

COMUNE DI PIACENZA

**NUOVO POLO BIBLIOTECARIO
VIALE DANTE**

**Viale Dante Alighieri n.46,
Piacenza**

**Intervento cofinanziato dalla Regione Emilia Romagna
con Fondi ATUSS - PR FESR EMILIA-ROMAGNA 2021-2027**

Priorità 4 Attrattività, coesione e sviluppo territoriale

**Obiettivo Specifico 5.1 Promuovere lo sviluppo sociale, economico e
ambientale integrato e inclusivo a livello locale, la cultura, il patrimonio
naturale, il turismo sostenibile e la sicurezza nelle aree urbane**

**Azione 5.1.1 Attuazione delle Agende Trasformative Urbane per lo Sviluppo
Sostenibile (ATUSS)**

**PROGETTO ESECUTIVO
(art.33 e 36. DPR n.207/2010)**

CUP: E33D21004310005

PROGETTO STRUTTURALE

RELAZIONE DI CALCOLO STRUTTURALE

COMMITTENTE:

COMUNE DI PIACENZA

Settore Sviluppo del Patrimonio - Servizio Lavori Pubblici

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Dirigente del Settore: ING. ENRICO MARI

RUP: ING. GIOVANNI CARINI

PROGETTISTA:

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**PROGETTO ESECUTIVO
NUOVO POLO BIBLIOTECARIO
VIALE DANTE**

**ELABORATO
ST R1**

Data: 09/10/2023

COMMITTENTE : **COMUNE DI PIACENZA**

OPERA : **NUOVO POLO BIBLIOTECARIO IN VIALE DANTE ALIGHIERI
N.46 A PIACENZA**

OGGETTO : **RELAZIONE DI CALCOLO STRUTTURALE**

Il progettista delle strutture

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DESCRIZIONE GENERALE DELLA STRUTTURA

Trattasi di edificio in cemento armato di nuova realizzazione ad uso biblioteca in via Dante Alighieri n.46 nel Comune di Piacenza (PC). La struttura è a pianta rettangolare di dimensioni 16.86x18.05 m. rispetto al filo esterno dei pilastri ed è costituito dai seguenti impalcati :

- Piano terra
- Piano copertura

Il piano terra è realizzato con una platea dello spessore di 40 cm. che si sviluppa per tutta la superficie del fabbricato.

La copertura è realizzata con solai in lastre tralicciate semi prefabbricate di larghezza nominale di 120 cm. ed altezza 24 cm. alleggeriti con pani di polistirene di spessore 114 cm. . Questo solaio è vincolato alle travi centrali e laterali si copertura mediante opportuna armatura di 2° fase.

I pilastri sono realizzati in cemento armato ed hanno le seguenti dimensioni in sezione :

- Pilastri centrali : 30x30 cm.
- Pilastri perimetrali : 50x25 cm. , 90x25 cm , 50x30 cm.

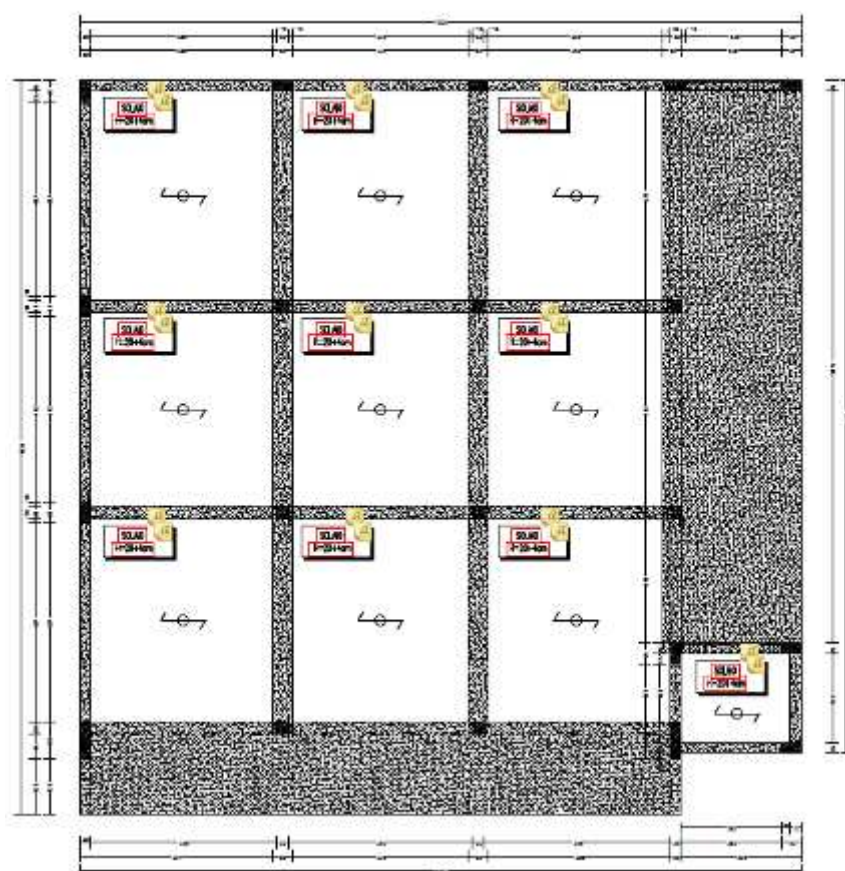
La maglia strutturale risulta essere costituita da 3 campate + una a sbalzo in direzione travi di copertura e da 3 campate + una a sbalzo in direzione solai di copertura.

Le travi di copertura hanno le seguenti dimensioni in sezione :

- Travi centrali : 50x24 cm.
- Travi laterali principali : 35x24 cm. e 85x24 cm.
- Travi laterali secondarie : 30x24 cm. e 25x24 cm.

Si riporta nella figura sottostante la pianta copertura :

PIANTA COPERTURA



NORMATIVE DI RIFERIMENTO

Il calcolo delle strutture in c.a. relative alla costruzioni in oggetto è effettuato in conformità alla normativa vigente ed in particolare:

- **D.M. 17/01/2018** – *“Norme tecniche per le costruzioni”*.
- **Circolare 21/01/2019** - *"Istruzioni per l'applicazione dell'aggiornamento delle "Norme tecniche per le costruzioni" di cui al D.M. 17/01/2018.*
- **Legge 05/11/1971, n. 1086** -

Norme per la disciplina delle opere in conglomerato cementizio armato, normale e precompresso ed a struttura metallica.

Si fa anche riferimento ai seguenti documenti di comprovata validità:

UNI EN 1992-1-1 (Eurocodice 2): *“Progettazione delle strutture di calcestruzzo”*

DEFINIZIONE DEI PARAMETRI DI PROGETTO ED AZIONI SULLA COSTRUZIONE

La struttura ricade all'interno del territorio comunale di Piacenza (PC) .

Lo spettro assunto a progetto per il sisma è stato dedotto in conformità a quanto riportato nelle NTC 2018.

SPETTRI DI RISPOSTA E DIAGRAMMI

In ottemperanza al punto 2.4.3. delle NTC 2018 l'azione sismica viene valutata in relazione ai seguenti

parametri:

periodo di riferimento: $V_R = V_N \times C_U = 50$ anni

vita nominale: $V_N = 50$ anni

classe d'uso: II

coefficiente d'uso: $C_U = 1.0$

categoria del sottosuolo: B

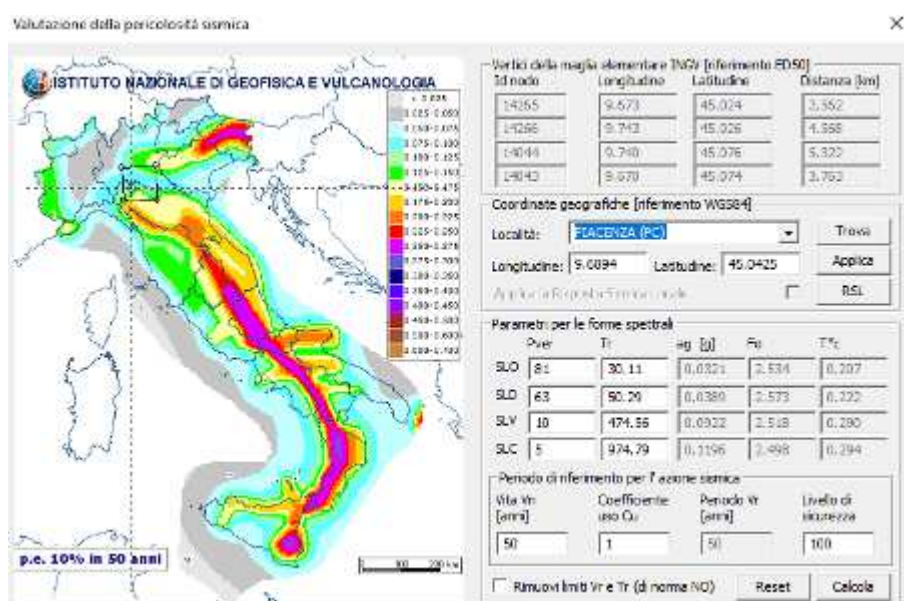
categoria topografica: T1

coeff. di amplificaz. Topografica: $S_T = 1$

coordinate di ubicazione geografica: Viale Dante alighieri n. 46- Piacenza (PC)

latitudine: 45.0425°

longitudine: 9.6894°



AZIONI SULLA COSTRUZIONE

Nel seguente paragrafo sono riportati i valori caratteristici delle azioni considerate per il calcolo della struttura, che a meno di indicazioni specifiche, sono stati presi in accordo con quanto indicato nel capitolo 3.1 del D.M. 17/01/2018.

Piano terra

CARICHI PERMANENTI STRUTTURALI $G1,k$

Peso proprio igloo H40 con getto a raso	= 150 daN/m ²
Soletta in c.a. sp. 5	= 125 daN/m ²
Isolante XPS sp.12	= 5 daN/m ²
Foamcem sp. 11	= 50 daN/m ²
Sottofondo pavimentazione sp. 5	= 80 daN/m ²
Pavimentazione in gres	= 20 daN/m ²
	430 daN/m² ($G1,k$)

CARICHI PERMANENTI NON STRUTTURALI $G2,k$

Tramezzi in cartongesso	= 50 daN/m ²
	50 daN/m² ($G2,k$)

CARICHI VARIABILI Q,k

<i>Variabili (Cat. E1)</i>	= 600 daN/m² (Q,k)
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Piano copertura

CARICHI PERMANENTI STRUTTURALI $G1,k$

Peso proprio solaio	= 380 daN/m ²
Barriera a vapore	= 10 daN/m ²
Isolante XPS sp.18	= 8 daN/m ²
Guaina poliofelina	= 2 daN/m ²
	400 daN/m² ($G1,k$)

CARICHI PERMANENTI NON STRUTTURALI $G_{2,k}$

-Zona con pannelli fotovoltaici

Controsoffitto = 30 daN/m²

Pannelli fotovoltaici = 20 daN/m²

50 daN/m² ($G_{2,k}$)

-Zona con impianti

Controsoffitto = 30 daN/m²

Impianti = 370 daN/m²

400 daN/m² ($G_{2,k}$)

CARICHI VARIABILI Q_k

Variabili (neve) = 120 daN/m² (Q_k)

Accumuli in corrispondenza di sporgenze:

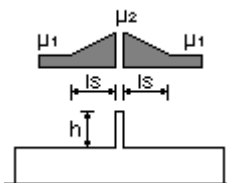
$h = 1.0$ m

$\mu_1 = 0.80 \Rightarrow Q_1 = 120$ daN/mq

$\mu_2 = 1.56 \Rightarrow Q_2 = 234$ daN/mq

$l_s = 5.0$ m

Schema di carico:



Piano copertura zona ingresso

CARICHI PERMANENTI STRUTTURALI $G_{1,k}$

$$\begin{aligned}\text{Peso proprio solaio (pannelli Sisco)} &= 15 \text{ daN/m}^2 \\ &= \mathbf{15 \text{ daN/m}^2} \quad (G_{1,k})\end{aligned}$$

CARICHI PERMANENTI NON STRUTTURALI $G_{2,k}$

$$\begin{aligned}\text{Controsoffitto} &= 30 \text{ daN/m}^2 \\ \text{Guaine} &= 20 \text{ daN/m}^2 \\ &= \mathbf{50 \text{ daN/m}^2} \quad (G_{2,k})\end{aligned}$$

CARICHI VARIABILI Q_{k}

$$\text{Variabili (neve)} = \mathbf{120 \text{ daN/m}^2} \quad (Q_{k})$$

CARICHI DEL VENTO $Q_{v,k}$

Zona vento = 2

Velocità base della zona, $V_{b,o} = 25 \text{ m/s}$ (Tab. 3.3.I)

Altitudine base della zona, $A_o = 750 \text{ m}$ (Tab. 3.3.I)

Altitudine del sito, $A_s = 61 \text{ m}$

Velocità di riferimento, $V_b = 25.00 \text{ m/s}$ ($V_b = V_{b,o}$ per $A_s \leq A_o$)

Periodo di ritorno, $T_r = 50 \text{ anni}$

$C_r = 1$ per $T_r = 50 \text{ anni}$

Velocità riferita al periodo di ritorno di progetto, $V_r = V_b C_r = 25.00 \text{ m/s}$

Classe di rugosità del terreno: B

[Aree urbane (non di classe A), suburbane, industriali e boschive]

Esposizione: Cat. IV - Entroterra fino a 500 m di altitudine

($K_r = 0.22$; $Z_o = 0.30 \text{ m}$; $Z_{min} = 8 \text{ m}$)

Pressione cinetica di riferimento, $q_b = 39 \text{ daN/m}^2$

Coefficiente di forma, $C_p = 1.00$

Coefficiente dinamico, $C_d = 1.00$

Coefficiente di esposizione, $C_e = 1.63$

Coefficiente di esposizione topografica, $C_t = 1.00$

Altezza dell'edificio, $h = 5.76 \text{ m}$

Pressione del vento, $p = q_b C_e C_p C_d = 64 \text{ daN/m}^2$

ESCRIZIONE DEI MATERIALI

Per le specifiche di progetto dei materiali si rimanda alla relazione specifica “RELAZIONE SULLE CARATTERISTICHE DEI MATERIALI ”.

ILLUSTRAZIONE DEI CRITERI DI PROGETTAZIONE E DI MODELLAZIONE

Calcolo dei fattori di comportamento secondo il D.M. 17/01/2018

La costruzione, nuova, è caratterizzata da regolarità sia in pianta sia in altezza ed è progettata considerando un comportamento non dissipativo (ND).

Parametri fattore in direzione x e y

Caratteristiche costruzione		
Tipologia	Nuova	
Regolarità pianta	SI	
Regolarità altezza	SI	
Classe di duttilità	ND	
Sistema costruttivo	Calcestruzzo	
Tipologia strutturale	Strutture a telaio, a pareti accoppiate, miste	
Definizione rapporto α_u/α_1	Valore come da normativa	
Riferimento normativo α_u/α_1	Strutture a telaio di un piano	

Parametri		
α_u/α_1	1.100	
$q_0 = 3.000 \alpha_u/\alpha_1$	3.300	
k_w	1.000	
K_R	1.0	
$q_D = q_0 \cdot k_w \cdot K_R$	3.300	
$q_{ND} = 2/3 \cdot q_D$	1.500 (≤ 1.5)	

Fattori di comportamento		
		Non dissipativi
q SLU x		1.500
q SLU y		1.500

PRINCIPALI COMBINAZIONI DELLE AZIONI DI CARICO

Condizioni di carico considerate :

CDC	Tipo	Sigla Id
1	Ggk	CDC=Ggk (peso proprio della struttura)
2	Gsk	CDC=G1sk (permanente solai-coperture)
3	Gsk	CDC=G2sk (permanente solai-coperture n.c.d.)
4	Gsk	CDC=G2pk (permanente pannelli n.c.d.)
5	Qsk	CDC=Qsk (variabile solai)
6	Qnk	CDC=Qnk (carico da neve)
7	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)
8	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -)
9	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)
10	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -)
11	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. +)
12	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. -)
13	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. +)
14	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. -)
15	Qvk	CDC=Qvk (carico da vento) dir X +
16	Qvk	CDC=Qvk (carico da vento) dir X -
17	Qvk	CDC=Qvk (carico da vento) dir Y +
18	Qvk	CDC=Qvk (carico da vento) dir Y -
19	Gk	CDC=G1k (permanente su platea)
20	Gk	CDC=G2k (permanente su platea)
21	Qk	CDC=Qk (variabile su platea)
22	Gk	CDC=G2k (permanente su sbalzo p. terra)
23	Qk	CDC=Qk (variabile su sbalzo p. terra)
24	Gk	CDC=G2k (permanente su sbalzo in copertura)
25	Qk	CDC=Qk (variabile su sbalzo in copertura)

Combinazioni di carico :

Cmb	Tipo	Sigla Id
1	SLU	Comb. SLU A1 1
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Cmb	Tipo	Sigla Id
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731	SLE(r)	Comb. SLE(rara) 731
732	SLE(r)	Comb. SLE(rara) 732
733	SLE(r)	Comb. SLE(rara) 733
734	SLE(r)	Comb. SLE(rara) 734
735	SLE(r)	Comb. SLE(rara) 735
736	SLE(r)	Comb. SLE(rara) 736
737	SLE(r)	Comb. SLE(rara) 737
738	SLE(r)	Comb. SLE(rara) 738
739	SLE(r)	Comb. SLE(rara) 739
740	SLE(r)	Comb. SLE(rara) 740
741	SLE(r)	Comb. SLE(rara) 741
742	SLE(r)	Comb. SLE(rara) 742
743	SLE(r)	Comb. SLE(rara) 743
744	SLE(r)	Comb. SLE(rara) 744
745	SLE(r)	Comb. SLE(rara) 745
746	SLE(r)	Comb. SLE(rara) 746
747	SLE(r)	Comb. SLE(rara) 747
748	SLE(r)	Comb. SLE(rara) 748
749	SLE(r)	Comb. SLE(rara) 749
750	SLE(r)	Comb. SLE(rara) 750
751	SLE(r)	Comb. SLE(rara) 751
752	SLE(r)	Comb. SLE(rara) 752
753	SLE(r)	Comb. SLE(rara) 753
754	SLE(r)	Comb. SLE(rara) 754
755	SLE(r)	Comb. SLE(rara) 755
756	SLE(r)	Comb. SLE(rara) 756
757	SLE(r)	Comb. SLE(rara) 757
758	SLE(r)	Comb. SLE(rara) 758
759	SLE(r)	Comb. SLE(rara) 759
760	SLE(r)	Comb. SLE(rara) 760
761	SLE(r)	Comb. SLE(rara) 761
762	SLE(r)	Comb. SLE(rara) 762
763	SLE(r)	Comb. SLE(rara) 763
764	SLE(r)	Comb. SLE(rara) 764
765	SLE(r)	Comb. SLE(rara) 765
766	SLE(r)	Comb. SLE(rara) 766
767	SLE(r)	Comb. SLE(rara) 767
768	SLE(r)	Comb. SLE(rara) 768
769	SLE(r)	Comb. SLE(rara) 769
770	SLE(r)	Comb. SLE(rara) 770

Cmb	Tipo	Sigla Id
771	SLE(r)	Comb. SLE(rara) 771
772	SLE(r)	Comb. SLE(rara) 772
773	SLE(r)	Comb. SLE(rara) 773
774	SLE(r)	Comb. SLE(rara) 774
775	SLE(r)	Comb. SLE(rara) 775
776	SLE(r)	Comb. SLE(rara) 776
777	SLE(r)	Comb. SLE(rara) 777
778	SLE(r)	Comb. SLE(rara) 778
779	SLE(r)	Comb. SLE(rara) 779
780	SLE(r)	Comb. SLE(rara) 780
781	SLE(r)	Comb. SLE(rara) 781
782	SLE(r)	Comb. SLE(rara) 782
783	SLE(r)	Comb. SLE(rara) 783
784	SLE(r)	Comb. SLE(rara) 784
785	SLE(r)	Comb. SLE(rara) 785
786	SLE(r)	Comb. SLE(rara) 786
787	SLE(r)	Comb. SLE(rara) 787
788	SLE(r)	Comb. SLE(rara) 788
789	SLE(r)	Comb. SLE(rara) 789
790	SLE(r)	Comb. SLE(rara) 790
791	SLE(r)	Comb. SLE(rara) 791
792	SLE(r)	Comb. SLE(rara) 792
793	SLE(r)	Comb. SLE(rara) 793
794	SLE(r)	Comb. SLE(rara) 794
795	SLE(r)	Comb. SLE(rara) 795
796	SLE(r)	Comb. SLE(rara) 796
797	SLE(r)	Comb. SLE(rara) 797
798	SLE(r)	Comb. SLE(rara) 798
799	SLE(r)	Comb. SLE(rara) 799
800	SLE(r)	Comb. SLE(rara) 800
801	SLE(r)	Comb. SLE(rara) 801
802	SLE(r)	Comb. SLE(rara) 802
803	SLE(r)	Comb. SLE(rara) 803
804	SLE(r)	Comb. SLE(rara) 804
805	SLE(r)	Comb. SLE(rara) 805
806	SLE(r)	Comb. SLE(rara) 806
807	SLE(r)	Comb. SLE(rara) 807
808	SLE(r)	Comb. SLE(rara) 808
809	SLE(r)	Comb. SLE(rara) 809
810	SLE(r)	Comb. SLE(rara) 810
811	SLE(r)	Comb. SLE(rara) 811
812	SLE(r)	Comb. SLE(rara) 812
813	SLE(r)	Comb. SLE(rara) 813
814	SLE(r)	Comb. SLE(rara) 814
815	SLE(r)	Comb. SLE(rara) 815
816	SLE(r)	Comb. SLE(rara) 816
817	SLE(r)	Comb. SLE(rara) 817
818	SLE(r)	Comb. SLE(rara) 818
819	SLE(r)	Comb. SLE(rara) 819
820	SLE(r)	Comb. SLE(rara) 820
821	SLE(r)	Comb. SLE(rara) 821
822	SLE(r)	Comb. SLE(rara) 822
823	SLE(r)	Comb. SLE(rara) 823
824	SLE(r)	Comb. SLE(rara) 824
825	SLE(r)	Comb. SLE(rara) 825
826	SLE(r)	Comb. SLE(rara) 826
827	SLE(r)	Comb. SLE(rara) 827
828	SLE(r)	Comb. SLE(rara) 828
829	SLE(r)	Comb. SLE(rara) 829
830	SLE(r)	Comb. SLE(rara) 830
831	SLE(r)	Comb. SLE(rara) 831
832	SLE(r)	Comb. SLE(rara) 832
833	SLE(r)	Comb. SLE(rara) 833
834	SLE(r)	Comb. SLE(rara) 834
835	SLE(r)	Comb. SLE(rara) 835
836	SLE(r)	Comb. SLE(rara) 836
837	SLE(r)	Comb. SLE(rara) 837
838	SLE(r)	Comb. SLE(rara) 838

Cmb	Tipo	Sigla Id
839	SLE(r)	Comb. SLE(rara) 839
840	SLE(r)	Comb. SLE(rara) 840
841	SLE(r)	Comb. SLE(rara) 841
842	SLE(r)	Comb. SLE(rara) 842
843	SLE(r)	Comb. SLE(rara) 843
844	SLE(r)	Comb. SLE(rara) 844
845	SLE(r)	Comb. SLE(rara) 845
846	SLE(r)	Comb. SLE(rara) 846
847	SLE(r)	Comb. SLE(rara) 847
848	SLE(r)	Comb. SLE(rara) 848
849	SLE(r)	Comb. SLE(rara) 849
850	SLE(r)	Comb. SLE(rara) 850
851	SLE(r)	Comb. SLE(rara) 851
852	SLE(r)	Comb. SLE(rara) 852
853	SLE(r)	Comb. SLE(rara) 853
854	SLE(r)	Comb. SLE(rara) 854
855	SLE(r)	Comb. SLE(rara) 855
856	SLE(r)	Comb. SLE(rara) 856
857	SLE(f)	Comb. SLE(freq.) 857
858	SLE(f)	Comb. SLE(freq.) 858
859	SLE(f)	Comb. SLE(freq.) 859
860	SLE(f)	Comb. SLE(freq.) 860
861	SLE(f)	Comb. SLE(freq.) 861
862	SLE(f)	Comb. SLE(freq.) 862
863	SLE(f)	Comb. SLE(freq.) 863
864	SLE(f)	Comb. SLE(freq.) 864
865	SLE(f)	Comb. SLE(freq.) 865
866	SLE(f)	Comb. SLE(freq.) 866
867	SLE(f)	Comb. SLE(freq.) 867
868	SLE(f)	Comb. SLE(freq.) 868
869	SLE(f)	Comb. SLE(freq.) 869
870	SLE(f)	Comb. SLE(freq.) 870
871	SLE(f)	Comb. SLE(freq.) 871
872	SLE(f)	Comb. SLE(freq.) 872
873	SLE(f)	Comb. SLE(freq.) 873
874	SLE(f)	Comb. SLE(freq.) 874
875	SLE(f)	Comb. SLE(freq.) 875
876	SLE(f)	Comb. SLE(freq.) 876
877	SLE(f)	Comb. SLE(freq.) 877
878	SLE(f)	Comb. SLE(freq.) 878
879	SLE(f)	Comb. SLE(freq.) 879
880	SLE(f)	Comb. SLE(freq.) 880
881	SLE(f)	Comb. SLE(freq.) 881
882	SLE(f)	Comb. SLE(freq.) 882
883	SLE(f)	Comb. SLE(freq.) 883
884	SLE(f)	Comb. SLE(freq.) 884
885	SLE(f)	Comb. SLE(freq.) 885
886	SLE(f)	Comb. SLE(freq.) 886
887	SLE(f)	Comb. SLE(freq.) 887
888	SLE(f)	Comb. SLE(freq.) 888
889	SLE(f)	Comb. SLE(freq.) 889
890	SLE(f)	Comb. SLE(freq.) 890
891	SLE(f)	Comb. SLE(freq.) 891
892	SLE(f)	Comb. SLE(freq.) 892
893	SLE(f)	Comb. SLE(freq.) 893
894	SLE(f)	Comb. SLE(freq.) 894
895	SLE(f)	Comb. SLE(freq.) 895
896	SLE(f)	Comb. SLE(freq.) 896
897	SLE(f)	Comb. SLE(freq.) 897
898	SLE(f)	Comb. SLE(freq.) 898
899	SLE(f)	Comb. SLE(freq.) 899
900	SLE(f)	Comb. SLE(freq.) 900
901	SLE(f)	Comb. SLE(freq.) 901
902	SLE(f)	Comb. SLE(freq.) 902
903	SLE(f)	Comb. SLE(freq.) 903
904	SLE(f)	Comb. SLE(freq.) 904
905	SLE(f)	Comb. SLE(freq.) 905
906	SLE(f)	Comb. SLE(freq.) 906

Cmb	Tipo	Sigla Id
907	SLE(f)	Comb. SLE(freq.) 907
908	SLE(f)	Comb. SLE(freq.) 908
909	SLE(f)	Comb. SLE(freq.) 909
910	SLE(f)	Comb. SLE(freq.) 910
911	SLE(f)	Comb. SLE(freq.) 911
912	SLE(f)	Comb. SLE(freq.) 912
913	SLE(f)	Comb. SLE(freq.) 913
914	SLE(f)	Comb. SLE(freq.) 914
915	SLE(f)	Comb. SLE(freq.) 915
916	SLE(f)	Comb. SLE(freq.) 916
917	SLE(p)	Comb. SLE(perm.) 917
918	SLE(p)	Comb. SLE(perm.) 918
919	SLE(p)	Comb. SLE(perm.) 919
920	SLE(p)	Comb. SLE(perm.) 920
921	SLE(p)	Comb. SLE(perm.) 921
922	SLE(p)	Comb. SLE(perm.) 922
923	SLE(p)	Comb. SLE(perm.) 923
924	SLE(p)	Comb. SLE(perm.) 924

Combinazioni di carico con coefficienti di partecipazione:

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
1	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
2	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
3	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
4	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
5	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
6	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
7	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
8	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
9	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
10	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
11	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
12	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
13	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
14	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
15	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
16	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
17	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
18	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
19	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
20	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
21	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
22	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
23	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
24	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
25	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
26	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
27	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
28	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
29	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
30	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
31	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
32	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
33	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
34	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
35	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
36	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
37	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00									

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
55	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
56	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
57	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
58	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
59	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
60	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
61	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
62	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
63	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
64	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
65	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
66	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
67	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
68	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
69	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
70	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
71	1.30	1.30	1.50	1										

[illegible]

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
122	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
123	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
124	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
125	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
126	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
127	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
128	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
129	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
130	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
131	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
132	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
133	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
134	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
135	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
136	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
137	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
138	1.													

[illegible]

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
189	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.50	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
190	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.50	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
191	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.50	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
192	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.50	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
193	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
194	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
195	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
196	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
197	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
198	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
199	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
200	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
201	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
202	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
203	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
204	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
205	1.30	1.												

[illegible]

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
256	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
257	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
258	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
259	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
260	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
261	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
262	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
263	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
264	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
265	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
266	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
267	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
268	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
269	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
270	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
271	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
272	1.													

[illegible]

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
323	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
324	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
325	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
326	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
327	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
328	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
329	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
330	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
331	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
332	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
333	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
334	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
335	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
336	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
337	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
338	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
339														

[illegible]

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
390	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
391	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
392	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
393	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
394	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
395	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
396	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
397	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
398	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
399	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
400	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
401	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
402	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
403	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
404	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
405	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
406	1.00	1.												

[illegible]

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
457	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
458	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
459	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
460	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
461	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
462	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
463	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
464	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
465	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
466	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
467	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
468	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
469	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
470	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
471	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
472	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
473	1.0													

[illegible]

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
524	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.50	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
525	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.50	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
526	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.50	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
527	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.50	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
528	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.50	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
529	1.00	1.00	1.00	1.00	0.0	0.0	-1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
530	1.00	1.00	1.00	1.00	0.0	0.0	-1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
531	1.00	1.00	1.00	1.00	0.0	0.0	1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
532	1.00	1.00	1.00	1.00	0.0	0.0	1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
533	1.00	1.00	1.00	1.00	0.0	0.0	-1.00	0.0	0.0	-0.30	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
534	1.00	1.00	1.00	1.00	0.0	0.0	-1.00	0.0	0.0	0.30	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
535	1.00	1.00	1.00	1.00	0.0	0.0	1.00	0.0	0.0	-0.30	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
536	1.00	1.00	1.00	1.00	0.0	0.0	1.00	0.0	0.0	0.30	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
537	1.00	1.00	1.00	1.00	0.0	0.0	0.0	-1.00	-0.30	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
538	1.00	1.00	1.00	1.00	0.0	0.0	0.0	-1.00	0.30	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
539	1.00	1.00	1.00	1.00	0.0	0.0	0.0	1.00	-0.30	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			</

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
558	1.00	1.00	1.00	1.00	0.0	0.0	0.0	-0.30	0.0	1.00	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
559	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.30	0.0	-1.00	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
560	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.30	0.0	1.00	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
561	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	-0.30	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
562	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.30	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
563	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	-0.30	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
564	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.30	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
565	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	-0.30
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
566	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	0.30
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
567	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.0	-0.30
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
568	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.0	0.30
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
569	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	-0.30	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
570	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.30	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
571	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	-0.30	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
572	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.30	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
573	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	-

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
591	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	-1.00
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
592	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	1.00
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
593	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
594	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
595	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
596	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
597	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
598	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
599	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
600	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
601	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
602	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
603	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
604	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
605	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
606	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
607	1.00	1.00	1.00	1.00	0.									

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
625	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
626	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
627	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
628	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
629	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
630	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
631	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
632	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
633	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
634	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
635	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
636	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
637	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
638	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
639	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
640	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0											

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
658	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
659	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
660	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
661	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
662	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
663	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
664	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
665	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
666	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
667	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
668	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
669	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
670	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
671	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
672	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
673	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.00	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
674	1.00	1.												

[illegible]

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
725	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.60	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
726	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.60	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
727	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.60	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
728	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.60	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
729	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
730	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
731	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
732	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
733	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
734	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
735	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
736	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
737	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
738	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
739	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
740	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
741	1.00	1.												

[illegible]

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
	0.20	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
893	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.20	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
894	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.20	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.80			
895	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.20	0.0	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.0			
896	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.20	0.0	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.80			
897	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.20	0.0	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.0			
898	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.20	0.0	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.80			
899	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.20	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.0			
900	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.20	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
901	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.20	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
902	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.20	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.80			
903	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.20	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.0			
904	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.20	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.80			
905	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.20	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.0			
906	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.20	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.80			
907	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.20	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.0			
908	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.20	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
909	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.20	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
910	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.20	1.00	1.00	0.0	1.00	0.0	1.00	0.80			
911	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.20	1.00	1.00	0.0	1.00	0.80	1.00	0.0			
912	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.20	1.00	1.00	0.0	1.00	0.80	1.00	0.80			
913	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.20	1.00	1.00	0.80	1.00	0.0	1.00	0.0			
914	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.20	1.00	1.00	0.80	1.00	0.0	1.00	0.80			
915	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.20	1.00	1.00	0.80	1.00	0.80	1.00	0.0			
916	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.20	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
917	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
918	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.80			
919	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.0			
920	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.80			
921	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.0			
922	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.80			
923	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.0			
924	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			

METODO DI ANALISI SEGUITO

La struttura in esame è stata analizzata seguendo il metodo di **ANALISI LINEARE DINAMICA** in quanto , essendo regolare in pianta ed in altezza , è quello che meglio descrive il reale comportamento delle strutture sotto sisma.

Nell'analisi lineare dinamica sono stati considerati i seguenti modi di vibrare con le relative masse partecipanti :

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	2.663	0.376	0.186	1.014e+04	3.2	2.327e+05	74.5	755.57	0.2	0.0	0.0
2	2.959	0.338	0.186	1.778e+05	56.9	1.439e+04	4.6	210.01	6.72e-02	0.0	0.0
3	4.428	0.226	0.186	7.177e+04	23.0	23.92	7.66e-03	743.03	0.2	0.0	0.0
4	6.848	0.146	0.186	70.61	2.26e-02	21.96	7.03e-03	1.029e+04	3.3	0.0	0.0
5	7.225	0.138	0.186	75.37	2.41e-02	8198.09	2.6	9.108e+04	29.2	0.0	0.0
6	7.828	0.128	0.181	1495.86	0.5	1508.67	0.5	727.56	0.2	0.0	0.0
7	8.125	0.123	0.179	415.65	0.1	124.10	3.97e-02	8.679e+04	27.8	0.0	0.0
8	8.537	0.117	0.175	19.12	6.12e-03	430.72	0.1	1.096e+04	3.5	0.0	0.0
9	9.109	0.110	0.171	1084.96	0.3	286.49	9.17e-02	3.096e+04	9.9	0.0	0.0
10	10.394	0.096	0.164	21.70	6.95e-03	2981.98	1.0	4.016e+04	12.9	0.0	0.0
11	11.052	0.090	0.161	1679.74	0.5	59.31	1.90e-02	3.017e+04	9.7	0.0	0.0
12	11.264	0.089	0.160	1.514e+04	4.8	512.57	0.2	1416.11	0.5	0.0	0.0
13	11.568	0.086	0.158	45.62	1.46e-02	4818.04	1.5	1470.17	0.5	0.0	0.0
14	11.883	0.084	0.157	3345.03	1.1	10.57	3.38e-03	2079.44	0.7	0.0	0.0
15	13.545	0.074	0.151	244.43	7.83e-02	1643.64	0.5	295.97	9.48e-02	0.0	0.0
16	13.767	0.073	0.151	1640.16	0.5	8250.09	2.6	321.02	0.1	0.0	0.0
17	14.353	0.070	0.149	1233.56	0.4	127.41	4.08e-02	2.20	7.06e-04	0.0	0.0
18	14.504	0.069	0.149	881.94	0.3	2.940e+04	9.4	133.31	4.27e-02	0.0	0.0
19	15.052	0.066	0.147	1184.84	0.4	2018.38	0.6	21.73	6.96e-03	0.0	0.0
20	15.524	0.064	0.146	56.55	1.81e-02	2254.74	0.7	36.70	1.18e-02	0.0	0.0
21	16.137	0.062	0.145	1.105e+04	3.5	667.83	0.2	50.09	1.60e-02	0.0	0.0
22	16.335	0.061	0.144	5679.33	1.8	2.67	8.55e-04	10.93	3.50e-03	0.0	0.0
23	17.443	0.057	0.142	3365.95	1.1	0.16	5.01e-05	756.21	0.2	0.0	0.0
24	17.731	0.056	0.142	3608.72	1.2	887.83	0.3	1273.89	0.4	0.0	0.0
25	19.022	0.053	0.140	0.87	2.79e-04	14.26	4.57e-03	1.19	3.81e-04	0.0	0.0
26	20.297	0.049	0.138	57.98	1.86e-02	333.79	0.1	10.45	3.35e-03	0.0	0.0
27	21.513	0.046	0.136	0.07	2.39e-05	15.57	4.98e-03	3.45	1.10e-03	0.0	0.0
28	22.833	0.044	0.135	1.19	3.81e-04	1.22	3.91e-04	10.98	3.52e-03	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
29	23.969	0.042	0.134	7.17e-04	0.0	46.06	1.47e-02	43.48	1.39e-02	0.0	0.0
30	24.429	0.041	0.133	19.21	6.15e-03	0.05	1.48e-05	47.99	1.54e-02	0.0	0.0
31	24.719	0.040	0.133	1.32	4.22e-04	1.46	4.69e-04	3.73	1.20e-03	0.0	0.0
32	25.063	0.040	0.133	72.06	2.31e-02	9.32	2.98e-03	1.84	5.90e-04	0.0	0.0
33	25.961	0.039	0.132	7.59	2.43e-03	14.44	4.62e-03	0.72	2.31e-04	0.0	0.0
34	26.686	0.037	0.131	23.62	7.56e-03	112.50	3.60e-02	12.56	4.02e-03	0.0	0.0
35	27.211	0.037	0.131	4.41	1.41e-03	19.97	6.39e-03	4.35	1.39e-03	0.0	0.0
36	27.739	0.036	0.131	0.91	2.91e-04	173.09	5.54e-02	3.22	1.03e-03	0.0	0.0
37	29.001	0.034	0.130	4.55	1.46e-03	38.17	1.22e-02	4.59	1.47e-03	0.0	0.0
38	29.454	0.034	0.129	2.06	6.60e-04	36.48	1.17e-02	55.21	1.77e-02	0.0	0.0
39	29.821	0.034	0.129	3.55	1.14e-03	3.94	1.26e-03	52.65	1.69e-02	0.0	0.0
40	30.123	0.033	0.129	9.66	3.09e-03	43.48	1.39e-02	1.56	5.00e-04	0.0	0.0
41	32.107	0.031	0.128	4.47	1.43e-03	14.12	4.52e-03	5.10	1.63e-03	0.0	0.0
42	32.600	0.031	0.128	1.96	6.27e-04	32.99	1.06e-02	32.64	1.05e-02	0.0	0.0
43	33.374	0.030	0.127	0.45	1.45e-04	0.44	1.39e-04	0.06	1.85e-05	0.0	0.0
44	33.999	0.029	0.127	0.09	2.82e-05	0.17	5.39e-05	8.83	2.83e-03	0.0	0.0
45	34.751	0.029	0.127	0.33	1.05e-04	0.04	1.15e-05	0.35	1.12e-04	0.0	0.0
46	35.331	0.028	0.126	0.03	1.01e-05	2.42	7.75e-04	5.29	1.69e-03	0.0	0.0
47	36.570	0.027	0.126	1.21	3.86e-04	1.33	4.25e-04	251.27	8.05e-02	0.0	0.0
48	37.095	0.027	0.126	1.43	4.58e-04	0.98	3.14e-04	18.18	5.82e-03	0.0	0.0
49	37.360	0.027	0.125	0.95	3.04e-04	2.25	7.19e-04	0.07	2.20e-05	0.0	0.0
50	38.787	0.026	0.125	0.01	4.17e-06	0.02	4.84e-06	0.26	8.36e-05	0.0	0.0
51	39.411	0.025	0.125	0.11	3.63e-05	8.55e-03	2.74e-06	0.09	2.86e-05	0.0	0.0
52	40.734	0.025	0.124	0.63	2.00e-04	0.04	1.44e-05	92.24	2.95e-02	0.0	0.0
53	41.304	0.024	0.124	1.34	4.30e-04	0.61	1.94e-04	250.67	8.03e-02	0.0	0.0
54	41.910	0.024	0.124	0.20	6.47e-05	0.02	6.59e-06	8.37	2.68e-03	0.0	0.0
55	42.534	0.024	0.124	7.82e-03	2.50e-06	0.37	1.18e-04	70.35	2.25e-02	0.0	0.0
56	42.862	0.023	0.124	0.0	0.0	1.64	5.24e-04	29.37	9.40e-03	0.0	0.0
57	43.264	0.023	0.123	0.18	5.86e-05	2.26	7.25e-04	88.88	2.85e-02	0.0	0.0
58	44.840	0.022	0.123	0.21	6.77e-05	0.48	1.55e-04	13.67	4.38e-03	0.0	0.0
59	45.905	0.022	0.123	0.02	7.76e-06	0.12	3.77e-05	1.10	3.51e-04	0.0	0.0
60	46.336	0.022	0.123	4.45e-03	1.42e-06	0.27	8.77e-05	6.87e-05	0.0	0.0	0.0
Risulta				3.123e+05		3.123e+05		3.118e+05			
In percentuale				99.99		99.98		99.85			

Masse partecipanti durante il sisma:

$M_x = 99.99\% > 85\%$ OK

$M_y = 99.85\% > 85\%$ OK

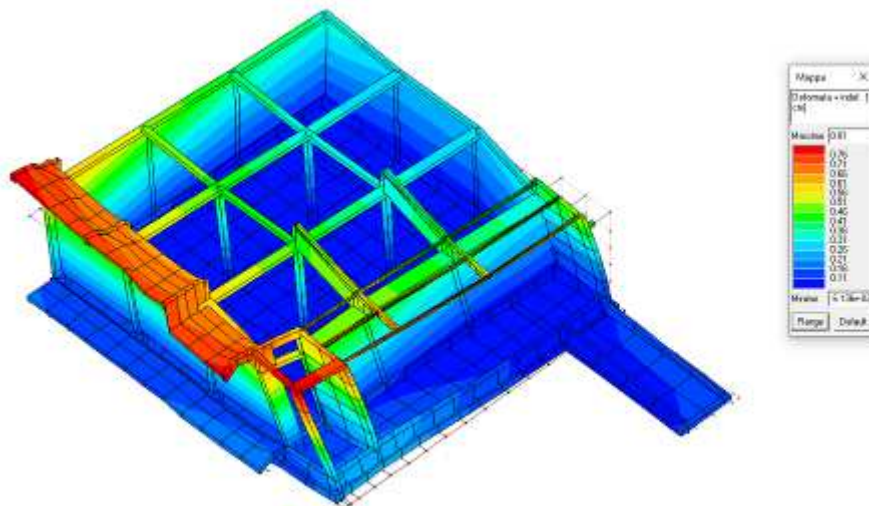
CRITERI DI VERIFICA

Le verifiche di resistenza e di stabilità degli elementi strutturali sono condotte utilizzando il metodo degli “stati limite”. Vista il tipo di struttura sono state condotte verifiche allo SLU, SLV, SLE in termini di resistenza .

RAPPRESENTAZIONE DELLE DEFORMATE E DELLE CARATTERISTICHE DI SOLLECITAZIONE

Di seguito si riportano le principali deformate e caratteristiche di sollecitazione per la struttura esaminata :

Deformata SLV X :



Deformata SLV Y :

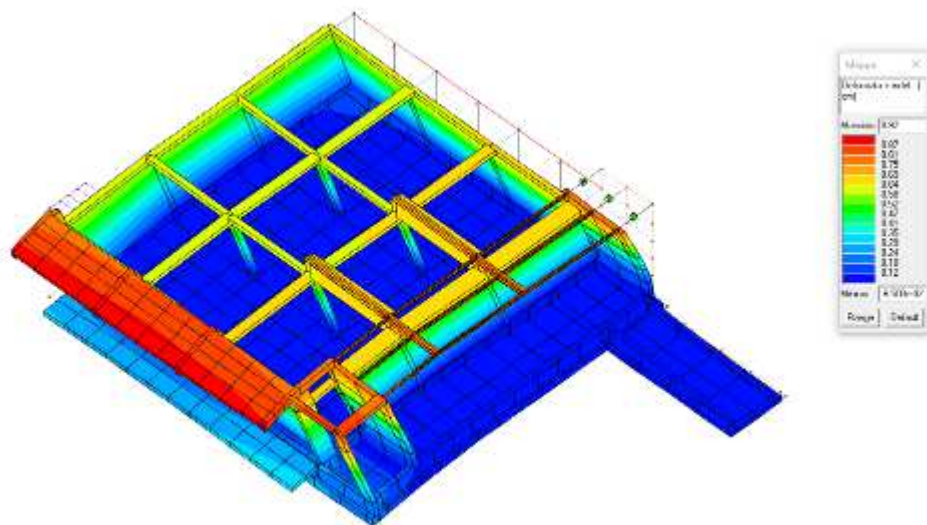


Diagramma momento flettente sotto sisma in direzione X :

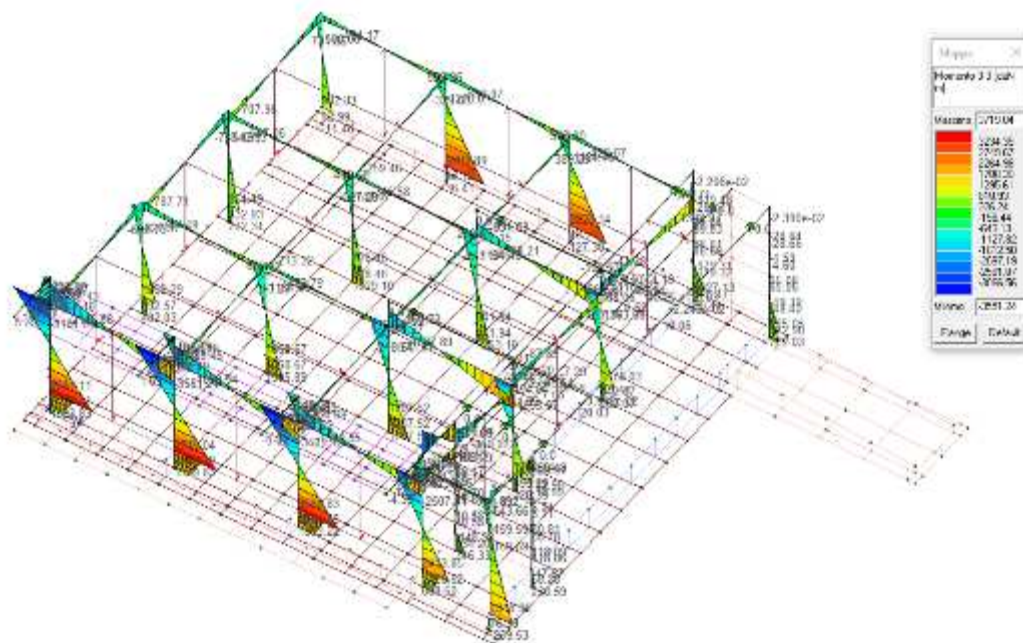


Diagramma momento flettente sotto sisma in direzione Y :

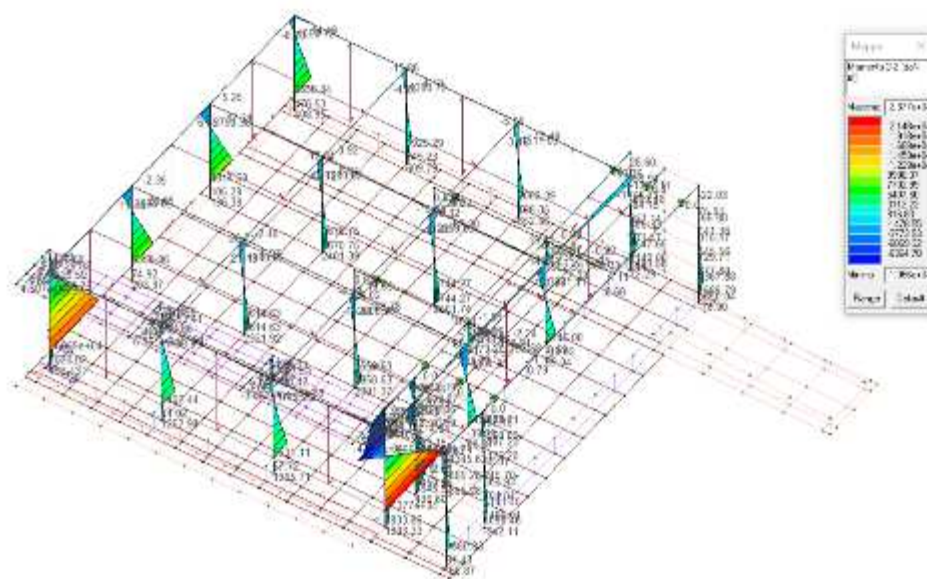


Diagramma azione tagliante sotto sisma in direzione X :

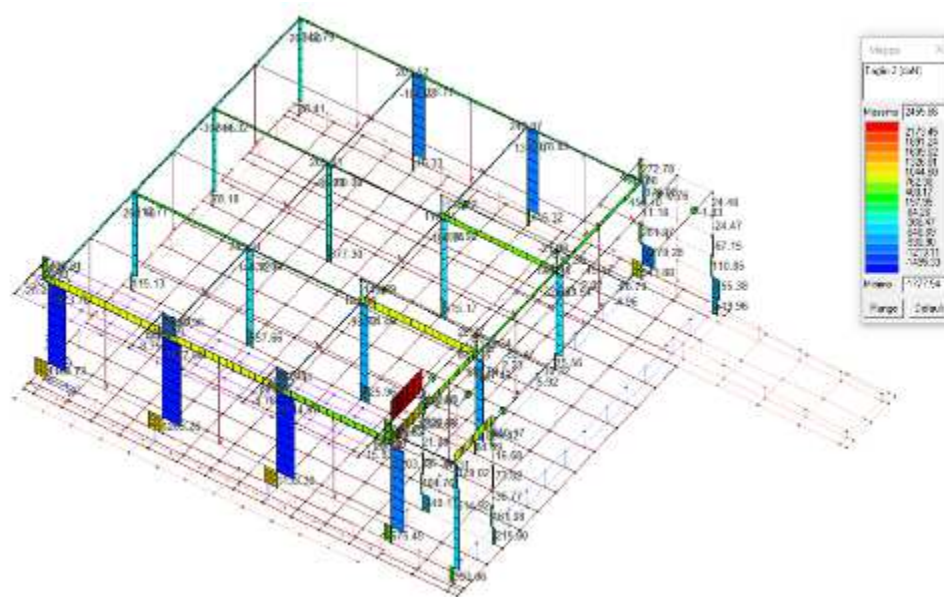
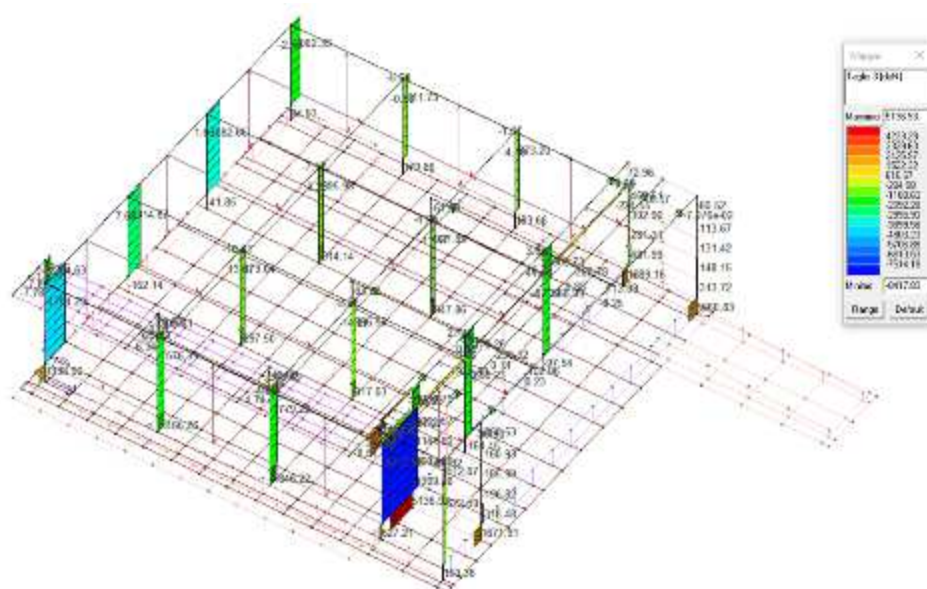


Diagramma azione tagliante sotto sisma in direzione Y :



ANALISI SISMICA

L'azione sismica viene definita in relazione ad un periodo di riferimento V_r che si ricava, per ciascun tipo di costruzione, moltiplicandone la vita nominale per il coefficiente d'uso (vedi tabella Parametri della struttura). Fissato il periodo di riferimento V_r e la probabilità di superamento P_{ver} associata a ciascuno degli stati limite considerati, si ottiene il periodo di ritorno T_r e i relativi parametri di pericolosità sismica (vedi tabella successiva):

ag: accelerazione orizzontale massima del terreno;

Fo: valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale;

T^*c : periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale;

Parametri della struttura

Classe d'uso	Vita V_n [anni]	Coeff. Uso	Periodo V_r [anni]	Tipo di suolo	Categoria topografica
II	50.0	1.0	50.0	B	T1

Individuati su reticolo di riferimento i parametri di pericolosità sismica si valutano i parametri spettrali riportati in tabella:

S è il coefficiente che tiene conto della categoria di sottosuolo e delle condizioni topografiche mediante la relazione seguente $S = S_s * S_t$ (3.2.3)

Fo è il fattore che quantifica l'amplificazione spettrale massima, su sito di riferimento rigido orizzontale

Fv è il fattore che quantifica l'amplificazione spettrale massima verticale, in termini di accelerazione orizzontale massima del terreno ag su sito di riferimento rigido orizzontale

Tb è il periodo corrispondente all'inizio del tratto dello spettro ad accelerazione costante.

Tc è il periodo corrispondente all'inizio del tratto dello spettro a velocità costante.

Td è il periodo corrispondente all'inizio del tratto dello spettro a spostamento costante.

Lo spettro di risposta elastico in accelerazione della componente orizzontale del moto sismico, S_e , è definito

dalle seguenti espressioni:

$$\begin{aligned}
 0 \leq T < T_B & S_s(T) = a_s \cdot S \cdot \eta \cdot F_o \cdot \left[\frac{T}{T_B} + \frac{1}{\eta \cdot F_o} \left(1 - \frac{T}{T_B} \right) \right] \\
 T_B \leq T < T_C & S_s(T) = a_s \cdot S \cdot \eta \cdot F_o \\
 T_C \leq T < T_D & S_s(T) = a_s \cdot S \cdot \eta \cdot F_o \cdot \left(\frac{T_C}{T} \right) \\
 T_D \leq T & S_s(T) = a_s \cdot S \cdot \eta \cdot F_o \cdot \left(\frac{T_C \cdot T_D}{T^2} \right)
 \end{aligned}$$

Dove per sottosuolo di categoria **A** i coefficienti S_s e C_c valgono 1; mentre per le categorie di sottosuolo B, C, D, E i coefficienti S_s e C_c vengono calcolati mediante le espressioni riportate nella seguente Tabella

Categoria sottosuolo	S_s	C_c
A	1,00	1,00
B	$1,00 \leq 1,40 - 0,40 \cdot F_o \cdot \frac{a_s}{g} \leq 1,20$	$1,10 \cdot (T_c^*)^{-0,20}$
C	$1,00 \leq 1,70 - 0,60 \cdot F_o \cdot \frac{a_s}{g} \leq 1,50$	$1,05 \cdot (T_c^*)^{-0,33}$
D	$0,90 \leq 2,40 - 1,50 \cdot F_o \cdot \frac{a_s}{g} \leq 1,80$	$1,25 \cdot (T_c^*)^{-0,50}$
E	$1,00 \leq 2,00 - 1,10 \cdot F_o \cdot \frac{a_s}{g} \leq 1,60$	$1,15 \cdot (T_c^*)^{-0,40}$

Per tenere conto delle condizioni topografiche e in assenza di specifiche analisi di risposta sismica locale, si utilizzano i valori del coefficiente topografico S_T riportati nella seguente Tabella

Categoria topografica	Ubicazione dell'opera o dell'intervento	S_T
T1	-	1,0
T2	In corrispondenza della sommità del pendio	1,2
T3	In corrispondenza della cresta di un rilievo con pendenza media minore o uguale a 30°	1,2
T4	In corrispondenza della cresta di un rilievo con pendenza media maggiore di 30°	1,4

Lo spettro di risposta elastico in accelerazione della componente verticale del moto sismico, S_{ve} , è definito dalle espressioni:

$$\begin{aligned}
 0 \leq T < T_B & S_{ve}(T) = a_s \cdot S \cdot \eta \cdot F_v \cdot \left[\frac{T}{T_B} + \frac{1}{\eta \cdot F_v} \left(1 - \frac{T}{T_B} \right) \right] \\
 T_B \leq T < T_C & S_{ve}(T) = a_s \cdot S \cdot \eta \cdot F_v \\
 T_C \leq T < T_D & S_{ve}(T) = a_s \cdot S \cdot \eta \cdot F_v \cdot \left(\frac{T_C}{T} \right) \\
 T_D \leq T & S_{ve}(T) = a_s \cdot S \cdot \eta \cdot F_v \cdot \left(\frac{T_C \cdot T_D}{T^2} \right)
 \end{aligned}$$

I valori di S_s , T_B , T_C e T_D , sono riportati nella seguente Tabella

Categoria di sottosuolo	S_s	T_B	T_C	T_D
A, B, C, D, E	1,0	0,05 s	0,15 s	1,0 s

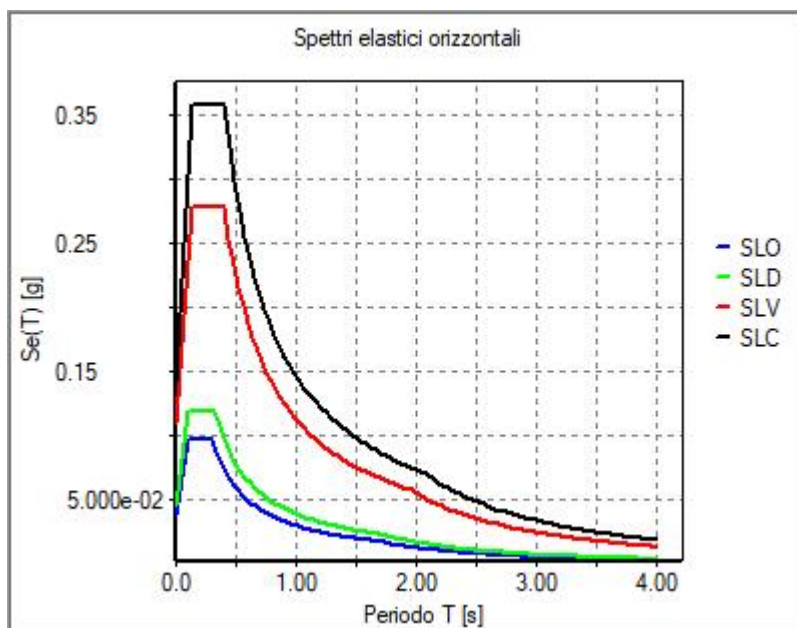
Id nodo	Longitudine	Latitudine	Distanza
			Km
Loc.	9.689	45.042	
14265	9.673	45.024	2.562
14266	9.743	45.026	4.568
14044	9.740	45.076	5.322

Id nodo	Longitudine	Latitudine	Distanza
14043	9.670	45.074	3.763

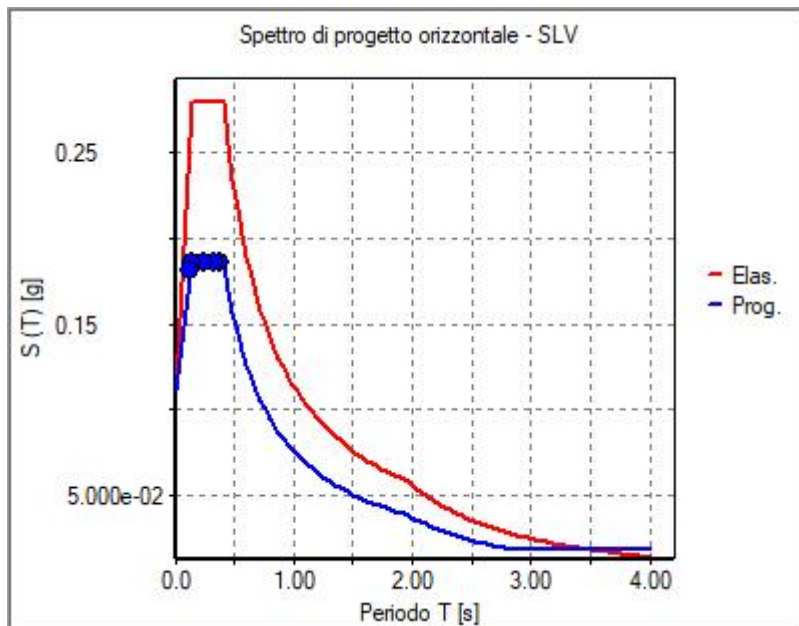
SL	Pver	Tr	ag	Fo	T*c
		Anni	g		sec
SLO	81.0	30.1	0.032	2.534	0.207
SLD	63.0	50.3	0.039	2.573	0.222
SLV	10.0	474.6	0.092	2.518	0.290
SLC	5.0	974.8	0.120	2.498	0.294

SL	ag	S	Fo	Fv	Tb	Tc	Td
	g				sec	sec	sec
SLO	0.032	1.200	2.534	0.613	0.104	0.312	1.728
SLD	0.039	1.200	2.573	0.685	0.110	0.330	1.756
SLV	0.092	1.200	2.518	1.032	0.136	0.409	1.969
SLC	0.120	1.200	2.498	1.166	0.138	0.413	2.078

Modo	Frequenza	Periodo	X M efficace x g	%	Y M efficace x g	%	Z M efficace x g	%	RZ M efficace x g	%
	1/sec	sec	daN		daN		daN		daN m2	
1	2.67	0.37	4761.4	1	2.398e+05	76	801.6	0	563.1	20
2	3.08	0.33	1.821e+05	58	7334.4	2	187.2	0	336.6	12
3	4.20	0.24	7.345e+04	23	52.5	0	584.2	0	1306.7	48
4	6.85	0.15	68.2	0	21.7	0	1.027e+04	3	0.2	0
5	7.23	0.14	94.2	0	8184.0	2	9.154e+04	29	22.8	0
6	7.82	0.13	1500.7	0	1524.1	0	656.0	0	2.0	0



24_DIA_SPETTRI_ELASTICI_O



24_DIA_SPETTRI_PROGETTO_SLV_O

VALUTAZIONE DEI RISULTATI E GIUDIZIO MOTIVATO SULLA LORO ACCETTABILITÀ

Il programma di calcolo utilizzato, PRO_SAP, è idoneo a produrre nel modello matematico il comportamento della struttura e gli elementi finiti disponibili utilizzati sono rappresentativi della realtà costruttiva.

Tutte le proprietà di rilevanza strutturale (materiali, sezioni, carichi, sconnessioni, etc.) sono state controllate attraverso le funzioni di indagine specificatamente previste.

Sono state sfruttate le funzioni di autodiagnostica presenti nel software che hanno accertato che non sussistono difetti formali di impostazione.

E' stato accertato che le risultanti delle azioni verticali sono in equilibrio con i carichi applicati. Sono state controllate le azioni taglianti di piano ed accertata la loro congruenza con quella ricavabile da semplici ed agevoli elaborazioni.

Definizione del momento flettente max sulla trave centrale della copertura :

P.p. trave	:	=	300	daN/m
permanente g1k	: $400 \cdot 9.835/2$	=	1967	daN/m
permanente g2k	: $50 \cdot 9835/2$	=	246	daN/m.
Sovr. variabile	: $120 \cdot 9.835/2$	=	590	daN/m
				<hr/>
				3103 daN/m

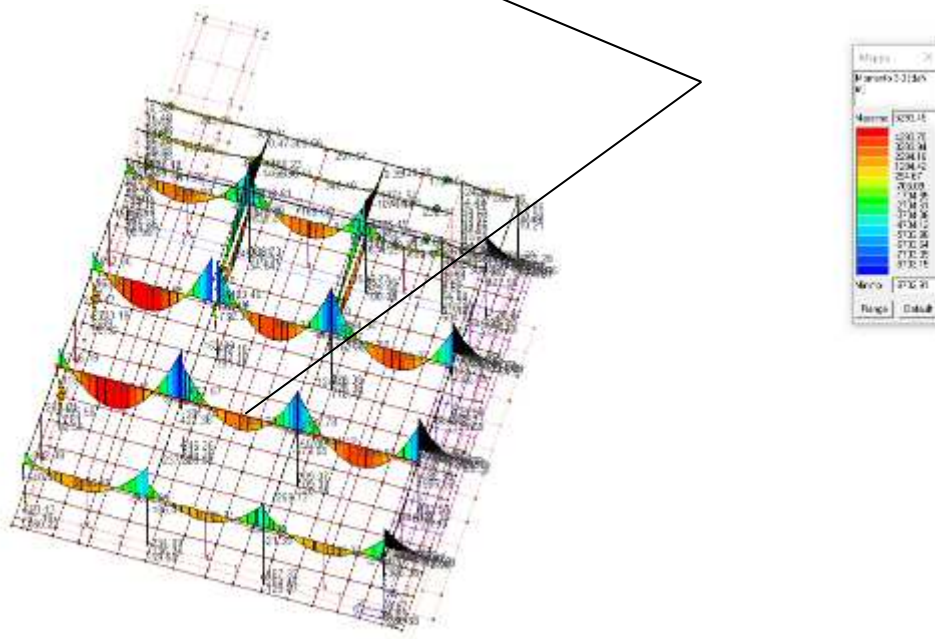
Luce di calcolo : $L_o = 5.12 \text{ m}$

Il momento flettente m_{ex} nella condizione di carico SLE rara risulta :

$$M_{SLE \text{ rara}} = 3103 \cdot 5.12^2 / 27 = 3012 \text{ daNm}$$

Il valore di momento flettente massimo dovuto al sisma ricavato dall'analisi strutturale mediante il programma di calcolo agli elementi finiti PRO_SAP , risulta pari a :

$$M(\text{sisma da analisi strutturale}) = 2945 \text{ daNm}$$



Tale valore risulta inferiore di circa il 2.5% rispetto a quello ricavato da un semplice calcolo manuale ; tale scostamento di valore risulta accettabile e se ne deduce quindi che i risultati forniti dal calcolo automatico del telaio spaziale risultano attendibili.

VERIFICA DEI PILASTRI

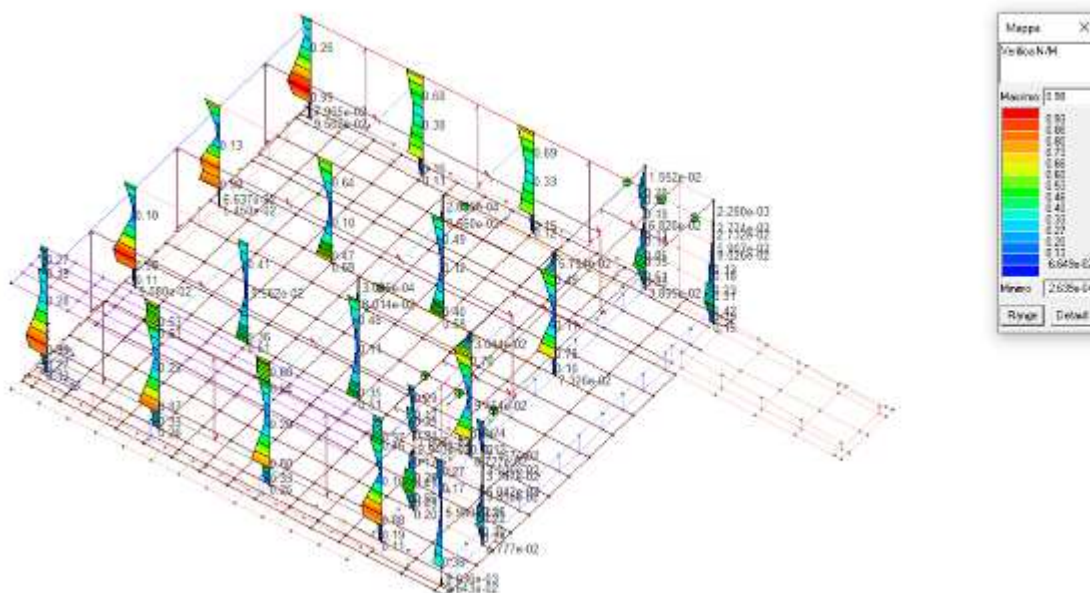
Si riportano di seguito le verifiche a pressoflessione deviata e a taglio relative ai pilastri maggiormente sollecitati :

- Verifica a pressoflessione per SLU

Il pilastro principale maggiormente sollecitato risulta avere il seguente coefficiente di sfruttamento dei materiali :

$$\eta = 0.99 \leq 1 \quad (\text{VERIFICATO})$$

Di seguito si riporta l'andamento del coefficiente di sfruttamento dei materiali a pressoflessione deviata lungo il fusto dei pilastri:

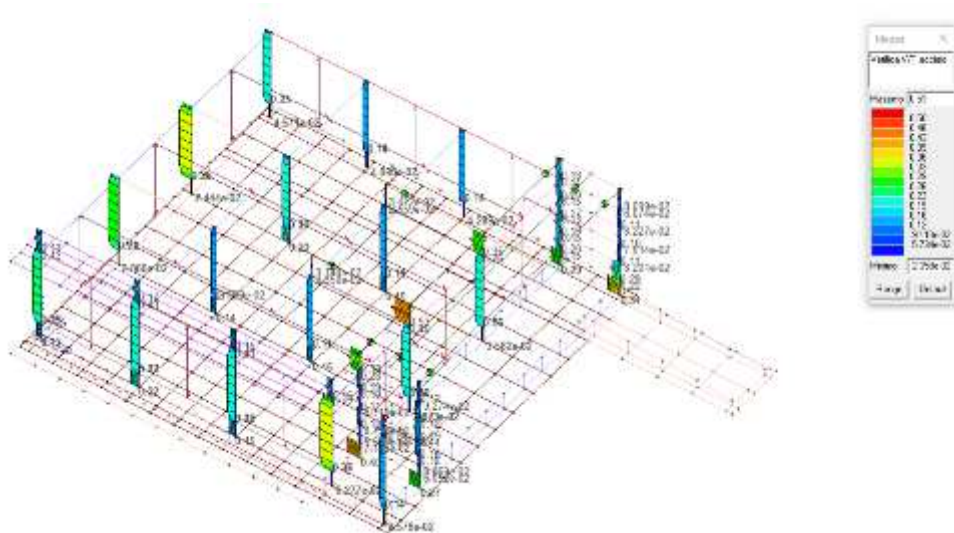


- Verifica a taglio lato acciaio per SLU

Il pilastro principale maggiormente sollecitato risulta avere il seguente coefficiente di sfruttamento dei materiali :

$$\eta = 0.53 \leq 1 \quad (\text{VERIFICATO})$$

Di seguito si riporta l'andamento del coefficiente di sfruttamento dei materiali a taglio lungo il fusto dei pilastri:

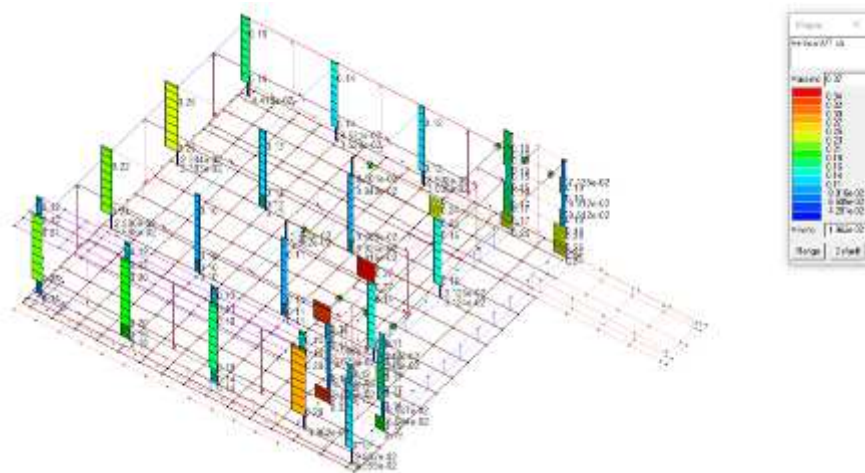


- Verifica a taglio lato cls per SLU

Il pilastro principale maggiormente sollecitato risulta avere il seguente coefficiente di sfruttamento dei materiali :

$$\eta = 0.37 \leq 1 \quad (\text{VERIFICATO})$$

Di seguito si riporta l'andamento del coefficiente di sfruttamento dei materiali a taglio lungo il fusto dei pilastri:



VERIFICA DELLE TRAVI PRINCIPALI

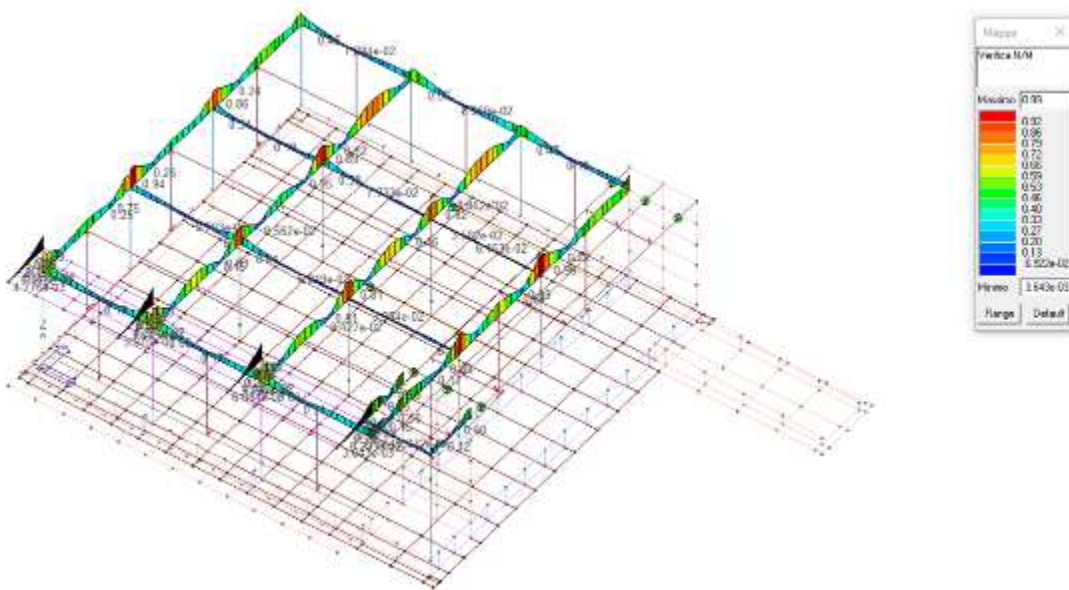
Si riportano di seguito le verifiche a flessione e a taglio relative alle travi maggiormente sollecitate :

- Verifica a flessione per SLU

La trave principale maggiormente sollecitata risulta avere il seguente coefficiente di sfruttamento dei materiali :

$$\eta = 0.99 \leq 1 \quad (\text{VERIFICATO})$$

Di seguito si riporta l'andamento del coefficiente di sfruttamento dei materiali a flessione deviata lungo l'asse delle travi:

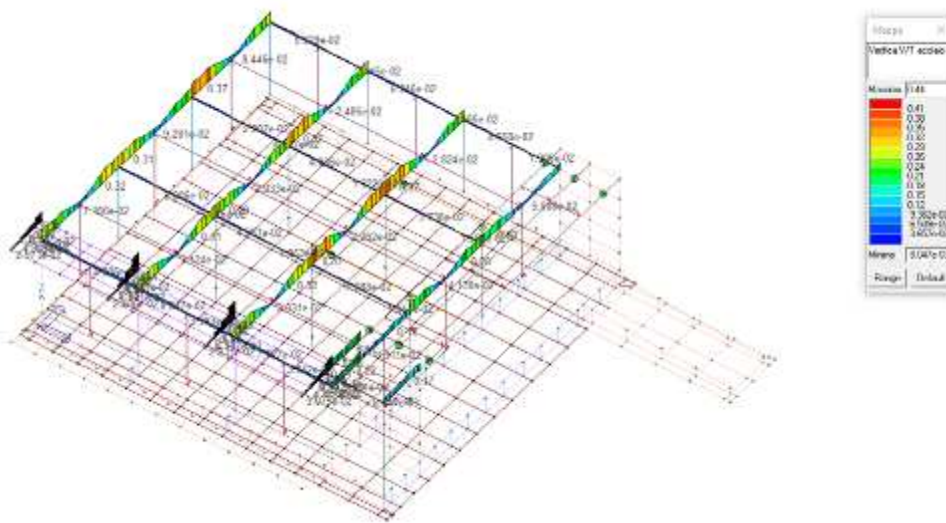


- Verifica a taglio lato acciaio per SLU

La trave principale maggiormente sollecitata risulta avere il seguente coefficiente di sfruttamento dei materiali :

$$\eta = 0.44 \leq 1 \quad (\text{VERIFICATO})$$

Di seguito si riporta l'andamento del coefficiente di sfruttamento dei materiali a taglio lungo l'asse delle travi:

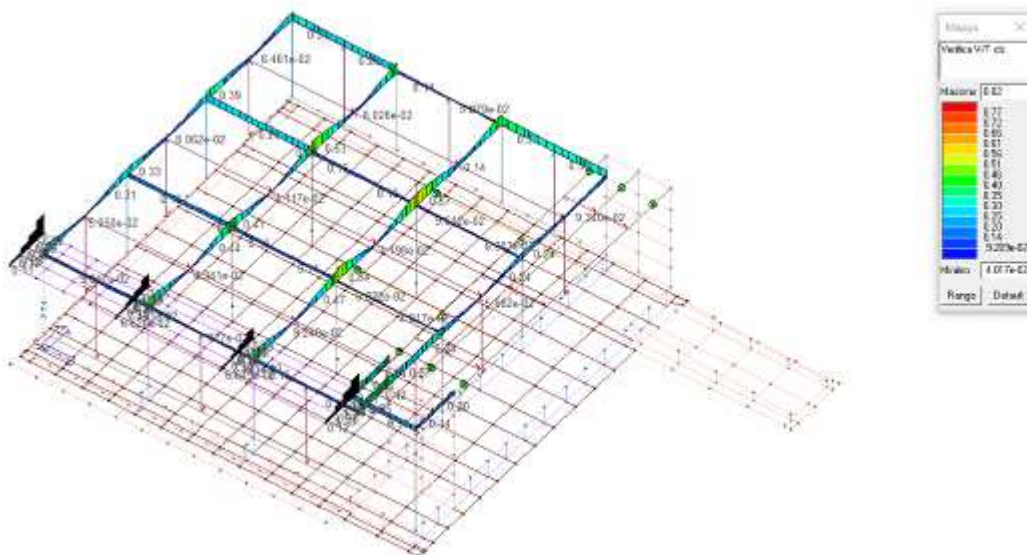


- Verifica a taglio lato cls per SLU

La trave principale maggiormente sollecitata risulta avere il seguente coefficiente di sfruttamento dei materiali :

$$\eta = 0.82 \leq 1 \quad (\text{VERIFICATO})$$

Di seguito si riporta l'andamento del coefficiente di sfruttamento dei materiali a taglio lungo l'asse delle travi:



VERIFICA DEI SOLAI

Solaio H24 DELLA COPERTURA

Analisi dei carichi

Permanenti Glk	: 400*1.20	= 480 daN/m
Permanenti non strutt. G2k	: 400*1.20	= 480 "
Variabili Q	: 120*1.20	= 144 "

Carico agente sul solaio allo SLE rara :

$$P_{SLE\ rara} = 480 + 480 + 144 = 1104 \text{ daN/m}$$

Carico agente sul solaio allo SLU :

$$P_{SLU} = 480 * 1.3 + 480 * 1.5 + 144 * 1.5 = 1560 \text{ daN/m}$$

Verifica a Flessione

Il momento max in mezzzeria risulta valere :

$$M_{SLE\ rara} = 1104 * 4.93^2 / 12.5 = 2146 \text{ daNm}$$

$$M_{SLU} = 1560 * 4.93^2 / 12.5 = 3033 \text{ daNm}$$

Per la verifica a flessione del solaio H24 si veda il fascicolo dei calcoli.

Il momento max negativo nell'appoggio centrale risulta valere :

$$M_{SLE\ rara} = 1104 * 4.93^2 / 10 = -2683 \text{ daNm}$$

$$M_{SLU} = 1560 * 4.93^2 / 10 = -3791 \text{ daNm}$$

Per la verifica a flessione del solaio H24 si veda il fascicolo dei calcoli.

VERIFICA DELLE FONDAZIONI

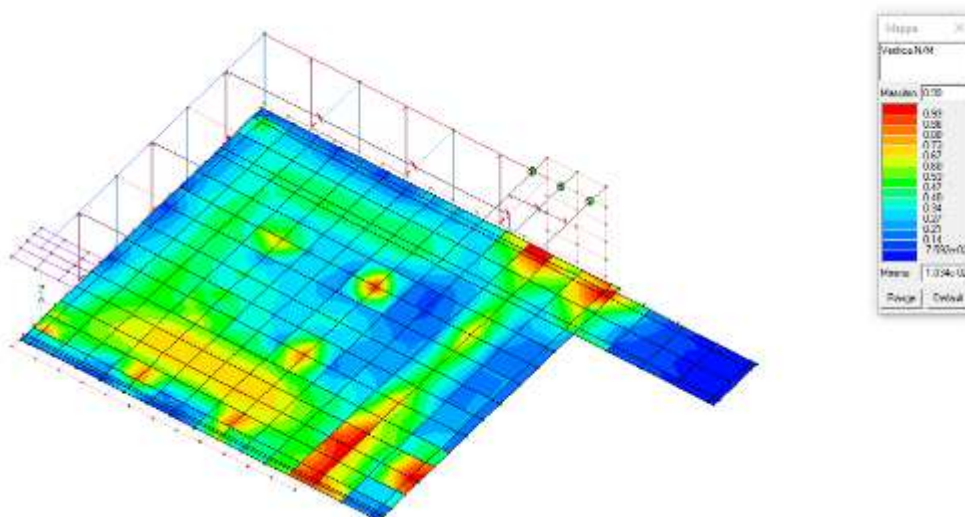
Si riportano di seguito le verifiche più rappresentative a flessione relative alla platea di fondazione :

- *Verifica a flessione per SLU*

La trave principale maggiormente sollecitata risulta avere il seguente coefficiente di sfruttamento dei materiali :

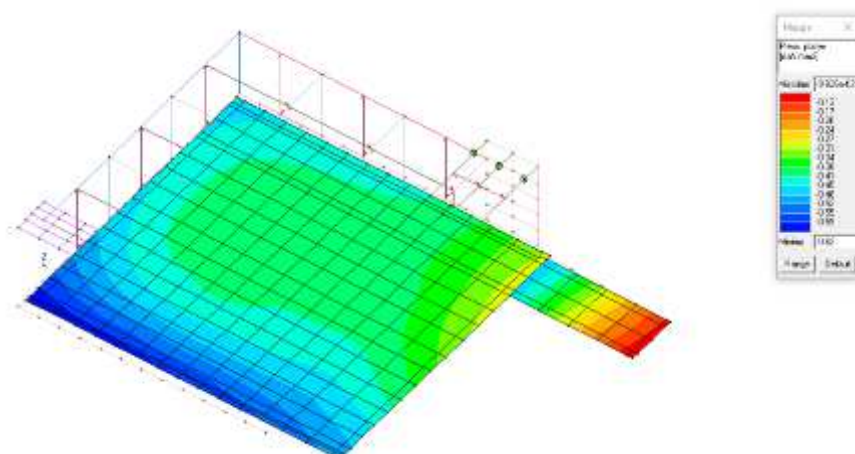
$$\eta = 1.0 \leq 1 \quad (\text{VERIFICATO})$$

Di seguito si riporta l'andamento del coefficiente di sfruttamento dei materiali a flessione sulla superficie della platea:

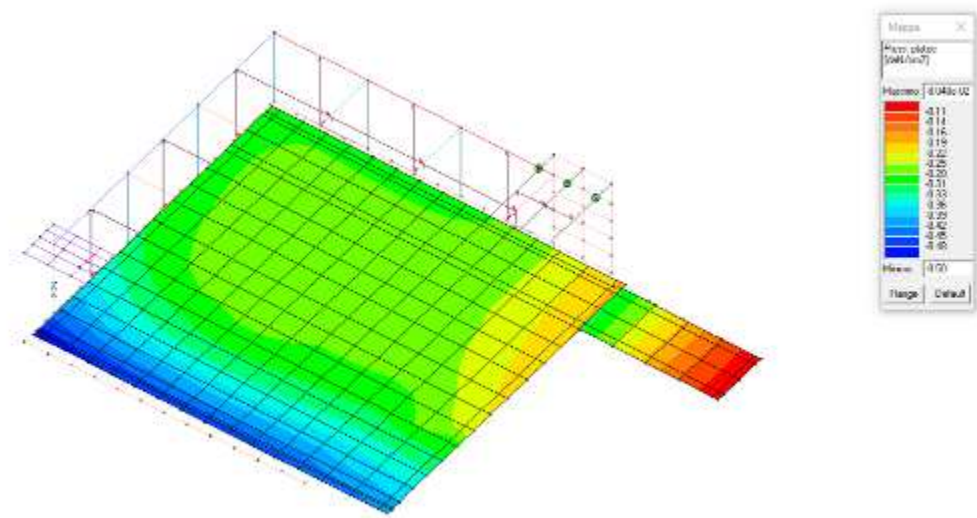


Si riportano di seguito la pressione esercitata dalla platea sul terreno sottostante nelle varie condizioni di carico :

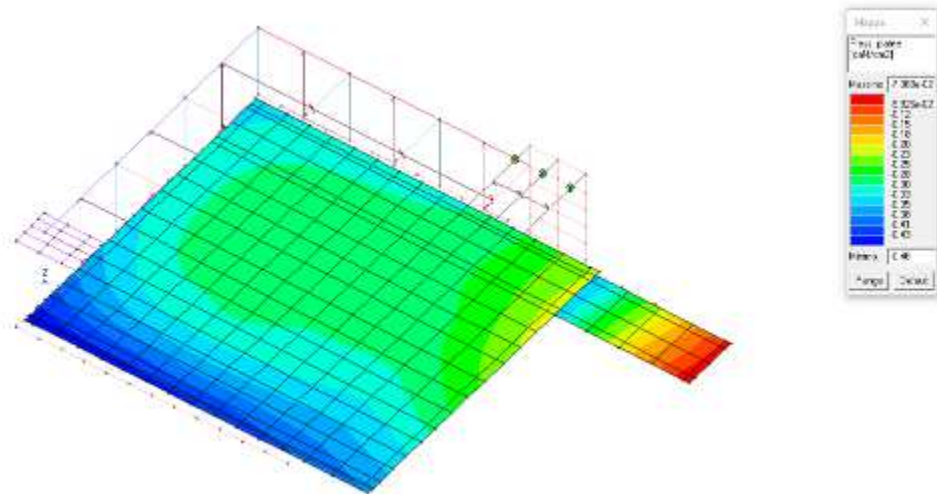
Condizione : SLU statica



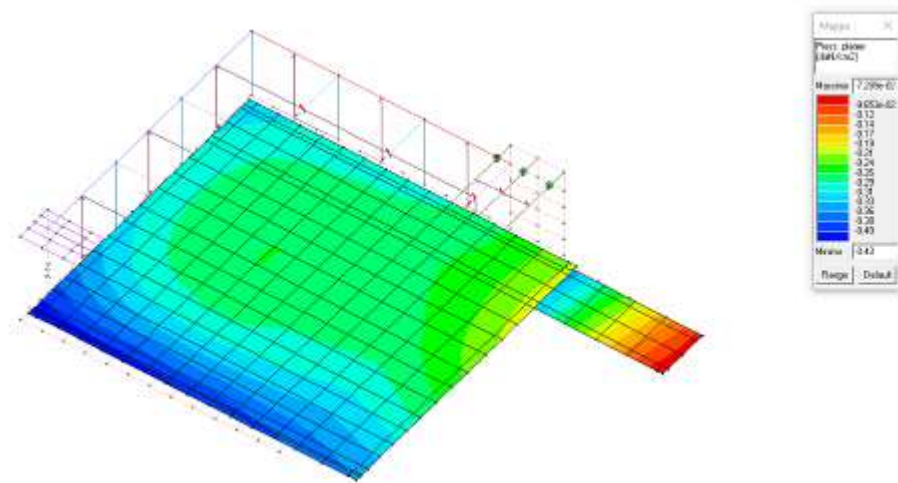
Condizione : SLV sismica



Condizione : SLE rara



Condizione : SLE q. perm.





Relazione di calcolo strutturale impostata e redatta secondo le modalità previste nel D.M. 17 Gennaio 2018 cap. 10 “Redazione dei progetti strutturali esecutivi e delle relazioni di calcolo”.

Origine e Caratteristiche dei Codici di Calcolo	
Codice di calcolo:	PRO_SAP PROfessional Structural Analysis Program
Versione:	PROFESSIONAL (build 2023-05-199B)
Produttore-Distributore:	2S.I. Software e Servizi per l'Ingegneria s.r.l. Via Garibaldi, 90 44121 Ferrara FE (Italy) Tel. +39 0532 200091 www.2si.it

Descrizione	
Progetto	NUOVO POLO BIBLIOTECARIO IN VIALE DANTE ALIGHIERI N.46 PIACENZA
Ubicazione	Comune di PIACENZA (PC) (Regione EMILIA-ROMAGNA)
	Località PIACENZA (PC)
	Longitudine 9.689, Latitudine 45.042
Progettista	Dott. Ing.StefanoTassi
	Via Pisaroni 14 Piacenza

In merito al punto 10.2 delle Norme Tecniche per le Costruzioni (*Affidabilità dei codici utilizzati*), si fa riferimento al **Documento di Affidabilità** “Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST” disponibile per il download sul sito: <https://www.2si.it/it/prodotti/affidabilita/>

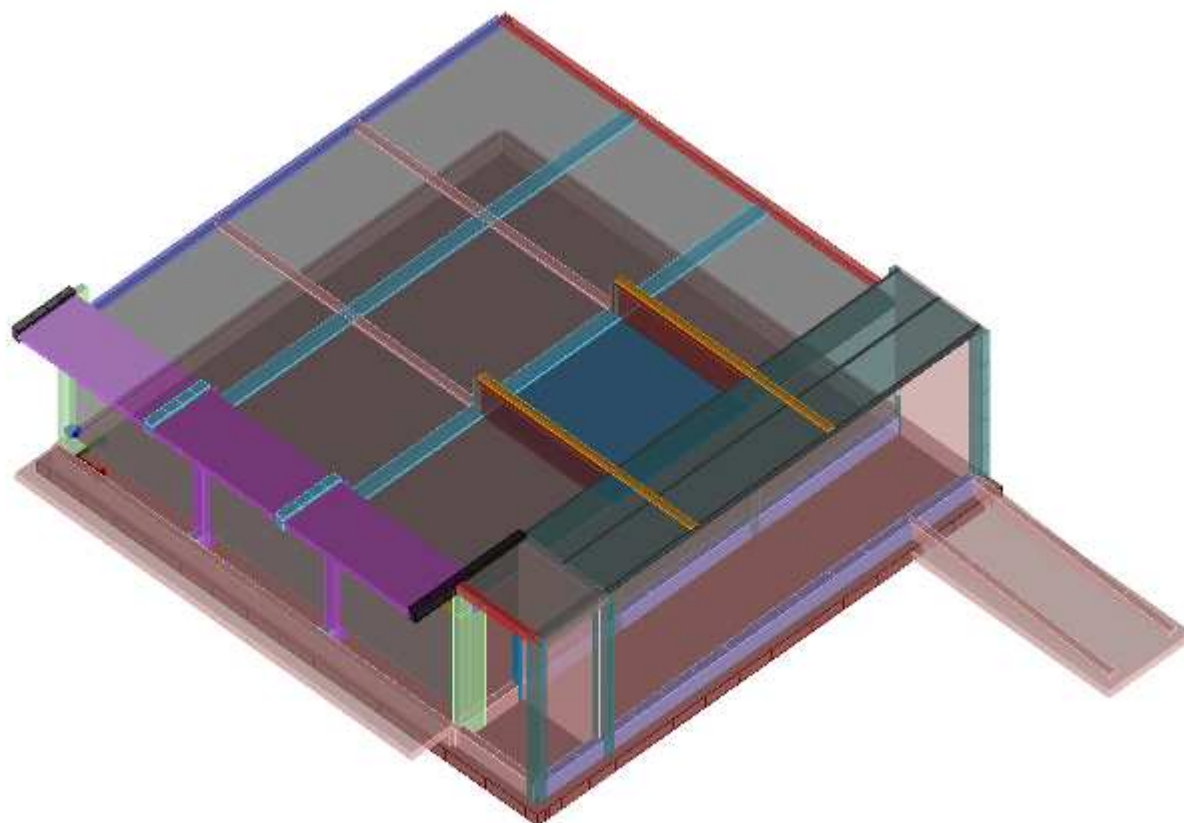
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INTESTAZIONE E CONTENUTI DELLA RELAZIONE

PROGETTO

Progetto : **NUOVO POLO BIBLIOTECARIO IN VIALE DANTE ALIGHIERI N.46 PIACENZA**



Modello 3D

RELAZIONE DI CALCOLO STRUTTURALE

DESCRIZIONE GENERALE DELL'OPERA

Descrizione generale dell'opera	
Fabbricato ad uso	Biblioteca
Ubicazione	Comune di PIACENZA (PC) (Regione EMILIA-ROMAGNA) Località PIACENZA (PC) Longitudine 9.689, Latitudine 45.042
Numero di piani	Fuori terra : Piano terra + piano copertura Interrati : -
Numero vani scale	-
Numero vani ascensore	-
Tipo di fondazione	Platea

Principali caratteristiche della struttura	
Struttura regolare in pianta	si
Struttura regolare in altezza	si
Classe di duttilità	Non Dissipativo
Travi: ricalate o in spessore	50x24,80x24,30x24,25x24
Pilastri	30x30,50x30,50x25,90x25
Pilastri in falso	-
Tipo di fondazione	Platea
Condizioni per cui è necessario considerare la componente verticale del sisma	Nessuna

Parametri della struttura			
Classe d'uso	Vita Vn [anni]	Coeff. Uso	Periodo Vr [anni]
II	50.0	1.0	50.0

Fattore di struttura/comportamento		
Caratteristiche costruzione		
Tipologia	Nuova	
Regolarità pianta	SI	
Regolarità altezza	SI	
Classe di duttilità	ND	
Sistema costruttivo	Calcestruzzo	
Tipologia strutturale	Strutture a telaio, a pareti accoppiate, miste	
Definizione rapporto α_u/α_1	Valore come da normativa	
Riferimento normativo α_u/α_1	Strutture a telaio di un piano	
Parametri		
α_u/α_1	1.100	
$q_0 = 3.000 \alpha_u/\alpha_1$	3.300	
k_w	1.000	
K_R	1.0	
$q_D = q_0 \cdot k_w \cdot K_R$	3.300	
$q_{ND} = 2/3 \cdot q_D$	1.500 (≤ 1.5)	
Fattori di comportamento		
		Non dissipativi
q SLU x		1.500
q SLU y		1.500

QUADRO NORMATIVO DI RIFERIMENTO ADOTTATO

Le norme ed i documenti assunti quale riferimento per la progettazione strutturale vengono indicati di seguito. Nel capitolo "normativa di riferimento" è comunque presente l'elenco completo delle normative disponibili.

Progetto-verifica degli elementi	
Progetto cemento armato	D.M. 17-01-2018
Progetto acciaio	D.M. 17-01-2018
Azione sismica	
Norma applicata per l'azione sismica	D.M. 17-01-2018

AZIONI DI PROGETTO SULLA COSTRUZIONE

Nei capitoli “modellazione delle azioni” e “schematizzazione dei casi di carico” sono indicate le azioni sulla costruzione.

Nel prosieguo si indicano tipo di analisi strutturale condotta (statico, dinamico, lineare o non lineare) e il metodo adottato per la risoluzione del problema strutturale nonché le metodologie seguite per la verifica o per il progetto-verifica delle sezioni. Si riportano le combinazioni di carico adottate e, nel caso di calcoli non lineari, i percorsi di carico seguiti; le configurazioni studiate per la struttura in esame *sono risultate effettivamente esaustive per la progettazione-verifica*.

La verifica della sicurezza degli elementi strutturali avviene con i metodi della scienza delle costruzioni. L'analisi strutturale è condotta con il metodo degli spostamenti per la valutazione dello stato tensodeformativo indotto da carichi statici. L'analisi strutturale è condotta con il metodo dell'analisi modale e dello spettro di risposta in termini di accelerazione per la valutazione dello stato tensodeformativo indotto da carichi dinamici (tra cui quelli di tipo sismico).

L'analisi strutturale viene effettuata con il metodo degli elementi finiti. Il metodo sopraindicato si basa sulla schematizzazione della struttura in elementi connessi solo in corrispondenza di un numero prefissato di punti denominati nodi. I nodi sono definiti dalle tre coordinate cartesiane in un sistema di riferimento globale. Le incognite del problema (nell'ambito del metodo degli spostamenti) sono le componenti di spostamento dei nodi riferite al sistema di riferimento globale (traslazioni secondo X, Y, Z, rotazioni attorno X, Y, Z). La soluzione del problema si ottiene con un sistema di equazioni algebriche lineari i cui termini noti sono costituiti dai carichi agenti sulla struttura opportunamente concentrati ai nodi:

$$\mathbf{K} \cdot \mathbf{u} = \mathbf{F} \text{ dove}$$

\mathbf{K} = matrice di rigidezza
 \mathbf{u} = vettore spostamenti nodali
 \mathbf{F} = vettore forze nodali

Dagli spostamenti ottenuti con la risoluzione del sistema vengono quindi dedotte le sollecitazioni e/o le tensioni di ogni elemento, riferite generalmente ad una terna locale all'elemento stesso.

Il sistema di riferimento utilizzato è costituito da una terna cartesiana destrorsa XYZ. Si assume l'asse Z verticale ed orientato verso l'alto.

Gli elementi utilizzati per la modellazione dello schema statico della struttura sono i seguenti:

Elemento tipo TRUSS	(biella-D2)
Elemento tipo BEAM	(trave-D2)
Elemento tipo MEMBRANE	(membrana-D3)
Elemento tipo PLATE	(piastra-guscio-D3)
Elemento tipo BOUNDARY	(molla)
Elemento tipo STIFFNESS	(matrice di rigidezza)
Elemento tipo BRICK	(elemento solido)
Elemento tipo SOLAIO	(macro elemento composto da più membrane)

MODELLO NUMERICO

In questa parte viene descritto il modello numerico utilizzato (o i modelli numerici utilizzati) per l'analisi della struttura. La presentazione delle informazioni deve essere, coerentemente con le prescrizioni del paragrafo 10.2 e relativi sottoparagrafi delle NTC-18, tale da garantirne la leggibilità, la corretta interpretazione e la riproducibilità

Tipo di analisi strutturale	
Sismica statica lineare	NO
Sismica dinamica lineare	SI
Sismica statica non lineare (prop. masse)	NO
Sismica statica non lineare (prop. modo)	NO
Sismica statica non lineare (triangolare)	NO
Non linearità geometriche (fattore P delta)	NO
Analisi lineare	SI

Di seguito si indicano l'origine e le caratteristiche dei codici di calcolo utilizzati riportando titolo, produttore e distributore, versione, estremi della licenza d'uso:

Informazioni sul codice di calcolo	
Titolo:	PRO_SAP PROfessional Structural Analysis Program
Versione:	PROFESSIONAL (build 2023-05-199B)
Produttore-Distributore:	2S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Un attento esame preliminare della documentazione a corredo del software **ha consentito di valutarne l'affidabilità e soprattutto l'idoneità al caso specifico**. La documentazione, fornita dal produttore e distributore del software, contiene una esauriente descrizione delle basi teoriche e degli algoritmi impiegati, l'individuazione dei campi d'impiego, nonché casi prova interamente risolti e commentati,

corredati dei file di input necessari a riprodurre l'elaborazione:

Affidabilità dei codici utilizzati

2S.I. ha verificato l'affidabilità e la robustezza del codice di calcolo attraverso un numero significativo di casi prova in cui i risultati dell'analisi numerica sono stati confrontati con soluzioni teoriche.
E' possibile reperire la documentazione contenente alcuni dei più significativi casi trattati al seguente link:
<https://www.2si.it/it/prodotti/affidabilita/>

Modellazione della geometria e proprietà meccaniche:

nodi	607
elementi D2 (per aste, travi, pilastri...)	124
elementi D3 (per pareti, platee, gusci...)	510
elementi solaio	28
elementi solidi	0

Dimensione del modello strutturale [cm]:

X min =	-42.50
Xmax =	2555.50
Ymin =	-214.00
Ymax =	1641.00
Zmin =	0.00
Zmax =	606.00

Strutture verticali:

Elementi di tipo asta	NO
Pilastri	SI
Pareti	SI
Setti (a comportamento membranale)	NO

Strutture non verticali:

Elementi di tipo asta	NO
Travi	SI
Gusci	SI
Membrane	NO

Orizzontamenti:

Solai con la proprietà piano rigido	SI
Solai senza la proprietà piano rigido	SI

Tipo di vincoli:

Nodi vincolati rigidamente	NO
Nodi vincolati elasticamente	NO
Nodi con isolatori sismici	NO
Fondazioni puntuali (plinti/plinti su palo)	NO
Fondazioni di tipo trave	NO
Fondazioni di tipo platea	SI
Fondazioni con elementi solidi	NO

MODELLAZIONE DELLE AZIONI

Si veda il capitolo **“Schematizzazione dei casi di carico”** per le informazioni necessarie alla comprensione ed alla ricostruzione delle azioni applicate al modello numerico, coerentemente con quanto indicato nella parte *“2.6. Azioni di progetto sulla costruzione”*.

COMBINAZIONI E/O PERCORSI DI CARICO

Si veda il capitolo **“Definizione delle combinazioni”** in cui sono indicate le combinazioni di carico adottate e, nel caso di calcoli non lineari, i percorsi di carico seguiti.

Combinazioni dei casi di carico

APPROCCIO PROGETTUALE	Approccio 2
SLU	SI
SLV (SLU con sisma)	SI

SLC	NO
SLD	SI
SLO	NO
SLU GEO A2 (per approccio 1)	NO
SLU EQU	NO
Combinazione caratteristica (rara)	SI
Combinazione frequente	SI
Combinazione quasi permanente (SLE)	SI
SLA (accidentale quale incendio)	NO

Principali risultati

I risultati devono costituire una sintesi completa ed efficace, presentata in modo da riassumere il comportamento della struttura, per ogni tipo di analisi svolta.

Nella presente relazione di calcolo sono riportati i seguenti risultati che il progettista ritiene di interesse per la descrizione e la comprensione del/i modello/i e del comportamento della struttura:

per l'analisi modale:

- periodi dei modi di vibrare della struttura
- masse eccitate dai singoli modi
- massa eccitata totale

deformate e sollecitazioni:

- spostamenti e rotazioni dei singoli nodi della struttura
- reazioni vincolari (nel caso siano presenti nodi vincolati rigidamente)
- pressioni sul terreno (nel caso siano presenti elementi di fondazione)
- sollecitazioni sugli elementi d2 nelle combinazioni di calcolo più significative
- tensioni sugli elementi d3 nelle combinazioni di calcolo più significative
- sollecitazioni sui macroelementi da elementi d3 nelle combinazioni di calcolo più significative

La presente relazione, oltre ad illustrare in modo esaustivo i dati in ingresso ed i risultati delle analisi in forma tabellare, riporta una serie di immagini:

per i dati in ingresso:

- modello solido della struttura
- numerazione di nodi e ed elementi
- configurazioni di carico statiche
- configurazioni di carico sismiche con baricentri delle masse e eccentricità

per le combinazioni più significative (statisticamente più gravose per la struttura):

- configurazioni deformate
- diagrammi e involucri delle azioni interne
- mappe delle tensioni
- reazioni vincolari
- mappe delle pressioni sul terreno

per il progetto-verifica degli elementi:

- diagrammi di armatura
- percentuali di sfruttamento
- mappe delle verifiche più significative per i vari stati limite

Informazioni generali sull'elaborazione e giudizio motivato di accettabilità dei risultati.

Il programma prevede una serie di controlli automatici (check) che consentono l'individuazione di errori di modellazione. Al termine dell'analisi un controllo automatico identifica la presenza di spostamenti o rotazioni abnormi. Si può pertanto asserire che l'elaborazione sia corretta e completa. I risultati delle elaborazioni sono stati sottoposti a controlli che ne comprovano l'attendibilità. Tale valutazione ha compreso il confronto con i risultati di semplici calcoli, eseguiti con metodi tradizionali e adottati, anche in fase di primo proporzionamento della struttura. Inoltre, sulla base di considerazioni riguardanti gli stati tensionali e deformativi determinati, si è valutata la validità delle scelte operate in sede di schematizzazione e di modellazione della struttura e delle azioni. Si allega al termine della presente relazione elenco sintetico dei controlli svolti (verifiche di equilibrio tra reazioni vincolari e carichi applicati, comparazioni tra i risultati delle analisi e quelli di valutazioni semplificate, etc.).

VERIFICHE AGLI STATI LIMITE ULTIMI

Nel capitolo relativo alla progettazione degli elementi strutturali agli SLU vengono indicate, con riferimento alla normativa adottata, le modalità ed i criteri seguiti per valutare la sicurezza della struttura nei confronti delle possibili situazioni di crisi ed i risultati delle valutazioni svolte. In via generale, oltre alle verifiche di resistenza e di spostamento, devono essere prese in considerazione verifiche nei confronti dei fenomeni di instabilità, locale e globale, di fatica, di duttilità, di degrado.

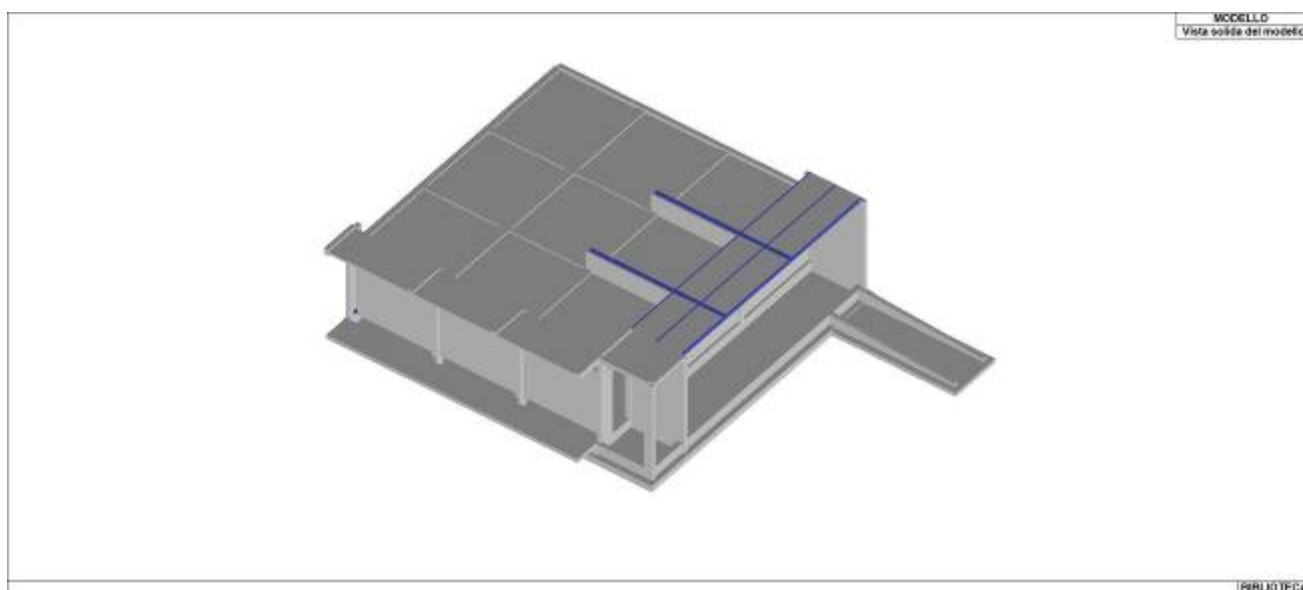
VERIFICHE AGLI STATI LIMITE DI ESERCIZIO

Nel capitolo relativo alla progettazione degli elementi strutturali agli SLE vengono indicate, con riferimento alla normativa adottata, le modalità seguite per valutare l'affidabilità della struttura nei confronti delle possibili situazioni di perdita di funzionalità (per eccessive deformazioni, fessurazioni, vibrazioni, etc.) ed i risultati delle valutazioni svolte.

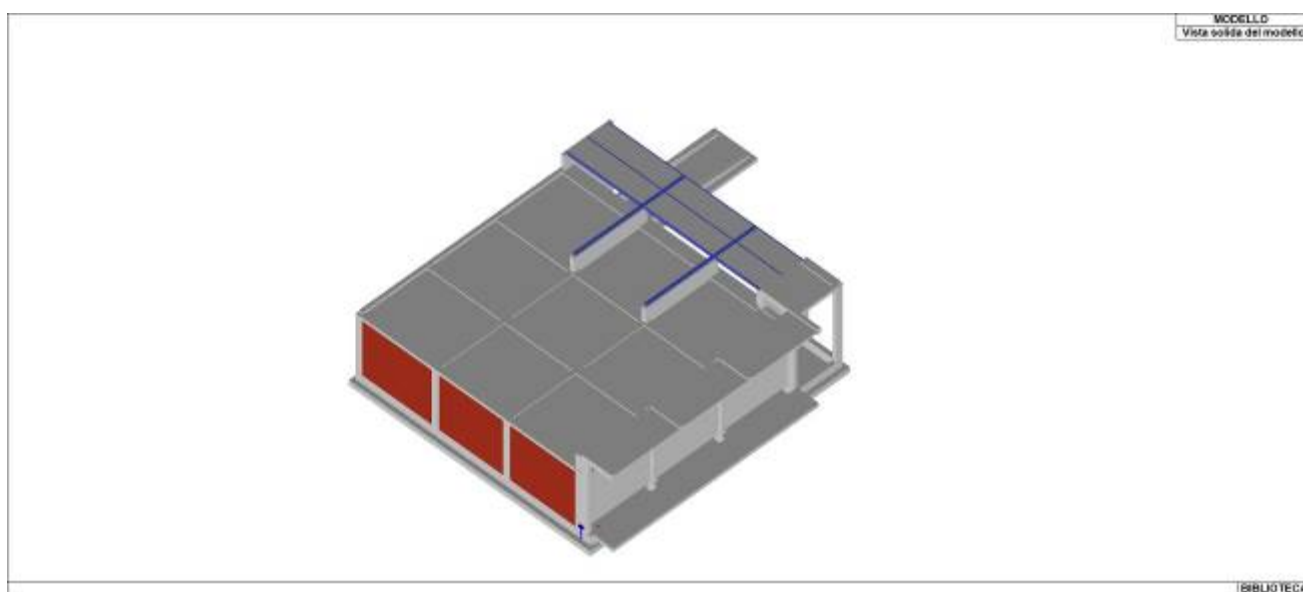
NORMATIVA DI RIFERIMENTO

2. D.Min. Infrastrutture Min. Interni e Prot. Civile 17 Gennaio 2018 e allegate "Norme tecniche per le costruzioni".
3. Circolare 21/01/19, n. 7 C.S.LL.PP "Istruzioni per l'applicazione dell'aggiornamento delle Norme Tecniche delle Costruzioni di cui al decreto ministeriale 17 gennaio 2018"
4. D.Min. Infrastrutture e trasporti 14 Settembre 2005 e allegate "Norme tecniche per le costruzioni".
5. D.M. LL.PP. 9 Gennaio 1996 "Norme tecniche per il calcolo, l'esecuzione ed il collaudo delle strutture in cemento armato, normale e precompresso e per le strutture metalliche".
6. D.M. LL.PP. 16 Gennaio 1996 "Norme tecniche relative ai <<Criteri generali per la verifica di sicurezza delle costruzioni e dei carichi e sovraccarichi>>".
7. D.M. LL.PP. 16 Gennaio 1996 "Norme tecniche per le costruzioni in zone sismiche".
8. Circolare 4/07/96, n.156AA.GG./STC. istruzioni per l'applicazione delle "Norme tecniche relative ai <<Criteri generali per la verifica di sicurezza delle costruzioni e dei carichi e sovraccarichi>>" di cui al D.M. 16/01/96.
9. Circolare 10/04/97, n.65AA.GG. istruzioni per l'applicazione delle "Norme tecniche per le costruzioni in zone sismiche" di cui al D.M. 16/01/96.
10. D.M. LL.PP. 20 Novembre 1987 "Norme tecniche per la progettazione, esecuzione e collaudo degli edifici in muratura e per il loro consolidamento".
11. Circolare 4 Gennaio 1989 n. 30787 "Istruzioni in merito alle norme tecniche per la progettazione, esecuzione e collaudo degli edifici in muratura e per il loro consolidamento".
12. D.M. LL.PP. 11 Marzo 1988 "Norme tecniche riguardanti le indagini sui terreni e sulle rocce, la stabilità dei pendii naturali e delle scarpate, i criteri generali e le prescrizioni per la progettazione, l'esecuzione e il collaudo delle opere di sostegno delle terre e delle opere di fondazione".
13. D.M. LL.PP. 3 Dicembre 1987 "Norme tecniche per la progettazione, esecuzione e collaudo delle costruzioni prefabbricate".
14. UNI 9502 - Procedimento analitico per valutare la resistenza al fuoco degli elementi costruttivi di conglomerato cementizio armato, normale e precompresso - edizione maggio 2001
15. Ordinanza del Presidente del Consiglio dei Ministri n. 3274 del 20 marzo 2003 "Primi elementi in materia di criteri generali per la classificazione sismica del territorio nazionale e di normative tecniche per le costruzioni in zona sismica" e successive modificazioni e integrazioni.
16. UNI EN 1990:2006 13/04/2006 Eurocodice 0 - Criteri generali di progettazione strutturale.
17. UNI EN 1991-1-1:2004 01/08/2004 Eurocodice 1 - Azioni sulle strutture - Parte 1-1: Azioni in generale - Pesi per unità di volume, pesi propri e sovraccarichi per gli edifici.
18. UNI EN 1991-2:2005 01/03/2005 Eurocodice 1 - Azioni sulle strutture - Parte 2: Carichi da traffico sui ponti.
19. UNI EN 1991-1-3:2004 01/10/2004 Eurocodice 1 - Azioni sulle strutture - Parte 1-3: Azioni in generale - Carichi da neve.
20. UNI EN 1991-1-4:2005 01/07/2005 Eurocodice 1 - Azioni sulle strutture - Parte 1-4: Azioni in generale - Azioni del vento.
21. UNI EN 1991-1-5:2004 01/10/2004 Eurocodice 1 - Azioni sulle strutture - Parte 1-5: Azioni in generale - Azioni termiche.
22. UNI EN 1992-1-1:2005 24/11/2005 Eurocodice 2 - Progettazione delle strutture di calcestruzzo - Parte 1-1: Regole generali e regole per gli edifici.
23. UNI EN 1992-1-2:2005 01/04/2005 Eurocodice 2 - Progettazione delle strutture di calcestruzzo - Parte 1-2: Regole generali - Progettazione strutturale contro l'incendio.
24. UNI EN 1993-1-1:2005 01/08/2005 Eurocodice 3 - Progettazione delle strutture di acciaio - Parte 1-1: Regole generali e regole per gli edifici.
25. UNI EN 1993-1-8:2005 01/08/2005 Eurocodice 3 - Progettazione delle strutture di acciaio - Parte 1-8: Progettazione dei collegamenti.
26. UNI EN 1994-1-1:2005 01/03/2005 Eurocodice 4 - Progettazione delle strutture composte acciaio-calcestruzzo - Parte 1-1: Regole generali e regole per gli edifici.
27. UNI EN 1994-2:2006 12/01/2006 Eurocodice 4 - Progettazione delle strutture composte acciaio-calcestruzzo - Parte 2: Regole generali e regole per i ponti.
28. UNI EN 1995-1-1:2005 01/02/2005 Eurocodice 5 - Progettazione delle strutture di legno - Parte 1-1: Regole generali - Regole comuni e regole per gli edifici.
29. UNI EN 1995-2:2005 01/01/2005 Eurocodice 5 - Progettazione delle strutture di legno - Parte 2: Ponti.
30. UNI EN 1996-1-1:2006 26/01/2006 Eurocodice 6 - Progettazione delle strutture di muratura - Parte 1-1: Regole generali per strutture di muratura armata e non armata.
31. UNI EN 1996-3:2006 09/03/2006 Eurocodice 6 - Progettazione delle strutture di muratura - Parte 3: Metodi di calcolo semplificato per strutture di muratura non armata.
32. UNI EN 1997-1:2005 01/02/2005 Eurocodice 7 - Progettazione geotecnica - Parte 1: Regole generali.
33. UNI EN 1998-1:2005 01/03/2005 Eurocodice 8 - Progettazione delle strutture per la resistenza sismica - Parte 1: Regole generali, azioni sismiche e regole per gli edifici.
34. UNI EN 1998-3:2005 01/08/2005 Eurocodice 8 - Progettazione delle strutture per la resistenza sismica - Parte 3: Valutazione e adeguamento degli edifici.
35. UNI EN 1998-5:2005 01/01/2005 Eurocodice 8 - Progettazione delle strutture per la resistenza sismica - Parte 5: Fondazioni, strutture di contenimento ed aspetti geotecnici.
36. CNR DT-200/2013 - Istruzioni per la Progettazione, l'Esecuzione ed il Controllo di Interventi di Consolidamento Statico mediante l'utilizzo di Compositi Fibrorinforzati
37. CNR DT-215/2018 - Istruzioni per la Progettazione, l'Esecuzione ed il Controllo di Interventi di Consolidamento Statico mediante l'utilizzo di Compositi Fibrorinforzati a Matrice Inorganica

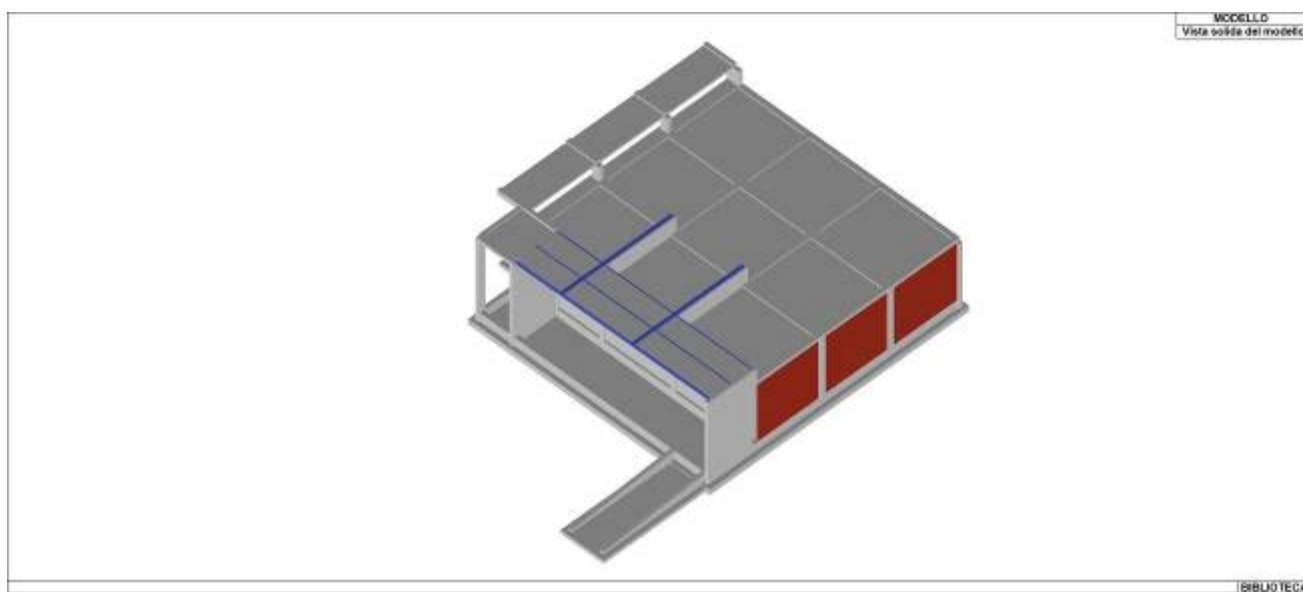
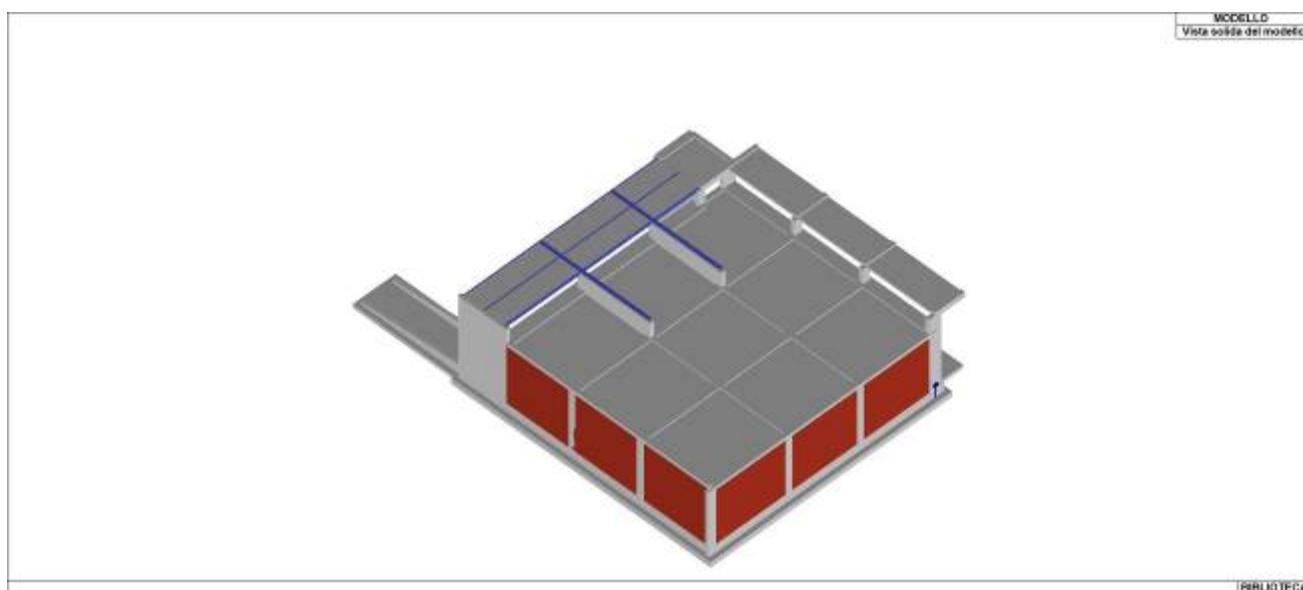
NOTA: il presente capitolo riporta l'elenco delle normative implementate nel software. Le norme utilizzate per la struttura oggetto della presente relazione sono indicate nel precedente capitolo "RELAZIONE DI CALCOLO STRUTTURALE" "ANALISI E VERIFICHE SVOLTE CON L'AUSILIO DI CODICI DI CALCOLO".



01_INT_VISTA_SOLIDA_001



01_INT_VISTA_SOLIDA_002



CARATTERISTICHE MATERIALI UTILIZZATI

LEGENDA TABELLA DATI MATERIALI

Il programma consente l'uso di materiali diversi. Sono previsti i seguenti tipi di materiale:

1	materiale tipo cemento armato
2	materiale tipo acciaio

I materiali utilizzati nella modellazione sono individuati da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni materiale vengono riportati in tabella i seguenti dati:

Young	modulo di elasticità normale E
Poisson	coefficiente di contrazione trasversale ν
G	modulo di elasticità tangenziale
Gamma	peso specifico
Alfa	coefficiente di dilatazione termica
Fattore di confidenza FC m	Fattore di confidenza specifico per materiale; (è riportato solo se diverso da quello globale della struttura)
Fattore di confidenza FC a	Fattore di confidenza specifico per l'armatura (è riportato solo se diverso da quello globale della struttura)
Elasto-plastico	Materiale elastico perfettamente plastico per aste non lineari
Massima compressione	Massima tensione di compressione per aste non lineari
Massima trazione	Massima tensione di trazione per aste non lineari
Fattore attrito	Coefficiente di attrito per aste non lineari
Rapporto HRDb	Rapporto di hardening a flessione
Rapporto HRDv	Rapporto di hardening a taglio

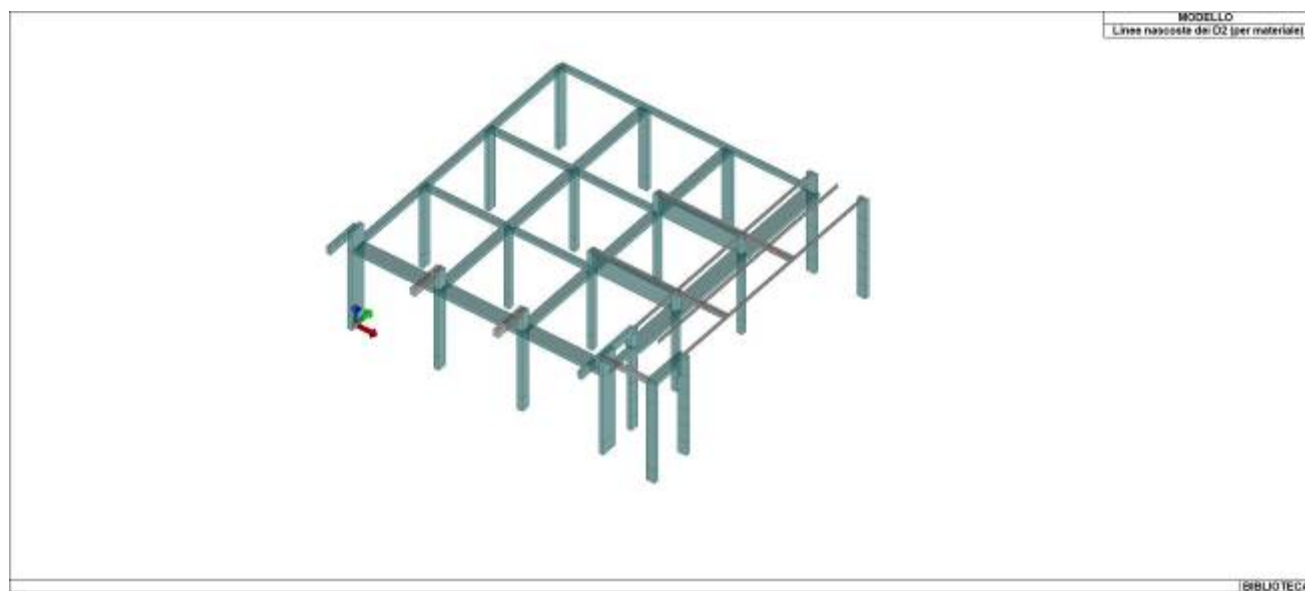
I dati soprariportati vengono utilizzati per la modellazione dello schema statico e per la determinazione dei carichi inerziali e termici. In relazione al tipo di materiale vengono riportati inoltre:

1 c.a.	Resistenza Rc Resistenza fctm Coefficiente ksb	resistenza a compressione cubica resistenza media a trazione semplice Coefficiente di riduzione della resistenza a compressione da utilizzare nello stress block
2 acciaio	Tensione ft Tensione fy Resistenza fd Resistenza fd (>40) Tensione ammissibile Tensione ammissibile(>40)	Valore della tensione di rottura Valore della tensione di snervamento Resistenza di calcolo per SL CNR-UNI 10011 Resistenza di calcolo per SL CNR-UNI 10011 per spessori > 40mm Tensione ammissibile CNR-UNI 10011 Tensione ammissibile CNR-UNI 10011 per spessori > 40mm

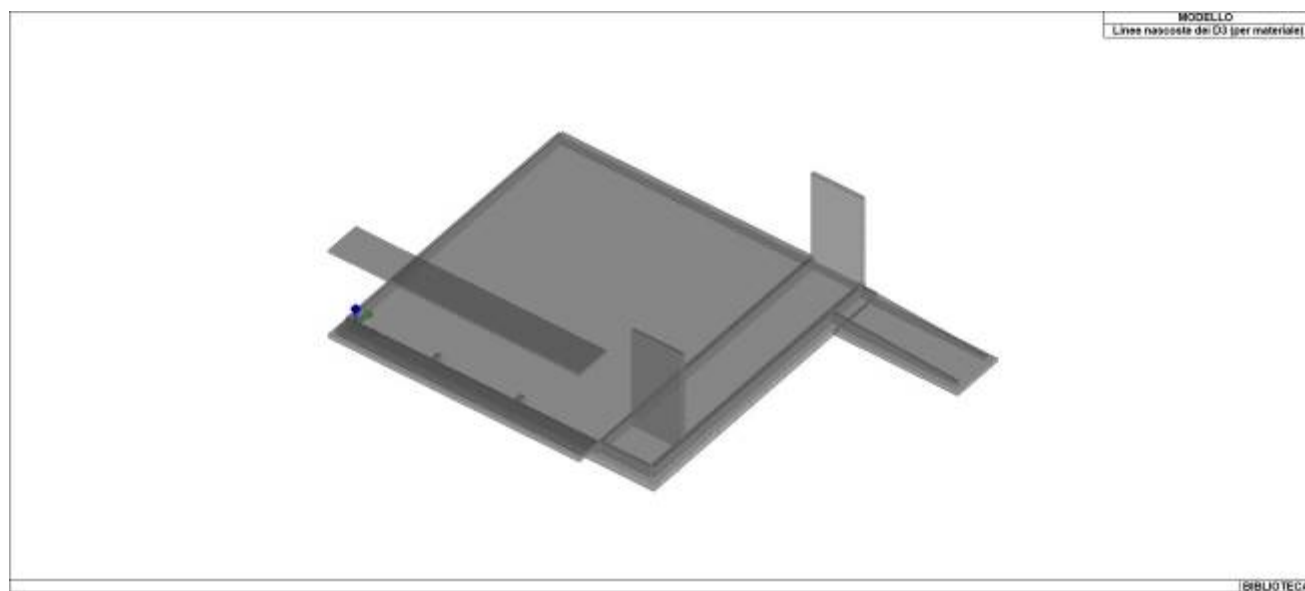
Vengono inoltre riportate le tabelle contenenti il riassunto delle informazioni assegnate nei criteri di progetto in uso.

Id	Tipo / Note	V. caratt.	V. medio	Young	Poisson	G	Gamma	Alfa	Altri
		daN/cm ²	daN/cm ²	daN/cm ²		daN/cm ²	daN/cm ³		
1	Calcestruzzo Classe C25/30			3.145e+05	0.20	1.310e+05	2.50e-03	0.0	
	Resistenza Rc	300.0							
	Resistenza fctm		25.6						
	Rapporto Rfessurata (assiale)								1.00
	Rapporto Rfessurata (flessione)								0.75
	Rapporto Rfessurata (taglio)								0.75
	Coefficiente ksb								0.85
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05
3	Calcestruzzo Classe C28/35			3.259e+05	0.20	1.358e+05	2.50e-03	0.0	
	Resistenza Rc	350.0							
	Resistenza fctm		28.4						
	Rapporto Rfessurata (assiale)								1.00
	Rapporto Rfessurata (flessione)								1.00
	Rapporto Rfessurata (taglio)								1.00
	Coefficiente ksb								0.85
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05
12	Acciaio Fe430 - S275-acciaio Fe430-S275			2.100e+06	0.30	8.077e+05	7.85e-03	0.0	

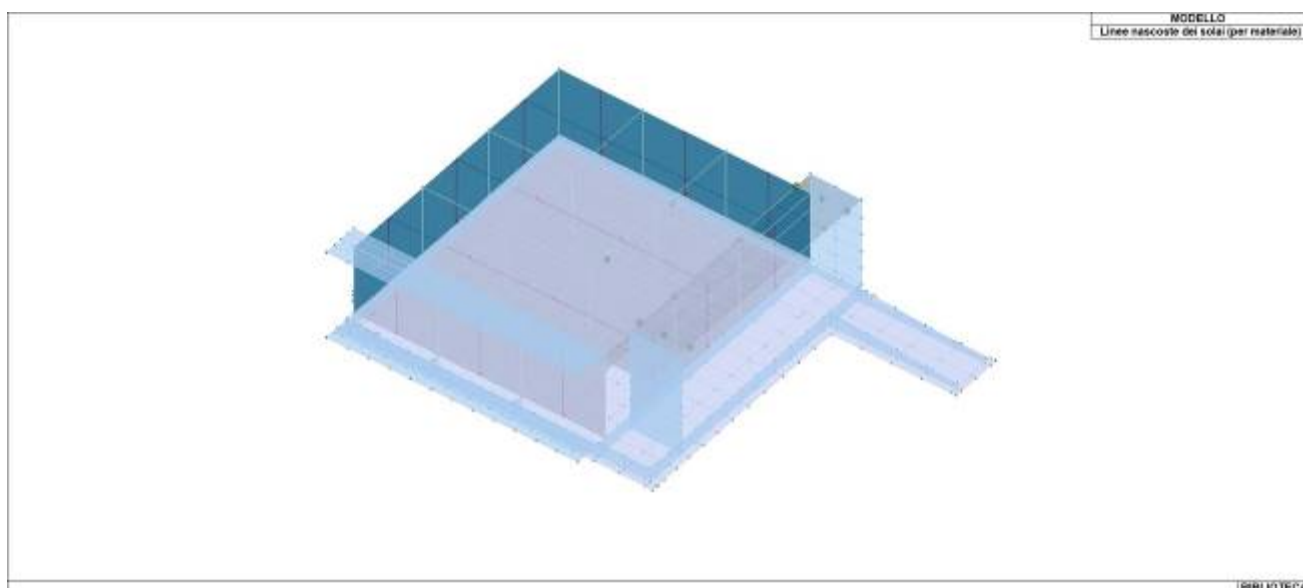
Id	Tipo / Note	V. caratt.	V. medio	Young	Poisson	G	Gamma	Alfa	Altri
	Tensione ft	4300.0							
	Resistenza fd	2750.0							
	Resistenza fd (>40)	2500.0							
	Tensione ammissibile	1900.0							
	Tensione ammissibile (>40)	1700.0							
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05



11_MOD_MATERIALI_D2



11_MOD_MATERIALI_D3



11_MOD_MATERIALI_SOLAI

MODELLAZIONE DELLE SEZIONI

LEGENDA TABELLA DATI SEZIONI

Il programma consente l'uso di sezioni diverse. Sono previsti i seguenti tipi di sezione:

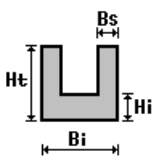
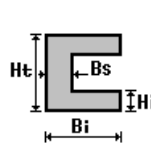
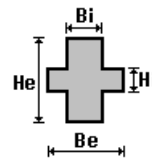
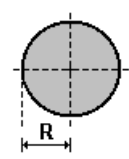
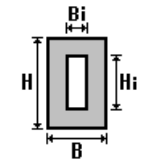
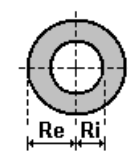
1. sezione di tipo generico
2. profilati semplici
3. profilati accoppiati e speciali

Le sezioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni sezione vengono riportati in tabella i seguenti dati:

Area	area della sezione
A V2	area della sezione/fattore di taglio (per il taglio in direzione 2)
A V3	area della sezione/fattore di taglio (per il taglio in direzione 3)
Jt	fattore torsionale di rigidezza
J2-2	momento d'inerzia della sezione riferito all'asse 2
J3-3	momento d'inerzia della sezione riferito all'asse 3
W2-2	modulo di resistenza della sezione riferito all'asse 2
W3-3	modulo di resistenza della sezione riferito all'asse 3
Wp2-2	modulo di resistenza plastico della sezione riferito all'asse 2
Wp3-3	modulo di resistenza plastico della sezione riferito all'asse 3

I dati sopra riportati vengono utilizzati per la determinazione dei carichi inerziali e per la definizione delle rigidezze degli elementi strutturali; qualora il valore di Area V2 (e/o Area V3) sia nullo la deformabilità per taglio V2 (e/o V3) è trascurata. La valutazione delle caratteristiche inerziali delle sezioni è condotta nel riferimento 2-3 dell'elemento.

rettangolare	a T	a T rovescia	a T di colmo	a L	a L specchiata
a L specchiata rovescia	a L rovescia	a L di colmo	a doppio T	a quattro specchiata	a quattro

					
a U	a C	a croce	circolare	rettangolare cava	circolare cava

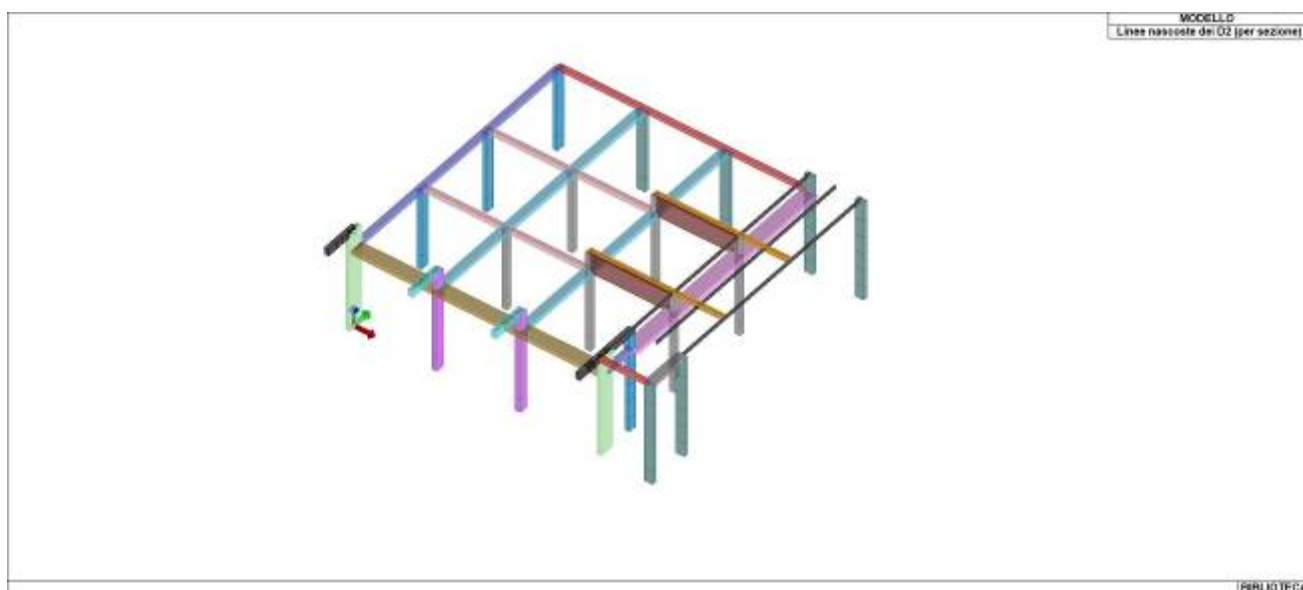
Per quanto concerne i profilati semplici ed accoppiati l'asse 2 del riferimento coincide con l'asse x riportato nei più diffusi profilati.

Per quanto concerne le sezioni di tipo generico (tipo 1.):

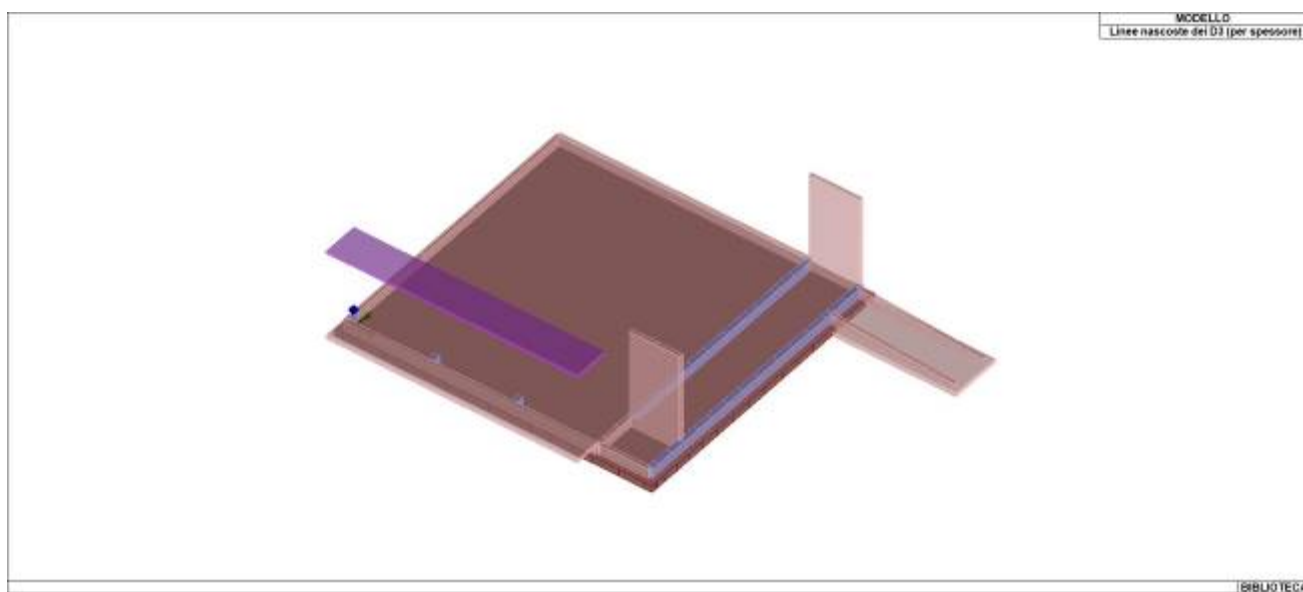
i valori dimensionali con prefisso B sono riferiti all'asse 2

i valori dimensionali con prefisso H sono riferiti all'asse 3

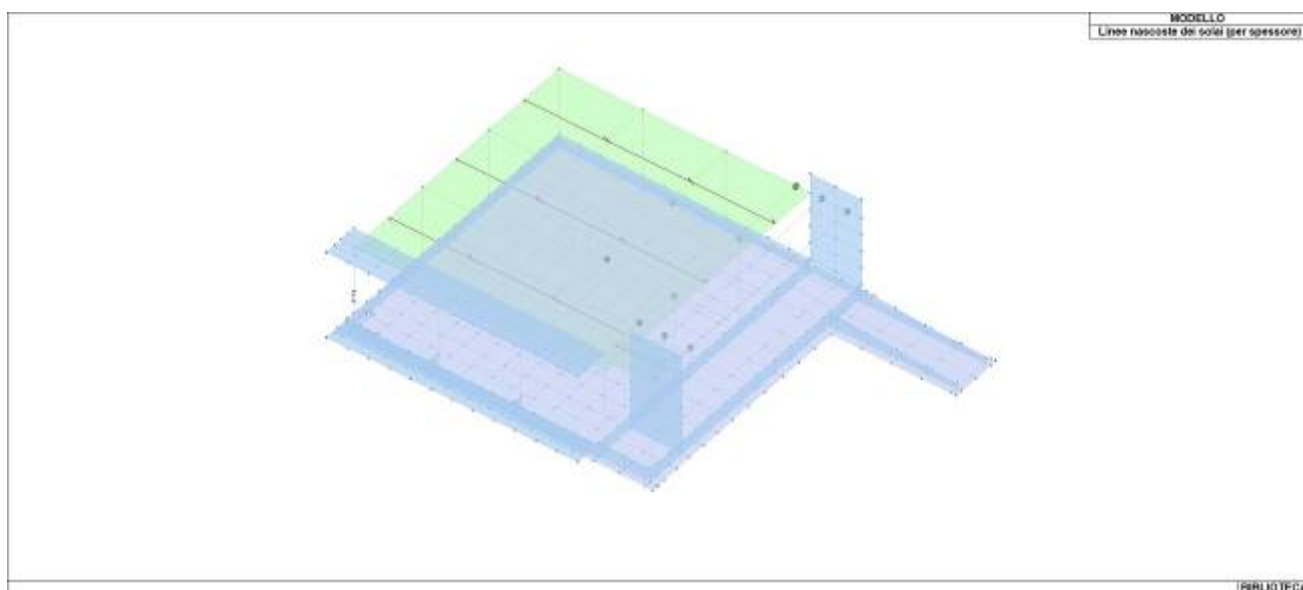
Id	Tipo	Area	A V2	A V3	Jt	J 2-2	J 3-3	W 2-2	W 3-3	Wp 2-2	Wp 3-3
		cm2	cm2	cm2	cm4	cm4	cm4	cm3	cm3	cm3	cm3
1	Pilastro - Rettangolare: b=30 h=30	900.00	750.00	750.00	1.139e+05	6.750e+04	6.750e+04	4500.00	4500.00	6750.00	6750.00
2	Pilastro - Rettangolare: b=50 h=25	1250.00	1041.67	1041.67	1.784e+05	2.604e+05	6.510e+04	1.042e+04	5208.33	1.562e+04	7812.50
3	Pilastro - Rettangolare: b=25 h=50	1250.00	1041.67	1041.67	1.784e+05	6.510e+04	2.604e+05	5208.33	1.042e+04	7812.50	1.562e+04
4	Pilastro - Rettangolare: b=90 h=25	2250.00	1875.00	1875.00	3.867e+05	1.519e+06	1.172e+05	3.375e+04	9375.00	5.062e+04	1.406e+04
5	Trave - Rettangolare: b=50 h=24	1200.00	1000.00	1000.00	1.607e+05	2.500e+05	5.760e+04	1.000e+04	4800.00	1.500e+04	7200.00
6	Trave - Rettangolare: b=35 h=24	840.00	700.00	700.00	9.287e+04	8.575e+04	4.032e+04	4900.00	3360.00	7350.00	5040.00
7	Trave - Rettangolare: b=85 h=24	2040.00	1700.00	1700.00	3.220e+05	1.228e+06	9.792e+04	2.890e+04	8160.00	4.335e+04	1.224e+04
8	Trave - Rettangolare: b=30 h=24	720.00	600.00	600.00	7.126e+04	5.400e+04	3.456e+04	3600.00	2880.00	5400.00	4320.00
9	Trave - Rettangolare: b=25 h=24	600.00	500.00	500.00	5.042e+04	3.125e+04	2.880e+04	2500.00	2400.00	3750.00	3600.00
10	HEB 240	106.00	0.0	0.0	102.70	3923.00	1.126e+04	326.90	938.30	498.40	1053.10
11	IPE 160	20.10	0.0	0.0	3.60	68.00	869.00	16.70	108.70	26.10	123.90
12	trave - Rettangolare: b=50 h=24	1200.00	1000.00	1000.00	1.607e+05	2.500e+05	5.760e+04	1.000e+04	4800.00	1.500e+04	7200.00
13	trave - Rettangolare: b=30 h=40	1200.00	1000.00	1000.00	1.946e+05	9.000e+04	1.600e+05	6000.00	8000.00	9000.00	1.200e+04
14	Tave - Rettangolare: b=25 h=40	1000.00	833.33	833.33	1.263e+05	5.208e+04	1.333e+05	4166.67	6666.67	6250.00	1.000e+04
15	Pilastro - Rettangolare: b=50 h=30	1500.00	1250.00	1250.00	2.799e+05	3.125e+05	1.125e+05	1.250e+04	7500.00	1.875e+04	1.125e+04
16	Trave alta di copertura - Rettangolare: b=30 h=118	3540.00	2950.00	2950.00	8.919e+05	2.655e+05	4.108e+06	1.770e+04	6.962e+04	2.655e+04	1.044e+05
17	Trave - Rettangolare: b=80 h=24	1920.00	1600.00	1600.00	2.990e+05	1.024e+06	9.216e+04	2.560e+04	7680.00	3.840e+04	1.152e+04



13_MOD_SEZIONI



13_MOD_SPESSORI_D3



13_MOD_SPESSORI_D5

MODELLAZIONE STRUTTURA: NODI

LEGENDA TABELLA DATI NODI

Il programma utilizza per la modellazione nodi strutturali.

Ogni nodo è individuato dalle coordinate cartesiane nel sistema di riferimento globale (X Y Z).

Ad ogni nodo è eventualmente associato un codice di vincolamento rigido, un codice di fondazione speciale, ed un set di sei molle (tre per le traslazioni, tre per le rotazioni). Le tabelle sottoriportate riflettono le succitate possibilità. In particolare per ogni nodo viene indicato in tabella:

Nodo	numero del nodo.
X	valore della coordinata X
Y	valore della coordinata Y
Z	valore della coordinata Z

Per i nodi ai quali sia associato un codice di vincolamento rigido, un codice di fondazione speciale o un set di molle viene indicato in tabella:

Nodo	numero del nodo.
X	valore della coordinata X
Y	valore della coordinata Y
Z	valore della coordinata Z
Note	eventuale codice di vincolo (es. v=110010 sei valori relativi ai sei gradi di libertà previsti per il nodo TxTyTzRxRyRz, il valore 1 indica che lo spostamento o rotazione relativo è impedito, il valore 0 indica che lo spostamento o rotazione relativo è libero).
Note	(FS = 1, 2,...) eventuale codice del tipo di fondazione speciale (1, 2,... fanno riferimento alle tipologie: plinto, palo, plinto su pali,...) che è collegato al nodo. (ISO = "id SIGLA") indice e sigla identificativa dell' eventuale isolatore sismico assegnato al nodo
Rig. TX	valore della rigidezza dei vincoli elastici eventualmente applicati al nodo, nello specifico TX (idem per TY, TZ, RX, RY, RZ).

Per strutture sismicamente isolate viene inoltre inserita la tabella delle caratteristiche per gli isolatori utilizzati; le caratteristiche sono indicate in conformità al cap. 7.10 del D.M. 17/01/18

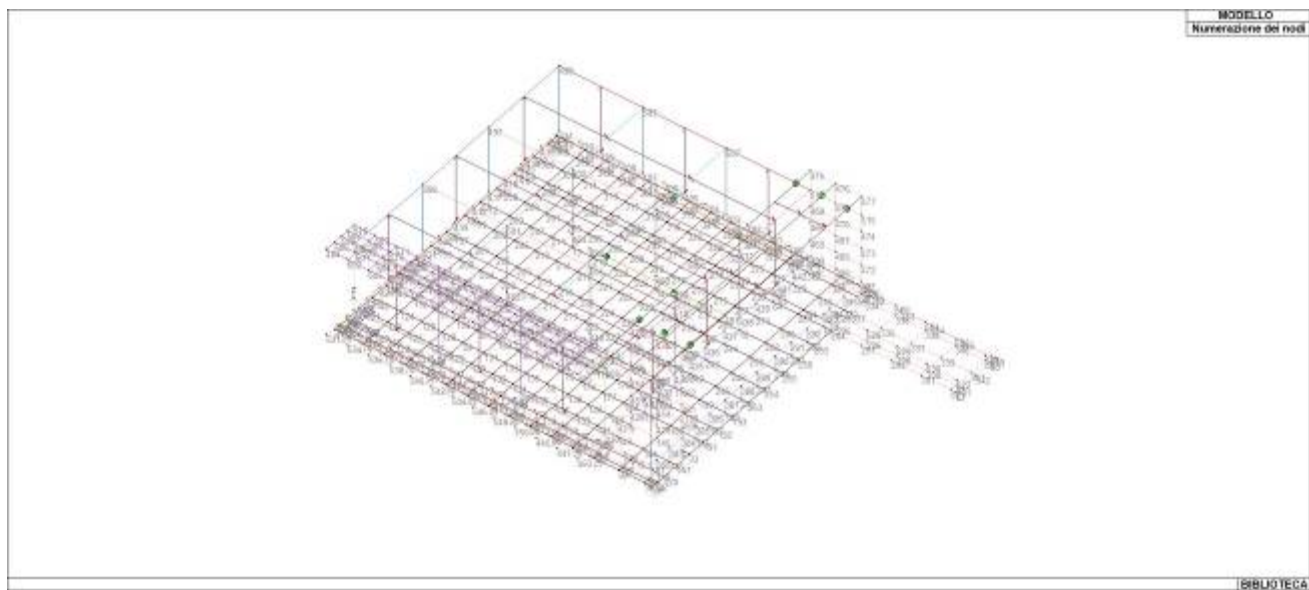
TABELLA DATI NODI

Nodo	X	Y	Z	Nodo	X	Y	Z	Nodo	X	Y	Z
	cm	cm	cm		cm	cm	cm		cm	cm	cm
1	0.0	0.0	0.0	2	493.5	0.0	0.0	3	983.5	0.0	0.0
4	1477.0	0.0	0.0	5	1777.5	-48.5	0.0	6	1777.5	198.5	0.0
7	1477.0	198.5	0.0	8	0.0	537.0	0.0	9	493.5	537.0	0.0
10	983.5	537.0	0.0	11	1477.0	537.0	0.0	12	0.0	1049.0	0.0
13	493.5	1049.0	0.0	14	983.5	1049.0	0.0	15	1477.0	1049.0	0.0
16	0.0	1598.5	0.0	17	493.5	1598.5	0.0	18	983.5	1598.5	0.0
19	1477.0	1598.5	0.0	20	1777.5	1598.5	0.0	21	1477.0	-48.5	0.0
22	1477.0	-62.5	0.0	23	983.5	-62.5	0.0	24	493.5	-62.5	0.0
25	0.0	-62.5	0.0	26	0.0	-91.0	0.0	27	493.5	-91.0	0.0
28	983.5	-91.0	0.0	29	1477.0	-91.0	0.0	30	1777.5	-91.0	0.0
31	1822.5	-91.0	0.0	32	1822.5	-48.5	0.0	33	1822.5	198.5	0.0
34	1627.2	1598.5	0.0	35	1822.5	1641.0	0.0	36	1777.5	1641.0	0.0
37	1477.0	1641.0	0.0	38	983.5	1641.0	0.0	39	493.5	1641.0	0.0
40	0.0	1641.0	0.0	41	-42.5	1641.0	0.0	42	-42.5	1598.5	0.0
43	-42.5	1049.0	0.0	44	-42.5	537.0	0.0	45	-42.5	0.0	0.0
46	-42.5	-62.5	0.0	47	-42.5	-91.0	0.0	48	0.0	198.5	0.0
49	493.5	198.5	0.0	50	983.5	198.5	0.0	51	-42.5	198.5	0.0
52	1777.5	1347.0	0.0	53	1777.5	1572.0	0.0	54	2525.5	1572.0	0.0
55	2525.5	1347.0	0.0	56	2525.5	1614.0	0.0	57	2525.5	1305.0	0.0
58	1777.5	1305.0	0.0	59	2555.5	1614.0	0.0	60	2555.5	1572.0	0.0
61	2555.5	1347.0	0.0	62	2555.5	1305.0	0.0	63	1477.0	1347.0	0.0
64	1477.0	1305.0	0.0	65	983.5	1347.0	0.0	66	983.5	1305.0	0.0
67	493.5	1347.0	0.0	68	493.5	1305.0	0.0	69	0.0	1347.0	0.0
70	0.0	1305.0	0.0	71	-42.5	1347.0	0.0	72	-42.5	1305.0	0.0
73	123.4	-62.5	0.0	74	123.4	-91.0	0.0	75	246.8	-62.5	0.0
76	246.8	-91.0	0.0	77	370.1	-62.5	0.0	78	370.1	-91.0	0.0
79	616.0	-62.5	0.0	80	616.0	-91.0	0.0	81	738.5	-62.5	0.0
82	738.5	-91.0	0.0	83	861.0	-62.5	0.0	84	861.0	-91.0	0.0

Nodo	X	Y	Z	Nodo	X	Y	Z	Nodo	X	Y	Z
85	1106.9	-62.5	0.0	86	1106.9	-91.0	0.0	87	1230.2	-62.5	0.0
88	1230.2	-91.0	0.0	89	1353.6	-62.5	0.0	90	1353.6	-91.0	0.0
91	1777.5	-62.5	0.0	92	1627.2	-62.5	0.0	93	1627.2	-91.0	0.0
94	1822.5	-62.5	0.0	95	1627.2	-48.5	0.0	96	983.5	-48.5	0.0
97	1106.9	-48.5	0.0	98	1230.2	-48.5	0.0	99	1353.6	-48.5	0.0
100	493.5	-48.5	0.0	101	616.0	-48.5	0.0	102	738.5	-48.5	0.0
103	861.0	-48.5	0.0	104	0.0	-48.5	0.0	105	123.4	-48.5	0.0
106	246.8	-48.5	0.0	107	370.1	-48.5	0.0	108	-42.5	-48.5	0.0
109	123.4	0.0	0.0	110	246.8	0.0	0.0	111	370.1	0.0	0.0
112	616.0	0.0	0.0	113	738.5	0.0	0.0	114	861.0	0.0	0.0
115	1106.9	0.0	0.0	116	1230.2	0.0	0.0	117	1353.6	0.0	0.0
118	1777.5	0.0	0.0	119	1627.2	0.0	0.0	120	1822.5	0.0	0.0
121	0.0	99.2	0.0	122	-42.5	99.2	0.0	123	123.4	99.2	0.0
124	123.4	198.5	0.0	125	246.8	99.2	0.0	126	246.8	198.5	0.0
127	370.1	99.2	0.0	128	370.1	198.5	0.0	129	493.5	99.2	0.0
130	616.0	99.2	0.0	131	616.0	198.5	0.0	132	738.5	99.2	0.0
133	738.5	198.5	0.0	134	861.0	99.2	0.0	135	861.0	198.5	0.0
136	983.5	99.2	0.0	137	1106.9	99.2	0.0	138	1106.9	198.5	0.0
139	1230.2	99.2	0.0	140	1230.2	198.5	0.0	141	1353.6	99.2	0.0
142	1353.6	198.5	0.0	143	1477.0	99.2	0.0	144	1627.2	99.2	0.0
145	1627.2	198.5	0.0	146	1777.5	99.2	0.0	147	1822.5	99.2	0.0
148	-42.5	308.0	0.0	149	0.0	308.0	0.0	150	-42.5	417.5	0.0
151	0.0	417.5	0.0	152	123.4	308.0	0.0	153	123.4	417.5	0.0
154	123.4	537.0	0.0	155	246.8	308.0	0.0	156	246.8	417.5	0.0
157	246.8	537.0	0.0	158	370.1	308.0	0.0	159	370.1	417.5	0.0
160	370.1	537.0	0.0	161	493.5	308.0	0.0	162	493.5	417.5	0.0
163	616.0	308.0	0.0	164	616.0	417.5	0.0	165	616.0	537.0	0.0
166	738.5	308.0	0.0	167	738.5	417.5	0.0	168	738.5	537.0	0.0
169	861.0	308.0	0.0	170	861.0	417.5	0.0	171	861.0	537.0	0.0
172	983.5	308.0	0.0	173	983.5	417.5	0.0	174	1106.9	308.0	0.0
175	1106.9	417.5	0.0	176	1106.9	537.0	0.0	177	1230.2	308.0	0.0
178	1230.2	417.5	0.0	179	1230.2	537.0	0.0	180	1353.6	308.0	0.0
181	1353.6	417.5	0.0	182	1353.6	537.0	0.0	183	1477.0	308.0	0.0
184	1477.0	417.5	0.0	185	1777.5	308.0	0.0	186	1627.2	308.0	0.0
187	1777.5	417.5	0.0	188	1627.2	417.5	0.0	189	1777.5	537.0	0.0
190	1627.2	537.0	0.0	191	1822.5	308.0	0.0	192	1822.5	417.5	0.0
193	1822.5	537.0	0.0	194	-42.5	660.0	0.0	195	0.0	660.0	0.0
196	-42.5	783.0	0.0	197	0.0	783.0	0.0	198	-42.5	926.0	0.0
199	0.0	926.0	0.0	200	123.4	660.0	0.0	201	123.4	783.0	0.0
202	123.4	926.0	0.0	203	123.4	1049.0	0.0	204	246.8	660.0	0.0
205	246.8	783.0	0.0	206	246.8	926.0	0.0	207	246.8	1049.0	0.0
208	370.1	660.0	0.0	209	370.1	783.0	0.0	210	370.1	926.0	0.0
211	370.1	1049.0	0.0	212	493.5	660.0	0.0	213	493.5	783.0	0.0
214	493.5	926.0	0.0	215	616.0	660.0	0.0	216	616.0	783.0	0.0
217	616.0	926.0	0.0	218	616.0	1049.0	0.0	219	738.5	660.0	0.0
220	738.5	783.0	0.0	221	738.5	926.0	0.0	222	738.5	1049.0	0.0
223	861.0	660.0	0.0	224	861.0	783.0	0.0	225	861.0	926.0	0.0
226	861.0	1049.0	0.0	227	983.5	660.0	0.0	228	983.5	783.0	0.0
229	983.5	926.0	0.0	230	1106.9	660.0	0.0	231	1106.9	783.0	0.0
232	1106.9	926.0	0.0	233	1106.9	1049.0	0.0	234	1230.2	660.0	0.0
235	1230.2	783.0	0.0	236	1230.2	926.0	0.0	237	1230.2	1049.0	0.0
238	1353.6	660.0	0.0	239	1353.6	783.0	0.0	240	1353.6	926.0	0.0
241	1353.6	1049.0	0.0	242	1477.0	660.0	0.0	243	1477.0	783.0	0.0
244	1477.0	926.0	0.0	245	1777.5	660.0	0.0	246	1627.2	660.0	0.0
247	1777.5	783.0	0.0	248	1627.2	783.0	0.0	249	1777.5	926.0	0.0
250	1627.2	926.0	0.0	251	1777.5	1049.0	0.0	252	1627.2	1049.0	0.0
253	1822.5	660.0	0.0	254	1822.5	783.0	0.0	255	1822.5	926.0	0.0
256	1822.5	1049.0	0.0	257	-42.5	1172.0	0.0	258	0.0	1172.0	0.0
259	123.4	1172.0	0.0	260	123.4	1305.0	0.0	261	246.8	1172.0	0.0
262	246.8	1305.0	0.0	263	370.1	1172.0	0.0	264	370.1	1305.0	0.0
265	493.5	1172.0	0.0	266	616.0	1172.0	0.0	267	616.0	1305.0	0.0
268	738.5	1172.0	0.0	269	738.5	1305.0	0.0	270	861.0	1172.0	0.0
271	861.0	1305.0	0.0	272	983.5	1172.0	0.0	273	1106.9	1172.0	0.0
274	1106.9	1305.0	0.0	275	1230.2	1172.0	0.0	276	1230.2	1305.0	0.0
277	1353.6	1172.0	0.0	278	1353.6	1305.0	0.0	279	1477.0	1172.0	0.0
280	1627.2	1172.0	0.0	281	1627.2	1305.0	0.0	282	1777.5	1172.0	0.0
283	1822.5	1172.0	0.0	284	1822.5	1305.0	0.0	285	123.4	1347.0	0.0
286	246.8	1347.0	0.0	287	370.1	1347.0	0.0	288	616.0	1347.0	0.0

Nodo	X	Y	Z	Nodo	X	Y	Z	Nodo	X	Y	Z
289	738.5	1347.0	0.0	290	861.0	1347.0	0.0	291	1106.9	1347.0	0.0
292	1230.2	1347.0	0.0	293	1353.6	1347.0	0.0	294	1627.2	1347.0	0.0
295	1822.5	1347.0	0.0	296	1998.2	1347.0	0.0	297	1998.2	1305.0	0.0
298	2174.0	1347.0	0.0	299	2174.0	1305.0	0.0	300	2349.8	1347.0	0.0
301	2349.8	1305.0	0.0	302	1477.0	1572.0	0.0	303	983.5	1572.0	0.0
304	493.5	1572.0	0.0	305	0.0	1572.0	0.0	306	-42.5	1572.0	0.0
307	-42.5	1459.5	0.0	308	0.0	1459.5	0.0	309	123.4	1459.5	0.0
310	123.4	1572.0	0.0	311	246.8	1459.5	0.0	312	246.8	1572.0	0.0
313	370.1	1459.5	0.0	314	370.1	1572.0	0.0	315	493.5	1459.5	0.0
316	616.0	1459.5	0.0	317	616.0	1572.0	0.0	318	738.5	1459.5	0.0
319	738.5	1572.0	0.0	320	861.0	1459.5	0.0	321	861.0	1572.0	0.0
322	983.5	1459.5	0.0	323	1106.9	1459.5	0.0	324	1106.9	1572.0	0.0
325	1230.2	1459.5	0.0	326	1230.2	1572.0	0.0	327	1353.6	1459.5	0.0
328	1353.6	1572.0	0.0	329	1477.0	1459.5	0.0	330	1627.2	1459.5	0.0
331	1627.2	1572.0	0.0	332	1777.5	1459.5	0.0	333	1822.5	1459.5	0.0
334	1822.5	1572.0	0.0	335	1998.2	1459.5	0.0	336	1998.2	1572.0	0.0
337	2174.0	1459.5	0.0	338	2174.0	1572.0	0.0	339	2349.8	1459.5	0.0
340	2349.8	1572.0	0.0	341	2525.5	1459.5	0.0	342	2555.5	1459.5	0.0
343	123.4	1598.5	0.0	344	246.8	1598.5	0.0	345	370.1	1598.5	0.0
346	616.0	1598.5	0.0	347	738.5	1598.5	0.0	348	861.0	1598.5	0.0
349	1106.9	1598.5	0.0	350	1230.2	1598.5	0.0	351	1353.6	1598.5	0.0
352	1822.5	1614.0	0.0	353	1998.2	1614.0	0.0	354	2174.0	1614.0	0.0
355	2349.8	1614.0	0.0	356	123.4	1641.0	0.0	357	246.8	1641.0	0.0
358	370.1	1641.0	0.0	359	616.0	1641.0	0.0	360	738.5	1641.0	0.0
361	861.0	1641.0	0.0	362	1106.9	1641.0	0.0	363	1230.2	1641.0	0.0
364	1353.6	1641.0	0.0	365	1627.2	1641.0	0.0	366	0.0	-62.5	80.0
367	123.4	-62.5	80.0	368	246.8	-62.5	80.0	369	370.1	-62.5	80.0
370	493.5	-62.5	80.0	371	616.0	-62.5	80.0	372	738.5	-62.5	80.0
373	861.0	-62.5	80.0	374	983.5	-62.5	80.0	375	1106.9	-62.5	80.0
376	1230.2	-62.5	80.0	377	1353.6	-62.5	80.0	378	1477.0	-62.5	80.0
379	1477.0	-48.5	80.0	380	1627.2	-48.5	80.0	381	1777.5	-48.5	80.0
382	1777.5	0.0	80.0	383	1777.5	99.2	80.0	384	1777.5	198.5	80.0
385	1777.5	308.0	80.0	386	1777.5	417.5	80.0	387	1777.5	537.0	80.0
388	1777.5	660.0	80.0	389	1777.5	783.0	80.0	390	1777.5	926.0	80.0
391	1777.5	1049.0	80.0	392	1777.5	1172.0	80.0	393	1777.5	1305.0	80.0
394	1777.5	1347.0	80.0	395	1777.5	1459.5	80.0	396	1777.5	1572.0	80.0
397	1777.5	1598.5	80.0	398	1627.2	1598.5	80.0	399	1477.0	1598.5	80.0
400	1353.6	1598.5	80.0	401	1230.2	1598.5	80.0	402	1106.9	1598.5	80.0
403	983.5	1598.5	80.0	404	861.0	1598.5	80.0	405	738.5	1598.5	80.0
406	616.0	1598.5	80.0	407	493.5	1598.5	80.0	408	370.1	1598.5	80.0
409	246.8	1598.5	80.0	410	123.4	1598.5	80.0	411	0.0	1598.5	80.0
412	0.0	1572.0	80.0	413	0.0	1459.5	80.0	414	0.0	1347.0	80.0
415	0.0	1305.0	80.0	416	0.0	1172.0	80.0	417	0.0	1049.0	80.0
418	0.0	926.0	80.0	419	0.0	783.0	80.0	420	0.0	660.0	80.0
421	0.0	537.0	80.0	422	0.0	417.5	80.0	423	0.0	308.0	80.0
424	0.0	198.5	80.0	425	0.0	99.2	80.0	426	0.0	0.0	80.0
427	0.0	-48.5	80.0	428	1627.2	198.5	80.0	429	1477.0	198.5	80.0
430	1477.0	0.0	80.0	431	1477.0	99.2	80.0	432	1477.0	308.0	80.0
433	1477.0	417.5	80.0	434	1477.0	537.0	80.0	435	1477.0	660.0	80.0
436	1477.0	783.0	80.0	437	1477.0	926.0	80.0	438	1477.0	1049.0	80.0
439	1477.0	1172.0	80.0	440	1477.0	1305.0	80.0	441	1477.0	1347.0	80.0
442	1477.0	1459.5	80.0	443	1477.0	1572.0	80.0	444	1230.2	-131.2	80.0
445	1230.2	-214.0	80.0	446	1353.6	-131.2	80.0	447	1353.6	-214.0	80.0
448	983.5	537.0	80.0	449	1477.0	-131.2	80.0	450	1477.0	-214.0	80.0
451	1477.0	198.5	182.2	452	493.5	537.0	80.0	453	1627.2	198.5	182.2
454	1477.0	198.5	284.5	455	1627.2	198.5	284.5	456	1477.0	198.5	386.8
457	1627.2	198.5	386.8	458	1627.2	198.5	489.0	459	1777.5	198.5	182.2
460	983.5	1049.0	80.0	461	1777.5	198.5	284.5	462	1777.5	198.5	386.8
463	1477.0	1598.5	182.2	464	493.5	1049.0	80.0	465	1627.2	1598.5	182.2
466	1477.0	1598.5	284.5	467	1627.2	1598.5	284.5	468	493.5	-48.5	80.0
469	1477.0	1598.5	386.8	470	1627.2	1598.5	386.8	471	1627.2	1598.5	489.0
472	1777.5	1598.5	182.2	473	1777.5	1598.5	284.5	474	1777.5	1598.5	386.8
475	1477.0	1598.5	606.0	476	1627.2	1598.5	606.0	477	1777.5	1598.5	606.0
478	1477.0	198.5	606.0	479	1627.2	198.5	606.0	480	1777.5	198.5	606.0
481	983.5	-48.5	80.0	482	983.5	0.0	80.0	483	1777.5	-48.5	606.0
484	0.0	-214.0	606.0	485	1477.0	-214.0	606.0	486	493.5	-214.0	606.0
487	983.5	-214.0	606.0	488	370.1	-214.0	606.0	489	1477.0	-48.5	606.0
490	1477.0	537.0	606.0	491	1777.5	537.0	606.0	492	1777.5	1049.0	606.0

Nodo	X	Y	Z	Nodo	X	Y	Z	Nodo	X	Y	Z
493	983.5	1049.0	606.0	494	983.5	537.0	606.0	495	0.0	0.0	489.0
496	0.0	537.0	489.0	497	0.0	1049.0	489.0	498	0.0	1598.5	489.0
499	493.5	0.0	80.0	500	493.5	0.0	489.0	501	493.5	537.0	489.0
502	493.5	1049.0	489.0	503	493.5	1598.5	489.0	504	983.5	0.0	489.0
505	983.5	537.0	489.0	506	983.5	1049.0	489.0	507	983.5	1598.5	489.0
508	1477.0	0.0	489.0	509	1477.0	198.5	489.0	510	1477.0	537.0	489.0
511	1477.0	1049.0	489.0	512	1477.0	1598.5	489.0	513	1777.5	-48.5	489.0
514	1777.5	198.5	489.0	515	1777.5	1598.5	489.0	516	0.0	0.0	606.0
517	493.5	0.0	606.0	518	983.5	0.0	606.0	519	1477.0	0.0	606.0
520	1998.2	1572.0	65.2	521	1477.0	1049.0	606.0	522	2525.5	1347.0	30.0
523	2525.5	1572.0	30.0	524	2174.0	1572.0	53.5	525	2349.8	1572.0	41.7
526	1822.5	1347.0	77.0	527	1822.5	1572.0	77.0	528	1998.2	1347.0	65.2
529	2174.0	1347.0	53.5	530	2349.8	1347.0	41.7	531	0.0	-214.0	80.0
532	123.4	-131.2	80.0	533	0.0	-131.2	80.0	534	123.4	-214.0	80.0
535	246.8	-131.2	80.0	536	246.8	-214.0	80.0	537	370.1	-131.2	80.0
538	370.1	-214.0	80.0	539	493.5	-131.2	80.0	540	493.5	-214.0	80.0
541	616.0	-131.2	80.0	542	616.0	-214.0	80.0	543	738.5	-131.2	80.0
544	738.5	-214.0	80.0	545	861.0	-131.2	80.0	546	861.0	-214.0	80.0
547	983.5	-131.2	80.0	548	983.5	-214.0	80.0	549	1106.9	-131.2	80.0
550	1106.9	-214.0	80.0	551	1627.2	537.0	606.0	552	1627.2	1049.0	606.0
553	983.5	-48.5	606.0	554	1106.9	-48.5	606.0	555	1106.9	0.0	606.0
556	1230.2	-48.5	606.0	557	1230.2	0.0	606.0	558	1353.6	-48.5	606.0
559	1353.6	0.0	606.0	560	493.5	-48.5	606.0	561	616.0	-48.5	606.0
562	616.0	0.0	606.0	563	738.5	-48.5	606.0	564	738.5	0.0	606.0
565	861.0	-48.5	606.0	566	861.0	0.0	606.0	567	0.0	-48.5	606.0
568	123.4	-48.5	606.0	569	123.4	0.0	606.0	570	246.8	-48.5	606.0
571	246.8	0.0	606.0	572	370.1	-48.5	606.0	573	370.1	0.0	606.0
574	983.5	-99.0	606.0	575	1106.9	-99.0	606.0	576	983.5	-149.5	606.0
577	1106.9	-149.5	606.0	578	1106.9	-214.0	606.0	579	1230.2	-99.0	606.0
580	1230.2	-149.5	606.0	581	1230.2	-214.0	606.0	582	1353.6	-99.0	606.0
583	1353.6	-149.5	606.0	584	1353.6	-214.0	606.0	585	1477.0	-99.0	606.0
586	1477.0	-149.5	606.0	587	493.5	-99.0	606.0	588	616.0	-99.0	606.0
589	493.5	-149.5	606.0	590	616.0	-149.5	606.0	591	616.0	-214.0	606.0
592	738.5	-99.0	606.0	593	738.5	-149.5	606.0	594	738.5	-214.0	606.0
595	861.0	-99.0	606.0	596	861.0	-149.5	606.0	597	861.0	-214.0	606.0
598	0.0	-99.0	606.0	599	123.4	-99.0	606.0	600	0.0	-149.5	606.0
601	123.4	-149.5	606.0	602	123.4	-214.0	606.0	603	246.8	-99.0	606.0
604	246.8	-149.5	606.0	605	246.8	-214.0	606.0	606	370.1	-99.0	606.0
607	370.1	-149.5	606.0								



14_MOD_NUMERAZIONE_NODI

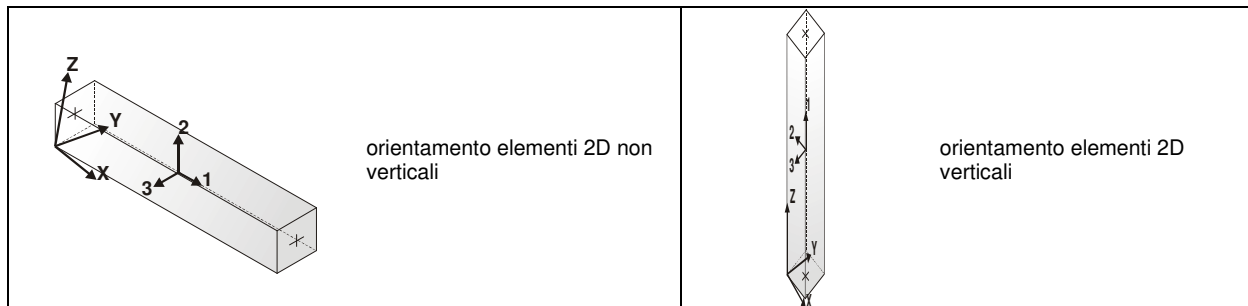
MODELLAZIONE STRUTTURA: ELEMENTI TRAVE

TABELLA DATI TRAVI

Il programma utilizza per la modellazione elementi a due nodi denominati in generale travi.

Ogni elemento trave è individuato dal nodo iniziale e dal nodo finale.

Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione.



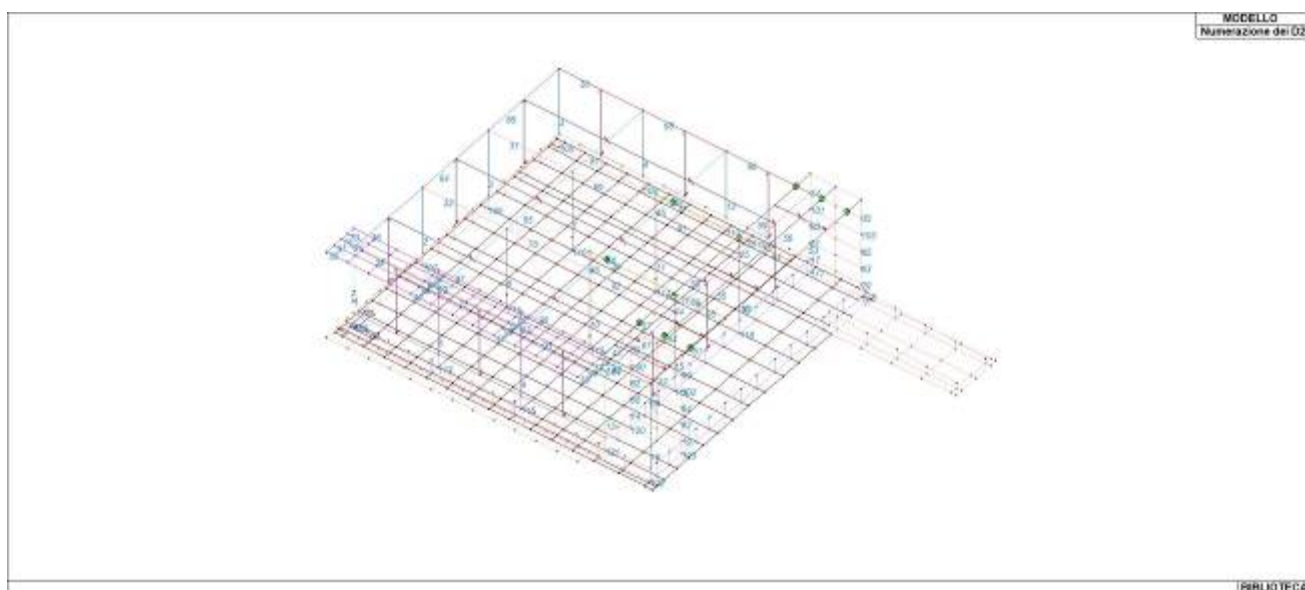
In particolare per ogni elemento viene indicato in tabella:

Elem.	numero dell'elemento
Note	codice di comportamento: trave, trave di fondazione, pilastro, asta, asta tesa, asta compressa,
Nodo I (J)	numero del nodo iniziale (finale)
Mat.	codice del materiale assegnato all'elemento
Sez.	codice della sezione assegnata all'elemento
Rotaz.	valore della rotazione dell'elemento, attorno al proprio asse, nel caso in cui l'orientamento di default non sia adottabile; l'orientamento di default prevede per gli elementi non verticali l'asse 2 contenuto nel piano verticale e l'asse 3 orizzontale, per gli elementi verticali l'asse 2 diretto secondo X negativo e l'asse 3 diretto secondo Y negativo
Svincolo I (J)	codici di svincolo per le azioni interne; i primi sei codici si riferiscono al nodo iniziale, i restanti sei al nodo finale (il valore 1 indica che la relativa azione interna non è attiva)
Wink V	costante di sottofondo (coefficiente di Winkler) per la modellazione della trave su suolo elastico
Wink O	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico orizzontale

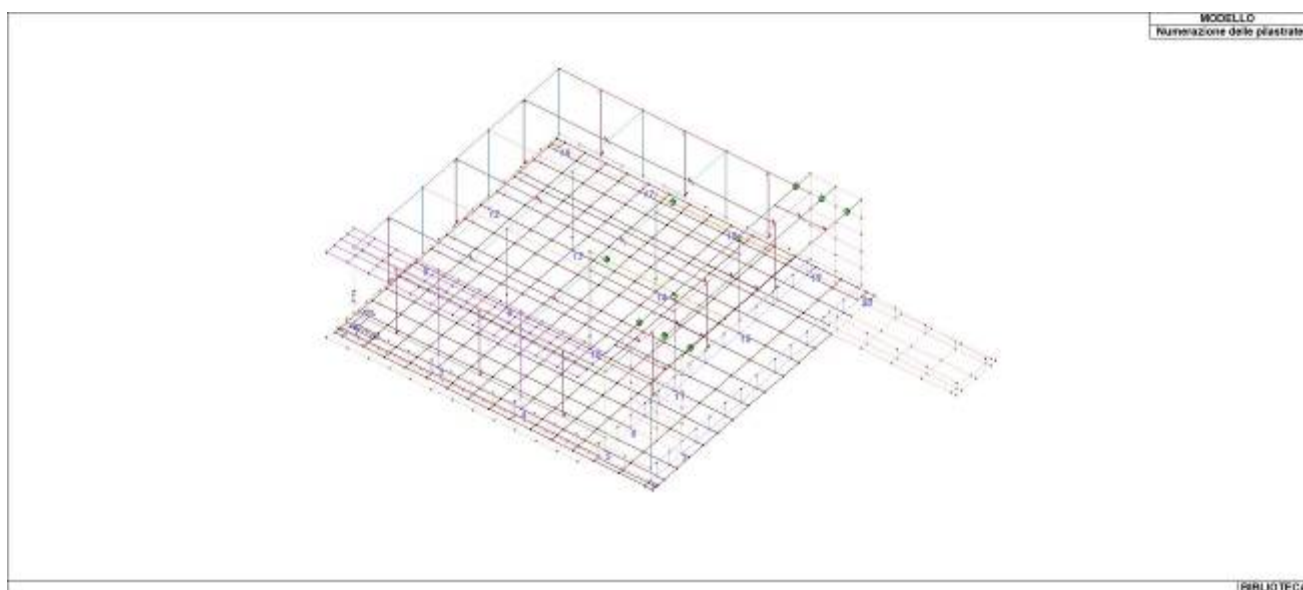
Elem.	Note	Nodo I	Nodo J	Mat.	Sez.	Crit.	Rotaz.	Svincolo I	Svincolo J	Wink V	Wink O
							gradi			daN/cm3	daN/cm3
1	Pilas.	426	495	3	4	3					
2	Pilas.	421	496	3	2	3					
3	Pilas.	417	497	3	2	3					
4	Pilas.	411	498	3	2	3					
5	Pilas.	499	500	3	15	3					
6	Pilas.	452	501	3	1	3					
7	Pilas.	464	502	3	1	3					
8	Pilas.	407	503	3	3	3					
9	Pilas.	482	504	3	15	3					
10	Pilas.	448	505	3	1	3					
11	Pilas.	460	506	3	1	3					
12	Pilas.	403	507	3	3	3					
13	Pilas.	430	508	3	4	3					
14	Pilas.	429	451	3	2	3					
15	Pilas.	434	510	3	1	3					
16	Pilas.	438	511	3	1	3					
17	Pilas.	399	463	3	3	3					
18	Pilas.	381	513	3	3	3					
19	Pilas.	384	459	3	3	3					
20	Pilas.	397	472	3	3	3					
21	Pilas.	495	516	3	4	3					
22	Pilas.	500	517	3	15	3					
23	Pilas.	504	518	3	15	3					
24	Pilas.	508	519	3	4	3					
25	Pilas.	511	521	3	1	3			000001		
26	Trave	495	496	3	6	8					

Elem.	Note	Nodo I	Nodo J	Mat.	Sez.	Crit.	Rotaz.	Svincolo I	Svincolo J	Wink V	Wink O
27	Trave	500	501	3	5	1					
28	Trave	504	505	3	5	1					
29	Trave	508	509	3	6	8					
30	Trave	498	503	3	9	8					
31	Trave	497	502	3	8	8					
32	Trave	496	501	3	8	8					
33	Trave	495	500	3	17	8					
34	Pilas.	512	475	3	3	3					
35	Pilas.	515	477	3	3	3					
36	Pilas.	513	483	3	3	3					
37	Trave	483	480	3	12	8					
38	Trave	485	586	3	14	8					
39	Trave	484	600	3	14	8					
40	Trave	486	589	1	13	8					
41	Trave	487	576	1	13	8					
42	Trave	489	483	1	9	8					
43	Trave	519	478	3	14	8					
44	Pilas.	510	490	3	1	3			000001		
45	Pilas.	506	493	3	1	3					
46	Pilas.	505	494	3	1	3					
47	Trave	493	521	12	10	1		000011			
48	Trave	494	490	12	10	1		000011			
49	Pilas.	514	480	3	3	3					
50	Pilas.	509	478	3	2	3					
51	Trave	480	491	12	11	3		000011			
52	Trave	491	492	12	11	3					
53	Trave	492	477	12	11	3			000011		
54	Trave	479	551	12	11	3		000011			
55	Trave	551	552	12	11	3					
56	Trave	552	476	12	11	3			000011		
57	Trave	478	490	12	11	3		000011			
58	Trave	490	521	12	11	3					
59	Trave	521	475	12	11	3			000011		
60	Pilas.	451	454	3	2	3					
61	Pilas.	463	466	3	3	3					
62	Pilas.	459	461	3	3	3					
63	Pilas.	472	473	3	3	3					
64	Trave	496	497	3	6	8					
65	Trave	501	502	3	5	1					
66	Trave	505	506	3	5	1					
67	Trave	509	510	3	7	8					
68	Trave	503	507	3	9	8					
69	Trave	502	506	3	8	8					
70	Trave	501	505	3	8	8					
71	Trave	500	504	3	17	8					
72	Trave	489	519	3	14	8					
73	Trave	567	516	3	14	8					
74	Trave	560	517	1	13	8					
75	Trave	553	518	1	13	8					
76	Trave	521	552	12	10	1					
77	Trave	490	551	12	10	1					
78	Trave	585	489	3	14	8					
79	Trave	598	567	3	14	8					
80	Trave	587	560	1	13	8					
81	Trave	574	553	1	13	8					
82	Pilas.	454	456	3	2	3					
83	Pilas.	466	469	3	3	3					
84	Pilas.	461	462	3	3	3					
85	Pilas.	473	474	3	3	3					
86	Trave	497	498	3	6	8					
87	Trave	502	503	3	5	1					
88	Trave	506	507	3	5	1					
89	Trave	510	511	3	7	8					
90	Trave	507	512	3	9	8					
91	Trave	506	511	3	16	1					
92	Trave	505	510	3	16	1					
93	Trave	504	508	3	17	8					
94	Trave	552	492	12	10	1					

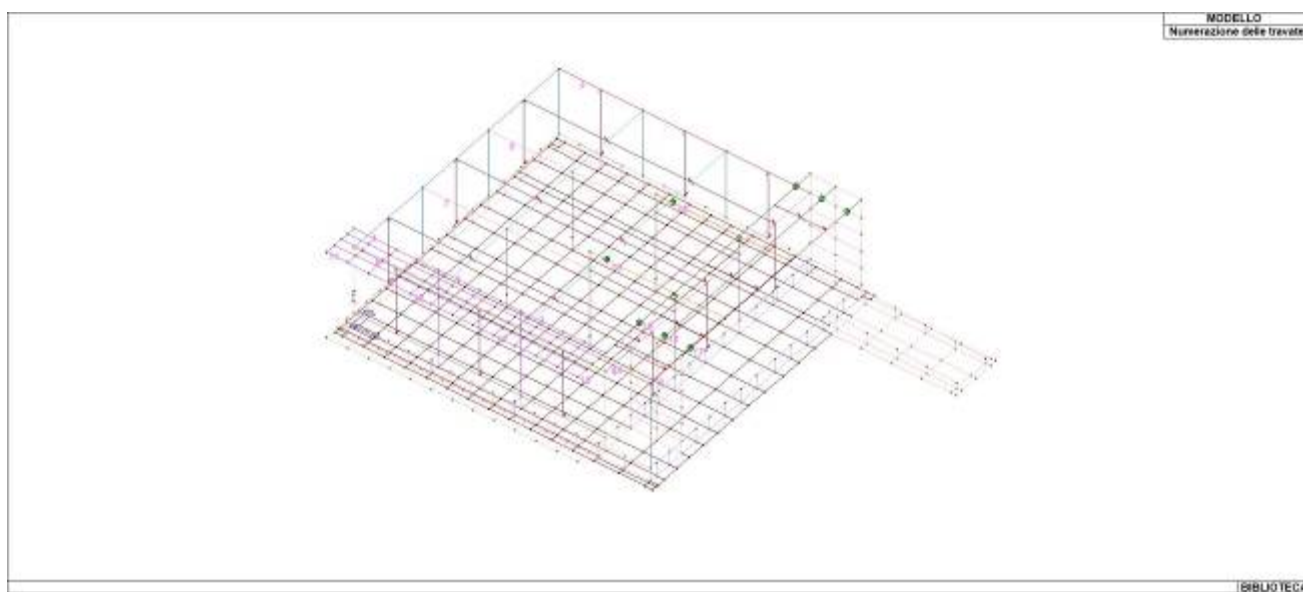
Elem.	Note	Nodo I	Nodo J	Mat.	Sez.	Crit.	Rotaz.	Svincolo I	Svincolo J	Wink V	Wink O
95	Trave	551	491	12	10	1					
96	Trave	586	585	3	14	8					
97	Trave	600	598	3	14	8					
98	Trave	589	587	1	13	8					
99	Trave	576	574	1	13	8					
100	Pilas.	456	509	3	2	3					
101	Pilas.	469	512	3	3	3					
102	Pilas.	462	514	3	3	3					
103	Pilas.	474	515	3	3	3					
104	Trave	511	512	3	7	8					
105	Pilas.	16	411	3	2	3					
106	Pilas.	12	417	3	2	3					
107	Pilas.	8	421	3	2	3					
108	Pilas.	1	426	3	4	3					
109	Pilas.	17	407	3	3	3					
110	Pilas.	13	464	3	1	3					
111	Pilas.	9	452	3	1	3					
112	Pilas.	2	499	3	15	3					
113	Pilas.	18	403	3	3	3					
114	Pilas.	14	460	3	1	3					
115	Pilas.	10	448	3	1	3					
116	Pilas.	3	482	3	15	3					
117	Pilas.	19	399	3	3	3					
118	Pilas.	15	438	3	1	3					
119	Pilas.	11	434	3	1	3					
120	Pilas.	7	429	3	2	3					
121	Pilas.	4	430	3	4	3					
122	Pilas.	5	381	3	3	3					
123	Pilas.	6	384	3	3	3					
124	Pilas.	20	397	3	3	3					



15_MOD_NUMERAZIONE_D2



15_MOD_NUMERAZIONE_D2_PILASTRATE



15_MOD_NUMERAZIONE_D2_TRAVATE

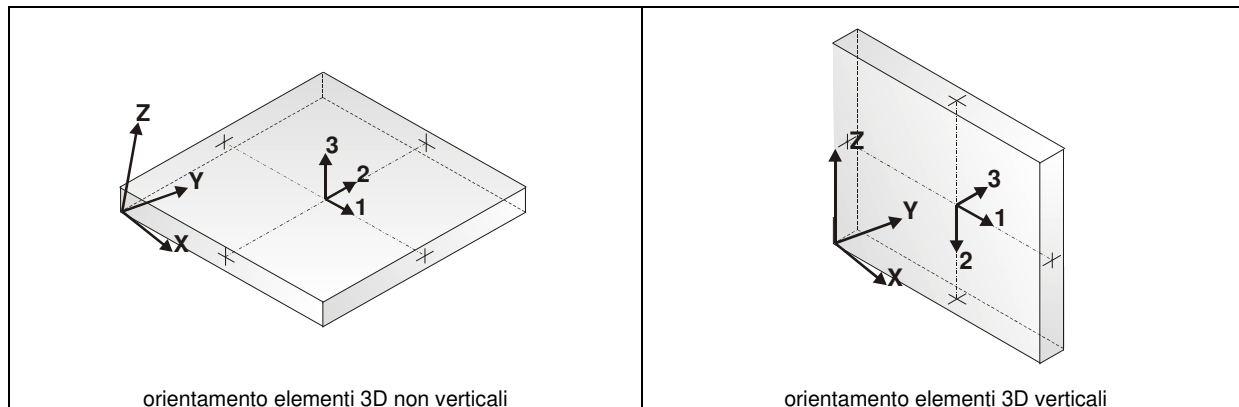
MODELLAZIONE STRUTTURA: ELEMENTI SHELL

LEGENDA TABELLA DATI SHELL

Il programma utilizza per la modellazione elementi a tre o quattro nodi denominati in generale shell.

Ogni elemento shell è individuato dai nodi I, J, K, L (L=I per gli elementi a tre nodi).

Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione.



In particolare per ogni elemento viene indicato in tabella:

Elem.	numero dell'elemento
Note	codice di comportamento: Guscio (elemento guscio in elevazione non verticale) Guscio fond. (elemento guscio su suolo elastico) Setto (elemento guscio in elevazione verticale) Membrana (elemento guscio con comportamento membranale)
Nodo I (J, K, L)	numero del nodo I (J, K, L)
Mat.	codice del materiale assegnato all'elemento
Spessore	spessore dell'elemento (costante)
Wink V	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico verticale
Wink O	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico orizzontale

Elem.	Note	Nodo I	Nodo J	Nodo K	Nodo L	Mat.	Crit.	Spessore	Svincolo	Wink V	Wink O
								cm		daN/cm3	daN/cm3
1	Guscio fond.	47	26	25	46	1	2	40.0		0.32	0.16
2	Guscio fond.	77	24	100	107	1	2	40.0		0.32	0.16
3	Guscio fond.	26	74	73	25	1	2	40.0		0.32	0.16
4	Guscio fond.	74	76	75	73	1	2	40.0		0.32	0.16
5	Guscio fond.	76	78	77	75	1	2	40.0		0.32	0.16
6	Guscio fond.	78	27	24	77	1	2	40.0		0.32	0.16
7	Guscio fond.	27	80	79	24	1	2	40.0		0.32	0.16
8	Guscio fond.	80	82	81	79	1	2	40.0		0.32	0.16
9	Guscio fond.	82	84	83	81	1	2	40.0		0.32	0.16
10	Guscio fond.	84	28	23	83	1	2	40.0		0.32	0.16
11	Guscio fond.	28	86	85	23	1	2	40.0		0.32	0.16
12	Guscio fond.	86	88	87	85	1	2	40.0		0.32	0.16
13	Guscio fond.	88	90	89	87	1	2	40.0		0.32	0.16
14	Guscio fond.	90	29	22	89	1	2	40.0		0.32	0.16
15	Guscio fond.	93	30	91	92	1	2	40.0		0.32	0.16
16	Guscio fond.	29	93	92	22	1	2	40.0		0.32	0.16
17	Guscio fond.	30	31	94	91	1	2	40.0		0.32	0.16
18	Guscio fond.	91	94	32	5	1	2	40.0		0.32	0.16
19	Guscio fond.	92	91	5	95	1	2	40.0		0.32	0.16
20	Guscio fond.	22	92	95	21	1	2	40.0		0.32	0.16
21	Guscio fond.	23	85	97	96	1	2	40.0		0.32	0.16
22	Guscio fond.	85	87	98	97	1	2	40.0		0.32	0.16
23	Guscio fond.	87	89	99	98	1	2	40.0		0.32	0.16
24	Guscio fond.	89	22	21	99	1	2	40.0		0.32	0.16

Elem.	Note	Nodo I	Nodo J	Nodo K	Nodo L	Mat.	Crit.	Spessore	Svincolo	Wink V	Wink O
25	Guscio fond.	24	79	101	100	1	2	40.0		0.32	0.16
26	Guscio fond.	79	81	102	101	1	2	40.0		0.32	0.16
27	Guscio fond.	81	83	103	102	1	2	40.0		0.32	0.16
28	Guscio fond.	83	23	96	103	1	2	40.0		0.32	0.16
29	Guscio fond.	25	73	105	104	1	2	40.0		0.32	0.16
30	Guscio fond.	73	75	106	105	1	2	40.0		0.32	0.16
31	Guscio fond.	75	77	107	106	1	2	40.0		0.32	0.16
32	Guscio fond.	46	25	104	108	1	2	40.0		0.32	0.16
33	Guscio fond.	108	104	1	45	1	2	40.0		0.32	0.16
34	Guscio fond.	104	105	109	1	1	2	40.0		0.32	0.16
35	Guscio fond.	105	106	110	109	1	2	40.0		0.32	0.16
36	Guscio fond.	106	107	111	110	1	2	40.0		0.32	0.16
37	Guscio fond.	107	100	2	111	1	2	40.0		0.32	0.16
38	Guscio fond.	100	101	112	2	1	2	40.0		0.32	0.16
39	Guscio fond.	101	102	113	112	1	2	40.0		0.32	0.16
40	Guscio fond.	102	103	114	113	1	2	40.0		0.32	0.16
41	Guscio fond.	103	96	3	114	1	2	40.0		0.32	0.16
42	Guscio fond.	96	97	115	3	1	2	40.0		0.32	0.16
43	Guscio fond.	97	98	116	115	1	2	40.0		0.32	0.16
44	Guscio fond.	98	99	117	116	1	2	40.0		0.32	0.16
45	Guscio fond.	99	21	4	117	1	2	40.0		0.32	0.16
46	Guscio fond.	95	5	118	119	1	2	40.0		0.32	0.16
47	Guscio fond.	21	95	119	4	1	2	40.0		0.32	0.16
48	Guscio fond.	5	32	120	118	1	2	40.0		0.32	0.16
49	Guscio fond.	45	1	121	122	1	2	40.0		0.32	0.16
50	Guscio fond.	122	121	48	51	1	2	40.0		0.32	0.16
51	Guscio fond.	1	109	123	121	1	2	40.0		0.32	0.16
52	Guscio fond.	121	123	124	48	1	2	40.0		0.32	0.16
53	Guscio fond.	109	110	125	123	1	2	40.0		0.32	0.16
54	Guscio fond.	123	125	126	124	1	2	40.0		0.32	0.16
55	Guscio fond.	110	111	127	125	1	2	40.0		0.32	0.16
56	Guscio fond.	125	127	128	126	1	2	40.0		0.32	0.16
57	Guscio fond.	111	2	129	127	1	2	40.0		0.32	0.16
58	Guscio fond.	127	129	49	128	1	2	40.0		0.32	0.16
59	Guscio fond.	2	112	130	129	1	2	40.0		0.32	0.16
60	Guscio fond.	129	130	131	49	1	2	40.0		0.32	0.16
61	Guscio fond.	112	113	132	130	1	2	40.0		0.32	0.16
62	Guscio fond.	130	132	133	131	1	2	40.0		0.32	0.16
63	Guscio fond.	113	114	134	132	1	2	40.0		0.32	0.16
64	Guscio fond.	132	134	135	133	1	2	40.0		0.32	0.16
65	Guscio fond.	114	3	136	134	1	2	40.0		0.32	0.16
66	Guscio fond.	134	136	50	135	1	2	40.0		0.32	0.16
67	Guscio fond.	3	115	137	136	1	2	40.0		0.32	0.16
68	Guscio fond.	136	137	138	50	1	2	40.0		0.32	0.16
69	Guscio fond.	115	116	139	137	1	2	40.0		0.32	0.16
70	Guscio fond.	137	139	140	138	1	2	40.0		0.32	0.16
71	Guscio fond.	116	117	141	139	1	2	40.0		0.32	0.16
72	Guscio fond.	139	141	142	140	1	2	40.0		0.32	0.16
73	Guscio fond.	117	4	143	141	1	2	40.0		0.32	0.16
74	Guscio fond.	141	143	7	142	1	2	40.0		0.32	0.16
75	Guscio fond.	4	119	144	143	1	2	40.0		0.32	0.16
76	Guscio fond.	143	144	145	7	1	2	40.0		0.32	0.16
77	Guscio fond.	119	118	146	144	1	2	40.0		0.32	0.16
78	Guscio fond.	144	146	6	145	1	2	40.0		0.32	0.16
79	Guscio fond.	118	120	147	146	1	2	40.0		0.32	0.16
80	Guscio fond.	146	147	33	6	1	2	40.0		0.32	0.16
81	Guscio fond.	51	48	149	148	1	2	40.0		0.32	0.16
82	Guscio fond.	148	149	151	150	1	2	40.0		0.32	0.16
83	Guscio fond.	150	151	8	44	1	2	40.0		0.32	0.16
84	Guscio fond.	48	124	152	149	1	2	40.0		0.32	0.16
85	Guscio fond.	149	152	153	151	1	2	40.0		0.32	0.16
86	Guscio fond.	151	153	154	8	1	2	40.0		0.32	0.16
87	Guscio fond.	124	126	155	152	1	2	40.0		0.32	0.16
88	Guscio fond.	152	155	156	153	1	2	40.0		0.32	0.16
89	Guscio fond.	153	156	157	154	1	2	40.0		0.32	0.16
90	Guscio fond.	126	128	158	155	1	2	40.0		0.32	0.16
91	Guscio fond.	155	158	159	156	1	2	40.0		0.32	0.16
92	Guscio fond.	156	159	160	157	1	2	40.0		0.32	0.16

Elem.	Note	Nodo I	Nodo J	Nodo K	Nodo L	Mat.	Crit.	Spessore	Svincolo	Wink V	Wink O
93	Guscio fond.	128	49	161	158	1	2	40.0		0.32	0.16
94	Guscio fond.	158	161	162	159	1	2	40.0		0.32	0.16
95	Guscio fond.	159	162	9	160	1	2	40.0		0.32	0.16
96	Guscio fond.	49	131	163	161	1	2	40.0		0.32	0.16
97	Guscio fond.	161	163	164	162	1	2	40.0		0.32	0.16
98	Guscio fond.	162	164	165	9	1	2	40.0		0.32	0.16
99	Guscio fond.	131	133	166	163	1	2	40.0		0.32	0.16
100	Guscio fond.	163	166	167	164	1	2	40.0		0.32	0.16
101	Guscio fond.	164	167	168	165	1	2	40.0		0.32	0.16
102	Guscio fond.	133	135	169	166	1	2	40.0		0.32	0.16
103	Guscio fond.	166	169	170	167	1	2	40.0		0.32	0.16
104	Guscio fond.	167	170	171	168	1	2	40.0		0.32	0.16
105	Guscio fond.	135	50	172	169	1	2	40.0		0.32	0.16
106	Guscio fond.	169	172	173	170	1	2	40.0		0.32	0.16
107	Guscio fond.	170	173	10	171	1	2	40.0		0.32	0.16
108	Guscio fond.	50	138	174	172	1	2	40.0		0.32	0.16
109	Guscio fond.	172	174	175	173	1	2	40.0		0.32	0.16
110	Guscio fond.	173	175	176	10	1	2	40.0		0.32	0.16
111	Guscio fond.	138	140	177	174	1	2	40.0		0.32	0.16
112	Guscio fond.	174	177	178	175	1	2	40.0		0.32	0.16
113	Guscio fond.	175	178	179	176	1	2	40.0		0.32	0.16
114	Guscio fond.	140	142	180	177	1	2	40.0		0.32	0.16
115	Guscio fond.	177	180	181	178	1	2	40.0		0.32	0.16
116	Guscio fond.	178	181	182	179	1	2	40.0		0.32	0.16
117	Guscio fond.	142	7	183	180	1	2	40.0		0.32	0.16
118	Guscio fond.	180	183	184	181	1	2	40.0		0.32	0.16
119	Guscio fond.	181	184	11	182	1	2	40.0		0.32	0.16
120	Guscio fond.	145	6	185	186	1	2	40.0		0.32	0.16
121	Guscio fond.	186	185	187	188	1	2	40.0		0.32	0.16
122	Guscio fond.	188	187	189	190	1	2	40.0		0.32	0.16
123	Guscio fond.	7	145	186	183	1	2	40.0		0.32	0.16
124	Guscio fond.	183	186	188	184	1	2	40.0		0.32	0.16
125	Guscio fond.	184	188	190	11	1	2	40.0		0.32	0.16
126	Guscio fond.	6	33	191	185	1	2	40.0		0.32	0.16
127	Guscio fond.	185	191	192	187	1	2	40.0		0.32	0.16
128	Guscio fond.	187	192	193	189	1	2	40.0		0.32	0.16
129	Guscio fond.	44	8	195	194	1	2	40.0		0.32	0.16
130	Guscio fond.	194	195	197	196	1	2	40.0		0.32	0.16
131	Guscio fond.	196	197	199	198	1	2	40.0		0.32	0.16
132	Guscio fond.	198	199	12	43	1	2	40.0		0.32	0.16
133	Guscio fond.	8	154	200	195	1	2	40.0		0.32	0.16
134	Guscio fond.	195	200	201	197	1	2	40.0		0.32	0.16
135	Guscio fond.	197	201	202	199	1	2	40.0		0.32	0.16
136	Guscio fond.	199	202	203	12	1	2	40.0		0.32	0.16
137	Guscio fond.	154	157	204	200	1	2	40.0		0.32	0.16
138	Guscio fond.	200	204	205	201	1	2	40.0		0.32	0.16
139	Guscio fond.	201	205	206	202	1	2	40.0		0.32	0.16
140	Guscio fond.	202	206	207	203	1	2	40.0		0.32	0.16
141	Guscio fond.	157	160	208	204	1	2	40.0		0.32	0.16
142	Guscio fond.	204	208	209	205	1	2	40.0		0.32	0.16
143	Guscio fond.	205	209	210	206	1	2	40.0		0.32	0.16
144	Guscio fond.	206	210	211	207	1	2	40.0		0.32	0.16
145	Guscio fond.	160	9	212	208	1	2	40.0		0.32	0.16
146	Guscio fond.	208	212	213	209	1	2	40.0		0.32	0.16
147	Guscio fond.	209	213	214	210	1	2	40.0		0.32	0.16
148	Guscio fond.	210	214	13	211	1	2	40.0		0.32	0.16
149	Guscio fond.	9	165	215	212	1	2	40.0		0.32	0.16
150	Guscio fond.	212	215	216	213	1	2	40.0		0.32	0.16
151	Guscio fond.	213	216	217	214	1	2	40.0		0.32	0.16
152	Guscio fond.	214	217	218	13	1	2	40.0		0.32	0.16
153	Guscio fond.	165	168	219	215	1	2	40.0		0.32	0.16
154	Guscio fond.	215	219	220	216	1	2	40.0		0.32	0.16
155	Guscio fond.	216	220	221	217	1	2	40.0		0.32	0.16
156	Guscio fond.	217	221	222	218	1	2	40.0		0.32	0.16
157	Guscio fond.	168	171	223	219	1	2	40.0		0.32	0.16
158	Guscio fond.	219	223	224	220	1	2	40.0		0.32	0.16
159	Guscio fond.	220	224	225	221	1	2	40.0		0.32	0.16
160	Guscio fond.	221	225	226	222	1	2	40.0		0.32	0.16

Elem.	Note	Nodo I	Nodo J	Nodo K	Nodo L	Mat.	Crit.	Spessore	Svincolo	Wink V	Wink O
161	Guscio fond.	171	10	227	223	1	2	40.0		0.32	0.16
162	Guscio fond.	223	227	228	224	1	2	40.0		0.32	0.16
163	Guscio fond.	224	228	229	225	1	2	40.0		0.32	0.16
164	Guscio fond.	225	229	14	226	1	2	40.0		0.32	0.16
165	Guscio fond.	10	176	230	227	1	2	40.0		0.32	0.16
166	Guscio fond.	227	230	231	228	1	2	40.0		0.32	0.16
167	Guscio fond.	228	231	232	229	1	2	40.0		0.32	0.16
168	Guscio fond.	229	232	233	14	1	2	40.0		0.32	0.16
169	Guscio fond.	176	179	234	230	1	2	40.0		0.32	0.16
170	Guscio fond.	230	234	235	231	1	2	40.0		0.32	0.16
171	Guscio fond.	231	235	236	232	1	2	40.0		0.32	0.16
172	Guscio fond.	232	236	237	233	1	2	40.0		0.32	0.16
173	Guscio fond.	179	182	238	234	1	2	40.0		0.32	0.16
174	Guscio fond.	234	238	239	235	1	2	40.0		0.32	0.16
175	Guscio fond.	235	239	240	236	1	2	40.0		0.32	0.16
176	Guscio fond.	236	240	241	237	1	2	40.0		0.32	0.16
177	Guscio fond.	182	11	242	238	1	2	40.0		0.32	0.16
178	Guscio fond.	238	242	243	239	1	2	40.0		0.32	0.16
179	Guscio fond.	239	243	244	240	1	2	40.0		0.32	0.16
180	Guscio fond.	240	244	15	241	1	2	40.0		0.32	0.16
181	Guscio fond.	190	189	245	246	1	2	40.0		0.32	0.16
182	Guscio fond.	246	245	247	248	1	2	40.0		0.32	0.16
183	Guscio fond.	248	247	249	250	1	2	40.0		0.32	0.16
184	Guscio fond.	250	249	251	252	1	2	40.0		0.32	0.16
185	Guscio fond.	11	190	246	242	1	2	40.0		0.32	0.16
186	Guscio fond.	242	246	248	243	1	2	40.0		0.32	0.16
187	Guscio fond.	243	248	250	244	1	2	40.0		0.32	0.16
188	Guscio fond.	244	250	252	15	1	2	40.0		0.32	0.16
189	Guscio fond.	189	193	253	245	1	2	40.0		0.32	0.16
190	Guscio fond.	245	253	254	247	1	2	40.0		0.32	0.16
191	Guscio fond.	247	254	255	249	1	2	40.0		0.32	0.16
192	Guscio fond.	249	255	256	251	1	2	40.0		0.32	0.16
193	Guscio fond.	43	12	258	257	1	2	40.0		0.32	0.16
194	Guscio fond.	257	258	70	72	1	2	40.0		0.32	0.16
195	Guscio fond.	12	203	259	258	1	2	40.0		0.32	0.16
196	Guscio fond.	258	259	260	70	1	2	40.0		0.32	0.16
197	Guscio fond.	203	207	261	259	1	2	40.0		0.32	0.16
198	Guscio fond.	259	261	262	260	1	2	40.0		0.32	0.16
199	Guscio fond.	207	211	263	261	1	2	40.0		0.32	0.16
200	Guscio fond.	261	263	264	262	1	2	40.0		0.32	0.16
201	Guscio fond.	211	13	265	263	1	2	40.0		0.32	0.16
202	Guscio fond.	263	265	68	264	1	2	40.0		0.32	0.16
203	Guscio fond.	13	218	266	265	1	2	40.0		0.32	0.16
204	Guscio fond.	265	266	267	68	1	2	40.0		0.32	0.16
205	Guscio fond.	218	222	268	266	1	2	40.0		0.32	0.16
206	Guscio fond.	266	268	269	267	1	2	40.0		0.32	0.16
207	Guscio fond.	222	226	270	268	1	2	40.0		0.32	0.16
208	Guscio fond.	268	270	271	269	1	2	40.0		0.32	0.16
209	Guscio fond.	226	14	272	270	1	2	40.0		0.32	0.16
210	Guscio fond.	270	272	66	271	1	2	40.0		0.32	0.16
211	Guscio fond.	14	233	273	272	1	2	40.0		0.32	0.16
212	Guscio fond.	272	273	274	66	1	2	40.0		0.32	0.16
213	Guscio fond.	233	237	275	273	1	2	40.0		0.32	0.16
214	Guscio fond.	273	275	276	274	1	2	40.0		0.32	0.16
215	Guscio fond.	237	241	277	275	1	2	40.0		0.32	0.16
216	Guscio fond.	275	277	278	276	1	2	40.0		0.32	0.16
217	Guscio fond.	241	15	279	277	1	2	40.0		0.32	0.16
218	Guscio fond.	277	279	64	278	1	2	40.0		0.32	0.16
219	Guscio fond.	15	252	280	279	1	2	40.0		0.32	0.16
220	Guscio fond.	279	280	281	64	1	2	40.0		0.32	0.16
221	Guscio fond.	252	251	282	280	1	2	40.0		0.32	0.16
222	Guscio fond.	280	282	58	281	1	2	40.0		0.32	0.16
223	Guscio fond.	251	256	283	282	1	2	40.0		0.32	0.16
224	Guscio fond.	282	283	284	58	1	2	40.0		0.32	0.16
225	Guscio fond.	72	70	69	71	1	2	40.0		0.32	0.16
226	Guscio fond.	70	260	285	69	1	2	40.0		0.32	0.16
227	Guscio fond.	260	262	286	285	1	2	40.0		0.32	0.16
228	Guscio fond.	262	264	287	286	1	2	40.0		0.32	0.16

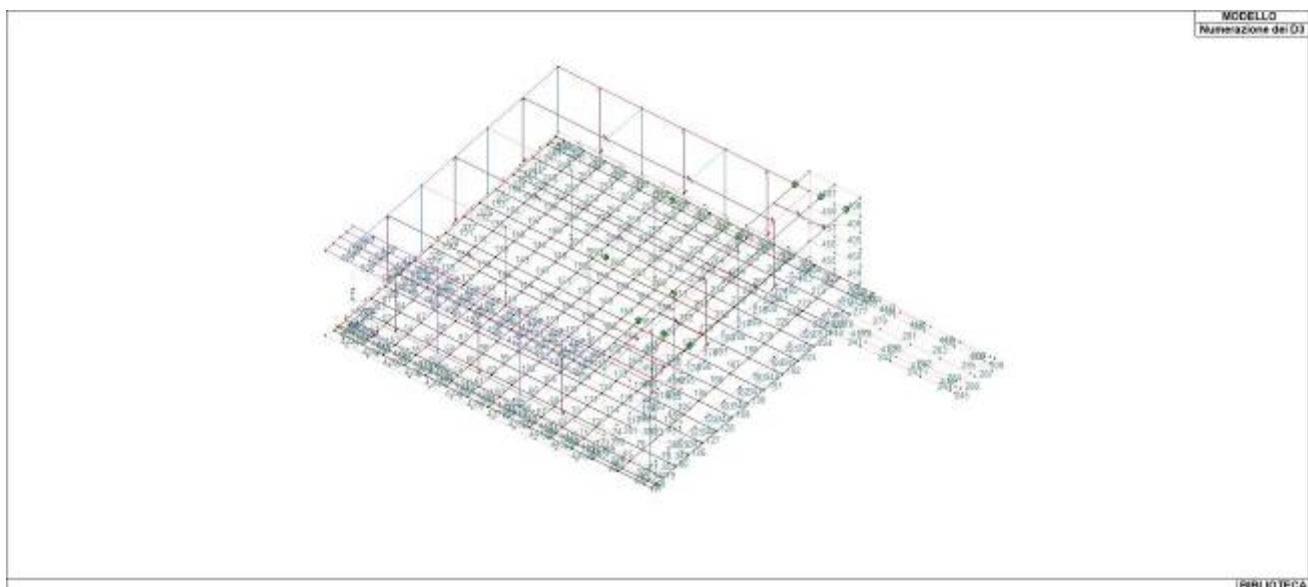
Elem.	Note	Nodo I	Nodo J	Nodo K	Nodo L	Mat.	Crit.	Spessore	Svincolo	Wink V	Wink O
229	Guscio fond.	264	68	67	287	1	2	40.0		0.32	0.16
230	Guscio fond.	68	267	288	67	1	2	40.0		0.32	0.16
231	Guscio fond.	267	269	289	288	1	2	40.0		0.32	0.16
232	Guscio fond.	269	271	290	289	1	2	40.0		0.32	0.16
233	Guscio fond.	271	66	65	290	1	2	40.0		0.32	0.16
234	Guscio fond.	66	274	291	65	1	2	40.0		0.32	0.16
235	Guscio fond.	274	276	292	291	1	2	40.0		0.32	0.16
236	Guscio fond.	276	278	293	292	1	2	40.0		0.32	0.16
237	Guscio fond.	278	64	63	293	1	2	40.0		0.32	0.16
238	Guscio fond.	64	281	294	63	1	2	40.0		0.32	0.16
239	Guscio fond.	281	58	52	294	1	2	40.0		0.32	0.16
240	Guscio fond.	58	284	295	52	1	2	40.0		0.32	0.16
241	Guscio fond.	284	297	296	295	1	2	25.0		0.53	0.26
242	Guscio fond.	297	299	298	296	1	2	25.0		0.53	0.26
243	Guscio fond.	299	301	300	298	1	2	25.0		0.53	0.26
244	Guscio fond.	301	57	55	300	1	2	25.0		0.53	0.26
245	Guscio fond.	57	62	61	55	1	2	25.0		0.53	0.26
246	Guscio fond.	71	69	308	307	1	2	40.0		0.32	0.16
247	Guscio fond.	307	308	305	306	1	2	40.0		0.32	0.16
248	Guscio fond.	69	285	309	308	1	2	40.0		0.32	0.16
249	Guscio fond.	308	309	310	305	1	2	40.0		0.32	0.16
250	Guscio fond.	285	286	311	309	1	2	40.0		0.32	0.16
251	Guscio fond.	309	311	312	310	1	2	40.0		0.32	0.16
252	Guscio fond.	286	287	313	311	1	2	40.0		0.32	0.16
253	Guscio fond.	311	313	314	312	1	2	40.0		0.32	0.16
254	Guscio fond.	287	67	315	313	1	2	40.0		0.32	0.16
255	Guscio fond.	313	315	304	314	1	2	40.0		0.32	0.16
256	Guscio fond.	67	288	316	315	1	2	40.0		0.32	0.16
257	Guscio fond.	315	316	317	304	1	2	40.0		0.32	0.16
258	Guscio fond.	288	289	318	316	1	2	40.0		0.32	0.16
259	Guscio fond.	316	318	319	317	1	2	40.0		0.32	0.16
260	Guscio fond.	289	290	320	318	1	2	40.0		0.32	0.16
261	Guscio fond.	318	320	321	319	1	2	40.0		0.32	0.16
262	Guscio fond.	290	65	322	320	1	2	40.0		0.32	0.16
263	Guscio fond.	320	322	303	321	1	2	40.0		0.32	0.16
264	Guscio fond.	65	291	323	322	1	2	40.0		0.32	0.16
265	Guscio fond.	322	323	324	303	1	2	40.0		0.32	0.16
266	Guscio fond.	291	292	325	323	1	2	40.0		0.32	0.16
267	Guscio fond.	323	325	326	324	1	2	40.0		0.32	0.16
268	Guscio fond.	292	293	327	325	1	2	40.0		0.32	0.16
269	Guscio fond.	325	327	328	326	1	2	40.0		0.32	0.16
270	Guscio fond.	293	63	329	327	1	2	40.0		0.32	0.16
271	Guscio fond.	327	329	302	328	1	2	40.0		0.32	0.16
272	Guscio fond.	63	294	330	329	1	2	40.0		0.32	0.16
273	Guscio fond.	329	330	331	302	1	2	40.0		0.32	0.16
274	Guscio fond.	294	52	332	330	1	2	40.0		0.32	0.16
275	Guscio fond.	330	332	53	331	1	2	40.0		0.32	0.16
276	Guscio fond.	52	295	333	332	1	2	40.0		0.32	0.16
277	Guscio fond.	332	333	334	53	1	2	40.0		0.32	0.16
278	Guscio fond.	295	296	335	333	1	2	25.0		0.53	0.26
279	Guscio fond.	333	335	336	334	1	2	25.0		0.53	0.26
280	Guscio fond.	296	298	337	335	1	2	25.0		0.53	0.26
281	Guscio fond.	335	337	338	336	1	2	25.0		0.53	0.26
282	Guscio fond.	298	300	339	337	1	2	25.0		0.53	0.26
283	Guscio fond.	337	339	340	338	1	2	25.0		0.53	0.26
284	Guscio fond.	300	55	341	339	1	2	25.0		0.53	0.26
285	Guscio fond.	339	341	54	340	1	2	25.0		0.53	0.26
286	Guscio fond.	55	61	342	341	1	2	25.0		0.53	0.26
287	Guscio fond.	341	342	60	54	1	2	25.0		0.53	0.26
288	Guscio fond.	306	305	16	42	1	2	40.0		0.32	0.16
289	Guscio fond.	305	310	343	16	1	2	40.0		0.32	0.16
290	Guscio fond.	310	312	344	343	1	2	40.0		0.32	0.16
291	Guscio fond.	312	314	345	344	1	2	40.0		0.32	0.16
292	Guscio fond.	314	304	17	345	1	2	40.0		0.32	0.16
293	Guscio fond.	304	317	346	17	1	2	40.0		0.32	0.16
294	Guscio fond.	317	319	347	346	1	2	40.0		0.32	0.16
295	Guscio fond.	319	321	348	347	1	2	40.0		0.32	0.16
296	Guscio fond.	321	303	18	348	1	2	40.0		0.32	0.16

Elem.	Note	Nodo I	Nodo J	Nodo K	Nodo L	Mat.	Crit.	Spessore	Svincolo	Wink V	Wink O
297	Guscio fond.	303	324	349	18	1	2	40.0		0.32	0.16
298	Guscio fond.	324	326	350	349	1	2	40.0		0.32	0.16
299	Guscio fond.	326	328	351	350	1	2	40.0		0.32	0.16
300	Guscio fond.	328	302	19	351	1	2	40.0		0.32	0.16
301	Guscio fond.	302	331	34	19	1	2	40.0		0.32	0.16
302	Guscio fond.	331	53	20	34	1	2	40.0		0.32	0.16
303	Guscio fond.	53	334	352	20	1	2	40.0		0.32	0.16
304	Guscio fond.	334	336	353	352	1	2	25.0		0.53	0.26
305	Guscio fond.	336	338	354	353	1	2	25.0		0.53	0.26
306	Guscio fond.	338	340	355	354	1	2	25.0		0.53	0.26
307	Guscio fond.	340	54	56	355	1	2	25.0		0.53	0.26
308	Guscio fond.	54	60	59	56	1	2	25.0		0.53	0.26
309	Guscio fond.	42	16	40	41	1	2	40.0		0.32	0.16
310	Guscio fond.	16	343	356	40	1	2	40.0		0.32	0.16
311	Guscio fond.	343	344	357	356	1	2	40.0		0.32	0.16
312	Guscio fond.	344	345	358	357	1	2	40.0		0.32	0.16
313	Guscio fond.	345	17	39	358	1	2	40.0		0.32	0.16
314	Guscio fond.	17	346	359	39	1	2	40.0		0.32	0.16
315	Guscio fond.	346	347	360	359	1	2	40.0		0.32	0.16
316	Guscio fond.	347	348	361	360	1	2	40.0		0.32	0.16
317	Guscio fond.	348	18	38	361	1	2	40.0		0.32	0.16
318	Guscio fond.	18	349	362	38	1	2	40.0		0.32	0.16
319	Guscio fond.	349	350	363	362	1	2	40.0		0.32	0.16
320	Guscio fond.	350	351	364	363	1	2	40.0		0.32	0.16
321	Guscio fond.	351	19	37	364	1	2	40.0		0.32	0.16
322	Guscio fond.	19	34	365	37	1	2	40.0		0.32	0.16
323	Guscio fond.	34	20	36	365	1	2	40.0		0.32	0.16
324	Guscio fond.	20	352	35	36	1	2	40.0		0.32	0.16
325	Setto	366	367	73	25	1	1	25.0			
326	Setto	367	368	75	73	1	1	25.0			
327	Setto	368	369	77	75	1	1	25.0			
328	Setto	369	370	24	77	1	1	25.0			
329	Setto	370	371	79	24	1	1	25.0			
330	Setto	371	372	81	79	1	1	25.0			
331	Setto	372	373	83	81	1	1	25.0			
332	Setto	373	374	23	83	1	1	25.0			
333	Setto	374	375	85	23	1	1	25.0			
334	Setto	375	376	87	85	1	1	25.0			
335	Setto	376	377	89	87	1	1	25.0			
336	Setto	377	378	22	89	1	1	25.0			
337	Setto	22	21	379	378	1	1	25.0			
338	Setto	379	380	95	21	1	1	25.0			
339	Setto	380	381	5	95	1	1	25.0			
340	Setto	5	118	382	381	1	1	30.0			
341	Setto	118	146	383	382	1	1	30.0			
342	Setto	146	6	384	383	1	1	30.0			
343	Setto	6	185	385	384	1	1	30.0			
344	Setto	185	187	386	385	1	1	30.0			
345	Setto	187	189	387	386	1	1	30.0			
346	Setto	189	245	388	387	1	1	30.0			
347	Setto	245	247	389	388	1	1	30.0			
348	Setto	247	249	390	389	1	1	30.0			
349	Setto	249	251	391	390	1	1	30.0			
350	Setto	251	282	392	391	1	1	30.0			
351	Setto	282	58	393	392	1	1	30.0			
352	Setto	58	52	394	393	1	1	30.0			
353	Setto	52	332	395	394	1	1	30.0			
354	Setto	332	53	396	395	1	1	30.0			
355	Setto	53	20	397	396	1	1	30.0			
356	Setto	398	397	20	34	1	1	25.0			
357	Setto	399	398	34	19	1	1	25.0			
358	Setto	400	399	19	351	1	1	25.0			
359	Setto	401	400	351	350	1	1	25.0			
360	Setto	402	401	350	349	1	1	25.0			
361	Setto	403	402	349	18	1	1	25.0			
362	Setto	404	403	18	348	1	1	25.0			
363	Setto	405	404	348	347	1	1	25.0			
364	Setto	406	405	347	346	1	1	25.0			

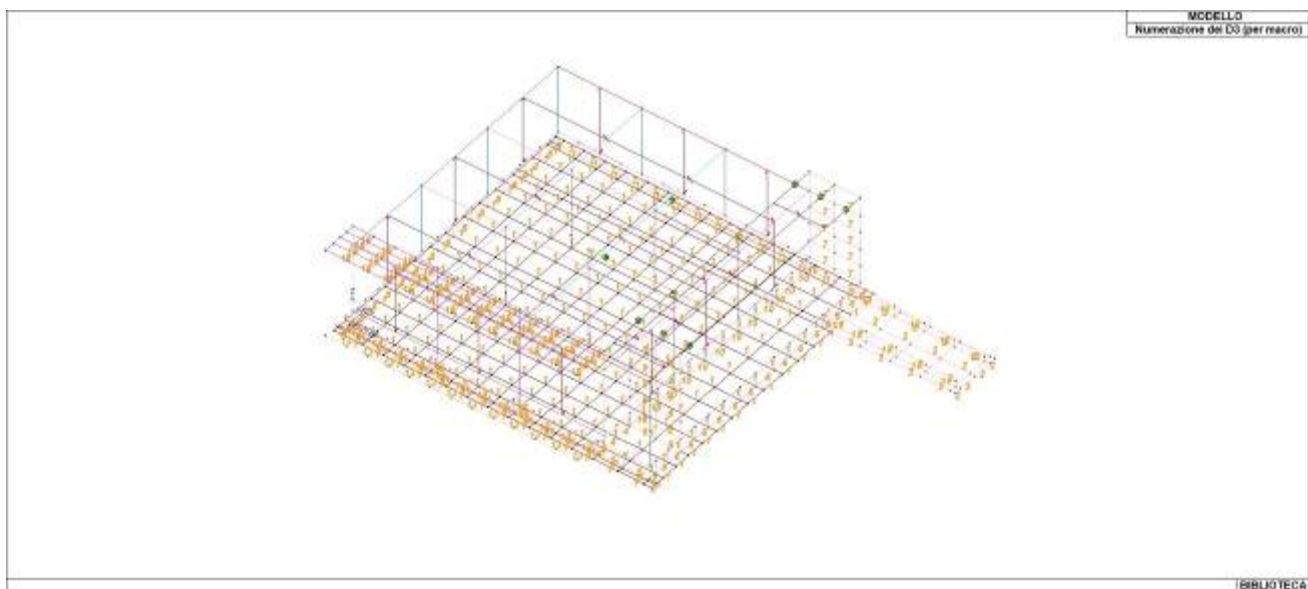
Elem.	Note	Nodo I	Nodo J	Nodo K	Nodo L	Mat.	Crit.	Spessore	Svincolo	Wink V	Wink O
365	Setto	407	406	346	17	1	1	25.0			
366	Setto	408	407	17	345	1	1	25.0			
367	Setto	409	408	345	344	1	1	25.0			
368	Setto	410	409	344	343	1	1	25.0			
369	Setto	411	410	343	16	1	1	25.0			
370	Setto	305	16	411	412	1	1	25.0			
371	Setto	308	305	412	413	1	1	25.0			
372	Setto	69	308	413	414	1	1	25.0			
373	Setto	70	69	414	415	1	1	25.0			
374	Setto	258	70	415	416	1	1	25.0			
375	Setto	12	258	416	417	1	1	25.0			
376	Setto	199	12	417	418	1	1	25.0			
377	Setto	197	199	418	419	1	1	25.0			
378	Setto	195	197	419	420	1	1	25.0			
379	Setto	8	195	420	421	1	1	25.0			
380	Setto	151	8	421	422	1	1	25.0			
381	Setto	149	151	422	423	1	1	25.0			
382	Setto	48	149	423	424	1	1	25.0			
383	Setto	121	48	424	425	1	1	25.0			
384	Setto	1	121	425	426	1	1	25.0			
385	Setto	104	1	426	427	1	1	25.0			
386	Setto	25	104	427	366	1	1	25.0			
387	Setto	428	384	6	145	1	1	25.0			
388	Setto	429	428	145	7	1	1	25.0			
389	Setto	21	4	430	379	1	1	25.0			
390	Setto	4	143	431	430	1	1	25.0			
391	Setto	143	7	429	431	1	1	25.0			
392	Setto	7	183	432	429	1	1	30.0			
393	Setto	183	184	433	432	1	1	30.0			
394	Setto	184	11	434	433	1	1	30.0			
395	Setto	11	242	435	434	1	1	30.0			
396	Setto	242	243	436	435	1	1	30.0			
397	Setto	243	244	437	436	1	1	30.0			
398	Setto	244	15	438	437	1	1	30.0			
399	Setto	15	279	439	438	1	1	30.0			
400	Setto	279	64	440	439	1	1	30.0			
401	Setto	64	63	441	440	1	1	30.0			
402	Setto	63	329	442	441	1	1	30.0			
403	Setto	329	302	443	442	1	1	30.0			
404	Setto	302	19	399	443	1	1	30.0			
405	Setto	470	474	473	467	1	1	25.0			
406	Setto	471	515	474	470	1	1	25.0			
407	Setto	475	476	471	512	1	1	25.0			
408	Setto	476	477	515	471	1	1	25.0			
409	Setto	478	479	458	509	1	1	25.0			
410	Setto	479	480	514	458	1	1	25.0			
411	Setto	526	528	296	295	1	1	25.0			
412	Setto	528	529	298	296	1	1	25.0			
413	Setto	529	530	300	298	1	1	25.0			
414	Setto	530	522	55	300	1	1	25.0			
415	Setto	527	520	336	334	1	1	25.0			
416	Setto	520	524	338	336	1	1	25.0			
417	Setto	524	525	340	338	1	1	25.0			
418	Setto	525	523	54	340	1	1	25.0			
419	Setto	394	526	295	52	1	1	25.0			
420	Setto	396	527	334	53	1	1	25.0			
421	Guscio	533	532	367	366	1	1	25.0			
422	Guscio	531	534	532	533	1	1	25.0			
423	Guscio	532	535	368	367	1	1	25.0			
424	Guscio	534	536	535	532	1	1	25.0			
425	Guscio	535	537	369	368	1	1	25.0			
426	Guscio	536	538	537	535	1	1	25.0			
427	Guscio	537	539	370	369	1	1	25.0			
428	Guscio	538	540	539	537	1	1	25.0			
429	Guscio	539	541	371	370	1	1	25.0			
430	Guscio	540	542	541	539	1	1	25.0			
431	Guscio	541	543	372	371	1	1	25.0			
432	Guscio	542	544	543	541	1	1	25.0			

Elem.	Note	Nodo I	Nodo J	Nodo K	Nodo L	Mat.	Crit.	Spessore	Svincolo	Wink V	Wink O
433	Setto	24	100	468	370	1	1	30.0			
434	Guscio	543	545	373	372	1	1	25.0			
435	Guscio	544	546	545	543	1	1	25.0			
436	Guscio	545	547	374	373	1	1	25.0			
437	Guscio	546	548	547	545	1	1	25.0			
438	Guscio	547	549	375	374	1	1	25.0			
439	Guscio	548	550	549	547	1	1	25.0			
440	Guscio	549	444	376	375	1	1	25.0			
441	Guscio	550	445	444	549	1	1	25.0			
442	Guscio	444	446	377	376	1	1	25.0			
443	Guscio	445	447	446	444	1	1	25.0			
444	Guscio	446	449	378	377	1	1	25.0			
445	Guscio	447	450	449	446	1	1	25.0			
446	Setto	451	453	428	429	1	1	25.0			
447	Setto	454	455	453	451	1	1	25.0			
448	Setto	456	457	455	454	1	1	25.0			
449	Setto	23	96	481	374	1	1	30.0			
450	Setto	509	458	457	456	1	1	25.0			
451	Setto	453	459	384	428	1	1	25.0			
452	Setto	455	461	459	453	1	1	25.0			
453	Setto	457	462	461	455	1	1	25.0			
454	Setto	458	514	462	457	1	1	25.0			
455	Setto	463	465	398	399	1	1	25.0			
456	Setto	466	467	465	463	1	1	25.0			
457	Setto	469	470	467	466	1	1	25.0			
458	Setto	512	471	470	469	1	1	25.0			
459	Setto	465	472	397	398	1	1	25.0			
460	Setto	467	473	472	465	1	1	25.0			
461	Guscio	553	554	555	518	1	8	15.0			
462	Guscio	554	556	557	555	1	8	15.0			
463	Guscio	556	558	559	557	1	8	15.0			
464	Guscio	558	489	519	559	1	8	15.0			
465	Guscio	560	561	562	517	1	8	15.0			
466	Guscio	561	563	564	562	1	8	15.0			
467	Guscio	563	565	566	564	1	8	15.0			
468	Guscio	565	553	518	566	1	8	15.0			
469	Guscio	567	568	569	516	1	8	15.0			
470	Guscio	568	570	571	569	1	8	15.0			
471	Guscio	570	572	573	571	1	8	15.0			
472	Guscio	572	560	517	573	1	8	15.0			
473	Guscio	574	575	554	553	1	8	15.0			
474	Guscio	576	577	575	574	1	8	15.0			
475	Guscio	487	578	577	576	1	8	15.0			
476	Guscio	575	579	556	554	1	8	15.0			
477	Guscio	577	580	579	575	1	8	15.0			
478	Guscio	578	581	580	577	1	8	15.0			
479	Guscio	579	582	558	556	1	8	15.0			
480	Guscio	580	583	582	579	1	8	15.0			
481	Guscio	581	584	583	580	1	8	15.0			
482	Guscio	582	585	489	558	1	8	15.0			
483	Guscio	583	586	585	582	1	8	15.0			
484	Guscio	584	485	586	583	1	8	15.0			
485	Guscio	587	588	561	560	1	8	15.0			
486	Guscio	589	590	588	587	1	8	15.0			
487	Guscio	486	591	590	589	1	8	15.0			
488	Guscio	588	592	563	561	1	8	15.0			
489	Guscio	590	593	592	588	1	8	15.0			
490	Guscio	591	594	593	590	1	8	15.0			
491	Guscio	592	595	565	563	1	8	15.0			
492	Guscio	593	596	595	592	1	8	15.0			
493	Guscio	594	597	596	593	1	8	15.0			
494	Guscio	595	574	553	565	1	8	15.0			
495	Guscio	596	576	574	595	1	8	15.0			
496	Guscio	597	487	576	596	1	8	15.0			
497	Guscio	598	599	568	567	1	8	15.0			
498	Guscio	600	601	599	598	1	8	15.0			
499	Guscio	484	602	601	600	1	8	15.0			
500	Guscio	599	603	570	568	1	8	15.0			

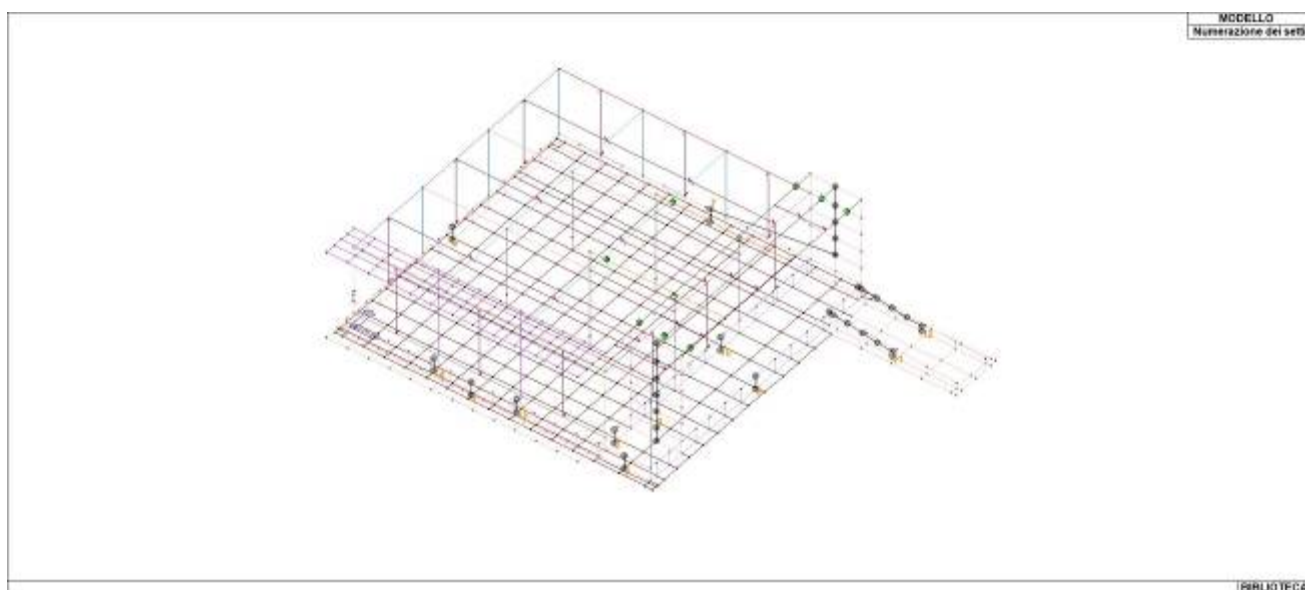
Elem.	Note	Nodo I	Nodo J	Nodo K	Nodo L	Mat.	Crit.	Spessore	Svincolo	Wink V	Wink O
501	Guscio	601	604	603	599	1	8	15.0			
502	Guscio	602	605	604	601	1	8	15.0			
503	Guscio	603	606	572	570	1	8	15.0			
504	Guscio	604	607	606	603	1	8	15.0			
505	Guscio	605	488	607	604	1	8	15.0			
506	Guscio	606	587	560	572	1	8	15.0			
507	Guscio	607	589	587	606	1	8	15.0			
508	Guscio	488	486	589	607	1	8	15.0			
509	Setto	100	2	499	468	1	1	30.0			
510	Setto	96	3	482	481	1	1	30.0			



16_MOD_NUMERAZIONE_D3



16_MOD_NUMERAZIONE_D3_MACRO



16_MOD_NUMERAZIONE_D3_PARETI

MODELLAZIONE DELLA STRUTTURA: ELEMENTI SOLAIO-PANNELLO

LEGENDA TABELLA DATI SOLAI-PANNELLI

Il programma utilizza per la modellazione elementi a tre o più nodi denominati in generale solaio o pannello.

Ogni elemento solaio-pannello è individuato da una poligonale di nodi 1,2, ..., N.

L'elemento solaio è utilizzato in primo luogo per la modellazione dei carichi agenti sugli elementi strutturali. In secondo luogo può essere utilizzato per la corretta ripartizione delle forze orizzontali agenti nel proprio piano. L'elemento balcone è derivato dall'elemento solaio.

I carichi agenti sugli elementi solaio, raccolti in un archivio, sono direttamente assegnati agli elementi utilizzando le informazioni raccolte nell' archivio (es. i coefficienti combinatori). La tabella seguente riporta i dati utilizzati per la definizione dei carichi e delle masse.

L'elemento pannello è utilizzato solo per l'applicazione dei carichi, quali pesi delle tamponature o spinte dovute al vento o terre. In questo caso i carichi sono applicati in analogia agli altri elementi strutturali (si veda il cap. SCHEMATIZZAZIONE DEI CASI DI CARICO).

Id.Arch.	Identificativo dell' archivio
Tipo	Tipo di carico Variab. Carico variabile generico Var. rid. Carico variabile generico con riduzione in funzione dell' area (c.5.5. ...) Neve Carico di neve
G1k	carico permanente (comprensivo del peso proprio)
G2k	carico permanente non strutturale e non compiutamente definito
Qk	carico variabile
Fatt. A	fattore di riduzione del carico variabile (0.5 o 0.75) per tipo "Var.rid."
S sis.	fattore di riduzione del carico variabile per la definizione delle masse sismiche per D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento")
Psi 0	Coefficiente combinatorio dei valori caratteristici delle azioni variabili: per valore raro
Psi 1	Coefficiente combinatorio dei valori caratteristici delle azioni variabili: per valore frequente
Psi 2	Coefficiente combinatorio dei valori caratteristici delle azioni variabili: per valore quasi permanente
Psi S 2	Coefficiente di combinazione che fornisce il valore quasi-permanente dell'azione variabile: per la definizione delle masse sismiche
Fatt. Fi	Coefficiente di correlazione dei carichi per edifici

Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione. In particolare per ogni elemento viene indicato in tabella:

Elem	numero dell'elemento
Tipo	codice di comportamento S elemento utilizzato solo per scarico C elemento utilizzato per scarico e per modellazione piano rigido P elemento utilizzato come pannello M scarico monodirezionale B scarico bidirezionale
Id.Arch.	Identificativo dell' archivio
Mat	codice del materiale assegnato all'elemento
Spessore	spessore dell'elemento (costante)
Orditura	angolo (rispetto all'asse X) della direzione dei travetti principali
Gk	carico permanente solaio (comprensivo del peso proprio)
Qk	carico variabile solaio
Nodi	numero dei nodi che definiscono l'elemento (5 per riga)

La progettazione viene eseguita con il metodo degli stati limite. I simboli utilizzati in tabella assumono il seguente significato:

Elem.	numero identificativo dell'elemento
Stato	Codici di verifica relativi alle tensioni normali e alle tensioni tangenziali
Note	Viene riportato il codice relativo alla sezione(s) e relativo al materiale(m);
Pos.	Ascissa del punto di verifica
F ist, F infi	Frecce istantanee e a tempo infinito
Momento	Momento flettente
Taglio	Sollecitazione di taglio
Af inf.	Area di armatura longitudinale posta all'intradosso della trave
Af sup.	Area di armatura longitudinale posta all'estradosso della trave
AfV	Area dell'armatura atta ad assorbire le azioni di taglio
Beff	Base della sezione di cls per l'assorbimento del taglio
x/d	rapporto tra posizione dell'asse neutro e altezza utile alla rottura della sezione (per sola flessione)
verif.	rapporto Sd/Su con sollecitazioni ultime proporzionali:

	valore minore o uguale a 1 per verifica positiva
Verif.V	rapporto Sd/Su con sollecitazioni taglianti proporzionali valore minore o uguale a 1 per verifica positiva
rRfck	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni rare [normalizzato a 1]
rFfck	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni freq. [normalizzato a 1]
rPfck	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni quasi perm. [normalizzato a 1]
rRfyk	rapporto tra la massima tensione nell'acciaio e la tensione fyk in combinazioni frequenti [normalizzato a 1]
rFyk	rapporto tra la massima tensione nell'acciaio e la tensione fyk in combinazioni rare [normalizzato a 1]
rPfyk	rapporto tra la massima tensione nell'acciaio e la tensione fyk in combinazioni quasi permanenti [normalizzato a 1]
wR	apertura caratteristica delle fessure in combinazioni rare [mm]
wF	apertura caratteristica delle fessure in combinazioni frequenti [mm]
wP	apertura caratteristica delle fessure in combinazioni quasi permanenti [mm]

Nel caso in cui si sia proceduto alla verifica delle tamponature secondo il D.M. 17.01.2018 - §7.2.3 viene riportata una tabella riassuntiva delle verifiche degli elementi pannello. La verifica confronta i momenti sollecitanti indotti dal sisma con i momenti resistenti, secondo tre ipotesi, due basate sulla resistenza a pressoflessione della tamponatura ed una basata sul cinematiso a seguito della formazione di tre cerniere plastiche sulla tamponatura (rif. Ufficio di Vigilanza sulle Costruzioni, Provincia di Terni). Qualora la tamponatura sia di tipo antiespulsione (nelle due possibili varianti ordinaria o armata) viene condotta una verifica con meccanismo ad arco con degrado di resistenza. La verifica confronta le pressioni sollecitanti indotte dal sisma con le pressioni resistenti che la tamponatura sviluppa attraverso il meccanismo ad arco. La verifica considera anche il degrado di resistenza dovuto al danneggiamento nel piano della tamponatura.

Per quest'ultima tamponatura sono disponibili, in funzione del materiale impiegato (materiale [52] o materiale [53]):

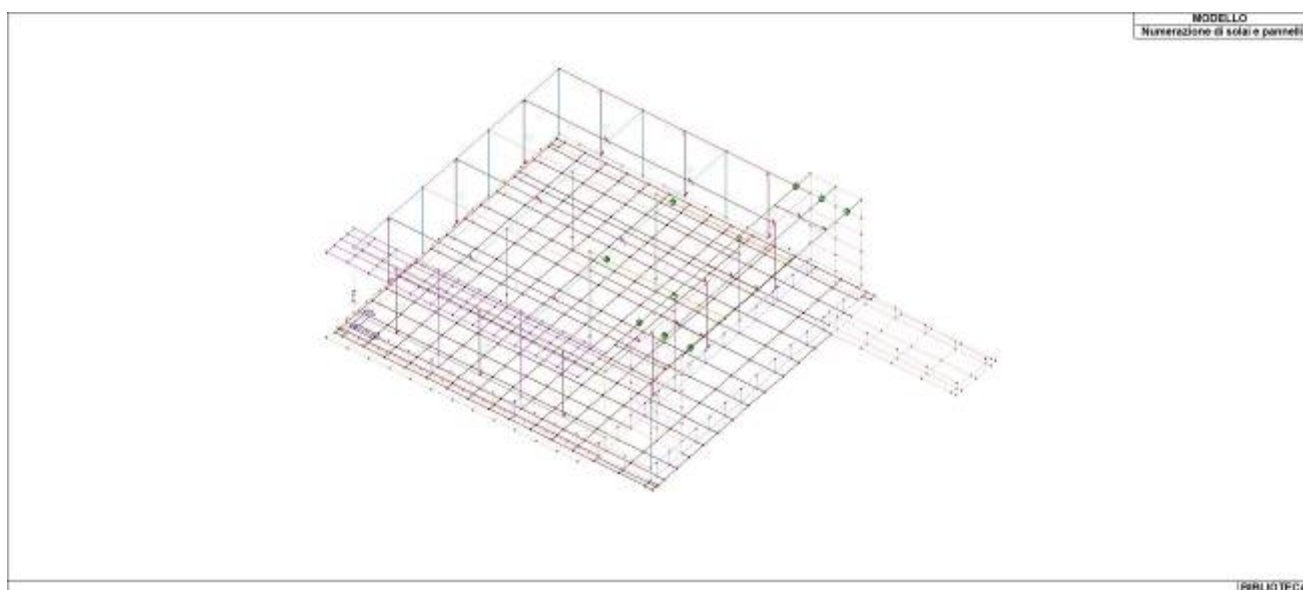
- **Tamponatura Antiespulsione ordinaria Poroton® Cis Edil** sp.30 cm; con metodo di verifica per meccanismo ad arco con degrado di resistenza, sviluppato attraverso i risultati di un progetto di ricerca sperimentale condotto dall'Università degli Studi di Padova.
Utilizzabile per il materiale [52].
- **Tamponatura Antiespulsione armata Poroton® Cis Edil** sp.30 cm; con metodo di verifica per meccanismo ad arco con degrado di resistenza, sviluppato attraverso i risultati di un progetto di ricerca sperimentale condotto dall'Università degli Studi di Padova.
Utilizzabile per il materiale [53].

La verifica è stata calibrata sulla base di prove sperimentali sul sistema di Tamponatura Antiespulsione anche in presenza di aperture. (rif. Rapporti di Prova redatti dal Dipartimento ICEA - Università degli Studi di Padova di test sperimentali condotti sul sistema Tamponatura Antiespulsione di Cis Edil)

In particolare i simboli utilizzati in tabella assumono il seguente significato:

Elem.	Numero identificativo dell'elemento
Stato	Codice di verifica
Ver. c.c.	Verifica nell'ipotesi di trave appoggiata con carico concentrato in mezzzeria
Ver. c.d.	Verifica nell'ipotesi di trave appoggiata con carico distribuito
Ver. c.cin.	Verifica nell'ipotesi di cinematiso con formazione di cerniere plastiche in appoggio e mezzzeria
Ver. CIS	Rapporto pa/pr (valore minore o uguale a 1 per verifica positiva)
Z	Quota del baricentro dell'elemento
T1	Periodo proprio dell'edificio nella direzione di interesse (ortogonale al pannello)
Ta	Periodo proprio della parete
Sa	Accelerazione massima, adimensionalizzata allo SLV
pa	Pressione sulla parete causata dall'azione sismica
pr	Pressione resistente del meccanismo ad arco
Drift	Spostamento relativo interpiano allo SLV valutato secondo il D.M. 14.01.2018 - § 7.3.3.3
Beta a	Coef. riduttivo per tener conto del danneggiamento del piano dipendente dallo spostamento, ottenuto sperimentalmente

ID Arch.	Tipo	G1	G2	Q	Fatt. A	s sis.	Psi 0	Psi 1	Psi 2	Psi S 2	Fatt. Fi
		daN/ m2	daN/ m2	daN/ m2							
1	Neve	400.00	50.00	120.00		1.00	0.50	0.20	0.0	0.0	1.00
	Variab.						0.70	0.50	0.30		
2	Neve	400.00	400.00	120.00		1.00	0.50	0.20	0.0	0.0	1.00
	Variab.						0.70	0.50	0.30		
3	Neve	15.00	50.00	120.00		1.00	0.50	0.20	0.0	0.0	1.00
	Variab.						0.70	0.50	0.30		



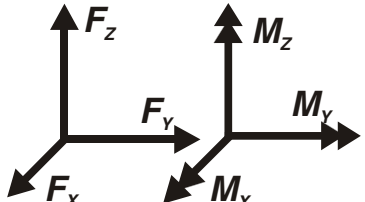
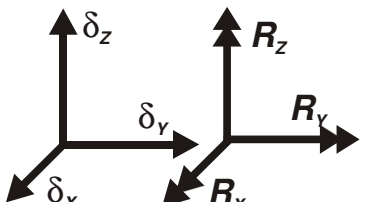
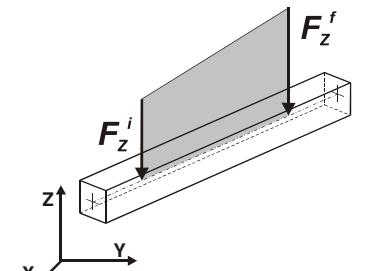
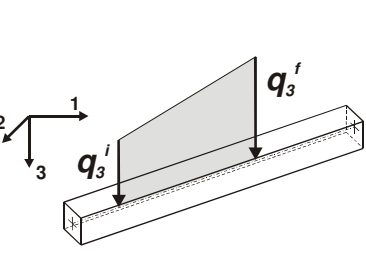
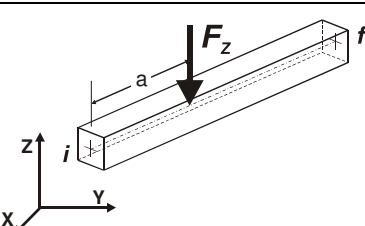
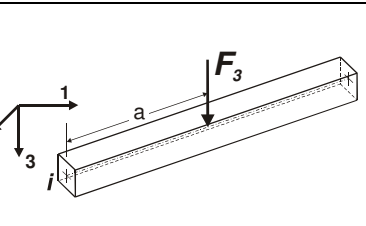
17_MOD_NUMERAZIONE_SOLAI

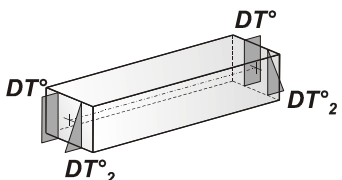
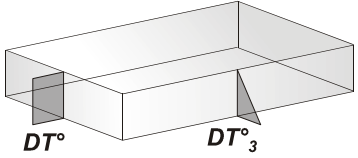
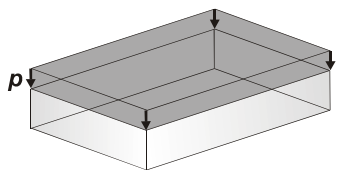
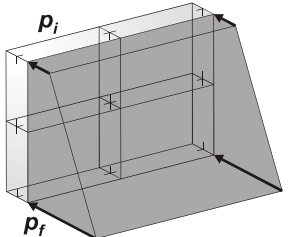
MODELLAZIONE DELLE AZIONI

LEGENDA TABELLA DATI AZIONI

Il programma consente l'uso di diverse tipologie di carico (azioni). Le azioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni azione applicata alla struttura viene di riportato il codice, il tipo e la sigla identificativa. Le tabelle successive dettagliano i valori caratteristici di ogni azione in relazione al tipo. Le tabelle riportano infatti i seguenti dati in relazione al tipo:

1	carico concentrato nodale 6 dati (forza F_x , F_y , F_z , momento M_x , M_y , M_z)
2	spostamento nodale impresso 6 dati (spostamento T_x , T_y , T_z , rotazione R_x , R_y , R_z)
3	carico distribuito globale su elemento tipo trave 7 dati (f_x , f_y , f_z , m_x , m_y , m_z , ascissa di inizio carico) 7 dati (f_x , f_y , f_z , m_x , m_y , m_z , ascissa di fine carico)
4	carico distribuito locale su elemento tipo trave 7 dati (f_1 , f_2 , f_3 , m_1 , m_2 , m_3 , ascissa di inizio carico) 7 dati (f_1 , f_2 , f_3 , m_1 , m_2 , m_3 , ascissa di fine carico)
5	carico concentrato globale su elemento tipo trave 7 dati (F_x , F_y , F_z , M_x , M_y , M_z , ascissa di carico)
6	carico concentrato locale su elemento tipo trave 7 dati (F_1 , F_2 , F_3 , M_1 , M_2 , M_3 , ascissa di carico)
7	variazione termica applicata ad elemento tipo trave 7 dati (variazioni termiche: uniforme, media e differenza in altezza e larghezza al nodo iniziale e finale)
8	carico di pressione uniforme su elemento tipo piastra 1 dato (pressione)
9	carico di pressione variabile su elemento tipo piastra 4 dati (pressione, quota, pressione, quota)
10	variazione termica applicata ad elemento tipo piastra 2 dati (variazioni termiche: media e differenza nello spessore)
11	carico variabile generale su elementi tipo trave e piastra 1 dato descrizione della tipologia 4 dati per segmento (posizione, valore, posizione, valore) la tipologia precisa l'ascissa di definizione, la direzione del carico, la modalità di carico e la larghezza d'influenza per gli elementi tipo trave
12	gruppo di carichi con impronta su piastra 9 dati (numero di ripetizioni in direzione X e Y, valore di ciascun carico, posizione centrale del primo, dimensioni dell'impronta, interasse tra i carichi)

 <p>Carico concentrato nodale</p>	 <p>Spostamento impresso</p>
 <p>Carico distribuito globale</p>	 <p>Carico distribuito locale</p>
 <p>Carico concentrato globale</p>	 <p>Carico concentrato locale</p>

 <p>Carico termico 2D</p>	 <p>Carico termico 3D</p>
 <p>Carico pressione uniforme</p>	 <p>Carico pressione variabile</p>

Tipo	carico di pressione uniforme su piastra
-------------	--

Id	Tipo	pressione
		daN/ m2
5	QVK PAN ++ vento*0.4 - P3:p= 5.120e-03	51.20
6	QVK PAN -- vento*0.4 - P3:p= 5.120e-03	51.20
7	QVK PAN ++ vento*0.4 - P3:p= 2.560e-03	25.60
8	QVK PAN -- vento*0.4 - P3:p= 2.560e-03	25.60

Tipo	carico variabile generale
-------------	----------------------------------

Id	Tipo	ascissa	valore	ascissa	valore
		m	daN/ m2	m	daN/ m2
9	g2k su sbalzo p. terra - QV:unif - Qz - Pres.				
	Unif. Qz Pres. L2=0.0		-100.00		
10	variabile su sbalzo p. terra - QV:unif - Qz - Pres.				
	Unif. Qz Pres. L2=0.0		-400.00		
11	g1k su platea - QV:unif - Qz - Pres.				
	Unif. Qz Pres. L2=0.0		-490.00		
12	g2k su platea - QV:unif - Qz - Pres.				
	Unif. Qz Pres. L2=0.0		-50.00		
13	variabile su platea - QV:unif - Qz - Pres.				
	Unif. Qz Pres. L2=0.0		-600.00		
14	g2k su soletta a sbalzo in copertura - QV:unif - Qz - Pres.				
	Unif. Qz Pres. L2=0.0		-50.00		
15	Varuabili su soltta a sbalzo in copertura - QV:unif - Qz - Pres.				
	Unif. Qz Pres. L2=0.0		-120.00		

SCHEMATIZZAZIONE DEI CASI DI CARICO

LEGENDA TABELLA CASI DI CARICO

Il programma consente l'applicazione di diverse tipologie di casi di carico.

Sono previsti i seguenti 11 tipi di casi di carico:

	Sigla	Tipo	Descrizione
1	Ggk	A	caso di carico comprensivo del peso proprio struttura
2	Gk	NA	caso di carico con azioni permanenti
3	Qk	NA	caso di carico con azioni variabili
4	Gsk	A	caso di carico comprensivo dei carichi permanenti sui solai e sulle coperture
5	Qsk	A	caso di carico comprensivo dei carichi variabili sui solai
6	Qnk	A	caso di carico comprensivo dei carichi di neve sulle coperture
7	Qtk	SA	caso di carico comprensivo di una variazione termica agente sulla struttura
8	Qvk	NA	caso di carico comprensivo di azioni da vento sulla struttura
9	Esk	SA	caso di carico sismico con analisi statica equivalente
10	Edk	SA	caso di carico sismico con analisi dinamica
11	Etik	NA	caso di carico comprensivo di azioni derivanti dall' incremento di spinta delle terre in condizione sismica
12	Pk	NA	caso di carico comprensivo di azioni derivanti da coazioni, cedimenti e precompressioni

Sono di tipo automatico A (ossia non prevedono introduzione dati da parte dell'utente) i seguenti casi di carico: 1-Ggk; 4-Gsk; 5-Qsk; 6-Qnk.

Sono di tipo semi-automatico SA (ossia prevedono una minima introduzione dati da parte dell'utente) i seguenti casi di carico:

7-Qtk, in quanto richiede solo il valore della variazione termica;

9-Esk e 10-Edk, in quanto richiedono il valore dell'angolo di ingresso del sisma e l'individuazione dei casi di carico partecipanti alla definizione delle masse.

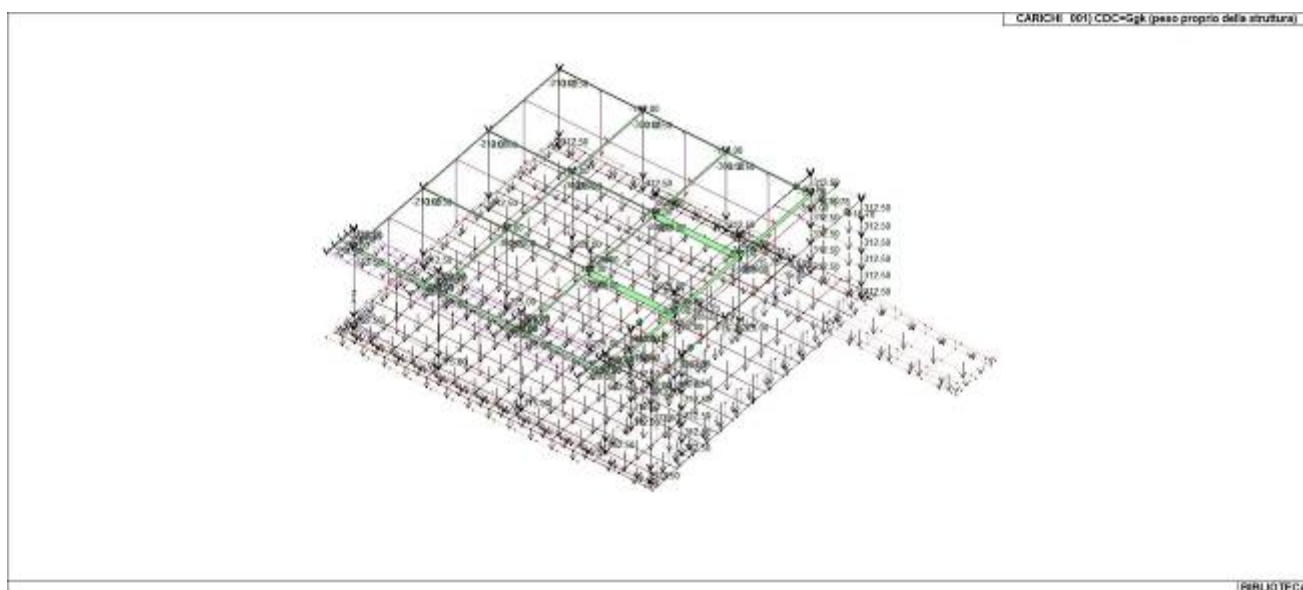
Sono di tipo non automatico NA ossia prevedono la diretta applicazione di carichi generici agli elementi strutturali (si veda il precedente punto Modellazione delle Azioni) i restanti casi di carico.

Nella tabella successiva vengono riportati i casi di carico agenti sulla struttura, con l'indicazione dei dati relativi al caso di carico stesso: *Numero Tipo e Sigla identificativa, Valore di riferimento* del caso di carico (se previsto).

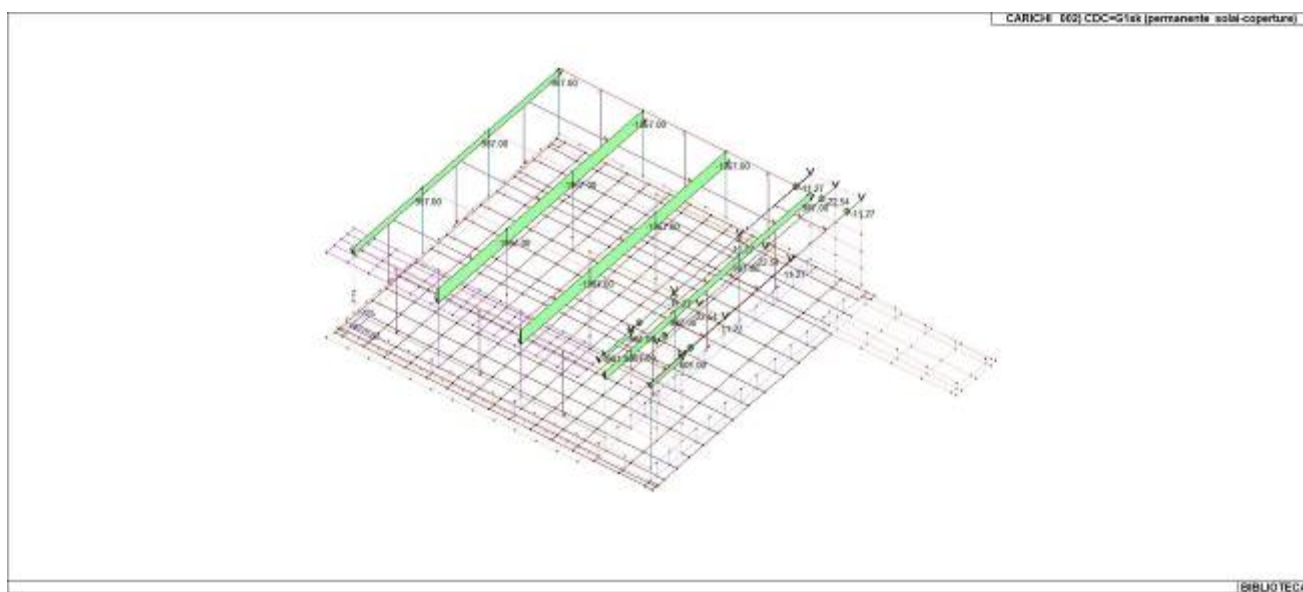
In successione, per i casi di carico non automatici, viene riportato l'elenco di nodi ed elementi direttamente caricati con la sigla identificativa del carico.

Per i casi di carico di tipo sismico (9-Esk e 10-Edk), viene riportata la tabella di definizione delle masse: per ogni caso di carico partecipante alla definizione delle masse viene indicata la relativa aliquota (partecipazione) considerata. Si precisa che per i caso di carico 5-Qsk e 6-Qnk la partecipazione è prevista localmente per ogni elemento solaio o copertura presente nel modello (si confronti il valore Sksol nel capitolo relativo agli elementi solaio) e pertanto la loro partecipazione è di norma pari a uno.

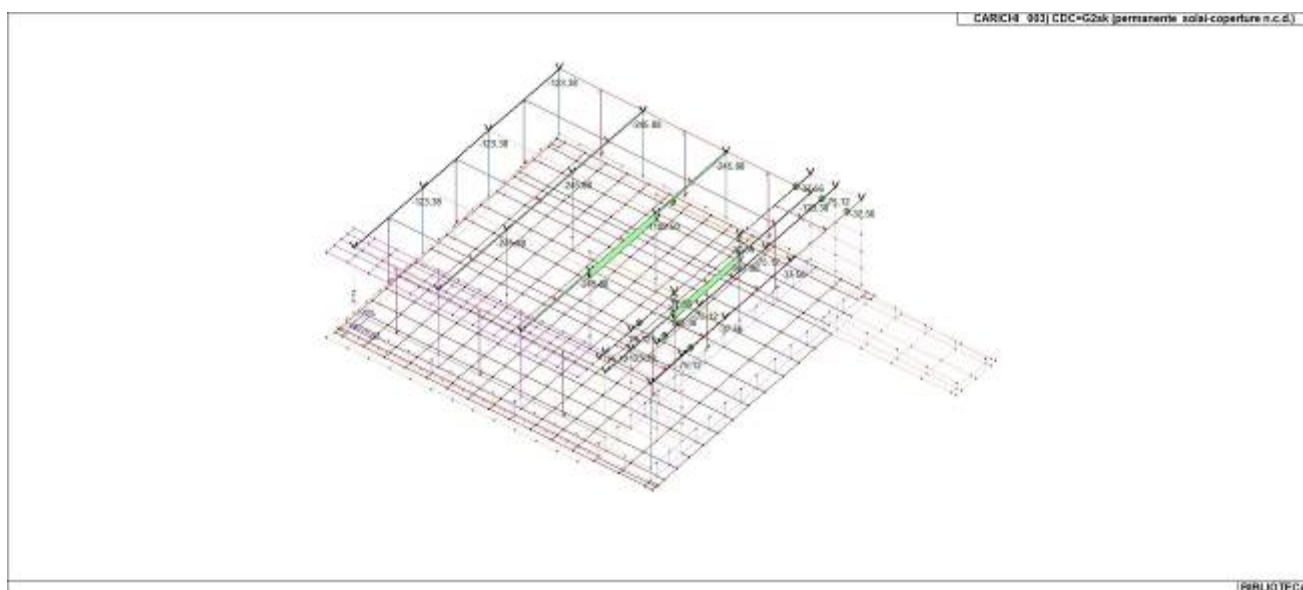
CDC	Tipo	Sigla Id
1	Ggk	CDC=Ggk (peso proprio della struttura)
2	Gsk	CDC=G1sk (permanente solai-coperture)
3	Gsk	CDC=G2sk (permanente solai-coperture n.c.d.)
4	Gsk	CDC=G2pk (permanente pannelli n.c.d.)
5	Qsk	CDC=Qsk (variabile solai)
6	Qnk	CDC=Qnk (carico da neve)
7	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)
8	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -)
9	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)
10	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -)
11	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. +)
12	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. -)
13	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. +)
14	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. -)
15	Qvk	CDC=Qvk (carico da vento) dir X +
16	Qvk	CDC=Qvk (carico da vento) dir X -
17	Qvk	CDC=Qvk (carico da vento) dir Y +
18	Qvk	CDC=Qvk (carico da vento) dir Y -
19	Gk	CDC=G1k (permanente su platea)
20	Gk	CDC=G2k (permanente su platea)
21	Qk	CDC=Qk (variabile su platea)
22	Gk	CDC=G2k (permanente su sbalzo p. terra)
23	Qk	CDC=Qk (variabile su sbalzo p. terra)
24	Gk	CDC=G2k (permanente su sbalzo in copertura)
25	Qk	CDC=Qk (variabile su sbalzo in copertura)



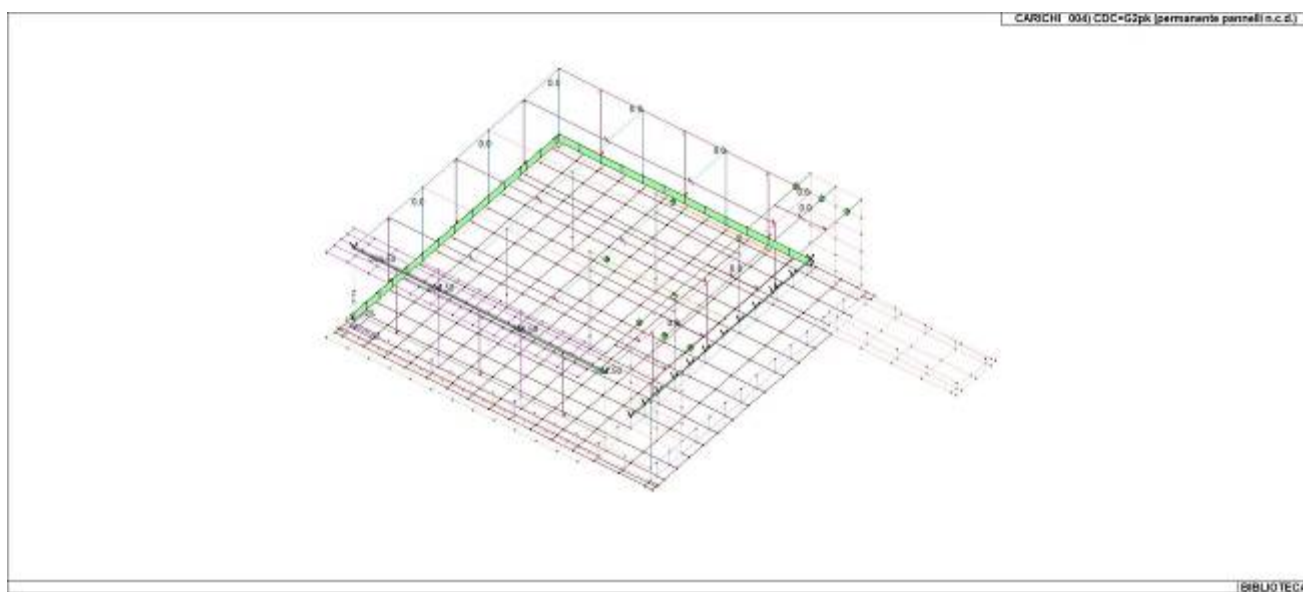
22_CDC_001_CDC=Ggk (peso proprio della struttura)



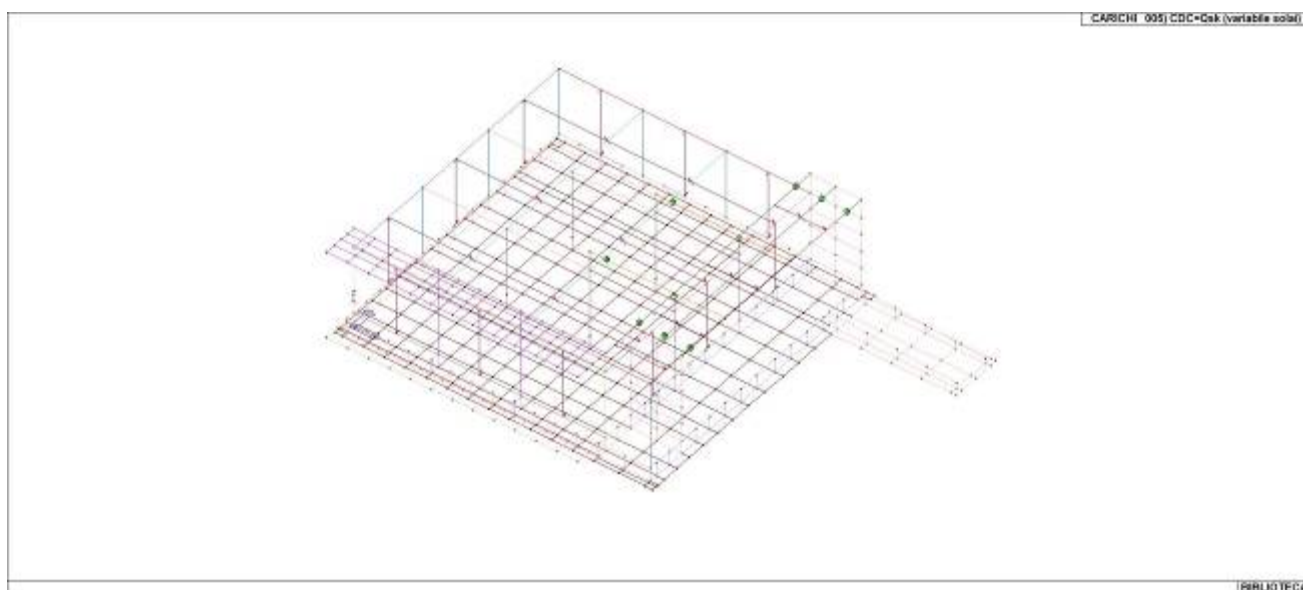
22_CDC_002_CDC=G1sk (permanente solai-coperture)



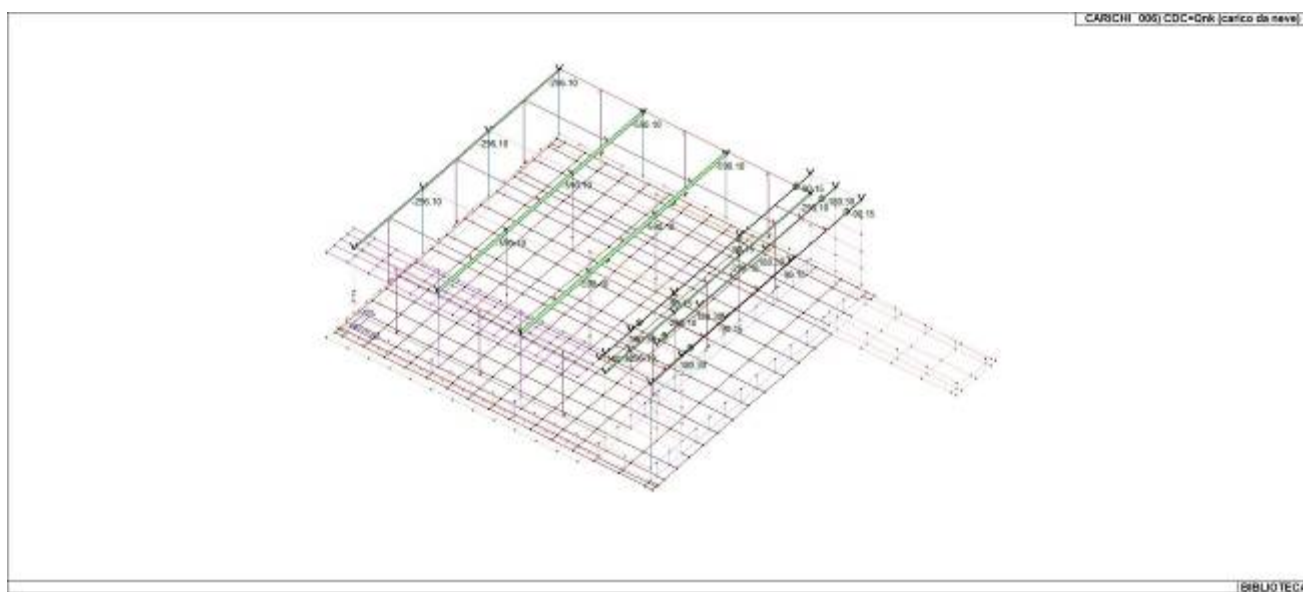
22_CDC_003_CDC=G2sk (permanente solai-coperture n.c.d.)



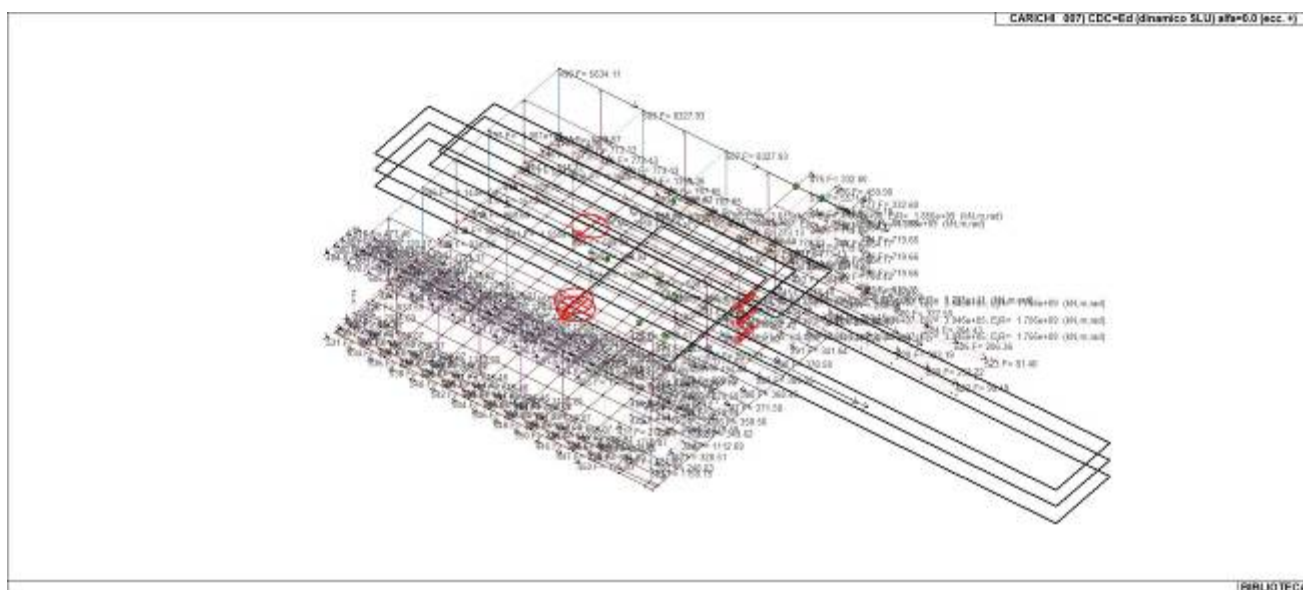
22_CDC_004_CDC=G2pk (permanente pannelli n.c.d.)



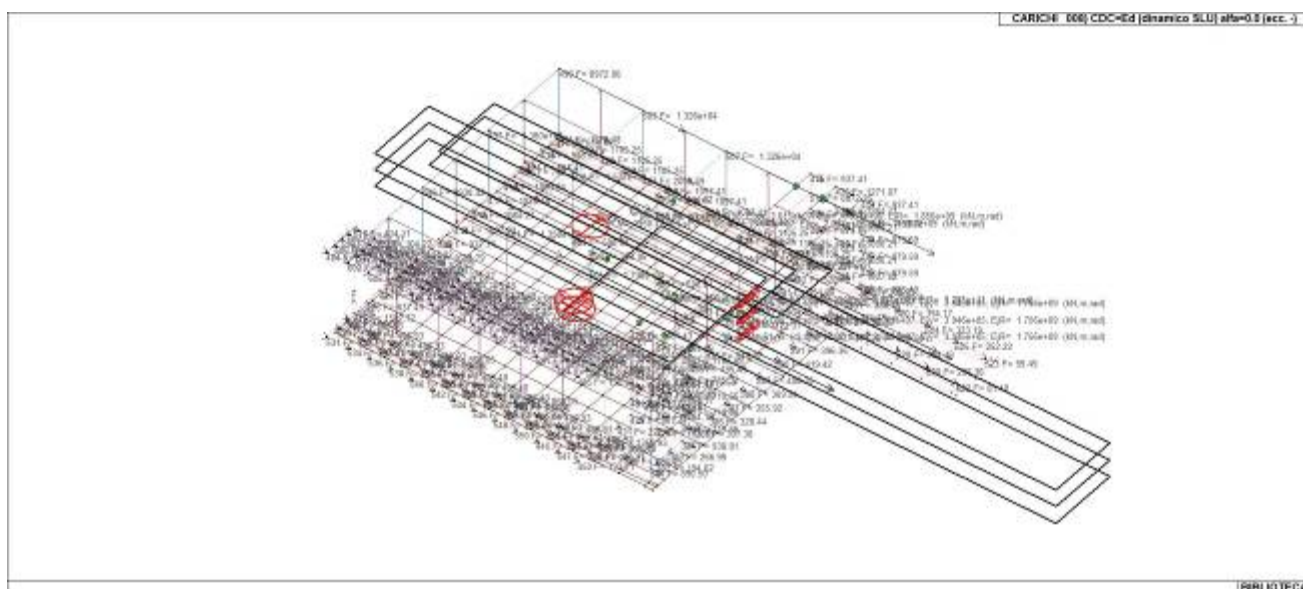
22_CDC_005_CDC=Qsk (variabile solai)



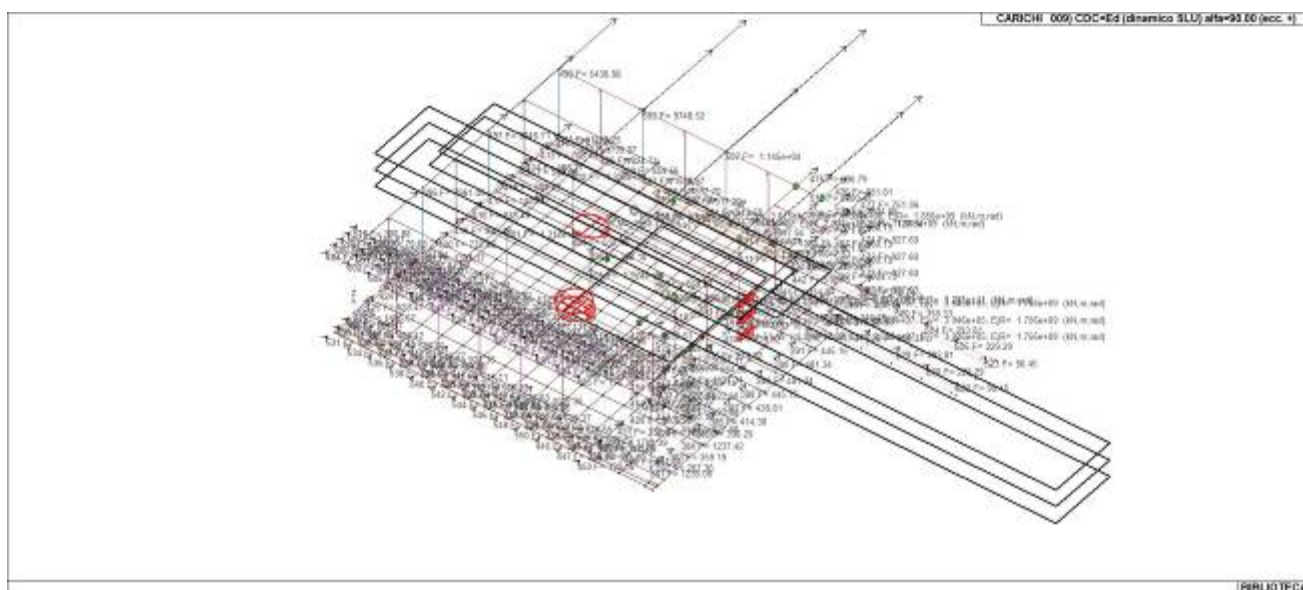
22_CDC_006_CDC=Qnk (carico da neve)



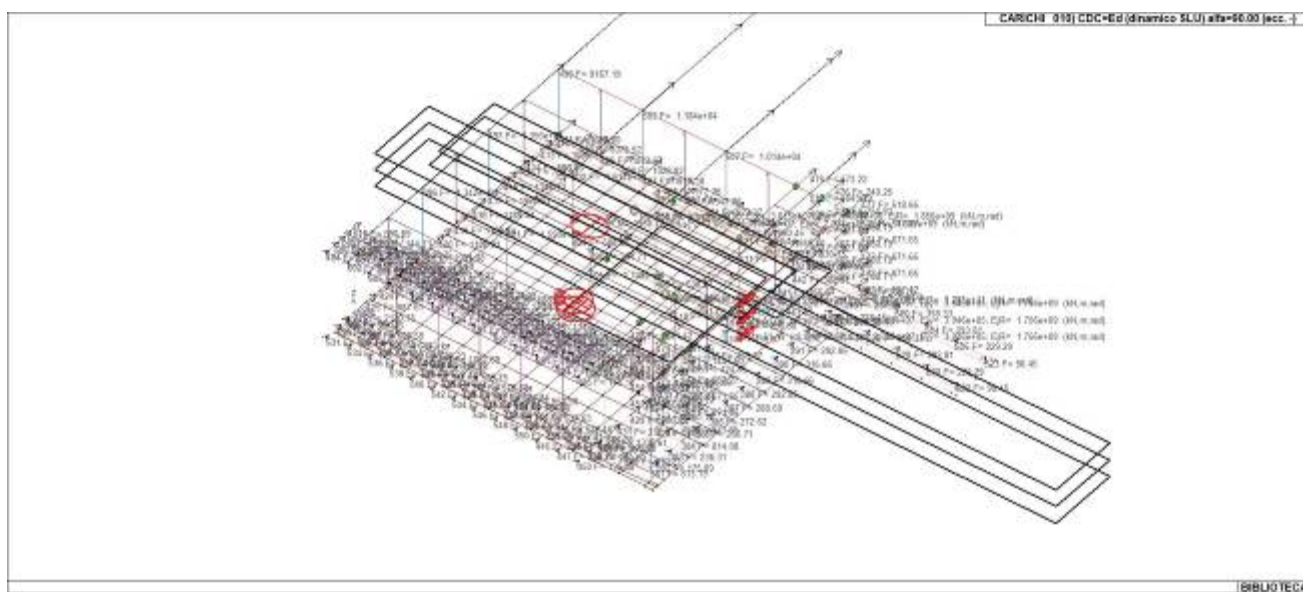
22_CDC_007_CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)



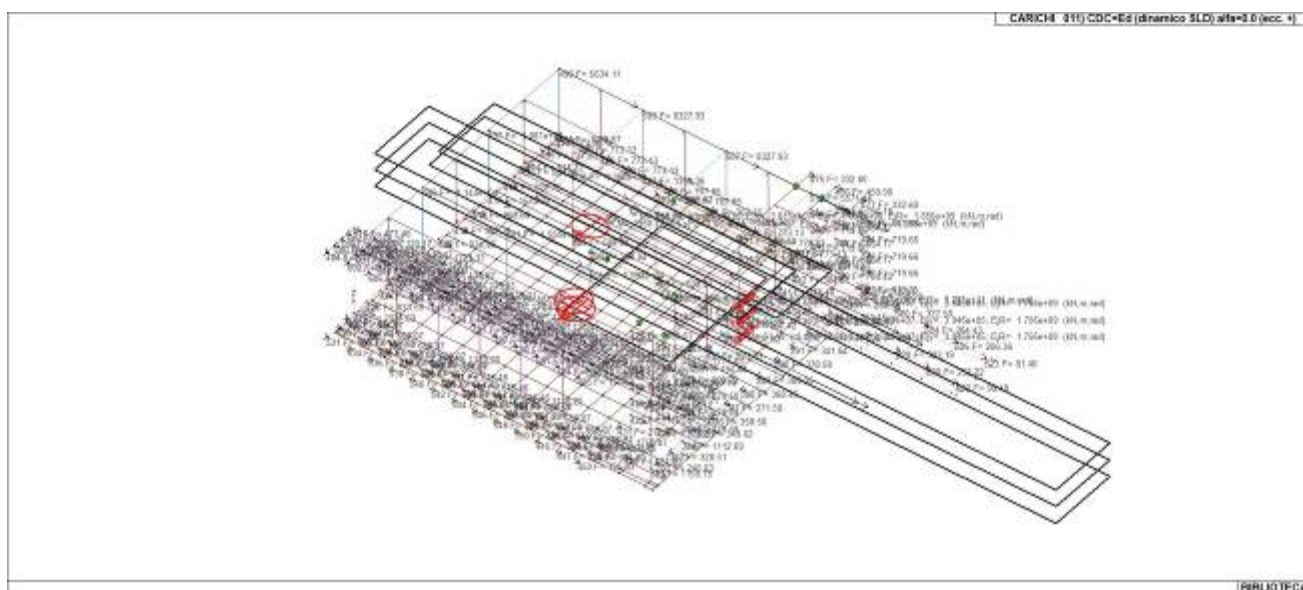
22_CDC_008_CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -)



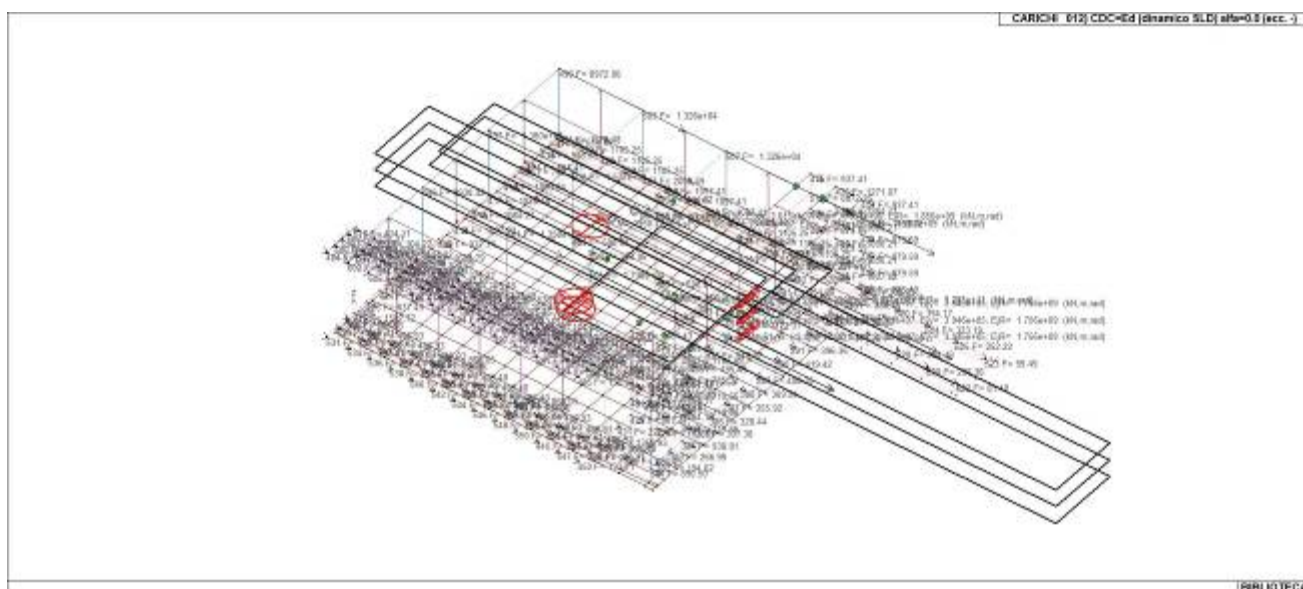
22_CDC_009_CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)



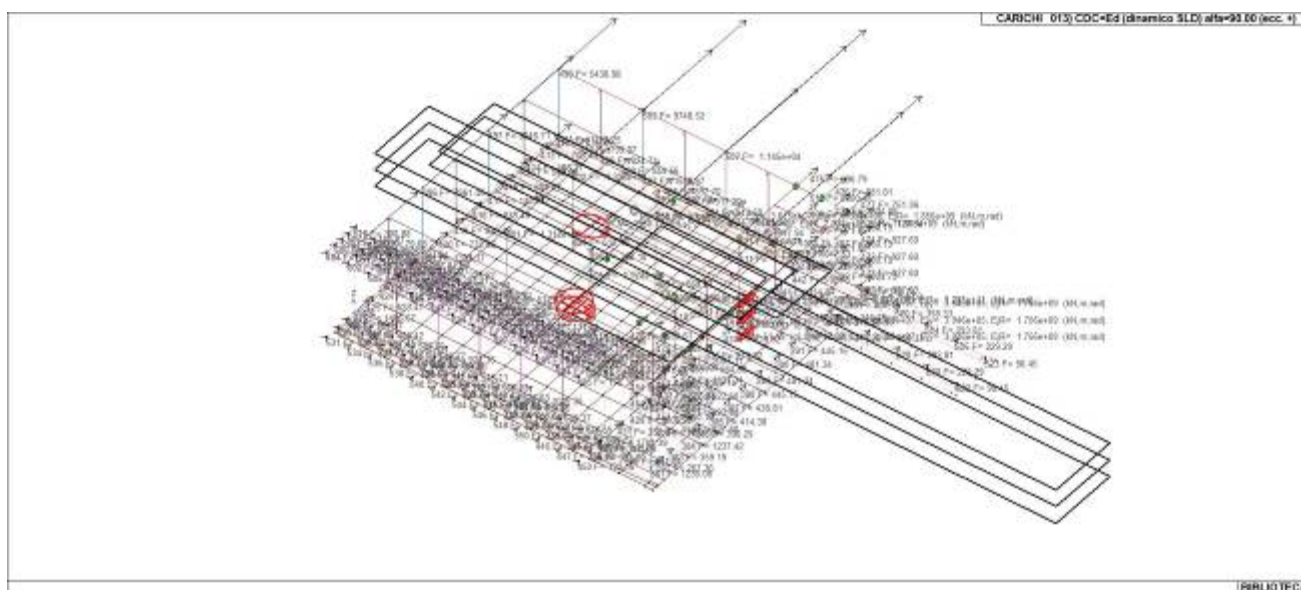
22_CDC_010_CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -)



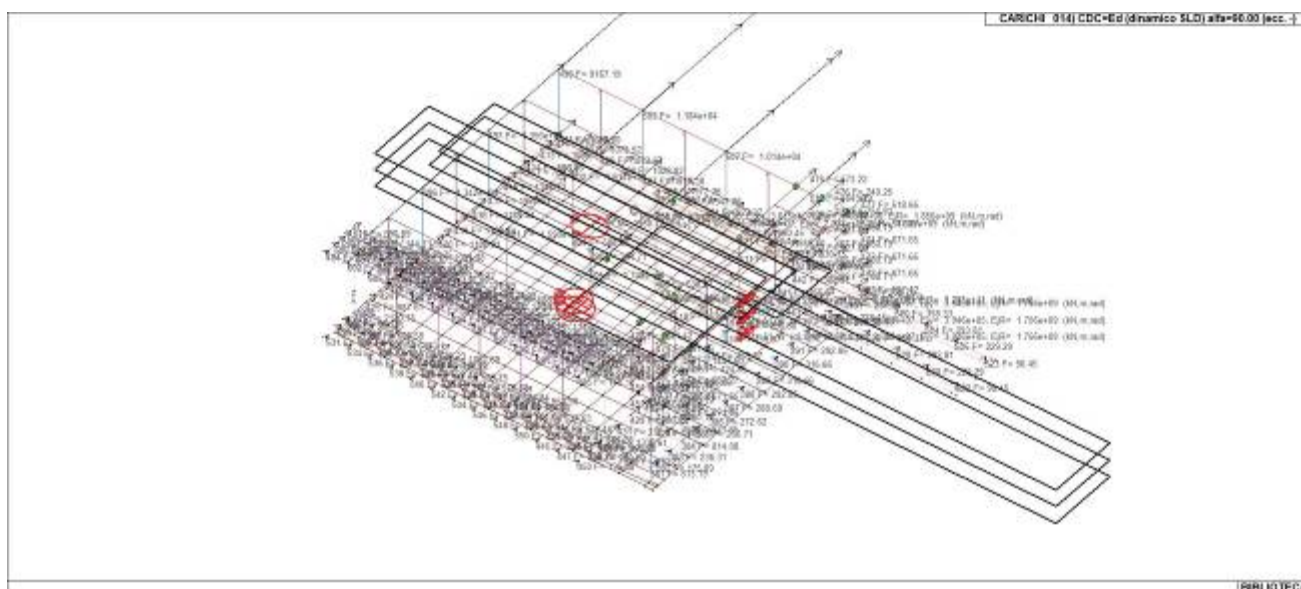
22_CDC_011_CDC=Ed (dinamico SLD) alfa=0.0 (ecc. +)



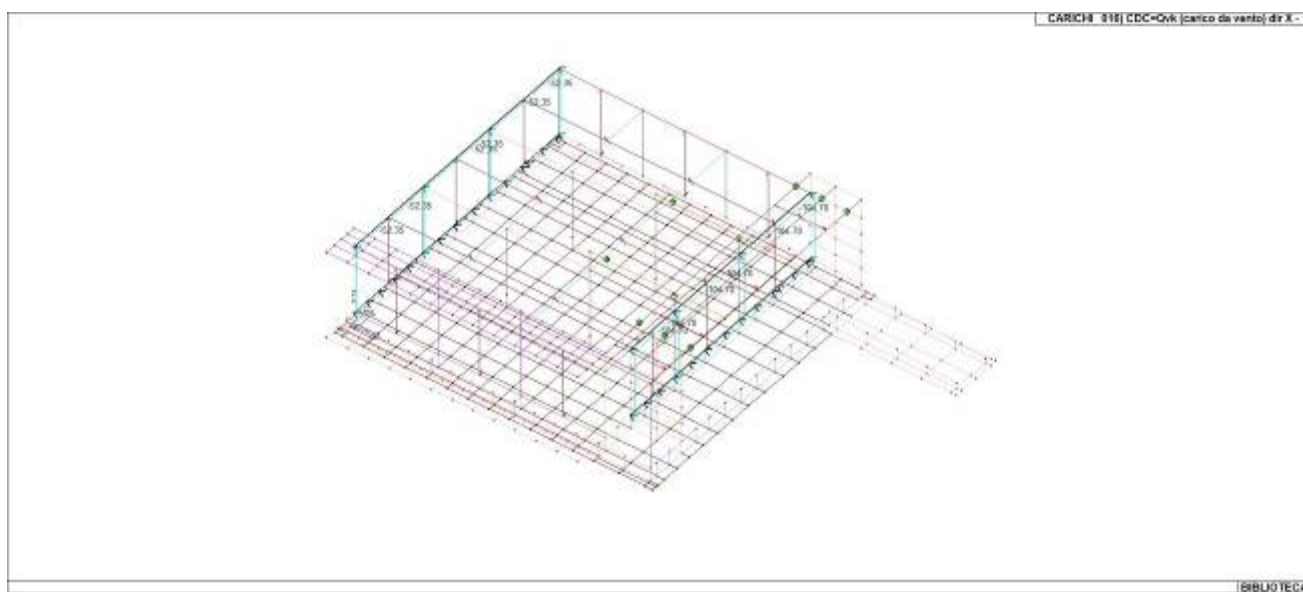
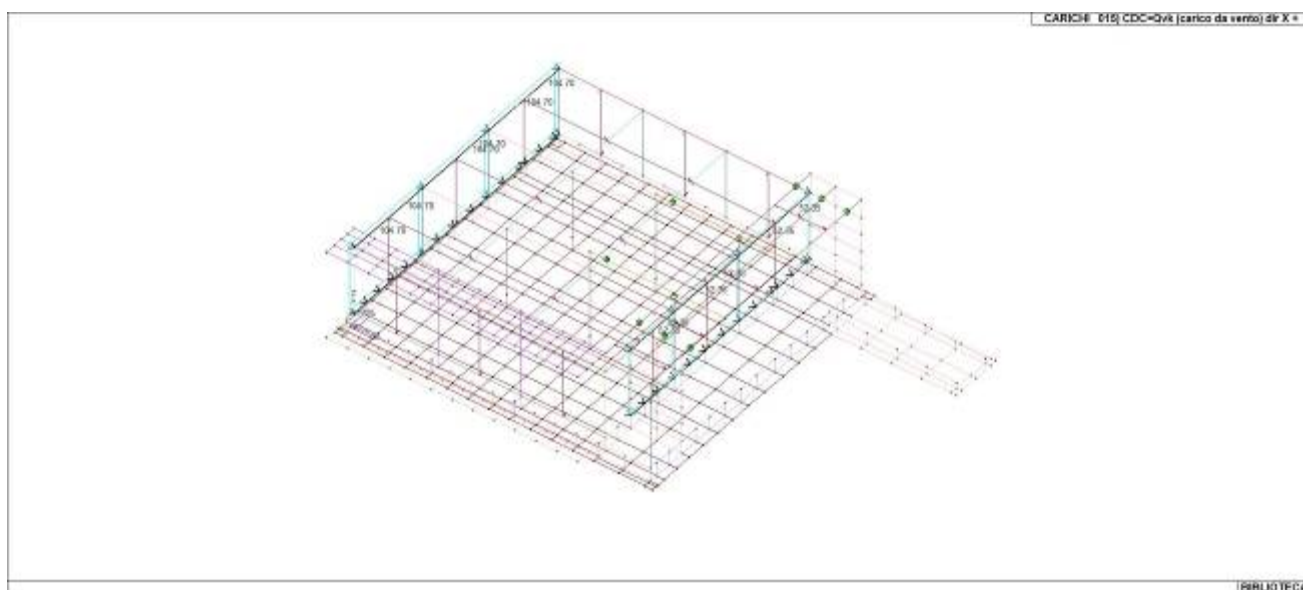
22_CDC_012_CDC=Ed (dinamico SLD) alfa=0.0 (ecc. -)

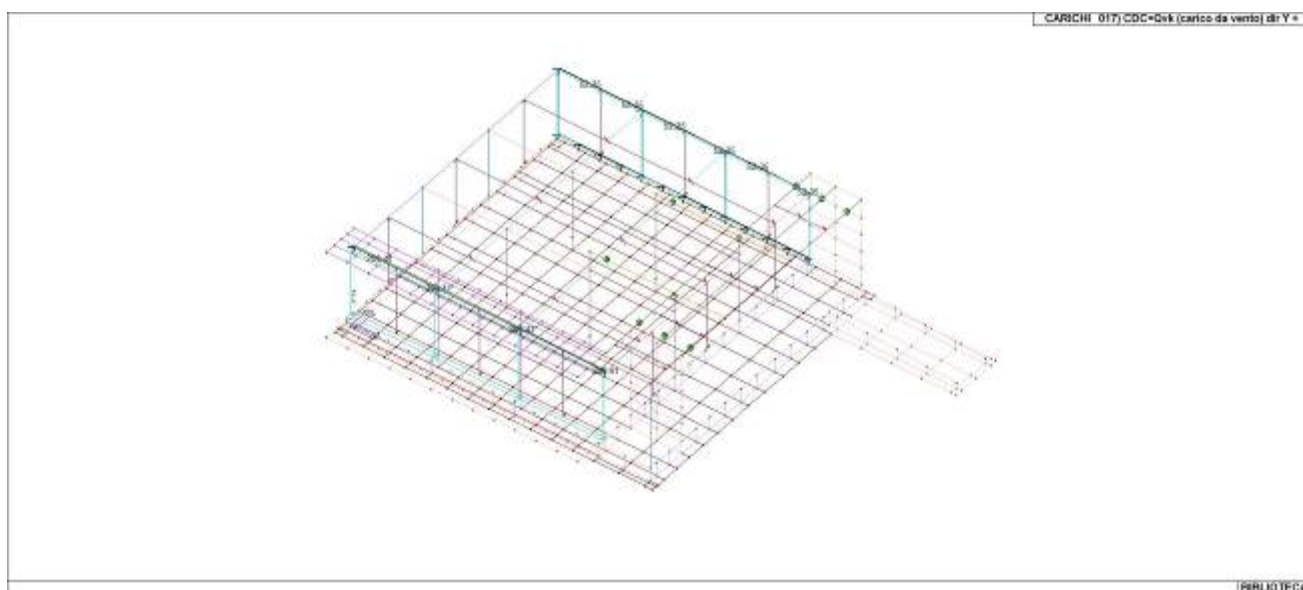


22_CDC_013_CDC=Ed (dinamico SLD) alfa=90.00 (ecc. +)

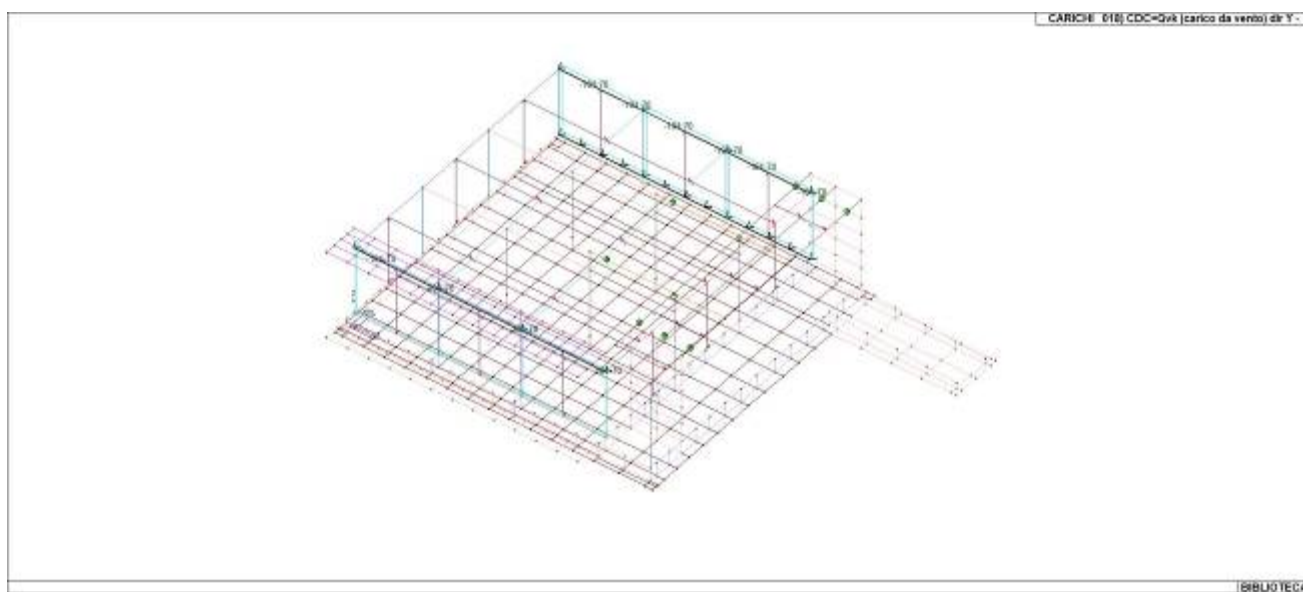


22_CDC_014_CDC=Ed (dinamico SLD) alfa=90.00 (ecc. -)

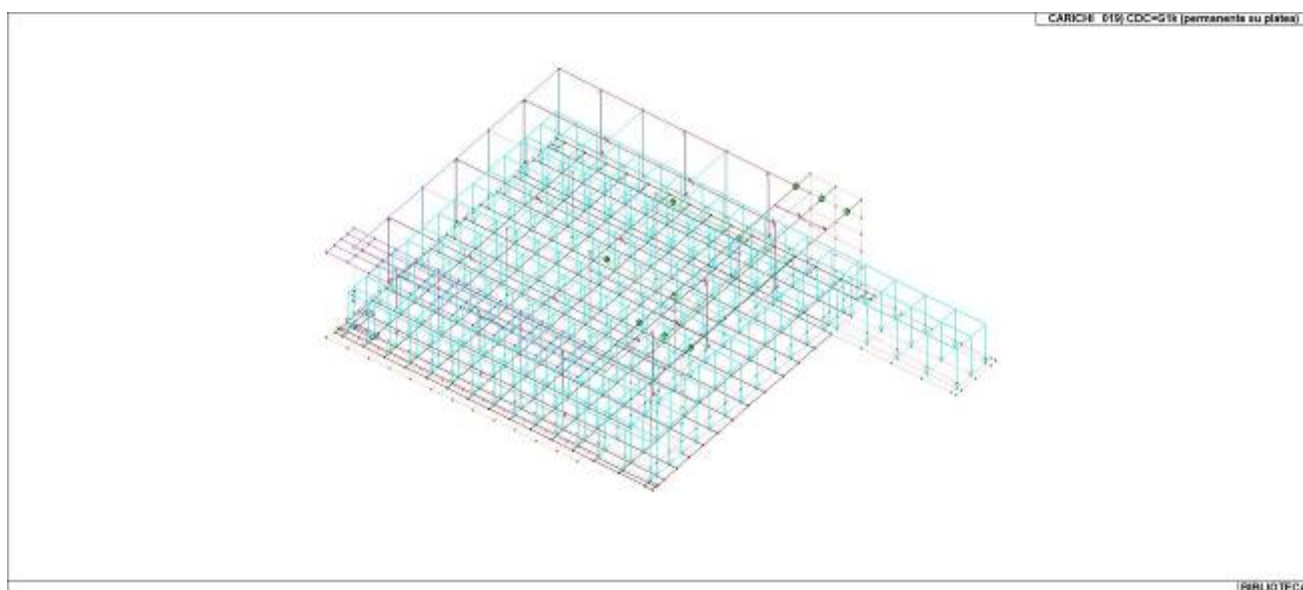




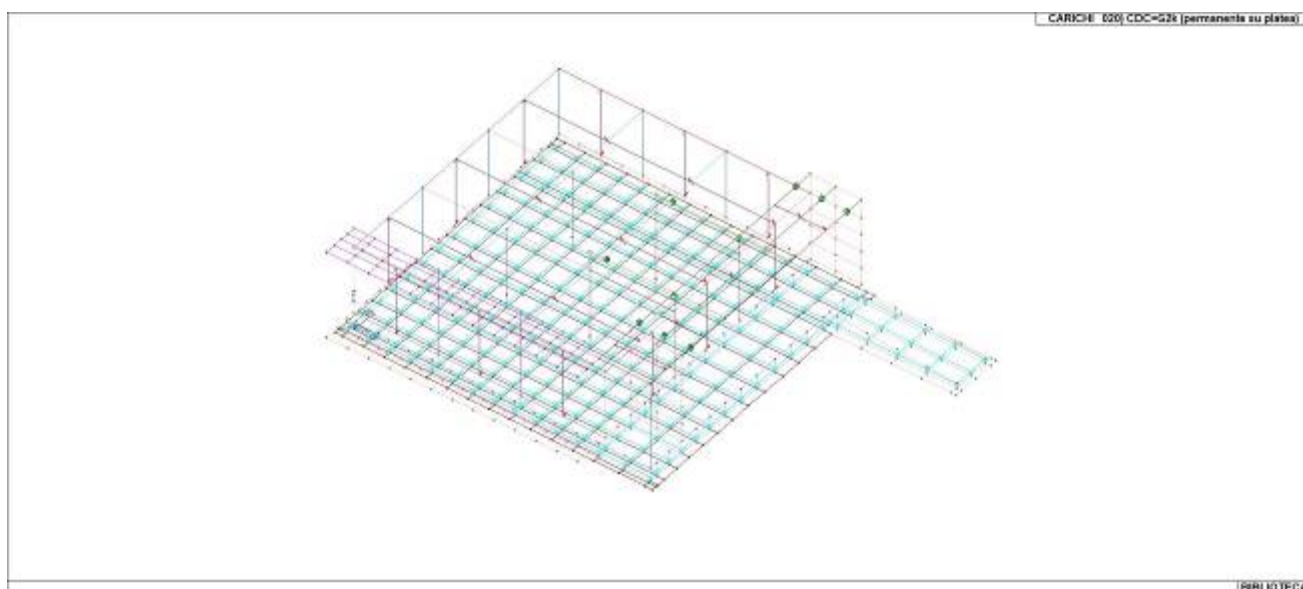
22_CDC_017_CDC=Qvk (carico da vento) dir Y +



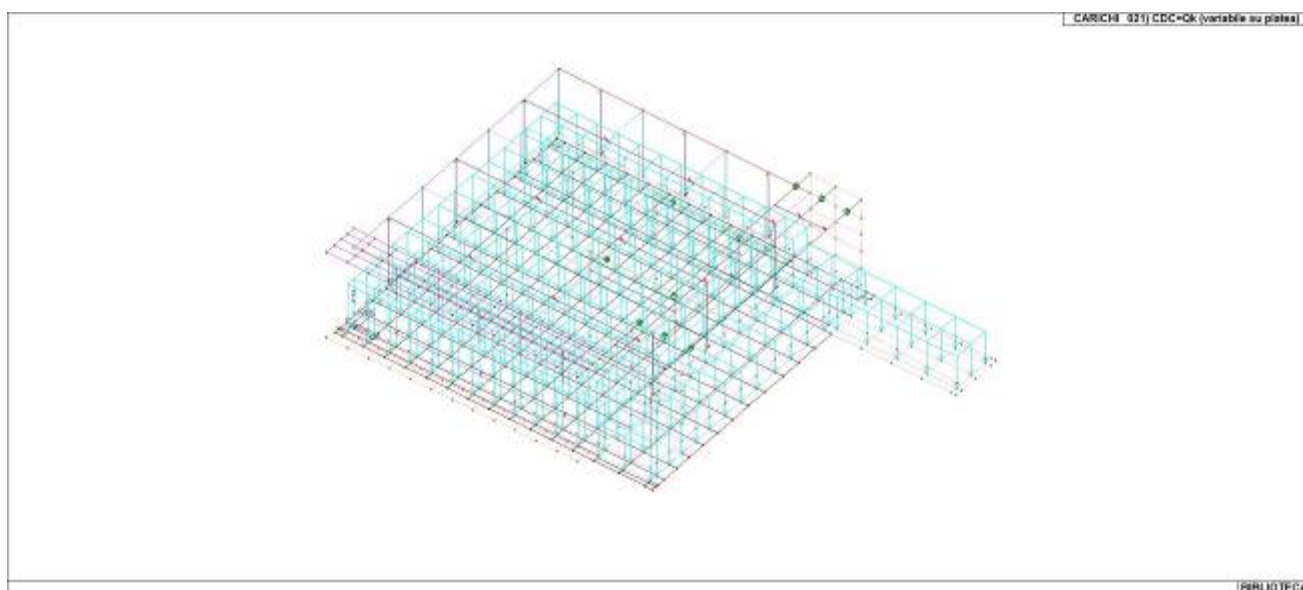
22_CDC_018_CDC=Qvk (carico da vento) dir Y -



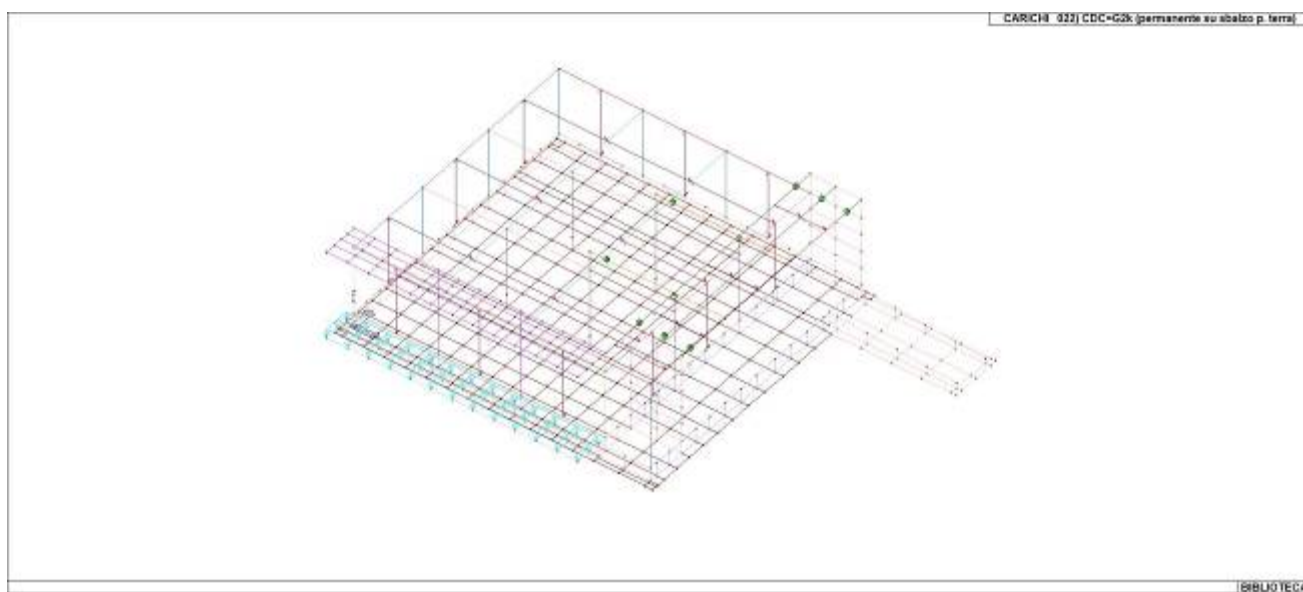
22_CDC_019_CDC=G1k (permanente su platea)



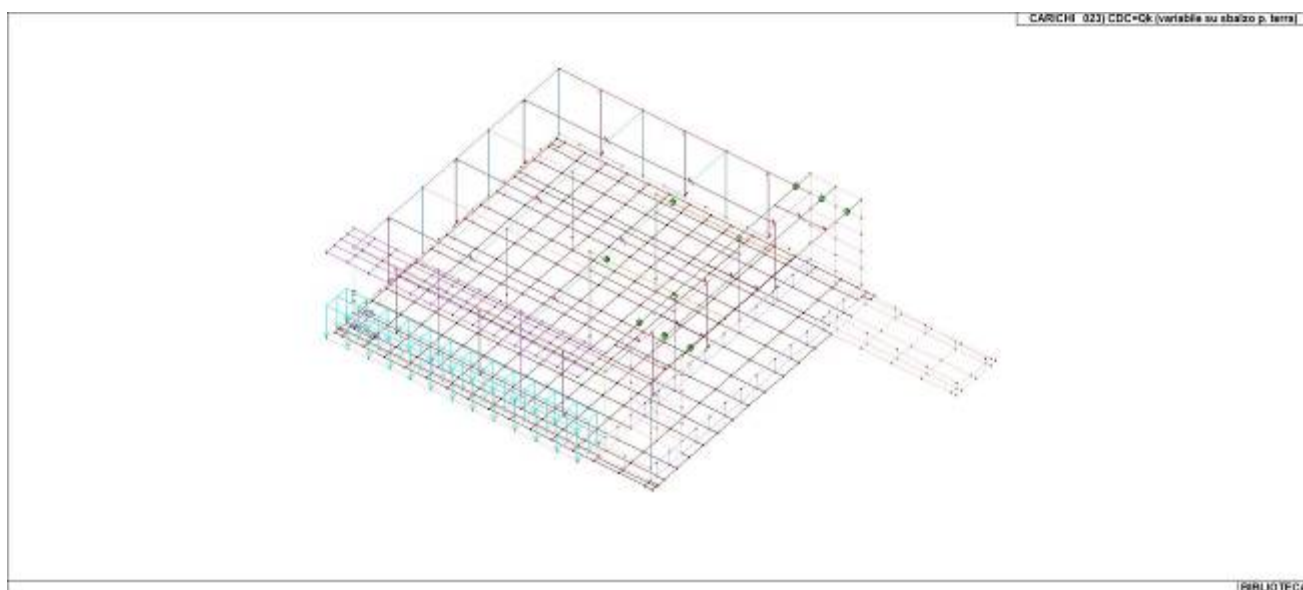
22_CDC_020_CDC=G2k (permanente su platea)



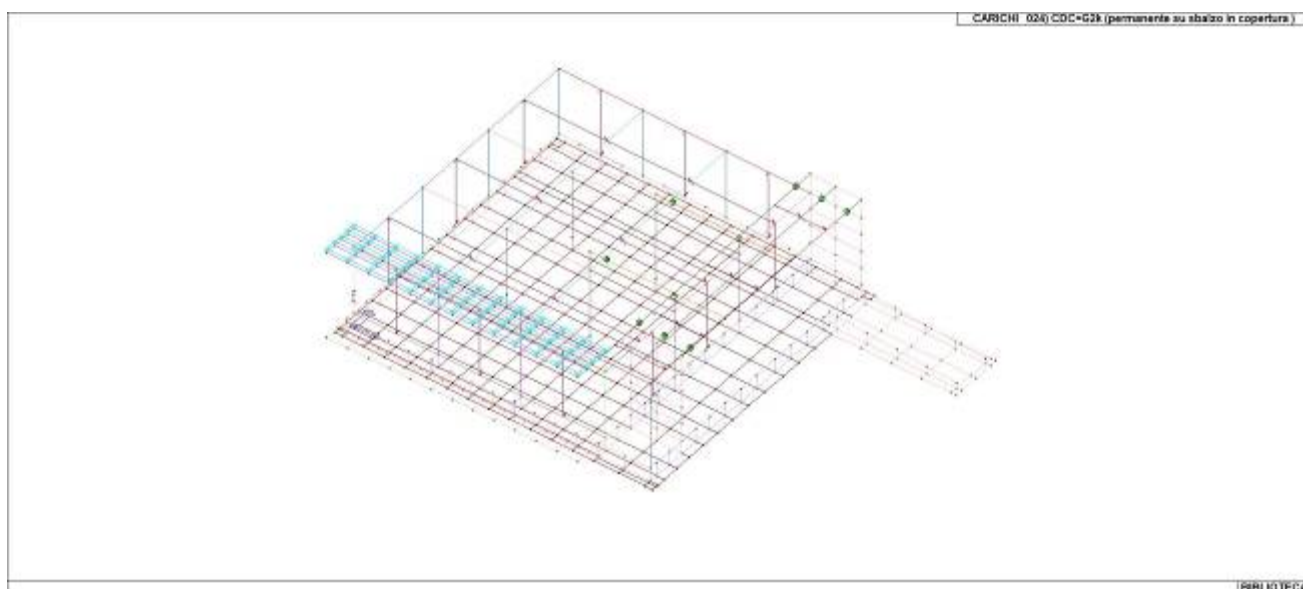
22_CDC_021_CDC=Qk (variabile su platea)



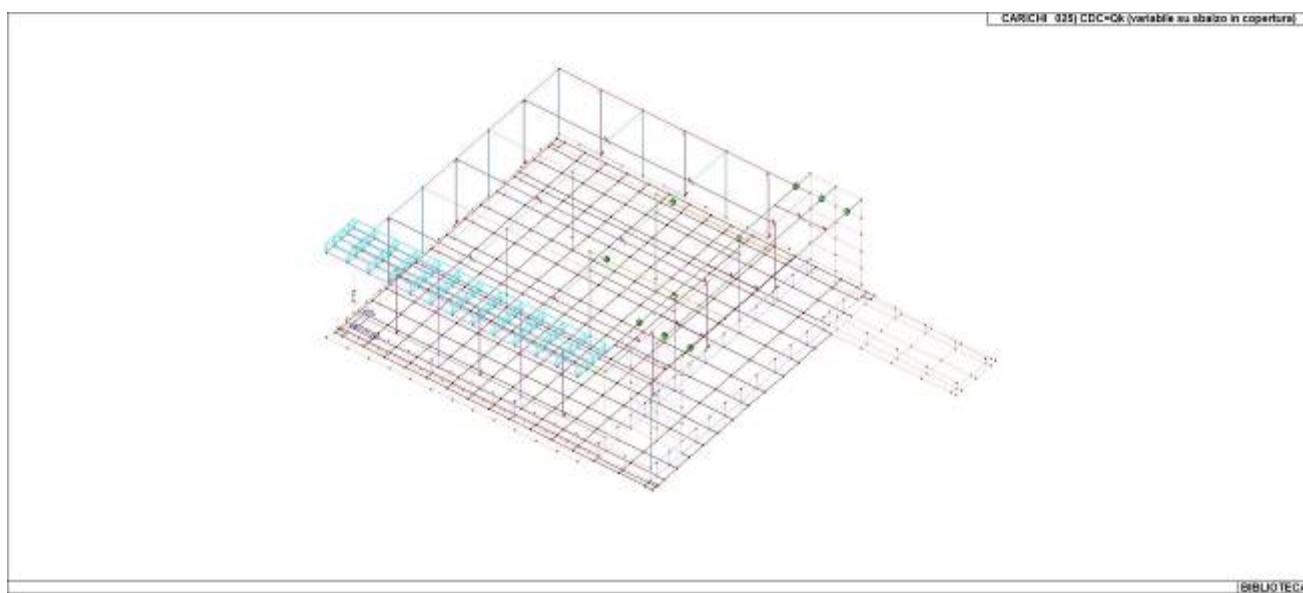
22_CDC_022_CDC=G2k (permanente su sbalzo p. terra)



22_CDC_023_CDC=Qk (variabile su sbalzo p. terra)



22_CDC_024_CDC=G2k (permanente su sbalzo in copertura)



22_CDC_025_CDC=Qk (variabile su sbalzo in copertura)

DEFINIZIONE DELLE COMBINAZIONI

LEGENDA TABELLA COMBINAZIONI DI CARICO

Il programma combina i diversi tipi di casi di carico (CDC) secondo le regole previste dalla normativa vigente.

Le combinazioni previste sono destinate al controllo di sicurezza della struttura ed alla verifica degli spostamenti e delle sollecitazioni.

La prima tabella delle combinazioni riportata di seguito comprende le seguenti informazioni: Numero, Tipo, Sigla identificativa. Una seconda tabella riporta il peso nella combinazione assunto per ogni caso di carico.

Ai fini delle verifiche degli stati limite si definiscono le seguenti combinazioni delle azioni:

Combinazione fondamentale SLU

$$\gamma G1 \cdot G1 + \gamma G2 \cdot G2 + \gamma P \cdot P + \gamma Q1 \cdot Qk1 + \gamma Q2 \cdot \psi 02 \cdot Qk2 + \gamma Q3 \cdot \psi 03 \cdot Qk3 + \dots$$

Combinazione caratteristica (rara) SLE

$$G1 + G2 + P + Qk1 + \psi 02 \cdot Qk2 + \psi 03 \cdot Qk3 + \dots$$

Combinazione frequente SLE

$$G1 + G2 + P + \psi 11 \cdot Qk1 + \psi 22 \cdot Qk2 + \psi 23 \cdot Qk3 + \dots$$

Combinazione quasi permanente SLE

$$G1 + G2 + P + \psi 21 \cdot Qk1 + \psi 22 \cdot Qk2 + \psi 23 \cdot Qk3 + \dots$$

Combinazione sismica, impiegata per gli stati limite ultimi e di esercizio connessi all'azione sismica E

$$E + G1 + G2 + P + \psi 21 \cdot Qk1 + \psi 22 \cdot Qk2 + \dots$$

Combinazione eccezionale, impiegata per gli stati limite connessi alle azioni eccezionali

$$G1 + G2 + Ad + P + \psi 21 \cdot Qk1 + \psi 22 \cdot Qk2 + \dots$$

Dove:

NTC 2018 Tabella 2.5.I

Destinazione d'uso/azione	$\psi 0$	$\psi 1$	$\psi 2$
Categoria A residenziali	0,70	0,50	0,30
Categoria B uffici	0,70	0,50	0,30
Categoria C ambienti suscettibili di affollamento	0,70	0,70	0,60
Categoria D ambienti ad uso commerciale	0,70	0,70	0,60
Categoria E biblioteche, archivi, magazzini,...	1,00	0,90	0,80
Categoria F Rimesse e parcheggi (autoveicoli $\leq 30kN$)	0,70	0,70	0,60
Categoria G Rimesse e parcheggi (autoveicoli $> 30kN$)	0,70	0,50	0,30
Categoria H Coperture	0,00	0,00	0,00
Vento	0,60	0,20	0,00
Neve a quota ≤ 1000 m	0,50	0,20	0,00
Neve a quota > 1000 m	0,70	0,50	0,20
Variazioni Termiche	0,60	0,50	0,00

Nelle verifiche possono essere adottati in alternativa due diversi approcci progettuali:

- per l'approccio 1 si considerano due diverse combinazioni di gruppi di coefficienti di sicurezza parziali per le azioni, per i materiali e per la resistenza globale (combinazione 1 con coefficienti A1 e combinazione 2 con coefficienti A2),
- per l'approccio 2 si definisce un'unica combinazione per le azioni, per la resistenza dei materiali e per la resistenza globale (con coefficienti A1).

NTC 2018 Tabella 2.6.I

		Coefficiente γ_f	EQU	A1	A2
Carichi permanenti	Favorevoli	$\gamma G1$	0,9	1,0	1,0
	Sfavorevoli		1,1	1,3	1,0
Carichi permanenti non strutturali (Non compiutamente definiti)	Favorevoli	$\gamma G2$	0,8	0,8	0,8
	Sfavorevoli		1,5	1,5	1,3
Carichi variabili	Favorevoli	γQi	0,0	0,0	0,0
	Sfavorevoli		1,5	1,5	1,3

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5	SLU	Comb. SLU A1 5
6	SLU	Comb. SLU A1 6
7	SLU	Comb. SLU A1 7

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441	SLU	Comb. SLU A1 441
442	SLU	Comb. SLU A1 442
443	SLU	Comb. SLU A1 443
444	SLU	Comb. SLU A1 444
445	SLU	Comb. SLU A1 445
446	SLU	Comb. SLU A1 446
447	SLU	Comb. SLU A1 447
448	SLU	Comb. SLU A1 448
449	SLU	Comb. SLU A1 449
450	SLU	Comb. SLU A1 450
451	SLU	Comb. SLU A1 451
452	SLU	Comb. SLU A1 452
453	SLU	Comb. SLU A1 453
454	SLU	Comb. SLU A1 454
455	SLU	Comb. SLU A1 455
456	SLU	Comb. SLU A1 456
457	SLU	Comb. SLU A1 457
458	SLU	Comb. SLU A1 458
459	SLU	Comb. SLU A1 459
460	SLU	Comb. SLU A1 460
461	SLU	Comb. SLU A1 461
462	SLU	Comb. SLU A1 462
463	SLU	Comb. SLU A1 463
464	SLU	Comb. SLU A1 464
465	SLU	Comb. SLU A1 465
466	SLU	Comb. SLU A1 466
467	SLU	Comb. SLU A1 467
468	SLU	Comb. SLU A1 468
469	SLU	Comb. SLU A1 469
470	SLU	Comb. SLU A1 470
471	SLU	Comb. SLU A1 471
472	SLU	Comb. SLU A1 472
473	SLU	Comb. SLU A1 473
474	SLU	Comb. SLU A1 474
475	SLU	Comb. SLU A1 475
476	SLU	Comb. SLU A1 476
477	SLU	Comb. SLU A1 477
478	SLU	Comb. SLU A1 478
479	SLU	Comb. SLU A1 479
480	SLU	Comb. SLU A1 480
481	SLU	Comb. SLU A1 481
482	SLU	Comb. SLU A1 482
483	SLU	Comb. SLU A1 483

Cmb	Tipo	Sigla Id
484	SLU	Comb. SLU A1 484
485	SLU	Comb. SLU A1 485
486	SLU	Comb. SLU A1 486
487	SLU	Comb. SLU A1 487
488	SLU	Comb. SLU A1 488
489	SLU	Comb. SLU A1 489
490	SLU	Comb. SLU A1 490
491	SLU	Comb. SLU A1 491
492	SLU	Comb. SLU A1 492
493	SLU	Comb. SLU A1 493
494	SLU	Comb. SLU A1 494
495	SLU	Comb. SLU A1 495
496	SLU	Comb. SLU A1 496
497	SLU	Comb. SLU A1 497
498	SLU	Comb. SLU A1 498
499	SLU	Comb. SLU A1 499
500	SLU	Comb. SLU A1 500
501	SLU	Comb. SLU A1 501
502	SLU	Comb. SLU A1 502
503	SLU	Comb. SLU A1 503
504	SLU	Comb. SLU A1 504
505	SLU	Comb. SLU A1 505
506	SLU	Comb. SLU A1 506
507	SLU	Comb. SLU A1 507
508	SLU	Comb. SLU A1 508
509	SLU	Comb. SLU A1 509
510	SLU	Comb. SLU A1 510
511	SLU	Comb. SLU A1 511
512	SLU	Comb. SLU A1 512
513	SLU	Comb. SLU A1 513
514	SLU	Comb. SLU A1 514
515	SLU	Comb. SLU A1 515
516	SLU	Comb. SLU A1 516
517	SLU	Comb. SLU A1 517
518	SLU	Comb. SLU A1 518
519	SLU	Comb. SLU A1 519
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522	SLU	Comb. SLU A1 522
523	SLU	Comb. SLU A1 523
524	SLU	Comb. SLU A1 524
525	SLU	Comb. SLU A1 525
526	SLU	Comb. SLU A1 526
527	SLU	Comb. SLU A1 527
528	SLU	Comb. SLU A1 528
529	SLU	Comb. SLU A1 (SLV sism.) 529
530	SLU	Comb. SLU A1 (SLV sism.) 530
531	SLU	Comb. SLU A1 (SLV sism.) 531
532	SLU	Comb. SLU A1 (SLV sism.) 532
533	SLU	Comb. SLU A1 (SLV sism.) 533
534	SLU	Comb. SLU A1 (SLV sism.) 534
535	SLU	Comb. SLU A1 (SLV sism.) 535
536	SLU	Comb. SLU A1 (SLV sism.) 536
537	SLU	Comb. SLU A1 (SLV sism.) 537
538	SLU	Comb. SLU A1 (SLV sism.) 538
539	SLU	Comb. SLU A1 (SLV sism.) 539
540	SLU	Comb. SLU A1 (SLV sism.) 540
541	SLU	Comb. SLU A1 (SLV sism.) 541
542	SLU	Comb. SLU A1 (SLV sism.) 542
543	SLU	Comb. SLU A1 (SLV sism.) 543
544	SLU	Comb. SLU A1 (SLV sism.) 544
545	SLU	Comb. SLU A1 (SLV sism.) 545
546	SLU	Comb. SLU A1 (SLV sism.) 546
547	SLU	Comb. SLU A1 (SLV sism.) 547
548	SLU	Comb. SLU A1 (SLV sism.) 548
549	SLU	Comb. SLU A1 (SLV sism.) 549
550	SLU	Comb. SLU A1 (SLV sism.) 550
551	SLU	Comb. SLU A1 (SLV sism.) 551

Cmb	Tipo	Sigla Id
552	SLU	Comb. SLU A1 (SLV sism.) 552
553	SLU	Comb. SLU A1 (SLV sism.) 553
554	SLU	Comb. SLU A1 (SLV sism.) 554
555	SLU	Comb. SLU A1 (SLV sism.) 555
556	SLU	Comb. SLU A1 (SLV sism.) 556
557	SLU	Comb. SLU A1 (SLV sism.) 557
558	SLU	Comb. SLU A1 (SLV sism.) 558
559	SLU	Comb. SLU A1 (SLV sism.) 559
560	SLU	Comb. SLU A1 (SLV sism.) 560
561	SLE(sis)	Comb. SLE (SLD Danno sism.) 561
562	SLE(sis)	Comb. SLE (SLD Danno sism.) 562
563	SLE(sis)	Comb. SLE (SLD Danno sism.) 563
564	SLE(sis)	Comb. SLE (SLD Danno sism.) 564
565	SLE(sis)	Comb. SLE (SLD Danno sism.) 565
566	SLE(sis)	Comb. SLE (SLD Danno sism.) 566
567	SLE(sis)	Comb. SLE (SLD Danno sism.) 567
568	SLE(sis)	Comb. SLE (SLD Danno sism.) 568
569	SLE(sis)	Comb. SLE (SLD Danno sism.) 569
570	SLE(sis)	Comb. SLE (SLD Danno sism.) 570
571	SLE(sis)	Comb. SLE (SLD Danno sism.) 571
572	SLE(sis)	Comb. SLE (SLD Danno sism.) 572
573	SLE(sis)	Comb. SLE (SLD Danno sism.) 573
574	SLE(sis)	Comb. SLE (SLD Danno sism.) 574
575	SLE(sis)	Comb. SLE (SLD Danno sism.) 575
576	SLE(sis)	Comb. SLE (SLD Danno sism.) 576
577	SLE(sis)	Comb. SLE (SLD Danno sism.) 577
578	SLE(sis)	Comb. SLE (SLD Danno sism.) 578
579	SLE(sis)	Comb. SLE (SLD Danno sism.) 579
580	SLE(sis)	Comb. SLE (SLD Danno sism.) 580
581	SLE(sis)	Comb. SLE (SLD Danno sism.) 581
582	SLE(sis)	Comb. SLE (SLD Danno sism.) 582
583	SLE(sis)	Comb. SLE (SLD Danno sism.) 583
584	SLE(sis)	Comb. SLE (SLD Danno sism.) 584
585	SLE(sis)	Comb. SLE (SLD Danno sism.) 585
586	SLE(sis)	Comb. SLE (SLD Danno sism.) 586
587	SLE(sis)	Comb. SLE (SLD Danno sism.) 587
588	SLE(sis)	Comb. SLE (SLD Danno sism.) 588
589	SLE(sis)	Comb. SLE (SLD Danno sism.) 589
590	SLE(sis)	Comb. SLE (SLD Danno sism.) 590
591	SLE(sis)	Comb. SLE (SLD Danno sism.) 591
592	SLE(sis)	Comb. SLE (SLD Danno sism.) 592
593	SLE(r)	Comb. SLE(rara) 593
594	SLE(r)	Comb. SLE(rara) 594
595	SLE(r)	Comb. SLE(rara) 595
596	SLE(r)	Comb. SLE(rara) 596
597	SLE(r)	Comb. SLE(rara) 597
598	SLE(r)	Comb. SLE(rara) 598
599	SLE(r)	Comb. SLE(rara) 599
600	SLE(r)	Comb. SLE(rara) 600
601	SLE(r)	Comb. SLE(rara) 601
602	SLE(r)	Comb. SLE(rara) 602
603	SLE(r)	Comb. SLE(rara) 603
604	SLE(r)	Comb. SLE(rara) 604
605	SLE(r)	Comb. SLE(rara) 605
606	SLE(r)	Comb. SLE(rara) 606
607	SLE(r)	Comb. SLE(rara) 607
608	SLE(r)	Comb. SLE(rara) 608
609	SLE(r)	Comb. SLE(rara) 609
610	SLE(r)	Comb. SLE(rara) 610
611	SLE(r)	Comb. SLE(rara) 611
612	SLE(r)	Comb. SLE(rara) 612
613	SLE(r)	Comb. SLE(rara) 613
614	SLE(r)	Comb. SLE(rara) 614
615	SLE(r)	Comb. SLE(rara) 615
616	SLE(r)	Comb. SLE(rara) 616
617	SLE(r)	Comb. SLE(rara) 617
618	SLE(r)	Comb. SLE(rara) 618
619	SLE(r)	Comb. SLE(rara) 619

Cmb	Tipo	Sigla Id
620	SLE(r)	Comb. SLE(rara) 620
621	SLE(r)	Comb. SLE(rara) 621
622	SLE(r)	Comb. SLE(rara) 622
623	SLE(r)	Comb. SLE(rara) 623
624	SLE(r)	Comb. SLE(rara) 624
625	SLE(r)	Comb. SLE(rara) 625
626	SLE(r)	Comb. SLE(rara) 626
627	SLE(r)	Comb. SLE(rara) 627
628	SLE(r)	Comb. SLE(rara) 628
629	SLE(r)	Comb. SLE(rara) 629
630	SLE(r)	Comb. SLE(rara) 630
631	SLE(r)	Comb. SLE(rara) 631
632	SLE(r)	Comb. SLE(rara) 632
633	SLE(r)	Comb. SLE(rara) 633
634	SLE(r)	Comb. SLE(rara) 634
635	SLE(r)	Comb. SLE(rara) 635
636	SLE(r)	Comb. SLE(rara) 636
637	SLE(r)	Comb. SLE(rara) 637
638	SLE(r)	Comb. SLE(rara) 638
639	SLE(r)	Comb. SLE(rara) 639
640	SLE(r)	Comb. SLE(rara) 640
641	SLE(r)	Comb. SLE(rara) 641
642	SLE(r)	Comb. SLE(rara) 642
643	SLE(r)	Comb. SLE(rara) 643
644	SLE(r)	Comb. SLE(rara) 644
645	SLE(r)	Comb. SLE(rara) 645
646	SLE(r)	Comb. SLE(rara) 646
647	SLE(r)	Comb. SLE(rara) 647
648	SLE(r)	Comb. SLE(rara) 648
649	SLE(r)	Comb. SLE(rara) 649
650	SLE(r)	Comb. SLE(rara) 650
651	SLE(r)	Comb. SLE(rara) 651
652	SLE(r)	Comb. SLE(rara) 652
653	SLE(r)	Comb. SLE(rara) 653
654	SLE(r)	Comb. SLE(rara) 654
655	SLE(r)	Comb. SLE(rara) 655
656	SLE(r)	Comb. SLE(rara) 656
657	SLE(r)	Comb. SLE(rara) 657
658	SLE(r)	Comb. SLE(rara) 658
659	SLE(r)	Comb. SLE(rara) 659
660	SLE(r)	Comb. SLE(rara) 660
661	SLE(r)	Comb. SLE(rara) 661
662	SLE(r)	Comb. SLE(rara) 662
663	SLE(r)	Comb. SLE(rara) 663
664	SLE(r)	Comb. SLE(rara) 664
665	SLE(r)	Comb. SLE(rara) 665
666	SLE(r)	Comb. SLE(rara) 666
667	SLE(r)	Comb. SLE(rara) 667
668	SLE(r)	Comb. SLE(rara) 668
669	SLE(r)	Comb. SLE(rara) 669
670	SLE(r)	Comb. SLE(rara) 670
671	SLE(r)	Comb. SLE(rara) 671
672	SLE(r)	Comb. SLE(rara) 672
673	SLE(r)	Comb. SLE(rara) 673
674	SLE(r)	Comb. SLE(rara) 674
675	SLE(r)	Comb. SLE(rara) 675
676	SLE(r)	Comb. SLE(rara) 676
677	SLE(r)	Comb. SLE(rara) 677
678	SLE(r)	Comb. SLE(rara) 678
679	SLE(r)	Comb. SLE(rara) 679
680	SLE(r)	Comb. SLE(rara) 680
681	SLE(r)	Comb. SLE(rara) 681
682	SLE(r)	Comb. SLE(rara) 682
683	SLE(r)	Comb. SLE(rara) 683
684	SLE(r)	Comb. SLE(rara) 684
685	SLE(r)	Comb. SLE(rara) 685
686	SLE(r)	Comb. SLE(rara) 686
687	SLE(r)	Comb. SLE(rara) 687

Cmb	Tipo	Sigla Id
688	SLE(r)	Comb. SLE(rara) 688
689	SLE(r)	Comb. SLE(rara) 689
690	SLE(r)	Comb. SLE(rara) 690
691	SLE(r)	Comb. SLE(rara) 691
692	SLE(r)	Comb. SLE(rara) 692
693	SLE(r)	Comb. SLE(rara) 693
694	SLE(r)	Comb. SLE(rara) 694
695	SLE(r)	Comb. SLE(rara) 695
696	SLE(r)	Comb. SLE(rara) 696
697	SLE(r)	Comb. SLE(rara) 697
698	SLE(r)	Comb. SLE(rara) 698
699	SLE(r)	Comb. SLE(rara) 699
700	SLE(r)	Comb. SLE(rara) 700
701	SLE(r)	Comb. SLE(rara) 701
702	SLE(r)	Comb. SLE(rara) 702
703	SLE(r)	Comb. SLE(rara) 703
704	SLE(r)	Comb. SLE(rara) 704
705	SLE(r)	Comb. SLE(rara) 705
706	SLE(r)	Comb. SLE(rara) 706
707	SLE(r)	Comb. SLE(rara) 707
708	SLE(r)	Comb. SLE(rara) 708
709	SLE(r)	Comb. SLE(rara) 709
710	SLE(r)	Comb. SLE(rara) 710
711	SLE(r)	Comb. SLE(rara) 711
712	SLE(r)	Comb. SLE(rara) 712
713	SLE(r)	Comb. SLE(rara) 713
714	SLE(r)	Comb. SLE(rara) 714
715	SLE(r)	Comb. SLE(rara) 715
716	SLE(r)	Comb. SLE(rara) 716
717	SLE(r)	Comb. SLE(rara) 717
718	SLE(r)	Comb. SLE(rara) 718
719	SLE(r)	Comb. SLE(rara) 719
720	SLE(r)	Comb. SLE(rara) 720
721	SLE(r)	Comb. SLE(rara) 721
722	SLE(r)	Comb. SLE(rara) 722
723	SLE(r)	Comb. SLE(rara) 723
724	SLE(r)	Comb. SLE(rara) 724
725	SLE(r)	Comb. SLE(rara) 725
726	SLE(r)	Comb. SLE(rara) 726
727	SLE(r)	Comb. SLE(rara) 727
728	SLE(r)	Comb. SLE(rara) 728
729	SLE(r)	Comb. SLE(rara) 729
730	SLE(r)	Comb. SLE(rara) 730
731	SLE(r)	Comb. SLE(rara) 731
732	SLE(r)	Comb. SLE(rara) 732
733	SLE(r)	Comb. SLE(rara) 733
734	SLE(r)	Comb. SLE(rara) 734
735	SLE(r)	Comb. SLE(rara) 735
736	SLE(r)	Comb. SLE(rara) 736
737	SLE(r)	Comb. SLE(rara) 737
738	SLE(r)	Comb. SLE(rara) 738
739	SLE(r)	Comb. SLE(rara) 739
740	SLE(r)	Comb. SLE(rara) 740
741	SLE(r)	Comb. SLE(rara) 741
742	SLE(r)	Comb. SLE(rara) 742
743	SLE(r)	Comb. SLE(rara) 743
744	SLE(r)	Comb. SLE(rara) 744
745	SLE(r)	Comb. SLE(rara) 745
746	SLE(r)	Comb. SLE(rara) 746
747	SLE(r)	Comb. SLE(rara) 747
748	SLE(r)	Comb. SLE(rara) 748
749	SLE(r)	Comb. SLE(rara) 749
750	SLE(r)	Comb. SLE(rara) 750
751	SLE(r)	Comb. SLE(rara) 751
752	SLE(r)	Comb. SLE(rara) 752
753	SLE(r)	Comb. SLE(rara) 753
754	SLE(r)	Comb. SLE(rara) 754
755	SLE(r)	Comb. SLE(rara) 755

Cmb	Tipo	Sigla Id
756	SLE(r)	Comb. SLE(rara) 756
757	SLE(r)	Comb. SLE(rara) 757
758	SLE(r)	Comb. SLE(rara) 758
759	SLE(r)	Comb. SLE(rara) 759
760	SLE(r)	Comb. SLE(rara) 760
761	SLE(r)	Comb. SLE(rara) 761
762	SLE(r)	Comb. SLE(rara) 762
763	SLE(r)	Comb. SLE(rara) 763
764	SLE(r)	Comb. SLE(rara) 764
765	SLE(r)	Comb. SLE(rara) 765
766	SLE(r)	Comb. SLE(rara) 766
767	SLE(r)	Comb. SLE(rara) 767
768	SLE(r)	Comb. SLE(rara) 768
769	SLE(r)	Comb. SLE(rara) 769
770	SLE(r)	Comb. SLE(rara) 770
771	SLE(r)	Comb. SLE(rara) 771
772	SLE(r)	Comb. SLE(rara) 772
773	SLE(r)	Comb. SLE(rara) 773
774	SLE(r)	Comb. SLE(rara) 774
775	SLE(r)	Comb. SLE(rara) 775
776	SLE(r)	Comb. SLE(rara) 776
777	SLE(r)	Comb. SLE(rara) 777
778	SLE(r)	Comb. SLE(rara) 778
779	SLE(r)	Comb. SLE(rara) 779
780	SLE(r)	Comb. SLE(rara) 780
781	SLE(r)	Comb. SLE(rara) 781
782	SLE(r)	Comb. SLE(rara) 782
783	SLE(r)	Comb. SLE(rara) 783
784	SLE(r)	Comb. SLE(rara) 784
785	SLE(r)	Comb. SLE(rara) 785
786	SLE(r)	Comb. SLE(rara) 786
787	SLE(r)	Comb. SLE(rara) 787
788	SLE(r)	Comb. SLE(rara) 788
789	SLE(r)	Comb. SLE(rara) 789
790	SLE(r)	Comb. SLE(rara) 790
791	SLE(r)	Comb. SLE(rara) 791
792	SLE(r)	Comb. SLE(rara) 792
793	SLE(r)	Comb. SLE(rara) 793
794	SLE(r)	Comb. SLE(rara) 794
795	SLE(r)	Comb. SLE(rara) 795
796	SLE(r)	Comb. SLE(rara) 796
797	SLE(r)	Comb. SLE(rara) 797
798	SLE(r)	Comb. SLE(rara) 798
799	SLE(r)	Comb. SLE(rara) 799
800	SLE(r)	Comb. SLE(rara) 800
801	SLE(r)	Comb. SLE(rara) 801
802	SLE(r)	Comb. SLE(rara) 802
803	SLE(r)	Comb. SLE(rara) 803
804	SLE(r)	Comb. SLE(rara) 804
805	SLE(r)	Comb. SLE(rara) 805
806	SLE(r)	Comb. SLE(rara) 806
807	SLE(r)	Comb. SLE(rara) 807
808	SLE(r)	Comb. SLE(rara) 808
809	SLE(r)	Comb. SLE(rara) 809
810	SLE(r)	Comb. SLE(rara) 810
811	SLE(r)	Comb. SLE(rara) 811
812	SLE(r)	Comb. SLE(rara) 812
813	SLE(r)	Comb. SLE(rara) 813
814	SLE(r)	Comb. SLE(rara) 814
815	SLE(r)	Comb. SLE(rara) 815
816	SLE(r)	Comb. SLE(rara) 816
817	SLE(r)	Comb. SLE(rara) 817
818	SLE(r)	Comb. SLE(rara) 818
819	SLE(r)	Comb. SLE(rara) 819
820	SLE(r)	Comb. SLE(rara) 820
821	SLE(r)	Comb. SLE(rara) 821
822	SLE(r)	Comb. SLE(rara) 822
823	SLE(r)	Comb. SLE(rara) 823

Cmb	Tipo	Sigla Id
824	SLE(r)	Comb. SLE(rara) 824
825	SLE(r)	Comb. SLE(rara) 825
826	SLE(r)	Comb. SLE(rara) 826
827	SLE(r)	Comb. SLE(rara) 827
828	SLE(r)	Comb. SLE(rara) 828
829	SLE(r)	Comb. SLE(rara) 829
830	SLE(r)	Comb. SLE(rara) 830
831	SLE(r)	Comb. SLE(rara) 831
832	SLE(r)	Comb. SLE(rara) 832
833	SLE(r)	Comb. SLE(rara) 833
834	SLE(r)	Comb. SLE(rara) 834
835	SLE(r)	Comb. SLE(rara) 835
836	SLE(r)	Comb. SLE(rara) 836
837	SLE(r)	Comb. SLE(rara) 837
838	SLE(r)	Comb. SLE(rara) 838
839	SLE(r)	Comb. SLE(rara) 839
840	SLE(r)	Comb. SLE(rara) 840
841	SLE(r)	Comb. SLE(rara) 841
842	SLE(r)	Comb. SLE(rara) 842
843	SLE(r)	Comb. SLE(rara) 843
844	SLE(r)	Comb. SLE(rara) 844
845	SLE(r)	Comb. SLE(rara) 845
846	SLE(r)	Comb. SLE(rara) 846
847	SLE(r)	Comb. SLE(rara) 847
848	SLE(r)	Comb. SLE(rara) 848
849	SLE(r)	Comb. SLE(rara) 849
850	SLE(r)	Comb. SLE(rara) 850
851	SLE(r)	Comb. SLE(rara) 851
852	SLE(r)	Comb. SLE(rara) 852
853	SLE(r)	Comb. SLE(rara) 853
854	SLE(r)	Comb. SLE(rara) 854
855	SLE(r)	Comb. SLE(rara) 855
856	SLE(r)	Comb. SLE(rara) 856
857	SLE(f)	Comb. SLE(freq.) 857
858	SLE(f)	Comb. SLE(freq.) 858
859	SLE(f)	Comb. SLE(freq.) 859
860	SLE(f)	Comb. SLE(freq.) 860
861	SLE(f)	Comb. SLE(freq.) 861
862	SLE(f)	Comb. SLE(freq.) 862
863	SLE(f)	Comb. SLE(freq.) 863
864	SLE(f)	Comb. SLE(freq.) 864
865	SLE(f)	Comb. SLE(freq.) 865
866	SLE(f)	Comb. SLE(freq.) 866
867	SLE(f)	Comb. SLE(freq.) 867
868	SLE(f)	Comb. SLE(freq.) 868
869	SLE(f)	Comb. SLE(freq.) 869
870	SLE(f)	Comb. SLE(freq.) 870
871	SLE(f)	Comb. SLE(freq.) 871
872	SLE(f)	Comb. SLE(freq.) 872
873	SLE(f)	Comb. SLE(freq.) 873
874	SLE(f)	Comb. SLE(freq.) 874
875	SLE(f)	Comb. SLE(freq.) 875
876	SLE(f)	Comb. SLE(freq.) 876
877	SLE(f)	Comb. SLE(freq.) 877
878	SLE(f)	Comb. SLE(freq.) 878
879	SLE(f)	Comb. SLE(freq.) 879
880	SLE(f)	Comb. SLE(freq.) 880
881	SLE(f)	Comb. SLE(freq.) 881
882	SLE(f)	Comb. SLE(freq.) 882
883	SLE(f)	Comb. SLE(freq.) 883
884	SLE(f)	Comb. SLE(freq.) 884
885	SLE(f)	Comb. SLE(freq.) 885
886	SLE(f)	Comb. SLE(freq.) 886
887	SLE(f)	Comb. SLE(freq.) 887
888	SLE(f)	Comb. SLE(freq.) 888
889	SLE(f)	Comb. SLE(freq.) 889
890	SLE(f)	Comb. SLE(freq.) 890
891	SLE(f)	Comb. SLE(freq.) 891

Cmb	Tipo	Sigla Id
892	SLE(f)	Comb. SLE(freq.) 892
893	SLE(f)	Comb. SLE(freq.) 893
894	SLE(f)	Comb. SLE(freq.) 894
895	SLE(f)	Comb. SLE(freq.) 895
896	SLE(f)	Comb. SLE(freq.) 896
897	SLE(f)	Comb. SLE(freq.) 897
898	SLE(f)	Comb. SLE(freq.) 898
899	SLE(f)	Comb. SLE(freq.) 899
900	SLE(f)	Comb. SLE(freq.) 900
901	SLE(f)	Comb. SLE(freq.) 901
902	SLE(f)	Comb. SLE(freq.) 902
903	SLE(f)	Comb. SLE(freq.) 903
904	SLE(f)	Comb. SLE(freq.) 904
905	SLE(f)	Comb. SLE(freq.) 905
906	SLE(f)	Comb. SLE(freq.) 906
907	SLE(f)	Comb. SLE(freq.) 907
908	SLE(f)	Comb. SLE(freq.) 908
909	SLE(f)	Comb. SLE(freq.) 909
910	SLE(f)	Comb. SLE(freq.) 910
911	SLE(f)	Comb. SLE(freq.) 911
912	SLE(f)	Comb. SLE(freq.) 912
913	SLE(f)	Comb. SLE(freq.) 913
914	SLE(f)	Comb. SLE(freq.) 914
915	SLE(f)	Comb. SLE(freq.) 915
916	SLE(f)	Comb. SLE(freq.) 916
917	SLE(p)	Comb. SLE(perm.) 917
918	SLE(p)	Comb. SLE(perm.) 918
919	SLE(p)	Comb. SLE(perm.) 919
920	SLE(p)	Comb. SLE(perm.) 920
921	SLE(p)	Comb. SLE(perm.) 921
922	SLE(p)	Comb. SLE(perm.) 922
923	SLE(p)	Comb. SLE(perm.) 923
924	SLE(p)	Comb. SLE(perm.) 924

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
1	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
2	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
3	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
4	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
5	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
6	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
7	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
8	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
9	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
10	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
11	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
12	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
13	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
14	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
15	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
16	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
17	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
18	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
19	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
20	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
21	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
22	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
23	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
24	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
25	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
26	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
27	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
28	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
29	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
30	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
31	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
32	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
33	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
34	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
35	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
36	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
37	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
38	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
39	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
40	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
41	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
42	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
43	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
44	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
45	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
46	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
47	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
48	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
49	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
50	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
51	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
52	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
53	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
54	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
55	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
56	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
57	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
58	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
59	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
60	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
61	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
62	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
63	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
64	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
65	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
66	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
67	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
68	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
69	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
70	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
71	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
72	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
73	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
74	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
75	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
76	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
77	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
78	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
79	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
80	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
81	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
82	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
83	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
84	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
85	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
86	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
87	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
88	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
89	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
90	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
91	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
92	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
93	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
94	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
95	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
96	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
97	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
98	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
99	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
100	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
101	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
102	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
103	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
104	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
105	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
106	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
107	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
108	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
109	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
110	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
111	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
112	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
113	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
114	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
115	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
116	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
117	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
118	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
119	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
120	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
121	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
122	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
123	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
124	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
125	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
126	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
127	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
128	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
129	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
130	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
131	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
132	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
133	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
134	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
135	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
136	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
137	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
138	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
139	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
140	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
141	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
142	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
143	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
144	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
145	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
146	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
147	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
148	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
149	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.90	0.0	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
150	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
184	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.50	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
185	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.50	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
186	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.50	0.0	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
187	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.50	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
188	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.50	0.0	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
189	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.50	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
190	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.50	0.0	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
191	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.50	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
192	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.50	0.0	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
193	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
194	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
195	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
196	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
197	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
198	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
199	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
200	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
201	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
202	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
203	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
204	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
205	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
206	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
207	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
208	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
209	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
210	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
211	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
212	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
213	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
214	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
215	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
216	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
217	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

[illegible]

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
251	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
252	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
253	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
254	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
255	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
256	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
257	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
258	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
259	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
260	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
261	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
262	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
263	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
264	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
265	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
266	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
267	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
268	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
269	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
270	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
271	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
272	1.00	1.00	0.80	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.90	0.0	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
273	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.50	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
274	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.50	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
275	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.50	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
276	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.50	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
277	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.50	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
278	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.50	0.0	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
279	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.50	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
280	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.50	0.0	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
281	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.50	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
282	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.50	0.0	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
283	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.50	0.0	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
284	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

[illegible]

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
318	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
319	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
320	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
321	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
322	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
323	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
324	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
325	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
326	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
327	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
328	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
329	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
330	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
331	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
332	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
333	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
334	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
335	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
336	1.30	1.30	1.50	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
337	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
338	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
339	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
340	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
341	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
342	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
343	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
344	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
345	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
346	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
347	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
348	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
349	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
350	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.90	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
351	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

[illegible]

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
385	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
386	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
387	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
388	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
389	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
390	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
391	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
392	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
393	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
394	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
395	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
396	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
397	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	1.50	1.50	0.0	1.50	0.0			
398	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	1.50	1.50	0.0	1.50	1.50			
399	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	1.50	1.50	1.50	1.50	0.0			
400	1.30	1.30	1.50	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.30	1.50	1.50	1.50	1.50	1.50	1.50			
401	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
402	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
403	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
404	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
405	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
406	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
407	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
408	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
409	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
410	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
411	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
412	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
413	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
414	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
415	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
416	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.50	0.0	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
417	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
418	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

[illegible]

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
452	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
453	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
454	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
455	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
456	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
457	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
458	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
459	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
460	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
461	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
462	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
463	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
464	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
465	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
466	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
467	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
468	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
469	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
470	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
471	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
472	1.00	1.00	0.80	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
473	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
474	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
475	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
476	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
477	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
478	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
479	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
480	1.00	1.00	0.80	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
481	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.30	1.50	0.0	1.50	0.0	1.50	0.0			
482	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.30	1.50	0.0	1.50	0.0	1.50	1.50			
483	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.30	1.50	0.0	1.50	1.50	1.50	0.0			
484	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.90	1.30	1.50	0.0	1.50	1.50	1.50	1.50			
485	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

[illegible]

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
519	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.50	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
520	1.00	1.00	0.80	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.50	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
521	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.50	1.00	0.80	0.0	0.80	0.0	0.80	0.0			
522	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.50	1.00	0.80	0.0	0.80	0.0	0.80	1.50			
523	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.50	1.00	0.80	0.0	0.80	1.50	0.80	0.0			
524	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.50	1.00	0.80	0.0	0.80	1.50	0.80	1.50			
525	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.50	1.00	0.80	1.50	0.80	0.0	0.80	0.0			
526	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.50	1.00	0.80	1.50	0.80	0.0	0.80	1.50			
527	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.50	1.00	0.80	1.50	0.80	1.50	0.80	0.0			
528	1.00	1.00	0.80	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.50	1.00	0.80	1.50	0.80	1.50	0.80	1.50			
529	1.00	1.00	1.00	1.00	0.0	0.0	-1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
530	1.00	1.00	1.00	1.00	0.0	0.0	-1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
531	1.00	1.00	1.00	1.00	0.0	0.0	1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
532	1.00	1.00	1.00	1.00	0.0	0.0	1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
533	1.00	1.00	1.00	1.00	0.0	0.0	-1.00	0.0	0.0	-0.30	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
534	1.00	1.00	1.00	1.00	0.0	0.0	-1.00	0.0	0.0	0.30	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
535	1.00	1.00	1.00	1.00	0.0	0.0	1.00	0.0	0.0	-0.30	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
536	1.00	1.00	1.00	1.00	0.0	0.0	1.00	0.0	0.0	0.30	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
537	1.00	1.00	1.00	1.00	0.0	0.0	0.0	-1.00	-0.30	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
538	1.00	1.00	1.00	1.00	0.0	0.0	0.0	-1.00	0.30	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
539	1.00	1.00	1.00	1.00	0.0	0.0	0.0	1.00	-0.30	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
540	1.00	1.00	1.00	1.00	0.0	0.0	0.0	1.00	0.30	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
541	1.00	1.00	1.00	1.00	0.0	0.0	0.0	-1.00	0.0	-0.30	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
542	1.00	1.00	1.00	1.00	0.0	0.0	0.0	-1.00	0.0	0.30	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
543	1.00	1.00	1.00	1.00	0.0	0.0	0.0	1.00	0.0	-0.30	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
544	1.00	1.00	1.00	1.00	0.0	0.0	0.0	1.00	0.0	0.30	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
545	1.00	1.00	1.00	1.00	0.0	0.0	-0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
546	1.00	1.00	1.00	1.00	0.0	0.0	-0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
547	1.00	1.00	1.00	1.00	0.0	0.0	0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
548	1.00	1.00	1.00	1.00	0.0	0.0	0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
549	1.00	1.00	1.00	1.00	0.0	0.0	0.0	-0.30	-1.00	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
550	1.00	1.00	1.00	1.00	0.0	0.0	0.0	-0.30	1.00	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
551	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.30	-1.00	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
552	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.30	1.00	0.0	0.0	0.0	0.0	0.0

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
553	1.00	1.00	1.00	1.00	0.0	0.0	-0.30	0.0	0.0	-1.00	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
554	1.00	1.00	1.00	1.00	0.0	0.0	-0.30	0.0	0.0	1.00	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
555	1.00	1.00	1.00	1.00	0.0	0.0	0.30	0.0	0.0	-1.00	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
556	1.00	1.00	1.00	1.00	0.0	0.0	0.30	0.0	0.0	1.00	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
557	1.00	1.00	1.00	1.00	0.0	0.0	0.0	-0.30	0.0	-1.00	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
558	1.00	1.00	1.00	1.00	0.0	0.0	0.0	-0.30	0.0	1.00	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
559	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.30	0.0	-1.00	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
560	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.30	0.0	1.00	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
561	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	-0.30	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
562	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.30	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
563	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	-0.30	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
564	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.30	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
565	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	-0.30
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
566	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	0.30
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
567	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.0	-0.30
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
568	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.0	

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
586	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	0.0	1.00
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
587	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	0.0	-1.00
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
588	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	0.0	1.00
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
589	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	-1.00
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
590	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	1.00
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
591	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	-1.00
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
592	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	1.00
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
593	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
594	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
595	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
596	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
597	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
598	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
599	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
600	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
601	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
602	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
603	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
604	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
605	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
606	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
607	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
608	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
609	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
610	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
611	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
612	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
613	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
614	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
615	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
616	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
617	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
618	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
619	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

[illegible]

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
653	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
654	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
655	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
656	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
657	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
658	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
659	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
660	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
661	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
662	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
663	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
664	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
665	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
666	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
667	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
668	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
669	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
670	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
671	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
672	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.60	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
673	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.00	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
674	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.00	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
675	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.00	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
676	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.00	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
677	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.00	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
678	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.00	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
679	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.00	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
680	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.00	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
681	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.00	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
682	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.00	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
683	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.00	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
684	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.00	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
685	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.00	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
686	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

[illegible]

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
720	1.00	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.60	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
721	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.60	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
722	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.60	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
723	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.60	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
724	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.60	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
725	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.60	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
726	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.60	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
727	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.60	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
728	1.00	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.60	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
729	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
730	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
731	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
732	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
733	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
734	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
735	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
736	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
737	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
738	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
739	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
740	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
741	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
742	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
743	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
744	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	1.00	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
745	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.60	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
746	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.60	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
747	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.60	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
748	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.60	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
749	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.60	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
750	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.60	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
751	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.60	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
752	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.60	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
753	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

[illegible]

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
787	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.00	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
788	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.00	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
789	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.00	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
790	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.00	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
791	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.00	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
792	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.00	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
793	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.00	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
794	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.00	0.0	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
795	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.00	0.0	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
796	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.00	0.0	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
797	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.00	0.0	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
798	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.00	0.0	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
799	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.00	0.0	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
800	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	1.00	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
801	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
802	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
803	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
804	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
805	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
806	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
807	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
808	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
809	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
810	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
811	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
812	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	0.0	1.00	1.00	1.00	1.00			
813	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	1.00	1.00	0.0	1.00	0.0			
814	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
815	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
816	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
817	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
818	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	0.0	1.00	0.0	1.00	1.00			
819	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.60	1.00	1.00	0.0	1.00	1.00	1.00	0.0			
820	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

[illegible]

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
854	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	0.0	1.00	1.00			
855	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.0			
856	1.00	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
857	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
858	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.80			
859	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.0			
860	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.80			
861	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.0			
862	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.80			
863	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.0			
864	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
865	1.00	1.00	1.00	1.00	0.0	0.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
866	1.00	1.00	1.00	1.00	0.0	0.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.80			
867	1.00	1.00	1.00	1.00	0.0	0.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.0			
868	1.00	1.00	1.00	1.00	0.0	0.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.80			
869	1.00	1.00	1.00	1.00	0.0	0.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.0			
870	1.00	1.00	1.00	1.00	0.0	0.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.80			
871	1.00	1.00	1.00	1.00	0.0	0.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.0			
872	1.00	1.00	1.00	1.00	0.0	0.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
873	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.90	1.00	0.0	1.00	0.0			
874	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.90	1.00	0.0	1.00	0.80			
875	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.90	1.00	0.80	1.00	0.0			
876	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.90	1.00	0.80	1.00	0.80			
877	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.90	1.00	0.0			
878	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.90	1.00	0.80			
879	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.90	1.00	0.0			
880	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.90	1.00	0.80			
881	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.90			
882	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.90			
883	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.90			
884	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.90			
885	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.20	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
886	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.20	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.80			
887	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
	0.20	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.0			
888	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.20	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.80			
889	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.20	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.0			
890	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.20	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.80			
891	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.20	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.0			
892	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.20	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
893	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.20	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
894	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.20	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.80			
895	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.20	0.0	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.0			
896	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.20	0.0	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.80			
897	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.20	0.0	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.0			
898	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.20	0.0	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.80			
899	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.20	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.0			
900	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.20	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
901	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.20	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
902	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.20	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.80			
903	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.20	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.0			
904	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.20	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.80			
905	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.20	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.0			
906	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.20	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.80			
907	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.20	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.0			
908	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.20	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
909	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.20	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
910	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.20	1.00	1.00	0.0	1.00	0.0	1.00	0.80			
911	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.20	1.00	1.00	0.0	1.00	0.80	1.00	0.0			
912	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.20	1.00	1.00	0.0	1.00	0.80	1.00	0.80			
913	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.20	1.00	1.00	0.80	1.00	0.0	1.00	0.0			
914	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.20	1.00	1.00	0.80	1.00	0.0	1.00	0.80			
915	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.20	1.00	1.00	0.80	1.00	0.80	1.00	0.0			
916	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.20	1.00	1.00	0.80	1.00	0.80	1.00	0.80			
917	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.0			
918	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0	1.00	0.80			
919	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.0			
920	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.80	1.00	0.80			

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
921	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.0			
922	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.0	1.00	0.80			
923	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.0			
924	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80	1.00	0.80			

AZIONE SISMICA

VALUTAZIONE DELL' AZIONE SISMICA

L'azione sismica sulle costruzioni è valutata a partire dalla "pericolosità sismica di base", in condizioni ideali di sito di riferimento rigido con superficie topografica orizzontale.

Allo stato attuale, la pericolosità sismica su reticolo di riferimento nell'intervallo di riferimento è fornita dai dati pubblicati sul sito <http://esse1.mi.ingv.it/>. Per punti non coincidenti con il reticolo di riferimento e periodi di ritorno non contemplati direttamente si opera come indicato nell' allegato alle NTC (rispettivamente media pesata e interpolazione).

L' azione sismica viene definita in relazione ad un periodo di riferimento V_r che si ricava, per ciascun tipo di costruzione, moltiplicandone la vita nominale per il coefficiente d'uso (vedi tabella Parametri della struttura). Fissato il periodo di riferimento V_r e la probabilità di superamento P_{ver} associata a ciascuno degli stati limite considerati, si ottiene il periodo di ritorno T_r e i relativi parametri di pericolosità sismica (vedi tabella successiva):

a_g : accelerazione orizzontale massima del terreno;

F_0 : valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale;

T^*c : periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale;

Parametri della struttura					
Classe d'uso	Vita V_n [anni]	Coeff. Uso	Periodo V_r [anni]	Tipo di suolo	Categoria topografica
II	50.0	1.0	50.0	B	T1

Individuati su reticolo di riferimento i parametri di pericolosità sismica si valutano i parametri spettrali riportati in tabella: S è il coefficiente che tiene conto della categoria di sottosuolo e delle condizioni topografiche mediante la relazione seguente $S = S_s \cdot S_t$ (3.2.3)

F_0 è il fattore che quantifica l'amplificazione spettrale massima, su sito di riferimento rigido orizzontale

F_v è il fattore che quantifica l'amplificazione spettrale massima verticale, in termini di accelerazione orizzontale massima del terreno a_g su sito di riferimento rigido orizzontale

T_b è il periodo corrispondente all'inizio del tratto dello spettro ad accelerazione costante.

T_c è il periodo corrispondente all'inizio del tratto dello spettro a velocità costante.

T_d è il periodo corrispondente all'inizio del tratto dello spettro a spostamento costante.

Lo spettro di risposta elastico in accelerazione della componente orizzontale del moto sismico, S_e , è definito dalle seguenti espressioni:

$$\begin{aligned}
 0 \leq T < T_b & \quad S_e(T) = a_g \cdot S_s \cdot \eta \cdot F_0 \cdot \left[\frac{T}{T_b} + \frac{1}{\eta \cdot F_0} \left(1 - \frac{T}{T_b} \right) \right] \\
 T_b \leq T < T_c & \quad S_e(T) = a_g \cdot S_s \cdot \eta \cdot F_0 \\
 T_c \leq T < T_d & \quad S_e(T) = a_g \cdot S_s \cdot \eta \cdot F_0 \cdot \left(\frac{T_c}{T} \right) \\
 T_d \leq T & \quad S_e(T) = a_g \cdot S_s \cdot \eta \cdot F_0 \cdot \left(\frac{T_c \cdot T_d}{T^2} \right)
 \end{aligned}$$

Dove per sottosuolo di categoria **A** i coefficienti S_s e C_c valgono 1; mentre per le categorie di sottosuolo B, C, D, E i coefficienti S_s e C_c vengono calcolati mediante le espressioni riportate nella seguente Tabella

Categoria sottosuolo	S_s	C_c
A	1,00	1,00
B	$1,00 \leq 1,40 - 0,40 \cdot F_0 \cdot \frac{a_g}{g} \leq 1,20$	$1,10 \cdot (T_c^*)^{-0,20}$
C	$1,00 \leq 1,70 - 0,60 \cdot F_0 \cdot \frac{a_g}{g} \leq 1,50$	$1,05 \cdot (T_c^*)^{-0,33}$
D	$0,90 \leq 2,40 - 1,50 \cdot F_0 \cdot \frac{a_g}{g} \leq 1,80$	$1,25 \cdot (T_c^*)^{-0,50}$
E	$1,00 \leq 2,00 - 1,10 \cdot F_0 \cdot \frac{a_g}{g} \leq 1,60$	$1,15 \cdot (T_c^*)^{-0,40}$

Per tenere conto delle condizioni topografiche e in assenza di specifiche analisi di risposta sismica locale, si utilizzano i valori del coefficiente topografico S_T riportati nella seguente Tabella

Categoria topografica	Ubicazione dell'opera o dell'intervento	S _T
T1	-	1,0
T2	In corrispondenza della sommità del pendio	1,2
T3	In corrispondenza della cresta di un rilievo con pendenza media minore o uguale a 30°	1,2
T4	In corrispondenza della cresta di un rilievo con pendenza media maggiore di 30°	1,4

Lo spettro di risposta elastico in accelerazione della componente verticale del moto sismico, S_{ve}, è definito dalle espressioni:

$$0 \leq T < T_B \quad S_{ve}(T) = a_g \cdot S \cdot \eta \cdot F_r \cdot \left[\frac{T}{T_B} + \frac{1}{\eta \cdot F_c} \left(1 - \frac{T}{T_B} \right) \right]$$

$$T_B \leq T < T_C \quad S_{ve}(T) = a_g \cdot S \cdot \eta \cdot F_r$$

$$T_C \leq T < T_D \quad S_{ve}(T) = a_g \cdot S \cdot \eta \cdot F_r \cdot \left(\frac{T_C}{T} \right)$$

$$T_D \leq T \quad S_{ve}(T) = a_g \cdot S \cdot \eta \cdot F_r \cdot \left(\frac{T_C \cdot T_D}{T^2} \right)$$

I valori di S_s, T_B, T_C e T_D, sono riportati nella seguente Tabella

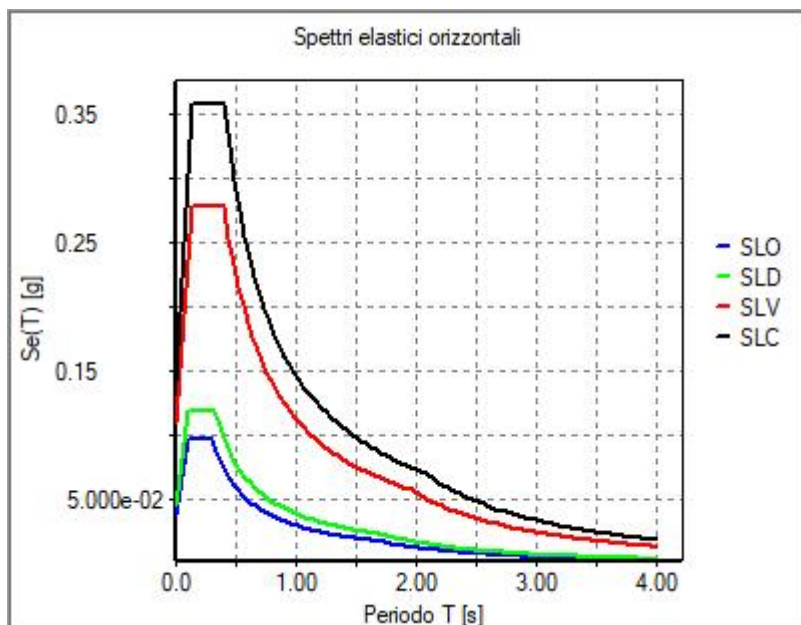
Categoria di sottosuolo	S _s	T _B	T _C	T _D
A, B, C, D, E	1,0	0,05 s	0,15 s	1,0 s

Id nodo	Longitudine	Latitudine	Distanza
			Km
Loc.	9.689	45.042	
14265	9.673	45.024	2.562
14266	9.743	45.026	4.568
14044	9.740	45.076	5.322
14043	9.670	45.074	3.763

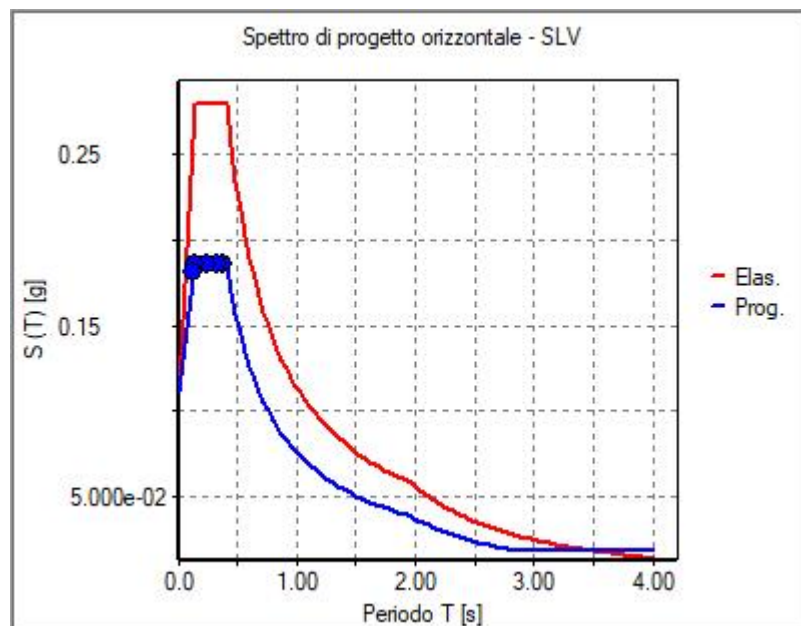
SL	Pver	Tr	ag	Fo	T*c
		Anni	g		sec
SLO	81.0	30.1	0.032	2.534	0.207
SLD	63.0	50.3	0.039	2.573	0.222
SLV	10.0	474.6	0.092	2.518	0.290
SLC	5.0	974.8	0.120	2.498	0.294

SL	ag	S	Fo	Fv	Tb	Tc	Td
	g				sec	sec	sec
SLO	0.032	1.200	2.534	0.613	0.104	0.312	1.728
SLD	0.039	1.200	2.573	0.685	0.110	0.330	1.756
SLV	0.092	1.200	2.518	1.032	0.136	0.409	1.969
SLC	0.120	1.200	2.498	1.166	0.138	0.413	2.078

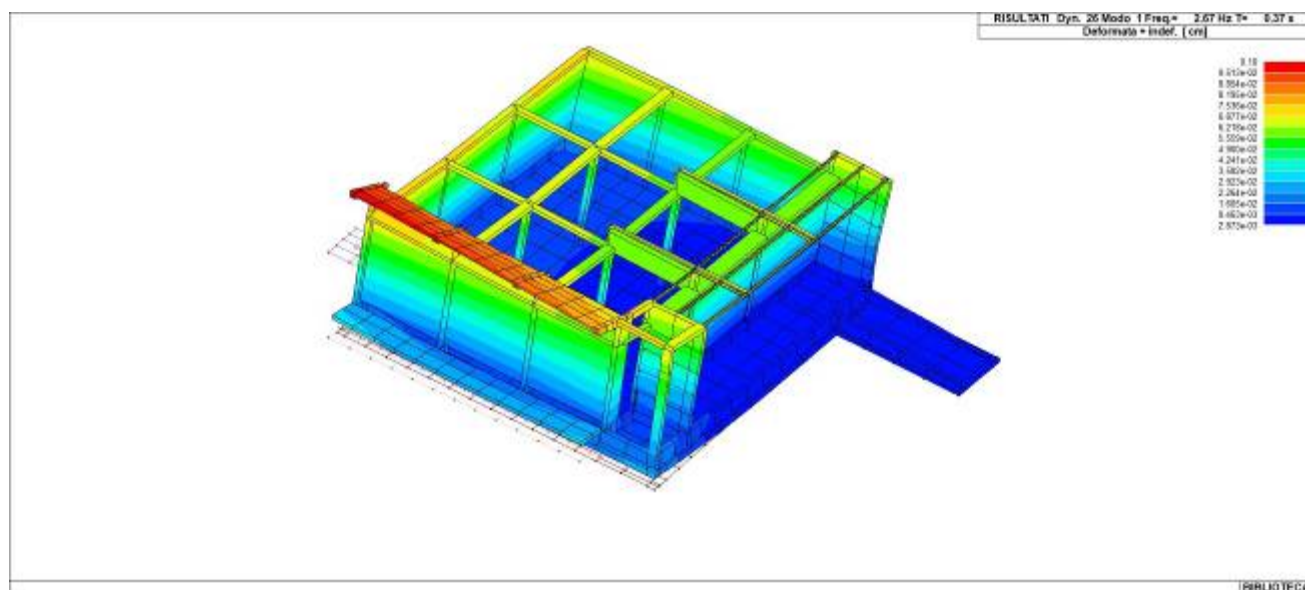
Modo	Frequenza	Periodo	X M efficace x g	%	Y M efficace x g	%	Z M efficace x g	%	RZ M efficace x g	%
	1/sec	sec	daN		daN		daN		daN m2	
1	2.67	0.37	4761.4	1	2.398e+05	76	801.6	0	563.1	20
2	3.08	0.33	1.821e+05	58	7334.4	2	187.2	0	336.6	12
3	4.20	0.24	7.345e+04	23	52.5	0	584.2	0	1306.7	48
4	6.85	0.15	68.2	0	21.7	0	1.027e+04	3	0.2	0
5	7.23	0.14	94.2	0	8184.0	2	9.154e+04	29	22.8	0
6	7.82	0.13	1500.7	0	1524.1	0	656.0	0	2.0	0



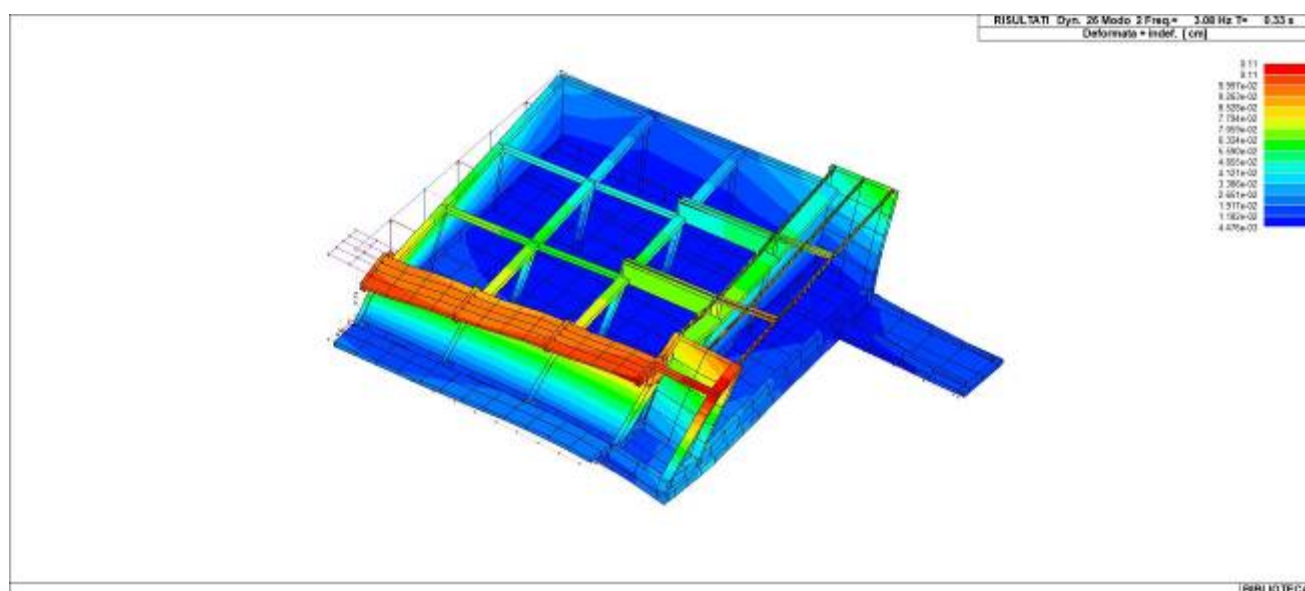
24_DIA_SPETTRI_ELASTICI_O



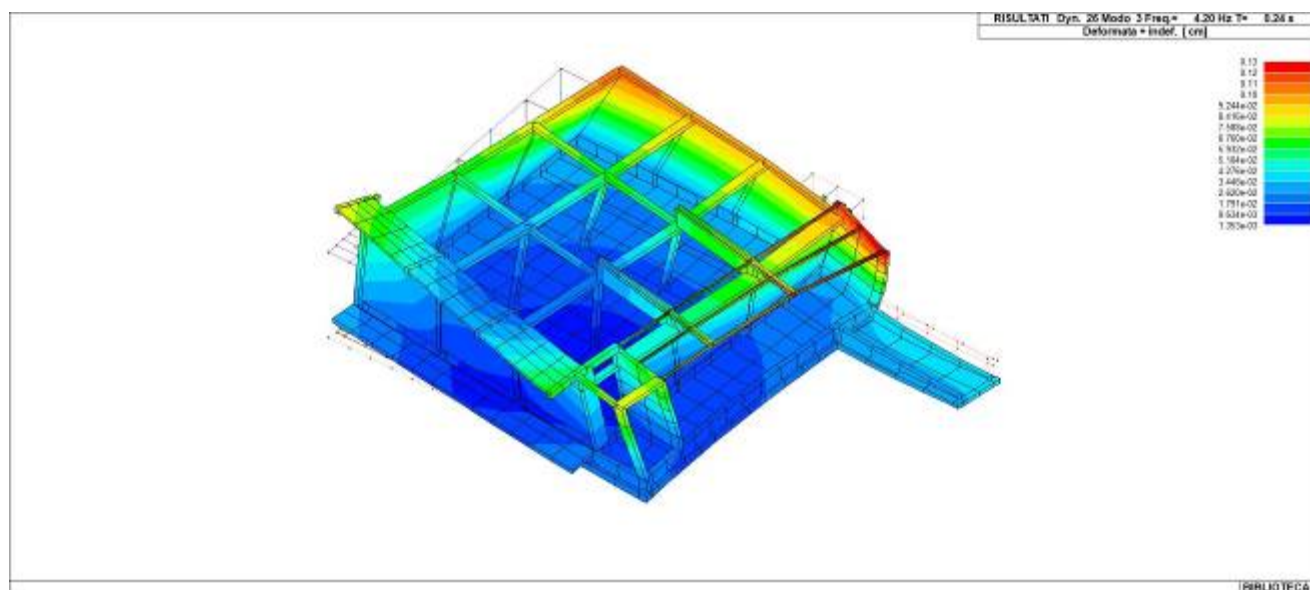
24_DIA_SPETTRI_PROGETTO_SLV_O



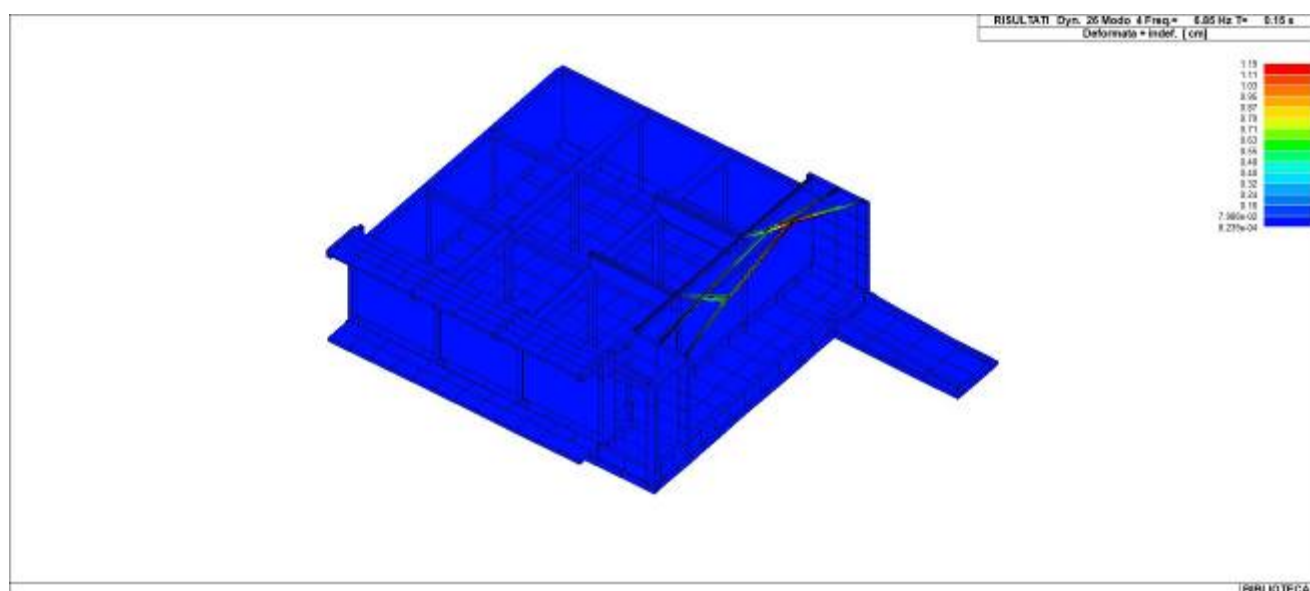
24_INPSIS_001_FORME MODALI



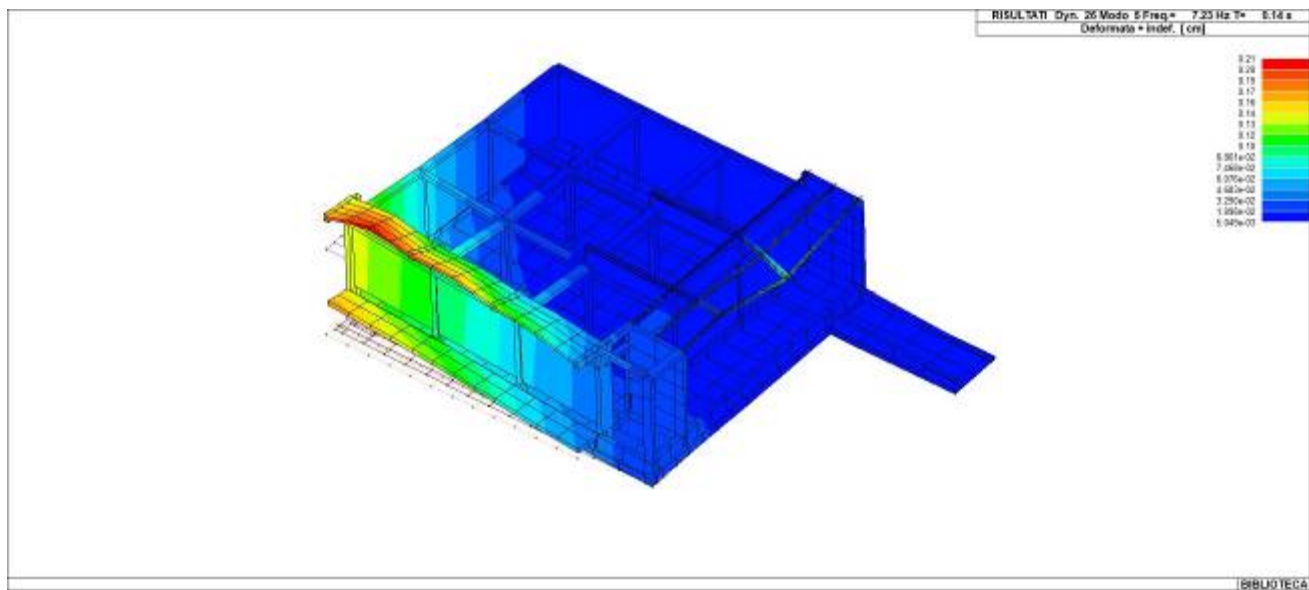
24_INPSIS_002_FORME MODALI



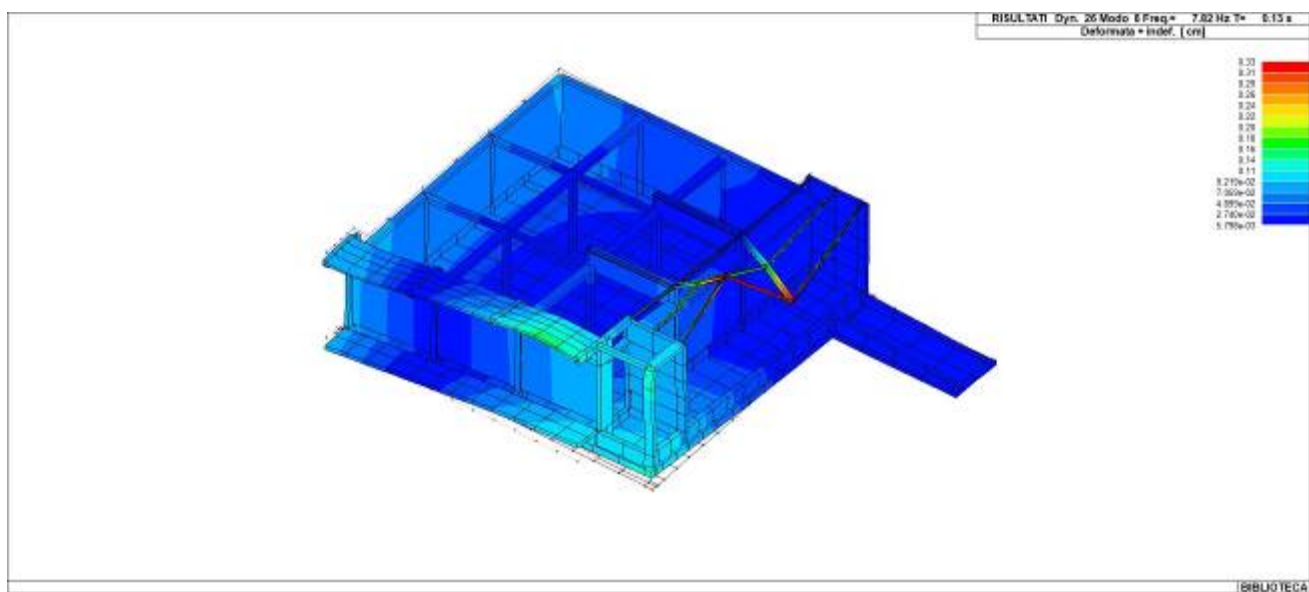
24_INPSIS_003_FORME MODALI



24_INPSIS_004_FORME MODALI



24_INPSIS_005_FORME MODALI



24_INPSIS_006_FORME MODALI

RISULTATI ANALISI SISMICHE

LEGENDA TABELLA ANALISI SISMICHE

Il programma consente l'analisi di diverse configurazioni sismiche.

Sono previsti, infatti, i seguenti casi di carico:

9. Esk caso di carico sismico con analisi statica equivalente

10. Edk caso di carico sismico con analisi dinamica

Ciascun caso di carico è caratterizzato da un angolo di ingresso e da una configurazione di masse determinante la forza sismica complessiva (si rimanda al capitolo relativo ai casi di carico per chiarimenti inerenti questo aspetto).

Nella colonna Note, in funzione della norma in uso sono riportati i parametri fondamentali che caratterizzano l'azione sismica: in particolare possono essere presenti i seguenti valori:

Angolo di ingresso	Angolo di ingresso dell'azione sismica orizzontale
Fattore di importanza	Fattore di importanza dell'edificio, in base alla categoria di appartenenza
Zona sismica	Zona sismica
Accelerazione ag	Accelerazione orizzontale massima sul suolo
Categoria suolo	Categoria di profilo stratigrafico del suolo di fondazione
Fattore q	Fattore di struttura/di comportamento. Dipendente dalla tipologia strutturale
Amplificazione ND	Coefficiente di amplificazione q/qND delle azioni sismiche (solo per elementi progettati in campo non dissipativo)
Fattore di sito S	Fattore dipendente dalla stratigrafia e dal profilo topografico
Classe di duttilità CD	Classe di duttilità della struttura – "A" duttilità alta, "B" duttilità bassa
Fattore riduz. SLD	Fattore di riduzione dello spettro elastico per lo stato limite di danno
Periodo proprio T1	Periodo proprio di vibrazione della struttura
Coefficiente Lambda	Coefficiente dipendente dal periodo proprio T1 e dal numero di piani della struttura
Ordinata spettro Sd(T1)	Valore delle ordinate dello spettro di progetto per lo stato limite ultimo, componente orizzontale (verticale Svd)
Ordinata spettro Se(T1)	Valore delle ordinate dello spettro elastico ridotta del fattore SLD per lo stato limite di danno, componente orizzontale (verticale Sve)
Ordinata spettro S (Tb-Tc)	Valore dell'ordinata dello spettro in uso nel tratto costante
N°di modi considerati	Numero di modi di vibrare della struttura considerati nell'analisi dinamica

Nel caso di elementi progettati in campo non dissipativo vengono adottate le sollecitazioni calcolate con un fattore qND ricavato come da 7.3.2 in funzione del fattore di comportamento q utilizzato per la struttura: $1 < qND = 2/3 \cdot q < 1.5$

Il coefficiente di amplificazione delle azioni sismiche rispetto alle azioni calcolate con il fattore di comportamento globale viene indicato nelle relative tabelle.

Per ciascun caso di carico sismico viene riportato l'insieme di dati sotto riportati (le masse sono espresse in unità di forza):

38. analisi sismica statica equivalente:

38.1. quota, posizione del centro di applicazione e azione orizzontale risultante, posizione del baricentro delle rigidezze, rapporto r/Ls (per strutture a nucleo), indici di regolarità e/r secondo EC8 4.2.3.2

38.2. azione sismica complessiva

39. analisi sismica dinamica con spettro di risposta:

39.1. quota, posizione del centro di massa e massa risultante, posizione del baricentro delle rigidezze, rapporto r/Ls (per strutture a nucleo), indici di regolarità e/r secondo EC8 4.2.3.2

39.2. frequenza, periodo, accelerazione spettrale, massa eccitata nelle tre direzioni globali per tutti i modi

39.3. massa complessiva ed aliquota di massa complessiva eccitata.

Per ciascuna combinazione sismica definita SLD o SLO viene riportato il livello di deformazione ϵ_{dT} (dr) degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso anche in unità $1000 \cdot \epsilon_{dT}/h$ da confrontare direttamente con i valori forniti nella norma (es. 5 per edifici con tamponamenti collegati rigidamente alla struttura, 10.0 per edifici con tamponamenti collegati elasticamente, 3 per edifici in muratura ordinaria, 4 per edifici in muratura armata).

Qualora si applichi il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") l'analisi sismica dinamica può essere comprensiva di sollecitazione verticale contemporanea a quella orizzontale, nel qual caso è effettuata una sovrapposizione degli effetti in ragione della radice dei quadrati degli effetti stessi. Per ciascuna combinazione sismica - analisi effettuate con il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") - viene riportato il livello di deformazione ϵ_{dT} , ϵ_{dP} e ϵ_{dD} degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso in unità $1000 \cdot \epsilon_{dT}/h$ da confrontare direttamente con il valore 2 o 4 per la verifica.

Per gli edifici sismicamente isolati si riportano di seguito le verifiche condotte sui dispositivi di isolamento. Le verifiche sono effettuate secondo la circolare n.7/2019 del C.S.LL.PP nelle combinazioni in SLC come previsto dal DM 17-01-2018. Per ogni combinazione è riportato il codice di verifica ed i valori utilizzati per la verifica: spostamento dE, area ridotta e dimensione A2, azione verticale, deformazioni di taglio dell'elastomero e tensioni nell'acciaio.

In particolare la tabella, per ogni combinazione di calcolo, riporta:

Nodo	Nodo di appoggio dell' isolatore
Cmb	Combinazione oggetto della verifica
Verif.	Codice di verifica ok – verifica positiva , NV – verifica negativa, ND – verifica non completata

dE	Spostamento relativo tra le due facce combinato con la regola del 30%
Ang fi	Angolo utilizzato per il calcolo dell' area ridotta Ar (per dispositivi circolari)
V	Azione verticale agente
Ar	Area ridotta efficace
Dim A2	Dimensione utile per il calcolo della deformazione per rotazione
Sig s	Tensione nell' inserto in acciaio
Gam c(a,s,t)	Deformazioni di taglio dell' elastomero
Vcr	Carico critico per instabilità

Affinché la verifica sia positiva deve essere:

- $V > 0$
- $Sig s < f_{yk}$
- $Gam t < 5$
- $Gam s < Gam * (caratteristica\ dell'\ elastomero)$
- $Gam s < 2$
- $V < 0.5 V_{cr}$

Calcolo dei fattori di comportamento secondo il D.M. 17/01/2018

Caratteristiche costruzione	
Tipologia	Nuova
Regolarità pianta	SI
Regolarità altezza	SI
Classe di duttilità	ND
Sistema costruttivo	Calcestruzzo
Tipologia strutturale	Strutture a telaio, a pareti accoppiate, miste
Definizione rapporto α_u/α_1	Valore come da normativa
Riferimento normativo α_u/α_1	Strutture a telaio di un piano

Parametri	
α_u/α_1	1.100
$q_0 = 3.000 \alpha_u/\alpha_1$	3.300
k_w	1.000
K_R	1.0
$q_D = q_0 \cdot k_w \cdot K_R$	3.300
$q_{ND} = 2/3 \cdot q_D$	1.500 (≤ 1.5)

Fattori di comportamento		
		Non dissipativi
q SLU x		1.500
q SLU y		1.500

CDC	Tipo	Sigla Id	Note
7	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)	
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.186 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.338 sec.
			fattore q: 1.500
			amplificazione ND (non dissipativi): 1.000
			fattore per spost. mu d: 1.605
			classe di duttilità CD: ND
			numero di modi considerati: 60
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
6.06	2.869e+04	11.37	2.08	0.0	-0.91	9.78	8.94	0.956	0.048	0.957
4.89	1.951e+05	7.96	7.87	0.0	-0.82	8.40	8.97	1.059	0.015	0.153
3.87	5118.89	16.27	8.98	0.0	-0.70	16.03	9.00	2.868	0.004	0.002

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
2.85	5118.89	16.27	8.98	0.0	-0.70	16.03	9.00	2.868	0.004	0.002
1.82	5118.89	16.27	8.98	0.0	-0.70	16.03	9.00	2.868	0.004	0.002
0.80	7.074e+04	8.15	6.52	0.0	-0.91	10.88	9.87	1.990	0.264	0.266
0.77	516.05	18.23	14.60	0.0	-0.11	0.0	0.0	0.0	0.0	0.0
0.65	716.66	19.98	14.60	0.0	-0.11	0.0	0.0	0.0	0.0	0.0
0.53	587.62	21.74	14.60	0.0	-0.11	0.0	0.0	0.0	0.0	0.0
0.42	458.58	23.50	14.60	0.0	-0.11	0.0	0.0	0.0	0.0	0.0
0.30	180.90	25.25	14.60	0.0	-0.11	0.0	0.0	0.0	0.0	0.0
Risulta	3.123e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	2.663	0.376	0.186	1.014e+04	3.2	2.327e+05	74.5	755.57	0.2	0.0	0.0
2	2.959	0.338	0.186	1.778e+05	56.9	1.439e+04	4.6	210.01	6.72e-02	0.0	0.0
3	4.428	0.226	0.186	7.177e+04	23.0	23.92	7.66e-03	743.03	0.2	0.0	0.0
4	6.848	0.146	0.186	70.61	2.26e-02	21.96	7.03e-03	1.029e+04	3.3	0.0	0.0
5	7.225	0.138	0.186	75.37	2.41e-02	8198.09	2.6	9.108e+04	29.2	0.0	0.0
6	7.828	0.128	0.181	1495.86	0.5	1508.67	0.5	727.56	0.2	0.0	0.0
7	8.125	0.123	0.179	415.65	0.1	124.10	3.97e-02	8.679e+04	27.8	0.0	0.0
8	8.537	0.117	0.175	19.12	6.12e-03	430.72	0.1	1.096e+04	3.5	0.0	0.0
9	9.109	0.110	0.171	1084.96	0.3	286.49	9.17e-02	3.096e+04	9.9	0.0	0.0
10	10.394	0.096	0.164	21.70	6.95e-03	2981.98	1.0	4.016e+04	12.9	0.0	0.0
11	11.052	0.090	0.161	1679.74	0.5	59.31	1.90e-02	3.017e+04	9.7	0.0	0.0
12	11.264	0.089	0.160	1.514e+04	4.8	512.57	0.2	1416.11	0.5	0.0	0.0
13	11.568	0.086	0.158	45.62	1.46e-02	4818.04	1.5	1470.17	0.5	0.0	0.0
14	11.883	0.084	0.157	3345.03	1.1	10.57	3.38e-03	2079.44	0.7	0.0	0.0
15	13.545	0.074	0.151	244.43	7.83e-02	1643.64	0.5	295.97	9.48e-02	0.0	0.0
16	13.767	0.073	0.151	1640.16	0.5	8250.09	2.6	321.02	0.1	0.0	0.0
17	14.353	0.070	0.149	1233.56	0.4	127.41	4.08e-02	2.20	7.06e-04	0.0	0.0
18	14.504	0.069	0.149	881.94	0.3	2.940e+04	9.4	133.31	4.27e-02	0.0	0.0
19	15.052	0.066	0.147	1184.84	0.4	2018.38	0.6	21.73	6.96e-03	0.0	0.0
20	15.524	0.064	0.146	56.55	1.81e-02	2254.74	0.7	36.70	1.18e-02	0.0	0.0
21	16.137	0.062	0.145	1.105e+04	3.5	667.83	0.2	50.09	1.60e-02	0.0	0.0
22	16.335	0.061	0.144	5679.33	1.8	2.67	8.55e-04	10.93	3.50e-03	0.0	0.0
23	17.443	0.057	0.142	3365.95	1.1	0.16	5.01e-05	756.21	0.2	0.0	0.0
24	17.731	0.056	0.142	3608.72	1.2	887.83	0.3	1273.89	0.4	0.0	0.0
25	19.022	0.053	0.140	0.87	2.79e-04	14.26	4.57e-03	1.19	3.81e-04	0.0	0.0
26	20.297	0.049	0.138	57.98	1.86e-02	333.79	0.1	10.45	3.35e-03	0.0	0.0
27	21.513	0.046	0.136	0.07	2.39e-05	15.57	4.98e-03	3.45	1.10e-03	0.0	0.0
28	22.833	0.044	0.135	1.19	3.81e-04	1.22	3.91e-04	10.98	3.52e-03	0.0	0.0
29	23.969	0.042	0.134	7.17e-04	0.0	46.06	1.47e-02	43.48	1.39e-02	0.0	0.0
30	24.429	0.041	0.133	19.21	6.15e-03	0.05	1.48e-05	47.99	1.54e-02	0.0	0.0
31	24.719	0.040	0.133	1.32	4.22e-	1.46	4.69e-	3.73	1.20e-	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
					04		04		03		
32	25.063	0.040	0.133	72.06	2.31e-02	9.32	2.98e-03	1.84	5.90e-04	0.0	0.0
33	25.961	0.039	0.132	7.59	2.43e-03	14.44	4.62e-03	0.72	2.31e-04	0.0	0.0
34	26.686	0.037	0.131	23.62	7.56e-03	112.50	3.60e-02	12.56	4.02e-03	0.0	0.0
35	27.211	0.037	0.131	4.41	1.41e-03	19.97	6.39e-03	4.35	1.39e-03	0.0	0.0
36	27.739	0.036	0.131	0.91	2.91e-04	173.09	5.54e-02	3.22	1.03e-03	0.0	0.0
37	29.001	0.034	0.130	4.55	1.46e-03	38.17	1.22e-02	4.59	1.47e-03	0.0	0.0
38	29.454	0.034	0.129	2.06	6.60e-04	36.48	1.17e-02	55.21	1.77e-02	0.0	0.0
39	29.821	0.034	0.129	3.55	1.14e-03	3.94	1.26e-03	52.65	1.69e-02	0.0	0.0
40	30.123	0.033	0.129	9.66	3.09e-03	43.48	1.39e-02	1.56	5.00e-04	0.0	0.0
41	32.107	0.031	0.128	4.47	1.43e-03	14.12	4.52e-03	5.10	1.63e-03	0.0	0.0
42	32.600	0.031	0.128	1.96	6.27e-04	32.99	1.06e-02	32.64	1.05e-02	0.0	0.0
43	33.374	0.030	0.127	0.45	1.45e-04	0.44	1.39e-04	0.06	1.85e-05	0.0	0.0
44	33.999	0.029	0.127	0.09	2.82e-05	0.17	5.39e-05	8.83	2.83e-03	0.0	0.0
45	34.751	0.029	0.127	0.33	1.05e-04	0.04	1.15e-05	0.35	1.12e-04	0.0	0.0
46	35.331	0.028	0.126	0.03	1.01e-05	2.42	7.75e-04	5.29	1.69e-03	0.0	0.0
47	36.570	0.027	0.126	1.21	3.86e-04	1.33	4.25e-04	251.27	8.05e-02	0.0	0.0
48	37.095	0.027	0.126	1.43	4.58e-04	0.98	3.14e-04	18.18	5.82e-03	0.0	0.0
49	37.360	0.027	0.125	0.95	3.04e-04	2.25	7.19e-04	0.07	2.20e-05	0.0	0.0
50	38.787	0.026	0.125	0.01	4.17e-06	0.02	4.84e-06	0.26	8.36e-05	0.0	0.0
51	39.411	0.025	0.125	0.11	3.63e-05	8.55e-03	2.74e-06	0.09	2.86e-05	0.0	0.0
52	40.734	0.025	0.124	0.63	2.00e-04	0.04	1.44e-05	92.24	2.95e-02	0.0	0.0
53	41.304	0.024	0.124	1.34	4.30e-04	0.61	1.94e-04	250.67	8.03e-02	0.0	0.0
54	41.910	0.024	0.124	0.20	6.47e-05	0.02	6.59e-06	8.37	2.68e-03	0.0	0.0
55	42.534	0.024	0.124	7.82e-03	2.50e-06	0.37	1.18e-04	70.35	2.25e-02	0.0	0.0
56	42.862	0.023	0.124	0.0	0.0	1.64	5.24e-04	29.37	9.40e-03	0.0	0.0
57	43.264	0.023	0.123	0.18	5.86e-05	2.26	7.25e-04	88.88	2.85e-02	0.0	0.0
58	44.840	0.022	0.123	0.21	6.77e-05	0.48	1.55e-04	13.67	4.38e-03	0.0	0.0
59	45.905	0.022	0.123	0.02	7.76e-06	0.12	3.77e-05	1.10	3.51e-04	0.0	0.0
60	46.336	0.022	0.123	4.45e-03	1.42e-06	0.27	8.77e-05	6.87e-05	0.0	0.0	0.0
Risulta				3.123e+05		3.123e+05		3.118e+05			
In percentuale				99.99		99.98		99.85			

CDC	Tipo	Sigla Id	Note
8	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -)	
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.186 g

CDC	Tipo	Sigla Id	Note
			angolo di ingresso:0.0
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.312 sec.
			fattore q: 1.500
			amplificazione ND (non dissipativi): 1.000
			fattore per spost. mu d: 1.656
			classe di duttilità CD: ND
			numero di modi considerati: 60
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
6.06	2.869e+04	11.37	2.08	0.0	0.91	9.78	8.94	0.956	0.048	0.957
4.89	1.951e+05	7.96	7.87	0.0	0.82	8.40	8.97	1.059	0.015	0.153
3.87	5118.89	16.27	8.98	0.0	0.70	16.03	9.00	2.868	0.004	0.002
2.85	5118.89	16.27	8.98	0.0	0.70	16.03	9.00	2.868	0.004	0.002
1.82	5118.89	16.27	8.98	0.0	0.70	16.03	9.00	2.868	0.004	0.002
0.80	7.074e+04	8.15	6.52	0.0	0.91	10.88	9.87	1.990	0.264	0.266
0.77	516.05	18.23	14.60	0.0	0.11	0.0	0.0	0.0	0.0	0.0
0.65	716.66	19.98	14.60	0.0	0.11	0.0	0.0	0.0	0.0	0.0
0.53	587.62	21.74	14.60	0.0	0.11	0.0	0.0	0.0	0.0	0.0
0.42	458.58	23.50	14.60	0.0	0.11	0.0	0.0	0.0	0.0	0.0
0.30	180.90	25.25	14.60	0.0	0.11	0.0	0.0	0.0	0.0	0.0
Risulta	3.123e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	2.670	0.374	0.186	2425.76	0.8	2.429e+05	77.8	826.99	0.3	0.0	0.0
2	3.207	0.312	0.186	1.922e+05	61.5	4075.08	1.3	204.64	6.55e-02	0.0	0.0
3	4.015	0.249	0.186	6.630e+04	21.2	120.08	3.84e-02	444.63	0.1	0.0	0.0
4	6.848	0.146	0.186	66.84	2.14e-02	21.55	6.90e-03	1.026e+04	3.3	0.0	0.0
5	7.226	0.138	0.186	116.48	3.73e-02	8175.92	2.6	9.194e+04	29.4	0.0	0.0
6	7.819	0.128	0.181	1522.28	0.5	1533.57	0.5	589.14	0.2	0.0	0.0
7	8.127	0.123	0.179	251.47	8.05e-02	126.42	4.05e-02	8.562e+04	27.4	0.0	0.0
8	8.538	0.117	0.175	6.40	2.05e-03	425.51	0.1	1.113e+04	3.6	0.0	0.0
9	9.084	0.110	0.171	1469.02	0.5	284.78	9.12e-02	3.141e+04	10.1	0.0	0.0
10	10.432	0.096	0.164	33.95	1.09e-02	3256.57	1.0	4.487e+04	14.4	0.0	0.0
11	11.107	0.090	0.160	50.88	1.63e-02	2.17	6.93e-04	2.640e+04	8.5	0.0	0.0
12	11.607	0.086	0.158	1152.22	0.4	5413.52	1.7	2554.75	0.8	0.0	0.0
13	11.726	0.085	0.158	610.86	0.2	3.53	1.13e-03	947.72	0.3	0.0	0.0
14	12.056	0.083	0.156	1.071e+04	3.4	4.75	1.52e-03	521.05	0.2	0.0	0.0
15	13.475	0.074	0.152	1594.80	0.5	1414.47	0.5	453.53	0.1	0.0	0.0
16	13.870	0.072	0.150	199.69	6.39e-02	9444.12	3.0	180.13	5.77e-02	0.0	0.0
17	14.378	0.070	0.149	1660.99	0.5	1706.69	0.5	2.57	8.23e-04	0.0	0.0
18	14.530	0.069	0.149	1511.89	0.5	2.726e+04	8.7	139.47	4.47e-02	0.0	0.0
19	15.129	0.066	0.147	2.34	7.48e-04	791.04	0.3	6.26	2.00e-03	0.0	0.0
20	15.455	0.065	0.146	1.678e+04	5.4	15.30	4.90e-03	39.07	1.25e-02	0.0	0.0
21	15.557	0.064	0.146	9921.64	3.2	3076.90	1.0	162.42	5.20e-02	0.0	0.0
22	16.993	0.059	0.143	2862.63	0.9	610.28	0.2	7.77	2.49e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
									03		
23	17.469	0.057	0.142	134.36	4.30e-02	233.04	7.46e-02	1563.49	0.5	0.0	0.0
24	17.798	0.056	0.142	589.48	0.2	423.60	0.1	424.44	0.1	0.0	0.0
25	19.023	0.053	0.140	5.49	1.76e-03	16.18	5.18e-03	1.18	3.79e-04	0.0	0.0
26	20.395	0.049	0.138	3.13	1.00e-03	314.20	0.1	14.21	4.55e-03	0.0	0.0
27	21.517	0.046	0.136	3.43	1.10e-03	16.72	5.35e-03	1.69	5.40e-04	0.0	0.0
28	22.765	0.044	0.135	0.58	1.87e-04	2.54	8.13e-04	30.27	9.69e-03	0.0	0.0
29	23.574	0.042	0.134	20.71	6.63e-03	26.25	8.41e-03	105.96	3.39e-02	0.0	0.0
30	23.845	0.042	0.134	14.29	4.58e-03	14.04	4.49e-03	3.05	9.76e-04	0.0	0.0
31	24.679	0.041	0.133	0.13	4.18e-05	1.26	4.04e-04	0.03	8.55e-06	0.0	0.0
32	24.911	0.040	0.133	36.83	1.18e-02	10.34	3.31e-03	5.21	1.67e-03	0.0	0.0
33	25.275	0.040	0.132	4.88	1.56e-03	0.02	6.64e-06	0.48	1.54e-04	0.0	0.0
34	26.170	0.038	0.132	4.25	1.36e-03	36.08	1.16e-02	0.18	5.68e-05	0.0	0.0
35	26.659	0.038	0.131	0.12	3.92e-05	104.95	3.36e-02	8.14	2.61e-03	0.0	0.0
36	27.114	0.037	0.131	0.75	2.39e-04	4.53	1.45e-03	4.45	1.42e-03	0.0	0.0
37	27.770	0.036	0.131	6.72e-03	2.15e-06	193.41	6.19e-02	5.28	1.69e-03	0.0	0.0
38	28.092	0.036	0.130	4.32	1.38e-03	1.43	4.56e-04	10.41	3.33e-03	0.0	0.0
39	28.984	0.035	0.130	0.86	2.76e-04	40.96	1.31e-02	22.20	7.11e-03	0.0	0.0
40	29.330	0.034	0.129	1.97	6.31e-04	0.48	1.55e-04	1.78	5.70e-04	0.0	0.0
41	29.812	0.034	0.129	0.50	1.59e-04	36.54	1.17e-02	71.51	2.29e-02	0.0	0.0
42	31.436	0.032	0.128	4.75	1.52e-03	70.76	2.27e-02	39.40	1.26e-02	0.0	0.0
43	32.474	0.031	0.128	0.47	1.49e-04	1.58	5.07e-04	0.27	8.77e-05	0.0	0.0
44	33.302	0.030	0.127	0.10	3.04e-05	0.68	2.16e-04	0.13	4.22e-05	0.0	0.0
45	34.388	0.029	0.127	0.26	8.38e-05	2.34	7.49e-04	0.33	1.05e-04	0.0	0.0
46	35.165	0.028	0.126	6.73e-04	0.0	1.47	4.71e-04	0.99	3.15e-04	0.0	0.0
47	36.019	0.028	0.126	5.85e-03	1.87e-06	2.92	9.35e-04	37.58	1.20e-02	0.0	0.0
48	36.677	0.027	0.126	1.59	5.09e-04	0.59	1.88e-04	245.12	7.85e-02	0.0	0.0
49	37.384	0.027	0.125	2.76	8.84e-04	3.87	1.24e-03	3.45	1.10e-03	0.0	0.0
50	38.492	0.026	0.125	0.04	1.34e-05	0.10	3.18e-05	0.07	2.30e-05	0.0	0.0
51	38.834	0.026	0.125	3.29e-03	1.05e-06	3.02e-04	0.0	0.35	1.11e-04	0.0	0.0
52	40.650	0.025	0.124	0.19	6.08e-05	0.15	4.89e-05	77.04	2.47e-02	0.0	0.0
53	41.088	0.024	0.124	0.08	2.64e-05	8.65e-03	2.77e-06	39.29	1.26e-02	0.0	0.0
54	41.476	0.024	0.124	0.41	1.32e-04	0.84	2.69e-04	163.75	5.24e-02	0.0	0.0
55	42.087	0.024	0.124	0.14	4.53e-05	2.71e-04	0.0	0.23	7.33e-05	0.0	0.0
56	42.809	0.023	0.124	7.43e-05	0.0	4.00	1.28e-03	239.11	7.66e-02	0.0	0.0
57	44.027	0.023	0.123	0.04	1.42e-05	1.04	3.32e-04	0.02	5.47e-06	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
58	44.991	0.022	0.123	0.07	2.35e-05	2.34e-05	0.0	6.79	2.17e-03	0.0	0.0
59	45.705	0.022	0.123	0.02	6.42e-06	0.37	1.19e-04	4.47	1.43e-03	0.0	0.0
60	46.005	0.022	0.123	0.02	5.97e-06	2.97e-03	0.0	0.35	1.11e-04	0.0	0.0
Risulta				3.123e+05		3.123e+05		3.118e+05			
In percentuale				99.99		99.98		99.84			

CDC	Tipo	Sigla Id	Note
9	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)	
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.186 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.373 sec.
			fattore q: 1.500
			amplificazione ND (non dissipativi): 1.000
			fattore per spost. mu d: 1.548
			classe di duttilità CD: ND
			numero di modi considerati: 60
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
6.06	2.869e+04	11.37	2.08	0.89	0.0	9.78	8.94	0.956	0.048	0.957
4.89	1.951e+05	7.96	7.87	0.89	0.0	8.40	8.97	1.059	0.015	0.153
3.87	5118.89	16.27	8.98	0.15	0.0	16.03	9.00	2.868	0.004	0.002
2.85	5118.89	16.27	8.98	0.15	0.0	16.03	9.00	2.868	0.004	0.002
1.82	5118.89	16.27	8.98	0.15	0.0	16.03	9.00	2.868	0.004	0.002
0.80	7.074e+04	8.15	6.52	0.89	0.0	10.88	9.87	1.990	0.264	0.266
0.77	516.05	18.23	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.65	716.66	19.98	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.53	587.62	21.74	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.42	458.58	23.50	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.30	180.90	25.25	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Risulta	3.123e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	2.680	0.373	0.186	97.25	3.11e-02	2.466e+05	79.0	828.89	0.3	0.0	0.0
2	3.072	0.326	0.186	1.906e+05	61.0	0.11	3.40e-05	44.11	1.41e-02	0.0	0.0
3	4.249	0.235	0.186	6.967e+04	22.3	373.69	0.1	960.60	0.3	0.0	0.0
4	6.848	0.146	0.186	66.40	2.13e-02	19.17	6.14e-03	1.015e+04	3.2	0.0	0.0
5	7.224	0.138	0.186	116.02	3.71e-02	8122.48	2.6	9.041e+04	28.9	0.0	0.0
6	7.822	0.128	0.181	1468.02	0.5	1505.92	0.5	587.19	0.2	0.0	0.0
7	8.125	0.123	0.179	336.19	0.1	140.87	4.51e-02	8.713e+04	27.9	0.0	0.0
8	8.538	0.117	0.175	14.24	4.56e-03	421.30	0.1	1.117e+04	3.6	0.0	0.0
9	9.094	0.110	0.171	1282.22	0.4	258.18	8.27e-02	3.195e+04	10.2	0.0	0.0
10	10.368	0.096	0.164	2.28	7.29e-04	1740.17	0.6	3.294e+04	10.5	0.0	0.0
11	10.965	0.091	0.161	870.98	0.3	1257.67	0.4	3.716e+04	11.9	0.0	0.0
12	11.452	0.087	0.159	3062.88	1.0	3425.59	1.1	386.80	0.1	0.0	0.0
13	11.645	0.086	0.158	5002.39	1.6	183.70	5.88e-03	2.43e-03	0.0	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
							02		05		
14	11.807	0.085	0.157	6947.88	2.2	1032.45	0.3	3963.16	1.3	0.0	0.0
15	13.543	0.074	0.151	447.04	0.1	1.53	4.89e-04	339.35	0.1	0.0	0.0
16	13.635	0.073	0.151	715.08	0.2	1.601e+04	5.1	305.50	9.78e-02	0.0	0.0
17	14.335	0.070	0.149	1829.25	0.6	23.52	7.53e-03	0.16	5.01e-05	0.0	0.0
18	14.550	0.069	0.149	4476.68	1.4	2.440e+04	7.8	167.71	5.37e-02	0.0	0.0
19	15.036	0.067	0.147	1808.58	0.6	63.48	2.03e-02	34.60	1.11e-02	0.0	0.0
20	15.499	0.065	0.146	235.44	7.54e-02	947.14	0.3	17.53	5.61e-03	0.0	0.0
21	15.946	0.063	0.145	1.744e+04	5.6	3771.08	1.2	85.14	2.73e-02	0.0	0.0
22	16.671	0.060	0.144	2244.07	0.7	385.67	0.1	9.75	3.12e-03	0.0	0.0
23	17.434	0.057	0.142	1142.40	0.4	71.92	2.30e-02	1035.91	0.3	0.0	0.0
24	17.521	0.057	0.142	2290.40	0.7	588.55	0.2	1031.75	0.3	0.0	0.0
25	19.022	0.053	0.140	1.97	6.30e-04	28.99	9.28e-03	0.07	2.15e-05	0.0	0.0
26	19.114	0.052	0.140	5.09	1.63e-03	223.31	7.15e-02	9.03	2.89e-03	0.0	0.0
27	21.490	0.047	0.136	0.91	2.93e-04	0.03	1.04e-05	4.52	1.45e-03	0.0	0.0
28	22.877	0.044	0.135	1.57	5.03e-04	0.02	6.83e-06	9.54	3.05e-03	0.0	0.0
29	23.763	0.042	0.134	3.70	1.19e-03	134.84	4.32e-02	43.81	1.40e-02	0.0	0.0
30	24.223	0.041	0.133	19.93	6.38e-03	1.22e-03	0.0	8.31	2.66e-03	0.0	0.0
31	24.640	0.041	0.133	7.01	2.25e-03	71.61	2.29e-02	42.89	1.37e-02	0.0	0.0
32	25.122	0.040	0.133	10.50	3.36e-03	9.14e-03	2.93e-06	0.02	6.26e-06	0.0	0.0
33	25.484	0.039	0.132	45.21	1.45e-02	147.67	4.73e-02	3.96	1.27e-03	0.0	0.0
34	25.770	0.039	0.132	0.03	1.10e-05	11.28	3.61e-03	3.49	1.12e-03	0.0	0.0
35	27.273	0.037	0.131	1.15	3.67e-04	3.92	1.26e-03	8.54	2.74e-03	0.0	0.0
36	28.056	0.036	0.130	2.32	7.42e-04	69.30	2.22e-02	22.34	7.15e-03	0.0	0.0
37	28.209	0.035	0.130	9.07	2.90e-03	69.08	2.21e-02	1.90	6.10e-04	0.0	0.0
38	28.857	0.035	0.130	0.31	9.85e-05	10.20	3.27e-03	14.40	4.61e-03	0.0	0.0
39	29.293	0.034	0.129	0.13	4.30e-05	3.97	1.27e-03	1.73	5.55e-04	0.0	0.0
40	29.763	0.034	0.129	3.84	1.23e-03	11.25	3.60e-03	98.22	3.14e-02	0.0	0.0
41	30.668	0.033	0.129	2.43	7.79e-04	90.45	2.90e-02	8.01	2.56e-03	0.0	0.0
42	30.800	0.032	0.129	1.94	6.21e-04	3.13	1.00e-03	0.07	2.29e-05	0.0	0.0
43	32.302	0.031	0.128	2.81	9.00e-04	0.49	1.58e-04	2.96	9.47e-04	0.0	0.0
44	32.744	0.031	0.128	1.03	3.31e-04	0.21	6.81e-05	18.41	5.89e-03	0.0	0.0
45	33.393	0.030	0.127	0.22	7.00e-05	0.33	1.05e-04	1.66	5.33e-04	0.0	0.0
46	35.383	0.028	0.126	0.02	5.13e-06	4.55	1.46e-03	26.97	8.64e-03	0.0	0.0
47	36.310	0.028	0.126	1.76	5.65e-04	1.64	5.26e-04	154.20	4.94e-02	0.0	0.0
48	36.716	0.027	0.126	0.48	1.54e-04	0.24	7.77e-05	91.90	2.94e-02	0.0	0.0
49	37.435	0.027	0.125	0.02	7.31e-05	0.53	1.70e-05	7.36	2.36e-05	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
					06		04		03		
50	38.286	0.026	0.125	1.12	3.58e-04	0.42	1.34e-04	0.75	2.39e-04	0.0	0.0
51	39.653	0.025	0.125	0.02	6.46e-06	6.61e-03	2.12e-06	1.86	5.97e-04	0.0	0.0
52	40.867	0.024	0.124	0.82	2.63e-04	0.01	4.03e-06	190.40	6.10e-02	0.0	0.0
53	41.475	0.024	0.124	0.41	1.30e-04	0.50	1.61e-04	7.16	2.29e-03	0.0	0.0
54	41.749	0.024	0.124	0.21	6.88e-05	1.37	4.38e-04	71.12	2.28e-02	0.0	0.0
55	42.247	0.024	0.124	0.28	8.86e-05	0.34	1.08e-04	83.99	2.69e-02	0.0	0.0
56	42.631	0.023	0.124	1.34e-03	0.0	2.29	7.35e-04	158.43	5.07e-02	0.0	0.0
57	43.108	0.023	0.123	5.32e-04	0.0	1.93	6.19e-04	10.62	3.40e-03	0.0	0.0
58	44.171	0.023	0.123	0.03	9.24e-06	0.16	5.00e-05	6.24	2.00e-03	0.0	0.0
59	45.798	0.022	0.123	0.02	6.97e-06	0.10	3.09e-05	0.44	1.42e-04	0.0	0.0
60	46.844	0.021	0.122	0.01	4.76e-06	0.17	5.31e-05	12.95	4.15e-03	0.0	0.0
Risulta				3.123e+05		3.123e+05		3.118e+05			
In percentuale				99.99		99.98		99.85			

CDC	Tipo	Sigla Id	Note
10	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -)	
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.186 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.382 sec.
			fattore q: 1.500
			amplificazione ND (non dissipativi): 1.000
			fattore per spost. mu d: 1.536
			classe di duttilità CD: ND
			numero di modi considerati: 60
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
6.06	2.869e+04	11.37	2.08	-0.89	0.0	9.78	8.94	0.956	0.048	0.957
4.89	1.951e+05	7.96	7.87	-0.89	0.0	8.40	8.97	1.059	0.015	0.153
3.87	5118.89	16.27	8.98	-0.15	0.0	16.03	9.00	2.868	0.004	0.002
2.85	5118.89	16.27	8.98	-0.15	0.0	16.03	9.00	2.868	0.004	0.002
1.82	5118.89	16.27	8.98	-0.15	0.0	16.03	9.00	2.868	0.004	0.002
0.80	7.074e+04	8.15	6.52	-0.89	0.0	10.88	9.87	1.990	0.264	0.266
0.77	516.05	18.23	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.65	716.66	19.98	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.53	587.62	21.74	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.42	458.58	23.50	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.30	180.90	25.25	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Risulta	3.123e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	2.619	0.382	0.186	1.135e+04	3.6	2.254e+05	72.2	709.27	0.2	0.0	0.0
2	3.115	0.321	0.186	1.795e+05	57.5	2.059e+04	6.6	388.98	0.1	0.0	0.0
3	4.209	0.238	0.186	6.945e+04	22.2	1160.31	0.4	304.39	9.75e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
4	6.848	0.146	0.186	69.79	2.23e-02	24.29	7.78e-03	1.036e+04	3.3	0.0	0.0
5	7.229	0.138	0.186	77.40	2.48e-02	8275.59	2.6	9.271e+04	29.7	0.0	0.0
6	7.825	0.128	0.181	1528.00	0.5	1559.68	0.5	783.90	0.3	0.0	0.0
7	8.127	0.123	0.179	319.93	0.1	108.22	3.47e-02	8.507e+04	27.2	0.0	0.0
8	8.537	0.117	0.175	9.10	2.91e-03	444.08	0.1	1.090e+04	3.5	0.0	0.0
9	9.097	0.110	0.171	1225.80	0.4	338.18	0.1	3.028e+04	9.7	0.0	0.0
10	10.413	0.096	0.164	2.73	8.73e-04	4767.74	1.5	4.658e+04	14.9	0.0	0.0
11	11.094	0.090	0.160	510.53	0.2	431.10	0.1	2.333e+04	7.5	0.0	0.0
12	11.346	0.088	0.159	8618.27	2.8	4253.03	1.4	1828.90	0.6	0.0	0.0
13	11.712	0.085	0.158	0.02	6.74e-06	1209.69	0.4	4611.49	1.5	0.0	0.0
14	12.247	0.082	0.156	7754.66	2.5	251.29	8.05e-02	0.07	2.08e-05	0.0	0.0
15	13.473	0.074	0.152	1065.46	0.3	2978.02	1.0	308.03	9.86e-02	0.0	0.0
16	13.967	0.072	0.150	657.87	0.2	2235.42	0.7	315.14	0.1	0.0	0.0
17	14.396	0.069	0.149	1789.25	0.6	2255.53	0.7	1.94	6.22e-04	0.0	0.0
18	14.544	0.069	0.149	2.72e-04	0.0	2.574e+04	8.2	66.40	2.13e-02	0.0	0.0
19	15.197	0.066	0.147	1746.95	0.6	3102.12	1.0	19.06	6.10e-03	0.0	0.0
20	15.571	0.064	0.146	2918.50	0.9	3861.08	1.2	112.05	3.59e-02	0.0	0.0
21	15.788	0.063	0.146	1.828e+04	5.9	949.20	0.3	51.73	1.66e-02	0.0	0.0
22	16.874	0.059	0.143	1898.32	0.6	155.75	4.99e-02	8.09	2.59e-03	0.0	0.0
23	17.407	0.057	0.142	1972.31	0.6	48.25	1.54e-02	674.08	0.2	0.0	0.0
24	17.768	0.056	0.142	1371.40	0.4	1265.50	0.4	1268.48	0.4	0.0	0.0
25	19.017	0.053	0.140	1.35	4.31e-04	31.31	1.00e-02	1.56	5.00e-04	0.0	0.0
26	21.324	0.047	0.137	14.91	4.77e-03	29.18	9.34e-03	19.38	6.20e-03	0.0	0.0
27	22.195	0.045	0.136	3.27	1.05e-03	295.42	9.46e-02	5.53	1.77e-03	0.0	0.0
28	22.735	0.044	0.135	1.27	4.05e-04	0.31	1.01e-04	32.57	1.04e-02	0.0	0.0
29	23.806	0.042	0.134	14.27	4.57e-03	19.13	6.13e-03	92.18	2.95e-02	0.0	0.0
30	23.964	0.042	0.134	24.54	7.86e-03	11.44	3.66e-03	7.58	2.43e-03	0.0	0.0
31	24.421	0.041	0.133	0.17	5.37e-05	2.11	6.74e-04	16.00	5.12e-03	0.0	0.0
32	24.987	0.040	0.133	55.03	1.76e-02	2.55	8.17e-04	2.89	9.26e-04	0.0	0.0
33	25.966	0.039	0.132	5.51	1.76e-03	18.16	5.82e-03	0.08	2.45e-05	0.0	0.0
34	26.981	0.037	0.131	0.01	3.57e-06	9.41	3.01e-03	12.59	4.03e-03	0.0	0.0
35	27.135	0.037	0.131	0.08	2.62e-05	16.31	5.22e-03	0.40	1.29e-04	0.0	0.0
36	28.162	0.036	0.130	6.10	1.95e-03	1.09	3.49e-04	2.92	9.36e-04	0.0	0.0
37	28.311	0.035	0.130	3.54	1.13e-03	67.12	2.15e-02	18.94	6.06e-03	0.0	0.0
38	28.695	0.035	0.130	0.03	1.04e-05	23.87	7.64e-03	0.26	8.23e-05	0.0	0.0
39	29.698	0.034	0.129	0.79	2.53e-04	238.32	7.63e-02	69.72	2.23e-02	0.0	0.0
40	29.832	0.034	0.129	2.64	8.45e-04	8.76	2.80e-03	13.70	4.39e-03	0.0	0.0
41	30.649	0.033	0.129	0.32	1.01e-04	0.06	2.00e-05	0.42	1.35e-04	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
42	31.279	0.032	0.128	0.08	2.70e-05	3.21	1.03e-03	4.93	1.58e-03	0.0	0.0
43	32.433	0.031	0.128	7.00	2.24e-03	61.76	1.98e-02	36.59	1.17e-02	0.0	0.0
44	33.225	0.030	0.127	0.54	1.71e-04	1.94	6.22e-04	0.40	1.28e-04	0.0	0.0
45	34.636	0.029	0.127	0.06	1.97e-05	0.56	1.79e-04	0.24	7.69e-05	0.0	0.0
46	35.997	0.028	0.126	0.06	1.92e-05	2.24	7.16e-04	21.64	6.93e-03	0.0	0.0
47	36.311	0.028	0.126	1.15	3.69e-04	0.15	4.65e-05	38.87	1.24e-02	0.0	0.0
48	36.978	0.027	0.126	0.38	1.23e-04	0.23	7.37e-05	227.49	7.28e-02	0.0	0.0
49	37.979	0.026	0.125	1.11	3.54e-04	2.09	6.68e-04	0.07	2.12e-05	0.0	0.0
50	38.143	0.026	0.125	1.08	3.45e-04	1.69	5.40e-04	1.16	3.70e-04	0.0	0.0
51	40.098	0.025	0.124	0.01	4.03e-06	0.06	1.95e-05	2.12	6.79e-04	0.0	0.0
52	41.079	0.024	0.124	0.96	3.07e-04	2.73e-03	0.0	38.00	1.22e-02	0.0	0.0
53	41.162	0.024	0.124	0.50	1.60e-04	0.36	1.15e-04	215.89	6.91e-02	0.0	0.0
54	41.956	0.024	0.124	0.08	2.44e-05	0.96	3.06e-04	83.38	2.67e-02	0.0	0.0
55	42.446	0.024	0.124	2.24e-04	0.0	0.36	1.15e-04	39.85	1.28e-02	0.0	0.0
56	42.892	0.023	0.124	0.09	2.93e-05	0.21	6.58e-05	79.40	2.54e-02	0.0	0.0
57	43.869	0.023	0.123	0.16	5.21e-05	0.79	2.54e-04	61.56	1.97e-02	0.0	0.0
58	45.265	0.022	0.123	4.81e-03	1.54e-06	0.19	6.10e-05	1.30	4.16e-04	0.0	0.0
59	45.912	0.022	0.123	0.05	1.58e-05	0.06	1.92e-05	9.92	3.18e-03	0.0	0.0
60	46.246	0.022	0.123	0.03	9.83e-06	2.05	6.58e-04	3.15	1.01e-03	0.0	0.0
Risulta				3.123e+05		3.123e+05		3.118e+05			
In percentuale				99.99		99.98		99.85			

CDC	Tipo	Sigla Id	Note
11	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. +)	
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.120 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.338 sec.
			numero di modi considerati: 60
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
6.06	2.869e+04	11.37	2.08	0.0	-0.91	9.78	8.94	0.956	0.048	0.957
4.89	1.951e+05	7.96	7.87	0.0	-0.82	8.40	8.97	1.059	0.015	0.153
3.87	5118.89	16.27	8.98	0.0	-0.70	16.03	9.00	2.868	0.004	0.002
2.85	5118.89	16.27	8.98	0.0	-0.70	16.03	9.00	2.868	0.004	0.002
1.82	5118.89	16.27	8.98	0.0	-0.70	16.03	9.00	2.868	0.004	0.002
0.80	7.074e+04	8.15	6.52	0.0	-0.91	10.88	9.87	1.990	0.264	0.266
0.77	516.05	18.23	14.60	0.0	-0.11	0.0	0.0	0.0	0.0	0.0
0.65	716.66	19.98	14.60	0.0	-0.11	0.0	0.0	0.0	0.0	0.0
0.53	587.62	21.74	14.60	0.0	-0.11	0.0	0.0	0.0	0.0	0.0
0.42	458.58	23.50	14.60	0.0	-0.11	0.0	0.0	0.0	0.0	0.0
0.30	180.90	25.25	14.60	0.0	-0.11	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
Risulta	3.123e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	2.663	0.376	0.106	1.014e+04	3.2	2.327e+05	74.5	755.57	0.2	0.0	0.0
2	2.959	0.338	0.117	1.778e+05	56.9	1.439e+04	4.6	210.01	6.72e-02	0.0	0.0
3	4.428	0.226	0.120	7.177e+04	23.0	23.92	7.66e-03	743.03	0.2	0.0	0.0
4	6.848	0.146	0.120	70.61	2.26e-02	21.96	7.03e-03	1.029e+04	3.3	0.0	0.0
5	7.225	0.138	0.120	75.37	2.41e-02	8198.09	2.6	9.108e+04	29.2	0.0	0.0
6	7.828	0.128	0.120	1495.86	0.5	1508.67	0.5	727.56	0.2	0.0	0.0
7	8.125	0.123	0.120	415.65	0.1	124.10	3.97e-02	8.679e+04	27.8	0.0	0.0
8	8.537	0.117	0.120	19.12	6.12e-03	430.72	0.1	1.096e+04	3.5	0.0	0.0
9	9.109	0.110	0.120	1084.96	0.3	286.49	9.17e-02	3.096e+04	9.9	0.0	0.0
10	10.394	0.096	0.111	21.70	6.95e-03	2981.98	1.0	4.016e+04	12.9	0.0	0.0
11	11.052	0.090	0.107	1679.74	0.5	59.31	1.90e-02	3.017e+04	9.7	0.0	0.0
12	11.264	0.089	0.106	1.514e+04	4.8	512.57	0.2	1416.11	0.5	0.0	0.0
13	11.568	0.086	0.104	45.62	1.46e-02	4818.04	1.5	1470.17	0.5	0.0	0.0
14	11.883	0.084	0.103	3345.03	1.1	10.57	3.38e-03	2079.44	0.7	0.0	0.0
15	13.545	0.074	0.096	244.43	7.83e-02	1643.64	0.5	295.97	9.48e-02	0.0	0.0
16	13.767	0.073	0.095	1640.16	0.5	8250.09	2.6	321.02	0.1	0.0	0.0
17	14.353	0.070	0.093	1233.56	0.4	127.41	4.08e-02	2.20	7.06e-04	0.0	0.0
18	14.504	0.069	0.093	881.94	0.3	2.940e+04	9.4	133.31	4.27e-02	0.0	0.0
19	15.052	0.066	0.091	1184.84	0.4	2018.38	0.6	21.73	6.96e-03	0.0	0.0
20	15.524	0.064	0.090	56.55	1.81e-02	2254.74	0.7	36.70	1.18e-02	0.0	0.0
21	16.137	0.062	0.088	1.105e+04	3.5	667.83	0.2	50.09	1.60e-02	0.0	0.0
22	16.335	0.061	0.088	5679.33	1.8	2.67	8.55e-04	10.93	3.50e-03	0.0	0.0
23	17.443	0.057	0.085	3365.95	1.1	0.16	5.01e-05	756.21	0.2	0.0	0.0
24	17.731	0.056	0.084	3608.72	1.2	887.83	0.3	1273.89	0.4	0.0	0.0
25	19.022	0.053	0.082	0.87	2.79e-04	14.26	4.57e-03	1.19	3.81e-04	0.0	0.0
26	20.297	0.049	0.080	57.98	1.86e-02	333.79	0.1	10.45	3.35e-03	0.0	0.0
27	21.513	0.046	0.078	0.07	2.39e-05	15.57	4.98e-03	3.45	1.10e-03	0.0	0.0
28	22.833	0.044	0.076	1.19	3.81e-04	1.22	3.91e-04	10.98	3.52e-03	0.0	0.0
29	23.969	0.042	0.075	7.17e-04	0.0	46.06	1.47e-02	43.48	1.39e-02	0.0	0.0
30	24.429	0.041	0.074	19.21	6.15e-03	0.05	1.48e-05	47.99	1.54e-02	0.0	0.0
31	24.719	0.040	0.074	1.32	4.22e-04	1.46	4.69e-04	3.73	1.20e-03	0.0	0.0
32	25.063	0.040	0.073	72.06	2.31e-02	9.32	2.98e-03	1.84	5.90e-04	0.0	0.0
33	25.961	0.039	0.072	7.59	2.43e-03	14.44	4.62e-03	0.72	2.31e-04	0.0	0.0
34	26.686	0.037	0.072	23.62	7.56e-03	112.50	3.60e-02	12.56	4.02e-03	0.0	0.0
35	27.211	0.037	0.071	4.41	1.41e-	19.97	6.39e-	4.35	1.39e-	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
					03		03		03		
36	27.739	0.036	0.071	0.91	2.91e-04	173.09	5.54e-02	3.22	1.03e-03	0.0	0.0
37	29.001	0.034	0.070	4.55	1.46e-03	38.17	1.22e-02	4.59	1.47e-03	0.0	0.0
38	29.454	0.034	0.069	2.06	6.60e-04	36.48	1.17e-02	55.21	1.77e-02	0.0	0.0
39	29.821	0.034	0.069	3.55	1.14e-03	3.94	1.26e-03	52.65	1.69e-02	0.0	0.0
40	30.123	0.033	0.069	9.66	3.09e-03	43.48	1.39e-02	1.56	5.00e-04	0.0	0.0
41	32.107	0.031	0.067	4.47	1.43e-03	14.12	4.52e-03	5.10	1.63e-03	0.0	0.0
42	32.600	0.031	0.067	1.96	6.27e-04	32.99	1.06e-02	32.64	1.05e-02	0.0	0.0
43	33.374	0.030	0.067	0.45	1.45e-04	0.44	1.39e-04	0.06	1.85e-05	0.0	0.0
44	33.999	0.029	0.066	0.09	2.82e-05	0.17	5.39e-05	8.83	2.83e-03	0.0	0.0
45	34.751	0.029	0.066	0.33	1.05e-04	0.04	1.15e-05	0.35	1.12e-04	0.0	0.0
46	35.331	0.028	0.066	0.03	1.01e-05	2.42	7.75e-04	5.29	1.69e-03	0.0	0.0
47	36.570	0.027	0.065	1.21	3.86e-04	1.33	4.25e-04	251.27	8.05e-02	0.0	0.0
48	37.095	0.027	0.065	1.43	4.58e-04	0.98	3.14e-04	18.18	5.82e-03	0.0	0.0
49	37.360	0.027	0.065	0.95	3.04e-04	2.25	7.19e-04	0.07	2.20e-05	0.0	0.0
50	38.787	0.026	0.064	0.01	4.17e-06	0.02	4.84e-06	0.26	8.36e-05	0.0	0.0
51	39.411	0.025	0.064	0.11	3.63e-05	8.55e-03	2.74e-06	0.09	2.86e-05	0.0	0.0
52	40.734	0.025	0.063	0.63	2.00e-04	0.04	1.44e-05	92.24	2.95e-02	0.0	0.0
53	41.304	0.024	0.063	1.34	4.30e-04	0.61	1.94e-04	250.67	8.03e-02	0.0	0.0
54	41.910	0.024	0.063	0.20	6.47e-05	0.02	6.59e-06	8.37	2.68e-03	0.0	0.0
55	42.534	0.024	0.062	7.82e-03	2.50e-06	0.37	1.18e-04	70.35	2.25e-02	0.0	0.0
56	42.862	0.023	0.062	0.0	0.0	1.64	5.24e-04	29.37	9.40e-03	0.0	0.0
57	43.264	0.023	0.062	0.18	5.86e-05	2.26	7.25e-04	88.88	2.85e-02	0.0	0.0
58	44.840	0.022	0.062	0.21	6.77e-05	0.48	1.55e-04	13.67	4.38e-03	0.0	0.0
59	45.905	0.022	0.061	0.02	7.76e-06	0.12	3.77e-05	1.10	3.51e-04	0.0	0.0
60	46.336	0.022	0.061	4.45e-03	1.42e-06	0.27	8.77e-05	6.87e-05	0.0	0.0	0.0
Risulta				3.123e+05		3.123e+05		3.118e+05			
In percentuale				99.99		99.98		99.85			

CDC	Tipo	Sigla Id	Note
12	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. -)	
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.120 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.312 sec.
			numero di modi considerati: 60
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
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Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
6.06	2.869e+04	11.37	2.08	0.0	0.91	9.78	8.94	0.956	0.048	0.957
4.89	1.951e+05	7.96	7.87	0.0	0.82	8.40	8.97	1.059	0.015	0.153
3.87	5118.89	16.27	8.98	0.0	0.70	16.03	9.00	2.868	0.004	0.002
2.85	5118.89	16.27	8.98	0.0	0.70	16.03	9.00	2.868	0.004	0.002
1.82	5118.89	16.27	8.98	0.0	0.70	16.03	9.00	2.868	0.004	0.002
0.80	7.074e+04	8.15	6.52	0.0	0.91	10.88	9.87	1.990	0.264	0.266
0.77	516.05	18.23	14.60	0.0	0.11	0.0	0.0	0.0	0.0	0.0
0.65	716.66	19.98	14.60	0.0	0.11	0.0	0.0	0.0	0.0	0.0
0.53	587.62	21.74	14.60	0.0	0.11	0.0	0.0	0.0	0.0	0.0
0.42	458.58	23.50	14.60	0.0	0.11	0.0	0.0	0.0	0.0	0.0
0.30	180.90	25.25	14.60	0.0	0.11	0.0	0.0	0.0	0.0	0.0
Risulta	3.123e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	2.670	0.374	0.106	2425.76	0.8	2.429e+05	77.8	826.99	0.3	0.0	0.0
2	3.207	0.312	0.120	1.922e+05	61.5	4075.08	1.3	204.64	6.55e-02	0.0	0.0
3	4.015	0.249	0.120	6.630e+04	21.2	120.08	3.84e-02	444.63	0.1	0.0	0.0
4	6.848	0.146	0.120	66.84	2.14e-02	21.55	6.90e-03	1.026e+04	3.3	0.0	0.0
5	7.226	0.138	0.120	116.48	3.73e-02	8175.92	2.6	9.194e+04	29.4	0.0	0.0
6	7.819	0.128	0.120	1522.28	0.5	1533.57	0.5	589.14	0.2	0.0	0.0
7	8.127	0.123	0.120	251.47	8.05e-02	126.42	4.05e-02	8.562e+04	27.4	0.0	0.0
8	8.538	0.117	0.120	6.40	2.05e-03	425.51	0.1	1.113e+04	3.6	0.0	0.0
9	9.084	0.110	0.120	1469.02	0.5	284.78	9.12e-02	3.141e+04	10.1	0.0	0.0
10	10.432	0.096	0.111	33.95	1.09e-02	3256.57	1.0	4.487e+04	14.4	0.0	0.0
11	11.107	0.090	0.107	50.88	1.63e-02	2.17	6.93e-04	2.640e+04	8.5	0.0	0.0
12	11.607	0.086	0.104	1152.22	0.4	5413.52	1.7	2554.75	0.8	0.0	0.0
13	11.726	0.085	0.104	610.86	0.2	3.53	1.13e-03	947.72	0.3	0.0	0.0
14	12.056	0.083	0.102	1.071e+04	3.4	4.75	1.52e-03	521.05	0.2	0.0	0.0
15	13.475	0.074	0.096	1594.80	0.5	1414.47	0.5	453.53	0.1	0.0	0.0
16	13.870	0.072	0.095	199.69	6.39e-02	9444.12	3.0	180.13	5.77e-02	0.0	0.0
17	14.378	0.070	0.093	1660.99	0.5	1706.69	0.5	2.57	8.23e-04	0.0	0.0
18	14.530	0.069	0.093	1511.89	0.5	2.726e+04	8.7	139.47	4.47e-02	0.0	0.0
19	15.129	0.066	0.091	2.34	7.48e-04	791.04	0.3	6.26	2.00e-03	0.0	0.0
20	15.455	0.065	0.090	1.678e+04	5.4	15.30	4.90e-03	39.07	1.25e-02	0.0	0.0
21	15.557	0.064	0.090	9921.64	3.2	3076.90	1.0	162.42	5.20e-02	0.0	0.0
22	16.993	0.059	0.086	2862.63	0.9	610.28	0.2	7.77	2.49e-03	0.0	0.0
23	17.469	0.057	0.085	134.36	4.30e-02	233.04	7.46e-02	1563.49	0.5	0.0	0.0
24	17.798	0.056	0.084	589.48	0.2	423.60	0.1	424.44	0.1	0.0	0.0
25	19.023	0.053	0.082	5.49	1.76e-03	16.18	5.18e-03	1.18	3.79e-04	0.0	0.0
26	20.395	0.049	0.079	3.13	1.00e-03	314.20	0.1	14.21	4.55e-03	0.0	0.0
27	21.517	0.046	0.078	3.43	1.10e-03	16.72	5.35e-03	1.69	5.40e-04	0.0	0.0
28	22.765	0.044	0.076	0.58	1.87e-04	2.54	8.13e-04	30.27	9.69e-03	0.0	0.0
29	23.574	0.042	0.075	20.71	6.63e-03	26.25	8.41e-03	105.96	3.39e-03	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
					03		03		02		
30	23.845	0.042	0.075	14.29	4.58e-03	14.04	4.49e-03	3.05	9.76e-04	0.0	0.0
31	24.679	0.041	0.074	0.13	4.18e-05	1.26	4.04e-04	0.03	8.55e-06	0.0	0.0
32	24.911	0.040	0.073	36.83	1.18e-02	10.34	3.31e-03	5.21	1.67e-03	0.0	0.0
33	25.275	0.040	0.073	4.88	1.56e-03	0.02	6.64e-06	0.48	1.54e-04	0.0	0.0
34	26.170	0.038	0.072	4.25	1.36e-03	36.08	1.16e-02	0.18	5.68e-05	0.0	0.0
35	26.659	0.038	0.072	0.12	3.92e-05	104.95	3.36e-02	8.14	2.61e-03	0.0	0.0
36	27.114	0.037	0.071	0.75	2.39e-04	4.53	1.45e-03	4.45	1.42e-03	0.0	0.0
37	27.770	0.036	0.071	6.72e-03	2.15e-06	193.41	6.19e-02	5.28	1.69e-03	0.0	0.0
38	28.092	0.036	0.070	4.32	1.38e-03	1.43	4.56e-04	10.41	3.33e-03	0.0	0.0
39	28.984	0.035	0.070	0.86	2.76e-04	40.96	1.31e-02	22.20	7.11e-03	0.0	0.0
40	29.330	0.034	0.069	1.97	6.31e-04	0.48	1.55e-04	1.78	5.70e-04	0.0	0.0
41	29.812	0.034	0.069	0.50	1.59e-04	36.54	1.17e-02	71.51	2.29e-02	0.0	0.0
42	31.436	0.032	0.068	4.75	1.52e-03	70.76	2.27e-02	39.40	1.26e-02	0.0	0.0
43	32.474	0.031	0.067	0.47	1.49e-04	1.58	5.07e-04	0.27	8.77e-05	0.0	0.0
44	33.302	0.030	0.067	0.10	3.04e-05	0.68	2.16e-04	0.13	4.22e-05	0.0	0.0
45	34.388	0.029	0.066	0.26	8.38e-05	2.34	7.49e-04	0.33	1.05e-04	0.0	0.0
46	35.165	0.028	0.066	6.73e-04	0.0	1.47	4.71e-04	0.99	3.15e-04	0.0	0.0
47	36.019	0.028	0.065	5.85e-03	1.87e-06	2.92	9.35e-04	37.58	1.20e-02	0.0	0.0
48	36.677	0.027	0.065	1.59	5.09e-04	0.59	1.88e-04	245.12	7.85e-02	0.0	0.0
49	37.384	0.027	0.065	2.76	8.84e-04	3.87	1.24e-03	3.45	1.10e-03	0.0	0.0
50	38.492	0.026	0.064	0.04	1.34e-05	0.10	3.18e-05	0.07	2.30e-05	0.0	0.0
51	38.834	0.026	0.064	3.29e-03	1.05e-06	3.02e-04	0.0	0.35	1.11e-04	0.0	0.0
52	40.650	0.025	0.063	0.19	6.08e-05	0.15	4.89e-05	77.04	2.47e-02	0.0	0.0
53	41.088	0.024	0.063	0.08	2.64e-05	8.65e-03	2.77e-06	39.29	1.26e-02	0.0	0.0
54	41.476	0.024	0.063	0.41	1.32e-04	0.84	2.69e-04	163.75	5.24e-02	0.0	0.0
55	42.087	0.024	0.063	0.14	4.53e-05	2.71e-04	0.0	0.23	7.33e-05	0.0	0.0
56	42.809	0.023	0.062	7.43e-05	0.0	4.00	1.28e-03	239.11	7.66e-02	0.0	0.0
57	44.027	0.023	0.062	0.04	1.42e-05	1.04	3.32e-04	0.02	5.47e-06	0.0	0.0
58	44.991	0.022	0.062	0.07	2.35e-05	2.34e-05	0.0	6.79	2.17e-03	0.0	0.0
59	45.705	0.022	0.061	0.02	6.42e-06	0.37	1.19e-04	4.47	1.43e-03	0.0	0.0
60	46.005	0.022	0.061	0.02	5.97e-06	2.97e-03	0.0	0.35	1.11e-04	0.0	0.0
Risulta				3.123e+05		3.123e+05		3.118e+05			
In percentuale				99.99		99.98		99.84			

CDC	Tipo	Sigla Id	Note
13	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. +)	

CDC	Tipo	Sigla Id	Note
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.120 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.373 sec.
			numero di modi considerati: 60
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
6.06	2.869e+04	11.37	2.08	0.89	0.0	9.78	8.94	0.956	0.048	0.957
4.89	1.951e+05	7.96	7.87	0.89	0.0	8.40	8.97	1.059	0.015	0.153
3.87	5118.89	16.27	8.98	0.15	0.0	16.03	9.00	2.868	0.004	0.002
2.85	5118.89	16.27	8.98	0.15	0.0	16.03	9.00	2.868	0.004	0.002
1.82	5118.89	16.27	8.98	0.15	0.0	16.03	9.00	2.868	0.004	0.002
0.80	7.074e+04	8.15	6.52	0.89	0.0	10.88	9.87	1.990	0.264	0.266
0.77	516.05	18.23	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.65	716.66	19.98	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.53	587.62	21.74	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.42	458.58	23.50	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.30	180.90	25.25	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Risulta	3.123e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	2.680	0.373	0.106	97.25	3.11e-02	2.466e+05	79.0	828.89	0.3	0.0	0.0
2	3.072	0.326	0.120	1.906e+05	61.0	0.11	3.40e-05	44.11	1.41e-02	0.0	0.0
3	4.249	0.235	0.120	6.967e+04	22.3	373.69	0.1	960.60	0.3	0.0	0.0
4	6.848	0.146	0.120	66.40	2.13e-02	19.17	6.14e-03	1.015e+04	3.2	0.0	0.0
5	7.224	0.138	0.120	116.02	3.71e-02	8122.48	2.6	9.041e+04	28.9	0.0	0.0
6	7.822	0.128	0.120	1468.02	0.5	1505.92	0.5	587.19	0.2	0.0	0.0
7	8.125	0.123	0.120	336.19	0.1	140.87	4.51e-02	8.713e+04	27.9	0.0	0.0
8	8.538	0.117	0.120	14.24	4.56e-03	421.30	0.1	1.117e+04	3.6	0.0	0.0
9	9.094	0.110	0.120	1282.22	0.4	258.18	8.27e-02	3.195e+04	10.2	0.0	0.0
10	10.368	0.096	0.111	2.28	7.29e-04	1740.17	0.6	3.294e+04	10.5	0.0	0.0
11	10.965	0.091	0.108	870.98	0.3	1257.67	0.4	3.716e+04	11.9	0.0	0.0
12	11.452	0.087	0.105	3062.88	1.0	3425.59	1.1	386.80	0.1	0.0	0.0
13	11.645	0.086	0.104	5002.39	1.6	183.70	5.88e-02	0.08	2.43e-05	0.0	0.0
14	11.807	0.085	0.103	6947.88	2.2	1032.45	0.3	3963.16	1.3	0.0	0.0
15	13.543	0.074	0.096	447.04	0.1	1.53	4.89e-04	339.35	0.1	0.0	0.0
16	13.635	0.073	0.096	715.08	0.2	1.601e+04	5.1	305.50	9.78e-02	0.0	0.0
17	14.335	0.070	0.093	1829.25	0.6	23.52	7.53e-03	0.16	5.01e-05	0.0	0.0
18	14.550	0.069	0.093	4476.68	1.4	2.440e+04	7.8	167.71	5.37e-02	0.0	0.0
19	15.036	0.067	0.091	1808.58	0.6	63.48	2.03e-02	34.60	1.11e-02	0.0	0.0
20	15.499	0.065	0.090	235.44	7.54e-02	947.14	0.3	17.53	5.61e-03	0.0	0.0
21	15.946	0.063	0.089	1.744e+04	5.6	3771.08	1.2	85.14	2.73e-02	0.0	0.0
22	16.671	0.060	0.087	2244.07	0.7	385.67	0.1	9.75	3.12e-03	0.0	0.0
23	17.434	0.057	0.085	1142.40	0.4	71.92	2.30e-	1035.91	0.3	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
							02				
24	17.521	0.057	0.085	2290.40	0.7	588.55	0.2	1031.75	0.3	0.0	0.0
25	19.022	0.053	0.082	1.97	6.30e-04	28.99	9.28e-03	0.07	2.15e-05	0.0	0.0
26	19.114	0.052	0.082	5.09	1.63e-03	223.31	7.15e-02	9.03	2.89e-03	0.0	0.0
27	21.490	0.047	0.078	0.91	2.93e-04	0.03	1.04e-05	4.52	1.45e-03	0.0	0.0
28	22.877	0.044	0.076	1.57	5.03e-04	0.02	6.83e-06	9.54	3.05e-03	0.0	0.0
29	23.763	0.042	0.075	3.70	1.19e-03	134.84	4.32e-02	43.81	1.40e-02	0.0	0.0
30	24.223	0.041	0.074	19.93	6.38e-03	1.22e-03	0.0	8.31	2.66e-03	0.0	0.0
31	24.640	0.041	0.074	7.01	2.25e-03	71.61	2.29e-02	42.89	1.37e-02	0.0	0.0
32	25.122	0.040	0.073	10.50	3.36e-03	9.14e-03	2.93e-06	0.02	6.26e-06	0.0	0.0
33	25.484	0.039	0.073	45.21	1.45e-02	147.67	4.73e-02	3.96	1.27e-03	0.0	0.0
34	25.770	0.039	0.073	0.03	1.10e-05	11.28	3.61e-03	3.49	1.12e-03	0.0	0.0
35	27.273	0.037	0.071	1.15	3.67e-04	3.92	1.26e-03	8.54	2.74e-03	0.0	0.0
36	28.056	0.036	0.070	2.32	7.42e-04	69.30	2.22e-02	22.34	7.15e-03	0.0	0.0
37	28.209	0.035	0.070	9.07	2.90e-03	69.08	2.21e-02	1.90	6.10e-04	0.0	0.0
38	28.857	0.035	0.070	0.31	9.85e-05	10.20	3.27e-03	14.40	4.61e-03	0.0	0.0
39	29.293	0.034	0.069	0.13	4.30e-05	3.97	1.27e-03	1.73	5.55e-04	0.0	0.0
40	29.763	0.034	0.069	3.84	1.23e-03	11.25	3.60e-03	98.22	3.14e-02	0.0	0.0
41	30.668	0.033	0.068	2.43	7.79e-04	90.45	2.90e-02	8.01	2.56e-03	0.0	0.0
42	30.800	0.032	0.068	1.94	6.21e-04	3.13	1.00e-03	0.07	2.29e-05	0.0	0.0
43	32.302	0.031	0.067	2.81	9.00e-04	0.49	1.58e-04	2.96	9.47e-04	0.0	0.0
44	32.744	0.031	0.067	1.03	3.31e-04	0.21	6.81e-05	18.41	5.89e-03	0.0	0.0
45	33.393	0.030	0.067	0.22	7.00e-05	0.33	1.05e-04	1.66	5.33e-04	0.0	0.0
46	35.383	0.028	0.066	0.02	5.13e-06	4.55	1.46e-03	26.97	8.64e-03	0.0	0.0
47	36.310	0.028	0.065	1.76	5.65e-04	1.64	5.26e-04	154.20	4.94e-02	0.0	0.0
48	36.716	0.027	0.065	0.48	1.54e-04	0.24	7.77e-05	91.90	2.94e-02	0.0	0.0
49	37.435	0.027	0.065	0.02	7.31e-06	0.53	1.70e-04	7.36	2.36e-03	0.0	0.0
50	38.286	0.026	0.064	1.12	3.58e-04	0.42	1.34e-04	0.75	2.39e-04	0.0	0.0
51	39.653	0.025	0.064	0.02	6.46e-06	6.61e-03	2.12e-06	1.86	5.97e-04	0.0	0.0
52	40.867	0.024	0.063	0.82	2.63e-04	0.01	4.03e-06	190.40	6.10e-02	0.0	0.0
53	41.475	0.024	0.063	0.41	1.30e-04	0.50	1.61e-04	7.16	2.29e-03	0.0	0.0
54	41.749	0.024	0.063	0.21	6.88e-05	1.37	4.38e-04	71.12	2.28e-02	0.0	0.0
55	42.247	0.024	0.062	0.28	8.86e-05	0.34	1.08e-04	83.99	2.69e-02	0.0	0.0
56	42.631	0.023	0.062	1.34e-03	0.0	2.29	7.35e-04	158.43	5.07e-02	0.0	0.0
57	43.108	0.023	0.062	5.32e-04	0.0	1.93	6.19e-04	10.62	3.40e-03	0.0	0.0
58	44.171	0.023	0.062	0.03	9.24e-06	0.16	5.00e-05	6.24	2.00e-03	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
59	45.798	0.022	0.061	0.02	6.97e-06	0.10	3.09e-05	0.44	1.42e-04	0.0	0.0
60	46.844	0.021	0.061	0.01	4.76e-06	0.17	5.31e-05	12.95	4.15e-03	0.0	0.0
Risulta				3.123e+05		3.123e+05		3.118e+05			
In percentuale				99.99		99.98		99.85			

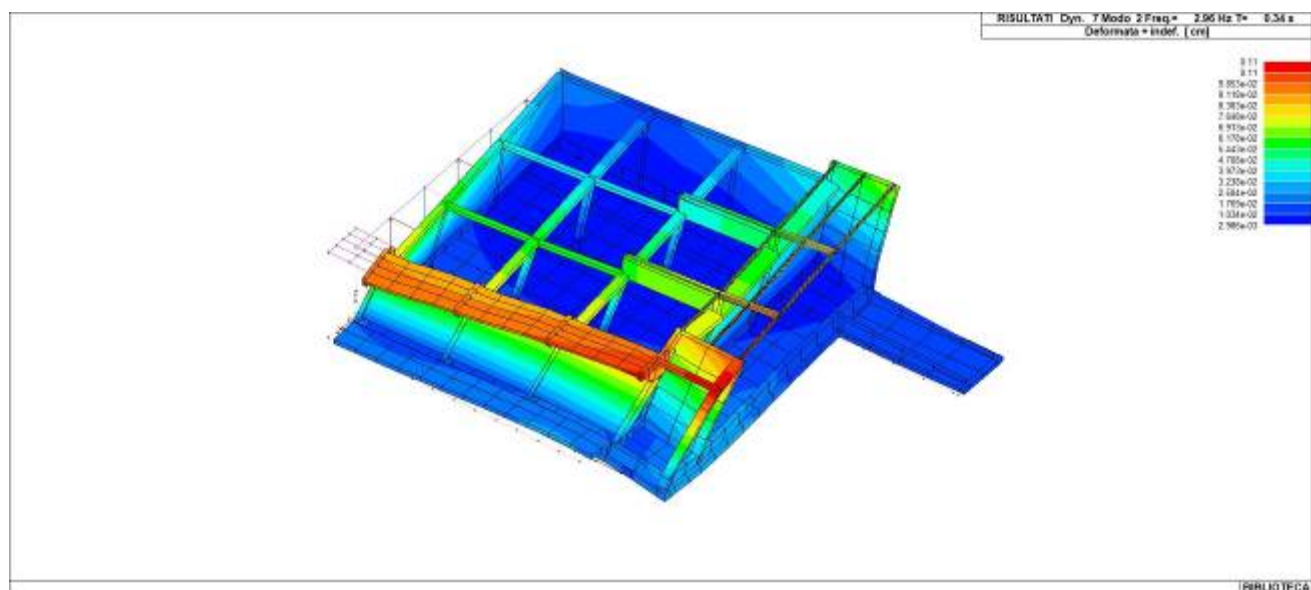
CDC	Tipo	Sigla Id	Note
14	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. -)	
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.120 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.382 sec.
			numero di modi considerati: 60
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
6.06	2.869e+04	11.37	2.08	-0.89	0.0	9.78	8.94	0.956	0.048	0.957
4.89	1.951e+05	7.96	7.87	-0.89	0.0	8.40	8.97	1.059	0.015	0.153
3.87	5118.89	16.27	8.98	-0.15	0.0	16.03	9.00	2.868	0.004	0.002
2.85	5118.89	16.27	8.98	-0.15	0.0	16.03	9.00	2.868	0.004	0.002
1.82	5118.89	16.27	8.98	-0.15	0.0	16.03	9.00	2.868	0.004	0.002
0.80	7.074e+04	8.15	6.52	-0.89	0.0	10.88	9.87	1.990	0.264	0.266
0.77	516.05	18.23	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.65	716.66	19.98	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.53	587.62	21.74	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.42	458.58	23.50	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.30	180.90	25.25	14.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Risulta	3.123e+05									

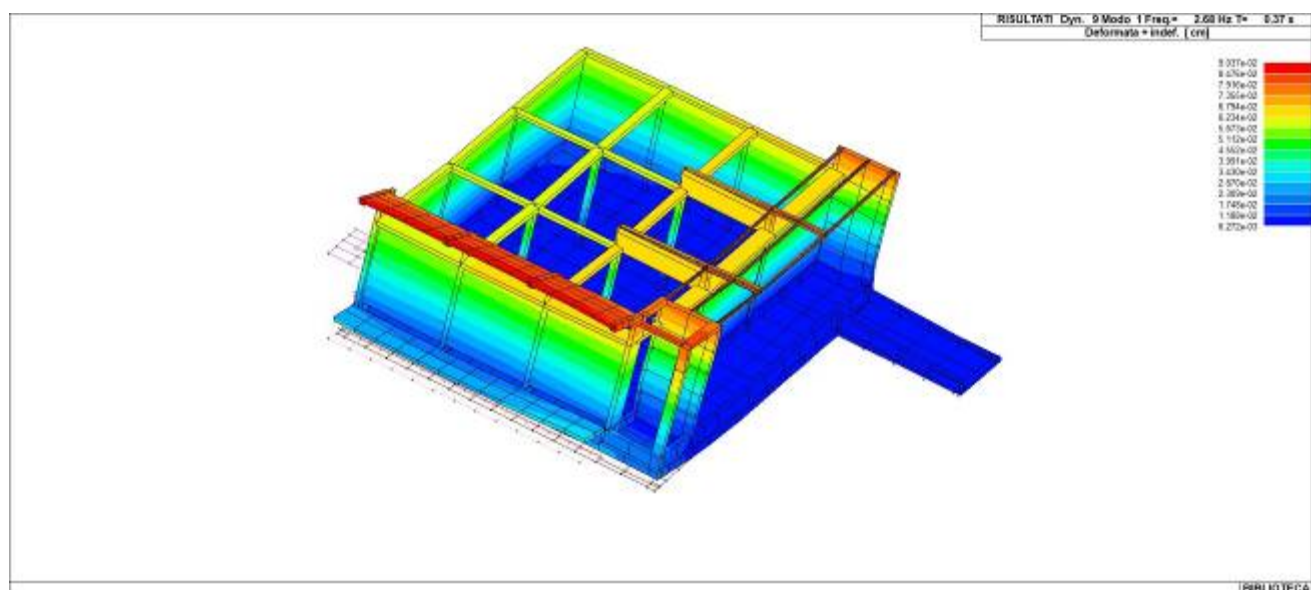
Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	2.619	0.382	0.104	1.135e+04	3.6	2.254e+05	72.2	709.27	0.2	0.0	0.0
2	3.115	0.321	0.120	1.795e+05	57.5	2.059e+04	6.6	388.98	0.1	0.0	0.0
3	4.209	0.238	0.120	6.945e+04	22.2	1160.31	0.4	304.39	9.75e-02	0.0	0.0
4	6.848	0.146	0.120	69.79	2.23e-02	24.29	7.78e-03	1.036e+04	3.3	0.0	0.0
5	7.229	0.138	0.120	77.40	2.48e-02	8275.59	2.6	9.271e+04	29.7	0.0	0.0
6	7.825	0.128	0.120	1528.00	0.5	1559.68	0.5	783.90	0.3	0.0	0.0
7	8.127	0.123	0.120	319.93	0.1	108.22	3.47e-02	8.507e+04	27.2	0.0	0.0
8	8.537	0.117	0.120	9.10	2.91e-03	444.08	0.1	1.090e+04	3.5	0.0	0.0
9	9.097	0.110	0.120	1225.80	0.4	338.18	0.1	3.028e+04	9.7	0.0	0.0
10	10.413	0.096	0.111	2.73	8.73e-04	4767.74	1.5	4.658e+04	14.9	0.0	0.0
11	11.094	0.090	0.107	510.53	0.2	431.10	0.1	2.333e+04	7.5	0.0	0.0
12	11.346	0.088	0.106	8618.27	2.8	4253.03	1.4	1828.90	0.6	0.0	0.0
13	11.712	0.085	0.104	0.02	6.74e-06	1209.69	0.4	4611.49	1.5	0.0	0.0
14	12.247	0.082	0.101	7754.66	2.5	251.29	8.05e-02	0.07	2.08e-05	0.0	0.0
15	13.473	0.074	0.096	1065.46	0.3	2978.02	1.0	308.03	9.86e-02	0.0	0.0
16	13.967	0.072	0.094	657.87	0.2	2235.42	0.7	315.14	0.1	0.0	0.0
17	14.396	0.069	0.093	1789.25	0.6	2255.53	0.7	1.94	6.22e-04	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
18	14.544	0.069	0.093	2.72e-04	0.0	2.574e+04	8.2	66.40	2.13e-02	0.0	0.0
19	15.197	0.066	0.091	1746.95	0.6	3102.12	1.0	19.06	6.10e-03	0.0	0.0
20	15.571	0.064	0.090	2918.50	0.9	3861.08	1.2	112.05	3.59e-02	0.0	0.0
21	15.788	0.063	0.089	1.828e+04	5.9	949.20	0.3	51.73	1.66e-02	0.0	0.0
22	16.874	0.059	0.086	1898.32	0.6	155.75	4.99e-02	8.09	2.59e-03	0.0	0.0
23	17.407	0.057	0.085	1972.31	0.6	48.25	1.54e-02	674.08	0.2	0.0	0.0
24	17.768	0.056	0.084	1371.40	0.4	1265.50	0.4	1268.48	0.4	0.0	0.0
25	19.017	0.053	0.082	1.35	4.31e-04	31.31	1.00e-02	1.56	5.00e-04	0.0	0.0
26	21.324	0.047	0.078	14.91	4.77e-03	29.18	9.34e-03	19.38	6.20e-03	0.0	0.0
27	22.195	0.045	0.077	3.27	1.05e-03	295.42	9.46e-02	5.53	1.77e-03	0.0	0.0
28	22.735	0.044	0.076	1.27	4.05e-04	0.31	1.01e-04	32.57	1.04e-02	0.0	0.0
29	23.806	0.042	0.075	14.27	4.57e-03	19.13	6.13e-03	92.18	2.95e-02	0.0	0.0
30	23.964	0.042	0.075	24.54	7.86e-03	11.44	3.66e-03	7.58	2.43e-03	0.0	0.0
31	24.421	0.041	0.074	0.17	5.37e-05	2.11	6.74e-04	16.00	5.12e-03	0.0	0.0
32	24.987	0.040	0.073	55.03	1.76e-02	2.55	8.17e-04	2.89	9.26e-04	0.0	0.0
33	25.966	0.039	0.072	5.51	1.76e-03	18.16	5.82e-03	0.08	2.45e-05	0.0	0.0
34	26.981	0.037	0.071	0.01	3.57e-06	9.41	3.01e-03	12.59	4.03e-03	0.0	0.0
35	27.135	0.037	0.071	0.08	2.62e-05	16.31	5.22e-03	0.40	1.29e-04	0.0	0.0
36	28.162	0.036	0.070	6.10	1.95e-03	1.09	3.49e-04	2.92	9.36e-04	0.0	0.0
37	28.311	0.035	0.070	3.54	1.13e-03	67.12	2.15e-02	18.94	6.06e-03	0.0	0.0
38	28.695	0.035	0.070	0.03	1.04e-05	23.87	7.64e-03	0.26	8.23e-05	0.0	0.0
39	29.698	0.034	0.069	0.79	2.53e-04	238.32	7.63e-02	69.72	2.23e-02	0.0	0.0
40	29.832	0.034	0.069	2.64	8.45e-04	8.76	2.80e-03	13.70	4.39e-03	0.0	0.0
41	30.649	0.033	0.068	0.32	1.01e-04	0.06	2.00e-05	0.42	1.35e-04	0.0	0.0
42	31.279	0.032	0.068	0.08	2.70e-05	3.21	1.03e-03	4.93	1.58e-03	0.0	0.0
43	32.433	0.031	0.067	7.00	2.24e-03	61.76	1.98e-02	36.59	1.17e-02	0.0	0.0
44	33.225	0.030	0.067	0.54	1.71e-04	1.94	6.22e-04	0.40	1.28e-04	0.0	0.0
45	34.636	0.029	0.066	0.06	1.97e-05	0.56	1.79e-04	0.24	7.69e-05	0.0	0.0
46	35.997	0.028	0.065	0.06	1.92e-05	2.24	7.16e-04	21.64	6.93e-03	0.0	0.0
47	36.311	0.028	0.065	1.15	3.69e-04	0.15	4.65e-05	38.87	1.24e-02	0.0	0.0
48	36.978	0.027	0.065	0.38	1.23e-04	0.23	7.37e-05	227.49	7.28e-02	0.0	0.0
49	37.979	0.026	0.064	1.11	3.54e-04	2.09	6.68e-04	0.07	2.12e-05	0.0	0.0
50	38.143	0.026	0.064	1.08	3.45e-04	1.69	5.40e-04	1.16	3.70e-04	0.0	0.0
51	40.098	0.025	0.063	0.01	4.03e-06	0.06	1.95e-05	2.12	6.79e-04	0.0	0.0
52	41.079	0.024	0.063	0.96	3.07e-04	2.73e-03	0.0	38.00	1.22e-02	0.0	0.0
53	41.162	0.024	0.063	0.50	1.60e-	0.36	1.15e-	215.89	6.91e-	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
54	41.956	0.024	0.063	0.08	2.44e-05	0.96	3.06e-04	83.38	2.67e-02	0.0	0.0
55	42.446	0.024	0.062	2.24e-04	0.0	0.36	1.15e-04	39.85	1.28e-02	0.0	0.0
56	42.892	0.023	0.062	0.09	2.93e-05	0.21	6.58e-05	79.40	2.54e-02	0.0	0.0
57	43.869	0.023	0.062	0.16	5.21e-05	0.79	2.54e-04	61.56	1.97e-02	0.0	0.0
58	45.265	0.022	0.061	4.81e-03	1.54e-06	0.19	6.10e-05	1.30	4.16e-04	0.0	0.0
59	45.912	0.022	0.061	0.05	1.58e-05	0.06	1.92e-05	9.92	3.18e-03	0.0	0.0
60	46.246	0.022	0.061	0.03	9.83e-06	2.05	6.58e-04	3.15	1.01e-03	0.0	0.0
Risulta				3.123e+05		3.123e+05		3.118e+05			
In percentuale				99.99		99.98		99.85			



31_RIS_MODALOX_002_CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)



31_RIS_MODALOY_001_CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)

RISULTATI OPERE DI FONDAZIONE

LEGENDA RISULTATI OPERE DI FONDAZIONE

Il controllo dei risultati delle analisi condotte, per quanto concerne le opere di fondazione, è possibile in relazione alle tabelle sotto riportate.

La prima tabella è riferita alle fondazioni tipo palo e plinto su pali.

Per questo tipo di fondazione vengono riportate le sei componenti di sollecitazione (esprese nel riferimento globale della struttura) per ogni palo componente l'opera.

In particolare viene riportato:

Nodo	numero del nodo a cui è applicato il plinto
Tipo	codice corrispondente al nome assegnato al tipo di plinto di fondazione: 3) palo singolo (<i>PALO</i>) 4) plinto su palo 5) plinto su due pali (<i>PL.2P</i>) 6) plinto su tre pali (<i>PL.3P</i>) 7) plinto su quattro pali (<i>PL.4P</i>) 8) plinto rettangolare su cinque pali (<i>PL.5P.R</i>) 9) plinto pentagonale su cinque pali (<i>PL.5P</i>) 10) plinto su sei pali (<i>PL.6P</i>)
Palo	numero del palo
Comb.	combinazione di carico in cui si verificano le sei componenti di sollecitazione.
Quota	quota assoluta della sezione del palo per cui si riportano le sei componenti di sollecitazione.

L'azione F_z (corrispondente allo sforzo normale nel palo) è costante poiché il peso del palo stesso non è considerato nella modellazione.

La seconda tabella è riferita alle fondazioni tipo plinto su suolo elastico.

Per questo tipo di fondazione vengono riportate le pressioni nei quattro vertici dell'impronta sul terreno.

In particolare viene riportato:

Nodo	numero del nodo a cui è applicato il plinto
Tipo	Codice identificativo del nome assegnato al plinto
area	area dell'impronta del plinto
Wink O Wink V	coefficienti di Winkler (orizzontale e verticale) adottati
Comb	Combinazione di carico in cui si verificano i valori riportati
Pt (P1 P2 P3 P4)	valori di pressione nei vertici

La terza tabella è riferita alle fondazioni tipo platea su suolo elastico.

Per questo tipo di fondazione vengono riportate le pressioni in ogni vertice (nodo) degli elementi costituenti la platea.

La quarta tabella è riferita alle fondazioni tipo trave su suolo elastico.

Per questo tipo di fondazione vengono riportate le pressioni alle estremità dell'elemento e la massima (in valore assoluto) pressione lungo lo sviluppo dell'elemento.

Vengono inoltre riportati, con funzione statistica, i valori massimo e minimo delle pressioni che compaiono nella tabella.

Nodo (G)	Pt 1/12	Pt 2/13	Pt 3...	Pt 4...							
	daN/cm ²	daN/cm ²	daN/cm ²	daN/cm ²	daN/cm ²	daN/cm ²	daN/cm ²	daN/cm ²	daN/cm ²	daN/cm ²	daN/cm ²
1	-0.59	-0.46	-0.44	-0.43	-0.41	-0.41					
2	-0.56	-0.43	-0.41	-0.41	-0.39	-0.39					
3	-0.55	-0.43	-0.41	-0.40	-0.38	-0.38					
4	-0.52	-0.42	-0.40	-0.39	-0.37	-0.36					
5	-0.50	-0.43	-0.40	-0.37	-0.36	-0.35					
6	-0.45	-0.39	-0.36	-0.34	-0.32	-0.32					
7	-0.48	-0.35	-0.34	-0.35	-0.34	-0.33					
8	-0.47	-0.33	-0.33	-0.35	-0.33	-0.32					
9	-0.41	-0.28	-0.28	-0.30	-0.28	-0.28					
10	-0.42	-0.30	-0.29	-0.31	-0.29	-0.29					
11	-0.42	-0.30	-0.30	-0.31	-0.29	-0.29					
12	-0.45	-0.32	-0.31	-0.33	-0.31	-0.30					
13	-0.40	-0.27	-0.27	-0.29	-0.27	-0.27					
14	-0.40	-0.28	-0.28	-0.30	-0.28	-0.27					
15	-0.38	-0.27	-0.26	-0.28	-0.26	-0.26					
16	-0.47	-0.36	-0.34	-0.34	-0.32	-0.32					

Nodo (G)	Pt 1/12	Pt 2/13	Pt 3...	Pt 4...							
17	-0.44	-0.33	-0.32	-0.32	-0.31	-0.30					
18	-0.42	-0.32	-0.31	-0.31	-0.30	-0.29					
19	-0.37	-0.28	-0.27	-0.27	-0.26	-0.26					
20	-0.31	-0.24	-0.23	-0.23	-0.22	-0.22					
21	-0.53	-0.44	-0.41	-0.40	-0.37	-0.37					
22	-0.54	-0.44	-0.41	-0.40	-0.38	-0.37					
23	-0.57	-0.46	-0.43	-0.42	-0.40	-0.39					
24	-0.59	-0.46	-0.44	-0.44	-0.41	-0.41					
25	-0.61	-0.49	-0.46	-0.45	-0.42	-0.42					
26	-0.62	-0.50	-0.47	-0.46	-0.43	-0.43					
27	-0.60	-0.48	-0.45	-0.44	-0.42	-0.41					
28	-0.58	-0.47	-0.44	-0.43	-0.41	-0.40					
29	-0.54	-0.46	-0.42	-0.40	-0.38	-0.38					
30	-0.51	-0.45	-0.41	-0.38	-0.36	-0.36					
31	-0.51	-0.45	-0.41	-0.38	-0.36	-0.36					
32	-0.50	-0.44	-0.40	-0.37	-0.35	-0.35					
33	-0.45	-0.40	-0.36	-0.33	-0.32	-0.31					
34	-0.34	-0.26	-0.25	-0.25	-0.24	-0.24					
35	-0.30	-0.24	-0.23	-0.23	-0.22	-0.21					
36	-0.31	-0.25	-0.24	-0.23	-0.22	-0.22					
37	-0.37	-0.28	-0.27	-0.28	-0.26	-0.26					
38	-0.43	-0.32	-0.31	-0.32	-0.30	-0.30					
39	-0.45	-0.33	-0.32	-0.33	-0.31	-0.31					
40	-0.48	-0.37	-0.35	-0.35	-0.33	-0.32					
41	-0.48	-0.37	-0.35	-0.35	-0.33	-0.32					
42	-0.48	-0.37	-0.35	-0.35	-0.33	-0.32					
43	-0.45	-0.33	-0.32	-0.33	-0.31	-0.31					
44	-0.48	-0.34	-0.34	-0.35	-0.33	-0.33					
45	-0.59	-0.46	-0.44	-0.44	-0.41	-0.41					
46	-0.61	-0.49	-0.46	-0.45	-0.43	-0.42					
47	-0.62	-0.50	-0.47	-0.46	-0.43	-0.43					
48	-0.53	-0.39	-0.38	-0.39	-0.37	-0.37					
49	-0.48	-0.35	-0.34	-0.35	-0.33	-0.33					
50	-0.47	-0.35	-0.34	-0.35	-0.33	-0.32					
51	-0.54	-0.40	-0.38	-0.39	-0.37	-0.37					
52	-0.30	-0.23	-0.22	-0.22	-0.21	-0.21					
53	-0.31	-0.24	-0.23	-0.23	-0.22	-0.22					
54	-0.14	-0.12	-0.11	-0.10	-0.10	-0.10					
55	-0.12	-0.09	-0.09	-0.09	-0.09	-0.08					
56	-0.14	-0.13	-0.12	-0.10	-0.10	-0.10					
57	-0.12	-0.09	-0.09	-0.09	-0.08	-0.08					
58	-0.30	-0.23	-0.22	-0.22	-0.21	-0.21					
59	-0.13	-0.12	-0.11	-0.09	-0.09	-0.09					
60	-0.12	-0.11	-0.10	-0.09	-0.09	-0.09					
61	-0.11	-0.08	-0.08	-0.08	-0.08	-0.08					
62	-0.10	-0.08	-0.08	-0.08	-0.07	-0.07					
63	-0.37	-0.27	-0.26	-0.27	-0.26	-0.25					
64	-0.37	-0.26	-0.26	-0.27	-0.26	-0.25					
65	-0.40	-0.29	-0.28	-0.29	-0.28	-0.27					
66	-0.40	-0.28	-0.28	-0.29	-0.28	-0.27					
67	-0.40	-0.29	-0.28	-0.30	-0.28	-0.27					
68	-0.40	-0.28	-0.28	-0.29	-0.28	-0.27					
69	-0.45	-0.33	-0.32	-0.33	-0.31	-0.31					
70	-0.45	-0.33	-0.32	-0.33	-0.31	-0.31					
71	-0.46	-0.34	-0.33	-0.33	-0.32	-0.31					
72	-0.46	-0.34	-0.33	-0.33	-0.32	-0.31					
73	-0.60	-0.48	-0.45	-0.44	-0.42	-0.41					
74	-0.61	-0.49	-0.46	-0.45	-0.43	-0.42					
75	-0.60	-0.47	-0.44	-0.44	-0.42	-0.41					
76	-0.61	-0.48	-0.46	-0.45	-0.42	-0.42					
77	-0.59	-0.47	-0.44	-0.44	-0.41	-0.41					
78	-0.61	-0.48	-0.45	-0.45	-0.42	-0.42					
79	-0.59	-0.46	-0.44	-0.43	-0.41	-0.40					
80	-0.60	-0.47	-0.45	-0.44	-0.42	-0.41					
81	-0.58	-0.46	-0.43	-0.43	-0.40	-0.40					
82	-0.59	-0.47	-0.44	-0.44	-0.41	-0.41					
83	-0.58	-0.46	-0.43	-0.43	-0.40	-0.40					
84	-0.59	-0.47	-0.44	-0.43	-0.41	-0.41					

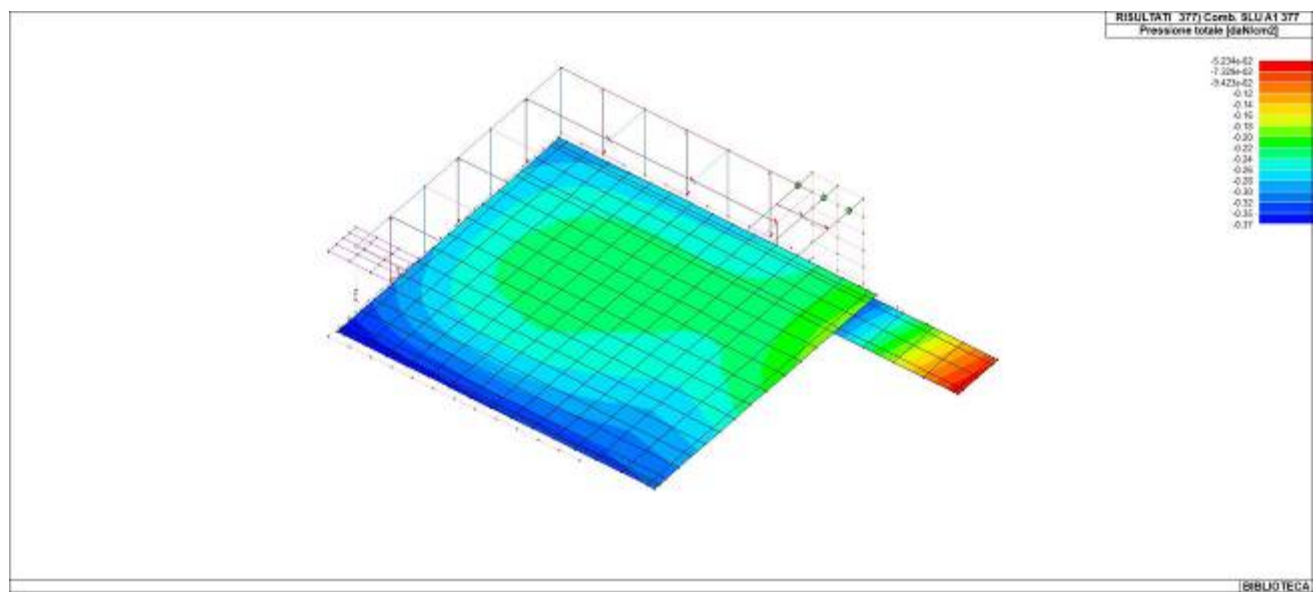
Nodo (G)	Pt 1/12	Pt 2/13	Pt 3...	Pt 4...						
85	-0.56	-0.45	-0.43	-0.42	-0.39	-0.39				
86	-0.57	-0.47	-0.44	-0.42	-0.40	-0.40				
87	-0.55	-0.45	-0.42	-0.41	-0.39	-0.38				
88	-0.56	-0.46	-0.43	-0.42	-0.40	-0.39				
89	-0.55	-0.45	-0.42	-0.40	-0.38	-0.38				
90	-0.55	-0.46	-0.43	-0.41	-0.39	-0.38				
91	-0.50	-0.44	-0.40	-0.38	-0.36	-0.36				
92	-0.52	-0.43	-0.40	-0.39	-0.37	-0.36				
93	-0.53	-0.44	-0.41	-0.39	-0.37	-0.37				
94	-0.50	-0.44	-0.40	-0.37	-0.36	-0.35				
95	-0.52	-0.43	-0.40	-0.38	-0.37	-0.36				
96	-0.57	-0.45	-0.43	-0.42	-0.40	-0.39				
97	-0.56	-0.45	-0.42	-0.41	-0.39	-0.39				
98	-0.55	-0.45	-0.42	-0.41	-0.39	-0.38				
99	-0.54	-0.44	-0.42	-0.40	-0.38	-0.38				
100	-0.58	-0.46	-0.43	-0.43	-0.41	-0.40				
101	-0.58	-0.45	-0.43	-0.43	-0.40	-0.40				
102	-0.57	-0.45	-0.43	-0.42	-0.40	-0.40				
103	-0.57	-0.45	-0.43	-0.42	-0.40	-0.39				
104	-0.61	-0.48	-0.45	-0.45	-0.42	-0.42				
105	-0.60	-0.47	-0.45	-0.44	-0.42	-0.41				
106	-0.59	-0.46	-0.44	-0.44	-0.41	-0.41				
107	-0.59	-0.46	-0.44	-0.43	-0.41	-0.40				
108	-0.61	-0.49	-0.46	-0.45	-0.42	-0.42				
109	-0.58	-0.45	-0.43	-0.43	-0.40	-0.40				
110	-0.57	-0.44	-0.42	-0.42	-0.40	-0.39				
111	-0.57	-0.44	-0.42	-0.42	-0.39	-0.39				
112	-0.56	-0.43	-0.41	-0.41	-0.39	-0.38				
113	-0.55	-0.43	-0.41	-0.41	-0.38	-0.38				
114	-0.55	-0.43	-0.41	-0.40	-0.38	-0.38				
115	-0.54	-0.43	-0.40	-0.40	-0.38	-0.37				
116	-0.53	-0.42	-0.40	-0.40	-0.37	-0.37				
117	-0.53	-0.42	-0.40	-0.39	-0.37	-0.37				
118	-0.49	-0.42	-0.39	-0.37	-0.35	-0.35				
119	-0.51	-0.41	-0.39	-0.38	-0.36	-0.35				
120	-0.49	-0.42	-0.39	-0.36	-0.35	-0.34				
121	-0.56	-0.42	-0.41	-0.41	-0.39	-0.38				
122	-0.56	-0.43	-0.41	-0.41	-0.39	-0.39				
123	-0.54	-0.41	-0.39	-0.40	-0.38	-0.37				
124	-0.51	-0.37	-0.37	-0.38	-0.36	-0.35				
125	-0.53	-0.40	-0.38	-0.39	-0.37	-0.36				
126	-0.49	-0.36	-0.35	-0.36	-0.34	-0.34				
127	-0.52	-0.39	-0.38	-0.38	-0.36	-0.36				
128	-0.48	-0.35	-0.34	-0.36	-0.34	-0.33				
129	-0.52	-0.39	-0.37	-0.38	-0.36	-0.36				
130	-0.51	-0.38	-0.37	-0.38	-0.36	-0.35				
131	-0.47	-0.34	-0.34	-0.35	-0.33	-0.32				
132	-0.51	-0.38	-0.37	-0.37	-0.35	-0.35				
133	-0.47	-0.34	-0.33	-0.35	-0.33	-0.32				
134	-0.51	-0.38	-0.37	-0.37	-0.35	-0.35				
135	-0.47	-0.34	-0.34	-0.35	-0.33	-0.32				
136	-0.51	-0.38	-0.37	-0.37	-0.35	-0.35				
137	-0.50	-0.38	-0.37	-0.37	-0.35	-0.35				
138	-0.47	-0.35	-0.34	-0.35	-0.33	-0.33				
139	-0.50	-0.38	-0.37	-0.37	-0.35	-0.35				
140	-0.47	-0.35	-0.34	-0.35	-0.33	-0.33				
141	-0.50	-0.39	-0.37	-0.37	-0.35	-0.35				
142	-0.48	-0.35	-0.34	-0.35	-0.34	-0.33				
143	-0.50	-0.38	-0.37	-0.37	-0.35	-0.35				
144	-0.48	-0.39	-0.37	-0.36	-0.34	-0.34				
145	-0.46	-0.36	-0.35	-0.35	-0.33	-0.32				
146	-0.47	-0.40	-0.37	-0.35	-0.33	-0.33				
147	-0.47	-0.41	-0.38	-0.35	-0.33	-0.33				
148	-0.51	-0.37	-0.36	-0.38	-0.36	-0.35				
149	-0.51	-0.36	-0.36	-0.37	-0.35	-0.35				
150	-0.50	-0.35	-0.35	-0.36	-0.34	-0.34				
151	-0.49	-0.35	-0.34	-0.36	-0.34	-0.33				
152	-0.48	-0.35	-0.34	-0.35	-0.34	-0.33				

Nodo (G)	Pt 1/12	Pt 2/13	Pt 3...	Pt 4...							
153	-0.46	-0.33	-0.32	-0.34	-0.32	-0.32					
154	-0.44	-0.31	-0.31	-0.33	-0.31	-0.30					
155	-0.46	-0.33	-0.33	-0.34	-0.32	-0.32					
156	-0.44	-0.31	-0.31	-0.32	-0.31	-0.30					
157	-0.42	-0.30	-0.29	-0.31	-0.30	-0.29					
158	-0.45	-0.32	-0.32	-0.33	-0.31	-0.31					
159	-0.43	-0.30	-0.30	-0.32	-0.30	-0.29					
160	-0.41	-0.29	-0.29	-0.30	-0.29	-0.28					
161	-0.44	-0.31	-0.31	-0.33	-0.31	-0.30					
162	-0.42	-0.29	-0.29	-0.31	-0.29	-0.29					
163	-0.44	-0.31	-0.31	-0.32	-0.31	-0.30					
164	-0.42	-0.29	-0.29	-0.31	-0.29	-0.29					
165	-0.40	-0.28	-0.28	-0.30	-0.28	-0.27					
166	-0.44	-0.31	-0.31	-0.32	-0.31	-0.30					
167	-0.42	-0.29	-0.29	-0.31	-0.29	-0.29					
168	-0.40	-0.28	-0.28	-0.30	-0.28	-0.27					
169	-0.44	-0.31	-0.31	-0.33	-0.31	-0.30					
170	-0.42	-0.30	-0.29	-0.31	-0.29	-0.29					
171	-0.41	-0.29	-0.28	-0.30	-0.28	-0.28					
172	-0.44	-0.32	-0.31	-0.33	-0.31	-0.31					
173	-0.43	-0.30	-0.30	-0.32	-0.30	-0.29					
174	-0.45	-0.32	-0.32	-0.33	-0.31	-0.31					
175	-0.43	-0.31	-0.30	-0.32	-0.30	-0.30					
176	-0.42	-0.30	-0.29	-0.31	-0.29	-0.29					
177	-0.45	-0.33	-0.32	-0.33	-0.32	-0.31					
178	-0.43	-0.31	-0.30	-0.32	-0.30	-0.30					
179	-0.42	-0.30	-0.29	-0.31	-0.29	-0.29					
180	-0.45	-0.33	-0.32	-0.34	-0.32	-0.31					
181	-0.44	-0.31	-0.30	-0.32	-0.31	-0.30					
182	-0.42	-0.30	-0.29	-0.31	-0.29	-0.29					
183	-0.45	-0.32	-0.32	-0.34	-0.32	-0.32					
184	-0.44	-0.31	-0.31	-0.32	-0.31	-0.30					
185	-0.43	-0.37	-0.34	-0.32	-0.30	-0.30					
186	-0.44	-0.34	-0.33	-0.33	-0.31	-0.31					
187	-0.40	-0.34	-0.32	-0.30	-0.29	-0.28					
188	-0.42	-0.33	-0.31	-0.31	-0.30	-0.29					
189	-0.38	-0.32	-0.30	-0.28	-0.27	-0.27					
190	-0.40	-0.31	-0.30	-0.30	-0.28	-0.28					
191	-0.42	-0.37	-0.34	-0.32	-0.30	-0.30					
192	-0.40	-0.35	-0.32	-0.30	-0.28	-0.28					
193	-0.37	-0.32	-0.30	-0.28	-0.27	-0.26					
194	-0.47	-0.33	-0.33	-0.34	-0.32	-0.32					
195	-0.46	-0.33	-0.32	-0.33	-0.32	-0.31					
196	-0.46	-0.33	-0.32	-0.33	-0.32	-0.31					
197	-0.45	-0.32	-0.32	-0.33	-0.31	-0.31					
198	-0.45	-0.33	-0.32	-0.33	-0.31	-0.31					
199	-0.45	-0.32	-0.31	-0.33	-0.31	-0.30					
200	-0.43	-0.30	-0.30	-0.32	-0.30	-0.29					
201	-0.42	-0.30	-0.30	-0.31	-0.29	-0.29					
202	-0.42	-0.30	-0.29	-0.31	-0.29	-0.29					
203	-0.42	-0.30	-0.30	-0.31	-0.29	-0.29					
204	-0.41	-0.29	-0.29	-0.30	-0.29	-0.28					
205	-0.41	-0.28	-0.28	-0.30	-0.28	-0.28					
206	-0.40	-0.28	-0.28	-0.30	-0.28	-0.27					
207	-0.41	-0.29	-0.28	-0.30	-0.28	-0.28					
208	-0.40	-0.28	-0.28	-0.30	-0.28	-0.27					
209	-0.40	-0.27	-0.27	-0.29	-0.27	-0.27					
210	-0.40	-0.27	-0.27	-0.29	-0.27	-0.27					
211	-0.40	-0.28	-0.27	-0.29	-0.28	-0.27					
212	-0.40	-0.27	-0.27	-0.29	-0.27	-0.27					
213	-0.39	-0.27	-0.27	-0.29	-0.27	-0.26					
214	-0.39	-0.27	-0.27	-0.29	-0.27	-0.26					
215	-0.39	-0.27	-0.27	-0.29	-0.27	-0.27					
216	-0.39	-0.27	-0.27	-0.29	-0.27	-0.26					
217	-0.39	-0.27	-0.26	-0.29	-0.27	-0.26					
218	-0.39	-0.27	-0.27	-0.29	-0.27	-0.26					
219	-0.39	-0.27	-0.27	-0.29	-0.27	-0.27					
220	-0.39	-0.27	-0.27	-0.29	-0.27	-0.26					

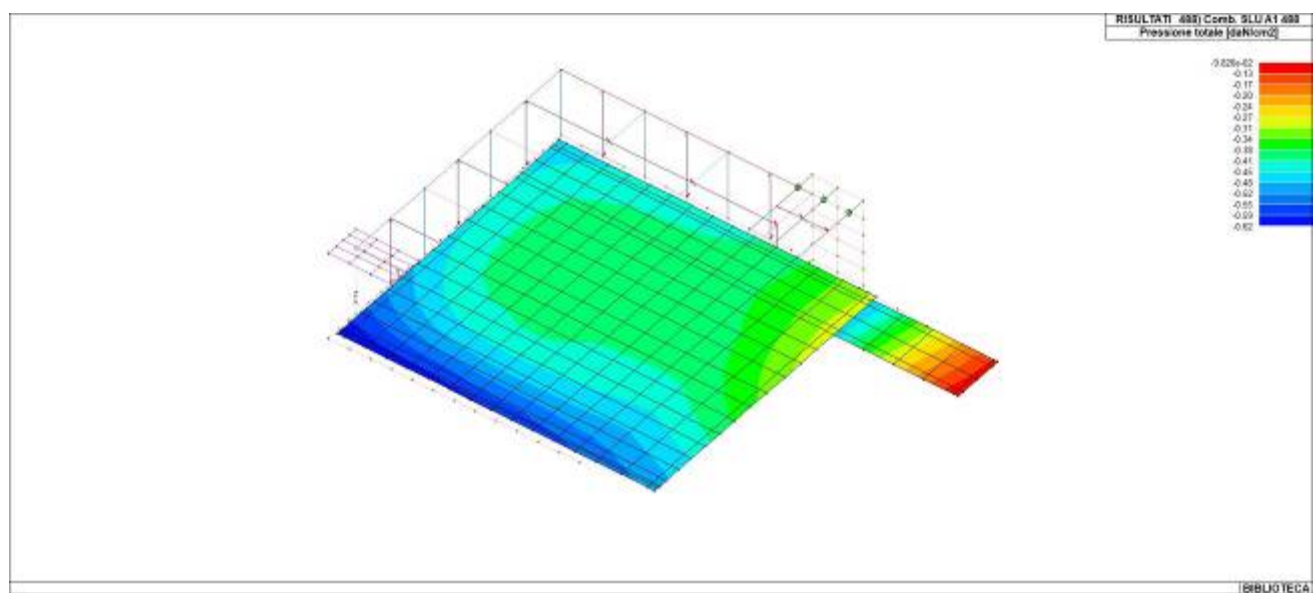
Nodo (G)	Pt 1/12	Pt 2/13	Pt 3...	Pt 4...						
221	-0.39	-0.27	-0.27	-0.29	-0.27	-0.26				
222	-0.39	-0.27	-0.27	-0.29	-0.27	-0.26				
223	-0.40	-0.28	-0.28	-0.29	-0.28	-0.27				
224	-0.39	-0.27	-0.27	-0.29	-0.27	-0.27				
225	-0.39	-0.27	-0.27	-0.29	-0.27	-0.27				
226	-0.40	-0.27	-0.27	-0.29	-0.27	-0.27				
227	-0.41	-0.28	-0.28	-0.30	-0.28	-0.28				
228	-0.40	-0.28	-0.27	-0.29	-0.28	-0.27				
229	-0.40	-0.28	-0.27	-0.29	-0.28	-0.27				
230	-0.41	-0.29	-0.28	-0.30	-0.28	-0.28				
231	-0.40	-0.28	-0.28	-0.30	-0.28	-0.27				
232	-0.40	-0.28	-0.27	-0.29	-0.28	-0.27				
233	-0.40	-0.28	-0.27	-0.29	-0.28	-0.27				
234	-0.41	-0.29	-0.28	-0.30	-0.28	-0.28				
235	-0.40	-0.28	-0.28	-0.30	-0.28	-0.27				
236	-0.40	-0.28	-0.27	-0.29	-0.27	-0.27				
237	-0.39	-0.28	-0.27	-0.29	-0.27	-0.27				
238	-0.41	-0.29	-0.28	-0.30	-0.28	-0.28				
239	-0.40	-0.28	-0.28	-0.29	-0.28	-0.27				
240	-0.39	-0.28	-0.27	-0.29	-0.27	-0.27				
241	-0.39	-0.27	-0.27	-0.29	-0.27	-0.26				
242	-0.40	-0.29	-0.28	-0.30	-0.28	-0.28				
243	-0.39	-0.28	-0.28	-0.29	-0.27	-0.27				
244	-0.38	-0.27	-0.27	-0.28	-0.27	-0.26				
245	-0.36	-0.30	-0.28	-0.27	-0.26	-0.25				
246	-0.39	-0.29	-0.28	-0.29	-0.27	-0.27				
247	-0.34	-0.27	-0.26	-0.26	-0.24	-0.24				
248	-0.37	-0.28	-0.27	-0.28	-0.26	-0.26				
249	-0.33	-0.25	-0.24	-0.24	-0.23	-0.23				
250	-0.36	-0.27	-0.26	-0.27	-0.25	-0.25				
251	-0.32	-0.24	-0.23	-0.23	-0.22	-0.22				
252	-0.35	-0.26	-0.25	-0.26	-0.25	-0.24				
253	-0.35	-0.30	-0.28	-0.26	-0.25	-0.25				
254	-0.33	-0.27	-0.26	-0.25	-0.24	-0.23				
255	-0.32	-0.25	-0.24	-0.24	-0.22	-0.22				
256	-0.30	-0.24	-0.23	-0.23	-0.22	-0.21				
257	-0.45	-0.33	-0.32	-0.33	-0.31	-0.31				
258	-0.45	-0.33	-0.32	-0.33	-0.31	-0.30				
259	-0.43	-0.31	-0.30	-0.31	-0.29	-0.29				
260	-0.43	-0.31	-0.30	-0.32	-0.30	-0.29				
261	-0.41	-0.29	-0.28	-0.30	-0.28	-0.28				
262	-0.42	-0.30	-0.29	-0.30	-0.29	-0.28				
263	-0.40	-0.28	-0.28	-0.29	-0.28	-0.27				
264	-0.41	-0.29	-0.28	-0.30	-0.28	-0.28				
265	-0.40	-0.28	-0.27	-0.29	-0.27	-0.27				
266	-0.39	-0.27	-0.27	-0.29	-0.27	-0.27				
267	-0.40	-0.28	-0.28	-0.29	-0.28	-0.27				
268	-0.39	-0.27	-0.27	-0.29	-0.27	-0.27				
269	-0.40	-0.28	-0.28	-0.29	-0.28	-0.27				
270	-0.39	-0.28	-0.27	-0.29	-0.27	-0.27				
271	-0.40	-0.28	-0.28	-0.29	-0.28	-0.27				
272	-0.40	-0.28	-0.28	-0.29	-0.28	-0.27				
273	-0.40	-0.28	-0.27	-0.29	-0.27	-0.27				
274	-0.39	-0.28	-0.28	-0.29	-0.27	-0.27				
275	-0.39	-0.28	-0.27	-0.29	-0.27	-0.27				
276	-0.39	-0.28	-0.27	-0.29	-0.27	-0.27				
277	-0.38	-0.27	-0.27	-0.28	-0.27	-0.26				
278	-0.38	-0.27	-0.27	-0.28	-0.27	-0.26				
279	-0.37	-0.27	-0.26	-0.28	-0.26	-0.26				
280	-0.34	-0.25	-0.24	-0.26	-0.24	-0.24				
281	-0.34	-0.25	-0.24	-0.25	-0.24	-0.24				
282	-0.31	-0.23	-0.22	-0.23	-0.22	-0.21				
283	-0.29	-0.22	-0.22	-0.22	-0.21	-0.21				
284	-0.48	-0.36	-0.35	-0.35	-0.34	-0.33				
285	-0.43	-0.32	-0.31	-0.32	-0.30	-0.30				
286	-0.42	-0.30	-0.29	-0.31	-0.29	-0.29				
287	-0.41	-0.29	-0.29	-0.30	-0.28	-0.28				
288	-0.40	-0.28	-0.28	-0.29	-0.28	-0.27				

Nodo (G)	Pt 1/12	Pt 2/13	Pt 3...	Pt 4...							
289	-0.40	-0.28	-0.28	-0.29	-0.28	-0.27					
290	-0.40	-0.28	-0.28	-0.29	-0.28	-0.27					
291	-0.40	-0.28	-0.28	-0.29	-0.28	-0.27					
292	-0.39	-0.28	-0.28	-0.29	-0.27	-0.27					
293	-0.38	-0.27	-0.27	-0.28	-0.27	-0.26					
294	-0.34	-0.25	-0.24	-0.25	-0.24	-0.24					
295	-0.48	-0.36	-0.35	-0.35	-0.34	-0.33					
296	-0.37	-0.29	-0.28	-0.28	-0.27	-0.26					
297	-0.37	-0.28	-0.28	-0.28	-0.27	-0.26					
298	-0.28	-0.22	-0.21	-0.21	-0.20	-0.20					
299	-0.27	-0.21	-0.20	-0.20	-0.20	-0.19					
300	-0.19	-0.15	-0.15	-0.14	-0.14	-0.14					
301	-0.19	-0.14	-0.14	-0.14	-0.14	-0.13					
302	-0.37	-0.28	-0.27	-0.27	-0.26	-0.26					
303	-0.42	-0.31	-0.30	-0.31	-0.29	-0.29					
304	-0.44	-0.32	-0.31	-0.32	-0.30	-0.30					
305	-0.47	-0.36	-0.34	-0.34	-0.32	-0.32					
306	-0.47	-0.36	-0.34	-0.35	-0.33	-0.32					
307	-0.47	-0.35	-0.33	-0.34	-0.32	-0.32					
308	-0.46	-0.35	-0.33	-0.34	-0.32	-0.31					
309	-0.45	-0.33	-0.32	-0.32	-0.31	-0.30					
310	-0.46	-0.35	-0.33	-0.33	-0.32	-0.31					
311	-0.43	-0.32	-0.31	-0.32	-0.30	-0.29					
312	-0.45	-0.33	-0.32	-0.33	-0.31	-0.31					
313	-0.42	-0.31	-0.30	-0.31	-0.29	-0.29					
314	-0.44	-0.33	-0.31	-0.32	-0.31	-0.30					
315	-0.42	-0.30	-0.29	-0.31	-0.29	-0.28					
316	-0.41	-0.30	-0.29	-0.30	-0.29	-0.28					
317	-0.43	-0.32	-0.31	-0.32	-0.30	-0.30					
318	-0.41	-0.30	-0.29	-0.30	-0.29	-0.28					
319	-0.43	-0.31	-0.31	-0.31	-0.30	-0.29					
320	-0.41	-0.30	-0.29	-0.30	-0.28	-0.28					
321	-0.43	-0.31	-0.31	-0.31	-0.30	-0.29					
322	-0.41	-0.30	-0.29	-0.30	-0.28	-0.28					
323	-0.40	-0.29	-0.29	-0.30	-0.28	-0.28					
324	-0.41	-0.31	-0.30	-0.30	-0.29	-0.28					
325	-0.39	-0.29	-0.28	-0.29	-0.28	-0.27					
326	-0.40	-0.30	-0.29	-0.30	-0.28	-0.28					
327	-0.38	-0.28	-0.27	-0.28	-0.27	-0.26					
328	-0.39	-0.29	-0.28	-0.29	-0.27	-0.27					
329	-0.37	-0.27	-0.26	-0.27	-0.26	-0.25					
330	-0.34	-0.25	-0.24	-0.25	-0.24	-0.24					
331	-0.34	-0.25	-0.25	-0.25	-0.24	-0.24					
332	-0.30	-0.23	-0.22	-0.23	-0.22	-0.21					
333	-0.48	-0.37	-0.36	-0.36	-0.34	-0.34					
334	-0.49	-0.39	-0.37	-0.37	-0.35	-0.35					
335	-0.38	-0.31	-0.29	-0.29	-0.27	-0.27					
336	-0.40	-0.33	-0.31	-0.30	-0.29	-0.28					
337	-0.29	-0.24	-0.23	-0.22	-0.21	-0.21					
338	-0.30	-0.26	-0.24	-0.23	-0.22	-0.21					
339	-0.20	-0.17	-0.16	-0.15	-0.15	-0.15					
340	-0.21	-0.19	-0.17	-0.16	-0.16	-0.15					
341	-0.13	-0.11	-0.10	-0.10	-0.09	-0.09					
342	-0.12	-0.09	-0.09	-0.09	-0.09	-0.08					
343	-0.46	-0.35	-0.33	-0.34	-0.32	-0.31					
344	-0.45	-0.34	-0.32	-0.33	-0.31	-0.31					
345	-0.45	-0.33	-0.32	-0.33	-0.31	-0.30					
346	-0.44	-0.32	-0.31	-0.32	-0.30	-0.30					
347	-0.43	-0.32	-0.31	-0.32	-0.30	-0.30					
348	-0.43	-0.32	-0.31	-0.32	-0.30	-0.29					
349	-0.42	-0.31	-0.30	-0.31	-0.29	-0.29					
350	-0.41	-0.31	-0.30	-0.30	-0.28	-0.28					
351	-0.39	-0.29	-0.28	-0.29	-0.27	-0.27					
352	-0.50	-0.40	-0.38	-0.37	-0.35	-0.35					
353	-0.40	-0.34	-0.32	-0.30	-0.29	-0.29					
354	-0.31	-0.27	-0.25	-0.23	-0.22	-0.22					
355	-0.22	-0.19	-0.18	-0.16	-0.16	-0.15					
356	-0.47	-0.36	-0.34	-0.34	-0.32	-0.32					

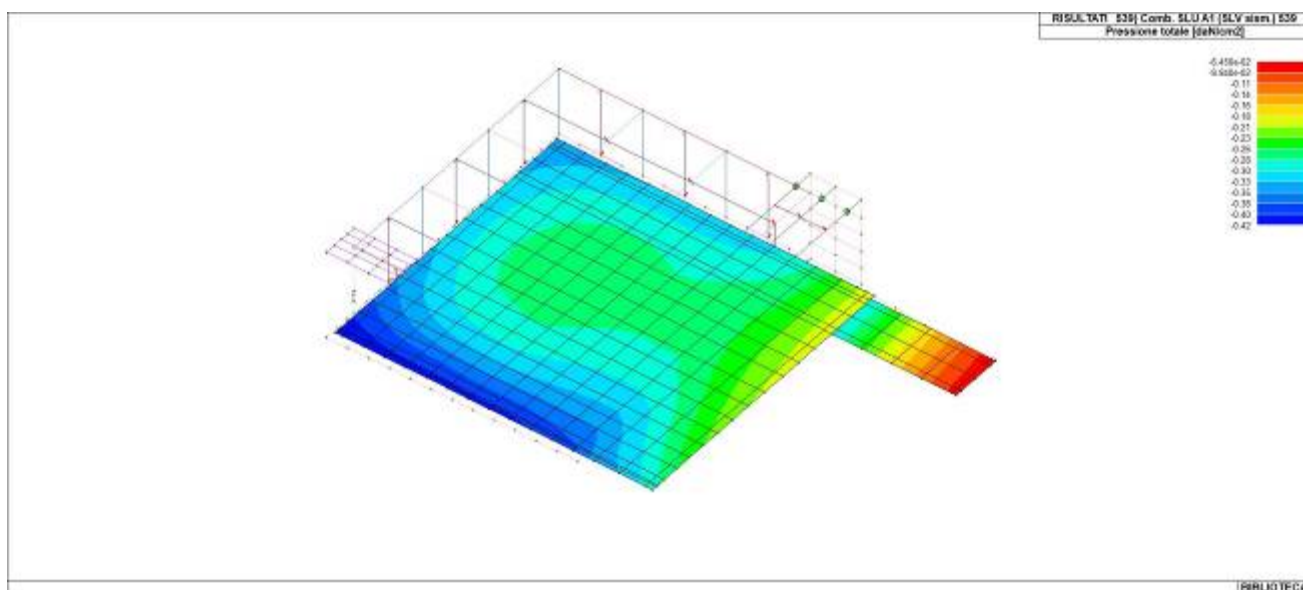
Nodo (G)	Pt 1/12	Pt 2/13	Pt 3...	Pt 4...							
357	-0.46	-0.35	-0.33	-0.34	-0.32	-0.31					
358	-0.45	-0.34	-0.33	-0.33	-0.31	-0.31					
359	-0.45	-0.33	-0.32	-0.33	-0.31	-0.30					
360	-0.44	-0.33	-0.32	-0.32	-0.31	-0.30					
361	-0.44	-0.33	-0.32	-0.32	-0.30	-0.30					
362	-0.42	-0.32	-0.31	-0.31	-0.29	-0.29					
363	-0.41	-0.31	-0.30	-0.30	-0.29	-0.28					
364	-0.39	-0.30	-0.29	-0.29	-0.28	-0.27					
365	-0.34	-0.26	-0.25	-0.26	-0.24	-0.24					
Nodo (G)	Pt 1/12	Pt 2/13	Pt 3...	Pt 4...							
	-0.62										
	-0.07										



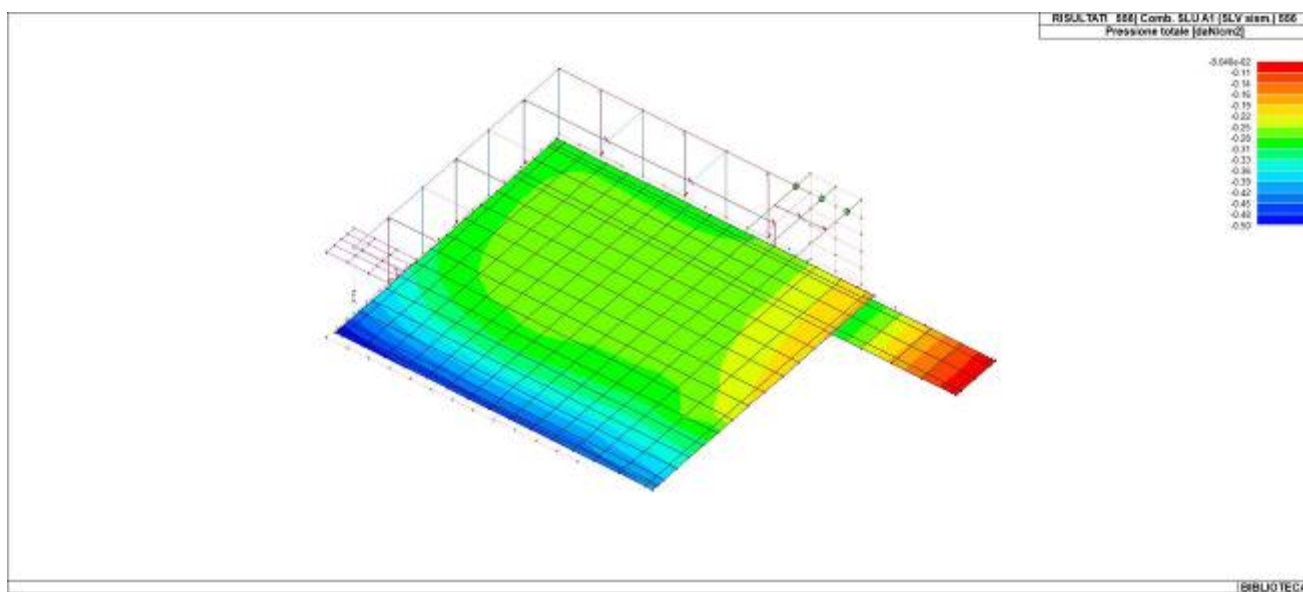
46_RIS_PRESSIONI_377_Comb. SLU A1 377



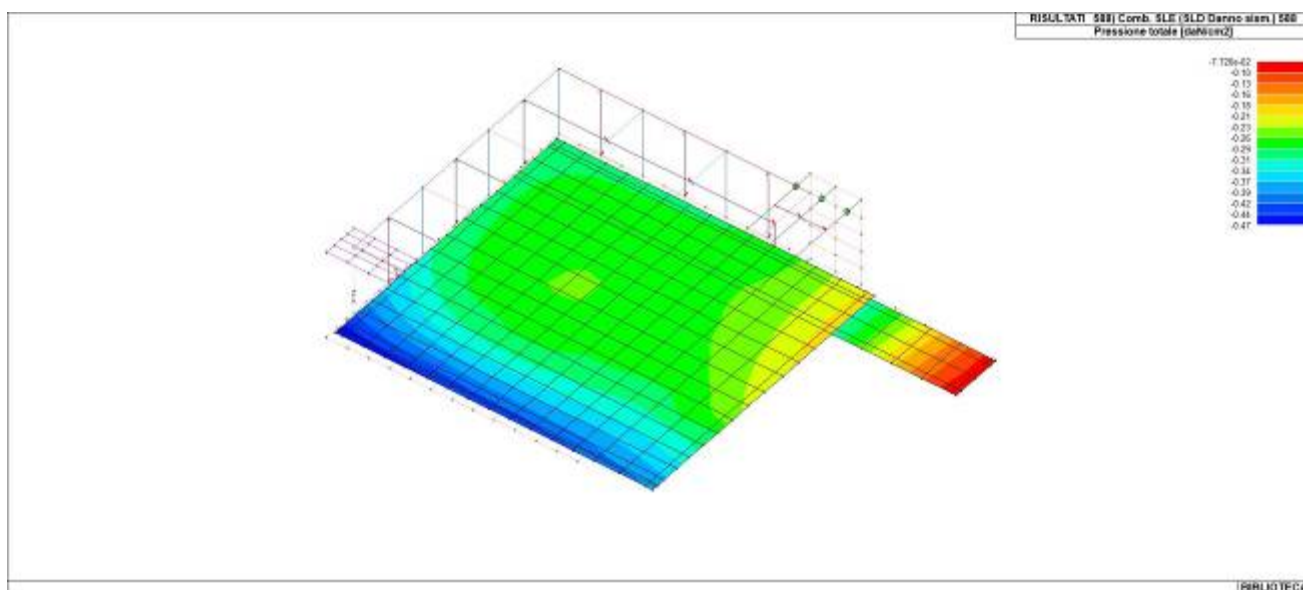
46_RIS_PRESSIONI_488_Comb. SLU A1 488



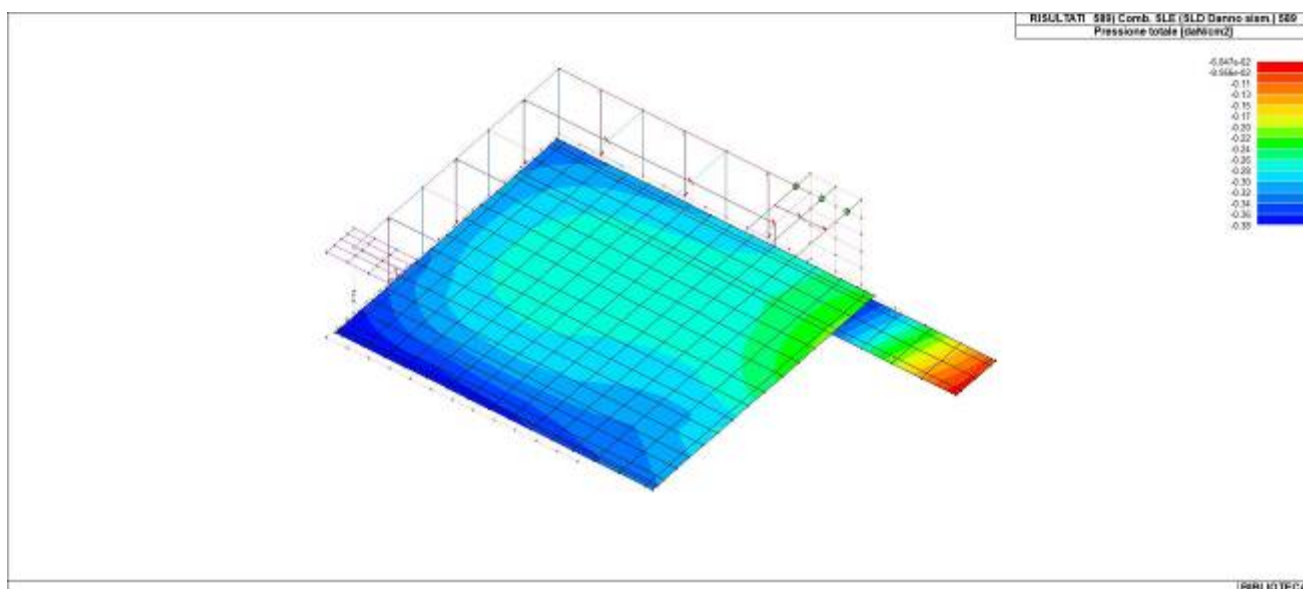
46_RIS_PRESSIONI_539_Comb. SLU A1 (SLV sism.) 539



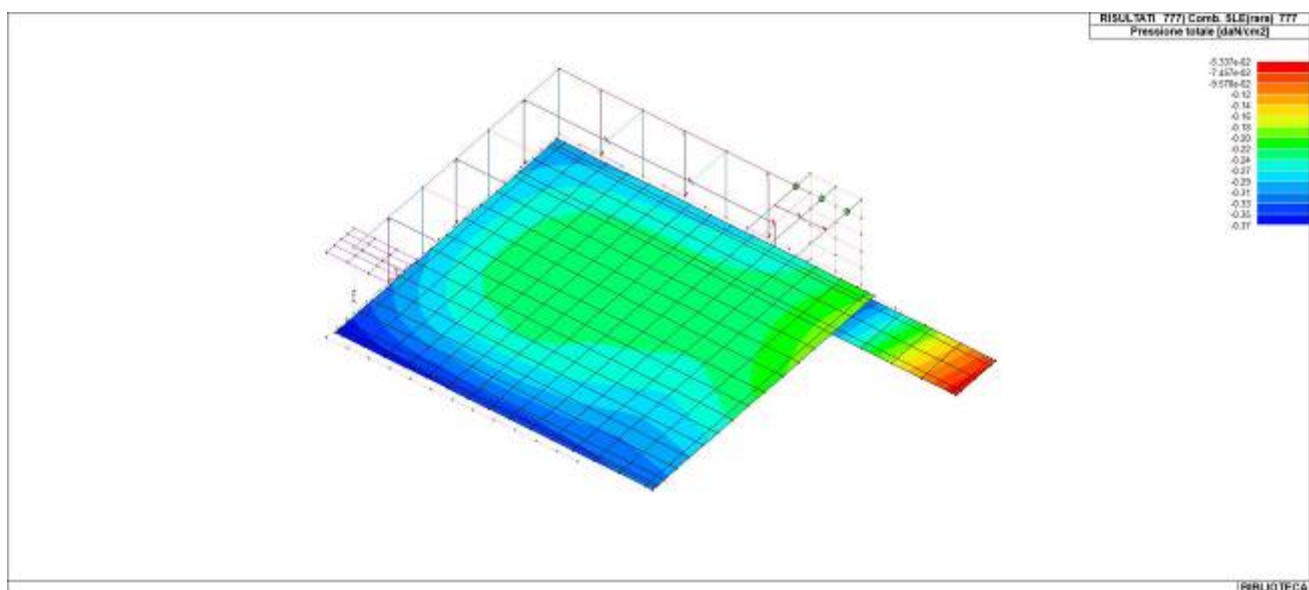
46_RIS_PRESSIONI_556_Comb. SLU A1 (SLV sism.) 556



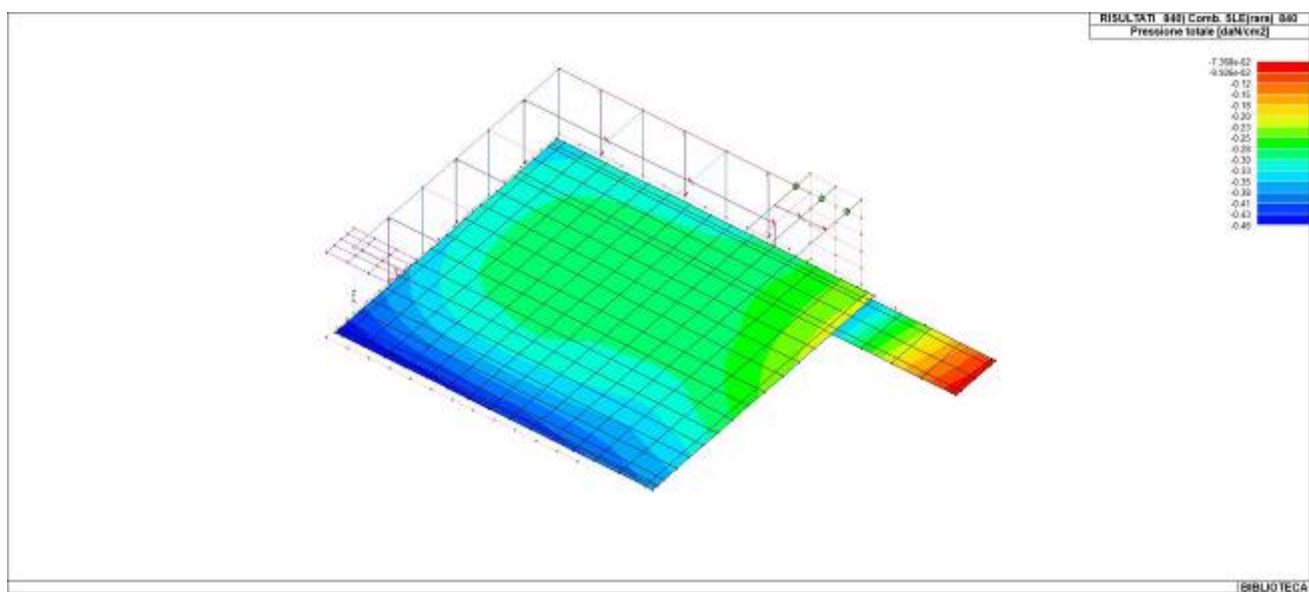
46_RIS_PRESSIONI_588_Comb. SLE (SLD Danno sism.) 588



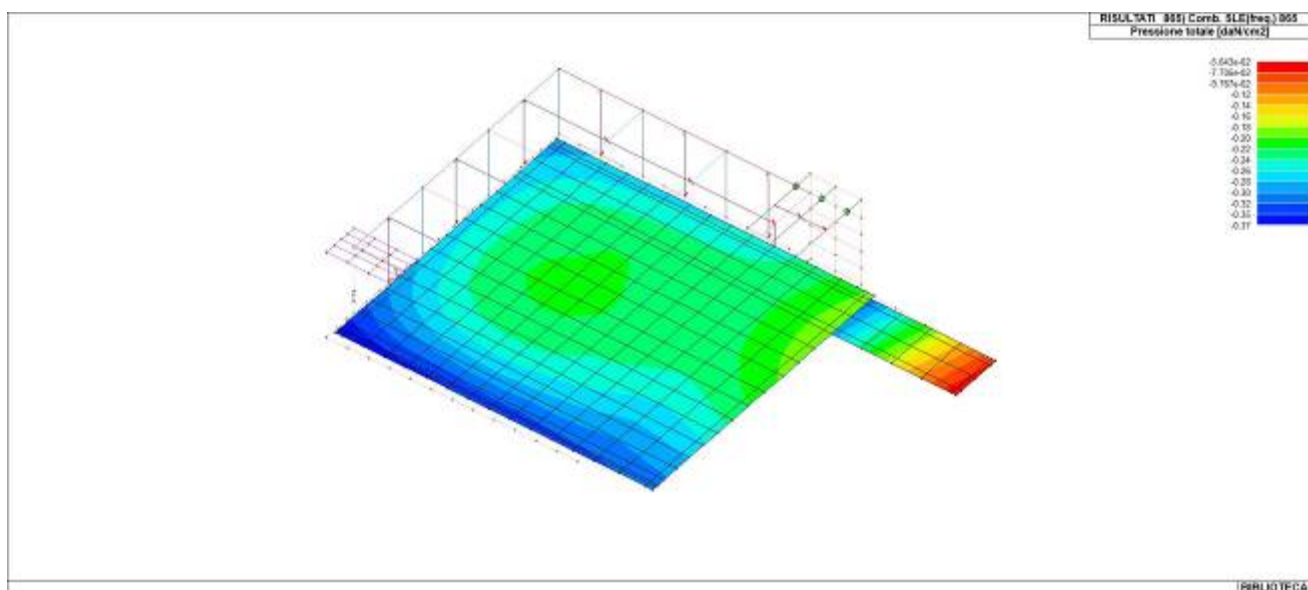
46_RIS_PRESSIONI_589_Comb. SLE (SLD Danno sism.) 589



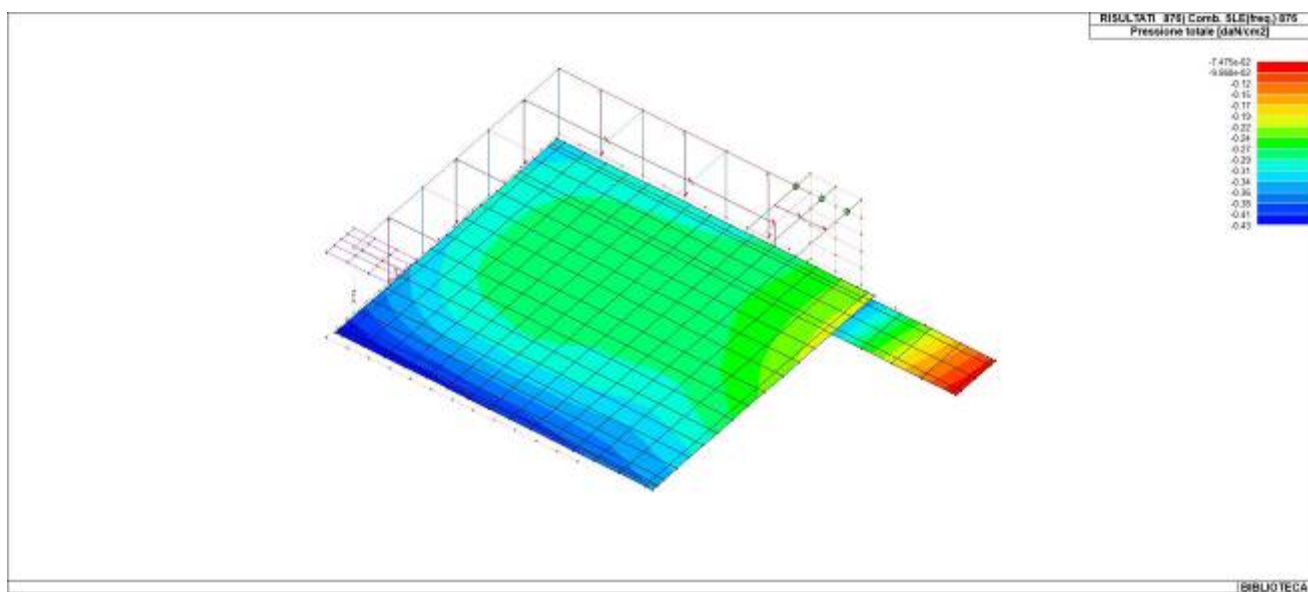
46_RIS_PRESSIONI_777_Comb. SLE(rara) 777



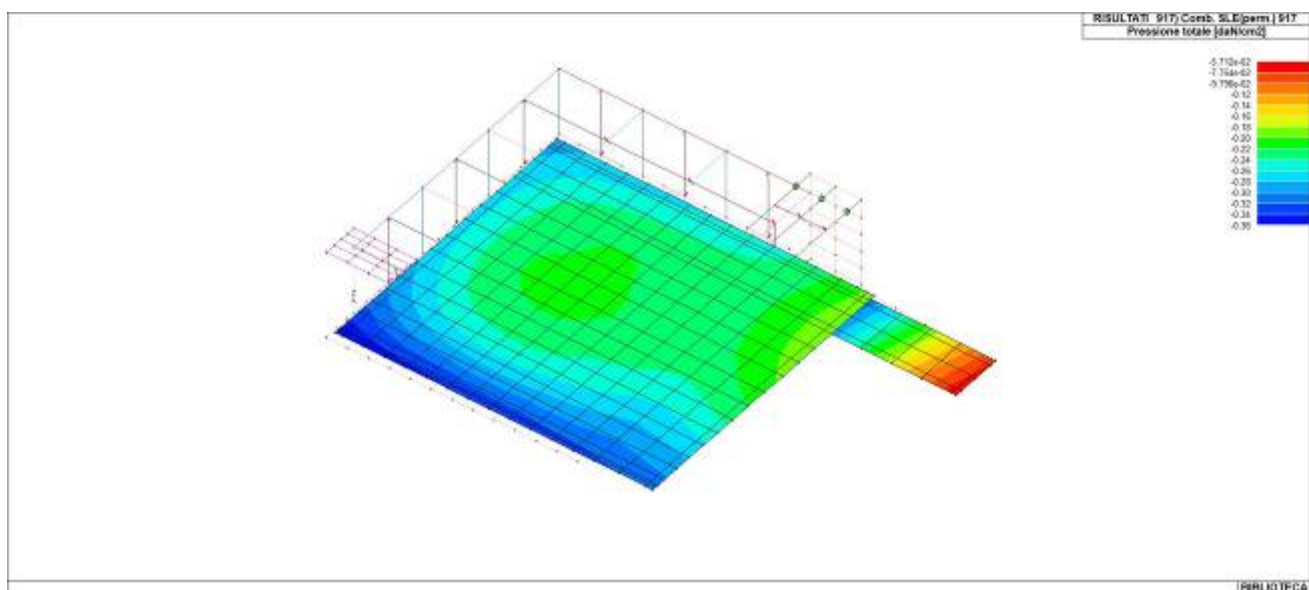
46_RIS_PRESSIONI_840_Comb. SLE(rara) 840



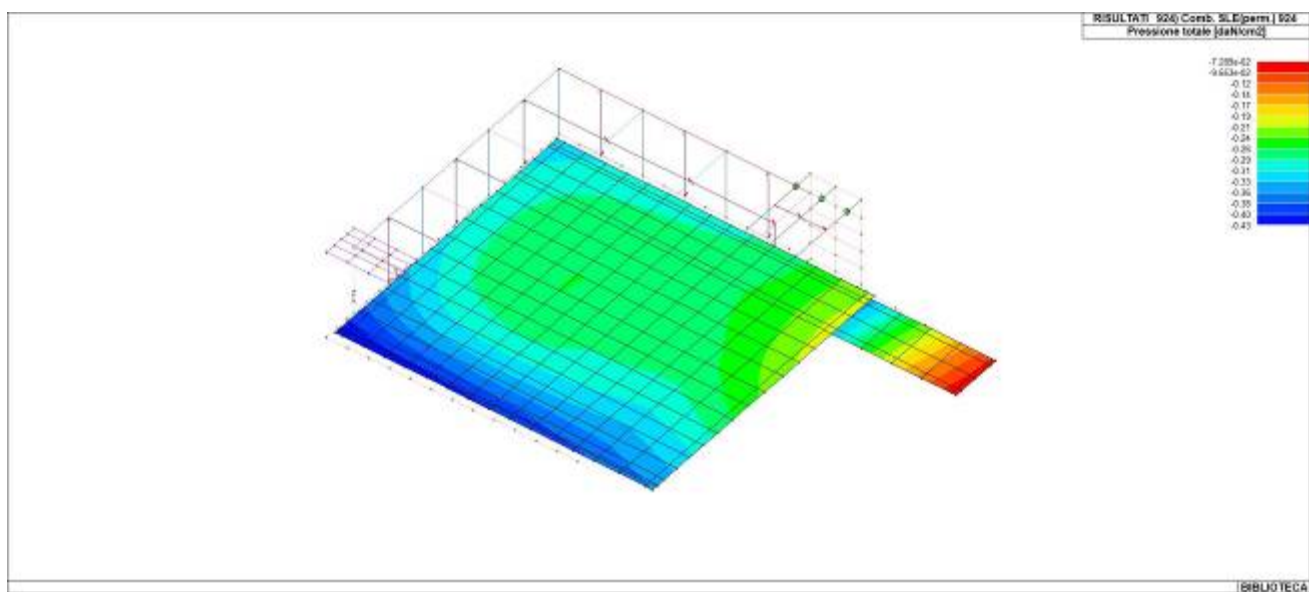
46_RIS_PRESSIONI_865_Comb. SLE(freq.) 865



46_RIS_PRESSIONI_876_Comb. SLE(freq.) 876



46_RIS_PRESSIONI_917_Comb. SLE(perm.) 917



46_RIS_PRESSIONI_924_Comb. SLE(perm.) 924

VERIFICHE PER ELEMENTI IN ACCIAIO

LEGENDA TABELLA VERIFICHE PER ELEMENTI IN ACCIAIO

Il programma consente la verifica dei seguenti tipi di elementi:

1. **aste** 2. **travi** 3. **pilastr**

L'esito delle verifiche è espresso con un codice come di seguito indicato

Ok: verifica con esito positivo

NV: verifica con esito negativo

Nr: verifica non richiesta.

Per comodità gli elementi vengono raggruppati in tabelle in relazione al tipo.

Ai fini delle verifiche (come da D.M. 17 Gennaio 2018 e circolare 21 Gennaio 2019 n.7) i tipi elementi differiscono per i seguenti aspetti:

Verifica		Aste	Travi	Pilastr
4.2.3.1	Classificazione	X	X	X
4.2.4.1.2.1	Trazione	X	X	X
4.2.4.1.2.2	Compressione	X	X	X
4.2.4.1.2.4	Taglio		X	X
4.2.4.1.2.5	Torsione		X	X
	Flessione, taglio e forza assiale		X	X
4.2.4.1.3.1	Aste compresse	X	X	X
4.2.4.1.3.2	Instabilità flessio-torsionale		X	X
4.2.4.1.3.3	Membrature inflesse e compresse		X	X

Ai fini delle verifiche per strutture dissipative (come da D.M. 17 Gennaio 2018 e 2018 e circolare 21 Gennaio 2019 n.7) per strutture intelaiate e a controventi concentrici) si considerano le verifiche del capitolo 4 con azioni amplificate e le verifiche del capitolo 7:

Verifica		Travi	Pilastr
4.2.4.1.2.1	Trazione	X	X
4.2.4.1.2.2	Compressione	X	X
4.2.4.1.2.4	Taglio	X	X
4.2.4.1.2.5	Torsione	X	X
	Flessione, taglio e forza assiale	X	X
4.2.4.1.3.1	Aste compresse	X	X
4.2.4.1.3.2	Instabilità flessio-torsionale	X	X
4.2.4.1.3.3	Membrature inflesse e compresse	X	X
7.5.3	Sfruttamento per momento	X	
7.5.4	Sfruttamento per sforzo normale	X	
7.5.5	Sfruttamento per taglio da capacità flessionale	X	
7.5.9	Sfruttamento per taglio amplificato		X

Viene inoltre riportata la verifica della "Gerarchia delle resistenze trave-colonna" per ogni colonna, considerando piede e testa in entrambe le direzioni globali X e Y.

L'insieme delle verifiche sopra riportate è condotto sugli elementi purché dotati di sezione idonea come da tabella seguente:

Azione	SEZIONI GENERICHE	PROFILI SEMPLICI	PROFILI ACCOPPIATI
4.2.3.1 Classificazione automatica	L, doppio T, C, rettangolare cava, circolare cava	Tutti	Da profilo semplice
4.2.3.1 Classificazione di default 2	Circolare		
4.2.3.1 Classificazione di default 3	restanti		
4.2.4.1.2.1 Trazione	si	si	si
4.2.4.1.2.2 Compressione	si	si	si
4.2.4.1.2.4 Taglio	si	si	si
4.2.4.1.2.5 Torsione	si	si	si
	Flessione, taglio e forza assiale	si	si
4.2.4.1.3.1 Aste compresse	si	si	per elementi ravvicinati e a croce o coppie calastrellate
4.2.4.1.3.2 Travi inflesse	doppio T simmetrica	doppio T	no

Le verifiche sono riportate in tabelle con il significato sotto indicato; le verifiche sono espresse dal rapporto tra l'azione di progetto e la capacità ultima, pertanto la verifica ha esito positivo per rapporti non superiori all'unità.

Asta	Trave	Pilastr	numero dell'elemento
	Stato		codice di verifica per resistenza, stabilità, svergolamento
	Note		sezione e materiali adottati per l'elemento

V N						(ASTE) verifica come da par. 4.2.4.1.2 per punto (4.2.6) e (4.2.10)
V V/T						(TRAVI E PILASTRI) verifica di resistenza come da par. 4.2.4.1.2 per azioni taglio-torsione (4.2.16 e 4.2.28)
V N/M						(TRAVI E PILASTRI) verifica di resistenza come da par. 4.2.4.1.2 per azioni composte (4.2.33) con riduzione per taglio (4.2.40) ove richiesto
N	M3	M2	V2	V3	T	sollecitazioni di interesse per la verifica
V stab						(ASTE) verifica come da par. 4.2.4.1.3.1 per punto (4.2.41)
V stab						(TRAVI E PILASTRI) verifica come da par. 4.2.4.1.3 per punti (C4.2.32) o (C4.2.36) (membrature inflesse e compresse senza/con presenza di instabilità flessione-torsionale)
BetaxL		B22xL		B33xL		lunghezze libere di inflessione (se indicato riferiti al piano di normale 22 o 33 rispettivamente)
Snellezza						snellezza massima
Classe						classe del profilo
Chi mn						coefficiente di riduzione (della capacità) per la modalità di instabilità pertinente
Rif. cmb						combinazioni in cui si sono rispettivamente attinti i valori di verifica più elevati
V flst						(TRAVI E PILASTRI) verifica di stabilità come da par. 4.2.4.1.3.2 per punto (4.2.48)
B1-1 x L						Beta1-1 x L: interasse tra i ritegni torsionali
Chi LT						coefficiente di riduzione (della capacità) per la modalità di instabilità flessione-torsionale
Snell adim						Valore della snellezza adimensionale, utilizzato per il controllo previsto al par. 7.5.5
v.Omeg						Valore del rapporto capacità/domanda per l' azione di interesse (momento per travi e azione assiale per aste) utilizzato per l' amplificazione delle azioni
f.Om. N						Fattore di amplificazione delle azioni assiali per travi e colonne (prodotto di 1.1 x Omega x gamma rd materiale); utilizzato come specificato al par. 7.5.5
f.Om. T						Fattore di amplificazione delle azioni (assiali, flettenti e taglianti) per colonne (prodotto di 1.1 x Omega x gamma rd materiale); utilizzato come specificato al par. 7.5.4
V.7.5.4 M Ed						Verifica come prevista al punto 7.5.4 e valore dell' azione flettente
V.7.5.5 N Ed						Verifica come prevista al punto 7.5.5 e valore dell' azione assiale
V.7.5.6 V Ed,G V Ed,M						Verifica come prevista al punto 7.5.6 e valore dei tagli dovuti ai carichi e alla capacità
V.7.5.10 V Ed						Verifica come prevista al punto 7.5.10 e valore dell' azione di taglio
sovr. Xi (Xi, Yi, Yf)						Valore della sovrarresistenza come prevista al par. 7.5.4.2 (i valori non sono normalizzati pertanto saranno maggiori uguali a gamma rd in base alla classe di duttilità)

Nel caso in cui λ_{S} sia minore di 0.2, oppure nel caso in cui la sollecitazione di calcolo N_{Ed} sia inferiore a $0.04 N_{cr}$, gli effetti legati ai fenomeni di instabilità sono trascurati, come da paragrafo 4.2.4.1.3.1

Trave	Stato	Note	V V/T	V N/M	V stab	Cl.	LamS 22	LamS 33	Snell.	Chi mn	V flst	LamS LT	Chi LT	Rif. cmb
47	ok	s=10,m=12	0.04	0.31	0.31	1	0.9	0.6	81.1	0.58	0.31	0.3	1.00	369,152,152,369
48	ok	s=10,m=12	0.03	0.23	0.23	1	0.9	0.6	81.1	0.58	0.23	0.5	0.98	484,486,488,484
51	ok	s=11,m=12	0.03	0.08	0.09	1	2.1	2.5	212.9	0.15	0.11	1.1	0.68	148,152,534,373
52	ok	s=11,m=12	0.04	0.14	0.15	1	3.2	2.5	278.4	0.09	0.29	1.4	0.49	373,369,534,148
53	ok	s=11,m=12	0.05	0.20	0.21	1	3.4	2.5	298.8	0.08	0.44	1.4	0.45	148,261,529,261
54	ok	s=11,m=12	0.06	0.19	0.30	1	2.1	2.5	212.9	0.15	0.28	1.1	0.68	484,259,375,484
55	ok	s=11,m=12	0.08	0.38	0.89	1	3.2	2.5	278.4	0.09	0.78	1.4	0.49	369,369,259,369
56	ok	s=11,m=12	0.10	0.39	0.99	1	3.4	2.5	298.8	0.08	0.85	1.4	0.45	372,372,259,372
57	ok	s=11,m=12	0.03	0.10	0.14	1	2.1	0.6	184.0	0.19	0.14	1.1	0.68	369,369,551,369
58	ok	s=11,m=12	0.04	0.19	0.52	1	3.2	0.9	278.4	0.09	0.38	1.4	0.49	484,484,487,484
59	ok	s=11,m=12	0.05	0.28	0.94	1	3.4	1.0	298.8	0.08	0.62	1.4	0.45	484,484,484,484
76	ok	s=10,m=12	0.09	0.31	0.26	1	0.3	0.3	29.2	0.95	0.31	9.94e-02	1.00	260,258,496,369
77	ok	s=10,m=12	0.06	0.24	0.23	1	0.3	0.3	29.2	0.95	0.23	9.93e-02	1.00	484,257,257,484
94	ok	s=10,m=12	0.03	0.08	0.08	1	0.3	0.3	29.2	0.95	0.08	9.06e-02	1.00	371,484,488,371
95	ok	s=10,m=12	0.02	0.06	0.06	1	0.3	0.3	29.2	0.95	0.06	9.06e-02	1.00	484,488,488,484
Trave			V V/T	V N/M	V stab		LamS 22	LamS 33	Snell.	Chi mn	V flst	LamS LT	Chi LT	
										0.08			0.45	
			0.10	0.39	0.99		3.44	2.45	298.75		0.85	1.45		

STATI LIMITE D' ESERCIZIO ACCIAIO

LEGENDA TABELLA STATI LIMITE D' ESERCIZIO ACCIAIO

In tabella vengono riportati i valori di interesse per il controllo degli stati limite d'esercizio.

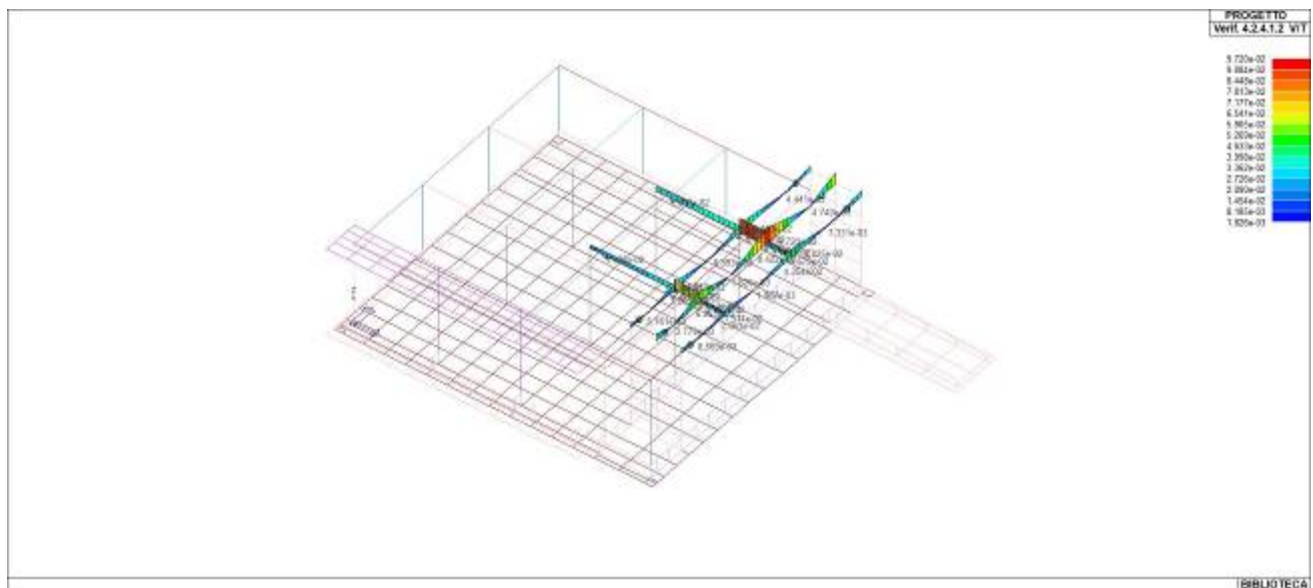
In particolare vengono riportati, per gli elementi trave, i risultati relativi alle combinazioni considerate (rare o caratteristiche).

I valori di interesse sono i seguenti:

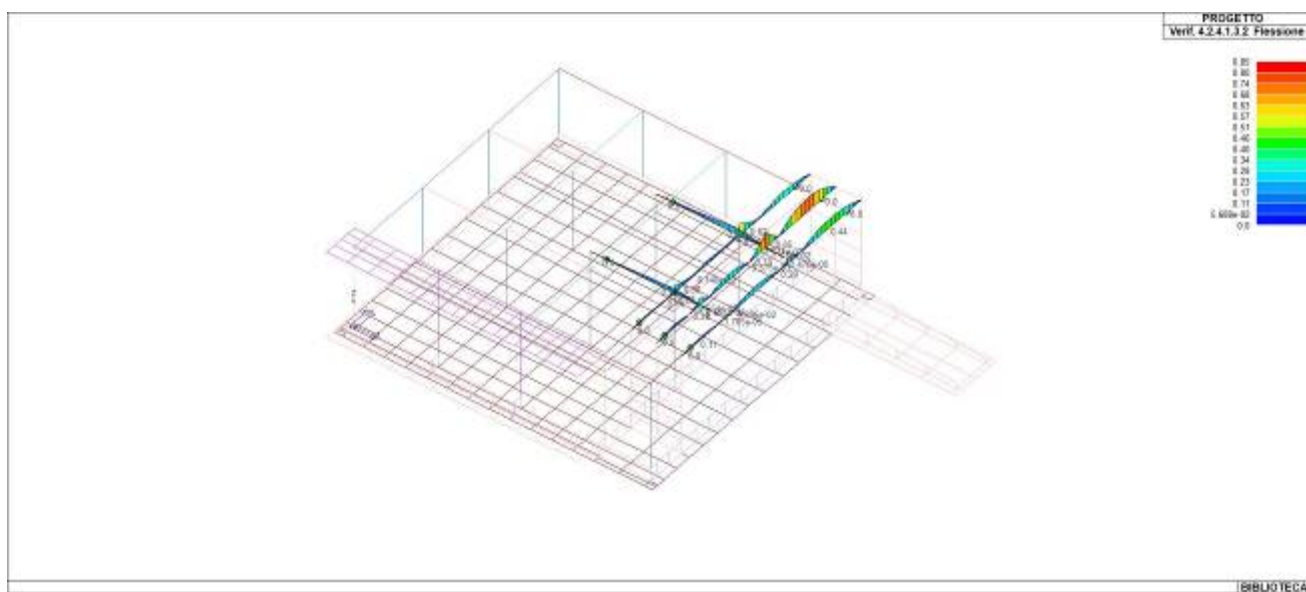
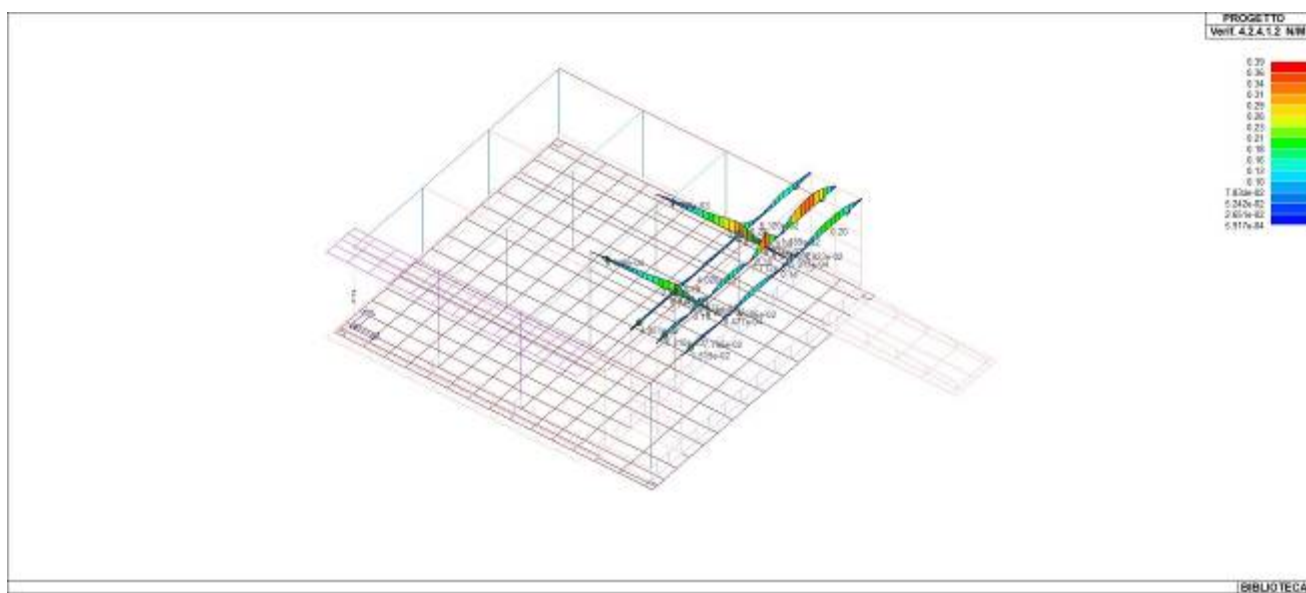
f*1000/L	massima deformazione normalizzata in combinazioni rare
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Si precisa che i valori di massima deformazione per travi sono riferiti ai due piani locali (1-2 con momenti flettenti 3-3 e 1-3 con momenti flettenti 2-2). Il valore riportato (massimo) è espresso in 1000/L per rendere agevole il confronto di più valori e in particolare di più range di valori (ad esempio 2 rappresenta L/500, 4 L/250 e così via).

Trave	f*1000/L	Trave	f*1000/L	Trave	f*1000/L	Trave	f*1000/L	Trave	f*1000/L	Trave	f*1000/L	Trave	f*1000/L
47	0.7	48	0.5	51	3.7	52	0.7	53	3.5	54	1.5	55	0.6
56	1.9	57	0.4	58	0.3	59	0.7	76	5.2	77	3.9	94	6.5
95	4.8												

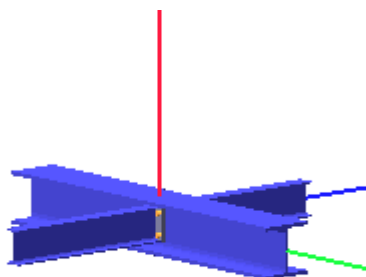


73_ST_15_Verif 42412 VT



VERIFICA NODO TRA HEB240 – IPE160

Verifica secondo il D.M. 17/01/2018



Trave 2

Tipo di profilo: HEB 240

Materiale: Acciaio S275 $f_y = 275 \text{ N/mm}^2$ $f_t = 430 \text{ N/mm}^2$ $\gamma_{ov} = 1.25$

Classe sezione: 1

Coefficienti di sicurezza utilizzati

$\gamma_{M0} = 1.05$

$\gamma_{M1} = 1.10$

$\gamma_{M2} = 1.25$

Trave lato 3+

Tipo di profilo: IPE 160

Materiale: Acciaio S275 $f_y = 275 \text{ N/mm}^2$ $f_t = 430 \text{ N/mm}^2$ $\gamma_{ov} = 1.25$

Classe sezione: 1

Flangia:

Materiale: Acciaio S275 $f_y = 275 \text{ N/mm}^2$ $f_t = 430 \text{ N/mm}^2$ $\gamma_{ov} = 1.25$

Dimensioni (B x H x Sp): 100.0 x 160.0 x 10.0 mm

Bullonature:

Viti cl. 8.8 Dadi 8 o 10 ($f_{yb} = 640 \text{ N/mm}^2$, $f_{tb} = 800 \text{ N/mm}^2$)

Diametro gambo $\varnothing = 16 \text{ mm}$ $A_{res} = 156.8 \text{ mm}^2$ (ridotta per filettatura)

Diametro dado/testa $d_m = 24 \text{ mm}$

Diametro foro $\varnothing_0 = 17 \text{ mm}$

Rigidità giunto (calcolata secondo EN 1993-1-8 : 2005 par. 6.3):

$S_{j,ini}$ non calcolabile

Saldature:

Materiale: Acciaio S275 $f_y = 275 \text{ N/mm}^2$ $f_t = 430 \text{ N/mm}^2$ $\beta_1 = 0.70$ $\beta_2 = 0.85$

Spessore cordoni d'angolo $s_c = 5 \text{ mm}$

Sollecitazioni nella sezione d'attacco dell'elemento:

Nodo.CMB	V2 [N]	V3 [N]	N [N]	M2 [N mm]	M3 [N mm]	T [N mm]
551.257	9127.4	4.5	-1743.5	-15279.0	-6046363.0	2771.0
551.484	9140.4	1.6	-1109.9	-5556.0	-6090298.0	2778.0

Calcolo resistenze

Resistenza a trazione dei bulloni

$$F_{tb,Rd} = 0.9 \cdot f_{tb} \cdot A_{res} / \gamma_{M2} =$$

90333.1 N

Resistenza a punzonamento flangia

$$B_{pf,Rd} = 0.6 \cdot \pi \cdot d_m \cdot t_f \cdot f_{tk} / \gamma_{M2} =$$

155621.9 N

Bull.	$F_{f,Rd}$ [N]	$F_{t,Rd}$ [N]
1	29092.5	29092.5
2	29092.5	29092.5
3	29092.5	29092.5
4	29092.5	29092.5

Legenda

$F_{f,Rd} = M_{res,m} / (B_m \cdot R_m)$ resistenza a flessione flangia

$F_{t,Rd} = \min [F_{tb,Rd} , B_{pf,Rd} , F_{f,Rd}]$ resistenza a trazione di progetto

Resistenza a taglio dei bulloni

$$F_{vb,Rd} = 0.6 \cdot f_{tb} \cdot A_{res} / \gamma_{M2} =$$

60222.1 N

Bull.	$F_{bf,x,Rd}$ [N]	$F_{ba,x,Rd}$ [N]	$F_{v,x,Rd}$ [N]	$F_{bf,y,Rd}$ [N]	$F_{ba,y,Rd}$ [N]	$F_{v,y,Rd}$ [N]
1	67451.0	137600.0	60222.1	78274.9	137600.0	60222.1
2	67451.0	137600.0	60222.1	78274.9	137600.0	60222.1
3	67451.0	137600.0	60222.1	78274.9	137600.0	60222.1
4	67451.0	137600.0	60222.1	78274.9	137600.0	60222.1

Legenda

$F_{bf,x,Rd} = k \cdot \alpha \cdot f_{tk} \cdot \varnothing \cdot t_f / \gamma_{M2}$ resistenza a rifollamento flangia in direzione x

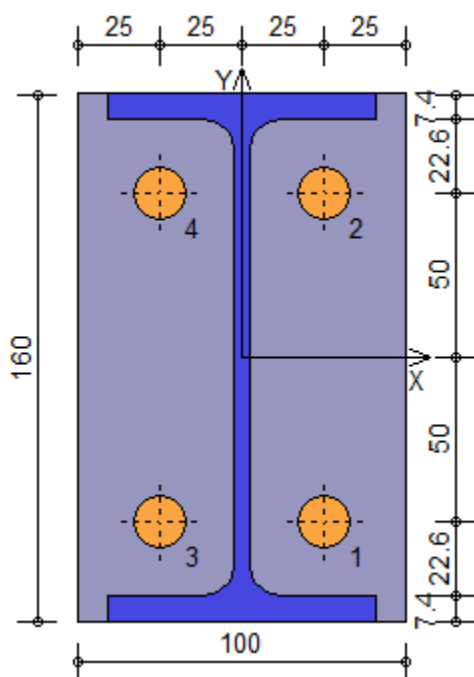
$F_{ba,x,Rd} = k \cdot \alpha \cdot f_{tk} \cdot \varnothing \cdot t_a / \gamma_{M2}$ resistenza a rifollamento anima passante in direzione x

$F_{v,x,Rd} = \min [F_{vb,Rd} , F_{bf,x,Rd} , F_{ba,x,Rd}]$ resistenza a taglio di progetto in direzione x

$F_{bf,y,Rd} = k \cdot \alpha \cdot f_{tk} \cdot \varnothing \cdot t_f / \gamma_{M2}$ resistenza a rifollamento flangia in direzione y

$F_{ba,y,Rd} = k \cdot \alpha \cdot f_{tk} \cdot \varnothing \cdot t_a / \gamma_{M2}$ resistenza a rifollamento anima passante in direzione y

$F_{v,y,Rd} = \min [F_{vb,Rd} , F_{bf,y,Rd} , F_{ba,y,Rd}]$ resistenza a taglio di progetto in direzione y



Verifiche sui bulloni

1-Taglio e trazione (Nodo n. 551, CMB n. 484)

Bull.	X [mm]	Y [mm]	$F_{v,Ed}$ [N]	$F_{v,Rd}$ [N]	$F_{t,Ed}$ [N]	$F_{t,Rd}$ [N]	FV ₁	VER
1	25.00	-50.00	2279.6	60222.1	24624.0	29092.5	0.642427	Ok
2	25.00	50.00	2279.6	60222.1	882.0	29092.5	0.059508	Ok
3	-25.00	-50.00	2290.7	60222.1	24640.9	29092.5	0.643027	Ok
4	-25.00	50.00	2290.7	60222.1	898.9	29092.5	0.060108	Ok

2-Trazione (Nodo n. 551, CMB n. 484)

Bull.	X [mm]	Y [mm]	$F_{t,Ed}$ [N]	$F_{t,Rd}$ [N]	FV ₂	VER
1	25.00	-50.00	24624.0	29092.5	0.846405	Ok
2	25.00	50.00	882.0	29092.5	0.030318	Ok
3	-25.00	-50.00	24640.9	29092.5	0.846985	Ok
4	-25.00	50.00	898.9	29092.5	0.030898	Ok

Legenda

$F_{v,Ed}$ forza di taglio agente sul bullone
 $F_{v,Rd}$ resistenza a taglio di progetto del bullone
 $F_{t,Ed}$ forza di trazione agente sul bullone
 $F_{t,Rd}$ resistenza a trazione di progetto del bullone
 $FV_1 = F_{v,Ed} / F_{v,Rd} + F_{t,Ed} / (1.4 \cdot F_{t,Rd})$
 $FV_2 = F_{t,Ed} / F_{t,Rd}$
 $VER \rightarrow FV_i \leq 1$

Verifiche sulle saldature profilo-flangia (versione beta)

Si considera la sezione di gola (avente altezza $a = s_c / 2^{0.5} = 3.536$) in posizione ribaltata: vengono considerate positive le tensioni normali di trazione e le tensioni tangenziali agenti verso destra e verso il basso. Tutte le tensioni sono espresse in N/mm².

Verifica formula (4.2.84) (Nodo n. 551, CMB n. 257)

Cordoni	Lung.[mm]	n_{\perp}	t_{\perp}	τ_{\parallel}	FV_1	VER_1
Ala inferiore interno lato destro	29.5	-132.83	0.00	0.01	132.83	Ok
Ala inferiore interno lato sinistro	29.5	-130.30	0.00	0.01	130.30	Ok
Anima lato destro	127.2	-117.63	0.00	10.15	118.07	Ok
Anima lato sinistro	127.2	-117.63	0.00	10.15	118.07	Ok
Ala superiore interno lato destro	29.5	127.66	0.00	0.01	127.66	Ok
Ala superiore interno lato sinistro	29.5	130.18	0.00	0.01	130.18	Ok

Verifica formula (4.2.85) (Nodo n. 551, CMB n. 257)

Cordoni	Lung.[mm]	n_{\perp}	t_{\perp}	τ_{\parallel}	FV_2	VER_2
Ala inferiore interno lato destro	29.5	-132.83	0.00	0.01	132.83	Ok
Ala inferiore interno lato sinistro	29.5	-130.30	0.00	0.01	130.30	Ok
Anima lato destro	127.2	-117.63	0.00	10.15	117.63	Ok
Anima lato sinistro	127.2	-117.63	0.00	10.15	117.63	Ok
Ala superiore interno lato destro	29.5	127.66	0.00	0.01	127.66	Ok
Ala superiore interno lato sinistro	29.5	130.18	0.00	0.01	130.18	Ok

Legenda

n_{\perp} tensione normale perpendicolare all'asse del cordone
 t_{\perp} tensione tangenziale perpendicolare all'asse del cordone
 τ_{\parallel} tensione tangenziale parallela all'asse del cordone
 $FV_1 = (n_{\perp}^2 + t_{\perp}^2 + \tau_{\parallel}^2)^{0.5}$
 $FV_2 = |n_{\perp}| + |t_{\perp}|$
 $VER_i \rightarrow FV_i \leq \beta_i \cdot f_{yk} \quad (\beta_1 \cdot f_{yk} = 192.50 \text{ N/mm}^2 \quad \beta_2 \cdot f_{yk} = 233.75 \text{ N/mm}^2)$

Verifica del momento di progetto del giunto (Nodo n. 551, CMB n. 484)

Momento resistente del giunto $M_{j,Rd} = 9309586.0 \text{ N mm}$
Momento di progetto $M_{j,Ed} = 6001506.0 \text{ N mm}$
 $M_{j,Ed} / M_{j,Rd} = 0.644659 \text{ Ok}$

Trave lato 3-

Tipo di profilo: IPE 160

Materiale: Acciaio S275 $f_y = 275 \text{ N/mm}^2$ $f_t = 430 \text{ N/mm}^2$ $\gamma_{ov} = 1.25$

Classe sezione: 1

Flangia:

Materiale: Acciaio S275 $f_y = 275 \text{ N/mm}^2$ $f_t = 430 \text{ N/mm}^2$ $\gamma_{ov} = 1.25$

Dimensioni (B x H x Sp): 89.8 x 160.0 x 17.0 mm

Bullonature:

Viti cl. 8.8 Dadi 8 o 10 ($f_{yb} = 640 \text{ N/mm}^2$, $f_{tb} = 800 \text{ N/mm}^2$)

Diametro gambo $\varnothing = 16 \text{ mm}$ $A_{res} = 156.8 \text{ mm}^2$ (ridotta per filettatura)

Diametro dado/testa $d_m = 24 \text{ mm}$

Diametro foro $\varnothing_0 = 17 \text{ mm}$

Rigidità giunto (calcolata secondo EN 1993-1-8 : 2005 par. 6.3):

$S_{j,ini}$ non calcolabile

Saldature:

Materiale: Acciaio S275 $f_y = 275 \text{ N/mm}^2$ $f_t = 430 \text{ N/mm}^2$ $\beta_1 = 0.70$ $\beta_2 = 0.85$

Spessore cordoni d'angolo $s_c = 4 \text{ mm}$

Sollecitazioni nella sezione d'attacco dell'elemento:

Nodo.CMB	V2 [N]	V3 [N]	N [N]	M2 [N mm]	M3 [N mm]	T [N mm]
551.1	0.0	0.0	0.0	0.0	0.0	0.0
551.484	0.0	0.0	0.0	0.0	0.0	0.0

Calcolo resistenze

Resistenza a trazione dei bulloni

$$F_{tb,Rd} = 0.9 \cdot f_{tb} \cdot A_{res} / \gamma_{M2} = 90333.1 \text{ N}$$

Resistenza a punzonamento flangia

$$B_{pf,Rd} = 0.6 \cdot \pi \cdot d_m \cdot t_f \cdot f_{tk} / \gamma_{M2} = 264557.3 \text{ N}$$

Bull.	$F_{f,Rd}$ [N]	$F_{t,Rd}$ [N]
1	81195.2	81195.2
2	81195.2	81195.2
3	81195.2	81195.2
4	81195.2	81195.2

Legenda

$F_{f,Rd} = M_{res,m} / (B_m \cdot R_m)$ resistenza a flessione flangia

$F_{t,Rd} = \min [F_{tb,Rd} , B_{pf,Rd} , F_{f,Rd}]$ resistenza a trazione di progetto

Resistenza a taglio dei bulloni

$$F_{vb,Rd} = 0.6 \cdot f_{tb} \cdot A_{res} / \gamma_{M2} = 60222.1 \text{ N}$$

Bull.	$F_{bf,x,Rd}$ [N]	$F_{ba,x,Rd}$ [N]	$F_{v,x,Rd}$ [N]	$F_{bf,y,Rd}$ [N]	$F_{ba,y,Rd}$ [N]	$F_{v,y,Rd}$ [N]
1	93568.0	137600.0	60222.1	89539.1	137600.0	60222.1
2	93568.0	137600.0	60222.1	89539.1	137600.0	60222.1
3	93568.0	137600.0	60222.1	89539.1	137600.0	60222.1
4	93568.0	137600.0	60222.1	89539.1	137600.0	60222.1

Legenda

$F_{bf,x,Rd} = k \cdot \alpha \cdot f_{tk} \cdot \emptyset \cdot t_f / \gamma_{M2}$ resistenza a rifollamento flangia in direzione x

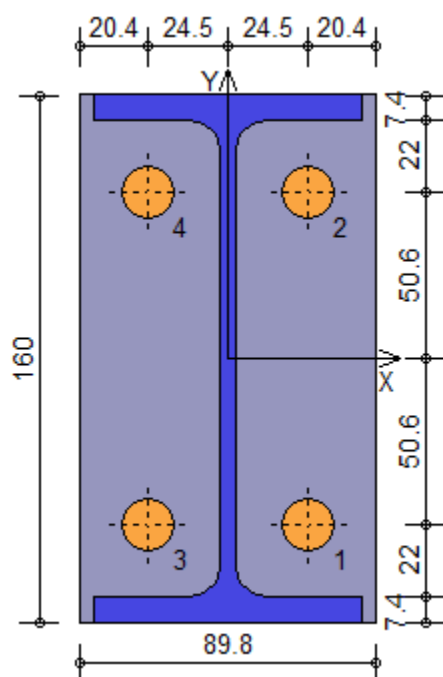
$F_{ba,x,Rd} = k \cdot \alpha \cdot f_{tk} \cdot \emptyset \cdot t_a / \gamma_{M2}$ resistenza a rifollamento anima passante in direzione x

$F_{v,x,Rd} = \min [F_{vb,Rd} , F_{bf,x,Rd} , F_{ba,x,Rd}]$ resistenza a taglio di progetto in direzione x

$F_{bf,y,Rd} = k \cdot \alpha \cdot f_{tk} \cdot \emptyset \cdot t_f / \gamma_{M2}$ resistenza a rifollamento flangia in direzione y

$F_{ba,y,Rd} = k \cdot \alpha \cdot f_{tk} \cdot \emptyset \cdot t_a / \gamma_{M2}$ resistenza a rifollamento anima passante in direzione y

$F_{v,y,Rd} = \min [F_{vb,Rd} , F_{bf,y,Rd} , F_{ba,y,Rd}]$ resistenza a taglio di progetto in direzione y



Verifiche sui bulloni

1-Taglio e trazione (Nodo n. 551, CMB n. 484)

Bull.	X [mm]	Y [mm]	$F_{v,Ed}$ [N]	$F_{v,Rd}$ [N]	$F_{t,Ed}$ [N]	$F_{t,Rd}$ [N]	FV ₁	VER
1	24.50	-50.60	0.0	60222.1	24640.9	81195.2	0.216769	Ok
2	24.50	50.60	0.0	60222.1	898.9	81195.2	0.007908	Ok
3	-24.50	-50.60	0.0	60222.1	24624.0	81195.2	0.216621	Ok
4	-24.50	50.60	0.0	60222.1	882.0	81195.2	0.007759	Ok

2-Trazione (Nodo n. 551, CMB n. 484)

Bull.	X [mm]	Y [mm]	$F_{t,Ed}$ [N]	$F_{t,Rd}$ [N]	FV ₂	VER
1	24.50	-50.60	24640.9	81195.2	0.303477	Ok
2	24.50	50.60	898.9	81195.2	0.011071	Ok
3	-24.50	-50.60	24624.0	81195.2	0.303269	Ok
4	-24.50	50.60	882.0	81195.2	0.010863	Ok

Legenda

$F_{v,Ed}$ forza di taglio agente sul bullone
 $F_{v,Rd}$ resistenza a taglio di progetto del bullone
 $F_{t,Ed}$ forza di trazione agente sul bullone
 $F_{t,Rd}$ resistenza a trazione di progetto del bullone
 $FV_1 = F_{v,Ed} / F_{v,Rd} + F_{t,Ed} / (1.4 \cdot F_{t,Rd})$
 $FV_2 = F_{t,Ed} / F_{t,Rd}$
 $VER \rightarrow FV_i \leq 1$

Verifiche sulle saldature profilo-flangia (versione beta)

Si considera la sezione di gola (avente altezza $a = s_c / 2^{0.5} = 2.828$) in posizione ribaltata: vengono considerate positive le tensioni normali di trazione e le tensioni tangenziali agenti verso destra e verso il basso. Tutte le tensioni sono espresse in N/mm².

Verifica formula (4.2.84) (Elemento non caricato)

Cordoni	Lung.[mm]	n_{\perp}	t_{\perp}	τ_{\parallel}	FV ₁	VER ₁
Ala inferiore interno lato destro	29.5	0.00	0.00	0.00	0.00	Ok
Ala inferiore interno lato sinistro	29.5	0.00	0.00	0.00	0.00	Ok
Anima lato destro	127.2	0.00	0.00	0.00	0.00	Ok
Anima lato sinistro	127.2	0.00	0.00	0.00	0.00	Ok
Ala superiore interno lato destro	29.5	0.00	0.00	0.00	0.00	Ok
Ala superiore interno lato sinistro	29.5	0.00	0.00	0.00	0.00	Ok

Verifica formula (4.2.85) (Elemento non caricato)

Cordoni	Lung.[mm]	n_{\perp}	t_{\perp}	τ_{\parallel}	FV ₂	VER ₂
Ala inferiore interno lato destro	29.5	0.00	0.00	0.00	0.00	Ok
Ala inferiore interno lato sinistro	29.5	0.00	0.00	0.00	0.00	Ok
Anima lato destro	127.2	0.00	0.00	0.00	0.00	Ok
Anima lato sinistro	127.2	0.00	0.00	0.00	0.00	Ok
Ala superiore interno lato destro	29.5	0.00	0.00	0.00	0.00	Ok
Ala superiore interno lato sinistro	29.5	0.00	0.00	0.00	0.00	Ok

Legenda

n_{\perp} tensione normale perpendicolare all'asse del cordone
 t_{\perp} tensione tangenziale perpendicolare all'asse del cordone
 τ_{\parallel} tensione tangenziale parallela all'asse del cordone
 $FV_1 = (n_{\perp}^2 + t_{\perp}^2 + \tau_{\parallel}^2)^{0.5}$
 $FV_2 = |n_{\perp}| + |t_{\perp}|$
 $VER_i \rightarrow FV_i \leq \beta_i \cdot f_{yk} \quad (\beta_1 \cdot f_{yk} = 192.50 \text{ N/mm}^2 \quad \beta_2 \cdot f_{yk} = 233.75 \text{ N/mm}^2)$

VERIFICHE ELEMENTI TRAVE E/O PILASTRO IN C.A.

LEGENDA TABELLA VERIFICHE ELEMENTI TRAVE E/O PILASTRO IN C.A.

In tabella vengono riportati per ogni elemento il numero identificativo ed il codice di verifica con le sigle **Ok** o **NV**.

Nel caso in cui si sia proceduto alla progettazione con il metodo degli stati limite (**S.L.**) vengono riportati: il rapporto x/d , le verifiche per sollecitazioni proporzionali e la verifica per compressione media con l'indicazione delle combinazioni in cui si sono attinti i rispettivi valori.

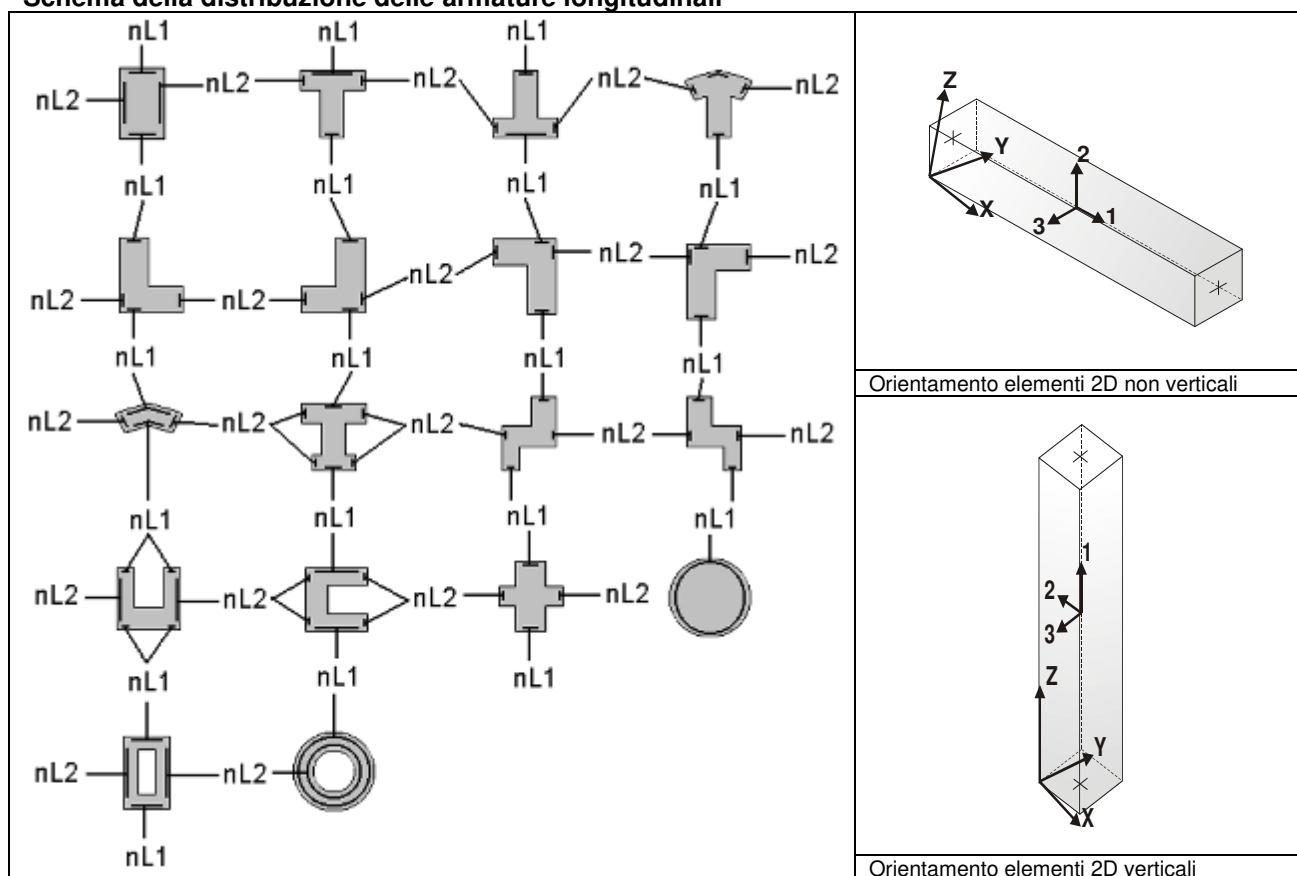
Nel caso in cui si sia proceduto alla progettazione con le tensioni ammissibili (**T.A.**) vengono riportate le massime tensioni nell'elemento (massima compressione nel calcestruzzo, massima compressione media nel calcestruzzo, massima tensione nell'acciaio, massima tensione tangenziale) con l'indicazione delle combinazioni in cui si sono attinti i rispettivi valori.

Nel caso in cui la struttura abbia comportamento dissipativo e sia prevista la progettazione con il criterio della gerarchia delle resistenze (**G.R.**) vengono riportate le verifiche di sovrarresistenza e del nodo.

Per gli elementi tipo pilastro sono riportati numero e diametro dei ferri di vertice, numero e diametro di ferri disposti lungo i lati L_1 (paralleli alla base della sezione) e lungo i lati L_2 (paralleli all'altezza della sezione).

Per gli elementi tipo trave sono riportati infine le quantità di armatura inferiore e superiore.

Schema della distribuzione delle armature longitudinali



Simbologia adottata nelle tabelle di verifica

Per le verifiche agli **S.L.** dei pilastri è presente una tabella con i simboli di seguito descritti:

M P X Y	Numero della pilastrata (P) e posizione in pianta (X,Y)
Pilas.	numero identificativo dell'elemento D2
Note	Codici identificativi delle sezione (s) e materiale (m) pilastro
Stato	Codici relativi all'esito delle verifiche effettuate appresso descritte
Quota	Quota sezione di verifica

%Af	Percentuale di area di armatura rispetto a quella di calcestruzzo
r. snell.	Rapporto di snellezza λ su λ^* : valore superiore a 1 per elementi snelli nel caso in cui viene effettuata la verifica con il metodo diretto dello stato di equilibrio
Armat. long.	Numero e diametro (d) dei ferri di armatura longitudinale distinti in ferri di vertice + ferri di lato nelle posizioni nL1 e nL2, come da schemi in figura precedente
V N/M	Verifica a pressoflessione con rapporto E_d/R_d : valore minore o uguale a 1 per verifica positiva
V N sis	Verifica a compressione solo calcestruzzo con rapporto N_{sd}/N_{rd} ed N_{rd} calcolato come al punto 7.4.4.2.1: valore minore o uguale a 1 per verifica positiva
Staffe	Dati tratto di staffatura oggetto di verifica, nello specifico: numero delle braccia, diametro, passo, lunghezza L tratto
V V/T cls	Verifica a taglio/torsione con rapporto V_{ed}/V_{rd} : valore minore o uguale a 1 per verifica positiva
Rif. cmb.	Riferimento combinazioni da cui si generano le verifiche più gravose per il pilastro

Per le verifiche di gerarchia delle resistenze dei pilastri è presente una tabella con i simboli di seguito descritti:

Pilas.	numero identificativo dell'elemento D2 pilastro
sovr. Xi (Xf)	Verifica sovrarresistenza come da formula 7.4.4 in direzione X, alla base (i) ed alla sommità (f): rapporto tra i momenti resistenti dei pilastri e delle travi. La verifica è positiva se maggiore del γ_{Rd} adottato
sovr. Yi (Yf)	Verifica sovrarresistenza come da formula 7.4.4 in direzione Y, alla base (i) ed alla sommità (f): rapporto tra i momenti resistenti dei pilastri e delle travi. La verifica è positiva se maggiore del γ_{Rd} adottato
M 2-2 i (f)	Valore del momento resistente 2-2 alla base (i) ed alla sommità (f) con massimo momento in presenza dello sforzo normale di calcolo
M 3-3 i (f)	Valore del momento resistente 3-3 alla base (i) ed alla sommità (f) con massimo momento in presenza dello sforzo normale di calcolo
Luce per V	Luce di calcolo per la definizione del taglio (generato dai momenti resistenti)
V M2-2 (M3-3)	Valore del taglio generato dai momenti resistenti 2-2 (3-3)

Per le verifiche dei dettagli costruttivi relativi alla duttilità è presente una tabella con i simboli di seguito descritti:

(Non presente nel caso di comportamento strutturale non dissipativo)

Pilas	Numero identificativo D2 pilastro
ni	Sforzo assiale adimensionalizzato di progetto relativo alla combinazione sismica SLV
alfaomega	Prodotto tra il coefficiente di efficacia del confinamento e il rapporto meccanico dell'armatura trasversale di confinamento all'interno del nodo
V.7.4.29 2-2 (3-3)	Rapporto tra la domanda di staffe minima nel nodo e il rapporto meccanico dell'armatura trasversale di confinamento inserito all'interno del nodo in direzione 2 (3)
V. 7.4.29 Stato	Codici relativi all'esito della verifica 7.4.29
dmu fi 2-2 (3-3)	Domanda in duttilità di curvatura in direzione 2 (3)
cmu fi 2-2 (3-3)	Capacità in duttilità di curvatura in direzione 2 (3)
V. dutt. 2-2 (3-3)	Rapporto tra la domanda in duttilità di curvatura e la capacità in duttilità di curvatura in direzione 2 (3)

Per le verifiche dei nodi trave-pilastro di elementi nuovi è presente una tabella con i simboli di seguito descritti:

Nodo	Numero identificativo del nodo trave-pilastro
Stato	Esito delle verifiche
Pilastro	Numero identificativo D2 pilastro
Diam st	Diametro staffe nodo
Passo	Passo staffe nodo
n. br. 2 (3)	Numero braccia staffe per il taglio in direzione 2 (3)
Bj2 (3)	Larghezza effettiva del nodo per il taglio in direzione 2 (3)
Hjc2 (3)	Distanza tra le giaciture più esterne delle armature del pilastro per il taglio in direzione 2 (3)
V. 7.4.8	Rapporto tra il taglio V_{jbd} e il taglio resistente come da formula 7.4.8
V. Ash	Rapporto tra il passo staffe calcolato secondo il capitolo 7.4.4.3.1. e il passo staffe effettivamente inserita nel nodo. Nel caso di valore indica passo staffe utilizzato deriva dalle formule presenti nel paragrafo 7.4.4.3.1. Nel caso di valore minore di 1 il passo staffe utilizzato deriva del pilastro superiore o inferiore al nodo
7.4.10	Check passo staffe valutato in funzione della formula 7.4.10: <ul style="list-style-type: none"> ➤ SI il passo staffe è calcolato utilizzando la formula 7.4.10; ➤ NO il passo staffe è calcolato utilizzando le formule 7.4.11 e/o 7.4.12; ➤ NR calcolo passo staffe non richiesto;
Rif. comb.	Riferimento combinazioni da cui si generano le verifiche più gravose per il nodo

Per le verifiche dei nodi trave-pilastro di elementi esistenti è presente una tabella con i simboli di seguito descritti:

Pilastro I	Numero identificativo D2 del pilastro inferiore.
Pilastro S	Numero identificativo D2 del pilastro superiore.
Nodo	Numero identificativo del nodo trave-pilastro.
SL cod	Stato limite di riferimento e relativo esito delle verifiche.
ver. (+)	Coefficiente di sicurezza, calcolato come rapporto D/C, nei riguardi della verifica di resistenza a trazione
V +	Azione di Taglio presente al di sopra del nodo nella verifica di resistenza a trazione
V + af s	Sollecitazione di trazione presente nell' armatura longitudinale superiore della trave nella verifica di resistenza a trazione
N +	Azione Assiale presente al di sopra del nodo nella verifica di resistenza a trazione

ver. (-)	Coefficiente di sicurezza, calcolato come rapporto D/C, nei riguardi della verifica di resistenza a compressione
V -	Azione di Taglio presente al di sopra del nodo nella verifica di resistenza a compressione
V - af s	Sollecitazione di trazione presente nell' armatura longitudinale superiore della trave nella verifica di resistenza a compressione
N -	Azione Assiale presente al di sopra del nodo nella verifica di resistenza a compressione
AreaV2	Area resistente del nodo in direzione 2 ($A_{12}=b_{12}*h_{ic2}$).
AreaV3	Area resistente del nodo in direzione 3 ($A_{13}=b_{13}*h_{ic3}$).
Rif. comb.	Combinazione (direzione) di riferimento nella verifica di trazione.

Per le verifiche agli S.L. delle travi è presente una tabella con i simboli di seguito descritti:

M T Z P P	Numero della travata (T), quota media (Z), n° pilastrata iniziale (P) e finale (P) (nodo in assenza di pilastrata)
Trave	numero identificativo dell'elemento D2
Note	Codici identificativi sezione (s) e materiale (m) trave; sono inoltre presenti le sigle relative all'esito delle verifiche effettuate appresso descritte
%Af	Percentuale di area di armatura rispetto a quella di calcestruzzo
Af inf.	Area di armatura longitudinale posta all'intradosso
Af sup	Area di armatura longitudinale posta all'estradosso
Af long.	Area complessiva armatura longitudinale
x/d	rapporto tra posizione dell'asse neutro e altezza utile
V N/M	Verifica a pressoflessione rapporto Ed/Rd: valore minore o uguale a 1 per verifica positiva
Staffe	Dati tratto di staffatura oggetto di verifica, nello specifico: numero delle braccia, diametro, passo, lunghezza L tratto
V V/T cls	Verifica a taglio/torsione con rapporto Ved/Vrd: valore minore o uguale a 1 per verifica positiva
Rif. cmb.	Riferimento combinazioni da cui si generano le verifiche più gravose per la trave

Per le verifiche di gerarchia delle resistenze delle travi è presente una tabella con i simboli di seguito descritti:

Trave	numero identificativo dell'elemento D2 trave
M negativo i (f)	Valore del momento resistente negativo all' estremità iniziale i (finale f) della trave
M positivo i (f)	Valore del momento resistente positivo all' estremità iniziale i (finale f) della trave
Luce per V	Luce di calcolo per la definizione del taglio (generato dai momenti resistenti)
V M-i M+f	Taglio generato dai momenti resistenti negativo i e positivo f
V M+i M-f	Taglio generato dai momenti resistenti positivo i e negativo f
VEd, min	Valore di taglio minimo per verifica condizioni p.to 7.4.4.1.1 armatura diagonale (solo per CD "A")
VEd, max	Valore di taglio massimo per verifica condizioni p.to 7.4.4.1.1 armatura diagonale (solo per CD "A")
Vr1	Valore di taglio come da formula 7.4.1 per armatura diagonale (solo per CD "A")
As	Area singolo ordine armature diagonali come da formula 7.4.2 (solo per CD "A")

Per le verifiche a taglio ciclico di travi e pilastri esistenti è presente una tabella con i simboli di seguito descritti:

Trave/Pilastro	Numero identificativo dell'elemento D2 trave/pilastro
V. SLV	Codice relativo all'esito delle verifiche
Nodo	Numero identificativo del nodo di verifica
Ver. VC	Fattore di sicurezza nei confronti della verifica a taglio ciclico (verificato se < 1.00)
Direz.	Direzione di verifica
N fr	Valore di sforzo normale calcolato con fattore di comportamento fragile
V fr	Valore di taglio calcolato con fattore di comportamento fragile
M fr	Valore di momento calcolato con fattore di comportamento fragile
N dutt	Valore di sforzo normale calcolato con fattore di comportamento duttile
LV	Lunghezza di taglio
Mud,pl	Parte plastica della domanda di duttilità
V cic	Resistenza a taglio in condizioni cicliche (C8.7.2.8)
Cmb	Riferimento combinazioni da cui si generano le verifiche più gravose

					M _P =1	X=1777.5	Y=-48.5					
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
			cm						L=cm			
122	s=3,m=3	ok,ok	0.0	1.51	0.05	4d20 0+2 d20	0.04	0.02	2+3d8/20 L=80	0.03	0.04	555,548,543,535
			40.0	1.51	0.05	4d20 0+2 d20	0.01	0.02	2+3d8/20 L=80	0.03	0.04	535,548,543,535
	[b=1.0;1.0]		80.0	1.51	0.05	4d20 0+2 d20	0.01	0.02	2+3d8/20 L=80	0.03	0.04	559,548,543,535
18	s=3,m=3	ok,ok	80.0	1.51	0.34	4d20 0+2 d20	0.38	0.03	2+3d8/15 L=45	0.13	0.11	529,548,529,529
			284.5	1.51	0.34	4d20 0+2 d20	0.13	0.03	2+3d8/20 L=319	0.13	0.14	529,548,529,529
	[b=1.0;1.0]		489.0	1.51	0.34	4d20 0+2 d20	0.17	0.02	2+3d8/15 L=45	0.13	0.11	548,548,529,529
36	s=3,m=3	ok,ok	489.0	1.51	0.08	4d20 0+2 d20	0.17	0.02	2+3d8/15 L=45	0.12	0.10	548,548,534,529

					M_P= 1	X=1777.5	Y=-48.5					
			547.5	1.51	0.08	4d20 0+2 d20	0.21	0.02	2+3d8/20 L=27	0.12	0.13	545,548,534,529
	[b=1.0;1.0]		606.0	1.51	0.08	4d20 0+2 d20	0.27	0.02	2+3d8/15 L=45	0.12	0.10	545,548,534,529
					M_P= 2	X=0.0	Y=0.0					
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
108	s=4,m=3	ok,ok	0.0	1.40	0.07	4d20 6+0 d20	0.13	0.04	5+2d8/20 L=80	0.11	0.13	534,554,555,535
			40.0	1.40	0.07	4d20 6+0 d20	0.19	0.04	5+2d8/20 L=80	0.11	0.13	535,554,555,535
	[b=1.0;1.0]		80.0	1.40	0.07	4d20 6+0 d20	0.27	0.04	5+2d8/20 L=80	0.11	0.13	535,554,555,535
1	s=4,m=3	ok,ok	80.0	1.95	0.48	4d20 8+2 d20	0.79	0.05	5+2d8/15 L=45	0.21	0.19	555,548,555,555
			284.5	1.40	0.48	4d20 6+0 d20	0.44	0.05	5+2d8/20 L=319	0.21	0.25	555,548,555,555
	[b=1.0;1.0]		489.0	1.40	0.48	4d20 6+0 d20	0.39	0.04	5+2d8/15 L=45	0.21	0.19	535,548,555,555
21	s=4,m=3	ok,ok	489.0	1.40	0.08	4d20 6+0 d20	0.24	0.02	5+2d8/15 L=45	0.12	0.13	534,547,555,392
			547.5	1.40	0.08	4d20 6+0 d20	0.21	0.02	5+2d8/20 L=27	0.12	0.17	536,547,555,392
	[b=1.0;1.0]		606.0	1.40	0.08	4d20 6+0 d20	0.27	0.01	5+2d8/15 L=45	0.12	0.13	535,547,555,392
					M_P= 3	X=493.5	Y=0.0					
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
112	s=15,m=3	ok,ok	0.0	1.26	0.10	4d20 2+0 d20	0.26	0.11	3+2d8/20 L=80	0.19	0.22	535,555,535,555
			40.0	1.26	0.10	4d20 2+0 d20	0.29	0.11	3+2d8/20 L=80	0.19	0.22	535,555,535,555
	[b=1.0;1.0]		80.0	1.26	0.10	4d20 2+0 d20	0.33	0.10	3+2d8/20 L=80	0.19	0.22	535,555,535,555
5	s=15,m=3	ok,ok	80.0	1.26	0.63	4d20 2+0 d20	0.87	0.13	3+2d8/15 L=45	0.20	0.17	555,554,535,534
			284.5	1.26	0.63	4d20 2+0 d20	0.30	0.12	3+2d8/20 L=319	0.20	0.23	555,554,535,534
	[b=1.0;1.0]		489.0	1.26	0.63	4d20 2+0 d20	0.52	0.12	3+2d8/15 L=45	0.20	0.17	535,554,535,534
22	s=15,m=3	ok,ok	489.0	1.26	0.11	4d20 2+0 d20	0.63	0.05	3+2d8/15 L=45	0.12	0.13	554,556,534,534
			547.5	1.26	0.11	4d20 2+0 d20	0.53	0.05	3+2d8/20 L=27	0.12	0.17	372,556,534,534
	[b=1.0;1.0]		606.0	1.26	0.11	4d20 2+0 d20	0.62	0.04	3+2d8/15 L=45	0.12	0.13	555,556,534,534
					M_P= 4	X=983.5	Y=0.0					
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
116	s=15,m=3	ok,ok	0.0	1.26	0.10	4d20 2+0 d20	0.25	0.09	3+2d8/20 L=80	0.14	0.15	535,545,529,529
			40.0	1.26	0.10	4d20 2+0 d20	0.28	0.09	3+2d8/20 L=80	0.14	0.15	535,545,529,529
	[b=1.0;1.0]		80.0	1.26	0.10	4d20 2+0 d20	0.33	0.09	3+2d8/20 L=80	0.14	0.15	535,545,529,529
9	s=15,m=3	ok,ok	80.0	1.26	0.62	4d20 2+0 d20	0.80	0.12	3+2d8/15 L=45	0.18	0.16	555,546,535,534
			284.5	1.26	0.62	4d20 2+0 d20	0.26	0.12	3+2d8/20 L=319	0.18	0.22	555,546,535,534
	[b=1.0;1.0]		489.0	1.26	0.62	4d20 2+0 d20	0.47	0.12	3+2d8/15 L=45	0.18	0.16	535,546,535,534
23	s=15,m=3	ok,ok	489.0	1.26	0.11	4d20 2+0 d20	0.54	0.05	3+2d8/15 L=45	0.13	0.11	553,546,534,534
			547.5	1.26	0.11	4d20 2+0 d20	0.56	0.04	3+2d8/20 L=27	0.13	0.15	553,546,534,534
	[b=1.0;1.0]		606.0	1.26	0.11	4d20 2+0 d20	0.60	0.04	3+2d8/15 L=45	0.13	0.11	555,546,534,534
					M_P= 5	X=1477.0	Y=0.0					
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
121	s=4,m=3	ok,ok	0.0	1.40	0.08	4d20 6+0	0.11	0.04	5+2d8/20	0.04	0.06	536,548,529,534

					M P= 1	X=1777.5	Y=-48.5					
						d20			L=80			
			40.0	1.40	0.08	4d20 6+0 d20	0.14	0.04	5+2d8/20 L=80	0.04	0.06	529,548,529,534
	[b=1.0;1.0]		80.0	1.40	0.08	4d20 6+0 d20	0.19	0.04	5+2d8/20 L=80	0.04	0.06	529,548,529,534
13	s=4,m=3	ok,ok	80.0	1.95	0.51	4d20 8+2 d20	0.77	0.08	5+2d8/15 L=45	0.28	0.27	545,548,529,545
			284.5	1.40	0.51	4d20 6+0 d20	0.28	0.07	5+2d8/20 L=319	0.28	0.35	545,548,529,545
	[b=1.0;1.0]		489.0	1.40	0.51	4d20 6+0 d20	0.55	0.07	5+2d8/15 L=45	0.28	0.27	545,548,529,545
24	s=4,m=3	ok,ok	489.0	1.40	0.11	4d20 6+0 d20	0.46	0.05	5+2d8/15 L=45	0.14	0.12	545,548,548,392
			547.5	1.40	0.11	4d20 6+0 d20	0.37	0.04	5+2d8/20 L=27	0.14	0.16	545,548,548,392
	[b=1.0;1.0]		606.0	1.40	0.11	4d20 6+0 d20	0.39	0.04	5+2d8/15 L=45	0.14	0.12	545,548,548,392
						M P= 6	X=1477.0	Y=198.5				
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
120	s=2,m=3	ok,ok	0.0	1.51	0.11	4d20 2+0 d20	0.21	0.09	3+2d8/20 L=80	0.32	0.40	535,536,545,545
			40.0	1.51	0.11	4d20 2+0 d20	0.29	0.09	3+2d8/20 L=80	0.32	0.40	545,536,545,545
	[b=1.0;1.0]		80.0	1.51	0.11	4d20 2+0 d20	0.49	0.09	3+2d8/20 L=80	0.32	0.40	545,536,545,545
14	s=2,m=3	ok,ok	80.0	1.51	0.17	4d20 2+0 d20	0.55	0.14	3+2d8/15 L=45	0.08	0.07	545,535,560,560
			131.1	1.51	0.17	4d20 2+0 d20	0.48	0.14	3+2d8/20 L=12	0.08	0.10	545,535,560,560
	[b=1.0;1.0]		182.2	1.51	0.17	4d20 2+0 d20	0.41	0.14	3+2d8/15 L=45	0.08	0.07	545,535,560,560
60	s=2,m=3	ok,ok	182.2	1.51	0.14	4d20 2+0 d20	0.29	0.09	3+2d8/15 L=45	0.10	0.09	545,535,554,545
			233.4	1.51	0.14	4d20 2+0 d20	0.23	0.09	3+2d8/20 L=12	0.10	0.12	545,535,554,545
	[b=1.0;1.0]		284.5	1.51	0.14	4d20 2+0 d20	0.17	0.09	3+2d8/15 L=45	0.10	0.09	545,535,554,545
82	s=2,m=3	ok,ok	284.5	1.51	0.11	4d20 2+0 d20	0.06	0.06	3+2d8/15 L=45	0.09	0.08	545,535,560,560
			335.6	1.51	0.11	4d20 2+0 d20	0.03	0.06	3+2d8/20 L=12	0.09	0.11	535,535,560,560
	[b=1.0;1.0]		386.8	1.51	0.11	4d20 2+0 d20	0.08	0.06	3+2d8/15 L=45	0.09	0.08	545,535,560,560
100	s=2,m=3	ok,ok	386.8	1.51	0.09	4d20 2+0 d20	0.21	0.04	3+2d8/15 L=45	0.11	0.10	545,555,559,551
			437.9	1.51	0.09	4d20 2+0 d20	0.28	0.04	3+2d8/20 L=12	0.11	0.13	545,555,559,551
	[b=1.0;1.0]		489.0	1.51	0.09	4d20 2+0 d20	0.35	0.04	3+2d8/15 L=45	0.11	0.10	545,555,559,551
50	s=2,m=3	ok,ok	489.0	1.51	0.08	4d20 2+0 d20	0.12	0.02	3+2d8/15 L=45	0.34	0.28	529,545,532,532
			547.5	1.51	0.08	4d20 2+0 d20	0.19	0.02	3+2d8/20 L=27	0.34	0.38	545,545,532,532
	[b=1.0;1.0]		606.0	1.51	0.08	4d20 2+0 d20	0.29	0.02	3+2d8/15 L=45	0.34	0.28	545,545,532,532
						M P= 7	X=1777.5	Y=198.5				
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
123	s=3,m=3	ok,ok	0.0	1.51	0.06	4d20 0+2 d20	0.07	0.03	2+3d8/20 L=80	0.19	0.27	548,534,545,545
			40.0	1.51	0.06	4d20 0+2 d20	0.11	0.03	2+3d8/20 L=80	0.19	0.27	545,534,545,545
	[b=1.0;1.0]		80.0	1.51	0.06	4d20 0+2 d20	0.25	0.03	2+3d8/20 L=80	0.19	0.27	545,534,545,545
19	s=3,m=3	ok,ok	80.0	1.51	0.14	4d20 0+2 d20	0.30	0.09	2+3d8/15 L=45	0.07	0.06	545,533,555,559
			131.1	1.51	0.14	4d20 0+2 d20	0.26	0.09	2+3d8/20 L=12	0.07	0.08	545,533,555,559
	[b=1.0;1.0]		182.2	1.51	0.14	4d20 0+2 d20	0.22	0.09	2+3d8/15 L=45	0.07	0.06	545,533,555,559

					M P= 1	X=1777.5	Y=-48.5					
62	s=3,m=3	ok,ok	182.2	1.51	0.12	4d20 0+2 d20	0.15	0.07	2+3d8/15 L=45	0.14	0.12	545,534,529,529
			233.4	1.51	0.12	4d20 0+2 d20	0.12	0.07	2+3d8/20 L=12	0.14	0.16	545,534,529,529
	[b=1.0;1.0]		284.5	1.51	0.12	4d20 0+2 d20	0.10	0.07	2+3d8/15 L=45	0.14	0.12	545,534,529,529
84	s=3,m=3	ok,ok	284.5	1.51	0.10	4d20 0+2 d20	0.06	0.04	2+3d8/15 L=45	0.17	0.14	529,534,529,529
			335.6	1.51	0.10	4d20 0+2 d20	0.04	0.04	2+3d8/20 L=12	0.17	0.19	532,534,529,529
	[b=1.0;1.0]		386.8	1.51	0.10	4d20 0+2 d20	0.03	0.04	2+3d8/15 L=45	0.17	0.14	532,534,529,529
102	s=3,m=3	ok,ok	386.8	1.51	0.07	4d20 0+2 d20	0.03	0.03	2+3d8/15 L=45	0.15	0.12	559,533,529,529
			437.9	1.51	0.07	4d20 0+2 d20	0.05	0.02	2+3d8/20 L=12	0.15	0.17	545,533,529,529
	[b=1.0;1.0]		489.0	1.51	0.07	4d20 0+2 d20	0.07	0.02	2+3d8/15 L=45	0.15	0.12	545,533,529,529
49	s=3,m=3	ok,ok	489.0	1.51	0.07	4d20 0+2 d20	0.12	0.02	2+3d8/15 L=45	0.11	0.09	545,529,534,534
			547.5	1.51	0.07	4d20 0+2 d20	0.18	0.02	2+3d8/20 L=27	0.11	0.12	545,529,534,534
	[b=1.0;1.0]		606.0	1.51	0.07	4d20 0+2 d20	0.24	0.01	2+3d8/15 L=45	0.11	0.09	545,529,534,534
					M P= 8	X=0.0	Y=537.0					
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
107	s=2,m=3	ok,ok	0.0	1.51	0.08	4d20 2+0 d20	0.09	0.05	3+2d8/20 L=80	0.03	0.03	534,554,534,529
			40.0	1.51	0.08	4d20 2+0 d20	0.10	0.05	3+2d8/20 L=80	0.03	0.03	534,554,534,529
	[b=1.0;1.0]		80.0	1.51	0.08	4d20 2+0 d20	0.11	0.05	3+2d8/20 L=80	0.03	0.03	534,554,534,529
2	s=2,m=3	ok,ok	80.0	2.51	0.59	4d20 4+2 d20	0.80	0.07	3+2d8/15 L=45	0.21	0.21	554,544,554,554
			284.5	1.51	0.59	4d20 2+0 d20	0.35	0.07	3+2d8/20 L=319	0.21	0.28	554,544,554,554
	[b=1.0;1.0]		489.0	1.51	0.59	4d20 2+0 d20	0.48	0.06	3+2d8/15 L=45	0.22	0.21	554,544,554,554
					M P= 9	X=493.5	Y=537.0					
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
111	s=1,m=3	ok,ok	0.0	1.40	0.15	4d20 0+0 d20	0.51	0.17	2+2d8/20 L=80	0.10	0.14	554,557,554,554
			40.0	1.40	0.15	4d20 0+0 d20	0.43	0.17	2+2d8/20 L=80	0.10	0.14	554,557,554,554
	[b=1.0;1.0]		80.0	1.40	0.15	4d20 0+0 d20	0.36	0.17	2+2d8/20 L=80	0.10	0.14	554,557,554,554
6	s=1,m=3	ok,ok	80.0	1.40	0.78	4d20 0+0 d20	0.36	0.17	2+2d8/15 L=45	0.10	0.10	554,557,554,554
			284.5	1.40	0.78	4d20 0+0 d20	0.10	0.16	2+2d8/20 L=319	0.10	0.13	371,557,554,554
	[b=1.0;1.0]		489.0	1.40	0.78	4d20 0+0 d20	0.41	0.16	2+2d8/15 L=45	0.10	0.10	555,557,554,554
					M P= 10	X=983.5	Y=537.0					
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
115	s=1,m=3	ok,ok	0.0	1.40	0.17	4d20 0+0 d20	0.51	0.22	2+2d8/20 L=80	0.11	0.15	552,543,534,554
			40.0	1.40	0.17	4d20 0+0 d20	0.43	0.22	2+2d8/20 L=80	0.11	0.15	552,543,534,554
	[b=1.0;1.0]		80.0	1.40	0.17	4d20 0+0 d20	0.35	0.22	2+2d8/20 L=80	0.11	0.15	552,543,534,554
10	s=1,m=3	ok,ok	80.0	1.40	0.86	4d20 0+0 d20	0.35	0.22	2+2d8/15 L=45	0.11	0.11	552,543,534,554
			284.5	1.40	0.86	4d20 0+0 d20	0.11	0.21	2+2d8/20 L=319	0.11	0.15	259,543,534,554
	[b=1.0;1.0]		489.0	1.40	0.86	4d20 0+0 d20	0.48	0.21	2+2d8/15 L=45	0.11	0.11	552,543,534,554
46	s=1,m=3	ok,ok	489.0	1.40	0.02	4d20 0+0 d20	0.08	1.19e-03	2+2d8/15 L=45	0.02	0.02	543,559,543,543

					M P= 1	X=1777.5	Y=-48.5					
			547.5	1.40	0.02	4d20 0+0 d20	0.04	0.0	2+2d8/20 L=27	0.02	0.03	543,0,543,543
	[b=1.0;1.0]		606.0	1.40	0.02	4d20 0+0 d20	3.04e-04	0.0	2+2d8/15 L=45	0.02	0.02	548,0,543,543
					M P= 11	X=1477.0	Y=537.0					
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
119	s=1,m=3	ok,ok	0.0	1.40	0.08	4d20 0+0 d20	0.09	0.07	2+2d8/20 L=80	0.03	0.04	543,548,558,558
			40.0	1.40	0.08	4d20 0+0 d20	0.10	0.07	2+2d8/20 L=80	0.03	0.04	543,548,558,558
	[b=1.0;1.0]		80.0	1.40	0.08	4d20 0+0 d20	0.12	0.07	2+2d8/20 L=80	0.03	0.04	543,548,558,558
15	s=1,m=3	ok,ok	80.0	1.40	0.77	4d20 0+0 d20	0.74	0.17	2+2d8/15 L=45	0.14	0.15	548,529,532,548
			284.5	1.40	0.77	4d20 0+0 d20	0.09	0.16	2+2d8/20 L=319	0.14	0.20	369,529,532,548
	[b=1.0;1.0]		489.0	1.40	0.77	4d20 0+0 d20	0.73	0.16	2+2d8/15 L=45	0.14	0.15	548,529,532,548
44	s=1,m=3	ok,ok	489.0	1.40	0.11	4d20 0+0 d20	0.76	0.02	2+2d8/15 L=45	0.37	0.40	548,558,532,548
			547.5	1.40	0.11	4d20 0+0 d20	0.33	0.02	2+2d8/20 L=27	0.37	0.53	548,558,532,548
	[b=1.0;1.0]		606.0	1.40	0.11	4d20 0+0 d20	0.10	0.02	2+2d8/15 L=45	0.37	0.40	548,558,532,548
					M P= 12	X=0.0	Y=1049.0					
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
106	s=2,m=3	ok,ok	0.0	1.51	0.07	4d20 2+0 d20	0.05	0.03	3+2d8/20 L=80	0.02	0.02	541,559,532,532
			40.0	1.51	0.07	4d20 2+0 d20	0.06	0.03	3+2d8/20 L=80	0.02	0.02	541,559,532,532
	[b=1.0;1.0]		80.0	1.51	0.07	4d20 2+0 d20	0.07	0.03	3+2d8/20 L=80	0.02	0.02	541,559,532,532
3	s=2,m=3	ok,ok	80.0	2.51	0.60	4d20 4+2 d20	0.90	0.07	3+2d8/15 L=45	0.25	0.26	554,539,554,554
			284.5	1.51	0.60	4d20 2+0 d20	0.37	0.07	3+2d8/20 L=319	0.25	0.35	554,539,554,554
	[b=1.0;1.0]		489.0	1.51	0.60	4d20 2+0 d20	0.65	0.06	3+2d8/15 L=45	0.25	0.26	554,539,554,554
					M P= 13	X=493.5	Y=1049.0					
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
110	s=1,m=3	ok,ok	0.0	1.40	0.16	4d20 0+0 d20	0.68	0.18	2+2d8/20 L=80	0.13	0.20	560,538,554,554
			40.0	1.40	0.16	4d20 0+0 d20	0.57	0.18	2+2d8/20 L=80	0.13	0.20	560,538,554,554
	[b=1.0;1.0]		80.0	1.40	0.16	4d20 0+0 d20	0.47	0.18	2+2d8/20 L=80	0.13	0.20	560,538,554,554
7	s=1,m=3	ok,ok	80.0	1.40	0.80	4d20 0+0 d20	0.47	0.18	2+2d8/15 L=45	0.13	0.15	560,538,554,554
			284.5	1.40	0.80	4d20 0+0 d20	0.12	0.17	2+2d8/20 L=319	0.13	0.20	484,538,554,554
	[b=1.0;1.0]		489.0	1.40	0.80	4d20 0+0 d20	0.64	0.17	2+2d8/15 L=45	0.13	0.15	560,538,554,554
					M P= 14	X=983.5	Y=1049.0					
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
114	s=1,m=3	ok,ok	0.0	1.40	0.17	4d20 0+0 d20	0.58	0.22	2+2d8/20 L=80	0.10	0.15	548,544,532,558
			40.0	1.40	0.17	4d20 0+0 d20	0.49	0.22	2+2d8/20 L=80	0.10	0.15	548,544,532,558
	[b=1.0;1.0]		80.0	1.40	0.17	4d20 0+0 d20	0.40	0.22	2+2d8/20 L=80	0.10	0.15	548,544,532,558
11	s=1,m=3	ok,ok	80.0	1.40	0.86	4d20 0+0 d20	0.40	0.22	2+2d8/15 L=45	0.10	0.11	548,544,532,558
			284.5	1.40	0.86	4d20 0+0 d20	0.12	0.22	2+2d8/20 L=319	0.10	0.15	260,544,532,558
	[b=1.0;1.0]		489.0	1.40	0.86	4d20 0+0 d20	0.49	0.21	2+2d8/15 L=45	0.10	0.11	548,544,532,558
45	s=1,m=3	ok,ok	489.0	1.40	2.70e-03	4d20 0+0	0.09	0.0	2+2d8/15	0.02	0.03	543,0,543,543

					M P= 1	X=1777.5	Y=-48.5					
						d20			L=45			
			547.5	1.40	2.70e-03	4d20 0+0 d20	0.04	0.0	2+2d8/20 L=27	0.02	0.03	543,0,543,543
	[b=1.0;1.0]		606.0	1.40	2.70e-03	4d20 0+0 d20	2.64e-04	0.0	2+2d8/15 L=45	0.02	0.03	548,0,543,543
					M P= 15	X=1477.0	Y=1049.0					
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
118	s=1,m=3	ok,ok	0.0	1.40	0.07	4d20 0+0 d20	0.07	0.04	2+2d8/20 L=80	0.03	0.04	543,551,534,534
			40.0	1.40	0.07	4d20 0+0 d20	0.09	0.04	2+2d8/20 L=80	0.03	0.04	543,551,534,534
	[b=1.0;1.0]		80.0	1.40	0.07	4d20 0+0 d20	0.10	0.04	2+2d8/20 L=80	0.03	0.04	543,551,534,534
16	s=1,m=3	ok,ok	80.0	1.40	0.84	4d20 0+0 d20	0.75	0.19	2+2d8/15 L=45	0.15	0.16	548,542,532,548
			284.5	1.40	0.84	4d20 0+0 d20	0.11	0.18	2+2d8/20 L=319	0.15	0.21	148,542,532,548
	[b=1.0;1.0]		489.0	1.40	0.84	4d20 0+0 d20	0.62	0.18	2+2d8/15 L=45	0.15	0.16	548,542,532,548
25	s=1,m=3	ok,ok	489.0	1.40	0.13	4d20 0+0 d20	0.49	0.03	2+2d8/15 L=45	0.24	0.26	548,545,548,548
			547.5	1.40	0.13	4d20 0+0 d20	0.19	0.03	2+2d8/20 L=27	0.24	0.35	548,545,548,548
	[b=1.0;1.0]		606.0	1.40	0.13	4d20 0+0 d20	0.11	0.03	2+2d8/15 L=45	0.24	0.26	548,545,548,548
					M P= 16	X=0.0	Y=1598.5					
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
105	s=2,m=3	ok,ok	0.0	1.51	0.06	4d20 2+0 d20	0.10	0.03	3+2d8/20 L=80	0.04	0.05	554,555,172,172
			40.0	1.51	0.06	4d20 2+0 d20	0.09	0.02	3+2d8/20 L=80	0.04	0.05	554,555,172,172
	[b=1.0;1.0]		80.0	1.51	0.06	4d20 2+0 d20	0.08	0.02	3+2d8/20 L=80	0.04	0.05	554,555,172,172
4	s=2,m=3	ok,ok	80.0	2.51	0.44	4d20 4+2 d20	0.76	0.05	3+2d8/15 L=45	0.16	0.15	554,559,554,554
			284.5	1.51	0.44	4d20 2+0 d20	0.52	0.04	3+2d8/20 L=319	0.16	0.21	554,559,554,554
	[b=1.0;1.0]		489.0	1.51	0.44	4d20 2+0 d20	0.39	0.04	3+2d8/15 L=45	0.16	0.15	555,559,554,554
					M P= 17	X=493.5	Y=1598.5					
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
109	s=3,m=3	ok,ok	0.0	1.51	0.06	4d20 0+2 d20	0.11	0.03	2+3d8/20 L=80	0.04	0.05	554,559,534,554
			40.0	1.51	0.06	4d20 0+2 d20	0.14	0.03	2+3d8/20 L=80	0.04	0.05	554,559,534,554
	[b=1.0;1.0]		80.0	1.51	0.06	4d20 0+2 d20	0.16	0.02	2+3d8/20 L=80	0.04	0.05	554,559,534,554
8	s=3,m=3	ok,ok	80.0	1.51	0.57	4d20 0+2 d20	0.64	0.07	2+3d8/15 L=45	0.14	0.10	544,555,535,543
			284.5	1.51	0.57	4d20 0+2 d20	0.38	0.06	2+3d8/20 L=319	0.14	0.14	544,555,535,543
	[b=1.0;1.0]		489.0	1.51	0.57	4d20 0+2 d20	0.68	0.06	2+3d8/15 L=45	0.14	0.10	373,555,535,543
					M P= 18	X=983.5	Y=1598.5					
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
113	s=3,m=3	ok,ok	0.0	1.51	0.04	4d20 0+2 d20	0.12	0.01	2+3d8/20 L=80	0.04	0.04	545,541,532,532
			40.0	1.51	0.04	4d20 0+2 d20	0.13	0.01	2+3d8/20 L=80	0.04	0.04	548,541,532,532
	[b=1.0;1.0]		80.0	1.51	0.04	4d20 0+2 d20	0.15	0.01	2+3d8/20 L=80	0.04	0.04	548,541,532,532
12	s=3,m=3	ok,ok	80.0	1.51	0.56	4d20 0+2 d20	0.61	0.07	2+3d8/15 L=45	0.12	0.11	544,545,543,545
			284.5	1.51	0.56	4d20 0+2 d20	0.33	0.06	2+3d8/20 L=319	0.12	0.15	544,545,543,545
	[b=1.0;1.0]		489.0	1.51	0.56	4d20 0+2 d20	0.69	0.06	2+3d8/15 L=45	0.12	0.11	373,545,543,545

					M P= 1	X=1777.5	Y=-48.5					
					M P= 19	X=1477.0	Y=1598.5					
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
117	s=3,m=3	ok,ok	0.0	1.51	0.06	4d20 0+2 d20	0.04	0.03	2+3d8/20 L=80	0.24	0.29	550,539,552,548
			40.0	1.51	0.06	4d20 0+2 d20	0.19	0.03	2+3d8/20 L=80	0.24	0.29	548,539,552,548
	[b=1.0;1.0]		80.0	1.51	0.06	4d20 0+2 d20	0.35	0.03	2+3d8/20 L=80	0.24	0.29	548,539,552,548
17	s=3,m=3	ok,ok	80.0	1.51	0.14	4d20 0+2 d20	0.51	0.10	2+3d8/15 L=45	0.17	0.15	548,539,543,543
			131.1	1.51	0.14	4d20 0+2 d20	0.43	0.10	2+3d8/20 L=12	0.17	0.20	548,539,543,543
	[b=1.0;1.0]		182.2	1.51	0.14	4d20 0+2 d20	0.35	0.09	2+3d8/15 L=45	0.17	0.15	548,539,543,543
61	s=3,m=3	ok,ok	182.2	1.51	0.11	4d20 0+2 d20	0.25	0.06	2+3d8/15 L=45	0.17	0.15	548,539,556,556
			233.4	1.51	0.11	4d20 0+2 d20	0.21	0.06	2+3d8/20 L=12	0.17	0.19	548,539,556,556
	[b=1.0;1.0]		284.5	1.51	0.11	4d20 0+2 d20	0.18	0.06	2+3d8/15 L=45	0.17	0.15	548,539,556,556
83	s=3,m=3	ok,ok	284.5	1.51	0.09	4d20 0+2 d20	0.11	0.04	2+3d8/15 L=45	0.15	0.13	550,539,556,556
			335.6	1.51	0.09	4d20 0+2 d20	0.07	0.04	2+3d8/20 L=12	0.15	0.17	538,539,556,556
	[b=1.0;1.0]		386.8	1.51	0.09	4d20 0+2 d20	0.07	0.04	2+3d8/15 L=45	0.15	0.13	373,539,556,556
101	s=3,m=3	ok,ok	386.8	1.51	0.07	4d20 0+2 d20	0.19	0.02	2+3d8/15 L=45	0.18	0.15	545,539,545,545
			437.9	1.51	0.07	4d20 0+2 d20	0.25	0.02	2+3d8/20 L=12	0.18	0.20	545,539,545,545
	[b=1.0;1.0]		489.0	1.51	0.07	4d20 0+2 d20	0.32	0.02	2+3d8/15 L=45	0.18	0.15	545,539,545,545
34	s=3,m=3	ok,ok	489.0	1.51	0.02	4d20 0+2 d20	0.28	1.27e-03	2+3d8/15 L=45	0.16	0.14	485,530,529,529
			547.5	1.51	0.02	4d20 0+2 d20	0.13	0.0	2+3d8/20 L=27	0.16	0.18	373,0,529,529
	[b=1.0;1.0]		606.0	1.51	0.02	4d20 0+2 d20	0.02	0.0	2+3d8/15 L=45	0.16	0.14	530,0,529,529
					M P= 20	X=1777.5	Y=1598.5					
Pilas.	Note	Stato	Quota	%Af	r. snell.	Armat. long.	V N/M	V N sis	Staffe	V V/T cls	V V/T acc	Rif. cmb
124	s=3,m=3	ok,ok	0.0	1.51	0.10	4d20 0+2 d20	0.15	0.08	2+3d8/20 L=80	0.24	0.34	541,541,548,548
			40.0	1.51	0.10	4d20 0+2 d20	0.21	0.08	2+3d8/20 L=80	0.24	0.34	550,541,548,548
	[b=1.0;1.0]		80.0	1.51	0.10	4d20 0+2 d20	0.39	0.08	2+3d8/20 L=80	0.24	0.34	548,541,548,548
20	s=3,m=3	ok,ok	80.0	1.51	0.17	4d20 0+2 d20	0.42	0.13	2+3d8/15 L=45	0.25	0.22	548,541,538,538
			131.1	1.51	0.17	4d20 0+2 d20	0.36	0.13	2+3d8/20 L=12	0.25	0.29	548,541,538,538
	[b=1.0;1.0]		182.2	1.51	0.17	4d20 0+2 d20	0.31	0.13	2+3d8/15 L=45	0.25	0.22	548,541,538,538
63	s=3,m=3	ok,ok	182.2	1.51	0.13	4d20 0+2 d20	0.23	0.08	2+3d8/15 L=45	0.10	0.08	548,541,533,533
			233.4	1.51	0.13	4d20 0+2 d20	0.21	0.08	2+3d8/20 L=12	0.10	0.11	548,541,533,533
	[b=1.0;1.0]		284.5	1.51	0.13	4d20 0+2 d20	0.18	0.08	2+3d8/15 L=45	0.10	0.08	548,541,533,533
85	s=3,m=3	ok,ok	284.5	1.51	0.09	4d20 0+2 d20	0.13	0.04	2+3d8/15 L=45	0.10	0.08	548,541,534,534
			335.6	1.51	0.09	4d20 0+2 d20	0.11	0.04	2+3d8/20 L=12	0.10	0.10	548,541,534,534
	[b=1.0;1.0]		386.8	1.51	0.09	4d20 0+2 d20	0.09	0.04	2+3d8/15 L=45	0.10	0.08	548,541,534,534
103	s=3,m=3	ok,ok	386.8	1.51	0.06	4d20 0+2 d20	0.06	0.02	2+3d8/15 L=45	0.10	0.08	548,541,529,532
			437.9	1.51	0.06	4d20 0+2 d20	0.04	0.02	2+3d8/20 L=12	0.10	0.11	532,541,529,532
	[b=1.0;1.0]		489.0	1.51	0.06	4d20 0+2	0.03	0.02	2+3d8/15	0.10	0.08	549,541,529,532

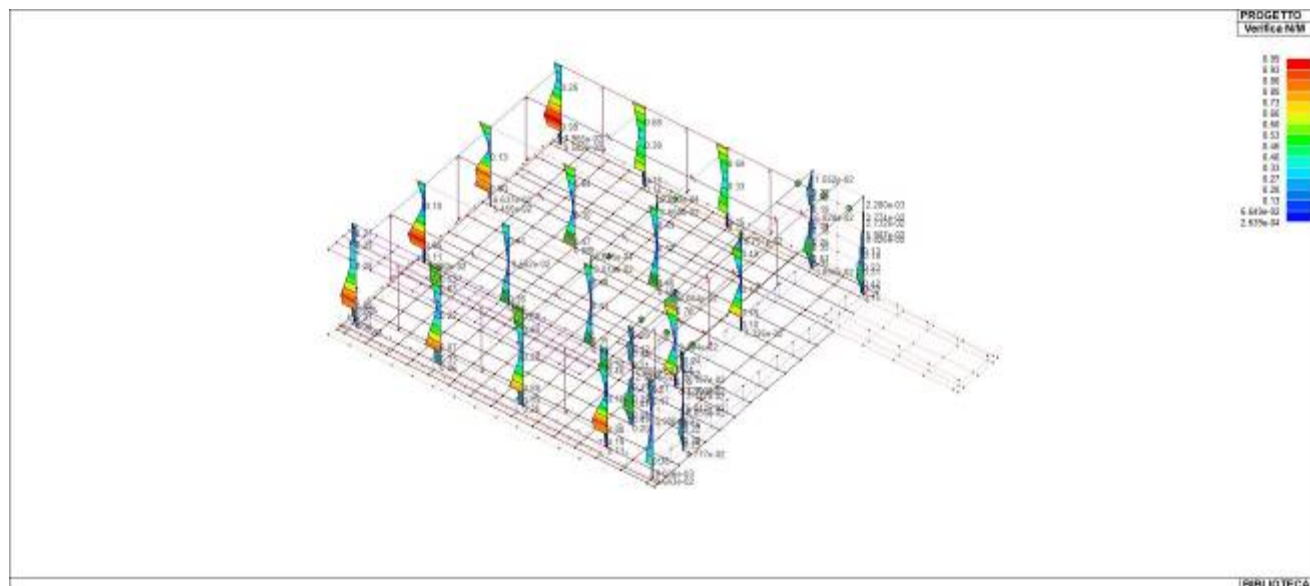
					M P= 1	X=1777.5	Y=-48.5					
						d20			L=45			
35	s=3,m=3	ok,ok	489.0	1.51	0.04	4d20 0+2 d20	0.03	5.92e-03	2+3d8/15 L=45	0.07	0.06	548,538,532,532
			547.5	1.51	0.04	4d20 0+2 d20	0.01	4.55e-03	2+3d8/20 L=27	0.07	0.08	532,538,532,532
	[b=1.0;1.0]		606.0	1.51	0.04	4d20 0+2 d20	5.16e-03	3.19e-03	2+3d8/15 L=45	0.07	0.06	548,538,532,532
Pilas.				%Af	r. snell.		V N/M	V N sis		V V/T cls	V V/T acc	
				2.51	0.86		0.90	0.22		0.37	0.53	

							M T= 1	Z=489.0	P=2	P=16		
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
		cm									L=cm	
26	ok,ok	0.0	0.96	8.0	8.0	0.0	0.22	0.66	0.29	0.28	2d8/10 L=60	554,147,486
	s=6,m=3	268.5	0.96	8.0	8.0	0.0	0.22	0.48	0.05	0.07	2d8/15 L=347	260,560,554
		537.0	0.96	8.0	8.0	0.0	0.22	0.75	0.31	0.29	2d8/10 L=60	555,147,371
64	ok,ok	0.0	0.96	8.0	8.0	0.0	0.22	0.94	0.33	0.31	2d8/10 L=60	554,148,484
	s=6,m=3	256.0	0.96	8.0	8.0	0.0	0.22	0.42	0.11	0.11	2d8/15 L=342	260,554,554
		512.0	0.96	8.0	8.0	0.0	0.22	0.67	0.28	0.26	2d8/10 L=60	555,149,373
86	ok,ok	0.0	1.20	8.0	10.1	0.0	0.25	0.86	0.39	0.35	2d8/10 L=60	484,148,484
	s=6,m=3	274.8	0.96	8.0	8.0	0.0	0.22	0.53	0.12	0.12	2d8/15 L=379	260,554,554
		549.5	0.96	8.0	8.0	0.0	0.22	0.56	0.30	0.27	2d8/10 L=60	555,149,373
							M T= 2	Z=489.0	P=3	P=17		
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
27	ok,ok	0.0	1.05	12.6	12.6	0.0	0.23	0.82	0.41	0.28	4d8/10 L=60	486,482,486
	s=5,m=3	268.5	1.05	12.6	12.6	0.0	0.23	0.63	0.04	0.03	4d8/15 L=377	371,547,555
		537.0	1.31	12.6	15.7	0.0	0.27	0.83	0.44	0.31	4d8/10 L=60	371,372,371
65	ok,ok	0.0	1.31	12.6	15.7	0.0	0.27	0.80	0.41	0.29	4d8/10 L=60	484,488,484
	s=5,m=3	256.0	1.05	12.6	12.6	0.0	0.23	0.47	0.04	0.02	4d8/15 L=362	150,554,554
		512.0	1.05	12.6	12.6	0.0	0.23	0.95	0.40	0.28	4d8/10 L=60	369,373,373
87	ok,ok	0.0	1.57	12.6	18.8	0.0	0.30	0.89	0.53	0.35	4d8/10 L=60	484,264,484
	s=5,m=3	274.8	1.05	12.6	12.6	0.0	0.23	0.80	0.11	0.06	4d8/15 L=402	148,544,484
		549.5	1.05	12.6	12.6	0.0	0.23	0.48	0.42	0.27	4d8/10 L=60	373,261,373
							M T= 3	Z=489.0	P=4	P=18		
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
28	ok,ok	0.0	1.05	12.6	12.6	0.0	0.23	0.78	0.41	0.28	4d8/10 L=60	486,260,486
	s=5,m=3	268.5	1.05	12.6	12.6	0.0	0.23	0.59	0.09	0.03	4d8/15 L=377	371,535,547
		537.0	1.31	12.6	15.7	0.0	0.27	0.91	0.47	0.31	4d8/10 L=60	371,371,371
66	ok,ok	0.0	1.57	12.6	18.8	0.0	0.30	0.81	0.54	0.37	4d8/10 L=60	484,488,484
	s=5,m=3	256.0	1.05	12.6	12.6	0.0	0.23	0.70	0.04	0.02	4d8/15 L=362	261,554,546
		512.0	1.57	12.6	18.8	0.0	0.30	0.79	0.53	0.37	4d8/10 L=60	369,373,373
88	ok,ok	0.0	1.83	12.6	22.0	0.0	0.34	0.82	0.57	0.35	4d8/10 L=60	484,260,484
	s=5,m=3	274.8	1.05	12.6	12.6	0.0	0.23	0.75	0.17	0.07	4d8/15 L=402	260,544,484
		549.5	1.05	12.6	12.6	0.0	0.23	0.49	0.45	0.27	4d8/10 L=60	373,261,373
							M T= 4	Z=489.0	P=5	P=19		
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
29	ok,ok	0.0	0.96	8.0	8.0	0.0	0.22	0.45	0.36	0.17	2d8/10 L=128	545,532,548
	s=6,m=3	99.2	0.96	8.0	8.0	0.0	0.22	0.19	0.37	0.17	2d8/10 L=128	545,529,545
		198.5	0.96	8.0	8.0	0.0	0.22	0.56	0.42	0.22	2d8/10 L=128	545,529,545
67	ok,ok	0.0	0.49	10.0	10.0	0.0	0.17	0.59	0.31	0.12	4d8/10 L=60	548,535,548
	s=7,m=3	169.2	0.49	10.0	10.0	0.0	0.17	0.28	0.29	0.11	4d8/15 L=178	537,543,545
		338.5	0.49	10.0	10.0	0.0	0.17	0.80	0.34	0.14	4d8/10 L=60	545,543,545
89	ok,ok	0.0	0.49	10.0	10.0	0.0	0.17	0.96	0.24	0.26	4d8/10 L=60	484,148,484

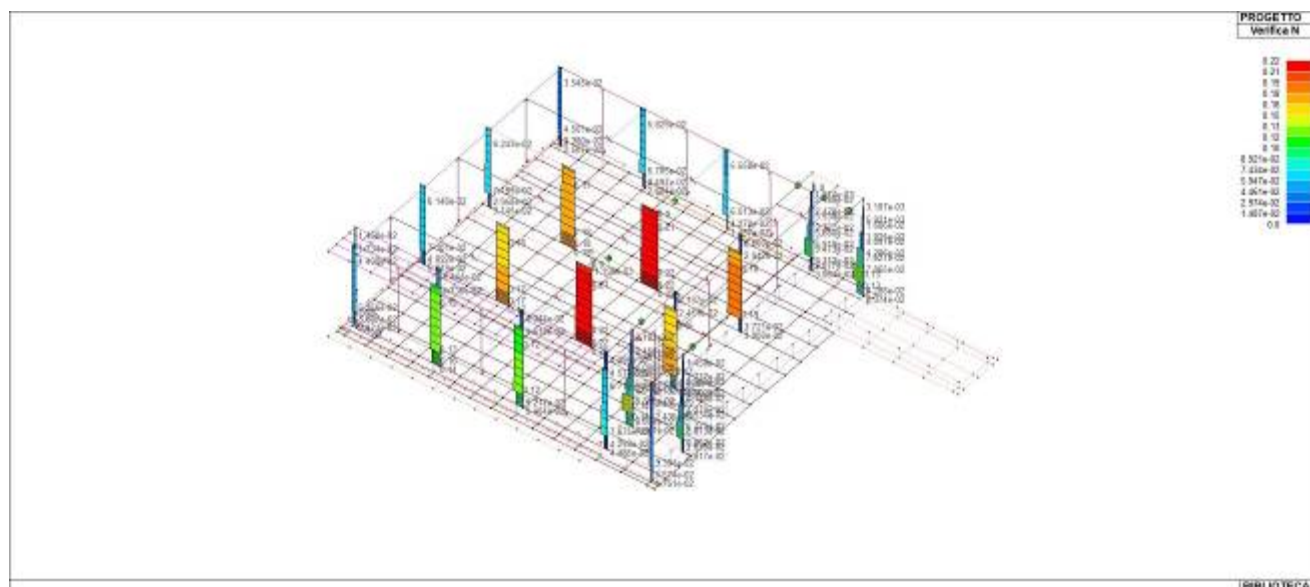
							M T= 1	Z=489.0	P=2	P=16			
	s=7,m=3	256.0	0.49	10.0	10.0	0.0	0.17	0.63	0.06	0.04	4d8/15 L=362	150,529,548	
		512.0	0.49	10.0	10.0	0.0	0.17	0.99	0.24	0.26	4d8/10 L=60	545,261,373	
104	ok,ok	0.0	0.59	10.0	12.1	0.0	0.19	0.96	0.24	0.21	4d8/10 L=60	548,260,484	
	s=7,m=3	274.8	0.49	10.0	10.0	0.0	0.17	0.51	0.11	0.08	4d8/15 L=402	484,544,548	
		549.5	0.49	10.0	10.0	0.0	0.17	0.72	0.20	0.17	4d8/10 L=60	545,261,373	
							M T= 5	Z=489.0	P=16	P=19			
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb	
30	ok,ok	0.0	0.67	4.0	4.0	0.0	0.24	0.45	0.31	0.04	2d8/10 L=60	544,373,544	
	s=9,m=3	246.7	0.67	4.0	4.0	0.0	0.24	0.11	0.26	0.03	2d8/15 L=336	539,373,544	
		493.5	0.67	4.0	4.0	0.0	0.24	0.30	0.28	0.03	2d8/10 L=60	544,369,541	
68	ok,ok	0.0	0.67	4.0	4.0	0.0	0.24	0.56	0.11	0.05	2d8/10 L=60	539,512,544	
	s=9,m=3	245.0	0.67	4.0	4.0	0.0	0.24	0.11	0.05	0.04	2d8/15 L=320	539,554,544	
		490.0	0.67	4.0	4.0	0.0	0.24	0.39	0.07	0.03	2d8/10 L=60	539,534,541	
90	ok,ok	0.0	0.67	4.0	4.0	0.0	0.24	0.47	0.37	0.04	2d8/10 L=60	539,485,539	
	s=9,m=3	246.8	0.67	4.0	4.0	0.0	0.24	0.14	0.32	0.03	2d8/15 L=323	539,261,539	
		493.5	0.67	4.0	4.0	0.0	0.24	0.26	0.35	0.03	2d8/10 L=60	539,481,538	
							M T= 6	Z=489.0	P=12	P=15			
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb	
31	ok,ok	0.0	0.56	4.0	4.0	0.0	0.22	0.34	0.29	0.04	2d8/10 L=60	544,554,544	
	s=8,m=3	246.8	0.56	4.0	4.0	0.0	0.22	0.11	0.26	0.02	2d8/15 L=346	369,554,541	
		493.5	0.56	4.0	4.0	0.0	0.22	0.30	0.29	0.04	2d8/10 L=60	541,554,541	
69	ok,ok	0.0	0.56	4.0	4.0	0.0	0.22	0.39	0.15	0.04	2d8/10 L=60	543,263,288	
	s=8,m=3	245.0	0.56	4.0	4.0	0.0	0.22	0.10	0.11	0.02	2d8/15 L=340	558,263,543	
		490.0	0.56	4.0	4.0	0.0	0.22	0.12	0.13	0.03	2d8/10 L=60	541,147,542	
91	ok,ok	0.0	0.35	12.6	12.6	0.0	0.05	0.04	0.10	0.03	2d8/10 L=114	542,260,284	
	s=16,m=3	246.8	0.35	12.6	12.6	0.0	0.05	0.06	0.07	0.02	2d8/20 L=235	542,532,543	
		493.5	0.35	12.6	12.6	0.0	0.05	0.04	0.09	0.03	2d8/10 L=114	542,484,542	
							M T= 7	Z=489.0	P=8	P=11			
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb	
32	ok,ok	0.0	0.56	4.0	4.0	0.0	0.22	0.36	0.18	0.04	2d8/10 L=60	535,555,535	
	s=8,m=3	246.8	0.56	4.0	4.0	0.0	0.22	0.11	0.17	0.03	2d8/15 L=346	146,554,534	
		493.5	0.56	4.0	4.0	0.0	0.22	0.41	0.20	0.05	2d8/10 L=60	534,554,534	
70	ok,ok	0.0	0.56	4.0	4.0	0.0	0.22	0.44	0.15	0.04	2d8/10 L=60	535,263,535	
	s=8,m=3	245.0	0.56	4.0	4.0	0.0	0.22	0.07	0.11	0.02	2d8/15 L=340	541,263,535	
		490.0	0.56	4.0	4.0	0.0	0.22	0.18	0.13	0.03	2d8/10 L=60	534,147,534	
92	ok,ok	0.0	0.35	12.6	12.6	0.0	0.05	0.08	0.07	0.03	2d8/10 L=114	535,371,543	
	s=16,m=3	246.8	0.35	12.6	12.6	0.0	0.05	0.09	0.04	0.03	2d8/20 L=235	535,379,543	
		493.5	0.35	12.6	12.6	0.0	0.05	0.10	0.06	0.03	2d8/10 L=114	535,529,542	
							M T= 8	Z=489.0	P=2	P=5			
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb	
33	ok,ok	0.0	0.42	8.0	8.0	0.0	0.16	0.62	0.13	0.07	4d8/10 L=60	535,375,535	
	s=17,m=3	246.8	0.42	8.0	8.0	0.0	0.16	0.18	0.11	0.04	4d8/15 L=346	558,534,534	
		493.5	0.42	8.0	8.0	0.0	0.16	0.62	0.15	0.07	4d8/10 L=60	534,534,534	
71	ok,ok	0.0	0.42	8.0	8.0	0.0	0.16	0.63	0.11	0.07	4d8/10 L=60	535,535,535	
	s=17,m=3	245.0	0.42	8.0	8.0	0.0	0.16	0.17	0.08	0.04	4d8/15 L=340	548,534,535	
		490.0	0.42	8.0	8.0	0.0	0.16	0.53	0.12	0.07	4d8/10 L=60	534,534,534	
93	ok,ok	0.0	0.42	8.0	8.0	0.0	0.16	0.60	0.15	0.07	4d8/10 L=60	536,535,536	
	s=17,m=3	246.8	0.42	8.0	8.0	0.0	0.16	0.23	0.12	0.03	4d8/15 L=346	532,535,536	
		493.5	0.42	8.0	8.0	0.0	0.16	0.44	0.12	0.06	4d8/10 L=60	533,555,533	
							M T= 9	Z=606.0	P=1	P=7			
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb	
37	ok,ok	0.0	0.67	8.0	8.0	0.0	0.24	0.29	0.17	0.15	2d8/10 L=60	545,532,548	

							M T= 1	Z=489.0	P=2	P=16			
	s=12,m=3	123.5	0.67	8.0	8.0	0.0	0.24	0.14	0.16	0.13	2d8/12 L=102	532,529,545	
		247.0	0.67	8.0	8.0	0.0	0.24	0.50	0.20	0.17	2d8/10 L=60	545,529,545	
							M T= 10	Z=606.0	P=5	P=6			
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb	
38	ok,ok	0.0	0.60	6.0	6.0	0.0	0.15	3.64e-03	0.12	0.03	2d8/20 L=64	550,502,502	
	s=14,m=3	32.2	0.60	6.0	6.0	0.0	0.15	0.03	0.12	0.04	2d8/20 L=64	502,502,502	
		64.5	0.60	6.0	6.0	0.0	0.15	0.06	0.13	0.04	2d8/20 L=64	502,502,502	
96	ok,ok	0.0	0.60	6.0	6.0	0.0	0.15	0.08	0.30	0.08	2d8/20 L=50	554,162,502	
	s=14,m=3	25.2	0.60	6.0	6.0	0.0	0.15	0.12	0.31	0.08	2d8/20 L=50	502,162,502	
		50.5	0.60	6.0	6.0	0.0	0.15	0.18	0.31	0.09	2d8/20 L=50	502,162,502	
78	ok,ok	0.0	0.60	6.0	6.0	0.0	0.15	0.19	0.52	0.13	2d8/20 L=50	502,162,502	
	s=14,m=3	25.2	0.60	6.0	6.0	0.0	0.15	0.27	0.52	0.13	2d8/20 L=50	502,162,502	
		50.5	0.60	6.0	6.0	0.0	0.15	0.36	0.53	0.14	2d8/20 L=50	502,162,502	
72	ok,ok	0.0	0.60	6.0	6.0	0.0	0.15	0.36	0.75	0.25	2d8/20 L=3	166,276,386	
	s=14,m=3	24.2	0.60	6.0	6.0	0.0	0.15	0.51	0.76	0.27	2d8/20 L=3	166,276,370	
		48.5	0.60	6.0	6.0	0.0	0.15	0.67	0.77	0.29	2d8/20 L=3	166,276,370	
43	ok,ok	0.0	0.60	6.0	6.0	0.0	0.15	0.56	0.32	0.19	2d8/10 L=128	548,548,548	
	s=14,m=3	99.2	0.60	6.0	6.0	0.0	0.15	0.15	0.31	0.19	2d8/10 L=128	548,529,545	
		198.5	0.60	6.0	6.0	0.0	0.15	0.59	0.34	0.21	2d8/10 L=128	548,529,545	
							M T= 11	Z=606.0	N=484	N=516			
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb	
39	ok,ok	0.0	0.60	6.0	6.0	0.0	0.15	4.78e-03	0.11	0.03	2d8/20 L=64	554,392,390	
	s=14,m=3	32.2	0.60	6.0	6.0	0.0	0.15	0.03	0.11	0.04	2d8/20 L=64	386,392,390	
		64.5	0.60	6.0	6.0	0.0	0.15	0.06	0.12	0.04	2d8/20 L=64	390,392,390	
97	ok,ok	0.0	0.60	6.0	6.0	0.0	0.15	0.07	0.28	0.08	2d8/20 L=50	390,392,390	
	s=14,m=3	25.2	0.60	6.0	6.0	0.0	0.15	0.12	0.28	0.08	2d8/20 L=50	390,392,390	
		50.5	0.60	6.0	6.0	0.0	0.15	0.17	0.28	0.09	2d8/20 L=50	390,392,390	
79	ok,ok	0.0	0.60	6.0	6.0	0.0	0.15	0.19	0.47	0.13	2d8/20 L=50	390,400,390	
	s=14,m=3	25.2	0.60	6.0	6.0	0.0	0.15	0.27	0.47	0.13	2d8/20 L=50	390,400,390	
		50.5	0.60	6.0	6.0	0.0	0.15	0.35	0.48	0.14	2d8/20 L=50	390,400,390	
73	ok,ok	0.0	0.60	6.0	6.0	0.0	0.15	0.37	0.81	0.21	2d8/20 L=3	390,400,392	
	s=14,m=3	24.2	0.60	6.0	6.0	0.0	0.15	0.50	0.82	0.22	2d8/20 L=3	390,400,392	
		48.5	0.60	6.0	6.0	0.0	0.15	0.63	0.82	0.22	2d8/20 L=3	390,400,392	
							M T= 12	Z=606.0	N=486	N=517			
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb	
40	ok,ok	0.0	0.50	6.0	6.0	0.0	0.15	0.01	0.07	0.02	2d8/20 L=64	482,535,376	
	s=13,m=1	32.2	0.50	6.0	6.0	0.0	0.15	0.01	0.07	0.03	2d8/20 L=64	545,535,376	
		64.5	0.50	6.0	6.0	0.0	0.15	0.04	0.07	0.04	2d8/20 L=64	376,535,376	
98	ok,ok	0.0	0.50	6.0	6.0	0.0	0.15	0.04	0.19	0.13	2d8/20 L=50	376,535,260	
	s=13,m=1	25.2	0.50	6.0	6.0	0.0	0.15	0.12	0.19	0.13	2d8/20 L=50	372,535,260	
		50.5	0.50	6.0	6.0	0.0	0.15	0.20	0.19	0.14	2d8/20 L=50	372,535,260	
80	ok,ok	0.0	0.50	6.0	6.0	0.0	0.15	0.22	0.31	0.24	2d8/20 L=50	372,534,260	
	s=13,m=1	25.2	0.50	6.0	6.0	0.0	0.15	0.37	0.31	0.25	2d8/20 L=50	372,534,260	
		50.5	0.50	6.0	6.0	0.0	0.15	0.52	0.32	0.25	2d8/20 L=50	372,534,260	
74	ok,ok	0.0	0.67	6.0	8.0	0.0	0.17	0.42	0.54	0.42	2d8/20 L=23	260,534,482	
	s=13,m=1	24.2	0.67	6.0	8.0	0.0	0.17	0.62	0.55	0.43	2d8/20 L=23	484,534,482	
		48.5	0.67	6.0	8.0	0.0	0.17	0.83	0.55	0.44	2d8/20 L=23	484,534,482	
							M T= 13	Z=606.0	N=487	N=518			
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb	
41	ok,ok	0.0	0.50	6.0	6.0	0.0	0.15	0.01	0.07	0.03	2d8/20 L=64	545,534,372	
	s=13,m=1	32.2	0.50	6.0	6.0	0.0	0.15	0.02	0.07	0.03	2d8/20 L=64	545,534,372	
		64.5	0.50	6.0	6.0	0.0	0.15	0.04	0.07	0.04	2d8/20 L=64	376,534,372	
99	ok,ok	0.0	0.50	6.0	6.0	0.0	0.15	0.05	0.18	0.12	2d8/20 L=50	376,534,484	
	s=13,m=1	25.2	0.50	6.0	6.0	0.0	0.15	0.12	0.18	0.13	2d8/20 L=50	372,534,484	
		50.5	0.50	6.0	6.0	0.0	0.15	0.20	0.18	0.14	2d8/20 L=50	372,534,484	
81	ok,ok	0.0	0.50	6.0	6.0	0.0	0.15	0.22	0.28	0.24	2d8/20 L=50	372,534,484	
	s=13,m=1	25.2	0.50	6.0	6.0	0.0	0.15	0.37	0.29	0.24	2d8/20 L=50	372,534,484	
		50.5	0.50	6.0	6.0	0.0	0.15	0.52	0.29	0.25	2d8/20 L=50	372,534,484	
75	ok,ok	0.0	0.67	6.0	8.0	0.0	0.17	0.42	0.49	0.42	2d8/20 L=23	372,535,482	
	s=13,m=1	24.2	0.67	6.0	8.0	0.0	0.17	0.62	0.49	0.42	2d8/20 L=23	148,535,482	
		48.5	0.67	6.0	8.0	0.0	0.17	0.82	0.49	0.43	2d8/20 L=23	148,535,482	
							M T= 14	Z=606.0	N=483	N=489			
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb	
42	ok,ok	0.0	0.67	4.0	4.0	0.0	0.25	0.23	0.21	0.03	2d8/10 L=60	386,552,394	

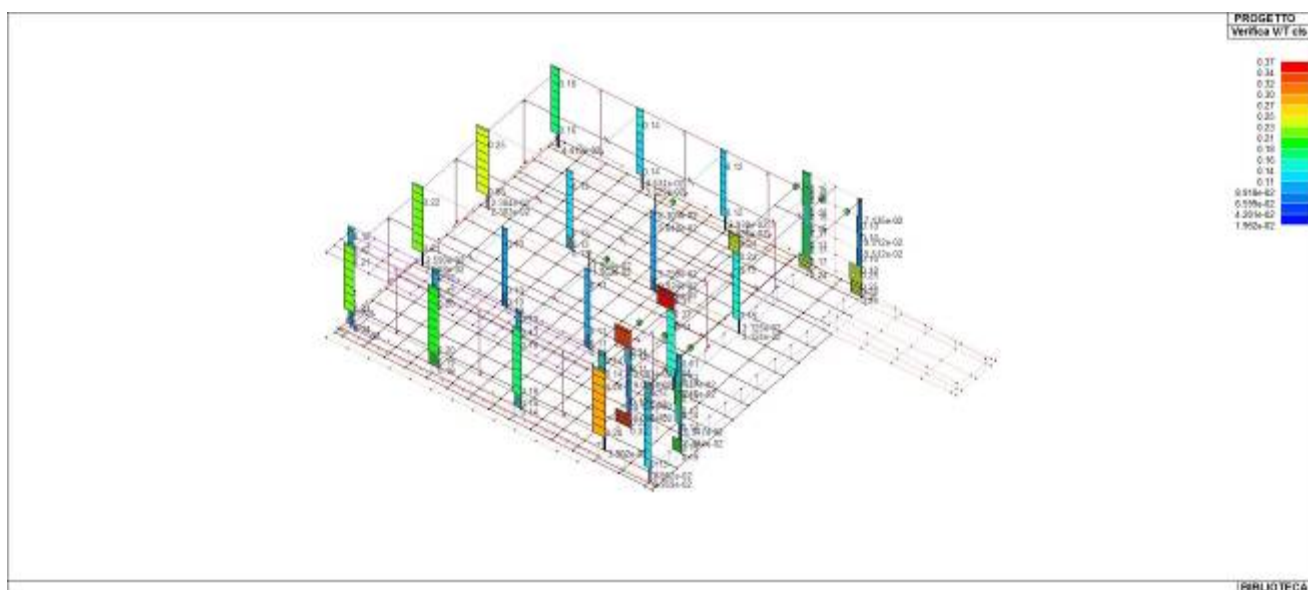
							M T= 1	Z=489.0	P=2	P=16		
	s=9,m=1	150.2	0.67	4.0	4.0	0.0	0.25	0.08	0.19	0.02	2d8/15 L=155	535,552,555
		300.5	0.67	4.0	4.0	0.0	0.25	0.14	0.20	0.01	2d8/10 L=60	535,546,554
Trave			%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc		
			1.83	12.56	21.98	0.0	0.34	0.99	0.82	0.44		



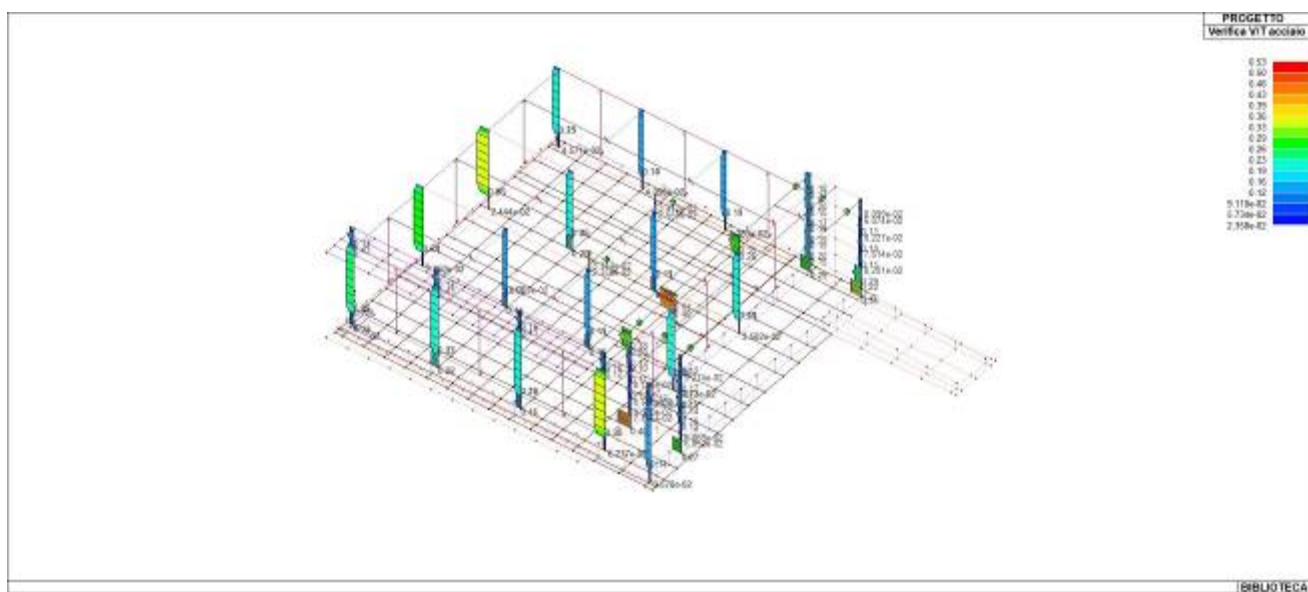
71_CA_PIL_17_Verifica NM



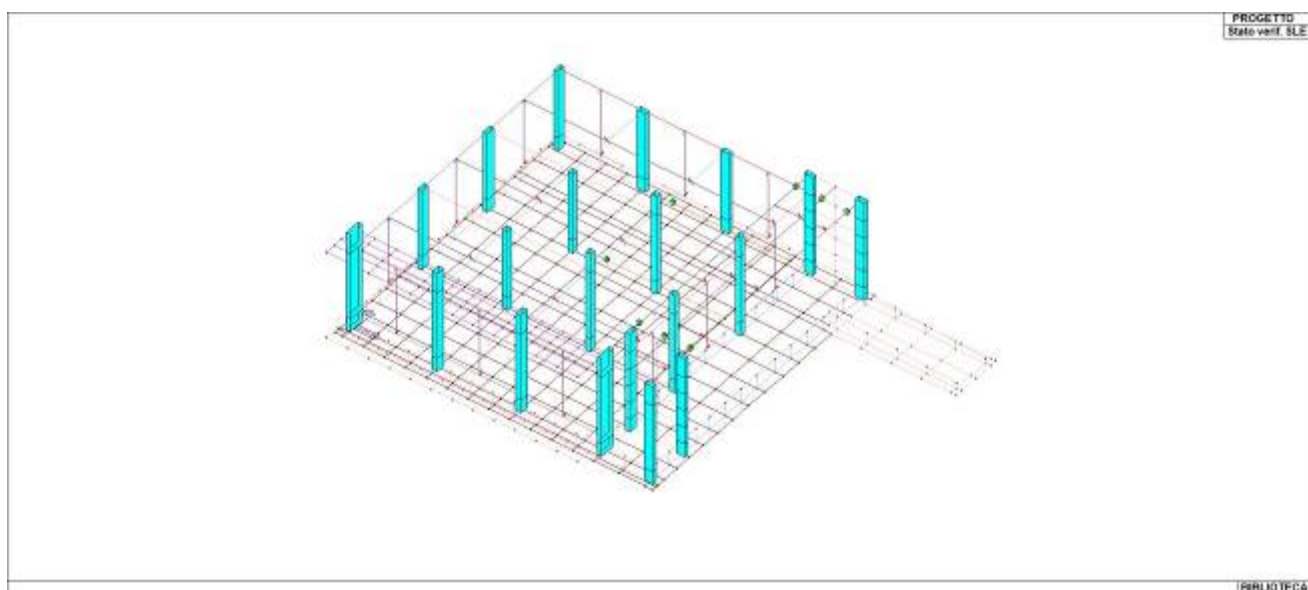
71_CA_PIL_18_Verifica N



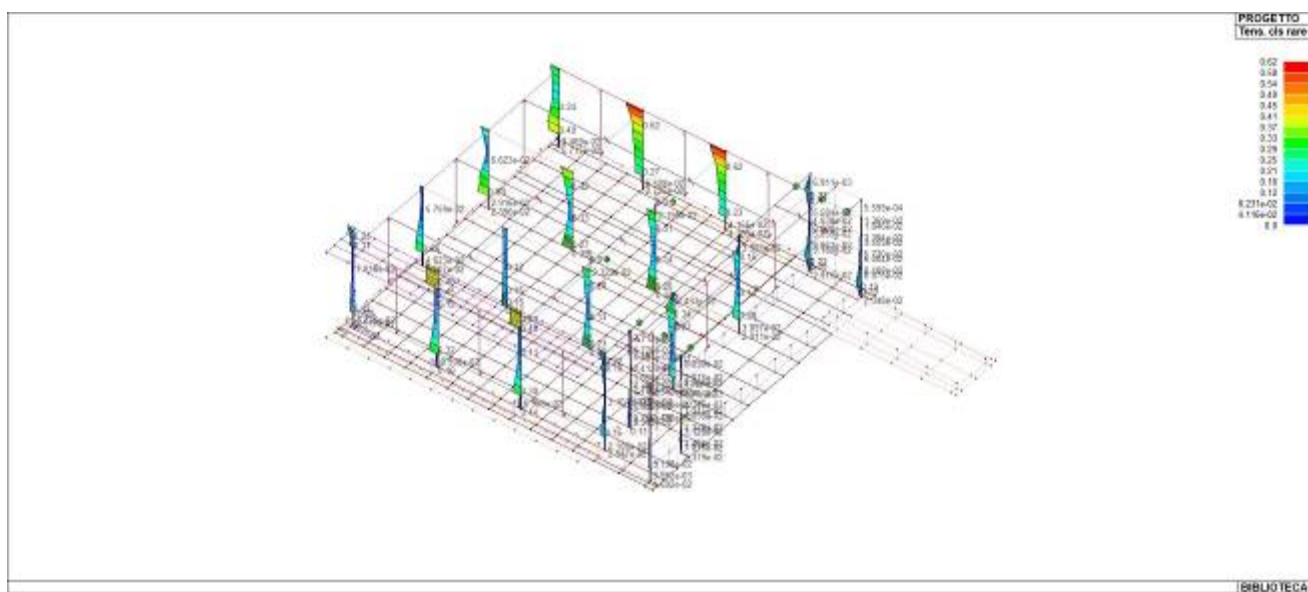
71_CA_PIL_20_Verifica VT cls



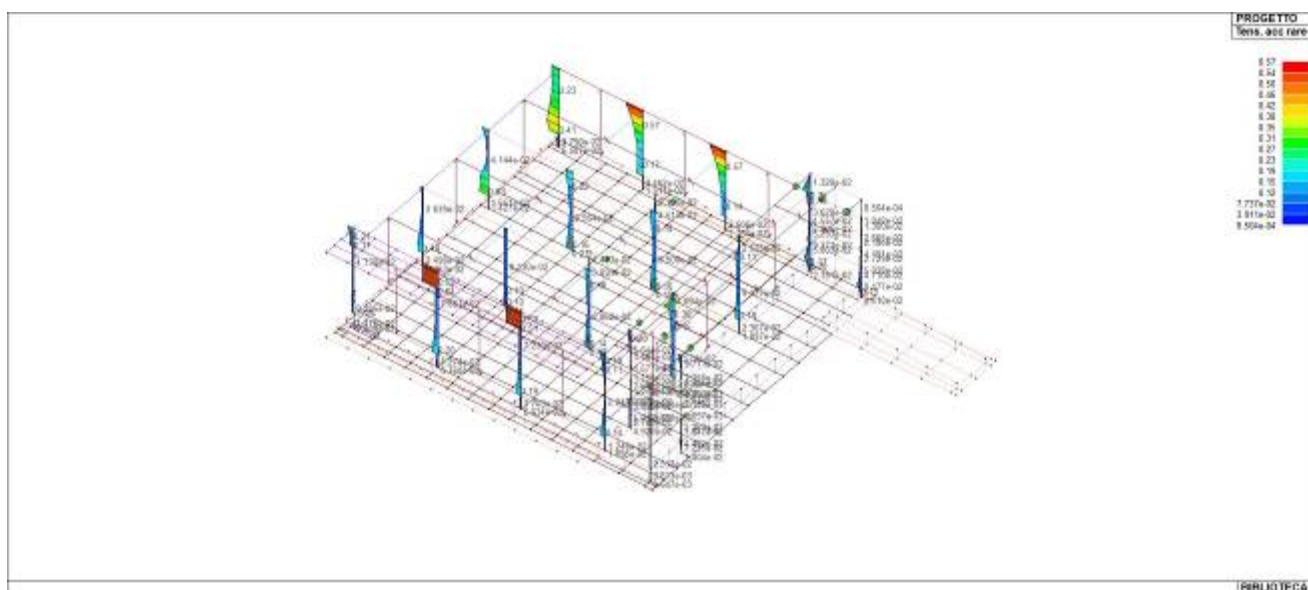
71_CA_PIL_21_Verifica VT acciaio



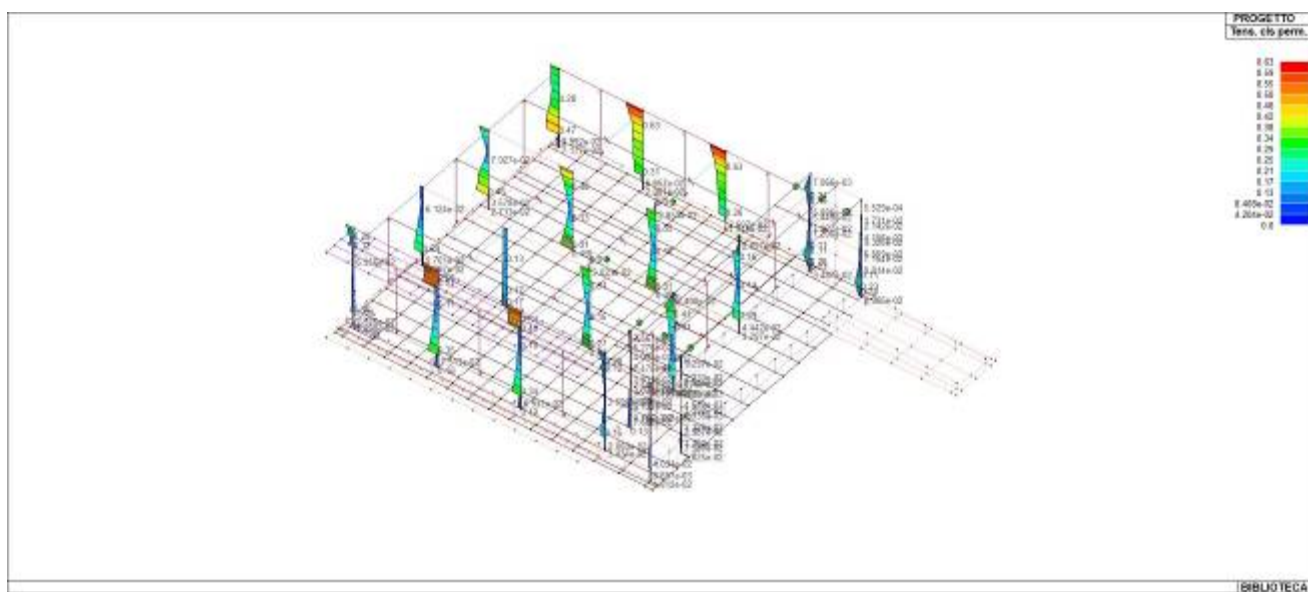
71_CA_PIL_36_Stato verif SLE



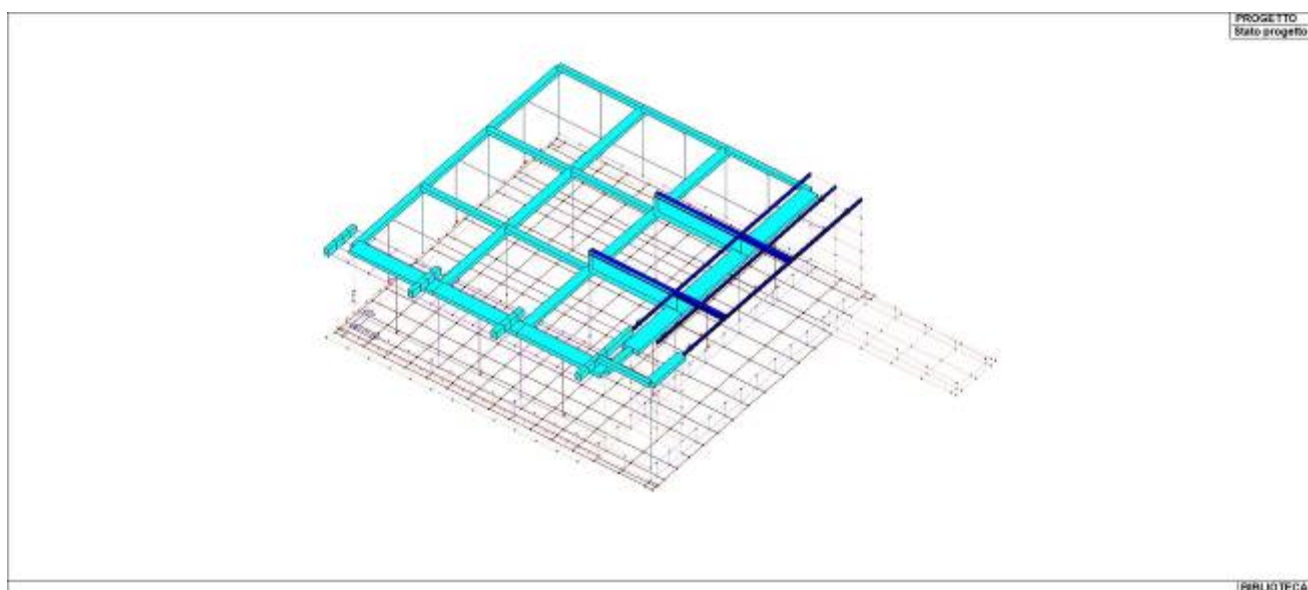
71_CA_PIL_37_Tens cls rare



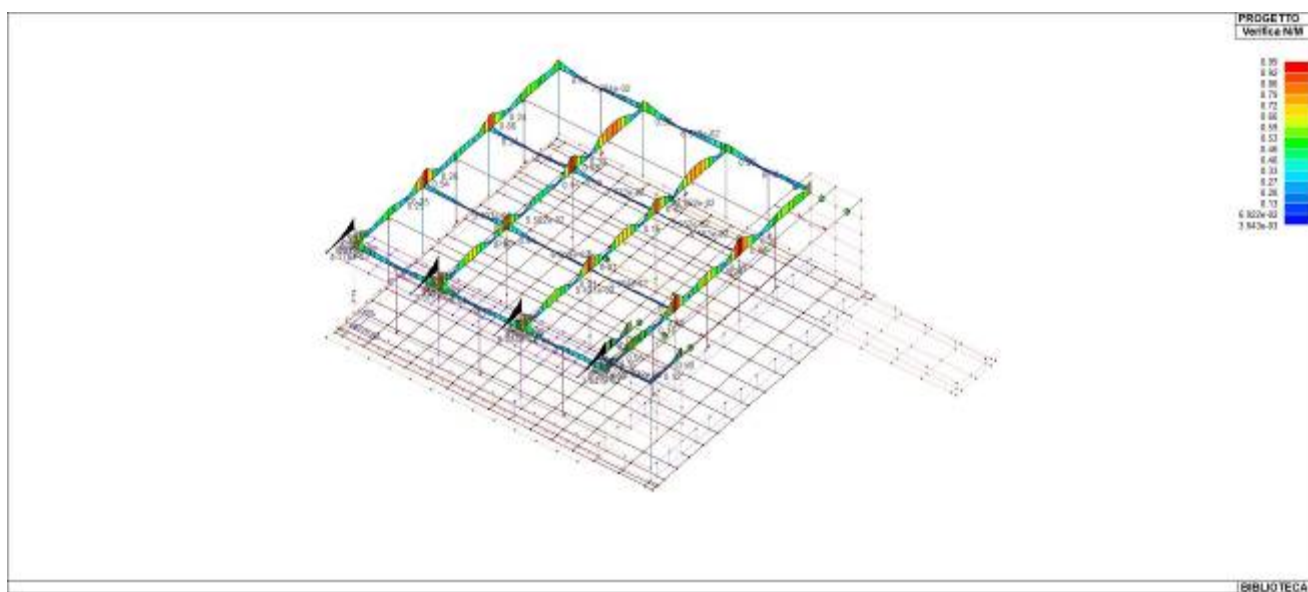
71_CA_PIL_38_Tens acc rare



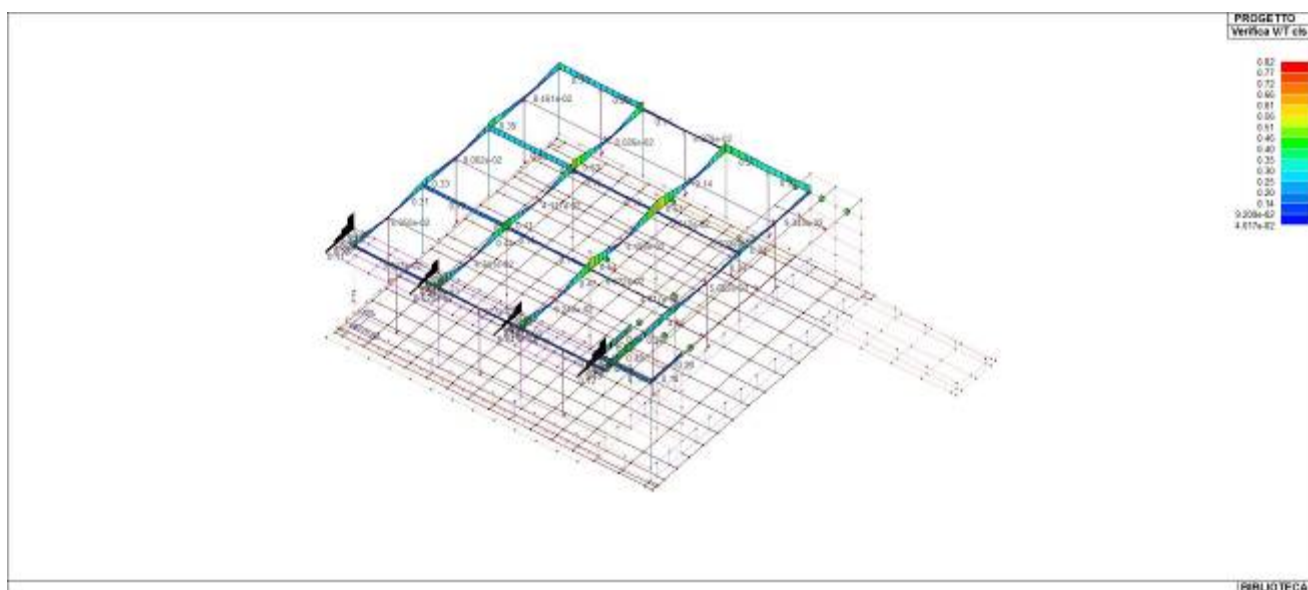
71_CA_PIL_39_Tens cls perm



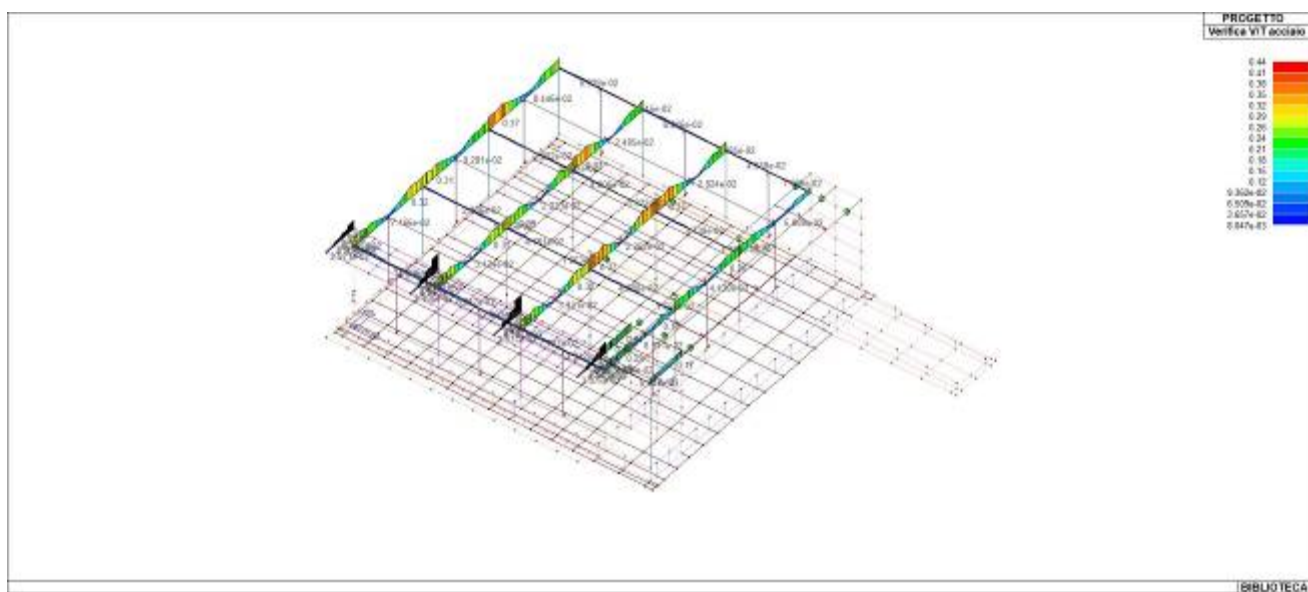
71_CA_TRV_01_Stato progetto



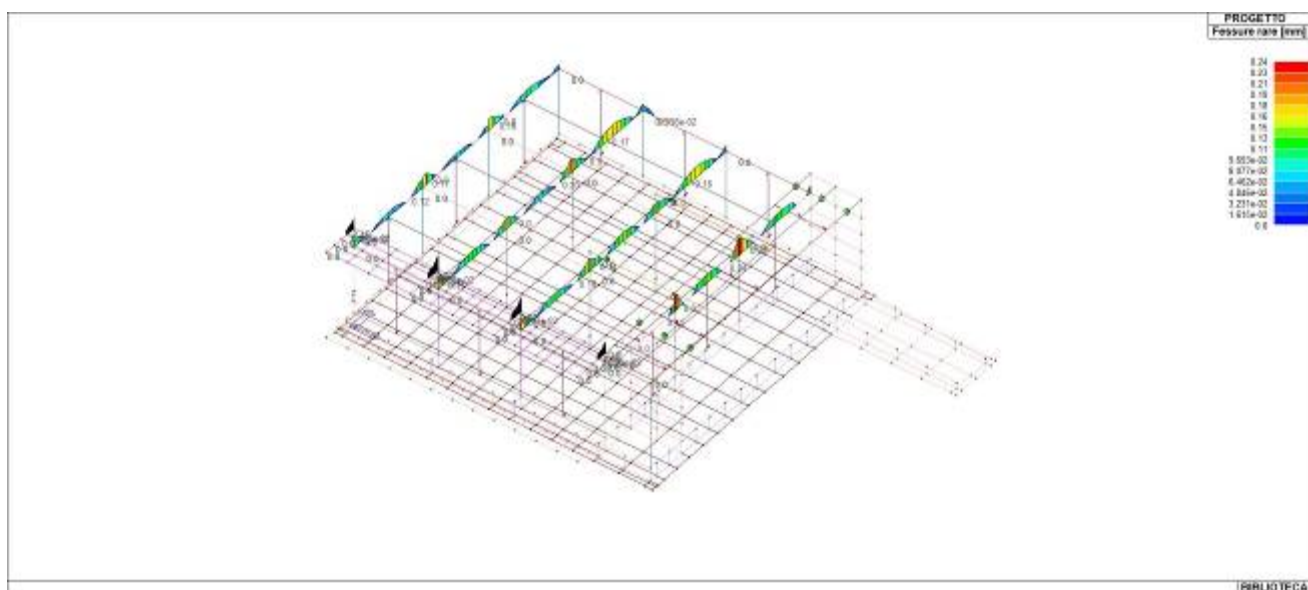
71_CA_TRV_09_Verifica NM



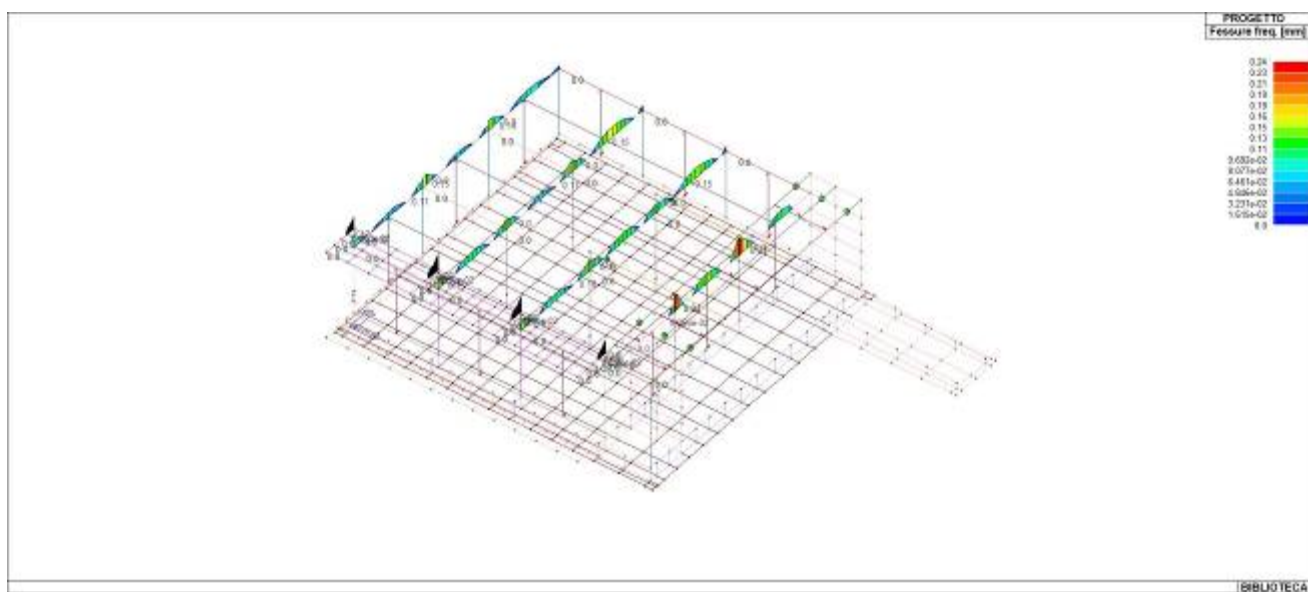
71_CA_TRV_11_Verifica VT cls



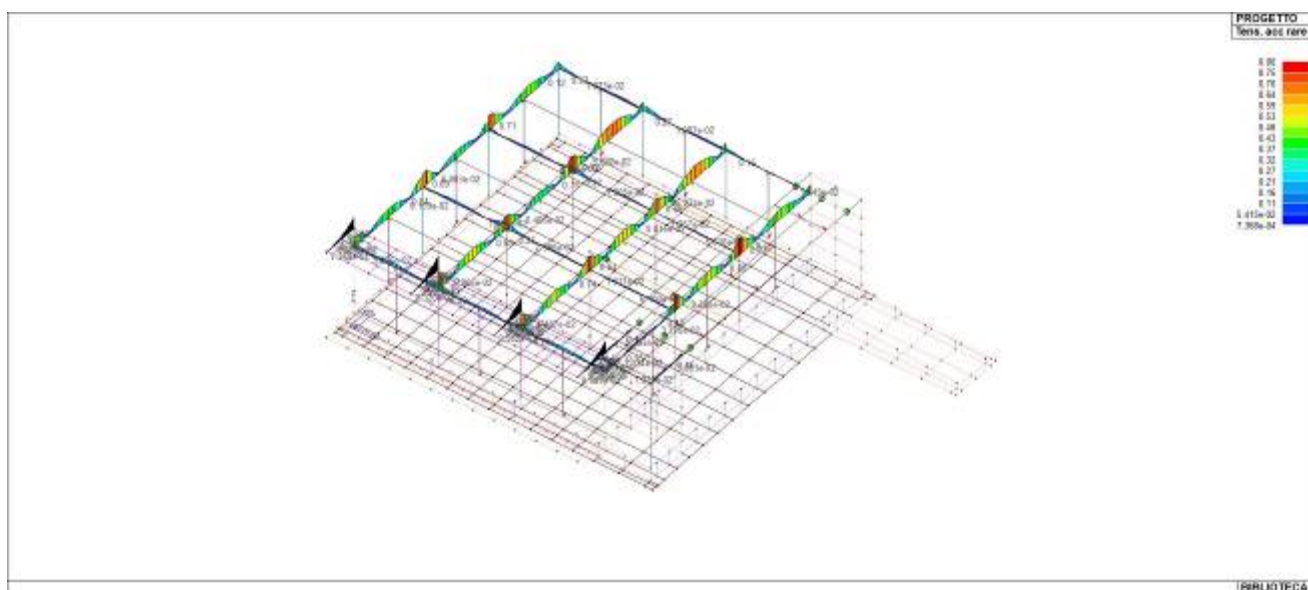
71_CA_TRV_12_Verifica VT acciaio



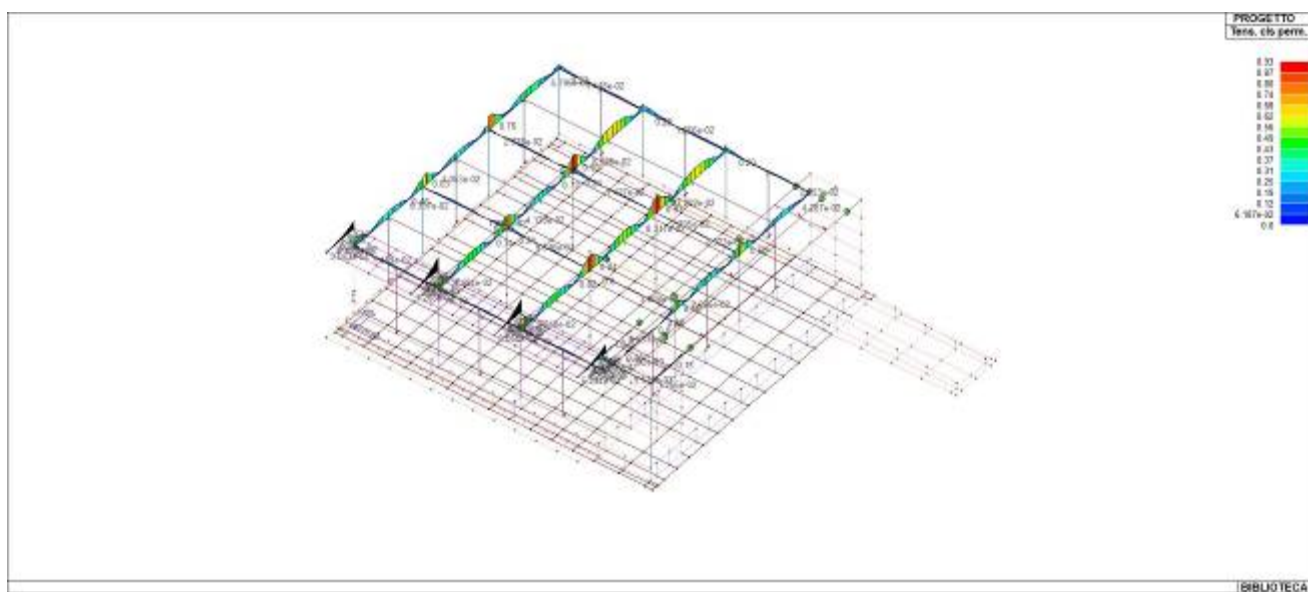
71_CA_TRV_20_Fessure rare



71_CA_TRV_21_Fessure freq



71_CA_TRV_24_Tens acc rare



71_CA_TRV_25_Tens cls perm

VERIFICHE ELEMENTI PARETE E/O GUSCIO IN C.A.

LEGENDA TABELLA VERIFICHE ELEMENTI PARETE E GUSCIO IN C.A.

Per le pareti in c.a., in ottemperanza al cap. 7 del DM 17-01-18, viene effettuata una doppia progettazione: sia come *Singolo Elemento* sia come *Parete Sismica* o *Parete Debolmente Armata*.

Per la progettazione come *Singolo Elemento* di ogni elemento vengono riportati il codice dello stato di verifica con le sigle **Ok e NV**, il rapporto x/d , la verifica per sollecitazioni ultime (verifica a compressione media gli sforzi membranali, verifica a presso-flessionale e verifica a sollecitazioni taglianti), gli sforzi membranali e flessionali, il quantitativo di armatura nella direzione principale e secondaria sia inferiore che superiore e il quantitativo di armatura a taglio.

Per la progettazione come *Parete Sismica* o *Parete Debolmente Armata* vengono riportate invece le caratteristiche geometriche della parete e delle zone dissipative (quest'ultime solo nel caso di parete sismica), i coefficienti di verifica a compressione assiale, pressoflessione e sollecitazioni taglianti.

Inoltre vengono riportate per ogni quota significativa l'armatura principale e secondaria, l'armatura in zona confinata (solo per parete sismica) e non confinata, l'armatura concentrata all'estremità (per pareti debolmente armate), lo sforzo assiale aggiuntivo per q superiore a 2 e i valori di involuppo di taglio e momento. Per le pareti debolmente armate viene riportato anche lo stato di verifica relativo alla snellezza.

Le azioni derivate dall'analisi, in ogni combinazione di calcolo, sono elaborate come previsto al punto 7.4.4.5.1: traslazione del momento, incremento e variazione diagramma taglio, incremento e decremento sforzo assiale

La progettazione nel caso dei gusci viene effettuata una progettazione come *Singolo Elemento*, riportando in tabella il rapporto x/d , la verifica per sollecitazioni ultime, (verifica a compressione media gli sforzi membranali, verifica a presso-flessionale e verifica a sollecitazioni taglianti) di ogni elemento.

Per ogni elemento, viene riportata inoltre la maglia di armatura necessaria in relazione alle risultanze della progettazione dei nodi dell'elemento stesso. Le quantità di armature necessarie sono armature (disposte rispettivamente in direzione principale e secondaria, inferiore e superiore) distribuite nell'elemento ed espresse in centimetri quadri per sviluppo lineare pari ad un metro.

Nel caso dei gusci viene effettuata, inoltre, la verifica a punzonamento, riportando in tabella il codice dello stato di verifica, il coefficiente di verifica per piastre prive di armature a taglio lungo il perimetro resistente e lungo il perimetro del pilastro, coefficiente di incremento dovuto ai momenti flettenti, fattore di amplificazione per le fondazioni, il fattore di amplificazione dell'altezza utile per individuare il perimetro di verifica lungo il quale l'armatura a taglio non è richiesta, il quantitativo di armatura a punzonamento, il numero di serie di armature, il numero di braccia di armatura ed il riferimento alla combinazione più gravosa.

Simbologia adottata nelle tabelle di verifica

Per gli elementi con progettazione di tipo "*Singolo Elemento* ..." è presente una tabella con i simboli di seguito descritti:

Macro Guscio	Numero del macroelemento di tipo guscio (elementi non verticali contigui ed analoghi per proprietà)
Macro Setto	Numero del macroelemento di tipo setto (elementi verticali contigui ed analoghi per proprietà)
Spessore	Spessore della parete
Id Materiale	Codice del materiale assegnato all'elemento
Id Criterio	Codice del criterio di progetto assegnato all'elemento
Progettazione	Sigla tipo di Elemento: - Singolo Elemento; - Singolo Elemento FONDAZIONE; - Singolo Elemento NON DISSIPATIVO

Per gli elementi con progettazione di tipo "*Parete Sismica*" e "*Parete Debolmente Armata*" è presente una tabella con i simboli di seguito descritti:

Parete	Numero della PARETE SISMICA
Parete PDA	Numero della PARETE DEBOLMENTE ARMATA
H totale	Altezza complessiva della parete
Spessore	Spessore della parete
H critica	Altezza come da punto 7.4.4.5.1 per traslazione momento (solo in Parete Sismica)
H critica V	Altezza della zona dissipativa (solo in Parete Sismica)
L totale	Larghezza di base della parete
L confinata	Lunghezza della zona dissipativa (solo in Parete Sismica)
Verif. N	Verifica di cui al punto 7.4.4.5.1 compressione semplice
Verif. N-M	Verifica di cui al punto 7.4.4.5.1 pressoflessione
Fattore V	Fattore di amplificazione del taglio di cui al punto 7.4.4.5.1
Diagramma V	Diagramma elaborato per effetto modi superiori come da fig. 7.4.4
Verif. V	Verifica di cui al punto 7.4.4.5.1 taglio (compressione cls, trazione acciaio, scorrimento in zona critica) (solo in Parete Sismica)
Verifica Snellezza	Verifica di cui al punto 7.4.4.5.1 limitazione compressione per prevenire l'instabilità (solo in Parete Debolmente Armata)
Prog. composta	Sigla per la progettazione composta

Sia per le verifiche degli elementi con progettazione di tipo "*Singolo Elemento* ..." e "*Parete* ..." è presente una tabella con i simboli di seguito descritti:

Nodo	numero del nodo
Stato	codice di verifica dell'elemento ok o NV
x/d	rapporto tra posizione dell'asse neutro e altezza utile alla rottura della sezione (per sola flessione)
V N/M	Verifica delle sollecitazioni Normali (momento e sforzo normale)
Ver. rid	Rapporto Nd/Nu (Nu ottenuto con riduzione del 25% di fcd)
Af pr+	quantità di armatura richiesta in direzione principale relativa alla faccia positiva (estradosso piastre) (valore derivante da calcolo o minimo normativo)
Af pr-	quantità di armatura richiesta in direzione principale relativa alla faccia negativa (intradosso piastre) (valore derivante da calcolo o minimo normativo)
Af sec+	quantità di armatura richiesta in direzione secondaria relativa alla faccia positiva (estradosso piastre) (valore derivante da calcolo o minimo normativo)
Af sec-	quantità di armatura richiesta in direzione secondaria relativa alla faccia negativa (intradosso piastre) (valore derivante da calcolo o minimo normativo)
Nz No Nzo	Sforzi membranali per pareti e/o setti verticali
Mz Mo Mzo	Sforzi flessionali per pareti e/o setti verticali
Nx Ny Nxy	Sforzi membranali per gusci orizzontali
Mx Mx Mxy	Sforzi flessionali per gusci orizzontali

Nodo	numero del nodo
Stato	codice di verifica dell'elemento ok o NV
Max tau	Tensione tangenziale Massima
Ver V pr	Verifica a taglio nella direzione principale lato calcestruzzo
Ver V sec	Verifica a taglio nella direzione secondaria lato calcestruzzo
Af V pr	Armatura nella direzione principale
V pr-	Verifica dell'armatura nella direzione principale
Af V sec	Armatura nella direzione secondaria
V sec-	Verifica dell'armatura nella direzione secondaria

Per le verifiche degli elementi con progettazione "*Parete Sismica o Parete Debolmente Armata*", oltre alla tabella con le verifiche per gli elementi con progettazione "*Singolo Elemento ...*", è presente una tabella con i simboli di seguito descritti:

Quota	Ascissa verticale di riferimento
Af conf.	Numero e diametro armatura presente in una zona confinata
Af std	Diametro e passo armatura in zona non confinata (doppia maglia)
Af estremi	Diametro dei ferri di estremità del pannello; se posto uguale 0, viene utilizzato il diametro standard
Af V (ori)	Diametro e passo armatura orizzontale (doppia maglia)
Ver. N	Rapporto tra azione di calcolo e resistenza a compressione (normalizzato a 1 in quanto da confrontare con 40% in CDB e 35 % in CDA)
Ver. N/M	Rapporto tra azione di calcolo e resistenza a pressoflessione
Ver. V acc(7)	Rapporto tra azione di calcolo e resistenza a taglio-trazione per alfaS minore di 2 secondo paragrafo 7.4.4.5.1
Ver. V cls	Rapporto tra azione di calcolo e resistenza a taglio-compressione
Ver. V acc	Rapporto tra azione di calcolo e resistenza a taglio-trazione
Ver. V scorr.	Rapporto tra azione di calcolo e resistenza a taglio scorrimento
N add	Sforzo assiale di cui al punto 7.4.4.5.1 da sommare e sottrarre nelle verifiche quando q supera 2
N invil M invil	Involuppo del Momento e Sforzo Normale come al punto 7.4.4.5.1 (informativo) (solo in Parete Sismica)

Quota	Ascissa verticale di riferimento
N v.N	Valore dello sforzo assiale per cui Ver. N attinge il massimo valore
N v.M/N, M v.M/N	Valore dello sforzo assiale e momento per cui Ver. N/M attinge il massimo valore
N v.M/N, M v.M/N Mo v.M/N	Valore dello sforzo assiale e dei momenti per cui Ver. N/M attinge il massimo valore (per le pareti estese debolmente armate)
N v.Vcls, V v.Vcls,	Valore dello sforzo assiale e taglio per cui Ver. V. cls attinge il massimo valore
N v.Vacc, M v.Vacc, V v.Vacc,	Valore dello sforzo assiale, momento e taglio per cui Ver. V. acc attinge il massimo valore
N v.Vscorr, M v.Vscorr, V v.Vscorr,	Valore dello sforzo assiale, momento e taglio per cui Ver. V. scorr.e
N v.N	Valore dello sforzo assiale per cui Ver. N attinge il massimo valore
N v.M/N, M v.M/N	Valore dello sforzo assiale e momento per cui Ver. N/M attinge il massimo valore
N v.M/N, M v.M/N Mo v.M/N	Valore dello sforzo assiale e dei momenti per cui Ver. N/M attinge il massimo valore (per le pareti estese debolmente armate)
N v.Vcls, V v.Vcls,	Valore dello sforzo assiale e taglio per cui Ver. V. cls attinge il massimo valore

Quota	Ascissa verticale di riferimento
CtgT Vcls	Valore di ctg(teta) adottato nella verifica V compressione cls
Vrsd Vcls	Valore della resistenza a taglio trazione (armatura di calcolo)
Vrcd Vcls	Valore della resistenza a taglio compressione
CtgT Vacc	Valore di ctg(teta) adottato nella verifica V trazione armatura
Vrsd Vacc	Valore della resistenza a taglio trazione (armatura presente)
Vrcd Vacc	Valore della resistenza a taglio compressione
Vdd	Valore del contributo alla resistenza allo scorrimento come da [7.4.20]
Vid	Valore del contributo alla resistenza allo scorrimento come da [7.4.21]
A s.i.	Somma delle aree di armature
Incli.	Angolo di inclinazione delle armature
Dist.	Distanza alla base tra le armature inclinate

Quota	Ascissa verticale di riferimento
V[7.4.16]	Verifica a taglio-trazione dell'armatura dell'anima (7.4.16)
N M V	Sollecitazioni di calcolo della condizione più gravosa
Alfas	Rapporto di Taglio
Vrd,c	Resistenza a taglio degli elementi non armati
VRd,s	Resistenza a taglio nei confronti dello scorrimento
V[7.4.17]	Verifica a taglio-trazione dell'armatura dell'anima (7.4.17)
roH	Rapporto tra l'armatura orizzontale e l'area della sezione relativa di calcestruzzo
roV	Rapporto tra l'armatura verticale e l'area della sezione relativa di calcestruzzo
roN	Sforzo normale adimensionalizzato Ned/(bw fyd)

Per la verifica a *Punzonamento* è presente una tabella con i simboli di seguito descritti:

Nodo	numero del nodo
Stato	codice di verifica dell'elemento ok o NV
V. 6.47	Fattore di sicurezza per la verifica per piastre prive di armature a taglio lungo il perimetro resistente U1
V. 6.53	Fattore di sicurezza per la verifica per piastre prive di armature a taglio lungo il perimetro del pilastro U0
Beta	Fattore di incremento dovuto ai momenti flettenti
f. a fon	fattore di amplificazione per le fondazioni (solo per gusci di fondazione)
f. Uout	fattore di amplificazione dell'altezza utile per individuare il perimetro di verifica lungo il quale l'armatura a taglio non è richiesta
Aw tot	Quantitativo di armatura per la verifica di piastre munite di armatura (formula 6.52 dell'EC2)
Asw,min	Quantitativo minimo di armatura previsto dai dettagli costruttivi (formula 9.11 dell'EC2)
n. x serie	Numero di serie di armature
n.ser 0(R)	Numero di braccia delle armatura in direzione 0 (o numero di braccia radiale)
n.ser 90	Numero di braccia delle armatura in direzione 90 (solo se armatura cruciforme)
Rif. cmb	Riferimento combinazioni da cui si generano le verifiche più gravose

Macro Setto	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
3	25.00	1	1	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									daN/ m	daN/ m	daN/ m	daN	daN	daN
22	ok	0.10	0.5	2.13e-02	5.7	5.7	3.9	3.9	-1095.0	8021.3	5333.1	-175.6	-83.4	-630.8
23	ok	0.10	0.4	8.92e-03	5.7	5.7	3.9	3.9	1210.9	9694.1	-5695.7	-35.7	-137.0	-315.8
24	ok	0.10	0.3	4.37e-03	5.7	5.7	3.9	3.9	2784.3	5145.7	-757.0	-331.2	-118.6	151.6
25	ok	0.10	0.2	1.39e-02	5.7	5.7	3.9	3.9	3857.4	2384.6	6683.1	-39.9	268.4	277.7
73	ok	0.10	0.2	6.27e-02	5.7	5.7	3.9	3.9	-8242.5	-7368.4	1.114e+04	-630.7	-259.7	416.7
75	ok	0.10	0.3	3.68e-02	5.7	5.7	3.9	3.9	-6460.4	-9534.1	406.9	-1286.2	-269.3	221.4
77	ok	0.10	0.3	5.11e-02	5.7	5.7	3.9	3.9	-6248.8	-6400.1	-4704.5	-1125.1	-234.8	112.0
79	ok	0.10	0.2	3.67e-02	5.7	5.7	3.9	3.9	-4336.0	-497.8	-1940.7	-733.2	-256.4	157.9
81	ok	0.10	0.2	3.47e-02	5.7	5.7	3.9	3.9	-4341.8	-1749.1	-4314.5	-813.2	-230.0	-45.5
83	ok	0.10	0.4	4.86e-02	5.7	5.7	3.9	3.9	-3474.3	2940.3	-1.192e+04	343.4	-195.1	-78.6
85	ok	0.10	0.3	3.13e-02	5.7	5.7	3.9	3.9	-4528.8	2494.0	7681.6	70.2	117.9	-207.3
87	ok	0.10	0.5	2.84e-02	5.7	5.7	3.9	3.9	-1108.3	7236.1	-3317.7	516.7	240.7	-385.9
89	ok	0.10	0.5	3.28e-02	5.7	5.7	3.9	3.9	271.4	7384.0	-3404.0	657.6	227.2	-150.1
366	ok	0.10	0.9	5.66e-02	5.7	5.7	3.9	3.9	-8283.9	3314.9	1.309e+04	2816.4	1701.9	503.6
367	ok	0.10	0.6	2.59e-02	5.7	5.7	3.9	3.9	-348.3	5589.8	6397.0	1861.1	-565.6	172.8
368	ok	0.10	0.5	1.17e-02	5.7	5.7	3.9	3.9	-1976.5	1.304e+04	2920.1	1220.7	218.7	170.8
369	ok	0.10	0.4	2.96e-02	5.7	5.7	3.9	3.9	-2215.2	5652.0	-3673.9	1386.5	502.0	2.3
370	ok	0.10	0.4	5.57e-02	5.7	5.7	3.9	3.9	-4969.6	-8810.7	4566.3	1668.1	759.5	236.6
371	ok	0.10	0.5	2.77e-02	5.7	5.7	3.9	3.9	-2234.7	7274.5	6184.7	1382.3	593.0	-95.6
372	ok	0.10	0.4	3.05e-02	5.7	5.7	3.9	3.9	-1715.4	-8183.2	-5013.6	972.5	445.4	-70.3
373	ok	0.10	0.5	5.58e-02	5.7	5.7	3.9	3.9	-1742.9	-1.150e+04	-1.055e+04	1158.2	620.6	42.5
374	ok	0.10	0.5	7.93e-02	5.7	5.7	3.9	3.9	-6089.4	-1.806e+04	5990.3	1658.4	370.5	-4.3
375	ok	0.10	0.7	6.54e-02	5.7	5.7	3.9	3.9	-1035.3	-1.325e+04	3831.2	1596.8	20.6	-256.8
376	ok	0.10	0.9	8.94e-02	5.7	5.7	3.9	3.9	460.7	-3.389e+04	-1798.3	1720.4	760.5	-340.3
377	ok	0.10	1.0	0.1	5.7	5.7	3.9	3.9	673.8	-3.331e+04	-4923.6	1848.9	909.1	-107.7
378	ok	0.10	1.0	0.1	5.7	5.7	3.9	3.9	-4707.7	-4.353e+04	1345.5	1775.6	-576.2	-991.3
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									-8283.90	-4.353e+04	-1.192e+04	-1286.24	-576.25	-991.32
		0.10	0.99	0.11	5.7	5.7	3.9	3.9	3857.35	1.304e+04	1.309e+04	2816.39	1701.87	503.60

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		daN/cm2					daN/ m	daN/ m
22	ok	1.20						
23	ok	1.09						
24	ok	1.17						
25	ok	1.54						
73	ok	1.70						
75	ok	1.70						
77	ok	1.66						
79	ok	1.40						
81	ok	1.40						
83	ok	1.35						
85	ok	1.24						
87	ok	1.73						
89	ok	1.73						
366	ok	2.97						
367	ok	2.97						
368	ok	1.70						
369	ok	1.66						
370	ok	1.99						
371	ok	1.99						
372	ok	1.40						
373	ok	1.82						
374	ok	1.82						
375	ok	1.34						
376	ok	2.20						
377	ok	3.15						
378	ok	3.15						
Nodo		Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		3.15						

Macro Setto	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
4	25.00	1	1	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									daN/ m	daN/ m	daN/ m	daN	daN	daN
4	ok	0.10	0.3	3.28e-02	5.7	5.7	3.9	3.9	-4991.7	8173.4	-3064.1	-775.2	-6.6	232.5
7	ok	0.10	0.4	4.65e-02	5.7	5.7	3.9	3.9	-9952.5	-785.3	1.182e+04	1581.1	75.5	-36.4
21	ok	0.10	0.2	0.1	5.7	5.7	3.9	3.9	-1466.3	-2.018e+04	-6963.4	106.5	124.5	21.0
22	ok	0.10	0.2	0.1	5.7	5.7	3.9	3.9	-1.050e+04	-3.415e+04	-1.410e+04	-117.1	158.2	-4.1
143	ok	0.10	0.3	5.38e-02	5.7	5.7	3.9	3.9	-6698.4	-6416.2	-9683.4	542.4	24.2	142.0
378	ok	0.16	1.0	2.26e-02	5.7	5.7	3.9	3.9	-225.0	4.765e+04	1.079e+04	-102.5	-2441.6	-34.3
379	ok	0.16	1.0	1.25e-02	5.7	5.7	3.9	3.9	1.057e+04	3.999e+04	1.051e+04	-183.6	-1543.5	-2.0
429	ok	0.13	1.0	9.65e-02	5.7	5.7	3.9	3.9	1768.9	6.491e+04	7703.2	-512.5	-808.0	134.9
430	ok	0.11	1.0	0.2	5.7	5.7	3.9	3.9	-4974.7	2.725e+04	3916.8	-137.5	807.7	339.5
431	ok	0.13	1.0	0.1	5.7	5.7	3.9	3.9	1956.9	7.612e+04	2031.7	547.4	624.6	-93.0
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									-1.050e+04	-3.415e+04	-1.410e+04	-775.16	-2441.62	-92.95
		0.16	0.99	0.16	5.7	5.7	3.9	3.9	1.057e+04	7.612e+04	1.182e+04	1581.08	807.68	339.53

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		daN/cm2					daN/ m	daN/ m
4	ok	3.72						
7	ok	2.26						
21	ok	3.05						
22	ok	3.05						
143	ok	2.26						
378	ok	3.52						
379	ok	3.52						
429	ok	3.35						
430	ok	3.02						
431	ok	3.35						

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		3.72						

Macro Setto	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
5	25.00	1	1	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									daN/ m	daN/ m	daN/ m	daN	daN	daN
5	ok	0.10	0.3	2.67e-02	5.7	5.7	3.9	3.9	-787.6	-2551.6	-8565.0	51.1	145.4	-27.7
21	ok	0.10	0.4	1.66e-02	5.7	5.7	3.9	3.9	-1524.3	6208.0	7837.9	-0.8	186.4	-415.4
95	ok	0.10	0.4	2.89e-02	5.7	5.7	3.9	3.9	-2255.2	-5065.5	-7355.0	708.1	336.4	-241.7
379	ok	0.11	1.0	0.2	5.7	5.7	3.9	3.9	-3683.8	-6.020e+04	6875.7	406.0	1151.9	-664.5
380	ok	0.11	1.0	0.1	5.7	5.7	3.9	3.9	548.5	2.397e+04	-5500.4	636.3	712.5	-507.9
381	ok	0.10	1.0	6.36e-02	5.7	5.7	3.9	3.9	-2028.5	2.356e+04	-9024.9	56.2	406.2	-147.9
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									-3683.81	-6.020e+04	-9024.91	-0.83	145.37	-664.47
		0.11	0.99	0.16	5.7	5.7	3.9	3.9	548.48	2.397e+04	7837.89	708.11	1151.94	-27.70

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		daN/cm2					daN/ m	daN/ m
5	ok	1.03						
21	ok	0.68						
95	ok	1.03						
379	ok	2.64						
380	ok	2.64						
381	ok	0.90						
Nodo		Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		2.64						

Macro Setto	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
6	30.00	1	1	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									daN/ m	daN/ m	daN/ m	daN	daN	daN
5	ok	0.08	0.2	1.56e-02	5.7	5.7	3.9	3.9	-1887.6	-3465.6	-4372.7	-135.0	-269.3	17.4
6	ok	0.08	0.7	2.11e-02	5.7	5.7	3.9	3.9	-4203.1	1.096e+04	8360.0	-244.0	83.3	130.3
20	ok	0.11	0.7	4.09e-02	5.7	5.7	3.9	3.9	-1.428e+04	1.177e+04	5900.6	-1589.2	-2720.8	1429.2
52	ok	0.08	0.3	4.87e-02	5.7	5.7	3.9	3.9	-8131.8	-1.517e+04	1510.6	1476.8	-101.6	256.1
53	ok	0.08	0.5	8.89e-02	5.7	5.7	3.9	3.9	-1.804e+04	-1.067e+04	1.774e+04	214.0	-1162.7	1259.9
58	ok	0.08	0.3	4.72e-02	5.7	5.7	3.9	3.9	-5083.1	-1.480e+04	-2032.3	995.5	76.0	-492.7
118	ok	0.08	0.3	2.69e-02	5.7	5.7	3.9	3.9	-1864.3	-3773.8	-6954.7	-39.1	-221.6	71.5
146	ok	0.08	0.5	2.97e-02	5.7	5.7	3.9	3.9	-2100.1	-7921.7	-7572.8	-304.3	-104.9	36.9
185	ok	0.08	0.7	4.83e-02	5.7	5.7	3.9	3.9	-6520.4	1.040e+04	-1.705e+04	-278.2	67.8	-379.0
187	ok	0.08	0.4	2.97e-02	5.7	5.7	3.9	3.9	-1111.5	3365.3	-1.103e+04	126.4	22.8	-381.2
189	ok	0.08	0.3	2.34e-02	5.7	5.7	3.9	3.9	-1118.4	-5998.3	-3141.5	-19.7	-15.0	-511.8
245	ok	0.08	0.2	2.06e-02	5.7	5.7	3.9	3.9	-784.9	-5991.0	-3419.7	-18.0	-10.4	-517.5
247	ok	0.08	9.42e-02	1.88e-02	5.7	5.7	3.9	3.9	-695.1	-6261.0	1310.1	29.4	7.3	-263.5
249	ok	0.08	7.66e-02	1.72e-02	5.7	5.7	3.9	3.9	-132.6	-6784.8	-872.1	-40.4	-25.5	-401.3
251	ok	0.08	8.62e-02	2.00e-02	5.7	5.7	3.9	3.9	317.2	-7219.9	-2597.4	-32.7	-24.8	-391.1
282	ok	0.08	0.1	3.18e-02	5.7	5.7	3.9	3.9	616.5	-1.005e+04	-4329.8	178.7	57.6	-423.1
332	ok	0.08	0.5	5.35e-02	5.7	5.7	3.9	3.9	-1152.2	-1.123e+04	1.171e+04	1439.9	226.3	338.3
381	ok	0.08	0.8	4.36e-02	5.7	5.7	3.9	3.9	-2004.8	2.089e+04	-6848.4	-57.8	-406.2	-35.0
382	ok	0.08	0.9	7.30e-02	5.7	5.7	3.9	3.9	-1492.2	3.702e+04	-8888.4	-153.2	-390.1	-31.9
383	ok	0.10	0.9	0.1	5.7	5.7	3.9	3.9	-803.8	3.498e+04	-6399.8	-347.0	-424.0	70.2
384	ok	0.10	0.9	0.2	5.7	5.7	3.9	3.9	-9680.7	-9.522e+04	-1.559e+04	113.2	1286.1	-47.4
385	ok	0.11	0.9	0.1	5.7	5.7	3.9	3.9	6616.1	8.995e+04	1.007e+04	6.9	-876.9	-113.2
386	ok	0.11	0.9	8.33e-02	5.7	5.7	3.9	3.9	-70.1	6.517e+04	2521.9	-76.8	-39.6	-123.6

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
387	ok	0.10	0.9	4.02e-02	5.7	5.7	3.9	3.9	-267.1	5.859e+04	818.1	3.3	-22.7	-273.4
388	ok	0.10	0.9	6.57e-03	5.7	5.7	3.9	3.9	-356.2	6.195e+04	2265.2	-24.8	-17.2	-261.5
389	ok	0.09	0.9	1.78e-03	5.7	5.7	3.9	3.9	-241.7	4.442e+04	875.7	-33.8	-22.1	-364.5
390	ok	0.09	0.9	1.39e-03	5.7	5.7	3.9	3.9	-246.9	4.608e+04	-889.0	-41.1	-67.4	-390.9
391	ok	0.09	0.9	1.34e-03	5.7	5.7	3.9	3.9	-258.8	4.727e+04	121.6	-58.6	-66.2	-376.2
392	ok	0.10	0.9	2.49e-03	5.7	5.7	3.9	3.9	-1028.7	6.176e+04	-2727.0	76.9	292.8	-536.8
393	ok	0.11	0.9	4.87e-03	5.7	5.7	3.9	3.9	-1988.9	8.300e+04	-372.9	92.7	-820.8	-705.1
394	ok	0.14	0.9	0.0	5.7	5.7	3.9	3.9	1479.8	8.186e+04	1371.5	-113.5	-2334.2	-249.1
395	ok	0.11	0.9	5.51e-03	5.7	5.7	3.9	3.9	-2000.2	6.018e+04	2904.2	755.6	810.2	610.6
396	ok	0.13	0.9	9.96e-02	5.7	5.7	3.9	3.9	437.5	-3.048e+04	2.091e+04	-321.2	-1504.4	1827.4
397	ok	0.12	0.9	0.2	5.7	5.7	3.9	3.9	-2.445e+04	-6.542e+04	3.586e+04	936.8	9275.9	1229.1
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									-2.445e+04	-9.522e+04	-1.705e+04	-1589.22	-2720.84	-705.08
		0.14	0.99	0.20	5.7	5.7	3.9	3.9	6616.08	8.995e+04	3.586e+04	1476.76	9275.85	1827.41

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		daN/cm2					daN/ m	daN/ m
5	ok	1.22						
6	ok	0.47						
20	ok	3.86						
52	ok	1.71						
53	ok	3.86						
58	ok	1.71						
118	ok	1.22						
146	ok	0.68						
185	ok	0.75						
187	ok	0.84						
189	ok	0.95						
245	ok	0.95						
247	ok	0.85						
249	ok	0.71						
251	ok	0.56						
282	ok	0.62						
332	ok	2.12						
381	ok	1.13						
382	ok	1.13						
383	ok	1.41						
384	ok	1.41						
385	ok	1.09						
386	ok	0.90						
387	ok	0.96						
388	ok	0.96						
389	ok	0.86						
390	ok	0.71						
391	ok	0.54						
392	ok	0.68						
393	ok	2.57						
394	ok	2.57						
395	ok	2.40						
396	ok	3.23						
397	ok	3.23						
Nodo		Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		3.86						

Macro Setto	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
7	25.00	1	1	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
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Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									daN/ m	daN/ m	daN/ m	daN	daN	daN
16	ok	0.10	0.2	1.70e-02	5.7	5.7	3.9	3.9	975.0	5.6	5013.1	392.3	-91.6	-219.2
17	ok	0.10	0.3	2.20e-02	5.7	5.7	3.9	3.9	-5516.2	6409.8	-4038.5	-342.0	-74.0	-78.7
18	ok	0.10	0.3	1.51e-02	5.7	5.7	3.9	3.9	-2923.9	1711.9	-3189.8	-485.7	-184.9	172.7
19	ok	0.10	0.7	3.62e-02	5.7	5.7	3.9	3.9	-5122.0	1.940e+04	-3086.1	103.5	-161.8	104.3
20	ok	0.10	0.5	3.16e-02	5.7	5.7	3.9	3.9	-4745.2	2784.6	-5066.8	-394.4	647.2	81.2
34	ok	0.10	0.6	2.05e-02	5.7	5.7	3.9	3.9	-1662.9	7077.2	9722.5	560.3	300.1	282.6
343	ok	0.10	0.2	3.84e-02	5.7	5.7	3.9	3.9	-4079.5	-4073.1	7466.0	337.0	130.7	-439.8
344	ok	0.10	0.1	3.16e-02	5.7	5.7	3.9	3.9	-4967.4	-5596.9	-2860.4	66.7	36.0	-272.1
345	ok	0.10	0.2	4.26e-02	5.7	5.7	3.9	3.9	-3738.3	-4438.7	-8524.0	-18.1	37.3	-244.8
346	ok	0.10	0.1	1.85e-02	5.7	5.7	3.9	3.9	-3475.7	-1144.0	-1021.6	-80.3	-22.4	71.9
347	ok	0.10	0.1	3.92e-02	5.7	5.7	3.9	3.9	-3527.7	-1124.8	-2971.2	-31.9	-2.9	65.0
348	ok	0.10	0.2	2.85e-02	5.7	5.7	3.9	3.9	-3709.3	3221.5	-7120.9	-70.2	-36.7	49.5
349	ok	0.10	0.3	1.38e-02	5.7	5.7	3.9	3.9	-2722.3	5853.4	-1939.2	-140.1	65.5	300.9
350	ok	0.10	0.3	1.98e-02	5.7	5.7	3.9	3.9	-1664.0	5708.1	-8118.6	13.2	68.2	182.6
351	ok	0.10	0.5	4.15e-02	5.7	5.7	3.9	3.9	-8003.2	8757.0	-1.320e+04	346.5	-37.7	328.3
397	ok	0.10	0.7	0.1	5.7	5.7	3.9	3.9	-2.016e+04	-3.621e+04	1.242e+04	1652.5	2010.1	-337.6
398	ok	0.10	0.8	5.43e-02	5.7	5.7	3.9	3.9	1.443e+04	-6405.9	-408.7	638.5	-846.1	-208.3
399	ok	0.10	0.9	0.3	5.7	5.7	3.9	3.9	-1.427e+04	-3.023e+04	-1.328e+04	1544.9	558.3	385.5
400	ok	0.10	1.0	0.2	5.7	5.7	3.9	3.9	-972.0	-7.207e+04	-8340.1	252.8	193.2	295.7
401	ok	0.10	0.6	0.2	5.7	5.7	3.9	3.9	-761.1	-6.501e+04	-2762.2	-36.4	148.2	200.9
402	ok	0.10	0.2	0.1	5.7	5.7	3.9	3.9	-5061.3	-3.665e+04	-5784.4	60.4	-298.5	362.8
403	ok	0.10	0.3	0.1	5.7	5.7	3.9	3.9	-417.7	-2.570e+04	3792.8	-99.4	543.3	317.9
404	ok	0.10	0.1	9.53e-02	5.7	5.7	3.9	3.9	-7601.0	-2.389e+04	7192.9	80.2	-128.9	44.9
405	ok	0.10	0.4	2.42e-02	5.7	5.7	3.9	3.9	1494.7	9613.0	3746.8	12.8	3.6	75.9
406	ok	0.10	0.6	1.42e-02	5.7	5.7	3.9	3.9	806.6	1.564e+04	-4207.3	-87.1	-68.5	89.7
407	ok	0.10	0.4	6.30e-02	5.7	5.7	3.9	3.9	-3592.8	1.037e+04	4464.5	-694.9	188.8	113.6
408	ok	0.10	0.7	2.48e-02	5.7	5.7	3.9	3.9	-943.4	2.232e+04	5675.4	18.4	-141.8	-268.3
409	ok	0.11	0.9	1.10e-02	5.7	5.7	3.9	3.9	-2518.0	3.391e+04	-3658.7	1.5	67.2	-278.7
410	ok	0.11	0.8	1.01e-02	5.7	5.7	3.9	3.9	-1765.7	2.729e+04	-1600.5	-10.8	460.6	-509.5
411	ok	0.10	0.5	1.21e-02	5.7	5.7	3.9	3.9	-2296.0	8054.7	4074.5	-255.6	-580.6	-80.0
463	ok	0.10	0.8	3.40e-02	5.7	5.7	3.9	3.9	-1.041e+04	1534.2	-6361.2	2584.4	197.3	-146.2
465	ok	0.10	0.7	5.30e-02	5.7	5.7	3.9	3.9	-8968.4	-6077.8	8439.5	1244.6	300.0	-63.4
466	ok	0.10	0.4	2.12e-02	5.7	5.7	3.9	3.9	-6509.8	-1077.7	-3548.5	747.7	-7.3	-120.2
467	ok	0.10	0.4	3.46e-02	5.7	5.7	3.9	3.9	-5511.9	-462.8	7301.0	727.5	96.0	-141.8
469	ok	0.10	0.5	2.21e-02	5.7	5.7	3.9	3.9	-2718.1	-1311.5	6173.2	1526.7	309.0	-208.3
470	ok	0.10	0.2	2.88e-02	5.7	5.7	3.9	3.9	-1068.0	-3802.2	6576.0	591.2	-112.3	-347.7
471	ok	0.10	0.4	2.48e-02	5.7	5.7	3.9	3.9	278.2	-7878.9	-332.5	667.6	424.4	-517.0
472	ok	0.10	0.6	4.86e-02	5.7	5.7	3.9	3.9	-1.588e+04	2359.1	7233.6	1398.1	196.1	-223.1
473	ok	0.10	0.4	3.04e-02	5.7	5.7	3.9	3.9	-7339.9	-544.5	5551.7	268.4	91.6	-198.5
474	ok	0.10	0.2	2.10e-02	5.7	5.7	3.9	3.9	-3437.6	-1407.6	3269.1	294.7	-38.5	-278.5
475	ok	0.10	0.3	5.23e-04	5.7	5.7	3.9	3.9	841.2	3945.1	1220.9	38.0	-40.2	581.5
476	ok	0.10	0.4	1.19e-02	5.7	5.7	3.9	3.9	-2185.2	-94.5	-2266.4	-399.1	90.7	-145.9
477	ok	0.10	0.3	2.33e-03	5.7	5.7	3.9	3.9	707.0	918.3	-1059.1	-63.5	-110.5	104.3
512	ok	0.10	0.6	4.96e-02	5.7	5.7	3.9	3.9	-1625.7	-1.293e+04	136.1	-1354.0	-655.4	-795.6
515	ok	0.10	0.2	1.07e-02	5.7	5.7	3.9	3.9	-1611.3	1413.3	-1478.3	284.3	182.5	253.6
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									-2.016e+04	-7.207e+04	-1.328e+04	-1353.98	-846.12	-795.62
		0.11	0.99	0.30	5.7	5.7	3.9	3.9	1.443e+04	3.391e+04	1.242e+04	2584.38	2010.09	581.55

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		daN/cm2					daN/ m	daN/ m
16	ok	0.60						
17	ok	1.07						
18	ok	0.96						
19	ok	2.22						
20	ok	3.23						
34	ok	3.23						
343	ok	0.60						
344	ok	0.43						
345	ok	0.85						
346	ok	1.07						
347	ok	0.69						
348	ok	0.84						

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
349	ok	0.96						
350	ok	0.52						
351	ok	1.89						
397	ok	3.84						
398	ok	3.84						
399	ok	2.61						
400	ok	1.84						
401	ok	0.31						
402	ok	1.86						
403	ok	1.86						
404	ok	1.69						
405	ok	0.18						
406	ok	1.88						
407	ok	1.88						
408	ok	1.71						
409	ok	0.28						
410	ok	0.78						
411	ok	0.78						
463	ok	0.88						
465	ok	0.88						
466	ok	0.90						
467	ok	0.90						
469	ok	1.30						
470	ok	1.30						
471	ok	1.62						
472	ok	0.66						
473	ok	0.63						
474	ok	0.55						
475	ok	2.12						
476	ok	2.12						
477	ok	0.71						
512	ok	1.62						
515	ok	0.30						
Nodo		Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		3.84						

Macro Setto	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
8	25.00	1	1	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
1	ok	0.10	0.6	2.49e-02	5.7	5.7	3.9	3.9	daN/ m	daN/ m	daN/ m	daN	daN	daN
8	ok	0.10	0.4	3.51e-02	5.7	5.7	3.9	3.9	-6689.8	1.285e+04	-980.0	695.1	-431.9	-434.8
12	ok	0.10	0.3	2.86e-02	5.7	5.7	3.9	3.9	-6632.8	4682.5	-5443.6	-457.8	-174.2	17.0
16	ok	0.10	0.6	1.28e-02	5.7	5.7	3.9	3.9	-6283.4	1.051e+04	2145.6	-280.7	-157.0	85.4
25	ok	0.10	0.3	0.1	5.7	5.7	3.9	3.9	922.6	1.791e+04	-6912.2	-166.6	100.3	151.6
48	ok	0.10	0.3	6.26e-02	5.7	5.7	3.9	3.9	-1360.5	-3.767e+04	-1.299e+04	-545.5	-38.3	-95.7
69	ok	0.10	0.2	4.18e-02	5.7	5.7	3.9	3.9	-4943.6	-1.031e+04	-3901.8	-134.7	-40.5	-272.2
69	ok	0.10	0.2	4.18e-02	5.7	5.7	3.9	3.9	-4103.0	-6517.2	7167.3	-82.3	-20.8	212.9
70	ok	0.10	0.2	4.02e-02	5.7	5.7	3.9	3.9	-3161.6	-6338.9	2809.2	-65.6	-9.7	200.7
104	ok	0.10	0.3	9.63e-02	5.7	5.7	3.9	3.9	5148.8	-2.297e+04	-7100.9	-684.1	-233.4	-307.1
121	ok	0.10	0.4	7.62e-02	5.7	5.7	3.9	3.9	-5003.7	-7525.3	-1.662e+04	-134.8	152.3	-355.4
149	ok	0.10	0.1	4.39e-02	5.7	5.7	3.9	3.9	-5507.2	-1.095e+04	4047.6	-99.9	-10.6	-190.5
151	ok	0.10	0.3	7.95e-02	5.7	5.7	3.9	3.9	-3881.4	-1.267e+04	1.495e+04	-212.8	-21.8	-103.6
195	ok	0.10	8.37e-02	4.93e-02	5.7	5.7	3.9	3.9	-2505.8	-1.012e+04	-7528.8	-187.3	38.7	-8.8
197	ok	0.10	0.2	4.66e-02	5.7	5.7	3.9	3.9	-2943.4	-4862.1	4854.4	33.3	23.1	42.8
199	ok	0.10	0.3	5.83e-02	5.7	5.7	3.9	3.9	-3866.6	-5767.8	1.274e+04	-172.2	32.4	76.7
258	ok	0.10	9.83e-02	4.23e-02	5.7	5.7	3.9	3.9	-2500.6	-6613.9	-7874.4	-122.0	-17.8	132.6
305	ok	0.10	0.5	4.39e-02	5.7	5.7	3.9	3.9	-2843.6	1.079e+04	7307.3	-377.8	-36.7	306.8
308	ok	0.10	0.3	6.84e-02	5.7	5.7	3.9	3.9	-5721.3	-6465.3	1.455e+04	-200.6	-95.3	324.2
366	ok	0.22	1.0	3.15e-02	5.7	5.7	3.9	3.9	-524.7	6.227e+04	2.185e+04	728.3	3280.8	145.7
411	ok	0.10	1.0	0.2	5.7	5.7	3.9	3.9	-5243.2	-6.031e+04	4033.4	217.3	1129.8	-68.5
412	ok	0.10	1.0	0.2	5.7	5.7	3.9	3.9	-1.650e+04	-5.958e+04	-7589.1	122.2	638.9	104.1
413	ok	0.11	1.0	4.77e-02	5.7	5.7	3.9	3.9	396.9	-1.864e+04	-13.0	-73.1	-170.3	252.8

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
414	ok	0.11	1.0	1.54e-02	5.7	5.7	3.9	3.9	-3020.5	4.248e+04	4463.4	-1.7	-49.0	218.7
415	ok	0.11	1.0	1.06e-02	5.7	5.7	3.9	3.9	-1845.9	4.764e+04	2756.8	14.1	-31.3	202.9
416	ok	0.11	0.8	4.97e-03	5.7	5.7	3.9	3.9	4341.0	4.734e+04	2368.7	122.1	-41.0	171.0
417	ok	0.10	0.7	6.82e-02	5.7	5.7	3.9	3.9	-8769.9	2.302e+04	-6537.3	-248.7	-118.8	-52.0
418	ok	0.11	1.0	2.22e-02	5.7	5.7	3.9	3.9	297.2	3.583e+04	-6393.7	114.4	-163.9	101.5
419	ok	0.11	0.9	1.72e-02	5.7	5.7	3.9	3.9	-4958.3	5.775e+04	3967.4	12.8	2.5	32.4
420	ok	0.13	1.0	1.97e-03	5.7	5.7	3.9	3.9	6166.2	7.142e+04	3113.9	87.9	12.0	31.2
421	ok	0.12	1.0	5.37e-02	5.7	5.7	3.9	3.9	-9466.8	3.489e+04	1.389e+04	-625.6	68.0	182.3
422	ok	0.13	1.0	8.67e-03	5.7	5.7	3.9	3.9	5301.6	7.778e+04	-4131.6	221.6	-246.1	-78.2
423	ok	0.14	1.0	9.21e-03	5.7	5.7	3.9	3.9	-1684.0	1.085e+05	7541.0	3.5	-29.0	-101.3
424	ok	0.15	1.0	3.56e-02	5.7	5.7	3.9	3.9	2903.2	1.200e+05	6412.6	8.8	-57.1	-194.4
425	ok	0.14	1.0	8.60e-02	5.7	5.7	3.9	3.9	2718.1	1.051e+05	-1165.0	-66.6	107.7	-322.6
426	ok	0.13	1.0	0.1	5.7	5.7	3.9	3.9	-4719.7	3.228e+04	7122.3	31.2	-1244.5	-584.3
427	ok	0.16	1.0	4.19e-02	5.7	5.7	3.9	3.9	9911.3	5.220e+04	1.525e+04	543.4	2035.1	-401.0
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									-1.650e+04	-6.031e+04	-1.662e+04	-684.11	-1244.52	-584.35
		0.22	0.99	0.16	5.7	5.7	3.9	3.9	9911.33	1.200e+05	2.185e+04	728.32	3280.79	324.25

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		daN/cm2					daN/ m	daN/ m
1	ok	4.34						
8	ok	0.81						
12	ok	0.51						
16	ok	1.23						
25	ok	3.92						
48	ok	1.22						
69	ok	0.14						
70	ok	0.28						
104	ok	4.34						
121	ok	1.22						
149	ok	0.43						
151	ok	0.81						
195	ok	0.68						
197	ok	0.39						
199	ok	0.41						
258	ok	0.51						
305	ok	1.23						
308	ok	0.32						
366	ok	3.66						
411	ok	1.23						
412	ok	1.23						
413	ok	0.39						
414	ok	0.13						
415	ok	0.12						
416	ok	0.87						
417	ok	0.87						
418	ok	0.86						
419	ok	0.12						
420	ok	1.12						
421	ok	1.40						
422	ok	1.40						
423	ok	0.37						
424	ok	0.65						
425	ok	1.70						
426	ok	3.50						
427	ok	3.66						
Nodo		Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		4.34						

Macro Setto	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
9	25.00	1	1	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									daN/ m	daN/ m	daN/ m	daN	daN	daN
6	ok	0.10	0.3	2.52e-02	5.7	5.7	3.9	3.9	-8920.2	-2661.1	1816.5	-588.2	-137.5	166.3
7	ok	0.10	0.2	2.36e-02	5.7	5.7	3.9	3.9	-1751.0	-2559.6	-3484.7	-18.7	-74.1	-17.2
145	ok	0.10	0.4	2.68e-02	5.7	5.7	3.9	3.9	-9748.1	-2575.3	746.3	-911.6	-173.9	104.7
384	ok	0.10	0.4	4.41e-02	5.7	5.7	3.9	3.9	-1.547e+04	-660.7	5430.8	-2207.3	-437.6	61.6
428	ok	0.10	0.6	3.44e-02	5.7	5.7	3.9	3.9	-9464.4	-272.3	4088.2	-1248.2	-55.8	-14.0
429	ok	0.10	0.3	9.11e-02	5.7	5.7	3.9	3.9	-1.452e+04	-1.433e+04	-1.310e+04	-429.3	-336.6	-97.2
451	ok	0.10	0.4	5.00e-02	5.7	5.7	3.9	3.9	-1.394e+04	-2949.6	-9567.8	156.0	-44.2	104.1
453	ok	0.10	0.4	4.10e-02	5.7	5.7	3.9	3.9	-1.306e+04	-1038.0	3370.1	-1312.4	-88.2	-187.1
454	ok	0.10	0.3	3.58e-02	5.7	5.7	3.9	3.9	-1.065e+04	-2149.5	-5640.6	144.7	103.8	145.1
455	ok	0.10	0.3	3.17e-02	5.7	5.7	3.9	3.9	-1.065e+04	-306.3	4605.9	-807.2	-168.0	-255.2
456	ok	0.10	0.2	3.21e-02	5.7	5.7	3.9	3.9	-5821.9	-2228.7	5455.1	775.9	-120.2	3.8
457	ok	0.10	0.2	2.44e-02	5.7	5.7	3.9	3.9	-3909.3	-550.4	3073.8	116.5	-149.5	-586.4
458	ok	0.10	0.5	1.98e-02	5.7	5.7	3.9	3.9	-1075.5	-5654.5	3527.3	198.1	-941.2	-547.7
459	ok	0.10	0.5	3.45e-02	5.7	5.7	3.9	3.9	-1.279e+04	1002.0	3255.0	-1922.8	-244.4	-203.6
461	ok	0.10	0.3	2.52e-02	5.7	5.7	3.9	3.9	-8035.0	-958.2	4013.6	-875.7	-199.4	-434.2
462	ok	0.10	0.2	1.88e-02	5.7	5.7	3.9	3.9	-5339.5	-1616.9	3336.7	-310.1	-258.9	-552.0
478	ok	0.10	0.3	1.10e-02	5.7	5.7	3.9	3.9	-1670.2	-1106.8	2180.2	600.2	-224.9	-996.3
479	ok	0.10	0.3	5.28e-03	5.7	5.7	3.9	3.9	988.8	3262.2	-2012.1	79.0	307.7	442.3
480	ok	0.10	0.4	1.07e-02	5.7	5.7	3.9	3.9	-1080.3	1968.7	400.8	1511.0	167.7	159.2
509	ok	0.10	0.7	2.78e-02	5.7	5.7	3.9	3.9	-3080.7	-5299.7	4047.6	726.1	-203.5	-628.7
514	ok	0.10	0.3	1.41e-02	5.7	5.7	3.9	3.9	-2277.0	-2141.0	264.9	1261.2	245.2	-534.1
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									-1.547e+04	-1.433e+04	-1.310e+04	-2207.29	-941.25	-996.27
		0.10	0.70	0.09	5.7	5.7	3.9	3.9	988.84	3262.16	5455.13	1511.04	307.74	442.26

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		daN/cm2					daN/ m	daN/ m
6	ok	2.41						
7	ok	2.87						
145	ok	2.87						
384	ok	3.01						
428	ok	3.34						
429	ok	3.34						
451	ok	0.99						
453	ok	0.99						
454	ok	0.96						
455	ok	0.96						
456	ok	1.03						
457	ok	1.03						
458	ok	1.47						
459	ok	0.57						
461	ok	0.53						
462	ok	0.46						
478	ok	1.61						
479	ok	1.61						
480	ok	1.37						
509	ok	1.47						
514	ok	0.84						
Nodo		Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		3.34						

Macro Setto	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
10	30.00	1	1	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									daN/ m	daN/ m	daN/ m	daN	daN	daN
7	ok	0.08	0.7	4.67e-02	5.7	5.7	3.9	3.9	-1.309e+04	1.058e+04	-1.642e+04	2404.7	174.0	186.5

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
11	ok	0.08	0.4	3.90e-02	5.7	5.7	3.9	3.9	-1.147e+04	7987.7	-7478.9	504.8	120.8	-186.1
15	ok	0.08	0.3	3.46e-02	5.7	5.7	3.9	3.9	-1.075e+04	1.023e+04	6283.7	288.7	108.1	-117.1
19	ok	0.09	0.7	1.62e-02	5.7	5.7	3.9	3.9	4478.3	3.605e+04	-1.153e+04	155.5	390.3	-45.0
63	ok	0.08	8.54e-02	2.73e-02	5.7	5.7	3.9	3.9	-4198.6	-6568.7	1196.4	226.5	49.1	-200.1
64	ok	0.08	7.88e-02	3.01e-02	5.7	5.7	3.9	3.9	-3023.4	-5487.8	3027.3	98.4	20.7	-160.3
183	ok	0.08	0.4	7.55e-02	5.7	5.7	3.9	3.9	-1.067e+04	-2729.7	-1.850e+04	1087.9	131.0	530.7
184	ok	0.08	0.2	6.49e-02	5.7	5.7	3.9	3.9	-4553.0	-1.534e+04	1.173e+04	476.4	31.3	-158.3
242	ok	0.08	0.1	6.21e-02	5.7	5.7	3.9	3.9	-3032.6	-1.372e+04	-1.240e+04	289.2	-1.1	-66.1
243	ok	0.08	9.90e-02	3.86e-02	5.7	5.7	3.9	3.9	-4776.6	-9785.6	5787.7	29.0	-8.1	-207.5
244	ok	0.08	0.2	6.36e-02	5.7	5.7	3.9	3.9	-3446.8	-1.005e+04	1.540e+04	135.3	-51.1	-284.9
279	ok	0.08	0.1	5.44e-02	5.7	5.7	3.9	3.9	-3172.3	-9401.0	-1.256e+04	156.4	-14.0	-43.8
302	ok	0.08	0.6	4.26e-02	5.7	5.7	3.9	3.9	-7037.4	5332.1	8476.1	471.2	-74.7	-276.0
329	ok	0.08	0.3	5.02e-02	5.7	5.7	3.9	3.9	-1952.2	-7990.0	1.239e+04	403.6	141.0	-388.1
399	ok	0.08	1.0	0.2	5.7	5.7	3.9	3.9	-1.198e+04	-6.856e+04	2.455e+04	34.4	-3035.8	269.4
429	ok	0.11	1.0	0.2	5.7	5.7	3.9	3.9	-3127.4	9.132e+04	-2093.1	-592.1	-246.7	411.6
432	ok	0.13	1.0	8.85e-02	5.7	5.7	3.9	3.9	7987.9	1.222e+05	1.211e+04	-157.1	1575.1	120.7
433	ok	0.11	1.0	5.03e-02	5.7	5.7	3.9	3.9	6828.9	8.355e+04	2845.1	-146.2	174.4	-112.1
434	ok	0.10	1.0	7.67e-02	5.7	5.7	3.9	3.9	-1.531e+04	5.595e+04	1.781e+04	603.6	-131.5	-367.6
435	ok	0.10	1.0	1.16e-02	5.7	5.7	3.9	3.9	8281.3	7.891e+04	4198.7	-172.6	83.4	-8.2
436	ok	0.10	1.0	6.31e-03	5.7	5.7	3.9	3.9	2801.8	6.835e+04	-1969.2	-10.2	25.7	-191.5
437	ok	0.09	0.8	2.15e-02	5.7	5.7	3.9	3.9	7555.4	4.842e+04	-6357.1	-261.1	154.1	-200.2
438	ok	0.08	0.5	8.63e-02	5.7	5.7	3.9	3.9	-1.742e+04	-9743.8	1.647e+04	280.8	-172.5	-322.6
439	ok	0.09	0.9	2.15e-02	5.7	5.7	3.9	3.9	8509.6	4.116e+04	6835.0	-240.2	123.9	-106.7
440	ok	0.09	1.0	6.94e-03	5.7	5.7	3.9	3.9	2830.4	5.292e+04	1972.6	-16.6	46.3	-161.2
441	ok	0.09	1.0	4.10e-03	5.7	5.7	3.9	3.9	-376.0	4.963e+04	1983.1	-1.6	64.7	-193.8
442	ok	0.09	1.0	2.69e-02	5.7	5.7	3.9	3.9	1419.0	4.999e+04	-4049.7	-98.7	415.8	-247.4
443	ok	0.09	1.0	0.1	5.7	5.7	3.9	3.9	-5642.9	-5.745e+04	1.500e+04	-117.0	-2340.3	139.4
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									-1.742e+04	-6.856e+04	-1.850e+04	-592.06	-3035.75	-388.07
		0.13	0.99	0.17	5.7	5.7	3.9	3.9	8509.63	1.222e+05	2.455e+04	2404.66	1575.08	530.66

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		daN/cm2					daN/ m	daN/ m
7	ok	1.99						
11	ok	1.29						
15	ok	0.66						
19	ok	1.89						
63	ok	0.65						
64	ok	0.59						
183	ok	1.99						
184	ok	1.08						
242	ok	1.29						
243	ok	0.89						
244	ok	0.50						
279	ok	0.66						
302	ok	1.89						
329	ok	0.73						
399	ok	2.03						
429	ok	3.32						
432	ok	3.32						
433	ok	0.77						
434	ok	1.82						
435	ok	1.82						
436	ok	0.53						
437	ok	0.96						
438	ok	1.02						
439	ok	1.02						
440	ok	0.53						
441	ok	0.53						
442	ok	1.13						
443	ok	2.03						
Nodo		Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		3.32						

Macro Setto	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
11	25.00	1	1	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									daN/ m	daN/ m	daN/ m	daN	daN	daN
52	ok	0.10	0.3	4.14e-02	5.7	5.7	3.9	3.9	-3904.3	2467.6	-1.162e+04	-22.3	-28.2	-43.4
55	ok	0.10	7.09e-02	7.63e-03	5.7	5.7	3.9	3.9	981.8	-424.6	-2472.4	-28.2	-8.0	13.0
295	ok	0.10	0.4	1.68e-03	5.7	5.7	3.9	3.9	1.001e+04	1.145e+04	1878.9	-94.1	-5.2	-228.5
296	ok	0.10	0.3	5.42e-02	5.7	5.7	3.9	3.9	-6737.7	-243.5	1.150e+04	261.5	43.7	-124.1
298	ok	0.10	9.97e-02	1.91e-02	5.7	5.7	3.9	3.9	-2031.9	-5561.2	-267.9	77.7	29.5	-40.6
300	ok	0.10	6.38e-02	1.38e-02	5.7	5.7	3.9	3.9	-527.9	-1665.6	-1897.5	30.8	15.8	8.3
394	ok	0.10	0.2	9.09e-02	5.7	5.7	3.9	3.9	-6881.2	-3.383e+04	-4565.3	-139.2	-585.5	3.9
522	ok	0.10	0.1	8.83e-04	5.7	5.7	3.9	3.9	-78.4	2465.9	-598.8	-0.3	-3.4	13.4
526	ok	0.10	0.1	0.1	5.7	5.7	3.9	3.9	341.0	-4.033e+04	-7354.2	-26.8	-391.4	-192.4
528	ok	0.10	0.6	4.61e-02	5.7	5.7	3.9	3.9	-732.2	-5966.1	3958.1	-1.3	110.2	-128.1
529	ok	0.10	0.9	2.62e-03	5.7	5.7	3.9	3.9	-29.1	2.915e+04	-1644.4	-0.2	31.8	-55.7
530	ok	0.10	0.6	8.01e-04	5.7	5.7	3.9	3.9	87.6	2.043e+04	-1913.7	5.4	6.6	5.2
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									-6881.23	-4.033e+04	-1.162e+04	-139.19	-585.54	-228.47
		0.10	0.94	0.13	5.7	5.7	3.9	3.9	1.001e+04	2.915e+04	1.150e+04	261.55	110.22	13.41

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		daN/cm2					daN/ m	daN/ m
52	ok	0.28						
55	ok	0.09						
295	ok	0.51						
296	ok	0.51						
298	ok	0.12						
300	ok	0.09						
394	ok	0.64						
522	ok	0.09						
526	ok	0.63						
528	ok	0.58						
529	ok	0.10						
530	ok	0.10						
Nodo		Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		0.64						

Macro Setto	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
12	25.00	1	1	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									daN/ m	daN/ m	daN/ m	daN	daN	daN
53	ok	0.10	0.8	2.44e-02	5.7	5.7	3.9	3.9	-7669.6	1.950e+04	-4208.9	283.8	-518.8	271.2
54	ok	0.10	8.01e-02	8.12e-03	5.7	5.7	3.9	3.9	1138.8	-428.3	-2652.8	-29.5	-8.5	15.1
334	ok	0.10	0.8	1.58e-02	5.7	5.7	3.9	3.9	5160.9	1.943e+04	1.015e+04	814.6	148.0	-185.0
336	ok	0.10	0.5	6.05e-02	5.7	5.7	3.9	3.9	-3440.5	7540.5	1.402e+04	36.3	82.8	-104.2
338	ok	0.10	0.2	1.99e-02	5.7	5.7	3.9	3.9	764.1	-5149.7	-2082.6	54.9	-5.4	44.2
340	ok	0.10	6.85e-02	1.32e-02	5.7	5.7	3.9	3.9	-831.6	-2243.0	-1656.4	-29.0	-16.5	54.0
396	ok	0.10	0.5	0.3	5.7	5.7	3.9	3.9	-1.129e+04	-1.128e+05	6882.7	-580.6	-2944.5	573.0
520	ok	0.10	0.8	0.1	5.7	5.7	3.9	3.9	642.9	-5.172e+04	7065.6	96.7	240.7	-211.9
523	ok	0.10	0.1	1.48e-03	5.7	5.7	3.9	3.9	-83.0	2803.8	-641.9	-2.7	-9.7	12.1
524	ok	0.10	1.0	2.64e-02	5.7	5.7	3.9	3.9	460.6	3.297e+04	-4911.7	-14.4	-61.4	21.9
525	ok	0.10	0.7	8.14e-04	5.7	5.7	3.9	3.9	-126.6	1.854e+04	-1347.4	-6.1	-21.3	60.3
527	ok	0.10	0.5	0.3	5.7	5.7	3.9	3.9	-1784.5	-1.106e+05	-668.7	-94.0	-1581.0	114.2

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									-1.129e+04	-1.128e+05	-4911.72	-580.57	-2944.48	-211.89
		0.10	0.99	0.30	5.7	5.7	3.9	3.9	5160.90	3.297e+04	1.402e+04	814.59	240.74	572.99

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		daN/cm2					daN/ m	daN/ m
53	ok	2.26						
54	ok	0.18						
334	ok	2.26						
336	ok	0.68						
338	ok	0.20						
340	ok	0.20						
396	ok	2.59						
520	ok	0.79						
523	ok	0.21						
524	ok	0.23						
525	ok	0.21						
527	ok	2.53						
Nodo		Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		2.59						

Macro Setto	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
14	30.00	1	1	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									daN/ m	daN/ m	daN/ m	daN	daN	daN
2	ok	0.08	0.2	9.99e-02	5.7	5.7	3.9	3.9	-3.291e+04	-1.997e+04	5829.5	-9.8	217.1	-42.5
24	ok	0.08	0.2	0.1	5.7	5.7	3.9	3.9	-7938.6	-3.950e+04	-9900.7	262.5	-70.6	54.5
100	ok	0.08	0.4	9.18e-02	5.7	5.7	3.9	3.9	3272.1	-2.924e+04	6739.9	337.5	-28.1	-167.4
370	ok	0.11	1.0	2.30e-02	5.7	5.7	3.9	3.9	4947.4	5.715e+04	1.813e+04	-169.9	905.2	-126.7
468	ok	0.10	1.0	4.36e-02	5.7	5.7	3.9	3.9	-5313.0	4.738e+04	1.854e+04	68.4	611.5	-269.4
499	ok	0.09	0.9	7.77e-02	5.7	5.7	3.9	3.9	-2.565e+04	3.846e+04	1.310e+04	418.7	-141.7	-375.2
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									-3.291e+04	-3.950e+04	-9900.68	-169.93	-141.66	-375.24
		0.11	0.99	0.12	5.7	5.7	3.9	3.9	4947.36	5.715e+04	1.854e+04	418.71	905.23	54.48

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		daN/cm2					daN/ m	daN/ m
2	ok	3.18						
24	ok	2.78						
100	ok	3.18						
370	ok	3.51						
468	ok	3.32						
499	ok	3.32						
Nodo		Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		3.51						

Macro Setto	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
15	30.00	1	1	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									daN/ m	daN/ m	daN/ m	daN	daN	daN
3	ok	0.08	0.4	9.53e-02	5.7	5.7	3.9	3.9	-2.821e+04	-1.820e+04	9700.6	1026.5	55.2	193.2

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
23	ok	0.08	0.1	0.2	5.7	5.7	3.9	3.9	-1.394e+04	-5.141e+04	-1.110e+04	298.2	-225.4	114.2
96	ok	0.08	0.3	0.1	5.7	5.7	3.9	3.9	2913.4	-3.490e+04	8961.6	524.2	-28.2	32.6
374	ok	0.12	1.0	2.06e-02	5.7	5.7	3.9	3.9	8820.4	7.495e+04	2.637e+04	-294.1	-805.4	-213.6
481	ok	0.11	1.0	5.09e-02	5.7	5.7	3.9	3.9	1.620e+04	6.478e+04	5594.0	-227.0	-753.2	-97.9
482	ok	0.09	0.9	7.37e-02	5.7	5.7	3.9	3.9	-2.348e+04	4.053e+04	1.445e+04	152.7	264.9	-201.0
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									-2.821e+04	-5.141e+04	-1.110e+04	294.11	-805.36	-213.55
		0.12	0.99	0.16	5.7	5.7	3.9	3.9	1.620e+04	7.495e+04	2.637e+04	1026.49	264.89	193.25

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		daN/cm2					daN/ m	daN/ m
3	ok	3.15						
23	ok	3.49						
96	ok	3.15						
374	ok	3.36						
481	ok	3.98						
482	ok	3.98						
Nodo		Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		3.98						

Macro Guscio	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
1	40.00	1	2	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy
									daN/ m	daN/ m	daN/ m	daN	daN	daN
1	ok	0.08	0.9	2.77e-02	5.7	5.7	5.7	5.7	-906.5	1.413e+04	865.0	-842.8	-2876.6	-2631.2
2	ok	0.08	0.8	1.18e-02	5.7	5.7	5.7	5.7	-3213.9	3512.6	2089.7	-3969.6	-5618.8	-334.5
3	ok	0.08	0.9	9.59e-03	5.7	5.7	5.7	5.7	716.0	6663.3	-1292.1	-4255.9	-4512.3	1147.9
4	ok	0.08	1.0	2.12e-02	5.7	5.7	5.7	5.7	1.156e+04	-1440.5	-3644.7	-5734.7	-1119.9	-131.3
5	ok	0.08	0.3	1.45e-02	5.7	5.7	5.7	5.7	-3024.7	-2779.3	-3845.9	-949.7	-708.7	-486.2
6	ok	0.08	1.0	3.38e-02	5.7	5.7	5.7	5.7	1430.8	1.993e+04	3285.5	-1015.1	-3736.1	-429.6
7	ok	0.09	1.0	1.95e-02	5.7	5.7	5.7	5.7	-4939.0	5001.2	5381.0	-1.037e+04	-3160.9	709.5
8	ok	0.08	0.2	5.70e-03	5.7	5.7	5.7	5.7	-598.0	18.4	2418.4	-1237.5	814.5	415.2
9	ok	0.08	0.5	5.76e-03	5.7	5.7	5.7	5.7	-698.4	-1549.1	88.8	-2816.5	-2908.4	819.4
10	ok	0.08	0.9	4.77e-03	5.7	5.7	5.7	5.7	-1630.5	-25.1	-467.3	-7022.4	-5760.0	197.2
11	ok	0.08	0.8	5.96e-03	5.7	5.7	5.7	5.7	-1361.3	2326.0	1014.4	-5905.0	-1296.0	-663.3
12	ok	0.08	0.3	5.13e-03	5.7	5.7	5.7	5.7	-280.3	7497.1	941.6	-561.5	-949.7	615.5
13	ok	0.08	0.7	5.81e-03	5.7	5.7	5.7	5.7	-447.7	-2062.8	82.1	-4757.5	-6232.7	-131.1
14	ok	0.08	1.0	2.68e-03	5.7	5.7	5.7	5.7	-520.5	-177.6	-342.9	-7930.1	-7444.9	-181.6
15	ok	0.08	0.7	6.68e-03	5.7	5.7	5.7	5.7	-2279.9	4757.0	-358.1	-5964.0	-1818.1	-481.4
16	ok	0.08	0.6	2.10e-02	5.7	5.7	5.7	5.7	1701.3	-1322.8	501.9	1067.2	1086.6	547.6
17	ok	0.08	0.3	3.18e-03	5.7	5.7	5.7	5.7	6177.3	912.5	-375.9	-945.7	-1494.4	213.7
18	ok	0.08	0.3	2.68e-03	5.7	5.7	5.7	5.7	6478.9	1587.7	-1054.1	-1073.8	-1139.6	-566.6
19	ok	0.08	1.0	2.50e-02	5.7	5.7	5.7	5.7	2.255e+04	-134.9	2949.7	-3992.2	-1201.0	-1298.0
20	ok	0.10	1.0	2.80e-02	5.7	5.7	5.7	5.7	2.052e+04	-1.005e+04	-1151.0	-8816.2	-3069.1	2934.1
21	ok	0.08	1.0	3.49e-02	5.7	5.7	5.7	5.7	-1.664e+04	-4344.3	2589.1	2510.2	938.9	1667.4
22	ok	0.08	1.0	3.12e-02	5.7	5.7	5.7	5.7	-1.364e+04	421.7	-1.003e+04	2716.9	1094.8	1274.6
23	ok	0.08	0.6	7.92e-03	5.7	5.7	5.7	5.7	1.660e+04	-2231.8	-5385.0	-1722.9	142.1	1432.4
24	ok	0.08	0.4	8.86e-03	5.7	5.7	5.7	5.7	5960.6	-1770.3	3873.8	-1041.9	288.9	-894.0
25	ok	0.08	0.3	1.01e-02	5.7	5.7	5.7	5.7	1352.9	-100.2	1437.9	1399.7	973.2	-1578.3
26	ok	0.08	0.2	8.49e-03	5.7	5.7	5.7	5.7	53.4	-211.6	-1798.6	1203.7	153.6	-570.4
27	ok	0.08	0.4	4.20e-04	5.7	5.7	5.7	5.7	1.202e+04	282.2	1052.4	-1037.6	-42.8	-230.0
28	ok	0.08	0.6	3.33e-04	5.7	5.7	5.7	5.7	2.154e+04	362.0	-1327.6	-1549.6	-34.6	375.5
29	ok	0.08	0.9	2.71e-02	5.7	5.7	5.7	5.7	1.506e+04	36.1	443.0	-3685.2	-152.6	-255.9
30	ok	0.08	0.2	1.14e-02	5.7	5.7	5.7	5.7	-5558.8	-804.8	-50.3	244.9	207.0	392.7
31	ok	0.08	9.42e-02	2.48e-03	5.7	5.7	5.7	5.7	805.1	512.1	84.6	-315.0	-193.0	-213.8
32	ok	0.08	0.2	1.06e-02	5.7	5.7	5.7	5.7	2405.6	-1446.3	1102.2	572.0	414.6	425.4
33	ok	0.08	1.0	3.13e-02	5.7	5.7	5.7	5.7	-636.3	2.529e+04	-1032.1	-78.5	-3550.2	-15.3
34	ok	0.08	0.7	1.31e-02	5.7	5.7	5.7	5.7	1.505e+04	4714.5	-6277.5	-1411.2	1466.4	1198.6
35	ok	0.08	0.3	1.24e-02	5.7	5.7	5.7	5.7	-3444.9	-2236.6	-3539.8	-1987.3	-425.8	1056.8

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy
36	ok	0.08	0.9	4.51e-03	5.7	5.7	5.7	5.7	2506.0	-631.9	2242.5	-4075.4	-261.4	1435.7
37	ok	0.08	0.9	3.19e-03	5.7	5.7	5.7	5.7	1.720e+04	-434.5	-1695.0	-3818.8	-411.8	-765.3
38	ok	0.08	0.3	6.92e-04	5.7	5.7	5.7	5.7	8762.9	39.3	-203.8	-1089.6	31.5	-390.1
39	ok	0.08	0.2	4.31e-04	5.7	5.7	5.7	5.7	3748.1	155.0	-166.7	-611.0	100.1	-114.0
40	ok	0.08	0.2	7.28e-03	5.7	5.7	5.7	5.7	-1628.6	139.0	-86.8	534.1	-191.6	410.3
41	ok	0.08	0.1	7.18e-03	5.7	5.7	5.7	5.7	221.4	-147.2	23.2	-4.6	62.3	-84.8
42	ok	0.08	0.1	8.57e-03	5.7	5.7	5.7	5.7	-1737.5	3462.0	2070.2	227.6	-252.9	235.3
43	ok	0.08	0.2	3.80e-03	5.7	5.7	5.7	5.7	343.5	3976.7	579.4	58.3	-804.1	406.4
44	ok	0.08	0.1	6.68e-03	5.7	5.7	5.7	5.7	-145.3	-441.3	508.3	77.5	973.9	8.5
45	ok	0.08	0.5	1.75e-02	5.7	5.7	5.7	5.7	1878.0	1.037e+04	-3952.8	73.2	-2068.3	-1026.4
46	ok	0.08	0.2	9.77e-03	5.7	5.7	5.7	5.7	-1027.0	1869.7	-158.2	482.7	886.5	-738.6
47	ok	0.08	0.2	3.59e-03	5.7	5.7	5.7	5.7	-2161.4	-1636.6	-56.5	-761.5	-283.9	353.6
48	ok	0.08	0.5	3.53e-02	5.7	5.7	5.7	5.7	-830.4	-2.129e+04	204.4	-279.4	4763.1	-753.4
49	ok	0.08	0.7	7.63e-03	5.7	5.7	5.7	5.7	-2957.7	-1230.6	-246.2	1886.3	6005.5	-208.5
50	ok	0.08	0.7	5.37e-03	5.7	5.7	5.7	5.7	-1585.0	1098.1	262.1	1090.3	5549.2	897.5
51	ok	0.08	0.4	3.29e-02	5.7	5.7	5.7	5.7	-857.7	-1.981e+04	-1266.5	109.5	4916.7	92.2
52	ok	0.08	0.7	3.53e-02	5.7	5.7	5.7	5.7	-3756.5	-1.645e+04	1812.8	-4169.4	1649.0	897.9
53	ok	0.09	1.0	2.49e-02	5.7	5.7	5.7	5.7	1.451e+04	-8955.5	-9265.4	-4718.4	-1740.5	2598.8
58	ok	0.08	0.4	4.18e-02	5.7	5.7	5.7	5.7	-5694.5	-2.305e+04	-2541.3	-2551.6	2494.3	-1142.4
63	ok	0.08	0.5	1.36e-02	5.7	5.7	5.7	5.7	3144.7	-3336.0	-1260.7	-3224.2	765.9	-793.2
64	ok	0.08	0.5	1.39e-02	5.7	5.7	5.7	5.7	2256.4	-6305.2	337.2	-3642.4	643.5	-463.3
65	ok	0.08	0.5	1.22e-03	5.7	5.7	5.7	5.7	2115.4	756.9	20.4	247.5	3463.4	-615.5
66	ok	0.08	0.5	8.17e-04	5.7	5.7	5.7	5.7	1600.6	676.6	115.1	252.0	3470.8	-622.7
67	ok	0.08	0.5	2.47e-03	5.7	5.7	5.7	5.7	-130.0	-220.8	385.7	1770.3	3854.9	-18.0
68	ok	0.08	0.5	2.43e-03	5.7	5.7	5.7	5.7	-57.9	-430.9	566.8	1858.2	3895.2	-103.6
69	ok	0.08	0.2	1.77e-02	5.7	5.7	5.7	5.7	200.9	-7632.1	-1119.1	-364.3	1391.7	1067.8
70	ok	0.08	0.2	1.82e-02	5.7	5.7	5.7	5.7	245.7	-8119.6	-392.3	-322.8	1549.1	1038.2
71	ok	0.08	0.2	1.65e-02	5.7	5.7	5.7	5.7	-194.1	-9051.9	-21.2	46.8	1744.1	101.0
72	ok	0.08	0.2	1.89e-02	5.7	5.7	5.7	5.7	7.3	-7365.1	756.4	51.9	1671.6	243.7
73	ok	0.08	0.3	3.50e-02	5.7	5.7	5.7	5.7	-7046.4	-3796.2	-31.8	665.2	-1394.6	-2261.7
74	ok	0.08	0.1	2.20e-02	5.7	5.7	5.7	5.7	-7125.6	659.6	1003.8	801.9	36.5	-717.8
75	ok	0.08	0.3	2.97e-02	5.7	5.7	5.7	5.7	-1.207e+04	-3497.1	-768.4	410.3	-1580.9	-1282.9
76	ok	0.08	0.1	2.92e-02	5.7	5.7	5.7	5.7	-1.035e+04	-28.0	457.3	859.0	26.2	-262.1
77	ok	0.08	0.2	2.08e-02	5.7	5.7	5.7	5.7	-7820.0	-2551.5	3635.2	477.6	-1622.2	113.8
78	ok	0.08	7.88e-02	1.89e-02	5.7	5.7	5.7	5.7	-6656.9	22.7	-273.8	702.2	112.5	-94.7
79	ok	0.08	0.3	1.66e-02	5.7	5.7	5.7	5.7	763.2	-1865.7	2052.9	-543.1	-1503.8	-698.4
80	ok	0.08	0.1	1.61e-02	5.7	5.7	5.7	5.7	-6170.6	-300.4	550.3	660.5	162.8	122.2
81	ok	0.08	0.2	2.29e-02	5.7	5.7	5.7	5.7	-1161.8	-2407.6	611.2	-387.5	-1312.2	573.5
82	ok	0.08	7.88e-02	2.25e-02	5.7	5.7	5.7	5.7	-8410.4	205.6	167.6	629.0	26.4	338.9
83	ok	0.08	0.4	1.97e-02	5.7	5.7	5.7	5.7	5100.4	-2470.5	4371.8	-567.4	-1108.4	1351.8
84	ok	0.08	0.2	1.10e-02	5.7	5.7	5.7	5.7	4787.3	139.7	-142.0	-491.4	-69.7	513.7
85	ok	0.08	0.5	1.69e-02	5.7	5.7	5.7	5.7	1.215e+04	186.3	838.9	-1135.3	-367.4	942.5
86	ok	0.08	0.4	1.37e-02	5.7	5.7	5.7	5.7	1.297e+04	554.6	-63.3	-1080.1	-80.8	290.7
87	ok	0.08	0.5	2.90e-02	5.7	5.7	5.7	5.7	1.261e+04	183.6	3104.5	-931.1	724.9	1411.9
88	ok	0.08	0.5	2.85e-02	5.7	5.7	5.7	5.7	1.359e+04	647.2	116.2	-1138.3	-69.5	385.2
89	ok	0.08	0.9	2.85e-02	5.7	5.7	5.7	5.7	-1.481e+04	-5864.7	1265.1	2861.5	-1313.7	1793.5
90	ok	0.08	0.9	2.65e-02	5.7	5.7	5.7	5.7	-1.573e+04	530.1	-2029.8	3054.9	-3.1	446.4
91	ok	0.08	0.2	1.11e-02	5.7	5.7	5.7	5.7	-440.5	-1304.6	1574.9	-502.2	-552.7	-300.5
92	ok	0.08	0.7	2.38e-02	5.7	5.7	5.7	5.7	1.360e+04	344.3	-751.5	-2708.0	-237.5	-155.8
93	ok	0.08	0.7	2.40e-02	5.7	5.7	5.7	5.7	1.406e+04	353.8	-989.1	-2763.0	-205.2	-159.1
94	ok	0.08	0.1	4.88e-03	5.7	5.7	5.7	5.7	526.8	2530.0	64.4	-376.5	-423.9	-408.1
95	ok	0.08	0.6	2.11e-02	5.7	5.7	5.7	5.7	9597.8	-2540.2	-7671.9	-2757.4	-795.3	-224.3
96	ok	0.08	0.7	8.99e-03	5.7	5.7	5.7	5.7	1.049e+04	-695.8	-2265.1	-1969.6	-1040.3	1531.4
97	ok	0.08	0.4	1.56e-02	5.7	5.7	5.7	5.7	9291.4	-1348.1	-715.5	-814.9	-725.3	969.2
98	ok	0.08	0.5	2.49e-02	5.7	5.7	5.7	5.7	1.099e+04	-277.1	3091.7	-875.4	1036.2	1525.3
99	ok	0.08	0.9	2.91e-02	5.7	5.7	5.7	5.7	-1.716e+04	-5208.4	720.6	2969.6	-1145.1	2017.3
100	ok	0.08	0.5	1.29e-02	5.7	5.7	5.7	5.7	3664.6	-1094.6	4615.1	-1360.4	-1235.6	-1125.4
101	ok	0.08	0.3	1.43e-02	5.7	5.7	5.7	5.7	-110.1	-2913.7	1950.1	277.6	-1710.4	-1155.0
102	ok	0.08	0.1	1.96e-02	5.7	5.7	5.7	5.7	-363.1	-2238.6	661.0	-240.5	-1120.3	609.0
103	ok	0.08	0.4	1.41e-02	5.7	5.7	5.7	5.7	5989.6	-1598.2	2739.6	-435.6	-1475.9	1513.6
104	ok	0.08	0.4	1.46e-02	5.7	5.7	5.7	5.7	247.3	-2788.7	750.3	1061.4	929.9	-1880.8
105	ok	0.08	0.4	2.75e-02	5.7	5.7	5.7	5.7	-4212.0	-1192.7	396.8	816.8	-1314.3	-2429.3
106	ok	0.08	0.3	2.61e-02	5.7	5.7	5.7	5.7	-6221.2	-3651.9	1855.0	58.8	-1522.0	-1548.9
107	ok	0.08	0.2	1.80e-02	5.7	5.7	5.7	5.7	-6272.1	-2826.5	1954.5	919.0	-1473.9	279.6
108	ok	0.08	0.3	1.01e-02	5.7	5.7	5.7	5.7	1129.6	3729.0	848.7	415.2	445.9	-921.1
109	ok	0.08	0.5	1.99e-02	5.7	5.7	5.7	5.7	-3700.2	-5467.8	-3766.0	1749.2	902.4	-2379.6
110	ok	0.08	0.3	1.77e-02	5.7	5.7	5.7	5.7	-5975.5	-5394.4	-1214.1	1607.8	1214.0	-1562.1

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy
111	ok	0.08	0.4	1.30e-02	5.7	5.7	5.7	5.7	-3764.4	-2741.3	-1138.2	2622.3	2555.3	-546.3
112	ok	0.08	0.3	1.09e-02	5.7	5.7	5.7	5.7	-2201.7	-373.5	-1123.0	1943.3	1566.6	574.7
113	ok	0.08	0.3	1.21e-02	5.7	5.7	5.7	5.7	-4195.9	-2708.7	832.7	1276.0	2348.4	339.0
114	ok	0.08	0.4	9.05e-03	5.7	5.7	5.7	5.7	-3109.7	-2660.5	600.3	2344.0	2466.7	251.4
115	ok	0.08	0.6	9.52e-03	5.7	5.7	5.7	5.7	3307.5	426.1	1712.2	1611.1	2064.6	1136.9
116	ok	0.08	0.5	1.53e-02	5.7	5.7	5.7	5.7	1662.2	-4042.6	820.3	1702.3	2265.3	808.3
117	ok	0.08	0.8	1.97e-02	5.7	5.7	5.7	5.7	-1.113e+04	-7481.4	-1720.4	3956.0	889.6	2091.8
118	ok	0.08	0.3	1.68e-02	5.7	5.7	5.7	5.7	-568.6	8684.6	554.5	-464.7	-889.6	214.7
119	ok	0.08	0.5	1.65e-02	5.7	5.7	5.7	5.7	102.4	-301.4	1058.6	828.4	1223.6	1035.6
120	ok	0.08	0.4	2.14e-02	5.7	5.7	5.7	5.7	21.9	1.146e+04	811.8	-289.3	-1088.3	286.0
121	ok	0.08	0.7	3.21e-02	5.7	5.7	5.7	5.7	-2684.8	-1.697e+04	-6322.1	-487.0	3998.6	-665.9
122	ok	0.08	0.6	2.42e-02	5.7	5.7	5.7	5.7	1661.1	-1.456e+04	-802.3	658.8	4421.7	42.9
123	ok	0.08	0.5	1.54e-02	5.7	5.7	5.7	5.7	-1910.6	-6737.9	-1234.4	2115.5	2935.3	-1835.3
124	ok	0.08	0.5	1.61e-02	5.7	5.7	5.7	5.7	-1833.5	-6608.0	-471.6	2422.6	3822.9	-1407.2
125	ok	0.08	0.6	1.32e-02	5.7	5.7	5.7	5.7	-2661.6	-5600.7	-1247.1	2725.0	3582.9	-1530.3
126	ok	0.08	0.6	1.19e-02	5.7	5.7	5.7	5.7	-2115.6	-5176.7	-922.8	3356.7	4785.1	-1112.6
127	ok	0.08	0.6	1.16e-02	5.7	5.7	5.7	5.7	-2871.2	-3064.8	-1695.5	2327.3	3569.0	-1185.7
128	ok	0.08	0.7	8.82e-03	5.7	5.7	5.7	5.7	-2663.7	-3013.0	-1193.5	2744.3	5490.3	-784.1
129	ok	0.08	0.8	1.07e-02	5.7	5.7	5.7	5.7	-4168.7	324.8	129.5	701.1	3870.5	-231.1
130	ok	0.08	0.6	8.97e-03	5.7	5.7	5.7	5.7	-3558.8	-1484.6	1921.6	1672.4	4185.1	479.1
131	ok	0.08	0.7	6.43e-03	5.7	5.7	5.7	5.7	-1986.3	-1505.3	564.9	2226.9	5796.7	406.7
132	ok	0.08	0.6	6.31e-03	5.7	5.7	5.7	5.7	-907.0	-2728.1	421.0	2117.1	4138.5	509.8
133	ok	0.08	0.7	5.13e-03	5.7	5.7	5.7	5.7	-1205.2	-1638.2	10.9	2429.9	5627.2	530.7
134	ok	0.08	0.6	7.67e-03	5.7	5.7	5.7	5.7	-894.4	-28.1	-799.7	1385.5	4528.5	160.1
135	ok	0.08	0.8	5.66e-03	5.7	5.7	5.7	5.7	-1165.1	-348.0	-655.4	1810.9	5611.8	595.9
136	ok	0.08	0.8	8.33e-03	5.7	5.7	5.7	5.7	-2303.0	2082.0	344.3	-437.5	3526.8	1424.8
137	ok	0.08	0.6	7.86e-03	5.7	5.7	5.7	5.7	841.0	-374.6	2145.3	1436.1	3268.7	1745.9
138	ok	0.08	0.7	6.44e-03	5.7	5.7	5.7	5.7	-774.4	-16.0	1381.9	1558.7	4650.1	1134.3
139	ok	0.08	0.5	1.06e-02	5.7	5.7	5.7	5.7	-1616.9	-3839.2	994.3	2312.8	3800.1	681.9
140	ok	0.08	0.5	8.42e-03	5.7	5.7	5.7	5.7	-826.5	-3462.0	188.4	2263.0	4257.7	437.9
141	ok	0.08	0.8	1.18e-02	5.7	5.7	5.7	5.7	-1972.2	-5522.1	362.6	4486.0	2944.9	912.1
142	ok	0.08	0.9	9.93e-03	5.7	5.7	5.7	5.7	3784.5	-4818.6	-1242.1	6066.7	3388.0	618.7
143	ok	0.08	1.0	1.40e-02	5.7	5.7	5.7	5.7	1630.6	3777.3	-2180.6	-5907.9	-3035.7	543.3
144	ok	0.08	0.5	9.81e-03	5.7	5.7	5.7	5.7	3543.0	-5324.3	2391.2	460.1	2738.8	339.7
145	ok	0.08	0.4	1.46e-02	5.7	5.7	5.7	5.7	582.2	2286.6	-5052.7	-814.0	-2499.9	-558.8
146	ok	0.08	0.8	2.97e-02	5.7	5.7	5.7	5.7	77.6	-1.785e+04	1223.2	268.7	3257.2	304.9
147	ok	0.08	0.9	3.41e-02	5.7	5.7	5.7	5.7	-1592.8	-2.058e+04	134.1	189.7	2890.4	323.0
148	ok	0.08	0.3	3.11e-02	5.7	5.7	5.7	5.7	-617.0	-1.635e+04	-858.0	73.6	3721.5	-148.5
149	ok	0.08	0.3	3.11e-02	5.7	5.7	5.7	5.7	-238.2	-1.581e+04	-1180.6	-268.1	3638.8	-652.7
150	ok	0.08	0.3	2.04e-02	5.7	5.7	5.7	5.7	-108.2	-7440.5	160.4	-86.8	2275.4	-345.0
151	ok	0.08	0.3	2.55e-02	5.7	5.7	5.7	5.7	89.5	-9272.8	4954.6	-509.4	2416.8	-805.7
152	ok	0.08	0.5	1.58e-02	5.7	5.7	5.7	5.7	-1868.8	-6548.8	-276.8	2667.7	3942.2	-877.9
153	ok	0.08	0.4	1.39e-02	5.7	5.7	5.7	5.7	-569.0	-6088.0	10.8	2966.3	3111.2	-557.5
154	ok	0.08	0.4	1.60e-02	5.7	5.7	5.7	5.7	1282.3	-7122.7	354.6	3430.3	2380.3	-108.6
155	ok	0.08	0.6	1.10e-02	5.7	5.7	5.7	5.7	-1902.1	-4763.9	-716.2	3754.4	4844.6	-519.1
156	ok	0.08	0.5	1.04e-02	5.7	5.7	5.7	5.7	-1273.1	-4628.3	-444.6	4111.8	3927.1	-36.0
157	ok	0.08	0.5	9.81e-03	5.7	5.7	5.7	5.7	-621.7	-4319.0	182.2	4355.0	2898.1	117.3
158	ok	0.08	0.7	7.95e-03	5.7	5.7	5.7	5.7	-2170.0	-3229.2	-808.1	3165.9	5591.1	-108.6
159	ok	0.08	0.5	7.61e-03	5.7	5.7	5.7	5.7	-1745.0	-3354.8	-457.3	3027.1	4398.5	666.4
160	ok	0.08	0.6	7.10e-03	5.7	5.7	5.7	5.7	-1235.7	-3130.7	-44.8	4664.3	2472.1	375.2
161	ok	0.08	0.7	5.87e-03	5.7	5.7	5.7	5.7	-2318.0	-1961.2	-387.3	2300.4	6158.4	59.6
162	ok	0.08	0.7	5.56e-03	5.7	5.7	5.7	5.7	-1858.4	-2271.0	-322.1	1703.1	5746.7	439.8
163	ok	0.08	0.7	5.22e-03	5.7	5.7	5.7	5.7	-1981.0	-1482.4	-124.1	2563.5	5848.0	81.9
164	ok	0.08	0.6	4.64e-03	5.7	5.7	5.7	5.7	-1915.2	-1467.2	-263.8	2419.5	4448.7	-447.6
165	ok	0.08	0.5	4.31e-03	5.7	5.7	5.7	5.7	-1731.1	-1396.0	-175.2	3998.3	2311.1	-91.6
166	ok	0.08	0.7	4.94e-03	5.7	5.7	5.7	5.7	-1652.5	-1080.8	-335.3	2682.7	5584.5	493.0
167	ok	0.08	0.5	4.67e-03	5.7	5.7	5.7	5.7	-1876.1	-967.1	-369.2	3083.2	4079.3	382.1
168	ok	0.08	0.4	4.31e-03	5.7	5.7	5.7	5.7	-1882.7	-896.2	-236.2	3340.5	2475.3	248.0
169	ok	0.08	0.7	4.99e-03	5.7	5.7	5.7	5.7	-1652.5	-388.6	-414.7	1877.6	5573.2	779.3
170	ok	0.08	0.5	4.75e-03	5.7	5.7	5.7	5.7	-1857.9	-432.1	-378.0	1485.8	3988.5	1183.6
171	ok	0.08	0.4	4.47e-03	5.7	5.7	5.7	5.7	-1946.0	-458.2	-188.3	3293.1	1097.1	-322.0
172	ok	0.08	0.7	4.71e-03	5.7	5.7	5.7	5.7	-1685.6	166.2	64.7	1108.9	5509.7	597.4
173	ok	0.08	0.7	4.48e-03	5.7	5.7	5.7	5.7	-1832.4	-354.0	87.9	191.2	5242.0	708.2
174	ok	0.08	0.6	4.93e-03	5.7	5.7	5.7	5.7	-1379.8	-418.9	761.9	1543.2	4473.5	195.8
175	ok	0.08	0.5	4.65e-03	5.7	5.7	5.7	5.7	-1688.8	-1732.1	-645.0	1558.1	2846.9	-564.9
176	ok	0.08	0.3	4.57e-03	5.7	5.7	5.7	5.7	-1374.2	-342.4	1.7	1987.4	1024.1	-409.6
177	ok	0.08	0.5	7.03e-03	5.7	5.7	5.7	5.7	-1057.2	-3311.6	-258.2	2589.1	4238.5	8.6

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy
178	ok	0.08	0.4	6.54e-03	5.7	5.7	5.7	5.7	95.2	-3749.3	-902.0	3022.1	2599.5	-152.7
179	ok	0.08	0.3	6.45e-03	5.7	5.7	5.7	5.7	-1147.1	-3041.8	-1470.5	2011.0	2153.0	-335.2
180	ok	0.08	0.7	9.03e-03	5.7	5.7	5.7	5.7	-2101.9	1765.9	2815.1	-5108.2	-1014.8	-354.6
181	ok	0.08	0.5	8.94e-03	5.7	5.7	5.7	5.7	306.6	-2802.9	-1522.8	2226.5	1540.8	-523.7
182	ok	0.08	0.4	1.11e-02	5.7	5.7	5.7	5.7	467.9	-4099.6	-2153.9	1954.8	1036.3	-865.9
183	ok	0.08	1.0	2.41e-02	5.7	5.7	5.7	5.7	919.8	519.7	5423.2	-7358.4	-1214.7	444.1
184	ok	0.08	0.8	1.89e-02	5.7	5.7	5.7	5.7	-308.5	-5880.4	1721.2	-5697.5	-555.6	519.9
185	ok	0.08	0.9	3.95e-02	5.7	5.7	5.7	5.7	3766.5	2.140e+04	4100.4	-627.7	-2426.2	-817.5
186	ok	0.08	0.5	1.53e-02	5.7	5.7	5.7	5.7	-1078.2	-6844.4	3587.7	-1842.6	607.5	906.0
187	ok	0.08	0.5	2.76e-02	5.7	5.7	5.7	5.7	-517.2	-1.574e+04	118.4	-49.5	2691.5	-430.2
188	ok	0.08	0.5	1.51e-02	5.7	5.7	5.7	5.7	-268.1	-5033.0	-235.6	127.7	2043.7	-1336.3
189	ok	0.08	0.3	2.11e-02	5.7	5.7	5.7	5.7	-160.9	-8898.8	914.4	335.0	1786.8	-1343.6
190	ok	0.08	0.4	1.74e-02	5.7	5.7	5.7	5.7	-46.4	-2793.6	814.4	115.7	1011.4	-1682.7
191	ok	0.08	0.9	3.94e-02	5.7	5.7	5.7	5.7	340.9	2.094e+04	-676.9	-407.2	-2866.7	-577.1
192	ok	0.08	0.4	3.29e-02	5.7	5.7	5.7	5.7	-1600.1	-1.982e+04	562.5	243.2	2456.8	401.0
193	ok	0.08	0.2	2.23e-02	5.7	5.7	5.7	5.7	77.8	-9489.2	151.6	-43.2	1549.7	-801.4
194	ok	0.08	0.3	1.73e-02	5.7	5.7	5.7	5.7	382.2	-3247.8	-218.3	85.9	2399.3	282.5
195	ok	0.08	0.3	2.27e-02	5.7	5.7	5.7	5.7	866.3	-6488.7	2316.5	251.0	2496.2	495.8
196	ok	0.08	0.2	1.85e-02	5.7	5.7	5.7	5.7	-180.9	-7111.3	-663.8	137.1	2082.6	189.7
197	ok	0.08	0.2	1.94e-02	5.7	5.7	5.7	5.7	-125.1	-7095.7	-1810.3	-82.6	1955.8	220.2
198	ok	0.08	0.1	6.99e-03	5.7	5.7	5.7	5.7	278.6	-3115.0	263.9	86.3	1081.1	-253.5
199	ok	0.08	0.1	1.26e-02	5.7	5.7	5.7	5.7	-315.7	-2297.8	4417.4	-479.9	850.8	112.8
200	ok	0.08	0.4	1.15e-02	5.7	5.7	5.7	5.7	-343.2	-4640.8	1469.8	2891.4	2388.6	351.7
201	ok	0.08	0.4	1.02e-02	5.7	5.7	5.7	5.7	-877.8	-3970.8	973.2	2762.5	2393.2	163.3
202	ok	0.08	0.4	8.09e-03	5.7	5.7	5.7	5.7	338.2	-3131.2	1226.6	2786.5	1560.2	222.6
203	ok	0.08	0.4	1.10e-02	5.7	5.7	5.7	5.7	1490.1	-3779.9	2229.6	3018.6	1313.3	548.7
204	ok	0.08	0.5	8.74e-03	5.7	5.7	5.7	5.7	-654.0	-3752.9	689.4	3999.6	2720.8	-19.7
205	ok	0.08	0.5	7.78e-03	5.7	5.7	5.7	5.7	-589.5	-3230.9	781.2	3720.7	2654.9	191.4
206	ok	0.08	0.5	7.41e-03	5.7	5.7	5.7	5.7	167.3	-3055.6	871.7	3814.4	1790.2	472.1
207	ok	0.08	0.5	7.59e-03	5.7	5.7	5.7	5.7	314.8	-2803.9	1351.2	3908.4	1568.2	337.5
208	ok	0.08	0.4	6.70e-03	5.7	5.7	5.7	5.7	-999.2	-3029.9	160.3	2865.4	3016.7	-528.2
209	ok	0.08	0.4	6.22e-03	5.7	5.7	5.7	5.7	-664.0	-2694.1	467.4	2952.7	3104.8	181.5
210	ok	0.08	0.4	6.06e-03	5.7	5.7	5.7	5.7	-195.0	-2322.3	607.0	3001.1	1601.4	909.7
211	ok	0.08	0.6	6.66e-03	5.7	5.7	5.7	5.7	153.6	-1324.3	951.0	3909.0	856.2	511.7
212	ok	0.08	0.5	4.80e-03	5.7	5.7	5.7	5.7	-1084.3	-2161.3	76.8	1633.3	4156.5	-122.1
213	ok	0.08	0.4	4.78e-03	5.7	5.7	5.7	5.7	-1008.1	-2028.4	300.9	2019.7	3465.3	178.9
214	ok	0.08	0.5	4.96e-03	5.7	5.7	5.7	5.7	-125.4	-1813.6	557.2	1125.6	3559.5	679.5
215	ok	0.08	0.4	3.77e-03	5.7	5.7	5.7	5.7	-1494.4	-1437.6	-3.0	2161.0	2848.1	672.4
216	ok	0.08	0.4	3.82e-03	5.7	5.7	5.7	5.7	-1218.5	-1337.7	206.1	2173.2	2950.0	19.3
217	ok	0.08	0.3	3.91e-03	5.7	5.7	5.7	5.7	-841.6	-1007.0	447.7	2281.7	1314.8	-711.3
218	ok	0.08	0.4	3.88e-03	5.7	5.7	5.7	5.7	-455.0	-832.5	313.3	3544.8	990.1	-370.4
219	ok	0.08	0.3	3.87e-03	5.7	5.7	5.7	5.7	-1706.6	-967.0	-93.7	2685.3	2462.0	-36.1
220	ok	0.08	0.3	3.39e-03	5.7	5.7	5.7	5.7	-1435.6	-836.3	102.0	2160.6	2565.5	-64.8
221	ok	0.08	0.3	2.91e-03	5.7	5.7	5.7	5.7	-1016.4	-583.9	307.9	2360.3	1384.3	-72.2
222	ok	0.08	0.3	2.31e-03	5.7	5.7	5.7	5.7	-530.8	-180.7	383.2	2684.4	696.4	-262.4
223	ok	0.08	0.4	4.26e-03	5.7	5.7	5.7	5.7	-1920.3	-676.6	-187.7	1484.1	2011.4	-815.1
224	ok	0.08	0.3	3.63e-03	5.7	5.7	5.7	5.7	-1565.2	-526.2	-6.9	1040.2	2744.8	-149.1
225	ok	0.08	0.2	2.84e-03	5.7	5.7	5.7	5.7	-1235.9	-244.7	195.3	1142.6	949.5	663.9
226	ok	0.08	0.3	2.02e-03	5.7	5.7	5.7	5.7	-247.2	-53.9	279.0	2090.0	-1291.2	-703.5
227	ok	0.08	0.5	4.35e-03	5.7	5.7	5.7	5.7	-1453.4	114.5	-191.7	-1434.9	2741.5	59.2
228	ok	0.08	0.4	3.79e-03	5.7	5.7	5.7	5.7	-1526.6	257.8	-24.0	-551.6	2635.0	-274.4
229	ok	0.08	0.4	2.77e-03	5.7	5.7	5.7	5.7	-1045.6	332.1	45.4	-1969.8	2476.8	-746.1
230	ok	0.08	0.3	4.69e-03	5.7	5.7	5.7	5.7	-1823.4	-928.0	-172.1	575.0	1927.9	371.5
231	ok	0.08	0.3	4.00e-03	5.7	5.7	5.7	5.7	-1703.6	-765.4	-210.0	330.0	2374.0	-318.3
232	ok	0.08	0.3	2.96e-03	5.7	5.7	5.7	5.7	-1081.7	64.8	0.9	-1194.8	-606.5	-1485.6
233	ok	0.08	0.2	2.24e-03	5.7	5.7	5.7	5.7	-283.0	319.3	-84.2	963.7	-1186.7	-135.1
234	ok	0.08	0.2	6.30e-03	5.7	5.7	5.7	5.7	-1431.7	-2373.9	-1844.5	1269.8	1766.1	-312.8
235	ok	0.08	0.2	5.56e-03	5.7	5.7	5.7	5.7	-1740.8	-1597.7	-451.1	532.2	1734.7	-446.5
236	ok	0.08	0.2	4.21e-03	5.7	5.7	5.7	5.7	-1225.9	-1167.2	-501.2	587.4	833.3	-607.5
237	ok	0.08	0.1	3.30e-03	5.7	5.7	5.7	5.7	-468.6	-736.1	-634.1	833.4	322.3	-433.5
238	ok	0.08	0.3	8.00e-03	5.7	5.7	5.7	5.7	-1662.6	-1174.5	339.5	-1898.3	1250.5	-219.4
239	ok	0.08	0.2	8.49e-03	5.7	5.7	5.7	5.7	-1859.0	-2257.5	-580.8	-1596.9	1136.6	-535.9
240	ok	0.08	0.2	6.88e-03	5.7	5.7	5.7	5.7	-1203.4	-350.0	306.3	-1713.0	387.0	111.6
241	ok	0.08	0.2	7.54e-03	5.7	5.7	5.7	5.7	-369.9	-37.9	-702.4	-1631.8	-488.9	-378.9
242	ok	0.08	0.6	1.88e-02	5.7	5.7	5.7	5.7	-507.6	-6187.3	2575.8	-4364.8	644.9	-683.2
243	ok	0.08	0.5	1.95e-02	5.7	5.7	5.7	5.7	-42.1	-7784.1	-1909.2	-3945.5	854.3	-616.9
244	ok	0.08	0.6	1.74e-02	5.7	5.7	5.7	5.7	-879.7	-2569.4	1848.7	-4652.9	-335.6	-651.6

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy
245	ok	0.08	0.2	1.88e-02	5.7	5.7	5.7	5.7	-225.2	-7731.2	922.8	338.2	1231.8	-1708.9
246	ok	0.08	0.2	1.37e-02	5.7	5.7	5.7	5.7	-297.3	-3539.8	565.2	-35.2	1197.6	-1537.6
247	ok	0.08	0.2	1.76e-02	5.7	5.7	5.7	5.7	-328.6	-8074.7	169.4	197.3	1210.8	-1612.2
248	ok	0.08	0.2	1.40e-02	5.7	5.7	5.7	5.7	-1204.4	-5481.4	37.8	-1257.5	1098.1	-772.3
249	ok	0.08	0.2	1.73e-02	5.7	5.7	5.7	5.7	-469.2	-9078.4	24.7	209.8	1308.8	-1349.0
250	ok	0.08	0.2	1.38e-02	5.7	5.7	5.7	5.7	-493.0	-5518.8	-760.3	-1351.8	581.2	-962.4
251	ok	0.08	0.2	2.19e-02	5.7	5.7	5.7	5.7	-299.2	-9821.4	340.8	113.8	1324.4	-1243.7
252	ok	0.08	0.2	1.71e-02	5.7	5.7	5.7	5.7	-89.2	-7288.5	-143.5	-841.7	697.5	-919.4
253	ok	0.08	0.2	1.95e-02	5.7	5.7	5.7	5.7	-78.3	-9795.4	39.6	70.1	1621.0	-888.1
254	ok	0.08	0.2	1.80e-02	5.7	5.7	5.7	5.7	46.3	-8249.8	-204.0	54.6	1241.2	-1109.5
255	ok	0.08	0.1	1.81e-02	5.7	5.7	5.7	5.7	93.9	-8430.9	-295.6	37.6	1213.9	-960.8
256	ok	0.08	0.1	2.14e-02	5.7	5.7	5.7	5.7	-140.7	-1.149e+04	-449.9	13.8	1259.0	-763.9
257	ok	0.08	0.2	1.34e-02	5.7	5.7	5.7	5.7	-139.4	-5266.6	57.8	-93.2	1703.9	374.1
258	ok	0.08	0.3	1.74e-02	5.7	5.7	5.7	5.7	737.0	-6970.5	2951.8	92.8	1819.2	1010.6
259	ok	0.08	0.4	8.80e-03	5.7	5.7	5.7	5.7	-358.7	-3341.8	1694.6	2442.8	1957.5	552.5
260	ok	0.08	0.4	9.27e-03	5.7	5.7	5.7	5.7	-1132.9	-3064.6	1374.4	2213.7	2483.2	682.7
261	ok	0.08	0.4	7.26e-03	5.7	5.7	5.7	5.7	-280.1	-2410.5	1671.8	3351.7	2215.3	73.2
262	ok	0.08	0.4	6.47e-03	5.7	5.7	5.7	5.7	-848.5	-2004.6	1360.2	2871.9	3075.8	345.1
263	ok	0.08	0.4	5.30e-03	5.7	5.7	5.7	5.7	-368.4	-1501.7	1176.3	2321.7	2434.8	-667.9
264	ok	0.08	0.4	4.25e-03	5.7	5.7	5.7	5.7	-544.4	-1067.5	1068.4	2443.7	3531.4	-53.3
265	ok	0.08	0.4	3.75e-03	5.7	5.7	5.7	5.7	-133.1	-706.1	638.6	954.3	2961.3	-225.7
266	ok	0.08	0.3	2.58e-03	5.7	5.7	5.7	5.7	80.4	-413.0	759.3	1889.3	2156.1	343.0
267	ok	0.08	0.5	2.40e-03	5.7	5.7	5.7	5.7	474.3	-204.6	308.7	1784.4	3638.6	-21.8
268	ok	0.08	0.3	1.64e-03	5.7	5.7	5.7	5.7	223.6	-106.7	605.4	2182.3	1925.3	-406.2
269	ok	0.08	0.4	2.04e-03	5.7	5.7	5.7	5.7	1008.2	-27.2	284.0	1623.9	3471.0	-424.3
270	ok	0.08	0.3	1.40e-03	5.7	5.7	5.7	5.7	301.2	177.7	389.2	1041.8	1412.9	-1240.8
271	ok	0.08	0.5	1.30e-03	5.7	5.7	5.7	5.7	1354.8	346.6	232.7	876.3	3416.8	-763.7
272	ok	0.08	0.4	1.50e-03	5.7	5.7	5.7	5.7	481.1	825.7	250.5	-1114.4	2570.9	-625.7
273	ok	0.08	0.2	1.61e-03	5.7	5.7	5.7	5.7	628.7	896.5	276.9	-1161.5	-48.6	925.7
274	ok	0.08	0.4	5.58e-04	5.7	5.7	5.7	5.7	1797.9	636.2	-18.6	248.9	2815.8	-280.7
275	ok	0.08	0.1	2.02e-03	5.7	5.7	5.7	5.7	601.4	439.5	-476.5	-645.1	908.8	-206.3
276	ok	0.08	0.3	1.17e-03	5.7	5.7	5.7	5.7	1908.6	695.5	-526.3	-986.5	1516.6	-353.6
277	ok	0.08	0.3	4.10e-03	5.7	5.7	5.7	5.7	259.9	135.3	-585.9	-1697.0	699.1	-617.4
278	ok	0.08	0.3	3.12e-03	5.7	5.7	5.7	5.7	2306.6	441.0	-551.4	-1825.6	1234.7	-661.0
279	ok	0.08	0.6	1.31e-02	5.7	5.7	5.7	5.7	-595.6	-1790.6	1897.4	-4771.0	-399.3	-293.4
280	ok	0.08	0.3	1.43e-02	5.7	5.7	5.7	5.7	-2041.1	-6197.1	-553.0	-1595.9	878.8	405.6
281	ok	0.08	0.3	1.18e-02	5.7	5.7	5.7	5.7	-5038.5	-5381.0	-1918.6	-2137.5	778.3	759.5
282	ok	0.08	0.2	3.56e-02	5.7	5.7	5.7	5.7	-2456.3	-1.633e+04	-1800.0	-406.3	1680.0	-1175.6
283	ok	0.08	0.2	3.57e-02	5.7	5.7	5.7	5.7	473.5	-2.027e+04	1924.9	410.7	1516.2	-644.4
284	ok	0.08	0.3	6.96e-02	5.7	5.7	5.7	5.7	-7073.1	-2.090e+04	-3258.6	-1864.8	3084.1	-829.3
285	ok	0.08	0.4	9.10e-03	5.7	5.7	5.7	5.7	-1217.6	-3025.3	1323.4	2094.6	2417.2	886.0
286	ok	0.08	0.4	6.16e-03	5.7	5.7	5.7	5.7	-1011.0	-1867.2	1210.4	2728.5	3063.0	536.5
287	ok	0.08	0.4	3.83e-03	5.7	5.7	5.7	5.7	-612.0	-920.9	935.4	2344.2	3580.5	163.0
288	ok	0.08	0.5	2.65e-03	5.7	5.7	5.7	5.7	613.4	-176.0	53.9	1696.6	3735.2	-137.7
289	ok	0.08	0.5	2.25e-03	5.7	5.7	5.7	5.7	1282.2	-57.0	111.2	1476.1	3590.1	-460.6
290	ok	0.08	0.5	1.53e-03	5.7	5.7	5.7	5.7	1736.1	410.2	149.7	785.0	3604.2	-716.3
291	ok	0.08	0.4	8.26e-04	5.7	5.7	5.7	5.7	2436.1	659.4	-80.7	244.9	2960.8	-515.4
292	ok	0.08	0.3	1.46e-03	5.7	5.7	5.7	5.7	2661.7	715.9	-436.2	-1141.0	1564.6	-460.6
293	ok	0.08	0.3	3.81e-03	5.7	5.7	5.7	5.7	2888.2	211.9	-864.7	-1993.9	1131.2	-725.7
294	ok	0.08	0.3	1.14e-02	5.7	5.7	5.7	5.7	-2196.6	-3351.4	-344.6	-2279.9	289.0	941.7
295	ok	0.08	0.5	3.61e-02	5.7	5.7	5.7	5.7	1.188e+04	-1.840e+04	-143.1	-1780.0	4592.2	532.9
302	ok	0.08	1.0	2.14e-02	5.7	5.7	5.7	5.7	1.644e+04	1753.3	2343.5	-3929.7	-1026.5	-1248.7
303	ok	0.08	0.3	2.79e-03	5.7	5.7	5.7	5.7	6832.7	1112.2	-1712.2	-651.1	1046.5	-880.1
304	ok	0.08	0.2	2.96e-03	5.7	5.7	5.7	5.7	-458.7	-469.4	-692.3	414.6	1195.7	-238.1
305	ok	0.08	0.5	2.14e-02	5.7	5.7	5.7	5.7	-126.2	1.231e+04	-1352.1	-441.6	-1155.6	1104.6
306	ok	0.08	0.3	9.98e-03	5.7	5.7	5.7	5.7	723.0	-1244.3	-105.5	-58.2	413.3	274.4
307	ok	0.08	0.3	8.93e-03	5.7	5.7	5.7	5.7	-141.7	-5208.0	990.0	69.7	1295.8	41.2
308	ok	0.08	0.4	1.77e-02	5.7	5.7	5.7	5.7	-402.5	-4359.3	-3541.9	-389.0	825.6	1450.6
309	ok	0.08	0.4	8.65e-03	5.7	5.7	5.7	5.7	-1274.8	-2227.5	967.5	1705.2	1664.7	1303.9
310	ok	0.08	0.3	1.39e-02	5.7	5.7	5.7	5.7	-2529.3	-700.1	3957.9	1243.1	271.4	1650.3
311	ok	0.08	0.4	5.48e-03	5.7	5.7	5.7	5.7	-1317.2	-1661.1	938.6	2153.8	2335.4	994.0
312	ok	0.08	0.3	8.96e-03	5.7	5.7	5.7	5.7	-4186.7	-98.3	52.1	1338.5	359.5	1226.4
313	ok	0.08	0.4	3.38e-03	5.7	5.7	5.7	5.7	-684.2	-482.8	576.5	1818.2	2798.6	576.1
314	ok	0.08	0.2	5.23e-03	5.7	5.7	5.7	5.7	-1417.3	1015.5	-2096.3	863.4	814.1	562.5
315	ok	0.08	0.4	3.43e-03	5.7	5.7	5.7	5.7	-365.2	616.1	-265.6	1376.1	3095.7	102.1
316	ok	0.08	0.4	3.75e-03	5.7	5.7	5.7	5.7	1052.3	-3.1	-819.2	1268.8	3021.3	-250.3
317	ok	0.08	0.2	5.32e-03	5.7	5.7	5.7	5.7	-1871.7	1287.8	-729.1	835.2	964.7	-398.1

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy
318	ok	0.08	0.4	3.29e-03	5.7	5.7	5.7	5.7	2000.8	-262.1	-592.2	1061.7	2939.3	-405.2
319	ok	0.08	0.2	7.68e-03	5.7	5.7	5.7	5.7	1327.6	-179.0	-1956.3	511.7	653.1	-343.4
320	ok	0.08	0.4	2.47e-03	5.7	5.7	5.7	5.7	2915.3	554.3	-329.8	510.6	3011.8	-620.8
321	ok	0.08	0.3	4.26e-03	5.7	5.7	5.7	5.7	5950.8	141.2	-2014.5	-624.7	537.5	-517.2
322	ok	0.08	0.4	2.07e-03	5.7	5.7	5.7	5.7	3844.3	904.2	-495.6	162.3	2854.5	-799.2
323	ok	0.08	0.4	2.30e-03	5.7	5.7	5.7	5.7	4642.0	609.5	-477.8	30.4	2493.1	-936.5
324	ok	0.08	0.3	5.24e-03	5.7	5.7	5.7	5.7	7967.2	338.1	-1269.4	-922.5	589.6	-1093.9
325	ok	0.08	0.3	2.32e-03	5.7	5.7	5.7	5.7	6021.0	645.6	-877.6	-1517.0	1265.4	-554.9
326	ok	0.08	0.5	4.48e-03	5.7	5.7	5.7	5.7	9970.8	987.0	-4133.8	-2022.3	62.7	-704.4
327	ok	0.08	0.5	3.67e-03	5.7	5.7	5.7	5.7	6092.7	967.7	-1604.0	-2593.0	562.1	-852.0
328	ok	0.08	0.8	7.38e-03	5.7	5.7	5.7	5.7	1.418e+04	-2737.5	-5627.8	-3305.7	-450.7	-1107.9
329	ok	0.08	0.6	1.27e-02	5.7	5.7	5.7	5.7	6221.2	517.2	-3173.4	-3661.7	-255.4	-923.8
330	ok	0.08	0.6	1.09e-02	5.7	5.7	5.7	5.7	5474.4	-1240.0	-792.7	-2610.3	-85.9	1535.5
331	ok	0.08	0.7	1.54e-02	5.7	5.7	5.7	5.7	1.498e+04	2875.4	-4402.0	-1427.1	943.3	1582.0
332	ok	0.08	0.7	2.43e-02	5.7	5.7	5.7	5.7	6652.7	-1.174e+04	-3803.9	-3610.3	1223.4	1795.4
333	ok	0.08	0.4	1.74e-02	5.7	5.7	5.7	5.7	7629.1	-9414.1	1369.4	-1448.6	1639.0	1557.4
334	ok	0.08	1.0	1.80e-02	5.7	5.7	5.7	5.7	3.067e+04	-6340.1	7214.9	-3749.4	-1071.0	684.7
343	ok	0.08	0.3	1.84e-02	5.7	5.7	5.7	5.7	-4383.8	1145.5	859.7	1015.8	-641.0	1958.0
344	ok	0.08	0.2	1.23e-02	5.7	5.7	5.7	5.7	-5028.8	646.4	669.5	1011.9	-418.8	1462.5
345	ok	0.08	0.2	9.17e-03	5.7	5.7	5.7	5.7	-767.6	237.6	1630.6	481.6	-449.9	1022.7
346	ok	0.08	0.2	6.12e-03	5.7	5.7	5.7	5.7	-2728.9	1216.8	-1136.2	785.8	486.3	-454.3
347	ok	0.08	0.2	9.36e-03	5.7	5.7	5.7	5.7	-2501.3	631.2	83.3	543.1	-58.9	-377.6
348	ok	0.08	0.3	4.47e-03	5.7	5.7	5.7	5.7	7091.6	-1509.9	-2024.0	-1101.7	-1098.1	-381.2
349	ok	0.08	0.4	7.22e-03	5.7	5.7	5.7	5.7	1.036e+04	23.0	452.5	-1181.1	-389.3	-1235.3
350	ok	0.08	0.6	3.52e-03	5.7	5.7	5.7	5.7	1.028e+04	318.3	794.2	-2183.1	-348.7	-757.7
351	ok	0.08	1.0	8.58e-03	5.7	5.7	5.7	5.7	2.094e+04	-90.0	-7311.7	-3627.1	-606.2	-1071.0
352	ok	0.09	1.0	1.71e-02	5.7	5.7	5.7	5.7	2.563e+04	2908.7	-7645.9	-4002.5	-725.4	2430.4
356	ok	0.08	0.2	1.34e-02	5.7	5.7	5.7	5.7	-4149.4	171.9	109.9	956.3	-12.8	600.6
357	ok	0.08	0.2	9.52e-03	5.7	5.7	5.7	5.7	-4225.3	31.9	-78.6	1088.5	-14.3	514.4
358	ok	0.08	0.1	3.77e-03	5.7	5.7	5.7	5.7	548.7	-37.0	49.5	383.2	-41.3	427.3
359	ok	0.08	0.1	5.08e-03	5.7	5.7	5.7	5.7	-2956.0	-521.3	-533.1	757.6	53.0	-192.1
360	ok	0.08	0.2	3.07e-03	5.7	5.7	5.7	5.7	-1798.1	377.2	-346.5	633.3	133.9	-276.7
361	ok	0.08	0.3	1.06e-03	5.7	5.7	5.7	5.7	5865.9	82.1	64.6	-894.0	59.3	-261.9
362	ok	0.08	0.3	8.57e-04	5.7	5.7	5.7	5.7	9901.5	-30.6	-215.2	-1099.8	-7.0	-468.2
363	ok	0.08	0.6	1.58e-03	5.7	5.7	5.7	5.7	1.288e+04	825.5	88.5	-2186.3	-130.1	-154.3
364	ok	0.08	1.0	2.23e-03	5.7	5.7	5.7	5.7	2.008e+04	176.0	1402.9	-3746.0	-187.3	-533.0
365	ok	0.08	0.8	5.06e-03	5.7	5.7	5.7	5.7	2.065e+04	215.2	-243.1	-1350.4	-489.6	1116.0
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy
									-1.716e+04	-2.305e+04	-1.003e+04	-1.037e+04	-7444.93	-2631.22
		0.10	0.99	0.07	5.7	5.7	5.7	5.7	3.067e+04	2.529e+04	7214.94	6066.74	6158.37	2934.12

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		daN/cm2					daN/ m	daN/ m
1	ok	0.0						
2	ok	0.0						
3	ok	0.0						
4	ok	0.0						
5	ok	0.0						
6	ok	0.0						
7	ok	0.0						
8	ok	0.0						
9	ok	0.0						
10	ok	0.0						
11	ok	0.0						
12	ok	0.0						
13	ok	0.0						
14	ok	0.0						
15	ok	0.0						
16	ok	0.0						
17	ok	0.0						
18	ok	0.0						
19	ok	0.0						
20	ok	0.0						
21	ok	0.0						

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
22	ok	0.0						
23	ok	0.0						
24	ok	0.0						
25	ok	0.0						
26	ok	0.0						
27	ok	0.0						
28	ok	0.0						
29	ok	0.0						
30	ok	0.0						
31	ok	0.0						
32	ok	0.0						
33	ok	0.0						
34	ok	2.10						
35	ok	0.0						
36	ok	0.0						
37	ok	0.0						
38	ok	0.0						
39	ok	0.0						
40	ok	0.0						
41	ok	0.0						
42	ok	0.0						
43	ok	0.0						
44	ok	0.0						
45	ok	0.0						
46	ok	0.0						
47	ok	0.0						
48	ok	0.95						
49	ok	0.76						
50	ok	0.64						
51	ok	0.49						
52	ok	1.87						
53	ok	0.0						
58	ok	1.87						
63	ok	0.61						
64	ok	0.65						
65	ok	0.23						
66	ok	0.50						
67	ok	0.30						
68	ok	0.35						
69	ok	0.70						
70	ok	0.70						
71	ok	0.34						
72	ok	0.35						
73	ok	2.18						
74	ok	2.18						
75	ok	1.43						
76	ok	1.43						
77	ok	1.32						
78	ok	0.90						
79	ok	1.22						
80	ok	1.00						
81	ok	1.22						
82	ok	0.75						
83	ok	1.34						
84	ok	1.34						
85	ok	1.15						
86	ok	1.15						
87	ok	1.50						
88	ok	1.50						
89	ok	2.54						
90	ok	2.54						
91	ok	0.0						
92	ok	1.56						
93	ok	1.56						
94	ok	0.0						
95	ok	1.32						
96	ok	0.0						
97	ok	1.05						

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
98	ok	1.28						
99	ok	1.84						
100	ok	0.0						
101	ok	1.22						
102	ok	1.22						
103	ok	1.23						
104	ok	0.0						
105	ok	1.31						
106	ok	1.32						
107	ok	1.32						
108	ok	0.0						
109	ok	1.08						
110	ok	1.15						
111	ok	1.50						
112	ok	1.49						
113	ok	1.07						
114	ok	1.39						
115	ok	1.16						
116	ok	1.02						
117	ok	1.77						
118	ok	0.0						
119	ok	0.97						
120	ok	0.0						
121	ok	0.0						
122	ok	0.0						
123	ok	0.99						
124	ok	0.95						
125	ok	0.91						
126	ok	0.50						
127	ok	1.50						
128	ok	0.76						
129	ok	1.50						
130	ok	1.49						
131	ok	0.75						
132	ok	0.88						
133	ok	0.49						
134	ok	1.39						
135	ok	0.64						
136	ok	1.39						
137	ok	1.16						
138	ok	0.54						
139	ok	0.85						
140	ok	0.85						
141	ok	2.09						
142	ok	2.09						
143	ok	0.0						
144	ok	1.83						
145	ok	1.83						
146	ok	1.24						
147	ok	0.79						
148	ok	0.49						
149	ok	0.83						
150	ok	0.68						
151	ok	1.00						
152	ok	0.83						
153	ok	1.00						
154	ok	1.00						
155	ok	0.38						
156	ok	0.38						
157	ok	0.38						
158	ok	0.43						
159	ok	1.22						
160	ok	1.22						
161	ok	0.43						
162	ok	1.22						
163	ok	0.42						
164	ok	1.13						
165	ok	1.13						

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
166	ok	0.40						
167	ok	0.57						
168	ok	0.57						
169	ok	0.63						
170	ok	1.59						
171	ok	1.59						
172	ok	0.63						
173	ok	1.59						
174	ok	0.54						
175	ok	1.30						
176	ok	1.30						
177	ok	0.81						
178	ok	0.75						
179	ok	0.52						
180	ok	2.00						
181	ok	1.11						
182	ok	1.11						
183	ok	2.00						
184	ok	1.11						
185	ok	1.17						
186	ok	1.83						
187	ok	1.22						
188	ok	0.84						
189	ok	1.22						
190	ok	0.78						
191	ok	1.17						
192	ok	1.22						
193	ok	1.22						
194	ok	0.84						
195	ok	0.86						
196	ok	0.33						
197	ok	0.64						
198	ok	0.52						
199	ok	0.83						
200	ok	0.86						
201	ok	0.64						
202	ok	0.83						
203	ok	0.83						
204	ok	0.30						
205	ok	0.27						
206	ok	0.35						
207	ok	0.35						
208	ok	1.00						
209	ok	0.41						
210	ok	1.29						
211	ok	1.29						
212	ok	1.00						
213	ok	0.41						
214	ok	1.29						
215	ok	0.86						
216	ok	0.35						
217	ok	1.12						
218	ok	1.12						
219	ok	0.42						
220	ok	0.34						
221	ok	0.48						
222	ok	0.49						
223	ok	1.24						
224	ok	0.48						
225	ok	1.47						
226	ok	1.47						
227	ok	1.24						
228	ok	0.48						
229	ok	1.47						
230	ok	1.01						
231	ok	0.37						
232	ok	1.24						
233	ok	1.24						

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
234	ok	0.43						
235	ok	0.36						
236	ok	0.38						
237	ok	0.39						
238	ok	1.00						
239	ok	0.62						
240	ok	0.95						
241	ok	0.95						
242	ok	1.00						
243	ok	0.62						
244	ok	0.95						
245	ok	1.15						
246	ok	0.73						
247	ok	1.01						
248	ok	0.53						
249	ok	0.86						
250	ok	0.80						
251	ok	0.74						
252	ok	0.80						
253	ok	1.15						
254	ok	1.01						
255	ok	0.86						
256	ok	0.74						
257	ok	0.71						
258	ok	0.73						
259	ok	0.73						
260	ok	0.70						
261	ok	0.33						
262	ok	0.28						
263	ok	1.13						
264	ok	0.35						
265	ok	1.13						
266	ok	1.00						
267	ok	0.33						
268	ok	0.49						
269	ok	0.32						
270	ok	1.42						
271	ok	0.50						
272	ok	1.42						
273	ok	1.17						
274	ok	0.42						
275	ok	0.39						
276	ok	0.39						
277	ok	0.94						
278	ok	0.65						
279	ok	0.94						
280	ok	0.76						
281	ok	0.65						
282	ok	0.97						
283	ok	0.97						
284	ok	1.87						
285	ok	0.70						
286	ok	0.36						
287	ok	0.30						
288	ok	0.28						
289	ok	0.26						
290	ok	0.26						
291	ok	0.23						
292	ok	0.36						
293	ok	0.61						
294	ok	0.65						
295	ok	1.87						
302	ok	0.0						
303	ok	0.0						
304	ok	0.0						
305	ok	0.0						
306	ok	0.0						
307	ok	0.53						

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
308	ok	0.61						
309	ok	0.61						
310	ok	0.70						
311	ok	0.62						
312	ok	0.72						
313	ok	0.73						
314	ok	0.78						
315	ok	0.73						
316	ok	0.68						
317	ok	0.70						
318	ok	0.62						
319	ok	0.72						
320	ok	0.62						
321	ok	0.72						
322	ok	0.61						
323	ok	0.53						
324	ok	0.54						
325	ok	0.48						
326	ok	0.54						
327	ok	0.53						
328	ok	1.10						
329	ok	0.53						
330	ok	0.93						
331	ok	1.38						
332	ok	1.48						
333	ok	1.48						
334	ok	0.0						
343	ok	0.80						
344	ok	0.72						
345	ok	0.78						
346	ok	0.70						
347	ok	0.72						
348	ok	0.72						
349	ok	0.54						
350	ok	0.54						
351	ok	1.10						
352	ok	0.0						
356	ok	0.80						
357	ok	0.63						
358	ok	0.55						
359	ok	0.52						
360	ok	0.34						
361	ok	0.33						
362	ok	0.53						
363	ok	0.53						
364	ok	0.47						
365	ok	2.10						
Nodo		Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		2.54						

Nodo	Stato	V 6.50	V 6.53	Beta	f. a fon	f. Uout	Aw tot cm2	Asw,min cm2	n. x serie	n.ser 0(R)	n.ser 90	Rif. cmb
1	ok	0.0	0.03	0.0	0.0	0.0	0.0	0.0	0	0	0	1
2	ok	0.13	0.10	1.17	2.00	0.0	0.0	0.0	0	0	0	555
3	ok	0.11	0.08	1.15	2.00	0.0	0.0	0.0	0	0	0	545
4	ok	0.0	0.04	0.0	0.0	0.0	0.0	0.0	0	0	0	1
5	ok	0.0	9.97e-03	0.0	0.0	0.0	0.0	0.0	0	0	0	1
6	ok	0.0	0.02	0.0	0.0	0.0	0.0	0.0	0	0	0	1
7	ok	0.07	0.06	1.09	2.00	0.0	0.0	0.0	0	0	0	536
8	ok	9.80e-03	0.03	1.08	2.00	0.0	0.0	0.0	0	0	0	554
9	ok	0.25	0.16	1.02	2.00	0.0	0.0	0.0	0	0	0	484
10	ok	0.33	0.20	1.05	2.00	0.0	0.0	0.0	0	0	0	259
11	ok	0.03	0.04	1.03	2.00	0.0	0.0	0.0	0	0	0	548
12	ok	0.0	0.02	0.0	0.0	0.0	0.0	0.0	0	0	0	1
13	ok	0.30	0.18	1.11	2.00	0.0	0.0	0.0	0	0	0	484

Nodo	Stato	V 6.50	V 6.53	Beta	f. a fon	f. Uout	Aw tot	Asw,min	n. x serie	n.ser 0(R)	n.ser 90	Rif. cmb
14	ok	0.35	0.20	1.07	2.00	0.0	0.0	0.0	0	0	0	484
15	ok	7.09e-03	0.03	1.02	2.00	0.0	0.0	0.0	0	0	0	260
16	ok	0.0	0.02	0.0	0.0	0.0	0.0	0.0	0	0	0	1
17	ok	0.0	0.02	0.0	0.0	0.0	0.0	0.0	0	0	0	1
18	ok	0.0	0.01	0.0	0.0	0.0	0.0	0.0	0	0	0	1
19	ok	0.0	0.02	0.0	0.0	0.0	0.0	0.0	0	0	0	1
20	ok	0.10	0.06	1.17	2.00	0.0	0.0	0.0	0	0	0	541

Macro Guscio	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
2	25.00	1	2	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy
									daN/ m	daN/ m	daN/ m	daN	daN	daN
54	ok	0.13	4.95e-02	3.65e-03	5.7	5.7	5.7	5.7	-171.4	92.5	-1043.9	71.0	68.6	-58.1
55	ok	0.13	3.46e-02	3.65e-03	5.7	5.7	5.7	5.7	321.1	134.8	662.0	7.1	-39.7	52.6
56	ok	0.13	2.64e-02	1.96e-03	5.7	5.7	5.7	5.7	-532.2	0.5	3.3	109.5	10.1	-8.8
57	ok	0.13	2.48e-02	2.22e-03	5.7	5.7	5.7	5.7	-476.7	11.6	-123.0	88.7	52.9	41.2
59	ok	0.13	1.03e-02	2.93e-04	5.7	5.7	5.7	5.7	56.3	118.2	15.8	-20.0	-15.6	-3.0
60	ok	0.13	1.62e-02	2.61e-03	5.7	5.7	5.7	5.7	-38.9	-240.4	-139.1	-11.6	10.9	-43.7
61	ok	0.13	1.56e-02	2.80e-03	5.7	5.7	5.7	5.7	61.9	-146.0	171.1	5.6	-52.4	50.8
62	ok	0.13	2.35e-02	3.55e-04	5.7	5.7	5.7	5.7	-5.5	-105.9	-20.4	36.8	31.9	36.5
284	ok	0.13	0.5	4.61e-02	5.7	5.7	5.7	5.7	-6200.2	-9214.1	-6851.4	-1302.1	416.3	271.5
295	ok	0.13	0.5	3.69e-02	5.7	5.7	5.7	5.7	9393.6	-9564.2	-6135.3	-641.7	1100.0	389.2
296	ok	0.13	0.2	1.96e-02	5.7	5.7	5.7	5.7	1731.1	3236.9	4057.0	-72.5	-281.1	398.0
297	ok	0.13	0.5	1.67e-02	5.7	5.7	5.7	5.7	7468.9	2905.2	2001.4	306.5	-38.3	433.0
298	ok	0.13	9.31e-02	1.72e-02	5.7	5.7	5.7	5.7	-1951.4	228.9	922.5	300.2	-169.4	74.3
299	ok	0.13	0.1	1.61e-02	5.7	5.7	5.7	5.7	-1482.1	96.5	309.7	455.1	73.4	52.4
300	ok	0.13	7.79e-02	1.02e-02	5.7	5.7	5.7	5.7	-1982.6	-35.6	-484.0	284.9	-67.5	-27.3
301	ok	0.13	8.29e-02	8.61e-03	5.7	5.7	5.7	5.7	-2272.8	1.8	-94.3	358.5	-7.0	-44.6
333	ok	0.13	0.5	1.62e-02	5.7	5.7	5.7	5.7	8572.7	-4990.5	-2149.4	-1160.7	181.2	330.0
334	ok	0.14	0.8	1.28e-02	5.7	5.7	5.7	5.7	1.726e+04	-2067.7	6168.8	-1426.9	-373.3	236.0
335	ok	0.13	0.2	8.45e-03	5.7	5.7	5.7	5.7	1602.1	-611.4	82.8	362.6	711.2	74.6
336	ok	0.13	0.4	2.03e-02	5.7	5.7	5.7	5.7	7649.2	1002.1	5851.1	-446.3	-485.4	141.9
337	ok	0.13	0.1	8.80e-03	5.7	5.7	5.7	5.7	-1353.6	-961.3	68.4	477.0	409.3	-94.7
338	ok	0.13	8.30e-02	1.60e-02	5.7	5.7	5.7	5.7	-4462.2	68.2	-522.4	292.0	-202.3	-110.9
339	ok	0.13	7.19e-02	6.97e-03	5.7	5.7	5.7	5.7	-1514.8	-531.4	124.3	300.7	67.9	-69.0
340	ok	0.13	7.58e-02	1.05e-02	5.7	5.7	5.7	5.7	-2522.9	-27.6	447.7	305.6	-92.3	-88.9
341	ok	0.13	7.59e-02	1.23e-03	5.7	5.7	5.7	5.7	-329.3	847.9	15.7	-79.1	-335.7	-63.1
342	ok	0.13	8.95e-02	1.85e-05	5.7	5.7	5.7	5.7	44.4	1895.4	-7.3	9.6	-324.9	-31.3
352	ok	0.14	0.8	6.78e-03	5.7	5.7	5.7	5.7	1.948e+04	1288.8	-811.0	-1694.8	-330.3	230.6
353	ok	0.13	0.4	1.80e-02	5.7	5.7	5.7	5.7	4391.7	34.5	-529.6	-319.8	-51.3	188.0
354	ok	0.13	9.11e-02	1.95e-02	5.7	5.7	5.7	5.7	-4035.7	-120.7	310.4	266.8	31.2	-188.3
355	ok	0.13	9.06e-02	9.79e-03	5.7	5.7	5.7	5.7	-2441.1	31.4	-37.2	399.7	-7.2	-0.8
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy
									-6200.18	-9564.22	-6851.42	-1694.83	-485.41	-188.25
		0.14	0.78	0.05	5.7	5.7	5.7	5.7	1.948e+04	3236.95	6168.81	476.96	1100.00	433.01

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		daN/cm2					daN/ m	daN/ m
54	ok	0.20						
55	ok	0.22						
56	ok	0.08						
57	ok	0.15						
59	ok	0.07						
60	ok	0.20						
61	ok	0.22						
62	ok	0.09						
284	ok	1.27						
295	ok	1.27						
296	ok	1.27						
297	ok	1.27						
298	ok	0.39						

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
299	ok	0.39						
300	ok	0.18						
301	ok	0.18						
333	ok	0.73						
334	ok	0.0						
335	ok	0.73						
336	ok	0.92						
337	ok	0.35						
338	ok	0.43						
339	ok	0.20						
340	ok	0.32						
341	ok	0.22						
342	ok	0.22						
352	ok	0.0						
353	ok	0.92						
354	ok	0.43						
355	ok	0.32						
Nodo		Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		1.27						

Macro Guscio	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
13	25.00	1	1	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy
									daN/ m	daN/ m	daN/ m	daN	daN	daN
366	ok	0.14	0.5	9.94e-03	7.8	7.8	7.8	7.8	6270.4	2.768e+04	-1.496e+04	221.5	2596.9	-296.2
367	ok	0.12	0.4	6.18e-02	7.8	7.8	7.8	7.8	7239.0	-1307.1	-6915.1	505.5	2075.9	-209.9
368	ok	0.12	0.3	1.38e-02	7.8	7.8	7.8	7.8	7835.2	-4259.5	-1506.4	549.0	1834.3	-194.2
369	ok	0.12	0.3	3.67e-02	7.8	7.8	7.8	7.8	2512.0	-1549.2	4027.1	404.3	1677.7	-131.0
370	ok	0.12	0.4	3.62e-02	7.8	7.8	7.8	7.8	-3128.4	1.266e+04	-6734.7	169.8	1652.1	-189.4
371	ok	0.12	0.3	3.34e-02	7.8	7.8	7.8	7.8	-1108.0	-1463.9	-2650.2	357.5	1602.3	-52.5
372	ok	0.12	0.3	3.10e-02	7.8	7.8	7.8	7.8	-1178.2	-3109.1	2924.2	429.6	1638.3	47.4
373	ok	0.12	0.3	5.46e-02	7.8	7.8	7.8	7.8	-3711.9	-1137.5	5947.1	307.3	1631.8	138.3
374	ok	0.12	0.5	5.65e-02	7.8	7.8	7.8	7.8	-1.403e+04	1.822e+04	1.263e+04	-122.4	1655.3	272.5
375	ok	0.12	0.3	6.08e-02	7.8	7.8	7.8	7.8	-1.018e+04	-1.175e+04	218.8	336.1	1575.4	215.5
376	ok	0.12	0.4	8.08e-02	7.8	7.8	7.8	7.8	-4712.4	-3013.3	354.0	382.7	1766.8	270.9
377	ok	0.12	0.6	0.1	7.8	7.8	7.8	7.8	-4210.3	-690.5	2840.8	345.1	2056.1	298.5
378	ok	0.12	1.0	0.1	7.8	7.8	7.8	7.8	1150.3	1.764e+04	6671.4	299.0	3145.5	380.6
444	ok	0.12	0.3	3.36e-02	7.8	7.8	7.8	7.8	1.146e+04	-3879.6	-2893.2	393.1	519.9	286.7
445	ok	0.12	0.3	9.73e-03	7.8	7.8	7.8	7.8	1.110e+04	2564.2	2249.6	-388.6	-54.9	214.4
446	ok	0.12	0.4	4.14e-02	7.8	7.8	7.8	7.8	5471.7	-3770.4	4789.6	159.8	788.7	375.9
447	ok	0.12	0.2	1.07e-02	7.8	7.8	7.8	7.8	2873.6	1707.0	-2403.7	201.0	-56.7	202.5
449	ok	0.12	0.5	4.09e-02	7.8	7.8	7.8	7.8	779.8	5677.9	3651.6	176.2	934.4	93.6
450	ok	0.12	9.96e-02	1.40e-02	7.8	7.8	7.8	7.8	-4161.0	-3541.6	1802.9	314.9	26.3	12.0
531	ok	0.12	4.20e-02	7.10e-03	7.8	7.8	7.8	7.8	-1479.8	-1296.2	778.9	219.6	-8.2	100.5
532	ok	0.12	0.3	1.98e-02	7.8	7.8	7.8	7.8	1.178e+04	-1929.0	-8521.7	253.3	692.5	-301.1
533	ok	0.12	0.2	9.86e-03	7.8	7.8	7.8	7.8	986.4	6228.1	-4024.4	159.7	798.6	-94.5
534	ok	0.12	0.1	1.06e-03	7.8	7.8	7.8	7.8	7822.4	749.3	-1012.1	200.4	-11.0	-205.2
535	ok	0.12	0.2	3.78e-03	7.8	7.8	7.8	7.8	1.038e+04	-66.7	-2765.8	253.1	556.1	-256.8
536	ok	0.12	0.2	1.10e-03	7.8	7.8	7.8	7.8	1.084e+04	-438.5	322.9	178.4	18.4	-177.2
537	ok	0.12	0.2	9.63e-03	7.8	7.8	7.8	7.8	8959.8	-1958.5	15.0	124.4	456.9	-185.2
538	ok	0.12	0.3	7.79e-04	7.8	7.8	7.8	7.8	9811.0	-116.6	1341.3	-84.9	10.8	-112.4
539	ok	0.12	0.1	8.08e-03	7.8	7.8	7.8	7.8	3069.6	2960.2	-893.5	-92.8	458.4	-156.3
540	ok	0.12	0.2	2.66e-03	7.8	7.8	7.8	7.8	7693.3	413.3	371.8	-179.6	-33.4	-152.9
541	ok	0.12	0.2	9.31e-03	7.8	7.8	7.8	7.8	8574.9	-1147.4	-1120.1	52.7	419.7	-101.9
542	ok	0.12	0.3	9.37e-04	7.8	7.8	7.8	7.8	7407.3	531.6	-298.6	-129.7	13.8	-116.1
543	ok	0.12	0.2	1.40e-02	7.8	7.8	7.8	7.8	7939.7	-408.1	1500.7	106.2	422.2	91.1
544	ok	0.12	0.3	7.20e-04	7.8	7.8	7.8	7.8	1.003e+04	2.9	953.7	-125.3	-26.9	116.4
545	ok	0.12	0.2	2.73e-02	7.8	7.8	7.8	7.8	3498.8	-1427.0	5968.0	-62.9	422.4	241.7
546	ok	0.12	0.3	3.28e-03	7.8	7.8	7.8	7.8	1.092e+04	347.6	405.6	-194.4	2.1	175.2
547	ok	0.12	0.2	3.28e-02	7.8	7.8	7.8	7.8	-4569.0	4228.5	2926.2	-192.4	478.8	259.8
548	ok	0.12	0.2	1.17e-02	7.8	7.8	7.8	7.8	4041.8	-671.5	-52.2	-276.4	6.3	214.8

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy
549	ok	0.12	0.2	3.24e-02	7.8	7.8	7.8	7.8	-2136.4	-2219.8	-3479.4	-63.8	467.9	267.8
550	ok	0.12	0.3	4.81e-03	7.8	7.8	7.8	7.8	1993.0	1248.4	437.8	-369.1	-23.5	113.6
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy
									-1.403e+04	-1.175e+04	-1.496e+04	-388.62	-56.72	-301.15
		0.14	0.97	0.11	7.8	7.8	7.8	7.8	1.178e+04	2.768e+04	1.263e+04	549.00	3145.48	380.65

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		daN/cm2					daN/ m	daN/ m
366	ok	0.82						
367	ok	0.82						
368	ok	0.81						
369	ok	0.80						
370	ok	0.70						
371	ok	0.78						
372	ok	0.78						
373	ok	0.78						
374	ok	0.74						
375	ok	0.78						
376	ok	0.78						
377	ok	0.94						
378	ok	0.94						
444	ok	0.78						
445	ok	0.36						
446	ok	0.94						
447	ok	0.44						
449	ok	0.94						
450	ok	0.44						
531	ok	0.40						
532	ok	0.82						
533	ok	0.82						
534	ok	0.40						
535	ok	0.81						
536	ok	0.37						
537	ok	0.80						
538	ok	0.34						
539	ok	0.70						
540	ok	0.32						
541	ok	0.78						
542	ok	0.32						
543	ok	0.78						
544	ok	0.33						
545	ok	0.78						
546	ok	0.33						
547	ok	0.74						
548	ok	0.32						
549	ok	0.78						
550	ok	0.33						
Nodo		Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		0.94						

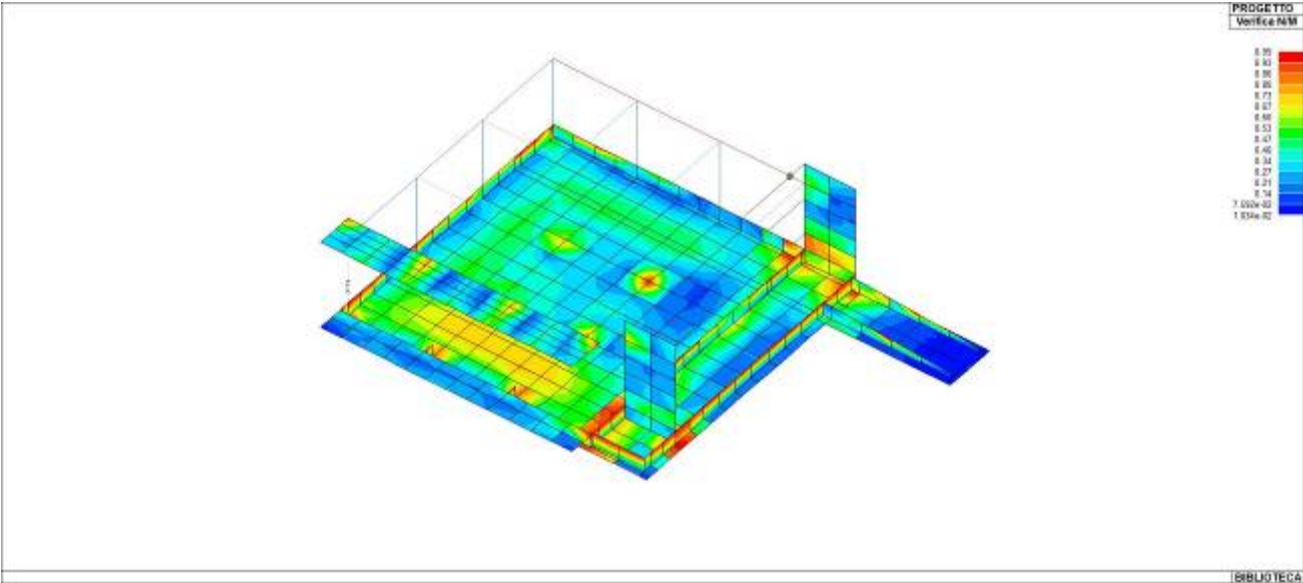
Macro Guscio	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
16	15.00	1	8	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy
									daN/ m	daN/ m	daN/ m	daN	daN	daN
484	ok	0.18	0.3	3.74e-03	5.2	5.2	5.2	5.2	45.9	-27.2	-180.7	754.2	57.3	-95.4
485	ok	0.18	0.3	2.98e-03	5.2	5.2	5.2	5.2	8.6	-28.4	157.7	831.6	66.1	101.5
486	ok	0.18	0.6	1.41e-02	5.2	5.2	5.2	5.2	1299.5	97.5	16.1	1219.9	94.0	55.3
487	ok	0.18	0.6	1.62e-02	5.2	5.2	5.2	5.2	5006.1	396.4	-128.3	1212.3	95.4	-39.4

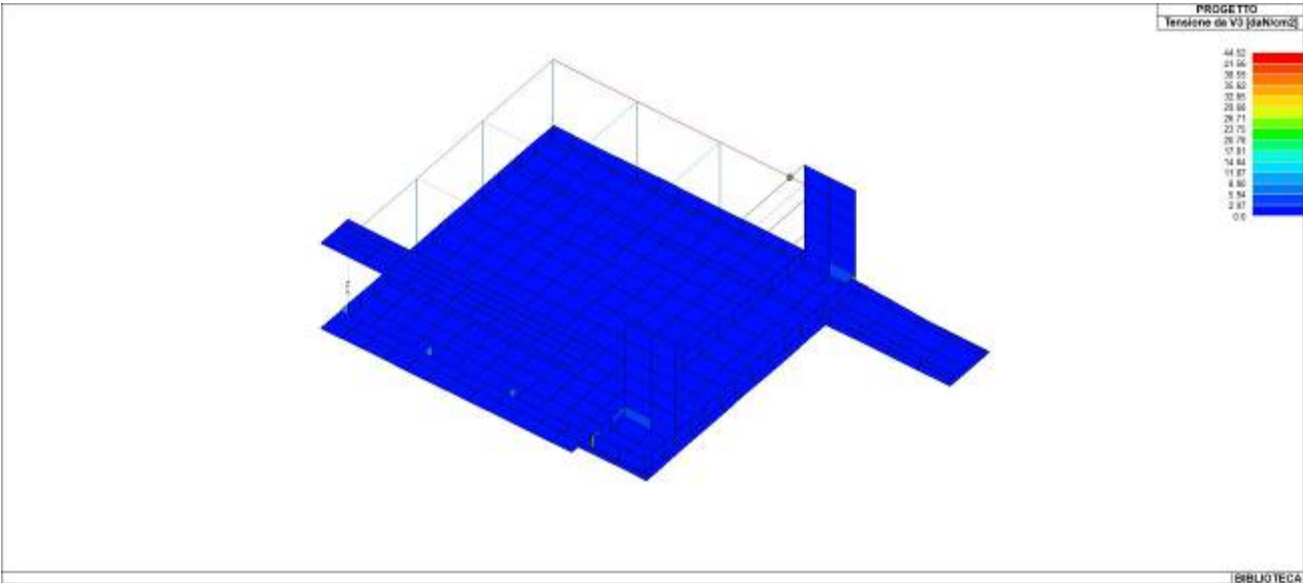
Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy
488	ok	0.18	0.2	8.82e-03	5.2	5.2	5.2	5.2	4360.7	57.2	-36.7	-297.4	19.7	-50.0
489	ok	0.18	0.7	2.40e-02	5.2	5.2	5.2	5.2	-1549.4	323.6	-201.2	1470.9	811.6	442.0
516	ok	0.18	0.9	4.73e-02	5.2	5.2	5.2	5.2	-8756.1	-538.1	1605.7	1911.0	777.1	-856.3
517	ok	0.18	0.8	4.22e-02	5.2	5.2	5.2	5.2	-8339.7	-399.4	-807.0	1761.5	1009.2	659.6
518	ok	0.18	0.8	4.18e-02	5.2	5.2	5.2	5.2	-6630.0	-299.6	603.6	1634.0	986.4	-625.4
519	ok	0.18	0.9	4.26e-02	5.2	5.2	5.2	5.2	-5396.7	-476.3	117.1	1766.0	783.0	827.5
553	ok	0.18	0.8	2.28e-02	5.2	5.2	5.2	5.2	-3051.1	-260.6	44.5	1928.5	1120.3	-29.8
554	ok	0.18	0.2	2.32e-02	5.2	5.2	5.2	5.2	-3400.8	-260.6	84.6	-450.4	6.6	90.3
555	ok	0.18	0.3	3.76e-02	5.2	5.2	5.2	5.2	-4913.2	-68.2	-369.7	-71.9	-503.9	224.6
556	ok	0.18	0.4	2.01e-02	5.2	5.2	5.2	5.2	-3688.8	164.5	444.1	-988.2	-28.3	166.9
557	ok	0.18	0.4	2.92e-02	5.2	5.2	5.2	5.2	-5782.4	-36.3	-11.6	-994.9	-30.0	93.1
558	ok	0.18	0.3	1.85e-02	5.2	5.2	5.2	5.2	-2396.6	153.3	866.7	-629.5	-18.5	198.3
559	ok	0.18	0.3	3.32e-02	5.2	5.2	5.2	5.2	-3838.4	347.4	-134.0	-578.1	-399.1	-135.0
560	ok	0.18	0.8	2.36e-02	5.2	5.2	5.2	5.2	-4284.8	-439.2	-124.6	2051.5	1144.0	51.9
561	ok	0.18	0.2	2.18e-02	5.2	5.2	5.2	5.2	-2446.8	-9.9	-93.3	-423.5	-13.5	-134.6
562	ok	0.18	0.2	3.70e-02	5.2	5.2	5.2	5.2	-3828.7	-94.4	-57.4	87.6	-481.7	84.0
563	ok	0.18	0.3	2.22e-02	5.2	5.2	5.2	5.2	-4383.3	92.5	29.5	-820.7	-19.1	49.9
564	ok	0.18	0.3	3.64e-02	5.2	5.2	5.2	5.2	-7026.0	203.9	164.4	-774.2	-26.3	39.8
565	ok	0.18	0.3	2.23e-02	5.2	5.2	5.2	5.2	-770.5	8.4	-546.2	-570.4	-20.4	126.7
566	ok	0.18	0.2	3.73e-02	5.2	5.2	5.2	5.2	-6395.4	-53.3	239.1	63.1	-467.1	-51.7
567	ok	0.18	0.6	1.12e-02	5.2	5.2	5.2	5.2	-1414.8	21.7	361.8	1251.5	801.9	-449.5
568	ok	0.18	0.3	2.18e-02	5.2	5.2	5.2	5.2	-3316.0	-205.8	-56.4	-580.5	50.1	-140.8
569	ok	0.18	0.3	3.03e-02	5.2	5.2	5.2	5.2	-4432.8	64.1	-728.1	-748.7	-399.0	191.6
570	ok	0.18	0.4	2.15e-02	5.2	5.2	5.2	5.2	-3779.4	100.4	-242.3	-1010.8	-29.4	-142.4
571	ok	0.18	0.4	3.30e-02	5.2	5.2	5.2	5.2	-5836.0	88.3	-192.9	-1038.7	-34.0	-64.3
572	ok	0.18	0.2	2.40e-02	5.2	5.2	5.2	5.2	-977.3	-106.9	-687.5	-568.4	-15.9	21.5
573	ok	0.18	0.2	3.90e-02	5.2	5.2	5.2	5.2	-7098.1	-76.0	610.1	-26.7	-515.6	-227.1
574	ok	0.18	0.7	9.77e-03	5.2	5.2	5.2	5.2	-1186.2	-131.5	-31.4	1639.5	605.2	67.7
575	ok	0.18	0.2	1.03e-02	5.2	5.2	5.2	5.2	-1213.8	-200.4	284.3	-336.8	141.5	191.5
576	ok	0.18	0.6	1.13e-02	5.2	5.2	5.2	5.2	349.9	34.8	-104.2	1361.2	322.1	49.2
577	ok	0.18	0.2	9.38e-03	5.2	5.2	5.2	5.2	958.2	-77.5	253.7	-309.1	50.3	136.3
578	ok	0.18	0.3	1.26e-02	5.2	5.2	5.2	5.2	4202.1	56.8	39.9	-324.0	18.5	67.0
579	ok	0.18	0.4	9.45e-03	5.2	5.2	5.2	5.2	-1505.5	-0.9	586.9	-960.3	-53.8	146.0
580	ok	0.18	0.4	7.00e-03	5.2	5.2	5.2	5.2	799.0	19.1	549.5	-974.2	-36.1	155.0
581	ok	0.18	0.4	9.35e-03	5.2	5.2	5.2	5.2	3707.4	2.7	34.8	-992.2	16.5	135.3
582	ok	0.18	0.2	9.20e-03	5.2	5.2	5.2	5.2	-1318.4	-133.7	534.4	-558.0	46.3	148.6
583	ok	0.18	0.3	4.82e-03	5.2	5.2	5.2	5.2	308.6	-59.5	594.7	-558.2	7.9	172.0
584	ok	0.18	0.3	4.24e-03	5.2	5.2	5.2	5.2	2255.9	19.5	56.1	-552.0	-13.0	241.7
585	ok	0.18	0.4	4.87e-03	5.2	5.2	5.2	5.2	-408.5	300.2	417.4	938.4	424.6	290.5
586	ok	0.18	0.3	3.55e-03	5.2	5.2	5.2	5.2	84.0	146.6	607.9	707.6	220.5	206.3
587	ok	0.18	0.7	8.60e-03	5.2	5.2	5.2	5.2	-1364.0	-155.1	95.2	1748.5	621.8	-37.8
588	ok	0.18	0.2	9.95e-03	5.2	5.2	5.2	5.2	-1230.4	-2.2	-35.1	-281.3	153.0	75.6
589	ok	0.18	0.6	8.58e-03	5.2	5.2	5.2	5.2	882.7	81.3	173.8	1458.9	337.1	-28.2
590	ok	0.18	0.2	9.43e-03	5.2	5.2	5.2	5.2	2372.0	230.5	861.6	-251.8	62.5	71.2
591	ok	0.18	0.3	1.55e-02	5.2	5.2	5.2	5.2	6996.7	309.2	979.4	-246.7	33.1	44.3
592	ok	0.18	0.3	8.89e-03	5.2	5.2	5.2	5.2	-1368.7	12.0	9.8	-795.0	-36.4	26.0
593	ok	0.18	0.4	1.07e-02	5.2	5.2	5.2	5.2	1640.1	1.0	-17.0	-795.7	-29.5	31.4
594	ok	0.18	0.5	1.62e-02	5.2	5.2	5.2	5.2	5502.9	-25.7	15.5	-802.7	19.4	34.4
595	ok	0.18	0.2	9.97e-03	5.2	5.2	5.2	5.2	-345.6	-87.6	-49.6	-427.4	82.2	-68.4
596	ok	0.18	0.2	1.10e-02	5.2	5.2	5.2	5.2	861.0	-35.8	-79.1	-337.1	26.0	-81.8
597	ok	0.18	0.3	1.66e-02	5.2	5.2	5.2	5.2	5510.8	59.0	-27.7	-257.4	25.0	38.3
598	ok	0.18	0.4	3.87e-03	5.2	5.2	5.2	5.2	-20.1	316.9	-672.0	841.0	397.3	-265.9
599	ok	0.18	0.3	8.79e-03	5.2	5.2	5.2	5.2	-1223.9	-325.3	-429.2	-634.1	30.4	-115.4
600	ok	0.18	0.3	4.35e-03	5.2	5.2	5.2	5.2	179.5	198.7	-898.8	631.5	204.9	-187.3
601	ok	0.18	0.3	5.35e-03	5.2	5.2	5.2	5.2	366.7	-142.3	-508.0	-608.6	-7.98e-02	-148.4
602	ok	0.18	0.4	4.31e-03	5.2	5.2	5.2	5.2	2406.4	39.8	-56.1	-596.3	-8.0	-217.3
603	ok	0.18	0.4	9.07e-03	5.2	5.2	5.2	5.2	-1569.2	13.7	-365.9	-978.0	-56.5	-120.4
604	ok	0.18	0.4	6.24e-03	5.2	5.2	5.2	5.2	656.6	14.0	-339.8	-991.5	-37.3	-127.0
605	ok	0.18	0.5	8.14e-03	5.2	5.2	5.2	5.2	3673.8	2.5	-14.0	-1009.8	17.1	-110.4
606	ok	0.18	0.2	1.07e-02	5.2	5.2	5.2	5.2	-1590.7	-160.7	-157.0	-338.7	143.0	-172.7
607	ok	0.18	0.2	7.19e-03	5.2	5.2	5.2	5.2	556.5	-74.3	-605.0	-323.0	31.4	-156.6
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy
									-8756.10	-538.06	-898.77	-1038.70	-515.63	-856.28
		0.18	0.90	0.05	5.2	5.2	5.2	5.2	6996.65	396.36	1605.70	2051.45	1144.04	827.48

Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		daN/cm2					daN/ m	daN/ m
484	ok	0.55						
485	ok	0.59						
486	ok	1.04						
487	ok	1.02						
488	ok	1.04						
489	ok	0.0						
516	ok	0.0						
517	ok	0.0						
518	ok	0.0						
519	ok	0.0						
553	ok	0.0						
554	ok	2.81						
555	ok	2.81						
556	ok	0.55						
557	ok	0.55						
558	ok	2.36						
559	ok	2.36						
560	ok	0.0						
561	ok	2.81						
562	ok	2.81						
563	ok	0.62						
564	ok	0.62						
565	ok	2.77						
566	ok	2.77						
567	ok	0.0						
568	ok	2.22						
569	ok	2.22						
570	ok	0.57						
571	ok	0.57						
572	ok	2.88						
573	ok	2.88						
574	ok	1.66						
575	ok	1.66						
576	ok	1.22						
577	ok	1.22						
578	ok	1.02						
579	ok	0.45						
580	ok	0.51						
581	ok	0.51						
582	ok	1.34						
583	ok	0.87						
584	ok	0.59						
585	ok	1.34						
586	ok	0.87						
587	ok	1.71						
588	ok	1.63						
589	ok	1.25						
590	ok	1.18						
591	ok	0.97						
592	ok	0.40						
593	ok	0.39						
594	ok	0.39						
595	ok	1.60						
596	ok	1.15						
597	ok	0.93						
598	ok	1.25						
599	ok	1.25						
600	ok	0.84						
601	ok	0.84						
602	ok	0.55						
603	ok	0.49						
604	ok	0.51						
605	ok	0.51						
606	ok	1.71						
607	ok	1.25						
Nodo		Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec

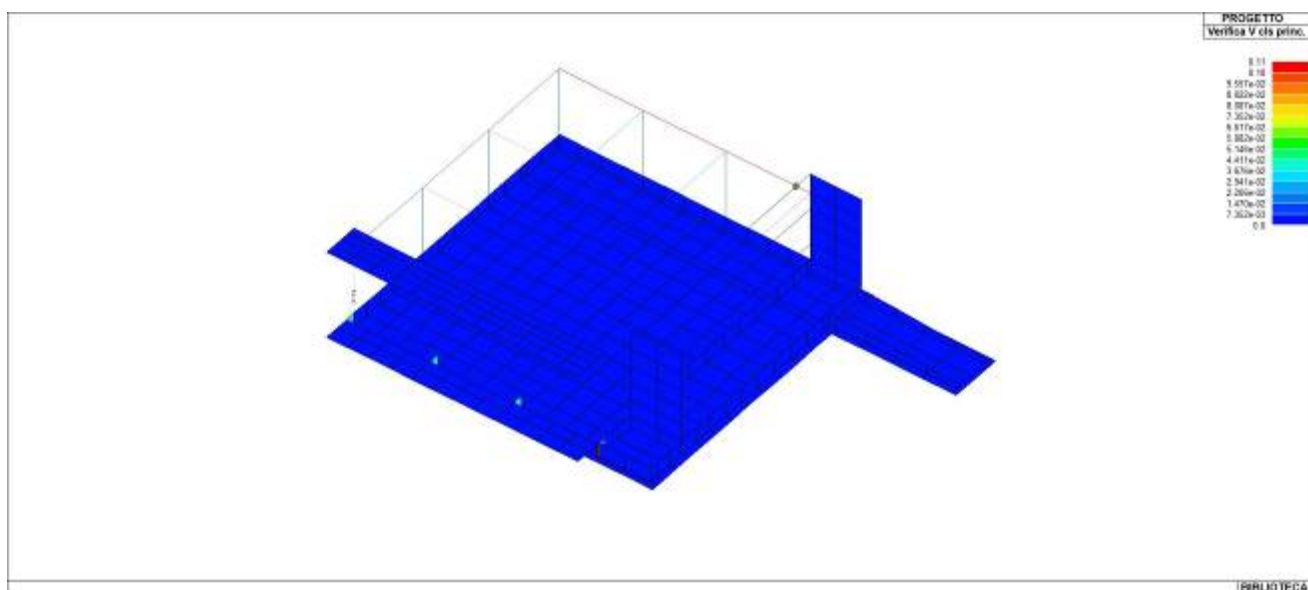
Nodo	Stato	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
		2.88						



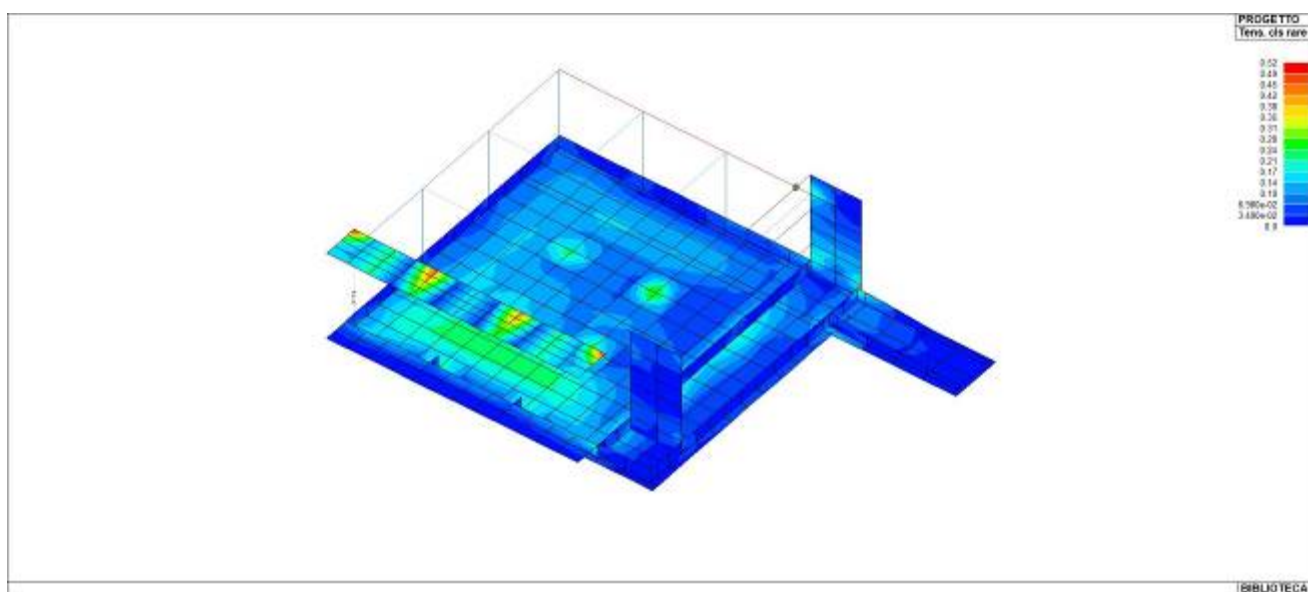
72_CA_D3_02_Verifica NM



72_CA_D3_05_Tensione da V3



72_CA_D3_06_Verifica V cls princ



72_CA_D3_21_Tens cls rare

STATI LIMITE D' ESERCIZIO

LEGENDA TABELLA STATI LIMITE D' ESERCIZIO

In tabella vengono riportati i valori di interesse per il controllo degli stati limite d'esercizio.

In particolare vengono riportati, in relazione al tipo di elemento strutturale, i risultati relativi alle tre categorie di combinazione considerate:

- Combinazioni rare
- Combinazioni frequenti
- Combinazioni quasi permanenti.

I valori di interesse sono i seguenti:

rRfck	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni rare [normalizzato a 1]
rRfyk	rapporto tra la massima tensione nell'acciaio e la tensione fyk in combinazioni rare [normalizzato a 1]
rPfck	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni quasi permanenti [normalizzato a 1]
wR	apertura caratteristica delle fessure in combinazioni rare [mm]
wF	apertura caratteristica delle fessure in combinazioni frequenti [mm]
wP	apertura caratteristica delle fessure in combinazioni quasi permanenti [mm]
dR	massima deformazione in combinazioni rare
dF	massima deformazione in combinazioni frequenti
dP	massima deformazione in combinazioni quasi permanenti

Per ognuno dei nove valori soprariportati viene indicata (Rif.cmb) la combinazione in cui si è verificato.

In relazione al tipo di elemento strutturale i valori sono selezionati nel modo seguente:

pilastrati	rRfck	rRfyk	rPfck	per sezioni significative
travi	rRfck wR dR	rRfyk wF dF	rPfck wP dP	per sezioni significative per sezioni significative massimi in campata
setti e gusci	rRfck wR	rRfyk wF	rPfck wP	massimi nei nodi dell'elemento massimi nei nodi dell'elemento

Si precisa che i valori di massima deformazione per travi sono riferiti al piano verticale (piano locale 1-2 con momenti flettenti 3-3).

Pilas.	Pos.	rRfck	rRfyk	rPfck	Rif. cmb	Pos.	rRfck	rRfyk	rPfck	Rif. cmb
	cm					cm				
1	0.0	0.13	0.08	0.10	800,800,924	204.5	0.09	0.06	0.08	795,795,919
	409.0	0.09	0.05	0.07	727,727,923					
2	0.0	0.26	0.16	0.29	844,844,920	204.5	0.11	0.07	0.13	852,852,920
	409.0	0.10	0.06	0.11	848,856,924					
3	0.0	0.39	0.33	0.45	852,844,920	204.5	0.14	0.08	0.16	844,852,920
	409.0	0.28	0.21	0.32	856,848,924					
4	0.0	0.36	0.31	0.43	848,844,924	204.5	0.24	0.26	0.28	836,852,920
	409.0	0.29	0.25	0.30	781,781,921					
5	0.0	0.32	0.20	0.35	788,788,920	204.5	0.15	0.10	0.16	779,779,919
	409.0	0.12	0.08	0.14	725,725,924					
6	0.0	0.16	0.10	0.17	840,840,924	204.5	0.12	0.08	0.13	779,779,919
	409.0	0.14	0.09	0.13	781,781,921					
7	0.0	0.27	0.16	0.31	840,840,924	204.5	0.16	0.10	0.17	836,836,920
	409.0	0.42	0.22	0.48	840,840,924					
8	0.0	0.27	0.20	0.31	848,736,924	204.5	0.34	0.23	0.38	728,728,924
	409.0	0.62	0.57	0.63	781,781,921					
9	0.0	0.30	0.19	0.34	788,787,920	204.5	0.14	0.09	0.15	779,779,919
	409.0	0.12	0.07	0.13	792,792,924					
10	0.0	0.23	0.14	0.27	840,840,924	204.5	0.14	0.10	0.17	724,724,920
	409.0	0.28	0.16	0.34	856,840,924					
11	0.0	0.26	0.16	0.31	836,836,920	204.5	0.14	0.10	0.16	724,724,920
	409.0	0.31	0.18	0.35	836,836,920					
12	0.0	0.25	0.16	0.26	781,741,920	204.5	0.31	0.21	0.35	728,724,924
	409.0	0.62	0.57	0.63	781,781,921					
13	0.0	0.15	0.13	0.15	788,787,920	204.5	0.05	0.03	0.05	795,795,919
	409.0	0.11	0.08	0.11	788,788,920					
14	0.0	0.10	0.06	0.09	793,793,917	51.1	0.08	0.05	0.08	793,793,917
	102.2	0.06	0.04	0.06	793,793,917					

Pilas.	Pos.	rRfck	rRfyk	rPfck	Rif. cmb	Pos.	rRfck	rRfyk	rPfck	Rif. cmb
15	0.0	0.22	0.13	0.25	852,836,920	204.5	0.12	0.08	0.13	781,781,921
	409.0	0.27	0.15	0.31	852,836,920					
16	0.0	0.26	0.16	0.29	852,836,920	204.5	0.13	0.09	0.15	840,840,924
	409.0	0.24	0.14	0.26	836,836,920					
17	0.0	0.22	0.17	0.26	844,844,920	51.1	0.15	0.11	0.18	844,844,920
	102.2	0.09	0.05	0.11	844,844,920					
18	0.0	0.05	0.03	0.04	797,797,923	204.5	0.02	0.01	0.02	797,797,924
	409.0	0.02	8.56e-03	0.01	852,852,920					
19	0.0	0.07	0.04	0.07	797,797,921	51.1	0.05	0.02	0.05	797,793,921
	102.2	0.03	0.02	0.03	797,797,921					
20	0.0	0.19	0.09	0.23	844,852,920	51.1	0.13	0.07	0.16	844,852,920
	102.2	0.09	0.05	0.11	844,852,920					
21	0.0	0.17	0.15	0.21	676,674,920	58.5	0.13	0.13	0.16	734,734,922
	117.0	0.23	0.21	0.29	800,800,924					
22	0.0	0.45	0.54	0.56	724,724,920	58.5	0.41	0.52	0.51	724,724,920
	117.0	0.44	0.54	0.56	842,850,918					
23	0.0	0.42	0.52	0.50	672,780,924	58.5	0.40	0.52	0.49	784,780,924
	117.0	0.43	0.53	0.54	726,726,922					
24	0.0	0.18	0.15	0.21	796,787,920	58.5	0.10	0.11	0.12	788,788,920
	117.0	0.22	0.19	0.26	796,788,920					
25	0.0	0.15	0.11	0.16	836,844,920	58.5	0.06	0.03	0.06	836,836,920
	117.0	0.07	0.04	0.05	836,836,920					
34	0.0	0.23	0.25	0.24	669,669,921	58.5	0.11	0.12	0.12	669,669,921
	117.0	6.91e-03	0.01	7.07e-03	836,724,920					
35	0.0	0.01	0.01	0.02	668,844,920	58.5	6.17e-03	4.87e-03	7.77e-03	668,732,920
	117.0	1.43e-03	2.74e-03	1.57e-03	836,732,920					
36	0.0	0.02	8.56e-03	0.01	852,852,920	58.5	0.02	0.01	0.01	852,852,920
	117.0	0.02	0.01	0.01	789,789,921					
44	0.0	0.34	0.36	0.41	856,848,924	58.5	0.15	0.14	0.19	856,848,924
	117.0	0.04	0.03	0.03	836,836,920					
45	0.0	0.02	0.05	0.03	732,723,920	58.5	0.01	0.03	0.01	732,724,920
	117.0	0.0	0.02	0.0	0,836,0					
46	0.0	0.02	0.04	0.03	736,728,924	58.5	0.01	0.03	0.01	736,728,924
	117.0	0.0	0.01	0.0	0,836,0					
49	0.0	0.02	0.01	0.02	793,793,917	58.5	0.05	0.05	0.06	781,797,921
	117.0	0.09	0.10	0.09	781,797,921					
50	0.0	0.05	0.06	0.06	726,854,922	58.5	0.05	0.06	0.05	795,795,919
	117.0	0.08	0.10	0.08	795,795,919					
60	0.0	0.05	0.03	0.05	793,793,917	51.1	0.04	0.02	0.04	793,793,917
	102.2	0.03	0.02	0.03	793,777,917					
61	0.0	0.10	0.09	0.11	844,844,920	51.1	0.08	0.07	0.09	852,844,920
	102.2	0.06	0.05	0.07	836,676,920					
62	0.0	0.03	0.02	0.03	797,793,921	51.1	0.02	0.01	0.02	797,793,921
	102.2	0.01	6.10e-03	9.94e-03	797,797,921					
63	0.0	0.08	0.05	0.10	844,844,920	51.1	0.07	0.04	0.08	844,844,920
	102.2	0.06	0.03	0.07	852,844,920					
82	0.0	0.02	0.02	0.03	793,777,917	51.1	0.02	0.01	0.02	723,723,919
	102.2	0.02	0.02	0.02	786,786,918					
83	0.0	0.07	0.06	0.08	852,844,920	51.1	0.05	0.05	0.06	836,686,920
	102.2	0.05	0.05	0.05	781,781,921					
84	0.0	0.01	6.63e-03	0.01	797,797,921	51.1	4.80e-03	3.18e-03	4.64e-03	687,687,924
	102.2	9.60e-03	0.01	0.01	778,730,918					
85	0.0	0.06	0.04	0.07	852,844,920	51.1	0.05	0.03	0.06	852,732,920
	102.2	0.04	0.02	0.04	836,740,920					
100	0.0	0.02	0.02	0.02	786,794,918	51.1	0.04	0.02	0.03	786,786,917
	102.2	0.05	0.03	0.04	785,785,917					
101	0.0	0.06	0.04	0.06	781,781,921	51.1	0.11	0.10	0.10	781,781,921
	102.2	0.17	0.16	0.15	781,781,921					
102	0.0	7.71e-03	4.00e-03	8.98e-03	738,778,918	51.1	0.01	0.01	0.02	793,785,917
	102.2	0.02	0.02	0.03	797,793,921					
103	0.0	0.03	0.03	0.04	836,852,920	51.1	0.03	0.02	0.03	836,724,920
	102.2	0.02	0.01	0.02	778,722,918					
105	0.0	0.06	0.07	0.07	836,844,920	40.0	0.04	0.05	0.05	836,844,920
	80.0	0.02	0.04	0.03	724,844,924					
106	0.0	0.02	0.01	0.03	684,684,920	40.0	0.02	0.01	0.03	681,665,917
	80.0	0.03	0.02	0.04	681,681,917					
107	0.0	0.04	0.02	0.04	684,684,920	40.0	0.04	0.02	0.05	684,684,920
	80.0	0.05	0.02	0.06	684,684,920					

Pilas.	Pos.	rRfck	rRfyk	rPfck	Rif. cmb	Pos.	rRfck	rRfyk	rPfck	Rif. cmb
108	0.0	0.04	0.02	0.04	684,684,920	40.0	0.03	0.02	0.03	684,684,920
	80.0	0.04	0.02	0.03	743,743,923					
109	0.0	0.03	0.02	0.02	781,781,921	40.0	0.04	0.02	0.03	844,844,920
	80.0	0.06	0.03	0.06	844,844,920					
110	0.0	0.39	0.21	0.45	856,840,924	40.0	0.32	0.18	0.38	840,840,924
	80.0	0.27	0.16	0.31	840,840,924					
111	0.0	0.17	0.11	0.19	840,840,924	40.0	0.17	0.10	0.18	840,840,924
	80.0	0.16	0.10	0.17	840,840,924					
112	0.0	0.10	0.07	0.13	794,794,918	40.0	0.08	0.05	0.10	742,798,922
	80.0	0.07	0.04	0.08	744,744,924					
113	0.0	0.04	0.03	0.03	781,781,921	40.0	0.04	0.03	0.02	781,781,920
	80.0	0.04	0.04	0.04	781,781,920					
114	0.0	0.34	0.19	0.39	836,836,920	40.0	0.30	0.17	0.35	836,836,920
	80.0	0.26	0.16	0.31	836,836,920					
115	0.0	0.28	0.17	0.34	840,840,924	40.0	0.25	0.15	0.30	840,840,924
	80.0	0.23	0.14	0.27	840,840,924					
116	0.0	0.11	0.07	0.13	794,794,918	40.0	0.08	0.05	0.09	778,778,918
	80.0	0.06	0.04	0.07	742,726,922					
117	0.0	0.03	0.02	0.03	777,684,917	40.0	0.11	0.11	0.13	844,844,920
	80.0	0.20	0.20	0.23	844,844,920					
118	0.0	0.03	0.02	0.03	740,724,920	40.0	0.03	0.02	0.04	724,724,920
	80.0	0.04	0.02	0.04	724,724,920					
119	0.0	0.04	0.02	0.04	740,724,920	40.0	0.04	0.03	0.05	724,724,920
	80.0	0.05	0.03	0.06	724,724,920					
120	0.0	0.11	0.06	0.13	724,724,920	40.0	0.09	0.05	0.10	793,793,917
	80.0	0.09	0.06	0.08	785,785,917					
121	0.0	0.03	0.02	0.03	740,724,920	40.0	0.02	0.01	0.02	741,741,921
	80.0	0.03	0.02	0.02	676,676,920					
122	0.0	0.02	9.65e-03	0.02	781,781,921	40.0	9.68e-03	5.92e-03	0.01	781,781,921
	80.0	6.50e-03	4.18e-03	7.44e-03	856,856,924					
123	0.0	0.02	0.01	0.03	672,672,924	40.0	0.05	0.03	0.05	797,797,921
	80.0	0.08	0.07	0.08	797,797,921					
124	0.0	0.07	0.04	0.09	669,669,921	40.0	0.13	0.07	0.16	852,844,920
	80.0	0.20	0.15	0.24	844,844,920					
Pilas.		rRfck	rRfyk	rPfck			rRfck	rRfyk	rPfck	
		0.62	0.57	0.63						

Trave	Pos.	rRfck	rRfyk	rPfck	Rif. cmb	wR	wF	wP	Rif. cmb	dR	dF	dP	Rif. cmb
	cm					mm	mm	mm		cm	cm	cm	
26	0.0	0.38	0.46	0.41	838,838,922	0.10	0.09	0.09	838,870,922	0.77	0.81	0.80	844,878,920
	268.5	0.33	0.40	0.36	779,724,919	0.08	0.08	0.07	724,868,920				
	537.0	0.45	0.54	0.46	779,779,919	0.12	0.11	0.10	779,867,919				
27	0.0	0.59	0.67	0.63	838,838,922	0.17	0.15	0.14	838,870,922	1.06	1.09	1.07	844,878,920
	268.5	0.45	0.51	0.48	779,779,919	0.12	0.11	0.10	723,867,919				
	537.0	0.69	0.68	0.74	779,779,919	0.16	0.14	0.13	779,867,919				
28	0.0	0.57	0.64	0.60	838,838,922	0.16	0.14	0.13	838,870,922	0.89	0.91	0.90	844,878,920
	268.5	0.43	0.49	0.45	779,723,919	0.11	0.10	0.10	667,867,919				
	537.0	0.75	0.74	0.82	779,779,919	0.18	0.16	0.15	779,867,919				
29	0.0	0.06	0.10	0.06	795,795,919	0.0	0.0	0.0	0,0,0	0.19	0.18	0.17	844,878,920
	99.2	0.04	0.07	0.04	726,779,922	0.0	0.0	0.0	0,0,0				
	198.5	0.10	0.15	0.10	795,795,919	0.0	0.0	0.0	0,0,0				
30	0.0	0.19	0.23	0.22	744,744,924	0.0	0.0	0.0	0,0,0	0.13	0.12	0.12	793,901,917
	246.7	0.07	0.08	0.09	728,742,924	0.0	0.0	0.0	0,0,0				
	493.5	0.06	0.07	0.05	744,744,924	0.0	0.0	0.0	0,0,0				
31	0.0	0.10	0.14	0.10	744,744,924	0.0	0.0	0.0	0,0,0	0.24	0.24	0.24	785,901,917
	246.8	0.07	0.10	0.09	681,738,917	0.0	0.0	0.0	0,0,0				
	493.5	0.12	0.16	0.15	673,673,917	0.0	0.0	0.0	0,0,0				
32	0.0	0.05	0.08	0.04	741,741,921	0.0	0.0	0.0	0,0,0	0.30	0.29	0.29	732,878,920
	246.8	0.07	0.10	0.09	684,793,920	0.0	0.0	0.0	0,0,0				
	493.5	0.16	0.22	0.20	676,676,920	0.0	0.0	0.0	0,0,0				
33	0.0	0.13	0.25	0.15	743,727,923	0.0	0.0	0.0	0,0,0	0.12	0.11	0.11	849,909,917
	246.8	0.08	0.17	0.11	673,850,917	0.0	0.0	0.0	0,0,0				
	493.5	0.16	0.30	0.20	674,674,918	0.0	0.0	0.0	0,0,0				
37	0.0	0.03	0.03	0.02	797,797,921	0.0	0.0	0.0	0,0,0	0.25	0.24	0.23	844,912,920
	123.5	0.08	0.10	0.08	836,835,920	0.0	0.0	0.0	0,0,0				

Trave	Pos.	rRfck	rRfyk	rPfck	Rif. cmb	wR	wF	wP	Rif. cmb	dR	dF	dP	Rif. cmb
	247.0	0.11	0.14	0.11	797,797,921	0.0	0.0	0.0	0,0,0				
38	0.0	4.32e-04	8.97e-04	5.29e-04	796,680,920	0.0	0.0	0.0	0,0,0	0.14	0.13	0.12	844,882,920
	32.2	0.02	0.02	0.02	846,846,922	0.0	0.0	0.0	0,0,0				
	64.5	0.03	0.05	0.04	846,846,922	0.0	0.0	0.0	0,0,0				
39	0.0	2.98e-04	7.37e-04	3.05e-04	784,792,924	0.0	0.0	0.0	0,0,0	0.16	0.14	0.14	848,884,924
	32.2	0.01	0.02	0.02	786,786,918	0.0	0.0	0.0	0,0,0				
	64.5	0.03	0.05	0.04	790,790,922	0.0	0.0	0.0	0,0,0				
40	0.0	6.26e-03	8.32e-03	7.91e-03	842,779,918	0.0	0.0	0.0	0,0,0	0.23	0.21	0.21	848,884,924
	32.2	6.02e-03	8.70e-03	7.57e-03	800,779,924	0.0	0.0	0.0	0,0,0				
	64.5	0.02	0.03	0.03	784,780,924	0.0	0.0	0.0	0,0,0				
41	0.0	5.93e-03	8.19e-03	7.46e-03	842,779,918	0.0	0.0	0.0	0,0,0	0.22	0.20	0.20	848,884,924
	32.2	6.71e-03	9.90e-03	8.47e-03	744,779,924	0.0	0.0	0.0	0,0,0				
	64.5	0.02	0.03	0.03	728,780,924	0.0	0.0	0.0	0,0,0				
42	0.0	0.17	0.19	0.22	786,786,918	0.0	0.0	0.0	0,0,0	0.16	0.13	0.13	744,876,924
	150.2	0.03	0.02	0.03	676,676,920	0.0	0.0	0.0	0,0,0				
	300.5	0.02	0.02	0.01	847,843,923	0.0	0.0	0.0	0,0,0				
43	0.0	0.06	0.09	0.04	795,795,919	0.0	0.0	0.0	0,0,0	0.21	0.19	0.19	844,878,920
	99.2	0.02	0.04	0.02	779,838,919	0.0	0.0	0.0	0,0,0				
	198.5	0.07	0.12	0.06	795,795,919	0.0	0.0	0.0	0,0,0				
64	0.0	0.57	0.69	0.63	836,836,920	0.17	0.15	0.14	836,868,920	-0.57	-0.52	-0.49	777,865,917
	256.0	0.29	0.35	0.31	665,724,917	0.07	0.06	0.06	724,868,920				
	512.0	0.33	0.40	0.31	781,781,921	0.08	0.06	0.06	781,869,921				
65	0.0	0.66	0.65	0.72	836,836,920	0.15	0.14	0.13	836,868,920	-0.62	-0.54	-0.49	837,869,921
	256.0	0.34	0.38	0.36	781,726,921	0.08	0.08	0.07	726,870,922				
	512.0	0.68	0.78	0.72	777,777,917	0.20	0.17	0.16	777,865,917				
66	0.0	0.74	0.64	0.84	836,836,920	0.14	0.13	0.13	836,868,920	-1.16	-1.08	-1.04	837,869,921
	256.0	0.49	0.56	0.56	781,725,921	0.14	0.13	0.12	725,869,921				
	512.0	0.72	0.63	0.80	777,777,917	0.14	0.12	0.12	777,865,917				
67	0.0	0.09	0.16	0.08	856,856,924	0.0	0.0	0.0	0,0,0	0.27	0.30	0.29	844,878,920
	169.2	0.06	0.12	0.06	777,777,917	0.0	0.0	0.0	0,0,0				
	338.5	0.25	0.42	0.28	777,777,917	0.11	0.09	0.09	777,901,917				
68	0.0	0.24	0.27	0.28	744,744,924	0.06	0.0	0.0	744,0,0	0.07	0.07	0.07	781,873,921
	245.0	0.05	0.03	0.07	785,730,917	0.0	0.0	0.0	0,0,0				
	490.0	0.10	0.09	0.09	744,744,924	0.0	0.0	0.0	0,0,0				
69	0.0	0.19	0.27	0.24	744,744,924	0.0	0.0	0.0	0,0,0	-0.05	-0.04	-0.04	736,876,924
	245.0	0.04	0.06	0.05	677,846,921	0.0	0.0	0.0	0,0,0				
	490.0	0.04	0.06	0.05	673,674,917	0.0	0.0	0.0	0,0,0				
70	0.0	0.17	0.25	0.21	743,744,923	0.0	0.0	0.0	0,0,0	-0.06	-0.06	-0.06	741,873,921
	245.0	0.04	0.07	0.05	677,790,921	0.0	0.0	0.0	0,0,0				
	490.0	0.07	0.10	0.08	676,674,920	0.0	0.0	0.0	0,0,0				
71	0.0	0.15	0.29	0.19	743,743,923	0.0	0.0	0.0	0,0,0	-0.07	-0.07	-0.07	672,880,924
	245.0	0.07	0.15	0.10	792,840,924	0.0	0.0	0.0	0,0,0				
	490.0	0.12	0.23	0.15	674,673,918	0.0	0.0	0.0	0,0,0				
72	0.0	0.19	0.30	0.24	846,678,922	0.08	0.08	0.07	678,883,922	0.13	0.13	0.12	844,912,920
	24.2	0.27	0.43	0.35	846,678,922	0.11	0.13	0.12	678,883,922				
	48.5	0.36	0.56	0.46	846,678,922	0.16	0.18	0.18	678,883,922				
73	0.0	0.19	0.32	0.24	792,678,924	0.08	0.08	0.08	678,883,922	0.16	0.16	0.15	848,916,924
	24.2	0.26	0.42	0.33	792,790,924	0.11	0.13	0.12	678,883,922				
	48.5	0.33	0.53	0.42	792,790,924	0.15	0.17	0.17	790,883,922				
74	0.0	0.28	0.35	0.36	780,668,920	0.08	0.10	0.10	668,882,920	0.25	0.24	0.24	848,884,924
	24.2	0.42	0.52	0.53	780,836,920	0.15	0.16	0.16	836,882,920				
	48.5	0.56	0.68	0.71	724,836,920	0.22	0.23	0.22	836,882,920				
75	0.0	0.28	0.35	0.36	724,668,920	0.08	0.10	0.09	668,882,920	0.23	0.23	0.22	848,884,924
	24.2	0.42	0.51	0.53	836,668,920	0.15	0.16	0.16	668,882,920				
	48.5	0.55	0.68	0.70	836,668,920	0.21	0.23	0.22	668,882,920				
78	0.0	0.10	0.17	0.13	846,846,922	0.0	0.0	0.0	0,0,0	0.10	0.09	0.09	844,882,920
	25.2	0.14	0.23	0.18	846,846,922	0.0	0.0	0.0	0,0,0				
	50.5	0.19	0.30	0.24	846,846,922	0.08	0.08	0.07	846,883,922				
79	0.0	0.10	0.16	0.12	792,678,924	0.0	0.0	0.0	0,0,0	0.12	0.10	0.10	848,916,924
	25.2	0.14	0.23	0.18	792,678,924	0.0	0.0	0.0	0,0,0				
	50.5	0.18	0.30	0.23	792,790,924	0.08	0.08	0.07	678,883,922				
80	0.0	0.12	0.18	0.16	780,784,920	0.0	0.0	0.0	0,0,0	0.25	0.28	0.26	848,884,924
	25.2	0.21	0.31	0.26	780,780,920	0.09	0.08	0.08	668,882,920				
	50.5	0.29	0.43	0.38	780,780,920	0.12	0.14	0.13	780,882,920				
81	0.0	0.12	0.18	0.16	724,784,920	0.0	0.0	0.0	0,0,0	0.24	0.27	0.25	848,884,924
	25.2	0.21	0.30	0.26	724,780,920	0.09	0.08	0.08	780,882,920				
	50.5	0.29	0.43	0.37	724,780,920	0.12	0.14	0.13	780,882,920				
86	0.0	0.68	0.71	0.76	836,836,920	0.16	0.14	0.14	836,868,920	-1.03	-0.94	-0.90	777,865,917

Trave	Pos.	rRfck	rRfyk	rPfck	Rif. cmb	wR	wF	wP	Rif. cmb	dR	dF	dP	Rif. cmb
	274.8	0.37	0.44	0.40	835,724,919	0.09	0.09	0.08	724,868,920				
	549.5	0.27	0.32	0.23	781,781,921	0.06	0.04	0.04	781,869,921				
87	0.0	0.83	0.72	0.91	836,836,920	0.16	0.14	0.14	836,868,920	-2.00	-1.76	-1.68	724,868,920
	274.8	0.58	0.65	0.63	836,668,920	0.16	0.15	0.14	668,868,920				
	549.5	0.35	0.39	0.34	781,781,921	0.09	0.07	0.06	781,869,921				
88	0.0	0.84	0.66	0.93	836,836,920	0.14	0.12	0.12	836,868,920	-1.85	-1.61	-1.53	724,868,920
	274.8	0.55	0.62	0.59	836,724,920	0.15	0.14	0.13	724,868,920				
	549.5	0.35	0.40	0.34	781,781,921	0.09	0.07	0.07	781,869,921				
89	0.0	0.48	0.80	0.56	836,836,920	0.24	0.24	0.24	836,868,920	-0.71	-0.75	-0.73	721,865,917
	256.0	0.31	0.53	0.37	837,670,921	0.13	0.14	0.14	670,870,922				
	512.0	0.48	0.80	0.55	781,781,921	0.24	0.23	0.23	781,869,921				
90	0.0	0.16	0.15	0.20	744,744,924	0.0	0.0	0.0	0,0,0	0.25	0.23	0.22	728,876,924
	246.8	0.05	0.03	0.06	681,685,917	0.0	0.0	0.0	0,0,0				
	493.5	0.03	0.02	0.03	673,673,917	0.0	0.0	0.0	0,0,0				
91	0.0	7.77e-03	0.02	7.85e-03	739,836,919	0.0	0.0	0.0	0,0,0	0.12	0.11	0.10	734,874,922
	246.8	0.02	0.06	0.03	729,684,917	0.0	0.0	0.0	0,0,0				
	493.5	8.14e-03	0.02	8.12e-03	739,836,919	0.0	0.0	0.0	0,0,0				
92	0.0	7.87e-03	0.03	8.67e-03	740,793,920	0.0	0.0	0.0	0,0,0	-0.07	-0.06	-0.06	683,887,919
	246.8	0.02	0.06	0.03	744,793,924	0.0	0.0	0.0	0,0,0				
	493.5	9.80e-03	0.03	0.01	740,795,920	0.0	0.0	0.0	0,0,0				
93	0.0	0.15	0.29	0.19	741,741,921	0.0	0.0	0.0	0,0,0	0.14	0.12	0.12	800,876,924
	246.8	0.08	0.17	0.11	789,742,921	0.0	0.0	0.0	0,0,0				
	493.5	0.12	0.22	0.14	676,684,920	0.0	0.0	0.0	0,0,0				
96	0.0	0.04	0.06	0.05	846,846,922	0.0	0.0	0.0	0,0,0	0.10	0.10	0.09	844,882,920
	25.2	0.06	0.11	0.08	846,846,922	0.0	0.0	0.0	0,0,0				
	50.5	0.09	0.15	0.12	846,846,922	0.0	0.0	0.0	0,0,0				
97	0.0	0.04	0.06	0.05	790,678,922	0.0	0.0	0.0	0,0,0	0.12	0.11	0.11	848,916,924
	25.2	0.06	0.10	0.08	790,678,922	0.0	0.0	0.0	0,0,0				
	50.5	0.09	0.15	0.12	790,790,922	0.0	0.0	0.0	0,0,0				
98	0.0	0.02	0.04	0.03	784,784,924	0.0	0.0	0.0	0,0,0	0.18	0.16	0.16	848,884,924
	25.2	0.07	0.10	0.09	780,784,920	0.0	0.0	0.0	0,0,0				
	50.5	0.11	0.17	0.15	780,780,920	0.0	0.0	0.0	0,0,0				
99	0.0	0.03	0.04	0.03	728,784,924	0.0	0.0	0.0	0,0,0	0.17	0.16	0.15	848,884,924
	25.2	0.07	0.10	0.09	724,784,920	0.0	0.0	0.0	0,0,0				
	50.5	0.12	0.17	0.15	724,780,920	0.0	0.0	0.0	0,0,0				
104	0.0	0.51	0.77	0.60	836,836,920	0.22	0.21	0.21	836,868,920	-0.65	-0.65	-0.62	724,868,920
	274.8	0.26	0.45	0.29	836,836,920	0.11	0.10	0.10	836,868,920				
	549.5	0.24	0.43	0.22	781,781,921	0.11	0.0	0.0	781,0,0				
Trave		rRfck	rRfyk	rPfck		wR	wF	wP		dR	dF	dP	
										-2.00	-1.76	-1.68	
		0.84	0.80	0.93		0.24	0.24	0.24		1.06	1.09	1.07	

Setto	rRfck	rRfyk	rPfck	Rif. cmb	wR	wF	wP	Rif. cmb
					mm	mm	mm	
325	0.24	0.78	0.30	795,724,919	0.0	0.0	0.0	0,0,0
326	0.16	0.52	0.20	780,724,920	0.0	0.0	0.0	0,0,0
327	0.15	0.43	0.19	724,834,920	0.0	0.0	0.0	0,0,0
328	0.14	0.28	0.17	855,728,923	0.0	0.0	0.0	0,0,0
329	0.15	0.29	0.18	792,731,924	0.0	0.0	0.0	0,0,0
330	0.13	0.29	0.17	856,852,924	0.0	0.0	0.0	0,0,0
331	0.13	0.37	0.17	856,836,924	0.0	0.0	0.0	0,0,0
332	0.16	0.39	0.20	788,675,920	0.0	0.0	0.0	0,0,0
333	0.14	0.31	0.17	792,672,924	0.0	0.0	0.0	0,0,0
334	0.15	0.29	0.18	668,835,920	0.0	0.0	0.0	0,0,0
335	0.17	0.38	0.21	668,683,920	0.0	0.0	0.0	0,0,0
336	0.26	0.49	0.31	779,683,919	0.0	0.0	0.0	0,0,0
337	0.08	0.76	0.10	667,675,919	0.38	0.34	0.33	683,877,919
338	0.06	0.14	0.05	742,676,922	0.0	0.0	0.0	0,0,0
339	0.02	0.23	0.02	781,676,921	0.0	0.0	0.0	0,0,0
340	0.02	0.19	0.02	781,844,921	0.0	0.0	0.0	0,0,0
341	0.01	0.21	9.77e-03	797,844,921	0.0	0.0	0.0	0,0,0
342	0.04	0.15	0.03	797,844,921	0.0	0.0	0.0	0,0,0
343	0.09	0.41	0.09	797,797,921	0.0	0.0	0.0	0,0,0
344	0.03	0.35	0.03	672,844,924	0.0	0.0	0.0	0,0,0
345	0.02	0.47	0.03	672,844,924	0.0	0.0	0.0	0,0,0

Setto	rRfck	rRfyk	rPfck	Rif. cmb	wR	wF	wP	Rif. cmb
346	0.02	0.59	0.02	669,844,921	0.0	0.0	0.0	0,0,0
347	0.02	0.71	0.02	669,844,921	0.0	0.0	0.0	0,0,0
348	0.02	0.80	0.03	665,676,917	0.0	0.0	0.0	0,0,0
349	0.02	0.77	0.03	673,684,917	0.0	0.0	0.0	0,0,0
350	0.03	0.75	0.05	675,665,919	0.0	0.0	0.0	0,0,0
351	0.09	0.77	0.12	673,665,917	0.27	0.29	0.28	665,865,917
352	0.09	0.72	0.12	673,665,917	0.23	0.25	0.25	665,865,917
353	0.10	0.68	0.12	681,777,917	0.26	0.25	0.25	777,865,917
354	0.16	0.65	0.20	681,665,917	0.25	0.24	0.23	777,865,917
355	0.49	0.71	0.60	688,685,924	0.15	0.15	0.15	685,889,921
356	0.20	0.45	0.24	844,852,924	0.0	0.0	0.0	0,0,0
357	0.19	0.36	0.20	844,852,920	0.0	0.0	0.0	0,0,0
358	0.16	0.65	0.18	725,742,921	0.0	0.0	0.0	0,0,0
359	0.11	0.26	0.12	744,737,924	0.0	0.0	0.0	0,0,0
360	0.08	0.23	0.09	744,781,924	0.0	0.0	0.0	0,0,0
361	0.08	0.20	0.09	725,781,921	0.0	0.0	0.0	0,0,0
362	0.08	0.20	0.08	725,781,924	0.0	0.0	0.0	0,0,0
363	0.05	0.28	0.06	840,793,924	0.0	0.0	0.0	0,0,0
364	0.02	0.39	0.02	781,737,924	0.0	0.0	0.0	0,0,0
365	0.05	0.46	0.06	844,777,920	0.0	0.0	0.0	0,0,0
366	0.05	0.64	0.06	781,777,920	0.0	0.0	0.0	0,0,0
367	0.04	0.75	0.04	852,777,920	0.0	0.0	0.0	0,0,0
368	0.04	0.77	0.05	852,777,920	0.0	0.0	0.0	0,0,0
369	0.07	0.60	0.09	740,721,920	0.0	0.0	0.0	0,0,0
370	0.12	0.56	0.15	844,852,920	0.0	0.0	0.0	0,0,0
371	0.07	0.54	0.08	844,777,920	0.0	0.0	0.0	0,0,0
372	0.04	0.74	0.04	668,777,920	0.0	0.0	0.0	0,0,0
373	0.03	0.78	0.04	684,779,920	0.0	0.0	0.0	0,0,0
374	0.03	0.77	0.03	684,780,920	0.0	0.0	0.0	0,0,0
375	0.03	0.77	0.04	681,780,917	0.0	0.0	0.0	0,0,0
376	0.05	0.74	0.06	668,788,920	0.0	0.0	0.0	0,0,0
377	0.03	0.78	0.03	688,836,924	0.30	0.34	0.34	836,878,920
378	0.02	0.78	0.02	676,844,920	0.30	0.35	0.34	836,878,920
379	0.05	0.76	0.06	668,844,920	0.27	0.29	0.29	844,878,920
380	0.05	0.79	0.06	668,852,920	0.27	0.29	0.29	852,878,920
381	0.03	0.79	0.03	840,852,924	0.26	0.27	0.26	852,878,920
382	0.04	0.66	0.05	684,852,920	0.19	0.19	0.19	852,878,920
383	0.06	0.55	0.07	684,852,920	0.14	0.14	0.14	852,912,920
384	0.10	0.50	0.12	780,852,920	0.12	0.11	0.11	852,912,920
385	0.09	0.60	0.10	744,795,924	0.36	0.34	0.33	788,878,920
386	0.09	0.70	0.11	740,836,919	0.29	0.29	0.28	836,878,920
387	0.09	0.11	0.08	797,797,921	0.0	0.0	0.0	0,0,0
388	0.08	0.28	0.09	795,795,919	0.0	0.0	0.0	0,0,0
389	0.05	0.62	0.06	684,795,920	0.25	0.24	0.23	795,877,919
390	0.05	0.33	0.06	725,852,920	0.0	0.0	0.0	0,0,0
391	0.11	0.42	0.12	723,852,919	0.0	0.0	0.0	0,0,0
392	0.14	0.51	0.16	723,793,919	0.10	0.10	0.10	852,878,920
393	0.05	0.51	0.06	740,844,920	0.13	0.0	0.0	844,0,0
394	0.07	0.68	0.08	724,844,920	0.22	0.23	0.22	844,878,920
395	0.06	0.75	0.07	724,844,920	0.26	0.28	0.27	844,878,920
396	0.02	0.80	0.02	743,844,920	0.30	0.33	0.33	844,878,920
397	0.03	0.80	0.03	728,852,924	0.29	0.33	0.33	852,878,920
398	0.07	0.80	0.08	724,732,920	0.0	0.0	0.0	0,0,0
399	0.06	0.80	0.06	724,788,920	0.0	0.0	0.0	0,0,0
400	0.02	0.80	0.02	777,788,917	0.0	0.0	0.0	0,0,0
401	0.02	0.77	0.02	740,777,920	0.0	0.0	0.0	0,0,0
402	0.03	0.78	0.04	740,777,920	0.0	0.0	0.0	0,0,0
403	0.06	0.59	0.07	732,777,920	0.0	0.0	0.0	0,0,0
404	0.13	0.77	0.16	844,844,920	0.0	0.0	0.0	0,0,0
405	0.09	0.13	0.11	852,844,920	0.0	0.0	0.0	0,0,0
406	0.05	0.06	0.06	836,677,920	0.0	0.0	0.0	0,0,0
407	0.24	0.48	0.25	839,728,923	0.0	0.0	0.0	0,0,0
408	0.04	0.13	0.05	777,723,917	0.0	0.0	0.0	0,0,0
409	0.10	0.39	0.11	785,737,917	0.0	0.0	0.0	0,0,0
410	0.10	0.17	0.10	781,781,921	0.0	0.0	0.0	0,0,0
411	0.08	0.37	0.10	681,669,917	0.0	0.0	0.0	0,0,0
412	0.02	0.71	0.03	669,728,921	0.0	0.0	0.0	0,0,0
413	0.01	0.75	0.01	781,728,921	0.0	0.0	0.0	0,0,0

Setto	rRfck	rRfyk	rPfck	Rif. cmb	wR	wF	wP	Rif. cmb
414	7.02e-03	0.47	8.47e-03	781,725,921	0.0	0.0	0.0	0,0,0
415	0.17	0.63	0.20	685,685,921	0.0	0.0	0.0	0,0,0
416	0.04	0.50	0.04	673,728,917	0.0	0.0	0.0	0,0,0
417	0.01	0.58	0.02	669,728,921	0.0	0.0	0.0	0,0,0
418	8.29e-03	0.49	0.01	777,725,917	0.0	0.0	0.0	0,0,0
419	0.07	0.27	0.09	681,669,917	0.0	0.0	0.0	0,0,0
420	0.29	0.60	0.35	685,669,921	0.0	0.0	0.0	0,0,0
433	0.07	0.67	0.08	792,788,924	0.23	0.25	0.24	792,880,924
446	0.08	0.18	0.08	795,793,919	0.0	0.0	0.0	0,0,0
447	0.04	0.05	0.05	793,785,917	0.0	0.0	0.0	0,0,0
448	0.03	0.04	0.03	777,785,917	0.0	0.0	0.0	0,0,0
449	0.09	0.72	0.11	800,744,924	0.24	0.25	0.24	728,880,924
450	0.11	0.33	0.11	785,793,917	0.0	0.0	0.0	0,0,0
451	0.10	0.13	0.09	797,797,921	0.0	0.0	0.0	0,0,0
452	0.04	0.06	0.04	797,797,921	0.0	0.0	0.0	0,0,0
453	0.02	0.05	0.02	670,737,922	0.0	0.0	0.0	0,0,0
454	0.03	0.08	0.04	797,781,921	0.0	0.0	0.0	0,0,0
455	0.22	0.39	0.24	844,852,920	0.0	0.0	0.0	0,0,0
456	0.14	0.25	0.16	844,844,920	0.0	0.0	0.0	0,0,0
457	0.10	0.14	0.11	852,844,920	0.0	0.0	0.0	0,0,0
458	0.17	0.20	0.13	781,852,921	0.0	0.0	0.0	0,0,0
459	0.20	0.46	0.23	844,852,920	0.0	0.0	0.0	0,0,0
460	0.12	0.26	0.14	844,844,920	0.0	0.0	0.0	0,0,0
509	0.07	0.75	0.08	744,788,924	0.30	0.0	0.0	788,0,0
510	0.08	0.77	0.09	726,792,922	0.27	0.29	0.28	792,880,924
Setto	rRfck	rRfyk	rPfck		wR	wF	wP	
	0.49	0.80	0.60		0.38	0.35	0.34	

Guscio	rRfck	rRfyk	rPfck	Rif. cmb	wR	wF	wP	Rif. cmb
					mm	mm	mm	
1	0.11	0.28	0.13	796,796,920	0.0	0.0	0.0	0,0,0
2	0.07	0.32	0.08	782,672,922	0.0	0.0	0.0	0,0,0
3	0.11	0.25	0.13	796,796,920	0.0	0.0	0.0	0,0,0
4	0.09	0.21	0.11	780,796,920	0.0	0.0	0.0	0,0,0
5	0.06	0.11	0.07	780,788,920	0.0	0.0	0.0	0,0,0
6	0.03	0.34	0.04	835,672,920	0.0	0.0	0.0	0,0,0
7	0.04	0.34	0.05	788,672,918	0.0	0.0	0.0	0,0,0
8	0.03	0.08	0.03	796,800,920	0.0	0.0	0.0	0,0,0
9	0.05	0.20	0.07	780,800,920	0.0	0.0	0.0	0,0,0
10	0.06	0.55	0.08	796,728,920	0.0	0.0	0.0	0,0,0
11	0.05	0.54	0.06	839,728,919	0.0	0.0	0.0	0,0,0
12	0.08	0.23	0.10	780,744,920	0.0	0.0	0.0	0,0,0
13	0.10	0.29	0.12	780,740,920	0.0	0.0	0.0	0,0,0
14	0.11	0.31	0.13	780,724,920	0.0	0.0	0.0	0,0,0
15	0.03	0.06	0.03	676,672,920	0.0	0.0	0.0	0,0,0
16	0.06	0.21	0.07	856,742,924	0.0	0.0	0.0	0,0,0
17	0.02	0.05	0.02	781,781,921	0.0	0.0	0.0	0,0,0
18	0.04	0.10	0.05	725,856,921	0.0	0.0	0.0	0,0,0
19	0.03	0.08	0.03	676,688,924	0.0	0.0	0.0	0,0,0
20	0.05	0.24	0.06	744,742,924	0.0	0.0	0.0	0,0,0
21	0.07	0.49	0.08	780,728,920	0.0	0.0	0.0	0,0,0
22	0.08	0.21	0.10	723,784,919	0.0	0.0	0.0	0,0,0
23	0.09	0.27	0.11	780,724,920	0.0	0.0	0.0	0,0,0
24	0.10	0.29	0.12	724,724,920	0.0	0.0	0.0	0,0,0
25	0.08	0.37	0.10	778,784,918	0.0	0.0	0.0	0,0,0
26	0.06	0.11	0.07	794,778,918	0.0	0.0	0.0	0,0,0
27	0.06	0.16	0.08	794,728,918	0.0	0.0	0.0	0,0,0
28	0.11	0.54	0.13	780,784,920	0.0	0.0	0.0	0,0,0
29	0.11	0.28	0.13	796,836,920	0.0	0.0	0.0	0,0,0
30	0.09	0.22	0.11	780,835,920	0.0	0.0	0.0	0,0,0
31	0.08	0.15	0.10	780,780,920	0.0	0.0	0.0	0,0,0
32	0.10	0.32	0.12	796,780,920	0.0	0.0	0.0	0,0,0
33	0.10	0.31	0.12	796,796,920	0.0	0.0	0.0	0,0,0
34	0.14	0.39	0.18	836,780,920	0.0	0.0	0.0	0,0,0
35	0.13	0.33	0.16	724,724,920	0.0	0.0	0.0	0,0,0

Guscio	rRfck	rRfyk	rPfck	Rif. cmb	wR	wF	wP	Rif. cmb
36	0.11	0.22	0.14	836,836,920	0.0	0.0	0.0	0,0,0
37	0.16	0.48	0.20	782,782,922	0.0	0.0	0.0	0,0,0
38	0.19	0.55	0.23	778,780,918	0.0	0.0	0.0	0,0,0
39	0.07	0.17	0.08	835,840,919	0.0	0.0	0.0	0,0,0
40	0.07	0.19	0.09	835,728,919	0.0	0.0	0.0	0,0,0
41	0.21	0.66	0.25	778,784,918	0.0	0.0	0.0	0,0,0
42	0.12	0.46	0.14	668,784,920	0.0	0.0	0.0	0,0,0
43	0.12	0.32	0.15	836,724,920	0.0	0.0	0.0	0,0,0
44	0.12	0.33	0.15	836,724,920	0.0	0.0	0.0	0,0,0
45	0.13	0.37	0.16	728,744,924	0.0	0.0	0.0	0,0,0
46	0.04	0.09	0.04	676,676,920	0.0	0.0	0.0	0,0,0
47	0.08	0.30	0.09	742,744,924	0.0	0.0	0.0	0,0,0
48	0.04	0.09	0.04	725,781,921	0.0	0.0	0.0	0,0,0
49	0.12	0.30	0.15	852,796,920	0.0	0.0	0.0	0,0,0
50	0.12	0.26	0.14	836,796,920	0.0	0.0	0.0	0,0,0
51	0.17	0.40	0.21	724,724,920	0.0	0.0	0.0	0,0,0
52	0.18	0.41	0.22	836,836,920	0.0	0.0	0.0	0,0,0
53	0.18	0.44	0.22	836,836,920	0.0	0.0	0.0	0,0,0
54	0.21	0.51	0.26	836,836,920	0.0	0.0	0.0	0,0,0
55	0.18	0.43	0.21	836,836,920	0.0	0.0	0.0	0,0,0
56	0.22	0.56	0.27	836,836,920	0.0	0.0	0.0	0,0,0
57	0.21	0.66	0.25	794,794,918	0.0	0.0	0.0	0,0,0
58	0.23	0.62	0.28	836,836,920	0.0	0.0	0.0	0,0,0
59	0.21	0.67	0.25	794,794,918	0.0	0.0	0.0	0,0,0
60	0.23	0.62	0.28	836,836,920	0.0	0.0	0.0	0,0,0
61	0.16	0.40	0.19	836,836,920	0.0	0.0	0.0	0,0,0
62	0.23	0.60	0.27	836,836,920	0.0	0.0	0.0	0,0,0
63	0.16	0.40	0.19	836,836,920	0.0	0.0	0.0	0,0,0
64	0.22	0.60	0.27	836,836,920	0.0	0.0	0.0	0,0,0
65	0.21	0.70	0.25	794,796,918	0.0	0.0	0.0	0,0,0
66	0.22	0.62	0.27	836,836,920	0.0	0.0	0.0	0,0,0
67	0.20	0.59	0.24	794,794,918	0.0	0.0	0.0	0,0,0
68	0.22	0.63	0.27	836,836,920	0.0	0.0	0.0	0,0,0
69	0.16	0.49	0.20	836,836,920	0.0	0.0	0.0	0,0,0
70	0.19	0.54	0.23	836,836,920	0.0	0.0	0.0	0,0,0
71	0.16	0.43	0.19	836,836,920	0.0	0.0	0.0	0,0,0
72	0.15	0.42	0.19	836,836,920	0.0	0.0	0.0	0,0,0
73	0.16	0.46	0.19	724,728,920	0.0	0.0	0.0	0,0,0
74	0.24	0.52	0.28	723,727,919	0.0	0.0	0.0	0,0,0
75	0.13	0.39	0.15	724,728,920	0.0	0.0	0.0	0,0,0
76	0.13	0.48	0.16	724,727,920	0.0	0.0	0.0	0,0,0
77	0.03	0.11	0.03	844,844,920	0.0	0.0	0.0	0,0,0
78	0.04	0.27	0.03	844,685,920	0.0	0.0	0.0	0,0,0
79	0.02	0.08	0.02	781,781,921	0.0	0.0	0.0	0,0,0
80	0.05	0.30	0.06	669,685,921	0.0	0.0	0.0	0,0,0
81	0.12	0.16	0.14	836,835,920	0.0	0.0	0.0	0,0,0
82	0.11	0.15	0.14	836,833,920	0.0	0.0	0.0	0,0,0
83	0.11	0.22	0.13	836,836,920	0.0	0.0	0.0	0,0,0
84	0.18	0.41	0.22	836,836,920	0.0	0.0	0.0	0,0,0
85	0.17	0.36	0.21	836,836,920	0.0	0.0	0.0	0,0,0
86	0.13	0.38	0.16	836,724,920	0.0	0.0	0.0	0,0,0
87	0.21	0.50	0.25	836,836,920	0.0	0.0	0.0	0,0,0
88	0.19	0.46	0.24	836,836,920	0.0	0.0	0.0	0,0,0
89	0.16	0.44	0.20	724,724,920	0.0	0.0	0.0	0,0,0
90	0.22	0.56	0.27	836,836,920	0.0	0.0	0.0	0,0,0
91	0.22	0.54	0.27	836,836,920	0.0	0.0	0.0	0,0,0
92	0.17	0.45	0.21	836,724,920	0.0	0.0	0.0	0,0,0
93	0.23	0.61	0.29	836,836,920	0.0	0.0	0.0	0,0,0
94	0.24	0.62	0.29	836,836,920	0.0	0.0	0.0	0,0,0
95	0.22	0.57	0.27	836,836,920	0.0	0.0	0.0	0,0,0
96	0.23	0.61	0.29	836,836,920	0.0	0.0	0.0	0,0,0
97	0.24	0.62	0.29	836,836,920	0.0	0.0	0.0	0,0,0
98	0.22	0.57	0.27	836,836,920	0.0	0.0	0.0	0,0,0
99	0.23	0.59	0.28	836,836,920	0.0	0.0	0.0	0,0,0
100	0.23	0.60	0.28	836,836,920	0.0	0.0	0.0	0,0,0
101	0.16	0.42	0.20	836,836,920	0.0	0.0	0.0	0,0,0
102	0.22	0.59	0.27	836,836,920	0.0	0.0	0.0	0,0,0
103	0.22	0.60	0.27	836,836,920	0.0	0.0	0.0	0,0,0

Guscio	rRfck	rRfyk	rPfck	Rif. cmb	wR	wF	wP	Rif. cmb
104	0.16	0.42	0.20	836,836,920	0.0	0.0	0.0	0,0,0
105	0.22	0.62	0.27	836,836,920	0.0	0.0	0.0	0,0,0
106	0.22	0.60	0.27	836,836,920	0.0	0.0	0.0	0,0,0
107	0.27	0.72	0.31	725,725,921	0.0	0.0	0.0	0,0,0
108	0.22	0.62	0.26	836,836,920	0.0	0.0	0.0	0,0,0
109	0.21	0.59	0.26	836,836,920	0.0	0.0	0.0	0,0,0
110	0.24	0.65	0.28	669,781,921	0.0	0.0	0.0	0,0,0
111	0.19	0.54	0.23	836,836,920	0.0	0.0	0.0	0,0,0
112	0.18	0.47	0.21	836,836,920	0.0	0.0	0.0	0,0,0
113	0.12	0.31	0.15	852,836,920	0.0	0.0	0.0	0,0,0
114	0.15	0.41	0.18	836,836,920	0.0	0.0	0.0	0,0,0
115	0.13	0.33	0.15	852,836,920	0.0	0.0	0.0	0,0,0
116	0.10	0.23	0.12	852,852,920	0.0	0.0	0.0	0,0,0
117	0.25	0.55	0.29	723,727,919	0.0	0.0	0.0	0,0,0
118	0.19	0.55	0.21	723,727,919	0.0	0.0	0.0	0,0,0
119	0.23	0.60	0.26	728,728,924	0.0	0.0	0.0	0,0,0
120	0.04	0.26	0.05	856,685,924	0.0	0.0	0.0	0,0,0
121	0.05	0.17	0.05	856,669,924	0.0	0.0	0.0	0,0,0
122	0.05	0.12	0.06	856,669,924	0.0	0.0	0.0	0,0,0
123	0.15	0.50	0.18	725,724,923	0.0	0.0	0.0	0,0,0
124	0.17	0.47	0.19	781,783,921	0.0	0.0	0.0	0,0,0
125	0.20	0.54	0.23	784,784,924	0.0	0.0	0.0	0,0,0
126	0.07	0.27	0.08	669,685,921	0.0	0.0	0.0	0,0,0
127	0.05	0.14	0.06	840,669,924	0.0	0.0	0.0	0,0,0
128	0.05	0.11	0.06	672,669,924	0.0	0.0	0.0	0,0,0
129	0.10	0.19	0.12	852,852,920	0.0	0.0	0.0	0,0,0
130	0.09	0.12	0.10	844,852,920	0.0	0.0	0.0	0,0,0
131	0.07	0.07	0.08	836,835,920	0.0	0.0	0.0	0,0,0
132	0.05	0.20	0.06	836,840,920	0.0	0.0	0.0	0,0,0
133	0.13	0.39	0.16	724,724,920	0.0	0.0	0.0	0,0,0
134	0.11	0.30	0.14	724,724,920	0.0	0.0	0.0	0,0,0
135	0.11	0.30	0.13	724,724,920	0.0	0.0	0.0	0,0,0
136	0.12	0.36	0.14	724,724,920	0.0	0.0	0.0	0,0,0
137	0.16	0.44	0.20	724,724,920	0.0	0.0	0.0	0,0,0
138	0.15	0.40	0.18	724,724,920	0.0	0.0	0.0	0,0,0
139	0.14	0.41	0.18	724,724,920	0.0	0.0	0.0	0,0,0
140	0.15	0.42	0.18	724,724,920	0.0	0.0	0.0	0,0,0
141	0.17	0.45	0.20	724,724,920	0.0	0.0	0.0	0,0,0
142	0.15	0.41	0.19	724,724,920	0.0	0.0	0.0	0,0,0
143	0.15	0.41	0.18	724,724,920	0.0	0.0	0.0	0,0,0
144	0.15	0.42	0.18	724,724,920	0.0	0.0	0.0	0,0,0
145	0.18	0.46	0.22	724,724,920	0.0	0.0	0.0	0,0,0
146	0.13	0.32	0.17	724,724,920	0.0	0.0	0.0	0,0,0
147	0.13	0.33	0.17	724,724,920	0.0	0.0	0.0	0,0,0
148	0.24	0.63	0.26	840,840,924	0.0	0.0	0.0	0,0,0
149	0.16	0.40	0.20	724,724,920	0.0	0.0	0.0	0,0,0
150	0.13	0.33	0.16	724,724,920	0.0	0.0	0.0	0,0,0
151	0.13	0.33	0.16	724,724,920	0.0	0.0	0.0	0,0,0
152	0.24	0.62	0.25	840,840,924	0.0	0.0	0.0	0,0,0
153	0.13	0.32	0.16	724,780,920	0.0	0.0	0.0	0,0,0
154	0.12	0.30	0.15	836,836,920	0.0	0.0	0.0	0,0,0
155	0.11	0.29	0.14	724,724,920	0.0	0.0	0.0	0,0,0
156	0.10	0.27	0.13	780,777,920	0.0	0.0	0.0	0,0,0
157	0.13	0.32	0.16	724,780,920	0.0	0.0	0.0	0,0,0
158	0.11	0.28	0.13	724,724,920	0.0	0.0	0.0	0,0,0
159	0.11	0.28	0.13	724,724,920	0.0	0.0	0.0	0,0,0
160	0.10	0.28	0.12	780,777,920	0.0	0.0	0.0	0,0,0
161	0.27	0.70	0.31	725,781,921	0.0	0.0	0.0	0,0,0
162	0.12	0.31	0.15	836,724,920	0.0	0.0	0.0	0,0,0
163	0.12	0.32	0.15	836,724,920	0.0	0.0	0.0	0,0,0
164	0.31	0.82	0.36	728,728,924	0.0	0.0	0.0	0,0,0
165	0.23	0.61	0.26	781,781,921	0.0	0.0	0.0	0,0,0
166	0.12	0.31	0.14	836,724,920	0.0	0.0	0.0	0,0,0
167	0.12	0.32	0.15	836,724,920	0.0	0.0	0.0	0,0,0
168	0.30	0.83	0.35	840,840,924	0.0	0.0	0.0	0,0,0
169	0.08	0.17	0.09	844,668,920	0.0	0.0	0.0	0,0,0
170	0.09	0.24	0.12	836,724,920	0.0	0.0	0.0	0,0,0
171	0.10	0.25	0.12	836,724,920	0.0	0.0	0.0	0,0,0

Guscio	rRfck	rRfyk	rPfck	Rif. cmb	wR	wF	wP	Rif. cmb
172	0.07	0.17	0.08	780,837,920	0.0	0.0	0.0	0,0,0
173	0.08	0.17	0.09	844,852,920	0.0	0.0	0.0	0,0,0
174	0.08	0.18	0.10	844,836,920	0.0	0.0	0.0	0,0,0
175	0.08	0.18	0.10	844,836,920	0.0	0.0	0.0	0,0,0
176	0.06	0.16	0.07	727,725,923	0.0	0.0	0.0	0,0,0
177	0.23	0.62	0.26	728,728,924	0.0	0.0	0.0	0,0,0
178	0.17	0.47	0.19	725,725,921	0.0	0.0	0.0	0,0,0
179	0.18	0.48	0.20	725,725,921	0.0	0.0	0.0	0,0,0
180	0.23	0.59	0.26	728,725,924	0.0	0.0	0.0	0,0,0
181	0.05	0.11	0.06	672,781,924	0.0	0.0	0.0	0,0,0
182	0.05	0.13	0.07	844,781,920	0.0	0.0	0.0	0,0,0
183	0.07	0.16	0.08	781,781,921	0.0	0.0	0.0	0,0,0
184	0.07	0.16	0.08	781,781,921	0.0	0.0	0.0	0,0,0
185	0.20	0.53	0.23	784,784,924	0.0	0.0	0.0	0,0,0
186	0.16	0.44	0.18	781,781,921	0.0	0.0	0.0	0,0,0
187	0.18	0.49	0.20	781,781,921	0.0	0.0	0.0	0,0,0
188	0.22	0.56	0.25	669,669,921	0.0	0.0	0.0	0,0,0
189	0.05	0.09	0.06	672,669,924	0.0	0.0	0.0	0,0,0
190	0.06	0.08	0.07	672,669,924	0.0	0.0	0.0	0,0,0
191	0.06	0.10	0.07	684,665,920	0.0	0.0	0.0	0,0,0
192	0.06	0.09	0.07	684,665,919	0.0	0.0	0.0	0,0,0
193	0.09	0.20	0.11	724,724,920	0.0	0.0	0.0	0,0,0
194	0.07	0.14	0.09	724,724,920	0.0	0.0	0.0	0,0,0
195	0.12	0.37	0.14	724,724,920	0.0	0.0	0.0	0,0,0
196	0.11	0.30	0.13	780,724,920	0.0	0.0	0.0	0,0,0
197	0.14	0.41	0.17	724,724,920	0.0	0.0	0.0	0,0,0
198	0.13	0.35	0.15	777,724,917	0.0	0.0	0.0	0,0,0
199	0.15	0.42	0.18	724,724,920	0.0	0.0	0.0	0,0,0
200	0.13	0.35	0.16	777,724,917	0.0	0.0	0.0	0,0,0
201	0.18	0.52	0.19	669,669,921	0.0	0.0	0.0	0,0,0
202	0.15	0.40	0.17	777,777,917	0.0	0.0	0.0	0,0,0
203	0.17	0.44	0.17	669,669,921	0.0	0.0	0.0	0,0,0
204	0.15	0.40	0.17	777,777,917	0.0	0.0	0.0	0,0,0
205	0.10	0.27	0.12	780,777,920	0.0	0.0	0.0	0,0,0
206	0.14	0.37	0.16	777,777,917	0.0	0.0	0.0	0,0,0
207	0.10	0.28	0.13	780,777,920	0.0	0.0	0.0	0,0,0
208	0.14	0.39	0.16	777,777,917	0.0	0.0	0.0	0,0,0
209	0.30	0.82	0.36	725,725,921	0.0	0.0	0.0	0,0,0
210	0.14	0.39	0.16	777,777,917	0.0	0.0	0.0	0,0,0
211	0.26	0.71	0.30	669,669,921	0.0	0.0	0.0	0,0,0
212	0.13	0.38	0.16	777,777,917	0.0	0.0	0.0	0,0,0
213	0.05	0.15	0.06	669,669,917	0.0	0.0	0.0	0,0,0
214	0.11	0.31	0.13	777,777,917	0.0	0.0	0.0	0,0,0
215	0.07	0.18	0.07	728,725,924	0.0	0.0	0.0	0,0,0
216	0.08	0.23	0.10	777,777,917	0.0	0.0	0.0	0,0,0
217	0.23	0.59	0.26	727,725,923	0.0	0.0	0.0	0,0,0
218	0.18	0.49	0.20	725,725,921	0.0	0.0	0.0	0,0,0
219	0.22	0.55	0.24	669,781,921	0.0	0.0	0.0	0,0,0
220	0.18	0.47	0.20	781,725,921	0.0	0.0	0.0	0,0,0
221	0.07	0.18	0.09	669,669,921	0.0	0.0	0.0	0,0,0
222	0.14	0.30	0.17	681,681,917	0.0	0.0	0.0	0,0,0
223	0.06	0.09	0.08	673,673,917	0.0	0.0	0.0	0,0,0
224	0.11	0.26	0.15	673,673,917	0.0	0.0	0.0	0,0,0
225	0.07	0.10	0.09	780,780,920	0.0	0.0	0.0	0,0,0
226	0.12	0.32	0.14	777,724,917	0.0	0.0	0.0	0,0,0
227	0.13	0.35	0.16	777,721,917	0.0	0.0	0.0	0,0,0
228	0.14	0.36	0.16	777,777,917	0.0	0.0	0.0	0,0,0
229	0.15	0.40	0.17	777,777,917	0.0	0.0	0.0	0,0,0
230	0.15	0.40	0.17	777,777,917	0.0	0.0	0.0	0,0,0
231	0.14	0.39	0.17	777,777,917	0.0	0.0	0.0	0,0,0
232	0.14	0.39	0.16	777,777,917	0.0	0.0	0.0	0,0,0
233	0.14	0.40	0.17	777,777,917	0.0	0.0	0.0	0,0,0
234	0.13	0.39	0.16	777,777,917	0.0	0.0	0.0	0,0,0
235	0.12	0.33	0.14	777,777,917	0.0	0.0	0.0	0,0,0
236	0.09	0.27	0.11	777,777,917	0.0	0.0	0.0	0,0,0
237	0.14	0.44	0.16	725,725,921	0.0	0.0	0.0	0,0,0
238	0.14	0.42	0.16	725,725,921	0.0	0.0	0.0	0,0,0
239	0.18	0.45	0.22	681,681,917	0.0	0.0	0.0	0,0,0

Guscio	rRfck	rRfyk	rPfck	Rif. cmb	wR	wF	wP	Rif. cmb
240	0.16	0.48	0.20	665,681,917	0.0	0.0	0.0	0,0,0
241	0.14	0.34	0.17	681,841,917	0.0	0.0	0.0	0,0,0
242	0.04	0.08	0.05	781,673,921	0.0	0.0	0.0	0,0,0
243	0.03	0.03	0.04	725,685,921	0.0	0.0	0.0	0,0,0
244	0.03	0.03	0.04	725,725,921	0.0	0.0	0.0	0,0,0
245	8.93e-03	0.03	0.01	677,672,921	0.0	0.0	0.0	0,0,0
246	0.07	0.18	0.08	777,844,920	0.0	0.0	0.0	0,0,0
247	0.06	0.28	0.08	777,844,920	0.0	0.0	0.0	0,0,0
248	0.11	0.30	0.14	777,724,917	0.0	0.0	0.0	0,0,0
249	0.11	0.29	0.14	777,780,917	0.0	0.0	0.0	0,0,0
250	0.13	0.35	0.16	777,777,917	0.0	0.0	0.0	0,0,0
251	0.12	0.33	0.15	777,777,917	0.0	0.0	0.0	0,0,0
252	0.14	0.36	0.16	777,777,917	0.0	0.0	0.0	0,0,0
253	0.12	0.32	0.14	777,777,917	0.0	0.0	0.0	0,0,0
254	0.15	0.40	0.17	777,777,917	0.0	0.0	0.0	0,0,0
255	0.12	0.33	0.13	777,777,917	0.0	0.0	0.0	0,0,0
256	0.14	0.39	0.17	777,777,917	0.0	0.0	0.0	0,0,0
257	0.12	0.33	0.13	777,777,917	0.0	0.0	0.0	0,0,0
258	0.14	0.39	0.17	777,777,917	0.0	0.0	0.0	0,0,0
259	0.11	0.32	0.13	777,777,917	0.0	0.0	0.0	0,0,0
260	0.14	0.39	0.16	777,777,917	0.0	0.0	0.0	0,0,0
261	0.12	0.34	0.13	777,777,917	0.0	0.0	0.0	0,0,0
262	0.14	0.40	0.17	777,777,917	0.0	0.0	0.0	0,0,0
263	0.12	0.34	0.14	777,777,917	0.0	0.0	0.0	0,0,0
264	0.13	0.38	0.16	777,777,917	0.0	0.0	0.0	0,0,0
265	0.11	0.34	0.13	777,777,917	0.0	0.0	0.0	0,0,0
266	0.11	0.33	0.13	777,777,917	0.0	0.0	0.0	0,0,0
267	0.10	0.32	0.12	777,728,917	0.0	0.0	0.0	0,0,0
268	0.09	0.31	0.11	777,728,917	0.0	0.0	0.0	0,0,0
269	0.09	0.41	0.10	777,744,917	0.0	0.0	0.0	0,0,0
270	0.13	0.45	0.15	726,728,922	0.0	0.0	0.0	0,0,0
271	0.12	0.53	0.14	724,744,920	0.0	0.0	0.0	0,0,0
272	0.12	0.44	0.14	726,728,922	0.0	0.0	0.0	0,0,0
273	0.09	0.52	0.10	724,740,920	0.0	0.0	0.0	0,0,0
274	0.17	0.58	0.22	681,681,917	0.0	0.0	0.0	0,0,0
275	0.14	0.73	0.17	685,685,921	0.0	0.0	0.0	0,0,0
276	0.11	0.44	0.13	669,681,921	0.0	0.0	0.0	0,0,0
277	0.12	0.57	0.14	669,685,921	0.0	0.0	0.0	0,0,0
278	0.10	0.37	0.12	681,681,917	0.0	0.0	0.0	0,0,0
279	0.10	0.57	0.13	681,685,917	0.0	0.0	0.0	0,0,0
280	0.07	0.14	0.09	665,665,917	0.0	0.0	0.0	0,0,0
281	0.07	0.20	0.09	665,681,917	0.0	0.0	0.0	0,0,0
282	0.05	0.07	0.06	781,665,921	0.0	0.0	0.0	0,0,0
283	0.05	0.08	0.06	777,665,917	0.0	0.0	0.0	0,0,0
284	0.03	0.07	0.03	665,725,917	0.0	0.0	0.0	0,0,0
285	0.03	0.07	0.04	665,725,917	0.0	0.0	0.0	0,0,0
286	0.03	0.09	0.04	725,725,921	0.0	0.0	0.0	0,0,0
287	0.03	0.09	0.04	725,725,921	0.0	0.0	0.0	0,0,0
288	0.05	0.25	0.06	852,844,920	0.0	0.0	0.0	0,0,0
289	0.09	0.30	0.11	724,724,920	0.0	0.0	0.0	0,0,0
290	0.08	0.23	0.10	724,780,920	0.0	0.0	0.0	0,0,0
291	0.08	0.18	0.10	777,780,917	0.0	0.0	0.0	0,0,0
292	0.06	0.22	0.07	777,836,917	0.0	0.0	0.0	0,0,0
293	0.05	0.16	0.05	844,668,920	0.0	0.0	0.0	0,0,0
294	0.03	0.14	0.03	777,777,917	0.0	0.0	0.0	0,0,0
295	0.05	0.27	0.05	848,840,924	0.0	0.0	0.0	0,0,0
296	0.06	0.28	0.07	844,840,920	0.0	0.0	0.0	0,0,0
297	0.06	0.28	0.07	840,672,924	0.0	0.0	0.0	0,0,0
298	0.06	0.34	0.08	724,672,920	0.0	0.0	0.0	0,0,0
299	0.08	0.41	0.10	724,744,920	0.0	0.0	0.0	0,0,0
300	0.09	0.54	0.11	740,744,920	0.0	0.0	0.0	0,0,0
301	0.04	0.53	0.05	740,742,920	0.0	0.0	0.0	0,0,0
302	0.14	0.68	0.16	685,685,921	0.0	0.0	0.0	0,0,0
303	0.25	0.57	0.30	669,685,921	0.18	0.0	0.0	685,0,0
304	0.08	0.57	0.10	685,685,921	0.0	0.0	0.0	0,0,0
305	0.05	0.18	0.06	669,681,921	0.0	0.0	0.0	0,0,0
306	0.03	0.04	0.04	728,685,924	0.0	0.0	0.0	0,0,0
307	0.03	0.03	0.04	781,781,921	0.0	0.0	0.0	0,0,0

Guscio	rRfck	rRfyk	rPfck	Rif. cmb	wR	wF	wP	Rif. cmb
308	0.01	0.04	0.01	677,685,921	0.0	0.0	0.0	0,0,0
309	0.06	0.18	0.08	740,844,920	0.0	0.0	0.0	0,0,0
310	0.09	0.21	0.11	724,852,920	0.0	0.0	0.0	0,0,0
311	0.08	0.16	0.10	724,724,920	0.0	0.0	0.0	0,0,0
312	0.08	0.17	0.09	722,724,918	0.0	0.0	0.0	0,0,0
313	0.05	0.20	0.06	777,672,917	0.0	0.0	0.0	0,0,0
314	0.04	0.18	0.04	777,668,917	0.0	0.0	0.0	0,0,0
315	0.02	0.08	0.02	777,680,917	0.0	0.0	0.0	0,0,0
316	0.03	0.28	0.04	736,840,924	0.0	0.0	0.0	0,0,0
317	0.05	0.32	0.06	781,669,921	0.0	0.0	0.0	0,0,0
318	0.07	0.34	0.08	777,728,917	0.0	0.0	0.0	0,0,0
319	0.07	0.36	0.08	724,728,920	0.0	0.0	0.0	0,0,0
320	0.07	0.46	0.09	724,742,920	0.0	0.0	0.0	0,0,0
321	0.08	0.55	0.10	724,742,920	0.0	0.0	0.0	0,0,0
322	0.05	0.46	0.05	732,742,920	0.0	0.0	0.0	0,0,0
323	0.13	0.58	0.16	685,685,921	0.0	0.0	0.0	0,0,0
324	0.20	0.68	0.24	669,685,921	0.0	0.0	0.0	0,0,0
421	0.13	0.54	0.16	724,724,920	0.14	0.13	0.13	834,878,918
422	0.05	0.24	0.06	779,724,919	0.0	0.0	0.0	0,0,0
423	0.14	0.33	0.18	724,836,920	0.0	0.0	0.0	0,0,0
424	0.05	0.26	0.06	780,723,920	0.0	0.0	0.0	0,0,0
425	0.13	0.24	0.16	724,834,920	0.0	0.0	0.0	0,0,0
426	0.04	0.27	0.05	780,723,920	0.0	0.0	0.0	0,0,0
427	0.11	0.40	0.14	848,792,923	0.0	0.0	0.0	0,0,0
428	0.04	0.27	0.05	787,723,919	0.0	0.0	0.0	0,0,0
429	0.11	0.42	0.13	847,792,923	0.0	0.0	0.0	0,0,0
430	0.03	0.29	0.04	848,835,924	0.0	0.0	0.0	0,0,0
431	0.11	0.19	0.14	856,852,924	0.0	0.0	0.0	0,0,0
432	0.03	0.29	0.04	736,835,924	0.0	0.0	0.0	0,0,0
434	0.11	0.23	0.14	856,728,924	0.0	0.0	0.0	0,0,0
435	0.03	0.28	0.04	688,667,924	0.0	0.0	0.0	0,0,0
436	0.11	0.51	0.13	847,792,923	0.0	0.0	0.0	0,0,0
437	0.03	0.23	0.04	672,835,924	0.0	0.0	0.0	0,0,0
438	0.11	0.47	0.14	675,792,919	0.0	0.0	0.0	0,0,0
439	0.04	0.20	0.05	667,667,919	0.0	0.0	0.0	0,0,0
440	0.13	0.21	0.16	668,848,920	0.0	0.0	0.0	0,0,0
441	0.05	0.21	0.06	780,667,920	0.0	0.0	0.0	0,0,0
442	0.14	0.27	0.18	668,835,920	0.0	0.0	0.0	0,0,0
443	0.06	0.20	0.07	724,739,920	0.0	0.0	0.0	0,0,0
444	0.19	0.67	0.22	744,683,924	0.17	0.18	0.17	683,877,919
445	0.06	0.22	0.07	724,740,920	0.0	0.0	0.0	0,0,0
461	0.45	0.62	0.56	742,780,922	0.13	0.14	0.13	780,881,918
462	0.23	0.31	0.29	848,724,924	0.0	0.0	0.0	0,0,0
463	0.22	0.30	0.28	856,724,924	0.0	0.0	0.0	0,0,0
464	0.50	0.77	0.63	684,786,920	0.17	0.19	0.18	786,881,918
465	0.40	0.57	0.50	728,784,924	0.12	0.12	0.12	784,884,924
466	0.19	0.25	0.24	680,780,924	0.0	0.0	0.0	0,0,0
467	0.19	0.25	0.24	736,780,924	0.0	0.0	0.0	0,0,0
468	0.38	0.55	0.48	674,668,918	0.11	0.11	0.11	780,882,920
469	0.52	0.67	0.65	784,800,924	0.13	0.15	0.15	792,884,924
470	0.23	0.28	0.29	784,780,924	0.0	0.0	0.0	0,0,0
471	0.23	0.31	0.30	790,780,924	0.0	0.0	0.0	0,0,0
472	0.47	0.65	0.60	842,834,918	0.13	0.15	0.14	834,881,918
473	0.42	0.61	0.54	734,722,922	0.12	0.13	0.13	724,881,918
474	0.36	0.54	0.46	722,722,918	0.11	0.12	0.11	722,881,918
475	0.30	0.50	0.38	722,842,918	0.10	0.10	0.10	842,881,918
476	0.23	0.31	0.29	848,740,924	0.0	0.0	0.0	0,0,0
477	0.22	0.35	0.28	848,846,924	0.0	0.0	0.0	0,0,0
478	0.22	0.41	0.28	848,846,924	0.0	0.0	0.0	0,0,0
479	0.22	0.31	0.28	848,730,924	0.0	0.0	0.0	0,0,0
480	0.22	0.35	0.28	848,846,924	0.0	0.0	0.0	0,0,0
481	0.22	0.42	0.28	728,846,924	0.0	0.0	0.0	0,0,0
482	0.38	0.57	0.48	676,844,920	0.12	0.13	0.12	844,882,920
483	0.24	0.37	0.30	676,676,920	0.0	0.0	0.0	0,0,0
484	0.19	0.30	0.23	674,678,918	0.0	0.0	0.0	0,0,0
485	0.39	0.57	0.49	728,728,924	0.12	0.12	0.11	784,884,924
486	0.35	0.53	0.45	726,726,922	0.11	0.11	0.11	726,883,922
487	0.31	0.52	0.39	728,846,924	0.11	0.11	0.10	846,883,922

Guscio	rRfck	rRfyk	rPfck	Rif. cmb	wR	wF	wP	Rif. cmb
488	0.18	0.25	0.23	736,738,924	0.0	0.0	0.0	0,0,0
489	0.18	0.31	0.22	792,846,924	0.0	0.0	0.0	0,0,0
490	0.18	0.38	0.22	800,846,924	0.0	0.0	0.0	0,0,0
491	0.18	0.25	0.23	792,738,924	0.0	0.0	0.0	0,0,0
492	0.18	0.31	0.22	792,846,924	0.0	0.0	0.0	0,0,0
493	0.18	0.38	0.22	800,846,924	0.0	0.0	0.0	0,0,0
494	0.37	0.54	0.47	674,668,918	0.11	0.11	0.11	780,882,920
495	0.34	0.51	0.43	674,850,918	0.11	0.11	0.10	850,881,918
496	0.30	0.52	0.38	682,846,918	0.11	0.10	0.10	846,883,922
497	0.33	0.49	0.42	800,736,924	0.10	0.10	0.09	736,884,924
498	0.21	0.35	0.26	800,792,924	0.0	0.0	0.0	0,0,0
499	0.17	0.30	0.21	792,842,924	0.0	0.0	0.0	0,0,0
500	0.22	0.32	0.28	674,740,918	0.0	0.0	0.0	0,0,0
501	0.22	0.36	0.28	678,846,922	0.0	0.0	0.0	0,0,0
502	0.22	0.44	0.28	780,846,920	0.0	0.0	0.0	0,0,0
503	0.23	0.31	0.29	674,724,918	0.0	0.0	0.0	0,0,0
504	0.22	0.36	0.28	678,846,922	0.0	0.0	0.0	0,0,0
505	0.22	0.43	0.28	792,846,924	0.0	0.0	0.0	0,0,0
506	0.45	0.64	0.57	842,834,918	0.13	0.14	0.14	834,881,918
507	0.38	0.58	0.49	842,850,918	0.12	0.13	0.12	850,881,918
508	0.32	0.53	0.41	834,842,918	0.11	0.11	0.11	842,881,918
Guscio	rRfck	rRfyk	rPfck		wR	wF	wP	
	0.52	0.83	0.65		0.18	0.19	0.18	

VERIFICA SOLAIO DI COPERTURA

SOLAIO DI COPERTURA

Poligonale n°1

Caratteristiche poligonale: Chiusa, Strutturale, Piena

Coefficiente di Omog.: 1

Materiale Poligonale: Cls C25/30

n° vertice Coord. X (cm) Coord. Y (cm)

1	-60	-12
2	60	-12
3	60	12
4	-60	12

Poligonale n°2

Caratteristiche poligonale: Chiusa, Strutturale, Vuota

Coefficiente di Omog.: 1

Materiale Poligonale: Cls C25/30

n° vertice Coord. X (cm) Coord. Y (cm)

1	5	-7
2	49	-7
3	49	7
4	5	7

Poligonale n°3

Caratteristiche poligonale: Chiusa, Strutturale, Vuota

Coefficiente di Omog.: 1

Materiale Poligonale: Cls C25/30

n° vertice Coord. X (cm) Coord. Y (cm)

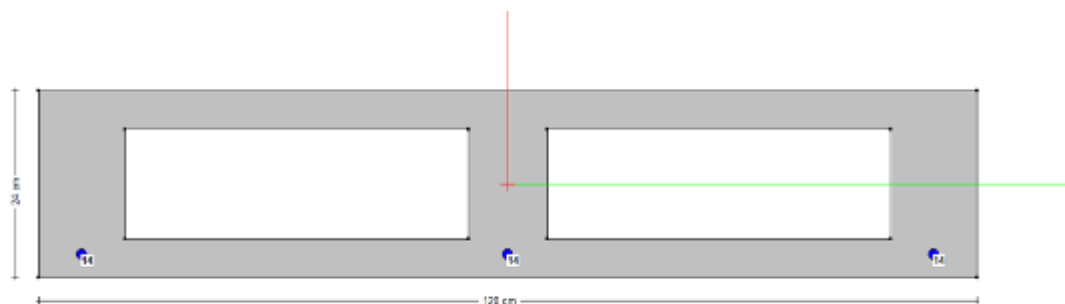
1	-49	-7
2	-5	-7
3	-5	7
4	-49	7

Materiale barre d'armatura: B450C

Coefficiente di Omog.: 15

n° barra armatura Coord. X (cm) Coord. Y (cm) Diametro (mm)

1	-54.5	-9	14
2	54.5	-9	14
3	0	-9	14



VERIFICA SLE RARA IN CAMPATA

VERIFICA A FLESSIONE

Sollecitazioni di verifica a flessione:

M13 = 2146 daNm

Pt.o appl.N Baricentro delle polig.: X= 0 cm Y= 0 cm

Coordinate Asse Neutro: X1 = 60 cm Y1 = 7.6196 cm
X2 = -60 cm Y2 = 7.6196 cm

Materiali poligonali:

Cls C25/30: Sigma Amm.Comp= 150 daN/cm² Sigma Amm.Traz= 0 daN/cm²

Materiali Armature Lente:

B450C: Sigma Amm.Comp= - Sigma Amm.Traz= 3600 daN/cm²

Materiali poligonali	Tens.Min	Tens.Max
Cls C25/30	-41.7872	0
Materiale armature	Tens.Min	Tens.Max
B450C	2378.16	2378.16

-----**VERIFICA SLU IN CAMPATA**-----

VERIFICA A FLESSIONE:

Sollecitazioni di verifica a flessione:

M13 = 3033 daNm

Pt.o appl.N Baricentro delle polig.: X= 0 cm Y= 0 cm

Deformazioni massime e minime:

Materiali:

B450C: Def.min= -0.0675 Def.max= 0.0675

Cls C25/30: Def.min= -0.0035 Def.max= 3.40282e+038

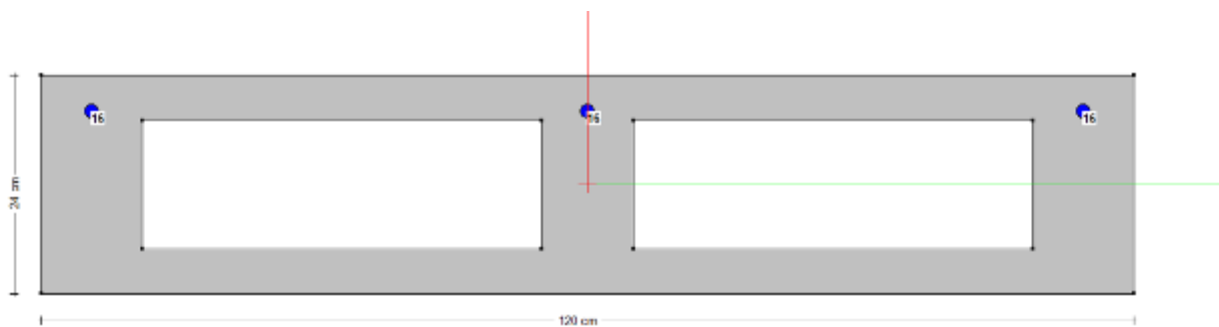
Deformazioni della verifica:

Cls C25/30	-0.0035	0
B450C	0.0524693	0.0524693

Valore Resistente SLU: M13r= 3696 daNm

Coeff.Sfrutt.SLU = 0.820537 < 1 OK

-----**VERIFICA AGLI APPOGGI**-----



-----**VERIFICA SLE RARA AGLI APPOGGI**-----

VERIFICA A FLESSIONE

Sollecitazioni di verifica a flessione:

M13 = -2683 daNm

Pt.o appl.N Baricentro delle polig.: X= 0 cm Y= 0 cm

Coordinate Asse Neutro: X1 = 60 cm Y1 = -7.21072 cm
 X2 = -60 cm Y2 = -7.21072 cm

Materiali poligonali:

Cls C25/30: Sigma Amm.Comp= 150 daN/cm² Sigma Amm.Traz= 0 daN/cm²

Materiali Armature Lente:

B450C: Sigma Amm.Comp= - Sigma Amm.Traz= 3600 daN/cm²

Materiali poligonali	Tens.Min	Tens.Max
Cls C25/30	-50.7337	0

Materiale armature	Tens.Min	Tens.Max
B450C	2416.95	2416.95

 ----- **Verifica slu agli aappoggi** -----

VERIFICA A FLESSIONE:

Sollecitazioni di verifica a flessione:

M13 = -3791 daNm

Pt.o appl.N Baricentro delle polig.: X= 0 cm Y= 0 cm

Deformazioni massime e minime:

Materiali:

B450C: Def.min= -0.0675 Def.max= 0.0675

Cls C25/30: Def.min= -0.0035 Def.max= 3.40282e+038

Deformazioni della verifica:

Cls C25/30	-0.0035	0
B450C	0.0373118	0.037312

Valore Resistente SLU: M13r= -4552 daNm

Coeff.Sfrutt.SLU = 0.832771 < 1 OK