243	7	1623	-4.29	-11.05	-0.04
143	SLV 15	-168	18	1827	-7.62	-8.22	-0.06
143	SLV 16	-168	18	1827	-7.62	-8.22	-0.06
144	SLU 1	-22	-314	2407	11.29	-0.78	0
144	SLU 2	-33	-314	2416	11.25	-1.27	0
144	SLU 3	-22	-314	2407	11.29	-0.78	0
144	SLU 4	-29	-314	2412	11.27	-1.07	0
144	SLU 5	-33	-314	2416	11.25	-1.27	0
144	SLU 6	-22	-314	2407	11.29	-0.78	0
144	SLU 7	-29	-314	2412	11.27	-1.07	0
144	SLU 8	-22	-314	2407	11.29	-0.78	0
144	SLU 9	-29	-314	2412	11.27	-1.07	0
144	SLU 10	-41	-475	3071	17.53	-1.58	0
144	SLU 11	-31	-475	3062	17.57	-1.09	0
144	SLU 12	-37	-475	3067	17.55	-1.38	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
144	SLU 13	-41	-475	3071	17.53	-1.58	0
144	SLU 14	-31	-475	3062	17.57	-1.09	0
144	SLU 15	-37	-475	3067	17.55	-1.38	0
144	SLU 16	-31	-475	3062	17.57	-1.09	0
144	SLU 17	-37	-475	3067	17.55	-1.38	0
144	SLU 18	-35	-544	3343	20.27	-1.22	0
144	SLU 19	-41	-544	3348	20.24	-1.51	0
144	SLU 20	-35	-544	3343	20.27	-1.22	0
144	SLU 21	-41	-544	3348	20.24	-1.51	0
144	SLU 22	-25	-401	2743	14.72	-0.89	0
144	SLU 23	-36	-401	2752	14.68	-1.38	0
144	SLU 24	-25	-401	2743	14.72	-0.89	0
144	SLU 25	-32	-401	2748	14.69	-1.18	0
144	SLU 26	-36	-401	2752	14.68	-1.38	0
144	SLU 27	-25	-401	2743	14.72	-0.89	0
144	SLU 28	-32	-401	2748	14.69	-1.18	0
144	SLU 29	-25	-401	2743	14.72	-0.89	0
144	SLU 30	-32	-401	2748	14.69	-1.18	0
144	SLU 31	-45	-562	3407	20.96	-1.69	0
144	SLU 32	-34	-562	3398	21	-1.19	0
144	SLU 33	-40	-562	3403	20.98	-1.49	0
144	SLU 34	-45	-562	3407	20.96	-1.69	0
144	SLU 35	-34	-562	3398	21	-1.19	0
144	SLU 36	-40	-562	3403	20.98	-1.49	0
144	SLU 37	-34	-562	3398	21	-1.19	0
144	SLU 38	-40	-562	3403	20.98	-1.49	0
144	SLU 39	-38	-631	3679	23.7	-1.32	0
144	SLU 40	-44	-631	3684	23.67	-1.62	0
144	SLU 41	-38	-631	3679	23.7	-1.32	0
144	SLU 42	-44	-631	3684	23.67	-1.62	0
144	SLU 43	-28	-379	3014	13.5	-0.98	0
144	SLU 44	-38	-379	3023	13.46	-1.47	0
144	SLU 45	-28	-379	3014	13.5	-0.98	0
144	SLU 46	-34	-379	3019	13.48	-1.27	0
144	SLU 47	-38	-379	3023	13.46	-1.47	0
144	SLU 48	-28	-379	3014	13.5	-0.98	0
144	SLU 49	-34	-379	3019	13.48	-1.27	0
144	SLU 50	-28	-379	3014	13.5	-0.98	0
144	SLU 51	-34	-379	3019	13.48	-1.27	0
144	SLU 52	-47	-539	3678	19.75	-1.77	0
144	SLU 53	-36	-540	3669	19.79	-1.28	0
144	SLU 54	-43	-539	3674	19.76	-1.58	0
144	SLU 55	-47	-539	3678	19.75	-1.77	0
144	SLU 56	-36	-540	3669	19.79	-1.28	0
144	SLU 57	-43	-539	3674	19.76	-1.58	0
144	SLU 58	-36	-540	3669	19.79	-1.28	0
144	SLU 59	-43	-539	3674	19.76	-1.58	0
144	SLU 60	-40	-609	3950	22.48	-1.41	0
144	SLU 61	-46	-608	3955	22.46	-1.71	0
144	SLU 62	-40	-609	3950	22.48	-1.41	0
144	SLU 63	-46	-608	3955	22.46	-1.71	0
144	SLU 64	-31	-466	3350	16.93	-1.09	0
144	SLU 65	-42	-466	3359	16.89	-1.58	0
144	SLU 66	-31	-466	3350	16.93	-1.09	0
144	SLU 67	-37	-466	3355	16.91	-1.38	0
144	SLU 68	-42	-466	3359	16.89	-1.58	0
144	SLU 69	-31	-466	3350	16.93	-1.09	0
144	SLU 70	-37	-466	3355	16.91	-1.38	0
144	SLU 71	-31	-466	3350	16.93	-1.09	0
144	SLU 72	-37	-466	3355	16.91	-1.38	0
144	SLU 73	-50	-626	4014	23.17	-1.88	0
144	SLU 74	-40	-627	4005	23.21	-1.39	0
144	SLU 75	-46	-626	4010	23.19	-1.69	0
144	SLU 76	-50	-626	4014	23.17	-1.88	0
144	SLU 77	-40	-627	4005	23.21	-1.39	0
144	SLU 78	-46	-626	4010	23.19	-1.69	0
144	SLU 79	-40	-627	4005	23.21	-1.39	0
144	SLU 80	-46	-626	4010	23.19	-1.69	0
144	SLU 81	-43	-696	4286	25.91	-1.52	0
144	SLU 82	-50	-695	4291	25.88	-1.82	0
144	SLU 83	-43	-696	4286	25.91	-1.52	0
144	SLU 84	-50	-695	4291	25.88	-1.82	0
144	SLE RA 1	-23	-339	2503	12.27	-0.81	0
144	SLE RA 2	-30	-339	2509	12.24	-1.14	0
144	SLE RA 3	-23	-339	2503	12.27	-0.81	0
144	SLE RA 4	-27	-339	2507	12.25	-1.01	0
144	SLE RA 5	-30	-339	2509	12.24	-1.14	0
144	SLE RA 6	-23	-339	2503	12.27	-0.81	0
144	SLE RA 7	-27	-339	2507	12.25	-1.01	0
144	SLE RA 8	-23	-339	2503	12.27	-0.81	0
144	SLE RA 9	-27	-339	2507	12.25	-1.01	0
144	SLE RA 10	-36	-446	2946	16.43	-1.34	0
144	SLE RA 11	-29	-446	2940	16.46	-1.01	0
144	SLE RA 12	-33	-446	2943	16.44	-1.21	0
144	SLE RA 13	-36	-446	2946	16.43	-1.34	0
144	SLE RA 14	-29	-446	2940	16.46	-1.01	0
144	SLE RA 15	-33	-446	2943	16.44	-1.21	0
144	SLE RA 16	-29	-446	2940	16.46	-1.01	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
144	SLE RA 17	-33	-446	2943	16.44	-1.21	0
144	SLE RA 18	-31	-492	3127	18.25	-1.1	0
144	SLE RA 19	-36	-492	3131	18.24	-1.3	0
144	SLE RA 20	-31	-492	3127	18.25	-1.1	0
144	SLE RA 21	-36	-492	3131	18.24	-1.3	0
144	SLE FR 1	-23	-339	2503	12.27	-0.81	0
144	SLE FR 2	-25	-339	2504	12.27	-0.88	0
144	SLE FR 3	-23	-339	2503	12.27	-0.81	0
144	SLE FR 4	-27	-385	2692	14.06	-0.96	0
144	SLE FR 5	-26	-385	2690	14.07	-0.9	0
144	SLE FR 6	-27	-416	2815	15.26	-0.96	0
144	SLE QP 1	-23	-339	2503	12.27	-0.81	0
144	SLE QP 2	-26	-385	2690	14.07	-0.9	0
144	SLD 1	113	-398	2533	15.25	4.25	0.01
144	SLD 2	113	-398	2533	15.25	4.25	0.01
144	SLD 3	92	-331	2713	11.02	5.15	0.01
144	SLD 4	92	-331	2713	11.02	5.15	0.01
144	SLD 5	47	-491	2369	20.84	-0.73	-0.01
144	SLD 6	47	-491	2369	20.84	-0.73	-0.01
144	SLD 7	-22	-267	2972	6.73	2.29	0.01
144	SLD 8	-22	-267	2972	6.73	2.29	0.01
144	SLD 9	-30	-503	2409	21.4	-4.08	-0.01
144	SLD 10	-30	-503	2409	21.4	-4.08	-0.01
144	SLD 11	-98	-280	3012	7.29	-1.07	0.01
144	SLD 12	-98	-280	3012	7.29	-1.07	0.01
144	SLD 13	-143	-439	2668	17.12	-6.95	-0.01
144	SLD 14	-143	-439	2668	17.12	-6.95	-0.01
144	SLD 15	-164	-372	2848	12.88	-6.04	-0.01
144	SLD 16	-164	-372	2848	12.88	-6.04	-0.01
144	SLV 1	300	-417	2317	17.09	11.27	0.01
144	SLV 2	300	-417	2317	17.09	11.27	0.01
144	SLV 3	252	-258	2744	6.63	13.38	0.02
144	SLV 4	252	-258	2744	6.63	13.38	0.02
144	SLV 5	145	-636	1930	30.84	-0.45	-0.01
144	SLV 6	145	-636	1930	30.84	-0.45	-0.01
144	SLV 7	-15	-105	3355	-4.03	6.59	0.02
144	SLV 8	-15	-105	3355	-4.03	6.59	0.02
144	SLV 9	-36	-665	2026	32.16	-8.38	-0.02
144	SLV 10	-36	-665	2026	32.16	-8.38	-0.02
144	SLV 11	-196	-134	3451	-2.71	-1.35	0.01
144	SLV 12	-196	-134	3451	-2.71	-1.35	0.01
144	SLV 13	-303	-513	2637	21.5	-15.18	-0.02
144	SLV 14	-303	-513	2637	21.5	-15.18	-0.02
144	SLV 15	-351	-354	3064	11.04	-13.07	-0.01
144	SLV 16	-351	-354	3064	11.04	-13.07	-0.01
145	SLU 1	-123	-4	1605	1.31	-4.54	0.02
145	SLU 2	-133	-5	1614	1.17	-4.98	0.02
145	SLU 3	-123	-4	1605	1.31	-4.54	0.02
145	SLU 4	-129	-5	1610	1.23	-4.8	0.02
145	SLU 5	-133	-5	1614	1.17	-4.98	0.02
145	SLU 6	-123	-4	1605	1.31	-4.54	0.02
145	SLU 7	-129	-5	1610	1.23	-4.8	0.02
145	SLU 8	-123	-4	1605	1.31	-4.54	0.02
145	SLU 9	-129	-5	1610	1.23	-4.8	0.02
145	SLU 10	-194	-7	1973	1.88	-7.15	0.03
145	SLU 11	-183	-7	1964	2.03	-6.72	0.03
145	SLU 12	-190	-7	1969	1.94	-6.98	0.03
145	SLU 13	-194	-7	1973	1.88	-7.15	0.03
145	SLU 14	-183	-7	1964	2.03	-6.72	0.03
145	SLU 15	-190	-7	1969	1.94	-6.98	0.03
145	SLU 16	-183	-7	1964	2.03	-6.72	0.03
145	SLU 17	-190	-7	1969	1.94	-6.98	0.03
145	SLU 18	-209	-8	2117	2.33	-7.65	0.03
145	SLU 19	-216	-8	2123	2.25	-7.91	0.03
145	SLU 20	-209	-8	2117	2.33	-7.65	0.03
145	SLU 21	-216	-8	2123	2.25	-7.91	0.03
145	SLU 22	-154	-6	1783	1.7	-5.63	0.02
145	SLU 23	-164	-6	1793	1.56	-6.07	0.02
145	SLU 24	-154	-6	1783	1.7	-5.63	0.02
145	SLU 25	-160	-6	1789	1.61	-5.9	0.02
145	SLU 26	-164	-6	1793	1.56	-6.07	0.02
145	SLU 27	-154	-6	1783	1.7	-5.63	0.02
145	SLU 28	-160	-6	1789	1.61	-5.9	0.02
145	SLU 29	-154	-6	1783	1.7	-5.63	0.02
145	SLU 30	-160	-6	1789	1.61	-5.9	0.02
145	SLU 31	-225	-9	2151	2.27	-8.25	0.03
145	SLU 32	-214	-8	2142	2.42	-7.81	0.03
145	SLU 33	-221	-8	2148	2.33	-8.07	0.03
145	SLU 34	-225	-9	2151	2.27	-8.25	0.03
145	SLU 35	-214	-8	2142	2.42	-7.81	0.03
145	SLU 36	-221	-8	2148	2.33	-8.07	0.03
145	SLU 37	-214	-8	2142	2.42	-7.81	0.03
145	SLU 38	-221	-8	2148	2.33	-8.07	0.03
145	SLU 39	-240	-9	2296	2.72	-8.74	0.04
145	SLU 40	-247	-9	2302	2.63	-9.01	0.03
145	SLU 41	-240	-9	2296	2.72	-8.74	0.04
145	SLU 42	-247	-9	2302	2.63	-9.01	0.03
145	SLU 43	-149	-5	2025	1.57	-5.53	0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione			
		x	y	z		x	y	z	
145	SLU 44	-160	-6	2035		1.43	-5.96	0.02	
145	SLU 45	-149	-5	2025		1.57	-5.53	0.02	
145	SLU 46	-155	-6	2031		1.49	-5.79	0.02	
145	SLU 47	-160	-6	2035		1.43	-5.96	0.02	
145	SLU 48	-149	-5	2025		1.57	-5.53	0.02	
145	SLU 49	-155	-6	2031		1.49	-5.79	0.02	
145	SLU 50	-149	-5	2025		1.57	-5.53	0.02	
145	SLU 51	-155	-6	2031		1.49	-5.79	0.02	
145	SLU 52	-220	-8	2393		2.14	-8.14	0.03	
145	SLU 53	-210	-8	2384		2.29	-7.7	0.03	
145	SLU 54	-216	-8	2390		2.2	-7.97	0.03	
145	SLU 55	-220	-8	2393		2.14	-8.14	0.03	
145	SLU 56	-210	-8	2384		2.29	-7.7	0.03	
145	SLU 57	-216	-8	2390		2.2	-7.97	0.03	
145	SLU 58	-210	-8	2384		2.29	-7.7	0.03	
145	SLU 59	-216	-8	2390		2.2	-7.97	0.03	
145	SLU 60	-236	-9	2538		2.59	-8.64	0.03	
145	SLU 61	-242	-9	2543		2.51	-8.9	0.03	
145	SLU 62	-236	-9	2538		2.59	-8.64	0.03	
145	SLU 63	-242	-9	2543		2.51	-8.9	0.03	
145	SLU 64	-180	-7	2204		1.96	-6.62	0.03	
145	SLU 65	-191	-7	2213		1.82	-7.06	0.03	
145	SLU 66	-180	-7	2204		1.96	-6.62	0.03	
145	SLU 67	-186	-7	2209		1.87	-6.88	0.03	
145	SLU 68	-191	-7	2213		1.82	-7.06	0.03	
145	SLU 69	-180	-7	2204		1.96	-6.62	0.03	
145	SLU 70	-186	-7	2209		1.87	-6.88	0.03	
145	SLU 71	-180	-7	2204		1.96	-6.62	0.03	
145	SLU 72	-186	-7	2209		1.87	-6.88	0.03	
145	SLU 73	-251	-9	2572		2.53	-9.24	0.03	
145	SLU 74	-241	-9	2562		2.68	-8.8	0.03	
145	SLU 75	-247	-9	2568		2.59	-9.06	0.03	
145	SLU 76	-251	-9	2572		2.53	-9.24	0.03	
145	SLU 77	-241	-9	2562		2.68	-8.8	0.03	
145	SLU 78	-247	-9	2568		2.59	-9.06	0.03	
145	SLU 79	-241	-9	2562		2.68	-8.8	0.03	
145	SLU 80	-247	-9	2568		2.59	-9.06	0.03	
145	SLU 81	-267	-10	2716		2.98	-9.73	0.04	
145	SLU 82	-273	-10	2722		2.89	-9.99	0.04	
145	SLU 83	-267	-10	2716		2.98	-9.73	0.04	
145	SLU 84	-273	-10	2722		2.89	-9.99	0.04	
145	SLE RA 1	-132	-5	1656		1.42	-4.85	0.02	
145	SLE RA 2	-139	-5	1662		1.33	-5.14	0.02	
145	SLE RA 3	-132	-5	1656		1.42	-4.85	0.02	
145	SLE RA 4	-136	-5	1660		1.37	-5.03	0.02	
145	SLE RA 5	-139	-5	1662		1.33	-5.14	0.02	
145	SLE RA 6	-132	-5	1656		1.42	-4.85	0.02	
145	SLE RA 7	-136	-5	1660		1.37	-5.03	0.02	
145	SLE RA 8	-132	-5	1656		1.42	-4.85	0.02	
145	SLE RA 9	-136	-5	1660		1.37	-5.03	0.02	
145	SLE RA 10	-179	-7	1901		1.8	-6.6	0.02	
145	SLE RA 11	-172	-6	1895		1.9	-6.3	0.02	
145	SLE RA 12	-176	-7	1899		1.84	-6.48	0.02	
145	SLE RA 13	-179	-7	1901		1.8	-6.6	0.02	
145	SLE RA 14	-172	-6	1895		1.9	-6.3	0.02	
145	SLE RA 15	-176	-7	1899		1.84	-6.48	0.02	
145	SLE RA 16	-172	-6	1895		1.9	-6.3	0.02	
145	SLE RA 17	-176	-7	1899		1.84	-6.48	0.02	
145	SLE RA 18	-189	-7	1998		2.1	-6.93	0.03	
145	SLE RA 19	-194	-7	2001		2.05	-7.1	0.03	
145	SLE RA 20	-189	-7	1998		2.1	-6.93	0.03	
145	SLE RA 21	-194	-7	2001		2.05	-7.1	0.03	
145	SLE FR 1	-132	-5	1656		1.42	-4.85	0.02	
145	SLE FR 2	-133	-5	1657		1.4	-4.91	0.02	
145	SLE FR 3	-132	-5	1656		1.42	-4.85	0.02	
145	SLE FR 4	-150	-6	1760		1.61	-5.53	0.02	
145	SLE FR 5	-149	-5	1758		1.63	-5.47	0.02	
145	SLE FR 6	-161	-6	1827		1.76	-5.89	0.02	
145	SLE QP 1	-132	-5	1656		1.42	-4.85	0.02	
145	SLE QP 2	-149	-5	1758		1.63	-5.47	0.02	
145	SLD 1	-10	-1	1652		-0.57	0.42	0.03	
145	SLD 2	-10	-1	1652		-0.57	0.42	0.03	
145	SLD 3	-35	4	1739		-1.74	-0.54	0.04	
145	SLD 4	-35	4	1739		-1.74	-0.54	0.04	
145	SLD 5	-70	-12	1595		2.75	-2.25	0.01	
145	SLD 6	-70	-12	1595		2.75	-2.25	0.01	
145	SLD 7	-153	5	1884		-1.16	-5.45	0.04	
145	SLD 8	-153	5	1884		-1.16	-5.45	0.04	
145	SLD 9	-145	-16	1633		4.42	-5.5	0	
145	SLD 10	-145	-16	1633		4.42	-5.5	0	
145	SLD 11	-228	1	1922		0.51	-8.7	0.03	
145	SLD 12	-228	1	1922		0.51	-8.7	0.03	
145	SLD 13	-263	-15	1778		5	-10.41	0.01	
145	SLD 14	-263	-15	1778		5	-10.41	0.01	
145	SLD 15	-288	-10	1865		3.82	-11.37	0.02	
145	SLD 16	-288	-10	1865		3.82	-11.37	0.02	
145	SLV 1	177	8	1507		-4.31	8.39	0.04	
145	SLV 2	177	8	1507		-4.31	8.39	0.04	



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
145	SLV 3	119	21	1712	-7.17	6.15	0.06
145	SLV 4	119	21	1712	-7.17	6.15	0.06
145	SLV 5	37	-20	1372	4.19	2.08	-0.01
145	SLV 6	37	-20	1372	4.19	2.08	-0.01
145	SLV 7	-157	21	2056	-5.35	-5.38	0.07
145	SLV 8	-157	21	2056	-5.35	-5.38	0.07
145	SLV 9	-141	-32	1461	8.6	-5.57	-0.02
145	SLV 10	-141	-32	1461	8.6	-5.57	-0.02
145	SLV 11	-335	9	2145	-0.93	-13.03	0.05
145	SLV 12	-335	9	2145	-0.93	-13.03	0.05
145	SLV 13	-417	-32	1804	10.42	-17.1	-0.02
145	SLV 14	-417	-32	1804	10.42	-17.1	-0.02
145	SLV 15	-475	-19	2010	7.56	-19.33	0
145	SLV 16	-475	-19	2010	7.56	-19.33	0
146	SLU 1	-137	-1	1466	0.59	-5.19	0
146	SLU 2	-150	-1	1478	0.17	-5.77	0
146	SLU 3	-137	-1	1466	0.59	-5.19	0
146	SLU 4	-145	-1	1473	0.34	-5.54	0
146	SLU 5	-150	-1	1478	0.17	-5.77	0
146	SLU 6	-137	-1	1466	0.59	-5.19	0
146	SLU 7	-145	-1	1473	0.34	-5.54	0
146	SLU 8	-137	-1	1466	0.59	-5.19	0
146	SLU 9	-145	-1	1473	0.34	-5.54	0
146	SLU 10	-213	-1	1762	0.48	-8.1	-0.01
146	SLU 11	-200	-1	1751	0.9	-7.53	-0.01
146	SLU 12	-208	-1	1758	0.65	-7.87	-0.01
146	SLU 13	-213	-1	1762	0.48	-8.1	-0.01
146	SLU 14	-200	-1	1751	0.9	-7.53	-0.01
146	SLU 15	-208	-1	1758	0.65	-7.87	-0.01
146	SLU 16	-200	-1	1751	0.9	-7.53	-0.01
146	SLU 17	-208	-1	1758	0.65	-7.87	-0.01
146	SLU 18	-227	-1	1873	1.03	-8.53	-0.01
146	SLU 19	-234	-1	1879	0.78	-8.87	-0.01
146	SLU 20	-227	-1	1873	1.03	-8.53	-0.01
146	SLU 21	-234	-1	1879	0.78	-8.87	-0.01
146	SLU 22	-168	-1	1604	0.76	-6.33	-0.01
146	SLU 23	-181	-1	1615	0.35	-6.91	0
146	SLU 24	-168	-1	1604	0.76	-6.33	-0.01
146	SLU 25	-176	-1	1611	0.51	-6.68	-0.01
146	SLU 26	-181	-1	1615	0.35	-6.91	0
146	SLU 27	-168	-1	1604	0.76	-6.33	-0.01
146	SLU 28	-176	-1	1611	0.51	-6.68	-0.01
146	SLU 29	-168	-1	1604	0.76	-6.33	-0.01
146	SLU 30	-176	-1	1611	0.51	-6.68	-0.01
146	SLU 31	-244	-1	1900	0.66	-9.24	-0.01
146	SLU 32	-231	-1	1888	1.07	-8.67	-0.01
146	SLU 33	-239	-1	1895	0.82	-9.01	-0.01
146	SLU 34	-244	-1	1900	0.66	-9.24	-0.01
146	SLU 35	-231	-1	1888	1.07	-8.67	-0.01
146	SLU 36	-239	-1	1895	0.82	-9.01	-0.01
146	SLU 37	-231	-1	1888	1.07	-8.67	-0.01
146	SLU 38	-239	-1	1895	0.82	-9.01	-0.01
146	SLU 39	-258	-1	2010	1.2	-9.67	-0.01
146	SLU 40	-265	-2	2017	0.96	-10.01	-0.01
146	SLU 41	-258	-1	2010	1.2	-9.67	-0.01
146	SLU 42	-265	-2	2017	0.96	-10.01	-0.01
146	SLU 43	-168	-1	1859	0.7	-6.36	-0.01
146	SLU 44	-180	-1	1870	0.29	-6.94	0
146	SLU 45	-168	-1	1859	0.7	-6.36	-0.01
146	SLU 46	-175	-1	1866	0.45	-6.71	0
146	SLU 47	-180	-1	1870	0.29	-6.94	0
146	SLU 48	-168	-1	1859	0.7	-6.36	-0.01
146	SLU 49	-175	-1	1866	0.45	-6.71	0
146	SLU 50	-168	-1	1859	0.7	-6.36	-0.01
146	SLU 51	-175	-1	1866	0.45	-6.71	0
146	SLU 52	-243	-1	2155	0.6	-9.27	-0.01
146	SLU 53	-231	-1	2144	1.01	-8.69	-0.01
146	SLU 54	-238	-1	2150	0.77	-9.04	-0.01
146	SLU 55	-243	-1	2155	0.6	-9.27	-0.01
146	SLU 56	-231	-1	2144	1.01	-8.69	-0.01
146	SLU 57	-238	-1	2150	0.77	-9.04	-0.01
146	SLU 58	-231	-1	2144	1.01	-8.69	-0.01
146	SLU 59	-238	-1	2150	0.77	-9.04	-0.01
146	SLU 60	-257	-1	2265	1.15	-9.7	-0.01
146	SLU 61	-265	-1	2272	0.9	-10.04	-0.01
146	SLU 62	-257	-1	2265	1.15	-9.7	-0.01
146	SLU 63	-265	-1	2272	0.9	-10.04	-0.01
146	SLU 64	-199	-1	1997	0.88	-7.5	-0.01
146	SLU 65	-211	-1	2008	0.46	-8.08	-0.01
146	SLU 66	-199	-1	1997	0.88	-7.5	-0.01
146	SLU 67	-206	-1	2003	0.63	-7.84	-0.01
146	SLU 68	-211	-1	2008	0.46	-8.08	-0.01
146	SLU 69	-199	-1	1997	0.88	-7.5	-0.01
146	SLU 70	-206	-1	2003	0.63	-7.84	-0.01
146	SLU 71	-199	-1	1997	0.88	-7.5	-0.01
146	SLU 72	-206	-1	2003	0.63	-7.84	-0.01
146	SLU 73	-274	-2	2292	0.77	-10.41	-0.01
146	SLU 74	-262	-1	2281	1.19	-9.83	-0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
146	SLU 75	-269	-2	2288	0.94	-10.18	-0.01
146	SLU 76	-274	-2	2292	0.77	-10.41	-0.01
146	SLU 77	-262	-1	2281	1.19	-9.83	-0.01
146	SLU 78	-269	-2	2288	0.94	-10.18	-0.01
146	SLU 79	-262	-1	2281	1.19	-9.83	-0.01
146	SLU 80	-269	-2	2288	0.94	-10.18	-0.01
146	SLU 81	-289	-2	2403	1.32	-10.83	-0.01
146	SLU 82	-296	-2	2410	1.07	-11.18	-0.01
146	SLU 83	-289	-2	2403	1.32	-10.83	-0.01
146	SLU 84	-296	-2	2410	1.07	-11.18	-0.01
146	SLE RA 1	-146	-1	1506	0.64	-5.52	0
146	SLE RA 2	-154	-1	1513	0.36	-5.9	0
146	SLE RA 3	-146	-1	1506	0.64	-5.52	0
146	SLE RA 4	-151	-1	1510	0.47	-5.75	0
146	SLE RA 5	-154	-1	1513	0.36	-5.9	0
146	SLE RA 6	-146	-1	1506	0.64	-5.52	0
146	SLE RA 7	-151	-1	1510	0.47	-5.75	0
146	SLE RA 8	-146	-1	1506	0.64	-5.52	0
146	SLE RA 9	-151	-1	1510	0.47	-5.75	0
146	SLE RA 10	-196	-1	1703	0.57	-7.46	-0.01
146	SLE RA 11	-188	-1	1695	0.84	-7.07	-0.01
146	SLE RA 12	-193	-1	1700	0.68	-7.31	-0.01
146	SLE RA 13	-196	-1	1703	0.57	-7.46	-0.01
146	SLE RA 14	-188	-1	1695	0.84	-7.07	-0.01
146	SLE RA 15	-193	-1	1700	0.68	-7.31	-0.01
146	SLE RA 16	-188	-1	1695	0.84	-7.07	-0.01
146	SLE RA 17	-193	-1	1700	0.68	-7.31	-0.01
146	SLE RA 18	-206	-1	1777	0.93	-7.74	-0.01
146	SLE RA 19	-211	-1	1781	0.77	-7.97	-0.01
146	SLE RA 20	-206	-1	1777	0.93	-7.74	-0.01
146	SLE RA 21	-211	-1	1781	0.77	-7.97	-0.01
146	SLE FR 1	-146	-1	1506	0.64	-5.52	0
146	SLE FR 2	-148	-1	1507	0.58	-5.6	0
146	SLE FR 3	-146	-1	1506	0.64	-5.52	0
146	SLE FR 4	-166	-1	1588	0.67	-6.26	-0.01
146	SLE FR 5	-164	-1	1587	0.72	-6.19	-0.01
146	SLE FR 6	-176	-1	1641	0.78	-6.63	-0.01
146	SLE QP 1	-146	-1	1506	0.64	-5.52	0
146	SLE QP 2	-164	-1	1587	0.72	-6.19	-0.01
146	SLD 1	-21	6	1481	-2.7	0.11	-0.02
146	SLD 2	-21	6	1481	-2.7	0.11	-0.02
146	SLD 3	-44	11	1538	-5.49	-0.89	-0.01
146	SLD 4	-44	11	1538	-5.49	-0.89	-0.01
146	SLD 5	-85	-6	1470	3.93	-2.79	-0.02
146	SLD 6	-85	-6	1470	3.93	-2.79	-0.02
146	SLD 7	-164	10	1658	-5.37	-6.1	0.01
146	SLD 8	-164	10	1658	-5.37	-6.1	0.01
146	SLD 9	-164	-12	1516	6.82	-6.27	-0.02
146	SLD 10	-164	-12	1516	6.82	-6.27	-0.02
146	SLD 11	-243	4	1704	-2.48	-9.58	0.01
146	SLD 12	-243	4	1704	-2.48	-9.58	0.01
146	SLD 13	-284	-13	1636	6.94	-11.48	0
146	SLD 14	-284	-13	1636	6.94	-11.48	0
146	SLD 15	-307	-8	1693	4.15	-12.48	0.01
146	SLD 16	-307	-8	1693	4.15	-12.48	0.01
146	SLV 1	174	21	1338	-8.21	8.69	-0.04
146	SLV 2	174	21	1338	-8.21	8.69	-0.04
146	SLV 3	119	32	1472	-14.92	6.38	-0.02
146	SLV 4	119	32	1472	-14.92	6.38	-0.02
146	SLV 5	21	-12	1308	8.22	1.78	-0.05
146	SLV 6	21	-12	1308	8.22	1.78	-0.05
146	SLV 7	-163	27	1756	-14.14	-5.92	0.02
146	SLV 8	-163	27	1756	-14.14	-5.92	0.02
146	SLV 9	-165	-29	1418	15.59	-6.45	-0.03
146	SLV 10	-165	-29	1418	15.59	-6.45	-0.03
146	SLV 11	-349	11	1865	-6.77	-14.15	0.04
146	SLV 12	-349	11	1865	-6.77	-14.15	0.04
146	SLV 13	-447	-34	1702	16.36	-18.75	0.01
146	SLV 14	-447	-34	1702	16.36	-18.75	0.01
146	SLV 15	-502	-22	1836	9.66	-21.07	0.03
146	SLV 16	-502	-22	1836	9.66	-21.07	0.03
147	SLU 1	-152	0	1371	0.29	-6.3	0
147	SLU 2	-166	0	1383	-0.48	-6.87	0
147	SLU 3	-152	0	1371	0.29	-6.3	0
147	SLU 4	-160	0	1378	-0.18	-6.64	0
147	SLU 5	-166	0	1383	-0.48	-6.87	0
147	SLU 6	-152	0	1371	0.29	-6.3	0
147	SLU 7	-160	0	1378	-0.18	-6.64	0
147	SLU 8	-152	0	1371	0.29	-6.3	0
147	SLU 9	-160	0	1378	-0.18	-6.64	0
147	SLU 10	-235	0	1621	-0.35	-9.74	0
147	SLU 11	-221	0	1610	0.42	-9.17	0
147	SLU 12	-229	0	1617	-0.04	-9.51	0
147	SLU 13	-235	0	1621	-0.35	-9.74	0
147	SLU 14	-221	0	1610	0.42	-9.17	0
147	SLU 15	-229	0	1617	-0.04	-9.51	0
147	SLU 16	-221	0	1610	0.42	-9.17	0
147	SLU 17	-229	0	1617	-0.04	-9.51	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
147	SLU 18	-251	0	1712	0.48	-10.4	0
147	SLU 19	-259	0	1719	0.02	-10.74	0
147	SLU 20	-251	0	1712	0.48	-10.4	0
147	SLU 21	-259	0	1719	0.02	-10.74	0
147	SLU 22	-185	0	1485	0.37	-7.66	0
147	SLU 23	-199	0	1496	-0.41	-8.23	0
147	SLU 24	-185	0	1485	0.37	-7.66	0
147	SLU 25	-193	0	1491	-0.1	-8	0
147	SLU 26	-199	0	1496	-0.41	-8.23	0
147	SLU 27	-185	0	1485	0.37	-7.66	0
147	SLU 28	-193	0	1491	-0.1	-8	0
147	SLU 29	-185	0	1485	0.37	-7.66	0
147	SLU 30	-193	0	1491	-0.1	-8	0
147	SLU 31	-268	0	1734	-0.27	-11.1	0
147	SLU 32	-254	0	1723	0.5	-10.53	0
147	SLU 33	-262	0	1730	0.04	-10.87	0
147	SLU 34	-268	0	1734	-0.27	-11.1	0
147	SLU 35	-254	0	1723	0.5	-10.53	0
147	SLU 36	-262	0	1730	0.04	-10.87	0
147	SLU 37	-254	0	1723	0.5	-10.53	0
147	SLU 38	-262	0	1730	0.04	-10.87	0
147	SLU 39	-284	0	1825	0.56	-11.76	0
147	SLU 40	-292	0	1832	0.1	-12.1	0
147	SLU 41	-284	0	1825	0.56	-11.76	0
147	SLU 42	-292	0	1832	0.1	-12.1	0
147	SLU 43	-187	0	1744	0.35	-7.73	0
147	SLU 44	-200	0	1755	-0.43	-8.3	0
147	SLU 45	-187	0	1744	0.35	-7.73	0
147	SLU 46	-195	0	1751	-0.12	-8.07	0
147	SLU 47	-200	0	1755	-0.43	-8.3	0
147	SLU 48	-187	0	1744	0.35	-7.73	0
147	SLU 49	-195	0	1751	-0.12	-8.07	0
147	SLU 50	-187	0	1744	0.35	-7.73	0
147	SLU 51	-195	0	1751	-0.12	-8.07	0
147	SLU 52	-269	0	1994	-0.29	-11.16	0
147	SLU 53	-256	0	1982	0.48	-10.59	0
147	SLU 54	-264	0	1989	0.02	-10.93	0
147	SLU 55	-269	0	1994	-0.29	-11.16	0
147	SLU 56	-256	0	1982	0.48	-10.59	0
147	SLU 57	-264	0	1989	0.02	-10.93	0
147	SLU 58	-256	0	1982	0.48	-10.59	0
147	SLU 59	-264	0	1989	0.02	-10.93	0
147	SLU 60	-285	0	2085	0.54	-11.82	0
147	SLU 61	-293	0	2091	0.08	-12.16	0
147	SLU 62	-285	0	2085	0.54	-11.82	0
147	SLU 63	-293	0	2091	0.08	-12.16	0
147	SLU 64	-220	0	1857	0.43	-9.09	0
147	SLU 65	-233	0	1869	-0.35	-9.66	0
147	SLU 66	-220	0	1857	0.43	-9.09	0
147	SLU 67	-228	0	1864	-0.04	-9.43	0
147	SLU 68	-233	0	1869	-0.35	-9.66	0
147	SLU 69	-220	0	1857	0.43	-9.09	0
147	SLU 70	-228	0	1864	-0.04	-9.43	0
147	SLU 71	-220	0	1857	0.43	-9.09	0
147	SLU 72	-228	0	1864	-0.04	-9.43	0
147	SLU 73	-302	0	2107	-0.21	-12.52	0
147	SLU 74	-289	0	2096	0.56	-11.95	0
147	SLU 75	-297	0	2102	0.1	-12.29	0
147	SLU 76	-302	0	2107	-0.21	-12.52	0
147	SLU 77	-289	0	2096	0.56	-11.95	0
147	SLU 78	-297	0	2102	0.1	-12.29	0
147	SLU 79	-289	0	2096	0.56	-11.95	0
147	SLU 80	-297	0	2102	0.1	-12.29	0
147	SLU 81	-318	0	2198	0.62	-13.18	0
147	SLU 82	-326	0	2205	0.16	-13.52	0
147	SLU 83	-318	0	2198	0.62	-13.18	0
147	SLU 84	-326	0	2205	0.16	-13.52	0
147	SLE RA 1	-162	0	1404	0.31	-6.69	0
147	SLE RA 2	-171	0	1411	-0.2	-7.07	0
147	SLE RA 3	-162	0	1404	0.31	-6.69	0
147	SLE RA 4	-167	0	1408	0	-6.92	0
147	SLE RA 5	-171	0	1411	-0.2	-7.07	0
147	SLE RA 6	-162	0	1404	0.31	-6.69	0
147	SLE RA 7	-167	0	1408	0	-6.92	0
147	SLE RA 8	-162	0	1404	0.31	-6.69	0
147	SLE RA 9	-167	0	1408	0	-6.92	0
147	SLE RA 10	-217	0	1570	-0.11	-8.98	0
147	SLE RA 11	-208	0	1563	0.4	-8.6	0
147	SLE RA 12	-213	0	1567	0.09	-8.83	0
147	SLE RA 13	-217	0	1570	-0.11	-8.98	0
147	SLE RA 14	-208	0	1563	0.4	-8.6	0
147	SLE RA 15	-213	0	1567	0.09	-8.83	0
147	SLE RA 16	-208	0	1563	0.4	-8.6	0
147	SLE RA 17	-213	0	1567	0.09	-8.83	0
147	SLE RA 18	-227	0	1631	0.44	-9.42	0
147	SLE RA 19	-233	0	1635	0.13	-9.65	0
147	SLE RA 20	-227	0	1631	0.44	-9.42	0
147	SLE RA 21	-233	0	1635	0.13	-9.65	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
147	SLE FR 1	-162	0	1404	0.31	-6.69	0
147	SLE FR 2	-163	0	1405	0.21	-6.77	0
147	SLE FR 3	-162	0	1404	0.31	-6.69	0
147	SLE FR 4	-183	0	1473	0.25	-7.59	0
147	SLE FR 5	-181	0	1472	0.35	-7.51	0
147	SLE FR 6	-195	0	1517	0.38	-8.06	0
147	SLE QP 1	-162	0	1404	0.31	-6.69	0
147	SLE QP 2	-181	0	1472	0.35	-7.51	0
147	SLD 1	-31	7	1371	-3.35	-1.03	0
147	SLD 2	-31	7	1371	-3.35	-1.03	0
147	SLD 3	-56	11	1414	-8.83	-2.09	-0.01
147	SLD 4	-56	11	1414	-8.83	-2.09	-0.01
147	SLD 5	-99	-5	1376	7.54	-3.97	0.01
147	SLD 6	-99	-5	1376	7.54	-3.97	0.01
147	SLD 7	-181	10	1520	-10.7	-7.48	-0.02
147	SLD 8	-181	10	1520	-10.7	-7.48	-0.02
147	SLD 9	-182	-10	1423	11.4	-7.54	0.01
147	SLD 10	-182	-10	1423	11.4	-7.54	0.01
147	SLD 11	-264	4	1568	-6.84	-11.05	-0.01
147	SLD 12	-264	4	1568	-6.84	-11.05	-0.01
147	SLD 13	-307	-11	1530	9.53	-12.93	0.01
147	SLD 14	-307	-11	1530	9.53	-12.93	0.01
147	SLD 15	-332	-7	1573	4.05	-13.99	0
147	SLD 16	-332	-7	1573	4.05	-13.99	0
147	SLV 1	173	19	1233	-9.02	7.74	-0.01
147	SLV 2	173	19	1233	-9.02	7.74	-0.01
147	SLV 3	115	29	1336	-22.02	5.29	-0.03
147	SLV 4	115	29	1336	-22.02	5.29	-0.03
147	SLV 5	12	-10	1244	17.27	0.79	0.02
147	SLV 6	12	-10	1244	17.27	0.79	0.02
147	SLV 7	-180	24	1588	-26.09	-7.39	-0.04
147	SLV 8	-180	24	1588	-26.09	-7.39	-0.04
147	SLV 9	-183	-25	1356	26.79	-7.63	0.03
147	SLV 10	-183	-25	1356	26.79	-7.63	0.03
147	SLV 11	-375	10	1700	-16.57	-15.81	-0.03
147	SLV 12	-375	10	1700	-16.57	-15.81	-0.03
147	SLV 13	-478	-30	1607	22.72	-20.31	0.03
147	SLV 14	-478	-30	1607	22.72	-20.31	0.03
147	SLV 15	-535	-19	1710	9.71	-22.76	0.01
147	SLV 16	-535	-19	1710	9.71	-22.76	0.01
148	SLU 1	-146	0	1291	0.16	-5.93	0
148	SLU 2	-162	1	1301	-0.98	-6.63	0
148	SLU 3	-146	0	1291	0.16	-5.93	0
148	SLU 4	-155	0	1297	-0.52	-6.35	0
148	SLU 5	-162	1	1301	-0.98	-6.63	0
148	SLU 6	-146	0	1291	0.16	-5.93	0
148	SLU 7	-155	0	1297	-0.52	-6.35	0
148	SLU 8	-146	0	1291	0.16	-5.93	0
148	SLU 9	-155	0	1297	-0.52	-6.35	0
148	SLU 10	-229	1	1500	-0.92	-9.32	0
148	SLU 11	-213	0	1490	0.21	-8.62	0
148	SLU 12	-223	0	1496	-0.47	-9.04	0
148	SLU 13	-229	1	1500	-0.92	-9.32	0
148	SLU 14	-213	0	1490	0.21	-8.62	0
148	SLU 15	-223	0	1496	-0.47	-9.04	0
148	SLU 16	-213	0	1490	0.21	-8.62	0
148	SLU 17	-223	0	1496	-0.47	-9.04	0
148	SLU 18	-242	0	1576	0.24	-9.78	0
148	SLU 19	-251	0	1582	-0.45	-10.19	0
148	SLU 20	-242	0	1576	0.24	-9.78	0
148	SLU 21	-251	0	1582	-0.45	-10.19	0
148	SLU 22	-177	0	1384	0.2	-7.17	0
148	SLU 23	-193	1	1394	-0.94	-7.86	0
148	SLU 24	-177	0	1384	0.2	-7.17	0
148	SLU 25	-186	0	1390	-0.49	-7.59	0
148	SLU 26	-193	1	1394	-0.94	-7.86	0
148	SLU 27	-177	0	1384	0.2	-7.17	0
148	SLU 28	-186	0	1390	-0.49	-7.59	0
148	SLU 29	-177	0	1384	0.2	-7.17	0
148	SLU 30	-186	0	1390	-0.49	-7.59	0
148	SLU 31	-260	1	1593	-0.89	-10.56	0
148	SLU 32	-244	0	1584	0.25	-9.86	0
148	SLU 33	-254	0	1590	-0.43	-10.28	0
148	SLU 34	-260	1	1593	-0.89	-10.56	0
148	SLU 35	-244	0	1584	0.25	-9.86	0
148	SLU 36	-254	0	1590	-0.43	-10.28	0
148	SLU 37	-244	0	1584	0.25	-9.86	0
148	SLU 38	-254	0	1590	-0.43	-10.28	0
148	SLU 39	-273	0	1669	0.27	-11.01	0
148	SLU 40	-283	0	1675	-0.41	-11.43	0
148	SLU 41	-273	0	1669	0.27	-11.01	0
148	SLU 42	-283	0	1675	-0.41	-11.43	0
148	SLU 43	-179	0	1646	0.2	-7.28	0
148	SLU 44	-195	1	1656	-0.94	-7.98	0
148	SLU 45	-179	0	1646	0.2	-7.28	0
148	SLU 46	-188	0	1652	-0.49	-7.7	0
148	SLU 47	-195	1	1656	-0.94	-7.98	0
148	SLU 48	-179	0	1646	0.2	-7.28	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione				Reazione a rotazione		
		x	y	z		x	y	z
148	SLU 49	-188	0	1652		-0.49	-7.7	0
148	SLU 50	-179	0	1646		0.2	-7.28	0
148	SLU 51	-188	0	1652		-0.49	-7.7	0
148	SLU 52	-262	1	1855		-0.89	-10.67	0
148	SLU 53	-246	0	1846		0.25	-9.98	0
148	SLU 54	-256	0	1851		-0.43	-10.39	0
148	SLU 55	-262	1	1855		-0.89	-10.67	0
148	SLU 56	-246	0	1846		0.25	-9.98	0
148	SLU 57	-256	0	1851		-0.43	-10.39	0
148	SLU 58	-246	0	1846		0.25	-9.98	0
148	SLU 59	-256	0	1851		-0.43	-10.39	0
148	SLU 60	-275	0	1931		0.27	-11.13	0
148	SLU 61	-285	0	1937		-0.41	-11.55	0
148	SLU 62	-275	0	1931		0.27	-11.13	0
148	SLU 63	-285	0	1937		-0.41	-11.55	0
148	SLU 64	-210	0	1740		0.23	-8.52	0
148	SLU 65	-226	1	1749		-0.91	-9.22	0
148	SLU 66	-210	0	1740		0.23	-8.52	0
148	SLU 67	-220	0	1746		-0.45	-8.94	0
148	SLU 68	-226	1	1749		-0.91	-9.22	0
148	SLU 69	-210	0	1740		0.23	-8.52	0
148	SLU 70	-220	0	1746		-0.45	-8.94	0
148	SLU 71	-210	0	1740		0.23	-8.52	0
148	SLU 72	-220	0	1746		-0.45	-8.94	0
148	SLU 73	-293	1	1949		-0.85	-11.91	0
148	SLU 74	-277	0	1939		0.28	-11.21	0
148	SLU 75	-287	0	1945		-0.4	-11.63	0
148	SLU 76	-293	1	1949		-0.85	-11.91	0
148	SLU 77	-277	0	1939		0.28	-11.21	0
148	SLU 78	-287	0	1945		-0.4	-11.63	0
148	SLU 79	-277	0	1939		0.28	-11.21	0
148	SLU 80	-287	0	1945		-0.4	-11.63	0
148	SLU 81	-306	0	2024		0.31	-12.37	0
148	SLU 82	-316	0	2030		-0.38	-12.79	0
148	SLU 83	-306	0	2024		0.31	-12.37	0
148	SLU 84	-316	0	2030		-0.38	-12.79	0
148	SLE RA 1	-155	0	1318		0.17	-6.28	0
148	SLE RA 2	-165	0	1324		-0.59	-6.75	0
148	SLE RA 3	-155	0	1318		0.17	-6.28	0
148	SLE RA 4	-161	0	1322		-0.28	-6.56	0
148	SLE RA 5	-165	0	1324		-0.59	-6.75	0
148	SLE RA 6	-155	0	1318		0.17	-6.28	0
148	SLE RA 7	-161	0	1322		-0.28	-6.56	0
148	SLE RA 8	-155	0	1318		0.17	-6.28	0
148	SLE RA 9	-161	0	1322		-0.28	-6.56	0
148	SLE RA 10	-210	0	1457		-0.55	-8.54	0
148	SLE RA 11	-200	0	1451		0.21	-8.08	0
148	SLE RA 12	-206	0	1454		-0.25	-8.36	0
148	SLE RA 13	-210	0	1457		-0.55	-8.54	0
148	SLE RA 14	-200	0	1451		0.21	-8.08	0
148	SLE RA 15	-206	0	1454		-0.25	-8.36	0
148	SLE RA 16	-200	0	1451		0.21	-8.08	0
148	SLE RA 17	-206	0	1454		-0.25	-8.36	0
148	SLE RA 18	-219	0	1508		0.22	-8.85	0
148	SLE RA 19	-225	0	1511		-0.23	-9.13	0
148	SLE RA 20	-219	0	1508		0.22	-8.85	0
148	SLE RA 21	-225	0	1511		-0.23	-9.13	0
148	SLE FR 1	-155	0	1318		0.17	-6.28	0
148	SLE FR 2	-157	0	1319		0.02	-6.38	0
148	SLE FR 3	-155	0	1318		0.17	-6.28	0
148	SLE FR 4	-176	0	1376		0.03	-7.15	0
148	SLE FR 5	-174	0	1375		0.19	-7.05	0
148	SLE FR 6	-187	0	1413		0.2	-7.57	0
148	SLE QP 1	-155	0	1318		0.17	-6.28	0
148	SLE QP 2	-174	0	1375		0.19	-7.05	0
148	SLD 1	-13	5	1292		4.13	0.01	-0.01
148	SLD 2	-13	5	1292		4.13	0.01	-0.01
148	SLD 3	-39	12	1327		12.68	-1.16	-0.02
148	SLD 4	-39	12	1327		12.68	-1.16	-0.02
148	SLD 5	-85	-10	1297		-11.6	-3.15	0.02
148	SLD 6	-85	-10	1297		-11.6	-3.15	0.02
148	SLD 7	-175	15	1413		16.9	-7.07	-0.03
148	SLD 8	-175	15	1413		16.9	-7.07	-0.03
148	SLD 9	-173	-16	1336		-16.53	-7.04	0.03
148	SLD 10	-173	-16	1336		-16.53	-7.04	0.03
148	SLD 11	-263	10	1452		11.97	-10.96	-0.02
148	SLD 12	-263	10	1452		11.97	-10.96	-0.02
148	SLD 13	-309	-12	1423		-12.31	-12.94	0.02
148	SLD 14	-309	-12	1423		-12.31	-12.94	0.02
148	SLD 15	-336	-5	1457		-3.76	-14.12	0
148	SLD 16	-336	-5	1457		-3.76	-14.12	0
148	SLV 1	208	12	1179		10.31	9.66	-0.01
148	SLV 2	208	12	1179		10.31	9.66	-0.01
148	SLV 3	145	30	1262		30.54	6.92	-0.05
148	SLV 4	145	30	1262		30.54	6.92	-0.05
148	SLV 5	36	-24	1190		-27.46	2.11	0.06
148	SLV 6	36	-24	1190		-27.46	2.11	0.06
148	SLV 7	-174	37	1467		39.97	-7.01	-0.08



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
148	SLV 8	-174	37	1467	39.97	-7.01	-0.08
148	SLV 9	-174	-37	1283	-39.6	-7.09	0.07
148	SLV 10	-174	-37	1283	-39.6	-7.09	0.07
148	SLV 11	-384	24	1559	27.83	-16.22	-0.06
148	SLV 12	-384	24	1559	27.83	-16.22	-0.06
148	SLV 13	-493	-30	1487	-30.17	-21.03	0.05
148	SLV 14	-493	-30	1487	-30.17	-21.03	0.05
148	SLV 15	-556	-12	1570	-9.94	-23.76	0.01
148	SLV 16	-556	-12	1570	-9.94	-23.76	0.01
149	SLU 1	-124	0	1239	0.09	-5.29	0
149	SLU 2	-140	1	1245	-1.35	-5.95	0
149	SLU 3	-124	0	1239	0.09	-5.29	0
149	SLU 4	-134	1	1243	-0.77	-5.69	0
149	SLU 5	-140	1	1245	-1.35	-5.95	0
149	SLU 6	-124	0	1239	0.09	-5.29	0
149	SLU 7	-134	1	1243	-0.77	-5.69	0
149	SLU 8	-124	0	1239	0.09	-5.29	0
149	SLU 9	-134	1	1243	-0.77	-5.69	0
149	SLU 10	-201	1	1415	-1.35	-8.53	0
149	SLU 11	-185	0	1408	0.1	-7.87	0
149	SLU 12	-195	1	1413	-0.77	-8.27	0
149	SLU 13	-201	1	1415	-1.35	-8.53	0
149	SLU 14	-185	0	1408	0.1	-7.87	0
149	SLU 15	-195	1	1413	-0.77	-8.27	0
149	SLU 16	-185	0	1408	0.1	-7.87	0
149	SLU 17	-195	1	1413	-0.77	-8.27	0
149	SLU 18	-211	0	1481	0.1	-8.98	0
149	SLU 19	-221	1	1485	-0.76	-9.37	0
149	SLU 20	-211	0	1481	0.1	-8.98	0
149	SLU 21	-221	1	1485	-0.76	-9.37	0
149	SLU 22	-152	0	1318	0.1	-6.45	0
149	SLU 23	-168	1	1324	-1.34	-7.11	0
149	SLU 24	-152	0	1318	0.1	-6.45	0
149	SLU 25	-161	1	1322	-0.76	-6.84	0
149	SLU 26	-168	1	1324	-1.34	-7.11	0
149	SLU 27	-152	0	1318	0.1	-6.45	0
149	SLU 28	-161	1	1322	-0.76	-6.84	0
149	SLU 29	-152	0	1318	0.1	-6.45	0
149	SLU 30	-161	1	1322	-0.76	-6.84	0
149	SLU 31	-228	1	1494	-1.34	-9.69	0
149	SLU 32	-212	0	1488	0.11	-9.03	0
149	SLU 33	-222	1	1492	-0.76	-9.43	0
149	SLU 34	-228	1	1494	-1.34	-9.69	0
149	SLU 35	-212	0	1488	0.11	-9.03	0
149	SLU 36	-222	1	1492	-0.76	-9.43	0
149	SLU 37	-212	0	1488	0.11	-9.03	0
149	SLU 38	-222	1	1492	-0.76	-9.43	0
149	SLU 39	-238	0	1560	0.11	-10.13	0
149	SLU 40	-248	1	1564	-0.75	-10.53	0
149	SLU 41	-238	0	1560	0.11	-10.13	0
149	SLU 42	-248	1	1564	-0.75	-10.53	0
149	SLU 43	-152	0	1583	0.12	-6.48	0
149	SLU 44	-168	1	1590	-1.33	-7.14	0
149	SLU 45	-152	0	1583	0.12	-6.48	0
149	SLU 46	-162	1	1587	-0.75	-6.88	0
149	SLU 47	-168	1	1590	-1.33	-7.14	0
149	SLU 48	-152	0	1583	0.12	-6.48	0
149	SLU 49	-162	1	1587	-0.75	-6.88	0
149	SLU 50	-152	0	1583	0.12	-6.48	0
149	SLU 51	-162	1	1587	-0.75	-6.88	0
149	SLU 52	-229	1	1760	-1.32	-9.72	0
149	SLU 53	-213	0	1753	0.12	-9.06	0
149	SLU 54	-223	1	1757	-0.74	-9.46	0
149	SLU 55	-229	1	1760	-1.32	-9.72	0
149	SLU 56	-213	0	1753	0.12	-9.06	0
149	SLU 57	-223	1	1757	-0.74	-9.46	0
149	SLU 58	-213	0	1753	0.12	-9.06	0
149	SLU 59	-223	1	1757	-0.74	-9.46	0
149	SLU 60	-239	0	1826	0.13	-10.17	0
149	SLU 61	-249	1	1830	-0.74	-10.56	0
149	SLU 62	-239	0	1826	0.13	-10.17	0
149	SLU 63	-249	1	1830	-0.74	-10.56	0
149	SLU 64	-180	0	1662	0.13	-7.64	0
149	SLU 65	-196	1	1669	-1.32	-8.3	0
149	SLU 66	-180	0	1662	0.13	-7.64	0
149	SLU 67	-189	1	1666	-0.74	-8.03	0
149	SLU 68	-196	1	1669	-1.32	-8.3	0
149	SLU 69	-180	0	1662	0.13	-7.64	0
149	SLU 70	-189	1	1666	-0.74	-8.03	0
149	SLU 71	-180	0	1662	0.13	-7.64	0
149	SLU 72	-189	1	1666	-0.74	-8.03	0
149	SLU 73	-256	1	1839	-1.31	-10.88	0
149	SLU 74	-240	0	1832	0.13	-10.22	0
149	SLU 75	-250	1	1836	-0.73	-10.62	0
149	SLU 76	-256	1	1839	-1.31	-10.88	0
149	SLU 77	-240	0	1832	0.13	-10.22	0
149	SLU 78	-250	1	1836	-0.73	-10.62	0
149	SLU 79	-240	0	1832	0.13	-10.22	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
149	SLU 80	-250	1	1836	-0.73	-10.62	0
149	SLU 81	-266	0	1905	0.14	-11.33	0
149	SLU 82	-276	1	1909	-0.73	-11.72	0
149	SLU 83	-266	0	1905	0.14	-11.33	0
149	SLU 84	-276	1	1909	-0.73	-11.72	0
149	SLE RA 1	-132	0	1261	0.1	-5.62	0
149	SLE RA 2	-143	1	1266	-0.87	-6.06	0
149	SLE RA 3	-132	0	1261	0.1	-5.62	0
149	SLE RA 4	-139	0	1264	-0.48	-5.89	0
149	SLE RA 5	-143	1	1266	-0.87	-6.06	0
149	SLE RA 6	-132	0	1261	0.1	-5.62	0
149	SLE RA 7	-139	0	1264	-0.48	-5.89	0
149	SLE RA 8	-132	0	1261	0.1	-5.62	0
149	SLE RA 9	-139	0	1264	-0.48	-5.89	0
149	SLE RA 10	-183	1	1379	-0.86	-7.78	0
149	SLE RA 11	-173	0	1374	0.1	-7.34	0
149	SLE RA 12	-179	0	1377	-0.48	-7.61	0
149	SLE RA 13	-183	1	1379	-0.86	-7.78	0
149	SLE RA 14	-173	0	1374	0.1	-7.34	0
149	SLE RA 15	-179	0	1377	-0.48	-7.61	0
149	SLE RA 16	-173	0	1374	0.1	-7.34	0
149	SLE RA 17	-179	0	1377	-0.48	-7.61	0
149	SLE RA 18	-190	0	1423	0.1	-8.08	0
149	SLE RA 19	-196	0	1426	-0.48	-8.34	0
149	SLE RA 20	-190	0	1423	0.1	-8.08	0
149	SLE RA 21	-196	0	1426	-0.48	-8.34	0
149	SLE FR 1	-132	0	1261	0.1	-5.62	0
149	SLE FR 2	-134	0	1262	-0.1	-5.71	0
149	SLE FR 3	-132	0	1261	0.1	-5.62	0
149	SLE FR 4	-152	0	1311	-0.09	-6.45	0
149	SLE FR 5	-150	0	1310	0.1	-6.36	0
149	SLE FR 6	-161	0	1342	0.1	-6.85	0
149	SLE QP 1	-132	0	1261	0.1	-5.62	0
149	SLE QP 2	-150	0	1310	0.1	-6.36	0
149	SLD 1	18	-15	1254	4.69	0.82	-0.01
149	SLD 2	18	-15	1254	4.69	0.82	-0.01
149	SLD 3	-11	-3	1284	16	-0.4	-0.05
149	SLD 4	-11	-3	1284	16	-0.4	-0.05
149	SLD 5	-56	-22	1248	-15.67	-2.36	0.06
149	SLD 6	-56	-22	1248	-15.67	-2.36	0.06
149	SLD 7	-152	17	1347	22.01	-6.42	-0.07
149	SLD 8	-152	17	1347	22.01	-6.42	-0.07
149	SLD 9	-147	-17	1273	-21.82	-6.3	0.07
149	SLD 10	-147	-17	1273	-21.82	-6.3	0.07
149	SLD 11	-243	22	1371	15.86	-10.36	-0.06
149	SLD 12	-243	22	1371	15.86	-10.36	-0.06
149	SLD 13	-288	3	1335	-15.8	-12.31	0.05
149	SLD 14	-288	3	1335	-15.8	-12.31	0.05
149	SLD 15	-317	15	1365	-4.5	-13.53	0.01
149	SLD 16	-317	15	1365	-4.5	-13.53	0.01
149	SLV 1	245	-36	1178	12.51	10.55	-0.02
149	SLV 2	245	-36	1178	12.51	10.55	-0.02
149	SLV 3	178	-9	1249	39.23	7.71	-0.12
149	SLV 4	178	-9	1249	39.23	7.71	-0.12
149	SLV 5	71	-53	1163	-36.7	3.02	0.13
149	SLV 6	71	-53	1163	-36.7	3.02	0.13
149	SLV 7	-153	39	1398	52.36	-6.44	-0.18
149	SLV 8	-153	39	1398	52.36	-6.44	-0.18
149	SLV 9	-146	-39	1221	-52.16	-6.27	0.18
149	SLV 10	-146	-39	1221	-52.16	-6.27	0.18
149	SLV 11	-370	53	1456	36.9	-15.74	-0.13
149	SLV 12	-370	53	1456	36.9	-15.74	-0.13
149	SLV 13	-477	9	1370	-39.03	-20.43	0.12
149	SLV 14	-477	9	1370	-39.03	-20.43	0.12
149	SLV 15	-545	36	1441	-12.31	-23.27	0.02
149	SLV 16	-545	36	1441	-12.31	-23.27	0.02
150	SLU 1	-92	0	1223	0.06	-4.11	0
150	SLU 2	-108	1	1227	-1.61	-4.81	0.01
150	SLU 3	-92	0	1223	0.06	-4.11	0
150	SLU 4	-102	1	1225	-0.94	-4.53	0
150	SLU 5	-108	1	1227	-1.61	-4.81	0.01
150	SLU 6	-92	0	1223	0.06	-4.11	0
150	SLU 7	-102	1	1225	-0.94	-4.53	0
150	SLU 8	-92	0	1223	0.06	-4.11	0
150	SLU 9	-102	1	1225	-0.94	-4.53	0
150	SLU 10	-155	1	1381	-1.63	-6.82	0.01
150	SLU 11	-140	0	1377	0.03	-6.11	0
150	SLU 12	-149	1	1379	-0.97	-6.54	0
150	SLU 13	-155	1	1381	-1.63	-6.82	0.01
150	SLU 14	-140	0	1377	0.03	-6.11	0
150	SLU 15	-149	1	1379	-0.97	-6.54	0
150	SLU 16	-140	0	1377	0.03	-6.11	0
150	SLU 17	-149	1	1379	-0.97	-6.54	0
150	SLU 18	-160	0	1443	0.02	-6.98	0
150	SLU 19	-169	1	1445	-0.98	-7.4	0
150	SLU 20	-160	0	1443	0.02	-6.98	0
150	SLU 21	-169	1	1445	-0.98	-7.4	0
150	SLU 22	-113	0	1295	0.05	-4.97	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
150	SLU 23	-129	1	1298	-1.62	-5.67	0.01
150	SLU 24	-113	0	1295	0.05	-4.97	0
150	SLU 25	-122	1	1297	-0.95	-5.39	0
150	SLU 26	-129	1	1298	-1.62	-5.67	0.01
150	SLU 27	-113	0	1295	0.05	-4.97	0
150	SLU 28	-122	1	1297	-0.95	-5.39	0
150	SLU 29	-113	0	1295	0.05	-4.97	0
150	SLU 30	-122	1	1297	-0.95	-5.39	0
150	SLU 31	-176	1	1452	-1.64	-7.68	0.01
150	SLU 32	-160	0	1449	0.03	-6.98	0
150	SLU 33	-170	1	1451	-0.97	-7.4	0
150	SLU 34	-176	1	1452	-1.64	-7.68	0.01
150	SLU 35	-160	0	1449	0.03	-6.98	0
150	SLU 36	-170	1	1451	-0.97	-7.4	0
150	SLU 37	-160	0	1449	0.03	-6.98	0
150	SLU 38	-170	1	1451	-0.97	-7.4	0
150	SLU 39	-180	0	1515	0.02	-7.84	0
150	SLU 40	-190	1	1517	-0.98	-8.26	0
150	SLU 41	-180	0	1515	0.02	-7.84	0
150	SLU 42	-190	1	1517	-0.98	-8.26	0
150	SLU 43	-113	0	1566	0.08	-5.04	0
150	SLU 44	-129	1	1569	-1.59	-5.75	0.01
150	SLU 45	-113	0	1566	0.08	-5.04	0
150	SLU 46	-122	1	1568	-0.92	-5.46	0
150	SLU 47	-129	1	1569	-1.59	-5.75	0.01
150	SLU 48	-113	0	1566	0.08	-5.04	0
150	SLU 49	-122	1	1568	-0.92	-5.46	0
150	SLU 50	-113	0	1566	0.08	-5.04	0
150	SLU 51	-122	1	1568	-0.92	-5.46	0
150	SLU 52	-176	1	1723	-1.62	-7.75	0.01
150	SLU 53	-160	0	1720	0.05	-7.05	0
150	SLU 54	-170	1	1722	-0.95	-7.47	0
150	SLU 55	-176	1	1723	-1.62	-7.75	0.01
150	SLU 56	-160	0	1720	0.05	-7.05	0
150	SLU 57	-170	1	1722	-0.95	-7.47	0
150	SLU 58	-160	0	1720	0.05	-7.05	0
150	SLU 59	-170	1	1722	-0.95	-7.47	0
150	SLU 60	-180	0	1786	0.04	-7.91	0
150	SLU 61	-190	1	1788	-0.96	-8.33	0
150	SLU 62	-180	0	1786	0.04	-7.91	0
150	SLU 63	-190	1	1788	-0.96	-8.33	0
150	SLU 64	-133	0	1637	0.07	-5.91	0
150	SLU 65	-149	1	1641	-1.6	-6.61	0.01
150	SLU 66	-133	0	1637	0.07	-5.91	0
150	SLU 67	-143	1	1639	-0.93	-6.33	0
150	SLU 68	-149	1	1641	-1.6	-6.61	0.01
150	SLU 69	-133	0	1637	0.07	-5.91	0
150	SLU 70	-143	1	1639	-0.93	-6.33	0
150	SLU 71	-133	0	1637	0.07	-5.91	0
150	SLU 72	-143	1	1639	-0.93	-6.33	0
150	SLU 73	-197	1	1795	-1.62	-8.62	0.01
150	SLU 74	-181	0	1791	0.05	-7.91	0
150	SLU 75	-190	1	1793	-0.95	-8.34	0
150	SLU 76	-197	1	1795	-1.62	-8.62	0.01
150	SLU 77	-181	0	1791	0.05	-7.91	0
150	SLU 78	-190	1	1793	-0.95	-8.34	0
150	SLU 79	-181	0	1791	0.05	-7.91	0
150	SLU 80	-190	1	1793	-0.95	-8.34	0
150	SLU 81	-201	0	1857	0.03	-8.77	0
150	SLU 82	-210	1	1859	-0.97	-9.2	0
150	SLU 83	-201	0	1857	0.03	-8.77	0
150	SLU 84	-210	1	1859	-0.97	-9.2	0
150	SLE RA 1	-98	0	1244	0.06	-4.35	0
150	SLE RA 2	-109	1	1246	-1.06	-4.82	0
150	SLE RA 3	-98	0	1244	0.06	-4.35	0
150	SLE RA 4	-104	1	1245	-0.61	-4.63	0
150	SLE RA 5	-109	1	1246	-1.06	-4.82	0
150	SLE RA 6	-98	0	1244	0.06	-4.35	0
150	SLE RA 7	-104	1	1245	-0.61	-4.63	0
150	SLE RA 8	-98	0	1244	0.06	-4.35	0
150	SLE RA 9	-104	1	1245	-0.61	-4.63	0
150	SLE RA 10	-140	1	1349	-1.07	-6.16	0
150	SLE RA 11	-130	0	1346	0.04	-5.69	0
150	SLE RA 12	-136	1	1348	-0.63	-5.97	0
150	SLE RA 13	-140	1	1349	-1.07	-6.16	0
150	SLE RA 14	-130	0	1346	0.04	-5.69	0
150	SLE RA 15	-136	1	1348	-0.63	-5.97	0
150	SLE RA 16	-130	0	1346	0.04	-5.69	0
150	SLE RA 17	-136	1	1348	-0.63	-5.97	0
150	SLE RA 18	-143	0	1390	0.03	-6.27	0
150	SLE RA 19	-149	1	1392	-0.64	-6.55	0
150	SLE RA 20	-143	0	1390	0.03	-6.27	0
150	SLE RA 21	-149	1	1392	-0.64	-6.55	0
150	SLE FR 1	-98	0	1244	0.06	-4.35	0
150	SLE FR 2	-100	0	1244	-0.17	-4.45	0
150	SLE FR 3	-98	0	1244	0.06	-4.35	0
150	SLE FR 4	-114	0	1288	-0.17	-5.02	0
150	SLE FR 5	-111	0	1288	0.05	-4.93	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
150	SLE FR 6	-121	0	1317	0.04	-5.31	0
150	SLE QP 1	-98	0	1244	0.06	-4.35	0
150	SLE QP 2	-111	0	1288	0.05	-4.93	0
150	SLD 1	57	-4	1252	5.73	2.43	-0.02
150	SLD 2	57	-4	1252	5.73	2.43	-0.02
150	SLD 3	27	-18	1281	18.96	1.15	-0.08
150	SLD 4	27	-18	1281	18.96	1.15	-0.08
150	SLD 5	-16	21	1232	-18.3	-0.78	0.09
150	SLD 6	-16	21	1232	-18.3	-0.78	0.09
150	SLD 7	-115	-27	1330	25.78	-5.04	-0.12
150	SLD 8	-115	-27	1330	25.78	-5.04	-0.12
150	SLD 9	-108	28	1245	-25.68	-4.81	0.12
150	SLD 10	-108	28	1245	-25.68	-4.81	0.12
150	SLD 11	-207	-21	1343	18.4	-9.07	-0.09
150	SLD 12	-207	-21	1343	18.4	-9.07	-0.09
150	SLD 13	-250	18	1294	-18.86	-11.01	0.08
150	SLD 14	-250	18	1294	-18.86	-11.01	0.08
150	SLD 15	-280	4	1323	-5.63	-12.29	0.02
150	SLD 16	-280	4	1323	-5.63	-12.29	0.02
150	SLV 1	286	-11	1202	16.02	12.46	-0.05
150	SLV 2	286	-11	1202	16.02	12.46	-0.05
150	SLV 3	217	-45	1272	47.28	9.47	-0.2
150	SLV 4	217	-45	1272	47.28	9.47	-0.2
150	SLV 5	113	49	1154	-42.59	4.81	0.21
150	SLV 6	113	49	1154	-42.59	4.81	0.21
150	SLV 7	-118	-65	1390	61.64	-5.13	-0.28
150	SLV 8	-118	-65	1390	61.64	-5.13	-0.28
150	SLV 9	-105	65	1185	-61.55	-4.72	0.28
150	SLV 10	-105	65	1185	-61.55	-4.72	0.28
150	SLV 11	-336	-49	1421	42.68	-14.67	-0.21
150	SLV 12	-336	-49	1421	42.68	-14.67	-0.21
150	SLV 13	-440	45	1303	-47.19	-19.33	0.2
150	SLV 14	-440	45	1303	-47.19	-19.33	0.2
150	SLV 15	-509	11	1374	-15.92	-22.31	0.05
150	SLV 16	-509	11	1374	-15.92	-22.31	0.05
151	SLU 1	-59	0	1252	0.04	-2.88	0
151	SLU 2	-73	2	1252	-1.74	-3.49	0.01
151	SLU 3	-59	0	1252	0.04	-2.88	0
151	SLU 4	-67	1	1252	-1.03	-3.25	0.01
151	SLU 5	-73	2	1252	-1.74	-3.49	0.01
151	SLU 6	-59	0	1252	0.04	-2.88	0
151	SLU 7	-67	1	1252	-1.03	-3.25	0.01
151	SLU 8	-59	0	1252	0.04	-2.88	0
151	SLU 9	-67	1	1252	-1.03	-3.25	0.01
151	SLU 10	-107	2	1407	-1.79	-5.07	0.01
151	SLU 11	-92	0	1406	-0.01	-4.46	0
151	SLU 12	-101	1	1406	-1.08	-4.83	0.01
151	SLU 13	-107	2	1407	-1.79	-5.07	0.01
151	SLU 14	-92	0	1406	-0.01	-4.46	0
151	SLU 15	-101	1	1406	-1.08	-4.83	0.01
151	SLU 16	-92	0	1406	-0.01	-4.46	0
151	SLU 17	-101	1	1406	-1.08	-4.83	0.01
151	SLU 18	-107	0	1473	-0.03	-5.14	0
151	SLU 19	-115	1	1473	-1.1	-5.5	0.01
151	SLU 20	-107	0	1473	-0.03	-5.14	0
151	SLU 21	-115	1	1473	-1.1	-5.5	0.01
151	SLU 22	-72	0	1323	0.02	-3.52	0
151	SLU 23	-86	2	1324	-1.76	-4.13	0.01
151	SLU 24	-72	0	1323	0.02	-3.52	0
151	SLU 25	-81	1	1324	-1.05	-3.89	0.01
151	SLU 26	-86	2	1324	-1.76	-4.13	0.01
151	SLU 27	-72	0	1323	0.02	-3.52	0
151	SLU 28	-81	1	1324	-1.05	-3.89	0.01
151	SLU 29	-72	0	1323	0.02	-3.52	0
151	SLU 30	-81	1	1324	-1.05	-3.89	0.01
151	SLU 31	-120	2	1479	-1.81	-5.71	0.01
151	SLU 32	-106	0	1478	-0.02	-5.1	0
151	SLU 33	-114	1	1478	-1.09	-5.47	0.01
151	SLU 34	-120	2	1479	-1.81	-5.71	0.01
151	SLU 35	-106	0	1478	-0.02	-5.1	0
151	SLU 36	-114	1	1478	-1.09	-5.47	0.01
151	SLU 37	-106	0	1478	-0.02	-5.1	0
151	SLU 38	-114	1	1478	-1.09	-5.47	0.01
151	SLU 39	-120	0	1544	-0.04	-5.78	0
151	SLU 40	-129	1	1545	-1.11	-6.15	0.01
151	SLU 41	-120	0	1544	-0.04	-5.78	0
151	SLU 42	-129	1	1545	-1.11	-6.15	0.01
151	SLU 43	-72	0	1602	0.06	-3.52	0
151	SLU 44	-86	2	1603	-1.73	-4.13	0.01
151	SLU 45	-72	0	1602	0.06	-3.52	0
151	SLU 46	-80	1	1603	-1.01	-3.89	0.01
151	SLU 47	-86	2	1603	-1.73	-4.13	0.01
151	SLU 48	-72	0	1602	0.06	-3.52	0
151	SLU 49	-80	1	1603	-1.01	-3.89	0.01
151	SLU 50	-72	0	1602	0.06	-3.52	0
151	SLU 51	-80	1	1603	-1.01	-3.89	0.01
151	SLU 52	-120	2	1758	-1.77	-5.71	0.01
151	SLU 53	-105	0	1757	0.01	-5.1	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
151	SLU 54	-114	1	1757	-1.06	-5.47	0.01
151	SLU 55	-120	2	1758	-1.77	-5.71	0.01
151	SLU 56	-105	0	1757	0.01	-5.1	0
151	SLU 57	-114	1	1757	-1.06	-5.47	0.01
151	SLU 58	-105	0	1757	0.01	-5.1	0
151	SLU 59	-114	1	1757	-1.06	-5.47	0.01
151	SLU 60	-120	0	1823	-0.01	-5.78	0
151	SLU 61	-128	1	1824	-1.08	-6.15	0.01
151	SLU 62	-120	0	1823	-0.01	-5.78	0
151	SLU 63	-128	1	1824	-1.08	-6.15	0.01
151	SLU 64	-85	0	1674	0.04	-4.17	0
151	SLU 65	-99	2	1675	-1.74	-4.78	0.01
151	SLU 66	-85	0	1674	0.04	-4.17	0
151	SLU 67	-94	1	1675	-1.03	-4.53	0.01
151	SLU 68	-99	2	1675	-1.74	-4.78	0.01
151	SLU 69	-85	0	1674	0.04	-4.17	0
151	SLU 70	-94	1	1675	-1.03	-4.53	0.01
151	SLU 71	-85	0	1674	0.04	-4.17	0
151	SLU 72	-94	1	1675	-1.03	-4.53	0.01
151	SLU 73	-133	2	1829	-1.79	-6.36	0.01
151	SLU 74	-119	0	1829	-0.01	-5.75	0
151	SLU 75	-127	1	1829	-1.08	-6.11	0.01
151	SLU 76	-133	2	1829	-1.79	-6.36	0.01
151	SLU 77	-119	0	1829	-0.01	-5.75	0
151	SLU 78	-127	1	1829	-1.08	-6.11	0.01
151	SLU 79	-119	0	1829	-0.01	-5.75	0
151	SLU 80	-127	1	1829	-1.08	-6.11	0.01
151	SLU 81	-133	0	1895	-0.03	-6.43	0
151	SLU 82	-142	1	1895	-1.1	-6.79	0.01
151	SLU 83	-133	0	1895	-0.03	-6.43	0
151	SLU 84	-142	1	1895	-1.1	-6.79	0.01
151	SLE RA 1	-62	0	1272	0.04	-3.06	0
151	SLE RA 2	-72	1	1272	-1.15	-3.47	0.01
151	SLE RA 3	-62	0	1272	0.04	-3.06	0
151	SLE RA 4	-68	1	1272	-0.68	-3.31	0
151	SLE RA 5	-72	1	1272	-1.15	-3.47	0.01
151	SLE RA 6	-62	0	1272	0.04	-3.06	0
151	SLE RA 7	-68	1	1272	-0.68	-3.31	0
151	SLE RA 8	-62	0	1272	0.04	-3.06	0
151	SLE RA 9	-68	1	1272	-0.68	-3.31	0
151	SLE RA 10	-94	1	1376	-1.19	-4.52	0.01
151	SLE RA 11	-85	0	1375	0	-4.12	0
151	SLE RA 12	-91	1	1375	-0.71	-4.36	0
151	SLE RA 13	-94	1	1376	-1.19	-4.52	0.01
151	SLE RA 14	-85	0	1375	0	-4.12	0
151	SLE RA 15	-91	1	1375	-0.71	-4.36	0
151	SLE RA 16	-85	0	1375	0	-4.12	0
151	SLE RA 17	-91	1	1375	-0.71	-4.36	0
151	SLE RA 18	-94	0	1419	-0.01	-4.57	0
151	SLE RA 19	-100	1	1420	-0.72	-4.81	0
151	SLE RA 20	-94	0	1419	-0.01	-4.57	0
151	SLE RA 21	-100	1	1420	-0.72	-4.81	0
151	SLE FR 1	-62	0	1272	0.04	-3.06	0
151	SLE FR 2	-64	0	1272	-0.2	-3.15	0
151	SLE FR 3	-62	0	1272	0.04	-3.06	0
151	SLE FR 4	-74	0	1316	-0.22	-3.6	0
151	SLE FR 5	-72	0	1316	0.02	-3.52	0
151	SLE FR 6	-78	0	1346	0.01	-3.82	0
151	SLE QP 1	-62	0	1272	0.04	-3.06	0
151	SLE QP 2	-72	0	1316	0.02	-3.52	0
151	SLD 1	60	-5	1331	7.12	2.24	-0.03
151	SLD 2	60	-5	1331	7.12	2.24	-0.03
151	SLD 3	89	-21	1368	21.11	3.48	-0.12
151	SLD 4	89	-21	1368	21.11	3.48	-0.12
151	SLD 5	-76	22	1266	-19.07	-3.67	0.12
151	SLD 6	-76	22	1266	-19.07	-3.67	0.12
151	SLD 7	20	-30	1386	27.57	0.46	-0.17
151	SLD 8	20	-30	1386	27.57	0.46	-0.17
151	SLD 9	-164	30	1246	-27.53	-7.49	0.17
151	SLD 10	-164	30	1246	-27.53	-7.49	0.17
151	SLD 11	-68	-22	1366	19.11	-3.37	-0.12
151	SLD 12	-68	-22	1366	19.11	-3.37	-0.12
151	SLD 13	-233	21	1265	-21.07	-10.51	0.12
151	SLD 14	-233	21	1265	-21.07	-10.51	0.12
151	SLD 15	-204	5	1301	-7.08	-9.28	0.03
151	SLD 16	-204	5	1301	-7.08	-9.28	0.03
151	SLV 1	239	-16	1351	20.27	10.09	-0.1
151	SLV 2	239	-16	1351	20.27	10.09	-0.1
151	SLV 3	307	-53	1438	53.38	12.98	-0.31
151	SLV 4	307	-53	1438	53.38	12.98	-0.31
151	SLV 5	-81	52	1196	-44.12	-3.82	0.29
151	SLV 6	-81	52	1196	-44.12	-3.82	0.29
151	SLV 7	144	-72	1484	66.25	5.82	-0.41
151	SLV 8	144	-72	1484	66.25	5.82	-0.41
151	SLV 9	-288	72	1149	-66.2	-12.85	0.41
151	SLV 10	-288	72	1149	-66.2	-12.85	0.41
151	SLV 11	-63	-51	1437	44.16	-3.21	-0.29
151	SLV 12	-63	-51	1437	44.16	-3.21	-0.29



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
151	SLV 13	-451	53	1195	-53.34	-20.01	0.31
151	SLV 14	-451	53	1195	-53.34	-20.01	0.31
151	SLV 15	-383	16	1281	-20.23	-17.12	0.1
151	SLV 16	-383	16	1281	-20.23	-17.12	0.1
152	SLU 1	-35	0	1323	0.04	-1.99	0
152	SLU 2	-47	2	1322	-1.75	-2.53	0.01
152	SLU 3	-35	0	1323	0.04	-1.99	0
152	SLU 4	-42	1	1322	-1.03	-2.32	0.01
152	SLU 5	-47	2	1322	-1.75	-2.53	0.01
152	SLU 6	-35	0	1323	0.04	-1.99	0
152	SLU 7	-42	1	1322	-1.03	-2.32	0.01
152	SLU 8	-35	0	1323	0.04	-1.99	0
152	SLU 9	-42	1	1322	-1.03	-2.32	0.01
152	SLU 10	-67	2	1494	-1.81	-3.47	0.01
152	SLU 11	-54	0	1495	-0.02	-2.93	0
152	SLU 12	-62	1	1495	-1.09	-3.25	0.01
152	SLU 13	-67	2	1494	-1.81	-3.47	0.01
152	SLU 14	-54	0	1495	-0.02	-2.93	0
152	SLU 15	-62	1	1495	-1.09	-3.25	0.01
152	SLU 16	-54	0	1495	-0.02	-2.93	0
152	SLU 17	-62	1	1495	-1.09	-3.25	0.01
152	SLU 18	-63	0	1569	-0.05	-3.33	0
152	SLU 19	-70	1	1568	-1.12	-3.65	0.01
152	SLU 20	-63	0	1569	-0.05	-3.33	0
152	SLU 21	-70	1	1568	-1.12	-3.65	0.01
152	SLU 22	-41	0	1403	0.02	-2.32	0
152	SLU 23	-54	2	1402	-1.77	-2.86	0.01
152	SLU 24	-41	0	1403	0.02	-2.32	0
152	SLU 25	-49	1	1403	-1.06	-2.64	0.01
152	SLU 26	-54	2	1402	-1.77	-2.86	0.01
152	SLU 27	-41	0	1403	0.02	-2.32	0
152	SLU 28	-49	1	1403	-1.06	-2.64	0.01
152	SLU 29	-41	0	1403	0.02	-2.32	0
152	SLU 30	-49	1	1403	-1.06	-2.64	0.01
152	SLU 31	-73	2	1575	-1.83	-3.79	0.01
152	SLU 32	-61	0	1575	-0.04	-3.26	0
152	SLU 33	-68	1	1575	-1.12	-3.58	0.01
152	SLU 34	-73	2	1575	-1.83	-3.79	0.01
152	SLU 35	-61	0	1575	-0.04	-3.26	0
152	SLU 36	-68	1	1575	-1.12	-3.58	0.01
152	SLU 37	-61	0	1575	-0.04	-3.26	0
152	SLU 38	-68	1	1575	-1.12	-3.58	0.01
152	SLU 39	-69	0	1649	-0.07	-3.66	0
152	SLU 40	-77	1	1649	-1.14	-3.98	0.01
152	SLU 41	-69	0	1649	-0.07	-3.66	0
152	SLU 42	-77	1	1649	-1.14	-3.98	0.01
152	SLU 43	-43	0	1692	0.06	-2.48	0
152	SLU 44	-55	2	1691	-1.73	-3.02	0.01
152	SLU 45	-43	0	1692	0.06	-2.48	0
152	SLU 46	-51	1	1691	-1.01	-2.8	0.01
152	SLU 47	-55	2	1691	-1.73	-3.02	0.01
152	SLU 48	-43	0	1692	0.06	-2.48	0
152	SLU 49	-51	1	1691	-1.01	-2.8	0.01
152	SLU 50	-43	0	1692	0.06	-2.48	0
152	SLU 51	-51	1	1691	-1.01	-2.8	0.01
152	SLU 52	-75	2	1863	-1.79	-3.95	0.01
152	SLU 53	-63	0	1864	0	-3.42	0
152	SLU 54	-70	1	1864	-1.07	-3.74	0.01
152	SLU 55	-75	2	1863	-1.79	-3.95	0.01
152	SLU 56	-63	0	1864	0	-3.42	0
152	SLU 57	-70	1	1864	-1.07	-3.74	0.01
152	SLU 58	-63	0	1864	0	-3.42	0
152	SLU 59	-70	1	1864	-1.07	-3.74	0.01
152	SLU 60	-71	0	1938	-0.03	-3.82	0
152	SLU 61	-78	1	1938	-1.1	-4.14	0.01
152	SLU 62	-71	0	1938	-0.03	-3.82	0
152	SLU 63	-78	1	1938	-1.1	-4.14	0.01
152	SLU 64	-50	0	1772	0.04	-2.81	0
152	SLU 65	-62	2	1771	-1.75	-3.34	0.01
152	SLU 66	-50	0	1772	0.04	-2.81	0
152	SLU 67	-57	1	1772	-1.03	-3.13	0.01
152	SLU 68	-62	2	1771	-1.75	-3.34	0.01
152	SLU 69	-50	0	1772	0.04	-2.81	0
152	SLU 70	-57	1	1772	-1.03	-3.13	0.01
152	SLU 71	-50	0	1772	0.04	-2.81	0
152	SLU 72	-57	1	1772	-1.03	-3.13	0.01
152	SLU 73	-81	2	1944	-1.81	-4.28	0.01
152	SLU 74	-69	0	1945	-0.02	-3.74	0
152	SLU 75	-76	1	1944	-1.1	-4.07	0.01
152	SLU 76	-81	2	1944	-1.81	-4.28	0.01
152	SLU 77	-69	0	1945	-0.02	-3.74	0
152	SLU 78	-76	1	1944	-1.1	-4.07	0.01
152	SLU 79	-69	0	1945	-0.02	-3.74	0
152	SLU 80	-76	1	1944	-1.1	-4.07	0.01
152	SLU 81	-77	0	2019	-0.05	-4.14	0
152	SLU 82	-85	1	2018	-1.12	-4.47	0.01
152	SLU 83	-77	0	2019	-0.05	-4.14	0
152	SLU 84	-85	1	2018	-1.12	-4.47	0.01



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
152	SLE RA 1	-37	0	1346	0.04	-2.09	0
152	SLE RA 2	-45	1	1345	-1.16	-2.45	0.01
152	SLE RA 3	-37	0	1346	0.04	-2.09	0
152	SLE RA 4	-42	1	1345	-0.68	-2.3	0
152	SLE RA 5	-45	1	1345	-1.16	-2.45	0.01
152	SLE RA 6	-37	0	1346	0.04	-2.09	0
152	SLE RA 7	-42	1	1345	-0.68	-2.3	0
152	SLE RA 8	-37	0	1346	0.04	-2.09	0
152	SLE RA 9	-42	1	1345	-0.68	-2.3	0
152	SLE RA 10	-58	1	1460	-1.2	-3.07	0.01
152	SLE RA 11	-50	0	1461	-0.01	-2.71	0
152	SLE RA 12	-55	1	1460	-0.72	-2.93	0
152	SLE RA 13	-58	1	1460	-1.2	-3.07	0.01
152	SLE RA 14	-50	0	1461	-0.01	-2.71	0
152	SLE RA 15	-55	1	1460	-0.72	-2.93	0
152	SLE RA 16	-50	0	1461	-0.01	-2.71	0
152	SLE RA 17	-55	1	1460	-0.72	-2.93	0
152	SLE RA 18	-55	0	1510	-0.02	-2.98	0
152	SLE RA 19	-60	1	1509	-0.74	-3.19	0
152	SLE RA 20	-55	0	1510	-0.02	-2.98	0
152	SLE RA 21	-60	1	1509	-0.74	-3.19	0
152	SLE FR 1	-37	0	1346	0.04	-2.09	0
152	SLE FR 2	-38	0	1346	-0.2	-2.16	0
152	SLE FR 3	-37	0	1346	0.04	-2.09	0
152	SLE FR 4	-44	0	1395	-0.22	-2.43	0
152	SLE FR 5	-42	0	1395	0.02	-2.36	0
152	SLE FR 6	-46	0	1428	0.01	-2.53	0
152	SLE QP 1	-37	0	1346	0.04	-2.09	0
152	SLE QP 2	-42	0	1395	0.02	-2.36	0
152	SLD 1	78	-8	1418	8.69	2.92	-0.06
152	SLD 2	78	-8	1418	8.69	2.92	-0.06
152	SLD 3	106	-23	1465	22.13	4.1	-0.15
152	SLD 4	106	-23	1465	22.13	4.1	-0.15
152	SLD 5	-48	20	1330	-17.76	-2.55	0.12
152	SLD 6	-48	20	1330	-17.76	-2.55	0.12
152	SLD 7	44	-30	1488	27.04	1.36	-0.18
152	SLD 8	44	-30	1488	27.04	1.36	-0.18
152	SLD 9	-129	30	1302	-27	-6.07	0.18
152	SLD 10	-129	30	1302	-27	-6.07	0.18
152	SLD 11	-37	-20	1460	17.8	-2.16	-0.12
152	SLD 12	-37	-20	1460	17.8	-2.16	-0.12
152	SLD 13	-191	23	1325	-22.1	-8.81	0.15
152	SLD 14	-191	23	1325	-22.1	-8.81	0.15
152	SLD 15	-163	8	1372	-8.66	-7.63	0.06
152	SLD 16	-163	8	1372	-8.66	-7.63	0.06
152	SLV 1	242	-24	1448	24.66	10.11	-0.16
152	SLV 2	242	-24	1448	24.66	10.11	-0.16
152	SLV 3	307	-59	1561	56.51	12.86	-0.37
152	SLV 4	307	-59	1561	56.51	12.86	-0.37
152	SLV 5	-56	46	1240	-40.9	-2.79	0.27
152	SLV 6	-56	46	1240	-40.9	-2.79	0.27
152	SLV 7	161	-71	1616	65.27	6.38	-0.43
152	SLV 8	161	-71	1616	65.27	6.38	-0.43
152	SLV 9	-246	71	1174	-65.23	-11.1	0.43
152	SLV 10	-246	71	1174	-65.23	-11.1	0.43
152	SLV 11	-29	-46	1550	40.93	-1.92	-0.27
152	SLV 12	-29	-46	1550	40.93	-1.92	-0.27
152	SLV 13	-392	59	1229	-56.47	-17.57	0.37
152	SLV 14	-392	59	1229	-56.47	-17.57	0.37
152	SLV 15	-327	24	1342	-24.62	-14.82	0.16
152	SLV 16	-327	24	1342	-24.62	-14.82	0.16
153	SLU 1	-31	0	1428	0.07	-2.05	0
153	SLU 2	-41	2	1427	-1.61	-2.47	0.01
153	SLU 3	-31	0	1428	0.07	-2.05	0
153	SLU 4	-37	1	1427	-0.94	-2.3	0.01
153	SLU 5	-41	2	1427	-1.61	-2.47	0.01
153	SLU 6	-31	0	1428	0.07	-2.05	0
153	SLU 7	-37	1	1427	-0.94	-2.3	0.01
153	SLU 8	-31	0	1428	0.07	-2.05	0
153	SLU 9	-37	1	1427	-0.94	-2.3	0.01
153	SLU 10	-53	2	1632	-1.68	-3.27	0.01
153	SLU 11	-43	0	1633	0.01	-2.84	0
153	SLU 12	-49	1	1633	-1	-3.1	0.01
153	SLU 13	-53	2	1632	-1.68	-3.27	0.01
153	SLU 14	-43	0	1633	0.01	-2.84	0
153	SLU 15	-49	1	1633	-1	-3.1	0.01
153	SLU 16	-43	0	1633	0.01	-2.84	0
153	SLU 17	-49	1	1633	-1	-3.1	0.01
153	SLU 18	-48	0	1721	-0.02	-3.18	0
153	SLU 19	-54	1	1721	-1.03	-3.44	0.01
153	SLU 20	-48	0	1721	-0.02	-3.18	0
153	SLU 21	-54	1	1721	-1.03	-3.44	0.01
153	SLU 22	-34	0	1524	0.05	-2.28	0
153	SLU 23	-43	2	1524	-1.63	-2.71	0.01
153	SLU 24	-34	0	1524	0.05	-2.28	0
153	SLU 25	-39	1	1524	-0.96	-2.54	0.01
153	SLU 26	-43	2	1524	-1.63	-2.71	0.01
153	SLU 27	-34	0	1524	0.05	-2.28	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
153	SLU 28	-39	1	1524	-0.96	-2.54	0.01
153	SLU 29	-34	0	1524	0.05	-2.28	0
153	SLU 30	-39	1	1524	-0.96	-2.54	0.01
153	SLU 31	-55	2	1729	-1.7	-3.5	0.01
153	SLU 32	-46	0	1729	-0.02	-3.08	0
153	SLU 33	-51	1	1729	-1.03	-3.33	0.01
153	SLU 34	-55	2	1729	-1.7	-3.5	0.01
153	SLU 35	-46	0	1729	-0.02	-3.08	0
153	SLU 36	-51	1	1729	-1.03	-3.33	0.01
153	SLU 37	-46	0	1729	-0.02	-3.08	0
153	SLU 38	-51	1	1729	-1.03	-3.33	0.01
153	SLU 39	-51	0	1817	-0.05	-3.42	0
153	SLU 40	-56	1	1817	-1.05	-3.67	0.01
153	SLU 41	-51	0	1817	-0.05	-3.42	0
153	SLU 42	-56	1	1817	-1.05	-3.67	0.01
153	SLU 43	-40	0	1823	0.1	-2.58	0
153	SLU 44	-49	2	1823	-1.58	-3.01	0.01
153	SLU 45	-40	0	1823	0.1	-2.58	0
153	SLU 46	-45	1	1823	-0.91	-2.84	0.01
153	SLU 47	-49	2	1823	-1.58	-3.01	0.01
153	SLU 48	-40	0	1823	0.1	-2.58	0
153	SLU 49	-45	1	1823	-0.91	-2.84	0.01
153	SLU 50	-40	0	1823	0.1	-2.58	0
153	SLU 51	-45	1	1823	-0.91	-2.84	0.01
153	SLU 52	-61	2	2028	-1.65	-3.8	0.01
153	SLU 53	-52	0	2028	0.03	-3.37	0
153	SLU 54	-57	1	2028	-0.97	-3.63	0.01
153	SLU 55	-61	2	2028	-1.65	-3.8	0.01
153	SLU 56	-52	0	2028	0.03	-3.37	0
153	SLU 57	-57	1	2028	-0.97	-3.63	0.01
153	SLU 58	-52	0	2028	0.03	-3.37	0
153	SLU 59	-57	1	2028	-0.97	-3.63	0.01
153	SLU 60	-57	0	2116	0.01	-3.71	0
153	SLU 61	-62	1	2116	-1	-3.97	0.01
153	SLU 62	-57	0	2116	0.01	-3.71	0
153	SLU 63	-62	1	2116	-1	-3.97	0.01
153	SLU 64	-42	0	1919	0.08	-2.82	0
153	SLU 65	-52	2	1919	-1.6	-3.24	0.01
153	SLU 66	-42	0	1919	0.08	-2.82	0
153	SLU 67	-48	1	1919	-0.93	-3.07	0.01
153	SLU 68	-52	2	1919	-1.6	-3.24	0.01
153	SLU 69	-42	0	1919	0.08	-2.82	0
153	SLU 70	-48	1	1919	-0.93	-3.07	0.01
153	SLU 71	-42	0	1919	0.08	-2.82	0
153	SLU 72	-48	1	1919	-0.93	-3.07	0.01
153	SLU 73	-64	2	2124	-1.67	-4.04	0.01
153	SLU 74	-54	0	2124	0.01	-3.61	0
153	SLU 75	-60	1	2124	-1	-3.87	0.01
153	SLU 76	-64	2	2124	-1.67	-4.04	0.01
153	SLU 77	-54	0	2124	0.01	-3.61	0
153	SLU 78	-60	1	2124	-1	-3.87	0.01
153	SLU 79	-54	0	2124	0.01	-3.61	0
153	SLU 80	-60	1	2124	-1	-3.87	0.01
153	SLU 81	-59	0	2212	-0.02	-3.95	0
153	SLU 82	-65	1	2212	-1.03	-4.21	0.01
153	SLU 83	-59	0	2212	-0.02	-3.95	0
153	SLU 84	-65	1	2212	-1.03	-4.21	0.01
153	SLE RA 1	-32	0	1455	0.06	-2.11	0
153	SLE RA 2	-38	1	1455	-1.06	-2.4	0.01
153	SLE RA 3	-32	0	1455	0.06	-2.11	0
153	SLE RA 4	-36	1	1455	-0.61	-2.29	0
153	SLE RA 5	-38	1	1455	-1.06	-2.4	0.01
153	SLE RA 6	-32	0	1455	0.06	-2.11	0
153	SLE RA 7	-36	1	1455	-0.61	-2.29	0
153	SLE RA 8	-32	0	1455	0.06	-2.11	0
153	SLE RA 9	-36	1	1455	-0.61	-2.29	0
153	SLE RA 10	-46	1	1592	-1.1	-2.93	0.01
153	SLE RA 11	-40	0	1592	0.02	-2.64	0
153	SLE RA 12	-44	1	1592	-0.65	-2.81	0
153	SLE RA 13	-46	1	1592	-1.1	-2.93	0.01
153	SLE RA 14	-40	0	1592	0.02	-2.64	0
153	SLE RA 15	-44	1	1592	-0.65	-2.81	0
153	SLE RA 16	-40	0	1592	0.02	-2.64	0
153	SLE RA 17	-44	1	1592	-0.65	-2.81	0
153	SLE RA 18	-43	0	1651	0	-2.87	0
153	SLE RA 19	-47	1	1650	-0.67	-3.04	0
153	SLE RA 20	-43	0	1651	0	-2.87	0
153	SLE RA 21	-47	1	1650	-0.67	-3.04	0
153	SLE FR 1	-32	0	1455	0.06	-2.11	0
153	SLE FR 2	-33	0	1455	-0.16	-2.17	0
153	SLE FR 3	-32	0	1455	0.06	-2.11	0
153	SLE FR 4	-36	0	1514	-0.18	-2.4	0
153	SLE FR 5	-35	0	1514	0.05	-2.34	0
153	SLE FR 6	-37	0	1553	0.03	-2.49	0
153	SLE QP 1	-32	0	1455	0.06	-2.11	0
153	SLE QP 2	-35	0	1514	0.05	-2.34	0
153	SLD 1	74	-12	1533	10.12	2.58	-0.08
153	SLD 2	74	-12	1533	10.12	2.58	-0.08



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
153	SLD 3	101	-24	1595	21.77	3.73	-0.15
153	SLD 4	101	-24	1595	21.77	3.73	-0.15
153	SLD 5	-44	15	1425	-14.59	-2.61	0.09
153	SLD 6	-44	15	1425	-14.59	-2.61	0.09
153	SLD 7	47	-26	1633	24.22	1.22	-0.16
153	SLD 8	47	-26	1633	24.22	1.22	-0.16
153	SLD 9	-117	26	1395	-24.13	-5.91	0.16
153	SLD 10	-117	26	1395	-24.13	-5.91	0.16
153	SLD 11	-27	-15	1603	14.68	-2.07	-0.09
153	SLD 12	-27	-15	1603	14.68	-2.07	-0.09
153	SLD 13	-171	25	1432	-21.68	-8.41	0.15
153	SLD 14	-171	25	1432	-21.68	-8.41	0.15
153	SLD 15	-144	12	1495	-10.03	-7.26	0.08
153	SLD 16	-144	12	1495	-10.03	-7.26	0.08
153	SLV 1	222	-34	1556	28.26	9.24	-0.21
153	SLV 2	222	-34	1556	28.26	9.24	-0.21
153	SLV 3	286	-63	1705	55.91	11.95	-0.39
153	SLV 4	286	-63	1705	55.91	11.95	-0.39
153	SLV 5	-55	34	1301	-33.42	-2.97	0.21
153	SLV 6	-55	34	1301	-33.42	-2.97	0.21
153	SLV 7	158	-63	1797	58.74	6.05	-0.39
153	SLV 8	158	-63	1797	58.74	6.05	-0.39
153	SLV 9	-229	63	1230	-58.65	-10.74	0.39
153	SLV 10	-229	63	1230	-58.65	-10.74	0.39
153	SLV 11	-15	-34	1727	33.51	-1.71	-0.21
153	SLV 12	-15	-34	1727	33.51	-1.71	-0.21
153	SLV 13	-356	63	1322	-55.81	-16.63	0.39
153	SLV 14	-356	63	1322	-55.81	-16.63	0.39
153	SLV 15	-292	34	1471	-28.17	-13.93	0.21
153	SLV 16	-292	34	1471	-28.17	-13.93	0.21
154	SLU 1	-47	0	1559	0.15	-2.72	0
154	SLU 2	-54	1	1562	-1.29	-3.03	0.01
154	SLU 3	-47	0	1559	0.15	-2.72	0
154	SLU 4	-51	1	1561	-0.72	-2.91	0
154	SLU 5	-54	1	1562	-1.29	-3.03	0.01
154	SLU 6	-47	0	1559	0.15	-2.72	0
154	SLU 7	-51	1	1561	-0.72	-2.91	0
154	SLU 8	-47	0	1559	0.15	-2.72	0
154	SLU 9	-51	1	1561	-0.72	-2.91	0
154	SLU 10	-62	2	1812	-1.34	-3.6	0.01
154	SLU 11	-56	0	1810	0.1	-3.29	0
154	SLU 12	-60	1	1811	-0.77	-3.48	0.01
154	SLU 13	-62	2	1812	-1.34	-3.6	0.01
154	SLU 14	-56	0	1810	0.1	-3.29	0
154	SLU 15	-60	1	1811	-0.77	-3.48	0.01
154	SLU 16	-56	0	1810	0.1	-3.29	0
154	SLU 17	-60	1	1811	-0.77	-3.48	0.01
154	SLU 18	-59	0	1917	0.08	-3.54	0
154	SLU 19	-63	1	1919	-0.79	-3.73	0.01
154	SLU 20	-59	0	1917	0.08	-3.54	0
154	SLU 21	-63	1	1919	-0.79	-3.73	0.01
154	SLU 22	-47	0	1677	0.14	-2.84	0
154	SLU 23	-54	1	1680	-1.31	-3.15	0.01
154	SLU 24	-47	0	1677	0.14	-2.84	0
154	SLU 25	-51	1	1679	-0.73	-3.02	0.01
154	SLU 26	-54	1	1680	-1.31	-3.15	0.01
154	SLU 27	-47	0	1677	0.14	-2.84	0
154	SLU 28	-51	1	1679	-0.73	-3.02	0.01
154	SLU 29	-47	0	1677	0.14	-2.84	0
154	SLU 30	-51	1	1679	-0.73	-3.02	0.01
154	SLU 31	-63	2	1931	-1.36	-3.72	0.01
154	SLU 32	-56	0	1928	0.08	-3.41	0
154	SLU 33	-60	1	1929	-0.78	-3.6	0.01
154	SLU 34	-63	2	1931	-1.36	-3.72	0.01
154	SLU 35	-56	0	1928	0.08	-3.41	0
154	SLU 36	-60	1	1929	-0.78	-3.6	0.01
154	SLU 37	-56	0	1928	0.08	-3.41	0
154	SLU 38	-60	1	1929	-0.78	-3.6	0.01
154	SLU 39	-60	0	2035	0.06	-3.66	0
154	SLU 40	-64	1	2037	-0.8	-3.84	0.01
154	SLU 41	-60	0	2035	0.06	-3.66	0
154	SLU 42	-64	1	2037	-0.8	-3.84	0.01
154	SLU 43	-61	0	1986	0.2	-3.49	0
154	SLU 44	-68	1	1989	-1.24	-3.81	0.01
154	SLU 45	-61	0	1986	0.2	-3.49	0
154	SLU 46	-65	1	1988	-0.67	-3.68	0
154	SLU 47	-68	1	1989	-1.24	-3.81	0.01
154	SLU 48	-61	0	1986	0.2	-3.49	0
154	SLU 49	-65	1	1988	-0.67	-3.68	0
154	SLU 50	-61	0	1986	0.2	-3.49	0
154	SLU 51	-65	1	1988	-0.67	-3.68	0
154	SLU 52	-76	2	2240	-1.29	-4.38	0.01
154	SLU 53	-70	0	2237	0.15	-4.07	0
154	SLU 54	-74	1	2239	-0.72	-4.26	0.01
154	SLU 55	-76	2	2240	-1.29	-4.38	0.01
154	SLU 56	-70	0	2237	0.15	-4.07	0
154	SLU 57	-74	1	2239	-0.72	-4.26	0.01
154	SLU 58	-70	0	2237	0.15	-4.07	0





Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
154	SLU 59	-74	1	2239	-0.72	-4.26	0.01
154	SLU 60	-73	0	2344	0.13	-4.31	0
154	SLU 61	-77	1	2346	-0.74	-4.5	0.01
154	SLU 62	-73	0	2344	0.13	-4.31	0
154	SLU 63	-77	1	2346	-0.74	-4.5	0.01
154	SLU 64	-61	0	2105	0.19	-3.61	0
154	SLU 65	-68	1	2107	-1.26	-3.92	0.01
154	SLU 66	-61	0	2105	0.19	-3.61	0
154	SLU 67	-65	1	2106	-0.68	-3.8	0.01
154	SLU 68	-68	1	2107	-1.26	-3.92	0.01
154	SLU 69	-61	0	2105	0.19	-3.61	0
154	SLU 70	-65	1	2106	-0.68	-3.8	0.01
154	SLU 71	-61	0	2105	0.19	-3.61	0
154	SLU 72	-65	1	2106	-0.68	-3.8	0.01
154	SLU 73	-77	2	2358	-1.31	-4.5	0.01
154	SLU 74	-70	0	2355	0.13	-4.19	0
154	SLU 75	-74	1	2357	-0.73	-4.37	0.01
154	SLU 76	-77	2	2358	-1.31	-4.5	0.01
154	SLU 77	-70	0	2355	0.13	-4.19	0
154	SLU 78	-74	1	2357	-0.73	-4.37	0.01
154	SLU 79	-70	0	2355	0.13	-4.19	0
154	SLU 80	-74	1	2357	-0.73	-4.37	0.01
154	SLU 81	-74	0	2462	0.11	-4.43	0
154	SLU 82	-78	1	2464	-0.75	-4.62	0.01
154	SLU 83	-74	0	2462	0.11	-4.43	0
154	SLU 84	-78	1	2464	-0.75	-4.62	0.01
154	SLE RA 1	-47	0	1593	0.15	-2.75	0
154	SLE RA 2	-52	1	1595	-0.82	-2.96	0.01
154	SLE RA 3	-47	0	1593	0.15	-2.75	0
154	SLE RA 4	-50	1	1594	-0.43	-2.88	0
154	SLE RA 5	-52	1	1595	-0.82	-2.96	0.01
154	SLE RA 6	-47	0	1593	0.15	-2.75	0
154	SLE RA 7	-50	1	1594	-0.43	-2.88	0
154	SLE RA 8	-47	0	1593	0.15	-2.75	0
154	SLE RA 9	-50	1	1594	-0.43	-2.88	0
154	SLE RA 10	-57	1	1762	-0.85	-3.34	0.01
154	SLE RA 11	-53	0	1760	0.11	-3.14	0
154	SLE RA 12	-56	1	1761	-0.47	-3.26	0
154	SLE RA 13	-57	1	1762	-0.85	-3.34	0.01
154	SLE RA 14	-53	0	1760	0.11	-3.14	0
154	SLE RA 15	-56	1	1761	-0.47	-3.26	0
154	SLE RA 16	-53	0	1760	0.11	-3.14	0
154	SLE RA 17	-56	1	1761	-0.47	-3.26	0
154	SLE RA 18	-55	0	1831	0.1	-3.3	0
154	SLE RA 19	-58	1	1833	-0.48	-3.42	0
154	SLE RA 20	-55	0	1831	0.1	-3.3	0
154	SLE RA 21	-58	1	1833	-0.48	-3.42	0
154	SLE FR 1	-47	0	1593	0.15	-2.75	0
154	SLE FR 2	-48	0	1593	-0.05	-2.79	0
154	SLE FR 3	-47	0	1593	0.15	-2.75	0
154	SLE FR 4	-51	0	1665	-0.06	-2.96	0
154	SLE FR 5	-50	0	1665	0.13	-2.92	0
154	SLE FR 6	-51	0	1712	0.12	-3.03	0
154	SLE QP 1	-47	0	1593	0.15	-2.75	0
154	SLE QP 2	-50	0	1665	0.13	-2.92	0
154	SLD 1	48	-16	1566	10.86	1.43	-0.09
154	SLD 2	48	-16	1566	10.86	1.43	-0.09
154	SLD 3	76	-25	1649	19.74	2.56	-0.13
154	SLD 4	76	-25	1649	19.74	2.56	-0.13
154	SLD 5	-63	8	1509	-10.12	-3.32	0.03
154	SLD 6	-63	8	1509	-10.12	-3.32	0.03
154	SLD 7	31	-20	1786	19.48	0.43	-0.1
154	SLD 8	31	-20	1786	19.48	0.43	-0.1
154	SLD 9	-130	20	1543	-19.22	-6.27	0.1
154	SLD 10	-130	20	1543	-19.22	-6.27	0.1
154	SLD 11	-36	-8	1820	10.38	-2.51	-0.03
154	SLD 12	-36	-8	1820	10.38	-2.51	-0.03
154	SLD 13	-175	25	1680	-19.48	-8.39	0.13
154	SLD 14	-175	25	1680	-19.48	-8.39	0.13
154	SLD 15	-147	16	1763	-10.6	-7.26	0.09
154	SLD 16	-147	16	1763	-10.6	-7.26	0.09
154	SLV 1	180	-43	1430	29.64	7.29	-0.24
154	SLV 2	180	-43	1430	29.64	7.29	-0.24
154	SLV 3	246	-63	1628	50.79	9.95	-0.33
154	SLV 4	246	-63	1628	50.79	9.95	-0.33
154	SLV 5	-81	17	1293	-23.09	-3.89	0.07
154	SLV 6	-81	17	1293	-23.09	-3.89	0.07
154	SLV 7	139	-49	1955	47.4	4.98	-0.24
154	SLV 8	139	-49	1955	47.4	4.98	-0.24
154	SLV 9	-239	49	1374	-47.14	-10.81	0.25
154	SLV 10	-239	49	1374	-47.14	-10.81	0.25
154	SLV 11	-18	-17	2036	23.35	-1.94	-0.07
154	SLV 12	-18	-17	2036	23.35	-1.94	-0.07
154	SLV 13	-345	64	1701	-50.53	-15.79	0.33
154	SLV 14	-345	64	1701	-50.53	-15.79	0.33
154	SLV 15	-279	44	1899	-29.38	-13.13	0.24
154	SLV 16	-279	44	1899	-29.38	-13.13	0.24
155	SLU 1	-96	0	1711	0.37	-5.07	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
155	SLU 2	-101	1	1719	-0.7	-5.32	0.01
155	SLU 3	-96	0	1711	0.37	-5.07	0
155	SLU 4	-99	0	1716	-0.27	-5.22	0
155	SLU 5	-101	1	1719	-0.7	-5.32	0.01
155	SLU 6	-96	0	1711	0.37	-5.07	0
155	SLU 7	-99	0	1716	-0.27	-5.22	0
155	SLU 8	-96	0	1711	0.37	-5.07	0
155	SLU 9	-99	0	1716	-0.27	-5.22	0
155	SLU 10	-117	1	2025	-0.7	-6.38	0.01
155	SLU 11	-112	0	2017	0.37	-6.13	0
155	SLU 12	-115	1	2021	-0.27	-6.28	0.01
155	SLU 13	-117	1	2025	-0.7	-6.38	0.01
155	SLU 14	-112	0	2017	0.37	-6.13	0
155	SLU 15	-115	1	2021	-0.27	-6.28	0.01
155	SLU 16	-112	0	2017	0.37	-6.13	0
155	SLU 17	-115	1	2021	-0.27	-6.28	0.01
155	SLU 18	-119	0	2147	0.38	-6.59	0
155	SLU 19	-122	1	2152	-0.27	-6.74	0.01
155	SLU 20	-119	0	2147	0.38	-6.59	0
155	SLU 21	-122	1	2152	-0.27	-6.74	0.01
155	SLU 22	-99	0	1856	0.38	-5.39	0
155	SLU 23	-104	1	1865	-0.69	-5.64	0.01
155	SLU 24	-99	0	1856	0.38	-5.39	0
155	SLU 25	-102	0	1861	-0.26	-5.54	0
155	SLU 26	-104	1	1865	-0.69	-5.64	0.01
155	SLU 27	-99	0	1856	0.38	-5.39	0
155	SLU 28	-102	0	1861	-0.26	-5.54	0
155	SLU 29	-99	0	1856	0.38	-5.39	0
155	SLU 30	-102	0	1861	-0.26	-5.54	0
155	SLU 31	-120	1	2170	-0.68	-6.7	0.01
155	SLU 32	-115	0	2162	0.39	-6.46	0
155	SLU 33	-118	1	2167	-0.25	-6.6	0.01
155	SLU 34	-120	1	2170	-0.68	-6.7	0.01
155	SLU 35	-115	0	2162	0.39	-6.46	0
155	SLU 36	-118	1	2167	-0.25	-6.6	0.01
155	SLU 37	-115	0	2162	0.39	-6.46	0
155	SLU 38	-118	1	2167	-0.25	-6.6	0.01
155	SLU 39	-122	0	2293	0.39	-6.91	0
155	SLU 40	-125	1	2298	-0.25	-7.06	0.01
155	SLU 41	-122	0	2293	0.39	-6.91	0
155	SLU 42	-125	1	2298	-0.25	-7.06	0.01
155	SLU 43	-124	0	2175	0.47	-6.48	0
155	SLU 44	-129	1	2183	-0.59	-6.73	0.01
155	SLU 45	-124	0	2175	0.47	-6.48	0
155	SLU 46	-127	0	2180	-0.17	-6.63	0
155	SLU 47	-129	1	2183	-0.59	-6.73	0.01
155	SLU 48	-124	0	2175	0.47	-6.48	0
155	SLU 49	-127	0	2180	-0.17	-6.63	0
155	SLU 50	-124	0	2175	0.47	-6.48	0
155	SLU 51	-127	0	2180	-0.17	-6.63	0
155	SLU 52	-145	1	2488	-0.59	-7.79	0.01
155	SLU 53	-140	0	2480	0.48	-7.55	0
155	SLU 54	-143	0	2485	-0.16	-7.69	0.01
155	SLU 55	-145	1	2488	-0.59	-7.79	0.01
155	SLU 56	-140	0	2480	0.48	-7.55	0
155	SLU 57	-143	0	2485	-0.16	-7.69	0.01
155	SLU 58	-140	0	2480	0.48	-7.55	0
155	SLU 59	-143	0	2485	-0.16	-7.69	0.01
155	SLU 60	-147	0	2611	0.48	-8	0
155	SLU 61	-150	0	2616	-0.16	-8.15	0.01
155	SLU 62	-147	0	2611	0.48	-8	0
155	SLU 63	-150	0	2616	-0.16	-8.15	0.01
155	SLU 64	-127	0	2320	0.49	-6.8	0
155	SLU 65	-132	1	2328	-0.58	-7.05	0.01
155	SLU 66	-127	0	2320	0.49	-6.8	0
155	SLU 67	-130	0	2325	-0.15	-6.95	0.01
155	SLU 68	-132	1	2328	-0.58	-7.05	0.01
155	SLU 69	-127	0	2320	0.49	-6.8	0
155	SLU 70	-130	0	2325	-0.15	-6.95	0.01
155	SLU 71	-127	0	2320	0.49	-6.8	0
155	SLU 72	-130	0	2325	-0.15	-6.95	0.01
155	SLU 73	-148	1	2633	-0.58	-8.11	0.01
155	SLU 74	-143	0	2625	0.49	-7.87	0
155	SLU 75	-146	0	2630	-0.15	-8.02	0.01
155	SLU 76	-148	1	2633	-0.58	-8.11	0.01
155	SLU 77	-143	0	2625	0.49	-7.87	0
155	SLU 78	-146	0	2630	-0.15	-8.02	0.01
155	SLU 79	-143	0	2625	0.49	-7.87	0
155	SLU 80	-146	0	2630	-0.15	-8.02	0.01
155	SLU 81	-150	0	2756	0.5	-8.32	0
155	SLU 82	-153	0	2761	-0.15	-8.47	0.01
155	SLU 83	-150	0	2756	0.5	-8.32	0
155	SLU 84	-153	0	2761	-0.15	-8.47	0.01
155	SLE RA 1	-97	0	1753	0.37	-5.16	0
155	SLE RA 2	-100	1	1758	-0.34	-5.33	0
155	SLE RA 3	-97	0	1753	0.37	-5.16	0
155	SLE RA 4	-99	0	1756	-0.05	-5.26	0
155	SLE RA 5	-100	1	1758	-0.34	-5.33	0



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
155	SLE RA 6	-97	0	1753	0.37	-5.16	0
155	SLE RA 7	-99	0	1756	-0.05	-5.26	0
155	SLE RA 8	-97	0	1753	0.37	-5.16	0
155	SLE RA 9	-99	0	1756	-0.05	-5.26	0
155	SLE RA 10	-111	1	1962	-0.34	-6.04	0.01
155	SLE RA 11	-108	0	1956	0.38	-5.87	0
155	SLE RA 12	-110	0	1960	-0.05	-5.97	0
155	SLE RA 13	-111	1	1962	-0.34	-6.04	0.01
155	SLE RA 14	-108	0	1956	0.38	-5.87	0
155	SLE RA 15	-110	0	1960	-0.05	-5.97	0
155	SLE RA 16	-108	0	1956	0.38	-5.87	0
155	SLE RA 17	-110	0	1960	-0.05	-5.97	0
155	SLE RA 18	-112	0	2044	0.38	-6.18	0
155	SLE RA 19	-114	0	2047	-0.05	-6.27	0
155	SLE RA 20	-112	0	2044	0.38	-6.18	0
155	SLE RA 21	-114	0	2047	-0.05	-6.27	0
155	SLE FR 1	-97	0	1753	0.37	-5.16	0
155	SLE FR 2	-98	0	1754	0.23	-5.2	0
155	SLE FR 3	-97	0	1753	0.37	-5.16	0
155	SLE FR 4	-102	0	1841	0.23	-5.5	0
155	SLE FR 5	-102	0	1840	0.37	-5.47	0
155	SLE FR 6	-105	0	1898	0.37	-5.67	0
155	SLE QP 1	-97	0	1753	0.37	-5.16	0
155	SLE QP 2	-102	0	1840	0.37	-5.47	0
155	SLD 1	-11	-18	1689	10.09	-1.25	-0.07
155	SLD 2	-11	-18	1689	10.09	-1.25	-0.07
155	SLD 3	19	-23	1804	15.76	-0.08	-0.08
155	SLD 4	19	-23	1804	15.76	-0.08	-0.08
155	SLD 5	-120	1	1622	-5.3	-5.98	0
155	SLD 6	-120	1	1622	-5.3	-5.98	0
155	SLD 7	-20	-13	2002	13.58	-2.08	-0.04
155	SLD 8	-20	-13	2002	13.58	-2.08	-0.04
155	SLD 9	-184	13	1678	-12.84	-8.86	0.05
155	SLD 10	-184	13	1678	-12.84	-8.86	0.05
155	SLD 11	-83	-1	2058	6.05	-4.96	0
155	SLD 12	-83	-1	2058	6.05	-4.96	0
155	SLD 13	-222	22	1876	-15.01	-10.85	0.09
155	SLD 14	-222	22	1876	-15.01	-10.85	0.09
155	SLD 15	-192	18	1991	-9.35	-9.68	0.08
155	SLD 16	-192	18	1991	-9.35	-9.68	0.08
155	SLV 1	111	-48	1478	26.65	4.43	-0.19
155	SLV 2	111	-48	1478	26.65	4.43	-0.19
155	SLV 3	182	-58	1750	40.21	7.18	-0.22
155	SLV 4	182	-58	1750	40.21	7.18	-0.22
155	SLV 5	-146	1	1319	-12.31	-6.68	0
155	SLV 6	-146	1	1319	-12.31	-6.68	0
155	SLV 7	92	-33	2225	32.89	2.51	-0.12
155	SLV 8	92	-33	2225	32.89	2.51	-0.12
155	SLV 9	-295	33	1455	-32.14	-13.44	0.12
155	SLV 10	-295	33	1455	-32.14	-13.44	0.12
155	SLV 11	-57	-2	2361	13.05	-4.25	0.01
155	SLV 12	-57	-2	2361	13.05	-4.25	0.01
155	SLV 13	-385	58	1930	-39.47	-18.12	0.23
155	SLV 14	-385	58	1930	-39.47	-18.12	0.23
155	SLV 15	-314	47	2201	-25.91	-15.36	0.19
155	SLV 16	-314	47	2201	-25.91	-15.36	0.19
156	SLU 1	-157	-3	1971	0.95	-9.1	-0.02
156	SLU 2	-160	-2	1988	0.39	-9.29	-0.02
156	SLU 3	-157	-3	1971	0.95	-9.1	-0.02
156	SLU 4	-158	-3	1982	0.61	-9.22	-0.02
156	SLU 5	-160	-2	1988	0.39	-9.29	-0.02
156	SLU 6	-157	-3	1971	0.95	-9.1	-0.02
156	SLU 7	-158	-3	1982	0.61	-9.22	-0.02
156	SLU 8	-157	-3	1971	0.95	-9.1	-0.02
156	SLU 9	-158	-3	1982	0.61	-9.22	-0.02
156	SLU 10	-187	-3	2373	0.54	-11.07	-0.02
156	SLU 11	-184	-4	2356	1.1	-10.88	-0.02
156	SLU 12	-186	-3	2367	0.76	-10.99	-0.02
156	SLU 13	-187	-3	2373	0.54	-11.07	-0.02
156	SLU 14	-184	-4	2356	1.1	-10.88	-0.02
156	SLU 15	-186	-3	2367	0.76	-10.99	-0.02
156	SLU 16	-184	-4	2356	1.1	-10.88	-0.02
156	SLU 17	-186	-3	2367	0.76	-10.99	-0.02
156	SLU 18	-196	-4	2521	1.16	-11.64	-0.02
156	SLU 19	-198	-3	2531	0.82	-11.75	-0.02
156	SLU 20	-196	-4	2521	1.16	-11.64	-0.02
156	SLU 21	-198	-3	2531	0.82	-11.75	-0.02
156	SLU 22	-165	-3	2157	1.04	-9.75	-0.02
156	SLU 23	-168	-3	2174	0.48	-9.94	-0.02
156	SLU 24	-165	-3	2157	1.04	-9.75	-0.02
156	SLU 25	-166	-3	2167	0.7	-9.86	-0.02
156	SLU 26	-168	-3	2174	0.48	-9.94	-0.02
156	SLU 27	-165	-3	2157	1.04	-9.75	-0.02
156	SLU 28	-166	-3	2167	0.7	-9.86	-0.02
156	SLU 29	-165	-3	2157	1.04	-9.75	-0.02
156	SLU 30	-166	-3	2167	0.7	-9.86	-0.02
156	SLU 31	-195	-3	2559	0.62	-11.71	-0.02
156	SLU 32	-192	-4	2542	1.19	-11.53	-0.02



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
156	SLU 33	-194	-4	2552	0.85	-11.64	-0.02
156	SLU 34	-195	-3	2559	0.62	-11.71	-0.02
156	SLU 35	-192	-4	2542	1.19	-11.53	-0.02
156	SLU 36	-194	-4	2552	0.85	-11.64	-0.02
156	SLU 37	-192	-4	2542	1.19	-11.53	-0.02
156	SLU 38	-194	-4	2552	0.85	-11.64	-0.02
156	SLU 39	-204	-4	2707	1.25	-12.29	-0.02
156	SLU 40	-206	-4	2717	0.91	-12.4	-0.02
156	SLU 41	-204	-4	2707	1.25	-12.29	-0.02
156	SLU 42	-206	-4	2717	0.91	-12.4	-0.02
156	SLU 43	-201	-4	2499	1.2	-11.61	-0.02
156	SLU 44	-204	-3	2516	0.64	-11.8	-0.02
156	SLU 45	-201	-4	2499	1.2	-11.61	-0.02
156	SLU 46	-203	-4	2509	0.87	-11.73	-0.02
156	SLU 47	-204	-3	2516	0.64	-11.8	-0.02
156	SLU 48	-201	-4	2499	1.2	-11.61	-0.02
156	SLU 49	-203	-4	2509	0.87	-11.73	-0.02
156	SLU 50	-201	-4	2499	1.2	-11.61	-0.02
156	SLU 51	-203	-4	2509	0.87	-11.73	-0.02
156	SLU 52	-231	-4	2901	0.79	-13.58	-0.02
156	SLU 53	-228	-4	2884	1.35	-13.39	-0.02
156	SLU 54	-230	-4	2894	1.02	-13.5	-0.02
156	SLU 55	-231	-4	2901	0.79	-13.58	-0.02
156	SLU 56	-228	-4	2884	1.35	-13.39	-0.02
156	SLU 57	-230	-4	2894	1.02	-13.5	-0.02
156	SLU 58	-228	-4	2884	1.35	-13.39	-0.02
156	SLU 59	-230	-4	2894	1.02	-13.5	-0.02
156	SLU 60	-240	-5	3049	1.42	-14.15	-0.03
156	SLU 61	-242	-4	3059	1.08	-14.26	-0.03
156	SLU 62	-240	-5	3049	1.42	-14.15	-0.03
156	SLU 63	-242	-4	3059	1.08	-14.26	-0.03
156	SLU 64	-209	-4	2685	1.29	-12.26	-0.02
156	SLU 65	-212	-4	2701	0.73	-12.45	-0.02
156	SLU 66	-209	-4	2685	1.29	-12.26	-0.02
156	SLU 67	-211	-4	2695	0.96	-12.37	-0.02
156	SLU 68	-212	-4	2701	0.73	-12.45	-0.02
156	SLU 69	-209	-4	2685	1.29	-12.26	-0.02
156	SLU 70	-211	-4	2695	0.96	-12.37	-0.02
156	SLU 71	-209	-4	2685	1.29	-12.26	-0.02
156	SLU 72	-211	-4	2695	0.96	-12.37	-0.02
156	SLU 73	-239	-4	3086	0.88	-14.22	-0.03
156	SLU 74	-236	-5	3070	1.44	-14.04	-0.03
156	SLU 75	-238	-4	3080	1.1	-14.15	-0.03
156	SLU 76	-239	-4	3086	0.88	-14.22	-0.03
156	SLU 77	-236	-5	3070	1.44	-14.04	-0.03
156	SLU 78	-238	-4	3080	1.1	-14.15	-0.03
156	SLU 79	-236	-5	3070	1.44	-14.04	-0.03
156	SLU 80	-238	-4	3080	1.1	-14.15	-0.03
156	SLU 81	-248	-5	3235	1.5	-14.8	-0.03
156	SLU 82	-250	-5	3245	1.17	-14.91	-0.03
156	SLU 83	-248	-5	3235	1.5	-14.8	-0.03
156	SLU 84	-250	-5	3245	1.17	-14.91	-0.03
156	SLE RA 1	-159	-3	2024	0.97	-9.29	-0.02
156	SLE RA 2	-161	-3	2036	0.6	-9.41	-0.02
156	SLE RA 3	-159	-3	2024	0.97	-9.29	-0.02
156	SLE RA 4	-160	-3	2031	0.75	-9.36	-0.02
156	SLE RA 5	-161	-3	2036	0.6	-9.41	-0.02
156	SLE RA 6	-159	-3	2024	0.97	-9.29	-0.02
156	SLE RA 7	-160	-3	2031	0.75	-9.36	-0.02
156	SLE RA 8	-159	-3	2024	0.97	-9.29	-0.02
156	SLE RA 9	-160	-3	2031	0.75	-9.36	-0.02
156	SLE RA 10	-179	-3	2292	0.7	-10.6	-0.02
156	SLE RA 11	-177	-3	2281	1.07	-10.47	-0.02
156	SLE RA 12	-178	-3	2288	0.85	-10.55	-0.02
156	SLE RA 13	-179	-3	2292	0.7	-10.6	-0.02
156	SLE RA 14	-177	-3	2281	1.07	-10.47	-0.02
156	SLE RA 15	-178	-3	2288	0.85	-10.55	-0.02
156	SLE RA 16	-177	-3	2281	1.07	-10.47	-0.02
156	SLE RA 17	-178	-3	2288	0.85	-10.55	-0.02
156	SLE RA 18	-185	-4	2391	1.12	-10.98	-0.02
156	SLE RA 19	-186	-3	2398	0.89	-11.05	-0.02
156	SLE RA 20	-185	-4	2391	1.12	-10.98	-0.02
156	SLE RA 21	-186	-3	2398	0.89	-11.05	-0.02
156	SLE FR 1	-159	-3	2024	0.97	-9.29	-0.02
156	SLE FR 2	-159	-3	2027	0.9	-9.31	-0.02
156	SLE FR 3	-159	-3	2024	0.97	-9.29	-0.02
156	SLE FR 4	-167	-3	2137	0.94	-9.82	-0.02
156	SLE FR 5	-167	-3	2134	1.02	-9.8	-0.02
156	SLE FR 6	-172	-3	2208	1.05	-10.13	-0.02
156	SLE QP 1	-159	-3	2024	0.97	-9.29	-0.02
156	SLE QP 2	-167	-3	2134	1.02	-9.8	-0.02
156	SLD 1	-87	-16	1876	7.04	-5.81	-0.03
156	SLD 2	-87	-16	1876	7.04	-5.81	-0.03
156	SLD 3	-52	-18	2051	9.68	-4.7	-0.03
156	SLD 4	-52	-18	2051	9.68	-4.7	-0.03
156	SLD 5	-196	-4	1792	-1.19	-10.29	-0.01
156	SLD 6	-196	-4	1792	-1.19	-10.29	-0.01
156	SLD 7	-79	-11	2374	7.63	-6.58	-0.03



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
156	SLD 8	-79	-11	2374	7.63	-6.58	-0.03
156	SLD 9	-254	5	1894	-5.59	-13.02	-0.01
156	SLD 10	-254	5	1894	-5.59	-13.02	-0.01
156	SLD 11	-138	-3	2477	3.22	-9.3	-0.02
156	SLD 12	-138	-3	2477	3.22	-9.3	-0.02
156	SLD 13	-281	12	2218	-7.65	-14.9	0
156	SLD 14	-281	12	2218	-7.65	-14.9	0
156	SLD 15	-246	10	2393	-5	-13.78	-0.01
156	SLD 16	-246	10	2393	-5	-13.78	-0.01
156	SLV 1	20	-36	1515	17.1	-0.45	-0.04
156	SLV 2	20	-36	1515	17.1	-0.45	-0.04
156	SLV 3	103	-42	1930	23.46	2.18	-0.06
156	SLV 4	103	-42	1930	23.46	2.18	-0.06
156	SLV 5	-236	-5	1320	-3.81	-10.97	-0.01
156	SLV 6	-236	-5	1320	-3.81	-10.97	-0.01
156	SLV 7	39	-23	2702	17.41	-2.23	-0.05
156	SLV 8	39	-23	2702	17.41	-2.23	-0.05
156	SLV 9	-372	17	1567	-15.37	-17.37	0.01
156	SLV 10	-372	17	1567	-15.37	-17.37	0.01
156	SLV 11	-98	-2	2949	5.85	-8.62	-0.03
156	SLV 12	-98	-2	2949	5.85	-8.62	-0.03
156	SLV 13	-436	35	2339	-21.43	-21.77	0.02
156	SLV 14	-436	35	2339	-21.43	-21.77	0.02
156	SLV 15	-354	30	2754	-15.06	-19.15	0.01
156	SLV 16	-354	30	2754	-15.06	-19.15	0.01
157	SLU 1	-299	-418	2643	12.11	-7.22	0.04
157	SLU 2	-302	-424	2673	12.19	-7.42	0.04
157	SLU 3	-299	-418	2643	12.11	-7.22	0.04
157	SLU 4	-301	-422	2661	12.16	-7.34	0.04
157	SLU 5	-302	-424	2673	12.19	-7.42	0.04
157	SLU 6	-299	-418	2643	12.11	-7.22	0.04
157	SLU 7	-301	-422	2661	12.16	-7.34	0.04
157	SLU 8	-299	-418	2643	12.11	-7.22	0.04
157	SLU 9	-301	-422	2661	12.16	-7.34	0.04
157	SLU 10	-363	-505	3213	14.37	-8.94	0.04
157	SLU 11	-360	-499	3184	14.29	-8.74	0.04
157	SLU 12	-362	-503	3201	14.34	-8.86	0.04
157	SLU 13	-363	-505	3213	14.37	-8.94	0.04
157	SLU 14	-360	-499	3184	14.29	-8.74	0.04
157	SLU 15	-362	-503	3201	14.34	-8.86	0.04
157	SLU 16	-360	-499	3184	14.29	-8.74	0.04
157	SLU 17	-362	-503	3201	14.34	-8.86	0.04
157	SLU 18	-387	-534	3415	15.22	-9.4	0.04
157	SLU 19	-388	-537	3433	15.27	-9.52	0.04
157	SLU 20	-387	-534	3415	15.22	-9.4	0.04
157	SLU 21	-388	-537	3433	15.27	-9.52	0.04
157	SLU 22	-326	-463	2908	13.39	-7.84	0.04
157	SLU 23	-329	-468	2938	13.47	-8.03	0.04
157	SLU 24	-326	-463	2908	13.39	-7.84	0.04
157	SLU 25	-328	-466	2926	13.44	-7.95	0.04
157	SLU 26	-329	-468	2938	13.47	-8.03	0.04
157	SLU 27	-326	-463	2908	13.39	-7.84	0.04
157	SLU 28	-328	-466	2926	13.44	-7.95	0.04
157	SLU 29	-326	-463	2908	13.39	-7.84	0.04
157	SLU 30	-328	-466	2926	13.44	-7.95	0.04
157	SLU 31	-390	-550	3478	15.65	-9.55	0.05
157	SLU 32	-387	-544	3449	15.57	-9.36	0.05
157	SLU 33	-389	-547	3466	15.62	-9.48	0.05
157	SLU 34	-390	-550	3478	15.65	-9.55	0.05
157	SLU 35	-387	-544	3449	15.57	-9.36	0.05
157	SLU 36	-389	-547	3466	15.62	-9.48	0.05
157	SLU 37	-387	-544	3449	15.57	-9.36	0.05
157	SLU 38	-389	-547	3466	15.62	-9.48	0.05
157	SLU 39	-413	-578	3680	16.51	-10.01	0.05
157	SLU 40	-415	-582	3698	16.56	-10.13	0.05
157	SLU 41	-413	-578	3680	16.51	-10.01	0.05
157	SLU 42	-415	-582	3698	16.56	-10.13	0.05
157	SLU 43	-380	-528	3346	15.3	-9.18	0.04
157	SLU 44	-383	-534	3375	15.38	-9.37	0.04
157	SLU 45	-380	-528	3346	15.3	-9.18	0.04
157	SLU 46	-382	-532	3363	15.35	-9.29	0.04
157	SLU 47	-383	-534	3375	15.38	-9.37	0.04
157	SLU 48	-380	-528	3346	15.3	-9.18	0.04
157	SLU 49	-382	-532	3363	15.35	-9.29	0.04
157	SLU 50	-380	-528	3346	15.3	-9.18	0.04
157	SLU 51	-382	-532	3363	15.35	-9.29	0.04
157	SLU 52	-444	-615	3915	17.56	-10.9	0.05
157	SLU 53	-441	-609	3886	17.48	-10.7	0.05
157	SLU 54	-443	-613	3904	17.53	-10.82	0.05
157	SLU 55	-444	-615	3915	17.56	-10.9	0.05
157	SLU 56	-441	-609	3886	17.48	-10.7	0.05
157	SLU 57	-443	-613	3904	17.53	-10.82	0.05
157	SLU 58	-441	-609	3886	17.48	-10.7	0.05
157	SLU 59	-443	-613	3904	17.53	-10.82	0.05
157	SLU 60	-467	-644	4117	18.42	-11.35	0.05
157	SLU 61	-469	-648	4135	18.47	-11.47	0.05
157	SLU 62	-467	-644	4117	18.42	-11.35	0.05
157	SLU 63	-469	-648	4135	18.47	-11.47	0.05



Nodo Ind.	Cont. N.br.	Reazione a traslazione			Reazione a rotazione		
		x	y	z	x	y	z
157	SLU 64	-407	-573	3611	16.58	-9.79	0.05
157	SLU 65	-410	-579	3640	16.66	-9.99	0.05
157	SLU 66	-407	-573	3611	16.58	-9.79	0.05
157	SLU 67	-408	-576	3628	16.63	-9.91	0.05
157	SLU 68	-410	-579	3640	16.66	-9.99	0.05
157	SLU 69	-407	-573	3611	16.58	-9.79	0.05
157	SLU 70	-408	-576	3628	16.63	-9.91	0.05
157	SLU 71	-407	-573	3611	16.58	-9.79	0.05
157	SLU 72	-408	-576	3628	16.63	-9.91	0.05
157	SLU 73	-471	-660	4180	18.85	-11.51	0.06
157	SLU 74	-468	-654	4151	18.76	-11.32	0.06
157	SLU 75	-469	-657	4168	18.81	-11.43	0.06
157	SLU 76	-471	-660	4180	18.85	-11.51	0.06
157	SLU 77	-468	-654	4151	18.76	-11.32	0.06
157	SLU 78	-469	-657	4168	18.81	-11.43	0.06
157	SLU 79	-468	-654	4151	18.76	-11.32	0.06
157	SLU 80	-469	-657	4168	18.81	-11.43	0.06
157	SLU 81	-494	-689	4382	19.7	-11.97	0.06
157	SLU 82	-496	-692	4400	19.75	-12.09	0.06
157	SLU 83	-494	-689	4382	19.7	-11.97	0.06
157	SLU 84	-496	-692	4400	19.75	-12.09	0.06
157	SLE RA 1	-307	-431	2719	12.47	-7.4	0.04
157	SLE RA 2	-309	-435	2739	12.53	-7.53	0.04
157	SLE RA 3	-307	-431	2719	12.47	-7.4	0.04
157	SLE RA 4	-308	-433	2731	12.5	-7.47	0.04
157	SLE RA 5	-309	-435	2739	12.53	-7.53	0.04
157	SLE RA 6	-307	-431	2719	12.47	-7.4	0.04
157	SLE RA 7	-308	-433	2731	12.5	-7.47	0.04
157	SLE RA 8	-307	-431	2719	12.47	-7.4	0.04
157	SLE RA 9	-308	-433	2731	12.5	-7.47	0.04
157	SLE RA 10	-350	-489	3099	13.98	-8.54	0.04
157	SLE RA 11	-348	-485	3079	13.93	-8.41	0.04
157	SLE RA 12	-349	-487	3091	13.96	-8.49	0.04
157	SLE RA 13	-350	-489	3099	13.98	-8.54	0.04
157	SLE RA 14	-348	-485	3079	13.93	-8.41	0.04
157	SLE RA 15	-349	-487	3091	13.96	-8.49	0.04
157	SLE RA 16	-348	-485	3079	13.93	-8.41	0.04
157	SLE RA 17	-349	-487	3091	13.96	-8.49	0.04
157	SLE RA 18	-365	-508	3234	14.55	-8.85	0.04
157	SLE RA 19	-366	-510	3245	14.58	-8.93	0.04
157	SLE RA 20	-365	-508	3234	14.55	-8.85	0.04
157	SLE RA 21	-366	-510	3245	14.58	-8.93	0.04
157	SLE FR 1	-307	-431	2719	12.47	-7.4	0.04
157	SLE FR 2	-307	-432	2723	12.48	-7.42	0.04
157	SLE FR 3	-307	-431	2719	12.47	-7.4	0.04
157	SLE FR 4	-325	-455	2877	13.11	-7.86	0.04
157	SLE FR 5	-324	-454	2873	13.1	-7.83	0.04
157	SLE FR 6	-336	-469	2976	13.51	-8.12	0.04
157	SLE QP 1	-307	-431	2719	12.47	-7.4	0.04
157	SLE QP 2	-324	-454	2873	13.1	-7.83	0.04
157	SLD 1	-251	-360	2438	10.11	-5.31	-0.01
157	SLD 2	-251	-360	2438	10.11	-5.31	-0.01
157	SLD 3	-266	-448	2725	13.54	-4.74	0.03
157	SLD 4	-266	-448	2725	13.54	-4.74	0.03
157	SLD 5	-280	-292	2307	7.01	-7.95	-0.03
157	SLD 6	-280	-292	2307	7.01	-7.95	-0.03
157	SLD 7	-330	-586	3265	18.42	-6.03	0.09
157	SLD 8	-330	-586	3265	18.42	-6.03	0.09
157	SLD 9	-319	-322	2482	7.77	-9.63	-0.01
157	SLD 10	-319	-322	2482	7.77	-9.63	-0.01
157	SLD 11	-369	-616	3440	19.18	-7.72	0.1
157	SLD 12	-369	-616	3440	19.18	-7.72	0.1
157	SLD 13	-383	-460	3022	12.65	-10.93	0.05
157	SLD 14	-383	-460	3022	12.65	-10.93	0.05
157	SLD 15	-398	-548	3309	16.08	-10.35	0.09
157	SLD 16	-398	-548	3309	16.08	-10.35	0.09
157	SLV 1	-152	-223	1832	6.06	-1.79	-0.07
157	SLV 2	-152	-223	1832	6.06	-1.79	-0.07
157	SLV 3	-187	-432	2513	14.15	-0.43	0.01
157	SLV 4	-187	-432	2513	14.15	-0.43	0.01
157	SLV 5	-219	-69	1528	-1.29	-8.08	-0.11
157	SLV 6	-219	-69	1528	-1.29	-8.08	-0.11
157	SLV 7	-337	-763	3798	25.68	-3.55	0.15
157	SLV 8	-337	-763	3798	25.68	-3.55	0.15
157	SLV 9	-312	-144	1949	0.51	-12.11	-0.07
157	SLV 10	-312	-144	1949	0.51	-12.11	-0.07
157	SLV 11	-430	-839	4219	27.48	-7.58	0.19
157	SLV 12	-430	-839	4219	27.48	-7.58	0.19
157	SLV 13	-461	-476	3234	12.04	-15.23	0.07
157	SLV 14	-461	-476	3234	12.04	-15.23	0.07
157	SLV 15	-497	-684	3915	20.13	-13.87	0.15
157	SLV 16	-497	-684	3915	20.13	-13.87	0.15

## 1.3 Risposta modale

**Modo:** identificativo del modo di vibrare.



Periodo: periodo. [s]

Massa X: massa partecipante in direzione globale X. Il valore è adimensionale.

Massa Y: massa partecipante in direzione globale Y. Il valore è adimensionale.

Massa Z: massa partecipante in direzione globale Z. Il valore è adimensionale.

Massa rot. X: massa rotazionale partecipante attorno la direzione globale X. Il valore è adimensionale.

Massa rot. Y: massa rotazionale partecipante attorno la direzione globale Y. Il valore è adimensionale.

Massa rot. Z: massa rotazionale partecipante attorno la direzione globale Z. Il valore è adimensionale.

Massa sX: massa partecipante in direzione Sisma X. Il valore è adimensionale.

Massa sY: massa partecipante in direzione Sisma Y. Il valore è adimensionale.

#### Totale masse partecipanti:

Traslazione X: 0.931917

Traslazione Y: 0.942062

Traslazione Z: 0

Rotazione X: 0.903368

Rotazione Y: 0.913988

Rotazione Z: 0.929121

Modo	Periodo	Massa X	Massa Y	Massa Z	Massa rot. X	Massa rot. Y	Massa rot. Z	Massa sX	Massa sY
1	5.990848493	0.000000508	0.011671455	0	0.001968119	0.000000122	0.011487855	0.000000508	0.011671455
2	2.923420828	0.000039043	0.050857469	0	0.116573057	0.00003874	0.049445354	0.000039043	0.050857469
3	2.358228097	0.190371651	0.000279806	0	0.000392563	0.233685308	0.003519369	0.190371651	0.000279806
4	2.188181239	0.000000478	0.003471453	0	0.000609338	0.00000294	0.002925512	0.000000478	0.003471453
5	2.083864882	0.000794676	0.068131858	0	0.11627918	0.001013308	0.071415312	0.000794676	0.068131858
6	1.38627952	0.002430618	0.000027115	0	0.000043478	0.001487916	0.000089193	0.002430618	0.000027115
7	1.157230403	0.00005529	0.001625696	0	0.000263709	0.00575912	0.001050048	0.00005529	0.001625696
8	1.011985208	0.000029452	0.001535369	0	0.000338462	0.022657903	0.002151214	0.000029452	0.001535369
9	1.007829912	0.000235014	0.001033872	0	0.00019017	0.000455829	0.00077978	0.000235014	0.001033872
10	0.958304576	0.000628428	0.013321513	0	0.002158249	0.005707624	0.016020146	0.000628428	0.013321513
11	0.878992223	0.00200732	0.009645806	0	0.000462415	0.001468147	0.013157386	0.00200732	0.009645806
12	0.86618774	0.044661435	0.000101754	0	0.00150825	0.002429209	0.000041905	0.044661435	0.000101754
13	0.855737348	0.000203567	0.028757357	0	0.003441626	0.000764122	0.025366155	0.000203567	0.028757357
14	0.808888853	0.02340282	0.002977074	0	0.000030293	0.0060595	0.004762104	0.02340282	0.002977074
15	0.787382312	0.011148682	0.004960892	0	0.012574339	0.001118691	0.00680251	0.011148682	0.004960892
16	0.659228622	0.000607603	0.000113436	0	0.000139948	0.005764945	0.000063075	0.000607603	0.000113436
17	0.645087217	0.041792279	0.000009318	0	0.00027667	0.00999673	0.000893781	0.041792279	0.000009318
18	0.609612307	0.000061646	0.000558044	0	0.000112281	0.000009776	0.000500481	0.000061646	0.000558044
19	0.587256367	0.000042296	0.034344518	0	0.094633425	0.000037274	0.033799302	0.000042296	0.034344518
20	0.562379652	0.001513406	0.001293909	0	0.00050412	0.015015933	0.001253291	0.001513406	0.001293909
21	0.534368098	0.001016637	0.005503756	0	0.002314493	0.001270486	0.003813814	0.001016637	0.005503756
22	0.512946652	0.016599246	0.00605317	0	0.008238234	0.018722152	0.007979123	0.016599246	0.00605317
23	0.507622017	0.000213439	0.003141943	0	0.000378888	0.000284567	0.0028537	0.000213439	0.003141943
24	0.486040666	0.001939437	0.004422471	0	0.002498774	0.002054707	0.003944563	0.001939437	0.004422471
25	0.485355989	0.000292216	0.000003523	0	0.000428586	0.000292955	0.000010094	0.000292216	0.000003523
26	0.476286982	0.000175278	0.000093807	0	0.000054178	0.000610583	0.000020021	0.000175278	0.000093807
27	0.460914746	0.000265736	0.001109281	0	0.000209962	0.000275481	0.000613624	0.000265736	0.001109281
28	0.448345831	0.000703713	0.000349676	0	0.000669877	0.001057877	0.000220629	0.000703713	0.000349676
29	0.424808716	0.006571811	0.004575026	0	0.004149553	0.010956613	0.004667516	0.006571811	0.004575026
30	0.414430027	0.001176941	0.003646994	0	0.000034531	0.000001301	0.004701831	0.001176941	0.003646994
31	0.408141863	0.002458619	0.0035668	0	0.001281599	0.000834907	0.004772587	0.002458619	0.0035668
32	0.390990909	0.000413738	0.003507437	0	0.000012067	0.000340897	0.003624344	0.000413738	0.003507437
33	0.373246742	0.001629738	0.000719098	0	0.000002227	0.000043992	0.000631617	0.001629738	0.000719098
34	0.359100871	0.000000853	0.004029686	0	0.000530036	0.000015614	0.004219129	0.000000853	0.004029686
35	0.335815075	0.000801966	0.013758424	0	0.004671892	0.000142661	0.014380541	0.000801966	0.013758424
36	0.327205666	0.005343105	0.003568241	0	0.001521125	0.000069859	0.00212294	0.005343105	0.003568241
37	0.308228285	0.002806823	0.00049548	0	0.000197344	0.001404319	0.0005089	0.002806823	0.00049548
38	0.299480851	0.000046638	0.01884276	0	0.006639664	0.000174754	0.017188564	0.000046638	0.01884276
39	0.264336934	0.002478359	0.014175144	0	0.000618745	0.006631214	0.013313734	0.002478359	0.014175144
40	0.252944556	0.014002292	0.006581177	0	0.001420879	0.026585962	0.004857607	0.014002292	0.006581177
41	0.231896301	0.000159254	0.010272573	0	0.009986174	0.000308183	0.011436534	0.000159254	0.010272573
42	0.229727868	0.030602138	0.000024242	0	0.000162471	0.022579114	0.000042268	0.030602138	0.000024242
43	0.185152445	0.008089168	0.012917158	0	0.012282037	0.029352372	0.011372103	0.008089168	0.012917158
44	0.182880844	0.055034921	0.00001649	0	0.000873504	0.057163773	0.000049241	0.055034921	0.00001649
45	0.161096739	0.027042744	0.005574071	0	0.012059418	0.047583089	0.004842932	0.027042744	0.005574071
46	0.142700663	0.003355043	0.024491278	0	0.03825626	0.002323123	0.019973787	0.003355043	0.024491278
47	0.116157507	0.029278159	0.00086698	0	0.000007738	0.001529979	0.000346666	0.029278159	0.00086698
48	0.113698443	0.005550244	0.052045385	0	0.068107215	0.01219542	0.043398746	0.005550244	0.052045385
49	0.06818303	0.040067036	0.05744137	0	0.057804982	0.063947288	0.053016185	0.040067036	0.05744137
50	0.062977033	0.081436695	0.035373144	0	0.040113435	0.127977142	0.052821353	0.081436695	0.035373144
51	0.037912491	0.014942131	0.387103512	0	0.258597096	0.009382483	0.376597856	0.014942131	0.387103512
52	0.035660874	0.246418209	0.021965464	0	0.013070252	0.152644828	0.012846135	0.246418209	0.021965464
53	0.025179833	0.004108667	0.000008487	0	0.000005485	0.000130571	0.000261475	0.004108667	0.000008487
54	0.02249889	0.006042027	0.00073517	0	0.000055954	0.00116167	0.00175663	0.006042027	0.00073517
55	0.017856089	0.000127614	0.00000618	0	0.000250789	0.000004946	0.00000001	0.000127614	0.00000618
56	0.01645149	0.00000071	0.000006963	0	0.000031796	0.000009943	0.000001349	0.00000071	0.000006963
57	0.015116211	0.000181189	0.000005184	0	0.000063045	0.000000009	0.000004878	0.000181189	0.000005184
58	0.013532836	0.000163397	0.000041617	0	0.000157398	0.000000761	0.000039655	0.000163397	0.000041617
59	0.0118209	0.000036629	0.000064379	0	0.000076484	0.000076817	0.000115654	0.000036629	0.000064379
60	0.010751992	0.000317755	0.000241166	0	0.000033864	0.000372187	0.000229078	0.000317755	0.000241166



## 1.4 Equilibrio globale forze

**Contributo:** Nome attribuito al sistema risultante.

**Fx:** Componente X di forza del sistema risultante. [daN]

**Fy:** Componente Y di forza del sistema risultante. [daN]

**Fz:** Componente Z di forza del sistema risultante. [daN]

**Mx:** Componente di momento attorno l'asse X del sistema risultante. [daN\*m]

**My:** Componente di momento attorno l'asse Y del sistema risultante. [daN\*m]

**Mz:** Componente di momento attorno l'asse Z del sistema risultante. [daN\*m]

**Bilancio in condizione di carico: Pesi strutturali**

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	-0.018	-4.337	-217251.061	-150526.6	-6383137.72	111.88
Reazioni	0.018	4.337	217251.061	150526.6	6383137.72	-111.88
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

**Bilancio in condizione di carico: Permanenti portati**

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	0	-43333.2	-39554.62	-1275950.25	0
Reazioni	0	0	43333.2	39554.62	1275950.25	0
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

**Bilancio in condizione di carico: Variabile A**

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	0	-56704.354	-52463.53	-1669070.21	0
Reazioni	0	0	56704.354	52463.53	1669070.21	0
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

**Bilancio in condizione di carico: Vento**

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	986.993	0	0	0	3213.71	-961.51
Reazioni	-986.993	0	0	0	-3213.71	961.51
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

**Bilancio in condizione di carico: Sisma X SLV**

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	61090.996	0	0	0	230484.91	-46446.27
Reazioni	-61090.996	0	0	0	-230484.91	46446.27
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

**Bilancio in condizione di carico: Sisma Y SLV**

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	61545.154	0	-232198.36	0	-1803029.45
Reazioni	0	-61545.154	0	232198.36	0	1803029.45
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

**Bilancio in condizione di carico: Sisma X SLD**

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	25858.667	0	0	0	97559.92	-19659.83
Reazioni	-25858.667	0	0	0	-97559.92	19659.83
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

**Bilancio in condizione di carico: Sisma Y SLD**

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	26083.2	0	-98407.04	0	-764134.55
Reazioni	0	-26083.2	0	98407.04	0	764134.55
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

**Bilancio in condizione di carico: Rig Ux**

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	0	0	0	0	0
Reazioni	0	0	0	0	0	0
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

**Bilancio in condizione di carico: Rig Uy**

Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	0	0	0	0	0
Reazioni	0	0	0	0	0	0
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

**Bilancio in condizione di carico: Rig Rz**

Contributo	Fx	Fy	Fz	Mx	My	Mz
------------	----	----	----	----	----	----





Contributo	Fx	Fy	Fz	Mx	My	Mz
Forze applicate	0	0	0	0	0	0
Reazioni	0	0	0	0	0	0
P-Delta	0	0	0	0	0	0
Totale	0	0	0	0	0	0

## 1.5 Risposta di spettro

**Spettro:** condizione elementare corrispondente allo spettro.

**N.b.:** nome breve della condizione elementare.

**Fx:** componente della forza lungo l'asse X. [daN]

**Fy:** componente della forza lungo l'asse Y. [daN]

**Fz:** componente della forza lungo l'asse Z. [daN]

**Mx:** componente della coppia attorno all'asse X. [daN\*m]

**My:** componente della coppia attorno all'asse Y. [daN\*m]

**Mz:** componente della coppia attorno all'asse Z. [daN\*m]

**Max X:** massima reazione lungo l'asse X.

**Valore:** valore massimo della reazione. [daN]

**Angolo:** angolo d'ingresso del sisma che provoca il valore massimo della reazione. [deg]

**Max Y:** massima reazione lungo l'asse Y.

**Valore:** valore massimo della reazione. [daN]

**Angolo:** angolo d'ingresso del sisma che provoca il valore massimo della reazione. [deg]

**Max Z:** massima reazione lungo l'asse Z.

**Valore:** valore massimo della reazione. [daN]

**Angolo:** angolo d'ingresso del sisma che provoca il valore massimo della reazione. [deg]

Spettro	Fx	Fy	Fz	Mx	My	Mz	Max X		Max Y		Max Z	
N.b.							Valore	Angolo	Valore	Angolo	Valore	Angolo
SLV X	20859.52	4976.26	0	15826.948	5.956E04	1.529E05	20872.92	2	27169.16	92	0	0
SLV Y	4976.26	27146.85	0	7.184E04	1.762E04	7.918E05	20872.92	2	27169.16	92	0	0
X SLD	8778.14	2121.77	0	6760.2797	2.513E04	6.515E04	8784.12	2	11509.3	92	0	0
Y SLD	2121.77	11500.1	0	3.040E04	7543.0939	3.354E05	8784.12	2	11509.3	92	0	0

## 1.6 Annotazioni solutore

**Informazioni:** informazioni fornite dal solutore al termine del calcolo del modello.

Informazioni

## 1.7 Statistiche soluzione

Tipo di equazioni	Lineari
Tecnica di soluzione	Intel MKL PARDISO
Numero equazioni	13458
Elemento min. diagonale	298.28366608
Elemento max diagonale	980142702.572534
Rapporto max/min	3285941.58524654
Elementi non nulli	480948

# 2 Verifiche

## 2.1 Verifica regolarità strutturale

Le unità di misura elencate nel capitolo sono in [m, daN] ove non espressamente specificato.

**Livello:**

**Descr:** descrizione livello.

**Quota:** quota livello. [m]

**Q:** quota livello. [m]

**Qinf:** quota livello precedente. [m]

**Comb:** combinazione.

**A1:** a1 (Distribuzione masse).

**A1n:** a1 numeratore (distanza tra centro massa vs. centro rigidezza [se presente] o centro dell'ingombro del piano). [m]

**A1d:** a1 denominatore (ingombro del piano nella medesima direzione [x o y globale]). [m]

**A1r:** a1 rapporto (distanza centro massa/rigidezza su ingombro del piano).



**A2:** a2 (Distribuzione rigidezze).  
**A2n:** a2 numeratore (rigidezza max [x o y globale]).  
**A2d:** a2 denominatore (rigidezza min [x o y globale]).  
**A2r:** a2 rapporto (rigidezza max/min).  
**A3:** a3 (Forma compatta).  
**A3n:** a3 numeratore (area convessa). [m<sup>2</sup>]  
**A3d:** a3 denominatore (area piano). [m<sup>2</sup>]  
**A3r:** a3 rapporto (area convessa/area piano).  
**B:** b (Rapporto lati).  
**Bn:** b numeratore (lato max [x o y globale]). [m]  
**Bd:** b denominatore (lato min [x o y globale]). [m]  
**Br:** b rapporto (lato max/min).  
**C:** c (Rapporto rigidezze piano).  
**Cn:** c numeratore (rigidezza elementi verticali).  
**Cd:** c denominatore (rigidezza piano).  
**Cr:** c rapporto (rigidezza elementi verticali/rigidezza piano).  
**E1:** e1 (Variazione masse).  
**E1n:** e1 numeratore (massa max). [daN]  
**E1d:** e1 denominatore (massa min). [daN]  
**E1r:** e1 rapporto (massa max/min).  
**E2:** e2 (Riduzione rigidezze).  
**E2n:** e2 numeratore (rigidezza relativa alla traslazione KUmax). [daN/m]  
**E2d:** e2 denominatore (rigidezza relativa alla traslazione KUmin). [daN/m]  
**E2r:** e2 rapporto (variazione massima in decremento Kmax/Kmin).  
**E3:** e3 (Incremento rigidezze).  
**E3n:** e3 numeratore (rigidezza relativa alla traslazione KUmax). [daN/m]  
**E3d:** e3 denominatore (rigidezza relativa alla traslazione KUmin). [daN/m]  
**E3r:** e3 rapporto (variazione massima in incremento Kmax/Kmin).  
**F:** f (Rapporto Capacità/Domanda).  
**Fn:** f numeratore (rapporto capacità/domanda massimo [c/d max]). [daN]  
**Fd:** f denominatore (rapporto capacità/domanda minimo [c/d min]). [daN]  
**Fr:** f rapporto (variazione massima [rapporto (c/d max)/(c/d min)]).  
**G1:** g1 (Rastremazione di piano).  
**G1n:** g1 numeratore (L1). [m]  
**G1d:** g1 denominatore (L2). [m]  
**G1r:** g1 rapporto (L1/L2).  
**G2:** g2 (Rastremazione totale).  
**G2n:** g2 numeratore (L0). [m]  
**G2d:** g2 denominatore (Li). [m]  
**G2r:** g2 rapporto (L0/Li).  
**Capacità/Domanda in X:**  
**VrdX:** taglio resistente complessivo in direzione X. [daN]  
**VedX:** taglio agente complessivo in direzione X. [daN]  
**|Rd/Ed|:** |Rd/Ed| (rapporto capacità/domanda in termini di resistenza a taglio).  
**Capacità/Domanda in Y:**  
**VrdY:** taglio resistente complessivo in direzione Y. [daN]  
**VedY:** taglio agente complessivo in direzione Y. [daN]

#### Verifica regolarità strutturale

Controllo regolarità edificio secondo D.M. 17-01-18 (N.T.C.) §7.2.1 - §C7.2.1

##### Avvertenze

La seguente procedura valuta la regolarità della costruzione secondo quanto indicato nelle NTC 2018 §7.2.1.

Tali valutazioni sono a carattere puramente informativo e vengono condotte sulla base del modello e delle verifiche presenti alla sua generazione, con le limitazioni indicate nella manualistica.

In ogni caso l'impostazione di regolarità della costruzione, in pianta ed elevazione, va indicata nelle preferenze di analisi dall'utente utilizzatore del software.

##### Sintesi dei risultati

Orizzontamenti considerati nella valutazione

Nessun livello di fondazione trovato

Livelli di elevazione considerati: Rialzato(L2), Primo(L3),

Regolarità in pianta - NO

L'edificio risulta NON regolare in pianta, in base alle condizioni indicate in NTC 2018 §7.2.1

Ok - Criterio A1 (Distribuzione masse) rispettato, con rapporto massimo 0,01 (limite=0,2) al livello Primo

N.V. - Criterio A2 (Distribuzione rigidezze) non valutabile al livello Rialzato

Ok - Criterio A3 (Forma compatta) rispettato, con rapporto massimo 0,99 (limite=1,05) al livello Primo

Ok - Criterio B (Rapporto lati) rispettato, con rapporto massimo 1,02 (limite=4) al livello Rialzato

No - Criterio C (Rapporto rigidezze piano) NON rispettato, con rapporto massimo > 999 (limite=0) al livello Rialzato

Regolarità in altezza - NO

L'edificio risulta NON regolare in altezza, in base alle condizioni indicate in NTC 2018 §7.2.1

Ok - Criterio D (Altezza elementi sismoresistenti) rispettato, con rapporto massimo 1 (limite=1,01)

Ok - Criterio E1 (Variazione masse) rispettato, con rapporto massimo 1,06 (limite=1,25) tra il livello Primo ed il precedente



N.V. - Criterio E2 (Riduzione rigidezze) non valutabile tra il livello Primo ed il precedente  
N.V. - Criterio E3 (Incremento rigidezze) non valutabile tra il livello Primo ed il precedente  
No - Criterio F (Rapporto Capacità/Domanda) NON rispettato, con rapporto massimo 30.3/10.3=2.9 (limite=1,3) tra il livello Primo ed il precedente  
Ok - Criterio G1 (Rastremazione di piano) rispettato, con rapporto massimo 0,01 (limite=0,1) tra il livello Primo ed il precedente  
Ok - Criterio G2 (Rastremazione totale) rispettato, con rapporto massimo 0,01 (limite=0,3) tra il livello Primo ed il precedente

#### Valori per piano

##### Verifiche di regolarità in pianta

Livello		A1			A2			A3			B			C		
Descr	Quota	A1n	A1d	A1r	A2n	A2d	A2r	A3n	A3d	A3r	Bn	Bd	Br	Cn	Cd	Cr
Rialzato	1.39	0.02	9.81	0				97.9584	99.9682	0.98	10.03	9.81	1.02	9999	1	9999
Primo	5.15	0.06	9.88	0.01				95.7597	97.1096	0.99	9.88	9.73	1.02	9999	1	9999

##### Verifiche di regolarità in elevazione

Rapporto di regolarità per la condizione D (Altezza elementi sismoresistenti): 3.76/3.76=0.01.

Livello		E1			E2			E3			F			G1			G2			
Descr	Q	Qinf	E1n	E1d	E1r	E2n	E2d	E2r	E3n	E3d	E3r	Fn	Fd	Fr	G1n	G1d	G1r	G2n	G2d	G2r
Primo	5.15	1.39	69371	65316	1.06							30.3	10.3	2.93	0.08	10.03	0.01	0.08	10.03	0.01

##### Dettaglio delle resistenze di piano a taglio (per valutazione punto F)

Livello			Capacità/Domanda in X			Capacità/Domanda in Y		
Descr	Q	Comb	VrdX	VedX	Rd/Ed	VrdY	VedY	Rd/Ed
Rialzato	1.39	SLV 1	66030	-21448	3.1	98686	-3255	30.3
Rialzato	1.39	SLV 2	66030	-21448	3.1	98686	-3255	30.3
Rialzato	1.39	SLV 3	66133	-21101	3.1	83753	10714	7.8
Rialzato	1.39	SLV 4	66133	-21101	3.1	83753	10714	7.8
Rialzato	1.39	SLV 5	73092	-6961	10.5	96109	-22166	4.3
Rialzato	1.39	SLV 6	73092	-6961	10.5	96109	-22166	4.3
Rialzato	1.39	SLV 7	74585	-5803	12.9	89405	24397	3.7
Rialzato	1.39	SLV 8	74585	-5803	12.9	89405	24397	3.7
Rialzato	1.39	SLV 9	78447	5803	13.5	95425	-24406	3.9
Rialzato	1.39	SLV 10	78447	5803	13.5	95425	-24406	3.9
Rialzato	1.39	SLV 11	78286	6961	11.2	98633	22157	4.5
Rialzato	1.39	SLV 12	78286	6961	11.2	98633	22157	4.5
Rialzato	1.39	SLV 13	79297	21101	3.8	98712	-10722	9.2
Rialzato	1.39	SLV 14	79297	21101	3.8	98712	-10722	9.2
Rialzato	1.39	SLV 15	80989	21448	3.8	100143	3247	30.8
Rialzato	1.39	SLV 16	80989	21448	3.8	100143	3247	30.8
Primo	5.15	SLV 1	39486	-8007	4.9	29012	-2805	10.3
Primo	5.15	SLV 2	39486	-8007	4.9	29012	-2805	10.3
Primo	5.15	SLV 3	39503	-7623	5.2	25354	3434	7.4
Primo	5.15	SLV 4	39503	-7623	5.2	25354	3434	7.4
Primo	5.15	SLV 5	39457	-2984	13.2	33164	-10303	3.2
Primo	5.15	SLV 6	39457	-2984	13.2	33164	-10303	3.2
Primo	5.15	SLV 7	39511	-1705	23.2	25824	10492	2.5
Primo	5.15	SLV 8	39511	-1705	23.2	25824	10492	2.5
Primo	5.15	SLV 9	39199	1705	23	33631	-10492	3.2
Primo	5.15	SLV 10	39199	1705	23	33631	-10492	3.2
Primo	5.15	SLV 11	39502	2984	13.2	32000	10303	3.1
Primo	5.15	SLV 12	39502	2984	13.2	32000	10303	3.1
Primo	5.15	SLV 13	39456	7623	5.2	33694	-3434	9.8
Primo	5.15	SLV 14	39456	7623	5.2	33694	-3434	9.8
Primo	5.15	SLV 15	39472	8007	4.9	35810	2805	12.8
Primo	5.15	SLV 16	39472	8007	4.9	35810	2805	12.8

## 2.2 Verifica sismica globale

**Desc.:** descrizione.

**Stato limite:** (muratura) V=Taglio; PF=Pressoflessione; PFFP=Pressoflessione fuori piano; R=Ribaltamento.

**Molt.:** moltiplicatore minimo della azione sismica che produce lo stato limite.

**Comb.:** combinazione.

**PGA:** accelerazione al suolo.

**iPGA (ZE):** indicatore di rischio sismico in termini di PGA ovvero rapporto tra l'azione sismica massima sopportabile dall'elemento e l'azione sismica massima che si utilizzerebbe nel progetto nuovo (§C8.3).

**TR:** tempo di ritorno.

**(TR/TRrif)^.41:** indicatore di rischio sismico in termini di periodo di ritorno.

**fa:** fattore di accelerazione.

**Stato limite:** (muratura) V=Taglio; PF=Presso flessione; PFFP=Pressoflessione fuori piano; R=Ribaltamento.

**Coeff.s.:** coefficiente minimo prodotto dallo stato limite.

**Verifica:** stato di verifica.

**Maschio:** maschio.

**Stato limite:** (maschio muratura) V=Taglio; PF=Presso flessione; PFFP=Presso flessione fuori piano; R=Ribaltamento.

**Trave:** trave di collegamento in muratura.

**Stato limite:** (trave muratura) V=Taglio; F=Flessione.

**S. L.:** stato limite di riferimento.

**TR,C:** periodo di ritorno di capacità.

**PGA,C:** accelerazione di aggancio di capacità.



**TR,Rif:** periodo di ritorno di riferimento.

**PGA,Rif:** accelerazione di aggancio di riferimento.

**Tipo rottura:** tipo di rottura che fornisce il valore minimo degli elementi considerati.

**PAM:** perdita media annua attesa.

**Classe PAM:** classe di rischio PAM.

**IS-V:** indice di sicurezza.

**Classe IS-V:** classe di rischio IS-V.

## Verifica di elementi dotati di indicatori di rischio sismico mediante analisi con fattore q

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.) § C8.7.1

### Accelerazioni e tempi di ritorno

Accelerazione di aggancio SLO ( $ag/g_{SLO} \cdot S \cdot ST$ )  $PGA, SLOrif = 0.081$

Accelerazione di aggancio SLD ( $ag/g_{SLD} \cdot S \cdot ST$ )  $PGA, SLDrif = 0.101$

Accelerazione di aggancio SLV ( $ag/g_{SLV} \cdot S \cdot ST$ )  $PGA, SLVrif = 0.244$

$Tr, SLOrif = 30$  anni

$Tr, SLDrif = 50$  anni

$Tr, SLVrif = 475$  anni

### Moltiplicatori minimi delle condizioni sismiche

(Il valore di  $\zeta E$  corrisponde al valore di I.R. PGA secondo quanto riportato nella Circolare 7 21-01-19 §C8.3)

#### Rottura a taglio

Moltiplicatore: 0

Maschio 4

Lunghezza: 2.535; altezza: 2.69; spessore: 0.45; sezione a quota: 1.39

Combinazione SLV 1 N = -654 V par. = 112 I' = 0 fvd = 8333 Vt scorrimento = 0 Vt fess. diag. = 0

Tempo di ritorno 0 anni

Indicatore  $iTr = (Tr/Tr, SLVrif)^{.41} = 0$

PGA 0

Indicatore  $iPGA = PGA/PGA, SLVrif = 0$

Fattore di accelerazione  $fa = 0$

#### Rottura a flessione

Moltiplicatore: 0

Maschio 4

Lunghezza: 2.535; altezza: 2.69; spessore: 0.45 sezione a quota 1.39

Combinazione SLV 1 N = -654 M = 837.13  $\sigma_0 = 0$  fd = 143750 Mu = 0

Tempo di ritorno 0 anni

Indicatore  $iTr = (Tr/Tr, SLVrif)^{.41} = 0$

PGA 0

Indicatore  $iPGA = PGA/PGA, SLVrif = 0$

Fattore di accelerazione  $fa = 0$

#### Rottura a pressoflessione nel piano ortogonale

Moltiplicatore: 0.228

Maschio 33

Lunghezza: 0.58; altezza: 3.76; spessore: 0.14; sezione a quota: 3.27

Combinazione SLV 3 fd = 143750 Ta = 0.17 Wa = 252 N = -136 M = 9.36 Mc = 9.4

Tempo di ritorno 11 anni

Indicatore  $iTr = (Tr/Tr, SLVrif)^{.41} = 0.214$

PGA 0.053

Indicatore  $iPGA = PGA/PGA, SLVrif = 0.218$

Fattore di accelerazione  $fa = 0.2124$

#### Rottura per meccanismi locali di collasso

Moltiplicatore: 0.014

Maschio 33

Lunghezza: 0.58; altezza: 3.76; spessore: 0.14 f.agg. = 0 a.lim. = 0.197821

Combinazione SLV 13 N top = -6 N base = -1 T orto = -5  $\alpha_0 = 0.018 M^* = 56 e^* = 0.99 a_0^* = 0.1323$

Tempo di ritorno 0 anni

Indicatore  $iTr = (Tr/Tr, SLVrif)^{.41} = 0$

PGA 0

Indicatore  $iPGA = PGA/PGA, SLVrif = 0$

Fattore di accelerazione  $fa = 0$

### Indicatori minimi riferiti al solo materiale muratura

Desc.	Stato limite	Molt.	Comb.	PGA	IPGA ( $\zeta E$ )	TR	$(Tr/Trrif)^{.41}$	fa
Maschio 4	PF	0	SLV 1	0	0	0	0	0
Maschio 4	V	0	SLV 1	0	0	0	0	0
Maschio 33	PFFP	0.228	SLV 3	0.0534	0.2184	11	0.2136	0.2124
Maschio 33	R	0.014	SLV 13	0	0	0	0	0
Trave di accoppiamento 20	PF	0	SLV 1	0	0	0	0	0
Trave di accoppiamento 1	V	0	SLV 1	0	0	0	0	0



# Coefficienti di sicurezza riferiti al solo materiale muratura

Desc.	Stato limite	Coeff.s.	Comb.	Verifica
Maschio 1	PF SLU	9.026	SLU 81	Si
Maschio 1	V SLU	4.205	SLU 81	Si
Maschio 1	PF	5.403	SLV 5	Si
Maschio 1	V	3.255	SLV 9	Si
Maschio 1	PFFP	10.348	SLV 15	Si
Maschio 1	R	0.134	SLV 1	No
Maschio 2	PF SLU	36.671	SLU 65	Si
Maschio 2	V SLU	38.873	SLU 82	Si
Maschio 2	PF	13.138	SLV 11	Si
Maschio 2	V	3.419	SLV 9	Si
Maschio 2	PFFP	15.021	SLV 13	Si
Maschio 2	R	0.08	SLV 3	No
Maschio 3	PF SLU	11.292	SLU 81	Si
Maschio 3	V SLU	3.093	SLU 81	Si
Maschio 3	PF	5.251	SLV 13	Si
Maschio 3	V	2.696	SLV 11	Si
Maschio 3	PFFP	13.782	SLV 13	Si
Maschio 3	R	0.104	SLV 1	No
Maschio 4	PF SLU	0	SLU 1	No
Maschio 4	V SLU	0	SLU 1	No
Maschio 4	PF	0	SLV 4	No
Maschio 4	V	0	SLV 1	No
Maschio 4	PFFP	3.468	SLV 1	Si
Maschio 4	R	0	SLV 4	No
Maschio 5	PF SLU	18.35	SLU 39	Si
Maschio 5	V SLU	4.543	SLU 81	Si
Maschio 5	PF	7.134	SLV 1	Si
Maschio 5	V	2.564	SLV 1	Si
Maschio 5	PFFP	11.666	SLV 11	Si
Maschio 5	R	0.115	SLV 9	No
Maschio 8	PF SLU	9.642	SLU 44	Si
Maschio 8	V SLU	2.951	SLU 82	Si
Maschio 8	PF	0	SLV 6	No
Maschio 8	V	0	SLV 1	No
Maschio 8	PFFP	0	SLV 6	No
Maschio 8	R	0	SLV 4	No
Maschio 9	PF SLU	7.463	SLU 40	Si
Maschio 9	V SLU	13.039	SLU 81	Si
Maschio 9	PF	5.936	SLV 9	Si
Maschio 9	V	4.59	SLV 1	Si
Maschio 9	PFFP	9.561	SLV 9	Si
Maschio 9	R	0.086	SLV 5	No
Maschio 11	PF SLU	5.529	SLU 82	Si
Maschio 11	V SLU	8.134	SLU 82	Si
Maschio 11	PF	2.006	SLV 13	Si
Maschio 11	V	4.916	SLV 13	Si
Maschio 11	PFFP	10.057	SLV 9	Si
Maschio 11	R	0.127	SLV 3	No
Maschio 12	PF SLU	5.629	SLU 2	Si
Maschio 12	V SLU	9.24	SLU 81	Si
Maschio 12	PF	2.432	SLV 3	Si
Maschio 12	V	3.037	SLV 13	Si
Maschio 12	PFFP	6.149	SLV 7	Si
Maschio 12	R	0.082	SLV 5	No
Maschio 13	PF SLU	1.378	SLU 39	Si
Maschio 13	V SLU	2.221	SLU 81	Si
Maschio 13	PF	1.351	SLV 3	Si
Maschio 13	V	1.497	SLV 15	Si
Maschio 13	PFFP	7.301	SLV 13	Si
Maschio 13	R	0.073	SLV 7	No
Maschio 14	PF SLU	0	SLU 84	No
Maschio 14	V SLU	0	SLU 1	No
Maschio 14	PF	0	SLV 16	No
Maschio 14	V	0	SLV 3	No
Maschio 14	PFFP	13.774	SLV 9	Si
Maschio 14	R	0	SLV 16	No
Maschio 15	PF SLU	23.983	SLU 82	Si
Maschio 15	V SLU	388.066	SLU 2	Si
Maschio 15	PF	13.795	SLV 11	Si
Maschio 15	V	3.533	SLV 11	Si
Maschio 15	PFFP	13.093	SLV 7	Si
Maschio 15	R	0.047	SLV 3	No
Maschio 18	PF SLU	2.497	SLU 39	Si
Maschio 18	V SLU	3.613	SLU 81	Si
Maschio 18	PF	0	SLV 9	No
Maschio 18	V	0	SLV 9	No
Maschio 18	PFFP	13.081	SLV 13	Si
Maschio 18	R	0.022	SLV 13	No
Maschio 19	PF SLU	1.379	SLU 81	Si
Maschio 19	V SLU	0.656	SLU 81	No
Maschio 19	PF	1.265	SLV 7	Si
Maschio 19	V	1.134	SLV 7	Si
Maschio 19	PFFP	15.457	SLV 13	Si
Maschio 19	R	0.07	SLV 3	No
Maschio 20	PF SLU	19.857	SLU 39	Si
Maschio 20	V SLU	18.722	SLU 81	Si
Maschio 20	PF	0	SLV 4	No



Desc.	Stato limite	Coeff.s.	Comb.	Verifica
Maschio 20	V	0	SLV 1	No
Maschio 20	PFFP	2.32	SLV 3	Si
Maschio 20	R	0	SLV 4	No
Maschio 21	PF SLU	4.72	SLU 39	Si
Maschio 21	V SLU	164.926	SLU 39	Si
Maschio 21	PF	1.569	SLV 3	Si
Maschio 21	V	3.236	SLV 7	Si
Maschio 21	PFFP	9.39	SLV 3	Si
Maschio 21	R	0.111	SLV 13	No
Maschio 23	PF SLU	2.557	SLU 10	Si
Maschio 23	V SLU	4.197	SLU 39	Si
Maschio 23	PF	0	SLV 5	No
Maschio 23	V	0	SLV 5	No
Maschio 23	PFFP	1.482	SLV 15	Si
Maschio 23	R	0	SLV 3	No
Maschio 24	PF SLU	4.3	SLU 40	Si
Maschio 24	V SLU	12.151	SLU 82	Si
Maschio 24	PF	3.543	SLV 15	Si
Maschio 24	V	2.786	SLV 11	Si
Maschio 24	PFFP	2.415	SLV 13	Si
Maschio 24	R	0	SLV 1	No
Maschio 25	PF SLU	1.509	SLU 40	Si
Maschio 25	V SLU	11.783	SLU 39	Si
Maschio 25	PF	0	SLV 16	No
Maschio 25	V	0	SLV 5	No
Maschio 25	PFFP	1.023	SLV 13	Si
Maschio 25	R	0	SLV 16	No
Maschio 26	PF SLU	8.357	SLU 39	Si
Maschio 26	V SLU	91.854	SLU 39	Si
Maschio 26	PF	2.692	SLV 1	Si
Maschio 26	V	3.042	SLV 1	Si
Maschio 26	PFFP	1.345	SLV 3	Si
Maschio 26	R	0.059	SLV 9	No
Maschio 27	PF SLU	3.12	SLU 39	Si
Maschio 27	V SLU	4.75	SLU 39	Si
Maschio 27	PF	1.626	SLV 1	Si
Maschio 27	V	1.982	SLV 1	Si
Maschio 27	PFFP	1.834	SLV 9	Si
Maschio 27	R	0	SLV 1	No
Maschio 28	PF SLU	58.49	SLU 2	Si
Maschio 28	V SLU	50.846	SLU 2	Si
Maschio 28	PF	1.957	SLV 1	Si
Maschio 28	V	2.424	SLV 1	Si
Maschio 28	PFFP	2.568	SLV 11	Si
Maschio 28	R	0.095	SLV 11	No
Maschio 29	PF SLU	3.159	SLU 40	Si
Maschio 29	V SLU	5.673	SLU 40	Si
Maschio 29	PF	2.204	SLV 1	Si
Maschio 29	V	2.46	SLV 13	Si
Maschio 29	PFFP	1.752	SLV 5	Si
Maschio 29	R	0.036	SLV 5	No
Maschio 31	PF SLU	0	SLU 1	No
Maschio 31	V SLU	0	SLU 1	No
Maschio 31	PF	0	SLV 1	No
Maschio 31	V	0	SLV 1	No
Maschio 31	PFFP	3.315	SLV 13	Si
Maschio 31	R	0.117	SLV 1	No
Maschio 32	PF SLU	0	SLU 1	No
Maschio 32	V SLU	0	SLU 1	No
Maschio 32	PF	0	SLV 14	No
Maschio 32	V	0	SLV 1	No
Maschio 32	PFFP	0	SLV 14	No
Maschio 32	R	0.035	SLV 15	No
Maschio 33	PF SLU	0	SLU 84	No
Maschio 33	V SLU	0	SLU 1	No
Maschio 33	PF	0	SLV 16	No
Maschio 33	V	0	SLV 1	No
Maschio 33	PFFP	0	SLV 8	No
Maschio 33	R	0	SLV 16	No
Maschio 34	PF SLU	11.413	SLU 82	Si
Maschio 34	V SLU	18.334	SLU 39	Si
Maschio 34	PF	0	SLV 4	No
Maschio 34	V	0	SLV 1	No
Maschio 34	PFFP	0	SLV 4	No
Maschio 34	R	0	SLV 4	No
Maschio 35	PF SLU	1.504	SLU 39	Si
Maschio 35	V SLU	49.779	SLU 39	Si
Maschio 35	PF	1	SLV 3	Si
Maschio 35	V	0.418	SLV 3	No
Maschio 35	PFFP	0	SLV 1	No
Maschio 35	R	0.013	SLV 1	No

#### Verifica maschi in muratura

Maschio	Stato limite	Molt.	Comb.	PGA	IPGA (ZE)	TR	(TR/TRrif)^.41	Verifica
1	PF	2.479	SLV 11	0.362	1.483	1618	1.653	Si
	V	2.319	SLV 11	0.362	1.483	1618	1.653	Si
	PFFP	2.832	SLV 15	0.362	1.483	1618	1.653	Si
	R	0.139	SLV 1	0.031	0.127	3	0.125	No
2	PF	1000	SLV 1	0.362	1.483	1618	1.653	Si



Maschio	Stato limite	Molt.	Comb.	PGA	iPGA (ZE)	TR	(TR/TRrif)^.41	Verifica
3	V	3.427	SLV 9	0.362	1.483	1618	1.653	Si
	PFFP	1000	SLV 1	0.362	1.483	1618	1.653	Si
	R	0.115	SLV 3	0.026	0.107	2	0.106	No
	PF	2.609	SLV 13	0.362	1.483	1618	1.653	Si
4	V	2.594	SLV 13	0.362	1.483	1618	1.653	Si
	PFFP	3.763	SLV 13	0.362	1.483	1618	1.653	Si
	R	0.128	SLV 1	0.026	0.107	2	0.106	No
	PF	0	SLV 1	0	0	0	0	No
5	V	0	SLV 1	0	0	0	0	No
	PFFP	1.727	SLV 1	0.362	1.483	1618	1.653	Si
	R	0.19	SLV 13	0.044	0.181	7	0.177	No
	PF	3.079	SLV 11	0.362	1.483	1618	1.653	Si
8	V	2.584	SLV 15	0.362	1.483	1618	1.653	Si
	PFFP	3.384	SLV 11	0.362	1.483	1618	1.653	Si
	R	0.135	SLV 3	0.031	0.127	3	0.125	No
	PF	0.565	SLV 1	0.136	0.555	109	0.547	No
9	V	0.557	SLV 1	0.133	0.546	105	0.539	No
	PFFP	0.588	SLV 5	0.141	0.576	119	0.567	No
	R	0.138	SLV 15	0.031	0.127	3	0.125	No
	PF	2.765	SLV 5	0.362	1.483	1618	1.653	Si
11	V	2.716	SLV 5	0.362	1.483	1618	1.653	Si
	PFFP	3.477	SLV 9	0.362	1.483	1618	1.653	Si
	R	0.145	SLV 11	0.031	0.127	3	0.125	No
	PF	1.668	SLV 13	0.362	1.483	1618	1.653	Si
12	V	1.574	SLV 13	0.362	1.483	1618	1.653	Si
	PFFP	3.137	SLV 9	0.362	1.483	1618	1.653	Si
	R	0.141	SLV 1	0.031	0.127	3	0.125	No
	PF	1.815	SLV 3	0.362	1.483	1618	1.653	Si
13	V	1.535	SLV 3	0.362	1.483	1618	1.653	Si
	PFFP	3.139	SLV 7	0.362	1.483	1618	1.653	Si
	R	0.104	SLV 5	0.02	0.08	1	0.08	No
	PF	1.238	SLV 13	0.301	1.234	890	1.294	Si
14	V	1.197	SLV 15	0.292	1.193	806	1.242	Si
	PFFP	1.973	SLV 13	0.362	1.483	1618	1.653	Si
	R	0.092	SLV 7	0.02	0.08	1	0.08	No
	PF	0	SLV 1	0	0	0	0	No
15	V	0	SLV 1	0	0	0	0	No
	PFFP	3.585	SLV 9	0.362	1.483	1618	1.653	Si
	R	0.092	SLV 3	0.02	0.08	1	0.08	No
	PF	1000	SLV 1	0.362	1.483	1618	1.653	Si
18	V	3.317	SLV 11	0.362	1.483	1618	1.653	Si
	PFFP	1000	SLV 1	0.362	1.483	1618	1.653	Si
	R	0.067	SLV 1	0	0	0	0	No
	PF	0.853	SLV 9	0.207	0.848	306	0.835	No
19	V	0.706	SLV 9	0.17	0.698	185	0.679	No
	PFFP	1000	SLV 1	0.362	1.483	1618	1.653	Si
	R	0.086	SLV 3	0.02	0.08	1	0.08	No
	PF	1.05	SLV 13	0.256	1.049	548	1.06	Si
20	V	1.05	SLV 13	0.256	1.049	548	1.06	Si
	PFFP	1.684	SLV 13	0.362	1.483	1618	1.653	Si
	R	0.073	SLV 1	0	0	0	0	No
	PF	0.828	SLV 1	0.201	0.822	282	0.808	No
21	V	0.703	SLV 1	0.17	0.694	183	0.676	No
	PFFP	1.124	SLV 3	0.274	1.122	670	1.151	Si
	R	0.133	SLV 13	0.031	0.127	3	0.125	No
	PF	1.235	SLV 3	0.301	1.231	883	1.289	Si
23	V	1.218	SLV 3	0.297	1.214	848	1.268	Si
	PFFP	2.203	SLV 3	0.362	1.483	1618	1.653	Si
	R	0.135	SLV 13	0.031	0.127	3	0.125	No
	PF	0.365	SLV 9	0.087	0.355	37	0.351	No
24	V	0.356	SLV 9	0.085	0.346	35	0.343	No
	PFFP	1.361	SLV 15	0.331	1.355	1202	1.463	Si
	R	0.074	SLV 7	0	0	0	0	No
	PF	1000	SLV 1	0.362	1.483	1618	1.653	Si
25	V	2.755	SLV 9	0.362	1.483	1618	1.653	Si
	PFFP	2.269	SLV 13	0.362	1.483	1618	1.653	Si
	R	0.025	SLV 5	0	0	0	0	No
	PF	0.229	SLV 9	0.053	0.218	11	0.214	No
26	V	0.227	SLV 9	0.053	0.218	11	0.214	No
	PFFP	1.016	SLV 13	0.248	1.016	497	1.019	Si
	R	0.102	SLV 5	0.02	0.08	1	0.08	No
	PF	2.336	SLV 1	0.362	1.483	1618	1.653	Si
27	V	1.762	SLV 1	0.362	1.483	1618	1.653	Si
	PFFP	1.316	SLV 3	0.32	1.311	1077	1.399	Si
	R	0.096	SLV 5	0.02	0.08	1	0.08	No
	PF	1.325	SLV 1	0.322	1.32	1101	1.412	Si
28	V	1.201	SLV 1	0.292	1.197	813	1.247	Si
	PFFP	1.493	SLV 9	0.362	1.483	1618	1.653	Si
	R	0.092	SLV 7	0.02	0.08	1	0.08	No
	PF	1.868	SLV 1	0.362	1.483	1618	1.653	Si
29	V	1.531	SLV 1	0.362	1.483	1618	1.653	Si
	PFFP	2.435	SLV 11	0.362	1.483	1618	1.653	Si
	R	0.099	SLV 11	0.02	0.08	1	0.08	No
	PF	1.579	SLV 13	0.362	1.483	1618	1.653	Si
31	V	1.39	SLV 13	0.338	1.384	1288	1.505	Si
	PFFP	1.494	SLV 5	0.362	1.483	1618	1.653	Si
	R	0.095	SLV 5	0.02	0.08	1	0.08	No
	PF	0	SLV 1	0	0	0	0	No
31	V	0	SLV 1	0	0	0	0	No



Maschio	Stato limite	Molt.	Comb.	PGA	iPGA (ZE)	TR	(TR/TRrif)^.41	Verifica
	PFFP	2.328	SLV 13	0.362	1.483	1618	1.653	Si
	R	0.122	SLV 1	0.026	0.107	2	0.106	No
32	PF	0	SLV 1	0	0	0	0	No
	V	0	SLV 1	0	0	0	0	No
	PFFP	0.846	SLV 13	0.205	0.841	300	0.828	No
	R	0.084	SLV 15	0	0	0	0	No
33	PF	0	SLV 1	0	0	0	0	No
	V	0	SLV 1	0	0	0	0	No
	PFFP	0.228	SLV 3	0.053	0.218	11	0.214	No
	R	0.014	SLV 13	0	0	0	0	No
34	PF	0.569	SLV 1	0.136	0.558	110	0.549	No
	V	0.539	SLV 1	0.129	0.528	97	0.521	No
	PFFP	0.399	SLV 1	0.095	0.388	45	0.381	No
	R	0.076	SLV 7	0	0	0	0	No
35	PF	0.999	SLV 3	0.244	0.999	474	0.999	No
	V	0.991	SLV 3	0.242	0.991	463	0.99	No
	PFFP	0.567	SLV 3	0.136	0.558	110	0.549	No
	R	0.104	SLV 11	0.02	0.08	1	0.08	No

#### Verifica travi di collegamento in muratura

Trave	Stato limite	Molt.	Comb.	PGA	iPGA (ZE)	TR	(TR/TRrif)^.41	Verifica
1	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
2	F	2.113	SLV 9	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
3	F	3.66	SLV 11	0.362	1.483	1618	1.653	Si
	V	0.143	SLV 7	0.031	0.127	3	0.125	No
4	F	1.842	SLV 7	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
5	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
6	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0.195	SLV 15	0.044	0.181	7	0.177	No
7	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0.551	SLV 3	0.132	0.539	102	0.532	No
8	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0.958	SLV 1	0.234	0.956	422	0.953	No
9	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
10	F	0.708	SLV 15	0.171	0.699	186	0.681	No
	V	0	SLV 1	0	0	0	0	No
11	F	2.945	SLV 1	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
12	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0.28	SLV 3	0.066	0.269	19	0.267	No
13	F	1000	SLV 1	0.362	1.483	1618	1.653	Si
	V	0.581	SLV 7	0.139	0.569	116	0.561	No
14	F	2.987	SLV 5	0.362	1.483	1618	1.653	Si
	V	0.186	SLV 9	0.041	0.169	6	0.167	No
15	F	1.193	SLV 9	0.291	1.189	797	1.236	Si
	V	0	SLV 1	0	0	0	0	No
16	F	3.026	SLV 7	0.362	1.483	1618	1.653	Si
	V	0.091	SLV 11	0.02	0.08	1	0.08	No
17	F	1.552	SLV 7	0.362	1.483	1618	1.653	Si
	V	0	SLV 1	0	0	0	0	No
18	F	1.211	SLV 13	0.295	1.207	833	1.259	Si
	V	0	SLV 1	0	0	0	0	No
19	F	1.189	SLV 1	0.29	1.185	789	1.231	Si
	V	0	SLV 1	0	0	0	0	No
20	F	0	SLV 1	0	0	0	0	No
	V	0	SLV 1	0	0	0	0	No
21	F	0.452	SLV 1	0.108	0.442	63	0.437	No
	V	0	SLV 1	0	0	0	0	No

#### Periodi di ritorno e accelerazioni di aggancio per gli Stati Limite

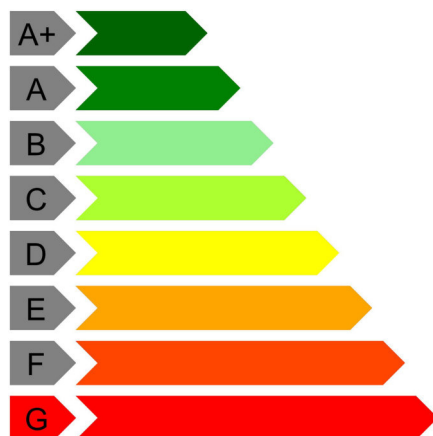
S. L.	TR,C	PGA,C	TR,Rif	PGA,Rif	Tipo rottura
Stato limite di salvaguardia della vita	0	0	475	0.244	taglio maschio muratura

#### Coefficienti relativi alle Linee guida per la classificazione del rischio sismico delle costruzioni secondo il D.M. 24 09/01/2020

TR,C	TR,Rif	PAM	Classe PAM	IS-V	Classe IS-V	Tipo rottura
0	475	8.22	G	0	F	taglio maschio muratura

Classe PAM





Classe IS-V



## 2.3 Verifiche maschi in muratura

Le unità di misura elencate nel capitolo sono in [m, daN, s] ove non espressamente specificato.

*X<sub>ini.</sub>*: coordinate del punto iniziale del maschio. [m]

*Y<sub>ini.</sub>*: coordinate del punto iniziale del maschio. [m]

*X<sub>fin.</sub>*: coordinate del punto finale del maschio. [m]

*Y<sub>fin.</sub>*: coordinate del punto finale del maschio. [m]

*Quota i.*: livello o falda inferiore.

*Quota s.*: livello o falda superiore.

*l*: lunghezza del maschio. [m]

*Sp.*: spessore. [m]

*h<sub>netta</sub>*: altezza netta (a filo solai). [m]

*h<sub>ini.</sub>*: altezza nel modello al punto iniziale. [m]

*h<sub>fin.</sub>*: altezza nel modello al punto finale. [m]

*a*: distanza tra irrigidimenti laterali. [m]

*a.s.,sx*: lunghezza di appoggio del solaio di sinistra. [m]

*a.s.,dx*: lunghezza di appoggio del solaio di destra. [m]

*f<sub>b</sub>*: resistenza normalizzata a compressione verticale dei blocchi. [daN/m<sup>2</sup>]

*f<sub>k</sub>*: resistenza caratteristica a compressione della muratura utilizzata. [daN/m<sup>2</sup>]

*f<sub>vk0</sub>*: resistenza caratteristica a taglio in assenza di carichi verticali. [daN/m<sup>2</sup>]

*f<sub>medio</sub>*: resistenza media a compressione della muratura utilizzata. [daN/m<sup>2</sup>]

*τ<sub>0</sub>*: resistenza media a taglio in assenza di azioni normali [C8.7.1.16]. [daN/m<sup>2</sup>]

*f<sub>v0</sub>*: resistenza media a taglio in assenza di azioni normali [C8.7.1.17]. [daN/m<sup>2</sup>]

*μ*: coefficiente di attrito [C8.7.1.17].

*φ*: coefficiente di ammortamento o ingranamento secondo Circolare 7 21-01-19 §C8.7.1.3.1.1.

*f<sub>v,lim</sub>*: valore massimo della resistenza a taglio che può essere impiegata nel calcolo. [daN/m<sup>2</sup>]

*E*: modulo di elasticità longitudinale della muratura utilizzato. [daN/m<sup>2</sup>]

*G*: modulo di elasticità tangenziale della muratura utilizzato. [daN/m<sup>2</sup>]

*FC*: fattore di confidenza della muratura.

*Comb.*: combinazione.

*Quota*: quota della sezione di verifica. [m]

*N*: sforzo normale. [daN]

*M*: momento flettente nel piano. [daN\*m]



$\sigma_0$ : tensione media di compressione. [daN/m<sup>2</sup>]

$M_u$ : momento flettente ultimo. [daN\*m]

$c.s.$ : coefficiente di sicurezza.

**Verifica**: stato di verifica.

$V_{par}$ : taglio nel piano. [daN]

$\sigma_N$ : tensione media di compressione sulla parte reagente. [daN/m<sup>2</sup>]

$l'$ : lunghezza della parte compressa della parete. [m]

$f_{vd}$ : resistenza a taglio di calcolo. [daN/m<sup>2</sup>]

$V_t$  scorr.: taglio ultimo per verifica a scorrimento. [daN]

$V_t$  fess.diag.: taglio ultimo per verifica a fessurazione diagonale regolare [C8.7.1.17]. [daN]

$V_t$  lim: taglio limite [C8.7.1.18]. [daN]

$c.s.$ : coefficiente di sicurezza a taglio.

$f_d$ : resistenza a compressione di calcolo. [daN/m<sup>2</sup>]

$S_a$ : accelerazione massima, adimensionalizzata rispetto a  $g$ , che l'elemento strutturale subisce durante il sisma.

$M$ : momento flettente fuori piano. [daN\*m]

$M_c$ : momento di collasso per azioni perpendicolari al piano. [daN\*m]

$Coeff.s.$ : coefficiente di sicurezza.

$N_{top}$ : sforzo normale in sommità. [daN]

$N_{base}$ : sforzo normale al piede. [daN]

$V_{orto}$ : taglio fuori piano. [daN]

$\alpha_0$ : moltiplicatore secondo [C8.7.1.1].

$M^*$ : massa partecipante al cinetismo. [daN/(m/s<sup>2</sup>)]

$e^*$ : frazione di massa partecipante della muratura [C8.7.1.5].

$\alpha_0^*$ : accelerazione spettrale di attivazione del meccanismo [C8.7.1.8]. [m/s<sup>2</sup>]

$a_{lim}$ : accelerazione limite [C7.2.11]. [m/s<sup>2</sup>]

**Stato limite**:  $pF_{SLU}$ =Presso flessione per azioni non sismiche;  $V_{SLU}$ =Taglio per azioni non sismiche;  $PF_{SLV}$ =Presso flessione per azioni sismiche;  $V_{SLV}$ =Taglio per azioni sismiche;  $PF_{FP}$ =Presso flessione fuori piano per azioni sismiche;  $R_{SLV}$ =Ribaltamento per azioni sismiche.

## Maschio 1

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.sx	a.s.dx
-34.183	-3.854	-34.183	-1.829	L1	L2	2.025	0.45	2.69	2.69	2.69			

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

f <sub>b</sub>	f <sub>k</sub>	f <sub>vk0</sub>	f <sub>medio</sub>	$\tau_0$	f <sub>v0</sub>	$\mu$	$\phi$	f <sub>v,lim</sub>	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma_0$	$M_u$	c.s.	Verifica
SLU 40	-1.3	-13137	-1203.46	14417	10947.4	9.097	Si
SLU 40	0.05	-10639	-325.37	11675	9228.21	28.362	Si
SLU 40	1.39	-7928	192.34	8700	7169.42	37.275	Si
SLU 83	-1.3	-15876	-1400.05	17423	12636.71	9.026	Si
SLU 83	0.05	-12750	-354.09	13992	10691.83	30.195	Si
SLU 83	1.39	-9331	256.35	10240	8260.22	32.222	Si
SLU 84	-1.3	-15802	-1390.83	17341	12593.27	9.055	Si
SLU 84	0.05	-12689	-351.23	13925	10651.64	30.326	Si
SLU 84	1.39	-9290	254.67	10195	8229.28	32.314	Si
SLU 81	-1.3	-15876	-1400.05	17423	12636.71	9.026	Si
SLU 81	0.05	-12750	-354.09	13992	10691.83	30.195	Si
SLU 81	1.39	-9331	256.35	10240	8260.22	32.222	Si
SLU 82	-1.3	-15802	-1390.83	17341	12593.27	9.055	Si
SLU 82	0.05	-12689	-351.23	13925	10651.64	30.326	Si
SLU 82	1.39	-9290	254.67	10195	8229.28	32.314	Si
SLU 42	-1.3	-13137	-1203.46	14417	10947.4	9.097	Si
SLU 42	0.05	-10639	-325.37	11675	9228.21	28.362	Si
SLU 42	1.39	-7928	192.34	8700	7169.42	37.275	Si
SLU 77	-1.3	-15112	-1294.34	16583	12185.58	9.415	Si
SLU 77	0.05	-12062	-310.59	13236	10227.96	32.931	Si
SLU 77	1.39	-8715	258.05	9564	7787.86	30.18	Si
SLU 41	-1.3	-13212	-1212.68	14499	10996.27	9.068	Si
SLU 41	0.05	-10700	-328.23	11742	9271.77	28.248	Si
SLU 41	1.39	-7968	194.03	8744	7201.88	37.118	Si
SLU 74	-1.3	-15112	-1294.34	16583	12185.58	9.415	Si
SLU 74	0.05	-12062	-310.59	13236	10227.96	32.931	Si
SLU 74	1.39	-8715	258.05	9564	7787.86	30.18	Si
SLU 39	-1.3	-13212	-1212.68	14499	10996.27	9.068	Si
SLU 39	0.05	-10700	-328.23	11742	9271.77	28.248	Si
SLU 39	1.39	-7968	194.03	8744	7201.88	37.118	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma_0$	$M_u$	c.s.	Verifica
SLV 5	-1.3	-13768	-2261.14	15109	12216.39	5.403	Si
SLV 5	0.05	-10537	-1074.05	11564	9659.42	8.993	Si
SLV 5	1.39	-7497	-222.64	8227	7079.26	31.797	Si
SLV 12	-1.3	-7389	556.74	8109	6985.03	12.546	Si



Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 12	0.05	-6144	714.3	6742	5877.25	8.228	Si
SLV 12	1.39	-4239	625.12	4652	4128.52	6.604	Si
SLV 15	-1.3	-7269	143.57	7977	6879.79	47.92	Si
SLV 15	0.05	-5948	429.2	6527	5700.26	13.281	Si
SLV 15	1.39	-4140	509.98	4543	4036.04	7.914	Si
SLV 1	-1.3	-13888	-1847.97	15240	12307.48	6.66	Si
SLV 1	0.05	-10734	-788.96	11779	9820.04	12.447	Si
SLV 1	1.39	-7595	-107.51	8335	7165.71	66.654	Si
SLV 9	-1.3	-12217	-1883.28	13407	11012.52	5.848	Si
SLV 9	0.05	-9394	-849.34	10309	8709.1	10.254	Si
SLV 9	1.39	-6680	-102.92	7330	6357.46	61.774	Si
SLV 11	-1.3	-7389	556.74	8109	6985.03	12.546	Si
SLV 11	0.05	-6144	714.3	6742	5877.25	8.228	Si
SLV 11	1.39	-4239	625.12	4652	4128.52	6.604	Si
SLV 16	-1.3	-7269	143.57	7977	6879.79	47.92	Si
SLV 16	0.05	-5948	429.2	6527	5700.26	13.281	Si
SLV 16	1.39	-4140	509.98	4543	4036.04	7.914	Si
SLV 6	-1.3	-13768	-2261.14	15109	12216.39	5.403	Si
SLV 6	0.05	-10537	-1074.05	11564	9659.42	8.993	Si
SLV 6	1.39	-7497	-222.64	8227	7079.26	31.797	Si
SLV 2	-1.3	-13888	-1847.97	15240	12307.48	6.66	Si
SLV 2	0.05	-10734	-788.96	11779	9820.04	12.447	Si
SLV 2	1.39	-7595	-107.51	8335	7165.71	66.654	Si
SLV 10	-1.3	-12217	-1883.28	13407	11012.52	5.848	Si
SLV 10	0.05	-9394	-849.34	10309	8709.1	10.254	Si
SLV 10	1.39	-6680	-102.92	7330	6357.46	61.774	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 62	-1.3	-15045	-1581	-1290.04		16510	2.025	7757	7068			4.47	Si
SLU 62	0.05	-12016	-84	-308.83		13187	2.025	7314	6665			79.21	Si
SLU 62	1.39	-8692	294	260.12		9538	2.025	6827	6221			21.19	Si
SLU 60	-1.3	-15045	-1581	-1290.04		16510	2.025	7757	7068			4.47	Si
SLU 60	0.05	-12016	-84	-308.83		13187	2.025	7314	6665			79.21	Si
SLU 60	1.39	-8692	294	260.12		9538	2.025	6827	6221			21.19	Si
SLU 81	-1.3	-15876	-1707	-1400.05		17423	2.025	7879	7179			4.21	Si
SLU 81	0.05	-12750	-89	-354.09		13992	2.025	7421	6762			75.65	Si
SLU 81	1.39	-9331	329	256.35		10240	2.025	6921	6307			19.14	Si
SLU 77	-1.3	-15112	-1593	-1294.34		16583	2.025	7767	7077			4.44	Si
SLU 77	0.05	-12062	-75	-310.59		13236	2.025	7320	6671			89.22	Si
SLU 77	1.39	-8715	312	258.05		9564	2.025	6831	6224			19.95	Si
SLU 75	-1.3	-15037	-1579	-1285.12		16501	2.025	7756	7067			4.48	Si
SLU 75	0.05	-12001	-79	-307.72		13170	2.025	7312	6663			84.38	Si
SLU 75	1.39	-8674	300	256.36		9519	2.025	6825	6219			20.7	Si
SLU 84	-1.3	-15802	-1693	-1390.83		17341	2.025	7868	7169			4.23	Si
SLU 84	0.05	-12689	-94	-351.23		13925	2.025	7412	6754			72.17	Si
SLU 84	1.39	-9290	318	254.67		10195	2.025	6915	6301			19.82	Si
SLU 83	-1.3	-15876	-1707	-1400.05		17423	2.025	7879	7179			4.21	Si
SLU 83	0.05	-12750	-89	-354.09		13992	2.025	7421	6762			75.65	Si
SLU 83	1.39	-9331	329	256.35		10240	2.025	6921	6307			19.14	Si
SLU 79	-1.3	-15112	-1593	-1294.34		16583	2.025	7767	7077			4.44	Si
SLU 79	0.05	-12062	-75	-310.59		13236	2.025	7320	6671			89.22	Si
SLU 79	1.39	-8715	312	258.05		9564	2.025	6831	6224			19.95	Si
SLU 82	-1.3	-15802	-1693	-1390.83		17341	2.025	7868	7169			4.23	Si
SLU 82	0.05	-12689	-94	-351.23		13925	2.025	7412	6754			72.17	Si
SLU 82	1.39	-9290	318	254.67		10195	2.025	6915	6301			19.82	Si
SLU 74	-1.3	-15112	-1593	-1294.34		16583	2.025	7767	7077			4.44	Si
SLU 74	0.05	-12062	-75	-310.59		13236	2.025	7320	6671			89.22	Si
SLU 74	1.39	-8715	312	258.05		9564	2.025	6831	6224			19.95	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 8	-1.3	-8940	946	178.88		9811	2.025	10296	9382			9.92	Si
SLV 8	0.05	-7287	2213	489.58		7997	2.025	9933	9051			4.09	Si
SLV 8	1.39	-5056	1963	505.39		5548	2.025	9443	8605			4.38	Si
SLV 6	-1.3	-13768	-3027	-2261.14		15109	2.025	11355	10347			3.42	Si
SLV 6	0.05	-10537	-1971	-1074.05		11564	2.025	10646	9701			4.92	Si
SLV 6	1.39	-7497	-1081	-222.64		8227	2.025	9979	9093			8.41	Si
SLV 9	-1.3	-12217	-3084	-1883.28		13407	2.025	11015	10037			3.26	Si
SLV 9	0.05	-9394	-2292	-849.34		10309	2.025	10395	9473			4.13	Si
SLV 9	1.39	-6680	-1538	-102.92		7330	2.025	9799	8930			5.81	Si
SLV 10	-1.3	-12217	-3084	-1883.28		13407	2.025	11015	10037			3.26	Si
SLV 10	0.05	-9394	-2292	-849.34		10309	2.025	10395	9473			4.13	Si
SLV 10	1.39	-6680	-1538	-102.92		7330	2.025	9799	8930			5.81	Si
SLV 13	-1.3	-8718	-1760	-588.43		9567	2.025	10247	9337			5.31	Si
SLV 13	0.05	-6923	-1202	-39.89		7597	2.025	9853	8978			7.47	Si
SLV 13	1.39	-4872	-1005	291.57		5347	2.025	9403	8568			8.53	Si
SLV 14	-1.3	-8718	-1760	-588.43		9567	2.025	10247	9337			5.31	Si
SLV 14	0.05	-6923	-1202	-39.89		7597	2.025	9853	8978			7.47	Si
SLV 14	1.39	-4872	-1005	291.57		5347	2.025	9403	8568			8.53	Si
SLV 5	-1.3	-13768	-3027	-2261.14		15109	2.025	11355	10347			3.42	Si
SLV 5	0.05	-10537	-1971	-1074.05		11564	2.025	10646	9701			4.92	Si
SLV 5	1.39	-7497	-1081	-222.64		8227	2.025	9979	9093			8.41	Si
SLV 12	-1.3	-7389	889	556.74		8109	2.025	9955	9072			10.2	Si
SLV 12	0.05	-6144	1892	714.3		6742	2.025	9682	8822			4.66	Si
SLV 12	1.39	-4239	1506	625.12		4652	2.025	9264	8442			5.6	Si
SLV 7	-1.3	-8940	946	178.88		9811	2.025	10296	9382			9.92	Si
SLV 7	0.05	-7287	2213	489.58		7997	2.025	9933	9051			4.09	Si



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 7	1.39	-5056	1963	505.39		5548	2.025	9443	8605			4.38	Si
SLV 11	-1.3	-7389	889	556.74		8109	2.025	9955	9072			10.2	Si
SLV 11	0.05	-6144	1892	714.3		6742	2.025	9682	8822			4.66	Si
SLV 11	1.39	-4239	1506	625.12		4652	2.025	9264	8442			5.6	Si

#### Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.045 Wa 0.08 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 15	143750	0.25	6527	-5948	122.41	1266.72	10.35	Si
SLV 16	143750	0.25	6527	-5948	122.41	1266.72	10.35	Si
SLV 11	143750	0.25	6742	-6144	122.41	1306.06	10.67	Si
SLV 12	143750	0.25	6742	-6144	122.41	1306.06	10.67	Si
SLV 14	143750	0.25	7597	-6923	122.41	1460.77	11.93	Si
SLV 13	143750	0.25	7597	-6923	122.41	1460.77	11.93	Si
SLV 8	143750	0.25	7997	-7287	122.41	1532.26	12.52	Si
SLV 7	143750	0.25	7997	-7287	122.41	1532.26	12.52	Si
SLV 10	143750	0.25	10309	-9394	122.41	1935.36	15.81	Si
SLV 9	143750	0.25	10309	-9394	122.41	1935.36	15.81	Si

#### Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 0.045 Wa = 0.08 Ta = 0.0269

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	a0*	aLim	Verifica
SLV 2	-7595	-13888	14	0.101	1125.8	0.92	1.59617	11.92381	No
SLV 1	-7595	-13888	14	0.101	1125.8	0.92	1.59617	11.92381	No
SLV 5	-7497	-13768	25	0.1	1115.9	0.919	1.58209	11.4846	No
SLV 6	-7497	-13768	25	0.1	1115.9	0.919	1.58209	11.4846	No
SLV 4	-6863	-12439	4	0.104	1052.5	0.916	1.64366	11.92381	No
SLV 3	-6863	-12439	4	0.104	1052.5	0.916	1.64366	11.92381	No
SLV 10	-6680	-12217	24	0.102	1034.2	0.915	1.61586	11.4846	No
SLV 9	-6680	-12217	24	0.102	1034.2	0.915	1.61586	11.4846	No
SLV 13	-4872	-8718	11	0.108	854.8	0.903	1.74081	11.92381	No
SLV 14	-4872	-8718	11	0.108	854.8	0.903	1.74081	11.92381	No

#### Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	9.026	SLU 81	Si
V_SLU	4.205	SLU 81	Si
PF_SLV	5.403	SLV 5	Si
V_SLV	3.255	SLV 9	Si
PFFP_SLV	10.348	SLV 15	Si
R_SLV	0.134	SLV 1	No

## Maschio 2

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

#### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-34.183	-0.829	-34.183	2.931	L1	L2	3.76	0.45	2.69	2.69	2.69			

#### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	$\tau_0$	fv0	$\mu$	$\phi$	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

#### Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 73	-1.3	-29635	858.04	17515	43734.63	50.97	Si
SLU 73	0.05	-28177	1109.33	16653	42143.04	37.99	Si
SLU 73	1.39	-27506	442.97	16257	41391.39	93.44	Si
SLU 68	-1.3	-25231	631.85	14912	38751.3	61.33	Si
SLU 68	0.05	-22991	982.04	13588	36012.48	36.671	Si
SLU 68	1.39	-21028	691.29	12428	33500.68	48.461	Si
SLU 65	-1.3	-25231	631.85	14912	38751.3	61.33	Si
SLU 65	0.05	-22991	982.04	13588	36012.48	36.671	Si
SLU 65	1.39	-21028	691.29	12428	33500.68	48.461	Si
SLU 67	-1.3	-25435	622.45	15032	38993.07	62.644	Si
SLU 67	0.05	-23167	967.64	13692	36233.68	37.445	Si
SLU 67	1.39	-21192	629.79	12525	33715.41	53.534	Si
SLU 47	-1.3	-22966	514.89	13573	35981.81	69.883	Si
SLU 47	0.05	-20361	858.27	12034	32623.67	38.011	Si
SLU 47	1.39	-17794	677.5	10517	29133.98	43.002	Si
SLU 26	-1.3	-20412	549.3	12064	32690.85	59.514	Si
SLU 26	0.05	-18883	824.94	11160	30636.89	37.138	Si
SLU 26	1.39	-17679	574.06	10449	28973.36	50.471	Si
SLU 23	-1.3	-20412	549.3	12064	32690.85	59.514	Si
SLU 23	0.05	-18883	824.94	11160	30636.89	37.138	Si
SLU 23	1.39	-17679	574.06	10449	28973.36	50.471	Si
SLU 72	-1.3	-25435	622.45	15032	38993.07	62.644	Si
SLU 72	0.05	-23167	967.64	13692	36233.68	37.445	Si
SLU 72	1.39	-21192	629.79	12525	33715.41	53.534	Si
SLU 70	-1.3	-25435	622.45	15032	38993.07	62.644	Si
SLU 70	0.05	-23167	967.64	13692	36233.68	37.445	Si
SLU 70	1.39	-21192	629.79	12525	33715.41	53.534	Si



Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 76	-1.3	-29635	858.04	17515	43734.63	50.97	Si
SLU 76	0.05	-28177	1109.33	16653	42143.04	37.99	Si
SLU 76	1.39	-27506	442.97	16257	41391.39	93.44	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 5	-1.3	-21426	-1535.9	12663	36106.61	23.508	Si
SLV 5	0.05	-19528	-870.95	11541	33244.8	38.171	Si
SLV 5	1.39	-17874	-651.17	10564	30698.03	47.143	Si
SLV 16	-1.3	-17208	1715.24	10170	29658.25	17.291	Si
SLV 16	0.05	-16562	1406.42	9789	28642.71	20.366	Si
SLV 16	1.39	-15521	934.49	9173	26989.26	28.881	Si
SLV 10	-1.3	-19387	-1143.25	11458	33030.12	28.891	Si
SLV 10	0.05	-18086	-747.53	10689	31026.97	41.506	Si
SLV 10	1.39	-16530	-454.84	9770	28592.05	62.862	Si
SLV 11	-1.3	-19694	2549.67	11640	33497.97	13.138	Si
SLV 11	0.05	-18330	2344.71	10833	31405.48	13.394	Si
SLV 11	1.39	-17390	1330.2	10278	29943.19	22.51	Si
SLV 9	-1.3	-19387	-1143.25	11458	33030.12	28.891	Si
SLV 9	0.05	-18086	-747.53	10689	31026.97	41.506	Si
SLV 9	1.39	-16530	-454.84	9770	28592.05	62.862	Si
SLV 7	-1.3	-21733	2157.02	12845	36563.08	16.951	Si
SLV 7	0.05	-19772	2221.29	11686	33616.9	15.134	Si
SLV 7	1.39	-18734	1133.86	11072	32028.16	28.247	Si
SLV 12	-1.3	-19694	2549.67	11640	33497.97	13.138	Si
SLV 12	0.05	-18330	2344.71	10833	31405.48	13.394	Si
SLV 12	1.39	-17390	1330.2	10278	29943.19	22.51	Si
SLV 15	-1.3	-17208	1715.24	10170	29658.25	17.291	Si
SLV 15	0.05	-16562	1406.42	9789	28642.71	20.366	Si
SLV 15	1.39	-15521	934.49	9173	26989.26	28.881	Si
SLV 6	-1.3	-21426	-1535.9	12663	36106.61	23.508	Si
SLV 6	0.05	-19528	-870.95	11541	33244.8	38.171	Si
SLV 6	1.39	-17874	-651.17	10564	30698.03	47.143	Si
SLV 8	-1.3	-21733	2157.02	12845	36563.08	16.951	Si
SLV 8	0.05	-19772	2221.29	11686	33616.9	15.134	Si
SLV 8	1.39	-18734	1133.86	11072	32028.16	28.247	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 80	-1.3	-29838	-325	848.64		17635	3.76	7907	13378			41.17	Si
SLU 80	0.05	-28354	-283	1094.92		16758	3.76	7790	13181			46.54	Si
SLU 80	1.39	-27671	-87	381.47		16354	3.76	7736	13089			150.78	Si
SLU 78	-1.3	-29838	-325	848.64		17635	3.76	7907	13378			41.17	Si
SLU 78	0.05	-28354	-283	1094.92		16758	3.76	7790	13181			46.54	Si
SLU 78	1.39	-27671	-87	381.47		16354	3.76	7736	13089			150.78	Si
SLU 40	-1.3	-26906	-315	863.03		15902	3.76	7676	12987			41.19	Si
SLU 40	0.05	-26469	-253	992.37		15644	3.76	7641	12929			51.04	Si
SLU 40	1.39	-27099	-18	157.83		16016	3.76	7691	13013			705.36	Si
SLU 73	-1.3	-29635	-330	858.04		17515	3.76	7891	13351			40.43	Si
SLU 73	0.05	-28177	-295	1109.33		16653	3.76	7776	13157			44.67	Si
SLU 73	1.39	-27506	-108	442.97		16257	3.76	7723	13067			121.41	Si
SLU 84	-1.3	-31726	-351	945.58		18750	3.76	8056	13630			38.87	Si
SLU 84	0.05	-30576	-293	1149.47		18071	3.76	7965	13477			46	Si
SLU 84	1.39	-30447	-52	275.05		17995	3.76	7955	13460			256.78	Si
SLU 83	-1.3	-32031	-343	931.49		18931	3.76	8080	13671			39.89	Si
SLU 83	0.05	-30842	-276	1127.87		18228	3.76	7986	13512			48.95	Si
SLU 83	1.39	-30694	-21	182.8		18141	3.76	7974	13493			636.58	Si
SLU 82	-1.3	-31726	-351	945.58		18750	3.76	8056	13630			38.87	Si
SLU 82	0.05	-30576	-293	1149.47		18071	3.76	7965	13477			46	Si
SLU 82	1.39	-30447	-52	275.05		17995	3.76	7955	13460			256.78	Si
SLU 76	-1.3	-29635	-330	858.04		17515	3.76	7891	13351			40.43	Si
SLU 76	0.05	-28177	-295	1109.33		16653	3.76	7776	13157			44.67	Si
SLU 76	1.39	-27506	-108	442.97		16257	3.76	7723	13067			121.41	Si
SLU 75	-1.3	-29838	-325	848.64		17635	3.76	7907	13378			41.17	Si
SLU 75	0.05	-28354	-283	1094.92		16758	3.76	7790	13181			46.54	Si
SLU 75	1.39	-27671	-87	381.47		16354	3.76	7736	13089			150.78	Si
SLU 81	-1.3	-32031	-343	931.49		18931	3.76	8080	13671			39.89	Si
SLU 81	0.05	-30842	-276	1127.87		18228	3.76	7986	13512			48.95	Si
SLU 81	1.39	-30694	-21	182.8		18141	3.76	7974	13493			636.58	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 8	-1.3	-21733	4599	2157.02		12845	3.76	10902	18447			4.01	Si
SLV 8	0.05	-19772	4809	2221.29		11686	3.76	10670	18054			3.75	Si
SLV 8	1.39	-18734	4064	1133.86		11072	3.76	10548	17847			4.39	Si
SLV 11	-1.3	-19694	4540	2549.67		11640	3.76	10661	18039			3.97	Si
SLV 11	0.05	-18330	4705	2344.71		10833	3.76	10500	17766			3.78	Si
SLV 11	1.39	-17390	3966	1330.2		10278	3.76	10389	17578			4.43	Si
SLV 13	-1.3	-17116	-1736	607.37		10116	3.76	10356	17523			10.1	Si
SLV 13	0.05	-16489	-1842	478.74		9745	3.76	10282	17398			9.44	Si
SLV 13	1.39	-15263	-1475	398.98		9021	3.76	10138	17153			11.63	Si
SLV 12	-1.3	-19694	4540	2549.67		11640	3.76	10661	18039			3.97	Si
SLV 12	0.05	-18330	4705	2344.71		10833	3.76	10500	17766			3.78	Si
SLV 12	1.39	-17390	3966	1330.2		10278	3.76	10389	17578			4.43	Si
SLV 10	-1.3	-19387	-5008	-1143.25		11458	3.76	10625	17977			3.59	Si
SLV 10	0.05	-18086	-5182	-747.53		10689	3.76	10471	17717			3.42	Si
SLV 10	1.39	-16530	-4229	-454.84		9770	3.76	10287	17406			4.12	Si
SLV 6	-1.3	-21426	-4948	-1535.9		12663	3.76	10866	18385			3.72	Si



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 6	0.05	-19528	-5078	-870.95		11541	3.76	10642	18006			3.55	Si
SLV 6	1.39	-17874	-4132	-651.17		10564	3.76	10446	17675			4.28	Si
SLV 7	-1.3	-21733	4599	2157.02		12845	3.76	10902	18447			4.01	Si
SLV 7	0.05	-19772	4809	2221.29		11686	3.76	10670	18054			3.75	Si
SLV 7	1.39	-18734	4064	1133.86		11072	3.76	10548	17847			4.39	Si
SLV 9	-1.3	-19387	-5008	-1143.25		11458	3.76	10625	17977			3.59	Si
SLV 9	0.05	-18086	-5182	-747.53		10689	3.76	10471	17717			3.42	Si
SLV 9	1.39	-16530	-4229	-454.84		9770	3.76	10287	17406			4.12	Si
SLV 5	-1.3	-21426	-4948	-1535.9		12663	3.76	10866	18385			3.72	Si
SLV 5	0.05	-19528	-5078	-870.95		11541	3.76	10642	18006			3.55	Si
SLV 5	1.39	-17874	-4132	-651.17		10564	3.76	10446	17675			4.28	Si
SLV 14	-1.3	-17116	-1736	607.37		10116	3.76	10356	17523			10.1	Si
SLV 14	0.05	-16489	-1842	478.74		9745	3.76	10282	17398			9.44	Si
SLV 14	1.39	-15263	-1475	398.98		9021	3.76	10138	17153			11.63	Si

#### Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.045 Wa 0.08 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 14	143750	0.25	9745	-16489	227.29	3414.13	15.02	Si
SLV 13	143750	0.25	9745	-16489	227.29	3414.13	15.02	Si
SLV 15	143750	0.25	9789	-16562	227.29	3427.98	15.08	Si
SLV 16	143750	0.25	9789	-16562	227.29	3427.98	15.08	Si
SLV 10	143750	0.25	10689	-18086	227.29	3713.33	16.34	Si
SLV 9	143750	0.25	10689	-18086	227.29	3713.33	16.34	Si
SLV 12	143750	0.25	10833	-18330	227.29	3758.63	16.54	Si
SLV 11	143750	0.25	10833	-18330	227.29	3758.63	16.54	Si
SLV 6	143750	0.25	11541	-19528	227.29	3978.77	17.51	Si
SLV 5	143750	0.25	11541	-19528	227.29	3978.77	17.51	Si

#### Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 0.045 Wa = 0.08 Ta = 0.0269

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	a0*	aLim	Verifica
SLV 3	-20001	-24004	-877	0.061	2684.6	0.934	0.95652	11.92381	No
SLV 4	-20001	-24004	-877	0.061	2684.6	0.934	0.95652	11.92381	No
SLV 2	-19743	-23912	-704	0.068	2658.5	0.934	1.06623	11.92381	No
SLV 1	-19743	-23912	-704	0.068	2658.5	0.934	1.06623	11.92381	No
SLV 13	-15263	-17116	554	0.073	2206.9	0.923	1.14484	11.92381	No
SLV 14	-15263	-17116	554	0.073	2206.9	0.923	1.14484	11.92381	No
SLV 7	-18734	-21733	-638	0.071	2556.6	0.931	1.10317	11.4846	No
SLV 8	-18734	-21733	-638	0.071	2556.6	0.931	1.10317	11.4846	No
SLV 16	-15521	-17208	381	0.082	2232.9	0.924	1.28491	11.92381	No
SLV 15	-15521	-17208	381	0.082	2232.9	0.924	1.28491	11.92381	No

#### Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	36.671	SLU 65	Si
V_SLU	38.873	SLU 82	Si
PF_SLV	13.138	SLV 11	Si
V_SLV	3.419	SLV 9	Si
PFFP_SLV	15.021	SLV 13	Si
R_SLV	0.08	SLV 3	No

## Maschio 3

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

#### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-34.183	3.931	-34.183	5.726	L1	L2	1.795	0.45	2.69	2.69	2.69			

#### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	$\tau_0$	fv0	$\mu$	$\phi$	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

#### Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 84	-1.3	-15992	953.58	19799	10864.53	11.393	Si
SLU 84	0.05	-14179	104.11	17554	9983.38	95.891	Si
SLU 84	1.39	-12192	-519.19	15093	8914.61	17.17	Si
SLU 83	-1.3	-16083	965.79	19911	10906.15	11.292	Si
SLU 83	0.05	-14264	115.54	17659	10026.58	86.776	Si
SLU 83	1.39	-12259	-500.49	15177	8952.72	17.888	Si
SLU 39	-1.3	-13534	828.02	16756	9648.5	11.652	Si
SLU 39	0.05	-12167	97.15	15063	8900.85	91.62	Si
SLU 39	1.39	-10689	-432.83	13233	8034.65	18.563	Si
SLU 77	-1.3	-15231	900.03	18856	10505.37	11.672	Si
SLU 77	0.05	-13396	102.11	16584	9575.06	93.768	Si
SLU 77	1.39	-11359	-476.87	14063	8434.82	17.688	Si
SLU 41	-1.3	-13534	828.02	16756	9648.5	11.652	Si
SLU 41	0.05	-12167	97.15	15063	8900.85	91.62	Si
SLU 41	1.39	-10689	-432.83	13233	8034.65	18.563	Si
SLU 60	-1.3	-15056	895.99	18640	10420.84	11.631	Si
SLU 60	0.05	-13197	119.72	16338	9468.72	79.093	Si



Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 60	1.39	-11115	-440.5	13760	8290.47	18.821	Si
SLU 79	-1.3	-15231	900.03	18856	10505.37	11.672	Si
SLU 79	0.05	-13396	102.11	16584	9575.06	93.768	Si
SLU 79	1.39	-11359	-476.87	14063	8434.82	17.688	Si
SLU 81	-1.3	-16083	965.79	19911	10906.15	11.292	Si
SLU 81	0.05	-14264	115.54	17659	10026.58	86.776	Si
SLU 81	1.39	-12259	-500.49	15177	8952.72	17.888	Si
SLU 62	-1.3	-15056	895.99	18640	10420.84	11.631	Si
SLU 62	0.05	-13197	119.72	16338	9468.72	79.093	Si
SLU 62	1.39	-11115	-440.5	13760	8290.47	18.821	Si
SLU 82	-1.3	-15992	953.58	19799	10864.53	11.393	Si
SLU 82	0.05	-14179	104.11	17554	9983.38	95.891	Si
SLU 82	1.39	-12192	-519.19	15093	8914.61	17.17	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 12	-1.3	-12134	1569.14	15022	9551.52	6.087	Si
SLV 12	0.05	-9900	622.93	12256	7994.03	12.833	Si
SLV 12	1.39	-8102	-230.44	10030	6674.66	28.965	Si
SLV 7	-1.3	-13075	1699.73	16187	10180.4	5.989	Si
SLV 7	0.05	-10826	742.47	13402	8650.23	11.651	Si
SLV 7	1.39	-9158	50.81	11337	7456.44	146.744	Si
SLV 9	-1.3	-7983	-494.13	9883	6585.1	13.327	Si
SLV 9	0.05	-7356	-613.84	9107	6110.03	9.954	Si
SLV 9	1.39	-5784	-704.79	7160	4886.7	6.934	Si
SLV 13	-1.3	-8338	75.66	10322	6851.07	90.554	Si
SLV 13	0.05	-7167	-320.44	8873	5965.11	18.615	Si
SLV 13	1.39	-5364	-866.9	6640	4552.15	5.251	Si
SLV 11	-1.3	-12134	1569.14	15022	9551.52	6.087	Si
SLV 11	0.05	-9900	622.93	12256	7994.03	12.833	Si
SLV 11	1.39	-8102	-230.44	10030	6674.66	28.965	Si
SLV 14	-1.3	-8338	75.66	10322	6851.07	90.554	Si
SLV 14	0.05	-7167	-320.44	8873	5965.11	18.615	Si
SLV 14	1.39	-5364	-866.9	6640	4552.15	5.251	Si
SLV 15	-1.3	-9583	694.64	11864	7765.86	11.18	Si
SLV 15	0.05	-7930	50.59	9817	6545.29	129.378	Si
SLV 15	1.39	-6059	-724.59	7501	5104.12	7.044	Si
SLV 16	-1.3	-9583	694.64	11864	7765.86	11.18	Si
SLV 16	0.05	-7930	50.59	9817	6545.29	129.378	Si
SLV 16	1.39	-6059	-724.59	7501	5104.12	7.044	Si
SLV 10	-1.3	-7983	-494.13	9883	6585.1	13.327	Si
SLV 10	0.05	-7356	-613.84	9107	6110.03	9.954	Si
SLV 10	1.39	-5784	-704.79	7160	4886.7	6.934	Si
SLV 8	-1.3	-13075	1699.73	16187	10180.4	5.989	Si
SLV 8	0.05	-10826	742.47	13402	8650.23	11.651	Si
SLV 8	1.39	-9158	50.81	11337	7456.44	146.744	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 83	-1.3	-16083	2144	965.79		19911	1.795	8210	6632			3.09	Si
SLU 83	0.05	-14264	514	115.54		17659	1.795	7910	6389			12.44	Si
SLU 83	1.39	-12259	-28	-500.49		15177	1.795	7579	6122			221.72	Si
SLU 80	-1.3	-15140	1977	887.82		18744	1.795	8055	6506			3.29	Si
SLU 80	0.05	-13311	477	90.68		16479	1.795	7753	6262			13.13	Si
SLU 80	1.39	-11292	6	-495.57		13979	1.795	7419	5993			1000	Si
SLU 77	-1.3	-15231	1990	900.03		18856	1.795	8070	6518			3.28	Si
SLU 77	0.05	-13396	465	102.11		16584	1.795	7767	6274			13.49	Si
SLU 77	1.39	-11359	-23	-476.87		14063	1.795	7431	6002			262.07	Si
SLU 78	-1.3	-15140	1977	887.82		18744	1.795	8055	6506			3.29	Si
SLU 78	0.05	-13311	477	90.68		16479	1.795	7753	6262			13.13	Si
SLU 78	1.39	-11292	6	-495.57		13979	1.795	7419	5993			1000	Si
SLU 75	-1.3	-15140	1977	887.82		18744	1.795	8055	6506			3.29	Si
SLU 75	0.05	-13311	477	90.68		16479	1.795	7753	6262			13.13	Si
SLU 75	1.39	-11292	6	-495.57		13979	1.795	7419	5993			1000	Si
SLU 81	-1.3	-16083	2144	965.79		19911	1.795	8210	6632			3.09	Si
SLU 81	0.05	-14264	514	115.54		17659	1.795	7910	6389			12.44	Si
SLU 81	1.39	-12259	-28	-500.49		15177	1.795	7579	6122			221.72	Si
SLU 82	-1.3	-15992	2131	953.58		19799	1.795	8195	6620			3.11	Si
SLU 82	0.05	-14179	525	104.11		17554	1.795	7896	6378			12.14	Si
SLU 82	1.39	-12192	1	-519.19		15093	1.795	7568	6113			1000	Si
SLU 79	-1.3	-15231	1990	900.03		18856	1.795	8070	6518			3.28	Si
SLU 79	0.05	-13396	465	102.11		16584	1.795	7767	6274			13.49	Si
SLU 79	1.39	-11359	-23	-476.87		14063	1.795	7431	6002			262.07	Si
SLU 84	-1.3	-15992	2131	953.58		19799	1.795	8195	6620			3.11	Si
SLU 84	0.05	-14179	525	104.11		17554	1.795	7896	6378			12.14	Si
SLU 84	1.39	-12192	1	-519.19		15093	1.795	7568	6113			1000	Si
SLU 74	-1.3	-15231	1990	900.03		18856	1.795	8070	6518			3.28	Si
SLU 74	0.05	-13396	465	102.11		16584	1.795	7767	6274			13.49	Si
SLU 74	1.39	-11359	-23	-476.87		14063	1.795	7431	6002			262.07	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 3	-1.3	-12720	1894	1129.94		15748	1.795	11483	9275			4.9	Si
SLV 3	0.05	-11015	303	449.07		13636	1.795	11061	8934			29.48	Si
SLV 3	1.39	-9578	-323	212.92		11858	1.795	10705	8647			26.75	Si
SLV 11	-1.3	-12134	3397	1569.14		15022	1.795	11338	9158			2.7	Si
SLV 11	0.05	-9900	2354	622.93		12256	1.795	10785	8711			3.7	Si
SLV 11	1.39	-8102	1586	-230.44		10030	1.795	10339	8352			5.26	Si



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 6	-1.3	-8924	-769	-363.54		11048	1.795	10543	8516			11.07	Si
SLV 6	0.05	-8282	-1781	-494.3		10253	1.795	10384	8388			4.71	Si
SLV 6	1.39	-6839	-1618	-423.53		8467	1.795	10027	8099			5.01	Si
SLV 15	-1.3	-9583	1976	694.64		11864	1.795	10706	8648			4.38	Si
SLV 15	0.05	-7930	1410	50.59		9817	1.795	10297	8317			5.9	Si
SLV 15	1.39	-6059	1123	-724.59		7501	1.795	9834	7943			7.07	Si
SLV 8	-1.3	-13075	3372	1699.73		16187	1.795	11571	9346			2.77	Si
SLV 8	0.05	-10826	2022	742.47		13402	1.795	11014	8896			4.4	Si
SLV 8	1.39	-9158	1153	50.81		11337	1.795	10601	8563			7.43	Si
SLV 5	-1.3	-8924	-769	-363.54		11048	1.795	10543	8516			11.07	Si
SLV 5	0.05	-8282	-1781	-494.3		10253	1.795	10384	8388			4.71	Si
SLV 5	1.39	-6839	-1618	-423.53		8467	1.795	10027	8099			5.01	Si
SLV 12	-1.3	-12134	3397	1569.14		15022	1.795	11338	9158			2.7	Si
SLV 12	0.05	-9900	2354	622.93		12256	1.795	10785	8711			3.7	Si
SLV 12	1.39	-8102	1586	-230.44		10030	1.795	10339	8352			5.26	Si
SLV 16	-1.3	-9583	1976	694.64		11864	1.795	10706	8648			4.38	Si
SLV 16	0.05	-7930	1410	50.59		9817	1.795	10297	8317			5.9	Si
SLV 16	1.39	-6059	1123	-724.59		7501	1.795	9834	7943			7.07	Si
SLV 4	-1.3	-12720	1894	1129.94		15748	1.795	11483	9275			4.9	Si
SLV 4	0.05	-11015	303	449.07		13636	1.795	11061	8934			29.48	Si
SLV 4	1.39	-9578	-323	212.92		11858	1.795	10705	8647			26.75	Si
SLV 7	-1.3	-13075	3372	1699.73		16187	1.795	11571	9346			2.77	Si
SLV 7	0.05	-10826	2022	742.47		13402	1.795	11014	8896			4.4	Si
SLV 7	1.39	-9158	1153	50.81		11337	1.795	10601	8563			7.43	Si

#### Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.045 Wa 0.08 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 14	143750	0.25	8873	-7167	108.5	1495.43	13.78	Si
SLV 13	143750	0.25	8873	-7167	108.5	1495.43	13.78	Si
SLV 10	143750	0.25	9107	-7356	108.5	1531.76	14.12	Si
SLV 9	143750	0.25	9107	-7356	108.5	1531.76	14.12	Si
SLV 15	143750	0.25	9817	-7930	108.5	1640.88	15.12	Si
SLV 16	143750	0.25	9817	-7930	108.5	1640.88	15.12	Si
SLV 5	143750	0.25	10253	-8282	108.5	1707	15.73	Si
SLV 6	143750	0.25	10253	-8282	108.5	1707	15.73	Si
SLV 11	143750	0.25	12256	-9900	108.5	2004.08	18.47	Si
SLV 12	143750	0.25	12256	-9900	108.5	2004.08	18.47	Si

#### Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 0.045 Wa = 0.08 Ta = 0.0269

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	a0*	aLim	Verifica
SLV 1	-8882	-11475	210	0.079	1214.3	0.931	1.23834	11.92381	No
SLV 2	-8882	-11475	210	0.079	1214.3	0.931	1.23834	11.92381	No
SLV 15	-6059	-9583	-201	0.079	930.5	0.916	1.25354	11.92381	No
SLV 16	-6059	-9583	-201	0.079	930.5	0.916	1.25354	11.92381	No
SLV 4	-9578	-12720	191	0.081	1284.6	0.934	1.26438	11.92381	No
SLV 3	-9578	-12720	191	0.081	1284.6	0.934	1.26438	11.92381	No
SLV 13	-5364	-8338	-182	0.081	861.1	0.911	1.2951	11.92381	No
SLV 14	-5364	-8338	-182	0.081	861.1	0.911	1.2951	11.92381	No
SLV 11	-8102	-12134	-86	0.091	1135.6	0.927	1.43102	11.4846	No
SLV 12	-8102	-12134	-86	0.091	1135.6	0.927	1.43102	11.4846	No

#### Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	11.292	SLU 81	Si
V_SLU	3.093	SLU 81	Si
PF_SLV	5.251	SLV 13	Si
V_SLV	2.696	SLV 11	Si
PFFP_SLV	13.782	SLV 13	Si
R_SLV	0.104	SLV 1	No

## Maschio 4

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

#### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.sx	a.s.dx
-31.648	1.306	-34.183	1.306	L1	L2	2.535	0.45	2.69	2.69	2.69			

#### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	$\tau_0$	fv0	$\mu$	$\phi$	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

#### Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 43	-1.3	-9131	2578.34	8004	10435.93	4.048	Si
SLU 43	0.05	-4869	2343.98	4268	5847.78	2.495	Si
SLU 43	1.39	-698	890	0	0	0	No, e>l/2
SLU 1	-1.3	-7113	2112.17	6235	8325.51	3.942	Si
SLU 1	0.05	-3825	1914.19	3353	4648.05	2.428	Si
SLU 1	1.39	-565	721.53	0	0	0	No, e>l/2
SLU 41	-1.3	-8377	3988.12	7344	9661.13	2.422	Si





Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 41	0.05	-4952	3527.96	4341	5941.79	1.684	Si
SLU 41	1.39	-962	1239.53	0	0	0	No, $e \geq l/2$
SLU 48	-1.3	-9131	2578.34	8004	10435.93	4.048	Si
SLU 48	0.05	-4869	2343.98	4268	5847.78	2.495	Si
SLU 48	1.39	-698	890	0	0	0	No, $e \geq l/2$
SLU 37	-1.3	-8100	3571.87	7100	9371.51	2.624	Si
SLU 37	0.05	-4704	3170.23	4123	5660.21	1.785	Si
SLU 37	1.39	-875	1126.13	0	0	0	No, $e \geq l/2$
SLU 40	-1.3	-8655	3687.4	7587	9948.62	2.698	Si
SLU 40	0.05	-5169	3430.1	4531	6187.12	1.804	Si
SLU 40	1.39	-1116	1415.84	0	0	0	No, $e \geq l/2$
SLU 39	-1.3	-8377	3988.12	7344	9661.13	2.422	Si
SLU 39	0.05	-4952	3527.96	4341	5941.79	1.684	Si
SLU 39	1.39	-962	1239.53	0	0	0	No, $e \geq l/2$
SLU 83	-1.3	-10395	4454.3	9113	11701.95	2.627	Si
SLU 83	0.05	-5996	3957.76	5256	7109.41	1.796	Si
SLU 83	1.39	-1094	1408	0	0	0	No, $e \geq l/2$
SLU 45	-1.3	-9131	2578.34	8004	10435.93	4.048	Si
SLU 45	0.05	-4869	2343.98	4268	5847.78	2.495	Si
SLU 45	1.39	-698	890	0	0	0	No, $e \geq l/2$
SLU 35	-1.3	-8100	3571.87	7100	9371.51	2.624	Si
SLU 35	0.05	-4704	3170.23	4123	5660.21	1.785	Si
SLU 35	1.39	-875	1126.13	0	0	0	No, $e \geq l/2$

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 4	-1.3	-5141	5600.07	4507	6276.16	1.121	Si
SLV 4	0.05	-2723	3437.65	2387	3384.21	0.984	No, $M > Mu$
SLV 4	1.39	150	-88.91	0	0	0	No, Trazione
SLV 2	-1.3	-4637	5793.5	4065	5682.08	0.981	No, $M > Mu$
SLV 2	0.05	-2403	3464.51	0	0	0	No, $e \geq l/2$
SLV 2	1.39	236	-198.83	0	0	0	No, Trazione
SLV 1	-1.3	-4637	5793.5	4065	5682.08	0.981	No, $M > Mu$
SLV 1	0.05	-2403	3464.51	0	0	0	No, $e \geq l/2$
SLV 1	1.39	236	-198.83	0	0	0	No, Trazione
SLV 5	-1.3	-5803	3801.87	5087	7049.13	1.854	Si
SLV 5	0.05	-3088	2671.24	2707	3827.82	1.433	Si
SLV 5	1.39	-255	359.63	0	0	0	No, $e \geq l/2$
SLV 6	-1.3	-5803	3801.87	5087	7049.13	1.854	Si
SLV 6	0.05	-3088	2671.24	2707	3827.82	1.433	Si
SLV 6	1.39	-255	359.63	0	0	0	No, $e \geq l/2$
SLV 8	-1.3	-7483	3157.12	6560	8975.82	2.843	Si
SLV 8	0.05	-4155	2581.69	3643	5110.04	1.979	Si
SLV 8	1.39	-544	726.04	0	0	0	No, $e \geq l/2$
SLV 7	-1.3	-7483	3157.12	6560	8975.82	2.843	Si
SLV 7	0.05	-4155	2581.69	3643	5110.04	1.979	Si
SLV 7	1.39	-544	726.04	0	0	0	No, $e \geq l/2$
SLV 12	-1.3	-8987	1256.58	7878	10656.21	8.48	Si
SLV 12	0.05	-5063	1874.88	4438	6184.29	3.299	Si
SLV 12	1.39	-1052	1314.64	923	1323.82	1.007	Si
SLV 11	-1.3	-8987	1256.58	7878	10656.21	8.48	Si
SLV 11	0.05	-5063	1874.88	4438	6184.29	3.299	Si
SLV 11	1.39	-1052	1314.64	923	1323.82	1.007	Si
SLV 3	-1.3	-5141	5600.07	4507	6276.16	1.121	Si
SLV 3	0.05	-2723	3437.65	2387	3384.21	0.984	No, $M > Mu$
SLV 3	1.39	150	-88.91	0	0	0	No, Trazione

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 40	-1.3	-8655	-122	3687.4		7619	2.5244	6571	7465			61.28	Si
SLU 40	0.05	-5169	-119	3430.1		6340	1.8117	6401	5218			44.02	Si
SLU 40	1.39	-1116	-45	1415.84		0	0	5556	0			0	No, $V_u < V$
SLU 41	-1.3	-8377	80	3988.12		7841	2.3743	6601	7053			88.07	Si
SLU 41	0.05	-4952	101	3527.96		6609	1.6651	6437	4823			47.67	Si
SLU 41	1.39	-962	263	1239.53		0	0	5556	0			0	No, $V_u < V$
SLU 45	-1.3	-9131	18	2578.34		8004	2.535	6623	7555			429.47	Si
SLU 45	0.05	-4869	31	2343.98		4588	2.3582	6167	6545			208.69	Si
SLU 45	1.39	-698	77	890		0	0	5556	0			0	No, $V_u < V$
SLU 37	-1.3	-8100	65	3571.87		7259	2.4795	6523	7279			111.55	Si
SLU 37	0.05	-4704	84	3170.23		5870	1.7806	6338	5079			60.41	Si
SLU 37	1.39	-875	217	1126.13		0	0	5556	0			0	No, $V_u < V$
SLU 39	-1.3	-8377	80	3988.12		7841	2.3743	6601	7053			88.07	Si
SLU 39	0.05	-4952	101	3527.96		6609	1.6651	6437	4823			47.67	Si
SLU 39	1.39	-962	263	1239.53		0	0	5556	0			0	No, $V_u < V$
SLU 48	-1.3	-9131	18	2578.34		8004	2.535	6623	7555			429.47	Si
SLU 48	0.05	-4869	31	2343.98		4588	2.3582	6167	6545			208.69	Si
SLU 48	1.39	-698	77	890		0	0	5556	0			0	No, $V_u < V$
SLU 35	-1.3	-8100	65	3571.87		7259	2.4795	6523	7279			111.55	Si
SLU 35	0.05	-4704	84	3170.23		5870	1.7806	6338	5079			60.41	Si
SLU 35	1.39	-875	217	1126.13		0	0	5556	0			0	No, $V_u < V$
SLU 1	-1.3	-7113	17	2112.17		6235	2.535	6387	7286			426.03	Si
SLU 1	0.05	-3825	28	1914.19		3694	2.301	6048	6262			221.25	Si
SLU 1	1.39	-565	70	721.53		0	0	5556	0			0	No, $V_u < V$
SLU 83	-1.3	-10395	81	4454.3		9178	2.517	6779	7679			95.3	Si
SLU 83	0.05	-5996	104	3957.76		7312	1.8223	6530	5355			51.38	Si
SLU 83	1.39	-1094	269	1408		0	0	5556	0			0	No, $V_u < V$
SLU 43	-1.3	-9131	18	2578.34		8004	2.535	6623	7555			429.47	Si
SLU 43	0.05	-4869	31	2343.98		4588	2.3582	6167	6545			208.69	Si



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 43	1.39	-698	77	890		0	0	5556	0			0	No, Vu<V

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 4	-1.3	-5141	2535	5600.07		21364	0.5348	12606	3034			1.2	Si
SLV 4	0.05	-2723	2125	3437.65		392564	0.0154	16250	113			0.05	No, Vu<V
SLV 4	1.39	150	1759	-88.91		0	0	8333	0			0	No, Vu<V
SLV 15	-1.3	-10153	-2817	-735.05		8900	2.535	10113	11537			4.1	Si
SLV 15	0.05	-5748	-2391	1081.6		5039	2.535	9341	10656			4.46	Si
SLV 15	1.39	-1544	-1715	1873.1		20990	0.1635	12531	922			0.54	No, Vu<V
SLV 2	-1.3	-4637	2879	5793.5		189352	0.0544	16250	398			0.14	No, Vu<V
SLV 2	0.05	-2403	2480	3464.51		0	0	8333	0			0	No, Vu<V
SLV 2	1.39	236	1939	-198.83		0	0	8333	0			0	No, Vu<V
SLV 1	-1.3	-4637	2879	5793.5		189352	0.0544	16250	398			0.14	No, Vu<V
SLV 1	0.05	-2403	2480	3464.51		0	0	8333	0			0	No, Vu<V
SLV 1	1.39	236	1939	-198.83		0	0	8333	0			0	No, Vu<V
SLV 6	-1.3	-5803	1407	3801.87		7020	1.837	9737	8050			5.72	Si
SLV 6	0.05	-3088	1313	2671.24		5683	1.2077	9470	5147			3.92	Si
SLV 6	1.39	-255	933	359.63		0	0	8333	0			0	No, Vu<V
SLV 16	-1.3	-10153	-2817	-735.05		8900	2.535	10113	11537			4.1	Si
SLV 16	0.05	-5748	-2391	1081.6		5039	2.535	9341	10656			4.46	Si
SLV 16	1.39	-1544	-1715	1873.1		20990	0.1635	12531	922			0.54	No, Vu<V
SLV 7	-1.3	-7483	261	3157.12		6560	2.535	9645	11003			42.23	Si
SLV 7	0.05	-4155	130	2581.69		4763	1.9387	9286	8101			62.33	Si
SLV 7	1.39	-544	333	726.04		0	0	8333	0			0	No, Vu<V
SLV 8	-1.3	-7483	261	3157.12		6560	2.535	9645	11003			42.23	Si
SLV 8	0.05	-4155	130	2581.69		4763	1.9387	9286	8101			62.33	Si
SLV 8	1.39	-544	333	726.04		0	0	8333	0			0	No, Vu<V
SLV 3	-1.3	-5141	2535	5600.07		21364	0.5348	12606	3034			1.2	Si
SLV 3	0.05	-2723	2125	3437.65		392564	0.0154	16250	113			0.05	No, Vu<V
SLV 3	1.39	150	1759	-88.91		0	0	8333	0			0	No, Vu<V
SLV 5	-1.3	-5803	1407	3801.87		7020	1.837	9737	8050			5.72	Si
SLV 5	0.05	-3088	1313	2671.24		5683	1.2077	9470	5147			3.92	Si
SLV 5	1.39	-255	933	359.63		0	0	8333	0			0	No, Vu<V

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.045 Wa 0.08 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 2	143750	0.25	2107	-2403	153.24	531.37	3.47	Si
SLV 1	143750	0.25	2107	-2403	153.24	531.37	3.47	Si
SLV 4	143750	0.25	2387	-2723	153.24	600.75	3.92	Si
SLV 3	143750	0.25	2387	-2723	153.24	600.75	3.92	Si
SLV 5	143750	0.25	2707	-3088	153.24	679.49	4.43	Si
SLV 6	143750	0.25	2707	-3088	153.24	679.49	4.43	Si
SLV 10	143750	0.25	3503	-3996	153.24	873.32	5.7	Si
SLV 9	143750	0.25	3503	-3996	153.24	873.32	5.7	Si
SLV 8	143750	0.25	3643	-4155	153.24	907.11	5.92	Si
SLV 7	143750	0.25	3643	-4155	153.24	907.11	5.92	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 0.045 Wa = 0.08 Ta = 0.0269

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	a0*	aLim	Verifica
SLV 4	150	-5141	95	0	0	0	0	11.92381	No, Trazione
SLV 2	236	-4637	66	0	0	0	0	11.92381	No, Trazione
SLV 1	236	-4637	66	0	0	0	0	11.92381	No, Trazione
SLV 3	150	-5141	95	0	0	0	0	11.92381	No, Trazione
SLV 13	-1458	-9648	-94	0.116	639.3	0.898	1.88	11.92381	No
SLV 14	-1458	-9648	-94	0.116	639.3	0.898	1.88	11.92381	No
SLV 15	-1544	-10153	-65	0.122	646.1	0.897	1.9815	11.92381	No
SLV 16	-1544	-10153	-65	0.122	646.1	0.897	1.9815	11.92381	No
SLV 10	-764	-7306	-71	0.129	590.8	0.922	2.03233	11.4846	No
SLV 9	-764	-7306	-71	0.129	590.8	0.922	2.03233	11.4846	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF SLU	0	SLU 1	No
V SLU	0	SLU 1	No
PF SLV	0	SLV 4	No
V SLV	0	SLV 1	No
PFFP SLV	3.468	SLV 1	Si
R SLV	0	SLV 4	No

## Maschio 5

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-30.548	-3.854	-34.183	-3.854	L1	L2	3.635	0.45	2.69	2.69	2.69			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	$\tau_0$	fv0	$\mu$	$\phi$	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2



Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 82	-1.3	-30455	2225.3	18619	42700.8	19.189	Si
SLU 82	0.05	-24716	-182.74	15110	36588.21	200.216	Si
SLU 82	1.39	-20731	-933.73	12674	31816.99	34.075	Si
SLU 84	-1.3	-30455	2225.3	18619	42700.8	19.189	Si
SLU 84	0.05	-24716	-182.74	15110	36588.21	200.216	Si
SLU 84	1.39	-20731	-933.73	12674	31816.99	34.075	Si
SLU 18	-1.3	-23735	1839.22	14510	35454.64	19.277	Si
SLU 18	0.05	-19305	-79.23	11802	30003.99	378.68	Si
SLU 18	1.39	-16230	-720.73	9922	25905.49	35.943	Si
SLU 20	-1.3	-23735	1839.22	14510	35454.64	19.277	Si
SLU 20	0.05	-19305	-79.23	11802	30003.99	378.68	Si
SLU 20	1.39	-16230	-720.73	9922	25905.49	35.943	Si
SLU 81	-1.3	-30495	2300.16	18643	42739.56	18.581	Si
SLU 81	0.05	-24740	-141.8	15124	36615.99	258.228	Si
SLU 81	1.39	-20749	-930.83	12684	31838.27	34.204	Si
SLU 41	-1.3	-25437	2038.44	15550	37405.59	18.35	Si
SLU 41	0.05	-21043	-71.57	12865	32206.04	449.986	Si
SLU 41	1.39	-18048	-797.02	11033	28358.98	35.581	Si
SLU 40	-1.3	-25397	1963.59	15526	37361.41	19.027	Si
SLU 40	0.05	-21019	-112.52	12850	32175.81	285.961	Si
SLU 40	1.39	-18031	-799.92	11023	28336.44	35.424	Si
SLU 39	-1.3	-25437	2038.44	15550	37405.59	18.35	Si
SLU 39	0.05	-21043	-71.57	12865	32206.04	449.986	Si
SLU 39	1.39	-18048	-797.02	11033	28358.98	35.581	Si
SLU 42	-1.3	-25397	1963.59	15526	37361.41	19.027	Si
SLU 42	0.05	-21019	-112.52	12850	32175.81	285.961	Si
SLU 42	1.39	-18031	-799.92	11023	28336.44	35.424	Si
SLU 83	-1.3	-30495	2300.16	18643	42739.56	18.581	Si
SLU 83	0.05	-24740	-141.8	15124	36615.99	258.228	Si
SLU 83	1.39	-20749	-930.83	12684	31838.27	34.204	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 1	-1.3	-24204	5419.47	14797	38663.85	7.134	Si
SLV 1	0.05	-18778	2141.01	11480	30922.76	14.443	Si
SLV 1	1.39	-14695	-114.02	8984	24744.4	217.025	Si
SLV 3	-1.3	-21958	4196.7	13424	35523.87	8.465	Si
SLV 3	0.05	-16943	937.32	10358	28183.89	30.068	Si
SLV 3	1.39	-13278	-878.57	8117	22529.64	25.644	Si
SLV 16	-1.3	-16348	-2809.83	9994	27282.62	9.71	Si
SLV 16	0.05	-12829	-2528.86	7843	21820.79	8.629	Si
SLV 16	1.39	-10563	-1071.01	6457	18183.16	16.978	Si
SLV 6	-1.3	-24862	4393.75	15199	39565.62	9.005	Si
SLV 6	0.05	-19479	2332.15	11908	31952.75	13.701	Si
SLV 6	1.39	-15398	710.61	9413	25829.19	36.348	Si
SLV 15	-1.3	-16348	-2809.83	9994	27282.62	9.71	Si
SLV 15	0.05	-12829	-2528.86	7843	21820.79	8.629	Si
SLV 15	1.39	-10563	-1071.01	6457	18183.16	16.978	Si
SLV 5	-1.3	-24862	4393.75	15199	39565.62	9.005	Si
SLV 5	0.05	-19479	2332.15	11908	31952.75	13.701	Si
SLV 5	1.39	-15398	710.61	9413	25829.19	36.348	Si
SLV 11	-1.3	-15691	-1784.11	9592	26279.04	14.729	Si
SLV 11	0.05	-12129	-2720	7415	20706.05	7.613	Si
SLV 11	1.39	-9860	-1895.64	6028	17036.58	8.987	Si
SLV 12	-1.3	-15691	-1784.11	9592	26279.04	14.729	Si
SLV 12	0.05	-12129	-2720	7415	20706.05	7.613	Si
SLV 12	1.39	-9860	-1895.64	6028	17036.58	8.987	Si
SLV 4	-1.3	-21958	4196.7	13424	35523.87	8.465	Si
SLV 4	0.05	-16943	937.32	10358	28183.89	30.068	Si
SLV 4	1.39	-13278	-878.57	8117	22529.64	25.644	Si
SLV 2	-1.3	-24204	5419.47	14797	38663.85	7.134	Si
SLV 2	0.05	-18778	2141.01	11480	30922.76	14.443	Si
SLV 2	1.39	-14695	-114.02	8984	24744.4	217.025	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 80	-1.3	-28976	2644	2003.55		17714	3.635	7917	12951			4.9	Si
SLU 80	0.05	-23216	1234	-226.57		14193	3.635	7448	12183			9.87	Si
SLU 80	1.39	-19186	679	-877.47		11729	3.635	7119	11646			17.16	Si
SLU 62	-1.3	-28793	2681	2100.93		17603	3.635	7903	12927			4.82	Si
SLU 62	0.05	-23002	1300	-149.46		14062	3.635	7430	12154			9.35	Si
SLU 62	1.39	-18931	774	-854.54		11573	3.635	7099	11612			15.01	Si
SLU 60	-1.3	-28793	2681	2100.93		17603	3.635	7903	12927			4.82	Si
SLU 60	0.05	-23002	1300	-149.46		14062	3.635	7430	12154			9.35	Si
SLU 60	1.39	-18931	774	-854.54		11573	3.635	7099	11612			15.01	Si
SLU 74	-1.3	-29015	2703	2078.41		17738	3.635	7921	12956			4.79	Si
SLU 74	0.05	-23240	1306	-185.63		14208	3.635	7450	12186			9.33	Si
SLU 74	1.39	-19203	764	-874.57		11740	3.635	7121	11648			15.25	Si
SLU 79	-1.3	-29015	2703	2078.41		17738	3.635	7921	12956			4.79	Si
SLU 79	0.05	-23240	1306	-185.63		14208	3.635	7450	12186			9.33	Si
SLU 79	1.39	-19203	764	-874.57		11740	3.635	7121	11648			15.25	Si
SLU 77	-1.3	-29015	2703	2078.41		17738	3.635	7921	12956			4.79	Si
SLU 77	0.05	-23240	1306	-185.63		14208	3.635	7450	12186			9.33	Si
SLU 77	1.39	-19203	764	-874.57		11740	3.635	7121	11648			15.25	Si
SLU 83	-1.3	-30495	2895	2300.16		18643	3.635	8041	13153			4.54	Si
SLU 83	0.05	-24740	1449	-141.8		15124	3.635	7572	12386			8.55	Si
SLU 83	1.39	-20749	903	-930.83		12684	3.635	7247	11854			13.13	Si



Comb.	Quota	N	V par	M	$\alpha 0$	$\alpha N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 84	-1.3	-30455	2836	2225.3		18619	3.635	8038	13148			4.64	Si
SLU 84	0.05	-24716	1378	-182.74		15110	3.635	7570	12383			8.99	Si
SLU 84	1.39	-20731	818	-933.73		12674	3.635	7245	11852			14.49	Si
SLU 81	-1.3	-30495	2895	2300.16		18643	3.635	8041	13153			4.54	Si
SLU 81	0.05	-24740	1449	-141.8		15124	3.635	7572	12386			8.55	Si
SLU 81	1.39	-20749	903	-930.83		12684	3.635	7247	11854			13.13	Si
SLU 82	-1.3	-30455	2836	2225.3		18619	3.635	8038	13148			4.64	Si
SLU 82	0.05	-24716	1378	-182.74		15110	3.635	7570	12383			8.99	Si
SLU 82	1.39	-20731	818	-933.73		12674	3.635	7245	11852			14.49	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma M = 2$

Comb.	Quota	N	V par	M	$\alpha 0$	$\alpha N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 4	-1.3	-21958	5878	4196.7		13424	3.635	11018	18023			3.07	Si
SLV 4	0.05	-16943	4975	937.32		10358	3.635	10405	17020			3.42	Si
SLV 4	1.39	-13278	3551	-878.57		8117	3.635	9957	16287			4.59	Si
SLV 13	-1.3	-18595	-2249	-1587.06		11368	3.635	10607	17350			7.72	Si
SLV 13	0.05	-14664	-3354	-1325.17		8965	3.635	10126	16564			4.94	Si
SLV 13	1.39	-11980	-2747	-306.46		7324	3.635	9798	16027			5.83	Si
SLV 3	-1.3	-21958	5878	4196.7		13424	3.635	11018	18023			3.07	Si
SLV 3	0.05	-16943	4975	937.32		10358	3.635	10405	17020			3.42	Si
SLV 3	1.39	-13278	3551	-878.57		8117	3.635	9957	16287			4.59	Si
SLV 14	-1.3	-18595	-2249	-1587.06		11368	3.635	10607	17350			7.72	Si
SLV 14	0.05	-14664	-3354	-1325.17		8965	3.635	10126	16564			4.94	Si
SLV 14	1.39	-11980	-2747	-306.46		7324	3.635	9798	16027			5.83	Si
SLV 6	-1.3	-24862	5441	4393.75		15199	3.635	11373	18604			3.42	Si
SLV 6	0.05	-19479	4222	2332.15		11908	3.635	10715	17527			4.15	Si
SLV 6	1.39	-15398	3216	710.61		9413	3.635	10216	16711			5.2	Si
SLV 15	-1.3	-16348	-3574	-2809.83		9994	3.635	10332	16901			4.73	Si
SLV 15	0.05	-12829	-4545	-2528.86		7843	3.635	9902	16197			3.56	Si
SLV 15	1.39	-10563	-3776	-1071.01		6457	3.635	9625	15744			4.17	Si
SLV 16	-1.3	-16348	-3574	-2809.83		9994	3.635	10332	16901			4.73	Si
SLV 16	0.05	-12829	-4545	-2528.86		7843	3.635	9902	16197			3.56	Si
SLV 16	1.39	-10563	-3776	-1071.01		6457	3.635	9625	15744			4.17	Si
SLV 5	-1.3	-24862	5441	4393.75		15199	3.635	11373	18604			3.42	Si
SLV 5	0.05	-19479	4222	2332.15		11908	3.635	10715	17527			4.15	Si
SLV 5	1.39	-15398	3216	710.61		9413	3.635	10216	16711			5.2	Si
SLV 1	-1.3	-24204	7203	5419.47		14797	3.635	11293	18472			2.56	Si
SLV 1	0.05	-18778	6165	2141.01		11480	3.635	10629	17387			2.82	Si
SLV 1	1.39	-14695	4580	-114.02		8984	3.635	10130	16570			3.62	Si
SLV 2	-1.3	-24204	7203	5419.47		14797	3.635	11293	18472			2.56	Si
SLV 2	0.05	-18778	6165	2141.01		11480	3.635	10629	17387			2.82	Si
SLV 2	1.39	-14695	4580	-114.02		8984	3.635	10130	16570			3.62	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.045 Wa 0.08 denominatore 8  $\gamma M = 2$

Comb.	fd	Sa	$\alpha 0$	N	M	Mc	Coeff.s.	Verifica
SLV 11	143750	0.25	7415	-12129	219.73	2563.33	11.67	Si
SLV 12	143750	0.25	7415	-12129	219.73	2563.33	11.67	Si
SLV 15	143750	0.25	7843	-12829	219.73	2701.34	12.29	Si
SLV 16	143750	0.25	7843	-12829	219.73	2701.34	12.29	Si
SLV 8	143750	0.25	8169	-13363	219.73	2805.6	12.77	Si
SLV 7	143750	0.25	8169	-13363	219.73	2805.6	12.77	Si
SLV 13	143750	0.25	8965	-14664	219.73	3057.39	13.91	Si
SLV 14	143750	0.25	8965	-14664	219.73	3057.39	13.91	Si
SLV 4	143750	0.25	10358	-16943	219.73	3489.06	15.88	Si
SLV 3	143750	0.25	10358	-16943	219.73	3489.06	15.88	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 0.045 Wa = 0.08 Ta = 0.0269

Comb.	N top	N base	V orto	$\alpha 0$	M*	e*	a0*	aLim	Verifica
SLV 10	-14583	-23179	332	0.084	2116.2	0.923	1.31709	11.4846	No
SLV 9	-14583	-23179	332	0.084	2116.2	0.923	1.31709	11.4846	No
SLV 6	-15398	-24862	309	0.085	2198.1	0.925	1.33239	11.4846	No
SLV 5	-15398	-24862	309	0.085	2198.1	0.925	1.33239	11.4846	No
SLV 7	-10675	-17374	-334	0.083	1725.3	0.91	1.33308	11.4846	No
SLV 8	-10675	-17374	-334	0.083	1725.3	0.91	1.33308	11.4846	No
SLV 11	-9860	-15691	-311	0.085	1644.4	0.907	1.36355	11.4846	No
SLV 12	-9860	-15691	-311	0.085	1644.4	0.907	1.36355	11.4846	No
SLV 3	-13278	-21958	-135	0.095	1985.2	0.919	1.50318	11.92381	No
SLV 4	-13278	-21958	-135	0.095	1985.2	0.919	1.50318	11.92381	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	18.35	SLU 39	Si
V_SLU	4.543	SLU 81	Si
PF_SLV	7.134	SLV 1	Si
V_SLV	2.564	SLV 1	Si
PFFP_SLV	11.666	SLV 11	Si
R_SLV	0.115	SLV 9	No

## Maschio 8

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)



## Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-25.893	-3.854	-26.838	-3.854	L1	L2	0.945	0.45	2.69	2.69	2.69			

## Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	τ0	fv0	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

## Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 51	-1.3	-5838	-235.11	13725	2293.98	9.757	Si
SLU 51	0.05	-3928	-8.1	9236	1646	203.305	Si
SLU 51	1.39	-2988	-27.07	7025	1290.31	47.669	Si
SLU 70	-1.3	-6026	-239.6	14169	2352.57	9.819	Si
SLU 70	0.05	-4052	-14.18	9527	1691.03	119.219	Si
SLU 70	1.39	-3143	-41.16	7389	1350.5	32.812	Si
SLU 67	-1.3	-6026	-239.6	14169	2352.57	9.819	Si
SLU 67	0.05	-4052	-14.18	9527	1691.03	119.219	Si
SLU 67	1.39	-3143	-41.16	7389	1350.5	32.812	Si
SLU 65	-1.3	-6052	-243.24	14229	2360.55	9.705	Si
SLU 65	0.05	-4074	-14.48	9579	1698.98	117.362	Si
SLU 65	1.39	-3161	-39.87	7433	1357.68	34.051	Si
SLU 68	-1.3	-6052	-243.24	14229	2360.55	9.705	Si
SLU 68	0.05	-4074	-14.48	9579	1698.98	117.362	Si
SLU 68	1.39	-3161	-39.87	7433	1357.68	34.051	Si
SLU 72	-1.3	-6026	-239.6	14169	2352.57	9.819	Si
SLU 72	0.05	-4052	-14.18	9527	1691.03	119.219	Si
SLU 72	1.39	-3143	-41.16	7389	1350.5	32.812	Si
SLU 47	-1.3	-5864	-238.75	13786	2302.09	9.642	Si
SLU 47	0.05	-3950	-8.39	9288	1654.02	197.182	Si
SLU 47	1.39	-3007	-25.78	7069	1297.58	50.329	Si
SLU 49	-1.3	-5838	-235.11	13725	2293.98	9.757	Si
SLU 49	0.05	-3928	-8.1	9236	1646	203.305	Si
SLU 49	1.39	-2988	-27.07	7025	1290.31	47.669	Si
SLU 44	-1.3	-5864	-238.75	13786	2302.09	9.642	Si
SLU 44	0.05	-3950	-8.39	9288	1654.02	197.182	Si
SLU 44	1.39	-3007	-25.78	7069	1297.58	50.329	Si
SLU 46	-1.3	-5838	-235.11	13725	2293.98	9.757	Si
SLU 46	0.05	-3928	-8.1	9236	1646	203.305	Si
SLU 46	1.39	-2988	-27.07	7025	1290.31	47.669	Si

## Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γM = 2

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLV 1	-1.3	82	602.52	0	0	0	No, Trazione
SLV 1	0.05	1420	456.83	0	0	0	No, Trazione
SLV 1	1.39	350	308.43	0	0	0	No, Trazione
SLV 10	-1.3	-5018	1117.91	11799	2142.63	1.917	Si
SLV 10	0.05	-75	-110.28	0	0	0	No, e>l/2
SLV 10	1.39	-2609	635.34	6133	1170.9	1.843	Si
SLV 6	-1.3	-2356	1334.18	0	0	0	No, e>l/2
SLV 6	0.05	1911	164.35	0	0	0	No, Trazione
SLV 6	1.39	-1058	714.63	0	0	0	No, e>l/2
SLV 9	-1.3	-5018	1117.91	11799	2142.63	1.917	Si
SLV 9	0.05	-75	-110.28	0	0	0	No, e>l/2
SLV 9	1.39	-2609	635.34	6133	1170.9	1.843	Si
SLV 7	-1.3	-4264	-1477.18	10025	1849.71	1.252	Si
SLV 7	0.05	-6115	84.61	14376	2549.68	30.134	Si
SLV 7	1.39	-2204	-710.25	5182	997.36	1.404	Si
SLV 2	-1.3	82	602.52	0	0	0	No, Trazione
SLV 2	0.05	1420	456.83	0	0	0	No, Trazione
SLV 2	1.39	350	308.43	0	0	0	No, Trazione
SLV 8	-1.3	-4264	-1477.18	10025	1849.71	1.252	Si
SLV 8	0.05	-6115	84.61	14376	2549.68	30.134	Si
SLV 8	1.39	-2204	-710.25	5182	997.36	1.404	Si
SLV 4	-1.3	-490	-240.88	0	0	0	No, e>l/2
SLV 4	0.05	-987	432.91	2321	457.75	1.057	Si
SLV 4	1.39	6	-119.03	0	0	0	No, Trazione
SLV 3	-1.3	-490	-240.88	0	0	0	No, e>l/2
SLV 3	0.05	-987	432.91	2321	457.75	1.057	Si
SLV 3	1.39	6	-119.03	0	0	0	No, Trazione
SLV 5	-1.3	-2356	1334.18	0	0	0	No, e>l/2
SLV 5	0.05	1911	164.35	0	0	0	No, Trazione
SLV 5	1.39	-1058	714.63	0	0	0	No, e>l/2

## Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, γM = 3

Comb.	Quota	N	V par	M	σ0	σN	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 80	-1.3	-6295	-1041	-241.42		14801	0.9452	7529	3202			3.08	Si
SLU 80	0.05	-4159	-118	-26.78		9779	0.9452	6859	2917			24.66	Si
SLU 80	1.39	-3297	298	-67.09		7753	0.9452	6589	2803			9.39	Si
SLU 83	-1.3	-6372	-1078	-236.74		14981	0.9452	7553	3213			2.98	Si
SLU 83	0.05	-4172	-121	-31.73		9809	0.9452	6863	2919			24.08	Si
SLU 83	1.39	-3336	346	-80.14		7843	0.9452	6601	2808			8.11	Si
SLU 81	-1.3	-6372	-1078	-236.74		14981	0.9452	7553	3213			2.98	Si
SLU 81	0.05	-4172	-121	-31.73		9809	0.9452	6863	2919			24.08	Si
SLU 81	1.39	-3336	346	-80.14		7843	0.9452	6601	2808			8.11	Si
SLU 82	-1.3	-6411	-1090	-242.2		15073	0.9452	7565	3218			2.95	Si



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 82	0.05	-4205	-128	-32.17		9886	0.9452	6874	2924			22.77	Si
SLU 82	1.39	-3364	339	-78.21		7909	0.9452	6610	2811			8.3	Si
SLU 78	-1.3	-6295	-1041	-241.42		14801	0.9452	7529	3202			3.08	Si
SLU 78	0.05	-4159	-118	-26.78		9779	0.9452	6859	2917			24.66	Si
SLU 78	1.39	-3297	298	-67.09		7753	0.9452	6589	2803			9.39	Si
SLU 73	-1.3	-6321	-1049	-245.06		14862	0.9452	7537	3206			3.06	Si
SLU 73	0.05	-4181	-123	-27.07		9830	0.9452	6866	2920			23.73	Si
SLU 73	1.39	-3316	293	-65.8		7796	0.9452	6595	2805			9.56	Si
SLU 84	-1.3	-6411	-1090	-242.2		15073	0.9452	7565	3218			2.95	Si
SLU 84	0.05	-4205	-128	-32.17		9886	0.9452	6874	2924			22.77	Si
SLU 84	1.39	-3364	339	-78.21		7909	0.9452	6610	2811			8.3	Si
SLU 75	-1.3	-6295	-1041	-241.42		14801	0.9452	7529	3202			3.08	Si
SLU 75	0.05	-4159	-118	-26.78		9779	0.9452	6859	2917			24.66	Si
SLU 75	1.39	-3297	298	-67.09		7753	0.9452	6589	2803			9.39	Si
SLU 63	-1.3	-6222	-1035	-237.71		14629	0.9452	7506	3193			3.08	Si
SLU 63	0.05	-4081	-123	-26.08		9595	0.9452	6835	2907			23.66	Si
SLU 63	1.39	-3209	288	-64.12		7545	0.9452	6562	2791			9.7	Si
SLU 76	-1.3	-6321	-1049	-245.06		14862	0.9452	7537	3206			3.06	Si
SLU 76	0.05	-4181	-123	-27.07		9830	0.9452	6866	2920			23.73	Si
SLU 76	1.39	-3316	293	-65.8		7796	0.9452	6595	2805			9.56	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 6	-1.3	-2356	-1425	1334.18		0	0	8333	0			0	No, Vu<V
SLV 6	0.05	1911	-705	164.35		0	0	8333	0			0	No, Vu<V
SLV 6	1.39	-1058	-1256	714.63		0	0	8333	0			0	No, Vu<V
SLV 7	-1.3	-4264	845	-1477.18		25038	0.3784	13341	2272			2.69	Si
SLV 7	0.05	-6115	1405	84.61		14376	0.9452	11209	4767			3.39	Si
SLV 7	1.39	-2204	1530	-710.25		10861	0.4509	10505	2132			1.39	Si
SLV 4	-1.3	-490	1063	-240.88		0	0	8333	0			0	No, Vu<V
SLV 4	0.05	-987	1653	432.91		21425	0.1024	12618	582			0.35	No, Vu<V
SLV 4	1.39	6	457	-119.03		0	0	8333	0			0	No, Vu<V
SLV 5	-1.3	-2356	-1425	1334.18		0	0	8333	0			0	No, Vu<V
SLV 5	0.05	1911	-705	164.35		0	0	8333	0			0	No, Vu<V
SLV 5	1.39	-1058	-1256	714.63		0	0	8333	0			0	No, Vu<V
SLV 8	-1.3	-4264	845	-1477.18		25038	0.3784	13341	2272			2.69	Si
SLV 8	0.05	-6115	1405	84.61		14376	0.9452	11209	4767			3.39	Si
SLV 8	1.39	-2204	1530	-710.25		10861	0.4509	10505	2132			1.39	Si
SLV 1	-1.3	82	382	602.52		0	0	8333	0			0	No, Vu<V
SLV 1	0.05	1420	1020	456.83		0	0	8333	0			0	No, Vu<V
SLV 1	1.39	350	-379	308.43		0	0	8333	0			0	No, Vu<V
SLV 2	-1.3	82	382	602.52		0	0	8333	0			0	No, Vu<V
SLV 2	0.05	1420	1020	456.83		0	0	8333	0			0	No, Vu<V
SLV 2	1.39	350	-379	308.43		0	0	8333	0			0	No, Vu<V
SLV 10	-1.3	-5018	-2293	1117.91		14880	0.7495	11309	3814			1.66	Si
SLV 10	0.05	-75	-1550	-110.28		0	0	8333	0			0	No, Vu<V
SLV 10	1.39	-2609	-1173	635.34		8437	0.6871	10021	3098			2.64	Si
SLV 9	-1.3	-5018	-2293	1117.91		14880	0.7495	11309	3814			1.66	Si
SLV 9	0.05	-75	-1550	-110.28		0	0	8333	0			0	No, Vu<V
SLV 9	1.39	-2609	-1173	635.34		8437	0.6871	10021	3098			2.64	Si
SLV 3	-1.3	-490	1063	-240.88		0	0	8333	0			0	No, Vu<V
SLV 3	0.05	-987	1653	432.91		21425	0.1024	12618	582			0.35	No, Vu<V
SLV 3	1.39	6	457	-119.03		0	0	8333	0			0	No, Vu<V

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.045 Wa 0.08 denominatore  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 6	143750	0.25	0	1911	57.13	0	0	No, Trazione
SLV 2	143750	0.25	0	1420	57.13	0	0	No, Trazione
SLV 1	143750	0.25	0	1420	57.13	0	0	No, Trazione
SLV 9	143750	0.25	0	-75	57.13	0	0	No, e>t/2
SLV 10	143750	0.25	0	-75	57.13	0	0	No, e>t/2
SLV 5	143750	0.25	0	1911	57.13	0	0	No, Trazione
SLV 3	143750	0.25	2321	-987	57.13	217.94	3.81	Si
SLV 4	143750	0.25	2321	-987	57.13	217.94	3.81	Si
SLV 14	143750	0.25	12232	-5203	57.13	1053.42	18.44	Si
SLV 13	143750	0.25	12232	-5203	57.13	1053.42	18.44	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 0.045 Wa = 0.08 Ta = 0.0269

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	$\alpha_0^*$	$\alpha_{lim}$	Verifica
SLV 1	350	82	15	0	0	0	0	11.92381	No, Trazione
SLV 4	6	-490	4	0	0	0	0	11.92381	No, Trazione
SLV 3	6	-490	4	0	0	0	0	11.92381	No, Trazione
SLV 2	350	82	15	0	0	0	0	11.92381	No, Trazione
SLV 15	-5162	-9365	-27	0.093	688.4	0.935	1.44832	11.92381	No
SLV 16	-5162	-9365	-27	0.093	688.4	0.935	1.44832	11.92381	No
SLV 14	-4818	-8792	-16	0.096	653.7	0.932	1.48971	11.92381	No
SLV 13	-4818	-8792	-16	0.096	653.7	0.932	1.48971	11.92381	No
SLV 12	-3754	-6926	-28	0.096	546.5	0.922	1.50828	11.4846	No
SLV 11	-3754	-6926	-28	0.096	546.5	0.922	1.50828	11.4846	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	9.642	SLU 44	Si
V_SLU	2.951	SLU 82	Si
PF_SLV	0	SLV 6	No



Stato limite	Coeff.s.	Comb.	Verifica
V_SLV	0	SLV 1	No
PFFP_SLV	0	SLV 6	No
R_SLV	0	SLV 4	No

## Maschio 9

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-34.183	5.726	-27.948	5.726	L1	L2	6.235	0.45	2.69	2.69	2.69			

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	τ0	fv0	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 41	-1.3	-34521	-1326.3	12304	91363.37	68.886	Si
SLU 41	0.05	-27609	2628.16	9840	75674.85	28.794	Si
SLU 41	1.39	-20492	7785.24	7304	58156.14	7.47	Si
SLU 40	-1.3	-34527	-1140.91	12306	91376.83	80.091	Si
SLU 40	0.05	-27645	2719.51	9853	75759.72	27.858	Si
SLU 40	1.39	-20542	7810.07	7321	58283.25	7.463	Si
SLU 21	-1.3	-32305	-1317.28	11514	86476.6	65.648	Si
SLU 21	0.05	-25650	2245.52	9142	70988.64	31.613	Si
SLU 21	1.39	-18620	6909.38	6636	53317.55	7.717	Si
SLU 18	-1.3	-32299	-1502.67	11512	86462.76	57.539	Si
SLU 18	0.05	-25614	2154.16	9129	70901.82	32.914	Si
SLU 18	1.39	-18570	6884.55	6618	53187.82	7.726	Si
SLU 39	-1.3	-34521	-1326.3	12304	91363.37	68.886	Si
SLU 39	0.05	-27609	2628.16	9840	75674.85	28.794	Si
SLU 39	1.39	-20492	7785.24	7304	58156.14	7.47	Si
SLU 20	-1.3	-32299	-1502.67	11512	86462.76	57.539	Si
SLU 20	0.05	-25614	2154.16	9129	70901.82	32.914	Si
SLU 20	1.39	-18570	6884.55	6618	53187.82	7.726	Si
SLU 82	-1.3	-41480	-1816.05	14784	105845.05	58.283	Si
SLU 82	0.05	-32795	2680.51	11688	87567.73	32.668	Si
SLU 82	1.39	-23523	8491.26	8384	65785.48	7.747	Si
SLU 42	-1.3	-34527	-1140.91	12306	91376.83	80.091	Si
SLU 42	0.05	-27645	2719.51	9853	75759.72	27.858	Si
SLU 42	1.39	-20542	7810.07	7321	58283.25	7.463	Si
SLU 19	-1.3	-32305	-1317.28	11514	86476.6	65.648	Si
SLU 19	0.05	-25650	2245.52	9142	70988.64	31.613	Si
SLU 19	1.39	-18620	6909.38	6636	53317.55	7.717	Si
SLU 84	-1.3	-41480	-1816.05	14784	105845.05	58.283	Si
SLU 84	0.05	-32795	2680.51	11688	87567.73	32.668	Si
SLU 84	1.39	-23523	8491.26	8384	65785.48	7.747	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γM = 2

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLV 14	-1.3	-24912	2795.97	8879	72018.99	25.758	Si
SLV 14	0.05	-19446	5635.42	6931	57184.35	10.147	Si
SLV 14	1.39	-13660	6775.69	4869	40888.77	6.035	Si
SLV 13	-1.3	-24912	2795.97	8879	72018.99	25.758	Si
SLV 13	0.05	-19446	5635.42	6931	57184.35	10.147	Si
SLV 13	1.39	-13660	6775.69	4869	40888.77	6.035	Si
SLV 11	-1.3	-32245	-2854.62	11493	91069.89	31.903	Si
SLV 11	0.05	-25338	881.65	9031	73152.92	82.973	Si
SLV 11	1.39	-18779	5063.02	6693	55336.52	10.93	Si
SLV 12	-1.3	-32245	-2854.62	11493	91069.89	31.903	Si
SLV 12	0.05	-25338	881.65	9031	73152.92	82.973	Si
SLV 12	1.39	-18779	5063.02	6693	55336.52	10.93	Si
SLV 10	-1.3	-22329	1495.7	7958	65077.31	43.51	Si
SLV 10	0.05	-16843	3516.33	6003	49929.6	14.199	Si
SLV 10	1.39	-9786	4992.65	3488	29635.74	5.936	Si
SLV 15	-1.3	-27887	1490.88	9939	79864.81	53.569	Si
SLV 15	0.05	-21994	4845.02	7839	64168.51	13.244	Si
SLV 15	1.39	-16358	6796.8	5830	48563.33	7.145	Si
SLV 5	-1.3	-23090	-923.92	8230	67136.07	72.665	Si
SLV 5	0.05	-17161	909.57	6116	50821.37	55.874	Si
SLV 5	1.39	-9162	3485.45	3266	27800.62	7.976	Si
SLV 16	-1.3	-27887	1490.88	9939	79864.81	53.569	Si
SLV 16	0.05	-21994	4845.02	7839	64168.51	13.244	Si
SLV 16	1.39	-16358	6796.8	5830	48563.33	7.145	Si
SLV 9	-1.3	-22329	1495.7	7958	65077.31	43.51	Si
SLV 9	0.05	-16843	3516.33	6003	49929.6	14.199	Si
SLV 9	1.39	-9786	4992.65	3488	29635.74	5.936	Si
SLV 6	-1.3	-23090	-923.92	8230	67136.07	72.665	Si
SLV 6	0.05	-17161	909.57	6116	50821.37	55.874	Si
SLV 6	1.39	-9162	3485.45	3266	27800.62	7.976	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, γM = 3

Comb.	Quota	N	V par	M	σ0	σN	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
-------	-------	---	-------	---	----	----	----	-----	-----------	---------------	--------	------	----------



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 79	-1.3	-39499	-1491	-2165.31		14078	6.235	7433	20854			13.99	Si
SLU 79	0.05	-30908	-311	2066.41		11016	6.235	7024	19709			63.3	Si
SLU 79	1.39	-21543	-209	7391.06		7678	6.235	6579	18460			88.47	Si
SLU 62	-1.3	-39253	-1505	-2177.81		13990	6.235	7421	20821			13.83	Si
SLU 62	0.05	-30763	-336	2115.16		10964	6.235	7017	19689			58.58	Si
SLU 62	1.39	-21551	-234	7565.74		7681	6.235	6580	18461			78.9	Si
SLU 60	-1.3	-39253	-1505	-2177.81		13990	6.235	7421	20821			13.83	Si
SLU 60	0.05	-30763	-336	2115.16		10964	6.235	7017	19689			58.58	Si
SLU 60	1.39	-21551	-234	7565.74		7681	6.235	6580	18461			78.9	Si
SLU 81	-1.3	-41474	-1620	-2001.44		14782	6.235	7526	21117			13.04	Si
SLU 81	0.05	-32759	-388	2589.15		11676	6.235	7112	19955			51.39	Si
SLU 81	1.39	-23473	-293	8466.43		8366	6.235	6671	18717			63.99	Si
SLU 82	-1.3	-41480	-1480	-1816.05		14784	6.235	7527	21118			14.27	Si
SLU 82	0.05	-32795	-225	2680.51		11688	6.235	7114	19960			88.52	Si
SLU 82	1.39	-23523	-122	8491.26		8384	6.235	6673	18724			153.71	Si
SLU 77	-1.3	-39499	-1491	-2165.31		14078	6.235	7433	20854			13.99	Si
SLU 77	0.05	-30908	-311	2066.41		11016	6.235	7024	19709			63.3	Si
SLU 77	1.39	-21543	-209	7391.06		7678	6.235	6579	18460			88.47	Si
SLU 39	-1.3	-34521	-1401	-1326.3		12304	6.235	7196	20190			14.41	Si
SLU 39	0.05	-27609	-384	2628.16		9840	6.235	6868	19269			50.21	Si
SLU 39	1.39	-20492	-318	7785.24		7304	6.235	6529	18320			57.53	Si
SLU 74	-1.3	-39499	-1491	-2165.31		14078	6.235	7433	20854			13.99	Si
SLU 74	0.05	-30908	-311	2066.41		11016	6.235	7024	19709			63.3	Si
SLU 74	1.39	-21543	-209	7391.06		7678	6.235	6579	18460			88.47	Si
SLU 83	-1.3	-41474	-1620	-2001.44		14782	6.235	7526	21117			13.04	Si
SLU 83	0.05	-32759	-388	2589.15		11676	6.235	7112	19955			51.39	Si
SLU 83	1.39	-23473	-293	8466.43		8366	6.235	6671	18717			63.99	Si
SLU 84	-1.3	-41480	-1480	-1816.05		14784	6.235	7527	21118			14.27	Si
SLU 84	0.05	-32795	-225	2680.51		11688	6.235	7114	19960			88.52	Si
SLU 84	1.39	-23523	-122	8491.26		8384	6.235	6673	18724			153.71	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 4	-1.3	-30424	-6290	-6574.51		10843	6.235	10502	29466			4.68	Si
SLV 4	0.05	-23053	-5254	-3844.2		8216	6.235	9977	27992			5.33	Si
SLV 4	1.39	-14281	-3156	1772.78		5090	6.235	9351	26237			8.31	Si
SLV 14	-1.3	-24912	4337	2795.97		8879	6.235	10109	28364			6.54	Si
SLV 14	0.05	-19446	4972	5635.42		6931	6.235	9719	27270			5.49	Si
SLV 14	1.39	-13660	3049	6775.69		4869	6.235	9307	26113			8.56	Si
SLV 5	-1.3	-23090	-2570	-923.92		8230	6.235	9979	27999			10.9	Si
SLV 5	0.05	-17161	-2164	909.57		6116	6.235	9557	26813			12.39	Si
SLV 5	1.39	-9162	-3267	3485.45		3266	6.235	8986	25214			7.72	Si
SLV 16	-1.3	-27887	4337	1490.88		9939	6.235	10321	28959			6.68	Si
SLV 16	0.05	-21994	5241	4845.02		7839	6.235	9901	27780			5.3	Si
SLV 16	1.39	-16358	4306	6796.8		5830	6.235	9499	26653			6.19	Si
SLV 15	-1.3	-27887	4337	1490.88		9939	6.235	10321	28959			6.68	Si
SLV 15	0.05	-21994	5241	4845.02		7839	6.235	9901	27780			5.3	Si
SLV 15	1.39	-16358	4306	6796.8		5830	6.235	9499	26653			6.19	Si
SLV 13	-1.3	-24912	4337	2795.97		8879	6.235	10109	28364			6.54	Si
SLV 13	0.05	-19446	4972	5635.42		6931	6.235	9719	27270			5.49	Si
SLV 13	1.39	-13660	3049	6775.69		4869	6.235	9307	26113			8.56	Si
SLV 6	-1.3	-23090	-2570	-923.92		8230	6.235	9979	27999			10.9	Si
SLV 6	0.05	-17161	-2164	909.57		6116	6.235	9557	26813			12.39	Si
SLV 6	1.39	-9162	-3267	3485.45		3266	6.235	8986	25214			7.72	Si
SLV 2	-1.3	-27449	-6289	-5269.41		9783	6.235	10290	28871			4.59	Si
SLV 2	0.05	-20505	-5523	-3053.8		7308	6.235	9795	27482			4.98	Si
SLV 2	1.39	-11583	-4413	1751.67		4128	6.235	9159	25698			5.82	Si
SLV 3	-1.3	-30424	-6290	-6574.51		10843	6.235	10502	29466			4.68	Si
SLV 3	0.05	-23053	-5254	-3844.2		8216	6.235	9977	27992			5.33	Si
SLV 3	1.39	-14281	-3156	1772.78		5090	6.235	9351	26237			8.31	Si
SLV 1	-1.3	-27449	-6289	-5269.41		9783	6.235	10290	28871			4.59	Si
SLV 1	0.05	-20505	-5523	-3053.8		7308	6.235	9795	27482			4.98	Si
SLV 1	1.39	-11583	-4413	1751.67		4128	6.235	9159	25698			5.82	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.045 Wa 0.08 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 10	143750	0.25	6003	-16843	376.9	3603.58	9.56	Si
SLV 9	143750	0.25	6003	-16843	376.9	3603.58	9.56	Si
SLV 5	143750	0.25	6116	-17161	376.9	3667.94	9.73	Si
SLV 6	143750	0.25	6116	-17161	376.9	3667.94	9.73	Si
SLV 13	143750	0.25	6931	-19446	376.9	4127.18	10.95	Si
SLV 14	143750	0.25	6931	-19446	376.9	4127.18	10.95	Si
SLV 1	143750	0.25	7308	-20505	376.9	4337.59	11.51	Si
SLV 2	143750	0.25	7308	-20505	376.9	4337.59	11.51	Si
SLV 16	143750	0.25	7839	-21994	376.9	4631.25	12.29	Si
SLV 15	143750	0.25	7839	-21994	376.9	4631.25	12.29	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 0.045 Wa = 0.08 Ta = 0.0269

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	$\alpha_0^*$	aLim	Verifica
SLV 6	-9162	-23090	938	0.06	2066.3	0.891	0.98657	11.4846	No
SLV 5	-9162	-23090	938	0.06	2066.3	0.891	0.98657	11.4846	No
SLV 10	-9786	-22329	877	0.065	2125.4	0.892	1.05896	11.4846	No
SLV 9	-9786	-22329	877	0.065	2125.4	0.892	1.05896	11.4846	No
SLV 11	-18779	-32245	-938	0.069	3005.9	0.911	1.10336	11.4846	No
SLV 12	-18779	-32245	-938	0.069	3005.9	0.911	1.10336	11.4846	No
SLV 8	-18156	-33007	-878	0.071	2943.9	0.91	1.13782	11.4846	No





Comb.	N top	N base	V orto	$\alpha 0$	M*	e*	a0*	aLim	Verifica
SLV 7	-18156	-33007	-878	0.071	2943.9	0.91	1.13782	11.4846	No
SLV 15	-16358	-27887	-373	0.092	2765.7	0.906	1.47662	11.92381	No
SLV 16	-16358	-27887	-373	0.092	2765.7	0.906	1.47662	11.92381	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	7.463	SLU 40	Si
V_SLU	13.039	SLU 81	Si
PF_SLV	5.936	SLV 9	Si
V_SLV	4.59	SLV 1	Si
PFFP_SLV	9.561	SLV 9	Si
R_SLV	0.086	SLV 5	No

## Maschio 11

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota l.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-26.628	5.726	-24.603	5.726	L1	L2	2.025	0.45	2.69	2.69	2.69			

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	$\tau 0$	fv0	$\mu$	$\phi$	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche,  $\gamma M = 3$

Comb.	Quota	N	M	$\alpha 0$	Mu	c.s.	Verifica
SLU 31	-1.3	-11499	1593.23	12619	9839.35	6.176	Si
SLU 31	0.05	-9176	1197.2	10070	8142.33	6.801	Si
SLU 31	1.39	-7005	1159.53	7687	6423.03	5.539	Si
SLU 84	-1.3	-14650	1985.98	16077	11905.63	5.995	Si
SLU 84	0.05	-11689	1478.89	12828	9971.55	6.743	Si
SLU 84	1.39	-8905	1435.11	9772	7934.64	5.529	Si
SLU 80	-1.3	-13984	1841.73	15346	11491.51	6.24	Si
SLU 80	0.05	-11062	1350.55	12140	9531.38	7.057	Si
SLU 80	1.39	-8255	1322.24	9059	7428.47	5.618	Si
SLU 82	-1.3	-14650	1985.98	16077	11905.63	5.995	Si
SLU 82	0.05	-11689	1478.89	12828	9971.55	6.743	Si
SLU 82	1.39	-8905	1435.11	9772	7934.64	5.529	Si
SLU 40	-1.3	-12151	1723.51	13335	10289.27	5.97	Si
SLU 40	0.05	-9808	1311.79	10763	8618.43	6.57	Si
SLU 40	1.39	-7675	1258.19	8423	6967.8	5.538	Si
SLU 73	-1.3	-13998	1855.69	15361	11500.16	6.197	Si
SLU 73	0.05	-11057	1364.3	12134	9527.88	6.984	Si
SLU 73	1.39	-8234	1336.46	9036	7412.37	5.546	Si
SLU 34	-1.3	-11499	1593.23	12619	9839.35	6.176	Si
SLU 34	0.05	-9176	1197.2	10070	8142.33	6.801	Si
SLU 34	1.39	-7005	1159.53	7687	6423.03	5.539	Si
SLU 42	-1.3	-12151	1723.51	13335	10289.27	5.97	Si
SLU 42	0.05	-9808	1311.79	10763	8618.43	6.57	Si
SLU 42	1.39	-7675	1258.19	8423	6967.8	5.538	Si
SLU 75	-1.3	-13984	1841.73	15346	11491.51	6.24	Si
SLU 75	0.05	-11062	1350.55	12140	9531.38	7.057	Si
SLU 75	1.39	-8255	1322.24	9059	7428.47	5.618	Si
SLU 76	-1.3	-13998	1855.69	15361	11500.16	6.197	Si
SLU 76	0.05	-11057	1364.3	12134	9527.88	6.984	Si
SLU 76	1.39	-8234	1336.46	9036	7412.37	5.546	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma M = 2$

Comb.	Quota	N	M	$\alpha 0$	Mu	c.s.	Verifica
SLV 9	-1.3	-7720	846.62	8472	7274.49	8.592	Si
SLV 9	0.05	-5770	842.82	6332	5539.66	6.573	Si
SLV 9	1.39	-3323	958.97	3646	3263.77	3.403	Si
SLV 12	-1.3	-12516	2139.37	13735	11247.88	5.258	Si
SLV 12	0.05	-9452	1438.21	10372	8757.63	6.089	Si
SLV 12	1.39	-6886	1331.76	7557	6541.05	4.912	Si
SLV 8	-1.3	-11935	1557.94	13098	10789.11	6.925	Si
SLV 8	0.05	-9547	850.78	10477	8837.54	10.388	Si
SLV 8	1.39	-7662	732.18	8408	7223.52	9.866	Si
SLV 16	-1.3	-11515	2365.25	12636	10452.93	4.419	Si
SLV 16	0.05	-8052	1915.16	8837	7563.35	3.949	Si
SLV 16	1.39	-4734	1900.79	5195	4589.73	2.415	Si
SLV 7	-1.3	-11935	1557.94	13098	10789.11	6.925	Si
SLV 7	0.05	-9547	850.78	10477	8837.54	10.388	Si
SLV 7	1.39	-7662	732.18	8408	7223.52	9.866	Si
SLV 10	-1.3	-7720	846.62	8472	7274.49	8.592	Si
SLV 10	0.05	-5770	842.82	6332	5539.66	6.573	Si
SLV 10	1.39	-3323	958.97	3646	3263.77	3.403	Si
SLV 13	-1.3	-10076	1977.43	11057	9278.64	4.692	Si
SLV 13	0.05	-6948	1736.54	7625	6595.73	3.798	Si
SLV 13	1.39	-3665	1788.96	4022	3588.96	2.006	Si
SLV 11	-1.3	-12516	2139.37	13735	11247.88	5.258	Si
SLV 11	0.05	-9452	1438.21	10372	8757.63	6.089	Si
SLV 11	1.39	-6886	1331.76	7557	6541.05	4.912	Si



Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 15	-1.3	-11515	2365.25	12636	10452.93	4.419	Si
SLV 15	0.05	-8052	1915.16	8837	7563.35	3.949	Si
SLV 15	1.39	-4734	1900.79	5195	4589.73	2.415	Si
SLV 14	-1.3	-10076	1977.43	11057	9278.64	4.692	Si
SLV 14	0.05	-6948	1736.54	7625	6595.73	3.798	Si
SLV 14	1.39	-3665	1788.96	4022	3588.96	2.006	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt <sub>lim</sub>	c.s.	Verifica
SLU 82	-1.3	-14650	863	1985.98	16077	2.025	7699	7016				8.13	Si
SLU 82	0.05	-11689	-470	1478.89	12828	2.025	7266	6621				14.07	Si
SLU 82	1.39	-8905	-19	1435.11	9772	2.025	6859	6250				333.62	Si
SLU 78	-1.3	-13984	811	1841.73	15346	2.025	7602	6927				8.54	Si
SLU 78	0.05	-11062	-455	1350.55	12140	2.025	7174	6537				14.35	Si
SLU 78	1.39	-8255	-67	1322.24	9059	2.025	6763	6163				91.79	Si
SLU 73	-1.3	-13998	827	1855.69	15361	2.025	7604	6929				8.38	Si
SLU 73	0.05	-11057	-443	1364.3	12134	2.025	7173	6537				14.76	Si
SLU 73	1.39	-8234	-48	1336.46	9036	2.025	6760	6160				129.47	Si
SLU 76	-1.3	-13998	827	1855.69	15361	2.025	7604	6929				8.38	Si
SLU 76	0.05	-11057	-443	1364.3	12134	2.025	7173	6537				14.76	Si
SLU 76	1.39	-8234	-48	1336.46	9036	2.025	6760	6160				129.47	Si
SLU 63	-1.3	-13911	827	1824.12	15266	2.025	7591	6917				8.37	Si
SLU 63	0.05	-11010	-430	1335.93	12083	2.025	7167	6531				15.19	Si
SLU 63	1.39	-8233	-41	1308.7	9035	2.025	6760	6160				149.79	Si
SLU 80	-1.3	-13984	811	1841.73	15346	2.025	7602	6927				8.54	Si
SLU 80	0.05	-11062	-455	1350.55	12140	2.025	7174	6537				14.35	Si
SLU 80	1.39	-8255	-67	1322.24	9059	2.025	6763	6163				91.79	Si
SLU 84	-1.3	-14650	863	1985.98	16077	2.025	7699	7016				8.13	Si
SLU 84	0.05	-11689	-470	1478.89	12828	2.025	7266	6621				14.07	Si
SLU 84	1.39	-8905	-19	1435.11	9772	2.025	6859	6250				333.62	Si
SLU 83	-1.3	-14629	839	1965.03	16054	2.025	7696	7013				8.36	Si
SLU 83	0.05	-11697	-490	1458.27	12836	2.025	7267	6622				13.53	Si
SLU 83	1.39	-8936	-48	1413.79	9806	2.025	6863	6254				130.09	Si
SLU 61	-1.3	-13911	827	1824.12	15266	2.025	7591	6917				8.37	Si
SLU 61	0.05	-11010	-430	1335.93	12083	2.025	7167	6531				15.19	Si
SLU 61	1.39	-8233	-41	1308.7	9035	2.025	6760	6160				149.79	Si
SLU 81	-1.3	-14629	839	1965.03	16054	2.025	7696	7013				8.36	Si
SLU 81	0.05	-11697	-490	1458.27	12836	2.025	7267	6622				13.53	Si
SLU 81	1.39	-8936	-48	1413.79	9806	2.025	6863	6254				130.09	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt <sub>lim</sub>	c.s.	Verifica
SLV 15	-1.3	-11515	1796	2365.25	12636	2.025	10861	9897				5.51	Si
SLV 15	0.05	-8052	545	1915.16	8837	2.025	10101	9204				16.9	Si
SLV 15	1.39	-4734	978	1900.79	5740	1.833	9481	7821				8	Si
SLV 14	-1.3	-10076	1954	1977.43	11057	2.025	10545	9609				4.92	Si
SLV 14	0.05	-6948	983	1736.54	7625	2.025	9858	8983				9.14	Si
SLV 14	1.39	-3665	1144	1788.96	5177	1.5733	9369	6633				5.8	Si
SLV 8	-1.3	-11935	-126	1557.94	13098	2.025	10953	9981				79.45	Si
SLV 8	0.05	-9547	-1400	850.78	10477	2.025	10429	9503				6.79	Si
SLV 8	1.39	-7662	-769	732.18	8408	2.025	10015	9126				11.86	Si
SLV 3	-1.3	-9579	-875	427.14	10512	2.025	10436	9510				10.87	Si
SLV 3	0.05	-8369	-1661	-42.94	9185	2.025	10170	9268				5.58	Si
SLV 3	1.39	-7319	-1412	-97.81	8032	2.025	9940	9058				6.42	Si
SLV 1	-1.3	-8141	-716	39.31	8933	2.025	10120	9222				12.88	Si
SLV 1	0.05	-7265	-1223	-221.56	7973	2.025	9928	9047				7.4	Si
SLV 1	1.39	-6250	-1246	-209.64	6858	2.025	9705	8844				7.1	Si
SLV 2	-1.3	-8141	-716	39.31	8933	2.025	10120	9222				12.88	Si
SLV 2	0.05	-7265	-1223	-221.56	7973	2.025	9928	9047				7.4	Si
SLV 2	1.39	-6250	-1246	-209.64	6858	2.025	9705	8844				7.1	Si
SLV 4	-1.3	-9579	-875	427.14	10512	2.025	10436	9510				10.87	Si
SLV 4	0.05	-8369	-1661	-42.94	9185	2.025	10170	9268				5.58	Si
SLV 4	1.39	-7319	-1412	-97.81	8032	2.025	9940	9058				6.42	Si
SLV 7	-1.3	-11935	-126	1557.94	13098	2.025	10953	9981				79.45	Si
SLV 7	0.05	-9547	-1400	850.78	10477	2.025	10429	9503				6.79	Si
SLV 7	1.39	-7662	-769	732.18	8408	2.025	10015	9126				11.86	Si
SLV 13	-1.3	-10076	1954	1977.43	11057	2.025	10545	9609				4.92	Si
SLV 13	0.05	-6948	983	1736.54	7625	2.025	9858	8983				9.14	Si
SLV 13	1.39	-3665	1144	1788.96	5177	1.5733	9369	6633				5.8	Si
SLV 16	-1.3	-11515	1796	2365.25	12636	2.025	10861	9897				5.51	Si
SLV 16	0.05	-8052	545	1915.16	8837	2.025	10101	9204				16.9	Si
SLV 16	1.39	-4734	978	1900.79	5740	1.833	9481	7821				8	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.045  $W_a$  0.08 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 10	143750	0.25	6332	-5770	122.41	1231.03	10.06	Si
SLV 9	143750	0.25	6332	-5770	122.41	1231.03	10.06	Si
SLV 5	143750	0.25	6437	-5865	122.41	1250.21	10.21	Si
SLV 6	143750	0.25	6437	-5865	122.41	1250.21	10.21	Si
SLV 13	143750	0.25	7625	-6948	122.41	1465.72	11.97	Si
SLV 14	143750	0.25	7625	-6948	122.41	1465.72	11.97	Si
SLV 1	143750	0.25	7973	-7265	122.41	1527.97	12.48	Si
SLV 2	143750	0.25	7973	-7265	122.41	1527.97	12.48	Si
SLV 16	143750	0.25	8837	-8052	122.41	1680.75	13.73	Si
SLV 15	143750	0.25	8837	-8052	122.41	1680.75	13.73	Si



## Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 0.045 Wa = 0.08 Ta = 0.0269

Comb.	N top	N base	V orto	$\alpha 0$	M*	e*	a0*	aLim	Verifica
SLV 4	-7319	-9579	-72	0.095	1098.1	0.918	1.51105	11.92381	No
SLV 3	-7319	-9579	-72	0.095	1098.1	0.918	1.51105	11.92381	No
SLV 1	-6250	-8141	-84	0.095	991.3	0.912	1.52157	11.92381	No
SLV 2	-6250	-8141	-84	0.095	991.3	0.912	1.52157	11.92381	No
SLV 15	-4734	-11515	84	0.098	841.2	0.902	1.58017	11.92381	No
SLV 16	-4734	-11515	84	0.098	841.2	0.902	1.58017	11.92381	No
SLV 11	-6886	-12516	44	0.099	1054.8	0.916	1.57215	11.4846	No
SLV 12	-6886	-12516	44	0.099	1054.8	0.916	1.57215	11.4846	No
SLV 13	-3665	-10076	72	0.103	737	0.895	1.6702	11.92381	No
SLV 14	-3665	-10076	72	0.103	737	0.895	1.6702	11.92381	No

## Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	5.529	SLU 82	Si
V_SLU	8.134	SLU 82	Si
PF_SLV	2.006	SLV 13	Si
V_SLV	4.916	SLV 13	Si
PFFP_SLV	10.057	SLV 9	Si
R_SLV	0.127	SLV 3	No

## Maschio 12

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-31.668	-0.629	-34.183	-0.629	L1	L2	2.515	0.3	2.69	2.69	2.69			

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	t0	fv0	$\mu$	$\phi$	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche,  $\gamma M = 3$

Comb.	Quota	N	M	$\sigma 0$	Mu	c.s.	Verifica
SLU 2	-1.3	-6697	-53.02	8876	7504.08	141.529	Si
SLU 2	0.05	-4992	233.42	6616	5767.13	24.707	Si
SLU 2	1.39	-2172	468.08	2879	2634.9	5.629	Si
SLU 9	-1.3	-6612	28.53	8763	7419.69	260.078	Si
SLU 9	0.05	-4918	249.8	6519	5690.02	22.778	Si
SLU 9	1.39	-2092	375.05	2773	2541.38	6.776	Si
SLU 4	-1.3	-6612	28.53	8763	7419.69	260.078	Si
SLU 4	0.05	-4918	249.8	6519	5690.02	22.778	Si
SLU 4	1.39	-2092	375.05	2773	2541.38	6.776	Si
SLU 47	-1.3	-8360	14.37	11081	9083.09	632.022	Si
SLU 47	0.05	-6159	324.74	8163	6968.95	21.46	Si
SLU 47	1.39	-2547	541.76	3376	3070.07	5.667	Si
SLU 7	-1.3	-6612	28.53	8763	7419.69	260.078	Si
SLU 7	0.05	-4918	249.8	6519	5690.02	22.778	Si
SLU 7	1.39	-2092	375.05	2773	2541.38	6.776	Si
SLU 5	-1.3	-6697	-53.02	8876	7504.08	141.529	Si
SLU 5	0.05	-4992	233.42	6616	5767.13	24.707	Si
SLU 5	1.39	-2172	468.08	2879	2634.9	5.629	Si
SLU 46	-1.3	-8275	95.92	10967	9004.52	93.874	Si
SLU 46	0.05	-6086	341.12	8066	6895.33	20.214	Si
SLU 46	1.39	-2467	448.73	3270	2977.77	6.636	Si
SLU 44	-1.3	-8360	14.37	11081	9083.09	632.022	Si
SLU 44	0.05	-6159	324.74	8163	6968.95	21.46	Si
SLU 44	1.39	-2547	541.76	3376	3070.07	5.667	Si
SLU 49	-1.3	-8275	95.92	10967	9004.52	93.874	Si
SLU 49	0.05	-6086	341.12	8066	6895.33	20.214	Si
SLU 49	1.39	-2467	448.73	3270	2977.77	6.636	Si
SLU 51	-1.3	-8275	95.92	10967	9004.52	93.874	Si
SLU 51	0.05	-6086	341.12	8066	6895.33	20.214	Si
SLU 51	1.39	-2467	448.73	3270	2977.77	6.636	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma M = 2$

Comb.	Quota	N	M	$\sigma 0$	Mu	c.s.	Verifica
SLV 16	-1.3	-8299	-2214.41	11000	9496.84	4.289	Si
SLV 16	0.05	-5792	-343.96	7676	6825.56	19.844	Si
SLV 16	1.39	-2883	910.84	3821	3511.59	3.855	Si
SLV 13	-1.3	-8910	-2356.09	11809	10121.7	4.296	Si
SLV 13	0.05	-6288	-190.32	8334	7367.72	38.711	Si
SLV 13	1.39	-3065	1111.73	4062	3726.06	3.352	Si
SLV 10	-1.3	-8567	-844.92	11355	9772.25	11.566	Si
SLV 10	0.05	-6408	378.01	8493	7498.2	19.836	Si
SLV 10	1.39	-2878	802.46	3814	3505.53	4.368	Si
SLV 9	-1.3	-8567	-844.92	11355	9772.25	11.566	Si
SLV 9	0.05	-6408	378.01	8493	7498.2	19.836	Si
SLV 9	1.39	-2878	802.46	3814	3505.53	4.368	Si
SLV 4	-1.3	-5283	2575.52	7002	6262.73	2.432	Si
SLV 4	0.05	-4482	767.71	5940	5361.77	6.984	Si



Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 4	1.39	-1739	-642.43	2305	2145.96	3.34	Si
SLV 14	-1.3	-8910	-2356.09	11809	10121.7	4.296	Si
SLV 14	0.05	-6288	-190.32	8334	7367.72	38.711	Si
SLV 14	1.39	-3065	1111.73	4062	3726.06	3.352	Si
SLV 3	-1.3	-5283	2575.52	7002	6262.73	2.432	Si
SLV 3	0.05	-4482	767.71	5940	5361.77	6.984	Si
SLV 3	1.39	-1739	-642.43	2305	2145.96	3.34	Si
SLV 1	-1.3	-5894	2433.83	7812	6937.86	2.851	Si
SLV 1	0.05	-4978	921.35	6598	5921.66	6.427	Si
SLV 1	1.39	-1922	-441.53	2547	2366.12	5.359	Si
SLV 2	-1.3	-5894	2433.83	7812	6937.86	2.851	Si
SLV 2	0.05	-4978	921.35	6598	5921.66	6.427	Si
SLV 2	1.39	-1922	-441.53	2547	2366.12	5.359	Si
SLV 15	-1.3	-8299	-2214.41	11000	9496.84	4.289	Si
SLV 15	0.05	-5792	-343.96	7676	6825.56	19.844	Si
SLV 15	1.39	-2883	910.84	3821	3511.59	3.855	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 40	-1.3	-9327	-533	-149.5		12362	2.515	7204	5435			10.2	Si
SLU 40	0.05	-7455	-523	332.7		9880	2.515	6873	5186			9.92	Si
SLU 40	1.39	-3970	275	374.59		5262	2.515	6257	4721			17.18	Si
SLU 41	-1.3	-9199	-445	-27.18		12192	2.515	7181	5418			12.18	Si
SLU 41	0.05	-7345	-426	357.27		9735	2.515	6854	5171			12.14	Si
SLU 41	1.39	-3850	504	235.04		5103	2.515	6236	4705			9.33	Si
SLU 84	-1.3	-10990	-541	-82.11		14566	2.515	7498	5657			10.45	Si
SLU 84	0.05	-8622	-529	424.02		11428	2.515	7079	5341			10.1	Si
SLU 84	1.39	-4345	285	448.27		5759	2.515	6323	4771			16.74	Si
SLU 83	-1.3	-10862	-453	40.21		14396	2.515	7475	5640			12.45	Si
SLU 83	0.05	-8512	-432	448.59		11282	2.515	7060	5327			12.33	Si
SLU 83	1.39	-4225	515	308.72		5600	2.515	6302	4755			9.24	Si
SLU 39	-1.3	-9199	-445	-27.18		12192	2.515	7181	5418			12.18	Si
SLU 39	0.05	-7345	-426	357.27		9735	2.515	6854	5171			12.14	Si
SLU 39	1.39	-3850	504	235.04		5103	2.515	6236	4705			9.33	Si
SLU 81	-1.3	-10862	-453	40.21		14396	2.515	7475	5640			12.45	Si
SLU 81	0.05	-8512	-432	448.59		11282	2.515	7060	5327			12.33	Si
SLU 81	1.39	-4225	515	308.72		5600	2.515	6302	4755			9.24	Si
SLU 34	-1.3	-8845	-497	-197.01		11723	2.515	7119	5371			10.81	Si
SLU 34	0.05	-7008	-494	283.57		9288	2.515	6794	5126			10.37	Si
SLU 34	1.39	-3677	36	465.11		4873	2.515	6205	4682			129.51	Si
SLU 82	-1.3	-10990	-541	-82.11		14566	2.515	7498	5657			10.45	Si
SLU 82	0.05	-8622	-529	424.02		11428	2.515	7079	5341			10.1	Si
SLU 82	1.39	-4345	285	448.27		5759	2.515	6323	4771			16.74	Si
SLU 31	-1.3	-8845	-497	-197.01		11723	2.515	7119	5371			10.81	Si
SLU 31	0.05	-7008	-494	283.57		9288	2.515	6794	5126			10.37	Si
SLU 31	1.39	-3677	36	465.11		4873	2.515	6205	4682			129.51	Si
SLU 42	-1.3	-9327	-533	-149.5		12362	2.515	7204	5435			10.2	Si
SLU 42	0.05	-7455	-523	332.7		9880	2.515	6873	5186			9.92	Si
SLU 42	1.39	-3970	275	374.59		5262	2.515	6257	4721			17.18	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 16	-1.3	-8299	-2334	-2214.41		11000	2.515	10533	7947			3.41	Si
SLV 16	0.05	-5792	-2409	-343.96		7676	2.515	9869	7446			3.09	Si
SLV 16	1.39	-2883	-892	910.84		3821	2.515	9097	6864			7.69	Si
SLV 7	-1.3	-5626	881	1064.35		7457	2.515	9825	7413			8.41	Si
SLV 7	0.05	-4361	670	199.38		5780	2.515	9489	7160			10.69	Si
SLV 7	1.39	-1927	1106	-333.16		2554	2.515	8844	6673			6.03	Si
SLV 3	-1.3	-5283	2230	2575.52		7624	2.31	9858	6832			3.06	Si
SLV 3	0.05	-4482	2192	767.71		5940	2.515	9521	7184			3.28	Si
SLV 3	1.39	-1739	1629	-642.43		2305	2.515	8794	6635			4.07	Si
SLV 2	-1.3	-5894	2017	2433.83		7812	2.515	9896	7466			3.7	Si
SLV 2	0.05	-4978	2117	921.35		6598	2.515	9653	7283			3.44	Si
SLV 2	1.39	-1922	1321	-441.53		2547	2.515	8843	6672			5.05	Si
SLV 4	-1.3	-5283	2230	2575.52		7624	2.31	9858	6832			3.06	Si
SLV 4	0.05	-4482	2192	767.71		5940	2.515	9521	7184			3.28	Si
SLV 4	1.39	-1739	1629	-642.43		2305	2.515	8794	6635			4.07	Si
SLV 8	-1.3	-5626	881	1064.35		7457	2.515	9825	7413			8.41	Si
SLV 8	0.05	-4361	670	199.38		5780	2.515	9489	7160			10.69	Si
SLV 8	1.39	-1927	1106	-333.16		2554	2.515	8844	6673			6.03	Si
SLV 14	-1.3	-8910	-2547	-2356.09		11809	2.515	10695	8070			3.17	Si
SLV 14	0.05	-6288	-2484	-190.32		8334	2.515	10000	7545			3.04	Si
SLV 14	1.39	-3065	-1200	1111.73		4062	2.515	9146	6900			5.75	Si
SLV 15	-1.3	-8299	-2334	-2214.41		11000	2.515	10533	7947			3.41	Si
SLV 15	0.05	-5792	-2409	-343.96		7676	2.515	9869	7446			3.09	Si
SLV 15	1.39	-2883	-892	910.84		3821	2.515	9097	6864			7.69	Si
SLV 13	-1.3	-8910	-2547	-2356.09		11809	2.515	10695	8070			3.17	Si
SLV 13	0.05	-6288	-2484	-190.32		8334	2.515	10000	7545			3.04	Si
SLV 13	1.39	-3065	-1200	1111.73		4062	2.515	9146	6900			5.75	Si
SLV 1	-1.3	-5894	2017	2433.83		7812	2.515	9896	7466			3.7	Si
SLV 1	0.05	-4978	2117	921.35		6598	2.515	9653	7283			3.44	Si
SLV 1	1.39	-1922	1321	-441.53		2547	2.515	8843	6672			5.05	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.045 Wa 0.05 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 7	143750	0.25	5780	-4361	101.35	623.26	6.15	Si
SLV 8	143750	0.25	5780	-4361	101.35	623.26	6.15	Si



Comb.	fd	Sa	σ0	N	M	Mc	Coeff.s.	Verifica
SLV 3	143750	0.25	5940	-4482	101.35	639.57	6.31	Si
SLV 4	143750	0.25	5940	-4482	101.35	639.57	6.31	Si
SLV 12	143750	0.25	6301	-4754	101.35	676.38	6.67	Si
SLV 11	143750	0.25	6301	-4754	101.35	676.38	6.67	Si
SLV 2	143750	0.25	6598	-4978	101.35	706.36	6.97	Si
SLV 1	143750	0.25	6598	-4978	101.35	706.36	6.97	Si
SLV 16	143750	0.25	7676	-5792	101.35	814.18	8.03	Si
SLV 15	143750	0.25	7676	-5792	101.35	814.18	8.03	Si

#### Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 0.045 Wa = 0.05 Ta = 0.0403

Comb.	N top	N base	V orto	α0	M*	e*	a0*	aLim	Verifica
SLV 6	-2535	-7662	78	0.061	562.3	0.891	0.9965	12.0884	No
SLV 5	-2535	-7662	78	0.061	562.3	0.891	0.9965	12.0884	No
SLV 11	-2270	-6531	-75	0.062	537.4	0.89	1.0193	12.0884	No
SLV 12	-2270	-6531	-75	0.062	537.4	0.89	1.0193	12.0884	No
SLV 16	-2883	-8299	-57	0.065	595.6	0.894	1.06138	12.0884	No
SLV 15	-2883	-8299	-57	0.065	595.6	0.894	1.06138	12.0884	No
SLV 9	-2878	-8567	55	0.066	595.1	0.894	1.06961	12.0884	No
SLV 10	-2878	-8567	55	0.066	595.1	0.894	1.06961	12.0884	No
SLV 2	-1922	-5894	61	0.067	505.2	0.889	1.09019	12.0884	No
SLV 1	-1922	-5894	61	0.067	505.2	0.889	1.09019	12.0884	No

#### Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	5.629	SLV 2	Si
V_SLV	9.24	SLV 81	Si
PF_SLV	2.432	SLV 3	Si
V_SLV	3.037	SLV 13	Si
PFFP_SLV	6.149	SLV 7	Si
R_SLV	0.082	SLV 5	No

## Maschio 13

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

#### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.sx	a.s.dx
-26.388	-0.629	-30.668	-0.629	L1	L2	4.28	0.3	2.69	2.69	2.69			

#### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	τ0	fν0	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

#### Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 18	-1.3	-30969	-26039.13	24119	46650.21	1.792	Si
SLU 18	0.05	-23675	-22570.53	18438	39195.93	1.737	Si
SLU 18	1.39	-13537	-17964.35	10543	25219.62	1.404	Si
SLU 82	-1.3	-38759	-31832.12	30186	52207.66	1.64	Si
SLU 82	0.05	-29597	-27424.88	23050	45414.25	1.656	Si
SLU 82	1.39	-16746	-21693.15	13042	30098.06	1.387	Si
SLU 40	-1.3	-35186	-30489.72	27404	49967.28	1.639	Si
SLU 40	0.05	-27149	-26238.33	21144	43018.57	1.64	Si
SLU 40	1.39	-15865	-20782.34	12356	28801.07	1.386	Si
SLU 41	-1.3	-35446	-30473.84	27606	50147.92	1.646	Si
SLU 41	0.05	-27355	-26413.82	21304	43229.08	1.637	Si
SLU 41	1.39	-16035	-21083.44	12489	29054.47	1.378	Si
SLU 81	-1.3	-39019	-31816.24	30389	52350.29	1.645	Si
SLU 81	0.05	-29802	-27600.38	23210	45604.19	1.652	Si
SLU 81	1.39	-16916	-21994.25	13174	30345.32	1.38	Si
SLU 39	-1.3	-35446	-30473.84	27606	50147.92	1.646	Si
SLU 39	0.05	-27355	-26413.82	21304	43229.08	1.637	Si
SLU 39	1.39	-16035	-21083.44	12489	29054.47	1.378	Si
SLU 83	-1.3	-39019	-31816.24	30389	52350.29	1.645	Si
SLU 83	0.05	-29802	-27600.38	23210	45604.19	1.652	Si
SLU 83	1.39	-16916	-21994.25	13174	30345.32	1.38	Si
SLU 42	-1.3	-35186	-30489.72	27404	49967.28	1.639	Si
SLU 42	0.05	-27149	-26238.33	21144	43018.57	1.64	Si
SLU 42	1.39	-15865	-20782.34	12356	28801.07	1.386	Si
SLU 84	-1.3	-38759	-31832.12	30186	52207.66	1.64	Si
SLU 84	0.05	-29597	-27424.88	23050	45414.25	1.656	Si
SLU 84	1.39	-16746	-21693.15	13042	30098.06	1.387	Si
SLU 20	-1.3	-30969	-26039.13	24119	46650.21	1.792	Si
SLU 20	0.05	-23675	-22570.53	18438	39195.93	1.737	Si
SLU 20	1.39	-13537	-17964.35	10543	25219.62	1.404	Si

#### Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γM = 2

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLV 3	-1.3	-30016	-15136.44	23377	51944.33	3.432	Si
SLV 3	0.05	-22454	-18968.36	17488	41174.87	2.171	Si
SLV 3	1.39	-13598	-19678.89	10591	26578.14	1.351	Si
SLV 7	-1.3	-26982	-22332.34	21014	47810.67	2.141	Si



Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 7	0.05	-20792	-19523.32	16193	38598.46	1.977	Si
SLV 7	1.39	-11754	-16346.17	9154	23268.35	1.423	Si
SLV 15	-1.3	-14291	-18300.62	11130	27797.15	1.519	Si
SLV 15	0.05	-10932	-9060.17	8514	21763.74	2.402	Si
SLV 15	1.39	-3852	-2228.74	3000	8040.81	3.608	Si
SLV 4	-1.3	-30016	-15136.44	23377	51944.33	3.432	Si
SLV 4	0.05	-22454	-18968.36	17488	41174.87	2.171	Si
SLV 4	1.39	-13598	-19678.89	10591	26578.14	1.351	Si
SLV 2	-1.3	-27899	-9917.79	21728	49086.37	4.949	Si
SLV 2	0.05	-20422	-15520.23	15905	38014.56	2.449	Si
SLV 2	1.39	-12256	-17300.46	9545	24178.24	1.398	Si
SLV 12	-1.3	-22264	-23281.59	17340	40884.35	1.756	Si
SLV 12	0.05	-17335	-16550.86	13501	32998.7	1.994	Si
SLV 12	1.39	-8830	-11111.12	6877	17832.1	1.605	Si
SLV 8	-1.3	-26982	-22332.34	21014	47810.67	2.141	Si
SLV 8	0.05	-20792	-19523.32	16193	38598.46	1.977	Si
SLV 8	1.39	-11754	-16346.17	9154	23268.35	1.423	Si
SLV 11	-1.3	-22264	-23281.59	17340	40884.35	1.756	Si
SLV 11	0.05	-17335	-16550.86	13501	32998.7	1.994	Si
SLV 11	1.39	-8830	-11111.12	6877	17832.1	1.605	Si
SLV 16	-1.3	-14291	-18300.62	11130	27797.15	1.519	Si
SLV 16	0.05	-10932	-9060.17	8514	21763.74	2.402	Si
SLV 16	1.39	-3852	-2228.74	3000	8040.81	3.608	Si
SLV 1	-1.3	-27899	-9917.79	21728	49086.37	4.949	Si
SLV 1	0.05	-20422	-15520.23	15905	38014.56	2.449	Si
SLV 1	1.39	-12256	-17300.46	9545	24178.24	1.398	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 82	-1.3	-38759	1066	-31832.12		32657	3.9562	9910	11762			11.04	Si
SLU 82	0.05	-29597	1061	-27424.88		27102	3.6401	9169	10013			9.44	Si
SLU 82	1.39	-16746	2821	-21693.15		22031	2.5336	8493	6455			2.29	Si
SLU 42	-1.3	-35186	1011	-30489.72		30700	3.8204	9649	11059			10.94	Si
SLU 42	0.05	-27149	1006	-26238.33		25705	3.5207	8983	9488			9.44	Si
SLU 42	1.39	-15865	2717	-20782.34		21237	2.4901	8387	6266			2.31	Si
SLU 39	-1.3	-35446	1229	-30473.84		30763	3.8408	9657	11128			9.06	Si
SLU 39	0.05	-27355	1228	-26413.82		25881	3.5232	9006	9519			7.75	Si
SLU 39	1.39	-16035	2802	-21083.44		21592	2.4755	8434	6264			2.24	Si
SLU 84	-1.3	-38759	1066	-31832.12		32657	3.9562	9910	11762			11.04	Si
SLU 84	0.05	-29597	1061	-27424.88		27102	3.6401	9169	10013			9.44	Si
SLU 84	1.39	-16746	2821	-21693.15		22031	2.5336	8493	6455			2.29	Si
SLU 81	-1.3	-39019	1284	-31816.24		32730	3.9738	9920	11826			9.21	Si
SLU 81	0.05	-29802	1283	-27600.38		27279	3.6416	9193	10043			7.83	Si
SLU 81	1.39	-16916	2906	-21994.25		22381	2.5194	8540	6454			2.22	Si
SLU 62	-1.3	-34542	1121	-27381.53		28486	4.0419	9354	11342			10.12	Si
SLU 62	0.05	-26122	1120	-23757.09		23587	3.6916	8700	9636			8.6	Si
SLU 62	1.39	-14418	2483	-18875.16		19282	2.4925	8126	6076			2.45	Si
SLU 60	-1.3	-34542	1121	-27381.53		28486	4.0419	9354	11342			10.12	Si
SLU 60	0.05	-26122	1120	-23757.09		23587	3.6916	8700	9636			8.6	Si
SLU 60	1.39	-14418	2483	-18875.16		19282	2.4925	8126	6076			2.45	Si
SLU 40	-1.3	-35186	1011	-30489.72		30700	3.8204	9649	11059			10.94	Si
SLU 40	0.05	-27149	1006	-26238.33		25705	3.5207	8983	9488			9.44	Si
SLU 40	1.39	-15865	2717	-20782.34		21237	2.4901	8387	6266			2.31	Si
SLU 83	-1.3	-39019	1284	-31816.24		32730	3.9738	9920	11826			9.21	Si
SLU 83	0.05	-29802	1283	-27600.38		27279	3.6416	9193	10043			7.83	Si
SLU 83	1.39	-16916	2906	-21994.25		22381	2.5194	8540	6454			2.22	Si
SLU 41	-1.3	-35446	1229	-30473.84		30763	3.8408	9657	11128			9.06	Si
SLU 41	0.05	-27355	1228	-26413.82		25881	3.5232	9006	9519			7.75	Si
SLU 41	1.39	-16035	2802	-21083.44		21592	2.4755	8434	6264			2.24	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 7	-1.3	-26982	3150	-22332.34		22845	3.937	12902	15239			4.84	Si
SLV 7	0.05	-20792	3612	-19523.32		19236	3.6031	12180	13166			3.65	Si
SLV 7	1.39	-11754	3002	-16346.17		17430	2.2478	11819	7970			2.65	Si
SLV 14	-1.3	-12174	-6524	-13081.96		12696	3.1963	10873	10426			1.6	Si
SLV 14	0.05	-8900	-6883	-5612.03		6931	4.28	9720	12480			1.81	Si
SLV 14	1.39	-2509	-1822	149.69		1954	4.28	8724	11202			6.15	Si
SLV 15	-1.3	-14291	-6213	-18300.62		18476	2.5783	12029	9304			1.5	Si
SLV 15	0.05	-10932	-6339	-9060.17		9263	3.9336	10186	12020			1.9	Si
SLV 15	1.39	-3852	-1284	-2228.74		3000	4.28	8933	11470			8.93	Si
SLV 8	-1.3	-26982	3150	-22332.34		22845	3.937	12902	15239			4.84	Si
SLV 8	0.05	-20792	3612	-19523.32		19236	3.6031	12180	13166			3.65	Si
SLV 8	1.39	-11754	3002	-16346.17		17430	2.2478	11819	7970			2.65	Si
SLV 4	-1.3	-30016	7635	-15136.44		23377	4.28	13009	16703			2.19	Si
SLV 4	0.05	-22454	7993	-18968.36		19262	3.8857	12186	14205			1.78	Si
SLV 4	1.39	-13598	4346	-19678.89		21808	2.0785	12695	7916			1.82	Si
SLV 2	-1.3	-27899	7325	-9917.79		21728	4.28	12679	16280			2.22	Si
SLV 2	0.05	-20422	7449	-15520.23		16443	4.1401	11622	14435			1.94	Si
SLV 2	1.39	-12256	3808	-17300.46		18696	2.1851	12072	7914			2.08	Si
SLV 13	-1.3	-12174	-6524	-13081.96		12696	3.1963	10873	10426			1.6	Si
SLV 13	0.05	-8900	-6883	-5612.03		6931	4.28	9720	12480			1.81	Si
SLV 13	1.39	-2509	-1822	149.69		1954	4.28	8724	11202			6.15	Si
SLV 3	-1.3	-30016	7635	-15136.44		23377	4.28	13009	16703			2.19	Si
SLV 3	0.05	-22454	7993	-18968.36		19262	3.8857	12186	14205			1.78	Si
SLV 3	1.39	-13598	4346	-19678.89		21808	2.0785	12695	7916			1.82	Si
SLV 1	-1.3	-27899	7325	-9917.79		21728	4.28	12679	16280			2.22	Si
SLV 1	0.05	-20422	7449	-15520.23		16443	4.1401	11622	14435			1.94	Si



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 1	1.39	-12256	3808	-17300.46		18696	2.1851	12072	7914			2.08	Si
SLV 16	-1.3	-14291	-6213	-18300.62		18476	2.5783	12029	9304			1.5	Si
SLV 16	0.05	-10932	-6339	-9060.17		9263	3.9336	10186	12020			1.9	Si
SLV 16	1.39	-3852	-1284	-2228.74		3000	4.28	8933	11470			8.93	Si

#### Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.045 Wa 0.05 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 13	143750	0.25	6931	-8900	172.48	1259.2	7.3	Si
SLV 14	143750	0.25	6931	-8900	172.48	1259.2	7.3	Si
SLV 9	143750	0.25	8226	-10562	172.48	1477.59	8.57	Si
SLV 10	143750	0.25	8226	-10562	172.48	1477.59	8.57	Si
SLV 16	143750	0.25	8514	-10932	172.48	1525.5	8.84	Si
SLV 15	143750	0.25	8514	-10932	172.48	1525.5	8.84	Si
SLV 6	143750	0.25	10918	-14018	172.48	1914.87	11.1	Si
SLV 5	143750	0.25	10918	-14018	172.48	1914.87	11.1	Si
SLV 11	143750	0.25	13501	-17335	172.48	2312.99	13.41	Si
SLV 12	143750	0.25	13501	-17335	172.48	2312.99	13.41	Si

#### Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 0.045 Wa = 0.05 Ta = 0.0403

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	a0*	aLim	Verifica
SLV 7	-11754	-26982	-174	0.056	1691.9	0.924	0.87668	12.0884	No
SLV 8	-11754	-26982	-174	0.056	1691.9	0.924	0.87668	12.0884	No
SLV 12	-8830	-22264	-180	0.055	1399.1	0.912	0.8789	12.0884	No
SLV 11	-8830	-22264	-180	0.055	1399.1	0.912	0.8789	12.0884	No
SLV 5	-7278	-19925	179	0.055	1245.1	0.905	0.88678	12.0884	No
SLV 6	-7278	-19925	179	0.055	1245.1	0.905	0.88678	12.0884	No
SLV 9	-4354	-15208	172	0.056	960.8	0.892	0.91078	12.0884	No
SLV 10	-4354	-15208	172	0.056	960.8	0.892	0.91078	12.0884	No
SLV 2	-12256	-27899	63	0.063	1742.4	0.925	0.98873	12.0884	No
SLV 1	-12256	-27899	63	0.063	1742.4	0.925	0.98873	12.0884	No

#### Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	1.378	SLU 39	Si
V_SLU	2.221	SLU 81	Si
PF_SLV	1.351	SLV 3	Si
V_SLV	1.497	SLV 15	Si
PFFP_SLV	7.301	SLV 13	Si
R_SLV	0.073	SLV 7	No

## Maschio 14

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

#### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-24.603	-0.629	-24.978	-0.629	L1	L2	0.375	0.3	2.69	2.69	2.69			

#### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	$\tau_0$	fv0	$\mu$	$\phi$	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

#### Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 58	-1.3	-140	-263.51	0	0	0	No, e>l/2
SLU 58	0.05	-2866	50.03	25480	369.35	7.383	Si
SLU 58	1.39	-873	1.53	7760	148.09	96.763	Si
SLU 59	-1.3	-138	-264.05	0	0	0	No, e>l/2
SLU 59	0.05	-2862	48.65	25442	369.05	7.586	Si
SLU 59	1.39	-849	-8.12	7544	144.39	17.777	Si
SLU 55	-1.3	-136	-264.41	0	0	0	No, e>l/2
SLU 55	0.05	-2859	47.73	25416	368.84	7.727	Si
SLU 55	1.39	-832	-14.56	7399	141.9	9.748	Si
SLU 1	-1.3	-509	-123.09	0	0	0	No, e>l/2
SLU 1	0.05	-1703	23.56	15134	259.93	11.035	Si
SLU 1	1.39	-582	3.34	5171	102.15	30.62	Si
SLU 57	-1.3	-138	-264.05	0	0	0	No, e>l/2
SLU 57	0.05	-2862	48.65	25442	369.05	7.586	Si
SLU 57	1.39	-849	-8.12	7544	144.39	17.777	Si
SLU 54	-1.3	-138	-264.05	0	0	0	No, e>l/2
SLU 54	0.05	-2862	48.65	25442	369.05	7.586	Si
SLU 54	1.39	-849	-8.12	7544	144.39	17.777	Si
SLU 53	-1.3	-140	-263.51	0	0	0	No, e>l/2
SLU 53	0.05	-2866	50.03	25480	369.35	7.383	Si
SLU 53	1.39	-873	1.53	7760	148.09	96.763	Si
SLU 61	-1.3	120	-316.02	0	0	0	No, Trazione
SLU 61	0.05	-3195	58.45	28403	390.22	6.676	Si
SLU 61	1.39	-911	-9.16	8096	153.8	16.788	Si
SLU 60	-1.3	118	-315.48	0	0	0	No, Trazione
SLU 60	0.05	-3200	59.83	28441	390.47	6.527	Si
SLU 60	1.39	-935	0.49	8312	157.44	320.377	Si



Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 56	-1.3	-140	-263.51	0	0	0	No, $e \geq l/2$
SLU 56	0.05	-2866	50.03	25480	369.35	7.383	Si
SLU 56	1.39	-873	1.53	7760	148.09	96.763	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 4	-1.3	-736	-128.26	6542	130.6	1.018	Si
SLV 4	0.05	-2196	96.38	19517	345.93	3.589	Si
SLV 4	1.39	-1412	281.89	0	0	0	No, $e \geq l/2$
SLV 7	-1.3	13	-202.22	0	0	0	No, Trazione
SLV 7	0.05	-2491	65.02	22139	382.38	5.881	Si
SLV 7	1.39	-780	145.29	6935	137.99	0.95	No, $M > \mu$
SLV 10	-1.3	-557	-142.87	0	0	0	No, $e \geq l/2$
SLV 10	0.05	-1566	0.9	13921	260.2	288.374	Si
SLV 10	1.39	-513	-139.36	0	0	0	No, $e \geq l/2$
SLV 3	-1.3	-736	-128.26	6542	130.6	1.018	Si
SLV 3	0.05	-2196	96.38	19517	345.93	3.589	Si
SLV 3	1.39	-1412	281.89	0	0	0	No, $e \geq l/2$
SLV 12	-1.3	376	-237.29	0	0	0	No, Trazione
SLV 12	0.05	-2472	29.55	21971	380.12	12.862	Si
SLV 12	1.39	-302	-10.47	2682	55.33	5.286	Si
SLV 13	-1.3	193	-216.83	0	0	0	No, Trazione
SLV 13	0.05	-1861	-30.45	16543	301.71	9.907	Si
SLV 13	1.39	119	-275.96	0	0	0	No, Trazione
SLV 14	-1.3	193	-216.83	0	0	0	No, Trazione
SLV 14	0.05	-1861	-30.45	16543	301.71	9.907	Si
SLV 14	1.39	119	-275.96	0	0	0	No, Trazione
SLV 8	-1.3	13	-202.22	0	0	0	No, Trazione
SLV 8	0.05	-2491	65.02	22139	382.38	5.881	Si
SLV 8	1.39	-780	145.29	6935	137.99	0.95	No, $M > \mu$
SLV 11	-1.3	376	-237.29	0	0	0	No, Trazione
SLV 11	0.05	-2472	29.55	21971	380.12	12.862	Si
SLV 11	1.39	-302	-10.47	2682	55.33	5.286	Si
SLV 9	-1.3	-557	-142.87	0	0	0	No, $e \geq l/2$
SLV 9	0.05	-1566	0.9	13921	260.2	288.374	Si
SLV 9	1.39	-513	-139.36	0	0	0	No, $e \geq l/2$

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 53	-1.3	-140	-647	-263.51	0	0	0	5556	0	0	0	0	No, $V_u < V$
SLU 53	0.05	-2866	-661	50.03	25480	0.375	8953	1007	0	0	0	1.52	Si
SLU 53	1.39	-873	-27	1.53	7760	0.375	6590	741	0	0	0	27.22	Si
SLU 1	-1.3	-509	-304	-123.09	0	0	0	5556	0	0	0	0	No, $V_u < V$
SLU 1	0.05	-1703	-312	23.56	15134	0.375	7573	852	0	0	0	2.73	Si
SLU 1	1.39	-582	-49	3.34	5171	0.375	6245	703	0	0	0	14.41	Si
SLU 57	-1.3	-138	-646	-264.05	0	0	0	5556	0	0	0	0	No, $V_u < V$
SLU 57	0.05	-2862	-661	48.65	25442	0.375	8948	1007	0	0	0	1.52	Si
SLU 57	1.39	-849	-13	-8.12	7544	0.375	6561	738	0	0	0	55.33	Si
SLU 58	-1.3	-140	-647	-263.51	0	0	0	5556	0	0	0	0	No, $V_u < V$
SLU 58	0.05	-2866	-661	50.03	25480	0.375	8953	1007	0	0	0	1.52	Si
SLU 58	1.39	-873	-27	1.53	7760	0.375	6590	741	0	0	0	27.22	Si
SLU 61	-1.3	120	-772	-316.02	0	0	0	5556	0	0	0	0	No, $V_u < V$
SLU 61	0.05	-3195	-790	58.45	28403	0.375	9343	1051	0	0	0	1.33	Si
SLU 61	1.39	-911	3	-9.16	8096	0.375	6635	746	0	0	0	254.57	Si
SLU 54	-1.3	-138	-646	-264.05	0	0	0	5556	0	0	0	0	No, $V_u < V$
SLU 54	0.05	-2862	-661	48.65	25442	0.375	8948	1007	0	0	0	1.52	Si
SLU 54	1.39	-849	-13	-8.12	7544	0.375	6561	738	0	0	0	55.33	Si
SLU 59	-1.3	-138	-646	-264.05	0	0	0	5556	0	0	0	0	No, $V_u < V$
SLU 59	0.05	-2862	-661	48.65	25442	0.375	8948	1007	0	0	0	1.52	Si
SLU 59	1.39	-849	-13	-8.12	7544	0.375	6561	738	0	0	0	55.33	Si
SLU 55	-1.3	-136	-644	-264.41	0	0	0	5556	0	0	0	0	No, $V_u < V$
SLU 55	0.05	-2859	-662	47.73	25416	0.375	8944	1006	0	0	0	1.52	Si
SLU 55	1.39	-832	-4	-14.56	7399	0.375	6542	736	0	0	0	180.45	Si
SLU 56	-1.3	-140	-647	-263.51	0	0	0	5556	0	0	0	0	No, $V_u < V$
SLU 56	0.05	-2866	-661	50.03	25480	0.375	8953	1007	0	0	0	1.52	Si
SLU 56	1.39	-873	-27	1.53	7760	0.375	6590	741	0	0	0	27.22	Si
SLU 60	-1.3	118	-774	-315.48	0	0	0	5556	0	0	0	0	No, $V_u < V$
SLU 60	0.05	-3200	-789	59.83	28441	0.375	9348	1052	0	0	0	1.33	Si
SLU 60	1.39	-935	-11	0.49	8312	0.375	6664	750	0	0	0	68.38	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 13	-1.3	193	-206	-216.83	0	0	0	8333	0	0	0	0	No, $V_u < V$
SLV 13	0.05	-1861	-557	-30.45	16543	0.375	11642	1310	0	0	0	2.35	Si
SLV 13	1.39	119	104	-275.96	0	0	0	8333	0	0	0	0	No, $V_u < V$
SLV 8	-1.3	13	-635	-202.22	0	0	0	8333	0	0	0	0	No, $V_u < V$
SLV 8	0.05	-2491	-540	65.02	22139	0.375	12761	1436	0	0	0	2.66	Si
SLV 8	1.39	-780	267	145.29	675305	0.0039	16250	19	0	0	0	0.07	No, $V_u < V$
SLV 9	-1.3	-557	-215	-142.87	0	0	0	8333	0	0	0	0	No, $V_u < V$
SLV 9	0.05	-1566	-329	0.9	13921	0.375	11118	1251	0	0	0	3.81	Si
SLV 9	1.39	-513	-340	-139.36	0	0	0	8333	0	0	0	0	No, $V_u < V$
SLV 14	-1.3	193	-206	-216.83	0	0	0	8333	0	0	0	0	No, $V_u < V$
SLV 14	0.05	-1861	-557	-30.45	16543	0.375	11642	1310	0	0	0	2.35	Si
SLV 14	1.39	119	104	-275.96	0	0	0	8333	0	0	0	0	No, $V_u < V$
SLV 11	-1.3	376	-532	-237.29	0	0	0	8333	0	0	0	0	No, $V_u < V$
SLV 11	0.05	-2472	-641	29.55	21971	0.375	12728	1432	0	0	0	2.23	Si
SLV 11	1.39	-302	420	-10.47	2682	0.375	8870	998	0	0	0	2.38	Si
SLV 4	-1.3	-736	-643	-128.26	61854	0.0397	16250	193	0	0	0	0.3	No, $V_u < V$





Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 4	0.05	-2196	-311	96.38		19517	0.375	12237	1377			4.42	Si
SLV 4	1.39	-1412	-177	281.89		0	0	8333	0			0	No, Vu<V
SLV 3	-1.3	-736	-643	-128.26		61854	0.0397	16250	193			0.3	No, Vu<V
SLV 3	0.05	-2196	-311	96.38		19517	0.375	12237	1377			4.42	Si
SLV 3	1.39	-1412	-177	281.89		0	0	8333	0			0	No, Vu<V
SLV 10	-1.3	-557	-215	-142.87		0	0	8333	0			0	No, Vu<V
SLV 10	0.05	-1566	-329	0.9		13921	0.375	11118	1251			3.81	Si
SLV 10	1.39	-513	-340	-139.36		0	0	8333	0			0	No, Vu<V
SLV 7	-1.3	13	-635	-202.22		0	0	8333	0			0	No, Vu<V
SLV 7	0.05	-2491	-540	65.02		22139	0.375	12761	1436			2.66	Si
SLV 7	1.39	-780	267	145.29		675305	0.0039	16250	19			0.07	No, Vu<V
SLV 12	-1.3	376	-532	-237.29		0	0	8333	0			0	No, Vu<V
SLV 12	0.05	-2472	-641	29.55		21971	0.375	12728	1432			2.23	Si
SLV 12	1.39	-302	420	-10.47		2682	0.375	8870	998			2.38	Si

#### Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.045 Wa 0.05 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 10	143750	0.25	13921	-1566	15.11	208.16	13.77	Si
SLV 9	143750	0.25	13921	-1566	15.11	208.16	13.77	Si
SLV 6	143750	0.25	14089	-1585	15.11	210.34	13.92	Si
SLV 5	143750	0.25	14089	-1585	15.11	210.34	13.92	Si
SLV 13	143750	0.25	16543	-1861	15.11	241.37	15.97	Si
SLV 14	143750	0.25	16543	-1861	15.11	241.37	15.97	Si
SLV 1	143750	0.25	17102	-1924	15.11	248.21	16.42	Si
SLV 2	143750	0.25	17102	-1924	15.11	248.21	16.42	Si
SLV 15	143750	0.25	18958	-2133	15.11	270.28	17.89	Si
SLV 16	143750	0.25	18958	-2133	15.11	270.28	17.89	Si

#### Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 0.045 Wa = 0.05 Ta = 0.0403

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	a0*	aLim	Verifica
SLV 8	-780	13	-10	0	0	0	0	12.0884	No, Trazione
SLV 15	183	473	-10	0	0	0	0	12.0884	No, Trazione
SLV 11	-302	376	-13	0	0	0	0	12.0884	No, Trazione
SLV 7	-780	13	-10	0	0	0	0	12.0884	No, Trazione
SLV 14	119	193	-4	0	0	0	0	12.0884	No, Trazione
SLV 16	183	473	-10	0	0	0	0	12.0884	No, Trazione
SLV 13	119	193	-4	0	0	0	0	12.0884	No, Trazione
SLV 12	-302	376	-13	0	0	0	0	12.0884	No, Trazione
SLV 2	-1476	-1016	7	0.06	193.3	0.938	0.9355	12.0884	No
SLV 1	-1476	-1016	7	0.06	193.3	0.938	0.9355	12.0884	No

#### Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	0	SLU 84	No
V_SLU	0	SLU 1	No
PF_SLV	0	SLV 16	No
V_SLV	0	SLV 3	No
PFFP_SLV	13.774	SLV 9	Si
R_SLV	0	SLV 16	No

## Maschio 15

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

#### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-29.378	-0.629	-29.378	5.726	L1	L2	6.355	0.26	2.69	2.69	2.69			

#### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	$\tau_0$	fv0	$\mu$	$\phi$	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

#### Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 60	-1.3	-49197	3249.51	29775	99183.45	30.523	Si
SLU 60	0.05	-45833	3941.99	27739	96041.25	24.364	Si
SLU 60	1.39	-42811	2089.28	25910	92763.27	44.4	Si
SLU 61	-1.3	-49162	3297.64	29753	99153.36	30.068	Si
SLU 61	0.05	-45802	3955.67	27720	96010.21	24.272	Si
SLU 61	1.39	-42786	2062.34	25895	92735.09	44.966	Si
SLU 63	-1.3	-49162	3297.64	29753	99153.36	30.068	Si
SLU 63	0.05	-45802	3955.67	27720	96010.21	24.272	Si
SLU 63	1.39	-42786	2062.34	25895	92735.09	44.966	Si
SLU 52	-1.3	-43572	2941.59	26371	93629.62	31.83	Si
SLU 52	0.05	-39890	3466.36	24142	89184.56	25.729	Si
SLU 52	1.39	-36717	1758.41	22222	84840.8	48.248	Si
SLU 81	-1.3	-56004	3391.53	33895	103907.12	30.637	Si
SLU 81	0.05	-53113	4245.45	32145	102168.28	24.065	Si
SLU 81	1.39	-50467	2299.37	30544	100231.29	43.591	Si
SLU 84	-1.3	-55969	3439.66	33873	103888.33	30.203	Si
SLU 84	0.05	-53082	4259.13	32126	102147.76	23.983	Si



Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 84	1.39	-50443	2272.43	30529	100211.91	44.099	Si
SLU 62	-1.3	-49197	3249.51	29775	99183.45	30.523	Si
SLU 62	0.05	-45833	3941.99	27739	96041.25	24.364	Si
SLU 62	1.39	-42811	2089.28	25910	92763.27	44.4	Si
SLU 55	-1.3	-43572	2941.59	26371	93629.62	31.83	Si
SLU 55	0.05	-39890	3466.36	24142	89184.56	25.729	Si
SLU 55	1.39	-36717	1758.41	22222	84840.8	48.248	Si
SLU 83	-1.3	-56004	3391.53	33895	103907.12	30.637	Si
SLU 83	0.05	-53113	4245.45	32145	102168.28	24.065	Si
SLU 83	1.39	-50467	2299.37	30544	100231.29	43.591	Si
SLU 82	-1.3	-55969	3439.66	33873	103888.33	30.203	Si
SLU 82	0.05	-53082	4259.13	32126	102147.76	23.983	Si
SLU 82	1.39	-50443	2272.43	30529	100211.91	44.099	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 10	-1.3	-33308	-301.66	20158	88374.27	292.955	Si
SLV 10	0.05	-30553	3624.82	18491	82390.33	22.729	Si
SLV 10	1.39	-26375	2596.99	15963	72858.92	28.055	Si
SLV 8	-1.3	-28738	3984.05	17393	78316.44	19.657	Si
SLV 8	0.05	-25600	881.78	15494	71029.61	80.553	Si
SLV 8	1.39	-24929	-237.06	15087	69430.26	292.88	Si
SLV 12	-1.3	-28669	5665.91	17351	78159	13.795	Si
SLV 12	0.05	-25606	2230.71	15497	71044.19	31.848	Si
SLV 12	1.39	-25160	213.89	15228	69984.06	327.199	Si
SLV 7	-1.3	-28738	3984.05	17393	78316.44	19.657	Si
SLV 7	0.05	-25600	881.78	15494	71029.61	80.553	Si
SLV 7	1.39	-24929	-237.06	15087	69430.26	292.88	Si
SLV 15	-1.3	-30211	5539.43	18284	81631.64	14.736	Si
SLV 15	0.05	-27345	4292.41	16550	75119.58	17.501	Si
SLV 15	1.39	-25856	1574.08	15649	71635.89	45.51	Si
SLV 11	-1.3	-28669	5665.91	17351	78159	13.795	Si
SLV 11	0.05	-25606	2230.71	15497	71044.19	31.848	Si
SLV 11	1.39	-25160	213.89	15228	69984.06	327.199	Si
SLV 9	-1.3	-33308	-301.66	20158	88374.27	292.955	Si
SLV 9	0.05	-30553	3624.82	18491	82390.33	22.729	Si
SLV 9	1.39	-26375	2596.99	15963	72858.92	28.055	Si
SLV 16	-1.3	-30211	5539.43	18284	81631.64	14.736	Si
SLV 16	0.05	-27345	4292.41	16550	75119.58	17.501	Si
SLV 16	1.39	-25856	1574.08	15649	71635.89	45.51	Si
SLV 14	-1.3	-31603	3749.16	19127	84699.76	22.592	Si
SLV 14	0.05	-28829	4710.64	17448	78523.09	16.669	Si
SLV 14	1.39	-26221	2289.01	15869	72495.24	31.671	Si
SLV 13	-1.3	-31603	3749.16	19127	84699.76	22.592	Si
SLV 13	0.05	-28829	4710.64	17448	78523.09	16.669	Si
SLV 13	1.39	-26221	2289.01	15869	72495.24	31.671	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 44	-1.3	-30585	1	2035.94		18510	6.355	8024	13257			1000	Si
SLU 44	0.05	-26142	22	2303.36		15822	6.355	7665	12665			564.08	Si
SLU 44	1.39	-22592	30	1091.15		13673	6.355	7379	12192			404.24	Si
SLU 81	-1.3	-56004	-38	3391.53		33895	6.355	10075	16647			437.03	Si
SLU 81	0.05	-53113	-6	4245.45		32145	6.355	9842	16261			1000	Si
SLU 81	1.39	-50467	-4	2299.37		30544	6.355	9628	15908			1000	Si
SLU 68	-1.3	-37392	-4	2177.96		22630	6.355	8573	14165			1000	Si
SLU 68	0.05	-33422	21	2606.82		20228	6.355	8253	13636			644.35	Si
SLU 68	1.39	-30248	30	1301.25		18307	6.355	7996	13213			444.04	Si
SLU 47	-1.3	-30585	1	2035.94		18510	6.355	8024	13257			1000	Si
SLU 47	0.05	-26142	22	2303.36		15822	6.355	7665	12665			564.08	Si
SLU 47	1.39	-22592	30	1091.15		13673	6.355	7379	12192			404.24	Si
SLU 65	-1.3	-37392	-4	2177.96		22630	6.355	8573	14165			1000	Si
SLU 65	0.05	-33422	21	2606.82		20228	6.355	8253	13636			644.35	Si
SLU 65	1.39	-30248	30	1301.25		18307	6.355	7996	13213			444.04	Si
SLU 5	-1.3	-25308	4	1622.07		15317	6.355	7598	12554			1000	Si
SLU 5	0.05	-22017	23	1857.11		13325	6.355	7332	12115			537.08	Si
SLU 5	1.39	-19388	30	884.4		11734	6.355	7120	11765			388.07	Si
SLU 2	-1.3	-25308	4	1622.07		15317	6.355	7598	12554			1000	Si
SLU 2	0.05	-22017	23	1857.11		13325	6.355	7332	12115			537.08	Si
SLU 2	1.39	-19388	30	884.4		11734	6.355	7120	11765			388.07	Si
SLU 83	-1.3	-56004	-38	3391.53		33895	6.355	10075	16647			437.03	Si
SLU 83	0.05	-53113	-6	4245.45		32145	6.355	9842	16261			1000	Si
SLU 83	1.39	-50467	-4	2299.37		30544	6.355	9628	15908			1000	Si
SLU 26	-1.3	-32116	-1	1764.09		19437	6.355	8147	13462			1000	Si
SLU 26	0.05	-29298	21	2160.57		17732	6.355	7920	13086			615.31	Si
SLU 26	1.39	-27045	30	1094.49		16368	6.355	7738	12785			427.43	Si
SLU 23	-1.3	-32116	-1	1764.09		19437	6.355	8147	13462			1000	Si
SLU 23	0.05	-29298	21	2160.57		17732	6.355	7920	13086			615.31	Si
SLU 23	1.39	-27045	30	1094.49		16368	6.355	7738	12785			427.43	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 12	-1.3	-28669	1218	5665.91		17351	6.355	11803	19503			16.01	Si
SLV 12	0.05	-25606	5347	2230.71		15497	6.355	11433	18890			3.53	Si
SLV 12	1.39	-25160	3345	213.89		15228	6.355	11379	18801			5.62	Si
SLV 10	-1.3	-33308	-704	-301.66		20158	6.355	12365	20431			29.03	Si
SLV 10	0.05	-30553	-5124	3624.82		18491	6.355	12032	19880			3.88	Si
SLV 10	1.39	-26375	-3569	2596.99		15963	6.355	11526	19044			5.34	Si



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 6	-1.3	-33377	-1259	-1983.53		20200	6.355	12373	20445			16.24	Si
SLV 6	0.05	-30547	-5352	2275.89		18487	6.355	12031	19879			3.71	Si
SLV 6	1.39	-26144	-3348	2146.05		15823	6.355	11498	18998			5.67	Si
SLV 5	-1.3	-33377	-1259	-1983.53		20200	6.355	12373	20445			16.24	Si
SLV 5	0.05	-30547	-5352	2275.89		18487	6.355	12031	19879			3.71	Si
SLV 5	1.39	-26144	-3348	2146.05		15823	6.355	11498	18998			5.67	Si
SLV 11	-1.3	-28669	1218	5665.91		17351	6.355	11803	19503			16.01	Si
SLV 11	0.05	-25606	5347	2230.71		15497	6.355	11433	18890			3.53	Si
SLV 11	1.39	-25160	3345	213.89		15228	6.355	11379	18801			5.62	Si
SLV 16	-1.3	-30211	1193	5539.43		18284	6.355	11990	19811			16.6	Si
SLV 16	0.05	-27345	1948	4292.41		16550	6.355	11643	19238			9.87	Si
SLV 16	1.39	-25856	667	1574.08		15649	6.355	11463	18940			28.41	Si
SLV 15	-1.3	-30211	1193	5539.43		18284	6.355	11990	19811			16.6	Si
SLV 15	0.05	-27345	1948	4292.41		16550	6.355	11643	19238			9.87	Si
SLV 15	1.39	-25856	667	1574.08		15649	6.355	11463	18940			28.41	Si
SLV 9	-1.3	-33308	-704	-301.66		20158	6.355	12365	20431			29.03	Si
SLV 9	0.05	-30553	-5124	3624.82		18491	6.355	12032	19880			3.88	Si
SLV 9	1.39	-26375	-3569	2596.99		15963	6.355	11526	19044			5.34	Si
SLV 7	-1.3	-28738	663	3984.05		17393	6.355	11812	19517			29.42	Si
SLV 7	0.05	-25600	5118	881.78		15494	6.355	11432	18889			3.69	Si
SLV 7	1.39	-24929	3566	-237.06		15087	6.355	11351	18755			5.26	Si
SLV 8	-1.3	-28738	663	3984.05		17393	6.355	11812	19517			29.42	Si
SLV 8	0.05	-25600	5118	881.78		15494	6.355	11432	18889			3.69	Si
SLV 8	1.39	-24929	3566	-237.06		15087	6.355	11351	18755			5.26	Si

#### Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.045 Wa 0.05 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 8	143750	0.25	15494	-25600	221.95	2906.01	13.09	Si
SLV 7	143750	0.25	15494	-25600	221.95	2906.01	13.09	Si
SLV 11	143750	0.25	15497	-25606	221.95	2906.61	13.1	Si
SLV 12	143750	0.25	15497	-25606	221.95	2906.61	13.1	Si
SLV 3	143750	0.25	16537	-27324	221.95	3071.4	13.84	Si
SLV 4	143750	0.25	16537	-27324	221.95	3071.4	13.84	Si
SLV 16	143750	0.25	16550	-27345	221.95	3073.34	13.85	Si
SLV 15	143750	0.25	16550	-27345	221.95	3073.34	13.85	Si
SLV 1	143750	0.25	17435	-28808	221.95	3210.68	14.47	Si
SLV 2	143750	0.25	17435	-28808	221.95	3210.68	14.47	Si

#### Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 0.045 Wa = 0.05 Ta = 0.0465

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	a0*	aLim	Verifica
SLV 3	-25083	-30442	517	0.037	3183.6	0.944	0.57267	12.0884	No
SLV 4	-25083	-30442	517	0.037	3183.6	0.944	0.57267	12.0884	No
SLV 1	-25448	-31834	508	0.038	3220.6	0.945	0.5793	12.0884	No
SLV 2	-25448	-31834	508	0.038	3220.6	0.945	0.5793	12.0884	No
SLV 14	-26221	-31603	-513	0.038	3298.9	0.946	0.57999	12.0884	No
SLV 13	-26221	-31603	-513	0.038	3298.9	0.946	0.57999	12.0884	No
SLV 15	-25856	-30211	-504	0.038	3262	0.945	0.5831	12.0884	No
SLV 16	-25856	-30211	-504	0.038	3262	0.945	0.5831	12.0884	No
SLV 10	-26375	-33308	-167	0.049	3314.6	0.946	0.75596	12.0884	No
SLV 9	-26375	-33308	-167	0.049	3314.6	0.946	0.75596	12.0884	No

#### Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	23.983	SLU 82	Si
V_SLU	388.066	SLU 2	Si
PF_SLV	13.795	SLV 11	Si
V_SLV	3.533	SLV 11	Si
PFFP_SLV	13.093	SLV 7	Si
R_SLV	0.047	SLV 3	No

## Maschio 18

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

#### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-26.838	-3.854	-26.838	-2.079	L1	L2	1.775	0.3	2.69	2.69	2.69			

#### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	t0	fv0	$\mu$	$\phi$	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

#### Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 18	-1.3	-12688	1790.07	23827	7966.79	4.451	Si
SLU 18	0.05	-12094	2814.25	22712	7740.84	2.751	Si
SLU 18	1.39	-6324	1560.41	11877	4794.49	3.073	Si
SLU 82	-1.3	-15849	2154.84	29764	8926.62	4.143	Si
SLU 82	0.05	-15025	3401.52	28215	8715.66	2.562	Si
SLU 82	1.39	-7811	1882.81	14668	5683.84	3.019	Si
SLU 81	-1.3	-15909	2177.6	29877	8940.85	4.106	Si



Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 81	0.05	-15092	3433.51	28342	8734.03	2.544	Si
SLU 81	1.39	-7851	1890.57	14744	5706.62	3.018	Si
SLU 40	-1.3	-14197	2112.9	26661	8475.88	4.011	Si
SLU 40	0.05	-13693	3307.23	25714	8316.21	2.515	Si
SLU 40	1.39	-7267	1861.74	13648	5369.15	2.884	Si
SLU 39	-1.3	-14257	2135.66	26773	8494.16	3.977	Si
SLU 39	0.05	-13761	3339.23	25841	8338.27	2.497	Si
SLU 39	1.39	-7307	1869.5	13723	5392.82	2.885	Si
SLU 84	-1.3	-15849	2154.84	29764	8926.62	4.143	Si
SLU 84	0.05	-15025	3401.52	28215	8715.66	2.562	Si
SLU 84	1.39	-7811	1882.81	14668	5683.84	3.019	Si
SLU 42	-1.3	-14197	2112.9	26661	8475.88	4.011	Si
SLU 42	0.05	-13693	3307.23	25714	8316.21	2.515	Si
SLU 42	1.39	-7267	1861.74	13648	5369.15	2.884	Si
SLU 20	-1.3	-12688	1790.07	23827	7966.79	4.451	Si
SLU 20	0.05	-12094	2814.25	22712	7740.84	2.751	Si
SLU 20	1.39	-6324	1560.41	11877	4794.49	3.073	Si
SLU 83	-1.3	-15909	2177.6	29877	8940.85	4.106	Si
SLU 83	0.05	-15092	3433.51	28342	8734.03	2.544	Si
SLU 83	1.39	-7851	1890.57	14744	5706.62	3.018	Si
SLU 41	-1.3	-14257	2135.66	26773	8494.16	3.977	Si
SLU 41	0.05	-13761	3339.23	25841	8338.27	2.497	Si
SLU 41	1.39	-7307	1869.5	13723	5392.82	2.885	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 8	-1.3	-12694	4469.54	23839	9068.18	2.029	Si
SLV 8	0.05	-8514	2029.02	15989	6567.65	3.237	Si
SLV 8	1.39	-4900	-1405.22	9201	4021.02	2.861	Si
SLV 9	-1.3	-4959	-2700.42	9313	4065.96	1.506	Si
SLV 9	0.05	-7426	859.47	13945	5838.22	6.793	Si
SLV 9	1.39	-2888	2883.57	0	0	0	No, $e > l/2$
SLV 11	-1.3	-11156	4000.98	20951	8203.46	2.05	Si
SLV 11	0.05	-7975	1238.96	14976	6210.27	5.012	Si
SLV 11	1.39	-4069	-1489.87	7641	3385.24	2.272	Si
SLV 12	-1.3	-11156	4000.98	20951	8203.46	2.05	Si
SLV 12	0.05	-7975	1238.96	14976	6210.27	5.012	Si
SLV 12	1.39	-4069	-1489.87	7641	3385.24	2.272	Si
SLV 10	-1.3	-4959	-2700.42	9313	4065.96	1.506	Si
SLV 10	0.05	-7426	859.47	13945	5838.22	6.793	Si
SLV 10	1.39	-2888	2883.57	0	0	0	No, $e > l/2$
SLV 13	-1.3	-5334	-901.58	10016	4345.64	4.82	Si
SLV 13	0.05	-6989	70.56	13124	5536.26	78.458	Si
SLV 13	1.39	-2332	1254.1	4380	1995.57	1.591	Si
SLV 14	-1.3	-5334	-901.58	10016	4345.64	4.82	Si
SLV 14	0.05	-6989	70.56	13124	5536.26	78.458	Si
SLV 14	1.39	-2332	1254.1	4380	1995.57	1.591	Si
SLV 7	-1.3	-12694	4469.54	23839	9068.18	2.029	Si
SLV 7	0.05	-8514	2029.02	15989	6567.65	3.237	Si
SLV 7	1.39	-4900	-1405.22	9201	4021.02	2.861	Si
SLV 6	-1.3	-6498	-2231.87	12202	5190.71	2.326	Si
SLV 6	0.05	-7965	1649.52	14958	6203.68	3.761	Si
SLV 6	1.39	-3719	2968.22	6984	3112.14	1.048	Si
SLV 5	-1.3	-6498	-2231.87	12202	5190.71	2.326	Si
SLV 5	0.05	-7965	1649.52	14958	6203.68	3.761	Si
SLV 5	1.39	-3719	2968.22	6984	3112.14	1.048	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 62	-1.3	-14341	-1147	1832.01		26931	1.775	9146	4870			4.25	Si
SLU 62	0.05	-13426	-1181	2908.54		25213	1.775	8917	4748			4.02	Si
SLU 62	1.39	-6868	-866	1581.47		12897	1.775	7275	3874			4.47	Si
SLU 83	-1.3	-15909	-1336	2177.6		29877	1.775	9539	5080			3.8	Si
SLU 83	0.05	-15092	-1376	3433.51		28342	1.775	9335	4971			3.61	Si
SLU 83	1.39	-7851	-997	1890.57		14744	1.775	7521	4005			4.02	Si
SLU 81	-1.3	-15909	-1336	2177.6		29877	1.775	9539	5080			3.8	Si
SLU 81	0.05	-15092	-1376	3433.51		28342	1.775	9335	4971			3.61	Si
SLU 81	1.39	-7851	-997	1890.57		14744	1.775	7521	4005			4.02	Si
SLU 41	-1.3	-14257	-1280	2135.66		26773	1.775	9125	4859			3.8	Si
SLU 41	0.05	-13761	-1317	3339.23		25841	1.775	9001	4793			3.64	Si
SLU 41	1.39	-7307	-946	1869.5		13723	1.775	7385	3933			4.16	Si
SLU 39	-1.3	-14257	-1280	2135.66		26773	1.775	9125	4859			3.8	Si
SLU 39	0.05	-13761	-1317	3339.23		25841	1.775	9001	4793			3.64	Si
SLU 39	1.39	-7307	-946	1869.5		13723	1.775	7385	3933			4.16	Si
SLU 60	-1.3	-14341	-1147	1832.01		26931	1.775	9146	4870			4.25	Si
SLU 60	0.05	-13426	-1181	2908.54		25213	1.775	8917	4748			4.02	Si
SLU 60	1.39	-6868	-866	1581.47		12897	1.775	7275	3874			4.47	Si
SLU 82	-1.3	-15849	-1323	2154.84		29764	1.775	9524	5072			3.83	Si
SLU 82	0.05	-15025	-1364	3401.52		28215	1.775	9318	4962			3.64	Si
SLU 82	1.39	-7811	-997	1882.81		14668	1.775	7511	4000			4.01	Si
SLU 42	-1.3	-14197	-1267	2112.9		26661	1.775	9110	4851			3.83	Si
SLU 42	0.05	-13693	-1305	3307.23		25714	1.775	8984	4784			3.66	Si
SLU 42	1.39	-7267	-947	1861.74		13648	1.775	7375	3927			4.15	Si
SLU 40	-1.3	-14197	-1267	2112.9		26661	1.775	9110	4851			3.83	Si
SLU 40	0.05	-13693	-1305	3307.23		25714	1.775	8984	4784			3.66	Si
SLU 40	1.39	-7267	-947	1861.74		13648	1.775	7375	3927			4.15	Si
SLU 84	-1.3	-15849	-1323	2154.84		29764	1.775	9524	5072			3.83	Si
SLU 84	0.05	-15025	-1364	3401.52		28215	1.775	9318	4962			3.64	Si



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 84	1.39	-7811	-997	1882.81		14668	1.775	7511	4000			4.01	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 11	-1.3	-11156	3876	4000.98		23438	1.5866	13021	6198			1.6	Si
SLV 11	0.05	-7975	3973	1238.96		14976	1.775	11329	6032			1.52	Si
SLV 11	1.39	-4069	1874	-1489.87		8672	1.564	10068	4724			2.52	Si
SLV 9	-1.3	-4959	-4315	-2700.42		16066	1.029	11546	3564			0.83	No, Vu<V
SLV 9	0.05	-7426	-4347	859.47		13945	1.775	11122	5923			1.36	Si
SLV 9	1.39	-2888	-2616	2883.57		0	0	8333	0			0	No, Vu<V
SLV 8	-1.3	-12694	3126	4469.54		26344	1.6062	13602	6554			2.1	Si
SLV 8	0.05	-8514	3120	2029.02		15989	1.775	11531	6140			1.97	Si
SLV 8	1.39	-4900	1710	-1405.22		9201	1.775	10174	5417			3.17	Si
SLV 7	-1.3	-12694	3126	4469.54		26344	1.6062	13602	6554			2.1	Si
SLV 7	0.05	-8514	3120	2029.02		15989	1.775	11531	6140			1.97	Si
SLV 7	1.39	-4900	1710	-1405.22		9201	1.775	10174	5417			3.17	Si
SLV 12	-1.3	-11156	3876	4000.98		23438	1.5866	13021	6198			1.6	Si
SLV 12	0.05	-7975	3973	1238.96		14976	1.775	11329	6032			1.52	Si
SLV 12	1.39	-4069	1874	-1489.87		8672	1.564	10068	4724			2.52	Si
SLV 1	-1.3	-10461	-3073	660.27		19645	1.775	12262	6530			2.12	Si
SLV 1	0.05	-8787	-3284	2704.08		16840	1.7393	11701	6105			1.86	Si
SLV 1	1.39	-5102	-1400	1536.28		9667	1.7591	10267	5418			3.87	Si
SLV 5	-1.3	-6498	-5065	-2231.87		13271	1.632	10988	5380			1.06	Si
SLV 5	0.05	-7965	-5200	1649.52		14958	1.775	11325	6031			1.16	Si
SLV 5	1.39	-3719	-2780	2968.22		46210	0.2683	16250	1308			0.47	No, Vu<V
SLV 10	-1.3	-4959	-4315	-2700.42		16066	1.029	11546	3564			0.83	No, Vu<V
SLV 10	0.05	-7426	-4347	859.47		13945	1.775	11122	5923			1.36	Si
SLV 10	1.39	-2888	-2616	2883.57		0	0	8333	0			0	No, Vu<V
SLV 2	-1.3	-10461	-3073	660.27		19645	1.775	12262	6530			2.12	Si
SLV 2	0.05	-8787	-3284	2704.08		16840	1.7393	11701	6105			1.86	Si
SLV 2	1.39	-5102	-1400	1536.28		9667	1.7591	10267	5418			3.87	Si
SLV 6	-1.3	-6498	-5065	-2231.87		13271	1.632	10988	5380			1.06	Si
SLV 6	0.05	-7965	-5200	1649.52		14958	1.775	11325	6031			1.16	Si
SLV 6	1.39	-3719	-2780	2968.22		46210	0.2683	16250	1308			0.47	No, Vu<V

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.045 Wa 0.05 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 14	143750	0.25	13124	-6989	71.53	935.71	13.08	Si
SLV 13	143750	0.25	13124	-6989	71.53	935.71	13.08	Si
SLV 16	143750	0.25	13434	-7153	71.53	955.05	13.35	Si
SLV 15	143750	0.25	13434	-7153	71.53	955.05	13.35	Si
SLV 9	143750	0.25	13945	-7426	71.53	986.74	13.79	Si
SLV 10	143750	0.25	13945	-7426	71.53	986.74	13.79	Si
SLV 6	143750	0.25	14958	-7965	71.53	1048.51	14.66	Si
SLV 5	143750	0.25	14958	-7965	71.53	1048.51	14.66	Si
SLV 11	143750	0.25	14976	-7975	71.53	1049.62	14.67	Si
SLV 12	143750	0.25	14976	-7975	71.53	1049.62	14.67	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 0.045 Wa = 0.05 Ta = 0.0403

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	a0*	aLim	Verifica
SLV 14	-2332	-5334	-215	0.016	449.1	0.897	0.2616	12.0884	No
SLV 13	-2332	-5334	-215	0.016	449.1	0.897	0.2616	12.0884	No
SLV 10	-2888	-4959	-202	0.025	503.5	0.904	0.39624	12.0884	No
SLV 9	-2888	-4959	-202	0.025	503.5	0.904	0.39624	12.0884	No
SLV 3	-5456	-12320	213	0.035	760.2	0.928	0.54533	12.0884	No
SLV 4	-5456	-12320	213	0.035	760.2	0.928	0.54533	12.0884	No
SLV 8	-4900	-12694	200	0.035	704.2	0.924	0.55246	12.0884	No
SLV 7	-4900	-12694	200	0.035	704.2	0.924	0.55246	12.0884	No
SLV 16	-2686	-7193	-125	0.042	483.7	0.901	0.68245	12.0884	No
SLV 15	-2686	-7193	-125	0.042	483.7	0.901	0.68245	12.0884	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF SLU	2.497	SLU 39	Si
V SLU	3.613	SLU 81	Si
PF SLV	0	SLV 9	No
V SLV	0	SLV 9	No
PFFP SLV	13.081	SLV 13	Si
R SLV	0.022	SLV 13	No

## Maschio 19

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-26.838	-1.079	-26.838	-0.629	L1	L2	0.45	0.3	2.69	2.69	2.69			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	$\tau_0$	fv0	$\mu$	$\phi$	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Sismicad 12.19 - Licenza assegnata a Sidel ingegneria Srl - Via Isonzo, 13 - Villanova di Castenaso (BO)



Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 81	-1.3	-6841	421.79	50672	581.71	1.379	Si
SLU 81	0.05	-10597	-38.03	78497	86.68	2.279	Si
SLU 81	1.39	-8723	-136.01	64617	405.79	2.983	Si
SLU 39	-1.3	-6343	402.5	46982	603.99	1.501	Si
SLU 39	0.05	-10017	-35.93	74197	200.9	5.592	Si
SLU 39	1.39	-8335	-127.83	61737	454	3.552	Si
SLU 42	-1.3	-6320	397.42	46813	604.77	1.522	Si
SLU 42	0.05	-9934	-35.38	73587	215.98	6.105	Si
SLU 42	1.39	-8219	-126.37	60881	467.15	3.697	Si
SLU 83	-1.3	-6841	421.79	50672	581.71	1.379	Si
SLU 83	0.05	-10597	-38.03	78497	86.68	2.279	Si
SLU 83	1.39	-8723	-136.01	64617	405.79	2.983	Si
SLU 40	-1.3	-6320	397.42	46813	604.77	1.522	Si
SLU 40	0.05	-9934	-35.38	73587	215.98	6.105	Si
SLU 40	1.39	-8219	-126.37	60881	467.15	3.697	Si
SLU 60	-1.3	-5993	363.54	44395	613.56	1.688	Si
SLU 60	0.05	-9164	-33.29	67879	343.71	10.325	Si
SLU 60	1.39	-7484	-119.67	55436	537.92	4.495	Si
SLU 41	-1.3	-6343	402.5	46982	603.99	1.501	Si
SLU 41	0.05	-10017	-35.93	74197	200.9	5.592	Si
SLU 41	1.39	-8335	-127.83	61737	454	3.552	Si
SLU 84	-1.3	-6818	416.7	50503	582.95	1.399	Si
SLU 84	0.05	-10515	-37.48	77887	103.71	2.767	Si
SLU 84	1.39	-8608	-134.56	63761	420.78	3.127	Si
SLU 62	-1.3	-5993	363.54	44395	613.56	1.688	Si
SLU 62	0.05	-9164	-33.29	67879	343.71	10.325	Si
SLU 62	1.39	-7484	-119.67	55436	537.92	4.495	Si
SLU 82	-1.3	-6818	416.7	50503	582.95	1.399	Si
SLU 82	0.05	-10515	-37.48	77887	103.71	2.767	Si
SLU 82	1.39	-8608	-134.56	63761	420.78	3.127	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 11	-1.3	-3059	431.81	22657	560.6	1.298	Si
SLV 11	0.05	-5860	-3.85	43407	850.1	220.682	Si
SLV 11	1.39	-4563	-89.48	33801	742.68	8.3	Si
SLV 15	-1.3	-2478	155.63	18354	473.75	3.044	Si
SLV 15	0.05	-3099	-3.76	22953	566.23	150.788	Si
SLV 15	1.39	-1165	-30.45	8629	243.61	8.001	Si
SLV 1	-1.3	-4410	224.73	32670	727.02	3.235	Si
SLV 1	0.05	-6871	-31.31	50895	902.01	28.809	Si
SLV 1	1.39	-6721	-97.03	49785	896.07	9.235	Si
SLV 16	-1.3	-2478	155.63	18354	473.75	3.044	Si
SLV 16	0.05	-3099	-3.76	22953	566.23	150.788	Si
SLV 16	1.39	-1165	-30.45	8629	243.61	8.001	Si
SLV 8	-1.3	-3620	502.38	26812	635.71	1.265	Si
SLV 8	0.05	-7277	-10.23	53901	915	89.443	Si
SLV 8	1.39	-6517	-116.53	48277	887.03	7.612	Si
SLV 12	-1.3	-3059	431.81	22657	560.6	1.298	Si
SLV 12	0.05	-5860	-3.85	43407	850.1	220.682	Si
SLV 12	1.39	-4563	-89.48	33801	742.68	8.3	Si
SLV 4	-1.3	-4348	390.88	32204	720.38	1.843	Si
SLV 4	0.05	-7821	-25.01	57933	925.38	36.993	Si
SLV 4	1.39	-7679	-120.59	56884	923.46	7.658	Si
SLV 7	-1.3	-3620	502.38	26812	635.71	1.265	Si
SLV 7	0.05	-7277	-10.23	53901	915	89.443	Si
SLV 7	1.39	-6517	-116.53	48277	887.03	7.612	Si
SLV 3	-1.3	-4348	390.88	32204	720.38	1.843	Si
SLV 3	0.05	-7821	-25.01	57933	925.38	36.993	Si
SLV 3	1.39	-7679	-120.59	56884	923.46	7.658	Si
SLV 2	-1.3	-4410	224.73	32670	727.02	3.235	Si
SLV 2	0.05	-6871	-31.31	50895	902.01	28.809	Si
SLV 2	1.39	-6721	-97.03	49785	896.07	9.235	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt <sub>lim</sub>	c.s.	Verifica
SLU 40	-1.3	-6320	972	397.42		46813	0.45	10833	1463			1.5	Si
SLU 40	0.05	-9934	996	-35.38		73587	0.45	10833	1463			1.47	Si
SLU 40	1.39	-8219	2101	-126.37		60881	0.45	10833	1463			0.7	No, Vu<V
SLU 62	-1.3	-5993	891	363.54		44395	0.45	10833	1463			1.64	Si
SLU 62	0.05	-9164	913	-33.29		67879	0.45	10833	1463			1.6	Si
SLU 62	1.39	-7484	1924	-119.67		55436	0.45	10833	1463			0.76	No, Vu<V
SLU 81	-1.3	-6841	1033	421.79		50672	0.45	10833	1463			1.42	Si
SLU 81	0.05	-10597	1059	-38.03		78497	0.45	10833	1463			1.38	Si
SLU 81	1.39	-8723	2230	-136.01		64617	0.45	10833	1463			0.66	No, Vu<V
SLU 39	-1.3	-6343	986	402.5		46982	0.45	10833	1463			1.48	Si
SLU 39	0.05	-10017	1011	-35.93		74197	0.45	10833	1463			1.45	Si
SLU 39	1.39	-8335	2124	-127.83		61737	0.45	10833	1463			0.69	No, Vu<V
SLU 82	-1.3	-6818	1020	416.7		50503	0.45	10833	1463			1.43	Si
SLU 82	0.05	-10515	1045	-37.48		77887	0.45	10833	1463			1.4	Si
SLU 82	1.39	-8608	2206	-134.56		63761	0.45	10833	1463			0.66	No, Vu<V
SLU 83	-1.3	-6841	1033	421.79		50672	0.45	10833	1463			1.42	Si
SLU 83	0.05	-10597	1059	-38.03		78497	0.45	10833	1463			1.38	Si
SLU 83	1.39	-8723	2230	-136.01		64617	0.45	10833	1463			0.66	No, Vu<V
SLU 60	-1.3	-5993	891	363.54		44395	0.45	10833	1463			1.64	Si
SLU 60	0.05	-9164	913	-33.29		67879	0.45	10833	1463			1.6	Si
SLU 60	1.39	-7484	1924	-119.67		55436	0.45	10833	1463			0.76	No, Vu<V



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 41	-1.3	-6343	986	402.5		46982	0.45	10833	1463			1.48	Si
SLU 41	0.05	-10017	1011	-35.93		74197	0.45	10833	1463			1.45	Si
SLU 41	1.39	-8335	2124	-127.83		61737	0.45	10833	1463			0.69	No, Vu<V
SLU 84	-1.3	-6818	1020	416.7		50503	0.45	10833	1463			1.43	Si
SLU 84	0.05	-10515	1045	-37.48		77887	0.45	10833	1463			1.4	Si
SLU 84	1.39	-8608	2206	-134.56		63761	0.45	10833	1463			0.66	No, Vu<V
SLU 42	-1.3	-6320	972	397.42		46813	0.45	10833	1463			1.5	Si
SLU 42	0.05	-9934	996	-35.38		73587	0.45	10833	1463			1.47	Si
SLU 42	1.39	-8219	2101	-126.37		60881	0.45	10833	1463			0.7	No, Vu<V

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 1	-1.3	-4410	751	224.73		32670	0.45	14867	2007			2.67	Si
SLV 1	0.05	-6871	749	-31.31		50895	0.45	16250	2194			2.93	Si
SLV 1	1.39	-6721	1496	-97.03		49785	0.45	16250	2194			1.47	Si
SLV 16	-1.3	-2478	182	155.63		18354	0.45	12004	1621			8.93	Si
SLV 16	0.05	-3099	205	-3.76		22953	0.45	12924	1745			8.51	Si
SLV 16	1.39	-1165	528	-30.45		8629	0.45	10059	1358			2.57	Si
SLV 11	-1.3	-3059	781	431.81		40543	0.2515	16250	1226			1.57	Si
SLV 11	0.05	-5860	828	-3.85		43407	0.45	16250	2194			2.65	Si
SLV 11	1.39	-4563	1515	-89.48		33801	0.45	15093	2038			1.34	Si
SLV 3	-1.3	-4348	1015	390.88		35758	0.4053	15485	1883			1.86	Si
SLV 3	0.05	-7821	1034	-25.01		57933	0.45	16250	2194			2.12	Si
SLV 3	1.39	-7679	1923	-120.59		56884	0.45	16250	2194			1.14	Si
SLV 12	-1.3	-3059	781	431.81		40543	0.2515	16250	1226			1.57	Si
SLV 12	0.05	-5860	828	-3.85		43407	0.45	16250	2194			2.65	Si
SLV 12	1.39	-4563	1515	-89.48		33801	0.45	15093	2038			1.34	Si
SLV 4	-1.3	-4348	1015	390.88		35758	0.4053	15485	1883			1.86	Si
SLV 4	0.05	-7821	1034	-25.01		57933	0.45	16250	2194			2.12	Si
SLV 4	1.39	-7679	1923	-120.59		56884	0.45	16250	2194			1.14	Si
SLV 2	-1.3	-4410	751	224.73		32670	0.45	14867	2007			2.67	Si
SLV 2	0.05	-6871	749	-31.31		50895	0.45	16250	2194			2.93	Si
SLV 2	1.39	-6721	1496	-97.03		49785	0.45	16250	2194			1.47	Si
SLV 8	-1.3	-3620	1031	502.38		46653	0.2586	16250	1261			1.22	Si
SLV 8	0.05	-7277	1077	-10.23		53901	0.45	16250	2194			2.04	Si
SLV 8	1.39	-6517	1934	-116.53		48277	0.45	16250	2194			1.13	Si
SLV 7	-1.3	-3620	1031	502.38		46653	0.2586	16250	1261			1.22	Si
SLV 7	0.05	-7277	1077	-10.23		53901	0.45	16250	2194			2.04	Si
SLV 7	1.39	-6517	1934	-116.53		48277	0.45	16250	2194			1.13	Si
SLV 15	-1.3	-2478	182	155.63		18354	0.45	12004	1621			8.93	Si
SLV 15	0.05	-3099	205	-3.76		22953	0.45	12924	1745			8.51	Si
SLV 15	1.39	-1165	528	-30.45		8629	0.45	10059	1358			2.57	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.045 Wa 0.05 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 13	143750	0.25	15915	-2149	18.13	280.3	15.46	Si
SLV 14	143750	0.25	15915	-2149	18.13	280.3	15.46	Si
SLV 10	143750	0.25	19947	-2693	18.13	337.99	18.64	Si
SLV 9	143750	0.25	19947	-2693	18.13	337.99	18.64	Si
SLV 15	143750	0.25	22953	-3099	18.13	377.48	20.82	Si
SLV 16	143750	0.25	22953	-3099	18.13	377.48	20.82	Si
SLV 5	143750	0.25	30441	-4110	18.13	462.86	25.52	Si
SLV 6	143750	0.25	30441	-4110	18.13	462.86	25.52	Si
SLV 11	143750	0.25	43407	-5860	18.13	566.73	31.25	Si
SLV 12	143750	0.25	43407	-5860	18.13	566.73	31.25	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 0.045 Wa = 0.05 Ta = 0.0403

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	a0*	aLim	Verifica
SLV 4	-7679	-4348	7	0.057	833.1	0.981	0.84775	12.0884	No
SLV 3	-7679	-4348	7	0.057	833.1	0.981	0.84775	12.0884	No
SLV 1	-6721	-4410	7	0.057	735.5	0.978	0.85144	12.0884	No
SLV 2	-6721	-4410	7	0.057	735.5	0.978	0.85144	12.0884	No
SLV 8	-6517	-3620	3	0.058	714.7	0.978	0.86142	12.0884	No
SLV 7	-6517	-3620	3	0.058	714.7	0.978	0.86142	12.0884	No
SLV 12	-4563	-3059	1	0.059	515.7	0.97	0.88866	12.0884	No
SLV 11	-4563	-3059	1	0.059	515.7	0.97	0.88866	12.0884	No
SLV 5	-3323	-3829	5	0.059	389.5	0.961	0.89685	12.0884	No
SLV 6	-3323	-3829	5	0.059	389.5	0.961	0.89685	12.0884	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	1.379	SLU 81	Si
V_SLU	0.656	SLU 81	No
PF_SLV	1.265	SLV 7	Si
V_SLV	1.134	SLV 7	Si
PFFP_SLV	15.457	SLV 13	Si
R_SLV	0.07	SLV 3	No

## Maschio 20

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)



## Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-24.603	-3.177	-25.893	-3.854	L1	L2	1.457	0.45	2.69	2.69	2.69			

## Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	τ0	fv0	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

## Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 32	-1.3	-7080	35.89	10801	4472.74	124.63	Si
SLU 32	0.05	-4905	112.84	7483	3244.43	28.752	Si
SLU 32	1.39	-3897	116.83	5946	2631.33	22.522	Si
SLU 36	-1.3	-7148	38.49	10904	4508.96	117.146	Si
SLU 36	0.05	-4957	114.08	7562	3275.03	28.708	Si
SLU 36	1.39	-3933	116.55	6000	2653.52	22.767	Si
SLU 41	-1.3	-7108	51.75	10844	4488.07	86.721	Si
SLU 41	0.05	-4940	131.59	7536	3265.09	24.813	Si
SLU 41	1.39	-4005	135.88	6110	2698.25	19.857	Si
SLU 39	-1.3	-7108	51.75	10844	4488.07	86.721	Si
SLU 39	0.05	-4940	131.59	7536	3265.09	24.813	Si
SLU 39	1.39	-4005	135.88	6110	2698.25	19.857	Si
SLU 37	-1.3	-7080	35.89	10801	4472.74	124.63	Si
SLU 37	0.05	-4905	112.84	7483	3244.43	28.752	Si
SLU 37	1.39	-3897	116.83	5946	2631.33	22.522	Si
SLU 42	-1.3	-7176	54.35	10948	4524.24	83.235	Si
SLU 42	0.05	-4992	132.83	7615	3295.64	24.811	Si
SLU 42	1.39	-4041	135.6	6164	2720.34	20.061	Si
SLU 38	-1.3	-7148	38.49	10904	4508.96	117.146	Si
SLU 38	0.05	-4957	114.08	7562	3275.03	28.708	Si
SLU 38	1.39	-3933	116.55	6000	2653.52	22.767	Si
SLU 33	-1.3	-7148	38.49	10904	4508.96	117.146	Si
SLU 33	0.05	-4957	114.08	7562	3275.03	28.708	Si
SLU 33	1.39	-3933	116.55	6000	2653.52	22.767	Si
SLU 40	-1.3	-7176	54.35	10948	4524.24	83.235	Si
SLU 40	0.05	-4992	132.83	7615	3295.64	24.811	Si
SLU 40	1.39	-4041	135.6	6164	2720.34	20.061	Si
SLU 35	-1.3	-7080	35.89	10801	4472.74	124.63	Si
SLU 35	0.05	-4905	112.84	7483	3244.43	28.752	Si
SLU 35	1.39	-3897	116.83	5946	2631.33	22.522	Si

## Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γM = 2

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLV 8	-1.3	-5753	2899.45	8777	3889.19	1.341	Si
SLV 8	0.05	-2619	1150.24	3995	1844.91	1.604	Si
SLV 8	1.39	-2120	420.62	3235	1503.4	3.574	Si
SLV 1	-1.3	-3157	-2899.05	0	0	0	No, e>l/2
SLV 1	0.05	-1566	-1820.89	0	0	0	No, e>l/2
SLV 1	1.39	264	-226.38	0	0	0	No, Trazione
SLV 5	-1.3	-5841	-4022.07	8911	3943.96	0.981	No, M>Mu
SLV 5	0.05	-4775	-1881.94	7284	3270.39	1.738	Si
SLV 5	1.39	-2656	-389.54	4052	1870.38	4.802	Si
SLV 2	-1.3	-3157	-2899.05	0	0	0	No, e>l/2
SLV 2	0.05	-1566	-1820.89	0	0	0	No, e>l/2
SLV 2	1.39	264	-226.38	0	0	0	No, Trazione
SLV 4	-1.3	-3131	-822.59	4776	2191.14	2.664	Si
SLV 4	0.05	-919	-911.24	0	0	0	No, e>l/2
SLV 4	1.39	424	16.67	0	0	0	No, Trazione
SLV 12	-1.3	-8027	4013.31	12246	5260.49	1.311	Si
SLV 12	0.05	-4723	2007.57	7205	3236.88	1.612	Si
SLV 12	1.39	-4462	523.82	6807	3068.93	5.859	Si
SLV 7	-1.3	-5753	2899.45	8777	3889.19	1.341	Si
SLV 7	0.05	-2619	1150.24	3995	1844.91	1.604	Si
SLV 7	1.39	-2120	420.62	3235	1503.4	3.574	Si
SLV 6	-1.3	-5841	-4022.07	8911	3943.96	0.981	No, M>Mu
SLV 6	0.05	-4775	-1881.94	7284	3270.39	1.738	Si
SLV 6	1.39	-2656	-389.54	4052	1870.38	4.802	Si
SLV 11	-1.3	-8027	4013.31	12246	5260.49	1.311	Si
SLV 11	0.05	-4723	2007.57	7205	3236.88	1.612	Si
SLV 11	1.39	-4462	523.82	6807	3068.93	5.859	Si
SLV 3	-1.3	-3131	-822.59	4776	2191.14	2.664	Si
SLV 3	0.05	-919	-911.24	0	0	0	No, e>l/2
SLV 3	1.39	424	16.67	0	0	0	No, Trazione

## Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, γM = 3

Comb.	Quota	N	V par	M	σ0	σN	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 39	-1.3	-7108	-235	51.75		10844	1.4567	7001	4589			19.53	Si
SLU 39	0.05	-4940	-181	131.59		7536	1.4567	6560	4300			23.74	Si
SLU 39	1.39	-4005	-159	135.88		6110	1.4567	6370	4176			26.26	Si
SLU 42	-1.3	-7176	-232	54.35		10948	1.4567	7015	4598			19.82	Si
SLU 42	0.05	-4992	-177	132.83		7615	1.4567	6571	4307			24.35	Si
SLU 42	1.39	-4041	-155	135.6		6164	1.4567	6377	4180			27.05	Si
SLU 82	-1.3	-9192	-257	41.57		14023	1.4567	7425	4867			18.97	Si
SLU 82	0.05	-6350	-185	136.66		9688	1.4567	6847	4488			24.27	Si
SLU 82	1.39	-4992	-159	141.17		7616	1.4567	6571	4307			27.02	Si
SLU 41	-1.3	-7108	-235	51.75		10844	1.4567	7001	4589			19.53	Si





Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 41	0.05	-4940	-181	131.59		7536	1.4567	6560	4300			23.74	Si
SLU 41	1.39	-4005	-159	135.88		6110	1.4567	6370	4176			26.26	Si
SLU 40	-1.3	-7176	-232	54.35		10948	1.4567	7015	4598			19.82	Si
SLU 40	0.05	-4992	-177	132.83		7615	1.4567	6571	4307			24.35	Si
SLU 40	1.39	-4041	-155	135.6		6164	1.4567	6377	4180			27.05	Si
SLU 81	-1.3	-9124	-259	38.97		13919	1.4567	7411	4858			18.72	Si
SLU 81	0.05	-6299	-189	135.41		9609	1.4567	6837	4481			23.7	Si
SLU 81	1.39	-4956	-164	141.45		7561	1.4567	6564	4302			26.26	Si
SLU 84	-1.3	-9192	-257	41.57		14023	1.4567	7425	4867			18.97	Si
SLU 84	0.05	-6350	-185	136.66		9688	1.4567	6847	4488			24.27	Si
SLU 84	1.39	-4992	-159	141.17		7616	1.4567	6571	4307			27.02	Si
SLU 83	-1.3	-9124	-259	38.97		13919	1.4567	7411	4858			18.72	Si
SLU 83	0.05	-6299	-189	135.41		9609	1.4567	6837	4481			23.7	Si
SLU 83	1.39	-4956	-164	141.45		7561	1.4567	6564	4302			26.26	Si
SLU 74	-1.3	-9096	-232	23.1		13876	1.4567	7406	4854			20.91	Si
SLU 74	0.05	-6264	-161	116.67		9556	1.4567	6830	4477			27.79	Si
SLU 74	1.39	-4848	-138	122.4		7397	1.4567	6542	4288			31.14	Si
SLU 77	-1.3	-9096	-232	23.1		13876	1.4567	7406	4854			20.91	Si
SLU 77	0.05	-6264	-161	116.67		9556	1.4567	6830	4477			27.79	Si
SLU 77	1.39	-4848	-138	122.4		7397	1.4567	6542	4288			31.14	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 2	-1.3	-3157	-3420	-2899.05		0	0	8333	0			0	No, Vu<V
SLV 2	0.05	-1566	-4283	-1820.89		0	0	8333	0			0	No, Vu<V
SLV 2	1.39	264	-3159	-226.38		0	0	8333	0			0	No, Vu<V
SLV 1	-1.3	-3157	-3420	-2899.05		0	0	8333	0			0	No, Vu<V
SLV 1	0.05	-1566	-4283	-1820.89		0	0	8333	0			0	No, Vu<V
SLV 1	1.39	264	-3159	-226.38		0	0	8333	0			0	No, Vu<V
SLV 8	-1.3	-5753	2536	2899.45		18995	0.6731	12132	3675			1.45	Si
SLV 8	0.05	-2619	2464	1150.24		6710	0.8673	9675	3776			1.53	Si
SLV 8	1.39	-2120	2931	420.62		3235	1.4567	8980	5887			2.01	Si
SLV 5	-1.3	-5841	-4181	-4022.07		108870	0.1192	16250	872			0.21	No, Vu<V
SLV 5	0.05	-4775	-4525	-1881.94		10583	1.0026	10450	4715			1.04	Si
SLV 5	1.39	-2656	-4277	-389.54		4052	1.4567	9144	5994			1.4	Si
SLV 4	-1.3	-3131	-1404	-822.59		4981	1.3968	9330	5864			4.18	Si
SLV 4	0.05	-919	-2186	-911.24		0	0	8333	0			0	No, Vu<V
SLV 4	1.39	424	-997	16.67		0	0	8333	0			0	No, Vu<V
SLV 12	-1.3	-8027	3898	4013.31		26037	0.6851	13541	4175			1.07	Si
SLV 12	0.05	-4723	4353	2007.57		11536	0.9097	10641	4356			1	Si
SLV 12	1.39	-4462	4136	523.82		6807	1.4567	9695	6355			1.54	Si
SLV 11	-1.3	-8027	3898	4013.31		26037	0.6851	13541	4175			1.07	Si
SLV 11	0.05	-4723	4353	2007.57		11536	0.9097	10641	4356			1	Si
SLV 11	1.39	-4462	4136	523.82		6807	1.4567	9695	6355			1.54	Si
SLV 3	-1.3	-3131	-1404	-822.59		4981	1.3968	9330	5864			4.18	Si
SLV 3	0.05	-919	-2186	-911.24		0	0	8333	0			0	No, Vu<V
SLV 3	1.39	424	-997	16.67		0	0	8333	0			0	No, Vu<V
SLV 7	-1.3	-5753	2536	2899.45		18995	0.6731	12132	3675			1.45	Si
SLV 7	0.05	-2619	2464	1150.24		6710	0.8673	9675	3776			1.53	Si
SLV 7	1.39	-2120	2931	420.62		3235	1.4567	8980	5887			2.01	Si
SLV 6	-1.3	-5841	-4181	-4022.07		108870	0.1192	16250	872			0.21	No, Vu<V
SLV 6	0.05	-4775	-4525	-1881.94		10583	1.0026	10450	4715			1.04	Si
SLV 6	1.39	-2656	-4277	-389.54		4052	1.4567	9144	5994			1.4	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.045 Wa 0.08 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 4	143750	0.25	1401	-919	88.05	204.33	2.32	Si
SLV 3	143750	0.25	1401	-919	88.05	204.33	2.32	Si
SLV 2	143750	0.25	2388	-1566	88.05	345.36	3.92	Si
SLV 1	143750	0.25	2388	-1566	88.05	345.36	3.92	Si
SLV 7	143750	0.25	3995	-2619	88.05	569.94	6.47	Si
SLV 8	143750	0.25	3995	-2619	88.05	569.94	6.47	Si
SLV 12	143750	0.25	7205	-4723	88.05	999.95	11.36	Si
SLV 11	143750	0.25	7205	-4723	88.05	999.95	11.36	Si
SLV 6	143750	0.25	7284	-4775	88.05	1010.3	11.47	Si
SLV 5	143750	0.25	7284	-4775	88.05	1010.3	11.47	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 0.045 Wa = 0.08 Ta = 0.0269

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	$\alpha_0^*$	$\alpha_{lim}$	Verifica
SLV 1	264	-3157	-326	0	0	0	0	11.92381	No, Trazione
SLV 3	424	-3131	-295	0	0	0	0	11.92381	No, Trazione
SLV 4	424	-3131	-295	0	0	0	0	11.92381	No, Trazione
SLV 2	264	-3157	-326	0	0	0	0	11.92381	No, Trazione
SLV 15	-7382	-10711	324	0.062	1003	0.932	0.9713	11.92381	No
SLV 16	-7382	-10711	324	0.062	1003	0.932	0.9713	11.92381	No
SLV 13	-7543	-10737	293	0.066	1019.2	0.933	1.02921	11.92381	No
SLV 14	-7543	-10737	293	0.066	1019.2	0.933	1.02921	11.92381	No
SLV 11	-4462	-8027	144	0.082	709.7	0.912	1.30399	11.4846	No
SLV 12	-4462	-8027	144	0.082	709.7	0.912	1.30399	11.4846	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	19.857	SLU 39	Si
V_SLU	18.722	SLU 81	Si
PF_SLV	0	SLV 4	No



Stato limite	Coeff.s.	Comb.	Verifica
V_SLV	0	SLV 1	No
PFFP_SLV	2.32	SLV 3	Si
R_SLV	0	SLV 4	No

## Maschio 21

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-24.603	5.726	-24.603	-3.177	L1	L2	8.903	0.45	2.69	2.69	2.69			

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	τ0	fv0	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 81	-1.3	-70846	-18901.13	17683	246912.28	13.063	Si
SLU 81	0.05	-55913	-28089.84	13956	206254.81	7.343	Si
SLU 81	1.39	-41200	-30256.71	10284	160249.11	5.296	Si
SLU 32	-1.3	-55596	-15400.18	13877	205328.02	13.333	Si
SLU 32	0.05	-43963	-22852.21	10973	169340.55	7.41	Si
SLU 32	1.39	-32626	-24690.98	8143	130715.15	5.294	Si
SLU 37	-1.3	-55596	-15400.18	13877	205328.02	13.333	Si
SLU 37	0.05	-43963	-22852.21	10973	169340.55	7.41	Si
SLU 37	1.39	-32626	-24690.98	8143	130715.15	5.294	Si
SLU 40	-1.3	-58470	-18049.73	14594	213648.52	11.837	Si
SLU 40	0.05	-46246	-26715.25	11543	176693.32	6.614	Si
SLU 40	1.39	-34841	-28694.07	8696	138537.18	4.828	Si
SLU 42	-1.3	-58470	-18049.73	14594	213648.52	11.837	Si
SLU 42	0.05	-46246	-26715.25	11543	176693.32	6.614	Si
SLU 42	1.39	-34841	-28694.07	8696	138537.18	4.828	Si
SLU 18	-1.3	-54710	-15158.91	13656	202717.14	13.373	Si
SLU 18	0.05	-43050	-22511.68	10745	166359.8	7.39	Si
SLU 18	1.39	-31696	-24146.23	7911	127394.26	5.276	Si
SLU 20	-1.3	-54710	-15158.91	13656	202717.14	13.373	Si
SLU 20	0.05	-43050	-22511.68	10745	166359.8	7.39	Si
SLU 20	1.39	-31696	-24146.23	7911	127394.26	5.276	Si
SLU 35	-1.3	-55596	-15400.18	13877	205328.02	13.333	Si
SLU 35	0.05	-43963	-22852.21	10973	169340.55	7.41	Si
SLU 35	1.39	-32626	-24690.98	8143	130715.15	5.294	Si
SLU 39	-1.3	-58103	-18211.84	14503	212598.17	11.674	Si
SLU 39	0.05	-45867	-26932.96	11448	175481.35	6.515	Si
SLU 39	1.39	-34423	-29040.8	8592	137072.59	4.72	Si
SLU 41	-1.3	-58103	-18211.84	14503	212598.17	11.674	Si
SLU 41	0.05	-45867	-26932.96	11448	175481.35	6.515	Si
SLU 41	1.39	-34423	-29040.8	8592	137072.59	4.72	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γM = 2

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLV 1	-1.3	-37004	-14235.2	9236	152273.16	10.697	Si
SLV 1	0.05	-27292	-16865.16	6812	114717.87	6.802	Si
SLV 1	1.39	-15796	-20565	3943	68047.73	3.309	Si
SLV 3	-1.3	-32258	-42174.8	8052	134134.38	3.18	Si
SLV 3	0.05	-23599	-38099.77	5890	99986.53	2.624	Si
SLV 3	1.39	-12708	-35117.98	3172	55099.86	1.569	Si
SLV 8	-1.3	-36776	-61000.88	9179	151411.17	2.482	Si
SLV 8	0.05	-28624	-52660.78	7145	119968.89	2.278	Si
SLV 8	1.39	-18506	-42369.03	4619	79265.02	1.871	Si
SLV 2	-1.3	-37004	-14235.2	9236	152273.16	10.697	Si
SLV 2	0.05	-27292	-16865.16	6812	114717.87	6.802	Si
SLV 2	1.39	-15796	-20565	3943	68047.73	3.309	Si
SLV 7	-1.3	-36776	-61000.88	9179	151411.17	2.482	Si
SLV 7	0.05	-28624	-52660.78	7145	119968.89	2.278	Si
SLV 7	1.39	-18506	-42369.03	4619	79265.02	1.871	Si
SLV 9	-1.3	-61216	43934.09	15280	238428.11	5.427	Si
SLV 9	0.05	-48935	26874.98	12214	196059.15	7.295	Si
SLV 9	1.39	-36859	14478.7	9200	151724.93	10.479	Si
SLV 11	-1.3	-45395	-49197.91	11331	183338.8	3.727	Si
SLV 11	0.05	-36624	-43907.04	9141	150835.65	3.435	Si
SLV 11	1.39	-26564	-34031.24	6630	111834.4	3.286	Si
SLV 4	-1.3	-32258	-42174.8	8052	134134.38	3.18	Si
SLV 4	0.05	-23599	-38099.77	5890	99986.53	2.624	Si
SLV 4	1.39	-12708	-35117.98	3172	55099.86	1.569	Si
SLV 10	-1.3	-61216	43934.09	15280	238428.11	5.427	Si
SLV 10	0.05	-48935	26874.98	12214	196059.15	7.295	Si
SLV 10	1.39	-36859	14478.7	9200	151724.93	10.479	Si
SLV 12	-1.3	-45395	-49197.91	11331	183338.8	3.727	Si
SLV 12	0.05	-36624	-43907.04	9141	150835.65	3.435	Si
SLV 12	1.39	-26564	-34031.24	6630	111834.4	3.286	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, γM = 3

Comb.	Quota	N	V par	M	σ0	σN	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
-------	-------	---	-------	---	----	----	----	-----	-----------	---------------	--------	------	----------



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 39	-1.3	-58103	-153	-18211.84		14503	8.9031	7489	30005			195.88	Si
SLU 39	0.05	-45867	-148	-26932.96		11448	8.9031	7082	28373			191.82	Si
SLU 39	1.39	-34423	-163	-29040.8		8592	8.9031	6701	26847			164.93	Si
SLU 84	-1.3	-71213	-160	-18739.01		17775	8.9031	7926	31753			197.89	Si
SLU 84	0.05	-56292	-150	-27872.14		14051	8.9031	7429	29763			197.81	Si
SLU 84	1.39	-41617	-162	-29909.99		10388	8.9031	6941	27807			171.93	Si
SLU 41	-1.3	-58103	-153	-18211.84		14503	8.9031	7489	30005			195.88	Si
SLU 41	0.05	-45867	-148	-26932.96		11448	8.9031	7082	28373			191.82	Si
SLU 41	1.39	-34423	-163	-29040.8		8592	8.9031	6701	26847			164.93	Si
SLU 40	-1.3	-58470	-156	-18049.73		14594	8.9031	7501	30054			192.59	Si
SLU 40	0.05	-46246	-148	-26715.25		11543	8.9031	7095	28424			192	Si
SLU 40	1.39	-34841	-157	-28694.07		8696	8.9031	6715	26903			170.84	Si
SLU 42	-1.3	-58470	-156	-18049.73		14594	8.9031	7501	30054			192.59	Si
SLU 42	0.05	-46246	-148	-26715.25		11543	8.9031	7095	28424			192	Si
SLU 42	1.39	-34841	-157	-28694.07		8696	8.9031	6715	26903			170.84	Si
SLU 81	-1.3	-70846	-158	-18901.13		17683	8.9031	7913	31704			201.19	Si
SLU 81	0.05	-55913	-150	-28089.84		13956	8.9031	7416	29713			197.64	Si
SLU 81	1.39	-41200	-167	-30256.71		10284	8.9031	6927	27751			166.13	Si
SLU 82	-1.3	-71213	-160	-18739.01		17775	8.9031	7926	31753			197.89	Si
SLU 82	0.05	-56292	-150	-27872.14		14051	8.9031	7429	29763			197.81	Si
SLU 82	1.39	-41617	-162	-29909.99		10388	8.9031	6941	27807			171.93	Si
SLU 83	-1.3	-70846	-158	-18901.13		17683	8.9031	7913	31704			201.19	Si
SLU 83	0.05	-55913	-150	-28089.84		13956	8.9031	7416	29713			197.64	Si
SLU 83	1.39	-41200	-167	-30256.71		10284	8.9031	6927	27751			166.13	Si
SLU 18	-1.3	-54710	-129	-15158.91		13656	8.9031	7376	29552			228.41	Si
SLU 18	0.05	-43050	-124	-22511.68		10745	8.9031	6988	27998			225.93	Si
SLU 18	1.39	-31696	-137	-24146.23		7911	8.9031	6610	26484			192.67	Si
SLU 20	-1.3	-54710	-129	-15158.91		13656	8.9031	7376	29552			228.41	Si
SLU 20	0.05	-43050	-124	-22511.68		10745	8.9031	6988	27998			225.93	Si
SLU 20	1.39	-31696	-137	-24146.23		7911	8.9031	6610	26484			192.67	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 9	-1.3	-61216	10601	43934.09		15280	8.9031	11389	45630			4.3	Si
SLV 9	0.05	-48935	10728	26874.98		12214	8.9031	10776	43173			4.02	Si
SLV 9	1.39	-36859	8037	14478.7		9200	8.9031	10173	40758			5.07	Si
SLV 6	-1.3	-52597	9778	32131.13		13128	8.9031	10959	43906			4.49	Si
SLV 6	0.05	-40934	9929	18121.25		10217	8.9031	10377	41573			4.19	Si
SLV 6	1.39	-28801	7178	6140.9		7189	8.9031	9771	39147			5.45	Si
SLV 3	-1.3	-32258	-4515	-42174.8		8052	8.9031	9944	39838			8.82	Si
SLV 3	0.05	-23599	-4509	-38099.77		6162	8.5112	9566	36637			8.13	Si
SLV 3	1.39	-12708	-3804	-35117.98		5576	5.064	9449	21531			5.66	Si
SLV 5	-1.3	-52597	9778	32131.13		13128	8.9031	10959	43906			4.49	Si
SLV 5	0.05	-40934	9929	18121.25		10217	8.9031	10377	41573			4.19	Si
SLV 5	1.39	-28801	7178	6140.9		7189	8.9031	9771	39147			5.45	Si
SLV 8	-1.3	-36776	-10733	-61000.88		9754	8.3785	10284	38775			3.61	Si
SLV 8	0.05	-28624	-10848	-52660.78		8118	7.8353	9957	35107			3.24	Si
SLV 8	1.39	-18506	-8176	-42369.03		6340	6.4861	9601	28024			3.43	Si
SLV 10	-1.3	-61216	10601	43934.09		15280	8.9031	11389	45630			4.3	Si
SLV 10	0.05	-48935	10728	26874.98		12214	8.9031	10776	43173			4.02	Si
SLV 10	1.39	-36859	8037	14478.7		9200	8.9031	10173	40758			5.07	Si
SLV 7	-1.3	-36776	-10733	-61000.88		9754	8.3785	10284	38775			3.61	Si
SLV 7	0.05	-28624	-10848	-52660.78		8118	7.8353	9957	35107			3.24	Si
SLV 7	1.39	-18506	-8176	-42369.03		6340	6.4861	9601	28024			3.43	Si
SLV 4	-1.3	-32258	-4515	-42174.8		8052	8.9031	9944	39838			8.82	Si
SLV 4	0.05	-23599	-4509	-38099.77		6162	8.5112	9566	36637			8.13	Si
SLV 4	1.39	-12708	-3804	-35117.98		5576	5.064	9449	21531			5.66	Si
SLV 11	-1.3	-45395	-9910	-49197.91		11331	8.9031	10599	42466			4.29	Si
SLV 11	0.05	-36624	-10049	-43907.04		9141	8.9031	10162	40711			4.05	Si
SLV 11	1.39	-26564	-7317	-34031.24		6630	8.9031	9659	38699			5.29	Si
SLV 12	-1.3	-45395	-9910	-49197.91		11331	8.9031	10599	42466			4.29	Si
SLV 12	0.05	-36624	-10049	-43907.04		9141	8.9031	10162	40711			4.05	Si
SLV 12	1.39	-26564	-7317	-34031.24		6630	8.9031	9659	38699			5.29	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 0.045 Wa 0.08 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 3	143750	0.25	5890	-23599	538.18	5053.75	9.39	Si
SLV 4	143750	0.25	5890	-23599	538.18	5053.75	9.39	Si
SLV 2	143750	0.25	6812	-27292	538.18	5798.33	10.77	Si
SLV 1	143750	0.25	6812	-27292	538.18	5798.33	10.77	Si
SLV 7	143750	0.25	7145	-28624	538.18	6063.74	11.27	Si
SLV 8	143750	0.25	7145	-28624	538.18	6063.74	11.27	Si
SLV 12	143750	0.25	9141	-36624	538.18	7623.88	14.17	Si
SLV 11	143750	0.25	9141	-36624	538.18	7623.88	14.17	Si
SLV 6	143750	0.25	10217	-40934	538.18	8440.07	15.68	Si
SLV 5	143750	0.25	10217	-40934	538.18	8440.07	15.68	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 0.045 Wa = 0.08 Ta = 0.0269

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	$\alpha_0^*$	aLim	Verifica
SLV 13	-42657	-65734	758	0.085	5881.9	0.93	1.32317	11.92381	No
SLV 14	-42657	-65734	758	0.085	5881.9	0.93	1.32317	11.92381	No
SLV 15	-39569	-60988	672	0.086	5570.6	0.927	1.35616	11.92381	No
SLV 16	-39569	-60988	672	0.086	5570.6	0.927	1.35616	11.92381	No
SLV 3	-12708	-32258	-785	0.085	2915	0.891	1.38381	11.92381	No
SLV 4	-12708	-32258	-785	0.085	2915	0.891	1.38381	11.92381	No
SLV 2	-15796	-37004	-699	0.088	3209.4	0.895	1.4307	11.92381	No



Comb.	N top	N base	V orto	$\alpha 0$	M*	e*	a0*	aLim	Verifica
SLV 1	-15796	-37004	-699	0.088	3209.4	0.895	1.4307	11.92381	No
SLV 9	-36859	-61216	349	0.094	5297.9	0.924	1.4719	11.4846	No
SLV 10	-36859	-61216	349	0.094	5297.9	0.924	1.4719	11.4846	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	4.72	SLU 39	Si
V_SLU	164.926	SLU 39	Si
PF_SLV	1.569	SLV 3	Si
V_SLV	3.236	SLV 7	Si
PFFP_SLV	9.39	SLV 3	Si
R_SLV	0.111	SLV 13	No

## Maschio 23

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-34.183	-1.829	-34.183	-2.979	L2	L3	1.15	0.3	3.76	3.76	3.76			

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	$\tau 0$	fv0	$\mu$	$\phi$	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche,  $\gamma M = 3$

Comb.	Quota	N	M	$\alpha 0$	Mu	c.s.	Verifica
SLU 84	1.39	-4820	138.34	13973	2295.68	16.595	Si
SLU 84	3.27	-3726	-282.71	10801	1857.99	6.572	Si
SLU 84	5.15	-248	-54.67	718	141.11	2.581	Si
SLU 34	1.39	-3772	109.01	10935	1877.46	17.224	Si
SLU 34	3.27	-2935	-223.51	8507	1510.92	6.76	Si
SLU 34	5.15	-199	-44.3	576	113.35	2.559	Si
SLU 10	1.39	-3470	100.04	10059	1748.54	17.479	Si
SLU 10	3.27	-2639	-196.49	7650	1374.6	6.996	Si
SLU 10	5.15	-163	-36.47	473	93.23	2.557	Si
SLU 82	1.39	-4820	138.34	13973	2295.68	16.595	Si
SLU 82	3.27	-3726	-282.71	10801	1857.99	6.572	Si
SLU 82	5.15	-248	-54.67	718	141.11	2.581	Si
SLU 42	1.39	-4078	119.2	11822	2004.19	16.813	Si
SLU 42	3.27	-3246	-251.05	9411	1650.66	6.575	Si
SLU 42	5.15	-236	-52.58	684	134.6	2.56	Si
SLU 19	1.39	-3776	110.23	10946	1879.05	17.046	Si
SLU 19	3.27	-2950	-224.03	8553	1518.1	6.776	Si
SLU 19	5.15	-201	-44.75	582	114.53	2.56	Si
SLU 13	1.39	-3470	100.04	10059	1748.54	17.479	Si
SLU 13	3.27	-2639	-196.49	7650	1374.6	6.996	Si
SLU 13	5.15	-163	-36.47	473	93.23	2.557	Si
SLU 40	1.39	-4078	119.2	11822	2004.19	16.813	Si
SLU 40	3.27	-3246	-251.05	9411	1650.66	6.575	Si
SLU 40	5.15	-236	-52.58	684	134.6	2.56	Si
SLU 21	1.39	-3776	110.23	10946	1879.05	17.046	Si
SLU 21	3.27	-2950	-224.03	8553	1518.1	6.776	Si
SLU 21	5.15	-201	-44.75	582	114.53	2.56	Si
SLU 31	1.39	-3772	109.01	10935	1877.46	17.224	Si
SLU 31	3.27	-2935	-223.51	8507	1510.92	6.76	Si
SLU 31	5.15	-199	-44.3	576	113.35	2.559	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma M = 2$

Comb.	Quota	N	M	$\alpha 0$	Mu	c.s.	Verifica
SLV 11	1.39	-2734	-75.68	7925	1469.63	19.419	Si
SLV 11	3.27	-1819	-287.72	5273	1000.61	3.478	Si
SLV 11	5.15	-113	64.86	329	65.05	1.003	Si
SLV 14	1.39	-2660	114.71	7712	1432.82	12.491	Si
SLV 14	3.27	-1985	-56.96	5756	1087.7	19.096	Si
SLV 14	5.15	-107	-91.05	0	0	0	No, e>l/2
SLV 7	1.39	-3036	-66.43	8802	1619.84	24.386	Si
SLV 7	3.27	-2018	-324.72	5851	1104.79	3.402	Si
SLV 7	5.15	-117	87.21	0	0	0	No, e>l/2
SLV 13	1.39	-2660	114.71	7712	1432.82	12.491	Si
SLV 13	3.27	-1985	-56.96	5756	1087.7	19.096	Si
SLV 13	5.15	-107	-91.05	0	0	0	No, e>l/2
SLV 10	1.39	-3164	233.83	9172	1682.43	7.195	Si
SLV 10	3.27	-2433	0.89	7053	1318	1000	Si
SLV 10	5.15	-110	-134.88	0	0	0	No, e>l/2
SLV 9	1.39	-3164	233.83	9172	1682.43	7.195	Si
SLV 9	3.27	-2433	0.89	7053	1318	1000	Si
SLV 9	5.15	-110	-134.88	0	0	0	No, e>l/2
SLV 8	1.39	-3036	-66.43	8802	1619.84	24.386	Si
SLV 8	3.27	-2018	-324.72	5851	1104.79	3.402	Si
SLV 8	5.15	-117	87.21	0	0	0	No, e>l/2
SLV 5	1.39	-3467	243.08	10050	1829.09	7.525	Si
SLV 5	3.27	-2632	-36.11	7631	1418.83	39.295	Si
SLV 5	5.15	-114	-112.54	0	0	0	No, e>l/2



Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 6	1.39	-3467	243.08	10050	1829.09	7.525	Si
SLV 6	3.27	-2632	-36.11	7631	1418.83	39.295	Si
SLV 6	5.15	-114	-112.54	0	0	0	No, $e \geq l/2$
SLV 12	1.39	-2734	-75.68	7925	1469.63	19.419	Si
SLV 12	3.27	-1819	-287.72	5273	1000.61	3.478	Si
SLV 12	5.15	-113	64.86	329	65.05	1.003	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt <sub>lim</sub>	c.s.	Verifica
SLU 40	1.39	-4078	-42	119.2		11822	1.1498	7132	2460			58.29	Si
SLU 40	3.27	-3246	559	-251.05		9411	1.1498	6810	2349			4.2	Si
SLU 40	5.15	-236	-94	-52.58		745	1.0566	5655	1792			19.02	Si
SLU 62	1.39	-4537	-46	128.69		13153	1.1498	7309	2521			54.6	Si
SLU 62	3.27	-3438	485	-256.98		9966	1.1498	6884	2375			4.89	Si
SLU 62	5.15	-213	-72	-46.45		663	1.0712	5644	1814			25.15	Si
SLU 42	1.39	-4078	-42	119.2		11822	1.1498	7132	2460			58.29	Si
SLU 42	3.27	-3246	559	-251.05		9411	1.1498	6810	2349			4.2	Si
SLU 42	5.15	-236	-94	-52.58		745	1.0566	5655	1792			19.02	Si
SLU 41	1.39	-4097	-44	118.52		11878	1.1498	7139	2463			56.29	Si
SLU 41	3.27	-3254	560	-252.35		9433	1.1498	6813	2350			4.2	Si
SLU 41	5.15	-237	-96	-52.2		743	1.0644	5655	1806			18.88	Si
SLU 81	1.39	-4839	-52	137.65		14029	1.1498	7426	2562			48.84	Si
SLU 81	3.27	-3734	575	-284		10824	1.1498	6999	2414			4.2	Si
SLU 81	5.15	-249	-92	-54.29		775	1.0698	5659	1816			19.83	Si
SLU 83	1.39	-4839	-52	137.65		14029	1.1498	7426	2562			48.84	Si
SLU 83	3.27	-3734	575	-284		10824	1.1498	6999	2414			4.2	Si
SLU 83	5.15	-249	-92	-54.29		775	1.0698	5659	1816			19.83	Si
SLU 84	1.39	-4820	-51	138.34		13973	1.1498	7419	2559			50.27	Si
SLU 84	3.27	-3726	574	-282.71		10801	1.1498	6996	2413			4.2	Si
SLU 84	5.15	-248	-90	-54.67		777	1.0624	5659	1804			20	Si
SLU 60	1.39	-4537	-46	128.69		13153	1.1498	7309	2521			54.6	Si
SLU 60	3.27	-3438	485	-256.98		9966	1.1498	6884	2375			4.89	Si
SLU 60	5.15	-213	-72	-46.45		663	1.0712	5644	1814			25.15	Si
SLU 82	1.39	-4820	-51	138.34		13973	1.1498	7419	2559			50.27	Si
SLU 82	3.27	-3726	574	-282.71		10801	1.1498	6996	2413			4.2	Si
SLU 82	5.15	-248	-90	-54.67		777	1.0624	5659	1804			20	Si
SLU 39	1.39	-4097	-44	118.52		11878	1.1498	7139	2463			56.29	Si
SLU 39	3.27	-3254	560	-252.35		9433	1.1498	6813	2350			4.2	Si
SLU 39	5.15	-237	-96	-52.2		743	1.0644	5655	1806			18.88	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt <sub>lim</sub>	c.s.	Verifica
SLV 11	1.39	-2734	-588	-75.68		7925	1.1498	9918	3421			5.82	Si
SLV 11	3.27	-1819	-763	-287.72		5273	1.1498	9388	3238			4.24	Si
SLV 11	5.15	-113	168	64.86		39372	0.0096	16208	47			0.28	No, $V_u < V$
SLV 13	1.39	-2660	440	114.71		7712	1.1498	9876	3407			7.74	Si
SLV 13	3.27	-1985	876	-56.96		5756	1.1498	9485	3272			3.74	Si
SLV 13	5.15	-107	-69	-91.05		0	0	8333	0			0	No, $V_u < V$
SLV 14	1.39	-2660	440	114.71		7712	1.1498	9876	3407			7.74	Si
SLV 14	3.27	-1985	876	-56.96		5756	1.1498	9485	3272			3.74	Si
SLV 14	5.15	-107	-69	-91.05		0	0	8333	0			0	No, $V_u < V$
SLV 8	1.39	-3036	-761	-66.43		8802	1.1498	10094	3482			4.58	Si
SLV 8	3.27	-2018	-947	-324.72		5851	1.1498	9504	3278			3.46	Si
SLV 8	5.15	-117	158	87.21		0	0	8333	0			0	No, $V_u < V$
SLV 7	1.39	-3036	-761	-66.43		8802	1.1498	10094	3482			4.58	Si
SLV 7	3.27	-2018	-947	-324.72		5851	1.1498	9504	3278			3.46	Si
SLV 7	5.15	-117	158	87.21		0	0	8333	0			0	No, $V_u < V$
SLV 12	1.39	-2734	-588	-75.68		7925	1.1498	9918	3421			5.82	Si
SLV 12	3.27	-1819	-763	-287.72		5273	1.1498	9388	3238			4.24	Si
SLV 12	5.15	-113	168	64.86		39372	0.0096	16208	47			0.28	No, $V_u < V$
SLV 10	1.39	-3164	684	233.83		9172	1.1498	10168	3507			5.13	Si
SLV 10	3.27	-2433	1428	0.89		7053	1.1498	9744	3361			2.35	Si
SLV 10	5.15	-110	-214	-134.88		0	0	8333	0			0	No, $V_u < V$
SLV 9	1.39	-3164	684	233.83		9172	1.1498	10168	3507			5.13	Si
SLV 9	3.27	-2433	1428	0.89		7053	1.1498	9744	3361			2.35	Si
SLV 9	5.15	-110	-214	-134.88		0	0	8333	0			0	No, $V_u < V$
SLV 6	1.39	-3467	511	243.08		10050	1.1498	10343	3568			6.98	Si
SLV 6	3.27	-2632	1244	-36.11		7631	1.1498	9860	3401			2.73	Si
SLV 6	5.15	-114	-224	-112.54		0	0	8333	0			0	No, $V_u < V$
SLV 5	1.39	-3467	511	243.08		10050	1.1498	10343	3568			6.98	Si
SLV 5	3.27	-2632	1244	-36.11		7631	1.1498	9860	3401			2.73	Si
SLV 5	5.15	-114	-224	-112.54		0	0	8333	0			0	No, $V_u < V$

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.27  $W_a$  0.05 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 16	143750	0.48	5222	-1801	174.47	258.64	1.48	Si
SLV 15	143750	0.48	5222	-1801	174.47	258.64	1.48	Si
SLV 11	143750	0.48	5273	-1819	174.47	261.07	1.5	Si
SLV 12	143750	0.48	5273	-1819	174.47	261.07	1.5	Si
SLV 13	143750	0.48	5756	-1985	174.47	283.79	1.63	Si
SLV 14	143750	0.48	5756	-1985	174.47	283.79	1.63	Si
SLV 7	143750	0.48	5851	-2018	174.47	288.25	1.65	Si
SLV 8	143750	0.48	5851	-2018	174.47	288.25	1.65	Si
SLV 10	143750	0.48	7053	-2433	174.47	343.88	1.97	Si
SLV 9	143750	0.48	7053	-2433	174.47	343.88	1.97	Si



## Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.27  $W_a = 0.05$   $T_a = 0.0787$

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	a0*	aLim	Verifica
SLV 11	-113	-2734	115	0	239.9	0.961	0	10.142	No
SLV 9	-110	-3164	-105	0	239.8	0.962	0	10.142	No
SLV 12	-113	-2734	115	0	239.9	0.961	0	10.142	No
SLV 10	-110	-3164	-105	0	239.8	0.962	0	10.142	No
SLV 4	-120	-3540	120	0	240.1	0.959	0	8.41479	No
SLV 7	-117	-3036	153	0	240	0.96	0	10.142	No
SLV 3	-120	-3540	120	0	240.1	0.959	0	8.41479	No
SLV 8	-117	-3036	153	0	240	0.96	0	10.142	No
SLV 6	-114	-3467	-68	0.023	239.9	0.961	0.35505	10.142	No
SLV 5	-114	-3467	-68	0.023	239.9	0.961	0.35505	10.142	No

## Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	2.557	SLU 10	Si
V_SLU	4.197	SLU 39	Si
PF_SLV	0	SLV 5	No
V_SLV	0	SLV 5	No
PFFP_SLV	1.482	SLV 15	Si
R_SLV	0	SLV 3	No

## Maschio 24

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-34.183	2.931	-34.183	-0.829	L2	L3	3.76	0.3	3.76	3.76	3.76			

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	t0	fv0	$\mu$	$\phi$	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 40	1.39	-19831	1671.08	17581	29236.05	17.495	Si
SLU 40	3.27	-18015	3528.58	15971	27227.81	7.716	Si
SLU 40	5.15	-15669	5682.11	13891	24434.39	4.3	Si
SLU 82	1.39	-22579	1780.87	20017	32017.42	17.978	Si
SLU 82	3.27	-19772	3602.83	17528	29172.41	8.097	Si
SLU 82	5.15	-16110	5772.69	14282	24976.94	4.327	Si
SLU 42	1.39	-19831	1671.08	17581	29236.05	17.495	Si
SLU 42	3.27	-18015	3528.58	15971	27227.81	7.716	Si
SLU 42	5.15	-15669	5682.11	13891	24434.39	4.3	Si
SLU 83	1.39	-22554	1714.08	19995	31993.94	18.665	Si
SLU 83	3.27	-19774	3566.41	17530	29175.03	8.181	Si
SLU 83	5.15	-16115	5740.39	14286	24982.78	4.352	Si
SLU 41	1.39	-19807	1604.28	17559	29209.82	18.207	Si
SLU 41	3.27	-18017	3492.16	15973	27230.6	7.798	Si
SLU 41	5.15	-15674	5649.82	13895	24440.32	4.326	Si
SLU 31	1.39	-17849	1473.36	15823	27037.51	18.351	Si
SLU 31	3.27	-15723	2955.31	13939	24501.06	8.291	Si
SLU 31	5.15	-12994	4697.36	11520	20974.33	4.465	Si
SLU 81	1.39	-22554	1714.08	19995	31993.94	18.665	Si
SLU 81	3.27	-19774	3566.41	17530	29175.03	8.181	Si
SLU 81	5.15	-16115	5740.39	14286	24982.78	4.352	Si
SLU 84	1.39	-22579	1780.87	20017	32017.42	17.978	Si
SLU 84	3.27	-19772	3602.83	17528	29172.41	8.097	Si
SLU 84	5.15	-16110	5772.69	14282	24976.94	4.327	Si
SLU 34	1.39	-17849	1473.36	15823	27037.51	18.351	Si
SLU 34	3.27	-15723	2955.31	13939	24501.06	8.291	Si
SLU 34	5.15	-12994	4697.36	11520	20974.33	4.465	Si
SLU 39	1.39	-19807	1604.28	17559	29209.82	18.207	Si
SLU 39	3.27	-18017	3492.16	15973	27230.6	7.798	Si
SLU 39	5.15	-15674	5649.82	13895	24440.32	4.326	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 12	1.39	-13101	-2174.49	11615	22289.18	10.25	Si
SLV 12	3.27	-10354	163.03	9179	18003.76	110.429	Si
SLV 12	5.15	-6839	3159.17	6063	12218.97	3.868	Si
SLV 11	1.39	-13101	-2174.49	11615	22289.18	10.25	Si
SLV 11	3.27	-10354	163.03	9179	18003.76	110.429	Si
SLV 11	5.15	-6839	3159.17	6063	12218.97	3.868	Si
SLV 7	1.39	-13389	-2549.65	11870	22726.32	8.914	Si
SLV 7	3.27	-10640	-505.16	9433	18458.81	36.54	Si
SLV 7	5.15	-6856	2593.02	6078	12248.15	4.724	Si
SLV 8	1.39	-13389	-2549.65	11870	22726.32	8.914	Si
SLV 8	3.27	-10640	-505.16	9433	18458.81	36.54	Si
SLV 8	5.15	-6856	2593.02	6078	12248.15	4.724	Si
SLV 13	1.39	-12639	2392.99	11205	21582.98	9.019	Si
SLV 13	3.27	-9896	3090.41	8773	17268.84	5.588	Si



Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 13	5.15	-6736	3073.17	5971	12044.02	3.919	Si
SLV 14	1.39	-12639	2392.99	11205	21582.98	9.019	Si
SLV 14	3.27	-9896	3090.41	8773	17268.84	5.588	Si
SLV 14	5.15	-6736	3073.17	5971	12044.02	3.919	Si
SLV 16	1.39	-12698	486.94	11257	21672.27	44.508	Si
SLV 16	3.27	-9954	2099.11	8824	17361.77	8.271	Si
SLV 16	5.15	-6774	3417.71	6005	12109.07	3.543	Si
SLV 10	1.39	-12907	4179.04	11443	21993.32	5.263	Si
SLV 10	3.27	-10162	3467.36	9009	17695.76	5.104	Si
SLV 10	5.15	-6711	2010.69	5949	12002.2	5.969	Si
SLV 9	1.39	-12907	4179.04	11443	21993.32	5.263	Si
SLV 9	3.27	-10162	3467.36	9009	17695.76	5.104	Si
SLV 9	5.15	-6711	2010.69	5949	12002.2	5.969	Si
SLV 15	1.39	-12698	486.94	11257	21672.27	44.508	Si
SLV 15	3.27	-9954	2099.11	8824	17361.77	8.271	Si
SLV 15	5.15	-6774	3417.71	6005	12109.07	3.543	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 83	1.39	-22554	-98	1714.08		19995	3.76	8222	9274			94.84	Si
SLU 83	3.27	-19774	-264	3566.41		17530	3.76	7893	8903			33.71	Si
SLU 83	5.15	-16115	-690	5740.39		14286	3.76	7460	8415			12.19	Si
SLU 39	1.39	-19807	-126	1604.28		17559	3.76	7897	8908			70.69	Si
SLU 39	3.27	-18017	-288	3492.16		15973	3.76	7685	8669			30.06	Si
SLU 39	5.15	-15674	-681	5649.82		13895	3.76	7408	8357			12.28	Si
SLU 42	1.39	-19831	-103	1671.08		17581	3.76	7900	8911			86.48	Si
SLU 42	3.27	-18015	-284	3528.58		15971	3.76	7685	8669			30.55	Si
SLU 42	5.15	-15669	-683	5682.11		13891	3.76	7408	8356			12.24	Si
SLU 63	1.39	-20719	-53	1579.83		18368	3.76	8005	9029			171.28	Si
SLU 63	3.27	-17659	-214	3018.17		15655	3.76	7643	8621			40.34	Si
SLU 63	5.15	-13638	-581	4842.33		12090	3.76	7168	8085			13.92	Si
SLU 84	1.39	-22579	-75	1780.87		20017	3.76	8224	9277			124	Si
SLU 84	3.27	-19772	-259	3602.83		17528	3.76	7893	8903			34.32	Si
SLU 84	5.15	-16110	-693	5772.69		14282	3.76	7460	8415			12.15	Si
SLU 41	1.39	-19807	-126	1604.28		17559	3.76	7897	8908			70.69	Si
SLU 41	3.27	-18017	-288	3492.16		15973	3.76	7685	8669			30.06	Si
SLU 41	5.15	-15674	-681	5649.82		13895	3.76	7408	8357			12.28	Si
SLU 40	1.39	-19831	-103	1671.08		17581	3.76	7900	8911			86.48	Si
SLU 40	3.27	-18015	-284	3528.58		15971	3.76	7685	8669			30.55	Si
SLU 40	5.15	-15669	-683	5682.11		13891	3.76	7408	8356			12.24	Si
SLU 82	1.39	-22579	-75	1780.87		20017	3.76	8224	9277			124	Si
SLU 82	3.27	-19772	-259	3602.83		17528	3.76	7893	8903			34.32	Si
SLU 82	5.15	-16110	-693	5772.69		14282	3.76	7460	8415			12.15	Si
SLU 81	1.39	-22554	-98	1714.08		19995	3.76	8222	9274			94.84	Si
SLU 81	3.27	-19774	-264	3566.41		17530	3.76	7893	8903			33.71	Si
SLU 81	5.15	-16115	-690	5740.39		14286	3.76	7460	8415			12.19	Si
SLU 61	1.39	-20719	-53	1579.83		18368	3.76	8005	9029			171.28	Si
SLU 61	3.27	-17659	-214	3018.17		15655	3.76	7643	8621			40.34	Si
SLU 61	5.15	-13638	-581	4842.33		12090	3.76	7168	8085			13.92	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 12	1.39	-13101	-2538	-2174.49		11615	3.76	10656	12020			4.74	Si
SLV 12	3.27	-10354	-4118	163.03		9179	3.76	10169	11471			2.79	Si
SLV 12	5.15	-6839	-2678	3159.17		6063	3.76	9546	10768			4.02	Si
SLV 6	1.39	-13195	2594	3803.88		11698	3.76	10673	12039			4.64	Si
SLV 6	3.27	-10447	4041	2799.16		9262	3.76	10186	11489			2.84	Si
SLV 6	5.15	-6728	2130	1444.54		5965	3.76	9526	10746			5.04	Si
SLV 11	1.39	-13101	-2538	-2174.49		11615	3.76	10656	12020			4.74	Si
SLV 11	3.27	-10354	-4118	163.03		9179	3.76	10169	11471			2.79	Si
SLV 11	5.15	-6839	-2678	3159.17		6063	3.76	9546	10768			4.02	Si
SLV 15	1.39	-12698	-603	486.94		11257	3.76	10585	11940			19.79	Si
SLV 15	3.27	-9954	-1543	2099.11		8824	3.76	10098	11391			7.38	Si
SLV 15	5.15	-6774	-1011	3417.71		6005	3.76	9534	10755			10.64	Si
SLV 9	1.39	-12907	2685	4179.04		11443	3.76	10622	11981			4.46	Si
SLV 9	3.27	-10162	3855	3467.36		9009	3.76	10135	11432			2.97	Si
SLV 9	5.15	-6711	2120	2010.69		5949	3.76	9523	10742			5.07	Si
SLV 16	1.39	-12698	-603	486.94		11257	3.76	10585	11940			19.79	Si
SLV 16	3.27	-9954	-1543	2099.11		8824	3.76	10098	11391			7.38	Si
SLV 16	5.15	-6774	-1011	3417.71		6005	3.76	9534	10755			10.64	Si
SLV 7	1.39	-13389	-2630	-2549.65		11870	3.76	10707	12078			4.59	Si
SLV 7	3.27	-10640	-3933	-505.16		9433	3.76	10220	11528			2.93	Si
SLV 7	5.15	-6856	-2667	2593.02		6078	3.76	9549	10771			4.04	Si
SLV 10	1.39	-12907	2685	4179.04		11443	3.76	10622	11981			4.46	Si
SLV 10	3.27	-10162	3855	3467.36		9009	3.76	10135	11432			2.97	Si
SLV 10	5.15	-6711	2120	2010.69		5949	3.76	9523	10742			5.07	Si
SLV 8	1.39	-13389	-2630	-2549.65		11870	3.76	10707	12078			4.59	Si
SLV 8	3.27	-10640	-3933	-505.16		9433	3.76	10220	11528			2.93	Si
SLV 8	5.15	-6856	-2667	2593.02		6078	3.76	9549	10771			4.04	Si
SLV 5	1.39	-13195	2594	3803.88		11698	3.76	10673	12039			4.64	Si
SLV 5	3.27	-10447	4041	2799.16		9262	3.76	10186	11489			2.84	Si
SLV 5	5.15	-6728	2130	1444.54		5965	3.76	9526	10746			5.04	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.27  $W_a 0.05$  denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 13	143750	0.48	8773	-9896	570.52	1377.83	2.42	Si
SLV 14	143750	0.48	8773	-9896	570.52	1377.83	2.42	Si



Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 15	143750	0.48	8824	-9954	570.52	1385.25	2.43	Si
SLV 16	143750	0.48	8824	-9954	570.52	1385.25	2.43	Si
SLV 10	143750	0.48	9009	-10162	570.52	1411.9	2.47	Si
SLV 9	143750	0.48	9009	-10162	570.52	1411.9	2.47	Si
SLV 12	143750	0.48	9179	-10354	570.52	1436.47	2.52	Si
SLV 11	143750	0.48	9179	-10354	570.52	1436.47	2.52	Si
SLV 5	143750	0.48	9262	-10447	570.52	1448.32	2.54	Si
SLV 6	143750	0.48	9262	-10447	570.52	1448.32	2.54	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.27  $W_a = 0.05$   $T_a = 0.0787$

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	a0*	aLim	Verifica
SLV 2	-6793	-13599	-582	0	1318.8	0.897	0	8.41479	No
SLV 1	-6793	-13599	-582	0	1318.8	0.897	0	8.41479	No
SLV 4	-6831	-13657	-570	0.001	1322.5	0.897	0.01004	8.41479	No
SLV 3	-6831	-13657	-570	0.001	1322.5	0.897	0.01004	8.41479	No
SLV 5	-6728	-13195	-471	0.01	1312.5	0.896	0.15609	10.142	No
SLV 6	-6728	-13195	-471	0.01	1312.5	0.896	0.15609	10.142	No
SLV 8	-6856	-13389	-433	0.014	1324.9	0.897	0.22066	10.142	No
SLV 7	-6856	-13389	-433	0.014	1324.9	0.897	0.22066	10.142	No
SLV 9	-6711	-12907	-365	0.02	1310.8	0.896	0.31927	10.142	No
SLV 10	-6711	-12907	-365	0.02	1310.8	0.896	0.31927	10.142	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	4.3	SLV 40	Si
V_SLV	12.151	SLV 82	Si
PF_SLV	3.543	SLV 15	Si
V_SLV	2.786	SLV 11	Si
PFFP_SLV	2.415	SLV 13	Si
R_SLV	0	SLV 1	No

## Maschio 25

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-34.183	5.726	-34.183	3.931	L2	L3	1.795	0.3	3.76	3.76	3.76			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

f <sub>b</sub>	f <sub>k</sub>	f <sub>vk0</sub>	f <sub>medio</sub>	$\tau_0$	f <sub>v0</sub>	$\mu$	$\phi$	f <sub>v,lim</sub>	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 36	1.39	-5526	-118.74	10262	4334.91	36.508	Si
SLU 36	3.27	-3196	378.76	5936	2659.63	7.022	Si
SLU 36	5.15	-119	-68.55	220	106.21	1.549	Si
SLU 31	1.39	-5493	-114.05	10201	4312.89	37.815	Si
SLU 31	3.27	-3203	361.12	5949	2665.04	7.38	Si
SLU 31	5.15	-118	-68.76	220	106.05	1.542	Si
SLU 39	1.39	-5991	-147.87	11126	4642.85	31.398	Si
SLU 39	3.27	-3426	462.94	6362	2834.56	6.123	Si
SLU 39	5.15	-145	-85.64	270	129.96	1.518	Si
SLU 21	1.39	-5575	-122.66	10353	4367.86	35.61	Si
SLU 21	3.27	-3235	395.14	6008	2689.39	6.806	Si
SLU 21	5.15	-121	-70.31	225	108.51	1.543	Si
SLU 34	1.39	-5493	-114.05	10201	4312.89	37.815	Si
SLU 34	3.27	-3203	361.12	5949	2665.04	7.38	Si
SLU 34	5.15	-118	-68.76	220	106.05	1.542	Si
SLU 40	1.39	-5942	-140.84	11035	4610.73	32.737	Si
SLU 40	3.27	-3436	436.48	6381	2842.58	6.513	Si
SLU 40	5.15	-145	-85.94	269	129.72	1.509	Si
SLU 38	1.39	-5526	-118.74	10262	4334.91	36.508	Si
SLU 38	3.27	-3196	378.76	5936	2659.63	7.022	Si
SLU 38	5.15	-119	-68.55	220	106.21	1.549	Si
SLU 41	1.39	-5991	-147.87	11126	4642.85	31.398	Si
SLU 41	3.27	-3426	462.94	6362	2834.56	6.123	Si
SLU 41	5.15	-145	-85.64	270	129.96	1.518	Si
SLU 19	1.39	-5575	-122.66	10353	4367.86	35.61	Si
SLU 19	3.27	-3235	395.14	6008	2689.39	6.806	Si
SLU 19	5.15	-121	-70.31	225	108.51	1.543	Si
SLU 42	1.39	-5942	-140.84	11035	4610.73	32.737	Si
SLU 42	3.27	-3436	436.48	6381	2842.58	6.513	Si
SLU 42	5.15	-145	-85.94	269	129.72	1.509	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 14	1.39	-2734	468.68	5077	2351.6	5.017	Si
SLV 14	3.27	-1914	8.11	3554	1667.55	205.594	Si
SLV 14	5.15	22	-33.06	0	0	0	No, Trazione
SLV 8	1.39	-5952	-724.57	11053	4858.57	6.705	Si





Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 8	3.27	-3181	364.97	5907	2716.98	7.444	Si
SLV 8	5.15	-37	95.31	0	0	0	No, $e \geq l/2$
SLV 13	1.39	-2734	468.68	5077	2351.6	5.017	Si
SLV 13	3.27	-1914	8.11	3554	1667.55	205.594	Si
SLV 13	5.15	22	-33.06	0	0	0	No, Trazione
SLV 11	1.39	-4972	-493.77	9233	4125.05	8.354	Si
SLV 11	3.27	-2808	202.93	5214	2412.45	11.888	Si
SLV 11	5.15	21	116.44	0	0	0	No, Trazione
SLV 12	1.39	-4972	-493.77	9233	4125.05	8.354	Si
SLV 12	3.27	-2808	202.93	5214	2412.45	11.888	Si
SLV 12	5.15	21	116.44	0	0	0	No, Trazione
SLV 9	1.39	-3288	572.67	6105	2803.17	4.895	Si
SLV 9	3.27	-2102	194.05	3904	1826.41	9.412	Si
SLV 9	5.15	-79	-151.5	0	0	0	No, $e \geq l/2$
SLV 5	1.39	-4268	341.88	7925	3581.71	10.477	Si
SLV 5	3.27	-2475	356.09	4597	2138.12	6.004	Si
SLV 5	5.15	-137	-172.63	0	0	0	No, $e \geq l/2$
SLV 6	1.39	-4268	341.88	7925	3581.71	10.477	Si
SLV 6	3.27	-2475	356.09	4597	2138.12	6.004	Si
SLV 6	5.15	-137	-172.63	0	0	0	No, $e \geq l/2$
SLV 10	1.39	-3288	572.67	6105	2803.17	4.895	Si
SLV 10	3.27	-2102	194.05	3904	1826.41	9.412	Si
SLV 10	5.15	-79	-151.5	0	0	0	No, $e \geq l/2$
SLV 7	1.39	-5952	-724.57	11053	4858.57	6.705	Si
SLV 7	3.27	-3181	364.97	5907	2716.98	7.444	Si
SLV 7	5.15	-37	95.31	0	0	0	No, $e \geq l/2$

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 42	1.39	-5942	-19	-140.84		11035	1.795	7027	3784			195.72	Si
SLU 42	3.27	-3436	-258	436.48		6381	1.795	6406	3450			13.36	Si
SLU 42	5.15	-145	126	-85.94		529	0.9146	5626	1544			12.27	Si
SLU 82	1.39	-7088	-28	-151.41		13162	1.795	7310	3937			142.36	Si
SLU 82	3.27	-4095	-281	491.07		7604	1.795	6569	3538			12.58	Si
SLU 82	5.15	-147	121	-84.19		503	0.9738	5623	1643			13.63	Si
SLU 39	1.39	-5991	-6	-147.87		11126	1.795	7039	3791			621.99	Si
SLU 39	3.27	-3426	-253	462.94		6362	1.795	6404	3448			13.63	Si
SLU 39	5.15	-145	132	-85.64		524	0.9242	5625	1560			11.78	Si
SLU 73	1.39	-6639	-50	-124.63		12328	1.795	7199	3877			77.81	Si
SLU 73	3.27	-3862	-261	415.71		7171	1.795	6512	3507			13.42	Si
SLU 73	5.15	-120	87	-67.01		392	1.0232	5608	1721			19.79	Si
SLU 83	1.39	-7137	-14	-158.44		13253	1.795	7323	3943			273.56	Si
SLU 83	3.27	-4084	-276	517.53		7584	1.795	6567	3536			12.81	Si
SLU 83	5.15	-147	127	-83.89		499	0.9831	5622	1658			13.04	Si
SLU 81	1.39	-7137	-14	-158.44		13253	1.795	7323	3943			273.56	Si
SLU 81	3.27	-4084	-276	517.53		7584	1.795	6567	3536			12.81	Si
SLU 81	5.15	-147	127	-83.89		499	0.9831	5622	1658			13.04	Si
SLU 40	1.39	-5942	-19	-140.84		11035	1.795	7027	3784			195.72	Si
SLU 40	3.27	-3436	-258	436.48		6381	1.795	6406	3450			13.36	Si
SLU 40	5.15	-145	126	-85.94		529	0.9146	5626	1544			12.27	Si
SLU 41	1.39	-5991	-6	-147.87		11126	1.795	7039	3791			621.99	Si
SLU 41	3.27	-3426	-253	462.94		6362	1.795	6404	3448			13.63	Si
SLU 41	5.15	-145	132	-85.64		524	0.9242	5625	1560			11.78	Si
SLU 84	1.39	-7088	-28	-151.41		13162	1.795	7310	3937			142.36	Si
SLU 84	3.27	-4095	-281	491.07		7604	1.795	6569	3538			12.58	Si
SLU 84	5.15	-147	121	-84.19		503	0.9738	5623	1643			13.63	Si
SLU 76	1.39	-6639	-50	-124.63		12328	1.795	7199	3877			77.81	Si
SLU 76	3.27	-3862	-261	415.71		7171	1.795	6512	3507			13.42	Si
SLU 76	5.15	-120	87	-67.01		392	1.0232	5608	1721			19.79	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 10	1.39	-3288	538	572.67		6105	1.795	9554	5145			9.57	Si
SLV 10	3.27	-2102	1486	194.05		3904	1.795	9114	4908			3.3	Si
SLV 10	5.15	-79	75	-151.5		0	0	8333	0			0	No, $V_u < V$
SLV 12	1.39	-4972	-984	-493.77		9233	1.795	10180	5482			5.57	Si
SLV 12	3.27	-2808	-1971	202.93		5214	1.795	9376	5049			2.56	Si
SLV 12	5.15	21	-139	116.44		0	0	8333	0			0	No, $V_u < V$
SLV 14	1.39	-2734	-436	468.68		5077	1.795	9349	5034			11.54	Si
SLV 14	3.27	-1914	78	8.11		3554	1.795	9044	4870			62.71	Si
SLV 14	5.15	22	-162	-33.06		0	0	8333	0			0	No, $V_u < V$
SLV 6	1.39	-4268	916	341.88		7925	1.795	9918	5341			5.83	Si
SLV 6	3.27	-2475	1655	356.09		4597	1.795	9253	4983			3.01	Si
SLV 6	5.15	-137	213	-172.63		0	0	8333	0			0	No, $V_u < V$
SLV 11	1.39	-4972	-984	-493.77		9233	1.795	10180	5482			5.57	Si
SLV 11	3.27	-2808	-1971	202.93		5214	1.795	9376	5049			2.56	Si
SLV 11	5.15	21	-139	116.44		0	0	8333	0			0	No, $V_u < V$
SLV 5	1.39	-4268	916	341.88		7925	1.795	9918	5341			5.83	Si
SLV 5	3.27	-2475	1655	356.09		4597	1.795	9253	4983			3.01	Si
SLV 5	5.15	-137	213	-172.63		0	0	8333	0			0	No, $V_u < V$
SLV 7	1.39	-5952	-606	-724.57		11053	1.795	10544	5678			9.37	Si
SLV 7	3.27	-3181	-1802	364.97		5907	1.795	9515	5124			2.84	Si
SLV 7	5.15	-37	0	95.31		0	0	8333	0			0	No, $V_u < V$
SLV 8	1.39	-5952	-606	-724.57		11053	1.795	10544	5678			9.37	Si
SLV 8	3.27	-3181	-1802	364.97		5907	1.795	9515	5124			2.84	Si
SLV 8	5.15	-37	0	95.31		0	0	8333	0			0	No, $V_u < V$
SLV 9	1.39	-3288	538	572.67		6105	1.795	9554	5145			9.57	Si
SLV 9	3.27	-2102	1486	194.05		3904	1.795	9114	4908			3.3	Si



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 9	5.15	-79	75	-151.5		0	0	8333	0			0	No, Vu<V
SLV 13	1.39	-2734	-436	468.68		5077	1.795	9349	5034			11.54	Si
SLV 13	3.27	-1914	78	8.11		3554	1.795	9044	4870			62.71	Si
SLV 13	5.15	22	-162	-33.06		0	0	8333	0			0	No, Vu<V

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.27 Wa 0.05 denominatore  $8 \gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 14	143750	0.48	3554	-1914	272.36	278.7	1.02	Si
SLV 13	143750	0.48	3554	-1914	272.36	278.7	1.02	Si
SLV 9	143750	0.48	3904	-2102	272.36	305.25	1.12	Si
SLV 10	143750	0.48	3904	-2102	272.36	305.25	1.12	Si
SLV 15	143750	0.48	3947	-2125	272.36	308.5	1.13	Si
SLV 16	143750	0.48	3947	-2125	272.36	308.5	1.13	Si
SLV 6	143750	0.48	4597	-2475	272.36	357.35	1.31	Si
SLV 5	143750	0.48	4597	-2475	272.36	357.35	1.31	Si
SLV 12	143750	0.48	5214	-2808	272.36	403.2	1.48	Si
SLV 11	143750	0.48	5214	-2808	272.36	403.2	1.48	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzaria = 3.27 Wa = 0.05 Ta = 0.0787

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	a0*	aLim	Verifica
SLV 12	21	-4972	-97	0	0	0	0	10.142	No, Trazione
SLV 13	22	-2734	19	0	0	0	0	8.41479	No, Trazione
SLV 14	22	-2734	19	0	0	0	0	8.41479	No, Trazione
SLV 15	52	-3239	-39	0	0	0	0	8.41479	No, Trazione
SLV 16	52	-3239	-39	0	0	0	0	8.41479	No, Trazione
SLV 11	21	-4972	-97	0	0	0	0	10.142	No, Trazione
SLV 5	-137	-4268	105	0.023	373.3	0.969	0.35097	10.142	No
SLV 6	-137	-4268	105	0.023	373.3	0.969	0.35097	10.142	No
SLV 9	-79	-3288	97	0.027	372.2	0.98	0.40429	10.142	No
SLV 10	-79	-3288	97	0.027	372.2	0.98	0.40429	10.142	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	1.509	SLU 40	Si
V_SLU	11.783	SLU 39	Si
PF_SLV	0	SLV 16	No
V_SLV	0	SLV 5	No
PFFP_SLV	1.023	SLV 13	Si
R_SLV	0	SLV 16	No

## Maschio 26

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-25.893	-3.854	-34.183	-3.854	L2	L3	8.29	0.3	3.76	3.76	3.76			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	$\tau_0$	fv0	$\mu$	$\phi$	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 37	1.39	-23667	8817.42	9516	86640.56	9.826	Si
SLU 37	3.27	-17257	3964.04	6939	65437.43	16.508	Si
SLU 37	5.15	-12626	-680.96	5077	49075.05	72.067	Si
SLU 81	1.39	-30348	10912.26	12203	106951.97	9.801	Si
SLU 81	3.27	-21843	4907.65	8782	80777.59	16.46	Si
SLU 81	5.15	-15618	-843.49	6280	59748.7	70.835	Si
SLU 18	1.39	-23824	9092.11	9579	87140.89	9.584	Si
SLU 18	3.27	-17419	4084.33	7004	65994.47	16.158	Si
SLU 18	5.15	-12828	-688.71	5158	49804.55	72.316	Si
SLU 42	1.39	-25236	10683.16	10147	91576.22	8.572	Si
SLU 42	3.27	-19300	4867.14	7760	72378.63	14.871	Si
SLU 42	5.15	-15326	-810.1	6162	58721.98	72.487	Si
SLU 41	1.39	-25183	10937.74	10126	91409.71	8.357	Si
SLU 41	3.27	-19285	4905.9	7754	72328	14.743	Si
SLU 41	5.15	-15324	-817.3	6162	58716.27	71.842	Si
SLU 20	1.39	-23824	9092.11	9579	87140.89	9.584	Si
SLU 20	3.27	-17419	4084.33	7004	65994.47	16.158	Si
SLU 20	5.15	-12828	-688.71	5158	49804.55	72.316	Si
SLU 40	1.39	-25236	10683.16	10147	91576.22	8.572	Si
SLU 40	3.27	-19300	4867.14	7760	72378.63	14.871	Si
SLU 40	5.15	-15326	-810.1	6162	58721.98	72.487	Si
SLU 35	1.39	-23667	8817.42	9516	86640.56	9.826	Si
SLU 35	3.27	-17257	3964.04	6939	65437.43	16.508	Si
SLU 35	5.15	-12626	-680.96	5077	49075.05	72.067	Si
SLU 39	1.39	-25183	10937.74	10126	91409.71	8.357	Si
SLU 39	3.27	-19285	4905.9	7754	72328	14.743	Si
SLU 39	5.15	-15324	-817.3	6162	58716.27	71.842	Si



Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 83	1.39	-30348	10912.26	12203	106951.97	9.801	Si
SLU 83	3.27	-21843	4907.65	8782	80777.59	16.46	Si
SLU 83	5.15	-15618	-843.49	6280	59748.7	70.835	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 9	1.39	-22727	6923.61	9138	87160.67	12.589	Si
SLV 9	3.27	-12853	8082.69	5168	51023.27	6.313	Si
SLV 9	5.15	-6436	14.71	2588	26113.97	1000	Si
SLV 4	1.39	-16376	20014.2	6585	64222.75	3.209	Si
SLV 4	3.27	-11733	4469.59	4718	46755.77	10.461	Si
SLV 4	5.15	-6332	-832.91	2546	25699.21	30.855	Si
SLV 15	1.39	-23027	-17208.83	9259	88215.58	5.126	Si
SLV 15	3.27	-13311	-5518.87	5352	52756.62	9.559	Si
SLV 15	5.15	-6303	-46.01	2534	25583.17	556.028	Si
SLV 2	1.39	-17312	25139.3	6961	67672.62	2.692	Si
SLV 2	3.27	-11776	9133.71	4735	46922.82	5.137	Si
SLV 2	5.15	-6389	-677.77	2569	25925.47	38.251	Si
SLV 3	1.39	-16376	20014.2	6585	64222.75	3.209	Si
SLV 3	3.27	-11733	4469.59	4718	46755.77	10.461	Si
SLV 3	5.15	-6332	-832.91	2546	25699.21	30.855	Si
SLV 6	1.39	-20732	18090.52	8336	80073.21	4.426	Si
SLV 6	3.27	-12380	11079.23	4978	49224.24	4.443	Si
SLV 6	5.15	-6445	-221.36	2591	26148.75	118.128	Si
SLV 10	1.39	-22727	6923.61	9138	87160.67	12.589	Si
SLV 10	3.27	-12853	8082.69	5168	51023.27	6.313	Si
SLV 10	5.15	-6436	14.71	2588	26113.97	1000	Si
SLV 1	1.39	-17312	25139.3	6961	67672.62	2.692	Si
SLV 1	3.27	-11776	9133.71	4735	46922.82	5.137	Si
SLV 1	5.15	-6389	-677.77	2569	25925.47	38.251	Si
SLV 16	1.39	-23027	-17208.83	9259	88215.58	5.126	Si
SLV 16	3.27	-13311	-5518.87	5352	52756.62	9.559	Si
SLV 16	5.15	-6303	-46.01	2534	25583.17	556.028	Si
SLV 5	1.39	-20732	18090.52	8336	80073.21	4.426	Si
SLV 5	3.27	-12380	11079.23	4978	49224.24	4.443	Si
SLV 5	5.15	-6445	-221.36	2591	26148.75	118.128	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 37	1.39	-23667	156	8817.42		9516	8.2902	6824	16973			109.09	Si
SLU 37	3.27	-17257	123	3964.04		6939	8.2902	6481	16118			131.04	Si
SLU 37	5.15	-12626	-16	-680.96		5077	8.2902	6232	15500			976.22	Si
SLU 32	1.39	-23667	156	8817.42		9516	8.2902	6824	16973			109.09	Si
SLU 32	3.27	-17257	123	3964.04		6939	8.2902	6481	16118			131.04	Si
SLU 32	5.15	-12626	-16	-680.96		5077	8.2902	6232	15500			976.22	Si
SLU 60	1.39	-28990	162	9066.63		11656	8.2902	7110	17682			109.37	Si
SLU 60	3.27	-19976	128	4086.08		8032	8.2902	6627	16480			128.97	Si
SLU 60	5.15	-13121	-17	-714.9		5276	8.2902	6259	15566			930.35	Si
SLU 83	1.39	-30348	192	10912.26		12203	8.2902	7183	17863			92.99	Si
SLU 83	3.27	-21843	152	4907.65		8782	8.2902	6727	16729			110.15	Si
SLU 83	5.15	-15618	-20	-843.49		6280	8.2902	6393	15899			806.24	Si
SLU 41	1.39	-25183	187	10937.74		10126	8.2902	6906	17175			91.85	Si
SLU 41	3.27	-19285	148	4905.9		7754	8.2902	6589	16388			110.8	Si
SLU 41	5.15	-15324	-19	-817.3		6162	8.2902	6377	15860			825.55	Si
SLU 35	1.39	-23667	156	8817.42		9516	8.2902	6824	16973			109.09	Si
SLU 35	3.27	-17257	123	3964.04		6939	8.2902	6481	16118			131.04	Si
SLU 35	5.15	-12626	-16	-680.96		5077	8.2902	6232	15500			976.22	Si
SLU 39	1.39	-25183	187	10937.74		10126	8.2902	6906	17175			91.85	Si
SLU 39	3.27	-19285	148	4905.9		7754	8.2902	6589	16388			110.8	Si
SLU 39	5.15	-15324	-19	-817.3		6162	8.2902	6377	15860			825.55	Si
SLU 20	1.39	-23824	157	9092.11		9579	8.2902	6833	16994			108.56	Si
SLU 20	3.27	-17419	124	4084.33		7004	8.2902	6489	16139			130.35	Si
SLU 20	5.15	-12828	-16	-688.71		5158	8.2902	6243	15527			957.1	Si
SLU 81	1.39	-30348	192	10912.26		12203	8.2902	7183	17863			92.99	Si
SLU 81	3.27	-21843	152	4907.65		8782	8.2902	6727	16729			110.15	Si
SLU 81	5.15	-15618	-20	-843.49		6280	8.2902	6393	15899			806.24	Si
SLU 18	1.39	-23824	157	9092.11		9579	8.2902	6833	16994			108.56	Si
SLU 18	3.27	-17419	124	4084.33		7004	8.2902	6489	16139			130.35	Si
SLU 18	5.15	-12828	-16	-688.71		5158	8.2902	6243	15527			957.1	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 14	1.39	-23963	-5679	-12083.73		9635	8.2902	10260	25518			4.49	Si
SLV 14	3.27	-13354	-4177	-854.75		5369	8.2902	9407	23396			5.6	Si
SLV 14	5.15	-6360	-2176	109.13		2557	8.2902	8845	21997			10.11	Si
SLV 3	1.39	-16376	5842	20014.2		6585	8.2902	9650	24001			4.11	Si
SLV 3	3.27	-11733	4306	4469.59		4718	8.2902	9277	23072			5.36	Si
SLV 3	5.15	-6332	2160	-832.91		2546	8.2902	8843	21992			10.18	Si
SLV 2	1.39	-17312	7777	25139.3		7143	8.0789	9762	23660			3.04	Si
SLV 2	3.27	-11776	5793	9133.71		4735	8.2902	9280	23081			3.98	Si
SLV 2	5.15	-6389	2657	-677.77		2569	8.2902	8847	22003			8.28	Si
SLV 13	1.39	-23963	-5679	-12083.73		9635	8.2902	10260	25518			4.49	Si
SLV 13	3.27	-13354	-4177	-854.75		5369	8.2902	9407	23396			5.6	Si
SLV 13	5.15	-6360	-2176	109.13		2557	8.2902	8845	21997			10.11	Si
SLV 16	1.39	-23027	-7614	-17208.83		9259	8.2902	10185	25331			3.33	Si
SLV 16	3.27	-13311	-5664	-5518.87		5352	8.2902	9404	23388			4.13	Si
SLV 16	5.15	-6303	-2673	-46.01		2534	8.2902	8840	21986			8.22	Si
SLV 1	1.39	-17312	7777	25139.3		7143	8.0789	9762	23660			3.04	Si



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 1	3.27	-11776	5793	9133.71		4735	8.2902	9280	23081			3.98	Si
SLV 1	5.15	-6389	2657	-677.77		2569	8.2902	8847	22003			8.28	Si
SLV 5	1.39	-20732	5325	18090.52		8336	8.2902	10001	24872			4.67	Si
SLV 5	3.27	-12380	4038	11079.23		4978	8.2902	9329	23201			5.75	Si
SLV 5	5.15	-6445	1545	-221.36		2591	8.2902	8852	22014			14.25	Si
SLV 6	1.39	-20732	5325	18090.52		8336	8.2902	10001	24872			4.67	Si
SLV 6	3.27	-12380	4038	11079.23		4978	8.2902	9329	23201			5.75	Si
SLV 6	5.15	-6445	1545	-221.36		2591	8.2902	8852	22014			14.25	Si
SLV 4	1.39	-16376	5842	20014.2		6585	8.2902	9650	24001			4.11	Si
SLV 4	3.27	-11733	4306	4469.59		4718	8.2902	9277	23072			5.36	Si
SLV 4	5.15	-6332	2160	-832.91		2546	8.2902	8843	21992			10.18	Si
SLV 15	1.39	-23027	-7614	-17208.83		9259	8.2902	10185	25331			3.33	Si
SLV 15	3.27	-13311	-5664	-5518.87		5352	8.2902	9404	23388			4.13	Si
SLV 15	5.15	-6303	-2673	-46.01		2534	8.2902	8840	21986			8.22	Si

#### Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.27 Wa 0.05 denominatore  $8 \gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 3	143750	0.48	4718	-11733	1257.91	1691.97	1.35	Si
SLV 4	143750	0.48	4718	-11733	1257.91	1691.97	1.35	Si
SLV 2	143750	0.48	4735	-11776	1257.91	1698.02	1.35	Si
SLV 1	143750	0.48	4735	-11776	1257.91	1698.02	1.35	Si
SLV 7	143750	0.48	4919	-12234	1257.91	1761.23	1.4	Si
SLV 8	143750	0.48	4919	-12234	1257.91	1761.23	1.4	Si
SLV 5	143750	0.48	4978	-12380	1257.91	1781.3	1.42	Si
SLV 6	143750	0.48	4978	-12380	1257.91	1781.3	1.42	Si
SLV 12	143750	0.48	5109	-12707	1257.91	1826.4	1.45	Si
SLV 11	143750	0.48	5109	-12707	1257.91	1826.4	1.45	Si

#### Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.27 Wa = 0.05 Ta = 0.0787

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	$\alpha_0^*$	aLim	Verifica
SLV 9	-6436	-22727	380	0.037	2112.6	0.891	0.60289	10.142	No
SLV 10	-6436	-22727	380	0.037	2112.6	0.891	0.60289	10.142	No
SLV 7	-6255	-17612	-355	0.039	2097	0.891	0.62899	10.142	No
SLV 8	-6255	-17612	-355	0.039	2097	0.891	0.62899	10.142	No
SLV 5	-6445	-20732	307	0.042	2113.3	0.891	0.68307	10.142	No
SLV 6	-6445	-20732	307	0.042	2113.3	0.891	0.68307	10.142	No
SLV 11	-6246	-19607	-282	0.044	2096.3	0.891	0.71016	10.142	No
SLV 12	-6246	-19607	-282	0.044	2096.3	0.891	0.71016	10.142	No
SLV 13	-6360	-23963	233	0.047	2106	0.891	0.76427	8.41479	No
SLV 14	-6360	-23963	233	0.047	2106	0.891	0.76427	8.41479	No

#### Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	8.357	SLU 39	Si
V_SLU	91.854	SLU 39	Si
PF_SLV	2.692	SLV 1	Si
V_SLV	3.042	SLV 1	Si
PFFP_SLV	1.345	SLV 3	Si
R_SLV	0.059	SLV 9	No

## Maschio 27

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

#### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-34.183	5.726	-33.043	5.726	L2	L3	1.14	0.3	3.76	3.76	3.76			

#### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	$\tau_0$	fv0	$\mu$	$\phi$	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

#### Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 84	1.39	-6430	193.71	18799	2819.2	14.554	Si
SLU 84	3.27	-5554	782.88	16238	2534.73	3.238	Si
SLU 84	5.15	-2018	148.25	5901	1067.07	7.198	Si
SLU 83	1.39	-6395	153.94	18698	2808.64	18.245	Si
SLU 83	3.27	-5576	805.13	16302	2542.19	3.157	Si
SLU 83	5.15	-2018	149.04	5901	1067.18	7.161	Si
SLU 20	1.39	-5023	108.53	14686	2346.93	21.626	Si
SLU 20	3.27	-4447	649.6	13001	2130.14	3.279	Si
SLU 20	5.15	-1655	122	4840	887.52	7.275	Si
SLU 18	1.39	-5023	108.53	14686	2346.93	21.626	Si
SLU 18	3.27	-4447	649.6	13001	2130.14	3.279	Si
SLU 18	5.15	-1655	122	4840	887.52	7.275	Si
SLU 81	1.39	-6395	153.94	18698	2808.64	18.245	Si
SLU 81	3.27	-5576	805.13	16302	2542.19	3.157	Si
SLU 81	5.15	-2018	149.04	5901	1067.18	7.161	Si
SLU 42	1.39	-5509	147.46	16106	2519.17	17.083	Si
SLU 42	3.27	-4958	725.03	14497	2323.36	3.204	Si



Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 42	5.15	-1972	143	5766	1044.58	7.305	Si
SLU 82	1.39	-6430	193.71	18799	2819.2	14.554	Si
SLU 82	3.27	-5554	782.88	16238	2534.73	3.238	Si
SLU 82	5.15	-2018	148.25	5901	1067.07	7.198	Si
SLU 40	1.39	-5509	147.46	16106	2519.17	17.083	Si
SLU 40	3.27	-4958	725.03	14497	2323.36	3.204	Si
SLU 40	5.15	-1972	143	5766	1044.58	7.305	Si
SLU 41	1.39	-5474	107.7	16006	2507.32	23.282	Si
SLU 41	3.27	-4980	747.29	14561	2331.35	3.12	Si
SLU 41	5.15	-1972	143.79	5767	1044.7	7.266	Si
SLU 39	1.39	-5474	107.7	16006	2507.32	23.282	Si
SLU 39	3.27	-4980	747.29	14561	2331.35	3.12	Si
SLU 39	5.15	-1972	143.79	5767	1044.7	7.266	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 3	1.39	-3573	-811.98	10446	1862.44	2.294	Si
SLV 3	3.27	-3846	601.84	11245	1990.56	3.307	Si
SLV 3	5.15	-847	135.81	2475	472.81	3.481	Si
SLV 1	1.39	-2677	-878.58	7827	1428.14	1.626	Si
SLV 1	3.27	-3408	562.78	9964	1784.14	3.17	Si
SLV 1	5.15	-799	135.64	2338	447.01	3.296	Si
SLV 6	1.39	-2246	-263.76	6567	1211.42	4.593	Si
SLV 6	3.27	-2540	390.58	7427	1359.89	3.482	Si
SLV 6	5.15	-752	85.62	2200	421.14	4.919	Si
SLV 13	1.39	-4432	1100.02	12958	2258.34	2.053	Si
SLV 13	3.27	-2389	200.97	6985	1283.97	6.389	Si
SLV 13	5.15	-822	-6.72	2403	459.29	68.298	Si
SLV 14	1.39	-4432	1100.02	12958	2258.34	2.053	Si
SLV 14	3.27	-2389	200.97	6985	1283.97	6.389	Si
SLV 14	5.15	-822	-6.72	2403	459.29	68.298	Si
SLV 4	1.39	-3573	-811.98	10446	1862.44	2.294	Si
SLV 4	3.27	-3846	601.84	11245	1990.56	3.307	Si
SLV 4	5.15	-847	135.81	2475	472.81	3.481	Si
SLV 16	1.39	-5328	1166.62	15577	2649.75	2.271	Si
SLV 16	3.27	-2827	240.03	8266	1502.56	6.26	Si
SLV 16	5.15	-869	-6.56	2541	485.06	73.986	Si
SLV 5	1.39	-2246	-263.76	6567	1211.42	4.593	Si
SLV 5	3.27	-2540	390.58	7427	1359.89	3.482	Si
SLV 5	5.15	-752	85.62	2200	421.14	4.919	Si
SLV 2	1.39	-2677	-878.58	7827	1428.14	1.626	Si
SLV 2	3.27	-3408	562.78	9964	1784.14	3.17	Si
SLV 2	5.15	-799	135.64	2338	447.01	3.296	Si
SLV 15	1.39	-5328	1166.62	15577	2649.75	2.271	Si
SLV 15	3.27	-2827	240.03	8266	1502.56	6.26	Si
SLV 15	5.15	-869	-6.56	2541	485.06	73.986	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 42	1.39	-5509	-467	147.46		16106	1.1401	7703	2635			5.64	Si
SLU 42	3.27	-4958	-525	725.03		14497	1.1401	7489	2561			4.87	Si
SLU 42	5.15	-1972	-195	143		5766	1.1401	6324	2163			11.11	Si
SLU 81	1.39	-6395	-552	153.94		18698	1.1401	8049	2753			4.98	Si
SLU 81	3.27	-5576	-552	805.13		16302	1.1401	7729	2644			4.78	Si
SLU 81	5.15	-2018	-207	149.04		5901	1.1401	6342	2169			10.5	Si
SLU 84	1.39	-6430	-480	193.71		18799	1.1401	8062	2757			5.75	Si
SLU 84	3.27	-5554	-538	782.88		16238	1.1401	7721	2641			4.91	Si
SLU 84	5.15	-2018	-211	148.25		5901	1.1401	6342	2169			10.29	Si
SLU 41	1.39	-5474	-540	107.7		16006	1.1401	7690	2630			4.87	Si
SLU 41	3.27	-4980	-540	747.29		14561	1.1401	7497	2564			4.75	Si
SLU 41	5.15	-1972	-190	143.79		5767	1.1401	6324	2163			11.36	Si
SLU 18	1.39	-5023	-463	108.53		14686	1.1401	7514	2570			5.55	Si
SLU 18	3.27	-4447	-463	649.6		13001	1.1401	7289	2493			5.39	Si
SLU 18	5.15	-1655	-167	122		4840	1.1401	6201	2121			12.73	Si
SLU 83	1.39	-6395	-552	153.94		18698	1.1401	8049	2753			4.98	Si
SLU 83	3.27	-5576	-552	805.13		16302	1.1401	7729	2644			4.78	Si
SLU 83	5.15	-2018	-207	149.04		5901	1.1401	6342	2169			10.5	Si
SLU 82	1.39	-6430	-480	193.71		18799	1.1401	8062	2757			5.75	Si
SLU 82	3.27	-5554	-538	782.88		16238	1.1401	7721	2641			4.91	Si
SLU 82	5.15	-2018	-211	148.25		5901	1.1401	6342	2169			10.29	Si
SLU 20	1.39	-5023	-463	108.53		14686	1.1401	7514	2570			5.55	Si
SLU 20	3.27	-4447	-463	649.6		13001	1.1401	7289	2493			5.39	Si
SLU 20	5.15	-1655	-167	122		4840	1.1401	6201	2121			12.73	Si
SLU 40	1.39	-5509	-467	147.46		16106	1.1401	7703	2635			5.64	Si
SLU 40	3.27	-4958	-525	725.03		14497	1.1401	7489	2561			4.87	Si
SLU 40	5.15	-1972	-195	143		5766	1.1401	6324	2163			11.11	Si
SLU 39	1.39	-5474	-540	107.7		16006	1.1401	7690	2630			4.87	Si
SLU 39	3.27	-4980	-540	747.29		14561	1.1401	7497	2564			4.75	Si
SLU 39	5.15	-1972	-190	143.79		5767	1.1401	6324	2163			11.36	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 5	1.39	-2246	-902	-263.76		6567	1.1401	9647	3299			3.66	Si
SLV 5	3.27	-2540	-1202	390.58		7427	1.1401	9819	3358			2.79	Si
SLV 5	5.15	-752	-224	85.62		2200	1.1401	8773	3001			13.4	Si
SLV 11	1.39	-5759	465	551.8		16837	1.1401	11701	4002			8.61	Si
SLV 11	3.27	-3695	764	412.23		10803	1.1401	10494	3589			4.7	Si
SLV 11	5.15	-916	14	43.47		2679	1.1401	8869	3033			220.44	Si



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 15	1.39	-5328	748	1166.62		16862	1.0532	11706	3698			4.95	Si
SLV 15	3.27	-2827	986	240.03		8266	1.1401	9987	3416			3.47	Si
SLV 15	5.15	-869	7	-6.56		2541	1.1401	8842	3024			432.56	Si
SLV 3	1.39	-3573	-926	-811.98		11582	1.0283	10650	3285			3.55	Si
SLV 3	3.27	-3846	-1013	601.84		11245	1.1401	10582	3619			3.57	Si
SLV 3	5.15	-847	-161	135.81		2475	1.1401	8828	3019			18.75	Si
SLV 4	1.39	-3573	-926	-811.98		11582	1.0283	10650	3285			3.55	Si
SLV 4	3.27	-3846	-1013	601.84		11245	1.1401	10582	3619			3.57	Si
SLV 4	5.15	-847	-161	135.81		2475	1.1401	8828	3019			18.75	Si
SLV 2	1.39	-2677	-1185	-878.58		12300	0.7254	10793	2349			1.98	Si
SLV 2	3.27	-3408	-1423	562.78		9964	1.1401	10326	3532			2.48	Si
SLV 2	5.15	-799	-217	135.64		2338	1.1401	8801	3010			13.86	Si
SLV 6	1.39	-2246	-902	-263.76		6567	1.1401	9647	3299			3.66	Si
SLV 6	3.27	-2540	-1202	390.58		7427	1.1401	9819	3358			2.79	Si
SLV 6	5.15	-752	-224	85.62		2200	1.1401	8773	3001			13.4	Si
SLV 1	1.39	-2677	-1185	-878.58		12300	0.7254	10793	2349			1.98	Si
SLV 1	3.27	-3408	-1423	562.78		9964	1.1401	10326	3532			2.48	Si
SLV 1	5.15	-799	-217	135.64		2338	1.1401	8801	3010			13.86	Si
SLV 12	1.39	-5759	465	551.8		16837	1.1401	11701	4002			8.61	Si
SLV 12	3.27	-3695	764	412.23		10803	1.1401	10494	3589			4.7	Si
SLV 12	5.15	-916	14	43.47		2679	1.1401	8869	3033			220.44	Si
SLV 16	1.39	-5328	748	1166.62		16862	1.0532	11706	3698			4.95	Si
SLV 16	3.27	-2827	986	240.03		8266	1.1401	9987	3416			3.47	Si
SLV 16	5.15	-869	7	-6.56		2541	1.1401	8842	3024			432.56	Si

#### Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.27 Wa 0.05 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 9	143750	0.48	6533	-2234	172.99	317.24	1.83	Si
SLV 10	143750	0.48	6533	-2234	172.99	317.24	1.83	Si
SLV 13	143750	0.48	6985	-2389	172.99	337.87	1.95	Si
SLV 14	143750	0.48	6985	-2389	172.99	337.87	1.95	Si
SLV 6	143750	0.48	7427	-2540	172.99	357.85	2.07	Si
SLV 5	143750	0.48	7427	-2540	172.99	357.85	2.07	Si
SLV 15	143750	0.48	8266	-2827	172.99	395.39	2.29	Si
SLV 16	143750	0.48	8266	-2827	172.99	395.39	2.29	Si
SLV 2	143750	0.48	9964	-3408	172.99	469.49	2.71	Si
SLV 1	143750	0.48	9964	-3408	172.99	469.49	2.71	Si

#### Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 3.27 Wa = 0.05 Ta = 0.0787

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	a0*	aLim	Verifica
SLV 3	-847	-3573	246	0	287.2	0.891	0	8.41479	No
SLV 14	-822	-4432	-245	0	285.1	0.892	0	8.41479	No
SLV 15	-869	-5328	-212	0	289.1	0.891	0	8.41479	No
SLV 4	-847	-3573	246	0	287.2	0.891	0	8.41479	No
SLV 1	-799	-2677	214	0	283.2	0.892	0	8.41479	No
SLV 2	-799	-2677	214	0	283.2	0.892	0	8.41479	No
SLV 16	-869	-5328	-212	0	289.1	0.891	0	8.41479	No
SLV 13	-822	-4432	-245	0	285.1	0.892	0	8.41479	No
SLV 10	-759	-2772	-122	0	279.9	0.893	0.00245	10.142	No
SLV 9	-759	-2772	-122	0	279.9	0.893	0.00245	10.142	No

#### Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	3.12	SLU 39	Si
V_SLU	4.75	SLU 39	Si
PF_SLV	1.626	SLV 1	Si
V_SLV	1.982	SLV 1	Si
PFFP_SLV	1.834	SLV 9	Si
R_SLV	0	SLV 1	No

## Maschio 28

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

#### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-30.833	5.726	-28.373	5.726	L2	L3	2.46	0.3	3.76	3.76	3.76			

#### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	$\tau_0$	fv0	$\mu$	$\phi$	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	32000000	128000000	1.2

#### Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 83	1.39	-16872	-190.25	22861	14928.03	78.465	Si
SLU 83	3.27	-13419	-110.28	18183	12820.88	116.255	Si
SLU 83	5.15	-4570	-30.11	6193	5193.91	172.474	Si
SLU 35	1.39	-13318	-155.54	18046	12752.12	81.986	Si
SLU 35	3.27	-10662	-90.26	14447	10788.3	119.52	Si
SLU 35	5.15	-3692	-24.2	5003	4262.7	176.124	Si
SLU 39	1.39	-14807	-184.09	20064	13726.79	74.565	Si



Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 39	3.27	-12151	-101.43	16465	11924.82	117.572	Si
SLU 39	5.15	-4472	-28.54	6059	5090.93	178.359	Si
SLU 44	1.39	-10513	146.53	14245	10669.53	72.813	Si
SLU 44	3.27	-7060	-38.06	9566	7663.92	201.386	Si
SLU 44	5.15	-1251	-12.22	1695	1506.26	123.278	Si
SLU 5	1.39	-8448	152.69	11448	8931.09	58.49	Si
SLU 5	3.27	-5792	-29.2	7849	6437.99	220.487	Si
SLU 5	5.15	-1152	-10.65	1561	1389.9	130.539	Si
SLU 47	1.39	-10513	146.53	14245	10669.53	72.813	Si
SLU 47	3.27	-7060	-38.06	9566	7663.92	201.386	Si
SLU 47	5.15	-1251	-12.22	1695	1506.26	123.278	Si
SLU 81	1.39	-16872	-190.25	22861	14928.03	78.465	Si
SLU 81	3.27	-13419	-110.28	18183	12820.88	116.255	Si
SLU 81	5.15	-4570	-30.11	6193	5193.91	172.474	Si
SLU 2	1.39	-8448	152.69	11448	8931.09	58.49	Si
SLU 2	3.27	-5792	-29.2	7849	6437.99	220.487	Si
SLU 2	5.15	-1152	-10.65	1561	1389.9	130.539	Si
SLU 37	1.39	-13318	-155.54	18046	12752.12	81.986	Si
SLU 37	3.27	-10662	-90.26	14447	10788.3	119.52	Si
SLU 37	5.15	-3692	-24.2	5003	4262.7	176.124	Si
SLU 41	1.39	-14807	-184.09	20064	13726.79	74.565	Si
SLU 41	3.27	-12151	-101.43	16465	11924.82	117.572	Si
SLU 41	5.15	-4472	-28.54	6059	5090.93	178.359	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 3	1.39	-10388	-5293.05	14076	11305.71	2.136	Si
SLV 3	3.27	-7170	-183.8	9715	8117.87	44.168	Si
SLV 3	5.15	-1895	84.5	2568	2281.75	27.001	Si
SLV 2	1.39	-9221	-5202.44	12495	10182.21	1.957	Si
SLV 2	3.27	-7322	-41.3	9922	8275.28	200.393	Si
SLV 2	5.15	-1885	103.96	2555	2270.45	21.839	Si
SLV 4	1.39	-10388	-5293.05	14076	11305.71	2.136	Si
SLV 4	3.27	-7170	-183.8	9715	8117.87	44.168	Si
SLV 4	5.15	-1895	84.5	2568	2281.75	27.001	Si
SLV 10	1.39	-7917	1614.62	10727	8882.81	5.501	Si
SLV 10	3.27	-7431	193.14	10069	8386.97	43.424	Si
SLV 10	5.15	-1859	-14.07	2519	2239.48	159.174	Si
SLV 9	1.39	-7917	1614.62	10727	8882.81	5.501	Si
SLV 9	3.27	-7431	193.14	10069	8386.97	43.424	Si
SLV 9	5.15	-1859	-14.07	2519	2239.48	159.174	Si
SLV 15	1.39	-10477	5032.12	14196	11389.3	2.263	Si
SLV 15	3.27	-7063	-78.89	9571	8007.38	101.495	Si
SLV 15	5.15	-1872	-132.01	2536	2254.37	17.077	Si
SLV 16	1.39	-10477	5032.12	14196	11389.3	2.263	Si
SLV 16	3.27	-7063	-78.89	9571	8007.38	101.495	Si
SLV 16	5.15	-1872	-132.01	2536	2254.37	17.077	Si
SLV 14	1.39	-9310	5122.73	12615	10268.61	2.005	Si
SLV 14	3.27	-7216	63.61	9778	8165.24	128.37	Si
SLV 14	5.15	-1862	-112.55	2523	2243.07	19.929	Si
SLV 13	1.39	-9310	5122.73	12615	10268.61	2.005	Si
SLV 13	3.27	-7216	63.61	9778	8165.24	128.37	Si
SLV 13	5.15	-1862	-112.55	2523	2243.07	19.929	Si
SLV 1	1.39	-9221	-5202.44	12495	10182.21	1.957	Si
SLV 1	3.27	-7322	-41.3	9922	8275.28	200.393	Si
SLV 1	5.15	-1885	103.96	2555	2270.45	21.839	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt <sub>lim</sub>	c.s.	Verifica
SLU 5	1.39	-8448	96	152.69	11448	2.46	7082	5226				54.54	Si
SLU 5	3.27	-5792	96	-29.2	7849	2.46	6602	4872				50.85	Si
SLU 5	5.15	-1152	-20	-10.65	1561	2.46	5764	4254				212.78	Si
SLU 13	1.39	-11923	74	86.08	16156	2.46	7710	5690				76.64	Si
SLU 13	3.27	-9267	74	-55.24	12557	2.46	7230	5336				71.87	Si
SLU 13	5.15	-2970	-13	-20.77	4025	2.46	6092	4496				346.89	Si
SLU 26	1.39	-9830	87	120.78	13320	2.46	7332	5411				61.86	Si
SLU 26	3.27	-7174	87	-45.39	9721	2.46	6852	5057				57.81	Si
SLU 26	5.15	-1873	-19	-14.77	2539	2.46	5894	4350				231.49	Si
SLU 44	1.39	-10513	97	146.53	14245	2.46	7455	5502				56.73	Si
SLU 44	3.27	-7060	97	-38.06	9566	2.46	6831	5041				51.98	Si
SLU 44	5.15	-1251	-21	-12.22	1695	2.46	5782	4267				207.29	Si
SLU 2	1.39	-8448	96	152.69	11448	2.46	7082	5226				54.54	Si
SLU 2	3.27	-5792	96	-29.2	7849	2.46	6602	4872				50.85	Si
SLU 2	5.15	-1152	-20	-10.65	1561	2.46	5764	4254				212.78	Si
SLU 23	1.39	-9830	87	120.78	13320	2.46	7332	5411				61.86	Si
SLU 23	3.27	-7174	87	-45.39	9721	2.46	6852	5057				57.81	Si
SLU 23	5.15	-1873	-19	-14.77	2539	2.46	5894	4350				231.49	Si
SLU 68	1.39	-11895	89	114.62	16118	2.46	7705	5686				64.16	Si
SLU 68	3.27	-8442	89	-54.25	11439	2.46	7081	5226				58.97	Si
SLU 68	5.15	-1972	-19	-16.34	2672	2.46	5912	4363				225.09	Si
SLU 10	1.39	-11923	74	86.08	16156	2.46	7710	5690				76.64	Si
SLU 10	3.27	-9267	74	-55.24	12557	2.46	7230	5336				71.87	Si
SLU 10	5.15	-2970	-13	-20.77	4025	2.46	6092	4496				346.89	Si
SLU 47	1.39	-10513	97	146.53	14245	2.46	7455	5502				56.73	Si
SLU 47	3.27	-7060	97	-38.06	9566	2.46	6831	5041				51.98	Si
SLU 47	5.15	-1251	-21	-12.22	1695	2.46	5782	4267				207.29	Si
SLU 65	1.39	-11895	89	114.62	16118	2.46	7705	5686				64.16	Si
SLU 65	3.27	-8442	89	-54.25	11439	2.46	7081	5226				58.97	Si



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 65	5.15	-1972	-19	-16.34		2672	2.46	5912	4363			225.09	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 6	1.39	-7890	-1385	-1482.93		10692	2.46	10472	7728			5.58	Si
SLV 6	3.27	-7463	-1011	161.67		10113	2.46	10356	7643			7.56	Si
SLV 6	5.15	-1866	44	50.88		2528	2.46	8839	6523			146.89	Si
SLV 1	1.39	-9221	-2821	-5202.44		15388	1.9974	11411	6838			2.42	Si
SLV 1	3.27	-7322	-2780	-41.3		9922	2.46	10318	7614			2.74	Si
SLV 1	5.15	-1885	122	103.96		2555	2.46	8844	6527			53.48	Si
SLV 14	1.39	-9310	2444	5122.73		15218	2.0392	11377	6960			2.85	Si
SLV 14	3.27	-7216	2642	63.61		9778	2.46	10289	7593			2.87	Si
SLV 14	5.15	-1862	-114	-112.55		2523	2.46	8838	6522			57.11	Si
SLV 15	1.39	-10477	2793	5032.12		15528	2.2491	11439	7718			2.76	Si
SLV 15	3.27	-7063	2752	-78.89		9571	2.46	10248	7563			2.75	Si
SLV 15	5.15	-1872	-119	-132.01		2536	2.46	8841	6524			55.04	Si
SLV 2	1.39	-9221	-2821	-5202.44		15388	1.9974	11411	6838			2.42	Si
SLV 2	3.27	-7322	-2780	-41.3		9922	2.46	10318	7614			2.74	Si
SLV 2	5.15	-1885	122	103.96		2555	2.46	8844	6527			53.48	Si
SLV 5	1.39	-7890	-1385	-1482.93		10692	2.46	10472	7728			5.58	Si
SLV 5	3.27	-7463	-1011	161.67		10113	2.46	10356	7643			7.56	Si
SLV 5	5.15	-1866	44	50.88		2528	2.46	8839	6523			146.89	Si
SLV 16	1.39	-10477	2793	5032.12		15528	2.2491	11439	7718			2.76	Si
SLV 16	3.27	-7063	2752	-78.89		9571	2.46	10248	7563			2.75	Si
SLV 16	5.15	-1872	-119	-132.01		2536	2.46	8841	6524			55.04	Si
SLV 4	1.39	-10388	-2473	-5293.05		16021	2.1615	11537	7481			3.03	Si
SLV 4	3.27	-7170	-2670	-183.8		9715	2.46	10276	7584			2.84	Si
SLV 4	5.15	-1895	118	84.5		2568	2.46	8847	6529			55.47	Si
SLV 3	1.39	-10388	-2473	-5293.05		16021	2.1615	11537	7481			3.03	Si
SLV 3	3.27	-7170	-2670	-183.8		9715	2.46	10276	7584			2.84	Si
SLV 3	5.15	-1895	118	84.5		2568	2.46	8847	6529			55.47	Si
SLV 13	1.39	-9310	2444	5122.73		15218	2.0392	11377	6960			2.85	Si
SLV 13	3.27	-7216	2642	63.61		9778	2.46	10289	7593			2.87	Si
SLV 13	5.15	-1862	-114	-112.55		2523	2.46	8838	6522			57.11	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.27  $W_a 0.05$  denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 11	143750	0.48	9380	-6923	373.27	958.7	2.57	Si
SLV 12	143750	0.48	9380	-6923	373.27	958.7	2.57	Si
SLV 7	143750	0.48	9424	-6955	373.27	962.76	2.58	Si
SLV 8	143750	0.48	9424	-6955	373.27	962.76	2.58	Si
SLV 16	143750	0.48	9571	-7063	373.27	976.51	2.62	Si
SLV 15	143750	0.48	9571	-7063	373.27	976.51	2.62	Si
SLV 4	143750	0.48	9715	-7170	373.27	989.98	2.65	Si
SLV 3	143750	0.48	9715	-7170	373.27	989.98	2.65	Si
SLV 13	143750	0.48	9778	-7216	373.27	995.76	2.67	Si
SLV 14	143750	0.48	9778	-7216	373.27	995.76	2.67	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 3.27  $W_a = 0.05$   $T_a = 0.0787$

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	a0*	aLim	Verifica
SLV 12	-1891	-11808	14	0.059	625.2	0.891	0.96803	10.142	No
SLV 11	-1891	-11808	14	0.059	625.2	0.891	0.96803	10.142	No
SLV 5	-1866	-7890	-14	0.06	623.1	0.891	0.97231	10.142	No
SLV 6	-1866	-7890	-14	0.06	623.1	0.891	0.97231	10.142	No
SLV 7	-1898	-11781	-5	0.061	625.8	0.891	1.00131	10.142	No
SLV 8	-1898	-11781	-5	0.061	625.8	0.891	1.00131	10.142	No
SLV 10	-1859	-7917	6	0.061	622.5	0.891	1.00145	10.142	No
SLV 9	-1859	-7917	6	0.061	622.5	0.891	1.00145	10.142	No
SLV 16	-1872	-10477	34	0.055	623.6	0.891	0.89501	8.41479	No
SLV 15	-1872	-10477	34	0.055	623.6	0.891	0.89501	8.41479	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF SLU	58.49	SLU 2	Si
V SLU	50.846	SLU 2	Si
PF SLV	1.957	SLV 1	Si
V SLV	2.424	SLV 1	Si
PFFP SLV	2.568	SLV 11	Si
R SLV	0.095	SLV 11	No

## Maschio 29

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s,sx	a.s,dx
-26.163	5.726	-24.603	5.726	L2	L3	1.56	0.3	3.76	3.76	3.76			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	$\tau_0$	fvd	$\mu$	$\phi$	fvl,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2





Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 84	1.39	-8783	-544.37	18768	5272.26	9.685	Si
SLU 84	3.27	-6954	-1401.08	14860	4434.6	3.165	Si
SLU 84	5.15	-2786	-216.53	5953	2014.04	9.301	Si
SLU 81	1.39	-8811	-578.2	18827	5283.84	9.138	Si
SLU 81	3.27	-6952	-1399.41	14855	4433.34	3.168	Si
SLU 81	5.15	-2786	-215.33	5954	2014.34	9.355	Si
SLU 21	1.39	-6920	-414.8	14786	4417.53	10.65	Si
SLU 21	3.27	-5560	-1126.73	11880	3703.87	3.287	Si
SLU 21	5.15	-2285	-177.54	4883	1675.57	9.438	Si
SLU 40	1.39	-7570	-449.76	16175	4731.73	10.52	Si
SLU 40	3.27	-6248	-1289.98	13351	4074.54	3.159	Si
SLU 40	5.15	-2724	-209.26	5822	1973.1	9.429	Si
SLU 42	1.39	-7570	-449.76	16175	4731.73	10.52	Si
SLU 42	3.27	-6248	-1289.98	13351	4074.54	3.159	Si
SLU 42	5.15	-2724	-209.26	5822	1973.1	9.429	Si
SLU 39	1.39	-7597	-483.6	16234	4744.68	9.811	Si
SLU 39	3.27	-6245	-1288.3	13346	4073.21	3.162	Si
SLU 39	5.15	-2725	-208.05	5823	1973.4	9.485	Si
SLU 41	1.39	-7597	-483.6	16234	4744.68	9.811	Si
SLU 41	3.27	-6245	-1288.3	13346	4073.21	3.162	Si
SLU 41	5.15	-2725	-208.05	5823	1973.4	9.485	Si
SLU 82	1.39	-8783	-544.37	18768	5272.26	9.685	Si
SLU 82	3.27	-6954	-1401.08	14860	4434.6	3.165	Si
SLU 82	5.15	-2786	-216.53	5953	2014.04	9.301	Si
SLU 83	1.39	-8811	-578.2	18827	5283.84	9.138	Si
SLU 83	3.27	-6952	-1399.41	14855	4433.34	3.168	Si
SLU 83	5.15	-2786	-215.33	5954	2014.34	9.355	Si
SLU 19	1.39	-6920	-414.8	14786	4417.53	10.65	Si
SLU 19	3.27	-5560	-1126.73	11880	3703.87	3.287	Si
SLU 19	5.15	-2285	-177.54	4883	1675.57	9.438	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 11	1.39	-6734	-150.21	14390	4633.97	30.849	Si
SLV 11	3.27	-4729	-933.71	10105	3383.45	3.624	Si
SLV 11	5.15	-1210	-111.23	2587	924.15	8.308	Si
SLV 16	1.39	-4863	1118.05	10392	3470.67	3.104	Si
SLV 16	3.27	-4460	-903.29	9531	3207.62	3.551	Si
SLV 16	5.15	-1132	-183.77	2420	865.72	4.711	Si
SLV 2	1.39	-5948	-1885.98	12710	4156.64	2.204	Si
SLV 2	3.27	-3181	-531.1	6798	2343.16	4.412	Si
SLV 2	5.15	-1163	-1.7	2486	888.79	522.742	Si
SLV 13	1.39	-3880	1261.03	8291	2820.99	2.237	Si
SLV 13	3.27	-3988	-797.34	8522	2893.66	3.629	Si
SLV 13	5.15	-1088	-189.58	2325	832.45	4.391	Si
SLV 12	1.39	-6734	-150.21	14390	4633.97	30.849	Si
SLV 12	3.27	-4729	-933.71	10105	3383.45	3.624	Si
SLV 12	5.15	-1210	-111.23	2587	924.15	8.308	Si
SLV 15	1.39	-4863	1118.05	10392	3470.67	3.104	Si
SLV 15	3.27	-4460	-903.29	9531	3207.62	3.551	Si
SLV 15	5.15	-1132	-183.77	2420	865.72	4.711	Si
SLV 1	1.39	-5948	-1885.98	12710	4156.64	2.204	Si
SLV 1	3.27	-3181	-531.1	6798	2343.16	4.412	Si
SLV 1	5.15	-1163	-1.7	2486	888.79	522.742	Si
SLV 14	1.39	-3880	1261.03	8291	2820.99	2.237	Si
SLV 14	3.27	-3988	-797.34	8522	2893.66	3.629	Si
SLV 14	5.15	-1088	-189.58	2325	832.45	4.391	Si
SLV 4	1.39	-6931	-2028.96	14811	4750.84	2.342	Si
SLV 4	3.27	-3653	-637.04	7807	2667.51	4.187	Si
SLV 4	5.15	-1208	4.11	2580	921.97	224.27	Si
SLV 3	1.39	-6931	-2028.96	14811	4750.84	2.342	Si
SLV 3	3.27	-3653	-637.04	7807	2667.51	4.187	Si
SLV 3	5.15	-1208	4.11	2580	921.97	224.27	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt <sub>lim</sub>	c.s.	Verifica
SLU 19	1.39	-6920	525	-414.8		14786	1.5599	7527	3523			6.71	Si
SLU 19	3.27	-5560	521	-1126.73		11880	1.5599	7140	3341			6.41	Si
SLU 19	5.15	-2285	95	-177.54		4883	1.5599	6207	2905			30.66	Si
SLU 42	1.39	-7570	609	-449.76		16175	1.5599	7712	3609			5.92	Si
SLU 42	3.27	-6248	605	-1289.98		13351	1.5599	7336	3433			5.67	Si
SLU 42	5.15	-2724	108	-209.26		5822	1.5599	6332	2963			27.33	Si
SLU 41	1.39	-7597	579	-483.6		16234	1.5599	7720	3613			6.24	Si
SLU 41	3.27	-6245	574	-1288.3		13346	1.5599	7335	3433			5.98	Si
SLU 41	5.15	-2725	109	-208.05		5823	1.5599	6332	2963			27.12	Si
SLU 84	1.39	-8783	620	-544.37		18768	1.5599	8058	3771			6.08	Si
SLU 84	3.27	-6954	616	-1401.08		14860	1.5599	7537	3527			5.72	Si
SLU 84	5.15	-2786	116	-216.53		5953	1.5599	6349	2971			25.67	Si
SLU 82	1.39	-8783	620	-544.37		18768	1.5599	8058	3771			6.08	Si
SLU 82	3.27	-6954	616	-1401.08		14860	1.5599	7537	3527			5.72	Si
SLU 82	5.15	-2786	116	-216.53		5953	1.5599	6349	2971			25.67	Si
SLU 81	1.39	-8811	590	-578.2		18827	1.5599	8066	3775			6.4	Si
SLU 81	3.27	-6952	585	-1399.41		14855	1.5599	7536	3527			6.03	Si
SLU 81	5.15	-2786	117	-215.33		5954	1.5599	6349	2971			25.48	Si
SLU 83	1.39	-8811	590	-578.2		18827	1.5599	8066	3775			6.4	Si
SLU 83	3.27	-6952	585	-1399.41		14855	1.5599	7536	3527			6.03	Si
SLU 83	5.15	-2786	117	-215.33		5954	1.5599	6349	2971			25.48	Si



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 40	1.39	-7570	609	-449.76		16175	1.5599	7712	3609			5.92	Si
SLU 40	3.27	-6248	605	-1289.98		13351	1.5599	7336	3433			5.67	Si
SLU 40	5.15	-2724	108	-209.26		5822	1.5599	6332	2963			27.33	Si
SLU 21	1.39	-6920	525	-414.8		14786	1.5599	7527	3523			6.71	Si
SLU 21	3.27	-5560	521	-1126.73		11880	1.5599	7140	3341			6.41	Si
SLU 21	5.15	-2285	95	-177.54		4883	1.5599	6207	2905			30.66	Si
SLU 39	1.39	-7597	579	-483.6		16234	1.5599	7720	3613			6.24	Si
SLU 39	3.27	-6245	574	-1288.3		13346	1.5599	7335	3433			5.98	Si
SLU 39	5.15	-2725	109	-208.05		5823	1.5599	6332	2963			27.12	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 1	1.39	-5948	-704	-1885.98		14277	1.3887	11189	4661			6.62	Si
SLV 1	3.27	-3181	-965	-531.1		6798	1.5599	9693	4536			4.7	Si
SLV 1	5.15	-1163	-66	-1.7		2486	1.5599	8830	4132			62.72	Si
SLV 15	1.39	-4863	1164	1118.05		10392	1.5599	10412	4873			4.18	Si
SLV 15	3.27	-4460	1421	-903.29		9531	1.5599	10240	4792			3.37	Si
SLV 15	5.15	-1132	176	-183.77		2420	1.5599	8817	4126			23.42	Si
SLV 4	1.39	-6931	-1161	-2028.96		15806	1.4617	11495	5041			4.34	Si
SLV 4	3.27	-3653	-1453	-637.04		7807	1.5599	9895	4631			3.19	Si
SLV 4	5.15	-1208	-124	4.11		2580	1.5599	8849	4141			33.46	Si
SLV 13	1.39	-3880	1622	1261.03		9476	1.3649	10228	4188			2.58	Si
SLV 13	3.27	-3988	1909	-797.34		8522	1.5599	10038	4697			2.46	Si
SLV 13	5.15	-1088	234	-189.58		2325	1.5599	8798	4117			17.59	Si
SLV 10	1.39	-3457	1341	326.39		7386	1.5599	9811	4591			3.42	Si
SLV 10	3.27	-3155	1473	-580.55		6741	1.5599	9682	4531			3.08	Si
SLV 10	5.15	-1063	197	-130.6		2270	1.5599	8787	4112			20.92	Si
SLV 9	1.39	-3457	1341	326.39		7386	1.5599	9811	4591			3.42	Si
SLV 9	3.27	-3155	1473	-580.55		6741	1.5599	9682	4531			3.08	Si
SLV 9	5.15	-1063	197	-130.6		2270	1.5599	8787	4112			20.92	Si
SLV 14	1.39	-3880	1622	1261.03		9476	1.3649	10228	4188			2.58	Si
SLV 14	3.27	-3988	1909	-797.34		8522	1.5599	10038	4697			2.46	Si
SLV 14	5.15	-1088	234	-189.58		2325	1.5599	8798	4117			17.59	Si
SLV 2	1.39	-5948	-704	-1885.98		14277	1.3887	11189	4661			6.62	Si
SLV 2	3.27	-3181	-965	-531.1		6798	1.5599	9693	4536			4.7	Si
SLV 2	5.15	-1163	-66	-1.7		2486	1.5599	8830	4132			62.72	Si
SLV 16	1.39	-4863	1164	1118.05		10392	1.5599	10412	4873			4.18	Si
SLV 16	3.27	-4460	1421	-903.29		9531	1.5599	10240	4792			3.37	Si
SLV 16	5.15	-1132	176	-183.77		2420	1.5599	8817	4126			23.42	Si
SLV 3	1.39	-6931	-1161	-2028.96		15806	1.4617	11495	5041			4.34	Si
SLV 3	3.27	-3653	-1453	-637.04		7807	1.5599	9895	4631			3.19	Si
SLV 3	5.15	-1208	-124	4.11		2580	1.5599	8849	4141			33.46	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.27 Wa 0.05 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 6	143750	0.48	6224	-2913	236.7	414.63	1.75	Si
SLV 5	143750	0.48	6224	-2913	236.7	414.63	1.75	Si
SLV 10	143750	0.48	6741	-3155	236.7	447.09	1.89	Si
SLV 9	143750	0.48	6741	-3155	236.7	447.09	1.89	Si
SLV 1	143750	0.48	6798	-3181	236.7	450.62	1.9	Si
SLV 2	143750	0.48	6798	-3181	236.7	450.62	1.9	Si
SLV 3	143750	0.48	7807	-3653	236.7	513	2.17	Si
SLV 4	143750	0.48	7807	-3653	236.7	513	2.17	Si
SLV 14	143750	0.48	8522	-3988	236.7	556.49	2.35	Si
SLV 13	143750	0.48	8522	-3988	236.7	556.49	2.35	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.27 Wa = 0.05 Ta = 0.0787

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	a0*	aLim	Verifica
SLV 6	-1085	-4077	-110	0.022	386.8	0.892	0.36384	10.142	No
SLV 5	-1085	-4077	-110	0.022	386.8	0.892	0.36384	10.142	No
SLV 12	-1210	-6734	109	0.024	397.5	0.891	0.38522	10.142	No
SLV 11	-1210	-6734	109	0.024	397.5	0.891	0.38522	10.142	No
SLV 2	-1163	-5948	-98	0.027	393.4	0.891	0.44269	8.41479	No
SLV 1	-1163	-5948	-98	0.027	393.4	0.891	0.44269	8.41479	No
SLV 15	-1132	-4863	97	0.027	390.8	0.892	0.44817	8.41479	No
SLV 16	-1132	-4863	97	0.027	390.8	0.892	0.44817	8.41479	No
SLV 9	-1063	-3457	-67	0.038	384.9	0.893	0.62375	10.142	No
SLV 10	-1063	-3457	-67	0.038	384.9	0.893	0.62375	10.142	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	3.159	SLU 40	Si
V_SLU	5.673	SLU 40	Si
PF_SLV	2.204	SLV 1	Si
V_SLV	2.46	SLV 13	Si
PFFP_SLV	1.752	SLV 5	Si
R_SLV	0.036	SLV 5	No

## Maschio 31

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)



## Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-26.838	-2.254	-26.838	-0.614	L2	L3	1.64	0.14	3.76	3.76	3.76			

## Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	τ0	fv0	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

## Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 1	1.39	-7771	897.19	33845	3724.53	4.151	Si
SLU 1	3.27	-6424	983.44	27980	3458.43	3.517	Si
SLU 1	5.15	-3748	3718.2	0	0	0	No, e>l/2
SLU 57	1.39	-17349	2213.25	75562	1029.78	0.465	No, M>Mu
SLU 57	3.27	-15322	2684.89	66734	2271.11	0.846	No, M>Mu
SLU 57	5.15	-9747	9678.73	0	0	0	No, e>l/2
SLU 61	1.39	-21071	2778.29	91771	0	0	No, Rottura per schiacciamento
SLU 61	3.27	-18818	3368.99	81958	0	0	No, Rottura per schiacciamento
SLU 61	5.15	-12174	12090.7	0	0	0	No, e>l/2
SLU 59	1.39	-17349	2213.25	75562	1029.78	0.465	No, M>Mu
SLU 59	3.27	-15322	2684.89	66734	2271.11	0.846	No, M>Mu
SLU 59	5.15	-9747	9678.73	0	0	0	No, e>l/2
SLU 56	1.39	-17595	2305.94	76633	854.71	0.371	No, M>Mu
SLU 56	3.27	-15395	2659.78	67051	2232.73	0.839	No, M>Mu
SLU 56	5.15	-9766	9696.27	0	0	0	No, e>l/2
SLU 54	1.39	-17349	2213.25	75562	1029.78	0.465	No, M>Mu
SLU 54	3.27	-15322	2684.89	66734	2271.11	0.846	No, M>Mu
SLU 54	5.15	-9747	9678.73	0	0	0	No, e>l/2
SLU 53	1.39	-17595	2305.94	76633	854.71	0.371	No, M>Mu
SLU 53	3.27	-15395	2659.78	67051	2232.73	0.839	No, M>Mu
SLU 53	5.15	-9766	9696.27	0	0	0	No, e>l/2
SLU 60	1.39	-21316	2870.98	92842	0	0	No, Rottura per schiacciamento
SLU 60	3.27	-18890	3343.88	82275	0	0	No, Rottura per schiacciamento
SLU 60	5.15	-12194	12108.24	0	0	0	No, e>l/2
SLU 55	1.39	-17185	2151.45	74848	1143.55	0.532	No, M>Mu
SLU 55	3.27	-15273	2701.63	66522	2296.45	0.85	No, M>Mu
SLU 55	5.15	-9734	9667.03	0	0	0	No, e>l/2
SLU 58	1.39	-17595	2305.94	76633	854.71	0.371	No, M>Mu
SLU 58	3.27	-15395	2659.78	67051	2232.73	0.839	No, M>Mu
SLU 58	5.15	-9766	9696.27	0	0	0	No, e>l/2

## Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γM = 2

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLV 1	1.39	-18063	3011.3	78671	5275.08	1.752	Si
SLV 1	3.27	-10950	569.85	47693	5474.4	9.607	Si
SLV 1	5.15	-6294	6370.08	0	0	0	No, e>l/2
SLV 6	1.39	-12626	-904.48	54992	5693.75	6.295	Si
SLV 6	3.27	-8694	2030.59	37866	4919.79	2.423	Si
SLV 6	5.15	-6479	6617.9	0	0	0	No, e>l/2
SLV 9	1.39	-8404	-2412.13	36602	4826.82	2.001	Si
SLV 9	3.27	-7662	2803.57	33373	4567.04	1.629	Si
SLV 9	5.15	-6384	6479.48	0	0	0	No, e>l/2
SLV 10	1.39	-8404	-2412.13	36602	4826.82	2.001	Si
SLV 10	3.27	-7662	2803.57	33373	4567.04	1.629	Si
SLV 10	5.15	-6384	6479.48	0	0	0	No, e>l/2
SLV 3	1.39	-18500	4860.03	80576	5166.25	1.063	Si
SLV 3	3.27	-11852	90.77	51622	5612.89	61.839	Si
SLV 3	5.15	-6040	6019.24	0	0	0	No, e>l/2
SLV 5	1.39	-12626	-904.48	54992	5693.75	6.295	Si
SLV 5	3.27	-8694	2030.59	37866	4919.79	2.423	Si
SLV 5	5.15	-6479	6617.9	0	0	0	No, e>l/2
SLV 8	1.39	-14085	5257.94	61344	5751.02	1.094	Si
SLV 8	3.27	-11701	433.64	50965	5593.03	12.898	Si
SLV 8	5.15	-5633	5448.44	0	0	0	No, e>l/2
SLV 4	1.39	-18500	4860.03	80576	5166.25	1.063	Si
SLV 4	3.27	-11852	90.77	51622	5612.89	61.839	Si
SLV 4	5.15	-6040	6019.24	0	0	0	No, e>l/2
SLV 7	1.39	-14085	5257.94	61344	5751.02	1.094	Si
SLV 7	3.27	-11701	433.64	50965	5593.03	12.898	Si
SLV 7	5.15	-5633	5448.44	0	0	0	No, e>l/2
SLV 2	1.39	-18063	3011.3	78671	5275.08	1.752	Si
SLV 2	3.27	-10950	569.85	47693	5474.4	9.607	Si
SLV 2	5.15	-6294	6370.08	0	0	0	No, e>l/2

## Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche, γM = 3

Comb.	Quota	N	V par	M	σ0	σN	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 1	1.39	-7771	-206	897.19		33845	1.64	10068	2312			11.2	Si
SLU 1	3.27	-6424	-286	983.44		27980	1.64	9286	2132			7.46	Si
SLU 1	5.15	-3748	-626	3718.2		0	0	5556	0			0	No, Vu<V
SLU 57	1.39	-17349	-519	2213.25		75562	1.64	10833	2487			4.8	Si
SLU 57	3.27	-15322	-705	2684.89		66734	1.64	10833	2487			3.53	Si
SLU 57	5.15	-9747	-1648	9678.73		0	0	5556	0			0	No, Vu<V
SLU 56	1.39	-17595	-530	2305.94		76633	1.64	10833	2487			4.7	Si



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 56	3.27	-15395	-718	2659.78		67051	1.64	10833	2487			3.46	Si
SLU 56	5.15	-9766	-1667	9696.27		0	0	5556	0			0	No, Vu<V
SLU 55	1.39	-17185	-511	2151.45		74848	1.64	10833	2487			4.87	Si
SLU 55	3.27	-15273	-697	2701.63		66522	1.64	10833	2487			3.57	Si
SLU 55	5.15	-9734	-1635	9667.03		0	0	5556	0			0	No, Vu<V
SLU 58	1.39	-17595	-530	2305.94		76633	1.64	10833	2487			4.7	Si
SLU 58	3.27	-15395	-718	2659.78		67051	1.64	10833	2487			3.46	Si
SLU 58	5.15	-9766	-1667	9696.27		0	0	5556	0			0	No, Vu<V
SLU 59	1.39	-17349	-519	2213.25		75562	1.64	10833	2487			4.8	Si
SLU 59	3.27	-15322	-705	2684.89		66734	1.64	10833	2487			3.53	Si
SLU 59	5.15	-9747	-1648	9678.73		0	0	5556	0			0	No, Vu<V
SLU 54	1.39	-17349	-519	2213.25		75562	1.64	10833	2487			4.8	Si
SLU 54	3.27	-15322	-705	2684.89		66734	1.64	10833	2487			3.53	Si
SLU 54	5.15	-9747	-1648	9678.73		0	0	5556	0			0	No, Vu<V
SLU 60	1.39	-21316	-660	2870.98		92842	1.64	10833	2487			3.77	Si
SLU 60	3.27	-18890	-891	3343.88		82275	1.64	10833	2487			2.79	Si
SLU 60	5.15	-12194	-2090	12108.24		0	0	5556	0			0	No, Vu<V
SLU 53	1.39	-17595	-530	2305.94		76633	1.64	10833	2487			4.7	Si
SLU 53	3.27	-15395	-718	2659.78		67051	1.64	10833	2487			3.46	Si
SLU 53	5.15	-9766	-1667	9696.27		0	0	5556	0			0	No, Vu<V
SLU 61	1.39	-21071	-649	2778.29		91771	1.64	10833	2487			3.83	Si
SLU 61	3.27	-18818	-878	3368.99		81958	1.64	10833	2487			2.83	Si
SLU 61	5.15	-12174	-2071	12090.7		0	0	5556	0			0	No, Vu<V

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 8	1.39	-14085	2389	5257.94		75074	1.3401	16250	3049			1.28	Si
SLV 8	3.27	-11701	1914	433.64		50965	1.64	16250	3731			1.95	Si
SLV 8	5.15	-5633	203	5448.44		0	0	8333	0			0	No, Vu<V
SLV 4	1.39	-18500	389	4860.03		80576	1.64	16250	3731			9.59	Si
SLV 4	3.27	-11852	-47	90.77		51622	1.64	16250	3731			79.58	Si
SLV 4	5.15	-6040	-1764	6019.24		0	0	8333	0			0	No, Vu<V
SLV 7	1.39	-14085	2389	5257.94		75074	1.3401	16250	3049			1.28	Si
SLV 7	3.27	-11701	1914	433.64		50965	1.64	16250	3731			1.95	Si
SLV 7	5.15	-5633	203	5448.44		0	0	8333	0			0	No, Vu<V
SLV 2	1.39	-18063	-1261	3011.3		78671	1.64	16250	3731			2.96	Si
SLV 2	3.27	-10950	-1525	569.85		47693	1.64	16250	3731			2.45	Si
SLV 2	5.15	-6294	-2718	6370.08		0	0	8333	0			0	No, Vu<V
SLV 5	1.39	-12626	-3112	-904.48		54992	1.64	16250	3731			1.2	Si
SLV 5	3.27	-8694	-3013	2030.59		37866	1.64	15907	3652			1.21	Si
SLV 5	5.15	-6479	-2976	6617.9		0	0	8333	0			0	No, Vu<V
SLV 3	1.39	-18500	389	4860.03		80576	1.64	16250	3731			9.59	Si
SLV 3	3.27	-11852	-47	90.77		51622	1.64	16250	3731			79.58	Si
SLV 3	5.15	-6040	-1764	6019.24		0	0	8333	0			0	No, Vu<V
SLV 6	1.39	-12626	-3112	-904.48		54992	1.64	16250	3731			1.2	Si
SLV 6	3.27	-8694	-3013	2030.59		37866	1.64	15907	3652			1.21	Si
SLV 6	5.15	-6479	-2976	6617.9		0	0	8333	0			0	No, Vu<V
SLV 1	1.39	-18063	-1261	3011.3		78671	1.64	16250	3731			2.96	Si
SLV 1	3.27	-10950	-1525	569.85		47693	1.64	16250	3731			2.45	Si
SLV 1	5.15	-6294	-2718	6370.08		0	0	8333	0			0	No, Vu<V
SLV 10	1.39	-8404	-3048	-2412.13		37542	1.5989	15842	3546			1.16	Si
SLV 10	3.27	-7662	-2810	2803.57		40175	1.3623	16250	3099			1.1	Si
SLV 10	5.15	-6384	-2244	6479.48		0	0	8333	0			0	No, Vu<V
SLV 9	1.39	-8404	-3048	-2412.13		37542	1.5989	15842	3546			1.16	Si
SLV 9	3.27	-7662	-2810	2803.57		40175	1.3623	16250	3099			1.1	Si
SLV 9	5.15	-6384	-2244	6479.48		0	0	8333	0			0	No, Vu<V

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.27  $W_a$  0.03 denominatore 8  $\gamma_M = 2$

Comb.	f <sub>d</sub>	S <sub>a</sub>	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 13	143750	0.48	32715	-7511	116.13	385.02	3.32	Si
SLV 14	143750	0.48	32715	-7511	116.13	385.02	3.32	Si
SLV 10	143750	0.48	33373	-7662	116.13	389.87	3.36	Si
SLV 9	143750	0.48	33373	-7662	116.13	389.87	3.36	Si
SLV 15	143750	0.48	36644	-8414	116.13	412.32	3.55	Si
SLV 16	143750	0.48	36644	-8414	116.13	412.32	3.55	Si
SLV 6	143750	0.48	37866	-8694	116.13	419.98	3.62	Si
SLV 5	143750	0.48	37866	-8694	116.13	419.98	3.62	Si
SLV 12	143750	0.48	46471	-10670	116.13	462.82	3.99	Si
SLV 11	143750	0.48	46471	-10670	116.13	462.82	3.99	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.27  $W_a = 0.03$   $T_a = 0.1686$

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	$\alpha_0^*$	aLim	Verifica
SLV 1	-6294	-18063	-17	0.018	762.7	0.953	0.27929	2.39674	No
SLV 2	-6294	-18063	-17	0.018	762.7	0.953	0.27929	2.39674	No
SLV 6	-6479	-12626	-16	0.018	781.5	0.954	0.27966	2.39674	No
SLV 5	-6479	-12626	-16	0.018	781.5	0.954	0.27966	2.39674	No
SLV 4	-6040	-18500	-14	0.019	736.9	0.952	0.2857	2.39674	No
SLV 3	-6040	-18500	-14	0.019	736.9	0.952	0.2857	2.39674	No
SLV 10	-6384	-8404	-13	0.019	771.8	0.954	0.28609	2.39674	No
SLV 9	-6384	-8404	-13	0.019	771.8	0.954	0.28609	2.39674	No
SLV 14	-5977	-3988	-7	0.02	730.5	0.952	0.30204	2.39674	No
SLV 13	-5977	-3988	-7	0.02	730.5	0.952	0.30204	2.39674	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
--------------	----------	-------	----------



Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	0	SLU 1	No
V_SLU	0	SLU 1	No
PF_SLV	0	SLV 1	No
V_SLV	0	SLV 1	No
PFFP_SLV	3.315	SLV 13	Si
R_SLV	0.117	SLV 1	No

## Maschio 32

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-25.983	-0.614	-26.838	-0.614	L2	L3	0.855	0.14	3.76	3.76	3.76			

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	τ0	fv0	μ	φ	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, γM = 3

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLU 61	1.39	-11171	1252.09	93332	0	0	No, Rottura per schiacciamento
SLU 61	3.27	-11843	1092.52	98944	0	0	No, Rottura per schiacciamento
SLU 61	5.15	-10977	12320.23	0	0	0	No, e>l/2
SLU 55	1.39	-9107	962.43	76085	256.79	0.267	No, M>Mu
SLU 55	3.27	-9437	920.82	78844	129.45	0.141	No, M>Mu
SLU 55	5.15	-8779	9869.4	0	0	0	No, e>l/2
SLU 59	1.39	-9126	1020.88	76241	249.87	0.245	No, M>Mu
SLU 59	3.27	-9571	884.61	79963	75.1	0.085	No, M>Mu
SLU 59	5.15	-8789	9867.68	0	0	0	No, e>l/2
SLU 53	1.39	-9154	1108.55	76474	239.45	0.216	No, M>Mu
SLU 53	3.27	-9772	830.3	81641	0	0	No, Rottura per schiacciamento
SLU 53	5.15	-8804	9865.1	0	0	0	No, e>l/2
SLU 60	1.39	-11199	1339.75	93564	0	0	No, Rottura per schiacciamento
SLU 60	3.27	-12044	1038.2	100622	0	0	No, Rottura per schiacciamento
SLU 60	5.15	-10991	12317.65	0	0	0	No, e>l/2
SLU 57	1.39	-9126	1020.88	76241	249.87	0.245	No, M>Mu
SLU 57	3.27	-9571	884.61	79963	75.1	0.085	No, M>Mu
SLU 57	5.15	-8789	9867.68	0	0	0	No, e>l/2
SLU 1	1.39	-3862	495.99	32264	997	2.01	Si
SLU 1	3.27	-3992	316.26	33350	1007.8	3.187	Si
SLU 1	5.15	-3379	3785.23	0	0	0	No, e>l/2
SLU 54	1.39	-9126	1020.88	76241	249.87	0.245	No, M>Mu
SLU 54	3.27	-9571	884.61	79963	75.1	0.085	No, M>Mu
SLU 54	5.15	-8789	9867.68	0	0	0	No, e>l/2
SLU 58	1.39	-9154	1108.55	76474	239.45	0.216	No, M>Mu
SLU 58	3.27	-9772	830.3	81641	0	0	No, Rottura per schiacciamento
SLU 58	5.15	-8804	9865.1	0	0	0	No, e>l/2
SLU 56	1.39	-9154	1108.55	76474	239.45	0.216	No, M>Mu
SLU 56	3.27	-9772	830.3	81641	0	0	No, Rottura per schiacciamento
SLU 56	5.15	-8804	9865.1	0	0	0	No, e>l/2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, γM = 2

Comb.	Quota	N	M	σ0	Mu	c.s.	Verifica
SLV 5	1.39	-4935	478.52	41229	1397.77	2.921	Si
SLV 5	3.27	-5288	454.18	44175	1443.15	3.178	Si
SLV 5	5.15	-4839	5724.38	0	0	0	No, e>l/2
SLV 10	1.39	-4357	-983.97	36402	1307.7	1.329	Si
SLV 10	3.27	-1957	1349.83	0	0	0	No, e>l/2
SLV 10	5.15	-4733	5943.05	0	0	0	No, e>l/2
SLV 2	1.39	-6388	2860.93	0	0	0	No, e>l/2
SLV 2	3.27	-10911	-865.28	91154	1184.6	1.369	Si
SLV 2	5.15	-5403	5633.87	0	0	0	No, e>l/2
SLV 8	1.39	-7161	2410.44	59827	1562.34	0.648	No, M>Mu
SLV 8	3.27	-10253	-330.19	85656	1310.36	3.969	Si
SLV 8	5.15	-6099	6194.68	0	0	0	No, e>l/2
SLV 4	1.39	-7056	3440.5	0	0	0	No, e>l/2
SLV 4	3.27	-12400	-1100.59	103599	806.45	0.733	No, M>Mu
SLV 4	5.15	-5781	5774.96	0	0	0	No, e>l/2
SLV 1	1.39	-6388	2860.93	0	0	0	No, e>l/2
SLV 1	3.27	-10911	-865.28	91154	1184.6	1.369	Si
SLV 1	5.15	-5403	5633.87	0	0	0	No, e>l/2
SLV 7	1.39	-7161	2410.44	59827	1562.34	0.648	No, M>Mu
SLV 7	3.27	-10253	-330.19	85656	1310.36	3.969	Si
SLV 7	5.15	-6099	6194.68	0	0	0	No, e>l/2
SLV 3	1.39	-7056	3440.5	0	0	0	No, e>l/2
SLV 3	3.27	-12400	-1100.59	103599	806.45	0.733	No, M>Mu
SLV 3	5.15	-5781	5774.96	0	0	0	No, e>l/2



Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 9	1.39	-4357	-983.97	36402	1307.7	1.329	Si
SLV 9	3.27	-1957	1349.83	0	0	0	No, $e>l/2$
SLV 9	5.15	-4733	5943.05	0	0	0	No, $e>l/2$
SLV 6	1.39	-4935	478.52	41229	1397.77	2.921	Si
SLV 6	3.27	-5288	454.18	44175	1443.15	3.178	Si
SLV 6	5.15	-4839	5724.38	0	0	0	No, $e>l/2$

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt <sub>lim</sub>	c.s.	Verifica
SLU 60	1.39	-11199	478	1339.75		93564	0.855	10833	1297			2.71	Si
SLU 60	3.27	-12044	452	1038.2		100622	0.855	10833	1297			2.87	Si
SLU 60	5.15	-10991	-9870	12317.65		0	0	5556	0			0	No, $V_u < V$
SLU 55	1.39	-9107	219	962.43		76085	0.855	10833	1297			5.91	Si
SLU 55	3.27	-9437	198	920.82		78844	0.855	10833	1297			6.55	Si
SLU 55	5.15	-8779	-7986	9869.4		0	0	5556	0			0	No, $V_u < V$
SLU 59	1.39	-9126	296	1020.88		76241	0.855	10833	1297			4.38	Si
SLU 59	3.27	-9571	275	884.61		79963	0.855	10833	1297			4.72	Si
SLU 59	5.15	-8789	-7952	9867.68		0	0	5556	0			0	No, $V_u < V$
SLU 56	1.39	-9154	411	1108.55		76474	0.855	10833	1297			3.16	Si
SLU 56	3.27	-9772	389	830.3		81641	0.855	10833	1297			3.33	Si
SLU 56	5.15	-8804	-7901	9865.1		0	0	5556	0			0	No, $V_u < V$
SLU 53	1.39	-9154	411	1108.55		76474	0.855	10833	1297			3.16	Si
SLU 53	3.27	-9772	389	830.3		81641	0.855	10833	1297			3.33	Si
SLU 53	5.15	-8804	-7901	9865.1		0	0	5556	0			0	No, $V_u < V$
SLU 58	1.39	-9154	411	1108.55		76474	0.855	10833	1297			3.16	Si
SLU 58	3.27	-9772	389	830.3		81641	0.855	10833	1297			3.33	Si
SLU 58	5.15	-8804	-7901	9865.1		0	0	5556	0			0	No, $V_u < V$
SLU 61	1.39	-11171	363	1252.09		93332	0.855	10833	1297			3.57	Si
SLU 61	3.27	-11843	337	1092.52		98944	0.855	10833	1297			3.85	Si
SLU 61	5.15	-10977	-9921	12320.23		0	0	5556	0			0	No, $V_u < V$
SLU 57	1.39	-9126	296	1020.88		76241	0.855	10833	1297			4.38	Si
SLU 57	3.27	-9571	275	884.61		79963	0.855	10833	1297			4.72	Si
SLU 57	5.15	-8789	-7952	9867.68		0	0	5556	0			0	No, $V_u < V$
SLU 1	1.39	-3862	214	495.99		32264	0.855	9857	1180			5.51	Si
SLU 1	3.27	-3992	205	316.26		33350	0.855	10002	1197			5.83	Si
SLU 1	5.15	-3379	-3024	3785.23		0	0	5556	0			0	No, $V_u < V$
SLU 54	1.39	-9126	296	1020.88		76241	0.855	10833	1297			4.38	Si
SLU 54	3.27	-9571	275	884.61		79963	0.855	10833	1297			4.72	Si
SLU 54	5.15	-8789	-7952	9867.68		0	0	5556	0			0	No, $V_u < V$

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt <sub>lim</sub>	c.s.	Verifica
SLV 3	1.39	-7056	3611	3440.5		0	0	8333	0			0	No, $V_u < V$
SLV 3	3.27	-12400	3503	-1100.59		103599	0.855	16250	1945			0.56	No, $V_u < V$
SLV 3	5.15	-5781	-3937	5774.96		0	0	8333	0			0	No, $V_u < V$
SLV 9	1.39	-4357	-689	-983.97		51445	0.605	16250	1376			2	Si
SLV 9	3.27	-1957	-1211	1349.83		0	0	8333	0			0	No, $V_u < V$
SLV 9	5.15	-4733	-4231	5943.05		0	0	8333	0			0	No, $V_u < V$
SLV 2	1.39	-6388	3631	2860.93		0	0	8333	0			0	No, $V_u < V$
SLV 2	3.27	-10911	3171	-865.28		91154	0.855	16250	1945			0.61	No, $V_u < V$
SLV 2	5.15	-5403	-3342	5633.87		0	0	8333	0			0	No, $V_u < V$
SLV 5	1.39	-4935	1316	478.52		41229	0.855	16250	1945			1.48	Si
SLV 5	3.27	-5288	633	454.18		44175	0.855	16250	1945			3.07	Si
SLV 5	5.15	-4839	-3500	5724.38		0	0	8333	0			0	No, $V_u < V$
SLV 6	1.39	-4935	1316	478.52		41229	0.855	16250	1945			1.48	Si
SLV 6	3.27	-5288	633	454.18		44175	0.855	16250	1945			3.07	Si
SLV 6	5.15	-4839	-3500	5724.38		0	0	8333	0			0	No, $V_u < V$
SLV 10	1.39	-4357	-689	-983.97		51445	0.605	16250	1376			2	Si
SLV 10	3.27	-1957	-1211	1349.83		0	0	8333	0			0	No, $V_u < V$
SLV 10	5.15	-4733	-4231	5943.05		0	0	8333	0			0	No, $V_u < V$
SLV 1	1.39	-6388	3631	2860.93		0	0	8333	0			0	No, $V_u < V$
SLV 1	3.27	-10911	3171	-865.28		91154	0.855	16250	1945			0.61	No, $V_u < V$
SLV 1	5.15	-5403	-3342	5633.87		0	0	8333	0			0	No, $V_u < V$
SLV 4	1.39	-7056	3611	3440.5		0	0	8333	0			0	No, $V_u < V$
SLV 4	3.27	-12400	3503	-1100.59		103599	0.855	16250	1945			0.56	No, $V_u < V$
SLV 4	5.15	-5781	-3937	5774.96		0	0	8333	0			0	No, $V_u < V$
SLV 8	1.39	-7161	1247	2410.44		187613	0.2726	16250	620			0.5	No, $V_u < V$
SLV 8	3.27	-10253	1741	-330.19		85656	0.855	16250	1945			1.12	Si
SLV 8	5.15	-6099	-5485	6194.68		0	0	8333	0			0	No, $V_u < V$
SLV 7	1.39	-7161	1247	2410.44		187613	0.2726	16250	620			0.5	No, $V_u < V$
SLV 7	3.27	-10253	1741	-330.19		85656	0.855	16250	1945			1.12	Si
SLV 7	5.15	-6099	-5485	6194.68		0	0	8333	0			0	No, $V_u < V$

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.27  $W_a$  0.03 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 13	143750	0.48	0	190	60.54	0	0	No, Trazione
SLV 14	143750	0.48	0	190	60.54	0	0	No, Trazione
SLV 16	143750	0.48	10854	-1299	60.54	82.86	1.37	Si
SLV 15	143750	0.48	10854	-1299	60.54	82.86	1.37	Si
SLV 9	143750	0.48	16352	-1957	60.54	118.67	1.96	Si
SLV 10	143750	0.48	16352	-1957	60.54	118.67	1.96	Si
SLV 3	143750	0.48	103599	-12400	60.54	132.05	2.18	Si
SLV 4	143750	0.48	103599	-12400	60.54	132.05	2.18	Si
SLV 2	143750	0.48	91154	-10911	60.54	193.98	3.2	Si
SLV 1	143750	0.48	91154	-10911	60.54	193.98	3.2	Si



## Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.27 Wa = 0.03 Ta = 0.1686

Comb.	N top	N base	V orto	$\alpha 0$	M*	e*	a0*	aLim	Verifica
SLV 16	-5429	-5130	84	0.006	616.1	0.969	0.0835	2.39674	No
SLV 15	-5429	-5130	84	0.006	616.1	0.969	0.0835	2.39674	No
SLV 11	-5994	-6583	78	0.008	673.6	0.971	0.11441	2.39674	No
SLV 12	-5994	-6583	78	0.008	673.6	0.971	0.11441	2.39674	No
SLV 13	-5051	-4462	64	0.008	577.6	0.967	0.12377	2.39674	No
SLV 14	-5051	-4462	64	0.008	577.6	0.967	0.12377	2.39674	No
SLV 7	-6099	-7161	53	0.012	684.3	0.972	0.17357	2.39674	No
SLV 8	-6099	-7161	53	0.012	684.3	0.972	0.17357	2.39674	No
SLV 2	-5403	-6388	-18	0.017	613.4	0.969	0.25293	2.39674	No
SLV 1	-5403	-6388	-18	0.017	613.4	0.969	0.25293	2.39674	No

## Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	0	SLU 1	No
V_SLU	0	SLU 1	No
PF_SLV	0	SLV 14	No
V_SLV	0	SLV 1	No
PFFP_SLV	0	SLV 14	No
R_SLV	0.035	SLV 15	No

## Maschio 33

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-24.603	-0.614	-25.183	-0.614	L2	L3	0.58	0.14	3.76	3.76	3.76			

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	t0	fv0	$\mu$	$\phi$	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma 0$	Mu	c.s.	Verifica
SLU 1	1.39	-145	-119.81	0	0	0	No, e>l/2
SLU 1	3.27	-836	143.81	10300	211.9	1.473	Si
SLU 1	5.15	-2	-241.4	0	0	0	No, e>l/2
SLU 61	1.39	203	-305.37	0	0	0	No, Trazione
SLU 61	3.27	-2094	431.7	25781	415	0.961	No, M>Mu
SLU 61	5.15	-21	-780.65	0	0	0	No, e>l/2
SLU 55	1.39	181	-288.87	0	0	0	No, Trazione
SLU 55	3.27	-1892	374.99	23300	391.77	1.045	Si
SLU 55	5.15	-23	-617.43	0	0	0	No, e>l/2
SLU 60	1.39	92	-271.69	0	0	0	No, Trazione
SLU 60	3.27	-1961	407.04	24147	400.11	0.983	No, M>Mu
SLU 60	5.15	-12	-789.09	0	0	0	No, e>l/2
SLU 59	1.39	107	-266.42	0	0	0	No, Trazione
SLU 59	3.27	-1804	358.55	22210	380.45	1.061	Si
SLU 59	5.15	-18	-623.05	0	0	0	No, e>l/2
SLU 58	1.39	-4	-232.74	0	0	0	No, e>l/2
SLU 58	3.27	-1671	333.9	20576	362.18	1.085	Si
SLU 58	5.15	-9	-631.49	0	0	0	No, e>l/2
SLU 54	1.39	107	-266.42	0	0	0	No, Trazione
SLU 54	3.27	-1804	358.55	22210	380.45	1.061	Si
SLU 54	5.15	-18	-623.05	0	0	0	No, e>l/2
SLU 57	1.39	107	-266.42	0	0	0	No, Trazione
SLU 57	3.27	-1804	358.55	22210	380.45	1.061	Si
SLU 57	5.15	-18	-623.05	0	0	0	No, e>l/2
SLU 53	1.39	-4	-232.74	0	0	0	No, e>l/2
SLU 53	3.27	-1671	333.9	20576	362.18	1.085	Si
SLU 53	5.15	-9	-631.49	0	0	0	No, e>l/2
SLU 56	1.39	-4	-232.74	0	0	0	No, e>l/2
SLU 56	3.27	-1671	333.9	20576	362.18	1.085	Si
SLU 56	5.15	-9	-631.49	0	0	0	No, e>l/2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma 0$	Mu	c.s.	Verifica
SLV 9	1.39	2028	-773.99	0	0	0	No, Trazione
SLV 9	3.27	-3720	692.01	45815	674.41	0.975	No, M>Mu
SLV 9	5.15	-14	-161.97	0	0	0	No, e>l/2
SLV 5	1.39	200	-224.77	0	0	0	No, Trazione
SLV 5	3.27	-1426	280.24	17563	354.16	1.264	Si
SLV 5	5.15	9	-276.62	0	0	0	No, Trazione
SLV 4	1.39	-3442	860.6	42388	651.96	0.758	No, M>Mu
SLV 4	3.27	3156	-556.07	0	0	0	No, Trazione
SLV 4	5.15	33	-629.96	0	0	0	No, Trazione
SLV 8	1.39	-2123	459.26	26142	483.94	1.054	Si
SLV 8	3.27	1506	-267.32	0	0	0	No, Trazione
SLV 8	5.15	4	-614.42	0	0	0	No, Trazione
SLV 10	1.39	2028	-773.99	0	0	0	No, Trazione
SLV 10	3.27	-3720	692.01	45815	674.41	0.975	No, M>Mu



Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 10	5.15	-14	-161.97	0	0	0	No, e>l/2
SLV 7	1.39	-2123	459.26	26142	483.94	1.054	Si
SLV 7	3.27	1506	-267.32	0	0	0	No, Trazione
SLV 7	5.15	4	-614.42	0	0	0	No, Trazione
SLV 6	1.39	200	-224.77	0	0	0	No, Trazione
SLV 6	3.27	-1426	280.24	17563	354.16	1.264	Si
SLV 6	5.15	9	-276.62	0	0	0	No, Trazione
SLV 3	1.39	-3442	860.6	42388	651.96	0.758	No, M>Mu
SLV 3	3.27	3156	-556.07	0	0	0	No, Trazione
SLV 3	5.15	33	-629.96	0	0	0	No, Trazione
SLV 1	1.39	-2745	655.39	33807	575.89	0.879	No, M>Mu
SLV 1	3.27	2277	-391.8	0	0	0	No, Trazione
SLV 1	5.15	35	-528.62	0	0	0	No, Trazione
SLV 2	1.39	-2745	655.39	33807	575.89	0.879	No, M>Mu
SLV 2	3.27	2277	-391.8	0	0	0	No, Trazione
SLV 2	5.15	35	-528.62	0	0	0	No, Trazione

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 58	1.39	-4	-618	-232.74	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 58	3.27	-1671	-616	333.9	44112	0.2706	10833	410	0	0.67	0	0	No, Vu<V
SLU 58	5.15	-9	2228	-631.49	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 57	1.39	107	-687	-266.42	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 57	3.27	-1804	-683	358.55	47078	0.2737	10833	415	0	0.61	0	0	No, Vu<V
SLU 57	5.15	-18	2194	-623.05	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 55	1.39	181	-733	-288.87	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 55	3.27	-1892	-727	374.99	49061	0.2755	10833	418	0	0.57	0	0	No, Vu<V
SLU 55	5.15	-23	2172	-617.43	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 61	1.39	203	-807	-305.37	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 61	3.27	-2094	-802	431.7	59472	0.2514	10833	381	0	0.48	0	0	No, Vu<V
SLU 61	5.15	-21	2752	-780.65	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 60	1.39	92	-738	-271.69	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 60	3.27	-1961	-735	407.04	56635	0.2473	10833	375	0	0.51	0	0	No, Vu<V
SLU 60	5.15	-12	2785	-789.09	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 1	1.39	-145	-292	-119.81	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 1	3.27	-836	-291	143.81	16866	0.3542	7804	387	0	1.33	0	0	Si
SLU 1	5.15	-2	850	-241.4	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 59	1.39	107	-687	-266.42	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 59	3.27	-1804	-683	358.55	47078	0.2737	10833	415	0	0.61	0	0	No, Vu<V
SLU 59	5.15	-18	2194	-623.05	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 54	1.39	107	-687	-266.42	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 54	3.27	-1804	-683	358.55	47078	0.2737	10833	415	0	0.61	0	0	No, Vu<V
SLU 54	5.15	-18	2194	-623.05	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 53	1.39	-4	-618	-232.74	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 53	3.27	-1671	-616	333.9	44112	0.2706	10833	410	0	0.67	0	0	No, Vu<V
SLU 53	5.15	-9	2228	-631.49	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 56	1.39	-4	-618	-232.74	0	0	0	5556	0	0	0	0	No, Vu<V
SLU 56	3.27	-1671	-616	333.9	44112	0.2706	10833	410	0	0.67	0	0	No, Vu<V
SLU 56	5.15	-9	2228	-631.49	0	0	0	5556	0	0	0	0	No, Vu<V

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 3	1.39	-3442	1940	860.6	204902	0.12	16250	273	0	0.14	0	0	No, Vu<V
SLV 3	3.27	3156	1450	-556.07	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 3	5.15	33	1546	-629.96	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 1	1.39	-2745	1501	655.39	127453	0.1539	16250	350	0	0.23	0	0	No, Vu<V
SLV 1	3.27	2277	1024	-391.8	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 1	5.15	35	1213	-528.62	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 7	1.39	-2123	963	459.26	68604	0.221	16250	503	0	0.52	0	0	No, Vu<V
SLV 7	3.27	1506	798	-267.32	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 7	5.15	4	1927	-614.42	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 4	1.39	-3442	1940	860.6	204902	0.12	16250	273	0	0.14	0	0	No, Vu<V
SLV 4	3.27	3156	1450	-556.07	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 4	5.15	33	1546	-629.96	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 10	1.39	2028	-1774	-773.99	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 10	3.27	-3720	-1606	692.01	85163	0.312	16250	710	0	0.44	0	0	No, Vu<V
SLV 10	5.15	-14	812	-161.97	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 5	1.39	200	-498	-224.77	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 5	3.27	-1426	-622	280.24	36311	0.2805	15596	613	0	0.99	0	0	No, Vu<V
SLV 5	5.15	9	818	-276.62	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 2	1.39	-2745	1501	655.39	127453	0.1539	16250	350	0	0.23	0	0	No, Vu<V
SLV 2	3.27	2277	1024	-391.8	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 2	5.15	35	1213	-528.62	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 8	1.39	-2123	963	459.26	68604	0.221	16250	503	0	0.52	0	0	No, Vu<V
SLV 8	3.27	1506	798	-267.32	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 8	5.15	4	1927	-614.42	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 9	1.39	2028	-1774	-773.99	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 9	3.27	-3720	-1606	692.01	85163	0.312	16250	710	0	0.44	0	0	No, Vu<V
SLV 9	5.15	-14	812	-161.97	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 6	1.39	200	-498	-224.77	0	0	8333	0	0	0	0	0	No, Vu<V
SLV 6	3.27	-1426	-622	280.24	36311	0.2805	15596	613	0	0.99	0	0	No, Vu<V
SLV 6	5.15	9	818	-276.62	0	0	8333	0	0	0	0	0	No, Vu<V

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.27 Wa 0.03 denominatore 8  $\gamma_M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 4	143750	0.48	0	3156	41.07	0	0	No, Trazione
SLV 1	143750	0.48	0	2277	41.07	0	0	No, Trazione





Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 3	143750	0.48	0	3156	41.07	0	0	No, Trazione
SLV 8	143750	0.48	0	1506	41.07	0	0	No, Trazione
SLV 7	143750	0.48	0	1506	41.07	0	0	No, Trazione
SLV 2	143750	0.48	0	2277	41.07	0	0	No, Trazione
SLV 11	143750	0.48	9708	-788	41.07	50.8	1.24	Si
SLV 12	143750	0.48	9708	-788	41.07	50.8	1.24	Si
SLV 5	143750	0.48	17563	-1426	41.07	85.48	2.08	Si
SLV 6	143750	0.48	17563	-1426	41.07	85.48	2.08	Si

#### Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzera = 3.27 Wa = 0.03 Ta = 0.1686

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	a0*	aLim	Verifica
SLV 3	33	-3442	-35	0	0	0	0	2.39674	No, Trazione
SLV 7	4	-2123	-4	0	0	0	0	2.39674	No, Trazione
SLV 10	-14	2028	-7	0	0	0	0	2.39674	No, Trazione
SLV 9	-14	2028	-7	0	0	0	0	2.39674	No, Trazione
SLV 5	9	200	-27	0	0	0	0	2.39674	No, Trazione
SLV 1	35	-2745	-42	0	0	0	0	2.39674	No, Trazione
SLV 4	33	-3442	-35	0	0	0	0	2.39674	No, Trazione
SLV 8	4	-2123	-4	0	0	0	0	2.39674	No, Trazione
SLV 2	35	-2745	-42	0	0	0	0	2.39674	No, Trazione
SLV 6	9	200	-27	0	0	0	0	2.39674	No, Trazione

#### Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	0	SLU 84	No
V_SLU	0	SLU 1	No
PF_SLV	0	SLV 16	No
V_SLV	0	SLV 1	No
PFFP_SLV	0	SLV 8	No
R_SLV	0	SLV 16	No

## Maschio 34

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

#### Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	l	Sp.	h netta	h ini.	h fin.	a	a.s.sx	a.s.dx
-24.603	-3.177	-25.893	-3.854	L2	L3	1.457	0.3	3.76	3.76	3.76			

#### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	$\tau_0$	fv0	$\mu$	$\phi$	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

#### Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, $\gamma_M = 3$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 73	1.39	-3273	-42.15	7490	2164.8	51.361	Si
SLU 73	3.27	-2468	-75.28	5648	1673.03	22.225	Si
SLU 73	5.15	-1747	105.23	3998	1210.06	11.499	Si
SLU 40	1.39	-2398	-42.47	5487	1628.9	38.354	Si
SLU 40	3.27	-2190	-53.97	5011	1496.79	27.734	Si
SLU 40	5.15	-2076	124.32	4750	1423.59	11.451	Si
SLU 41	1.39	-2367	-43.59	5417	1609.55	36.921	Si
SLU 41	3.27	-2177	-53.17	4982	1488.75	27.999	Si
SLU 41	5.15	-2075	124.16	4749	1423.46	11.465	Si
SLU 39	1.39	-2367	-43.59	5417	1609.55	36.921	Si
SLU 39	3.27	-2177	-53.17	4982	1488.75	27.999	Si
SLU 39	5.15	-2075	124.16	4749	1423.46	11.465	Si
SLU 81	1.39	-3172	-48.35	7259	2104.55	43.53	Si
SLU 81	3.27	-2596	-71.66	5940	1752.84	24.46	Si
SLU 81	5.15	-2113	126.72	4836	1447.88	11.426	Si
SLU 76	1.39	-3273	-42.15	7490	2164.8	51.361	Si
SLU 76	3.27	-2468	-75.28	5648	1673.03	22.225	Si
SLU 76	5.15	-1747	105.23	3998	1210.06	11.499	Si
SLU 82	1.39	-3203	-47.22	7329	2122.9	44.954	Si
SLU 82	3.27	-2609	-72.46	5969	1760.66	24.299	Si
SLU 82	5.15	-2114	126.88	4837	1448.01	11.413	Si
SLU 84	1.39	-3203	-47.22	7329	2122.9	44.954	Si
SLU 84	3.27	-2609	-72.46	5969	1760.66	24.299	Si
SLU 84	5.15	-2114	126.88	4837	1448.01	11.413	Si
SLU 42	1.39	-2398	-42.47	5487	1628.9	38.354	Si
SLU 42	3.27	-2190	-53.97	5011	1496.79	27.734	Si
SLU 42	5.15	-2076	124.32	4750	1423.59	11.451	Si
SLU 83	1.39	-3172	-48.35	7259	2104.55	43.53	Si
SLU 83	3.27	-2596	-71.66	5940	1752.84	24.46	Si
SLU 83	5.15	-2113	126.72	4836	1447.88	11.426	Si

#### Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche, $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 2	1.39	1100	-575.48	0	0	0	No, Trazione
SLV 2	3.27	1045	2.17	0	0	0	No, Trazione
SLV 2	5.15	-860	-12.83	1968	616.32	48.042	Si
SLV 6	1.39	-1659	-1533.44	0	0	0	No, e>/2



Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 6	3.27	-788	-324.19	1802	565.18	1.743	Si
SLV 6	5.15	-801	154.36	1833	574.65	3.723	Si
SLV 3	1.39	1234	309	0	0	0	No, Trazione
SLV 3	3.27	993	188.86	0	0	0	No, Trazione
SLV 3	5.15	-897	-93.25	2052	642.29	6.888	Si
SLV 1	1.39	1100	-575.48	0	0	0	No, Trazione
SLV 1	3.27	1045	2.17	0	0	0	No, Trazione
SLV 1	5.15	-860	-12.83	1968	616.32	48.042	Si
SLV 7	1.39	-1211	1414.84	0	0	0	No, e>l/2
SLV 7	3.27	-961	298.13	2198	687.15	2.305	Si
SLV 7	5.15	-924	-113.7	2114	661.28	5.816	Si
SLV 5	1.39	-1659	-1533.44	0	0	0	No, e>l/2
SLV 5	3.27	-788	-324.19	1802	565.18	1.743	Si
SLV 5	5.15	-801	154.36	1833	574.65	3.723	Si
SLV 12	1.39	-3441	1478.21	7874	2344.78	1.586	Si
SLV 12	3.27	-2583	205.09	5911	1790.42	8.73	Si
SLV 12	5.15	-910	-50.81	2083	651.61	12.824	Si
SLV 11	1.39	-3441	1478.21	7874	2344.78	1.586	Si
SLV 11	3.27	-2583	205.09	5911	1790.42	8.73	Si
SLV 11	5.15	-910	-50.81	2083	651.61	12.824	Si
SLV 8	1.39	-1211	1414.84	0	0	0	No, e>l/2
SLV 8	3.27	-961	298.13	2198	687.15	2.305	Si
SLV 8	5.15	-924	-113.7	2114	661.28	5.816	Si
SLV 4	1.39	1234	309	0	0	0	No, Trazione
SLV 4	3.27	993	188.86	0	0	0	No, Trazione
SLV 4	5.15	-897	-93.25	2052	642.29	6.888	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLU 81	1.39	-3172	-154	-48.35		7259	1.4567	6523	2851			18.53	Si
SLU 81	3.27	-2596	-111	-71.66		5940	1.4567	6348	2774			25.06	Si
SLU 81	5.15	-2113	-2	126.72		4836	1.4567	6200	2710			1000	Si
SLU 40	1.39	-2398	-146	-42.47		5487	1.4567	6287	2748			18.84	Si
SLU 40	3.27	-2190	-105	-53.97		5011	1.4567	6224	2720			25.81	Si
SLU 40	5.15	-2076	-3	124.32		4750	1.4567	6189	2705			1000	Si
SLU 82	1.39	-3203	-150	-47.22		7329	1.4567	6533	2855			19.02	Si
SLU 82	3.27	-2609	-108	-72.46		5969	1.4567	6351	2776			25.6	Si
SLU 82	5.15	-2114	-3	126.88		4837	1.4567	6200	2710			1000	Si
SLU 84	1.39	-3203	-150	-47.22		7329	1.4567	6533	2855			19.02	Si
SLU 84	3.27	-2609	-108	-72.46		5969	1.4567	6351	2776			25.6	Si
SLU 84	5.15	-2114	-3	126.88		4837	1.4567	6200	2710			1000	Si
SLU 20	1.39	-2437	-125	-37.37		5577	1.4567	6299	2753			22.02	Si
SLU 20	3.27	-2044	-90	-53.57		4677	1.4567	6179	2700			30.03	Si
SLU 20	5.15	-1736	-1	104.04		3973	1.4567	6085	2659			1000	Si
SLU 18	1.39	-2437	-125	-37.37		5577	1.4567	6299	2753			22.02	Si
SLU 18	3.27	-2044	-90	-53.57		4677	1.4567	6179	2700			30.03	Si
SLU 18	5.15	-1736	-1	104.04		3973	1.4567	6085	2659			1000	Si
SLU 39	1.39	-2367	-150	-43.59		5417	1.4567	6278	2743			18.33	Si
SLU 39	3.27	-2177	-108	-53.17		4982	1.4567	6220	2718			25.25	Si
SLU 39	5.15	-2075	-2	124.16		4749	1.4567	6189	2704			1000	Si
SLU 42	1.39	-2398	-146	-42.47		5487	1.4567	6287	2748			18.84	Si
SLU 42	3.27	-2190	-105	-53.97		5011	1.4567	6224	2720			25.81	Si
SLU 42	5.15	-2076	-3	124.32		4750	1.4567	6189	2705			1000	Si
SLU 83	1.39	-3172	-154	-48.35		7259	1.4567	6523	2851			18.53	Si
SLU 83	3.27	-2596	-111	-71.66		5940	1.4567	6348	2774			25.06	Si
SLU 83	5.15	-2113	-2	126.72		4836	1.4567	6200	2710			1000	Si
SLU 41	1.39	-2367	-150	-43.59		5417	1.4567	6278	2743			18.33	Si
SLU 41	3.27	-2177	-108	-53.17		4982	1.4567	6220	2718			25.25	Si
SLU 41	5.15	-2075	-2	124.16		4749	1.4567	6189	2704			1000	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 11	1.39	-3441	3342	1478.21		12798	0.8963	10893	2929			0.88	No, Vu<V
SLV 11	3.27	-2583	2740	205.09		5911	1.4567	9516	4158			1.52	Si
SLV 11	5.15	-910	1097	-50.81		2083	1.4567	8750	3824			3.49	Si
SLV 4	1.39	1234	-792	309		0	0	8333	0			0	No, Vu<V
SLV 4	3.27	993	-585	188.86		0	0	8333	0			0	No, Vu<V
SLV 4	5.15	-897	-100	-93.25		2052	1.4567	8744	3821			38.12	Si
SLV 8	1.39	-1211	2380	1414.84		0	0	8333	0			0	No, Vu<V
SLV 8	3.27	-961	1984	298.13		2554	1.2541	8844	3327			1.68	Si
SLV 8	5.15	-924	861	-113.7		2114	1.4567	8756	3826			4.45	Si
SLV 5	1.39	-1659	-3474	-1533.44		0	0	8333	0			0	No, Vu<V
SLV 5	3.27	-788	-2835	-324.19		2763	0.9502	8886	2533			0.89	No, Vu<V
SLV 5	5.15	-801	-1098	154.36		1833	1.4567	8700	3802			3.46	Si
SLV 6	1.39	-1659	-3474	-1533.44		0	0	8333	0			0	No, Vu<V
SLV 6	3.27	-788	-2835	-324.19		2763	0.9502	8886	2533			0.89	No, Vu<V
SLV 6	5.15	-801	-1098	154.36		1833	1.4567	8700	3802			3.46	Si
SLV 12	1.39	-3441	3342	1478.21		12798	0.8963	10893	2929			0.88	No, Vu<V
SLV 12	3.27	-2583	2740	205.09		5911	1.4567	9516	4158			1.52	Si
SLV 12	5.15	-910	1097	-50.81		2083	1.4567	8750	3824			3.49	Si
SLV 7	1.39	-1211	2380	1414.84		0	0	8333	0			0	No, Vu<V
SLV 7	3.27	-961	1984	298.13		2554	1.2541	8844	3327			1.68	Si
SLV 7	5.15	-924	861	-113.7		2114	1.4567	8756	3826			4.45	Si
SLV 1	1.39	1100	-2548	-575.48		0	0	8333	0			0	No, Vu<V
SLV 1	3.27	1045	-2030	2.17		0	0	8333	0			0	No, Vu<V
SLV 1	5.15	-860	-688	-12.83		1968	1.4567	8727	3814			5.54	Si
SLV 3	1.39	1234	-792	309		0	0	8333	0			0	No, Vu<V
SLV 3	3.27	993	-585	188.86		0	0	8333	0			0	No, Vu<V



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 3	5.15	-897	-100	-93.25		2052	1.4567	8744	3821			38.12	Si
SLV 2	1.39	1100	-2548	-575.48			0	8333	0			0	No, Vu<V
SLV 2	3.27	1045	-2030	2.17			0	8333	0			0	No, Vu<V
SLV 2	5.15	-860	-688	-12.83		1968	1.4567	8727	3814			5.54	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.27 Wa 0.05 denominatore 8 yM = 2

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 5	143750	0.48	0	-961	221.03	0	0	No, e>t/2
SLV 4	143750	0.48	0	993	221.03	0	0	No, Trazione
SLV 5	143750	0.48	0	-788	221.03	0	0	No, e>t/2
SLV 7	143750	0.48	0	-961	221.03	0	0	No, e>t/2
SLV 2	143750	0.48	0	1045	221.03	0	0	No, Trazione
SLV 6	143750	0.48	0	-788	221.03	0	0	No, e>t/2
SLV 3	143750	0.48	0	993	221.03	0	0	No, Trazione
SLV 1	143750	0.48	0	1045	221.03	0	0	No, Trazione
SLV 9	143750	0.48	5515	-2410	221.03	345.2	1.56	Si
SLV 10	143750	0.48	5515	-2410	221.03	345.2	1.56	Si

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzeria = 3.27 Wa = 0.05 Ta = 0.0787

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	a0*	aLim	Verifica
SLV 5	-801	-1659	463	0	343.9	0.898	0	10.142	No
SLV 4	-897	1234	-190	0	0	0	0	8.41479	No, Trazione
SLV 1	-860	1100	97	0	0	0	0	8.41479	No, Trazione
SLV 9	-787	-3890	490	0	342.9	0.898	0	10.142	No
SLV 8	-924	-1211	-494	0	353.8	0.894	0	10.142	No
SLV 6	-801	-1659	463	0	343.9	0.898	0	10.142	No
SLV 7	-924	-1211	-494	0	353.8	0.894	0	10.142	No
SLV 10	-787	-3890	490	0	342.9	0.898	0	10.142	No
SLV 3	-897	1234	-190	0	0	0	0	8.41479	No, Trazione
SLV 2	-860	1100	97	0	0	0	0	8.41479	No, Trazione

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	11.413	SLU 82	Si
V_SLU	18.334	SLU 39	Si
PF_SLV	0	SLV 4	No
V_SLV	0	SLV 1	No
PFFP_SLV	0	SLV 4	No
R_SLV	0	SLV 4	No

## Maschio 35

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	X fin.	Y fin.	Quota i.	Quota.s	I	Sp.	h netta	h ini.	h fin.	a	a.s.,sx	a.s.,dx
-24.603	-3.177	-24.603	5.726	L2	L3	8.903	0.3	3.76	3.76	3.76			

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fk	fvk0	fmedio	t0	fv0	$\mu$	$\phi$	fv,lim	E	G	FC
600000			345000	9000	20000	0.58	0.77	32500	320000000	128000000	1.2

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni non sismiche, yM = 3

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 21	1.39	-20852	11085.08	7807	83925.87	7.571	Si
SLU 21	3.27	-7413	16818.31	2775	31872.97	1.895	Si
SLU 21	5.15	-4591	7425.8	1719	20005.83	2.694	Si
SLU 39	1.39	-20790	13683.53	7784	83704.49	6.117	Si
SLU 39	3.27	-7060	20213.97	2643	30406.2	1.504	Si
SLU 39	5.15	-5392	8789.45	2019	23406.91	2.663	Si
SLU 37	1.39	-20410	10897.26	7641	82331.1	7.555	Si
SLU 37	3.27	-7267	16541.71	2721	31268.38	1.89	Si
SLU 37	5.15	-4486	7291.27	1679	19556.56	2.682	Si
SLU 41	1.39	-20790	13683.53	7784	83704.49	6.117	Si
SLU 41	3.27	-7060	20213.97	2643	30406.2	1.504	Si
SLU 41	5.15	-5392	8789.45	2019	23406.91	2.663	Si
SLU 18	1.39	-20446	11446.4	7655	82462.63	7.204	Si
SLU 18	3.27	-7268	16903.28	2721	31273.87	1.85	Si
SLU 18	5.15	-4554	7404.77	1705	19848.2	2.68	Si
SLU 42	1.39	-21196	13322.21	7936	85162.02	6.392	Si
SLU 42	3.27	-7204	20129	2697	31006.54	1.54	Si
SLU 42	5.15	-5429	8810.48	2033	23563.27	2.674	Si
SLU 32	1.39	-20410	10897.26	7641	82331.1	7.555	Si
SLU 32	3.27	-7267	16541.71	2721	31268.38	1.89	Si
SLU 32	5.15	-4486	7291.27	1679	19556.56	2.682	Si
SLU 35	1.39	-20410	10897.26	7641	82331.1	7.555	Si
SLU 35	3.27	-7267	16541.71	2721	31268.38	1.89	Si
SLU 35	5.15	-4486	7291.27	1679	19556.56	2.682	Si
SLU 20	1.39	-20446	11446.4	7655	82462.63	7.204	Si
SLU 20	3.27	-7268	16903.28	2721	31273.87	1.85	Si
SLU 20	5.15	-4554	7404.77	1705	19848.2	2.68	Si



Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLU 40	1.39	-21196	13322.21	7936	85162.02	6.392	Si
SLU 40	3.27	-7204	20129	2697	31006.54	1.54	Si
SLU 40	5.15	-5429	8810.48	2033	23563.27	2.674	Si

Verifica a pressoflessione nel piano secondo D.M. 17-01-18 NTC §7.8.2.2.1 in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	M	$\sigma_0$	Mu	c.s.	Verifica
SLV 11	1.39	-18541	23251.29	6942	77847.03	3.348	Si
SLV 11	3.27	-7031	15610.12	2632	30623.82	1.962	Si
SLV 11	5.15	-2151	3622.45	805	9511.85	2.626	Si
SLV 6	1.39	-20518	-13940.21	7682	85593.03	6.14	Si
SLV 6	3.27	-8492	502.91	3179	36819.29	73.212	Si
SLV 6	5.15	-2603	3988.07	975	11496.82	2.883	Si
SLV 7	1.39	-10942	30694.41	4097	47075.16	1.534	Si
SLV 7	3.27	-4660	17276.74	1745	20446.06	1.183	Si
SLV 7	5.15	-1601	3981.27	599	7090.55	1.781	Si
SLV 8	1.39	-10942	30694.41	4097	47075.16	1.534	Si
SLV 8	3.27	-4660	17276.74	1745	20446.06	1.183	Si
SLV 8	5.15	-1601	3981.27	599	7090.55	1.781	Si
SLV 5	1.39	-20518	-13940.21	7682	85593.03	6.14	Si
SLV 5	3.27	-8492	502.91	3179	36819.29	73.212	Si
SLV 5	5.15	-2603	3988.07	975	11496.82	2.883	Si
SLV 2	1.39	-8300	10365.55	3108	36010.12	3.474	Si
SLV 2	3.27	-4384	8318.14	1641	19254.32	2.315	Si
SLV 2	5.15	-1611	4404.31	603	7133.87	1.62	Si
SLV 4	1.39	-5428	23755.93	2032	23759.96	1	Si
SLV 4	3.27	-3234	13350.29	1211	14255.58	1.068	Si
SLV 4	5.15	-1310	4402.27	490	5806.73	1.319	Si
SLV 3	1.39	-5428	23755.93	2032	23759.96	1	Si
SLV 3	3.27	-3234	13350.29	1211	14255.58	1.068	Si
SLV 3	5.15	-1310	4402.27	490	5806.73	1.319	Si
SLV 1	1.39	-8300	10365.55	3108	36010.12	3.474	Si
SLV 1	3.27	-4384	8318.14	1641	19254.32	2.315	Si
SLV 1	5.15	-1611	4404.31	603	7133.87	1.62	Si
SLV 12	1.39	-18541	23251.29	6942	77847.03	3.348	Si
SLV 12	3.27	-7031	15610.12	2632	30623.82	1.962	Si
SLV 12	5.15	-2151	3622.45	805	9511.85	2.626	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni non sismiche,  $\gamma_M = 3$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt <sub>lim</sub>	c.s.	Verifica
SLU 41	1.39	-20790	174	13683.53		7784	8.9031	6593	17610			101.31	Si
SLU 41	3.27	-7060	178	20213.97		4939	4.7646	6214	8882			49.78	Si
SLU 41	5.15	-5392	165	8789.45		2123	8.4642	5839	14826			90.12	Si
SLU 40	1.39	-21196	172	13322.21		7936	8.9031	6614	17665			102.52	Si
SLU 40	3.27	-7204	175	20129		4830	4.9721	6199	9247			52.97	Si
SLU 40	5.15	-5429	150	8810.48		2132	8.4858	5840	14867			98.81	Si
SLU 83	1.39	-26425	180	13564.16		9894	8.9031	6875	18362			101.98	Si
SLU 83	3.27	-9519	183	20477.6		4598	6.9008	6169	12771			69.7	Si
SLU 83	5.15	-5565	169	9037.96		2187	8.4821	5847	14879			88.14	Si
SLU 39	1.39	-20790	174	13683.53		7784	8.9031	6593	17610			101.31	Si
SLU 39	3.27	-7060	178	20213.97		4939	4.7646	6214	8882			49.78	Si
SLU 39	5.15	-5392	165	8789.45		2123	8.4642	5839	14826			90.12	Si
SLU 81	1.39	-26425	180	13564.16		9894	8.9031	6875	18362			101.98	Si
SLU 81	3.27	-9519	183	20477.6		4598	6.9008	6169	12771			69.7	Si
SLU 81	5.15	-5565	169	9037.96		2187	8.4821	5847	14879			88.14	Si
SLU 42	1.39	-21196	172	13322.21		7936	8.9031	6614	17665			102.52	Si
SLU 42	3.27	-7204	175	20129		4830	4.9721	6199	9247			52.97	Si
SLU 42	5.15	-5429	150	8810.48		2132	8.4858	5840	14867			98.81	Si
SLU 84	1.39	-26831	179	13202.85		10046	8.9031	6895	18416			103.15	Si
SLU 84	3.27	-9663	179	20392.64		4586	7.0236	6167	12994			72.45	Si
SLU 84	5.15	-5602	155	9058.99		2196	8.503	5848	14919			96.4	Si
SLU 18	1.39	-20446	148	11446.4		7655	8.9031	6576	17565			118.94	Si
SLU 18	3.27	-7268	150	16903.28		3799	6.3777	6062	11599			77.2	Si
SLU 18	5.15	-4554	138	7404.77		1791	8.4767	5794	14735			106.49	Si
SLU 20	1.39	-20446	148	11446.4		7655	8.9031	6576	17565			118.94	Si
SLU 20	3.27	-7268	150	16903.28		3799	6.3777	6062	11599			77.2	Si
SLU 20	5.15	-4554	138	7404.77		1791	8.4767	5794	14735			106.49	Si
SLU 82	1.39	-26831	179	13202.85		10046	8.9031	6895	18416			103.15	Si
SLU 82	3.27	-9663	179	20392.64		4586	7.0236	6167	12994			72.45	Si
SLU 82	5.15	-5602	155	9058.99		2196	8.503	5848	14919			96.4	Si

Verifica a taglio nel piano secondo D.M. 17-01-18 (N.T.C.) §7.8.2.2.2 con rottura per scorrimento in combinazioni sismiche,  $\gamma_M = 2$

Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt <sub>lim</sub>	c.s.	Verifica
SLV 8	1.39	-10942	4807	30694.41		7385	4.939	9810	14536			3.02	Si
SLV 8	3.27	-4660	4067	17276.74		6961	2.2312	9726	6510			1.6	Si
SLV 8	5.15	-1601	3154	3981.27		905	5.8929	8514	15052			4.77	Si
SLV 4	1.39	-5428	2618	23755.93		80651	0.2243	16250	1094			0.42	No, Vu < V
SLV 4	3.27	-3234	1929	13350.29		11092	0.972	10552	3077			1.6	Si
SLV 4	5.15	-1310	1359	4402.27		1335	3.2707	8600	8439			6.21	Si
SLV 6	1.39	-20518	-3912	-13940.21		7682	8.9031	9870	26361			6.74	Si
SLV 6	3.27	-8492	-3482	502.91		3179	8.9031	8969	23956			6.88	Si
SLV 6	5.15	-2603	-2773	3988.07		991	8.7591	8531	22418			8.08	Si
SLV 12	1.39	-18541	4067	23251.29		6942	8.9031	9722	25966			6.38	Si
SLV 12	3.27	-7031	3635	15610.12		3501	6.6939	9034	18141			4.99	Si
SLV 12	5.15	-2151	2914	3622.45		864	8.3022	8506	21186			7.27	Si
SLV 10	1.39	-28117	-4652	-21383.34		10527	8.9031	10439	27881			5.99	Si
SLV 10	3.27	-10863	-3914	-1163.71		4067	8.9031	9147	24430			6.24	Si
SLV 10	5.15	-3154	-3013	3629.25		1181	8.9031	8569	22888			7.6	Si
SLV 5	1.39	-20518	-3912	-13940.21		7682	8.9031	9870	26361			6.74	Si



Comb.	Quota	N	V par	M	$\sigma_0$	$\sigma_N$	I'	fvd	Vt scorr.	Vt fess.diag.	Vt,lim	c.s.	Verifica
SLV 5	3.27	-8492	-3482	502.91		3179	8.9031	8969	23956			6.88	Si
SLV 5	5.15	-2603	-2773	3988.07		991	8.7591	8531	22418			8.08	Si
SLV 7	1.39	-10942	4807	30694.41		7385	4.939	9810	14536			3.02	Si
SLV 7	3.27	-4660	4067	17276.74		6961	2.2312	9726	6510			1.6	Si
SLV 7	5.15	-1601	3154	3981.27		905	5.8929	8514	15052			4.77	Si
SLV 11	1.39	-18541	4067	23251.29		6942	8.9031	9722	25966			6.38	Si
SLV 11	3.27	-7031	3635	15610.12		3501	6.6939	9034	18141			4.99	Si
SLV 11	5.15	-2151	2914	3622.45		864	8.3022	8506	21186			7.27	Si
SLV 9	1.39	-28117	-4652	-21383.34		10527	8.9031	10439	27881			5.99	Si
SLV 9	3.27	-10863	-3914	-1163.71		4067	8.9031	9147	24430			6.24	Si
SLV 9	5.15	-3154	-3013	3629.25		1181	8.9031	8569	22888			7.6	Si
SLV 3	1.39	-5428	2618	23755.93		80651	0.2243	16250	1094			0.42	No, Vu<V
SLV 3	3.27	-3234	1929	13350.29		11092	0.972	10552	3077			1.6	Si
SLV 3	5.15	-1310	1359	4402.27		1335	3.2707	8600	8439			6.21	Si

Verifica a pressoflessione fuori piano D.M. 17-01-18 (N.T.C.)

quota 3.27 Wa 0.05 denominatore  $8 \gamma M = 2$

Comb.	fd	Sa	$\sigma_0$	N	M	Mc	Coeff.s.	Verifica
SLV 3	143750	0.48	0	-3234	1350.91	0	0	No, $e>t/2$
SLV 1	143750	0.48	0	-4384	1350.91	0	0	No, $e>t/2$
SLV 5	143750	0.48	0	-8492	1350.91	0	0	No, $e>t/2$
SLV 4	143750	0.48	0	-3234	1350.91	0	0	No, $e>t/2$
SLV 11	143750	0.48	0	-7031	1350.91	0	0	No, $e>t/2$
SLV 12	143750	0.48	0	-7031	1350.91	0	0	No, $e>t/2$
SLV 7	143750	0.48	0	-4660	1350.91	0	0	No, $e>t/2$
SLV 6	143750	0.48	0	-8492	1350.91	0	0	No, $e>t/2$
SLV 2	143750	0.48	0	-4384	1350.91	0	0	No, $e>t/2$
SLV 8	143750	0.48	0	-4660	1350.91	0	0	No, $e>t/2$

Verifica dei meccanismi locali di collasso con analisi cinematica lineare

forza di aggancio al piano = 0 quota mezzaria = 3.27 Wa = 0.05 Ta = 0.0787

Comb.	N top	N base	V orto	$\alpha_0$	M*	e*	a0*	aLim	Verifica
SLV 2	-1611	-8300	713	0.007	1885.8	0.94	0.10538	8.41479	No
SLV 1	-1611	-8300	713	0.007	1885.8	0.94	0.10538	8.41479	No
SLV 16	-3144	-30758	-716	0.011	1974.2	0.913	0.17016	8.41479	No
SLV 15	-3144	-30758	-716	0.011	1974.2	0.913	0.17016	8.41479	No
SLV 3	-1310	-5428	598	0.017	1872.7	0.948	0.26039	8.41479	No
SLV 4	-1310	-5428	598	0.017	1872.7	0.948	0.26039	8.41479	No
SLV 13	-3445	-33631	-601	0.021	1994.6	0.909	0.3295	8.41479	No
SLV 14	-3445	-33631	-601	0.021	1994.6	0.909	0.3295	8.41479	No
SLV 11	-2151	-18541	-391	0.037	1913.4	0.928	0.58251	10.142	No
SLV 12	-2151	-18541	-391	0.037	1913.4	0.928	0.58251	10.142	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLU	1.504	SLU 39	Si
V_SLU	49.779	SLU 39	Si
PF_SLV	1	SLV 3	Si
V_SLV	0.418	SLV 3	No
PFFP_SLV	0	SLV 1	No
R_SLV	0.013	SLV 1	No

## 2.4 Verifiche travi di accoppiamento in muratura

Le unità di misura elencate nel capitolo sono in [m, daN] ove non espressamente specificato.

**X<sub>ini.</sub>**: coordinata punto iniziale. [m]

**Y<sub>ini.</sub>**: coordinata punto iniziale. [m]

**Z<sub>ini.inf.</sub>**: coordinata punto iniziale. [m]

**Z<sub>ini.sup.</sub>**: coordinata punto iniziale. [m]

**H<sub>ini.</sub>**: altezza della sezione iniziale. [m]

**X<sub>fin.</sub>**: coordinata punto finale. [m]

**Y<sub>fin.</sub>**: coordinata punto finale. [m]

**Z<sub>fin.inf.</sub>**: coordinata punto finale. [m]

**Z<sub>fin.sup.</sub>**: coordinata punto finale. [m]

**H<sub>fin.</sub>**: altezza della sezione finale. [m]

**Luce**: lunghezza della trave. [m]

**Spessore**: spessore. [m]

**R. Trazione**: resistenza a trazione dell'elemento teso disposto orizzontalmente. [daN]

**f<sub>b</sub>**: resistenza normalizzata a compressione in direzione orizzontale dei blocchi. [daN/m<sup>2</sup>]

**f<sub>hk</sub>**: resistenza caratteristica a compressione della muratura utilizzata in direzione orizzontale. [daN/m<sup>2</sup>]

**f<sub>vk0</sub>**: resistenza caratteristica a taglio in assenza di carichi verticali. [daN/m<sup>2</sup>]

**f<sub>hmedio</sub>**: resistenza media a compressione della muratura utilizzata in direzione orizzontale. [daN/m<sup>2</sup>]

**$\tau_0$** : resistenza media a taglio in assenza di azioni normali [C8.7.1.16]. [daN/m<sup>2</sup>]

**f<sub>v0</sub>**: resistenza media a taglio in assenza di azioni normali [C8.7.1.17]. [daN/m<sup>2</sup>]

**$\mu$** : coefficiente di attrito [C8.7.1.17].

**$\varphi$** : coefficiente di ammortamento o ingranamento secondo Circolare 7 21-01-19 §C8.7.1.3.1.1.



**fvk,lim:** valore caratteristico massimo della resistenza a taglio che può essere impiegata nel calcolo (§11.10.3.3). [daN/m<sup>2</sup>]

**E:** modulo di elasticità longitudinale della muratura utilizzato. [daN/m<sup>2</sup>]

**G:** modulo di elasticità tangenziale della muratura utilizzato. [daN/m<sup>2</sup>]

**FC:** fattore di confidenza della muratura.

**Sezione:** sezione di verifica.

**γM:** fattore parziale di sicurezza del materiale.

**N:** sforzo normale. [daN]

**M:** momento flettente nel piano. [daN\*m]

**Mu:** momento ultimo. [daN\*m]

**Comb.:** combinazione.

**c.s.:** coefficiente di sicurezza.

**Verifica:** stato di verifica.

**M:** momento flettente. [daN\*m]

**V:** taglio nel piano. [daN]

**Vt:** resistenza a taglio secondo [7.8.4]. [daN]

**Vp:** resistenza a taglio secondo [7.8.6]. [daN]

**Vt fess. diag.:** resistenza a taglio per fessurazione diagonale secondo §C8.7.1.3.1.1 formule [C8.7.1.16] ovvero [C8.7.1.17]. [daN]

**Vt,lim:** taglio limite [C8.1.7.18]. [daN]

**Stato limite:** pF\_SLV=Presso flessione per azioni sismiche; V\_SLV=Taglio per azioni sismiche.

**Coeff.s.:** coefficiente di sicurezza.

## Trave di accoppiamento 1

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-34.183	-1.829	-1.3	0.7	2	-34.183	-0.829	-1.3	0.7	2	1	0.45	3500

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

f <sub>b</sub>	f <sub>hk</sub>	fvk0	f <sub>h</sub> medio	τ <sub>0</sub>	f <sub>v0</sub>	μ	φ	fvk,lim	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

### Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-566	-950.67	3277.21	SLV 9	3.45	Si
fin.	2	-2361	533.75	3277.21	SLV 9	6.14	Si
ini.	2	-1564	153.39	3277.21	SLV 11	21.37	Si
fin.	2	-690	-715.82	3277.21	SLV 11	4.58	Si
ini.	2	-1564	153.39	3277.21	SLV 12	21.37	Si
fin.	2	-690	-715.82	3277.21	SLV 12	4.58	Si
ini.	2	-566	-950.67	3277.21	SLV 10	3.45	Si
fin.	2	-2361	533.75	3277.21	SLV 10	6.14	Si
ini.	2	-521	-590.84	3277.21	SLV 14	5.55	Si
fin.	2	-1292	39.87	3277.21	SLV 14	82.21	Si
ini.	2	-1902	176.18	3277.21	SLV 8	18.6	Si
fin.	2	-1105	-667.36	3277.21	SLV 8	4.91	Si
ini.	2	-903	-927.88	3277.21	SLV 5	3.53	Si
fin.	2	-2776	582.21	3277.21	SLV 5	5.63	Si
ini.	2	-521	-590.84	3277.21	SLV 13	5.55	Si
fin.	2	-1292	39.87	3277.21	SLV 13	82.21	Si
ini.	2	-1902	176.18	3277.21	SLV 7	18.6	Si
fin.	2	-1105	-667.36	3277.21	SLV 7	4.91	Si
ini.	2	-903	-927.88	3277.21	SLV 6	3.53	Si
fin.	2	-2776	582.21	3277.21	SLV 6	5.63	Si

### Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-927.88	1596			5199	1957	SLV 5	1.23	Si
fin.	2	0	582.21	5537			5199	1957	SLV 5	0.35	No
ini.	2	0	-950.67	1664			5199	1957	SLV 9	1.18	Si
fin.	2	0	533.75	5054			5199	1957	SLV 9	0.39	No
ini.	2	0	176.18	-3400			5199	1957	SLV 7	0.58	No
fin.	2	0	-667.36	16			5199	1957	SLV 7	120.25	Si
ini.	2	0	-950.67	1664			5199	1957	SLV 10	1.18	Si
fin.	2	0	533.75	5054			5199	1957	SLV 10	0.39	No
ini.	2	0	176.18	-3400			5199	1957	SLV 8	0.58	No
fin.	2	0	-667.36	16			5199	1957	SLV 8	120.25	Si
ini.	2	0	153.39	-3331			5199	1957	SLV 12	0.59	No
fin.	2	0	-715.82	-467			5199	1957	SLV 12	4.19	Si
ini.	2	0	-514.87	-233			5199	1957	SLV 1	8.41	Si
fin.	2	0	201.4	4169			5199	1957	SLV 1	0.47	No
ini.	2	0	-927.88	1596			5199	1957	SLV 6	1.23	Si
fin.	2	0	582.21	5537			5199	1957	SLV 6	0.35	No
ini.	2	0	153.39	-3331			5199	1957	SLV 11	0.59	No
fin.	2	0	-715.82	-467			5199	1957	SLV 11	4.19	Si
ini.	2	0	-514.87	-233			5199	1957	SLV 2	8.41	Si
fin.	2	0	201.4	4169			5199	1957	SLV 2	0.47	No

### Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
--------------	----------	-------	----------



Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	3.447	SLV 9	Si
V_SLV	0.353	SLV 5	No

## Trave di accoppiamento 2

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-34.183	-1.829	1.1	1.39	0.29	-34.183	-0.829	1.1	1.39	0.29	1	0.45	3500

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	f <sub>hk</sub>	f <sub>vk0</sub>	f <sub>hmedio</sub>	τ <sub>0</sub>	f <sub>v0</sub>	μ	φ	f <sub>vk,lim</sub>	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

### Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	28	-87.74	284.71	SLV 2	3.24	Si
fin.	2	271	-44.9	284.71	SLV 2	6.34	Si
ini.	2	28	-87.74	284.71	SLV 1	3.24	Si
fin.	2	271	-44.9	284.71	SLV 1	6.34	Si
ini.	2	442	24.11	284.71	SLV 8	11.81	Si
fin.	2	-390	-99.13	284.71	SLV 8	2.87	Si
ini.	2	-399	-119.09	284.71	SLV 14	2.39	Si
fin.	2	547	34.12	284.71	SLV 14	8.34	Si
ini.	2	-553	-174.25	284.71	SLV 10	1.63	Si
fin.	2	859	50.56	284.71	SLV 10	5.63	Si
ini.	2	-425	-164.84	284.71	SLV 5	1.73	Si
fin.	2	776	26.85	284.71	SLV 5	10.6	Si
ini.	2	-399	-119.09	284.71	SLV 13	2.39	Si
fin.	2	547	34.12	284.71	SLV 13	8.34	Si
ini.	2	-553	-174.25	284.71	SLV 9	1.63	Si
fin.	2	859	50.56	284.71	SLV 9	5.63	Si
ini.	2	442	24.11	284.71	SLV 7	11.81	Si
fin.	2	-390	-99.13	284.71	SLV 7	2.87	Si
ini.	2	-425	-164.84	284.71	SLV 6	1.73	Si
fin.	2	776	26.85	284.71	SLV 6	10.6	Si

### Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-87.74	647			503	189	SLV 1	0.29	No
fin.	2	0	-44.9	-270			503	189	SLV 1	0.7	No
ini.	2	0	-164.84	839			503	189	SLV 5	0.23	No
fin.	2	0	26.85	50			503	189	SLV 5	3.78	Si
ini.	2	0	-174.25	786			503	189	SLV 9	0.24	No
fin.	2	0	50.56	124			503	189	SLV 9	1.53	Si
ini.	2	0	24.11	113			503	189	SLV 8	1.68	Si
fin.	2	0	-99.13	-617			503	189	SLV 8	0.31	No
ini.	2	0	-164.84	839			503	189	SLV 6	0.23	No
fin.	2	0	26.85	50			503	189	SLV 6	3.78	Si
ini.	2	0	24.11	113			503	189	SLV 7	1.68	Si
fin.	2	0	-99.13	-617			503	189	SLV 7	0.31	No
ini.	2	0	14.7	59			503	189	SLV 12	3.19	Si
fin.	2	0	-75.43	-543			503	189	SLV 12	0.35	No
ini.	2	0	14.7	59			503	189	SLV 11	3.19	Si
fin.	2	0	-75.43	-543			503	189	SLV 11	0.35	No
ini.	2	0	-87.74	647			503	189	SLV 2	0.29	No
fin.	2	0	-44.9	-270			503	189	SLV 2	0.7	No
ini.	2	0	-174.25	786			503	189	SLV 10	0.24	No
fin.	2	0	50.56	124			503	189	SLV 10	1.53	Si

### Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.634	SLV 9	Si
V_SLV	0.225	SLV 5	No

## Trave di accoppiamento 3

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-34.183	2.931	-1.3	0.7	2	-34.183	3.931	-1.3	0.7	2	1	0.45	3500

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	f <sub>hk</sub>	f <sub>vk0</sub>	f <sub>hmedio</sub>	τ <sub>0</sub>	f <sub>v0</sub>	μ	φ	f <sub>vk,lim</sub>	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2



#### Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-1841	764.78	3277.21	SLV 11	4.29	Si
fin.	2	-528	-1185.74	3277.21	SLV 11	2.76	Si
ini.	2	-1016	150.03	3277.21	SLV 16	21.84	Si
fin.	2	-483	-658.42	3277.21	SLV 16	4.98	Si
ini.	2	-1431	-955.59	3277.21	SLV 6	3.43	Si
fin.	2	-2047	386.65	3277.21	SLV 6	8.48	Si
ini.	2	-1841	764.78	3277.21	SLV 12	4.29	Si
fin.	2	-528	-1185.74	3277.21	SLV 12	2.76	Si
ini.	2	-982	-963.91	3277.21	SLV 9	3.4	Si
fin.	2	-1666	371.47	3277.21	SLV 9	8.82	Si
ini.	2	-2291	773.11	3277.21	SLV 8	4.24	Si
fin.	2	-909	-1170.56	3277.21	SLV 8	2.8	Si
ini.	2	-1431	-955.59	3277.21	SLV 5	3.43	Si
fin.	2	-2047	386.65	3277.21	SLV 5	8.48	Si
ini.	2	-2291	773.11	3277.21	SLV 7	4.24	Si
fin.	2	-909	-1170.56	3277.21	SLV 7	2.8	Si
ini.	2	-1016	150.03	3277.21	SLV 15	21.84	Si
fin.	2	-483	-658.42	3277.21	SLV 15	4.98	Si
ini.	2	-982	-963.91	3277.21	SLV 10	3.4	Si
fin.	2	-1666	371.47	3277.21	SLV 10	8.82	Si

#### Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	177.77	-2768			5199	1957	SLV 3	0.71	No
fin.	2	0	-607.84	370			5199	1957	SLV 3	5.29	Si
ini.	2	0	764.78	-4396			5199	1957	SLV 11	0.45	No
fin.	2	0	-1185.74	-2069			5199	1957	SLV 11	0.95	No
ini.	2	0	773.11	-4612			5199	1957	SLV 7	0.42	No
fin.	2	0	-1170.56	-1811			5199	1957	SLV 7	1.08	Si
ini.	2	0	-955.59	1376			5199	1957	SLV 5	1.42	Si
fin.	2	0	386.65	3560			5199	1957	SLV 5	0.55	No
ini.	2	0	773.11	-4612			5199	1957	SLV 8	0.42	No
fin.	2	0	-1170.56	-1811			5199	1957	SLV 8	1.08	Si
ini.	2	0	177.77	-2768			5199	1957	SLV 4	0.71	No
fin.	2	0	-607.84	370			5199	1957	SLV 4	5.29	Si
ini.	2	0	764.78	-4396			5199	1957	SLV 12	0.45	No
fin.	2	0	-1185.74	-2069			5199	1957	SLV 12	0.95	No
ini.	2	0	-955.59	1376			5199	1957	SLV 6	1.42	Si
fin.	2	0	386.65	3560			5199	1957	SLV 6	0.55	No
ini.	2	0	-963.91	1592			5199	1957	SLV 10	1.23	Si
fin.	2	0	371.47	3301			5199	1957	SLV 10	0.59	No
ini.	2	0	-963.91	1592			5199	1957	SLV 9	1.23	Si
fin.	2	0	371.47	3301			5199	1957	SLV 9	0.59	No

#### Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	2.764	SLV 11	Si
V_SLV	0.424	SLV 7	No

#### Trave di accoppiamento 4

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

##### Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-34.183	2.931	1.1	1.39	0.29	-34.183	3.931	1.1	1.39	0.29	1	0.45	3500

##### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	f <sub>hk</sub>	f <sub>vk0</sub>	f <sub>hmedio</sub>	τ <sub>0</sub>	f <sub>v0</sub>	μ	φ	f <sub>vk,lim</sub>	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

#### Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	789	25.55	284.71	SLV 8	11.14	Si
fin.	2	-528	-197.77	284.71	SLV 8	1.44	Si
ini.	2	-545	-149.53	284.71	SLV 10	1.9	Si
fin.	2	424	8.52	284.71	SLV 10	33.41	Si
ini.	2	536	-16.67	284.71	SLV 4	17.08	Si
fin.	2	-327	-158	284.71	SLV 4	1.8	Si
ini.	2	789	25.55	284.71	SLV 7	11.14	Si
fin.	2	-528	-197.77	284.71	SLV 7	1.44	Si
ini.	2	-404	-136.97	284.71	SLV 6	2.08	Si
fin.	2	337	-12.87	284.71	SLV 6	22.13	Si
ini.	2	536	-16.67	284.71	SLV 3	17.08	Si
fin.	2	-327	-158	284.71	SLV 3	1.8	Si
ini.	2	648	12.99	284.71	SLV 11	21.92	Si
fin.	2	-441	-176.38	284.71	SLV 11	1.61	Si
ini.	2	648	12.99	284.71	SLV 12	21.92	Si
fin.	2	-441	-176.38	284.71	SLV 12	1.61	Si
ini.	2	-545	-149.53	284.71	SLV 9	1.9	Si
fin.	2	424	8.52	284.71	SLV 9	33.41	Si
ini.	2	-404	-136.97	284.71	SLV 5	2.08	Si





Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
fin.	2	337	-12.87	284.71	SLV 5	22.13	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-16.67	374			503	189	SLV 4	0.51	No
fin.	2	0	-158	-771			503	189	SLV 4	0.25	No
ini.	2	0	12.99	61			503	189	SLV 11	3.09	Si
fin.	2	0	-176.38	-955			503	189	SLV 11	0.2	No
ini.	2	0	12.99	61			503	189	SLV 12	3.09	Si
fin.	2	0	-176.38	-955			503	189	SLV 12	0.2	No
ini.	2	0	-149.53	815			503	189	SLV 9	0.23	No
fin.	2	0	8.52	-164			503	189	SLV 9	1.15	Si
ini.	2	0	-136.97	837			503	189	SLV 6	0.23	No
fin.	2	0	-12.87	-207			503	189	SLV 6	0.91	No
ini.	2	0	-16.67	374			503	189	SLV 3	0.51	No
fin.	2	0	-158	-771			503	189	SLV 3	0.25	No
ini.	2	0	-149.53	815			503	189	SLV 10	0.23	No
fin.	2	0	8.52	-164			503	189	SLV 10	1.15	Si
ini.	2	0	25.55	84			503	189	SLV 8	2.26	Si
fin.	2	0	-197.77	-998			503	189	SLV 8	0.19	No
ini.	2	0	25.55	84			503	189	SLV 7	2.26	Si
fin.	2	0	-197.77	-998			503	189	SLV 7	0.19	No
ini.	2	0	-136.97	837			503	189	SLV 5	0.23	No
fin.	2	0	-12.87	-207			503	189	SLV 5	0.91	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.44	SLV 7	Si
V_SLV	0.19	SLV 7	No

## Trave di accoppiamento 5

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-27.948	5.726	-1.3	0.7	2	-27.448	5.726	-1.3	0.7	2	0.5	0.45	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

f <sub>b</sub>	f <sub>tk</sub>	f <sub>vk0</sub>	f <sub>hmedio</sub>	τ <sub>0</sub>	f <sub>v0</sub>	μ	φ	f <sub>vk,lim</sub>	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-1620	-190.75	3277.21	SLV 7	17.18	Si
fin.	2	-1669	-605.14	3277.21	SLV 7	5.42	Si
ini.	2	-1620	-190.75	3277.21	SLV 8	17.18	Si
fin.	2	-1669	-605.14	3277.21	SLV 8	5.42	Si
ini.	2	-1965	145.13	3277.21	SLV 16	22.58	Si
fin.	2	-967	-633.87	3277.21	SLV 16	5.17	Si
ini.	2	-957	-426.44	3277.21	SLV 1	7.69	Si
fin.	2	-1308	-217.4	3277.21	SLV 1	15.07	Si
ini.	2	-957	-426.44	3277.21	SLV 2	7.69	Si
fin.	2	-1308	-217.4	3277.21	SLV 2	15.07	Si
ini.	2	-1871	-25.17	3277.21	SLV 12	130.22	Si
fin.	2	-1488	-690.12	3277.21	SLV 12	4.75	Si
ini.	2	-1871	-25.17	3277.21	SLV 11	130.22	Si
fin.	2	-1488	-690.12	3277.21	SLV 11	4.75	Si
ini.	2	-1795	125.51	3277.21	SLV 14	26.11	Si
fin.	2	-703	-500.67	3277.21	SLV 14	6.55	Si
ini.	2	-1965	145.13	3277.21	SLV 15	22.58	Si
fin.	2	-967	-633.87	3277.21	SLV 15	5.17	Si
ini.	2	-1795	125.51	3277.21	SLV 13	26.11	Si
fin.	2	-703	-500.67	3277.21	SLV 13	6.55	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-190.75	-2181			5199	1957	SLV 7	0.9	No
fin.	2	0	-605.14	96			5199	1957	SLV 7	20.31	Si
ini.	2	0	145.13	-5252			5199	1957	SLV 15	0.37	No
fin.	2	0	-633.87	-2498			5199	1957	SLV 15	0.78	No
ini.	2	0	145.13	-5252			5199	1957	SLV 16	0.37	No
fin.	2	0	-633.87	-2498			5199	1957	SLV 16	0.78	No
ini.	2	0	-190.75	-2181			5199	1957	SLV 8	0.9	No
fin.	2	0	-605.14	96			5199	1957	SLV 8	20.31	Si
ini.	2	0	-90.56	-2553			5199	1957	SLV 10	0.77	No
fin.	2	0	-246.13	-750			5199	1957	SLV 10	2.61	Si
ini.	2	0	-25.17	-3800			5199	1957	SLV 12	0.51	No
fin.	2	0	-690.12	-1169			5199	1957	SLV 12	1.67	Si
ini.	2	0	125.51	-4878			5199	1957	SLV 14	0.4	No
fin.	2	0	-500.67	-2373			5199	1957	SLV 14	0.82	No
ini.	2	0	-25.17	-3800			5199	1957	SLV 11	0.51	No
fin.	2	0	-690.12	-1169			5199	1957	SLV 11	1.67	Si



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	125.51	-4878			5199	1957	SLV 13	0.4	No
fin.	2	0	-500.67	-2373			5199	1957	SLV 13	0.82	No
ini.	2	0	-90.56	-2553			5199	1957	SLV 9	0.77	No
fin.	2	0	-246.13	-750			5199	1957	SLV 9	2.61	Si

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	4.749	SLV 11	Si
V_SLV	0.373	SLV 15	No

## Trave di accoppiamento 6

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-27.948	5.726	1	1.39	0.39	-27.448	5.726	1	1.39	0.39	0.5	0.45	3500

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

f <sub>b</sub>	f <sub>mk</sub>	f <sub>vk0</sub>	f <sub>hmedio</sub>	τ <sub>0</sub>	f <sub>v0</sub>	μ	φ	f <sub>vk,lim</sub>	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

### Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	508	-47.02	459.71	SLV 1	9.78	Si
fin.	2	529	23.8	459.71	SLV 1	19.31	Si
ini.	2	508	-47.02	459.71	SLV 2	9.78	Si
fin.	2	529	23.8	459.71	SLV 2	19.31	Si
ini.	2	288	89.72	459.71	SLV 14	5.12	Si
fin.	2	261	-143.14	459.71	SLV 14	3.21	Si
ini.	2	641	42.16	459.71	SLV 11	10.9	Si
fin.	2	644	-87.4	459.71	SLV 11	5.26	Si
ini.	2	641	42.16	459.71	SLV 12	10.9	Si
fin.	2	644	-87.4	459.71	SLV 12	5.26	Si
ini.	2	415	89.86	459.71	SLV 15	5.12	Si
fin.	2	395	-144.38	459.71	SLV 15	3.18	Si
ini.	2	217	41.7	459.71	SLV 9	11.02	Si
fin.	2	199	-83.26	459.71	SLV 9	5.52	Si
ini.	2	415	89.86	459.71	SLV 16	5.12	Si
fin.	2	395	-144.38	459.71	SLV 16	3.18	Si
ini.	2	288	89.72	459.71	SLV 13	5.12	Si
fin.	2	261	-143.14	459.71	SLV 13	3.21	Si
ini.	2	217	41.7	459.71	SLV 10	11.02	Si
fin.	2	199	-83.26	459.71	SLV 10	5.52	Si

### Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	1.14	-106			791	298	SLV 8	2.82	Si
fin.	2	0	-37.32	-265			791	298	SLV 8	1.12	Si
ini.	2	0	89.72	-311			791	298	SLV 14	0.96	No
fin.	2	0	-143.14	-466			791	298	SLV 14	0.64	No
ini.	2	0	1.14	-106			791	298	SLV 7	2.82	Si
fin.	2	0	-37.32	-265			791	298	SLV 7	1.12	Si
ini.	2	0	89.86	-370			791	298	SLV 16	0.8	No
fin.	2	0	-144.38	-525			791	298	SLV 16	0.57	No
ini.	2	0	89.72	-311			791	298	SLV 13	0.96	No
fin.	2	0	-143.14	-466			791	298	SLV 13	0.64	No
ini.	2	0	41.7	-63			791	298	SLV 10	4.71	Si
fin.	2	0	-83.26	-220			791	298	SLV 10	1.35	Si
ini.	2	0	42.16	-259			791	298	SLV 12	1.15	Si
fin.	2	0	-87.4	-416			791	298	SLV 12	0.71	No
ini.	2	0	41.7	-63			791	298	SLV 9	4.71	Si
fin.	2	0	-83.26	-220			791	298	SLV 9	1.35	Si
ini.	2	0	89.86	-370			791	298	SLV 15	0.8	No
fin.	2	0	-144.38	-525			791	298	SLV 15	0.57	No
ini.	2	0	42.16	-259			791	298	SLV 11	1.15	Si
fin.	2	0	-87.4	-416			791	298	SLV 11	0.71	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	3.184	SLV 15	Si
V_SLV	0.567	SLV 15	No

## Trave di accoppiamento 7

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-27.128	5.726	-1.3	0.7	2	-26.628	5.726	-1.3	0.7	2	0.5	0.45	3500



## Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	f <sub>hk</sub>	f <sub>vk0</sub>	f <sub>hmedio</sub>	t <sub>0</sub>	f <sub>v0</sub>	μ	φ	f <sub>vk,lim</sub>	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

## Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-1739	-421.32	3277.21	SLV 11	7.78	Si
fin.	2	-1493	-625.89	3277.21	SLV 11	5.24	Si
ini.	2	-1439	-610.19	3277.21	SLV 4	5.37	Si
fin.	2	-1690	184.26	3277.21	SLV 4	17.79	Si
ini.	2	-1779	-551.12	3277.21	SLV 8	5.95	Si
fin.	2	-1738	-297.66	3277.21	SLV 8	11.01	Si
ini.	2	-978	-98.38	3277.21	SLV 13	33.31	Si
fin.	2	-584	-824.97	3277.21	SLV 13	3.97	Si
ini.	2	-1308	-177.54	3277.21	SLV 15	18.46	Si
fin.	2	-871	-909.82	3277.21	SLV 15	3.6	Si
ini.	2	-1739	-421.32	3277.21	SLV 12	7.78	Si
fin.	2	-1493	-625.89	3277.21	SLV 12	5.24	Si
ini.	2	-1779	-551.12	3277.21	SLV 7	5.95	Si
fin.	2	-1738	-297.66	3277.21	SLV 7	11.01	Si
ini.	2	-1308	-177.54	3277.21	SLV 16	18.46	Si
fin.	2	-871	-909.82	3277.21	SLV 16	3.6	Si
ini.	2	-1439	-610.19	3277.21	SLV 3	5.37	Si
fin.	2	-1690	184.26	3277.21	SLV 3	17.79	Si
ini.	2	-978	-98.38	3277.21	SLV 14	33.31	Si
fin.	2	-584	-824.97	3277.21	SLV 14	3.97	Si

## Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-531.03	1968			5199	1957	SLV 2	0.99	No
fin.	2	0	269.12	2773			5199	1957	SLV 2	0.71	No
ini.	2	0	-531.03	1968			5199	1957	SLV 1	0.99	No
fin.	2	0	269.12	2773			5199	1957	SLV 1	0.71	No
ini.	2	0	-610.19	2039			5199	1957	SLV 3	0.96	No
fin.	2	0	184.26	3116			5199	1957	SLV 3	0.63	No
ini.	2	0	-177.54	-2253			5199	1957	SLV 15	0.87	No
fin.	2	0	-909.82	-1710			5199	1957	SLV 15	1.14	Si
ini.	2	0	-177.54	-2253			5199	1957	SLV 16	0.87	No
fin.	2	0	-909.82	-1710			5199	1957	SLV 16	1.14	Si
ini.	2	0	-98.38	-2324			5199	1957	SLV 14	0.84	No
fin.	2	0	-824.97	-2053			5199	1957	SLV 14	0.95	No
ini.	2	0	-551.12	619			5199	1957	SLV 8	3.16	Si
fin.	2	0	-297.66	1828			5199	1957	SLV 8	1.07	Si
ini.	2	0	-610.19	2039			5199	1957	SLV 4	0.96	No
fin.	2	0	184.26	3116			5199	1957	SLV 4	0.63	No
ini.	2	0	-98.38	-2324			5199	1957	SLV 13	0.84	No
fin.	2	0	-824.97	-2053			5199	1957	SLV 13	0.95	No
ini.	2	0	-551.12	619			5199	1957	SLV 7	3.16	Si
fin.	2	0	-297.66	1828			5199	1957	SLV 7	1.07	Si

## Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	3.602	SLV 15	Si
V_SLV	0.628	SLV 3	No

## Trave di accoppiamento 8

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-27.128	5.726	1	1.39	0.39	-26.628	5.726	1	1.39	0.39	0.5	0.45	3500

## Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	f <sub>hk</sub>	f <sub>vk0</sub>	f <sub>hmedio</sub>	t <sub>0</sub>	f <sub>v0</sub>	μ	φ	f <sub>vk,lim</sub>	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

## Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	241	-46.71	459.71	SLV 5	9.84	Si
fin.	2	245	3.32	459.71	SLV 5	138.41	Si
ini.	2	241	-46.71	459.71	SLV 6	9.84	Si
fin.	2	245	3.32	459.71	SLV 6	138.41	Si
ini.	2	1030	29.39	459.71	SLV 14	15.64	Si
fin.	2	1043	-60.25	459.71	SLV 14	7.63	Si
ini.	2	1188	34.85	459.71	SLV 15	13.19	Si
fin.	2	1196	-67.04	459.71	SLV 15	6.86	Si
ini.	2	100	-77.89	459.71	SLV 2	5.9	Si
fin.	2	92	25.38	459.71	SLV 2	18.11	Si
ini.	2	259	-72.44	459.71	SLV 4	6.35	Si
fin.	2	246	18.6	459.71	SLV 4	24.72	Si
ini.	2	1030	29.39	459.71	SLV 13	15.64	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
fin.	2	1043	-60.25	459.71	SLV 13	7.63	Si
ini.	2	259	-72.44	459.71	SLV 3	6.35	Si
fin.	2	246	18.6	459.71	SLV 3	24.72	Si
ini.	2	1188	34.85	459.71	SLV 16	13.19	Si
fin.	2	1196	-67.04	459.71	SLV 16	6.86	Si
ini.	2	100	-77.89	459.71	SLV 1	5.9	Si
fin.	2	92	25.38	459.71	SLV 1	18.11	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-72.44	273			791	298	SLV 4	1.09	Si
fin.	2	0	18.6	146			791	298	SLV 4	2.04	Si
ini.	2	0	34.85	-146			791	298	SLV 15	2.04	Si
fin.	2	0	-67.04	-275			791	298	SLV 15	1.08	Si
ini.	2	0	29.39	-112			791	298	SLV 14	2.65	Si
fin.	2	0	-60.25	-301			791	298	SLV 14	0.99	No
ini.	2	0	34.85	-146			791	298	SLV 16	2.04	Si
fin.	2	0	-67.04	-275			791	298	SLV 16	1.08	Si
ini.	2	0	-46.71	200			791	298	SLV 6	1.49	Si
fin.	2	0	3.32	-59			791	298	SLV 6	5.06	Si
ini.	2	0	-72.44	273			791	298	SLV 3	1.09	Si
fin.	2	0	18.6	146			791	298	SLV 3	2.04	Si
ini.	2	0	-77.89	307			791	298	SLV 2	0.97	No
fin.	2	0	25.38	120			791	298	SLV 2	2.49	Si
ini.	2	0	-46.71	200			791	298	SLV 5	1.49	Si
fin.	2	0	3.32	-59			791	298	SLV 5	5.06	Si
ini.	2	0	-77.89	307			791	298	SLV 1	0.97	No
fin.	2	0	25.38	120			791	298	SLV 1	2.49	Si
ini.	2	0	29.39	-112			791	298	SLV 13	2.65	Si
fin.	2	0	-60.25	-301			791	298	SLV 13	0.99	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	5.902	SLV 1	Si
V_SLV	0.97	SLV 1	No

## Trave di accoppiamento 9

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-30.668	-0.629	0.87	1.39	0.52	-31.668	-0.629	0.87	1.39	0.52	1	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	f <sub>hk</sub>	f <sub>vk0</sub>	f <sub>hmedio</sub>	τ <sub>0</sub>	f <sub>v0</sub>	μ	φ	f <sub>vk,lim</sub>	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	922	-65.47	575.81	SLV 11	8.79	Si
fin.	2	775	15.18	575.81	SLV 11	37.93	Si
ini.	2	520	-50.06	575.81	SLV 8	11.5	Si
fin.	2	405	1.9	575.81	SLV 8	303.42	Si
ini.	2	951	-58.82	575.81	SLV 14	9.79	Si
fin.	2	796	23.45	575.81	SLV 14	24.55	Si
ini.	2	245	-27.57	575.81	SLV 9	20.88	Si
fin.	2	143	4.06	575.81	SLV 9	141.66	Si
ini.	2	951	-58.82	575.81	SLV 13	9.79	Si
fin.	2	796	23.45	575.81	SLV 13	24.55	Si
ini.	2	922	-65.47	575.81	SLV 12	8.79	Si
fin.	2	775	15.18	575.81	SLV 12	37.93	Si
ini.	2	1155	-70.19	575.81	SLV 15	8.2	Si
fin.	2	985	26.79	575.81	SLV 15	21.5	Si
ini.	2	1155	-70.19	575.81	SLV 16	8.2	Si
fin.	2	985	26.79	575.81	SLV 16	21.5	Si
ini.	2	520	-50.06	575.81	SLV 7	11.5	Si
fin.	2	405	1.9	575.81	SLV 7	303.42	Si
ini.	2	245	-27.57	575.81	SLV 10	20.88	Si
fin.	2	143	4.06	575.81	SLV 10	141.66	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-7.45	158			601	226	SLV 1	1.43	Si
fin.	2	0	-20.82	-485			601	226	SLV 1	0.47	No
ini.	2	0	-70.19	496			601	226	SLV 15	0.46	No
fin.	2	0	26.79	-166			601	226	SLV 15	1.36	Si
ini.	2	0	-18.82	184			601	226	SLV 4	1.23	Si
fin.	2	0	-17.49	-473			601	226	SLV 4	0.48	No
ini.	2	0	-7.45	158			601	226	SLV 2	1.43	Si
fin.	2	0	-20.82	-485			601	226	SLV 2	0.47	No
ini.	2	0	-70.19	496			601	226	SLV 16	0.46	No
fin.	2	0	26.79	-166			601	226	SLV 16	1.36	Si



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-65.47	417			601	226	SLV 12	0.54	No
fin.	2	0	15.18	-260			601	226	SLV 12	0.87	No
ini.	2	0	-58.82	470			601	226	SLV 13	0.48	No
fin.	2	0	23.45	-178			601	226	SLV 13	1.27	Si
ini.	2	0	-18.82	184			601	226	SLV 3	1.23	Si
fin.	2	0	-17.49	-473			601	226	SLV 3	0.48	No
ini.	2	0	-58.82	470			601	226	SLV 14	0.48	No
fin.	2	0	23.45	-178			601	226	SLV 14	1.27	Si
ini.	2	0	-65.47	417			601	226	SLV 11	0.54	No
fin.	2	0	15.18	-260			601	226	SLV 11	0.87	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	8.204	SLV 15	Si
V_SLV	0.456	SLV 15	No

## Trave di accoppiamento 10

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-24.978	-0.629	0.76	1.39	0.63	-26.388	-0.629	0.76	1.39	0.63	1.41	0.3	3500

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb <sub>m</sub>	f <sub>hk</sub>	f <sub>vk0</sub>	f <sub>hmedio</sub>	τ <sub>0</sub>	f <sub>v0</sub>	μ	φ	f <sub>vk,lim</sub>	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

### Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	1000	-483.25	768.31	SLV 10	1.59	Si
fin.	2	1884	173.03	768.31	SLV 10	4.44	Si
ini.	2	637	-955.15	768.31	SLV 15	0.8	No
fin.	2	4243	859.59	768.31	SLV 15	0.89	No
ini.	2	1000	-483.25	768.31	SLV 9	1.59	Si
fin.	2	1884	173.03	768.31	SLV 9	4.44	Si
ini.	2	1181	-942.18	768.31	SLV 13	0.82	No
fin.	2	4425	693.69	768.31	SLV 13	1.11	Si
ini.	2	-1516	-146.06	768.31	SLV 8	5.26	Si
fin.	2	-1082	445.68	768.31	SLV 8	1.72	Si
ini.	2	-815	-526.46	768.31	SLV 11	1.46	Si
fin.	2	1278	726.05	768.31	SLV 11	1.06	Si
ini.	2	1181	-942.18	768.31	SLV 14	0.82	No
fin.	2	4425	693.69	768.31	SLV 14	1.11	Si
ini.	2	-815	-526.46	768.31	SLV 12	1.46	Si
fin.	2	1278	726.05	768.31	SLV 12	1.06	Si
ini.	2	637	-955.15	768.31	SLV 16	0.8	No
fin.	2	4243	859.59	768.31	SLV 16	0.89	No
ini.	2	-1516	-146.06	768.31	SLV 7	5.26	Si
fin.	2	-1082	445.68	768.31	SLV 7	1.72	Si

### Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-146.06	1600			728	274	SLV 7	0.17	No
fin.	2	0	445.68	-746			728	274	SLV 7	0.37	No
ini.	2	0	-955.15	1495			728	274	SLV 16	0.18	No
fin.	2	0	859.59	-518			728	274	SLV 16	0.53	No
ini.	2	0	-146.06	1600			728	274	SLV 8	0.17	No
fin.	2	0	445.68	-746			728	274	SLV 8	0.37	No
ini.	2	0	-955.15	1495			728	274	SLV 15	0.18	No
fin.	2	0	859.59	-518			728	274	SLV 15	0.53	No
ini.	2	0	-942.18	1359			728	274	SLV 13	0.2	No
fin.	2	0	693.69	-488			728	274	SLV 13	0.56	No
ini.	2	0	-942.18	1359			728	274	SLV 14	0.2	No
fin.	2	0	693.69	-488			728	274	SLV 14	0.56	No
ini.	2	0	312.88	1412			728	274	SLV 4	0.19	No
fin.	2	0	-74.97	-816			728	274	SLV 4	0.34	No
ini.	2	0	-526.46	1625			728	274	SLV 12	0.17	No
fin.	2	0	726.05	-656			728	274	SLV 12	0.42	No
ini.	2	0	312.88	1412			728	274	SLV 3	0.19	No
fin.	2	0	-74.97	-816			728	274	SLV 3	0.34	No
ini.	2	0	-526.46	1625			728	274	SLV 11	0.17	No
fin.	2	0	726.05	-656			728	274	SLV 11	0.42	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	0.804	SLV 15	No
V_SLV	0.169	SLV 11	No



## Trave di accoppiamento 11

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-26.838	-2.079	0.8	1.39	0.59	-26.838	-1.079	0.8	1.39	0.59	1	0.3	3500

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

f <sub>b</sub>	f <sub>hk</sub>	f <sub>vk0</sub>	f <sub>hmedio</sub>	τ <sub>0</sub>	f <sub>v0</sub>	μ	φ	f <sub>vk,lim</sub>	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

### Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-1509	-380.97	698.31	SLV 6	1.83	Si
fin.	2	-132	170.49	698.31	SLV 6	4.1	Si
ini.	2	1069	-260.96	698.31	SLV 7	2.68	Si
fin.	2	1646	-95.21	698.31	SLV 7	7.33	Si
ini.	2	1069	-260.96	698.31	SLV 8	2.68	Si
fin.	2	1646	-95.21	698.31	SLV 8	7.33	Si
ini.	2	-797	-424.79	698.31	SLV 2	1.64	Si
fin.	2	535	165.69	698.31	SLV 2	4.21	Si
ini.	2	-1346	-307.41	698.31	SLV 9	2.27	Si
fin.	2	-170	94.9	698.31	SLV 9	7.36	Si
ini.	2	-1346	-307.41	698.31	SLV 10	2.27	Si
fin.	2	-170	94.9	698.31	SLV 10	7.36	Si
ini.	2	-23	-388.79	698.31	SLV 3	1.8	Si
fin.	2	1069	85.98	698.31	SLV 3	8.12	Si
ini.	2	-23	-388.79	698.31	SLV 4	1.8	Si
fin.	2	1069	85.98	698.31	SLV 4	8.12	Si
ini.	2	-797	-424.79	698.31	SLV 1	1.64	Si
fin.	2	535	165.69	698.31	SLV 1	4.21	Si
ini.	2	-1509	-380.97	698.31	SLV 5	1.83	Si
fin.	2	-132	170.49	698.31	SLV 5	4.1	Si

### Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-424.79	2959			682	257	SLV 1	0.09	No
fin.	2	0	165.69	291			682	257	SLV 1	0.88	No
ini.	2	0	-388.79	2270			682	257	SLV 4	0.11	No
fin.	2	0	85.98	188			682	257	SLV 4	1.36	Si
ini.	2	0	-179.58	1723			682	257	SLV 13	0.15	No
fin.	2	0	-86.29	-179			682	257	SLV 13	1.43	Si
ini.	2	0	-307.41	2958			682	257	SLV 10	0.09	No
fin.	2	0	94.9	105			682	257	SLV 10	2.44	Si
ini.	2	0	-179.58	1723			682	257	SLV 14	0.15	No
fin.	2	0	-86.29	-179			682	257	SLV 14	1.43	Si
ini.	2	0	-424.79	2959			682	257	SLV 2	0.09	No
fin.	2	0	165.69	291			682	257	SLV 2	0.88	No
ini.	2	0	-307.41	2958			682	257	SLV 9	0.09	No
fin.	2	0	94.9	105			682	257	SLV 9	2.44	Si
ini.	2	0	-380.97	3329			682	257	SLV 5	0.08	No
fin.	2	0	170.49	246			682	257	SLV 5	1.04	Si
ini.	2	0	-380.97	3329			682	257	SLV 6	0.08	No
fin.	2	0	170.49	246			682	257	SLV 6	1.04	Si
ini.	2	0	-388.79	2270			682	257	SLV 3	0.11	No
fin.	2	0	85.98	188			682	257	SLV 3	1.36	Si

### Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.644	SLV 1	Si
V_SLV	0.077	SLV 5	No

## Trave di accoppiamento 12

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-34.183	-2.979	1.39	3.39	2	-34.183	-3.479	1.39	3.39	2	0.5	0.3	3500

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

f <sub>b</sub>	f <sub>hk</sub>	f <sub>vk0</sub>	f <sub>hmedio</sub>	τ <sub>0</sub>	f <sub>v0</sub>	μ	φ	f <sub>vk,lim</sub>	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

### Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	342	-317.04	3165.81	SLV 7	9.99	Si
fin.	2	-560	-200.16	3165.81	SLV 7	15.82	Si
ini.	2	342	-317.04	3165.81	SLV 8	9.99	Si
fin.	2	-560	-200.16	3165.81	SLV 8	15.82	Si
ini.	2	-215	399.59	3165.81	SLV 14	7.92	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
fin.	2	182	90.3	3165.81	SLV 14	35.06	Si
ini.	2	-218	546.36	3165.81	SLV 10	5.79	Si
fin.	2	439	226.01	3165.81	SLV 10	14.01	Si
ini.	2	-90	443.88	3165.81	SLV 6	7.13	Si
fin.	2	377	217.15	3165.81	SLV 6	14.58	Si
ini.	2	215	-214.56	3165.81	SLV 12	14.75	Si
fin.	2	-498	-191.3	3165.81	SLV 12	16.55	Si
ini.	2	-218	546.36	3165.81	SLV 9	5.79	Si
fin.	2	439	226.01	3165.81	SLV 9	14.01	Si
ini.	2	-215	399.59	3165.81	SLV 13	7.92	Si
fin.	2	182	90.3	3165.81	SLV 13	35.06	Si
ini.	2	215	-214.56	3165.81	SLV 11	14.75	Si
fin.	2	-498	-191.3	3165.81	SLV 11	16.55	Si
ini.	2	-90	443.88	3165.81	SLV 5	7.13	Si
fin.	2	377	217.15	3165.81	SLV 5	14.58	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	546.36	-2254			3466	1304	SLV 9	0.58	No
fin.	2	0	226.01	-227			3466	1304	SLV 9	5.76	Si
ini.	2	0	-170.27	144			3466	1304	SLV 3	9.04	Si
fin.	2	0	-64.45	2224			3466	1304	SLV 3	0.59	No
ini.	2	0	443.88	-1990			3466	1304	SLV 6	0.66	No
fin.	2	0	217.15	386			3466	1304	SLV 6	3.38	Si
ini.	2	0	58.01	-699			3466	1304	SLV 2	1.87	Si
fin.	2	0	60.75	1705			3466	1304	SLV 2	0.76	No
ini.	2	0	-317.04	819			3466	1304	SLV 7	1.59	Si
fin.	2	0	-200.16	2115			3466	1304	SLV 7	0.62	No
ini.	2	0	443.88	-1990			3466	1304	SLV 5	0.66	No
fin.	2	0	217.15	386			3466	1304	SLV 5	3.38	Si
ini.	2	0	-170.27	144			3466	1304	SLV 4	9.04	Si
fin.	2	0	-64.45	2224			3466	1304	SLV 4	0.59	No
ini.	2	0	-317.04	819			3466	1304	SLV 8	1.59	Si
fin.	2	0	-200.16	2115			3466	1304	SLV 8	0.62	No
ini.	2	0	546.36	-2254			3466	1304	SLV 10	0.58	No
fin.	2	0	226.01	-227			3466	1304	SLV 10	5.76	Si
ini.	2	0	58.01	-699			3466	1304	SLV 1	1.87	Si
fin.	2	0	60.75	1705			3466	1304	SLV 1	0.76	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	5.794	SLV 9	Si
V_SLV	0.579	SLV 9	No

## Trave di accoppiamento 13

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-34.183	-2.979	4.19	5.15	0.96	-34.183	-3.479	4.19	5.15	0.96	0.5	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fhk	fvk0	fhmedio	τ0	fv0	μ	φ	fvk,lim	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	114	-252.49	1345.81	SLV 4	5.33	Si
fin.	2	42	7.99	1345.81	SLV 4	168.41	Si
ini.	2	114	-252.49	1345.81	SLV 3	5.33	Si
fin.	2	42	7.99	1345.81	SLV 3	168.41	Si
ini.	2	792	-126.2	1345.81	SLV 10	10.66	Si
fin.	2	768	-39.42	1345.81	SLV 10	34.14	Si
ini.	2	939	-190.85	1345.81	SLV 6	7.05	Si
fin.	2	863	-31.68	1345.81	SLV 6	42.48	Si
ini.	2	-593	-169.64	1345.81	SLV 8	7.93	Si
fin.	2	-569	15.46	1345.81	SLV 8	87.02	Si
ini.	2	-593	-169.64	1345.81	SLV 7	7.93	Si
fin.	2	-569	15.46	1345.81	SLV 7	87.02	Si
ini.	2	574	-258.85	1345.81	SLV 2	5.2	Si
fin.	2	472	-6.15	1345.81	SLV 2	218.74	Si
ini.	2	792	-126.2	1345.81	SLV 9	10.66	Si
fin.	2	768	-39.42	1345.81	SLV 9	34.14	Si
ini.	2	939	-190.85	1345.81	SLV 5	7.05	Si
fin.	2	863	-31.68	1345.81	SLV 5	42.48	Si
ini.	2	574	-258.85	1345.81	SLV 1	5.2	Si
fin.	2	472	-6.15	1345.81	SLV 1	218.74	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-104.99	641			1664	626	SLV 11	0.98	No
fin.	2	0	7.73	444			1664	626	SLV 11	1.41	Si



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-258.85	548			1664	626	SLV 2	1.14	Si
fin.	2	0	-6.15	292			1664	626	SLV 2	2.14	Si
ini.	2	0	-104.99	641			1664	626	SLV 12	0.98	No
fin.	2	0	7.73	444			1664	626	SLV 12	1.41	Si
ini.	2	0	-252.49	752			1664	626	SLV 4	0.83	No
fin.	2	0	7.99	513			1664	626	SLV 4	1.22	Si
ini.	2	0	-169.64	803			1664	626	SLV 7	0.78	No
fin.	2	0	15.46	595			1664	626	SLV 7	1.05	Si
ini.	2	0	-258.85	548			1664	626	SLV 1	1.14	Si
fin.	2	0	-6.15	292			1664	626	SLV 1	2.14	Si
ini.	2	0	-252.49	752			1664	626	SLV 3	0.83	No
fin.	2	0	7.99	513			1664	626	SLV 3	1.22	Si
ini.	2	0	-169.64	803			1664	626	SLV 8	0.78	No
fin.	2	0	15.46	595			1664	626	SLV 8	1.05	Si
ini.	2	0	-126.2	-41			1664	626	SLV 10	15.34	Si
fin.	2	0	-39.42	-295			1664	626	SLV 10	2.12	Si
ini.	2	0	-126.2	-41			1664	626	SLV 9	15.34	Si
fin.	2	0	-39.42	-295			1664	626	SLV 9	2.12	Si

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	5.199	SLV 1	Si
V_SLV	0.78	SLV 7	No

## Trave di accoppiamento 14

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-34.183	-0.829	1.39	2.39	1	-34.183	-1.829	1.39	2.39	1	1	0.3	3500

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	fhk	fvk0	fmedio	t0	f0	μ	φ	fvk,lim	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

### Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-484	384.56	1415.81	SLV 5	3.68	Si
fin.	2	837	-568	1415.81	SLV 5	2.49	Si
ini.	2	-484	384.56	1415.81	SLV 6	3.68	Si
fin.	2	837	-568	1415.81	SLV 6	2.49	Si
ini.	2	-811	331.74	1415.81	SLV 13	4.27	Si
fin.	2	-392	-174.95	1415.81	SLV 13	8.09	Si
ini.	2	290	-7.66	1415.81	SLV 2	184.93	Si
fin.	2	1039	-348.35	1415.81	SLV 2	4.06	Si
ini.	2	626	-396.67	1415.81	SLV 7	3.57	Si
fin.	2	-17	232.98	1415.81	SLV 7	6.08	Si
ini.	2	-811	331.74	1415.81	SLV 14	4.27	Si
fin.	2	-392	-174.95	1415.81	SLV 14	8.09	Si
ini.	2	626	-396.67	1415.81	SLV 8	3.57	Si
fin.	2	-17	232.98	1415.81	SLV 8	6.08	Si
ini.	2	-814	486.38	1415.81	SLV 10	2.91	Si
fin.	2	408	-515.99	1415.81	SLV 10	2.74	Si
ini.	2	290	-7.66	1415.81	SLV 1	184.93	Si
fin.	2	1039	-348.35	1415.81	SLV 1	4.06	Si
ini.	2	-814	486.38	1415.81	SLV 9	2.91	Si
fin.	2	408	-515.99	1415.81	SLV 9	2.74	Si

### Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-294.85	662			1733	652	SLV 11	0.98	No
fin.	2	0	285	608			1733	652	SLV 11	1.07	Si
ini.	2	0	-396.67	925			1733	652	SLV 7	0.71	No
fin.	2	0	232.98	746			1733	652	SLV 7	0.87	No
ini.	2	0	486.38	-1552			1733	652	SLV 10	0.42	No
fin.	2	0	-515.99	-1610			1733	652	SLV 10	0.4	No
ini.	2	0	384.56	-1290			1733	652	SLV 5	0.51	No
fin.	2	0	-568	-1472			1733	652	SLV 5	0.44	No
ini.	2	0	-294.85	662			1733	652	SLV 12	0.98	No
fin.	2	0	285	608			1733	652	SLV 12	1.07	Si
ini.	2	0	384.56	-1290			1733	652	SLV 6	0.51	No
fin.	2	0	-568	-1472			1733	652	SLV 6	0.44	No
ini.	2	0	331.74	-1084			1733	652	SLV 13	0.6	No
fin.	2	0	-174.95	-995			1733	652	SLV 13	0.66	No
ini.	2	0	331.74	-1084			1733	652	SLV 14	0.6	No
fin.	2	0	-174.95	-995			1733	652	SLV 14	0.66	No
ini.	2	0	486.38	-1552			1733	652	SLV 9	0.42	No
fin.	2	0	-515.99	-1610			1733	652	SLV 9	0.4	No
ini.	2	0	-396.67	925			1733	652	SLV 8	0.71	No
fin.	2	0	232.98	746			1733	652	SLV 8	0.87	No





Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	2.493	SLV 5	Si
V_SLV	0.405	SLV 9	No

## Trave di accoppiamento 15

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

## Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-34.183	-0.829	4.29	5.15	0.86	-34.183	-1.829	4.29	5.15	0.86	1	0.3	3500

## Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb <sub>u</sub>	f <sub>hk</sub>	f <sub>vk0</sub>	f <sub>hmedio</sub>	τ <sub>0</sub>	f <sub>v0</sub>	μ	φ	f <sub>vk,lim</sub>	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

## Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	γM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	1056	-340.58	1170.81	SLV 8	3.44	Si
fin.	2	300	205.82	1170.81	SLV 8	5.69	Si
ini.	2	-1684	618.16	1170.81	SLV 14	1.89	Si
fin.	2	-992	-541.14	1170.81	SLV 14	2.16	Si
ini.	2	1056	-340.58	1170.81	SLV 7	3.44	Si
fin.	2	300	205.82	1170.81	SLV 7	5.69	Si
ini.	2	846	479.38	1170.81	SLV 2	2.44	Si
fin.	2	515	-270.81	1170.81	SLV 2	4.32	Si
ini.	2	-1389	1037.26	1170.81	SLV 10	1.13	Si
fin.	2	-633	-754.12	1170.81	SLV 10	1.55	Si
ini.	2	846	479.38	1170.81	SLV 1	2.44	Si
fin.	2	515	-270.81	1170.81	SLV 1	4.32	Si
ini.	2	-1389	1037.26	1170.81	SLV 9	1.13	Si
fin.	2	-633	-754.12	1170.81	SLV 9	1.55	Si
ini.	2	-1684	618.16	1170.81	SLV 13	1.89	Si
fin.	2	-992	-541.14	1170.81	SLV 13	2.16	Si
ini.	2	-630	995.62	1170.81	SLV 5	1.18	Si
fin.	2	-181	-673.02	1170.81	SLV 5	1.74	Si
ini.	2	-630	995.62	1170.81	SLV 6	1.18	Si
fin.	2	-181	-673.02	1170.81	SLV 6	1.74	Si

## Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	γM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	995.62	-1243			1282	482	SLV 5	0.39	No
fin.	2	0	-673.02	-1645			1282	482	SLV 5	0.29	No
ini.	2	0	1037.26	-1541			1282	482	SLV 9	0.31	No
fin.	2	0	-754.12	-1931			1282	482	SLV 9	0.25	No
ini.	2	0	217.3	-605			1282	482	SLV 15	0.8	No
fin.	2	0	-277.49	-995			1282	482	SLV 15	0.49	No
ini.	2	0	995.62	-1243			1282	482	SLV 6	0.39	No
fin.	2	0	-673.02	-1645			1282	482	SLV 6	0.29	No
ini.	2	0	618.16	-1197			1282	482	SLV 13	0.4	No
fin.	2	0	-541.14	-1581			1282	482	SLV 13	0.31	No
ini.	2	0	-340.58	729			1282	482	SLV 7	0.66	No
fin.	2	0	205.82	308			1282	482	SLV 7	1.56	Si
ini.	2	0	618.16	-1197			1282	482	SLV 14	0.4	No
fin.	2	0	-541.14	-1581			1282	482	SLV 14	0.31	No
ini.	2	0	217.3	-605			1282	482	SLV 16	0.8	No
fin.	2	0	-277.49	-995			1282	482	SLV 16	0.49	No
ini.	2	0	1037.26	-1541			1282	482	SLV 10	0.31	No
fin.	2	0	-754.12	-1931			1282	482	SLV 10	0.25	No
ini.	2	0	-340.58	729			1282	482	SLV 8	0.66	No
fin.	2	0	205.82	308			1282	482	SLV 8	1.56	Si

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.129	SLV 9	Si
V_SLV	0.25	SLV 9	No

## Trave di accoppiamento 16

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

## Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-34.183	3.931	1.39	2.39	1	-34.183	2.931	1.39	2.39	1	1	0.3	3500

## Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb <sub>u</sub>	f <sub>hk</sub>	f <sub>vk0</sub>	f <sub>hmedio</sub>	τ <sub>0</sub>	f <sub>v0</sub>	μ	φ	f <sub>vk,lim</sub>	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2



## Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-396	241.29	1415.81	SLV 6	5.87	Si
fin.	2	279	-390.06	1415.81	SLV 6	3.63	Si
ini.	2	-754	342.07	1415.81	SLV 9	4.14	Si
fin.	2	-213	-325.4	1415.81	SLV 9	4.35	Si
ini.	2	-396	241.29	1415.81	SLV 5	5.87	Si
fin.	2	279	-390.06	1415.81	SLV 5	3.63	Si
ini.	2	679	-378.37	1415.81	SLV 3	3.74	Si
fin.	2	493	20.09	1415.81	SLV 3	70.49	Si
ini.	2	259	-430.37	1415.81	SLV 11	3.29	Si
fin.	2	-764	421.64	1415.81	SLV 11	3.36	Si
ini.	2	679	-378.37	1415.81	SLV 4	3.74	Si
fin.	2	493	20.09	1415.81	SLV 4	70.49	Si
ini.	2	616	-531.15	1415.81	SLV 8	2.67	Si
fin.	2	-273	356.98	1415.81	SLV 8	3.97	Si
ini.	2	259	-430.37	1415.81	SLV 12	3.29	Si
fin.	2	-764	421.64	1415.81	SLV 12	3.36	Si
ini.	2	-754	342.07	1415.81	SLV 10	4.14	Si
fin.	2	-213	-325.4	1415.81	SLV 10	4.35	Si
ini.	2	616	-531.15	1415.81	SLV 7	2.67	Si
fin.	2	-273	356.98	1415.81	SLV 7	3.97	Si

## Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-42.45	1126			1733	652	SLV 15	0.58	No
fin.	2	0	235.61	-283			1733	652	SLV 15	2.31	Si
ini.	2	0	-430.37	1795			1733	652	SLV 12	0.36	No
fin.	2	0	421.64	992			1733	652	SLV 12	0.66	No
ini.	2	0	342.07	-582			1733	652	SLV 9	1.12	Si
fin.	2	0	-325.4	-1697			1733	652	SLV 9	0.38	No
ini.	2	0	342.07	-582			1733	652	SLV 10	1.12	Si
fin.	2	0	-325.4	-1697			1733	652	SLV 10	0.38	No
ini.	2	0	-42.45	1126			1733	652	SLV 16	0.58	No
fin.	2	0	235.61	-283			1733	652	SLV 16	2.31	Si
ini.	2	0	-430.37	1795			1733	652	SLV 11	0.36	No
fin.	2	0	421.64	992			1733	652	SLV 11	0.66	No
ini.	2	0	-531.15	1656			1733	652	SLV 8	0.39	No
fin.	2	0	356.98	1278			1733	652	SLV 8	0.51	No
ini.	2	0	-531.15	1656			1733	652	SLV 7	0.39	No
fin.	2	0	356.98	1278			1733	652	SLV 7	0.51	No
ini.	2	0	241.29	-721			1733	652	SLV 6	0.9	No
fin.	2	0	-390.06	-1411			1733	652	SLV 6	0.46	No
ini.	2	0	241.29	-721			1733	652	SLV 5	0.9	No
fin.	2	0	-390.06	-1411			1733	652	SLV 5	0.46	No

## Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	2.666	SLV 7	Si
V_SLV	0.363	SLV 11	No

## Trave di accoppiamento 17

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-34.183	3.931	4.29	5.15	0.86	-34.183	2.931	4.29	5.15	0.86	1	0.3	3500

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb <sub>m</sub>	f <sub>hk</sub>	f <sub>vk0</sub>	f <sub>hmedio</sub>	τ <sub>0</sub>	f <sub>v0</sub>	μ	φ	f <sub>vk,lim</sub>	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

## Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-825	-530.23	1170.81	SLV 11	2.21	Si
fin.	2	-737	787.1	1170.81	SLV 11	1.49	Si
ini.	2	-265	-453.17	1170.81	SLV 8	2.58	Si
fin.	2	-377	818.04	1170.81	SLV 8	1.43	Si
ini.	2	511	280.14	1170.81	SLV 5	4.18	Si
fin.	2	423	-426.85	1170.81	SLV 5	2.74	Si
ini.	2	511	280.14	1170.81	SLV 6	4.18	Si
fin.	2	423	-426.85	1170.81	SLV 6	2.74	Si
ini.	2	660	-106.62	1170.81	SLV 4	10.98	Si
fin.	2	322	418.43	1170.81	SLV 4	2.8	Si
ini.	2	-825	-530.23	1170.81	SLV 12	2.21	Si
fin.	2	-737	787.1	1170.81	SLV 12	1.49	Si
ini.	2	-49	203.09	1170.81	SLV 10	5.77	Si
fin.	2	63	-457.79	1170.81	SLV 10	2.56	Si
ini.	2	660	-106.62	1170.81	SLV 3	10.98	Si
fin.	2	322	418.43	1170.81	SLV 3	2.8	Si
ini.	2	-49	203.09	1170.81	SLV 9	5.77	Si
fin.	2	63	-457.79	1170.81	SLV 9	2.56	Si
ini.	2	-265	-453.17	1170.81	SLV 7	2.58	Si



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
fin.	2	-377	818.04	1170.81	SLV 7	1.43	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-453.17	1602			1282	482	SLV 7	0.3	No
fin.	2	0	818.04	1080			1282	482	SLV 7	0.45	No
ini.	2	0	-453.17	1602			1282	482	SLV 8	0.3	No
fin.	2	0	818.04	1080			1282	482	SLV 8	0.45	No
ini.	2	0	-106.62	1296			1282	482	SLV 3	0.37	No
fin.	2	0	418.43	272			1282	482	SLV 3	1.77	Si
ini.	2	0	280.14	-132			1282	482	SLV 6	3.64	Si
fin.	2	0	-426.85	-962			1282	482	SLV 6	0.5	No
ini.	2	0	-106.62	1296			1282	482	SLV 4	0.37	No
fin.	2	0	418.43	272			1282	482	SLV 4	1.77	Si
ini.	2	0	280.14	-132			1282	482	SLV 5	3.64	Si
fin.	2	0	-426.85	-962			1282	482	SLV 5	0.5	No
ini.	2	0	203.09	-390			1282	482	SLV 9	1.24	Si
fin.	2	0	-457.79	-882			1282	482	SLV 9	0.55	No
ini.	2	0	203.09	-390			1282	482	SLV 10	1.24	Si
fin.	2	0	-457.79	-882			1282	482	SLV 10	0.55	No
ini.	2	0	-530.23	1344			1282	482	SLV 12	0.36	No
fin.	2	0	787.1	1160			1282	482	SLV 12	0.42	No
ini.	2	0	-530.23	1344			1282	482	SLV 11	0.36	No
fin.	2	0	787.1	1160			1282	482	SLV 11	0.42	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.431	SLV 7	Si
V_SLV	0.301	SLV 7	No

## Trave di accoppiamento 18

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-33.043	5.726	4.16	5.15	0.99	-30.833	5.726	4.16	5.15	0.99	2.21	0.3	3500

Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	f <sub>hk</sub>	f <sub>vk0</sub>	f <sub>hmedio</sub>	τ <sub>0</sub>	f <sub>v0</sub>	μ	φ	f <sub>vk,lim</sub>	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-169	-697.93	1398.31	SLV 3	2	Si
fin.	2	1049	492.24	1398.31	SLV 3	2.84	Si
ini.	2	-768	-766.34	1398.31	SLV 1	1.82	Si
fin.	2	328	435.64	1398.31	SLV 1	3.21	Si
ini.	2	337	820.06	1398.31	SLV 16	1.71	Si
fin.	2	-759	-1160.57	1398.31	SLV 16	1.2	Si
ini.	2	-1137	140.55	1398.31	SLV 9	9.95	Si
fin.	2	-1687	-704.72	1398.31	SLV 9	1.98	Si
ini.	2	-1137	140.55	1398.31	SLV 10	9.95	Si
fin.	2	-1687	-704.72	1398.31	SLV 10	1.98	Si
ini.	2	-169	-697.93	1398.31	SLV 4	2	Si
fin.	2	1049	492.24	1398.31	SLV 4	2.84	Si
ini.	2	-768	-766.34	1398.31	SLV 2	1.82	Si
fin.	2	328	435.64	1398.31	SLV 2	3.21	Si
ini.	2	337	820.06	1398.31	SLV 15	1.71	Si
fin.	2	-759	-1160.57	1398.31	SLV 15	1.2	Si
ini.	2	-262	751.65	1398.31	SLV 14	1.86	Si
fin.	2	-1479	-1217.17	1398.31	SLV 14	1.15	Si
ini.	2	-262	751.65	1398.31	SLV 13	1.86	Si
fin.	2	-1479	-1217.17	1398.31	SLV 13	1.15	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	368.57	556			1144	430	SLV 12	0.77	No
fin.	2	0	-516.05	-2205			1144	430	SLV 12	0.2	No
ini.	2	0	820.06	331			1144	430	SLV 16	1.3	Si
fin.	2	0	-1160.57	-2539			1144	430	SLV 16	0.17	No
ini.	2	0	820.06	331			1144	430	SLV 15	1.3	Si
fin.	2	0	-1160.57	-2539			1144	430	SLV 15	0.17	No
ini.	2	0	-766.34	2272			1144	430	SLV 2	0.19	No
fin.	2	0	435.64	-645			1144	430	SLV 2	0.67	No
ini.	2	0	751.65	630			1144	430	SLV 14	0.68	No
fin.	2	0	-1217.17	-2321			1144	430	SLV 14	0.19	No
ini.	2	0	-314.85	2046			1144	430	SLV 5	0.21	No
fin.	2	0	-208.88	-978			1144	430	SLV 5	0.44	No
ini.	2	0	-314.85	2046			1144	430	SLV 6	0.21	No
fin.	2	0	-208.88	-978			1144	430	SLV 6	0.44	No
ini.	2	0	368.57	556			1144	430	SLV 11	0.77	No
fin.	2	0	-516.05	-2205			1144	430	SLV 11	0.2	No



Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-766.34	2272			1144	430	SLV 1	0.19	No
fin.	2	0	435.64	-645			1144	430	SLV 1	0.67	No
ini.	2	0	751.65	630			1144	430	SLV 13	0.68	No
fin.	2	0	-1217.17	-2321			1144	430	SLV 13	0.19	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.149	SLV 13	Si
V_SLV	0.17	SLV 15	No

## Trave di accoppiamento 19

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-28.373	5.726	4.16	5.15	0.99	-26.163	5.726	4.16	5.15	0.99	2.21	0.3	3500

### Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

f <sub>b</sub>	f <sub>mk</sub>	f <sub>vk0</sub>	f <sub>hmedio</sub>	τ <sub>0</sub>	f <sub>v0</sub>	μ	φ	f <sub>vk,lim</sub>	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

### Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	727	500.21	1398.31	SLV 16	2.8	Si
fin.	2	-263	-885.92	1398.31	SLV 16	1.58	Si
ini.	2	-12	468.27	1398.31	SLV 13	2.99	Si
fin.	2	-886	-940.89	1398.31	SLV 13	1.49	Si
ini.	2	-448	-1202	1398.31	SLV 3	1.16	Si
fin.	2	426	816.81	1398.31	SLV 3	1.71	Si
ini.	2	727	500.21	1398.31	SLV 15	2.8	Si
fin.	2	-263	-885.92	1398.31	SLV 15	1.58	Si
ini.	2	-1637	-675.41	1398.31	SLV 5	2.07	Si
fin.	2	-1164	101.75	1398.31	SLV 5	13.74	Si
ini.	2	-12	468.27	1398.31	SLV 14	2.99	Si
fin.	2	-886	-940.89	1398.31	SLV 14	1.49	Si
ini.	2	-1186	-1233.93	1398.31	SLV 2	1.13	Si
fin.	2	-196	761.84	1398.31	SLV 2	1.84	Si
ini.	2	-1637	-675.41	1398.31	SLV 6	2.07	Si
fin.	2	-1164	101.75	1398.31	SLV 6	13.74	Si
ini.	2	-448	-1202	1398.31	SLV 4	1.16	Si
fin.	2	426	816.81	1398.31	SLV 4	1.71	Si
ini.	2	-1186	-1233.93	1398.31	SLV 1	1.13	Si
fin.	2	-196	761.84	1398.31	SLV 1	1.84	Si

### Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	468.27	815			1144	430	SLV 13	0.53	No
fin.	2	0	-940.89	-2118			1144	430	SLV 13	0.2	No
ini.	2	0	468.27	815			1144	430	SLV 14	0.53	No
fin.	2	0	-940.89	-2118			1144	430	SLV 14	0.2	No
ini.	2	0	-1233.93	2569			1144	430	SLV 2	0.17	No
fin.	2	0	761.84	-366			1144	430	SLV 2	1.18	Si
ini.	2	0	-1202	2398			1144	430	SLV 3	0.18	No
fin.	2	0	816.81	-289			1144	430	SLV 3	1.49	Si
ini.	2	0	-1233.93	2569			1144	430	SLV 1	0.17	No
fin.	2	0	761.84	-366			1144	430	SLV 1	1.18	Si
ini.	2	0	-675.41	2155			1144	430	SLV 5	0.2	No
fin.	2	0	101.75	-1068			1144	430	SLV 5	0.4	No
ini.	2	0	500.21	644			1144	430	SLV 16	0.67	No
fin.	2	0	-885.92	-2042			1144	430	SLV 16	0.21	No
ini.	2	0	-1202	2398			1144	430	SLV 4	0.18	No
fin.	2	0	816.81	-289			1144	430	SLV 4	1.49	Si
ini.	2	0	500.21	644			1144	430	SLV 15	0.67	No
fin.	2	0	-885.92	-2042			1144	430	SLV 15	0.21	No
ini.	2	0	-675.41	2155			1144	430	SLV 6	0.2	No
fin.	2	0	101.75	-1068			1144	430	SLV 6	0.4	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	1.133	SLV 1	Si
V_SLV	0.168	SLV 1	No

## Trave di accoppiamento 20

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-26.838	-3.254	3.39	5.15	1.76	-26.838	-2.254	3.39	5.15	1.76	1	0.14	3500



## Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	f <sub>hk</sub>	f <sub>vk0</sub>	f <sub>hmedio</sub>	t <sub>0</sub>	f <sub>v0</sub>	μ	φ	f <sub>vk,lim</sub>	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

## Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-916	-91.9	2363.89	SLV 11	25.72	Si
fin.	2	-42	-4579.73	2363.89	SLV 11	0.52	No
ini.	2	1124	-780.48	2363.89	SLV 1	3.03	Si
fin.	2	1291	-3071.27	2363.89	SLV 1	0.77	No
ini.	2	-441	-535.63	2363.89	SLV 15	4.41	Si
fin.	2	-607	-2290.35	2363.89	SLV 15	1.03	Si
ini.	2	450	-431.41	2363.89	SLV 3	5.48	Si
fin.	2	1225	-4400.54	2363.89	SLV 3	0.54	No
ini.	2	-441	-535.63	2363.89	SLV 16	4.41	Si
fin.	2	-607	-2290.35	2363.89	SLV 16	1.03	Si
ini.	2	-649	-60.63	2363.89	SLV 7	38.99	Si
fin.	2	507	-5212.79	2363.89	SLV 7	0.45	No
ini.	2	1124	-780.48	2363.89	SLV 2	3.03	Si
fin.	2	1291	-3071.27	2363.89	SLV 2	0.77	No
ini.	2	-916	-91.9	2363.89	SLV 12	25.72	Si
fin.	2	-42	-4579.73	2363.89	SLV 12	0.52	No
ini.	2	450	-431.41	2363.89	SLV 4	5.48	Si
fin.	2	1225	-4400.54	2363.89	SLV 4	0.54	No
ini.	2	-649	-60.63	2363.89	SLV 8	38.99	Si
fin.	2	507	-5212.79	2363.89	SLV 8	0.45	No

## Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-780.48	-2539			1423	536	SLV 1	0.21	No
fin.	2	0	-3071.27	-2540			1423	536	SLV 1	0.21	No
ini.	2	0	-780.48	-2539			1423	536	SLV 2	0.21	No
fin.	2	0	-3071.27	-2540			1423	536	SLV 2	0.21	No
ini.	2	0	-91.9	-3861			1423	536	SLV 11	0.14	No
fin.	2	0	-4579.73	-4246			1423	536	SLV 11	0.13	No
ini.	2	0	-535.63	-1180			1423	536	SLV 15	0.45	No
fin.	2	0	-2290.35	-1938			1423	536	SLV 15	0.28	No
ini.	2	0	-60.63	-4705			1423	536	SLV 8	0.11	No
fin.	2	0	-5212.79	-4842			1423	536	SLV 8	0.11	No
ini.	2	0	-431.41	-3993			1423	536	SLV 4	0.13	No
fin.	2	0	-4400.54	-3923			1423	536	SLV 4	0.14	No
ini.	2	0	-91.9	-3861			1423	536	SLV 12	0.14	No
fin.	2	0	-4579.73	-4246			1423	536	SLV 12	0.13	No
ini.	2	0	-535.63	-1180			1423	536	SLV 16	0.45	No
fin.	2	0	-2290.35	-1938			1423	536	SLV 16	0.28	No
ini.	2	0	-60.63	-4705			1423	536	SLV 7	0.11	No
fin.	2	0	-5212.79	-4842			1423	536	SLV 7	0.11	No
ini.	2	0	-431.41	-3993			1423	536	SLV 3	0.13	No
fin.	2	0	-4400.54	-3923			1423	536	SLV 3	0.14	No

## Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	0.453	SLV 7	No
V_SLV	0.111	SLV 7	No

## Trave di accoppiamento 21

Verifiche condotte secondo D.M. 17-01-18 (N.T.C.)

### Dati geometrici

X ini.	Y ini.	Z ini.inf.	Z ini.sup.	H ini.	X fin.	Y fin.	Z fin.inf.	Z fin.sup.	H fin.	Luce	Spessore	R. Trazione
-25.183	-0.614	3.39	5.15	1.76	-25.983	-0.614	3.39	5.15	1.76	0.8	0.14	3500

## Caratteristiche del materiale

(Circolare 7 21-01-19 C8.5.I) Muratura in mattoni pieni e malta di calce LC2\_Corti

fb	f <sub>hk</sub>	f <sub>vk0</sub>	f <sub>hmedio</sub>	t <sub>0</sub>	f <sub>v0</sub>	μ	φ	f <sub>vk,lim</sub>	E	G	FC
120000			172500	9000	20000	0.577	0.767	6500	320000000	128000000	1.2

## Verifiche a pressoflessione delle travi in muratura in combinazioni sismiche

Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
ini.	2	-2563	-1366.62	2363.89	SLV 16	1.73	Si
fin.	2	-3557	2216.49	2363.89	SLV 16	1.07	Si
ini.	2	-355	-1924.18	2363.89	SLV 1	1.23	Si
fin.	2	-4936	-4087.02	2363.89	SLV 1	0.58	No
ini.	2	-684	-1209.95	2363.89	SLV 3	1.95	Si
fin.	2	-6290	-3995.21	2363.89	SLV 3	0.59	No
ini.	2	-2563	-1366.62	2363.89	SLV 15	1.73	Si
fin.	2	-3557	2216.49	2363.89	SLV 15	1.07	Si
ini.	2	-355	-1924.18	2363.89	SLV 2	1.23	Si
fin.	2	-4936	-4087.02	2363.89	SLV 2	0.58	No
ini.	2	-684	-1209.95	2363.89	SLV 4	1.95	Si
fin.	2	-6290	-3995.21	2363.89	SLV 4	0.59	No
ini.	2	-1193	-2859.3	2363.89	SLV 10	0.83	No



Sezione	yM	N	M	Mu	Comb.	c.s.	Verifica
fin.	2	-1579	-156.52	2363.89	SLV 10	15.1	Si
ini.	2	-629	-2812.29	2363.89	SLV 5	0.84	No
fin.	2	-2399	-2020.03	2363.89	SLV 5	1.17	Si
ini.	2	-1193	-2859.3	2363.89	SLV 9	0.83	No
fin.	2	-1579	-156.52	2363.89	SLV 9	15.1	Si
ini.	2	-629	-2812.29	2363.89	SLV 6	0.84	No
fin.	2	-2399	-2020.03	2363.89	SLV 6	1.17	Si

Verifiche a taglio delle travi in muratura secondo §C8.7.1.3.1 in combinazioni sismiche

Sezione	yM	N	M	V	Vt	Vp	Vt fess. diag.	Vt,lim	Comb.	c.s.	Verifica
ini.	2	0	-1209.95	-8805			1423	536	SLV 4	0.06	No
fin.	2	0	-3995.21	-9575			1423	536	SLV 4	0.06	No
ini.	2	0	-1209.95	-8805			1423	536	SLV 3	0.06	No
fin.	2	0	-3995.21	-9575			1423	536	SLV 3	0.06	No
ini.	2	0	-1924.18	-7934			1423	536	SLV 1	0.07	No
fin.	2	0	-4087.02	-8693			1423	536	SLV 1	0.06	No
ini.	2	0	-2080.86	4155			1423	536	SLV 13	0.13	No
fin.	2	0	2124.68	3434			1423	536	SLV 13	0.16	No
ini.	2	0	-2080.86	4155			1423	536	SLV 14	0.13	No
fin.	2	0	2124.68	3434			1423	536	SLV 14	0.16	No
ini.	2	0	-1924.18	-7934			1423	536	SLV 2	0.07	No
fin.	2	0	-4087.02	-8693			1423	536	SLV 2	0.06	No
ini.	2	0	-2812.29	-2687			1423	536	SLV 5	0.2	No
fin.	2	0	-2020.03	-3420			1423	536	SLV 5	0.16	No
ini.	2	0	-431.51	-5589			1423	536	SLV 7	0.1	No
fin.	2	0	-1714.01	-6359			1423	536	SLV 7	0.08	No
ini.	2	0	-2812.29	-2687			1423	536	SLV 6	0.2	No
fin.	2	0	-2020.03	-3420			1423	536	SLV 6	0.16	No
ini.	2	0	-431.51	-5589			1423	536	SLV 8	0.1	No
fin.	2	0	-1714.01	-6359			1423	536	SLV 8	0.08	No

Tabella dei coefficienti di sicurezza minimi

Stato limite	Coeff.s.	Comb.	Verifica
PF_SLV	0.578	SLV 1	No
V_SLV	0.056	SLV 3	No